

SOCIJALISTIČKA FEDERATIVNA REPUBLIKA JUGOSLAVIJA — RÉPUBLIQUE SOCIALISTE FÉDÉRATIVE DE YOUGOSLAVIE  
HIDROMETEOROLŠKA SLUŽBA — SERVICE HYDRO-MÉTÉOROLOGIQUE

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# METEOROLOŠKI GODIŠNjak I

## ANNUAIRE METEOROLOGIQUE I

GODINA 1977 ANNÉE



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IZDANJE SAVEZNOG HIDROMETEOROLOŠKOG ZAVODA  
PUBLIÉ PAR L'INSTITUT HYDROMÉTÉOROLOGIQUE FÉDÉRAL  
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## O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljaju se podaci 8 odabranih stanica, i to: Ljubljana-Beograd, Zagreb-Grič, Split-Marjan, Bjelovar, Sarajevo, Beograd, Titograd i Skopje. U delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

$\varphi$  = geografska širina,  $\lambda$  = geografska dužina od Griniča,  $\Delta G$  vremenska razlika u odnosu na Grinič,  $H_s$  = nadmorska visina podnožja termometarskog zaklona,  $H_b$  = nadmorska visina rezervoara barometra,  $h_t$  = visina rezervoara termometra iznad tla,  $h_r$  = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebljene prema međunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

P = vazdušni pritisak u mm visine živinog stuba, reducirane na  $0^{\circ}\text{C}$ ; T = temperatura u  $^{\circ}\text{C}$ ; e = pritisak vodene pare u mm visine živinog stuba; U = relativna vlažnost u procentima; D = pravac vetra po ruži vetra od 16 ili 8 pravaca; F = jačina vetra po Boforovoj skali (0-12); v = brzina vetra u m/sek; V = vidljivost u km; N = oblačnost (0-10); insola - cija = trajanje osunčavanja u satima; R = padavine u mm; R<sub>s</sub> = padavine u mm; h<sub>s</sub> = snežni pokrivač u cm; W = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan međunarodnim simbolima.

U rubrici "razvoj vremena" su potrebljene ove skraćenice:

n = u toku noći; a = pre podne; p = posle podne; i = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14, i 21 h po lokalnom vremenu računate su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente (P, e, U, N) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri su očitavani i uredjivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h predhodnog dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebljene su oznake  $M_{\overline{ax}}$  i  $M_{\overline{in}}$ ; za rubrike broj dana sa  $\bullet$  ili  $\circ$ ,  $\times$  ili  $\Delta$ , i  $\otimes$  prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Ažbučnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SFRJ sa naznačenim klimatološkim stanicama u 1977 godini čiji brojevi odgovaraju brojevima stanica sa podacima u tablicama B.

## NOTICE EXPLICATIVE

L'Annuaire météorologique I a deux parties: A) Observations journalières et: B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd et Skopje. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

$\varphi$  = latitude,  $\lambda$  = longitude E de Greenwich,  $\Delta G$  = différence entre l'heure locale et l'heure de Greenwich,  $h_s$  = altitude du pied de l'abri météorologique,  $h_b$  = altitude de la ouvette du baromètre,  $h_t$  = hauteur, au-dessus du sol, du réservoir du thermomètre,  $h_x$  = hauteur, au dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

La désignation des éléments météorologiques particuliers sont conformes aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

P = pression atmosphérique en mm (hauteur de la colonne de mercure réduite à 0°C); T = température en °C; e = tension de vapeur d'eau en mm de la hauteur de la colonne de mercure; U = humidité relative en %; D = direction du vent en rose des vents de 8 ou de 16 directions; F = force du vent d'après l'échelle Beaufort (0-12); v = vitesse du vent en m/s; V = visibilité en km; N = nébulosité (0-10); insolation = durée d'insolation en heures; R = = précipitations en mm;  $h_s$  = épaisseur de la couche de neige en cm; W = évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux.

Dans la colonne "Kazvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

n = pendant la nuit; a = avant midi; p = après midi; i = avec interruption.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

et pour les autres éléments (P, e, U, N) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7h, 14 h et 21 h.

Les lectures des thermomètres à maxima et minima suivies de leur amorçage, ont été faits à 21 h et les valeurs insorites le même jour.

Les valeurs journalières des précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau, de la force du vent  $F \geq 6$  (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air les indications  $M_{\overline{ax}}$  et  $M_{\overline{In}}$  ont été utilisées; dans les colonnes "Broj dana sa" (Nombre de jours avec) • ou , , \* ou  $\Delta$ , et  $\times$  sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1977; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

AZBUČNI SPISAK STANICA  
PO SOCIJALISTIČKIM REPUBLIKAMA

WENI SPISAK STAN  
PO SOCIALISTICKUM PRVNUJEMU

Znak x pokazuje da stanica raspolaze odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14.

I

A Z B U Č N I S P I S A K S T A N I C A  
PO S O C I J A L I S T I Č K I M R E P U B L I K A M A

II Žnak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

A Z B U Č N I S P I S A K S T A N I C A  
PO SOCIJALISTIČKIM REPUBLIKAMA

PO SOCIETATE ROMÂNĂM, BUCURESTIAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14  
PO SOJUZISTICKIM REPUBLIKAMA

III

AZBUČNI SPISAK STANICA  
PO SOCIJALISTIČKIM REPUBLIKAMA

IV

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

## AZBUČNI SPISAK STANICA

BO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14.

v

A Z B U Č N I S P I S A K S T A N I C A

PO SOCIJALISTIČKIM REPUBLIKAMA

VI

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Nadmorska visina H, m	Geografska širina φ N	Geografska dužina λ° E Gr.	Broj stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblakost	Insolacija	Padačine	Broj karak. teorijskih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
<b>S O C I J A L I S T I Č K A R E P U B L I K A C R N A G O R A</b>													
Veliko Gradište	182	82	44°45'	21°31'	gl	x	x	x	x	x	x	x	x
Vladimirci	168	120	44 37	19 47	ob		x	x	x	x	x	x	x
Vlasina	230	1190	42 44	22 21	ob		x	x	x	x	x	x	x
Vlasotince	227	270	42 58	22 08	ob		x	x	x	x	x	x	x
Vranje	225	433	42 33	21 55	gl	x	x	x	x	x	x	x	x
Vrbas	154	87	45 34	19 39	ob		x	x	x	x	x	x	x
Vrnjačka Banja	197	235	43 37	20 54	ob		x	x	x	x	x	x	x
Vršac	163	83	45 09	21 19	gl	x	x	x	x	x	x	x	x
Zaječar	209	137	43 53	22 18	ob		x	x	x	x	x	x	x
Zlatibor	188	1029	43 44	19 43	gl	x	x	x	x	x	x	x	x
Zrenjanin	160	80	45 24	20 21	gl		x	x	x	x	x	x	x
Žagubica	183	314	44 12	21 47	ob		x	x	x	x	x	x	x
<b>S O C I J A L I S T I Č K A R E P U B L I K A M A K E D O N I J A</b>													
Berovo	280	824	41°43'	22°51'	gl	x	x	x	x	x	x	x	x
Bitola	264	586	41 03	21 22	gl	x	x	x	x	x	x	x	x
Debar	254	675	41 31	20 32	ob		x	x	x	x	x	x	x
Delčevko	279	630	41 58	22 46	ob		x	x	x	x	x	x	x
Demir Kapija	272	125	41 25	22 15	gl	x	x	x	x	x	x	x	x
Erdželija	269	253	41 50	22 02	ob		x	x	x	x	x	x	x
Gevgelija	275	59	41 09	22 30	ob		x	x	x	x	x	x	x
Gostivar	259	525	41 48	20 55	ob		x	x	x	x	x	x	x
Kavadarci	270	265	41 26	22 02	ob		x	x	x	x	x	x	x
Kičevo	260	620	41 31	20 58	ob		x	x	x	x	x	x	x
Kočani	273	345	41 55	22 25	ob		x	x	x	x	x	x	x
Kratovo	252	640	42 05	22 09	ob		x	x	x	x	x	x	x

AZBUČNI SPISAK STANICA  
PO SOCIJALISTIČKIM REPUBLIKAMA

PO SOCIJALISTICKIM REBUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14  
PO SOVJETSKIM REPUBLIKAMA

VII

## **A) Dnevna osmatranja**

$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$  Gr.  $\Delta G = + 58$  min.

BR. ST. 13

D S	Vzdušni pritisak P mm			Temperatura vazduha T °C						Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	735.0	734.5	733.6	03.4	05.7	04.6	04.6	06.6	-06.2	-07.0	04.9	04.9	06.0	83	71	94	83	W 2	W 2	W 2
2	733.1	734.9	737.7	01.7	02.8	01.9	02.1	05.1	01.5	00.7	05.1	05.5	05.2	98	98	98	98	SE 1	E 1	NE 1
3	741.2	741.6	743.0	01.8	02.2	01.3	01.7	02.4	01.2	00.5	05.1	05.3	04.9	98	98	97	98	NNE 1	- 0	ENE 1
4	744.9	746.2	748.5	00.4	00.7	00.4	00.5	01.5	00.2	00.1	04.6	04.7	04.5	98	96	95	96	NNW 1	NE 1	SE 1
5	748.5	749.3	749.2	-00.4	00.2	00.4	00.2	01.1	-00.6	-01.0	04.2	04.3	04.5	94	93	95	94	S 1	SE 1	SW 1
6	747.5	746.7	746.0	00.4	01.9	01.3	01.2	02.2	00.2	-30.1	04.5	05.0	04.9	95	95	97	96	ENE 1	S 1	NNE 1
7	744.9	743.0	742.9	01.0	02.0	01.2	01.4	02.1	00.8	00.1	04.8	05.1	04.9	97	97	98	97	NNE 1	SW 1	SSW 1
8	741.2	741.1	739.1	00.7	03.3	00.8	01.4	03.4	00.6	00.2	04.7	04.3	04.3	96	74	88	86	SSE 1	E 2	SW 1
9	738.0	736.7	734.5	-01.4	01.2	-00.4	-00.3	01.4	-01.5	-04.0	04.0	03.3	03.8	97	66	85	83	SSW 1	E 1	NE 2
10	730.3	728.6	728.3	-00.8	00.1	00.4	00.0	00.8	-01.2	-01.8	04.0	04.3	04.4	92	93	93	93	E 1	NNE 1	N 1
11	726.8	724.6	723.2	01.4	04.2	02.8	02.8	04.6	00.4	00.0	04.7	05.7	05.4	93	92	97	94	S 1	NNE 1	NNW 1
12	719.5	720.6	722.9	03.4	07.4	02.0	03.7	08.0	01.9	00.4	05.7	05.8	04.8	97	75	90	87	ENE 1	SW 2	NE 1
13	723.8	725.9	729.1	01.0	00.6	01.2	01.0	02.1	00.3	-02.3	04.7	04.5	04.7	95	95	95	95	SE 1	W 1	S 1
14	730.3	730.3	729.0	-00.6	00.2	01.0	00.4	01.4	-01.6	-00.7	04.1	04.0	04.7	93	86	95	91	NW 1	NE 2	NNE 1
15	726.1	726.7	729.5	00.8	02.0	00.9	01.2	02.6	00.4	-00.2	04.6	05.0	04.6	95	95	95	95	NW 2	NNW 1	SSW 2
16	731.5	732.4	734.1	-01.6	01.2	-00.2	-00.2	02.0	-01.7	-05.1	03.9	04.2	04.2	97	85	93	92	ESE 1	SW 1	ENE 1
17	736.1	736.6	737.5	-02.6	01.4	-02.5	-01.6	02.0	-03.4	-02.7	03.5	03.7	03.5	92	73	92	86	NNW 1	SSE 1	NNE 1
18	737.6	737.6	737.5	-05.1	01.4	-02.4	-02.1	02.4	-05.3	-09.8	02.9	03.4	03.3	93	67	86	82	NW 1	NE 1	NE 1
19	736.9	735.3	735.1	-07.0	00.7	-04.3	-03.7	01.5	-07.8	-11.9	02.5	02.9	02.8	93	61	85	80	NE 1	S 2	W 1
20	734.4	734.4	734.5	-03.7	00.2	-00.2	-01.0	01.0	-05.4	-10.1	03.2	03.8	04.0	90	81	87	86	NE 2	SSW 1	E 1
21	733.9	735.3	736.5	00.4	05.0	03.2	03.0	05.7	-00.4	-03.2	04.0	05.1	05.0	85	79	88	84	NE 1	WSW 2	NE 2
22	735.9	735.8	736.1	00.7	02.9	05.1	03.5	05.4	00.6	-00.1	04.4	05.2	05.7	91	92	87	90	NE 1	ENE 1	NW 2
23	734.4	733.1	731.8	04.4	07.0	04.9	05.3	07.6	03.9	01.5	05.6	06.7	06.0	90	89	93	91	NW 1	WNW 1	NNW 1
24	730.5	730.6	732.9	02.3	08.7	02.2	03.9	09.0	02.0	00.1	05.1	06.4	04.9	93	75	92	87	NE 1	SSW 1	- 0
25	733.9	732.2	730.9	01.0	02.2	06.4	04.0	06.7	00.8	-03.0	04.7	05.0	05.6	95	93	77	88	N 1	ESE 1	W 3
MES. VRED.	733.8	733.6	733.9	00.7	03.1	01.8	01.9	04.1	-00.2	-01.8	04.6	04.9	04.8	93	85	91	90	1.1	1.2	1.3

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1	729.6	730.4	731.3	00.3	01.5	00.0	00.5	03.0	-00.2	-00.1	04.5	04.6	03.6	96	90	79	88	SSW 1	SSW 1	S 1
2	732.0	733.0	734.5	-01.2	01.4	-01.0	-00.5	01.8	-01.7	-04.0	03.0	02.9	03.1	72	57	72	67	S 2	E 2	SSE 2
3	735.5	735.9	735.7	-03.2	01.9	-02.8	-01.7	02.1	-03.4	-02.7	03.2	02.6	03.0	87	50	82	73	SW 2	ESE 2	NNE 1
4	735.4	736.3	736.8	-04.3	01.0	00.1	-00.8	03.4	-04.4	-05.6	02.9	03.2	04.0	88	65	86	80	SSW 1	NE 1	NE 1
5	736.2	735.8	736.4	-02.1	03.0	01.2	00.8	04.4	-02.3	-05.6	03.8	04.4	04.4	96	77	88	87	NNE 1	E 1	NNW 1
6	735.2	733.8	733.6	00.0	04.0	02.3	02.2	06.3	00.6	-00.7	04.3	05.0	05.1	93	82	93	89	WNW 1	NNE 1	NW 1
7	736.5	735.9	735.7	02.0	06.2	03.6	03.9	07.4	01.2	-00.2	05.1	05.8	05.6	97	82	94	91	NNE 2	E 2	NNW 2
8	733.2	730.8	729.9	02.2	08.0	07.6	06.4	08.2	00.8	-00.1	04.9	05.6	05.9	92	70	76	79	NE 1	W 3	WNW 3
9	730.2	730.7	730.3	04.9	08.8	06.6	06.7	09.3	02.4	02.6	05.2	06.3	06.7	80	74	92	82	NNE 2	WSW 2	W 2
10	728.3	724.4	721.4	05.2	07.6	08.0	07.2	08.3	05.1	04.8	06.3	06.9	07.4	94	88	92	91	NNE 1	ENE 1	ENE 1
11	722.2	722.1	723.9	08.2	11.0	6.6.2	7.5	11.4	6.6.2	04.7	06.6	05.3	05.9	81	54	84	73	WSW 2	WNW 3	N 1
12	719.4	718.6	722.6	04.7	06.6	07.0	06.3	07.4	04.4	01.6	06.0	06.7	06.4	94	92	85	90	NW 2	NNE 2	W 2
13	728.9	731.5	731.9	03.3	06.6	03.8	04.4	07.6	02.6	01.2	05.3	06.4	05.6	91	88	97	92	WNW 1	WSW 2	S 1
14	730.1	728.0	728.4	04.0	06.7	04.4	04.9	07.0	02.8	03.4	05.9	05.7	05.7	97	77	91	88	N 1	NNE 1	SW 1
15	728.5	728.2	728.9	00.4	06.5	04.8	04.1	09.8	-00.4	-02.6	04.6	05.5	04.7	96	76	73	82	W 1	S 2	SSW 1
16	730.1	730.3	731.8	-01.2	04.3	00.8	01.2	05.5	-01.8	-03.6	03.9	04.9	04.6	93	76	95	89	ENE 1	ENE 1	NE 1
17	734.6	734.7	735.3	-01.0	05.3	01.4	01.8	08.3	-02.2	-05.6	04.2	04.7	04.6	98	71	92	87	NE 1	SE 1	ENE 1
18	735.7	736.2	737.8	-00.8	11.3	6.6.9	6.6.1	11.6	-01.2	-05.0	04.1	03.4	06.4	94	34	85	71	- 0	WSW 3	WSW 2
19	736.8	735.2	734.9	06.4	09.3	08.4	08.1	10.4	03.6	04.3	06.6	07.1	07.1	92	81	66	86	WNW 2	WNW 2	WNW 2
20	733.8	732.3	730.6	08.6	10.4	08.9	09.2	10.7	06.6	06.2	07.3	07.1	07.6	87	75	89	84	WSW 2	WNW 2	WNW 2
21	725.8	723.3	725.8	09.9	09.7	07.2	08.5	10.9	07.1	07.6	07.7	08.5	07.2	84	94	95	91	SSW 2	NE 2	ESE 1
22	730.6	731.2	729.3	02.3	10.5	06.9	06.7	11.0	01.4	-00.9	05.3	07.1	07.1	98	75	95	89	NE 1	ENE 1	NNW 2
23	727.6	733.8	737.4	10.3	13.5	08.8	10.4	14.9	03.6	04.7	06.1	05.5	05.6	65	47	66	59	WSW 4	SSW 3	N 1
24	736.8	734.8	733.3	01.3	07.5	06.8	05.6	09.9	00.2	-00.2	05.0	06.2	06.1	98	79	83	87	ESE 1	E 1	E 1
25	727.4	726.8	729.9	05.0	12.0	07.0	07.8	13.0	04.0	01.6	06.3	05.8	05.5	96	55	74	75	NE 1	WSW 3	- 0
26	732.0	729.9	730.9	01.2	09.6	06.4	05.9	10.4	01.2	-03.7	04.7	05.2	05.8	95	58	81	78	NNE 1	S 1	S 1
27	732.9	734.6	735.3	00.2	02.5	01.1	01.2	07.5	-00.2	-05.2	04.4	04.7	04.1	95	86	83	88	ENE 1	ESE 2	ESE 2
28	737.9	739.6	744.0	-00.9	04.5	-00.2	00.8	05.8	-01.2	-J3.0	03.4	02.0	02.2	79	32	49	5			

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$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10	10○	10●	10.0	00.0	00.0	28		
2	2	10○	10○≡	10○≡	10.0	00.0	07.6	16		
3	3	10○	10○≡	10○	10.0	00.0	12.0	05		
4	4	10*	10○*	10○*	10.0	00.0	12.2	08		
5	5	10●	10●	10	10.0	00.0	12.5	12		
6	4	10○	10○	10≡	10.0	00.0	05.6	12		
7	3	10○	10○≡	10	10.0	00.0	00.7	10		
8	7	10○	02○	10	07.3	02.6	00.6	05		
9	6	10	10	10	10.0	00.2	•	01		
10	4	10*	10●	10	10.0	00.0	02.7	12		
11	5	10	10○	10○≡	10.0	00.4	03.8	13		
12	7	10	10●	00	06.7	00.0	14.1	09		
13	4	10○	10*	09	05.7	00.0	07.5	07		
14	6	09	09○*	10○	09.3	02.5	06.1	07		
15	5	100*	10	10	10.0	00.0	17.0	06		
16	6	10≡	09	10	09.7	01.9	10.5	05		
17	5	10	01○	00	03.7	03.9	•	05		
18	6	10	01○	00	03.7	03.6	00.0	05		
19	6	06	00○	00	06.0	04.8	00.0	05		
20	5	10	10	10	10.0	00.0	00.2	05		
21	7	10	05○	09	09.3	01.0	00.0	05		
22	5	10	10	09	09.7	00.0	00.0	05		
23	7	10	10●	10●	10.0	00.0	00.2	04		
24	6	10≡	03○	00	04.3	03.5	02.2	•		
25	3	10○	10≡	05	08.3	00.0	•	•		
26	7	10○	10○	10●	10.0	00.0	00.0	•		
27	6	10●	10○	06	08.7	00.0	15.1	•		
28	4	100≡	10	10○	10.0	00.0	15.8	•		
29	4	10○	10○	10○	10.0	00.0	09.6	•		
30	7	09	02○	09	06.7	05.0	07.9	•		
31	6	10○	10○	10●	10.0	00.0	04.3	•		
<b>MES.</b>										
<b>VRED.</b>		09.6	08.3	08.0	08.6	29.4	168.2			

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1	6	10*	10*	10	10.0	00.0	15.4	03	= 0-24, * <sup>0</sup> 0-135, * <sup>0</sup> 125-2030, ○, □
2	6	10	02○	09	07.0	03.0	00.8	04	= 0-30, 2130-2124, = 00 930-2130, ○, □
3	6	10	01○	00	03.7	04.0	•	02	= 0-120, 1730-2124, * <sup>0</sup> 945-1015, = 00 1230-1730, ○, □
4	5	10	05○	10	08.3	04.2	00.0	01	= 0-24, ○, □
5	5	10=	07○	09	08.7	00.4	•	01	= 0-610, 1130-1930-2124, = 00 610-1130, * <sup>0</sup> 125-1145, □, 2330-2124, ○, □
6	5	10	04○	10=	06.0	32.7	00.0	•	$\square^0-0-755 = -1515, 2230-2124, \square^0-755-805, \square^{0+0} 805-1215, 2210-2310, = 0-2 1630-2220, ○$
7	5	10	08○	00=	06.0	33.0	05.7	•	$= 0-116, 16-2030, -2-116, 1045, 2230-2124, = 0-2 1030-2030, \square^0-116-1924, ○$
8	7	10	10	10	10.0	00.0	•	•	$\square^0-810 = -1-2-0-250, = 0-1030-8330, = 330-1320, \square^0-810-1030,$
9	6	07	10	10●	09.0	00.4	00.0	•	$= 732-1030-1745-2330, = 00 1030-1745, = 0-1030-1730-2124, = 0-123-2124, ○$
10	5	10=	10●	10●	10.0	00.0	00.9	•	$*^0-2-0-1120, = 0-116, 932-1145, = 0-1030-930, = 1115-24, \square^0-2-0-1120-2124.$
11	8	09	09	00	06.0	05.1	18.7	•	$*^0-0-2-0-010, 310-310, = 0-116, 1045-1505, ○$
12	6	10●	10●	10●	10.0	00.8	14.5	•	$\square^0-1-1030-1416, = 532-1705, ○$
13	6	08	10●	10	09.3	00.2	18.6	•	$*^0-0-1-0-015, 4415-1630-2115-2215, = 0-116, 1030; = 0-830-1030; = 0-845-930, ○$
14	7	10	05○	09	05.3	00.0	06.1	•	$= 112-1030-1330-1330-2124, \square^0-1030-1330-1330-2124, = 0-1030-1330-1330-2124, = 0-532-1330, ○$
15	6	10=	03○	00	04.3	04.1	00.2	•	$= 0-230, 1115-1430, = 0-116, 1052, = 0-116, 1145, ○$
16	5	10=	05○	00	06.3	00.1	•	•	$\square^0-1-132-090-1930-2124, = 0-116, 1320-1320-1430-1430, = 0-2-430-515-730-830, = 0-2 515-730, ○$
17	5	10=	01○	00	03.7	04.0	•	•	$\square^0-0-1030, 2015-2115, = 0-116, 1130-1130-1430-1430, = 0-22-1130-1130-1545, ○$
18	6	05	05○	10●	06.7	07.4	•	•	$\square^0-0-1030, 2015-2115, = 0-116, 1130-1130-1430-1430, = 0-22-1130-1130-1545, ○$
19	7	09	09	10●	05.3	00.3	01.3	•	$= 0-745, 050-0-035, = 0-1305-520-1015-2335, ○$
20	7	10●	10●	10●	10.0	00.0	02.2	•	$\square^0-36345, 045-1030, 1335-2141, = 532-1120$
21	7	10●	10●	05	06.3	00.0	03.4	•	$*^0-0-1120, = 2015-2124$
22	6	10=	09○	10●	05.7	01.4	20.8	•	$= 0-455, 1025-2124, = 0-116, 1055, = 0-615-1005, = 0-116, 1055-1152-2124, ○$
23	6	07	03○	01	03.7	07.6	32.0	•	$*^0-0-610, = 0-530, = 530-1120, \square^0-1120-835, = 0-116, 930, \square^0-1120-2230-2124, ○$
24	7	10=	09	09	09.3	00.6	00.0	•	$\square^0-0-116, = 1120-1030-1330-1330-2124, = 0-116, 1030-1030-1330-1330-2124, = 0-116, 1030, ○$
25	8	05	07○	09	06.3	03.4	•	•	$= 0-1030, 2025-2124, \square^0-116, 1030-1330-1330-2124, = 0-116, 1030-1330-1330-2124, = 0-116, 1030, ○$
26	7	10=	09○	07	08.7	01.7	03.0	•	$= 0-510-1030, \square^0-0-25-0230-0230-0230, = 0-116, 1030, = 0-510-1030, = 0-510-1030, = 0-116, 1030, = 0-116, 1030, ○$
27	7	06	10●	10	06.7	00.4	•	•	$\zeta^0-0-1030, = 0-116, 1030-1330-1330-2124, = 0-116, 1030-1330-1330-2124, = 0-116, 1030, ○$
28	8	09	04○	00	04.3	07.0	01.6	•	$*^0-0-515, 830-1035, = 0-1030, = 2215-2124, ○$

$\varphi = 46^{\circ}04'$  N  $\lambda = 14^{\circ}31'$  E Gr.  $\Delta G = + 58$  min.

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Dan	Vzdušni pritisak P mm			Temperatura vazduha T °C°						Napon vodenih parov e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	Sred. Dnes	7	14	21	
1	742.8	740.9	743.5	-05.0	07.3	01.0	01.1	09.2	-06.0	-19.7	02.9	03.7	02.5	93	48	50	64	E 1 ENE 2 NNE 1
2	744.2	741.3	740.3	-04.2	07.4	05.6	03.6	08.0	-04.6	-08.6	03.1	03.0	03.9	92	39	58	63	- 0 WSW 4 SW 3
3	739.1	736.5	735.4	00.4	10.8	06.2	05.9	11.0	00.3	-02.0	04.2	04.9	04.5	89	51	64	68	N 2 SSW 3 NW 2
4	736.0	735.2	735.6	02.3	10.6	05.3	07.9	10.7	-03.4	-10.5	04.7	06.5	07.0	87	68	79	76	NW 1 WSW 2 SW 2
5	738.1	737.9	739.8	02.4	10.3	06.2	09.5	20.0	02.0	-03.0	05.1	05.1	05.2	94	30	64	63	WNW 1 WNW 3 WNW 1
6	738.6	738.6	740.1	00.2	10.6	10.4	09.3	17.2	-01.1	-15.0	04.4	05.9	06.6	95	43	70	69	NE 1 SW 2 WSW 2
7	743.5	744.5	746.8	00.8	13.1	07.2	07.1	13.7	-01.2	-14.6	04.7	04.6	04.3	97	42	57	65	ENE 1 E 2 ESE 1
8	748.8	748.1	748.5	01.0	12.0	06.1	06.3	13.9	00.6	-03.1	04.6	05.1	05.2	93	49	74	72	E 1 WNW 1 NNE 1
9	746.8	744.1	742.8	00.9	13.6	05.2	08.3	14.2	00.6	-03.2	04.6	06.0	06.0	93	51	69	71	E 1 WSW 4 W 3
10	740.3	737.8	736.1	04.7	15.7	10.1	19.2	17.2	03.0	03.4	05.6	06.5	06.8	87	48	73	69	NNE 1 ESE 2 NNN 1
11	734.5	733.7	732.9	04.4	09.2	08.6	07.7	09.6	03.6	-01.2	05.8	06.7	07.4	93	77	89	86	SW 1 WNW 2 SE 1
12	731.3	730.0	730.6	07.4	09.6	08.3	08.4	10.4	07.1	16.3	07.2	08.1	07.7	93	90	94	92	NNE 1 ESE 2 NW 2
13	729.3	730.9	734.1	05.9	11.4	06.3	07.5	12.4	03.9	03.4	06.3	06.3	05.2	90	63	73	75	SE 2 SSW 2 ESE 1
14	737.8	737.3	738.8	02.6	15.0	09.6	09.2	15.2	01.2	-02.4	05.4	05.1	05.3	98	40	59	66	E 1 WSW 3 WSW 2
15	743.4	743.7	742.4	07.3	14.9	07.1	09.1	14.9	05.4	02.5	06.3	04.2	04.7	82	33	63	59	SSW 2 S 2 ENE 1
16	745.2	743.3	743.0	00.4	17.0	05.7	09.2	17.0	00.1	-04.4	04.5	03.7	05.6	95	25	62	61	NNE 1 WSW 3 WSW 3
17	741.1	738.9	738.5	02.5	16.8	10.4	05.8	17.0	J1.7	-01.0	05.1	05.4	05.5	94	37	60	64	ENE 1 WSW 4 WSW 2
18	736.4	734.7	734.2	03.6	17.7	11.4	11.0	17.8	02.9	-06.4	05.7	04.3	04.7	95	28	47	57	NNE 1 W 3 WSW 2
19	732.8	730.3	730.4	03.7	13.4	08.3	08.4	14.7	03.7	-01.1	05.2	05.9	07.7	86	51	94	77	ESE 2 SSW 1 ESE 1
20	729.9	730.7	732.0	06.8	11.8	05.3	09.3	14.0	06.6	04.2	07.0	05.6	06.2	95	54	70	73	ESE 1 WNW 2 NE 2
21	733.1	733.9	735.8	05.5	12.6	05.2	05.4	14.6	05.4	00.4	06.6	05.4	05.2	97	46	60	68	SE 1 WSW 2 WSW 2
22	736.1	735.8	737.6	06.0	18.2	12.4	12.3	18.5	05.1	01.0	06.2	06.8	07.9	85	44	73	69	NW 1 W 2 NW 2
23	739.8	738.5	738.8	05.4	21.4	15.6	14.5	23.4	05.2	0.0	06.5	06.4	03.2	97	34	24	52	ENE 2 NE 1 W 1
24	738.1	736.1	736.6	03.9	22.0	14.2	13.6	24.1	03.4	-00.3	05.5	03.4	05.3	91	17	43	50	ENE 1 NE 1 ENE 1
25	737.5	736.7	737.8	06.4	23.4	14.4	14.7	24.6	16.0	01.0	06.0	06.0	07.0	84	28	57	56	NE 1 ENE 2 ENE 1
MES. VRED.	737.2	736.4	736.8	03.3	13.5	08.7	08.6	14.7	02.4	-00.8	05.4	05.4	05.5	91	49	66	65	1.3 2.3 1.7

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1	737.7	736.5	735.2	00.2	08.4	04.5	04.4	10.4	-06.9	-02.0	04.3	04.5	04.6	93	54	75	74	NE 1 SSW 2 SW 2
2	732.4	729.8	730.0	-03.2	13.0	09.2	07.8	15.4	-01.4	-05.9	04.4	06.7	05.3	98	42	61	67	S 1 WNW 1 SE 1
3	728.4	725.5	726.7	02.6	14.6	09.4	09.4	16.4	02.4	-01.9	05.3	05.6	05.5	97	45	62	68	E 1 SSE 2 WSW 3
4	730.6	732.3	732.4	07.2	07.5	07.2	07.3	09.6	07.1	05.6	06.6	07.0	06.6	87	90	87	88	NE 2 ENE 2 NW 1
5	732.3	734.5	736.0	06.6	03.3	02.5	03.7	07.6	02.5	05.6	06.6	05.5	05.3	90	95	97	94	ENE 1 S 2 E 1
6	735.5	732.3	733.1	02.5	11.2	07.2	07.0	12.9	01.4	01.9	05.1	05.1	03.6	94	51	47	64	NW 1 SSW 2 W 2
7	728.4	727.4	725.5	08.4	16.6	08.5	08.6	13.4	05.4	-03.4	04.7	05.0	07.8	56	88	94	79	WSW 2 NW 2 NE 1
8	722.9	721.6	720.3	07.7	10.8	07.6	08.5	11.1	07.6	03.4	07.7	08.7	07.6	97	90	96	94	E 1 NE 1 NNE 1
9	719.1	720.1	720.2	00.8	04.0	02.6	02.5	07.8	00.8	-03.4	04.6	05.2	05.1	95	85	92	91	SW 1 E 1 ENE 1
10	723.5	725.9	729.6	02.9	09.8	02.7	03.0	05.4	01.0	02.2	05.2	05.0	05.1	92	83	92	89	ENE 1 NNE 2 E 2
11	733.3	732.3	732.6	01.2	07.2	03.5	04.1	08.3	00.7	-00.6	03.7	02.8	03.8	75	37	63	58	SF 2 S 2 E 1
12	733.8	732.8	734.2	-00.3	09.5	03.4	04.0	09.9	-00.7	-04.2	04.2	03.1	04.9	93	35	85	71	ENE 1 ESE 2 WSW 2
13	734.3	730.8	729.7	01.2	14.4	05.9	05.9	14.7	00.3	-01.3	04.6	03.8	04.8	91	31	52	58	SW 1 SW 2 SSW 2
14	729.1	728.1	729.1	00.8	04.4	02.2	04.1	10.4	01.5	01.7	05.2	05.7	05.2	88	69	97	85	E 1 SSE 2 NW 2
15	728.0	728.4	730.2	02.7	08.2	04.7	05.1	09.6	01.2	00.0	05.4	04.6	04.8	97	56	75	76	ESE 1 SSW 3 WSW 2
16	731.5	733.0	736.0	-00.4	10.9	07.0	06.1	11.8	-02.5	-07.4	04.0	02.0	02.8	91	21	37	50	E 1 NNE 3 NNW 2
17	738.8	736.0	735.4	-01.2	14.4	07.1	06.9	14.6	-03.3	-08.1	03.4	02.5	04.6	81	20	60	54	NNE 1 S 3 SW 3
18	735.7	734.4	735.7	00.9	17.9	11.0	10.2	18.8	00.6	-05.7	04.4	03.7	05.0	90	24	51	55	ENE 1 WSW 2 SW 2
19	737.8	735.6	737.3	04.6	16.4	11.8	11.2	17.1	01.9	-03.2	06.0	05.6	05.9	94	36	57	62	E 1 WSW 1 ENE 4
20	742.0	742.6	743.0	04.7	11.0	06.3	07.1	12.6	04.6	-03.4	05.8	04.0	03.7	90	41	51	61	SSE 2 E 2 ENE 2
21	743.4	741.2	740.8	01.4	14.7	07.6	07.8	15.6	-00.4	-04.3	04.7	02.7	03.8	93	21	48	54	NE 1 ESE 3 ESE 2
22	740.4	737.1	735.8	02.5	19.4	13.6	12.3	20.3	01.4	-02.8	04.4	04.4	04.4	81	26	33	47	ENE 1 WSW 3 WSW 2
23	733.9	731.4	730.1	06.0	18.0	13.4	12.9	19.2	05.8	00.5	05.7	05.8	06.2	81	34	54	57	ENE 1 W 3 W 2
24	729.1	729.2	727.9	05.0	05.8	05.3	04.4	13.4	06.6	01.9	07.0	08.1	08.5	82	89	96	89	E 2 WNW 2 ESE 1
25	735.1	735.4	737.1	06.4	16.7	11.4	11.5	17.6	04.6	-01.1	05.5	03.8	05.3	76	27	53	52	ESE 2 SW 2 S 2
26	738.2	735.5	735.3	07.5	20.7	12.2	10.2	21.1	02.2	-01.4	06.1	04.9	04.4	78	27	41	49	NE 1 SW 2 SW 2
27	734.8	733.4	734.2	06.4	20.8	15.3	14.5	21.2	03.3	-02.0	05.9	05.1	06.5	82	27	65	58	ENE 1 WSW 4 WSW 2
28	735.7	734.8	734.4	11.8	14.6	13.0	13.1	18.3	10.5	-09.7	09.3	08.4	09.4	90	67	84	80	NE 1 NE 2 S 1
29	734.0	732.3	732.8	09.4	24.0	16.0	10.8	24.6	06.5	02.8	08.6	06.2	06.8	98	28	47	58	S 1 SW 4 WSW 2
30	732.5	731.2	732.5	11.7	24.2	16.4	17.2	25.2	07.4	02.0	08.0	06.6	06.0	78	29	43	50	ENE 1 WSW 2 E 1
MES. VRED.	733.1	732.0	732.4	04.3	13.0	08.6	08.6	14.5	02.7	-00.5	05.5	05						

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolaciju broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7 01	01○	00	00.7	08.8	00.2	.			
2	7 01	09○	09	06.3	04.6	.	.			
3	7 04○	10○	02	05.3	03.7	.	.			
4	6 10	05○	10	05.7	00.1	.	.			
5	8 00○	03○	00	01.0	08.8	00.0	.			
6	7 06○	01○	03	03.3	08.5	.	.			
7	8 05≡	06○	00	03.7	07.7	.	.			
8	7 04	10○	00	04.7	03.0	.	.			
9	7 06○	01○	00	02.3	08.3	.	.			
10	6 05	01○	00	03.3	07.8	.	.			
11	6 10	10○	10○	10.0	00.0	.	.			
12	5 10○	10	10	10.0	00.0	00.9	.			
13	8 10	09○	00	06.3	01.3	13.7	.			
14	7 10○≡	04○	03	05.7	06.7	00.1	.			
15	8 09	06○	00	05.0	05.7	00.2	.			
16	8 01○	05○	00	02.0	09.5	.	.			
17	7 01○	03○	00	01.3	08.5	.	.			
18	7 05○	09○	00	04.7	03.8	.	.			
19	7 09○	10	10○	05.7	02.2	.	.			
20	8 09≡	09○	04	07.3	04.2	06.7	.			
21	6 05	05○	00	04.7	05.5	03.4	.			
22	7 10○	04○	00	04.7	08.4	00.0	.			
23	8 09≡	08○	00	05.7	08.0	00.0	.			
24	8 02○	04○	09	05.0	09.6	.	.			
25	8 09	02○	00	03.7	07.7	.	.			
26	6 01○	05○	02	02.7	10.0	.	.			
27	8 19○	10○	05	05.3	00.3	.	.			
28	8 09○	08○	10○	09.0	02.4	00.0	.			
29	7 10○	10	10	10.0	00.0	06.0	.			
30	6 10*	10*	10*	10.0	00.0	14.5	01			
31	7 10*	10	10	10.0	00.0	07.8	08			
MES. RED.		06.7	06.5	03.9	05.7	156.3	53.9			

1	7 05	07○	01	05.7	06.4	00.1	03			
2	7 10≡	01○	00	03.7	07.7	.	.			
3	7 10	04○	00	04.7	05.6	.	.			
4	7 10*	10○	10	10.0	00.0	00.1	.			
5	6 10○	10○	10	10.0	00.0	01.6	.			
6	7 10	05○	00	05.0	05.2	25.6	.			
7	6 07○	10○	09	06.7	01.7	.	.			
8	7 10≡	10○	10○	10.0	00.0	02.1	.			
9	7 10*	10	10○	10.0	00.0	00.0	01			
10	7 10	10○	10○	10.0	00.0	13.4	.			
11	7 09	07○	05	07.0	08.4	04.0	.			
12	8 07○	05○	00	05.3	04.6	.	.			
13	8 09	04○	08	07.0	05.7	00.3	.			
14	7 10*	10○	10○	10.0	01.0	00.0	.			
15	8 10	09○	00	06.3	02.8	21.6	.			
16	9 02○	06○	00	02.3	06.9	00.0	.			
17	8 00○	00○	00	00.0	12.5	.	.			
18	8 06○	02○	00	02.7	10.5	.	.			
19	7 06○	04○	07	05.7	07.5	.	.			
20	7 10○	05○	00	06.3	03.7	01.4	.			
21	8 00○	01○	02	01.0	12.5	00.1	.			
22	6 06○	09○	00	05.0	05.8	.	.			
23	7 10	10	10	10.0	00.2	.	.			
24	5 10	10○	10	10.0	00.0	.	.			
25	9 02○	03○	02	02.3	11.4	21.2	.			
26	8 08	07○	00	05.0	05.7	.	.			
27	8 02○	07○	10	06.3	08.4	.	.			
28	7 10○	09○	05	08.0	02.5	04.5	.			
29	7 10≡	04○	05	06.3	09.0	02.3	.			
30	8 05○	04○	06	05.0	10.4	.	.			
MES. RED.		07.6	06.8	04.7	06.3	162.0	147.4			

$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$  Gr.  $\Delta G = + 58$  min.

BR. ST. 13

DN	Vzdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	732.8	732.7	734.8	10.2	24.0	16.4	16.8	24.0	07.3	00.4	07.2	06.1	07.0	77	27	50	51	ENE 1	W	3	NNE 1	
2	736.4	736.4	736.7	12.4	20.1	15.2	15.7	22.6	05.9	04.6	08.7	11.3	11.1	80	64	86	77	E 1	SE 2	2	WSW 2	
3	736.8	734.8	734.0	09.0	23.2	18.7	17.4	24.4	08.1	02.2	08.2	07.4	08.5	95	35	53	61	NNE 1	SE 1	1	ENE 2	
4	733.5	731.3	731.3	11.1	25.9	18.6	18.6	27.1	09.6	04.0	09.2	08.0	06.7	93	32	42	56	ENE 1	SSE 2	2	WNW 1	
5	731.6	734.2	735.0	14.4	16.1	13.0	14.1	18.6	13.0	10.4	10.5	06.2	06.5	86	45	58	63	ENE 1	NW 2	W	3	
6	737.6	736.1	736.5	06.6	18.8	10.2	11.5	19.9	04.1	-02.4	06.1	05.8	07.7	84	36	82	67	NE 2	ESE 2	2	S 1	
7	735.9	734.0	733.5	05.4	15.4	11.0	10.7	18.4	04.0	-01.1	06.4	05.4	07.5	96	41	76	71	SSW 1	WNW 3	3	E 1	
8	732.5	730.9	730.4	08.5	11.6	09.0	09.5	12.7	08.3	07.6	08.0	08.0	06.9	96	78	80	85	S 1	NNE 2	1	ENE 1	
9	731.3	732.7	734.5	13.4	10.5	10.7	14.1	10.6	07.6	03.4	07.7	06.4	07.6	95	56	80	77	-	O	SW 1	WSW 2	
10	735.6	734.6	735.2	06.2	19.2	12.8	19.4	06.1	-00.3	06.6	04.4	07.1	93	26	64	61	SSW 1	W 2	SW 2			
11	736.4	733.8	734.1	06.8	20.8	14.9	14.4	21.6	05.6	00.4	06.5	05.9	06.0	88	32	47	56	E 1	SW 3	3	SM 3	
12	733.2	730.4	729.3	11.3	21.8	16.3	16.4	22.3	09.6	04.8	07.9	07.1	07.1	79	36	51	55	ENE 1	WSW 4	2	SW 2	
13	727.3	727.6	726.4	14.6	17.9	14.4	15.3	18.6	12.8	06.6	08.9	10.0	09.6	71	65	78	71	SW 2	W 2	2	NNW 2	
14	723.8	724.7	726.1	11.7	17.2	13.2	13.8	19.1	09.7	09.9	09.8	08.8	08.4	95	60	74	76	ENE 2	ENE 1	1	S 1	
15	726.4	727.0	727.7	10.9	12.6	10.0	10.9	13.7	09.6	07.0	08.4	08.7	08.7	86	80	94	87	NW 1	W 1	W 1		
16	728.5	728.7	729.9	10.0	17.6	12.6	13.2	18.4	09.2	06.6	08.3	07.2	09.4	90	48	86	75	NW 1	WSW 2	2	SM 1	
17	732.4	735.3	737.4	09.2	17.0	14.0	13.6	18.7	08.6	04.6	08.4	07.9	10.2	96	54	85	78	ENE 1	WNW 2	2	E 1	
18	739.7	739.3	740.0	10.4	15.2	13.6	13.2	15.6	08.5	03.2	08.6	11.3	11.1	91	87	95	91	E 1	ENE 2	2	NNW 2	
19	737.7	735.3	734.4	14.0	21.7	17.7	17.8	22.3	13.2	12.6	11.1	11.1	12.9	93	57	85	78	ESE 1	S 2	SSE 1		
20	732.5	732.7	734.2	15.1	25.0	18.1	19.1	25.3	14.4	09.5	12.6	07.3	07.2	98	31	46	58	W 1	SSW 3	3	SW 2	
21	734.8	734.4	734.4	13.0	24.9	18.8	18.9	25.0	09.6	04.6	08.3	08.4	10.5	74	35	64	58	ESE 1	W 3	2	WSW 2	
22	735.2	735.0	737.4	14.3	22.2	14.3	16.3	23.1	13.5	09.4	10.2	08.8	11.5	84	44	94	74	NE 2	SW 3	3	E 1	
23	738.3	738.9	739.8	09.8	12.2	05.7	10.4	14.3	09.6	08.4	07.7	06.4	08.0	84	60	89	78	ENE 2	SE 2	2	SSE 1	
24	740.1	736.5	738.0	08.2	19.0	13.2	13.4	20.0	07.6	04.6	07.8	06.3	06.9	96	36	61	65	ESE 1	SE 2	2	E 1	
25	736.4	733.9	733.8	09.2	23.4	19.7	18.0	24.9	06.2	01.3	07.4	07.2	08.8	85	33	51	56	ENE 1	NE 1	1	E 2	
26	734.8	734.3	735.9	13.3	20.5	12.7	14.8	21.1	10.2	05.5	09.8	08.0	09.6	85	44	87	72	ENE 1	SE 3	SSE 1		
27	736.3	737.8	738.9	09.8	10.6	06.9	08.6	12.7	06.9	07.6	07.3	05.4	06.0	80	56	80	72	S 2	ESE 2	2	ESE 1	
28	738.4	736.5	736.5	03.1	17.6	11.8	11.1	18.2	02.0	02.5	05.7	05.0	05.4	100	33	52	62	SSE 1	SSE 2	2	S 2	
29	735.9	733.8	733.1	07.3	21.0	15.6	14.9	22.7	03.6	-01.0	06.1	04.7	06.6	79	25	50	51	E 1	S 2	2	WSW 2	
30	733.1	731.7	732.0	11.0	21.9	16.2	16.3	22.3	07.4	02.4	07.8	07.9	07.0	80	40	51	57	ENE 1	SW 3	2	WSW 2	
31	733.4	734.0	737.4	12.6	15.4	09.9	12.0	16.7	09.9	08.4	08.4	09.3	06.8	76	71	96	81	NNE 1	ENE 1	1	SSE 2	
MES.	VRED.	734.2	733.6	734.1	10.2	18.8	13.8	14.2	19.9	08.6	04.8	08.2	07.5	08.3	87	47	70	68	1.2	2.1	1.6	

1	739.1	738.2	738.7	08.5	15.6	05.8	10.5	16.4	07.6	06.3	06.5	04.9	04.4	78	37	49	55	SSE 2	ENE 3	NE 1	
2	738.3	735.8	736.2	07.3	18.2	13.0	12.9	19.0	02.9	-01.9	05.4	04.6	05.7	70	29	50	50	N 1	ESE 3	E 2	
3	734.8	733.2	733.1	09.7	17.6	13.0	13.3	18.3	07.0	01.6	06.5	05.5	06.6	72	37	59	56	SSE 1	SE 2	SE 2	
4	733.1	732.0	732.3	07.0	18.4	13.4	13.1	19.3	05.1	00.9	06.6	06.5	08.4	88	41	73	67	S 1	SE 2	NNW 1	
5	732.4	729.8	729.3	11.2	20.3	15.0	15.4	21.2	10.6	05.6	08.9	07.7	08.0	90	43	62	65	ENE 1	SW 3	W 2	
6	729.0	729.2	730.5	11.2	19.6	17.0	16.2	20.7	05.8	05.0	08.6	09.1	06.5	86	53	65	68	ESE 1	SW 2	W 2	
7	731.0	731.8	733.4	13.7	19.6	15.7	16.2	20.7	11.6	06.3	10.2	10.2	08.6	86	60	64	70	SW 1	S 2	NNW 2	
8	734.9	735.5	736.3	15.6	24.0	18.9	19.4	24.4	11.6	06.4	09.9	09.8	07.9	75	44	48	56	NNE 1	W 2	SW 3	
9	736.5	735.1	734.8	14.8	26.1	15.8	20.1	26.3	12.3	06.1	09.2	09.3	09.1	73	37	52	54	ENE 2	WSW 4	SW 2	
10	733.3	731.7	731.9	15.8	27.2	21.7	21.6	27.3	13.2	07.6	10.7	10.2	10.4	80	38	53	57	NE 1	WSW 4	NNW 2	
11	732.0	731.6	732.7	17.8	29.1	22.0	22.7	30.1	15.0	10.6	11.3	12.0	11.9	74	40	60	58	ESE 2	S 2	SSW 1	
12	735.9	732.5	732.9	18.4	28.4	24.2	23.8	29.8	15.6	14.6	12.6	11.3	12.5	79	39	55	58	SSE 1	S 3	SW 2	
13	733.0	730.8	730.7	19.1	30.4	23.7	24.2	32.0	15.4	10.2	12.9	10.5	11.2	78	32	51	54	SE 1	SW 2	SW 2	
14	730.1	729.7	729.4	18.0	27.2	20.4	21.5	27.5	15.1	09.4	12.1	10.0	08.7	78	37	48	54	E 1	WSW 3	W 3	
15	729.8	729.2	730.3	17.7	24.3	18.0	19.5	24.4	16.4	11.1	10.4	08.0	09.2	68	35	60	54	WSW 2	SW 3	SW 2	
16	730.4	730.1	730.7	15.4	23.8	19.0	19.3	24.1	14.3	12.2	11.2	10.0	11.9	85	45	72	67	SSW 2	NE 2	S 2	
17	731.7	731.3	732.9	16.1	26.8	20.6	21.0	27.3	13.3	07.7	11.2	10.1	10.7	82	38	59	60	ESE 1	2	NE 2	
18	733.9	732.0	731.1	18.4	28.2	21.7	22.5	29.3	15.2	15.3	11.6	09.7	09.7	73	34	50	52	ENE 1	S 2	WSW 2	
19	730.9	730.4	730.8	17.4	26.9	20.9	21.5	27.4	14.8	08.5	10.8	08.8	05.7	72	31	52	52	E 1	SW 3	WSW 2	
20	732.0	731.1	732.7	16.6	26.4	18.4	20.0	28.3	15.0	11.6	10.8	08.9	10.7	82	34	67	61	NE 1	W 2	SSW 1	
21	733.9	732.7	732.1																		

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vremenska časovna 0-9	Oblačnost N (0-10)					Insolacij srednji baric	Padavina R mm	Snožni potkriven h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8 01	05	07	05	05	05.7	09.5	.	.	= 0-4 <sup>10</sup> □ 0-9 <sup>20</sup> ○	
2	8 02	02	08	05	05	05.0	07.9	.	.	□ 0-4 <sup>10</sup> 9 <sup>20</sup> 13 <sup>20</sup> 15 <sup>20</sup> 13 <sup>15</sup> 15 <sup>20</sup> 13 <sup>15</sup> 15 <sup>20</sup> 13 <sup>15</sup> 15 <sup>20</sup> 13 <sup>15</sup> 15 <sup>20</sup> ○	
3	8 04	07	07	05	05	05.3	06.7	01.3	.	= 0-4 <sup>10</sup> 7 <sup>20</sup> □ 0-4 <sup>10</sup> 6 <sup>20</sup> ○	
4	8 03	06	06	09	09	06.0	07.2	.	.	□ 0-4 <sup>10</sup> 0-9 <sup>20</sup> □ 0-4 <sup>10</sup> 10 <sup>20</sup> ○	
5	8 10	07	07	00	00	05.7	04.2	00.6	.	□ 0-4 <sup>10</sup> 11 <sup>20</sup> 12 <sup>20</sup> ○	
6	8 09	04	00	04	03	07.0	00.0	.	.	□ 0-4 <sup>10</sup> 0-4 <sup>20</sup> 19 <sup>20</sup> 24 <sup>10</sup> □ 0-4 <sup>10</sup> 5 <sup>20</sup> 14 <sup>20</sup> 17 <sup>20</sup> ○	
7	7 04	09	09	07	03	08.6	00.0	.	.	□ 0-2 <sup>10</sup> 17 <sup>20</sup> 20-22 <sup>20</sup> □ 0-2 <sup>10</sup> 14 <sup>20</sup> 6 <sup>20</sup> ○	
8	7 10	09	10	06	07	06.7	04.3	04.5	.	= 0 <sup>20</sup> 17 <sup>20</sup> 15 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 12 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 19 <sup>20</sup> ○	
9	7 10	09	09	09	09	09.3	00.8	03.8	.	□ 0-4 <sup>10</sup> 10 <sup>20</sup> 14 <sup>20</sup> 12 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 13 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 15 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> ○	
10	8 05	08	00	05	07	05.7	09.3	00.4	.	= 0 <sup>20</sup> 3 <sup>20</sup> 6 <sup>20</sup> 9 <sup>20</sup> □ 0-4 <sup>10</sup> 6 <sup>20</sup> 13 <sup>20</sup> 12 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> ○	
11	8 05	05	04	04	07	08.9	.	.	.	□ 0-4 <sup>10</sup> 0-8 <sup>20</sup> 23 <sup>20</sup> 24 <sup>10</sup> = 0-2 <sup>10</sup> 10 <sup>20</sup> ○	
12	8 09	04	01	04	07	09.8	.	.	.	□ 0-2 <sup>10</sup> 10 <sup>20</sup> 15 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 12 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 19 <sup>20</sup> ○	
13	7 06	09	10	08	03	08.3	01.6	.	.	● 0-2 <sup>10</sup> 10 <sup>20</sup> 15 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 12 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 19 <sup>20</sup> ○	
14	8 10	09	10	05	07	05.7	04.7	09.1	.	● 0-2 <sup>10</sup> 0-4 <sup>20</sup> 11 <sup>20</sup> = 0-9 <sup>20</sup> □ 0-2 <sup>10</sup> 15 <sup>20</sup> 24 <sup>10</sup> ○	
15	7 09	10	09	09	03	09.3	00.7	12.0	.	□ 0-2 <sup>10</sup> 0-2 <sup>10</sup> 10 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 12 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 19 <sup>20</sup> ○	
16	7 10	05	04	07	07	04.1	04.0	.	.	= 0 <sup>20</sup> 9 <sup>20</sup> T 14 <sup>20</sup> 15 <sup>20</sup> 12 <sup>20</sup> 15 <sup>20</sup> ○	
17	8 10	09	03	07	03	04.0	01.5	.	.	= 0 <sup>20</sup> 10 <sup>20</sup> 4 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> ○	
18	6 10	10	10	10	00	00.0	00.7	.	.	□ 0-2 <sup>10</sup> 10 <sup>20</sup> 12 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> ○	
19	6 10	10	10	10	00	01.8	05.8	.	.	= 0-2 <sup>10</sup> 0-17 <sup>20</sup> 19 <sup>20</sup> ○	
20	8 06	04	02	05	03	08.4	00.0	.	.	= 0-4 <sup>10</sup> 17 <sup>20</sup> 9 <sup>20</sup> = 0-4 <sup>10</sup> 4 <sup>20</sup> 4 <sup>20</sup> = 0-2 <sup>10</sup> 7 <sup>20</sup> 5 <sup>20</sup> ○	
21	8 00	04	02	02	02	02.0	11.2	.	.	□ 0-2 <sup>10</sup> 15 <sup>20</sup> 16 <sup>20</sup> 17 <sup>20</sup> 18 <sup>20</sup> 19 <sup>20</sup> 20 <sup>20</sup> 21 <sup>20</sup> 22 <sup>20</sup> 23 <sup>20</sup> 24 <sup>20</sup> 25 <sup>20</sup> ○	
22	8 07	08	10	08	03	08.3	05.4	00.0	.	● 0-4 <sup>10</sup> 5 <sup>20</sup> 16 <sup>20</sup> 17 <sup>20</sup> 18 <sup>20</sup> 19 <sup>20</sup> 20 <sup>20</sup> 21 <sup>20</sup> 22 <sup>20</sup> 23 <sup>20</sup> 24 <sup>20</sup> 25 <sup>20</sup> ○	
23	7 10	10	09	05	07	00.0	11.6	.	.	● 0-1 <sup>20</sup> 15 <sup>20</sup> 16 <sup>20</sup> 17 <sup>20</sup> 18 <sup>20</sup> 19 <sup>20</sup> 20 <sup>20</sup> 21 <sup>20</sup> 22 <sup>20</sup> 23 <sup>20</sup> 24 <sup>20</sup> 25 <sup>20</sup> ○	
24	8 10	02	00	04	00	09.3	02.7	.	.	= 0-2 <sup>10</sup> 10 <sup>20</sup> 12 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> ○	
25	8 06	01	06	02.3	02.3	12.0	.	.	.	□ 0-2 <sup>10</sup> 9 <sup>20</sup> 22 <sup>20</sup> 24 <sup>10</sup> = 0-2 <sup>10</sup> 7 <sup>20</sup> 5 <sup>20</sup> ○	
26	7 09	06	10	08	03	08.3	06.3	.	.	□ 0-2 <sup>10</sup> 15 <sup>20</sup> 16 <sup>20</sup> 17 <sup>20</sup> 18 <sup>20</sup> 19 <sup>20</sup> 20 <sup>20</sup> 21 <sup>20</sup> 22 <sup>20</sup> 23 <sup>20</sup> 24 <sup>20</sup> ○	
27	7 10	10	01	07	00	00.0	01.8	.	.	● 0-1 <sup>20</sup> 13 <sup>20</sup> □ 0-2 <sup>10</sup> 19 <sup>20</sup> 24 <sup>10</sup> = 0-2 <sup>10</sup> 24 <sup>20</sup> ○	
28	8 10	00	01	03	07	10.2	00.2	.	.	□ 0-2 <sup>10</sup> 10 <sup>20</sup> 12 <sup>20</sup> 14 <sup>20</sup> 13 <sup>20</sup> 11 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> 10 <sup>20</sup> ○	
29	8 00	01	00	00.3	01	01.3	12.7	.	.	□ 0-2 <sup>10</sup> 9 <sup>20</sup> ○	
30	7 00	01	01	00.7	01	00.7	12.8	.	.	□ 0-2 <sup>10</sup> 9 <sup>20</sup> ○	
31	7 09	10	10	09.7	01.0	01.0	01.0	.	.	= 0-1 <sup>20</sup> 9 <sup>20</sup> 14 <sup>20</sup> ; = 0-15 <sup>20</sup> 17 <sup>20</sup> ; = 0-15 <sup>20</sup> 16 <sup>20</sup> ; = 0-15 <sup>20</sup> 14 <sup>20</sup> ; = 0-15 <sup>20</sup> 12 <sup>20</sup> ; = 0-15 <sup>20</sup> 10 <sup>20</sup> ; = 0-15 <sup>20</sup> 8 <sup>20</sup> ; = 0-15 <sup>20</sup> 6 <sup>20</sup> ; = 0-15 <sup>20</sup> 4 <sup>20</sup> ; = 0-15 <sup>20</sup> 2 <sup>20</sup> ; = 0-15 <sup>20</sup> 0 <sup>20</sup> ; = 0-15 <sup>20</sup> -2 <sup>20</sup> ; = 0-15 <sup>20</sup> -4 <sup>20</sup> ; = 0-15 <sup>20</sup> -6 <sup>20</sup> ; = 0-15 <sup>20</sup> -8 <sup>20</sup> ; = 0-15 <sup>20</sup> -10 <sup>20</sup> ; = 0-15 <sup>20</sup> -12 <sup>20</sup> ; = 0-15 <sup>20</sup> -14 <sup>20</sup> ; = 0-15 <sup>20</sup> -16 <sup>20</sup> ; = 0-15 <sup>20</sup> -18 <sup>20</sup> ; = 0-15 <sup>20</sup> -20 <sup>20</sup> ; = 0-15 <sup>20</sup> -22 <sup>20</sup> ; = 0-15 <sup>20</sup> -24 <sup>20</sup> ; = 0-15 <sup>20</sup> -26 <sup>20</sup> ; = 0-15 <sup>20</sup> -28 <sup>20</sup> ; = 0-15 <sup>20</sup> -30 <sup>20</sup> ; = 0-15 <sup>20</sup> -32 <sup>20</sup> ; = 0-15 <sup>20</sup> -34 <sup>20</sup> ; = 0-15 <sup>20</sup> -36 <sup>20</sup> ; = 0-15 <sup>20</sup> -38 <sup>20</sup> ; = 0-15 <sup>20</sup> -40 <sup>20</sup> ; = 0-15 <sup>20</sup> -42 <sup>20</sup> ; = 0-15 <sup>20</sup> -44 <sup>20</sup> ; = 0-15 <sup>20</sup> -46 <sup>20</sup> ; = 0-15 <sup>20</sup> -48 <sup>20</sup> ; = 0-15 <sup>20</sup> -50 <sup>20</sup> ; = 0-15 <sup>20</sup> -52 <sup>20</sup> ; = 0-15 <sup>20</sup> -54 <sup>20</sup> ; = 0-15 <sup>20</sup> -56 <sup>20</sup> ; = 0-15 <sup>20</sup> -58 <sup>20</sup> ; = 0-15 <sup>20</sup> -60 <sup>20</sup> ; = 0-15 <sup>20</sup> -62 <sup>20</sup> ; = 0-15 <sup>20</sup> -64 <sup>20</sup> ; = 0-15 <sup>20</sup> -66 <sup>20</sup> ; = 0-15 <sup>20</sup> -68 <sup>20</sup> ; = 0-15 <sup>20</sup> -70 <sup>20</sup> ; = 0-15 <sup>20</sup> -72 <sup>20</sup> ; = 0-15 <sup>20</sup> -74 <sup>20</sup> ; = 0-15 <sup>20</sup> -76 <sup>20</sup> ; = 0-15 <sup>20</sup> -78 <sup>20</sup> ; = 0-15 <sup>20</sup> -80 <sup>20</sup> ; = 0-15 <sup>20</sup> -82 <sup>20</sup> ; = 0-15 <sup>20</sup> -84 <sup>20</sup> ; = 0-15 <sup>20</sup> -86 <sup>20</sup> ; = 0-15 <sup>20</sup> -88 <sup>20</sup> ; = 0-15 <sup>20</sup> -90 <sup>20</sup> ; = 0-15 <sup>20</sup> -92 <sup>20</sup> ; = 0-15 <sup>20</sup> -94 <sup>20</sup> ; = 0-15 <sup>20</sup> -96 <sup>20</sup> ; = 0-15 <sup>20</sup> -98 <sup>20</sup> ; = 0-15 <sup>20</sup> -100 <sup>20</sup> ; = 0-15 <sup>20</sup> -102 <sup>20</sup> ; = 0-15 <sup>20</sup> -104 <sup>20</sup> ; = 0-15 <sup>20</sup> -106 <sup>20</sup> ; = 0-15 <sup>20</sup> -108 <sup>20</sup> ; = 0-15 <sup>20</sup> -110 <sup>20</sup> ; = 0-15 <sup>20</sup> -112 <sup>20</sup> ; = 0-15 <sup>20</sup> -114 <sup>20</sup> ; = 0-15 <sup>20</sup> -116 <sup>20</sup> ; = 0-15 <sup>20</sup> -118 <sup>20</sup> ; = 0-15 <sup>20</sup> -120 <sup>20</sup> ; = 0-15 <sup>20</sup> -122 <sup>20</sup> ; = 0-15 <sup>20</sup> -124 <sup>20</sup> ; = 0-15 <sup>20</sup> -126 <sup>20</sup> ; = 0-15 <sup>20</sup> -128 <sup>20</sup> ; = 0-15 <sup>20</sup> -130 <sup>20</sup> ; = 0-15 <sup>20</sup> -132 <sup>20</sup> ; = 0-15 <sup>20</sup> -134 <sup>20</sup> ; = 0-15 <sup>20</sup> -136 <sup>20</sup> ; = 0-15 <sup>20</sup> -138 <sup>20</sup> ; = 0-15 <sup>20</sup> -140 <sup>20</sup> ; = 0-15 <sup>20</sup> -142 <sup>20</sup> ; = 0-15 <sup>20</sup> -144 <sup>20</sup> ; = 0-15 <sup>20</sup> -146 <sup>20</sup> ; = 0-15 <sup>20</sup> -148 <sup>20</sup> ; = 0-15 <sup>20</sup> -150 <sup>20</sup> ; = 0-15 <sup>20</sup> -152 <sup>20</sup> ; = 0-15 <sup>20</sup> -154 <sup>20</sup> ; = 0-15 <sup>20</sup> -156 <sup>20</sup> ; = 0-15 <sup>20</sup> -158 <sup>20</sup> ; = 0-15 <sup>20</sup> -160 <sup>20</sup> ; = 0-15 <sup>20</sup> -162 <sup>20</sup> ; = 0-15 <sup>20</sup> -164 <sup>20</sup> ; = 0-15 <sup>20</sup> -166 <sup>20</sup> ; = 0-15 <sup>20</sup> -168 <sup>20</sup> ; = 0-15 <sup>20</sup> -170 <sup>20</sup> ; = 0-15 <sup>20</sup> -172 <sup>20</sup> ; = 0-15 <sup>20</sup> -174 <sup>20</sup> ; = 0-15 <sup>20</sup> -176 <sup>20</sup> ; = 0-15 <sup>20</sup> -178 <sup>20</sup> ; = 0-15 <sup>20</sup> -180 <sup>20</sup> ; = 0-15 <sup>20</sup> -182 <sup>20</sup> ; = 0-15 <sup>20</sup> -184 <sup>20</sup> ; = 0-15 <sup>20</sup> -186 <sup>20</sup> ; = 0-15 <sup>20</sup> -188 <sup>20</sup> ; = 0-15 <sup>20</sup> -190 <sup>20</sup> ; = 0-15 <sup>20</sup> -192 <sup>20</sup> ; = 0-15 <sup>20</sup> -194 <sup>20</sup> ; = 0-15 <sup>20</sup> -196 <sup>20</sup> ; = 0-15 <sup>20</sup> -198 <sup>20</sup> ; = 0-15 <sup>20</sup> -200 <sup>20</sup> ; = 0-15 <sup>20</sup> -202 <sup>20</sup> ; = 0-15 <sup>20</sup> -204 <sup>20</sup> ; = 0-15 <sup>20</sup> -206 <sup>20</sup> ; = 0-15 <sup>20</sup> -208 <sup>20</sup> ; = 0-15 <sup>20</sup> -210 <sup>20</sup> ; = 0-15 <sup>20</sup> -212 <sup>20</sup> ; = 0-15 <sup>20</sup> -214 <sup>20</sup> ; = 0-15 <sup>20</sup> -216 <sup>20</sup> ; = 0-15 <sup>20</sup> -218 <sup>20</sup> ; = 0-15 <sup>20</sup> -220 <sup>20</sup> ; = 0-15 <sup>20</sup> -222 <sup>20</sup> ; = 0-15 <sup>20</sup> -224 <sup>20</sup> ; = 0-15 <sup>20</sup> -226 <sup>20</sup> ; = 0-15 <sup>20</sup> -228 <sup>20</sup> ; = 0-15 <sup>20</sup> -230 <sup>20</sup> ; = 0-15 <sup>20</sup> -232 <sup>20</sup> ; = 0-15 <sup>20</sup> -234 <sup>20</sup> ; = 0-15 <sup>20</sup> -236 <sup>20</sup> ; = 0-15 <sup>20</sup> -238 <sup>20</sup> ; = 0-15 <sup>20</sup> -240 <sup>20</sup> ; = 0-15 <sup>20</sup> -242 <sup>20</sup> ; = 0-15 <sup>20</sup> -244 <sup>20</sup> ; = 0-15 <sup>20</sup> -246 <sup>20</sup> ; = 0-15 <sup>20</sup> -248 <sup>20</sup> ; = 0-15 <sup>20</sup> -250 <sup>20</sup> ; = 0-15 <sup>20</sup> -252 <sup>20</sup> ; = 0-15 <sup>20</sup> -254 <sup>20</sup> ; = 0-15 <sup>20</sup> -256 <sup>20</sup> ; = 0-15 <sup>20</sup> -258 <sup>20</sup> ; = 0-15 <sup>20</sup> -260 <sup>20</sup> ; = 0-15 <sup>20</sup> -262 <sup>20</sup> ; = 0-15 <sup>20</sup> -264 <sup>20</sup> ; = 0-15 <sup>20</sup> -266 <sup>20</sup> ; = 0-15 <sup>20</sup> -268 <sup>20</sup> ; = 0-15 <sup>20</sup> -270 <sup>20</sup> ; = 0-15 <sup>20</sup> -272 <sup>20</sup> ; = 0-15 <sup>20</sup> -274 <sup>20</sup> ; = 0-15 <sup>20</sup> -276 <sup>20</sup> ; = 0-15 <sup>20</sup> -278 <sup>20</sup> ; = 0-15 <sup>20</sup> -280 <sup>20</sup> ; = 0-15 <sup>20</sup> -282 <sup>20</sup> ; = 0-15 <sup>20</sup> -284 <sup>20</sup> ; = 0-15 <sup>20</sup> -286 <sup>20</sup> ; = 0-15 <sup>20</sup> -288 <sup>20</sup> ; = 0-15 <sup>20</sup> -290 <sup>20</sup> ; = 0-15 <sup>20</sup> -292 <sup>20</sup> ; = 0-15 <sup>20</sup> -294 <sup>20</sup> ; = 0-15 <sup>20</sup> -296 <sup>20</sup> ; = 0-15 <sup>20</sup> -298 <sup>20</sup> ; = 0-15 <sup>20</sup> -300 <sup>20</sup> ; = 0-15 <sup>20</sup> -302 <sup>20</sup> ; = 0-15 <sup>20</sup> -304 <sup>20</sup> ; = 0-15 <sup>20</sup> -306 <sup>20</sup> ; = 0-15 <sup>20</sup> -308 <sup>20</sup> ; = 0-15 <sup>20</sup> -310 <sup>20</sup> ; = 0-15 <sup>20</sup> -312 <sup>20</sup> ; = 0-15 <sup>20</sup> -314 <sup>20</sup> ; = 0-15 <sup>20</sup> -316 <sup>20</sup> ; = 0-15 <sup>20</sup> -318 <sup>20</sup> ; = 0-15 <sup>20</sup> -320 <sup>20</sup> ; = 0-15 <sup>20</sup> -322 <sup>20</sup> ; = 0-15 <sup>20</sup> -324 <sup>20</sup> ; = 0-15 <sup>20</sup> -326 <sup>20</sup> ; = 0-15 <sup>20</sup> -328 <sup>20</sup> ; = 0-15 <sup>20</sup> -330 <sup>20</sup> ; = 0-15 <sup>20</sup> -332 <sup>20</sup> ; = 0-15 <sup>20</sup> -334 <sup>20</sup> ; = 0-15 <sup>20</sup> -336 <sup>20</sup> ; = 0-15 <sup>20</sup> -338 <sup>20</sup> ; = 0-15 <sup>20</sup> -340 <sup>20</sup> ; = 0-15 <sup>20</sup> -342 <sup>20</sup> ; = 0-15 <sup>20</sup> -344 <sup>20</sup> ; = 0-15 <sup>20</sup> -346 <sup>20</sup> ; = 0-15 <sup>20</sup> -348 <sup>20</sup> ; = 0-15 <sup>20</sup> -350 <sup>20</sup> ; = 0-15 <sup>20</sup> -352 <sup>20</sup> ; = 0-15 <sup>20</sup> -354 <sup>20</sup> ; = 0-15 <sup>20</sup> -356 <sup>20</sup> ; = 0-15 <sup>20</sup> -358 <sup>20</sup> ; = 0-15 <sup>20</sup> -3	

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 $\varphi = 46^{\circ}04'$  N  $\lambda = 14^{\circ}31'$  E Gr.  $\Delta G = + 58$  min.

BR. ST. 13

D S	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodené pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21	
1	736.5	738.4	739.6	15.1	23.2	16.4	17.8	24.4	11.6	12.0	11.1	10.2	11.2	86	48	80	71	ESE 1	SSE 2	NE 1	
2	740.3	738.3	737.8	12.2	26.4	15.8	19.6	27.3	16.6	08.9	09.7	07.8	10.3	91	30	59	60	ESE 1	ESE 3	ENE 1	
3	737.9	735.7	734.1	16.2	29.4	23.2	23.0	29.6	12.7	08.1	11.1	12.2	11.3	81	40	53	58	SSE 1	WSW 3	SW 2	
4	732.7	731.4	730.3	18.1	29.0	23.6	23.6	29.4	14.7	10.0	12.3	13.0	13.3	79	43	61	61	NE 1	W 1	SW 2	
5	730.1	729.2	729.0	17.7	21.7	17.6	18.7	23.6	17.0	12.2	13.6	13.0	12.0	90	67	80	79	NNE 2	SW 2	NNE 2	
6	731.2	730.6	731.3	16.8	24.7	20.5	20.8	26.6	14.4	09.7	11.2	10.0	11.7	78	43	63	61	SSE 2	W 2	E 1	
7	731.5	730.1	731.0	17.0	26.9	21.2	21.6	27.1	14.2	08.7	12.3	12.8	13.7	85	48	73	69	E 2	WSW 3	SW 1	
8	730.1	728.8	727.8	19.6	25.0	21.7	22.0	27.2	18.2	14.3	14.5	11.0	14.1	85	46	72	68	ESE 1	SSW 3	W 2	
9	728.8	730.2	732.8	19.0	22.3	18.0	19.3	24.2	16.0	10.0	13.7	14.1	14.0	83	70	91	81	NW 1	WNW 2	SW 2	
10	734.0	733.6	734.5	15.3	22.0	15.8	17.2	24.4	15.1	10.0	12.5	11.9	12.7	96	60	94	83	SSE 1	S 3	SW 1	
11	735.5	734.3	735.1	13.9	27.4	21.0	20.8	29.3	13.6	05.8	10.9	09.6	12.1	92	35	65	64	SSE 2	WNW 2	S 1	
12	735.9	734.4	734.8	15.8	29.8	23.0	22.9	30.2	12.8	07.4	11.1	09.6	13.6	82	39	64	59	ENE 1	W 2	SW 2	
13	735.6	733.4	732.9	17.8	30.1	22.4	23.2	30.2	15.0	10.3	13.0	12.3	12.1	85	39	60	61	NNE 1	SW 3	W 1	
14	732.3	731.8	730.2	18.6	17.3	20.7	19.3	25.6	16.1	11.4	13.3	12.9	14.6	83	87	66	83	ESE 2	WNW 2	ESE 2	
15	730.6	732.6	735.9	16.4	16.8	15.0	15.8	21.7	14.6	10.0	12.2	12.6	11.2	87	88	88	88	E 2	SE 2	NE 1	
16	738.5	737.5	735.4	13.8	21.0	17.6	17.5	21.9	12.8	10.0	10.0	07.9	11.5	84	42	76	67	N 1	SSE 2	ENE 1	
17	734.5	734.6	734.6	15.3	22.1	19.1	18.9	23.9	13.3	08.3	11.1	10.7	12.6	85	54	76	72	SW 2	SSE 2	NE 1	
18	734.9	733.3	731.3	15.6	19.7	18.9	18.3	23.4	14.6	09.2	11.7	12.8	13.4	88	74	82	81	E 1	N 2	WNW 1	
19	731.7	732.7	733.4	16.6	18.6	15.6	18.6	22.7	15.3	10.4	11.9	12.9	13.7	84	80	81	81	ENE 2	S 1	SE 1	
20	734.5	732.8	731.7	17.3	25.1	21.2	21.2	25.8	15.7	10.6	12.7	11.5	13.6	86	48	72	69	S 1	E 2	SE 1	
21	730.5	734.0	735.2	17.0	18.4	16.7	17.2	21.2	15.1	12.6	13.8	11.2	10.3	95	71	72	79	SE 1	S 2	SE 2	
22	736.0	735.7	736.3	14.7	16.8	15.0	15.4	17.1	14.0	11.6	11.3	09.7	11.5	90	68	80	83	SSE 2	SE 1	ESE 1	
23	736.7	736.2	736.4	11.4	23.4	16.6	17.0	25.7	10.6	04.3	09.8	07.8	11.2	97	36	79	71	SSW 1	SE 2	NNE 1	
24	736.1	732.3	731.1	12.9	27.3	19.6	19.9	27.8	10.6	05.2	05.2	10.4	11.0	83	38	64	62	WNW 1	W 2	SSW 2	
25	728.9	725.2	725.0	16.6	25.4	20.1	20.6	26.4	13.4	07.5	11.6	11.1	12.7	82	45	72	66	NE 1	SW 3	W 1	
26	727.2	730.6	731.1	11.4	11.9	10.8	11.2	20.1	10.0	09.4	09.5	09.4	09.0	94	50	93	92	NNW 4	NNW 2	NNE 2	
27	733.0	733.8	734.3	11.2	21.2	14.2	15.2	22.0	09.8	05.1	08.8	08.3	10.1	89	44	84	72	E 1	SE 3	E 1	
28	734.1	733.0	733.7	11.6	22.6	15.7	16.4	23.6	05.6	04.4	09.2	09.0	11.5	90	44	86	73	NE 1	SW 2	NE 1	
29	734.8	733.3	733.4	12.1	25.8	20.6	19.8	26.2	10.7	05.6	10.4	11.1	12.2	98	45	67	70	NNE 1	SW 2	W 1	
30	733.1	731.9	730.3	16.8	25.4	22.1	21.6	28.3	15.6	11.1	12.2	11.9	15.6	85	49	78	71	N 1	N 1	W 1	
31	725.5	724.9	724.5	17.8	21.0	16.7	18.1	22.1	16.7	12.1	13.9	11.1	12.1	91	60	85	79	S 2	S 4	S 2	
MES. RED.	733.4	732.7	732.7	15.5	23.2	18.9	19.1	25.1	13.7	09.5	11.6	11.0	12.2	87	54	75	72	1.4	2.2	1.4	

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LJUBLJANA-BEŽIGRAD

1	725.3	728.6	731.0	15.1	23.8	17.8	18.6	24.8	14.7	10.2	12.2	07.1	06.6	95	32	43	57	SW 2	NNE 3	NE 2
2	731.3	731.1	731.4	11.0	22.1	15.8	16.2	24.1	05.2	04.5	08.0	07.1	10.0	82	35	74	64	E 1	W 2	ESE 2
3	732.4	732.2	733.8	12.6	24.9	16.1	18.4	25.0	10.6	02.0	09.7	10.7	13.6	89	43	57	64	E 1	WSW 3	SW 2
4	736.8	736.1	736.8	13.6	27.0	20.3	20.3	27.4	11.3	07.5	10.2	11.3	12.7	87	42	71	67	ENE 1	W 2	SSW 2
5	736.7	734.6	735.1	14.4	27.3	19.1	20.0	27.4	12.6	06.7	11.3	11.3	12.2	92	41	74	69	ENE 2	SSW 2	SW 1
6	735.6	734.6	735.0	15.4	27.7	20.4	21.6	28.1	12.7	06.5	11.3	11.8	12.6	86	42	70	66	W 1	SE 3	E 2
7	734.7	732.9	732.5	14.6	27.4	19.4	20.2	27.7	13.8	07.4	11.7	11.4	12.6	94	42	75	70	NW 1	SSE 2	NNE 1
8	733.0	732.6	733.4	15.2	27.3	20.7	20.0	27.3	14.0	10.6	11.9	12.5	14.7	92	46	60	73	NE 1	W 2	ESE 1
9	735.1	735.3	735.4	17.7	22.5	16.7	19.4	24.5	15.8	12.3	11.4	12.8	14.4	75	63	85	76	WNW 1	E 1	WW 1
10	734.8	734.3	734.5	17.4	22.7	19.2	19.6	23.6	15.8	11.0	12.8	15.2	13.4	86	74	80	80	S 2	S 2	NNE 2
11	734.3	733.3	734.4	14.0	23.8	16.3	17.6	24.1	13.0	11.0	10.9	10.7	12.8	91	46	92	77	NW 2	ENE 2	ENE 2
12	734.1	733.5	733.3	15.4	21.4	17.6	18.1	22.2	14.8	10.7	11.7	11.5	13.2	89	60	86	78	NE 1	E 2	SE 1
13	733.0	732.8	733.7	15.7	25.0	16.1	19.2	25.8	14.8	12.4	12.0	10.5	10.7	91	44	69	66	NW 1	WNW 2	NE 1
14	733.3	734.7	735.7	15.1	19.2	15.4	16.3	21.6	14.5	10.4	11.6	12.2	14.4	90	73	87	83	S 1	W 1	E 1
15	736.8	735.9	737.3	12.6	23.2	17.3	17.6	25.0	11.8	08.2	10.3	10.3	12.0	94	48	81	74	ENE 1	ENE 2	S 2
16	737.7	735.8	735.4	13.9	26.4	16.7	16.9	27.0	12.7	08.8	11.4	12.5	11.4	96	48	66	70	ENE 1	S 2	SW 1
17	735.6	734.7	734.1	15.1	24.5	19.6	19.7	25.8	14.0	08.3	11.4	12.8	15.3	89	56	89	78	SSE 1	ESE 1	ENE 1
18	732.5	731.4	730.3	16.4	26.3	21.8	21.6	26.4	16.0	10.2	13.7	13.8	13.9	98	54	71	74	SE 1	SW 4	ENE 1
19	727.2	726.3	728.7	16.3	24.4	13.3	16.8	24.5	12.9	12.4	12.8	11.4	10.6	92	50	92	78	NNE 1	W 3	NNE 1
20	729.8	728.9	728.9	12.1	18.8	15.7	15.6	19.2	11.6	10.5	09.9	12.9	12.6	93	79	94	89	W 1	W 1	SSW 2
21	725.7	722.9	720.5	14.7	15.0	15.0	14.9	16.2	14.5	09.8	11.5	11.7	1							

ER. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vremensko- čas	Oblačnost N (0-10)					Podavina R mm	Snežni pokriven h cm	Rezerv vremena w
		14	7	14	21	Sred Dnes			
1	8 09	090	030	00	04.0	08.6	11.4	.	$\overline{\Delta}^o 0.730, \overline{\Delta}^o 0-24, \odot$
2	7 02	020	020	09	01.3	13.5	.	.	$\overline{\Delta}^o 0.730, 2030-24, \overline{\Delta}^o 2-30 i, \overline{\Delta}^o 2.5-6-60, \odot$
3	8 00	030	010	00	00.3	13.5	.	.	$\overline{\Delta}^o 1.0-745, \overline{\Delta}^o 430-730, \odot$
4	7 00	050	10	05.0	08.4	.	.	.	$\overline{\Delta}^o 1732-1050, \overline{\Delta}^o 2030-24, \odot$
5	7 10	10K	100	04	08.0	00.0	.	.	$\overline{\Delta}^o 0-100, \overline{\Delta}^o 1030, \overline{\Delta}^o 2030-1045, T^o 645-80, 15^o 10-1205, \overline{\Delta}^o 10-85-1540, \overline{\Delta}^o 10-85-925, \odot$
6	8 06	010	06	04.3	08.6	04.1	.	.	$\overline{\Delta}^o 2230-24, \odot$
7	7 03	030	10	05.3	09.2	.	.	.	$\overline{\Delta}^o 0-745, \overline{\Delta}^o 130-830, \overline{\Delta}^o 0.8-2145, \overline{\Delta}^o 110-1520, \odot$
8	8 09	090	10	09.3	03.2	00.0	.	.	$T^o 2030, \overline{\Delta}^o 2130-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
9	8 02	09	10K	09	09.3	02.6	17.7	.	$\overline{\Delta}^o 0-105, \overline{\Delta}^o 1030, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 1430-2350, T^o 10-2345, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
10	7 10	10K	02	07.3	03.1	05.1	.	.	$\overline{\Delta}^o 0-105, \overline{\Delta}^o 1030, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 1430-2350, T^o 10-2345, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
11	8 10	040	01	05.0	11.0	03.6	.	.	$\overline{\Delta}^o 0-510 i, \overline{\Delta}^o 30-840 i, \odot$
12	8 01	030	00	01.3	12.3	.	.	.	$\overline{\Delta}^o 0-510, \odot$
13	7 01	040	06	03.7	11.3	.	.	.	$\overline{\Delta}^o 10-2345, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
14	7 01	090	09K	06.3	08.3	00.2	.	.	$\overline{\Delta}^o 10-2345, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
15	7 10	100	10	10.0	00.0	12.7	.	.	$\overline{\Delta}^o 0-405, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
16	7 07	090	07	07.7	06.3	21.2	.	.	$\overline{\Delta}^o 215-730, \overline{\Delta}^o 2230-24, \odot$
17	8 05	09	09	05.0	05.0	00.0	.	.	$\overline{\Delta}^o 0-60, \overline{\Delta}^o 2130-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
18	7 09	090	04	07.3	6.7	00.3	.	.	$\overline{\Delta}^o 10-2345, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
19	7 05	080	09	07.3	05.4	00.2	.	.	$\overline{\Delta}^o 10-2345, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
20	7 07	080	09	08.0	06.7	03.7	.	.	$\overline{\Delta}^o 0-845, \overline{\Delta}^o 10-2345, \odot$
21	9 09	09	09	09.0	00.8	05.9	.	.	$\overline{\Delta}^o 0-510, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
22	7 10	100	10	09.7	00.0	10.6	.	.	$\overline{\Delta}^o 0-105, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
23	8 10	040	00	04.7	09.9	01.8	.	.	$\overline{\Delta}^o 0-9-2345, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \odot$
24	7 00	000	00	00.0	12.3	.	.	.	$\overline{\Delta}^o 0-815, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \odot$
25	8 00	050	01	02.0	10.7	.	.	.	$\overline{\Delta}^o 0-232-730, \overline{\Delta}^o 2030-24, \overline{\Delta}^o 10-2345, \odot$
MES.	PRED.	06.5	06.4	05.5	06.1	213.1	144.0		

1	8 05	090	04	07.3	05.1	13.9	.	.	$\overline{\Delta}^o 0-315, \odot$
2	8 09	060	00	05.0	04.3	.	.	.	$\overline{\Delta}^o 10-2345, \odot$
3	8 030	040	01	02.7	10.8	.	.	.	$\overline{\Delta}^o 10-0-9-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
4	8 000	030	01	01.3	11.8	.	.	.	$\overline{\Delta}^o 10-0-9-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
5	7 020	080	00	03.3	08.3	.	.	.	$\overline{\Delta}^o 10-0-9-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
6	7 000	030	05	02.7	10.3	.	.	.	$\overline{\Delta}^o 10-0-9-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
7	5 10	010	04	05.0	09.3	00.2	.	.	$\overline{\Delta}^o 0-45, \overline{\Delta}^o 2230-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
8	6 000	040	05	03.0	05.2	.	.	.	$\overline{\Delta}^o 10-0-9-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
9	7 020	060	09	05.7	03.7	.	.	.	$\overline{\Delta}^o 0-50, \overline{\Delta}^o 2230-24, = 630-830, \odot$
10	7 07	060	070	10K	07.7	06.8	01.7	.	$\overline{\Delta}^o 0-50, \overline{\Delta}^o 2230-24, = 630-830, \odot$
11	8 08	030	03	04.7	07.4	03.2	.	.	$T^o 230-415, R^o 45-50, 10^o 10-1205, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
12	7 10	050	07	08.7	02.3	08.3	.	.	$\overline{\Delta}^o 0-10, \overline{\Delta}^o 2230-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
13	8 030	040	C3	03.3	10.5	05.2	.	.	$\overline{\Delta}^o 0-6-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
14	8 10	090	00	06.3	04.5	C1.4	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
15	8 10	05	05	06.0	05.7	00.8	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
16	7 10	010	00	03.7	09.8	.	.	.	$\overline{\Delta}^o 10-0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
17	7 09	090	01	06.3	03.0	.	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
18	7 10	080	090	09.0	02.5	00.0	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
19	8 10	040	05	06.3	05.0	08.3	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
20	6 10	090	100	05.7	00.4	35.0	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
21	6 10	100	100	10.0	00.0	21.6	.	.	$\overline{\Delta}^o 0-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
22	7 060	10K	090	08.3	00.5	52.2	.	.	$\overline{\Delta}^o 0-50, \overline{\Delta}^o 2230-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
23	7 09	06K0	100	08.3	03.5	12.0	.	.	$\overline{\Delta}^o 0-50, \overline{\Delta}^o 2230-24, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 10-2345, \odot$
24	8 07	050	03	04.6	06.6	08.5	.	.	$\overline{\Delta}^o 0-9-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
25	7 10	020	00	04.0	08.4	.	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
26	7 10	040	01	05.0	08.5	.	.	.	$\overline{\Delta}^o 10-0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
27	7 020	060	06	04.7	04.6	.	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
28	5 10	100	10	10.0	00.0	00.5	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
29	7 10	09	10	09.7	00.9	25.8	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
30	7 10	050	05	05.3	01.8	00.2	.	.	$\overline{\Delta}^o 0-70, \overline{\Delta}^o 10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
31	7 09	10	07	06.7	01.5	.	.	.	$\overline{\Delta}^o 0-10-2345, \overline{\Delta}^o 2030-24, = 630-830, \odot$
MES.	PRED.	07.2	06.4	05.0	06.2	163.8	159.8		

$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$  Gr.  $\Delta G = + 58$  min.

BR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	734.4	734.1	734.9	16.2	26.2	20.4	20.8	26.3	15.6	12.0	13.1	13.2	15.3	95	52	85	77	E	1	SE 2 E 1
2	735.1	734.5	735.1	15.5	24.9	16.7	18.5	25.0	14.2	09.3	12.5	10.0	11.7	95	42	82	73	E	1	ESE 3 NE 1
3	735.2	734.5	735.5	15.1	25.2	16.2	18.2	25.4	13.5	07.0	11.2	10.3	11.7	87	43	84	71	S	1	ESE 3 N 1
4	736.3	735.8	736.9	11.6	25.8	17.7	18.2	26.3	10.9	05.2	09.5	09.9	12.9	93	40	85	73	NNE	1	SE 3 NNE 1
5	738.4	737.8	739.2	14.7	25.2	16.4	18.2	25.9	13.6	10.8	11.6	10.4	12.0	93	43	85	74	ESE	1	E 2 NNE 2
6	741.2	740.0	740.4	11.8	26.1	16.2	17.6	26.8	11.2	04.7	10.0	11.4	12.5	97	45	90	77	ENE	1	SSE 2 E 1
7	740.7	739.3	739.0	12.6	27.4	17.6	18.8	27.4	11.6	05.4	10.9	10.6	13.4	100	39	89	76	ESE	1	S 2 NE 1
8	738.8	736.5	734.7	14.4	26.9	20.4	20.5	27.5	13.8	13.1	11.9	12.8	12.7	97	48	71	72	NE	1	SE 2 SW 2
9	731.9	733.8	739.9	13.3	11.5	09.7	11.1	20.6	05.7	09.3	10.7	09.4	08.4	94	92	93	93	NE	1	NNW 2 ENE 1
10	741.6	740.1	739.8	08.3	19.4	12.8	13.3	20.2	07.5	03.4	07.9	05.2	08.9	96	31	81	69	NE	1	SW 2 W 1
11	739.0	738.8	740.3	11.6	22.9	17.1	17.2	23.4	10.9	08.4	09.1	10.3	11.3	89	49	78	72	NE	1	SW 2 SSE 1
12	740.9	738.4	738.4	12.4	25.9	18.0	18.6	26.9	10.7	07.8	10.6	10.9	11.4	98	44	74	72	-	0	W 2 SW 2
13	737.8	737.9	742.2	11.8	23.1	13.6	15.5	23.6	11.6	07.3	10.0	10.6	10.6	97	50	90	79	NW	1	SE 3 SE 3
14	745.5	744.3	743.3	10.4	17.4	09.1	11.5	17.6	09.1	06.5	06.8	06.3	07.4	72	42	85	66	SSE	2	E 2 E 1
15	740.6	736.1	733.9	05.2	22.3	12.6	13.2	23.9	02.9	01.8	06.3	07.0	07.7	96	34	70	67	E	1	NE 1 ENE 1
16	732.3	731.2	734.2	08.0	20.6	12.0	13.2	20.9	06.6	03.2	07.4	10.1	09.9	92	56	94	81	NNW	1	SE 2 ESE 2
17	734.9	735.1	734.9	06.8	06.2	05.9	06.2	12.0	05.9	05.7	06.9	06.4	06.7	93	90	96	93	ENE	2	SE 3 E 1
18	733.7	734.5	736.5	05.2	06.5	06.0	05.9	06.9	04.5	03.6	06.3	06.9	06.6	96	95	94	95	NNW	1	SW 1 N 1
19	738.2	738.1	738.0	04.3	13.4	10.3	09.6	14.3	03.9	02.2	06.0	06.8	07.0	96	59	74	76	NNW	1	SE 2 ESE 2
20	736.4	735.8	735.5	05.4	08.3	07.2	07.0	10.3	05.4	04.5	06.4	06.5	07.3	96	79	96	90	ENE	1	S 1 NNW 1
21	733.4	733.7	734.6	07.4	14.0	07.8	09.3	15.7	07.0	06.1	07.0	06.3	07.2	91	53	91	78	W	1	NNE 1 ENE 1
22	734.8	734.8	735.7	07.4	15.4	10.2	10.8	16.4	06.4	02.2	07.5	06.7	09.0	97	51	96	81	S	1	NNE 2 NNE 1
23	736.2	735.1	735.6	05.7	14.2	11.1	10.5	14.6	05.2	01.2	06.0	07.0	07.5	99	58	75	77	NE	1	NNE 1 ESE 1
24	736.2	735.8	737.4	09.3	14.5	08.4	10.2	15.6	08.4	07.4	07.9	06.7	07.4	90	54	90	78	NNW	1	SE 1 NNE 1
25	738.1	738.0	740.1	05.6	17.2	09.6	10.5	17.8	04.4	00.0	06.7	07.2	08.2	99	45	91	80	ENE	1	E 2 NW 1
26	741.1	740.6	741.6	07.0	15.8	12.0	11.7	17.2	06.2	01.8	07.4	06.2	08.1	99	46	77	74	S	1	SSE 1 NE 1
27	742.4	743.7	745.1	09.6	13.7	10.2	10.9	14.1	09.4	07.6	08.0	05.9	06.3	89	50	68	69	E	1	E 2 E 2
28	745.7	746.0	746.8	03.4	13.6	04.4	06.5	13.8	02.5	-01.4	05.6	04.7	05.5	95	40	88	74	N	1	ESE 2 ENE 1
29	746.5	744.8	744.3	00.9	14.4	09.7	08.7	15.3	-00.6	-04.5	04.8	05.8	07.7	98	47	86	77	ENE	1	ENE 1 W 1
30	743.2	740.6	738.9	04.7	18.6	12.4	12.0	21.2	03.8	-00.7	06.3	06.4	04.1	99	40	38	59	NE	1	E 1 SSW 3

MES.

VRED. 738.4 737.6 738.4 09.2 18.6 12.4 13.1 19.8 08.2 05.0 08.4 08.3 09.2 94 52 83 76 1.0 1.9 1.3

1977 OKTOBAR	LJUBLJANA-BEŽIGRAD																				
1	736.1	735.5	730.1	05.6	13.0	12.0	10.7	13.8	03.4	-00.6	06.1	09.8	10.0	90	87	95	91	E	1	NNW 1 E 1	
2	731.4	732.7	733.2	09.2	06.8	05.0	06.5	12.5	05.0	08.5	07.3	05.7	05.1	84	77	79	80	SE	2	ESE 3 SSE 1	
3	733.1	734.4	736.3	02.2	17.2	05.2	17.8	01.0	02.8	05.1	04.9	06.1	95	34	91	73	E	2	SE 1 NNE 1		
4	740.1	738.2	737.9	02.2	17.1	08.6	09.1	17.7	00.4	-03.9	05.3	06.6	06.8	98	45	81	75	ENE	1	W 3 W 2	
5	737.9	737.3	737.1	04.6	16.9	12.9	11.8	18.4	04.3	00.0	05.9	08.1	05.0	93	56	81	77	N	1	NNW 2 W 1	
6	734.7	734.0	733.9	13.8	18.4	16.0	16.1	19.7	12.7	07.7	10.1	10.7	10.6	85	67	78	77	NNE	1	SSW 3 MNN 2	
7	732.4	732.0	732.1	15.8	19.5	16.5	17.1	19.7	15.0	13.5	11.5	11.5	10.7	85	68	76	76	W	2	SM 3 WSW 3	
8	731.5	730.3	730.3	14.9	22.4	13.4	16.0	22.4	13.4	08.8	10.7	10.3	10.7	84	51	92	76	WSW	1	NW 2 SSW 2	
9	729.8	729.2	730.1	09.4	20.2	15.8	15.3	21.2	09.2	05.0	08.6	09.9	11.3	98	56	84	79	E	1	S 1 E 1	
10	729.9	729.8	731.6	12.8	20.2	13.6	15.1	21.0	12.7	10.5	10.5	11.0	11.2	95	62	96	84	E	1	NE 1 NE 1	
11	731.7	733.6	736.6	13.1	14.2	11.6	12.6	14.7	11.3	12.1	10.9	08.9	09.7	97	74	94	88	E	1	- 0 S 1	
12	737.3	738.0	739.4	10.8	15.1	12.4	12.7	15.4	10.3	09.1	09.4	09.0	05.8	96	70	91	86	NE	1	SW 2 -	
13	739.6	739.2	740.1	11.4	17.8	13.6	14.1	18.8	11.2	09.4	09.4	10.3	10.7	93	68	91	84	N	1	S 2 NNE 1	
14	739.4	738.7	739.0	09.4	14.7	13.4	12.7	16.0	09.0	04.3	08.6	09.9	10.5	98	56	89	89	E	1	NE 1 NNE 1	
15	736.1	738.4	739.6	11.9	15.4	12.2	12.9	15.6	11.8	10.7	10.1	08.8	06.9	97	67	84	83	E	1	ENE 1 ENE 1	
16	740.6	740.0	740.7	10.4	14.7	08.4	10.5	15.4	06.4	06.4	08.5	06.9	07.3	89	55	89	78	NNW	1	SSE 1 E 1	
17	741.1	740.1	740.9	03.9	15.7	06.4	08.1	16.4	03.7	-04.4	06.0	06.6	06.7	98	49	93	80	-	0	SE 1 N 1	
18	741.6	741.0	741.7	03.3	14.4	11.0	09.9	17.6	02.1	-00.2	05.7	06.8	07.8	98	55	80	78	E	1	SW 2	
19	741.7	741.1	742.1	03.2	16.7	10.7	10.3	16.9	03.0	-01.8	05.6	07.2	07.7	97	51	79	76	E	1	SW 4 SW 3	
20	742.8	741.8	742.4	02.2	18.6	09.0	09.7	18.7	02.1	-01.1	05.3	07.5	07.9	98	46	91	78	E	1	SW 1 -	
21	742.3	741.2	742.1	04.0	15.3	07.4	08.5	16.0	03.4	-01.3	06.1	07.7	07.3	100	55	95	85	E	1	E 1 NNW 1	
22	741.6	740.8	741.7	06.9	16.9	14.9	13.4	17.3	06.1	-00.4	07.1	09.8	09.9	95	68	78	80	NNW	1	S 2 W 3	
23	741.6	741.9	743.3	12.6	16.7	11.0	12.8	17.0	11.0	05.8	08.4	08.5	08.3	76	60	84	73	W	3	SW 2 SW 1	
24	744.1	743.8	743.2	05.6	16.2																

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

MES. 08-0 05-5 04-6 06-0 120-3 87-1

LJUBLJANA-BEŽIGRAD

1977 OKTOBER

PES. 07.7 05.4 04.9 06.0 58.5 41.1  
RED.

$\varphi = 46^{\circ}04' N$   $\lambda = 14^{\circ}31' E$  Gr.  $\Delta G = + 58$  min.

BR. ST. 13

Dan	Vzdušni pritisak P mm			Temperatura vazduha T °C							Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	732.7	732.1	734.8	07.0	09.6	08.8	08.6	09.9	06.8	02.2	07.4	08.4	08.2	95	94	96	96	NE	1	WSW	1	S	2
2	736.4	735.4	734.9	07.4	12.6	06.7	08.4	12.9	06.7	05.0	07.5	06.7	06.9	97	61	93	84	NE	1	ENE	1	NW	1
3	733.7	734.1	734.6	04.0	13.7	12.9	10.9	14.8	03.8	-00.2	05.7	08.3	07.9	94	70	71	78	ESE	1	WSW	3	W	2
4	733.5	732.9	734.1	11.9	15.2	14.8	14.2	15.4	11.7	09.7	09.2	10.8	11.1	88	82	88	66	NNW	1	W	2	W	2
5	735.3	737.3	738.1	12.5	12.7	10.9	11.8	15.3	10.8	08.5	09.7	10.4	09.0	89	94	92	92	NNE	1	E	2	-	0
6	736.9	735.9	737.4	10.4	14.6	10.4	11.5	14.8	09.4	09.0	09.1	09.9	09.0	96	80	95	90	-	0	SW	1	E	1
7	739.8	740.4	742.0	07.7	10.6	08.9	09.0	10.7	07.2	03.9	07.8	08.7	08.4	99	91	95	96	NNE	1	SSW	1	NW	1
8	742.6	742.4	742.6	07.2	10.1	08.0	08.3	11.0	06.7	06.7	07.4	07.0	07.7	97	75	96	89	E	1	NE	1	ENE	1
9	743.6	742.3	741.3	05.7	07.6	06.8	06.7	08.8	05.4	05.1	06.7	07.4	07.2	97	95	97	96	ENE	1	ENE	1	E	1
10	740.0	740.4	741.8	05.0	10.6	07.7	07.8	11.6	04.4	03.3	06.4	08.0	07.6	95	84	94	53	E	1	E	1	E	1
11	742.0	739.7	740.1	04.7	13.7	06.7	08.0	16.6	04.6	-00.8	06.4	07.4	06.8	100	63	92	85	NE	1	ESE	1	NNE	1
12	738.2	735.4	732.0	03.2	12.2	11.7	09.7	12.7	01.8	-03.2	05.6	07.7	08.2	97	72	80	83	WSW	3	WSW	3	W	3
13	728.7	725.2	727.1	13.5	09.2	02.4	06.9	14.6	02.0	06.7	08.6	08.1	05.2	74	93	95	87	WNW	2	NW	2	S	1
14	728.8	728.2	725.6	01.4	02.5	01.1	01.5	03.2	00.4	-01.0	05.0	05.3	04.9	98	57	68	98	ESE	1	S	2	SSW	2
15	720.6	721.0	721.3	05.7	07.3	06.4	06.5	07.7	00.8	-00.9	06.1	07.5	06.6	89	97	92	93	NW	2	SE	1	NW	1
16	718.4	719.5	721.0	05.9	06.0	04.6	05.3	07.6	04.0	04.9	06.9	06.3	05.7	96	50	60	93	NE	1	S	2	SE	1
17	722.1	721.1	722.2	00.5	05.3	02.7	02.8	05.9	00.2	-04.5	04.8	05.4	05.4	100	80	97	92	SE	1	S	2	NW	2
18	726.7	728.8	731.6	01.9	06.2	00.2	02.1	06.6	00.2	-02.5	04.9	04.9	04.4	93	69	95	86	WNW	1	S	1	S	1
19	734.3	735.7	736.1	-00.6	02.9	-01.6	-00.2	03.6	-01.6	-07.1	04.2	04.3	04.1	96	71	100	91	ENE	1	ENE	1	E	1
20	737.1	733.9	732.2	-02.7	-01.0	-02.4	-02.1	00.0	-03.6	-03.8	03.7	04.1	03.8	99	97	98	98	ENE	2	S	1	WNW	1
21	729.4	727.0	721.5	-03.0	09.6	04.7	04.0	11.0	-04.4	-03.6	03.6	04.3	06.2	99	48	97	81	ENE	1	SW	2	NW	3
22	721.6	724.6	728.6	07.7	11.1	01.7	05.6	11.5	01.6	01.6	05.9	04.7	04.5	74	47	87	69	SSW	2	WNW	3	W	1
23	731.2	733.4	736.0	01.5	08.6	06.1	06.6	08.8	00.1	-06.1	04.6	04.8	00.4	90	58	05	51	NW	1	S	2	NW	1
24	736.2	733.1	730.9	-01.7	-00.2	03.0	01.0	05.3	-03.0	-06.8	04.0	04.4	04.4	98	76	78	91	ESE	2	ENE	1	N	1
25	728.8	727.6	728.1	00.4	04.0	04.2	03.2	06.0	-01.7	-07.4	04.6	05.2	04.7	96	85	76	86	ENE	1	NW	2	E	3
26	723.5	721.0	721.5	02.0	02.5	01.6	01.9	04.4	01.4	00.0	04.4	04.9	04.6	84	89	90	88	E	3	NW	1	SSW	2
27	723.6	726.7	731.0	01.7	06.2	01.0	02.5	06.6	01.0	-00.8	03.8	02.7	04.0	74	38	81	64	SW	2	WNW	3	SW	2
28	734.7	735.8	737.7	-02.0	04.8	01.7	01.6	05.2	-02.7	-06.8	03.7	03.8	04.0	94	59	77	77	NNE	1	SSE	1	ESE	2
29	739.4	738.3	737.7	-00.4	03.0	-01.0	00.2	03.4	-01.5	-01.7	02.9	02.0	02.9	65	36	65	57	ENE	2	E	2	SE	1
30	733.5	731.2	732.1	-01.0	-00.1	-00.2	-00.4	00.6	-01.4	-02.9	03.3	03.4	04.0	77	75	89	80	N	1	SSW	2	E	1
MES.	VRED.	732.4	732.0	732.6	03.9	07.7	05.1	05.5	08.9	02.4	00.2	05.8	06.2	05.9	92	76	87	85	1.3	1.6	1.4		

1	732.5	732.1	732.7	-00.4	01.1	-06.6	-00.1	01.5	-00.6	-11.4	04.3	03.5	03.8	96	71	87	85	ENE	1	SSE	2	S	1
2	733.0	733.5	736.5	-01.4	03.6	-01.3	-00.1	04.2	-01.9	-04.3	03.8	02.9	03.4	93	48	80	74	W	2	ENE	2	SW	2
3	739.4	741.0	744.1	-04.9	01.4	00.0	-00.4	02.0	-05.2	-08.0	02.8	03.1	03.7	87	80	86	76	SSW	2	S	1	W	2
4	746.0	744.7	744.1	-01.6	03.7	-03.6	-01.0	03.7	-03.0	-06.0	03.7	03.4	02.2	91	57	87	78	SSE	1	SSW	2	ESE	1
5	741.1	737.0	734.5	-06.2	-00.8	-06.1	-04.8	00.5	-06.9	-09.4	02.9	03.3	02.7	99	76	94	90	NNE	1	S	1	ENE	1
6	730.3	726.9	725.4	-06.1	-01.0	01.3	-01.1	01.7	-08.4	-09.4	02.9	04.0	04.9	100	97	57	98	NNE	1	E	1	WNW	1
7	728.1	732.0	734.9	00.6	03.9	02.4	02.3	04.2	00.2	01.3	04.7	05.2	05.0	98	86	92	92	S	1	SE	1	SSW	1
8	734.7	733.7	732.9	00.8	01.5	01.6	01.4	03.0	00.5	02.2	04.9	04.9	05.1	100	97	98	98	WNW	1	S	1	NNE	1
9	731.2	731.0	732.0	01.6	03.0	02.3	02.3	03.1	01.3	01.2	05.1	05.4	05.2	98	55	97	97	W	1	S	1	ESE	1
10	733.8	735.7	739.3	01.4	02.0	02.0	01.9	03.2	01.1	01.7	04.9	05.1	04.9	97	97	93	96	S	2	WNW	1	SE	1
11	743.0	745.8	747.7	01.3	01.2	-00.6	00.3	02.4	-00.6	-02.0	04.5	03.9	03.5	90	78	80	82	SE	2	SSE	2	SE	2
12	748.6	748.5	748.8	-01.4	-01.5	-03.0	-02.2	-00.1	-03.0	-00.6	03.2	03.1	02.8	79	75	76	77	E	1	S	2	SSE	2
13	747.0	746.6	747.3	-04.4	-02.9	-04.0	-03.8	-02.7	-04.4	-03.0	02.5	02.6	02.6	75	73	76	74	S	2	-	0	SSE	2
14	747.5	747.2	745.9	-03.7	00.3	-00.2	-01.0	00.2	-04.3	-04.7	02.7	03.1	03.3	76	68	74	73	E	2	S	1	WNW	1
15	744.9	744.1	745.1	-00.2	02.8	01.8	01.6	03.0	-00.6	-01.6	04.2	04.4	04.4	93	78	63	85	E	1	SSE	1	E	1
16	748.3	748.8	748.5	02.2	04.5	-01.4	01.0	05.1	-01.4	-00.6	04.9	04.8	04.6	92	75	96	88	WNW	1	WNW	1	E	1
17	747.3	747.0	747.2	-02.4	-01.0	-01.0	-01.4	-00.4	-02.6	-05.1	03.8	04.1	03.6	98	97	85	93	ENE	1	ENE	1	S	2
18	745.5	744.2	744.0	-02.1	-01.6	-03.1	-02.5	-00.8	-03.6	-02.3	03.3	03.4	03.3	83	84	91	86	SSW	1	ESE	1	E	1
19	742.6	742.6	743.6	-04.3	-04.1	-04.6	-04.4	-02.6	-04.9	-06.2	03.3	03.0	03.0	98	90	93	94	E	1	ESE	2	NNE	1
20	743.0	743.2	744.3	-05.4	-04.6	-																	

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrhnost 0-9	Občutnost N (0-10)					Insolacije broj sati	Padavine R mm	Snožni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	5	10≡	10*	10*	10.6	00.0	.	Δ <sup>2</sup> 0-9 <sup>30</sup> ; = 0-02, 9 <sup>30</sup> 24; = 0-02, 10 <sup>5</sup> ; = 0-10 <sup>5</sup> 9 <sup>30</sup> ; 0-10 <sup>5</sup> 21 <sup>30</sup>		
2	7	07	09○	00	05.3	01.0	24.6	= 0-11 <sup>30</sup> ; Δ <sup>2</sup> 0-9 <sup>30</sup> ; = 0-02, 10 <sup>5</sup> ; Δ <sup>2</sup> 10 <sup>5</sup> 24, ○		
3	7	08	07	10	06.3	02.6	.	Δ <sup>2</sup> 0-11 <sup>30</sup> ; Δ <sup>2</sup> 0-11 <sup>30</sup> , ○		
4	7	10*	10	09	09.7	00.0	00.1	0-10 <sup>5</sup> 4 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> ; 10 <sup>5</sup> 10 <sup>5</sup> 24		
5	7	10	10*	10*	10.6	00.0	00.2	0-10 <sup>5</sup> 4 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> ; 10 <sup>5</sup> 10 <sup>5</sup> 24; 0-10 <sup>5</sup> 21 <sup>30</sup>		
6	6	10	08	05≡	07.7	00.2	05.3	0-10 <sup>5</sup> 5 <sup>30</sup> ; = 0-11 <sup>30</sup> ; 19-20 <sup>50</sup> ; Δ <sup>2</sup> 0-17 <sup>30</sup> 24; = 0-10 <sup>5</sup> 21 <sup>30</sup> ; = 0-10 <sup>5</sup> 24, ○		
7	3	10≡	05○	10≡	05.7	00.0	.	Δ <sup>2</sup> 0-13 <sup>30</sup> ; = 0-10 <sup>5</sup> 10 <sup>5</sup> 24; = 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-13 <sup>30</sup> 24, ○		
8	6	10≡	04○	10	08.0	01.8	00.2	= 0-10 <sup>5</sup> 6 <sup>30</sup> 11 <sup>30</sup> 23 <sup>30</sup> 24; Δ <sup>2</sup> 0-17 <sup>30</sup> 24, ○		
9	3	10≡	10≡	10≡	10.6	00.0	00.0	Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> ; 10 <sup>5</sup> 10 <sup>5</sup> 24; Δ <sup>2</sup> 0-13 <sup>30</sup> 13 <sup>30</sup> , ○		
10	6	10	10○	09≡	09.7	00.2	00.1	0-10 <sup>5</sup> 24; = 0-10 <sup>5</sup> 5 <sup>30</sup> ; = 0-10 <sup>5</sup> 10 <sup>5</sup> 24; Δ <sup>2</sup> 0-13 <sup>30</sup> 24; Δ <sup>2</sup> 0-16 <sup>30</sup> , ○		
11	7	10≡	00○	00	03.3	04.9	00.0	0-10 <sup>5</sup> 17 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> ; = 0-10 <sup>5</sup> 11 <sup>30</sup> ; = 0-10 <sup>5</sup> 13 <sup>30</sup> 24; Δ <sup>2</sup> 0-13 <sup>30</sup> 16 <sup>30</sup> , ○		
12	7	05	10*	10*	08.3	00.0	.	Δ <sup>2</sup> 0-2 <sup>30</sup> ; = 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> , ○		
13	7	07	10*	10*	05.0	00.0	00.0	0-10 <sup>5</sup> 13 <sup>30</sup> 11 <sup>30</sup> 17 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> ; Δ <sup>2</sup> 0-17 <sup>30</sup> 24, ○		
14	3	10	10≡	10≡	10.0	00.0	45.2	0-10 <sup>5</sup> 24; = 0-10 <sup>5</sup> 13 <sup>30</sup> ; 10 <sup>5</sup> 10 <sup>5</sup> 24; Δ <sup>2</sup> 0-13 <sup>30</sup> 13 <sup>30</sup> , ○	04	
15	5	08	10	10*	09.3	00.0	.	= 0-5, 23 <sup>30</sup> 24; = 0-5, 6 <sup>30</sup> 9 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> 24; Δ <sup>2</sup> 0-13 <sup>30</sup> 13 <sup>30</sup> , ○		
16	7	10	10*	09	09.7	00.0	07.2	0-10 <sup>5</sup> 17 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> ; = 0-10 <sup>5</sup> 11 <sup>30</sup> ; = 0-10 <sup>5</sup> 13 <sup>30</sup> 24; Δ <sup>2</sup> 0-13 <sup>30</sup> 16 <sup>30</sup> , ○		
17	6	10	09○	10	09.7	01.0	01.6	0-10 <sup>5</sup> 24; = 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> , ○		
18	6	10	01○	00	03.7	04.2	00.3	= 0-10 <sup>5</sup> 13 <sup>30</sup> 11 <sup>30</sup> 17 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> ; Δ <sup>2</sup> 0-17 <sup>30</sup> 24, ○		
19	6	10	00○	10≡	06.7	02.8	.	= 0-10 <sup>5</sup> 13 <sup>30</sup> 11 <sup>30</sup> 17 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> ; Δ <sup>2</sup> 0-17 <sup>30</sup> 24, ○		
20	3	10≡	10≡	10≡	10.0	00.0	.	= 0-10 <sup>5</sup> 12 <sup>30</sup> 24; = 0-10 <sup>5</sup> 11 <sup>30</sup> 24; = 0-10 <sup>5</sup> 10 <sup>5</sup> 24, ○		
21	8	10≡	06○	10*	08.7	03.4	.	Δ <sup>2</sup> 0-10 <sup>5</sup> 17 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> ; = 0-10 <sup>5</sup> 11 <sup>30</sup> ; = 0-10 <sup>5</sup> 13 <sup>30</sup> 24, ○		
22	8	10*	02○	00	04.0	06.8	22.8	0-10 <sup>5</sup> 24; = 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> , ○		
23	7	07	02○	00	03.0	06.5	00.1	= 0-10 <sup>5</sup> 20 <sup>30</sup> 24; = 0-10 <sup>5</sup> 17 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> , ○		
24	2	10≡	07○	09≡	08.7	00.4	.	= 0-10 <sup>5</sup> 15 <sup>30</sup> 24; = 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 23 <sup>30</sup> ; Δ <sup>2</sup> 0-17 <sup>30</sup> 24, ○		
25	7	09	10*	10*	09.7	00.8	.	= 0-10 <sup>5</sup> 13 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> 24; = 0-10 <sup>5</sup> 11 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> 24, ○		
26	6	10	10*	10	10.0	00.0	04.1	0-10 <sup>5</sup> 12 <sup>30</sup> 15 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 10 <sup>35</sup> ; = 0-10 <sup>5</sup> 8 <sup>35</sup> ; = 0-10 <sup>5</sup> 12 <sup>30</sup>		
27	8	10	10	02	07.3	00.0	00.6	0-10 <sup>5</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> , ○		
28	8	09	07○	10	08.7	03.0	.	= 0-10 <sup>5</sup> 10 <sup>35</sup> 24; = 0-10 <sup>5</sup> 9 <sup>35</sup> 24; = 0-10 <sup>5</sup> 8 <sup>35</sup> 24, ○		
29	8	09	02○	08	06.3	07.0	.	= 0-10 <sup>5</sup> 10 <sup>35</sup> 24; = 0-10 <sup>5</sup> 9 <sup>35</sup> 24; = 0-10 <sup>5</sup> 8 <sup>35</sup> 24, ○		
30	6	10	10*	10	10.0	00.0	.	= 0-10 <sup>5</sup> 13 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> 24, ○		
MES. RED.			09.3	07.4	07.7	08.2	46.6	113.0		

1	7	10	09	10	05.7	00.0	00.3	.	= 0-13 <sup>30</sup> 16 <sup>30</sup> 24; Δ <sup>2</sup> 0-15 <sup>30</sup> 15 <sup>45</sup>		
2	7	10	09○	00	06.3	01.0	00.0	.	= 0-12 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , 15 <sup>45</sup> 24; ○		
3	7	01	09○	10	06.7	02.1	.	Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○			
4	7	00	02○	00	00.7	06.1	.	= 0-12 <sup>30</sup> 16 <sup>30</sup> 24; = 0-10 <sup>5</sup> 10 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 24, ○			
5	6	01≡	01○	00	00.7	03.5	.	= 0-12 <sup>30</sup> 13 <sup>30</sup> 24; = 0-5 <sup>15</sup> , 10 <sup>30</sup> 15 <sup>45</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 24, ○			
6	3	09	10≡*	10≡	09.7	00.0	.	0-9 <sup>30</sup> ; = 0-8, = 0-8-24, Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> ; = 0-10 <sup>5</sup> 11 <sup>30</sup> 12 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 12 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 12 <sup>30</sup> , ○			
7	5	10*	09	10	05.7	00.0	15.1	01	= 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 12 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 12 <sup>30</sup> , ○		
8	4	10	10*	10	10.0	00.0	01.0	.	= 0-24; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○		
9	4	10*	10	10*	10.0	00.0	05.0	.	= 0-24; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 14 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 12 <sup>30</sup> , ○		
10	5	10*	10	10*	10.0	00.0	07.1	.	= 0-24; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 24, ○		
11	7	10*	10	10	10.0	00.0	01.1	.	= 0-10 <sup>5</sup> 15 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 24, ○		
12	7	10	09	10	09.7	00.0	00.0	.	= 0-10 <sup>5</sup> 13 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 24, ○		
13	7	10	10	10	10.0	00.0	.	= 0-10 <sup>5</sup> 13 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 24, ○			
14	5	10	10	10	10.0	00.0	.	= 0-10 <sup>5</sup> 13 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 24, ○			
15	6	10	09	10	09.7	01.1	.	= 0-10 <sup>5</sup> 13 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 24, ○			
16	6	10	06○	00	05.3	01.0	00.0	.	= 0-14 <sup>30</sup> 17 <sup>30</sup> 24; = 0-10 <sup>5</sup> 13 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 19 <sup>30</sup> 24, ○		
17	2	10≡	10≡	10	10.0	00.0	.	= 0-10 <sup>5</sup> 16 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 15 <sup>30</sup> ; = 0-10 <sup>5</sup> 16 <sup>30</sup> , ○			
18	6	10	09	10	05.7	04.0	.	= 0-24; Δ <sup>2</sup> 0-10 <sup>5</sup> 16 <sup>30</sup> 24; ○			
19	5	10	10	10	10.0	00.0	.	= 0-10 <sup>5</sup> 16 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 15 <sup>30</sup> ; = 0-10 <sup>5</sup> 10 <sup>45</sup> i, Δ <sup>2</sup> 0-10 <sup>5</sup> 12 <sup>30</sup> 24, ○			
20	4	10	10	10	10.0	00.0	01.6	.	= 0-24; Δ <sup>2</sup> 0-10 <sup>5</sup> 16 <sup>30</sup> 24; = 0-10 <sup>5</sup> 12 <sup>30</sup> 24; Δ <sup>2</sup> 0-10 <sup>5</sup> 11 <sup>30</sup> 24, ○		
21	3	10	10≡	10	10.0	00.0	00.0	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○		
22	6	10	10	10	10.0	00.0	00.0	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○		
23	6	10	05○	10	08.3	00.5	00.0	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○		
24	6	08	09○	10	05.0	04.0	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○			
25	6	10	02○	01	04.3	03.1	01.6	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○		
26	5	04	04○	01	03.0	03.2	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○			
27	5	10≡	04○	10○	08.0	02.2	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○			
28	5	10*	10*	10	10.0	00.0	15.6	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10 <sup>5</sup> 13 <sup>30</sup> , ○		
29	4	10≡	09○	10	05.7	00.1	25.2	.	= 0-10 <sup>5</sup> 19 <sup>30</sup> 24; = 0-10 <sup>5</sup> 16 <sup>30</sup> ; Δ <sup>2</sup> 0-10<sup		

$\varphi = 45^{\circ}49' N$   $\lambda = 15^{\circ}59' E$  Gr.  $\Delta G = +1h\ 04\ min.$ 

BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodené pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	748.8	748.0	748.2	-01.9	04.9	04.0	02.8	05.4	-05.8	-	03.3	04.5	05.1	82	70	84	79	ENE 1	WSW 2	WSW 1			
2	748.3	749.0	752.0	02.0	03.0	02.6	02.6	04.0	01.8	-	04.3	04.8	05.1	82	84	92	86	ENE 1	ENE 2	ENE 1			
3	755.3	756.2	757.3	01.9	02.0	01.5	01.7	02.9	01.5	-	05.2	05.1	04.8	98	96	93	96	ENE 1	ENE 1	NE 1			
4	759.4	761.3	763.6	01.1	00.4	00.2	00.5	01.5	00.2	-	04.0	04.4	03.8	97	93	82	91	ENE 2	ENE 2	NE 2			
5	763.6	764.0	763.8	-00.1	00.0	-00.3	-00.2	00.2	-00.9	-	03.9	03.9	04.0	85	86	90	87	ENE 2	ENE 1	- 0			
6	762.1	760.9	760.0	00.3	01.5	01.5	01.2	01.9	-00.3	-	04.4	04.7	04.6	93	92	90	92	NE 1	SSE 1	NE 1			
7	759.3	758.1	757.6	01.1	00.3	00.0	00.4	01.8	-00.4	-	04.5	04.6	04.4	91	98	96	95	ENE 1	ENE 1	SE 1			
8	755.6	755.6	752.7	-00.3	01.5	00.3	00.5	01.9	-00.8	-	04.3	04.2	04.2	96	81	90	89	ENE 1	SE 2	WSW 1			
9	752.6	750.8	748.9	-00.3	01.8	00.3	00.5	02.1	-01.6	-	04.0	02.6	03.4	89	50	72	70	ESE 2	SSE 1	NNE 1			
10	744.4	742.1	741.8	-00.1	03.7	05.2	03.5	05.3	-00.4	-	03.5	04.2	05.2	77	71	79	76	ENE 1	WSW 2	WSW 1			
11	740.4	738.6	737.8	05.1	08.0	09.3	07.9	09.3	04.9	-	05.1	05.8	05.6	77	72	64	71	E 1	E 1	ENE 2			
12	733.0	735.0	736.7	07.5	08.0	06.2	07.0	08.5	05.6	-	05.8	07.2	05.5	74	89	77	80	ENE 2	ENE 2	NNE 1			
13	736.7	739.9	743.2	02.5	02.0	01.5	01.9	06.6	00.8	-	04.6	05.0	04.8	84	95	95	91	ENE 3	SSW 2	W 1			
14	744.3	743.9	743.6	00.4	01.2	04.3	02.6	04.4	-00.4	-	04.6	04.8	04.7	98	96	75	90	SSW 1	WSW 2	ENE 1			
15	740.9	740.1	743.5	04.1	04.2	02.3	03.2	04.9	02.3	-	04.4	05.6	04.4	72	89	83	81	NE 3	NNW 1	ENE 1			
16	745.4	746.0	747.8	01.1	02.1	00.5	01.1	02.4	00.0	-	04.5	05.1	04.6	91	94	96	94	WNW 1	SSE 1	S 1			
17	749.5	749.9	751.0	00.3	04.7	02.8	02.7	04.8	-00.4	-	04.2	03.2	03.4	89	42	62	67	S 1	N 3	ENE 1			
18	751.4	751.4	751.8	01.9	02.3	-00.9	00.6	02.9	-00.9	-	03.6	03.4	03.2	68	64	74	69	NNE 3	NE 3	ENE 1			
19	751.0	750.2	748.9	-03.9	-01.1	-01.8	-02.2	-00.2	-00.9	-	03.0	03.3	02.9	86	78	71	78	SE 1	S 1	WSW 2			
20	748.3	746.3	748.3	-01.7	00.7	-00.2	-00.1	-00.4	01.0	-03.1	-	03.1	03.9	04.2	77	83	92	84	SSW 1	ESE 1	NW 1		
21	747.7	748.5	750.7	00.7	04.1	01.8	02.1	04.4	-00.1	-	04.4	04.9	04.4	91	79	84	85	N 1	SE 1	NE 1			
22	750.5	749.3	748.8	00.9	04.3	04.8	03.7	05.5	00.4	-	04.2	05.0	05.3	86	80	82	83	ENE 1	S 1	W 2			
23	747.6	746.3	745.2	06.1	12.1	09.4	09.3	12.7	04.7	-	04.9	06.6	07.0	69	63	80	71	W 2	WSW 3	WW 2			
24	743.9	744.1	746.8	06.1	09.1	03.3	05.5	09.9	03.3	-	05.9	06.7	05.2	84	77	90	84	NE 1	E 1	ENE 1			
25	747.7	745.5	749.9	02.8	05.2	04.5	04.3	05.2	02.1	-	05.4	06.0	06.0	97	89	95	94	ENE 1	SSW 1	SSW 1			
26	742.4	740.4	739.9	07.9	11.6	10.2	10.0	12.1	04.4	-	06.1	06.8	06.9	76	66	74	72	W 3	SW 4	W 2			
27	739.3	742.6	743.4	08.4	05.9	05.4	06.3	10.2	05.4	-	07.7	06.6	06.0	94	96	90	93	NE 2	WSW 2	WSW 2			
28	746.3	746.1	744.4	00.3	02.5	01.9	01.7	05.4	00.2	-	04.5	05.3	05.0	96	96	97	96	WSW 1	SE 1	SE 1			
29	737.7	732.3	733.7	04.2	08.0	05.2	05.7	08.2	01.6	-	06.0	06.8	06.3	97	84	95	92	ENE 1	E 1	WSW 2			
30	739.4	741.9	744.1	05.4	11.8	07.8	08.2	11.9	05.2	-	05.2	05.6	06.1	77	54	77	69	WSW 2	W 2	ENE 1			
31	746.7	746.2	744.9	04.4	04.5	04.2	04.3	07.8	04.1	-	05.5	05.8	05.5	88	91	88	89	NE 2	NE 2	NNE 2			
MES.	VRED.			747.8	747.5	747.9	02.2	04.2	03.2	03.2	05.3	01.0	-	04.7	05.0	04.9	86	81	84	84	1.5	1.6	1.3

## 1977 FEBRUAR

## ZAGREB-GRIC

1	742.6	744.4	745.7	01.6	01.2	01.0	01.2	04.3	00.3	-	04.5	04.6	03.6	87	92	73	84	N 3	S 2	E 2
2	746.4	747.7	748.9	-01.6	00.1	-01.9	-01.3	01.0	-01.9	-	02.7	02.8	03.0	67	62	75	68	NNE 2	SSW 2	WW 2
3	751.3	750.3	750.1	-04.9	00.1	-02.8	-02.6	00.5	-04.9	-	02.7	03.2	03.1	84	70	83	79	W 1	SSW 2	N 1
4	749.9	751.0	751.1	-04.4	-01.6	-01.5	-02.3	-00.4	-05.2	-	03.0	03.2	03.3	92	78	80	83	ESE 1	SSW 1	S 1
5	749.9	749.7	750.1	-02.5	02.4	01.5	00.7	02.8	-02.6	-	03.3	03.9	04.2	85	72	81	79	WSW 1	SW 1	NE 1
6	748.5	747.0	747.1	01.3	02.8	01.2	01.6	03.3	00.9	-	04.3	05.5	04.7	85	98	94	92	W 1	SW 1	ENE 1
7	750.0	749.9	749.1	01.0	04.5	02.0	02.4	04.6	00.8	-	04.8	06.2	05.1	98	97	96	97	WSW 1	ESE 1	SE 1
8	746.0	743.4	742.5	01.0	10.0	09.3	07.4	11.0	-00.6	-	04.8	06.6	05.4	98	72	62	77	SW 1	SE 3	WWN 1
9	743.4	744.0	743.8	06.6	11.3	08.5	08.7	11.4	05.8	-	06.1	06.4	06.3	84	64	76	75	WWN 1	ESE 1	ENE 1
10	741.6	737.3	734.6	07.2	12.9	12.4	11.2	13.3	07.1	-	07.1	07.2	07.2	93	65	67	75	E 1	WSW 3	WW 2
11	735.4	734.3	736.8	11.2	14.7	10.6	11.8	15.0	0.95	-	06.3	05.4	06.3	64	43	66	58	NW 2	SW 3	WW 2
12	732.0	731.5	735.3	08.2	13.3	09.1	09.9	13.4	0.81	-	07.1	07.4	06.3	87	64	72	74	NNE 1	WSW 2	WW 2
13	741.7	743.9	745.3	07.8	13.4	05.2	09.9	13.8	0.71	-	06.1	05.6	04.8	77	49	55	60	NW 2	WWN 2	ENE 3
14	743.2	741.3	742.0	07.1	07.6	05.2	06.3	09.2	0.52	-	05.5	05.7	05.4	73	72	81	75	ESE 2	ENE 2	S 1
15	742.1	742.0	742.8	03.5	08.6	05.2	05.6	09.0	0.94	-	05.0	06.3	05.6	85	74	84	81	W 1	S 1	0
16	744.0	744.0	745.1	02.3	07.7	04.9	05.0	08.6	01.7	-	04.9	05.4	05.4	90	68	84	81	NE 1	SSE 2	ENE 1
17	747.6	748.8	749.4	03.3	07.7	04.9	05.2	08.6	02.2	-	05.4	04.9	05.1	94	62	79	78	NNE 1	WSW 2	NW 1
18	749.9	749.3	751.0	01.7	12.0	07.4	07.1	12.3	0.17	-	04.4	05.4	05.7	85	51	74	70	WWN 1	WSW 4	WSW 2
19	750.5	748.3	748.0	08.5	14.4	10.3	10.9	14.4	0.69	-	06.2	07.0	06.8	74	57	72	68	WSW 2	WSW 4	W 3
20	747.3	745.6	743.8	09.6	14.9	12.1	12.2	15.3	0.91	-	07.1	07.2	06.2	80	56	58	65	WWN 2	WWN 5	WSW 3
21	739.6	737.5	739.6	12.5	14.9	11.4	12.6	15.5	11.4	-	06.2	07.2	08.3	57	56	82	65	SSW 2	SSW 4	W 2
22	744.2	745.2	743.1	09.4	13.3	10.1	10.7	13.7	0.89	-	07.1	07.6	08.6	81	67	92	80	ENE 1	E 2	NNE 2
23	740.5	746.6	751.2	11.5	15.2	10.3	11.8	15.4	10.1	-	07.4</td									

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vrijeme O- G-	Oblačnost N (0-10)					Precip. mm	Padavine R mm	Snožni pokriven h cm	Rezervi vremena w	
		14	7	14	21	Sred Dies				7	7
1	5 10	06○	10	06.7	02.2	.	11	= n-n, [x]			
2	5 10*	10	10*	10.0	00.0	00.8	08	= n-n, [x]	n-12, 18-n; [x]		
3	6 10*	10	10*	10.0	00.0	22.4	04	[x] n-H <sup>10</sup> , 15-n;	= n-n, = 8-10 <sup>20</sup> , [x]		
4	5 10*	10*	10	10.0	00.0	09.4	02	= n-n, [x] n-pj, B <sup>10</sup> , 19 <sup>20</sup> ; [x]			
5	6 10	10	10*	10.0	00.0	01.4	02	[x] n-n, [x] n-pj, 16 <sup>20</sup> ; [x]			
6	4 10	10=	10	10.0	00.0	01.8	.	~ n-dn = n-n, = 8-14 <sup>45</sup>			
7	3 10	10=	10	10.0	00.0	.	.	= n-H <sup>10</sup> , 14 <sup>20</sup> ; [x] = 8-14 <sup>45</sup> , [x] 13 <sup>20</sup> , 15 <sup>20</sup>			
8	5 10	09○	00	06.3	01.1	00.2	.	= n-H <sup>10</sup> , 14 <sup>20</sup> ; [x] = 7-14 <sup>45</sup>			
9	7 10	09	07	08.7	01.1	.	.	= n-H <sup>10</sup> , 17 <sup>15</sup> , [x]			
10	5 10*	08○	10	09.3	03.1	00.0	.	= n-n, [x] 6 <sup>20</sup> -8 <sup>20</sup>			
11	5 08	10	08	08.7	00.1	00.1	.	= n-n, [x] 9 <sup>20</sup> , H <sup>10</sup> , 15 <sup>15</sup> -15 <sup>45</sup>			
12	7 10	09	10	09.7	01.2	00.0	.	= n-H <sup>10</sup> , 10 <sup>20</sup> ; [x] = 10 <sup>20</sup> , 12 <sup>20</sup> ; [x] H <sup>10</sup> , 14 <sup>20</sup>			
13	7 10*	10	10*	10.0	00.0	11.1	.	= n-n, [x] = n-80, 8-10 <sup>20</sup> , 14 <sup>20</sup> ; [x] 7-17 <sup>20</sup> , 15 <sup>20</sup> , [x] 9 <sup>20</sup>			
14	3 10=	10=	01	07.0	02.5	05.6	.	[x] n-pj, [x] 10 <sup>20</sup> , 13 <sup>20</sup> , [x] 13 <sup>20</sup> , [x] 12 <sup>20</sup>			
15	5 10*	10*	08	09.3	00.0	01.6	.	= n-n, [x] b <sup>20</sup> , 17 <sup>20</sup> , H <sup>10</sup> , 18 <sup>20</sup>			
16	4 02	10=	09	07.0	04.5	05.6	.	~ n-n, = n-7 <sup>45</sup> , 13 <sup>20</sup> ; [x] = 7 <sup>45</sup> , 9 <sup>45</sup> , = 9-15 <sup>10</sup>			
17	7 10	03○	10	07.7	00.4	.	.	= n-H <sup>10</sup> , [x] 8 <sup>45</sup>			
18	6 10*	03	00	04.3	03.6	00.0	.	[x] n-pj, [x] 5-12 <sup>20</sup> , [x] 7 <sup>20</sup> , [x] 14 <sup>20</sup>			
19	5 00	06○	08	04.7	00.0	00.0	.	~ n-H, = n-pj, 14 <sup>20</sup> , [x] = 8-14 <sup>45</sup>			
20	6 10	10*	10	10.0	00.0	.	.	= n-n, ~ n-dn, [x] 12 <sup>20</sup> , 15 <sup>20</sup>			
21	4 10	08=	10	09.3	01.0	00.8	02	= n-8 <sup>45</sup> , 14 <sup>20</sup> ; [x] = 8 <sup>45</sup> , 14 <sup>45</sup> , [x]			
22	6 10	10	05	08.3	00.9	.	.	= n-n			
23	8 01	07○	10	06.0	03.7	.	.				
24	5 10	10	00	06.7	00.4	.	.	= n-n, [x] 7 <sup>20</sup> , 9 <sup>20</sup>			
25	4 10*=	10	00	06.7	00.0	00.0	.	[x] n-7 <sup>45</sup> , = 11-13 <sup>45</sup> , = 13 <sup>45</sup>			
26	8 08	10	10*	09.3	00.8	00.0	.	= n-10 <sup>20</sup> , [x] 7, 19 <sup>45</sup> , n-i			
27	6 10*	10*	00	06.7	00.0	09.7	.	= n-pj, [x] n-17 <sup>20</sup>			
28	3 10=	10=	10=	10.0	00.0	06.4	.	~ n-n			
29	6 10	10	05	05.7	00.0	.	.	= n-n, [x] 9 <sup>20</sup> , 17 <sup>20</sup>			
30	7 01	07○	10*	06.0	06.8	00.9	.	[x] 14 <sup>20</sup> , 15, 16 <sup>20</sup> , 17 <sup>20</sup> , [x] 18-xx			
31	6 10	10	10	10.0	00.0	01.6	.	= n-n, [x] n-pj			
MES. VRED.	08.7	08.9	07.6	08.4	33.9	79.5					

1	5 10*	10*	10	10.0	00.0	17.9	01	= n-n, R, n, [x] n, [x] 14 <sup>20</sup> , 14 <sup>45</sup> , 10 <sup>20</sup> , [x] H <sup>10</sup> , 14 <sup>20</sup> ; [x] 15, [x]			
2	6 10	09	02	07.0	00.0	00.8	.	= n-n, [x] 15 <sup>20</sup> , 20 <sup>20</sup>			
3	5 00	03○	00	01.0	04.9	.	.	= n-n, [x] n-dn			
4	6 10=	08○	08	08.7	01.4	00.0	.	~ n-pj, [x] n-12 <sup>20</sup> , [x] 15 <sup>20</sup> , = 12 <sup>20</sup> , n			
5	5 03	10	10	07.7	00.3	00.1	.	= n-n, [x] 8 <sup>20</sup> , g <sup>20</sup>			
6	3 10	10=	10=	10.0	00.0	.	.	= n-7 <sup>45</sup> , = 17 <sup>20</sup> , 14 <sup>45</sup> , [x] 10 <sup>20</sup> , 13 <sup>20</sup> , = 10 <sup>20</sup> , n, R, 23 <sup>20</sup>			
7	3 10=	10=	10=	10.0	00.0	07.9	.	~ n-n			
8	5 08	09○	10	09.0	01.9	.	.	[x] n-14 <sup>20</sup> , [x] 15 <sup>20</sup> , 18 <sup>20</sup>			
9	6 09	09	10	09.3	00.2	.	.	= n-n, [x] 7 <sup>20</sup> , 9 <sup>20</sup>			
10	7 10=	10	10	10.0	01.5	00.0	.	[x] n-9 <sup>20</sup> , = 9 <sup>20</sup>			
11	8 09	08○	00	05.7	05.3	00.4	.	• n, [x] 5 <sup>20</sup> , 5 <sup>20</sup> , = 8 <sup>20</sup> , 10 <sup>20</sup>			
12	8 10*	08	02	06.7	04.2	06.2	.	• n, [x] 9 <sup>20</sup> , 16 <sup>20</sup> , 17 <sup>20</sup> ; [x] = n-8 <sup>20</sup> , [x] 14 <sup>20</sup> , 16			
13	9 09	05○	06	06.7	04.5	10.7	.	~ n-16 <sup>20</sup> , [x] 13 <sup>20</sup>			
14	6 10*	10	10	10.0	00.1	00.0	.	= n-n, [x] n-9 <sup>20</sup>			
15	5 10	03○	00	04.3	04.2	00.0	.	= n-n			
16	5 10=	09	09	09.3	02.3	.	.	= 10-9 <sup>20</sup> , = 9 <sup>20</sup>			
17	6 10*	07	00	05.7	04.6	00.0	.	= n-n, [x] 7 <sup>20</sup> , 9 <sup>20</sup>			
18	6 03	07○	00	03.3	07.7	00.0	.	= n-13 <sup>20</sup> , [x] 3-pj-dp, F <sub>sw</sub> 15 <sup>20</sup>			
19	8 10	08○	10	09.3	04.0	.	.	• 8 <sup>20</sup> , F <sub>sw</sub> 10 <sup>20</sup> , F <sub>sw</sub> 17 <sup>20</sup>			
20	8 10	06○	10	08.7	06.2	00.0	.	F <sub>sw</sub> 10-17 <sup>20</sup>			
21	8 10	10	10	10.0	00.0	.	.	F <sub>sw</sub> 7 <sup>20</sup> , 13 <sup>20</sup> ; [x] 14 <sup>20</sup> , 18 <sup>20</sup>			
22	8 10	09	10*	09.7	01.4	05.0	.	= n-10 <sup>20</sup> , [x] 16 <sup>20</sup> , [x] 17 <sup>20</sup>			
23	8 05	01○	00	02.0	08.6	12.4	.	• n, [x] 6 <sup>20</sup> , 6 <sup>20</sup> , 13 <sup>20</sup> ; [x] 13 <sup>20</sup> , 18 <sup>20</sup>			
24	6 05	09○	09	07.7	06.8	.	.	= n-n			
25	5 10	10	03	07.7	02.1	.	.	= n-13 <sup>20</sup> , [x] 12 <sup>20</sup> , 13 <sup>20</sup> , F <sub>sw</sub> 12 <sup>20</sup> , 12 <sup>20</sup>			
26	8 09	06○	00	05.0	01.6	00.9	.	= n-10 <sup>20</sup> , [x] 10 <sup>20</sup> , 10 <sup>20</sup> , 16 <sup>20</sup> , 19 <sup>20</sup>			
27	6 10	10*	10*	10.0	00.0	01.3	.	= n-n, [x] 10 <sup>20</sup> , n-i			
28	7 00	08	00	02.7	05.7	03.2	02	= n-n, [x]			
MES. VRED.	08.2	07.9	06.0	07.4	79.5	66.8					

$\varphi = 45^{\circ}49' N$   $\lambda = 15^{\circ}59' E$  Gr.  $\Delta G = +1h\ 04\ min.$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C						Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	757.2	756.2	757.8	-02.8	06.2	03.3	02.5	06.6	-02.8	-	02.8	03.2	03.2	75	45	56	59	NNW 1	WSW 2	ENE 2			
2	758.2	755.5	753.0	00.2	07.4	06.5	05.2	07.9	-00.1	-	03.0	03.3	03.6	65	43	49	52	NNW 1	SSW 2	W 2			
3	751.0	749.0	747.3	07.1	13.5	12.5	11.6	13.8	06.5	-	04.4	05.1	05.0	58	44	45	49	NW 4	NW 3	NW 2			
4	748.8	748.0	747.3	09.3	12.5	11.6	11.3	12.9	08.6	-	06.8	06.4	06.3	77	59	62	66	ENE 1	SW 2	NW 3			
5	752.4	752.8	754.0	07.0	12.7	09.3	09.6	13.2	07.0	-	05.7	05.5	05.7	76	50	65	64	E 2	SE 2	- 0			
6	751.2	751.4	754.4	03.9	17.9	10.8	10.9	18.6	03.9	-	05.4	05.4	04.5	89	35	46	57	W 2	WSW 3	ENE 3			
7	757.5	758.7	760.8	07.0	12.8	09.2	09.6	13.0	05.6	-	04.4	04.7	04.6	59	42	52	51	ENE 1	ESE 2	ENE 2			
8	762.8	762.0	762.1	06.2	13.0	10.1	09.9	13.4	06.1	-	04.4	04.9	05.4	63	44	59	55	E 2	SSW 2	NE 1			
9	759.4	756.6	755.1	05.8	17.6	12.4	12.1	18.1	04.8	-	05.4	06.0	06.2	78	40	57	58	WWN 2	W 3	W 2			
10	752.8	751.7	749.9	09.3	14.8	11.9	12.0	15.1	09.3	-	06.2	06.4	06.4	70	51	62	61	WWN 3	SSE 2	ENE 2			
11	748.1	746.7	746.6	08.4	15.9	12.1	12.1	15.9	08.2	-	04.6	06.4	06.0	56	47	56	53	ESE 1	WSW 3	WSW 2			
12	745.0	744.1	744.3	10.6	14.8	10.2	11.5	14.9	09.2	-	06.3	07.0	08.2	66	55	88	70	NNE 1	ENE 2	ENE 2			
13	742.5	745.0	747.8	09.3	08.7	06.5	07.8	10.2	06.5	-	07.9	06.6	06.7	90	78	92	87	NNE 2	ENE 2	WWN 2			
14	751.1	751.1	752.3	02.8	14.8	11.5	10.2	15.0	02.5	-	05.2	05.0	05.2	94	39	51	61	NNE 1	SW 2	NE 1			
15	757.0	757.6	757.9	09.8	13.1	10.0	10.7	13.9	09.2	-	06.2	05.8	05.1	68	52	55	58	WWN 1	WWN 3	NNN 1			
16	759.1	757.9	756.6	04.2	15.7	12.7	11.3	16.8	04.2	-	05.2	05.6	04.6	84	42	42	56	- 0	SSE 2	ENE 2			
17	754.8	752.6	751.5	06.1	17.9	15.1	13.6	19.0	05.9	-	05.3	05.8	05.6	76	38	44	53	ENE 1	SSE 2	NE 1			
18	750.0	747.4	746.9	07.4	18.3	13.5	13.2	19.5	07.2	-	05.7	05.8	05.1	74	37	44	52	NNW 1	WSW 2	W 1			
19	745.8	743.9	743.3	08.3	19.1	14.5	14.1	19.1	07.8	-	05.6	06.3	06.6	68	38	53	53	NNE 1	SSE 2	NNE 1			
20	744.1	744.0	745.5	09.1	17.2	12.3	12.7	17.9	08.9	-	07.3	05.2	05.2	84	35	48	56	- 0	WSW 3	SW 1			
21	747.0	747.7	749.8	09.2	15.7	11.7	12.1	16.2	08.0	-	07.4	07.4	05.2	85	56	60	64	WWN 2	WSW 3	WSW 2			
22	750.0	749.0	750.6	08.8	18.6	14.3	14.0	19.5	07.8	-	05.8	07.4	08.2	68	46	67	60	ENE 1	WSW 2	N 2			
23	752.0	752.1	751.8	11.1	22.1	18.7	17.7	23.1	10.6	-	07.3	07.4	06.6	74	37	41	51	ESE 1	SSW 2	NNE 2			
24	751.3	749.7	749.4	09.5	23.2	20.1	18.2	24.0	09.5	-	06.7	04.5	04.8	75	21	27	41	- 0	SSE 1	NNE 2			
25	750.0	750.2	750.8	12.6	22.8	18.6	18.2	22.8	11.9	-	07.1	08.3	08.8	65	40	55	53	NNE 1	E 2	NNE 1			
26	751.3	749.0	747.1	11.9	19.6	15.8	15.8	20.1	11.2	-	08.5	09.2	08.8	81	54	65	67	- 0	SSE 2	NE 2			
27	744.2	741.3	740.4	10.6	20.0	14.4	14.9	20.1	09.9	-	08.5	07.4	06.8	88	42	55	62	- 0	WSW 3	W 2			
28	738.8	737.7	737.1	11.8	16.9	12.8	13.6	17.1	11.5	-	07.0	07.0	06.9	67	48	62	59	W 1	WSW 4	WWN 1			
29	741.3	746.4	749.5	03.9	03.3	04.4	04.0	13.1	02.4	-	05.1	05.2	03.8	83	90	60	78	ENE 3	SSW 1	ENE 3			
30	750.1	748.5	746.1	-00.1	-00.2	-00.8	-00.5	04.4	-00.8	-	03.7	03.8	03.5	80	86	81	82	NE 3	ENE 3	NE 3			
31	746.8	750.0	751.4	-00.9	02.0	00.5	00.5	02.3	-01.2	-	03.8	04.3	04.0	90	82	84	85	SSW 1	S 2	SSW 1			
MES.	VRED.			750.7	750.1	750.3	07.0	14.4	11.2	11.0	15.4	06.4	-	05.8	05.9	05.7	75	49	57	60	1.3	2.3	1.7

1	752.0	750.4	749.0	00.7	08.2	06.3	05.4	09.5	00.1	-	04.4	05.2	05.6	91	63	78	77	ENE 1	SSW 2	NNE 2
2	745.4	744.4	744.1	03.9	10.8	08.3	07.8	11.3	02.9	-	05.3	06.8	06.8	88	70	83	80	- 0	SSE 2	ENE 1
3	742.0	739.7	739.3	07.5	11.9	10.2	10.0	13.9	07.4	-	07.5	08.0	07.8	96	76	84	85	S 1	SSE 1	NNE 1
4	744.9	746.0	746.2	09.8	11.2	09.2	09.9	11.2	09.2	-	05.7	06.8	05.5	63	68	63	65	ENE 2	ENE 2	NNE 2
5	745.7	748.0	749.1	08.2	06.6	05.0	06.2	09.2	04.8	-	06.3	07.0	06.0	77	94	91	87	SSW 1	WSW 1	WSW 2
6	749.3	746.2	743.3	01.6	11.9	09.5	08.1	13.3	08.8	-	05.0	05.8	05.2	96	56	58	70	ENE 1	SW 3	WSW 2
7	741.6	740.2	738.9	08.3	15.8	12.8	12.4	16.4	08.0	-	04.6	07.3	07.5	56	54	68	59	NNW 2	WSW 4	ESE 1
8	736.4	735.0	733.7	11.4	14.5	10.3	11.6	15.5	10.3	-	08.8	09.0	09.0	87	72	95	85	ESE 2	ESE 2	ENE 1
9	731.4	734.1	736.1	05.5	05.6	04.0	04.8	10.3	04.0	-	06.0	06.2	05.6	89	85	92	90	SW 3	S 2	NNW 1
10	737.8	739.8	743.7	02.5	05.2	03.8	03.8	05.7	02.1	-	05.0	05.6	05.2	92	83	86	87	ESE 2	ESE 2	NNE 2
11	747.5	746.3	746.7	02.3	06.8	04.5	04.5	07.7	02.2	-	03.5	04.0	04.4	65	54	70	63	ENE 1	SSW 2	ENE 2
12	746.9	746.6	748.0	02.1	09.2	05.4	05.5	09.8	01.8	-	04.0	03.6	04.4	74	41	66	60	NNW 1	ENE 2	E 1
13	748.0	745.2	744.6	03.8	11.8	08.4	08.1	12.8	02.7	-	05.1	04.4	06.0	85	42	73	67	NNW 1	SSW 2	ENE 2
14	743.4	742.6	742.1	05.8	09.5	05.6	06.7	10.3	05.2	-	06.1	06.5	06.3	89	73	92	85	ESE 1	S 2	NNW 1
15	742.2	741.7	743.2	03.1	09.3	07.4	06.8	09.5	02.6	-	05.3	04.0	03.8	92	46	50	63	ENE 2	ESE 2	NNE 3
16	744.7	745.4	750.1	04.8	09.8	07.5	07.4	11.0	03.1	-	03.9	03.6	02.7	60	40	35	45	WNW 2	WNW 2	NNE 2
17	752.4	749.9	748.5	04.2	12.8	09.2	08.9	13.9	03.6	-	03.0	03.4	04.0	48	31	45	41	WSW 1	SSW 2	SSW 1
18	748.4	748.2	748.9	05.0	17.3	13.2	12.2	17.8	03.7	-	04.4	05.0	03.9	68	34	44	45	W 1	SSW 2	NE 2
19	751.6	750.9	751.7	07.5	15.9	11.0	11.4	16.1	05.7	-	05.5	05.7	05.5	70	44	56	57	- 0	ESE 2	ENE 2
20	756.9	756.8	757.0	08.2	12.5	08.0	09.2	13.1	07.1	-	03.9	03.7	03.5	48	34	44	42	NE 2	ESE 3	NE 2
21	757.2	755.7	754.3	05.1	14.4	09.7	09.7	14.8	04.0	-	04.5	03.7	03.6	68	30	40	46	- 0	E 3	NE 2
22	753.5	750.9	748.3	06.2	18.6	15.4	13.9	19.5	05.4	-	04.8	05.0	05.4	68	31	41	47	WSW 1	SSW 2	NNW 2
23	746.3																			

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 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insoljacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	02	01	00	01.0	05.4	00.1	.	= n-10 <sup>45</sup>	
2	7	00	04	10	04.7	08.0	.	.	= n-10 <sup>30</sup>	
3	7	08	10	10	05.3	04.0	.	.	= n-12 <sup>30</sup> , F <sub>NW</sub> 4 <sup>45</sup> 6 <sup>45</sup>	
4	6	10	09	10	05.7	01.8	.	.	= n-10, F <sub>NE</sub> 0 <sup>40</sup> 7 <sup>55</sup> 9 <sup>20</sup> , F <sub>NW</sub> 13 <sup>04</sup> 20 <sup>45</sup>	
5	7	04	01	02	02.3	07.1	00.0	.	= n-0 <sup>20</sup> , = n-11 <sup>15</sup> , F <sub>NW</sub> 0 <sup>20</sup> 2, = n-11 <sup>15</sup>	
6	6	04	03	01	02.7	09.7	.	.	= n-n, F <sub>NE</sub> 5 <sup>20</sup> 16 <sup>30</sup> n	
7	7	08	10	01	06.3	07.5	.	.	= n-13 <sup>30</sup> , 17 <sup>30</sup> n; ⊕ 13 <sup>45</sup> -14 <sup>30</sup>	
8	7	08	10	00	06.0	05.9	.	.	= n-9 <sup>30</sup> , 16 <sup>30</sup> n; ⊕ 10 <sup>20</sup> -14 <sup>30</sup>	
9	7	08	06	00	04.7	09.2	.	.	= n-10 <sup>30</sup> , 16 <sup>30</sup> n	
10	6	02	04	00	02.0	06.5	.	.	= n-n	
11	5	00	09	10	06.3	05.4	.	.	= n-8 <sup>45</sup> , = 8 <sup>45</sup> n	
12	5	10	10	10	10.0	00.1	00.0	.	= n-n, F <sub>NE</sub> 6 <sup>20</sup> 8 <sup>15</sup> i, 13 <sup>52</sup> 14 <sup>30</sup> , 19 <sup>45</sup> n, ⊕ 0 <sup>20</sup> -14 <sup>30</sup> , 15 <sup>45</sup> , 18 <sup>52</sup> 19 <sup>45</sup>	
13	6	10	10	00	06.7	00.0	22.9	.	= n-13 <sup>30</sup> , 18 <sup>30</sup> n; ⊕ 10 <sup>20</sup> -18 <sup>30</sup> i, F <sub>NE</sub> 8 <sup>45</sup> 9 <sup>04</sup>	
14	7	00	09	06	05.0	05.9	03.6	.	= n-9 <sup>30</sup> , 17 <sup>45</sup> n	
15	9	10	04	00	04.7	03.8	00.0	.	= n-9 <sup>15</sup> , F <sub>NE</sub> 6 <sup>20</sup> n i, ⊕ 14 <sup>20</sup> -17 <sup>45</sup>	
16	9	00	03	00	01.0	10.0	00.0	.	= n-10 <sup>45</sup> , ⊕ 14 <sup>20</sup> -16 <sup>45</sup>	
17	8	00	08	03	03.7	09.3	.	.	= n-9 <sup>30</sup>	
18	7	08	09	00	05.7	06.4	.	.	= n-10 <sup>30</sup> ⊕ 10 <sup>45</sup> -12 <sup>30</sup>	
19	7	04	07	10	07.0	06.0	.	.	= n-11 <sup>30</sup>	
20	8	01	02	07	03.3	10.2	00.0	.	= n-9 <sup>30</sup> , ⊕ n	
21	8	09	07	00	05.3	05.1	04.0	.	= n-8 <sup>45</sup> , ⊕ 7 <sup>45</sup> -7 <sup>45</sup> i	
22	8	01	04	00	01.7	08.5	00.2	.	= n-12 <sup>30</sup>	
23	7	09	09	00	06.0	05.1	.	.	= n-14 <sup>30</sup>	
24	7	06	06	01	04.3	10.5	.	.	= n-11 <sup>30</sup>	
25	6	10	08	02	06.7	07.1	.	.	= n-13 <sup>45</sup> , 17 <sup>45</sup> n	
26	5	08	09	03	06.7	07.0	.	.	= n-n	
27	6	10	10	04	08.0	00.7	.	.	= n-13 <sup>30</sup> , ⊕ 12 <sup>30</sup> -13 <sup>30</sup>	
28	7	07	09	09	08.3	04.3	.	.	= n-8 <sup>30</sup>	
29	5	10	10*	10	10.0	00.0	03.0	.	= n-n, F <sub>NE</sub> 9 <sup>15</sup> , 14 <sup>30</sup> 17 <sup>15</sup> , ⊕ 9 <sup>15</sup> -14 <sup>30</sup>	
30	4	10*	10*	10*	10.0	00.0	05.4	05	= n-7 <sup>45</sup> , 15 <sup>15</sup> 16 <sup>45</sup> , ⊕ 10 <sup>20</sup> -n i, = 7 <sup>30</sup> n i, Δ 13 <sup>20</sup> -14 <sup>30</sup> , ⊕	
31	5	10*	10*	10	10.0	00.0	14.3	14	= n-n, ⊕ 15 <sup>15</sup> , ⊕	
MES.	VRED.	06.0	07.1	04.2	05.8	178.5	53.7			

1	6	05	00	00	01.7	09.2	00.7	06	= n-n, ⊕	
2	5	10	10	08	09.3	02.6	.	.	= n-9 <sup>30</sup> , = 9 <sup>30</sup> n	
3	6	09	06	00	05.0	03.7	00.3	.	= n-7 <sup>45</sup> , = 14 <sup>20</sup> n, ⊕ 11-13, Δ 23 <sup>25</sup> -23 <sup>40</sup>	
4	8	05	10	07	08.7	00.9	.	.	= n-8 <sup>5</sup> , ⊕ 12 <sup>40</sup> -12 <sup>40</sup>	
5	5	10	10	09	09.7	00.0	00.0	.	= n-n, ⊕ 8 <sup>40</sup> -19 <sup>45</sup>	
6	7	10	01	00	03.7	08.0	15.6	.	= n-8 <sup>45</sup> , = 8 <sup>45</sup> 9 <sup>30</sup> , = 9 <sup>30</sup> -10 <sup>30</sup>	
7	7	04	08	07	06.3	04.5	.	.	= n-8 <sup>45</sup> , 19 <sup>30</sup> n	
8	5	09	10	10	05.7	02.8	01.9	.	= n-13 <sup>30</sup> n i, = n-14 <sup>20</sup> n, ⊕ 14 <sup>45</sup> -12 <sup>30</sup> , Δ 14 <sup>45</sup>	
9	5	10	10	10	10.0	00.0	27.6	.	= n-n, ⊕ n-kv	
10	6	10	10	10	10.0	00.0	11.8	.	= n-n, ⊕ n-10 <sup>40</sup> , 13 <sup>52</sup> -22 <sup>30</sup>	
11	7	09	08	10	09.0	05.5	05.5	.	= n-11 <sup>45</sup>	
12	7	05	08	10	09.0	06.2	.	.	= n-9 <sup>45</sup>	
13	7	10	05	08	09.0	02.5	.	.	= n-9 <sup>30</sup> , Δ n-dn, ⊕ 10 <sup>20</sup> -19 <sup>30</sup> , 19 <sup>40</sup>	
14	6	10	10	10	10.0	00.0	00.0	.	= n-n, ⊕ 8 <sup>45</sup> 9 <sup>30</sup> , 14 <sup>45</sup> -21 <sup>45</sup>	
15	7	10	10	07	09.0	00.0	17.8	.	= n-10 <sup>30</sup> , ⊕ 9 <sup>30</sup>	
16	8	01	08	00	03.0	08.2	00.0	.	Δ n-ne 16 <sup>22</sup> -17 <sup>46</sup>	
17	9	00	00	01	06.3	12.8	.	.	Δ n-n	
18	7	01	06	01	02.7	12.6	.	.	= n-11 <sup>30</sup> ⊕ 10 <sup>20</sup> -12 <sup>30</sup> , Δ pp-n	
19	7	05	08	02	06.3	08.2	.	.	= n-10 <sup>30</sup>	
20	8	10	06	00	05.3	07.2	.	.	= n-n, ⊕ 10 <sup>20</sup> -n, ⊕ n-8 <sup>30</sup>	
21	8	00	00	04	01.3	12.3	.	.	= n-8 <sup>30</sup>	
22	8	10	08	05	07.7	04.2	.	.	= n-n	
23	5	10	10	04	08.0	00.2	.	.	= n-n, ⊕ 10 <sup>30</sup>	
24	6	10	09	05	08.0	01.3	.	.	= n-8 <sup>30</sup> , ⊕ n, ⊕ n, ⊕ n	
25	8	09	07	00	05.3	09.5	05.5	.	= n-8 <sup>30</sup> , ⊕ n, ⊕ n, ⊕ n	
26	8	10	03	00	04.3	07.4	.	.	= n-8 <sup>30</sup>	
27	7	00	07	10	05.7	11.2	.	.	= n-9 <sup>45</sup>	
28	7	10	10	10	10.0	01.3	.	.	= n-9 <sup>45</sup>	
29	8	09	05	00	04.7	11.2	00.1	.	= n-10 <sup>30</sup> , ⊕ 7 <sup>12</sup> -7 <sup>45</sup>	
30	8	04	06	05	05.0	05.2	05.2	.	= n-10 <sup>30</sup>	
MES.	VRED.	07.6	07.1	05.1	06.6	164.4	51.8			

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 $\varphi = 45^{\circ}49' N$   $\lambda = 15^{\circ}59' E$  Gr.  $\Delta G = + 1h 04 min.$ 

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D n	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	745.8	745.5	747.2	15.4	26.1	19.2	20.0	26.7	13.3	-	08.8	08.4	07.3	67	33	44	48	NNE 1	SW 2	NNW 2	
2	749.3	749.6	749.5	14.9	23.1	19.4	19.2	23.4	13.5	-	09.6	10.2	10.3	76	48	61	62	NE 1	SSW 2	NNE 2	
3	749.6	748.2	746.7	15.3	24.5	20.8	20.4	25.1	13.2	-	10.3	09.7	09.4	79	42	51	57	SSW 1	SSE 2	NNE 2	
4	746.1	745.2	744.0	16.6	25.7	22.2	21.7	26.8	15.2	-	10.7	09.9	10.0	76	40	50	55	SSW 1	SE 1	NE 1	
5	744.6	746.2	747.9	17.6	20.7	16.1	17.6	24.1	16.1	-	11.5	09.6	05.4	76	52	39	56	W 1	NNW 3	NW 2	
6	750.9	749.2	749.3	12.4	19.8	15.1	15.6	20.4	09.9	-	06.9	07.6	07.4	64	44	58	55	ENE 1	SE 2	NNW 2	
7	749.0	746.8	747.1	12.2	20.1	13.1	14.6	20.2	10.0	-	08.0	06.4	08.0	75	36	70	60	- 0	SSW 2	ENE 1	
8	746.0	744.0	743.5	11.1	13.2	10.7	11.4	15.2	10.7	-	07.3	07.6	08.3	74	67	86	76	ESE 2	NNW 2	W 1	
9	745.1	745.7	747.6	09.8	14.6	12.2	12.2	15.6	09.8	-	08.4	07.6	06.6	93	61	62	72	NE 1	W 2	NNW 2	
10	748.6	748.0	748.4	13.2	18.2	13.4	14.6	19.2	10.8	-	06.0	05.8	06.2	53	37	54	48	N 2	ENE 1	N 1	
11	749.2	747.6	747.2	11.0	21.0	16.3	16.2	21.7	08.9	-	07.2	06.6	07.6	73	35	55	54	- 0	SW 2	S 1	
12	746.6	743.3	742.1	12.6	24.0	16.9	17.6	24.5	10.7	-	08.0	07.8	06.4	73	35	44	51	- 0	SSW 3	W 2	
13	741.0	740.4	739.4	15.0	22.1	18.0	18.3	22.7	14.1	-	06.7	08.0	08.6	52	40	55	49	NNW 1	WSW 3	WSW 1	
14	737.8	736.4	740.4	15.0	18.4	14.6	15.7	21.5	14.6	-	09.5	11.2	10.7	74	71	86	77	ENE 1	NNW 2	ENE 1	
15	739.9	739.6	740.7	12.4	15.4	13.2	13.6	17.9	11.7	-	09.4	09.3	08.6	87	71	76	78	NE 1	NNW 2		
16	741.8	741.8	743.6	12.6	19.4	14.7	15.4	20.1	11.2	-	10.0	08.8	08.2	91	52	66	70	WSW 1	SSE 2	WSW 2	
17	746.3	748.3	750.9	12.8	21.2	16.4	16.7	21.7	10.3	-	09.2	09.8	11.5	83	51	82	72	N 1	WSW 2	NNE 1	
18	753.2	752.5	752.6	16.2	18.0	18.3	17.7	18.4	12.9	-	10.8	12.4	11.5	78	80	73	77	S 1	ENE 2	NE 2	
19	750.7	749.0	747.7	18.0	22.2	20.2	20.2	22.2	17.6	-	11.3	13.2	14.2	73	66	80	73	ESE 2	NE 2	NNW 1	
20	745.6	745.6	746.9	18.6	27.1	22.0	22.4	27.1	16.7	-	14.0	10.8	07.9	87	41	40	56	SE 1	WSW 3	NNW 2	
21	748.1	746.7	747.0	17.1	26.1	21.3	21.5	27.0	15.9	-	10.3	08.9	09.3	71	35	49	52	W 1	SSW 2	NW 2	
22	748.7	749.0	752.1	16.0	19.6	14.3	16.1	21.3	14.3	-	10.6	10.4	07.4	78	61	61	67	E 2	ENE 2	ENE 3	
23	753.2	753.0	753.3	11.3	13.7	10.4	11.5	14.3	10.4	-	07.5	07.0	08.5	74	60	90	75	NNE 1	ENE 2	NNW 2	
24	753.2	752.5	751.5	11.2	19.5	15.4	15.4	20.5	09.3	-	08.8	06.4	06.7	89	38	51	59	NNE 1	E 2	NNW 2	
25	749.9	748.0	747.5	12.6	22.3	18.0	17.7	23.1	10.1	-	07.9	08.0	08.2	72	40	53	55	SSE 1	S 2	NNE 2	
26	748.4	748.7	749.3	15.7	20.0	16.2	17.0	20.3	13.4	-	09.6	07.7	04.8	72	44	35	50	S 1	E 3	NE 3	
27	750.6	752.7	752.7	10.1	08.9	08.2	08.9	16.2	08.2	-	05.7	07.2	06.8	61	85	83	76	E 2	E 1	NNW 1	
28	751.8	750.7	750.1	08.5	16.6	12.5	12.5	18.4	06.3	-	06.9	05.2	06.0	83	37	55	58	NE 1	NE 2	N 2	
29	749.1	747.8	746.8	10.9	20.9	15.9	15.9	21.5	08.6	-	06.6	05.4	06.2	67	29	46	47	ENE 1	SN 2	S 1	
30	746.2	744.2	744.6	12.2	23.9	18.1	18.1	25.0	10.0	-	07.4	08.7	07.3	70	39	47	52	ESE 1	SSW 2	NNW 2	
31	747.0	747.6	751.0	15.4	17.0	10.5	13.4	18.1	10.4	-	08.8	11.2	08.2	67	77	87	77	N 1	ENE 1	E 1	
MES.	VRED.	747.5	747.0	747.4	13.7	20.1	15.9	16.4	21.3	11.9	-	08.8	08.6	08.2	74	50	61	62	1.1	2.0	1.6

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1	753.0	752.5	752.5	10.2	16.5	12.5	12.9	17.4	09.4	-	06.3	05.4	05.0	68	38	46	51	ENE 1	NE 2	NE 2
2	752.1	750.0	749.6	11.6	18.2	13.6	14.3	19.1	09.2	-	05.0	05.2	05.6	49	23	48	43	ENE 2	E 3	NNE 2
3	748.4	747.0	746.8	11.0	17.9	14.2	14.3	19.4	08.5	-	06.8	06.2	05.6	69	40	46	52	E 1	ENE 2	NE 2
4	746.3	745.2	745.5	13.4	19.3	14.3	15.3	19.8	10.5	-	07.5	07.0	09.0	65	42	74	60	NNE 1	ENE 2	NW 1
5	745.5	743.3	742.4	13.3	22.3	15.4	16.6	22.6	12.9	-	09.3	08.6	10.2	81	43	78	67	- 0	S 2	N 1
6	742.3	742.1	743.6	14.9	23.4	18.0	18.6	23.7	13.6	-	09.5	09.7	08.2	75	45	53	58	- 0	SW 4	W 2
7	744.8	744.8	746.0	16.7	21.4	18.4	18.7	24.2	13.9	-	09.7	10.6	09.3	68	49	60	59	WNW 1	W 3	W 2
8	748.4	748.1	748.7	16.9	26.4	20.1	20.9	26.8	14.7	-	10.3	10.3	10.4	71	40	59	57	W 2	WSW 4	WSW 2
9	749.1	747.6	747.1	18.3	28.5	22.2	22.8	29.2	16.3	-	09.7	11.1	10.6	62	38	53	51	WNW 2	WSW 4	WSW 2
10	746.1	744.2	743.9	18.3	29.1	24.2	24.0	30.4	16.0	-	10.3	12.1	12.7	66	40	56	54	W 2	SSW 2	W 2
11	744.3	744.4	745.0	22.0	29.5	25.4	25.6	30.0	19.0	-	11.0	13.0	12.7	56	42	52	50	NW 2	SSE 2	NNE 2
12	746.2	745.3	745.8	23.0	28.9	24.2	25.1	29.5	20.5	-	14.5	14.3	14.0	69	48	62	60	NE 1	E 2	NNE 1
13	746.2	744.1	743.3	22.6	31.1	26.4	26.6	31.5	20.5	-	13.5	14.2	13.7	66	42	53	54	NE 1	S 2	NE 1
14	742.7	741.7	741.8	22.4	30.2	22.1	24.2	30.4	20.1	-	13.7	13.2	13.0	68	41	45	51	NW 1	SW 3	WSW 3
15	742.4	741.7	742.6	19.7	25.5	21.0	21.8	26.6	17.1	-	10.7	10.8	10.8	62	44	58	55	W 2	NNW 2	NNW 2
16	743.4	743.0	743.3	18.3	21.5	19.7	19.8	22.4	17.3	-	11.7	11.6	11.7	74	60	68	67	SW 1	E 2	NW 1
17	744.6	744.9	745.7	17.4	25.3	22.0	21.7	25.8	16.4	-	12.4	12.4	13.9	83	51	70	68	ENE 1	SE 2	SW 1
18	746.0	745.1	743.8	21.2	29.0	24.0	24.6	29.7	18.6	-	13.9	13.2	14.6	74	44	65	61	- 0	SSE 2	W 1
19	743.6	742.9	743.3	21.2	29.0	22.6	23.9	29.9	19.3	-	12.1	10.2	10.3	64	34	50	49	WSW 2	WSW 3	W 2
20	744.5	744.1	746.0	20.3	27.6	22.1	23.0	27.9	17.8	-	12.0	09.2	11.2	67	33	56	52	NE 1	SW 2	ENE 1
21	747.3	745.4	744.3	20.1	26.4	21.0	22.1	26.4	18.0	-	10.6	10.6	12.9	60	41	69	57	NW 1	SE 2	ENE 1
22	744.9	744.1	745.6	16.4	20.6	15.3	16.9	22.1	14.4	-	11.7	13.5	12.1	84	74	93	84	N 1	2	

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 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vremenska časnost O-9	Oblačnost N (0-10)					Imečnost broj	Padavina R mm	Snežni pokriven h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	000	010	01	00.7	10.4	.	.	.	
2	8	10	080	01	06.3	04.7	.	.	.	
3	8	040	090	02	05.0	10.8	00.0	.	.	
4	7	090	100	08	09.0	08.6	.	.		$\equiv n-10^{10} \oplus 13-15^{15}$
5	7	060	10	00	05.3	05.9	.	.		$\equiv n-10^{15} \oplus 13-15^{15}$
6	7	010	060	08	05.0	09.3	00.4	.	.	$\equiv n-12^{30}$
7	7	000	060	06	04.0	09.9	.	.	.	$\equiv n-11^{15} \oplus 15^{15}-15^{20}$
8	6	10	100	09	09.7	00.6	00.4	.	.	$\equiv n-n \oplus 11^{30} 16^{30} i$
9	6	100	09	09	09.3	04.8	08.9	.	.	$\equiv n-n \oplus 13^{30} n-9^{30} \oplus 14^{30} 15^{22} i$
10	6	08	060	02	05.3	07.6	00.6	.	.	$\equiv n-13^{10} 19^{30} n-12^{30} 14^{30} i$
11	7	10	040	04	06.0	09.7	00.0	.	.	$\equiv n-11^{20}$
12	7	050	060	01	04.0	10.9	.	.	.	$\equiv n-10^{15}$
13	7	080	10	10	05.3	04.9	.	.	.	$\equiv n-11^{15} \oplus 13^{30} i$
14	5	100	070	02	06.3	02.5	00.3	.	.	$\equiv n-13^{10} \oplus 14-13^{30} i, 18^{30} 19^{45} i, R-12^{30} 12^{45}, \Delta 17^{30}-n$
15	8	080	070	08	07.7	05.6	01.6	.	.	$\equiv n-12^{30} 14^{30} i, 15^{30} \Delta 12^{30}$
16	8	10	10	06	08.7	02.8	03.5	.	.	$\equiv n-8^{30} \oplus 19^{30} KV$
17	7	100	080	09	09.0	05.4	00.0	.	.	$\equiv n-11^{30} \oplus 6^{30} 7^{30} 10^{30} 19^{25}$
18	4	10	100	10	10.0	00.3	00.0	.	.	$\equiv n-n \oplus 10^{30} 15^{30}$
19	6	10	10	10	10.0	01.0	00.6	.	.	$\equiv n-n$
20	7	10	050	05	06.7	08.4	.	.	.	$\equiv n-11^{30}$
21	8	000	050	00	01.7	11.1	.	.	.	
22	7	070	100	10	09.0	05.6	.	.	.	$\equiv R-12, 13^{30}, \oplus 13^{30}-15^{30}, 15^{15}-n i$
23	8	10	10	100	10.0	00.0	01.5	.	.	$\equiv n-8^{30} \oplus 14^{30} 14^{30}, 17^{30}-21^{40}$
24	8	010	020	00	01.0	13.3	03.7	.	.	$\equiv n-10^{30}$
25	8	000	000	01	00.3	12.3	.	.	.	$\equiv n-9^{30}$
26	7	080	070	10	08.3	07.6	.	.	.	$\equiv n-10^{15}$
27	6	100	100	04	08.0	00.1	00.5	.	.	$\equiv n-12^{30} \oplus 15^{30} 14^{30} i$
28	7	000	040	00	01.3	12.4	05.8	.	.	$\equiv n-10^{15} \oplus 10^{30} 15^{30}$
29	8	000	020	00	00.7	13.7	.	.	.	$\equiv n-8^{30} \Delta n-dp$
30	8	000	010	01	00.7	11.6	.	.	.	$\equiv n-n \oplus 12^{30} n, \oplus 12^{30} n i, F_{\text{NE}} 15-17$
31	6	09	10	100	05.7	01.0	.	.	.	
MES. VRED.					06.3	06.9	05.1	06.1	212.8	27.8

1	7	09	060	00	05.0	08.1	06.0	.		$\equiv n-8^{45}$
2	8	010	070	00	02.7	13.5	.	.	.	$\equiv n-8^{30}$
3	7	09	070	07	07.7	07.2	.	.	.	$\equiv n-12^{30} \oplus 17^{30}$
4	7	070	080	08	07.7	06.5	.	.	.	$\equiv n-10^{30} \oplus 16^{30} 18^{45}, \oplus 13-15^{15}, \oplus 14^{50} 15^{45}, \oplus 15^{30} 15^{31}$
5	7	10	08	04	07.3	04.4	00.0	.	.	
6	6	020	08	02	04.0	04.8	01.3	.	.	$\equiv n-13^{30} \oplus 14-16^{40}$
7	6	10	09	00	06.3	04.4	.	.	.	$\equiv n-10 \oplus 15^{30} 16^{45}$
8	7	000	060	02	02.7	12.6	.	.	.	$\equiv n-9^{30} \oplus 15-17^{30}$
9	7	000	010	00	00.3	13.5	.	.	.	$\equiv n-9^{45}$
10	7	010	030	00	01.3	12.6	.	.	.	$\equiv n-9^{45}$
11	7	000	060	07	04.3	10.0	.	.	.	$\equiv n-11^{30}$
12	6	09	080	00	05.7	07.3	.	.	.	$\equiv n-n$
13	6	000	040	00	01.3	11.6	.	.	.	$\equiv n-n$
14	7	000	030	00	01.0	13.5	.	.	.	$\equiv n-10^{15}$
15	7	040	08	01	04.3	09.9	.	.	.	
16	6	100	10	08	09.3	00.3	00.2	.	.	$\equiv n-n, \Delta n, \oplus 12^{30} 14^{30}, \oplus 15^{30}$
17	6	10	070	03	06.7	03.7	03.0	.	.	$\equiv n-n$
18	6	000	030	00	01.0	11.6	.	.	.	$\equiv n-n, \Delta n-dp$
19	8	010	030	03	02.3	13.0	.	.	.	$\equiv n-n, \Delta n-dp$
20	8	040	060	01	03.7	11.3	.	.	.	$\equiv n-8^{30}, \oplus 15^{30}, \oplus 16^{30} 14^{45}$
21	8	08	060	10	06.0	05.9	00.0	.	.	$\equiv 15^{45}-n, \oplus 16^{30} n, \oplus 16^{40} 17^{40}$
22	8	060	100	10	08.7	05.5	15.8	.	.	$\equiv 15-12^{30} 17^{30} i, \oplus 13^{30} 14^{40} i, \oplus 14^{30} 14^{40}, \oplus 14^{40}-17^{40}$
23	8	08	09	01	06.0	08.2	30.2	.	.	$\equiv 15-13^{45} \oplus 15^{30} 12^{15} \oplus 13^{45} 20^{45}$
24	7	030	08	04	05.0	09.0	00.0	.	.	$\equiv n-9^{45} \oplus 15^{30} 12^{15} \oplus 13^{45} 20^{45}$
25	7	09	070	03	06.3	04.6	00.2	.	.	$\equiv n-10^{30}, \oplus 14^{30} 16^{40}, \oplus 16^{40}-16^{45}$
26	7	10	090	10	09.7	05.2	00.0	.	.	$\equiv n-11^{15}, \oplus 14^{30} 14^{40} \oplus 15^{45}, \oplus 15^{45} 18^{45}$
27	6	10	10	03	07.7	00.2	07.0	.	.	$\equiv n-n, \oplus 15^{30} 14^{45} i$
28	6	000	040	00	01.3	13.3	.	.	.	$\equiv n-15^{30}$
29	8	030	040	08	05.0	11.7	.	.	.	$\equiv n-10^{30}$
30	6	10	10	100	10.0	03.2	.	.	.	$\equiv n-n, \oplus 17^{30} 18^{45}, 12^{30}, 21^{40} n i; \oplus 17^{30} 20^{30}, \oplus 17^{30} 18^{45} n i$
MES. VRED.					05.1	06.6	03.5	05.1	246.6	62.7

$\gamma = 45^{\circ}49' N$   $\lambda = 15^{\circ}59' E$  Gr.  $\Delta G = +1h\ 04\ min.$ 

BR. ST. 57

D E N	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodené pare • mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	751.7	752.1	752.3	15.4	22.7	19.2	19.1	23.2	14.8	-	12.1	09.8	10.6	92	47	62	67	NW	1	N	2	N	2
2	752.8	751.7	750.8	18.2	25.5	21.2	21.5	26.0	15.0	-	10.7	09.6	11.3	68	39	60	56	WSW	1	NNW	1	NW	1
3	750.8	749.2	746.9	17.7	28.3	24.2	23.6	29.5	15.8	-	11.9	13.0	14.0	80	45	62	62	NW	1	SSW	2	S	1
4	745.1	745.0	743.4	22.7	25.7	23.4	23.8	27.6	18.0	-	12.9	11.7	13.6	62	47	63	57	NW	2	E	2	SE	1
5	743.5	741.6	742.2	20.1	24.5	18.2	20.3	25.7	18.2	-	12.7	13.4	13.4	73	58	85	72	E	1	E	2	NE	2
6	744.4	744.3	744.7	16.9	24.1	20.5	20.7	25.0	14.3	-	11.3	10.8	11.5	80	48	62	63	NNE	1	SW	2	S	2
7	744.5	743.4	744.4	17.9	27.0	19.3	20.9	27.8	16.1	-	12.3	12.6	13.6	80	47	61	69	ENE	1	SSW	3	ENE	1
8	743.5	741.3	740.6	20.0	28.5	24.0	24.1	29.1	17.4	-	13.9	14.6	13.4	79	60	63	63	SW	1	WSW	2	WNW	2
9	741.2	742.6	744.2	22.1	24.3	20.2	21.7	26.1	19.8	-	14.0	14.3	15.1	70	63	85	73	WSW	2	WNW	3	NE	1
10	746.2	746.4	746.8	20.0	18.4	17.9	18.6	25.1	16.7	-	13.0	13.8	13.6	74	87	88	83	SE	1	ENE	3	W	2
11	747.7	747.5	748.1	19.3	26.0	21.2	21.9	26.6	15.6	-	11.1	11.1	09.6	66	44	51	54	NNW	2	N	2	NE	1
12	748.2	747.1	747.7	21.1	28.7	23.6	24.3	29.6	17.6	-	10.9	10.4	12.4	58	35	57	50	NNW	2	NNW	2	NE	2
13	748.5	746.7	745.3	20.0	30.1	24.7	24.9	30.4	18.0	-	12.3	12.5	13.3	70	39	57	55	SSE	1	SSE	2	NE	2
14	744.6	743.3	743.3	20.5	27.0	22.5	23.1	28.5	19.4	-	12.7	13.6	13.9	71	51	68	63	WSW	1	SW	1	ENE	2
15	744.6	746.2	749.7	16.5	16.2	15.5	15.9	22.3	15.4	-	12.4	13.3	11.5	88	96	87	90	E	1	NE	2	NNE	1
16	752.4	751.2	749.1	16.3	22.1	18.4	18.8	22.9	14.6	-	10.4	08.4	10.5	75	42	66	61	NE	1	SSE	3	SE	1
17	747.2	747.9	747.9	16.5	24.0	20.5	20.4	24.9	14.6	-	11.8	09.3	11.3	84	41	62	62	NE	1	E	2	NE	1
18	748.3	746.2	744.1	18.8	25.4	21.0	21.6	26.3	17.5	-	08.8	12.2	14.0	54	50	75	60	ENE	1	S	2	NNE	1
19	744.8	745.7	746.9	18.4	22.2	20.2	20.3	23.2	17.0	-	13.5	11.6	11.6	85	58	65	69	W	1	ENE	1	NNE	2
20	747.8	746.2	745.3	19.8	26.7	22.6	22.9	27.0	19.0	-	12.0	10.8	13.2	69	41	64	58	ENE	1	SE	2	NE	2
21	743.7	747.4	748.6	18.0	19.7	17.2	18.0	22.8	15.4	-	14.6	12.8	13.1	94	74	89	86	NW	2	ENE	2	NNW	1
22	749.4	749.0	748.8	15.3	17.4	16.9	16.6	18.5	14.6	-	11.9	10.7	11.9	91	72	82	82	SSE	1	NNE	1	S	1
23	749.4	749.3	749.6	18.6	23.5	18.4	19.7	24.0	16.6	-	08.6	08.3	09.5	53	38	60	50	SSE	3	ENE	2	NNE	1
24	748.8	746.3	743.8	18.6	26.3	21.2	21.8	26.5	15.9	-	10.3	11.0	12.5	64	43	66	58	W	1	SSW	3	S	1
25	741.4	737.7	737.8	17.8	29.3	21.3	22.4	29.4	15.9	-	12.7	12.0	11.8	83	39	62	61	NE	1	SSW	3	SW	2
26	739.4	743.3	744.2	18.0	14.5	12.9	14.6	21.3	12.9	-	12.1	11.2	10.1	78	56	86	86	ENE	2	E	1	NNW	1
27	745.6	747.6	747.7	13.3	21.3	16.4	16.9	21.6	11.2	-	10.2	09.5	10.3	89	52	73	71	ENE	1	E	2	NNW	1
28	747.2	746.6	746.6	14.6	22.9	18.4	18.6	23.2	13.1	-	10.2	11.5	12.3	82	55	77	71	ENE	1	S	1	NE	1
29	747.5	747.1	746.3	17.0	24.9	20.7	20.8	25.9	14.7	-	12.1	11.4	13.2	83	48	72	68	ENE	1	S	2	NNW	1
30	746.0	744.8	743.2	19.5	26.4	23.3	23.1	27.5	18.7	-	13.7	14.2	15.5	79	57	72	69	ENE	1	S	2	S	1
31	738.3	738.0	737.4	21.4	24.2	19.4	21.1	25.6	19.4	-	16.1	11.3	11.5	84	50	68	67	SE	1	SW	4	SW	3
MES.	VRED.	746.3	745.9	745.7	18.4	24.1	20.2	20.7	25.6	16.2	-	12.0	11.6	12.4	76	53	70	66	1.3	2.1	1.4		

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1	737.4	741.4	744.0	15.9	23.4	16.5	18.3	23.6	15.4	-	12.1	09.1	08.0	89	42	56	62	NNW	2	NNW	2	NNW	2
2	744.2	745.1	745.2	16.3	16.5	15.9	16.2	20.2	15.9	-	08.1	10.3	11.0	59	72	81	71	NNW	1	NNW	2	W	1
3	745.1	745.5	746.8	13.9	23.9	15.2	19.1	24.6	12.9	-	10.4	10.9	12.2	87	49	73	70	WSW	1	SW	2	NNE	1
4	749.8	749.5	749.7	16.9	26.0	21.6	21.5	26.5	15.2	-	10.9	12.4	13.2	76	49	68	64	NE	1	S	2	ENE	1
5	749.5	747.9	748.0	18.2	28.0	21.1	22.1	28.0	17.2	-	12.8	14.2	14.8	82	50	79	70	NE	1	SSE	2	NNW	2
6	748.1	747.8	747.6	19.1	27.5	23.7	23.5	27.9	17.3	-	13.3	12.4	11.5	81	45	53	60	ENE	1	ENE	2	NE	2
7	746.9	746.2	745.4	19.1	25.6	22.6	22.5	26.2	17.5	-	12.4	14.6	14.4	75	59	70	68	NNW	1	ENE	2	NE	2
8	745.8	745.5	746.4	19.5	27.8	23.3	23.5	28.0	18.1	-	13.4	12.9	13.3	79	46	62	62	NE	1	E	2	NNE	2
9	747.9	747.3	748.5	20.7	27.5	19.9	22.0	27.8	18.5	-	14.6	14.9	14.6	80	54	84	73	NE	1	ESE	2	SSE	2
10	748.0	746.6	746.9	17.7	25.2	18.0	19.7	26.0	15.0	-	12.9	14.4	13.4	85	60	87	77	NE	1	SE	1	N	1
11	747.7	747.4	747.5	16.7	21.6	20.3	19.7	22.3	15.5	-	13.0	13.0	11.8	91	67	66	75	SW	1	S	1	NE	2
12	747.5	747.1	746.6	17.2	21.9	19.8	19.7	22.6	16.0	-	10.6	12.8	13.0	72	65	75	71	ENE	2	ENE	1	NNE	2
13	746.0	746.1	747.0	18.8	23.8	15.1	20.2	24.0	17.4	-	14.3	11.5	13.2	89	52	80	74	NNW	1	NNW	2	ENE	1
14	746.9	747.3	748.4	17.8	22.1	18.3	19.1	22.7	16.2	-	12.7	11.6	11.6	83	58	74	72	ENE	1	NNW	2	NNW	1
15	749.4	749.2	750.0	16.5	25.0	19.4	20.1	25.4	14.5	-	11.5	09.0	12.0	82	38	71	64	W	1	E	1	NW	1
16	750.8	749.5	748.9	17.1	25.1	22.1	21.6	25.7	15.6	-	11.6	12.2	13.8	79	51	66	66	-	0	SSE	2	NE	2
17	748.8	747.6	746.8	18.9	25.5	22.0	22.1	25.7	17.0	-	12.5	14.2	15.1	76	58	76	70	NE	1	SE	2	NE	2
18	745.1	743.9	744.2	19.1	25.9	24.0	23.3	27.9	18.1	-	14.3	15.8	13.4	87	63	60	70	E	1	SW	2	W	1
19	740.3	739.4	741.1	18.9	26.2	16.7	19.6	26.8	16.7	-</													

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$ 

Dan	Vrijeme 0-9 0-9	Oblačnost N (0-10)					Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes			
1	8 10	070	06	07.7	05.1	08.4	.	.	= n-10 <sup>30</sup>
2	7 08	100	07	08.3	00.7	.	.	.	= n-10 <sup>30</sup>
3	8 06	370	02	05.0	06.0	01.5	.	.	= n-10 <sup>30</sup>
4	6 010	050	03	03.0	12.7	.	.	.	= n-10 <sup>30</sup>
5	6 000	060	06	04.0	10.6	.	.	.	= n-10 <sup>30</sup>
6	7 07	06	01	04.7	08.4	05.3	.	.	= n-8 <sup>30</sup> , R <sup>0</sup> 16 <sup>10</sup> 16 <sup>45</sup> , F=16 <sup>0</sup> -16 <sup>30</sup> , V <sup>0</sup> -16 <sup>53</sup>
7	8 01	01	04	02.0	10.0	.	.	.	= n-10 <sup>30</sup>
8	6 10	09	07	06.7	07.1	00.0	.	.	= n-10 <sup>30</sup>
9	7 000	080	08	05.3	07.5	00.0	.	.	= n-10 <sup>30</sup>
10	6 030	100	01	04.7	04.8	04.3	.	.	= n-10 <sup>30</sup> , V <sup>0</sup> -13 <sup>0</sup> -13 <sup>5</sup> , R <sup>0</sup> 13 <sup>0</sup> -13 <sup>5</sup> , H <sup>0</sup> -10 <sup>30</sup>
11	7 030	050	00	02.7	11.2	08.2	.	.	= n-9 <sup>30</sup> , △ n-dp
12	7 010	020	00	01.0	12.5	.	.	.	= n-9 <sup>30</sup>
13	6 000	020	05	02.3	12.3	.	.	.	= n-14 <sup>30</sup>
14	6 010	09	08	06.0	09.1	.	.	.	= n-15 <sup>30</sup>
15	7 09	100	10	05.7	00.7	14.5	.	.	= n-n, V <sup>0</sup> n, 10 <sup>0</sup> -10 <sup>40</sup> , R <sup>0</sup> 10 <sup>0</sup> -H <sup>30</sup>
16	8 09	000	00	03.0	09.0	24.7	.	.	= n-10 <sup>30</sup>
17	6 04	060	02	04.0	09.1	01.3	.	.	= n-n, = n-10 <sup>30</sup>
18	7 030	060	03	04.0	10.4	.	.	.	= n-9 <sup>30</sup>
19	7 10	10	03	07.7	02.8	00.0	.	.	= n-9 <sup>30</sup>
20	7 070	040	04	05.0	10.9	00.0	.	.	= n-11 <sup>30</sup>
21	6 10	10	10	10.0	02.0	05.6	.	.	= n-11 <sup>30</sup> , R <sup>0</sup> n-11 <sup>30</sup> , V <sup>0</sup> n-12 <sup>30</sup>
22	6 10	10	10	10.0	00.0	16.3	.	.	= n-n, R <sup>0</sup> n-10 <sup>30</sup>
23	6 060	08	00	04.7	10.2	00.0	.	.	= n-10 <sup>30</sup>
24	8 060	050	00	03.7	12.0	.	.	.	= n-10 <sup>30</sup>
25	8 000	030	04	02.3	12.5	.	.	.	= n-10 <sup>30</sup> , △ n-dp
26	6 100	100	00	06.7	00.8	06.1	.	.	= n-n, = n-10 <sup>30</sup>
27	5 09	020	00	03.7	08.4	07.4	.	.	= n-10 <sup>30</sup> , △ H <sup>30</sup> , RV
28	7 050	07	02	04.7	09.0	.	.	.	= n-11 <sup>30</sup> , △ n-dp, R <sup>0</sup> 15 <sup>30</sup> -15 <sup>30</sup>
29	7 000	070	04	03.7	12.5	00.1	.	.	= n-10 <sup>30</sup> , △ n-dp
30	7 09	09	05	07.7	05.2	.	.	.	= n-12 <sup>30</sup>
31	9 080	020	08	06.0	07.3	.	.	.	= n-10 <sup>15</sup> , = 9 <sup>30</sup> -10 <sup>30</sup> , F=10 <sup>30</sup> -16 <sup>30</sup> , △ 10 <sup>30</sup> -10 <sup>30</sup>
MES.	VRED.	05.2	06.1	03.9	05.1	247.6	109.8		

1	8 10	070	06	07.7	05.1	08.4	.	.	= H <sup>30</sup> , RV
2	7 08	100	07	08.3	00.7	.	.	.	= n-10 <sup>30</sup>
3	8 06	370	02	05.0	06.0	01.5	.	.	= n-10 <sup>30</sup>
4	6 010	050	03	03.0	12.7	.	.	.	= n-10 <sup>30</sup>
5	6 000	060	06	04.0	10.6	.	.	.	= n-10 <sup>30</sup>
6	6 000	050	10	05.0	10.7	00.0	.	.	= n-15 <sup>30</sup> , 18 <sup>10</sup> -n, □ n-dp, = 10 <sup>30</sup> -18 <sup>30</sup>
7	6 10	10	00	06.7	08.7	00.0	.	.	= n-n
8	6 000	020	03	01.7	10.5	.	.	.	= n-n
9	6 040	09	03	05.3	05.5	.	.	.	= n-n, R <sup>0</sup> 15 <sup>40</sup> -17 <sup>15</sup> , = 15 <sup>30</sup> -17 <sup>30</sup>
10	6 040	10	05	06.3	07.0	00.0	.	.	= n-n, = 8 <sup>15</sup> , 15 <sup>10</sup> -16 <sup>10</sup> , R <sup>0</sup> 15-16 <sup>0</sup> , V <sup>0</sup> 15 <sup>40</sup> -16 <sup>0</sup>
11	6 040	10	09	07.7	03.9	30.6	.	.	= n-13 <sup>30</sup>
12	6 10	080	00	06.0	02.5	.	.	.	= n-n
13	6 05	040	07	05.3	07.5	07.1	.	.	= n-pj, = 12 <sup>30</sup> , R <sup>0</sup> 13 <sup>45</sup>
14	6 10	08	07	08.3	04.4	.	.	.	= n-n, = 13 <sup>30</sup> , R <sup>0</sup> 13 <sup>45</sup> -13 <sup>45</sup>
15	7 00	050	00	01.7	11.9	00.1	.	.	= n-11 <sup>30</sup>
16	7 050	020	09	05.3	11.8	.	.	.	= n-13 <sup>30</sup>
17	6 000	09	04	04.3	09.0	.	.	.	= n-n
18	6 09	09	10	05.3	03.5	00.0	.	.	= n-n, = 8 <sup>30</sup> , H <sup>30</sup> , H <sup>30</sup> , = 14 <sup>45</sup>
19	8 100	040	100	08.0	05.7	08.2	.	.	= 14 <sup>45</sup> , = 15 <sup>10</sup> -21 <sup>15</sup> , = 15 <sup>30</sup> -15 <sup>30</sup> , 10 <sup>40</sup> -20, R <sup>0</sup> 18 <sup>30</sup> -19 <sup>30</sup>
20	7 080	070	10	06.3	07.2	00.5	.	.	= n-11 <sup>30</sup>
21	6 100	10	10	10.0	00.0	01.3	.	.	= n-9 <sup>30</sup> , = 14 <sup>30</sup> , = n-10 <sup>30</sup>
22	8 020	100	06	06.0	03.9	03.6	.	.	= n-11 <sup>30</sup> , = 10 <sup>30</sup> , 20 <sup>30</sup> , = 11 <sup>30</sup>
23	8 090	080	100	05.0	04.3	01.3	.	.	= n-10 <sup>30</sup> , = 17 <sup>30</sup> , 17 <sup>30</sup> , R <sup>0</sup> 17 <sup>30</sup> , = 18 <sup>30</sup> , = 17 <sup>30</sup> , 21 <sup>30</sup>
24	8 10	080	03	07.0	09.5	40.9	.	.	= n-9 <sup>30</sup>
25	7 000	020	05	02.3	11.7	.	.	.	= n-10 <sup>30</sup>
26	7 040	020	03	01.7	10.6	.	.	.	= n-12 <sup>15</sup> , 17 <sup>30</sup> , R <sup>0</sup>
27	6 070	050	04	05.3	09.8	.	.	.	= n-n, □ n-pj, = 10 <sup>30</sup>
28	6 10	10	10	10.0	01.9	00.0	.	.	= n-n=n-n
29	6 000	10	10	06.7	03.7	01.6	.	.	= n-n
30	7 09	040	01	04.7	07.9	.	.	.	= n-10 <sup>30</sup>
31	6 09	060	06	07.0	04.4	.	.	.	= n-n, R <sup>0</sup> 8 <sup>30</sup> -10 <sup>30</sup> , = 9 <sup>30</sup> -10 <sup>30</sup> , V <sup>0</sup>
MES.	VRED.	05.5	06.8	05.8	06.0	213.4	105.1		

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$  Gr.  $\Delta G = +1h\ 04\ min.$ 

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D S	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodené pare e mm			Relativna vlažnost. v %				Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	747.5	747.4	747.9	17.6	25.7	21.4	21.5	25.8	17.5	-	13.0	11.4	10.7	86	46	56	63	E	1	ENE	1	NNE	2
2	748.3	748.0	747.5	18.3	23.1	21.3	21.0	23.9	16.6	-	11.7	12.3	12.0	74	58	63	65	SE	1	ENE	2	NNE	2
3	747.6	747.5	748.3	17.3	25.1	21.7	21.5	25.5	16.8	-	11.9	11.4	08.6	80	48	44	57	S	1	ENE	2	NE	2
4	749.0	748.7	749.7	16.3	26.8	21.3	21.4	26.8	15.1	-	10.8	10.0	11.0	78	38	56	57	NE	1	ENE	2	NNE	2
5	750.8	750.6	751.5	17.7	26.3	22.4	22.2	26.3	16.5	-	11.4	11.3	11.8	75	54	59	59	NNE	1	NE	2	NNE	2
6	753.6	752.9	752.9	17.1	24.3	19.8	20.3	25.5	16.2	-	11.7	12.8	11.8	80	56	68	68	-	0	NE	1	NNE	1
7	753.3	752.5	752.0	16.9	25.3	20.1	20.6	25.8	16.1	-	11.8	12.6	13.6	82	52	77	70	NNE	1	SSE	1	N	1
8	751.7	749.7	747.6	17.0	27.0	21.6	21.8	27.0	16.3	-	12.0	12.6	13.4	87	47	69	68	ENE	1	SSW	2	S	1
9	744.2	749.3	754.0	16.8	12.9	11.4	13.1	24.8	11.4	-	12.2	10.0	09.2	85	89	91	88	W	1	E	2	WSW	2
10	754.9	754.2	753.5	09.6	17.5	13.4	13.5	17.8	08.8	-	08.5	08.2	08.6	95	54	75	75	WSW	1	SSW	2	NW	1
11	752.2	752.4	753.6	13.2	22.0	17.9	17.8	22.0	12.2	-	08.3	10.3	10.8	73	52	70	65	WSW	2	SSW	2	NE	2
12	754.0	751.8	750.9	14.8	24.4	19.2	19.4	25.0	14.0	-	10.6	12.2	12.0	84	53	72	70	E	1	SSE	2	NW	1
13	750.4	751.6	757.0	15.9	21.9	12.2	15.6	22.3	12.2	-	11.8	10.2	08.4	87	52	79	73	NE	1	NE	3	NE	3
14	759.6	758.4	756.9	11.2	16.6	11.6	12.8	16.7	10.6	-	05.6	06.0	06.1	56	42	60	53	NE	2	NE	2	NNE	1
15	753.9	749.9	746.3	08.1	20.5	17.5	15.9	21.5	07.4	-	06.8	07.0	07.5	83	35	50	57	W	1	SSW	2	NW	1
16	745.5	745.9	748.4	15.5	17.0	13.3	14.8	19.0	12.5	-	07.5	08.9	07.4	57	61	64	61	NNE	2	E	3	ENE	2
17	748.7	749.6	749.4	09.0	07.4	06.5	07.6	13.3	06.9	-	07.0	06.7	06.7	82	88	91	87	ENE	2	E	2	NNE	1
18	747.4	747.8	749.6	07.6	08.4	07.6	07.9	08.6	06.6	-	06.9	07.6	07.6	88	92	96	92	ENE	2	NE	1	WSW	1
19	751.6	752.2	752.4	07.9	13.8	10.2	10.5	14.3	07.6	-	07.5	07.0	07.9	93	59	85	79	NW	1	SSE	2	ENE	2
20	749.3	749.4	749.1	07.6	10.1	09.2	09.0	10.1	06.8	-	06.5	06.4	07.9	83	70	87	80	SW	1	NE	2	NNE	1
21	746.8	747.6	748.2	08.7	12.5	05.8	10.2	12.7	08.6	-	07.8	07.8	08.0	93	72	89	85	WSW	1	SW	2	NE	1
22	748.7	748.6	749.0	09.8	14.6	11.0	11.6	14.6	08.6	-	08.3	09.9	09.0	92	79	91	87	E	1	S	2	NNE	1
23	749.6	748.7	748.8	10.1	14.3	10.9	11.6	15.0	08.2	-	07.8	08.2	08.9	93	64	86	81	NNE	1	NNE	3	NNE	3
24	749.6	749.3	750.4	11.9	14.6	12.4	12.8	15.1	11.8	-	07.0	07.4	08.8	68	59	81	69	NNE	2	ENE	1	ENE	1
25	751.3	752.1	753.9	10.5	16.2	11.8	12.6	16.5	10.2	-	08.7	07.5	07.9	92	54	76	74	-	0	SE	2	NNE	2
MES.	RED.	751.6	751.4	751.8	12.0	18.1	14.4	14.8	19.1	11.0	-	08.7	08.8	08.9	81	56	71	70	1.2	1.9	1.5		

1	749.1	745.7	743.5	09.9	18.8	16.0	15.2	19.3	09.2	-	06.2	09.8	07.5	67	60	79	69	W	2	WSW	4	W	2
2	747.0	747.4	746.7	08.4	07.7	06.1	07.1	16.7	06.1	-	07.9	07.5	06.6	96	95	93	95	E	2	S	2	NW	2
3	746.6	745.0	752.0	03.9	12.5	08.4	08.3	13.9	02.9	-	05.8	07.8	06.9	95	71	84	83	ENE	1	SSW	2	NNE	1
4	753.7	751.6	751.0	03.2	17.2	10.9	10.6	17.8	03.2	-	05.5	06.6	06.8	95	45	69	70	WNW	1	SW	3	W	2
5	750.7	750.4	749.9	09.3	19.6	14.4	14.4	19.6	08.5	-	07.3	08.6	09.3	83	50	76	70	WSW	2	SW	4	W	3
6	747.7	746.8	746.3	12.1	20.7	15.6	16.0	20.8	11.9	-	08.7	10.4	09.4	82	57	71	70	SW	1	WSW	4	W	3
7	745.4	745.7	744.8	14.0	22.6	16.1	17.2	22.6	12.3	-	09.9	11.5	10.8	82	56	79	72	WSW	2	WSW	4	W	2
8	744.7	743.7	743.2	13.1	21.7	16.0	16.7	21.9	12.8	-	09.7	10.2	10.3	86	52	68	69	SW	1	SSE	2	NNE	2
9	742.9	742.4	743.0	11.2	20.9	16.1	17.1	21.4	11.1	-	09.1	11.0	10.9	91	59	70	73	ENE	1	SSE	1	NNE	1
10	743.3	743.7	744.9	13.8	16.5	14.7	14.9	18.1	13.7	-	11.0	11.6	11.6	93	82	92	89	NE	1	ENE	2	NE	1
11	745.0	747.1	749.2	14.3	13.7	13.0	13.5	14.9	13.0	-	11.1	10.0	09.7	91	85	86	87	ENE	2	ENE	3	NNE	3
12	750.1	751.5	752.9	13.6	14.6	13.8	14.0	14.7	13.0	-	09.6	09.7	10.3	82	78	87	82	NNE	2	E	3	ENE	1
13	753.1	752.7	753.4	13.5	17.3	15.1	15.3	17.3	13.0	-	10.6	11.1	11.2	91	76	87	85	SSE	1	E	1	N	1
14	753.0	752.4	752.4	13.2	16.4	14.8	14.8	16.4	13.2	-	09.9	10.6	10.5	87	76	83	82	E	1	S	1	NE	1
15	751.9	752.3	753.6	13.3	16.5	13.2	14.1	16.5	13.0	-	10.0	09.2	08.9	87	65	78	77	ENE	1	ENE	2	NE	1
16	754.6	754.3	754.6	11.1	15.1	11.3	12.2	15.2	11.1	-	06.5	07.2	07.0	65	56	70	64	ENE	2	ENE	2	NE	2
17	755.5	754.2	754.8	05.9	14.4	09.3	05.7	14.5	05.9	-	06.3	07.0	06.6	90	57	76	74	NNE	1	SSE	2	NNE	1
18	755.5	754.9	754.4	03.9	14.4	10.8	10.0	14.7	03.9	-	05.7	07.6	07.8	94	62	80	79	ENE	1	S	2	NNW	2
19	754.8	754.0	754.9	06.8	18.6	14.2	13.5	19.1	06.7	-	06.6	07.7	07.8	89	48	64	67	WNW	2	WSM	3	NW	3
20	755.8	755.5	755.8	09.4	16.7	11.6	12.3	16.8	05.4	-	07.1	08.4	08.5	81	59	83	74	W	2	SSE	2	NNE	1
21	756.0	755.1	755.6	06.6	15.6	12.1	11.6	16.0	06.6	-	06.8	09.0	08.4	93	68	80	80	ENE	1	ESE	2	ENE	1
22	755.4	754.3	754.8	10.8	16.3	12.8	13.2	16.6	10.8	-	08.6	09.8	09.5	88	76	86	81	ESE	1	SSE	1	-	0
23	754.3	754.5	756.7	10.5	20.5	12.1	13.8	20.5	10.4	-	09.0	09.8	09.4	94	54	88	79	WSW	2	WNW	2	ENE	1
24	757.6	757.1	757.2	09.2	12.0	09.7	10.2	12.1	09.6	-	08.4	08.9	08.6	96	85	94	92	NE	1	SE	1	WSW	1
25	757.2	756.5	756.7	06.5	13.0	09.9	09.8	13.4	06.5	-	07.1	09.1	08.2	97	81	90	89	W	1	ESE	1	ENE	1
26	756.9	756.4	756.4	06.4</td																			

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 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$ 

Dan	Vrij.	Oblačnost N (0-10)					Isostatična broj seri	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6 08	030	10	07.0	06.8	14.2	.	== n-n			
2	5 09	09	07	08.3	01.5	.	.	== n-n			
3	8 010	050	00	02.0	09.5	.	.	== n-H <sup>15</sup>			
4	8 010	030	01	01.7	10.2	.	.	== n-g <sup>30</sup> , △ n-B <sup>30</sup>			
5	7 070	050	00	04.0	10.2	.	.	== 10 <sup>30</sup> -n			
6	6 010	06	00	02.3	08.0	.	.	== rj-n			
7	5 000	09	00	03.0	07.2	.	.	== rj-n			
8	6 000	000	00	00.0	10.4	.	.	== rj-n			
9	6 030	100	02	05.0	03.4	.	.	== H-17 <sup>45</sup> , ○ <sup>tr-o</sup> H <sup>45</sup> -16 <sup>45</sup> i, F <sup>tr-o</sup> H <sup>20</sup> -12 <sup>45</sup> , F <sup>tr-o</sup> 12 <sup>00</sup> -16 <sup>30</sup> i, ○ <sup>tr-o</sup> 12 <sup>00</sup> -14 <sup>15</sup>			
10	8 10	040	02	05.3	07.1	17.9	.	== H-10 <sup>30</sup> , △ n-dp			
11	8 09	030	00	04.0	08.4	.	.	== n-g <sup>45</sup> -16 <sup>30</sup> -n			
12	8 000	000	00	00.0	11.2	.	.	== n-H <sup>15</sup>			
13	8 000	030	100	04.3	08.9	.	.	== n-H <sup>15</sup> , ○ <sup>tr-o</sup> 19 <sup>30</sup> -10V-i			
14	8 010	060	00	02.3	10.5	05.5	.	== n-g <sup>35</sup>			
15	8 080	040	00	04.0	10.9	.	.	== n-g <sup>35</sup>			
16	7 000	09	100	06.3	03.2	.	.	== n-n, ○ <sup>tr-o</sup> 20 <sup>30</sup> -n			
17	6 100	100	100	10.0	00.0	02.5	.	== n-n, ○ <sup>tr-o</sup> n-n-i			
18	7 100	100	10	10.0	00.0	23.2	.	● <sup>tr-o</sup> n-n-i, □ <sup>tr-o</sup> 17 <sup>30</sup> -KV			
19	7 10	10	100	10.0	02.0	06.1	.	○ <sup>tr-o</sup> rj-10 <sup>30</sup> , ○ <sup>tr-o</sup> 19 <sup>45</sup> -n-i			
20	6 10	10	10	10.0	00.0	16.9	.	● <sup>tr-o</sup> n-6 <sup>30</sup> -B <i>i</i> , ○ <sup>tr-o</sup> rj-10V			
21	6 10	080	09	09.0	02.3	00.7	.	○ <sup>tr-o</sup> n = rj-10V			
22	6 10	09	05	05.3	00.6	.	.	== rj-n, ○ <sup>tr-o</sup> H <sup>15</sup>			
23	7 10=	09	100	09.7	00.1	00.6	.	== rj-8 <sup>30</sup> , = 8 <sup>30</sup> -12 <sup>45</sup> , 17 <sup>30</sup> -n; ○ <sup>tr-o</sup> 17 <sup>10</sup> -n-i			
24	6 10	09	05	09.3	02.1	01.8	.	== n-n			
25	7 10	06	00	05.3	05.9	.	.	== rj-10			
26	7 000	030	00	01.0	07.4	.	.	== n-n, △ rj-dp			
27	7 10	030	09	07.3	02.5	.	.	== n-n			
28	6 010	010	00	00.7	08.9	.	.	== n-g <sup>35</sup>			
29	6 020	070	09	06.0	05.8	.	.	== n-n, △ rj-dp			
30	6 010	040	00	01.7	10.0	.	.	== n-13 <sup>30</sup>			
MES. VRED.		05.4	05.9	04.6	05.3	175.2	89.5				

1	6 010	09	10	06.7	04.8	.	.	== n-n, △ n-dp, F <sup>tr-o</sup> H-17			
2	5 100	100	07	09.0	00.0	37.9	.	== n-10 <sup>30</sup> , ○ <sup>tr-o</sup> n-17 <sup>45</sup>			
3	8 00=	030	00	01.0	07.7	18.8	.	△ <sup>tr-o</sup> n-8 <sup>30</sup> , ○ <sup>tr-o</sup> 6 <sup>30</sup> -7 <sup>10</sup> , □ <sup>tr-o</sup> 7 <sup>10</sup> -7 <sup>10</sup> , ○ <sup>tr-o</sup> 7 <sup>45</sup> -12 <sup>45</sup> , ○ <sup>tr-o</sup> 16 <sup>30</sup> -16 <sup>45</sup>			
4	9 010	020	01	01.3	09.3	00.0	.	○ <sup>tr-o</sup> 9 <sup>30</sup> , △ <sup>tr-o</sup> n-dp, F <sup>tr-o</sup> H <sup>40</sup> -16 <sup>30</sup>			
5	7 010	050	05	03.7	09.0	.	.	○ <sup>tr-o</sup> 9 <sup>30</sup> , □ <sup>tr-o</sup> n-dp, ○ <sup>tr-o</sup> 10 <sup>30</sup> , F <sup>tr-o</sup> H <sup>30</sup> -16 <sup>30</sup>			
6	8 010	060	03	03.3	08.9	.	.	== n-8 <sup>30</sup> , F <sup>tr-o</sup> H <sup>20</sup> -15			
7	7 050	060	03	04.7	08.5	.	.	== n-g <sup>30</sup>			
8	6 000	020	02	01.3	09.4	.	.	== rj-n, △ rj-B <sup>30</sup>			
9	6 010	010	10	04.0	08.8	.	.	== n-n			
10	6 09	10	100	09.7	01.4	01.3	.	== n-n, ○ <sup>tr-o</sup> 10-10 <sup>45</sup> i, 13 <sup>45</sup> -n			
11	5 10	100	100	10.0	00.0	00.8	.	== n-n, ○ <sup>tr-o</sup> n-8 <sup>30</sup> -9 <sup>30</sup> , 12 <sup>45</sup> -n			
12	5 10	10	10	10.0	00.0	06.5	.	== n-n, ○ <sup>tr-o</sup> H <sup>30</sup>			
13	4 10	10	10	10.0	00.0	00.0	.	== n-n			
14	5 10	10	10	10.0	00.0	00.0	.	== n-n			
15	6 10	090	10	09.7	00.0	.	.	== n-n			
16	6 040	010	00	01.7	08.1	.	.	== n-n			
17	6 020	010	00	01.0	08.2	.	.	== n-n, △ n-dp			
18	6 02=	000	00	00.7	07.4	.	.	○ <sup>tr-o</sup> n-dp, ○ <sup>tr-o</sup> n-9 <sup>30</sup> = 9 <sup>30</sup> -n			
19	6 000	000	00	00.0	09.2	.	.	○ <sup>tr-o</sup> n-n, △ <sup>tr-o</sup> n-dp			
20	6 000	000	00	00.0	08.2	.	.	○ <sup>tr-o</sup> n-n, △ <sup>tr-o</sup> n-dp			
21	5 02=	000	07	03.0	04.2	.	.	△ <sup>tr-o</sup> n-dp, == n-B <sup>30</sup> , = 8 <sup>30</sup> -n			
22	3 08=	02=	02	04.0	02.6	.	.	○ <sup>tr-o</sup> n-15 <sup>30</sup> , == 15 <sup>30</sup> -n			
23	6 040	010	02	02.3	08.1	.	.	○ <sup>tr-o</sup> n-n, △ <sup>tr-o</sup> n-B <sup>30</sup>			
24	3 10=	10	10	10.0	00.0	.	.	○ <sup>tr-o</sup> 9 <sup>30</sup> , == 9 <sup>30</sup> -13 <sup>30</sup> -n			
25	4 10=	080	00=	06.0	02.8	.	.	○ <sup>tr-o</sup> 9 <sup>30</sup> , == 9 <sup>30</sup> -12 <sup>45</sup> -n, 16 <sup>30</sup> -n; == 12 <sup>45</sup> -16 <sup>45</sup>			
26	4 10=	040	00	04.7	03.4	.	.	○ <sup>tr-o</sup> n-9 <sup>45</sup> , == 9 <sup>30</sup> -10 <sup>45</sup> , == 10 <sup>45</sup> -n			
27	3 10=	040	100	08.0	09.9	.	.	○ <sup>tr-o</sup> 11 <sup>30</sup> , 16 <sup>30</sup> -n, == 11 <sup>30</sup> -16 <sup>30</sup>			
28	4 10=	080	00=	06.0	01.8	.	.	○ <sup>tr-o</sup> 10 <sup>30</sup> , == 10 <sup>30</sup> -12 <sup>45</sup> , 16 <sup>30</sup> -n; == 12 <sup>45</sup> -16 <sup>30</sup>			
29	3 10	100	10	10.0	00.0	.	.	○ <sup>tr-o</sup> 8 <sup>30</sup> -H <sup>30</sup> -n; ○ <sup>tr-o</sup> 11 <sup>30</sup> -13 <sup>30</sup> -n, == 11 <sup>30</sup> -n			
30	4 10	10	10	10.0	00.0	00.1	.	== n-n			
31	5 10	100	10	10.0	00.0	00.0	.	== n-n, ○ <sup>tr-o</sup> 8 <sup>30</sup> -10 <sup>45</sup> , 13 <sup>30</sup> -H <sup>30</sup>			
MES. VRED.		05.8	05.5	05.2	05.5	132.7	65.4				

$\varphi = 45^{\circ}49' N$   $\lambda = 15^{\circ}59' E$  Gr.  $\Delta G = +1h\ 04\ min.$ 

BR. ST. 57

	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodené pare e mm			Relativna vlažnost U %			Pravac i jačina vetrova D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	746.7	745.5	747.9	09.6	13.9	11.1	11.4	13.9	09.6	-	08.3	09.0	08.6	93	76	87	85	S 1	S 1	ENE 3	
2	749.8	749.0	748.8	09.0	13.4	09.1	10.2	13.4	09.0	-	07.8	07.1	06.6	90	62	76	76	NE 1	SM 2	W 1	
3	746.8	746.2	747.0	06.8	16.1	12.6	12.0	17.2	06.8	-	06.2	07.8	06.0	84	57	73	71	WSW 2	WSW 3	W 3	
4	746.2	745.9	747.3	14.0	17.3	16.6	16.1	18.0	10.3	-	09.3	10.6	10.4	77	72	73	74	W 3	WSW 3	WW 2	
5	749.3	751.7	752.2	13.9	11.0	11.3	11.9	16.6	10.9	-	11.0	09.2	09.2	93	93	91	92	ENE 2	ENE 2	ENE 1	
6	751.2	750.3	750.9	10.7	12.2	11.7	11.6	12.4	10.3	-	09.0	09.9	09.9	93	93	96	94	SE 1	S 1	WW 1	
7	753.3	754.5	755.6	10.6	12.0	10.2	10.8	12.0	10.2	-	09.4	09.6	08.8	98	91	94	94	NE 1	NNE 1	NN 1	
8	756.5	756.7	757.6	08.7	09.5	08.9	09.0	10.2	08.3	-	08.0	08.4	08.2	95	94	96	95	WSW 1	SSW 1	S 1	
9	751.6	756.1	754.8	07.3	08.8	08.0	08.0	08.9	07.3	-	07.5	08.0	07.6	97	94	95	95	WSW 2	SW 1	WSW 2	
10	752.5	753.0	754.8	07.0	17.4	12.7	12.5	18.4	06.5	-	07.0	08.1	09.0	93	54	82	76	W 1	W 2	W 1	
11	754.6	752.8	752.4	07.3	17.0	12.8	12.5	17.7	07.3	-	07.2	08.6	08.3	93	59	75	76	ENE 1	SSW 1	S 1	
12	756.6	746.7	743.8	08.7	17.7	14.7	14.0	17.7	07.6	-	06.4	08.7	08.4	75	57	67	66	WW 2	WW 3	W 4	
13	741.8	740.3	740.3	14.4	07.7	03.8	07.4	15.4	03.8	-	09.1	07.2	05.4	74	91	89	85	E 1	NE 4	ENE 3	
14	742.8	741.9	738.7	03.2	05.9	04.8	04.7	06.0	01.2	-	05.5	05.9	05.5	95	85	86	89	NE 1	WSW 2	SSW 2	
15	733.0	735.1	735.2	04.5	08.2	07.6	07.0	08.9	03.2	-	05.2	08.0	07.2	83	97	91	90	W 3	N 1	ENE 2	
16	731.7	732.9	734.5	06.9	06.4	05.4	06.0	07.7	05.4	-	07.3	06.7	05.7	97	94	85	92	ENE 2	ENE 1	E 2	
17	736.1	734.8	735.3	02.8	08.6	05.9	05.8	08.6	02.8	-	05.2	05.7	05.9	92	67	84	81	SW 1	S 1	WW 1	
18	740.3	742.5	744.9	01.5	04.3	01.4	02.2	05.9	01.4	-	04.8	05.8	04.9	93	94	98	95	W 1	SSE 1	N 1	
19	748.0	749.9	752.0	00.0	03.0	01.7	01.6	03.0	00.0	-	04.5	04.8	05.1	100	84	98	94	ENE 1	SW 2	SSE 1	
20	751.3	748.6	746.5	-00.2	02.1	00.4	00.7	02.1	-00.2	-	04.5	05.2	04.2	100	96	89	95	S 1	SSE 1	SW 2	
21	743.8	740.1	735.8	-00.9	06.7	03.7	03.3	09.4	-00.9	-	03.8	05.0	04.6	85	66	76	78	S 1	SW 1	ENE 2	
22	734.5	737.9	742.2	09.9	12.2	07.5	09.3	12.2	03.7	-	08.7	05.1	05.0	95	48	64	69	W 2	NW 2	NE 2	
23	745.1	748.3	750.1	04.7	05.0	03.0	03.9	07.6	03.0	-	06.0	05.5	05.0	94	84	87	88	ENE 2	SSE 2	SW 1	
24	750.1	747.1	746.8	00.1	03.1	01.2	01.4	03.4	-00.1	-	04.5	04.7	04.4	98	82	88	89	WSW 1	SSE 2	ENE 1	
25	742.5	741.7	741.1	01.7	08.4	06.0	05.5	08.4	00.7	-	04.3	05.7	05.6	84	70	80	78	ENE 2	E 1	NE 3	
26	737.2	734.0	735.4	02.6	02.9	02.8	02.8	06.1	02.2	-	04.5	05.0	05.1	81	90	91	87	NE 3	NNE 3	E 1	
27	737.3	740.5	744.8	00.7	03.3	02.8	02.4	03.3	00.5	-	04.7	05.3	05.1	96	92	92	93	WSW 2	WSW 1	E 1	
28	748.8	750.6	752.6	01.4	03.3	01.9	02.1	03.9	01.4	-	04.4	04.3	03.5	87	74	67	76	NE 1	ENE 2	ENE 2	
29	754.1	753.0	752.0	-01.0	02.5	-00.6	00.1	02.5	-01.0	-	02.9	03.5	03.2	68	64	74	69	ENE 2	ESE 2	NE 1	
30	748.0	745.5	746.4	-00.3	01.3	-00.9	-00.2	01.5	-00.9	-	03.3	04.3	03.9	73	86	90	83	SE 1	SSE 1	ENE 1	
MES.	VRED.	746.0	745.8	746.3	05.5	08.7	06.6	06.9	09.7	04.3	-	06.3	06.8	06.4	89	79	84	84	1.5	1.7	1.7

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1	747.0	746.7	747.1	-00.6	00.2	-00.2	-00.2	00.4	-00.7	-	03.6	03.6	04.2	82	77	92	84	ENE 1	ENE 1	ENE 1
2	747.2	747.8	751.1	-00.1	02.7	01.0	01.2	02.7	-00.3	-	04.1	03.6	03.1	91	66	62	73	ENE 1	NE 3	ENE 3
3	753.9	755.6	758.4	00.9	01.7	01.9	01.6	01.9	00.5	-	03.1	03.4	03.8	63	65	72	67	SW 1	NNE 3	ENE 3
4	760.8	759.4	758.6	-01.4	02.3	-01.6	-00.6	02.4	-01.6	-	03.3	03.2	03.0	81	60	74	72	NNE 1	ESE 2	ENE 1
5	755.2	751.9	749.0	-06.8	-04.1	-05.3	-05.4	-01.6	-06.8	-	02.4	02.8	02.7	87	82	87	85	SE 1	ESE 2	SSE 1
6	744.2	740.2	738.8	-06.6	-01.2	01.2	-01.4	01.2	-06.8	-	02.5	03.0	04.2	89	72	63	81	S 1	S 1	ENE 2
7	741.3	745.7	746.6	03.0	05.2	04.0	04.1	05.3	01.2	-	05.3	05.0	05.3	94	75	87	85	W 1	WSW 2	NW 2
8	749.1	747.8	746.8	-00.3	02.5	02.5	01.8	04.0	-00.6	-	04.5	05.0	04.9	100	92	90	94	NNW 1	ENE 2	ENE 1
9	745.4	745.3	745.8	02.0	02.8	03.0	02.7	03.0	01.7	-	05.0	05.3	05.2	95	95	92	94	ESE 1	ESE 1	ENE 2
10	747.6	750.1	753.9	02.8	02.9	01.9	02.4	03.2	01.9	-	04.9	05.0	04.7	87	90	89	89	NE 3	ENE 2	ENE 2
11	758.3	760.6	762.7	00.2	00.3	-00.8	-00.3	01.9	-00.8	-	04.0	03.6	03.3	86	77	75	79	E 2	ENE 2	ENE 2
12	763.9	764.3	763.6	-02.6	-02.2	-02.1	-02.3	-00.8	-02.8	-	03.1	02.8	02.9	83	74	73	77	ENE 2	E 2	E 1
13	761.7	761.7	762.4	-02.7	-02.0	-03.6	-03.0	-01.7	-03.6	-	02.6	02.5	02.4	70	64	68	67	NE 2	E 2	ENE 1
14	762.3	761.7	766.2	-02.7	-01.4	-01.2	-01.6	-00.2	-04.3	-	03.0	03.1	03.2	79	76	76	77	SW 1	W 1	W 2
15	759.0	757.8	759.3	-00.7	02.7	02.5	01.8	03.5	-01.4	-	03.7	04.4	05.0	86	80	91	86	ENE 1	ENE 1	NNW 1
16	763.1	762.7	761.9	00.7	03.2	03.2	02.6	04.0	00.3	-	04.3	04.7	05.0	85	81	87	86	SE 1	WSW 2	M 2
17	761.1	761.3	761.7	00.4	01.8	00.6	01.0	03.9	-00.2	-	04.4	04.1	03.7	93	79	76	83	S 1	NNE 2	N 1
18	760.0	758.3	758.8	-00.8	-00.1	-02.2	-01.3	01.0	-02.2	-	03.6	03.4	03.3	83	75	85	81	E 1	SSE 1	ENE 1
19	757.8	757.6	758.3	-03.1	-02.9	-03.0	-03.0	-02.2	-03.9	-	03.2	03.0	03.0	89	79	81	83	SE 1	ENE 1	E 1
20	757.8	758.3	759.1	-03.2	-03.1	-03.5	-03.3	-02.8	-03.9	-	03.0	02.9	02.8	84	81	80	82	S 1	SSE 1	S 2
21	758.9	758.3	759.3	-04.3	-04.0	-03.5	-03.8	-03.0	-04.3	-	03.0	02.9	02.8	90	86	80	85	S 1	SSW 1	E 1
22	761.1	761.6	761.8	-03.1	-02.0	-01.9	-02.2	-01.6	-04.0	-	02.8	02.8	03.4	78	70	83	77	SSE 2	W 1	SW 2
23	760.6	759.9	760.1	-02.7	-02.6	-03.5	-03.1	-01.8	-03.6	-	03.0	03.0	03.0	79	80	84	81	SW 2	WSW 2	SSE 2
24	758.7	755.2	756.9	-03.9	01.0	02.1	00.3	02.1	-05.1	-	03.0	03.7	04.4	88	76	82	82	S 1</		

BR. ST. 57

$$H_s = 157 \text{ m} \quad H_b = 162,5 \text{ m} \quad h_t = 6.0 \text{ m} \quad h_r = 2.0 \text{ m}$$

Den	Hod. Vrh O	Oblačnost N (0-10)					Padačina R mm	Snežni pokrivač h cm	Rezovj vremena w
		14	7	14	21	Sred Dnes			
1	4	10≡	10	10*	10.0	00.0	.	.	$\equiv^o n-730, \equiv^o 730 n, \bullet^{tr-o} 4430 n i$
2	6	10	09	00	06.3	02.9	08.7	.	$\bullet n-n, \equiv^o n-n i$
3	7	10	08○	00	06.0	04.1	.	.	$\equiv^o n-10^o 1330 n$
4	7	09	10	05	09.3	02.8	.	.	$\equiv^o n-9^o, \bullet^{tr-o} 1330$
5	6	10*	10*	10	10.0	00.1	09.3	.	$\equiv n-n, \bullet^{tr-o} n-1310$
6	6	10	10	10	10.0	00.0	26.7	.	$\equiv^o n-n, \bullet^{tr-o} 345^o 1345^o, \bullet^o 730-830$
7	5	100≡	10	10	10.0	00.0	00.5	.	$\equiv^o n-830, \bullet^o 730-1130, \equiv^o 830 n$
8	4	10*	10	10*	10.0	00.0	00.1	.	$\equiv^o n-16^o, \bullet^o 730-1030, 1230 n, \equiv^o 745^o 915^o, \equiv^o 1630 n$
9	4	10*	10	10*	10.0	00.0	00.1	.	$\equiv^o n-830, \bullet^o 730-1030, \equiv^o 830-1630, \equiv^o 1630 n$
10	7	09	10	00	06.3	00.1	.	.	$\equiv n-145^o, \bullet^o 730-830$
11	6	08≡	d0○	00	02.7	07.6	.	.	$\Delta^o n-830, \equiv^o n-830, \equiv^o 830 n$
12	6	07○	08○	10	06.3	06.0	.	.	$\equiv n-n, \bullet^o 11^o-14^o, \bullet^o 1315^o 2320$
13	6	10	10*	10*	10.0	00.0	.	.	$\equiv n-n, \bullet^o 11^o-14^o, \bullet^o 1315^o 2230, 12^o 1330-2445^o, \bullet^o 2230 n$
14	7	10	10	10	10.0	00.0	46.3	.	$\equiv n-1230, 1230 n, \bullet^o 730$
15	3	03	10*	10	07.7	01.2	00.0	.	$\equiv 1030 n, \bullet^o 1030 1730 i, \equiv^o 1230-1430$
16	4	10*	10*	10*	10.0	00.0	29.4	.	$\equiv n-j-n, \bullet^{tr-o} n-j-n$
17	8	02	07○	10	06.3	05.0	09.9	.	$\equiv n-830, \bullet^o 1130-1230, \bullet^o 1315^o$
18	2	03≡	10*	10*	07.7	01.0	00.2	.	$\equiv^o n-j-830, 1130-1530, \bullet^o 1315^o n, 1530 n$
19	2	10≡	10≡	10	10.0	00.0	.	.	$\equiv n-j-1530, \bullet^o 1530 n$
20	5	10≡	10	10	10.0	00.0	.	.	$\equiv^o n-j-1030, \bullet^o 1030 n$
21	6	10	02○	10	07.3	05.7	.	.	$\equiv n-1315^o, 1645^o n$
22	7	10	09	10	09.7	02.1	11.9	.	$\equiv n-1430, \bullet^o 11^o-1645^o n$
23	6	10*	10	00	06.7	00.0	00.3	.	$\equiv n-1430, \bullet^o n-j-1330$
24	6	10≡	01○	10	07.0	05.4	00.4	.	$\equiv n-1430, \bullet^o 1030-1130, \equiv^o 1130 n$
25	5	06	10	10*	08.7	04.2	.	.	$\equiv n-1330, \bullet^o n-j-1030, \bullet^o 1030 n$
26	6	10*	100*	10*	10.0	00.0	00.8	.	$\equiv n-1130, \bullet^o 11^o-830, 1445 n, \bullet^o 830-1450$
27	5	100*	10*	10	10.0	00.0	11.7	.	$\equiv n-n, \bullet^o n-730, \bullet^o 730-830, \bullet^o 830-1450, \boxed{}$
28	7	10	10	10	10.0	00.2	03.1	.	$\equiv n-1030$
29	7	04	06○	06	05.3	05.1	.	.	$\equiv n-1030$
30	6	10	10*	10*	10.0	00.0	.	.	$\equiv n-n, \bullet^o 1230 n i, \sim 1730 n$

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1	5	10	10*	10*	10.0	00.0	01.1	.	= n-n, $\cap$ $n-10^{15}$ , $\times^{tr-o} 12^m - n$ , $\boxed{n}$
2	6	10*	09	09	09.3	00.2	03.2	04	= n-n, $\times^{tr-o} n-10^{15}$ , $\boxed{n}$
3	7	10	10	10	10.0	02.5	00.0	01	= n-10 <sup>15</sup> , 15 <sup>32</sup> n; $\times^{tr} 16^{15} \cap 17^{15}$ , $\boxed{n}$
4	6	00	01○	00	00.3	06.8	00.0	.	= n-n,
5	4	00	10	10	06.7	01.8	.	.	$\sqrt[n]{n-10^{15}} = n-16^{15}, \equiv^o 10^{15} 12^{15}, 16^{15} n$
6	4	10	10	10	10.0	00.0	00.0	.	V <sup>o</sup> n-n = $\equiv^{o-1} n-8^{15} = 8^{15} 10^{30} = 10^{22} n, \times^{tr} 20^{15} n$
7	6	10	10	10	00	06.7	00.7	05.3	$\bullet^{tr-o} n-8^{15} = \equiv^o n-7^{15} = 7^{15} n$
8	5	10	10	10*	10.0	00.0	00.6	.	= n-n, $\times^{tr-o} n-10^{15}$ , $\times^{tr} 14^{32} n; \times^{tr-1} 7^{15} 9^{15} = 8^{15} 9^{15}, \bullet^o 13^{32} 14^{30}$
9	4	10	10	10	10.0	00.0	01.6	.	= n-n, $\times^{tr-o} n-10^{15}$ , $\times^{tr} 14^{32} n$
10	5	10	10	10	10.0	00.0	09.3	.	= n-n, $\bullet^{tr-o} n-20^{30}$
11	6	10*	10	10	10.0	00.0	03.5	.	V <sup>o</sup> n-n = $\equiv^{o-1} n-8^{15} = 8^{15} 10^{30} = 10^{22} n, \times^{tr} 20^{15} n$
12	6	10	10	10	10.0	00.2	00.0	.	$\bullet^{tr-o} n-8^{15} = \equiv^o n-7^{15} = 7^{15} n$
13	5	10	10	10	10.0	00.0	.	= n-n,	
14	4	10	10	10	10.0	00.0	.	= n-n,	
15	3	10	10	10*	10.0	00.0	.	= n-7 <sup>30</sup> , 16 <sup>32</sup> n; $\equiv^o 7^{32} 16^{30}, \bullet^o 13^{25} n$	
16	5	10	01○	10	07.0	02.3	01.0	.	= n-n,
17	5	01	10	10	07.0	00.0	.	= n-n,	
18	6	10	08○	04	07.3	01.5	.	= n-n,	
19	5	10	10	10	10.0	00.0	.	= n-n, $\times^{tr} 8^{15}$	
20	5	10	10	10	10.0	00.0	00.0	.	= n-n,
21	5	10	10	10	10.0	00.0	.	= n-n, $\Delta^{tr} 12^{15}, 13^{15}$	
22	6	10	10	10	10.0	00.0	00.0	.	= n-n,
23	6	10	10	10	10.0	00.0	.	= n-n,	
24	4	09	10	03	07.3	00.0	.	= n-n, $\bullet^o 19^{15}$	
25	5	10	07○	01	06.0	03.2	04.6	.	$\bullet^{tr-o} n-8 = \bullet^o 16^{30}$
26	5	01	08○	09	06.0	02.3	02.7	.	= n-n,
27	5	06	07○	08	07.0	02.7	.	= n-n,	
28	4	10	10	10*	10.0	00.0	.	= n-n, $\times^{tr} 14^{32}, 15^{15}$	
29	3	10	10	10	10.0	00.0	16.5	.	= n-16 <sup>30</sup> = 16 <sup>32</sup> 17 <sup>30</sup> , $\equiv^o 17^{32} n$
30	5	10	10	10	10.0	00.1	.	= n-10 <sup>30</sup> , $\times^{tr} 9^{32} 8 = 10^{22} n$	
31	6	04	01○	08	04.3	07.8	00.1	.	$\bullet n = n-10^{30}, 17^{32} n$

VIRILJIVOST OSMATRANA U 13 ČASOVA

$\varphi = 43^{\circ}31' N$   $\lambda = 16^{\circ}26' E$  Gr.  $\Delta G = +1h\ 06\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	-7	14	21			
	1	754.3	753.9	753.0	04.0	08.8	08.6	07.5	09.6	03.9	-	03.9	05.6	06.5	65	66	78	70	NE	2	ESE	3	ESE
2	752.4	752.7	755.2	09.6	10.1	10.4	10.1	11.1	07.8	-	07.0	08.2	08.0	78	88	85	84	ESE	5	ESE	4	E	3
3	756.5	757.0	758.1	11.0	10.2	09.8	11.0	11.5	07.8	-	08.3	08.8	09.0	84	94	99	92	ESE	3	ESE	3	NNE	1
4	758.6	759.5	761.2	10.6	11.8	11.8	11.5	12.3	09.5	-	09.4	09.2	08.1	98	89	78	88	E	3	ESE	4	ESE	5
5	762.9	764.0	764.8	09.8	10.4	09.1	09.6	12.0	08.4	-	07.6	07.1	05.7	83	75	65	74	ESE	5	ESE	4	E	2
6	764.7	763.4	762.4	08.8	11.4	09.6	09.9	11.7	07.1	-	06.2	07.0	07.2	73	69	81	74	NE	2	-	0	SSW	1
7	761.2	759.7	758.4	09.0	11.2	10.1	10.1	11.6	08.6	-	07.3	08.4	08.2	85	84	88	86	SW	1	-	0	NW	1
8	754.6	754.2	754.2	09.0	09.8	05.4	07.4	10.6	05.2	-	08.1	04.9	02.9	94	44	43	60	WNW	1	NNE	5	NNE	3
9	754.0	752.9	751.7	03.8	08.8	06.0	06.2	09.0	03.1	-	02.6	03.4	02.6	43	44	51	46	NE	3	SSE	1	NNE	2
10	748.7	747.7	747.9	06.8	09.6	09.9	09.1	10.2	05.1	-	03.6	05.0	07.8	49	63	86	66	ESE	3	ESE	5	ESE	4
11	745.9	744.2	743.7	10.6	11.5	11.2	11.1	12.0	09.7	-	07.7	08.0	08.6	80	79	86	82	SE	6	SSE	6	SSE	6
12	739.4	740.9	739.8	12.0	11.8	11.4	11.7	13.5	11.0	-	07.8	07.9	07.8	74	76	78	76	S	7	S	4	SSE	4
13	738.5	742.2	745.6	08.4	07.2	06.3	07.1	11.6	06.2	-	07.1	06.7	05.7	86	88	80	85	SW	3	WNW	2	WSW	1
14	748.9	750.0	749.9	04.5	09.4	08.0	07.5	09.7	03.9	-	03.7	05.1	05.5	58	58	69	62	-	0	SE	1	SE	4
15	747.0	743.4	745.4	08.2	08.8	08.5	08.5	09.5	07.6	-	07.3	08.2	05.8	90	96	65	85	SE	8	SE	8	NNE	1
16	746.7	746.6	747.1	06.5	08.0	05.4	06.3	09.2	05.1	-	03.9	04.5	03.5	54	56	52	54	NE	1	WNW	1	NNE	4
17	749.3	749.5	750.4	04.8	06.6	04.4	05.1	07.1	04.0	-	02.8	02.8	02.6	43	39	42	41	NNE	5	NNE	6	NNE	5
18	747.9	747.6	748.8	04.9	06.4	05.2	07.0	04.4	-	03.0	02.8	02.7	46	39	40	42	NNE	5	NNE	5	NNE	2	
19	749.9	750.8	751.8	03.1	08.2	05.6	05.6	08.7	02.6	-	02.0	04.0	03.3	36	49	49	45	NE	3	SSW	1	-	0
20	752.7	752.7	752.7	04.8	07.9	07.9	07.1	08.3	04.0	-	03.8	05.5	07.1	59	69	88	72	NE	2	ESE	3	ESE	3
MES.	VRED.	750.6	750.4	750.7	08.2	10.4	09.1	09.2	11.2	07.2	-	06.2	06.8	06.6	72	71	74	72	3.1	3.2	2.8		

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1	743.0	743.5	743.9	10.6	11.9	10.0	10.6	12.7	05.9	-	08.7	08.0	06.8	91	77	74	81	WSW	1	NNW	2	NE	1
2	743.0	745.8	747.3	05.8	05.4	06.2	05.9	10.4	04.2	-	06.1	05.4	03.9	89	80	55	75	NNE	3	NNE	4	NNE	3
3	748.0	748.7	749.4	03.4	08.6	05.6	05.8	08.8	02.6	-	03.2	03.8	03.1	55	45	45	48	NNE	3	NNE	1	NNE	4
4	750.6	751.3	752.4	03.2	09.2	07.4	06.8	09.6	02.7	-	02.7	02.8	03.2	46	32	42	40	NE	1	NNW	1	NNE	2
5	752.9	753.6	754.1	06.8	11.5	08.6	08.9	11.9	05.5	-	02.7	06.1	06.5	37	60	78	58	NNW	1	NNW	2	NNW	2
6	752.0	750.7	750.1	07.5	08.0	07.5	07.6	10.0	06.4	-	05.8	06.7	05.6	76	72	68	72	ENE	2	ESE	1	E	3
7	754.9	754.6	754.8	08.4	11.8	09.6	09.9	12.0	08.0	-	05.6	07.4	07.2	68	72	81	74	ENE	2	ESE	4	E	3
8	753.1	750.9	748.2	09.2	12.2	10.3	10.5	12.4	05.4	-	05.6	06.8	06.7	64	64	71	66	ENE	3	ESE	3	NE	3
9	744.5	745.5	746.3	10.6	11.9	11.3	11.3	12.4	08.8	-	07.6	07.9	07.1	79	76	71	75	ENE	4	ESE	2	-	0
10	747.2	745.2	743.1	11.2	12.4	12.0	11.9	12.7	10.4	-	07.5	08.7	10.0	75	80	95	83	E	2	ESE	5	ESE	6
11	740.6	741.8	743.1	12.5	11.2	11.2	11.4	13.2	05.2	-	05.6	07.9	06.8	88	80	69	79	ENE	2	ESE	3	ESE	3
12	739.3	740.3	743.0	12.6	14.9	11.8	12.8	15.2	10.8	-	09.4	09.3	08.3	86	73	80	80	SE	6	SSW	4	SW	2
13	746.6	747.3	746.4	10.5	14.2	11.6	12.1	14.6	09.7	-	07.0	07.3	06.3	74	60	60	65	NE	2	ESE	1	NNE	2
14	741.5	740.3	743.6	11.4	12.6	09.2	10.6	13.0	09.2	-	05.5	04.3	05.1	55	39	59	51	N	2	NNE	3	W	2
15	745.8	746.4	746.9	07.0	09.0	07.1	07.6	09.6	06.8	-	04.9	06.5	06.9	65	76	91	77	E	2	ESE	2	NE	2
16	746.8	747.5	748.2	06.0	06.6	06.8	06.6	09.6	05.4	-	05.4	06.2	05.8	77	85	79	80	E	3	NE	2	NE	2
17	748.5	750.5	752.3	04.3	10.0	08.2	07.2	10.5	03.5	-	05.8	05.2	04.0	93	57	49	66	WNW	2	NNW	3	NNE	3
18	754.1	755.7	756.4	05.9	09.9	09.9	08.9	10.2	05.1	-	03.9	06.3	06.9	56	69	75	67	E	2	ESE	3	ESE	3
19	755.9	755.0	754.6	10.2	11.1	11.4	11.0	11.8	05.3	-	07.4	08.0	08.3	79	81	82	81	ESE	5	ESE	5	SE	5
20	753.5	753.0	751.6	11.4	13.4	12.2	12.3	14.2	11.0	-	09.2	09.1	09.1	91	79	86	85	ESE	4	ESE	5	ESE	5
21	748.1	746.9	747.0	12.2	12.4	13.4	12.9	14.2	10.8	-	09.0	09.4	09.6	85	87	83	85	SE	7	SE	7	ESE	6
22	748.5	749.7	749.2	13.2	14.2	14.0	13.9	15.0	12.8	-	09.7	10.1	09.8	85	84	81	83	ESE	5	SE	5	SE	6
23	749.0	753.1	754.9	14.0	17.2	13.6	14.6	17.2	13.0	-	09.5	09.1	07.6	79	62	65	69	SE	5	SW	1	NE	1
24	752.9	751.9	750.5	14.7	16.0	15.4	15.4	16.1	12.2	-	06.9	08.8	08.7	71	64	66	67	SE	6	ESE	6	ESE	6
25	746.5	746.2	748.2	14.5	14.5	11.0	12.8	16.2	10.2	-	08.7	09.4	07.8	70	76	80	75	ESE	6	ESE	5	SE	1
26	749.5	748.4	748.4	09.6	14.6	10.2	11.2	15.1	05.1	-	07.5	07.5	05.8	83	60	62	68	SSE	1	SSW	3	NE	2
27	748.9	749.8	749.5	08.4	12.5	09.6	10.0	13.3	07.3	-	05.0	06.0	05.5	61	55	61	59	NE	3	SW	2	NNE	2
28	748.6	752.3	758.5	04.7	05.0	01.8	03.3	09.9	01.5	-	03.2	01.8	01.7	51	28	33	37	NNE	6	NNE	6	ENE	6
MES.	VRED.	748.4	748.8	749.4	09.2	11.5	09.9	10.1	12.6	07.9	-	06.6	07.0	06.7	72	67	71	70	3.0	3.2	3.0		

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 $H_s = 122 \text{ m}$   $H_b = 128.0 \text{ m}$   $h_t = 6.5 \text{ m}$   $H_r = 1.0 \text{ m}$ 

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacije broj seti	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	9	03	10	09	07.3	02.3	.	.	.	.	.
2	8	10	10	10	10.0	00.0	00.3	.	.	.	.
3	8	10	10	10	10.0	00.0	00.0	.	.	.	.
4	8	10	10	10	10.0	00.0	00.0	20.4	.	.	.
5	7	10	10	10	10.0	00.0	05.2	.	.	.	.
6	6	10	08	03	07.0	00.3	02.9	.	.	.	.
7	6	10	10	10	10.0	00.2	.	.	.	.	.
8	8	09	09	00	06.0	01.3	04.3	.	.	.	.
9	8	25	01	08	04.7	05.5	.	.	.	.	.
10	8	09	09	04	07.5	03.1	.	.	.	.	.
11	8	10	10	10	10.0	00.0	00.0	.	.	.	.
12	8	10	10	10	10.0	00.0	04.2	.	.	.	.
13	7	10	10	06	08.7	01.3	02.8	.	.	.	.
14	9	02	03	08	04.3	06.7	01.4	.	.	.	.
15	6	10	10	10	10.0	00.0	05.7	.	.	.	.
16	8	03	02	00	01.7	05.8	22.4	.	.	.	.
17	6	03	04	00	02.3	08.2	.	.	.	.	.
18	8	01	00	00	00.3	08.2	.	.	.	.	.
19	8	00	01	00	00.3	08.2	.	.	.	.	.
20	7	05	10	10	09.7	00.0	.	.	.	.	.
21	7	10	09	09	06.3	00.0	.	.	.	.	.
22	8	10	09	00	06.3	01.5	.	.	.	.	.
23	8	09	09	10	09.3	00.0	.	.	.	.	.
24	8	10	06	06	08.3	00.3	04.5	.	.	.	.
25	8	01	03	01	01.7	07.8	00.1	.	.	.	.
26	7	05	14	10	05.7	00.7	.	.	.	.	.
27	7	09	09	09	09.0	00.5	12.6	.	.	.	.
28	8	02	10	10	07.3	00.3	.	.	.	.	.
29	7	09	10	09	09.3	00.4	.	.	.	.	.
30	8	09	09	04	07.3	03.8	01.5	.	.	.	.
31	8	08	10	10	05.3	01.7	.	.	.	.	.
MES. RED.			07.4	07.9	06.6	07.3	66.1	85.3			

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1	8	10	05	09	09.3	01.3	04.5	.	$\overline{\text{FSE}} 0-3^{\circ}$ , $\bullet 0^{\circ}-5^{\circ}$ , $23^{\circ}24'$ , $\triangle^{\circ} \text{nj}$	.	.
2	8	10	10	09	09.7	00.0	17.6	.	$\bullet 0-11^{\circ}$ , $\text{v}$	.	.
3	8	06	05	00	01.7	08.9	05.2	.	.	.	.
4	9	01	04	01	02.0	08.9	.	.	.	.	.
5	7	08	02	01	05.7	06.8	.	.	.	.	.
6	6	10	10	04	10.0	00.0	.	.	$\bullet 17^{\circ}17^{\circ}$ , $20^{\circ}-n$	.	.
7	8	02	07	00	03.0	08.0	03.8	.	$\triangle^{\circ} \text{nj}, g^{\circ}$	.	.
8	8	02	05	04	03.7	07.4	.	.	$\text{FSE} 19^{\circ}24'$	.	.
9	8	07	10	10	05.7	00.0	.	.	$\bullet 10^{\circ}-15^{\circ}$ , $10^{\circ}-n$ , $20^{\circ}21^{\circ}$	.	.
10	7	09	09	10	05.3	00.0	12.2	.	$\triangle^{\circ} \text{Kv-n}$	.	.
11	9	10	02	05	05.7	04.1	03.8	.	$\bullet 0^{\circ}-12^{\circ}5^{\circ}$ , $\text{R} 6^{\circ}10^{\circ}$	.	.
12	8	10	14	05	05.7	08.7	17.5	.	$\bullet 17^{\circ}23^{\circ}$ , $8^{\circ}8^{\circ}$ , $\text{FSE-SSW} 3-13^{\circ}$	.	.
13	9	08	18	06	06.1	04.2	00.0	.	.	.	.
14	9	10	10	06	06.7	00.0	.	.	$\bullet 2-10^{\circ}$ , $\text{FSE} 16^{\circ}24'$	.	.
15	8	04	05	00	14.3	00.1	.	.	$\triangle^{\circ} n, T^{\circ} 10^{\circ}$ , $\bullet 10^{\circ}-H^{\circ}$ , $18^{\circ}-18^{\circ}$	.	.
16	8	08	08	06	07.3	2.7	01.2	.	$\triangle^{\circ} \text{nj}, 8^{\circ}8^{\circ} H^{\circ}$ , $\bullet 17^{\circ}23^{\circ}$	.	.
17	8	04	08	00	01.7	00.0	13.7	.	$\bullet 0^{\circ}-2^{\circ}4^{\circ}$ , $14^{\circ}14^{\circ}$	.	.
18	8	08	10	10	05.3	00.0	00.7	.	.	.	.
19	7	10	05	09	09.3	00.0	01.1	.	$\bullet 2-10^{\circ}$ , $\text{FSE} 16^{\circ}24'$	.	.
20	8	04	14	09	05.7	07.8	.	.	$\triangle^{\circ} 0-10^{\circ}, 14^{\circ}24'$ , $\triangle^{\circ} \text{nj}-8^{\circ}$	.	.
21	7	09	10	10	05.7	01.3	.	.	$\text{FSE} 0-9^{\circ}$ , $\bullet 17^{\circ}17^{\circ}$	.	.
22	7	10	10	10	06.0	00.1	01.0	.	$\bullet 0-4^{\circ}6^{\circ}$ , $17^{\circ}24^{\circ}$	.	.
23	8	10	16	00	05.3	05.8	.	.	$\text{FSE} 0-6^{\circ}10^{\circ}$	.	.
24	8	09	10	10	05.7	00.0	00.2	.	$\triangle^{\circ} 15^{\circ}15^{\circ}$ , $\text{FSE} 16-17^{\circ}$ , $T 16^{\circ}17^{\circ}$	.	.
25	8	10	10	00	06.7	01.0	01.7	.	$\triangle^{\circ} \text{nj}-10^{\circ}$ , $\bullet 20^{\circ}-23^{\circ}$ , $\text{FSE} 21^{\circ}-n$	.	.
26	6	09	04	10	07.7	07.0	02.5	.	$\bullet 17^{\circ}23^{\circ}$ , $\bullet 23^{\circ}24^{\circ}$	.	.
27	5	12	02	00	02.2	09.7	03.0	.	$\bullet 0^{\circ}-4^{\circ}10^{\circ}$ , $\text{FSE} 0-24^{\circ}$	.	.
28	8	06	31	03	03.3	03.3	01.7	.	$\bullet 0^{\circ}-4^{\circ}10^{\circ}$ , $\text{FSE} 0-24^{\circ}$	.	.
MES. RED.			07.1	07.0	05.4	06.5	10.5	7.1			

$\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$  Gr.  $\Delta G = + 1h 06 min.$ 

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D S E	Vozdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	759.8	758.3	759.1	00.4	08.1	05.9	05.1	09.9	00.2	-	02.6	02.9	02.3	55	35	33	41	NNW	3	NW	3	NNE	5
2	760.6	759.2	758.1	04.3	09.4	06.9	06.9	09.4	03.3	-	02.4	03.4	04.4	38	38	59	45	NNE	4	SSW	3	W	3
3	757.1	755.4	755.1	06.7	12.2	09.6	09.5	13.2	05.4	-	04.8	06.8	06.7	66	64	75	68	WSW	2	SW	4	NNE	1
4	754.0	754.3	754.4	07.7	12.6	10.2	10.2	13.0	07.2	-	05.6	07.9	07.4	71	72	79	74	NE	1	SSE	2	ESE	4
5	755.2	756.4	757.2	09.0	14.4	11.5	11.6	14.6	08.1	-	06.9	08.6	08.5	80	78	83	78	NE	2	SSW	2	NNW	2
6	757.3	757.5	757.8	09.2	14.2	11.2	11.5	14.6	08.5	-	08.3	07.8	09.1	95	64	91	83	SE	1	SSW	1	NNW	1
7	758.0	759.0	760.7	09.0	15.8	12.0	12.2	16.0	08.3	-	06.6	07.8	06.7	77	58	64	66	NE	3	SSW	2	S	1
8	763.8	765.2	765.6	10.5	16.6	13.0	13.3	17.0	10.4	-	04.6	07.0	04.4	48	50	39	46	NE	4	SSW	2	WSW	1
9	764.9	763.0	761.1	08.6	14.8	14.8	11.3	15.2	07.0	-	05.7	07.7	07.7	68	61	79	69	NNE	1	SSW	1	SSW	1
10	757.7	754.3	753.1	08.6	15.2	12.1	12.0	15.6	08.5	-	07.1	08.9	07.7	85	69	73	76	NNE	1	SW	3	NW	2
11	752.7	752.0	751.3	10.4	12.4	11.8	11.6	13.0	09.5	-	08.6	07.5	08.5	91	68	82	80	ESE	3	ESE	4	ESE	5
12	749.2	748.1	746.9	12.0	13.3	12.3	12.5	14.0	11.2	-	09.1	09.8	09.9	87	85	92	88	SE	5	SE	5	SE	5
13	744.0	744.7	749.0	11.2	12.4	10.4	11.1	13.2	09.4	-	09.2	08.7	05.5	92	80	58	77	WSW	1	NNW	2	NNE	1
14	753.6	754.8	755.4	09.4	15.4	13.0	12.7	15.8	08.3	-	05.1	07.4	05.5	58	57	49	55	SW	1	SSW	1	NNE	1
15	757.5	758.6	759.8	10.4	17.8	13.0	13.6	18.0	08.5	-	05.2	06.0	04.7	55	39	42	45	ESE	1	SSW	2	NE	1
16	761.1	761.1	760.6	10.5	16.7	12.6	13.1	16.9	09.9	-	04.7	05.5	05.5	49	39	51	46	NE	4	SW	3	WSW	1
17	758.9	757.5	755.9	09.6	15.8	11.9	12.3	16.3	08.9	-	05.1	07.0	07.2	57	52	69	59	ENE	2	SSW	2	SE	1
18	754.8	753.6	752.1	09.8	16.2	12.6	12.8	16.4	09.1	-	06.1	08.4	09.6	67	59	88	71	NE	1	SSW	1	NNE	1
19	749.8	748.5	748.1	12.2	14.5	13.6	13.5	15.4	10.9	-	06.5	08.1	08.6	61	65	75	67	ESE	3	ESE	5	SE	5
20	746.3	749.3	749.6	11.6	14.4	13.4	13.2	15.6	10.9	-	06.7	08.0	09.3	65	70	81	72	ENE	2	SSE	4	SE	5
21	750.4	752.8	754.0	13.0	17.2	13.5	14.5	17.4	11.8	-	09.6	09.6	06.3	87	65	78	77	SSE	5	SSW	2	SE	4
22	754.4	754.6	755.3	13.8	17.7	16.4	16.1	18.0	13.0	-	09.0	08.2	06.1	76	54	44	58	SE	6	SE	6	SE	4
23	755.6	755.5	755.0	19.0	22.5	20.6	20.4	23.2	16.2	-	04.5	06.6	04.2	27	32	24	28	ENE	2	SSW	2	E	2
24	754.1	753.2	752.1	16.7	23.0	19.4	19.6	23.1	16.0	-	05.6	07.2	05.5	40	34	33	36	ENE	1	SSE	1	ENE	1
25	751.9	752.8	753.1	14.9	17.9	15.8	16.1	19.9	14.2	-	08.1	10.2	09.1	64	66	68	66	WNW	1	WSW	1	SW	1
26	752.5	750.6	749.2	14.6	21.3	19.5	18.7	21.7	13.4	-	07.8	11.3	06.8	63	59	40	54	SSE	1	SW	2	SE	2
27	748.1	747.0	745.6	15.6	21.0	16.3	17.3	21.4	15.4	-	06.7	09.0	08.9	51	48	64	54	NE	2	SW	2	SSW	1
28	744.4	743.2	742.5	14.3	15.9	13.0	14.0	16.8	13.0	-	09.7	09.7	11.4	80	72	98	83	SE	3	SE	5	SSE	3
29	741.9	743.0	744.4	13.7	16.0	14.8	14.8	17.0	13.0	-	09.9	10.0	10.3	84	73	82	80	SE	4	SE	5	SE	5
30	742.6	740.3	740.7	11.2	16.0	13.3	13.5	16.5	08.2	-	07.1	08.0	11.0	71	59	96	75	NNE	3	ESE	5	SSW	5
31	747.9	751.2	752.7	10.9	13.5	11.7	12.0	14.3	10.5	-	08.3	07.0	07.5	85	60	73	73	WNW	2	NNW	2	NE	1
MES.	VRED.	753.6	753.4	753.4	10.9	15.6	13.6	13.1	16.2	10.0	-	06.7	07.8	07.4	68	59	66	64	2.3	2.7	2.4		

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1	753.2	752.5	750.6	10.6	14.2	12.8	12.6	14.5	09.3	-	06.0	07.8	06.1	63	64	55	61	NNE	2	SSE	1	NNE	2
2	747.2	746.3	745.9	11.2	12.1	11.6	11.6	13.1	10.7	-	07.5	08.6	08.5	75	81	83	80	SSE	1	SSW	1	WSW	1
3	744.2	743.6	744.6	11.3	15.0	12.8	13.0	15.5	10.7	-	09.5	10.6	08.9	94	84	81	86	SW	1	SSW	1	E	1
4	747.0	748.5	749.2	11.8	18.0	14.8	14.9	18.9	10.8	-	09.2	08.7	07.7	89	56	61	69	WSW	1	SW	1	SW	2
5	749.1	748.3	747.5	14.4	18.2	13.8	15.1	18.5	13.1	-	06.7	10.0	11.1	71	64	94	76	SE	2	SE	3	NW	4
6	750.2	749.7	748.9	10.6	16.0	11.5	12.4	16.5	09.3	-	04.4	06.0	06.5	46	44	64	51	NE	4	SSW	3	WSW	1
7	747.3	746.0	748.8	12.4	15.8	15.2	14.7	16.5	09.2	-	06.2	08.5	07.5	57	63	58	59	SE	4	SE	5	ESE	5
8	740.6	740.1	736.7	15.4	15.8	15.3	15.5	16.5	14.7	-	08.5	08.4	09.4	64	62	72	66	ESE	6	SE	5	SE	7
9	734.3	736.5	738.0	13.1	08.1	08.7	09.7	15.3	06.4	-	08.9	06.6	06.5	79	81	77	79	SSE	5	WNW	5	SE	5
10	738.5	740.8	743.0	09.4	09.0	07.8	08.5	14.0	05.1	-	05.9	06.1	05.1	67	71	65	68	SSE	3	NNW	4	NE	3
11	744.7	745.5	746.1	07.5	11.5	36.0	08.8	12.0	06.4	-	03.5	03.0	03.4	45	30	42	39	NE	5	NE	3	NE	4
12	746.3	746.6	748.5	06.5	11.0	07.5	08.1	11.2	05.5	-	02.4	02.3	02.6	34	24	34	31	NE	5	NE	5	NNE	3
13	749.4	748.4	747.6	07.9	13.1	11.0	10.8	14.0	05.7	-	03.1	03.5	04.5	39	31	46	39	NNE	2	NE	1	NE	1
14	745.8	744.9	743.3	10.4	14.0	09.9	11.1	15.9	09.3	-	05.5	06.1	07.6	62	63	68	71	ENE	1	SSW	2	ENE	2
15	738.2	740.2	743.7	07.5	07.9	08.4	08.1	10.5	06.5	-	05.9	04.0	03.9	76	50	47	58	NE	4	NNE	5	N	3
16	747.0	748.4	751.5	07.4	12.6	08.4	09.2	13.4	06.4	-	03.5	02.8	05.9	45	26	47	39	NNW	3	NNW	3	NNE	2
17	754.3	753.3	753.1	08.2	13.4	10.6	14.6	16.2	06.2	-	03.3	03.3	04.1	40	29	43	37	NNE	3	NNW	2	NNW	1
18	753.0	752.9	753.3	09.0	15.0	11.6	11.8	15.4	06.9	-	04.6	07.4	07.4	54	56	72	61	ENE	2	SSW	3	SSW	1
19	754.2	753.9	753.7	10.7</																			

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijnost 0-9	Oblačnost N (0-10)					Insolacij broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8	010	010	00	08.7	49.8	.	.	.	.	.
2	8	010	000	10	08.7	49.8	.	.	.	.	.
3	8	050	06	09	07.3	07.4	.	.	.	.	.
4	7	08	10	06	08.0	01.2	.	.	.	.	.
5	6	06	030	07	05.3	07.5	.	.	.	.	.
6	7	09	010	00	03.3	06.8	.	.	.	.	.
7	7	08	070	05	06.7	05.5	.	.	.	.	.
8	8	010	040	00	01.7	06.2	.	.	.	.	.
9	7	010	030	00	01.3	09.0	.	.	.	.	.
10	6	010	000	00	00.3	07.8	.	.	.	.	.
11	5	030	10	05	07.3	00.4	.	.	.	.	.
12	7	10	10	10	10.0	00.5	.	.	.	.	.
13	6	10*	10	05	08.3	00.1	05.3	.	.	.	.
14	8	000	080	00	02.7	10.0	01.2	.	.	.	.
15	8	030	050	00	02.7	10.8	.	.	.	.	.
16	9	000	010	00	00.3	10.6	.	.	.	.	.
17	8	000	010	00	00.3	10.5	.	.	.	.	.
18	8	060	070	00	04.3	05.3	.	.	.	.	.
19	8	040	07	10	07.0	05.9	.	.	.	.	.
20	8	07	06	07	06.7	05.5	.	.	.	.	.
21	8	10	070	08	08.3	06.1	07.2	.	.	.	.
22	8	050	070	02	06.0	02.4	00.1	.	.	.	.
23	9	030	010	00	01.3	10.8	.	.	.	.	.
24	9	040	030	00	02.3	05.6	.	.	.	.	.
25	7	10	10	09	05.7	00.2	00.4	.	.	.	.
MES.											
RED.		05.1	05.7	04.5	05.1	189.6	36.4				

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1	8	08	09	09	08.7	00.6	.	.	.	.	.
2	5	10	10	10	10.4	00.3	.	.	.	.	.
3	6	10	09	06	06.3	02.5	01.6	.	.	.	.
4	7	000	080	02	03.3	08.7	00.2	.	.	.	.
5	7	040	020	10*	05.7	08.4	.	.	.	.	.
6	5	000	010	00	04.3	10.4	01.4	.	.	.	.
7	8	050	060	10	08.7	00.7	.	.	.	.	.
8	7	09	10*	10	05.7	03.5	.	.	.	.	.
9	5	10	10	06	06.7	01.6	12.7	.	.	.	.
10	8	09	030	02	04.7	07.6	06.9	.	.	.	.
11	8	020	050	00	02.3	11.5	00.2	.	.	.	.
12	8	030	070	03	04.3	09.0	.	.	.	.	.
13	8	070	070	09	07.7	07.6	.	.	.	.	.
14	8	060	10*	10*	08.7	03.9	.	.	.	.	.
15	7	10*	10	10	10.0	00.0	14.3	.	.	.	.
16	9	140	060	00	03.3	10.0	00.6	.	.	.	.
17	9	020	000	00	06.0	02.1	.	.	.	.	.
18	8	020	050	02	04.0	01.9	.	.	.	.	.
19	8	040	060	09	06.3	05.0	.	.	.	.	.
20	8	090	090	02	06.7	00.2	.	.	.	.	.
21	8	000	010	00	01.3	12.4	.	.	.	.	.
22	9	040	060	05	03.7	12.2	.	.	.	.	.
23	8	160	050	07	06.0	09.1	.	.	.	.	.
24	8	08	040	07	06.3	10.7	.	.	.	.	.
25	9	100*	020	03	05.0	09.9	00.2	.	.	.	.
26	9	090	020	00	03.7	10.1	00.5	.	.	.	.
27	8	040	030	10	09.7	11.0	.	.	.	.	.
28	8	05	050	19	17.7	08.0	.	.	.	.	.
29	8	050	070	03	05.0	09.8	.	.	.	.	.
30	8	090	090	05	07.7	11.4	.	.	.	.	.
MES.											
RED.		05.7	06.0	05.3	05.7	288.7	28.6				

$\varphi = 43^{\circ}31' N$   $\lambda = 16^{\circ}26' E$  Gr.  $\Delta G = +1h\ 06\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21	
1	749.6	750.1	751.1	20.4	24.3	19.4	20.9	24.8	17.9	-	06.4	07.0	06.6	36	31	35	35	ESE 2	SE 4	NNW 2	
2	752.0	752.5	752.5	18.8	22.8	19.8	20.3	24.5	17.4	-	07.7	08.8	07.6	47	42	44	44	SSE 1	SSE 4	SE 2	
3	752.3	751.5	750.1	19.4	26.8	20.9	22.0	27.0	17.5	-	07.5	08.4	08.8	45	32	47	41	ENE 1	SW 1	WSH 1	
4	749.3	748.8	747.3	20.9	24.9	22.2	22.6	25.6	18.4	-	07.2	07.1	06.0	39	30	35	33	E 2	SSE 5	SSW 3	
5	748.5	751.4	752.1	20.0	18.8	15.3	17.4	22.5	14.9	-	09.0	12.2	11.1	51	75	85	73	S 4	WSH 1	NW 2	
6	752.3	752.4	752.5	16.0	19.8	16.4	17.2	21.5	14.3	-	11.0	06.9	07.1	81	40	51	57	ESE 1	NNW 3	NNW 2	
7	751.9	750.4	749.4	15.7	18.7	15.8	16.5	21.6	13.3	-	06.6	11.7	07.8	49	66	56	56	E 1	SW 3	NW 2	
8	747.1	746.3	746.3	14.4	16.5	14.4	14.9	19.0	13.0	-	06.8	07.3	08.0	55	52	65	57	ENE 1	N 2	ENE 2	
9	747.6	748.1	749.3	12.4	17.3	10.7	12.8	20.2	10.2	-	08.5	07.2	08.2	78	48	85	70	ESE 2	E 3	NE 2	
10	749.7	750.6	751.2	11.7	17.7	14.4	14.6	18.1	10.0	-	08.8	09.3	09.1	85	61	74	73	SE 1	SW 2	NNW 2	
11	751.9	750.6	750.9	14.5	21.2	17.3	17.6	22.0	12.3	-	06.6	08.6	07.4	54	46	50	50	NE 2	W 3	NNE 2	
12	750.7	749.2	747.8	16.0	22.0	18.0	18.5	22.5	12.3	-	08.0	08.0	04.4	59	49	29	43	SSE 1	SW 2	ESE 1	
13	746.8	746.2	744.8	17.0	20.0	18.2	18.4	20.6	14.1	-	07.2	08.1	07.7	50	46	49	48	ESE 2	SE 5	SE 6	
14	742.6	743.5	743.5	15.4	16.6	15.6	15.6	18.8	14.6	-	11.5	11.7	11.7	88	63	86	86	SSE 1	SE 1	SE 5	
15	744.0	743.4	743.7	13.6	20.2	15.6	16.3	21.0	13.5	-	10.7	10.3	11.6	91	58	87	79	ENE 3	SSE 3	SW 2	
16	745.0	746.0	747.1	15.9	20.4	16.7	17.4	22.0	13.4	-	10.7	10.8	10.6	79	61	75	71	SE 3	SW 2	SE 3	
17	749.0	752.0	753.1	17.3	19.9	16.1	18.9	20.4	15.7	-	10.0	10.9	09.2	67	62	55	61	SE 5	SE 5	ENE 2	
18	753.1	751.8	751.6	16.0	25.8	23.0	22.5	26.2	17.9	-	10.5	10.1	09.2	58	41	44	51	NE 2	SE 2	SSE 2	
19	751.0	750.9	749.8	23.4	26.2	25.1	25.0	27.1	21.8	-	08.9	07.1	11.2	41	38	47	42	SE 5	SE 4	SE 5	
20	749.6	750.9	750.9	22.0	22.6	21.0	21.7	25.4	21.0	-	11.1	11.5	10.3	56	56	55	56	SE 5	SE 5	SE 5	
21	751.0	751.4	751.6	21.0	26.8	20.1	22.0	27.1	15.7	-	11.7	10.8	10.9	63	41	62	55	SSE 2	S 2	SSW 1	
22	751.8	751.7	752.0	20.2	25.7	21.7	22.3	27.0	17.7	-	10.2	10.8	16.1	57	45	52	51	-	SW 3	NW 2	
23	752.3	752.0	751.5	20.8	26.9	22.3	23.1	27.8	16.4	-	08.1	05.9	09.3	45	37	46	43	ENE 2	SW 2	WWN 2	
24	751.6	751.6	750.6	21.0	28.0	22.0	23.3	28.1	16.8	-	10.1	10.5	08.4	54	37	44	44	NE 2	SSW 2	NE 3	
25	751.0	750.2	749.5	19.6	25.4	20.2	21.4	26.0	16.7	-	08.2	09.2	11.3	48	38	63	50	S 1	SW 3	SSE 1	
26	748.8	748.8	749.8	20.6	26.7	18.6	21.1	27.0	17.1	-	10.7	10.3	11.6	59	35	72	57	SSE 1	SW 2	NNE 4	
27	748.6	748.3	749.0	18.4	21.4	15.6	17.8	22.0	15.6	-	12.4	12.3	09.0	78	55	67	70	SE 2	NNE 3	NE 3	
28	749.3	750.4	751.3	14.8	21.6	15.4	16.6	22.6	12.2	-	06.1	07.4	05.4	49	38	41	42	NE 5	SW 3	NE 4	
29	750.9	750.4	750.7	16.4	21.0	16.5	17.6	22.5	13.1	-	04.5	06.3	06.4	32	34	46	37	NNE 3	SW 3	WWN 2	
30	750.4	750.0	749.5	16.6	23.5	17.3	18.7	23.6	13.1	-	07.5	07.5	06.6	53	35	60	49	ENE 1	SW 2	NNW 2	
31	749.8	750.2	749.2	18.0	23.9	19.4	20.2	24.3	14.9	-	07.9	09.4	08.9	51	42	53	49	SSE 1	SSW 3	W 1	
MES.	VRED.	749.7	749.7	749.7	17.7	22.4	16.3	19.2	23.5	15.5	-	08.8	09.3	08.8	58	47	57	54	2.3	3.1	2.5

1	749.9	751.3	751.6	17.5	22.3	15.6	17.8	22.5	15.6	-	07.8	09.0	06.6	52	45	50	49	ENE 5	SSW 2	NE 5
2	750.3	750.3	750.6	16.6	19.4	15.1	16.6	23.4	14.5	-	05.1	08.9	10.9	36	53	65	58	NE 3	SW 3	E 1
3	748.8	747.1	746.7	16.9	22.8	18.2	20.3	23.7	13.4	-	08.6	07.5	06.0	59	36	38	44	E 1	SW 3	NE 2
4	745.7	745.3	745.7	17.0	23.0	18.4	19.2	23.6	15.0	-	04.1	07.0	05.0	28	33	32	31	ENE 4	SW 2	NE 5
5	747.4	746.6	746.7	17.8	22.6	18.7	19.5	23.9	15.6	-	06.2	07.6	10.3	41	37	64	47	ENE 3	WSW 4	SSE 2
6	747.5	747.9	748.5	17.8	24.2	15.2	20.1	24.6	15.6	-	11.3	09.5	05.6	72	42	58	57	S 1	SSW 2	SE 3
7	749.1	750.2	751.2	18.3	21.2	16.5	19.3	22.4	16.2	-	07.7	12.2	11.8	68	64	72	68	SE 4	SE 4	SE 3
8	752.6	752.6	753.1	20.3	26.6	20.3	21.9	27.0	17.5	-	09.5	10.6	11.9	53	41	67	54	ENE 2	SSW 2	NW 2
9	753.0	753.0	751.7	20.6	25.8	24.6	23.6	27.5	17.8	-	12.2	12.5	09.0	57	50	40	52	-	SW 2	N 4
10	750.4	749.1	748.7	22.7	28.7	25.0	25.0	29.1	19.9	-	10.8	10.4	09.4	52	35	40	42	SSE 1	SW 2	WWN 2
11	748.5	748.6	748.2	23.0	28.9	25.5	25.5	29.6	21.4	-	12.3	13.5	10.4	53	39	43	44	S 1	SW 2	NNW 2
12	748.6	748.3	748.8	24.0	28.6	22.0	24.2	29.5	22.0	-	12.2	12.2	10.2	54	36	62	64	S 1	SW 2	S 1
13	749.1	748.1	747.7	23.2	28.1	25.4	26.0	30.7	20.2	-	16.3	12.8	11.2	78	43	46	56	SSE 1	SW 2	FNE 2
14	746.9	747.1	747.0	25.2	28.2	23.7	25.2	30.6	21.7	-	12.8	15.4	10.3	53	47	51	51	SE 4	SW 3	NNW 1
15	747.2	746.7	746.0	22.9	27.4	22.4	23.8	28.0	21.3	-	10.7	10.9	09.4	51	46	46	46	NW 2	SW 3	NE 1
16	744.8	744.5	744.8	19.4	20.2	19.5	19.7	23.7	17.2	-	09.5	11.7	12.6	56	66	74	65	NNW 2	W 3	NNW 1
17	745.3	746.1	746.7	22.0	28.5	25.3	29.4	30.0	19.0	-	13.8	04.2	02.6	68	14	31	31	SSE 2	WSW 2	NNW 2
18	748.5	748.9	748.4	24.4	29.7	24.0	25.5	29.8	21.8	-	12.3	12.4	12.9	54	40	58	51	SSW 1	SW 3	WSW 1
19	749.1	748.8	747.8	23.2	25.4	24.2	25.3	31.2	21.2	-	15.3	10.4	13.9	72	34	61	56	S 1	SW 3	WSW 1
20	747.5	747.9	748.8	24.4	28.2	25.4	25.9	29.7	21.7	-	12.9	12.2	09.1	56	42	37	45	SSW 1	SW 3	NNW 2
21	749.7	749.3	748.1	22.8	25.5	23.3	24.1	28.4	20.0	-	10.3	13.0	11.8	47	52	55	51	ENE 1	SSW 3	NE 1
22	747.1	746.7	747.0	22.7	28.1	23.5	23.5	28.5	21.0	-	09.9	05.7	10.2	49	33	53	45	NW 1	2	1
23	748.8	749.0	750.0	21.4	24.0	21.6	22.2	26.5	18.6	-	10.1	12.5	12.0	53	56	62	57	SSW		

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	9	02	03	03	02.7	11.8	.	.	.	W 19 <sup>45</sup> 20 <sup>05</sup>	.
2	8	05	03	02	04.7	06.5	.	.	.	.	.
3	8	06	03	02	03.7	05.8	.	.	.	.	.
4	8	06	06	08	06.7	05.6	.	.	.	.	.
5	7	09	10	06	08.3	01.2	.	.	.	• 17-18 <sup>00</sup> i	.
6	8	05	07	00	04.6	07.3	03.6	.	.	= rj-9 <sup>30</sup> , □ <sup>2</sup> rj-10 <sup>20</sup> , • tr 10 <sup>25</sup> -12 <sup>35</sup> i	.
7	8	02	05	02	03.6	11.2	00.1	.	.	.	.
8	7	09	09	06	08.0	02.9	.	.	.	.	.
9	7	08	07	10	08.3	05.6	00.1	.	.	• tr 5 <sup>45</sup> 6 <sup>00</sup> , 14 <sup>10</sup> N; T' H <sup>10</sup> 17 <sup>35</sup> , R <sup>1</sup> H <sup>40</sup> 13 <sup>30</sup>	.
10	7	10	09	00	06.3	03.4	18.3	.	.	• 0-6 <sup>30</sup>	.
11	7	00	05	00	01.7	10.8	.	.	.	• H <sup>20</sup> 15 <sup>50</sup> i, R <sup>1</sup> 15 <sup>10</sup> 15 <sup>20</sup>	.
12	8	01	01	01	01.0	13.2	00.1	.	.	.	.
13	8	04	07	09	06.7	08.6	.	.	.	■ SE 9 <sup>30</sup> 24 i	.
14	7	10	09	07	08.7	01.2	01.5	.	.	■ SE-SF 0-20, 0-14 <sup>02</sup> 9 <sup>20</sup> i	.
15	8	09	08	10	09.0	09.2	02.1	.	.	• 5 <sup>00</sup> 6 <sup>40</sup> , 20 <sup>30</sup> N; ▲ 19 <sup>15</sup> 20 <sup>25</sup>	.
16	8	08	04	08	06.7	10.5	00.2	.	.	• 10 <sup>22</sup> 21 <sup>10</sup> i	.
17	7	07	07	10	06.0	06.9	00.0	.	.	.	.
18	9	10	08	10	05.3	02.1	.	.	.	• tr 8 <sup>05</sup> 9 <sup>10</sup> i	.
19	9	03	10	07	06.7	00.9	00.2	.	.	■ SE 8 <sup>05</sup> 10 <sup>10</sup>	.
20	7	04	10	03	05.7	02.5	.	.	.	.	.
21	8	05	07	02	06.0	08.2	.	.	.	.	.
22	8	05	01	00	12.0	13.4	.	.	.	.	.
23	8	00	02	00	06.7	12.1	.	.	.	.	.
24	8	01	06	01	02.7	12.9	.	.	.	.	.
25	8	00	00	00	00.0	13.4	.	.	.	.	.
26	8	03	03	10	05.3	05.4	.	.	.	• tr 10 <sup>45</sup> 22 i, R <sup>1</sup> 19 <sup>30</sup> 20 <sup>10</sup>	.
27	8	09	08	10	09.0	02.2	01.4	.	.	• 10 <sup>45</sup> 24 i, R <sup>1</sup> 9 <sup>20</sup> i, 20 <sup>30</sup> N; R <sup>1</sup> 7 <sup>20</sup> 7 <sup>40</sup> , 10 <sup>25</sup> , T' 19 <sup>12</sup> N	.
28	9	08	06	00	04.7	08.6	02.1	.	.	.	.
29	8	00	02	00	05.7	13.5	.	.	.	.	.
30	8	00	01	00	05.3	13.7	.	.	.	.	.
31	8	00	01	04	01.7	12.0	.	.	.	.	.
MES.	VRED.	05.1	05.4	04.2	04.9	250.3	29.7				

1	8	10	10	02	07.3	02.7	.	.	.	• tr 0 H <sup>10</sup> -22 i	.
2	7	05	10	10	05.7	01.6	.	.	.	.	.
3	8	01	07	09	05.7	21.3	02.5	.	.	.	.
4	8	06	01	01	02.7	01.7	.	.	.	.	.
5	8	00	08	09	05.7	08.5	.	.	.	.	.
6	8	11	04	09	07.7	06.9	.	.	.	= rj-9	.
7	7	11	09	02	07.0	08.7	.	.	.	.	.
8	7	00	01	03	01.3	12.9	.	.	.	= rj-13 <sup>30</sup>	.
9	7	00	06	09	05.0	08.8	.	.	.	.	.
10	8	01	00	00	01.3	12.3	.	.	.	.	.
11	8	01	03	01	01.7	12.4	.	.	.	.	.
12	7	00	02	00	05.7	13.0	.	.	.	■ 18 <sup>30</sup> N	.
13	7	04	05	00	02.3	12.7	.	.	.	■ rj-9, ■ 9-13 <sup>20</sup>	.
14	7	04	07	04	04.6	09.2	.	.	.	.	.
15	8	05	04	01	03.3	12.4	.	.	.	.	.
16	8	09	09	00	06.0	02.6	.	.	.	• tr 8 <sup>05</sup> 9 <sup>20</sup> i, 13 <sup>30</sup> 13 <sup>58</sup> ; T' 16 <sup>40</sup>	.
17	8	01	02	00	01.3	12.7	01.0	.	.	.	.
18	8	00	01	00	00.3	12.4	.	.	.	= rj-9 <sup>30</sup>	.
19	7	00	06	00	02.6	13.3	.	.	.	.	.
20	8	00	01	01	05.7	13.2	.	.	.	.	.
21	8	06	10	08	10.1	05.5	.	.	.	⊕ 10 <sup>30</sup> -10 <sup>50</sup>	.
22	8	08	05	10	07.3	08.8	00.4	.	.	• 10 <sup>20</sup> -20 <sup>30</sup> 6 <sup>35</sup>	.
23	8	01	06	03	15.3	17.6	.	.	.	■ 15 <sup>12</sup> 16 <sup>05</sup> 8 <sup>12</sup> 15 <sup>30</sup> , ⊕ 15 <sup>23</sup> 15 <sup>40</sup> , ⊕ 15 <sup>30</sup> -15 <sup>40</sup> T' 16 <sup>05</sup> -16 <sup>15</sup>	.
24	7	05	03	03	05.7	16.4	06.5	.	.	■ 15 <sup>05</sup> 14 <sup>55</sup> 12, △ 15 <sup>05</sup> -14 <sup>55</sup> 12, ▽ 13 <sup>25</sup> 13 <sup>50</sup> , ⊕ 14 <sup>50</sup> -15 <sup>15</sup>	.
25	7	01	03	07	05.7	13.0	15.9	.	.	■ 15 <sup>35</sup>	.
26	8	08	45	79	17.3	11.6	01.2	.	.	T' rj H <sup>30</sup> 11 <sup>40</sup> 13 <sup>02</sup> 13 <sup>15</sup> ; ⊕ 8 <sup>15</sup> 7 <sup>05</sup> 22 <sup>30</sup> 23 <sup>30</sup>	.
27	6	17	08	09	06.3	10.3	04.2	.	.	T' H <sup>11</sup> 10 <sup>05</sup> 10 <sup>30</sup> 12 <sup>30</sup> 12 <sup>30</sup> i, 14 <sup>10</sup> 13 <sup>05</sup> i	.
28	8	01	02	00	01.3	13.0	01.4	.	.	.	.
29	8	01	03	04	32.7	13.8	.	.	.	.	.
30	8	06	07	04	05.7	05.1	.	.	.	T' 11 <sup>10</sup> 15 <sup>15</sup> , ⊕ 14 <sup>55</sup> 13 <sup>10</sup> , 18 <sup>10</sup> 19 <sup>40</sup> , ■ NNE 12 <sup>15</sup> 12 <sup>35</sup> , R <sup>2</sup> 17 <sup>50</sup> 19 <sup>35</sup>	.
MES.	VRED.	03.6	05.3	02.9	04.3	284.3	28.1				

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 $\varphi = 43^{\circ}31' N$   $\lambda = 16^{\circ}26' E$  Gr.  $\Delta G = +1h\ 06\ min.$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodené pare e mm			Relativna vlažnost v %			Pravac i jačina veta D, I (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	752.3	752.6	753.4	20.7	24.6	21.5	22.1	26.6	18.1	-	10.5	09.5	08.4	57	41	44	47	NNE	2	NE	4	NE	3
2	753.7	753.3	752.6	21.7	28.3	24.8	24.8	28.5	15.2	-	08.9	11.7	09.4	46	41	40	42	NNE	1	SW	2	NE	2
3	752.9	752.4	750.8	23.0	28.5	22.9	24.3	29.0	20.9	-	10.1	11.0	15.6	48	38	75	54	NNE	1	SW	2	SW	2
4	749.3	748.1	747.0	23.2	28.5	22.5	24.2	29.1	21.0	-	15.8	12.4	11.8	74	42	58	58	SSE	1	SW	3	-	0
5	746.1	745.3	744.6	22.8	28.3	23.6	24.6	29.0	20.4	-	16.0	16.2	12.1	77	56	55	63	SSW	1	SSW	2	WNW	3
6	744.4	745.6	746.6	22.5	27.4	24.8	24.9	28.4	21.4	-	12.1	14.6	09.4	59	53	40	51	NE	2	SW	2	N	3
7	748.2	748.9	748.4	23.3	28.8	24.4	25.2	29.4	21.2	-	08.5	12.8	11.1	40	43	48	44	ENE	1	SW	2	WNW	1
8	747.5	746.2	745.0	24.3	27.3	25.5	25.7	28.0	22.0	-	10.9	12.5	11.0	46	46	45	46	ESE	3	SE	5	SE	6
9	747.2	748.0	748.1	25.0	29.8	24.5	26.0	29.9	23.4	-	15.2	18.2	17.7	64	58	77	66	SSE	3	SSW	2	WNW	1
10	749.5	748.9	748.8	24.4	26.5	24.1	24.8	28.6	22.3	-	17.8	17.1	13.6	78	66	58	67	SSW	1	SW	4	W	2
11	749.7	749.3	749.7	24.1	29.9	25.4	26.2	30.8	21.5	-	11.4	09.8	07.6	51	31	31	36	NE	1	NNW	2	NE	3
12	750.2	749.4	749.7	24.3	29.3	27.0	26.9	30.4	21.9	-	10.2	10.1	10.3	45	33	38	39	NNE	1	NNW	3	N	2
13	751.0	750.4	749.6	26.2	30.8	25.5	27.0	31.1	23.3	-	09.8	11.5	12.2	38	35	50	41	ENE	1	WSW	3	SSE	1
14	749.4	748.9	747.2	24.5	29.7	26.0	26.6	31.2	22.1	-	13.6	12.2	09.9	55	35	39	46	SSE	1	SW	2	SE	4
15	747.1	746.2	747.6	24.0	27.8	24.8	25.4	28.4	21.9	-	13.5	12.5	16.6	60	45	71	59	SE	4	SE	4	SE	3
16	751.2	751.8	750.6	23.2	30.5	24.8	25.8	30.9	22.0	-	11.3	14.9	14.0	53	45	60	53	NE	3	SW	2	WSW	1
17	748.9	749.2	749.2	24.6	28.3	24.7	25.6	30.2	22.8	-	14.0	15.3	12.7	60	53	55	56	ENE	1	SW	4	WNW	3
18	750.0	749.3	748.3	24.0	29.5	25.2	26.0	30.0	21.6	-	12.0	14.6	05.3	54	47	39	47	NE	1	SW	2	NNW	2
19	748.0	748.2	748.2	23.8	29.3	25.0	25.6	30.3	21.3	-	13.0	12.9	10.3	59	42	43	48	SSE	1	SW	3	WNW	3
20	748.6	748.2	747.8	23.6	30.2	26.4	26.7	31.6	22.4	-	12.5	12.6	12.5	57	35	48	48	NE	1	SW	3	WNW	2
21	747.4	747.0	746.8	25.0	29.7	25.3	26.3	30.5	22.6	-	11.7	12.8	13.8	49	41	57	49	ESE	1	SE	4	ESE	4
22	745.4	746.0	747.3	23.8	29.2	20.6	21.1	27.2	19.2	-	12.7	13.9	09.5	58	63	52	64	ENE	3	NW	3	ESE	3
23	747.8	749.4	750.2	21.2	23.6	21.6	22.0	24.3	19.5	-	09.2	08.5	07.6	49	39	39	42	NE	4	NE	4	ESE	3
24	750.1	748.7	747.2	22.8	27.7	24.1	24.7	29.0	20.6	-	07.7	12.4	11.4	37	45	51	44	ENE	2	SW	4	WNW	1
25	745.7	744.0	743.0	22.2	27.0	23.7	24.2	28.4	20.6	-	11.9	12.5	12.9	59	47	59	55	ENE	2	SW	2	SSE	1
MES.	VRED.	748.4	748.3	748.0	23.6	28.2	24.4	25.2	29.4	21.4	-	11.9	12.8	11.6	55	45	51	50	1.8	2.9	2.3		

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1	742.5	744.5	746.0	21.4	22.8	21.9	22.0	26.4	19.9	-	12.8	10.9	07.9	67	52	40	52	W	1	NNW	2	E NE	4
2	746.6	746.1	746.8	21.0	28.0	22.5	23.5	28.4	19.5	-	06.6	10.2	10.8	35	36	53	41	NNE	2	SW	4	NNW	2
3	748.2	749.2	750.2	20.9	27.1	21.8	22.9	28.0	18.6	-	08.9	11.1	12.1	48	41	62	50	NE	1	SW	3	NE	2
4	752.2	752.9	752.6	21.8	28.8	23.8	24.6	29.6	19.8	-	11.7	10.1	14.2	60	34	64	53	ENE	1	SW	3	ESE	1
5	751.7	750.9	748.8	23.9	27.6	25.9	25.8	28.7	21.8	-	16.7	10.2	09.7	48	37	39	41	E	1	SSW	1	SSE	2
6	748.0	747.9	747.9	23.2	30.2	26.4	26.6	31.4	22.9	-	14.6	12.1	07.8	59	38	32	42	NE	4	SSW	2	NE	4
7	747.5	746.9	746.8	25.5	31.8	26.8	27.7	32.5	23.9	-	09.9	12.6	12.4	40	30	47	39	NE	3	SW	3	ESE	1
8	747.3	747.9	749.1	24.4	30.6	24.9	26.2	31.4	23.6	-	13.8	14.0	12.2	60	43	52	52	FSE	1	SSW	3	NNE	1
9	750.4	750.6	750.8	24.0	30.0	25.1	26.1	30.5	22.4	-	11.8	14.8	15.0	52	47	63	54	E	2	SW	3	NNW	1
10	750.4	750.2	750.0	22.9	30.2	25.0	25.8	30.8	22.2	-	13.3	14.4	12.9	64	45	59	56	ESE	1	SW	2	SSE	1
11	749.0	748.4	747.9	23.7	25.3	24.6	25.7	31.0	21.7	-	13.2	15.5	12.5	60	51	56	56	ESE	1	SW	3	ESE	1
12	747.9	748.2	748.5	23.2	30.0	25.6	26.1	30.6	21.7	-	11.4	14.2	11.7	54	44	47	48	ENE	1	SW	2	SSW	1
13	748.6	750.4	750.0	23.2	21.4	23.1	22.7	26.0	19.7	-	12.0	15.6	12.6	56	82	60	66	ENE	1	ENE	2	NW	3
14	749.8	750.2	750.2	22.6	24.4	22.2	22.9	28.0	20.9	-	15.5	15.5	14.0	66	66	70	68	ENE	2	SW	1	NW	2
15	751.2	751.2	751.9	21.8	27.8	24.1	24.5	28.1	19.2	-	11.0	14.0	11.3	56	50	50	52	ENE	2	SW	3	NW	2
16	752.3	752.1	751.5	22.0	29.2	22.6	24.6	29.8	21.1	-	09.8	11.7	15.0	50	38	48	52	ENE	1	SW	3	ESE	1
17	751.2	751.3	751.1	22.4	30.6	24.5	25.5	30.6	21.3	-	10.7	14.5	13.8	53	44	60	52	NNE	2	SW	2	ESE	1
18	749.1	749.9	747.7	25.6	30.0	24.6	27.2	30.4	24.9	-	12.3	12.5	11.8	50	35	45	45	ESE	1	SE	2	ESE	4
19	746.8	746.2	745.2	22.0	27.7	22.5	24.2	29.0	22.0	-	17.5	16.6	11.0	88	60	51	66	SSE	3	SW	2	NNW	2
20	747.0	746.8	746.8	22.4	28.8	23.4	24.5	29.4	21.6	-	13.6	13.1	14.3	68	44	66	59	S	1	SSW	2	SSE	4
21	742.3	742.6	725.6	23.2	20.9	24.2	21.1	26.5	18.7	-	17.4	17.6	14.5	62	95	82	86	SE	5	NNW	6		
22	739.5	739.5	744.3	19.8	24.5	21.6	21.6	25.4	17.1	-	14.3	15.8	08.7	62	68	47	66	ENE	1	SW	3	NNE	1
23	742.5	743.6	743.9	19.4	22.0	22.6	18.6	27.0	15.6	-	11.1	13.5	12.5	66	66	85	74	NE	2	SE	2	ENE	3
24	744.4	745.9	749.1	18.2	22.0	18.4	18.3	22.6	16.4	-	10.0	17.7	07.2	64	39	45	49	NE	3	NE	5	NE	3
25	751.1	750.7	750.9	17.6	24.5	21.8	21.4	25.0	15.8	-	17.2	18.6	09.7	48	37	45	45	SSE	1	NW	3	N	3
26	751.4	751.5	751.5	18.8	25.4	21.6	21.9</																

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Insolacije broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	9	010	050	00	02.0	13.2	61.1	.	.	.
2	7	000	030	00	01.0	13.6	.	.	.	.
3	8	000	000	00	00.0	13.3	.	.	.	.
4	8	030	080	05	05.3	12.4	.	.	.	.
5	7	070	080	07	07.3	05.8	.	.	.	.
6	8	06	040	02	04.0	11.9	00.0	.	.	.
7	8	000	020	00	00.7	13.2	.	.	$\overline{P}_{SE}^{tr} H^{30} 24.2$	.
8	8	020	090	00	03.7	08.6	.	.	$\overline{P}_{SE}^{tr} 0-30$	.
9	7	010	020	04	02.3	13.2	.	.	.	.
10	8	010	090	01	03.7	09.4	.	.	.	.
11	8	000	040	01	01.7	13.4	.	.	.	.
12	8	010	060	00	02.3	12.6	.	.	.	.
13	8	000	010	00	00.3	12.5	.	.	.	.
14	8	010	020	01	01.3	11.8	.	.	.	.
15	8	080	010	09	06.0	07.7	00.8	.	$\bullet^{tr} 6^0-10^{35} i, R^0 7^{35} 7^0$	.
16	7	010	020	00	01.0	11.4	00.5	.	$\overline{P}_{SE}^{tr} rj-11^{30}$	.
17	7	04	040	00	02.7	11.2	.	.	$\overline{P}_{SE}^{tr} 8^{30}$	.
18	8	000	010	01	00.7	13.6	.	.	$\overline{P}_{SE}^{tr} rj-8^{30}$	.
19	8	000	010	00	00.3	13.0	.	.	.	.
20	8	000	030	00	01.0	13.2	.	.	$\overline{P}_{SE}^{tr} rj-8$	.
21	8	010	020	07	03.3	11.3	.	.	$\overline{P}_{NE}^{tr} 20^{35} n, \bullet^{tr} 10^{35} 20^{35} 20^{35}$	.
22	7	09	100R	08	09.0	03.1	00.5	.	$\overline{P}_{NE}^{tr} rj-10^{35} 14^{30} i, \bullet^{tr} 6^0-6^{35} 0^{20}, 10^{45}-14^{10}, R^0 12^{30}-14^{05}, P_{SE}^{tr} 15^{35}-15^{30}$	.
23	8	040	060	01	03.7	09.9	04.7	.	.	.
24	8	040	000	00	01.3	13.0	.	.	.	.
25	7	000	070	00	02.3	12.3	.	.	$\overline{P}_{SE}^{tr} rj-8$	.
26	7	080	080	09	08.3	02.0	.	.	$\bullet^{tr} 16^{35} 18^{35} i, \bullet^{tr} 20^{30} n$	.
27	9	010	010	01	01.0	12.2	00.5	.	$\bullet^{tr} 4^{30}-4^{35}$	.
28	8	030	020	00	01.7	12.6	.	.	.	.
29	8	020	020	01	01.7	13.5	.	.	.	.
30	8	020	010	00	01.0	11.4	.	.	.	.
31	8	07	010	05	04.3	10.0	00.1	.	$\overline{P}_{SE}^{tr} n, \bullet^{tr} 5-5^{30}$	.
MES.		02.5	03.7	02.0	02.7	347.9	68.2			

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1	8	08	09	10	09.0	02.1	.	$\overline{P}_{SE}^{tr} 12^{30}, R^2 n$	.	.
2	9	010	040	01	02.0	12.6	00.0	.	.	.
3	8	000	020	00	00.7	13.4	.	.	.	.
4	8	000	020	01	01.0	12.6	.	.	.	.
5	8	08	10	06	08.0	03.2	.	$\bullet^{tr} 10^{35} H^{10}$	.	.
6	8	08	060	02	05.3	04.5	00.2	.	.	.
7	7	000	020	00	00.7	12.3	.	.	.	.
8	7	000	040	00	01.3	10.6	.	.	$\overline{P}_{SE}^{tr} rj-10^{30}, 19^{30} n$	.
9	7	000	020	00	00.7	12.2	.	.	$\overline{P}_{SE}^{tr} rj-9^{30}$	.
10	7	060	030	00	03.7	09.3	.	.	$\overline{P}_{SE}^{tr} rj-9$	.
11	7	040	020	00	02.0	10.7	.	.	$\overline{P}_{SE}^{tr} rj-9$	.
12	7	030	030	00	04.0	12.7	.	.	$\overline{P}_{SE}^{tr} 10^{35} 7^{45}, H^{28}-13^{40} i, \bullet^{tr} 10^{35} 13^{30} i, R^2 12^{30}-12^{15}$	.
13	7	08	070	01	05.3	13.2	.	.	$\overline{P}_{SE}^{tr} 10^{35} 12^{30}, \bullet^{tr} 10^{35} 16^{30}, \bullet^{tr} 10^{35} 13^{30} i, R^2 12^{30}-12^{15}$	.
14	8	040	080	00	04.0	08.2	05.6	.	.	.
15	8	000	010	00	00.3	12.3	02.3	.	.	.
16	8	000	010	01	00.7	12.6	.	.	.	.
17	8	000	010	00	00.3	12.1	.	.	.	.
18	8	080	08	06	07.0	05.6	.	.	.	.
19	8	100	040	00	04.7	07.2	03.0	.	$\bullet^{tr} rj-7^{55}, T^4 15^{40} 16^{10}$	.
20	8	020	020	02	02.0	12.5	00.1	.	.	.
21	8	09	140	00R	05.7	01.2	.	$\bullet^{tr} 10^{35} n i, \overline{P}_{SE}^{tr} 21, R^2 H^{45} n$	.	.
22	8	04	070	02	04.3	08.2	45.4	.	$\overline{P}_{SE}^{tr} 10^{35}$	.
23	8	070	09	09	08.3	06.3	00.0	.	$\overline{P}_{SE}^{tr} 13^{30}-17^{45}, \bullet^{tr} 13^{32}-13^{30}, 16^{35}-20^{30} i$	.
24	8	060	050	00	05.7	10.5	20.8	.	.	.
25	8	000	010	00	00.0	12.4	.	.	.	.
26	8	000	010	03	01.3	12.0	.	.	.	.
27	8	040	020	00	02.0	11.7	.	.	.	.
28	8	060	040	00	02.3	09.3	.	.	.	.
29	8	010	010	01	01.0	11.4	.	.	.	.
30	8	000	000	00	00.0	11.4	.	.	.	.
31	8	10	10	07	09.0	00.0	00.1	.	$R^1 rj, 8^{05}-H^{25} i, \bullet^{tr} 5^{10}-5^{30}, \overline{P}_{SE}^{tr} 15^{35}-16^{10}$	.
MES.		03.7	04.2	02.0	02.3	282.9	61.5			

$\varphi = 43^{\circ}31' N$   $\lambda = 16^{\circ}26' E$  Gr.  $\Delta G = +1h\ 06\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C						Napon vodené pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	749.0	749.4	749.8	21.8	27.2	22.9	23.7	27.6	21.1	-	11.3	16.9	15.3	58	62	73	64	ESE 2	SSW 2	NNW 1	
2	748.8	749.0	748.0	21.6	25.4	22.2	22.9	28.0	20.5	-	14.4	16.0	12.5	75	66	62	68	SSE 1	WSW 1	NE 3	
3	747.8	748.3	749.2	21.3	26.8	22.2	23.1	28.1	20.4	-	15.5	16.1	12.5	83	61	62	69	-	0	SSW 3	NNE 2
4	749.3	749.3	749.8	21.8	28.1	24.0	24.5	28.4	20.5	-	19.1	11.9	11.0	51	42	45	47	NE 3	SW 1	NE 5	
5	751.2	751.6	752.1	23.2	29.2	24.9	25.6	29.5	22.5	-	09.2	14.6	10.3	42	35	44	41	ENE 3	SW 2	NE 4	
6	753.8	754.0	754.6	23.8	30.3	24.6	25.8	30.5	23.0	-	05.5	10.5	9.9	43	32	43	39	NE 3	SW 3	NNE 3	
7	754.4	753.7	753.3	23.0	29.2	24.8	25.5	29.5	22.2	-	10.8	11.1	10.1	51	36	43	43	ENE 3	WSW 2	ENE 4	
8	753.1	752.3	751.2	22.2	28.7	24.4	24.9	29.3	21.9	-	09.9	11.3	10.6	49	38	46	44	ENE 3	SW 3	WSW 1	
9	749.2	748.5	749.9	21.4	26.6	18.6	21.2	27.6	18.2	-	12.3	15.4	17.0	65	59	43	56	ESE 1	SW 2	NE 7	
10	754.3	754.8	756.0	16.2	28.5	17.2	17.8	21.0	12.2	-	05.4	05.3	16.3	39	29	43	37	NE 6	NE 5	NNE 3	
11	755.6	755.0	756.0	17.4	24.8	21.8	21.5	25.7	15.5	-	05.7	10.7	10.2	38	37	52	42	WSW 1	WNW 2	WNW 3	
12	756.4	756.0	755.0	20.3	27.7	22.4	23.2	27.7	15.4	-	10.1	12.4	10.5	57	45	47	50	NE 1	SW 2	WNW 1	
13	753.2	752.6	752.5	20.0	27.2	23.2	23.4	27.5	19.5	-	10.0	12.7	12.9	57	47	60	55	SE 4	SW 2	E 1	
14	755.4	756.5	756.2	19.0	25.4	15.6	20.5	26.0	16.8	-	07.9	10.1	9.7	48	41	44	44	NE 6	SW 3	NE 4	
15	755.6	753.5	751.2	16.2	23.6	19.5	19.7	24.0	15.4	-	08.4	08.7	10.8	31	44	64	56	ENE 1	SW 3	E 2	
16	748.8	747.7	747.3	16.8	23.7	16.0	19.6	24.1	15.5	-	07.9	11.9	13.5	55	54	82	64	ENE 1	SW 2	NE 1	
17	746.2	745.2	743.9	15.6	19.0	18.0	17.7	20.0	14.2	-	11.6	11.3	13.8	87	65	69	82	FSE 3	ENE 3	E 3	
18	744.6	746.4	748.9	18.3	18.1	15.6	16.9	20.0	15.4	-	13.9	14.6	15.4	88	93	71	84	S 1	SW 3	SW 1	
19	752.0	752.7	748.7	13.8	17.2	18.5	17.0	18.8	13.0	-	07.8	08.9	12.3	66	60	77	68	NE 3	NNW 2	SE 5	
20	748.1	748.7	748.6	17.8	22.0	17.6	18.6	22.5	16.0	-	13.2	12.0	11.6	86	61	73	72	NNW 3	SW 2	NW 1	
21	749.0	750.2	751.1	15.6	19.8	16.8	17.1	20.0	15.5	-	09.0	12.6	10.6	87	65	74	70	NE 1	SSE 2	ENE 1	
22	751.5	750.9	750.3	14.7	20.6	16.8	17.1	20.7	13.8	-	08.0	08.0	10.0	64	46	69	60	ENE 2	WSW 1	SE 3	
23	746.9	747.1	747.2	15.8	16.5	13.5	14.8	17.4	13.0	-	08.3	17.7	17.2	61	55	62	59	NE 5	NNE 4	NE 5	
24	747.3	748.6	750.8	15.0	19.3	15.0	16.1	19.5	13.5	-	06.5	05.9	05.6	51	35	44	43	NE 5	NE 5	NE 4	
25	751.6	752.5	753.9	14.5	19.0	15.8	16.3	20.4	13.6	-	06.7	07.4	17.4	54	45	55	51	NE 3	NNW 1	NE 3	
26	754.5	754.7	755.4	14.6	20.5	16.1	16.8	21.0	13.9	-	06.2	08.0	16.3	50	44	46	47	NE 3	SW 2	NE 4	
27	755.8	756.3	757.6	13.7	18.8	13.5	14.9	19.1	13.4	-	05.1	04.7	14.3	43	26	37	36	NE 5	NE 2	NE 4	
28	758.5	759.1	759.8	12.8	18.4	14.0	14.8	18.9	12.2	-	04.4	05.2	14.8	42	33	43	38	NE 5	SSW 2	NE 4	
29	760.3	759.5	758.7	10.8	18.1	15.3	14.9	18.4	10.1	-	04.3	06.5	17.5	44	42	57	48	NE 2	SW 2	E 2	
30	758.8	758.0	757.0	12.7	19.4	16.0	16.0	19.7	12.0	-	04.0	08.2	18.8	36	48	64	49	ENE 4	SW 4	W 1	
MES.	VRED.	752.0	752.1	752.1	17.7	25.0	19.1	19.8	23.7	16.5	-	06.9	10.4	19.6	57	48	57	54	2.6	2.4	2.6

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1	755.7	753.6	751.4	14.0	20.4	16.7	17.0	20.5	13.4	-	07.2	10.4	16.8	60	58	76	65	ENE 1	SW 2	SE 5
2	747.7	744.9	744.4	17.4	19.0	16.1	17.1	19.5	16.0	-	11.9	12.6	14.4	80	76	76	77	SE 5	SE 5	NNE 3
3	746.4	749.2	752.8	14.4	19.9	14.2	15.7	20.4	16.3	-	05.2	02.5	03.7	42	26	31	31	NE 2	NE 2	NE 4
4	756.3	757.2	756.7	12.9	18.5	14.6	15.2	19.8	11.9	-	04.0	06.6	07.7	35	41	46	46	LNE 3	SW 2	SSE 1
5	756.6	756.4	755.5	12.4	18.8	15.6	15.6	19.8	13.6	-	05.2	08.6	09.9	48	53	75	59	ENE 2	SE 3	ESE 3
6	754.0	752.5	752.0	14.2	19.7	17.3	17.1	20.0	13.9	-	07.6	10.6	11.4	62	61	77	67	ENE 3	SE 5	SE 2
7	751.0	750.3	750.4	17.4	20.6	17.7	18.4	21.0	16.7	-	10.8	12.3	12.2	72	68	81	74	ENE 3	SE 5	SE 4
8	749.1	748.0	746.2	16.9	21.2	18.5	18.8	21.7	16.4	-	11.1	11.3	11.3	77	68	71	69	ESE 3	SE 4	SE 4
9	744.5	744.5	745.5	29.2	19.2	17.7	18.7	20.8	16.5	-	12.5	14.4	10.7	65	67	73	74	SE 4	SE 4	E 3
10	745.5	747.1	748.4	16.6	28.6	16.0	17.0	20.6	15.7	-	11.5	14.6	13.3	81	91	86	86	ENE 2	SSW 1	ESE 4
11	746.2	747.2	749.7	16.8	20.8	17.4	18.1	21.3	16.4	-	13.2	13.5	11.6	92	76	78	82	SE 4	SSW 2	E 3
12	750.7	751.6	752.2	15.2	19.3	17.0	17.1	19.8	15.1	-	19.4	11.2	09.2	73	68	64	66	NE 2	WNW 1	NE 3
13	752.4	752.4	753.4	17.4	22.4	18.9	19.4	22.6	16.6	-	07.9	06.3	08.0	53	41	49	48	KE 4	SW 2	NE 4
14	752.5	751.9	752.0	16.4	22.0	16.1	16.2	21.4	15.6	-	07.4	09.0	07.2	53	46	43	47	NE 3	SW 2	NE 4
15	751.8	752.2	752.9	17.0	21.7	18.4	18.7	22.1	16.6	-	07.1	08.7	06.9	49	44	45	46	ENE 4	WSW 2	ENE 3
16	753.7	754.2	754.6	16.0	23.1	16.5	17.2	20.6	15.7	-	16.3	07.7	07.2	46	44	51	47	NE 4	SW 2	ENE 1
17	755.5	755.9	756.4	13.2	18.4	15.7	16.5	18.6	12.6	-	05.5	06.6	09.2	47	42	69	53	ENE 3	SW 3	NNE 1
18	757.9	758.6	759.2	12.6	18.6	14.9	15.3	18.9	12.4	-	05.5	09.4	09.7	55	59	76	65	ENE 2	SSW 2	NW 2
19	759.9	759.6	759.7	12.4	18.3	15.1	15.2	18.5	12.1	-	07.3	11.4	10.4	68	66	81	74	NE 3	SSW 3	NNW 3
20	759.3	758.7	758.5	14.0	19.6	16.0	16.5	19.8	13.1	-	19.3	10.9	09.8	77	61	71	73	NNW 2	WSW 2	NNW 2
21	758.5	758.1	758.2	14.2	19.6	16.4	16.9	19.5	13.8	-	08.2	10.9	16.8	58	66	77	76	ESE 2	SW 2	SF 1
22	758.7	758.8	759.3	15.6	19.9	17.2	17.3	19.4	15.2	-	10.2	05.5	05.3	77	58	63	66	SSE 1	SE 2	NNW 1
23	755.6	755.5	759.3	14.8	19.5	16.7	16.7	19.6	14.8	-	06.1	13.9	11.5	64	76	83	74	ESE 1	SW 2	NNW 3
24	759.8	758.5	757.8	15.1	20.3	16.8	16.4	20.0	15.6	-	05.3	11.2	14.6	72	63					

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vremenska časnost 0-9	Oblačnost N (0-10)					Insolacij broj sunca	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8	010	010	10	01.0	10.9	05.3	.	.	.	.
2	7	090	090	01	06.7	02.1	.	.	.	.	.
3	8	040	070	04	05.0	05.6	.	.	.	$T^0 14^{00} 15^{30}, \Delta 19^{45} N, i$	.
4	8	000	020	00	01.0	11.2	02.1	.	.	$T^0 16^{00} 18, \Delta 17^{00} 17^{47}, \Delta 17^{50} 17^{53}, \Theta^{tr-1} 17^{52} 18^{32}, i$	.
5	8	010	030	00	01.3	10.7	.	.	.	.	.
6	8	010	010	00	06.7	08.8	.	.	.	$T^1 15^{35} 16^{45}, \Theta^{tr-1} 15^{40} 16^{40}$	.
7	7	000	020	00	00.7	09.2	01.7	.	.	$\Delta 9^{32} 12$	.
8	7	000	010	00	00.3	10.2	.	.	.	$\Delta 9^{32} 11$	.
9	6	000	040	07	03.7	10.1	.	.	.	$\Delta 18^{02} 04, \Theta 22-22^{40} T^1 N$	.
10	8	060	030	00	03.7	09.5	01.6	.	.	$\Delta_{NE} 0-11^{40}, \Theta 9^{32} 10^{45}$	.
11	8	090	040	00	04.3	08.8	.	.	.	.	.
12	8	000	000	01	00.3	11.4	.	.	.	.	.
13	8	020	080	00	03.3	10.5	.	.	.	.	.
14	9	040	010	03	01.7	10.5	.	.	.	.	.
15	8	060	010	00	02.3	10.6	.	.	.	.	.
16	8	000	060	04	03.3	09.1	.	.	.	.	.
17	7	100	09	100	05.7	00.6	24.6	.	.	$\Theta^{tr-1} 22^{00} 7, 18^{40} 22^{40}, \Theta^{tr-1} 7-12^{10}, i, 22^{40}-23^{20}, \Delta 9^{20} 10^{20}$	.
18	7	10	10	03	07.7	04.4	68.7	.	.	$\Theta^{tr-1} 12^{00} 17^{20}, i, \Delta 12^{40} 13^{40}, \Delta 15^{45} 16^{45}, \Theta 19^{32} N$	.
19	8	000	10	100	06.7	03.6	08.3	.	.	$\Theta^{tr-1} 14^{05} N, \Delta 21^{02} 24^{40}, i, \Delta_{NE} 0-230$	.
20	8	10	060	09	08.3	04.4	04.2	.	.	$\Theta N, \Delta N, \Delta_{NE} 0-230$	.
21	8	09	080	08	08.3	03.6	.	.	.	.	.
22	8	040	09	100	07.7	04.9	.	.	.	$\Delta^1 rj-9, \Theta^{tr-1} 19^{02} 22^{50}$	.
23	8	10	10	07	09.0	00.6	02.5	.	.	$\Delta^{tr-1} 0^{40} 2^{40}, \Delta 15^{05}-19^{10}, i, \Delta_{NE} 1^{45} 10^{40}, i$	.
24	8	040	030	02	03.0	09.0	01.3	.	.	$\Delta_{NE} 6^{02}-9^{20}$	.
25	8	050	09	01	05.0	03.5	.	.	.	.	.
MES.											
VRED.		03.7	04.4	03.0	03.7	228.3	120.3				

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1	8	010	010	10	04.0	10.0	.	.	.	$\Theta^{tr-1} 22^{05} 23^{40}, i$	.
2	7	09	10	01	06.7	02.1	.	.	.	.	.
3	9	010	010	00	00.7	10.5	06.0	.	.	.	.
4	9	000	000	00	00.0	10.7	.	.	.	.	.
5	9	06	010	00	02.3	09.0	.	.	.	.	.
6	8	09	010	00	03.3	08.5	.	.	.	.	.
7	8	08	030	00	03.7	08.1	.	.	.	.	.
8	8	010	020	C3	02.0	05.7	.	.	.	.	.
9	7	090	09	07	08.3	02.6	.	.	.	.	.
10	7	100	070	100	05.0	04.9	12.4	.	.	$\Theta^{tr-1} 0^{40} 2^{40}, \Delta 8^{20}-8^{45}, \Delta 15^{20} 13^{45}, i, 20^{30}-21^{45}, T^1 rj-8^{10}, \Delta 13^{16}-13^{18}$	.
11	8	10	07	09	08.7	03.0	15.5	.	.	$\Theta^{tr-1} 0^{50} 2^{00} j, 14^{45}-15^{20}, i; \Delta 10^{20} 10^{30}, \Delta 10^{25} 11^{45}$	.
12	7	07	090	09	08.3	00.2	05.8	.	.	$\Theta^{tr-1} 18^{32} 19^{00}, i$	.
13	8	010	030	00	01.3	08.5	00.1	.	.	.	.
14	7	010	010	03	01.7	05.2	.	.	.	.	.
15	7	000	030	00	01.0	07.8	.	.	.	.	.
16	8	040	060	00	01.3	08.8	.	.	.	.	.
17	8	010	040	00	01.7	09.6	.	.	.	$\Theta 12^{20} 16^{30}, i$	.
18	7	000	010	00	00.3	10.4	.	.	.	$\Delta^2 rj-8$	.
19	6	000	000	00	00.0	10.2	.	.	.	$\Delta^2 rj-10, \Delta^2 rj-n$	.
20	6	000	010	00	00.3	09.2	.	.	.	$\Delta^2 rj-n, \Delta^2 rj-10, \Theta 14-14^{40}$	.
21	6	010	000	00	00.3	07.7	.	.	.	$\Delta^1 rj-10, \Delta^1 rj-n$	.
22	7	10	05	09	09.3	00.5	.	.	.	.	.
23	6	000	020	00	00.7	08.6	.	.	.	$\Delta^1 rj-9, \Delta^1 rj-n$	.
24	6	010	030	00	01.3	07.7	.	.	.	$\Delta^1 rj-n, \Delta^2 rj-9^{40}$	.
25	6	060	080	00	04.7	14.5	.	.	.	$\Delta^1 rj-n, \Delta^2 rj-10, \Theta 14-14^{40}$	.
26	7	010	010	02	21.3	08.1	.	.	.	$\Delta^1 rj-9^{30}$	.
27	6	010	010	00	00.7	08.5	.	.	.	$\Delta^2 rj-9^{45}, \Delta^1 rj-n$	.
28	6	000	070	02	03.0	06.6	.	.	.	$\Delta^1 rj-10, \Delta^2 rj-11^{30}$	.
29	6	010	010	00	00.7	07.8	.	.	.	$\Delta^2 rj-11, \Delta^1 rj-n$	.
30	6	09	060	06	07.0	06.5	.	.	.	$\Delta^2 rj-11^{45}, \Delta^1 rj-10^{30}$	.
31	6	05	09	01	06.3	05.3	.	.	.	$\Delta^1 rj-9^{45}, \Delta^1 rj-15^{45}$	.
MES.											
VRED.		03.8	03.6	02.3	03.2	221.2	34.2				

$\varphi = 43^{\circ}31' N$   $\lambda = 16^{\circ}26' E$  Gr.  $\Delta G = +1h\ 06\ min.$

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D S	Vzdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare • mm			Relativna vlažnost % u			Pravac i jačina veta D, f (0—12)		
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21
1	750.8	749.0	748.1	14.4	15.4	12.6	13.9	17.0	12.5	-	11.3	11.5	10.1	92	88	91	90	SSE 1	SSE 2	NE 3
2	749.1	749.8	750.9	12.9	17.3	13.1	14.1	17.6	11.5	-	06.2	06.8	06.2	56	46	55	52	NE 4	ENE 1	ENE 3
3	751.5	752.6	753.6	11.8	16.2	14.0	14.0	16.6	10.9	-	05.9	08.4	07.7	57	61	64	61	NE 2	SSW 1	ENE 2
4	753.2	753.0	753.4	13.6	17.5	16.2	15.9	18.0	12.5	-	06.6	10.1	09.9	57	67	72	65	ENE 2	SE 4	SE 3
5	753.4	752.7	754.1	16.6	18.5	17.0	17.3	18.7	15.0	-	09.7	12.7	12.9	68	79	89	79	ESE 3	SE 5	ESE 2
6	753.6	753.5	754.5	16.1	19.4	16.8	17.3	20.0	16.0	-	10.8	12.9	12.7	79	76	88	81	ENE 1	SSE 2	NNW 1
7	755.8	756.3	757.0	15.3	19.0	16.4	16.8	19.4	14.7	-	10.8	12.4	10.7	83	75	76	78	NNE 2	WSW 3	- 0
8	757.6	757.6	758.5	13.5	18.2	14.8	15.3	18.3	12.6	-	09.1	10.8	10.2	78	69	81	76	NE 2	SSW 2	SSE 1
9	758.9	758.5	758.0	11.8	16.8	13.9	14.1	17.2	11.5	-	08.2	09.3	09.6	79	65	80	75	NE 1	SSW 1	SSE 1
10	757.1	757.0	757.5	11.2	15.4	14.2	13.8	15.6	10.7	-	08.7	09.5	09.7	87	73	80	80	NNE 1	WSW 1	NNW 1
11	758.2	757.9	758.0	13.5	18.4	15.6	15.8	18.7	13.3	-	07.9	10.6	10.4	68	67	78	71	NNE 1	SSW 1	NW 1
12	756.2	754.3	752.5	13.6	16.4	15.2	15.1	17.2	13.5	-	08.2	11.0	11.4	70	79	88	79	- 0	WNW 1	E 2
13	747.9	744.5	740.6	14.6	16.9	17.2	16.5	17.2	14.0	-	09.7	11.1	11.4	78	77	78	76	ENE 1	SE 4	SSE 4
14	739.5	740.2	741.9	13.4	18.4	13.2	14.1	17.8	13.2	-	05.9	07.4	08.1	51	53	71	58	NE 5	ESE 2	NE 2
15	741.1	740.2	740.0	11.8	15.4	15.6	14.6	16.4	11.4	-	08.5	09.3	10.4	62	71	78	77	SSW 2	SE 4	SE 4
16	736.2	734.3	734.2	15.4	13.0	10.4	12.3	16.5	08.5	-	10.8	09.8	06.4	82	87	68	79	SSW 3	NNW 2	WNW 2
17	739.4	740.0	738.6	06.4	09.8	10.8	09.5	11.1	05.7	-	04.8	06.9	07.9	67	76	82	75	WSW 2	SSE 4	ENE 3
18	741.6	743.6	745.7	09.6	13.0	10.4	10.9	13.3	05.8	-	05.4	07.0	05.1	60	63	54	59	ENE 2	SSW 2	ENE 1
19	746.6	749.6	752.4	08.2	10.3	07.4	08.3	11.0	07.3	-	04.9	03.1	02.9	61	33	38	44	NE 4	NE 3	ENE 3
20	751.7	750.0	749.4	05.0	10.2	07.9	07.8	10.6	04.9	-	02.6	03.5	02.6	40	37	33	37	NE 3	SSW 2	ENE 2
21	748.9	746.0	743.8	05.3	11.6	11.5	10.0	12.0	04.7	-	03.5	06.2	08.2	52	61	81	65	ENE 3	SSE 5	SSE 7
22	740.3	741.6	743.9	16.0	13.7	12.2	13.5	16.4	11.5	-	11.0	08.3	06.6	81	70	62	71	S 6	NW 3	NE 1
23	745.4	747.9	750.4	08.9	09.6	08.4	08.8	12.5	08.4	-	07.3	06.2	04.4	85	69	53	69	NNW 3	NNW 3	ENE 3
24	752.0	751.4	750.2	06.3	11.4	08.6	08.7	11.4	05.8	-	03.5	04.4	04.3	49	44	51	48	NE 4	SSE 2	ESE 3
25	746.8	743.1	739.6	07.2	10.8	12.2	10.6	12.4	06.5	-	04.8	05.6	06.4	63	58	60	60	ESE 3	SE 5	NNW 1
MES. VRED.	748.4	748.3	748.6	10.6	13.8	12.0	12.1	14.9	05.4	-	07.0	08.0	07.8	69	64	70	68	2.6	2.7	2.5

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1	745.3	744.1	743.4	11.4	14.2	12.1	12.5	14.8	10.6	-	08.4	08.8	09.1	83	73	86	81	ENE 1	SSW 1	SE 1
2	740.5	743.1	744.6	03.2	04.8	04.2	04.1	12.5	03.0	-	04.3	02.9	02.5	75	44	40	53	ENE 6	NNE 6	NE 8
3	750.5	751.3	753.3	03.0	05.6	06.5	05.4	06.6	02.5	-	02.4	01.9	03.2	43	24	38	38	NE 5	NE 5	NE 6
4	755.0	755.6	756.0	06.0	08.0	05.7	06.4	09.4	05.4	-	02.3	01.9	01.8	33	24	26	28	NE 5	NE 5	NE 5
5	753.7	752.3	751.9	03.6	08.2	04.0	05.0	08.6	02.9	-	02.0	02.2	02.6	33	27	42	34	ENE 4	SSW 2	ENE 2
6	750.0	747.3	743.2	04.2	05.4	16.0	08.4	10.7	03.0	-	03.2	06.0	08.3	51	68	90	70	ENE 3	SE 5	SSE 7
7	744.0	747.9	750.8	09.4	09.8	08.4	09.0	11.5	08.0	-	06.7	06.8	05.6	76	75	68	73	K 2	W 2	NE 2
8	751.5	750.5	749.4	06.5	11.4	11.0	10.0	11.9	06.0	-	04.7	06.3	06.0	64	63	61	63	ENE 2	SE 3	ESE 4
9	746.6	744.9	742.8	12.8	13.0	12.5	12.7	13.6	10.6	-	07.8	09.4	10.8	70	94	83	83	SE 6	SE 5	ESE 4
10	743.0	745.9	749.0	12.4	14.2	12.0	12.7	14.7	10.6	-	08.0	07.4	05.1	74	61	49	61	E 3	ESE 4	NE 3
11	753.4	755.6	757.4	09.3	13.7	08.5	10.0	14.0	08.5	-	04.7	06.2	04.0	53	52	45	51	NE 5	S 3	NE 4
12	759.1	759.4	760.0	06.6	11.2	07.5	08.2	11.5	06.0	-	03.5	04.0	02.3	48	40	29	39	ENE 4	SSW 2	NE 2
13	759.8	758.7	758.2	04.8	08.6	05.2	06.0	09.0	04.1	-	02.2	03.0	02.5	34	36	38	36	NE 2	NN 1	NE 3
14	758.5	759.1	759.6	04.9	10.1	08.0	07.8	10.3	04.0	-	01.8	02.8	02.2	26	30	27	28	NE 3	SW 1	NE 4
15	758.7	758.3	757.9	07.2	10.4	08.4	08.6	10.6	05.5	-	02.9	04.2	04.6	38	45	55	46	NNW 1	NNW 2	NW 1
16	760.6	761.1	761.0	06.4	09.8	06.2	07.2	10.1	05.9	-	02.9	03.3	02.5	40	36	35	37	NE 5	NE 2	NE 4
17	758.8	759.6	760.7	07.4	07.4	05.2	06.3	09.5	05.2	-	02.6	02.5	01.8	34	32	27	31	NNE 2	NE 4	ENE 3
18	757.8	756.3	756.0	04.8	09.8	08.4	07.9	10.2	04.2	-	01.5	02.9	02.3	24	32	27	28	NE 2	SW 1	ENE 2
19	755.1	755.2	755.8	05.7	10.1	08.2	08.1	10.5	05.1	-	01.7	03.0	02.6	25	32	32	30	NE 2	SSW 1	NE 2
20	756.2	756.0	756.1	05.5	10.0	08.4	08.1	10.2	04.5	-	02.6	04.9	03.3	36	53	36	43	NE 3	1	ENE 1
21	756.7	756.5	756.9	06.4	10.7	08.4	08.5	10.9	05.5	-	02.7	03.8	03.1	38	39	37	38	ENE 2	SSW 1	NE 1
22	758.0	759.1	760.4	05.2	09.9	07.1	07.3	10.2	04.3	-	02.8	03.5	03.2	43	39	42	41	NE 2	SSW 1	ENE 2
23	761.6	761.9	762.8	04.9	09.2	07.0	07.0	09.4	03.7	-	03.0	05.1	03.8	46	59	50	52	NE 1	SSW 2	N 1
24	762.5	761.6	759.7	06.5	09.4	08.8	08.4	09.9	05.6	-	04.1	06.1	06.3	57	69	74	67	NE 1	SSW 1	ENE 1
25	753.5	750.7	752.8	09.0	08.1	09.3	08.9	10.6	07.9	-	06.9	07.7	05.5	80	95	62	79	ESE 3	ENE 3	NW 3
26	755.5	755.4	755.3	09.8	11.2	08.8	09.7	11.7	08.2	-	04.5	04.4	03.9	50	44	46	47	NE 2	NNE 4	ENE 3
27	753.2	751.4	750.1	07.7	10.8	08.5	09.1	11.7	06.6	-	03.4	05.6	05.6	43	58	65	55	ENE 3	SSE 2	SE 3
28	747.9	746.9	748.1	10.3	11.5	12.8	11.9	13.2	08.6	-	06.6	08.2	05							

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vr. Mj.	Oblačnost N (0-10)					Insečcija četvrti čas	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10	100	100	10.0	00.0	.	.	.	$\Delta^2 p_j-7^{25} = p_j-10^{30}, \bullet^0 7^{30}-9^{25} i, 13^{20} n, i$
2	9	030	050	00	02.7	08.3	21.3	.	.	.
3	8	060	050	00	03.7	07.3	.	.	.	.
4	8	09	090	09	09.0	04.7	.	.	.	$\oplus 12^{20}-13^{25}$
5	7	10	050	03	07.3	00.5	.	.	.	$\bullet^0 15^{25}-16^{20}$
6	7	09	09	04	07.3	02.8	00.0	.	.	$\Delta^2 p_j-9$
7	7	080	020	00	03.3	06.3	.	.	.	$\Delta^2 p_j-10 = p_j-13^{25}$
8	7	020	010	00	01.0	08.3	.	.	.	$\Delta^2 p_j-11^{20} = p_j-12^{30}, 15^{20} n$
9	6	000	030	00	01.0	07.7	.	.	.	$\equiv n-n, \Delta^2 p_j-10^{20}$
10	6	08	090	07	08.0	00.1	.	.	.	$\equiv n-n, \Delta^2 p_j-10^{20}$
11	6	02	d10	00	01.0	08.5	.	.	.	$\equiv n-n, \Delta^2 p_j-13^{20}$
12	6	000	000	07	02.3	08.1	.	.	.	$\equiv n-n, \Delta^2 p_j-12^{20}, 17^{20}$
13	7	10	10	10	10.0	00.0	.	.	.	$\equiv n-n, \Delta^2 p_j-17^{20}, \Delta^2 n-15^{25}, 20, i$
14	8	08	080	04	06.7	01.8	.	.	.	$\bullet^0 13^{25}-14^{20}$
15	9	05	09	04	06.0	04.2	00.0	.	.	$\Delta^2 p_j-10^{20}$
16	8	09	080	090	06.7	01.5	.	.	.	$\bullet^0 24^{20}-13^{25} i, 16^{20} n, i, \Delta^2 19^{25}-19^{30}, \Delta^2 19^{25}-19^{35}$
17	6	01	100	10	07.0	02.9	07.6	.	.	$\bullet^0 12^{20} n, i, \Delta^2 19^{25}-19^{35}$
18	8	07	030	06	05.3	06.8	11.5	.	.	$\bullet^0 7^{20} B, i$
19	9	10	020	00	04.0	05.8	00.1	.	.	$\bullet^0 7^{20} B, i$
20	9	01	010	00	00.7	09.0	00.0	.	.	.
21	8	050	09	10	08.0	04.8	.	.	.	$\Delta^2 H^{25}-24, \bullet^0 18^{20}-20$
22	7	10	100	09	09.7	00.0	01.0	.	.	$\Delta^2 3-0-10^{20} i, \bullet^0 7^{20} g^{20} i, 13^{25}-15^{20} i$
23	8	100	10	05	08.3	00.0	03.2	.	.	$\bullet^0 5-14^{20} i$
24	9	00	020	04	02.0	08.7	02.2	.	.	.
25	8	08	09	10	09.0	00.2	.	.	.	$\bullet^0 24^{20}$
26	8	100	10	100	10.0	00.0	15.7	.	.	$\bullet^0 0-10^{20}, H^{20} 21, i, \Delta^2 20^{20}-21^{20} i$
27	9	04	050	04	04.3	07.9	02.1	.	.	$\bullet^0 17^{20} 24 i, T^0 20^{20}-20^{20}, \Delta^2 20^{20} n$
28	9	03	07	10	06.7	04.5	.	.	.	$\bullet^0 0-1$
29	8	01	07	09	05.7	05.4	07.3	.	.	$\bullet^0 6-50, g^{20}-12^{20} i, H^{20} 23, i$
30	7	10	09	100	09.7	00.5	00.5	.	.	.
MES. RED.		06.0	06.4	05.5	05.9	126.6	72.5			

1	7	09	080	10	09.0	03.7	02.7	.	.	$\bullet^0 20^{25}-24$
2	8	100	09	10	09.7	01.1	20.4	.	.	$\bullet^0 0-9^{20} i, \Delta^2 H^{20}-NE 4^{20} 24$
3	8	07	070	03	05.7	02.4	00.0	.	.	$\Delta^2 0-24 i$
4	8	04	020	00	02.0	08.5	.	.	.	$\Delta^2 NE 0-8^{20} i$
5	9	01	000	00	00.3	08.8	.	.	.	.
6	8	08	10	100	09.3	02.4	.	.	.	$\Delta^2 H^{25}-24, \bullet^0 18^{20}-20$
7	8	10	09	00	06.3	02.4	14.5	.	.	$\bullet^0 0-440 i, 7^{20} 7^{20}, \Delta^2 0-145$
8	8	05	08	09	07.3	02.6	00.0	.	.	.
9	7	100	10	100	10.0	00.0	00.2	.	.	$\bullet^0 0-10^{20}, \Delta^2 24 i, \Delta^2 2^{20} 12, 19^{20} 24 i$
10	8	100	09	02	07.0	01.4	21.2	.	.	$\bullet^0 0-9^{20} i$
11	8	01	000	00	00.3	07.6	00.8	.	.	.
12	8	01	000	00	00.3	08.2	.	.	.	.
13	8	00	040	03	02.3	06.6	.	.	.	.
14	8	02	000	00	00.7	07.9	.	.	.	.
15	8	08	020	04	04.7	03.5	.	.	.	$\Delta^2 H^{25}-24$
16	8	00	010	00	00.3	07.3	.	.	.	$\Delta^2 H^{20}-NE 0-12^{20} i$
17	8	00	010	00	00.3	08.0	.	.	.	$\Delta^2 10^{20}-12^{20} i$
18	8	00	000	00	00.6	08.5	.	.	.	.
19	9	00	010	00	00.3	08.5	.	.	.	.
20	8	01	030	00	01.3	08.2	.	.	.	.
21	8	02	010	00	01.0	08.0	.	.	.	.
22	8	00	010	00	00.3	08.1	.	.	.	.
23	7	00	010	00	00.3	07.5	.	.	.	.
24	7	10	10	10	10.0	00.0	.	.	.	.
25	5	10	100	01	07.0	00.0	.	.	.	$\bullet^0 0-16^{20}, \Delta^2 18^{20} n$
26	8	08	050	09	07.3	06.5	15.0	.	.	.
27	8	00	010	01	00.7	08.3	.	.	.	.
28	7	10	10	100	10.0	00.0	.	.	.	$\Delta^2 H^{25}-NE 10^{20}, \bullet^0 20^{20}-23^{20} i$
29	7	100	100	100	10.0	00.0	22.6	.	.	$\bullet^0 0-24 i, \Delta^2 20-20 i$
30	8	10	09	07	08.7	03.0	11.3	.	.	$\bullet^0 0-6^{20} i$
31	9	09	010	00	03.3	07.8	02.1	.	.	$\bullet^0 0-6^{20}, \Delta^2 H^{20}-NE 5^{20} 7^{20}$
MES. RED.		05.0	04.6	03.5	04.4	157.2	110.8			

$\varphi = 43^{\circ} 43' N \lambda = 18^{\circ} 16' E$  Gr.  $\Delta G = + 1h 13 min.$ 

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S D	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare • mm			Relativna vlažnost % u%			Pravac i jačina vetra D, f (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	594.2	593.7	593.1	-03.2	-02.2	-03.0	-02.9	-01.2	-03.2	-	03.5	03.8	03.6	97	96	97	97	SW	3	SW	2	SW	5
2	592.5	593.0	596.0	-03.6	-02.2	-01.0	-02.0	-01.0	-03.9	-	03.4	03.8	04.2	97	98	99	98	SW	8	SW	7	SW	4
3	597.1	597.7	598.3	-00.6	-00.2	-01.2	-00.8	-00.1	-01.4	-	04.4	04.5	04.2	99	100	99	99	SW	3	-	0	SW	4
4	599.0	600.0	601.2	-01.3	-00.4	-01.1	-01.0	-00.4	-01.3	-	04.1	04.4	04.2	99	100	99	99	SW	4	SSW	5	S	5
5	602.0	602.0	602.2	-03.1	02.2	-00.6	-01.0	00.3	-03.2	-	03.5	04.7	04.4	97	100	99	99	S	5	SSW	5	-	0
6	602.7	602.2	601.1	-01.4	-01.0	-02.5	-01.5	-00.5	-02.5	-	04.1	04.2	03.7	99	99	98	99	NW	1	NW	1	-	0
7	599.8	598.2	596.8	-03.3	-02.9	-02.5	-02.8	-02.3	-03.3	-	03.5	03.6	03.7	97	97	98	97	N	2	N	1	SW	5
8	593.4	592.6	591.2	-05.8	-10.4	-12.8	-10.5	-02.3	-12.8	-	02.8	01.9	01.5	94	90	88	91	NNW	6	N	7	N	8
9	590.0	589.9	589.8	-10.8	-10.8	-08.5	-09.7	-08.5	-12.9	-	01.8	01.8	02.1	96	93	88	89	N	10	N	5	N	2
10	587.5	585.4	584.3	-05.6	-04.8	-04.4	-04.8	-04.4	-05.0	-	02.9	02.9	03.2	95	92	96	94	SSW	9	SSW	11	SSW	12
11	584.9	580.2	580.8	-04.5	-03.4	-03.0	-03.5	-03.0	-04.8	-	03.1	03.5	03.6	96	97	97	97	SSW	13	SSW	14	SSW	14
12	583.6	581.9	582.3	-02.6	-02.2	-03.6	-02.6	-02.0	-04.4	-	03.7	03.8	03.4	97	97	97	97	SSW	16	SSW	11	SSW	7
13	579.1	581.5	583.6	-03.8	-04.0	-05.0	-04.5	-03.4	-05.0	-	03.3	03.3	03.0	96	96	95	96	SW	13	SW	5	SW	7
14	586.4	587.8	588.7	-04.4	-06.4	-06.0	-05.7	-03.2	-06.4	-	03.2	02.7	02.8	96	94	94	95	SW	3	SW	6	SW	7
15	585.9	581.7	585.9	-03.4	-03.4	-03.8	-03.6	-02.6	-06.0	-	03.5	03.5	03.3	97	97	96	97	SW	13	W	12	SW	3
16	586.2	585.7	585.0	-07.0	-07.2	-11.6	-09.4	-03.6	-11.6	-	02.5	02.5	01.6	93	93	81	90	NW	2	N	4	N	10
17	583.4	582.6	583.7	-12.0	-12.4	-12.7	-12.5	-11.5	-12.8	-	01.6	01.6	01.5	85	85	86	89	N	12	N	12	N	12
18	585.7	586.1	588.1	-13.1	-12.1	-12.6	-12.6	-12.0	-13.1	-	01.5	01.6	01.5	88	88	88	89	N	11	N	10	N	7
19	588.1	588.2	588.0	-09.2	-06.6	-06.6	-07.0	-06.1	-12.6	-	02.1	02.6	02.7	91	94	94	93	E	10	S	7	S	13
20	589.1	589.6	590.1	-06.3	-06.7	-06.6	-06.6	-06.0	-07.0	-	02.7	02.6	02.6	94	94	94	94	SSW	11	SSW	7	SSW	7
21	590.4	591.4	593.0	-06.1	-05.6	-04.8	-05.3	-04.6	-06.6	-	02.7	02.9	03.1	94	95	95	95	SSW	8	SSW	7	WSW	6
22	593.4	593.2	593.8	-04.7	-04.3	-03.8	-04.2	-03.7	-05.6	-	03.1	03.2	03.3	95	96	95	96	W	5	WSW	5	SSW	8
23	593.2	591.8	590.3	-03.8	-02.6	-02.6	-02.9	-02.4	-04.0	-	03.3	03.7	03.7	96	97	97	97	SW	8	SSW	9	S	7
24	587.2	587.8	588.8	-02.6	-01.8	-02.4	-02.3	-01.6	-02.7	-	03.7	03.9	03.8	97	98	98	93	SSW	7	SSW	5	NNW	5
25	590.4	591.0	591.5	-03.2	-02.4	-01.8	-02.3	-01.7	-04.0	-	03.5	03.8	03.9	97	98	98	98	NNW	5	W	2	W	4
26	589.2	587.6	585.8	-01.9	-01.4	-01.8	-01.7	-01.3	-02.0	-	03.9	04.1	03.9	98	99	98	98	SW	11	SW	9	SW	10
27	585.2	585.8	587.5	-01.6	-00.8	-01.5	-01.4	-00.7	-02.3	-	04.0	04.3	04.0	98	95	99	99	SW	10	SW	10	SW	6
28	589.7	590.3	589.0	-05.6	-01.0	-01.6	-02.4	-00.9	-05.3	-	02.9	02.6	03.2	95	94	95	95	NNW	2	SW	6	SW	8
29	585.4	580.7	582.5	-01.0	-00.4	-01.6	-01.2	-00.3	-02.2	-	04.2	04.4	04.0	99	100	98	99	SW	8	SW	10	SW	10
30	586.6	588.3	588.0	-03.2	-03.0	-03.4	-03.3	-01.6	-03.4	-	03.5	03.6	03.5	97	97	97	97	SW	7	SW	7	SW	8
31	589.5	588.7	587.3	-03.8	-03.6	-03.6	-03.7	-03.3	-03.8	-	03.3	03.4	03.4	96	97	97	97	SW	6	SW	8	SW	8
MES.	VRED.			590.0	589.6	590.0	-04.6	-04.1	-04.4	-04.4	-03.1	-05.6	-	03.2	03.4	03.3	96	96	95	96	7.5	6.8	6.7

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1	583.5	585.2	589.5	-03.2	-02.4	-02.4	-02.6	-02.2	-03.6	-	03.5	03.8	03.8	97	98	98	98	SW	10	SW	5	SW	6
2	584.6	585.4	586.3	-02.8	-02.6	-04.0	-03.4	-02.4	-04.0	-	03.6	03.7	03.3	97	97	96	97	SSW	7	S	7	SSW	6
3	587.0	587.7	588.0	-05.6	-07.0	-08.8	-07.6	-04.0	-08.8	-	02.9	02.5	02.2	95	93	92	93	N	2	NE	3	N	3
4	588.0	590.0	592.0	-11.2	-08.6	-08.2	-09.1	-08.0	-11.8	-	01.8	02.2	02.3	90	92	92	91	N	6	N	5	N	5
5	592.4	593.3	593.8	-04.0	-04.4	00.2	-02.0	00.2	-08.2	-	03.3	03.2	04.7	96	96	100	97	NW	4	N	4	N	7
6	593.0	590.0	588.0	-00.8	-00.8	-04.4	-02.6	00.8	-04.4	-	04.3	04.3	03.2	99	99	96	98	SSW	7	SW	8	N	11
7	590.0	592.4	592.8	-05.6	-06.5	-04.4	-05.2	-04.4	-06.6	-	02.9	02.6	03.2	95	94	95	95	N	4	N	7	NNE	7
8	591.6	590.0	587.4	-02.7	-01.7	-04.2	-02.8	-02.4	-04.4	-	03.7	04.1	03.0	97	97	98	98	SSW	11	SW	12	SW	12
9	588.2	589.1	589.0	-02.6	-01.7	-01.9	-02.0	-01.5	-03.2	-	03.7	04.0	03.9	97	98	98	98	SW	9	SW	7	SW	7
10	588.4	585.1	587.3	-02.7	-01.7	-01.3	-00.2	-00.2	-02.9	-	03.7	04.1	04.5	97	99	100	99	SW	8	SW	13	SW	12
11	582.7	581.7	585.6	00.0	-01.4	-00.7	-00.7	00.0	-01.8	-	04.6	04.1	04.4	100	95	100	100	SW	13	W	11	SW	9
12	578.7	581.6	583.4	-06.4	-01.0	-02.7	-01.7	-00.3	-02.7	-	04.5	04.3	03.7	100	100	97	99	SSW	14	SSW	11	SSW	10
13	586.2	589.3	588.7	-03.8	-02.9	-01.7	-02.5	-01.2	-03.5	-	03.3	03.6	04.0	96	97	98	97	SW	11	SW	5	E	5
14	588.3	582.4	583.1	-05.2	-06.5	-07.1	-06.5	-01.4	-07.1	-	03.0	02.6	02.5	95	94	93	94	N	8	N	6	N	7
15	585.7	585.5	586.6	-05.8	-02.2	-05.0	-04.5	-02.1	-07.3	-	02.8	03.8	03.2	94	98	100	97	WSW	2	SW	7	SW	6
16	586.7	586.9	587.5	-05.8	-04.6	-05.1	-05.2	-04.4	-05.8	-	02.8	03.1	03.0	94	95	95	95	SW	6	SW	8	SW	5
17	587.6	589.2	591.0	-06.4	-05.8	-06.8	-06.5	-05.1	-07.0	-	02.7	02.8	02.6	94	94	94	94	N	4	N	5	N	2
18	592.2	593.9	595.4	-03.8	-02.3	-02.1	-02.6	-02.0	-07.0	-	03.3	03.8	03.8	96	98	98	97	SW	6	WSW	5	WSW	5
19	594.7	594.3	592.3	-02.0	-01.5	-02.2	-02.1	-01.8	-02.2	-	03.9	03.9	03.8	98	98	98	98	SW	7	SW	8	SW	10

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 $H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vrijednost O₉	Oblačnost N (0-10)					Isotermalni broj seni	Padavina R mm	Snežni pokrivac h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies					
1	8	06	05	06	07.0	00.2	.	12t			
2	1	09	10	10	05.7	00.0	.	124			
3	6	09	09	10	06.3	00.0	.	122			
4	1	28	10	10	05.3	00.0	.	110			
5	1	08	10	05	07.7	01.0	00.8	111			
6	1	08	10	10	09.0	00.6	.	109			
7	9	17	10	10	10.0	00.0	0.1	101			
8	0	10	10	10	06.7	00.0	02.0	101			
9	9	16	08	02	06.7	04.7	01.2	102			
10	8	10	10	10	05.3	01.5	.	97			
11	6	10	10	10	10.0	00.0	.	96			
12	6	10	16	10	10.0	00.0	02.1	95			
13	0	10	10	10	10.0	00.0	22.2	122			
14	1	10	02	02	04.0	06.1	10.0	128			
15	0	10	10	10	10.0	00.0	.	120			
16	0	10	10	10	10.0	00.0	13.2	134			
17	0	10	10	10	10.0	00.0	0.0	141			
18	0	10	10	03	06.7	00.0	10.7	150			
19	9	00	01	02	01.0	09.5	01.0	148			
20	0	10	10	10	10.0	00.6	.	143			
21	6	10	10	10	00	06.7	00.0	146			
22	9	05	02	10	05.7	08.1	02.2	146			
23	8	08	10	10	10	05.3	02.3	.	141		
24	0	10	10	10	10	10.0	00.0	144			
25	8	10	04	01	05.0	06.8	02.1	147			
26	0	02	10	10	10	07.3	00.0	.	147		
27	0	10	10	10	10	10.0	00.0	02.7	150		
28	8	00	08	10	06.0	05.4	01.0	151			
29	0	10	10	10	10	10.0	00.0	01.8	150		
30	1	10	10	10	10	10.0	00.0	07.7	157		
31	0	10	10	10	10	10.0	00.0	06.7	164		
MES. VRED.		08.5	08.7	07.6	06.3	47.9	105.6				

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1	1	10	10	10	10	00.0	06.4	170			
2	0	10	10	10	10	10.0	00.0	17.4	185		
3	3	10	01	10	07	02.6	05.6	185			
4	8	00	04	02	02.0	09.2	.	182			
5	9	08	05	05	06.0	07.3	.	170			
6	0	09	10	10	09.7	00.4	.	160			
7	5	10	05	01	06.7	03.5	03.6	154			
8	9	01	09	10	06.7	06.9	01.0	154			
9	0	10	10	10	10.0	00.0	.	151			
10	0	10	10	10	10	10.0	00.0	00.3	149		
11	6	10	10	10	10	10.0	00.3	10.3	131		
12	0	10	10	10	10	10.0	00.0	14.0	139		
13	0	10	10	10	10	10.0	00.0	14.0	146		
14	0	10	10	10	10	10.0	00.0	12.0	157		
15	0	10	10	10	10	10.0	01.9	42.0	197		
16	2	10	10	10	10	10.0	00.9	.	190		
17	1	10	10	10	10	10.0	00.0	02.5	193		
18	8	02	06	00	02.7	05.6	.	191			
19	1	10	10	10	10	10.0	00.0	.	187		
20	0	10	10	10	10	10.0	00.0	04.7	192		
21	6	10	10	10	10	10.0	00.0	.	188		
22	0	10	10	10	10	10.0	00.0	05.1	186		
23	3	10	10	10	10	06.7	00.0	12.0	165		
24	8	08	08	01	05.7	02.2	00.8	157			
25	8	09	10	10	10	09.7	01.5	.	140		
26	8	10	10	10	10	10.0	04.4	00.4	132		
27	8	10	04	04	06.0	05.7	06.0	132			
28	0	10	10	10	10	10.0	00.7	02.7	132		
MES. VRED.		08.8	08.8	08.0	06.5	53.1	161.8				

$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$  Gr  $\Delta G = +1h\ 13\ min.$ 

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d	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenе pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	588.6	590.5	590.8	-17.2	-13.2	-12.6	-13.9	-12.6	-18.4	-	01.0	01.5	01.5	85	88	88	87	N	13	N	12	N	11
2	591.2	593.4	593.8	-13.4	-11.8	-11.8	-12.2	-11.6	-13.4	-	01.4	01.7	01.7	88	89	89	89	N	10	N	7	N	8
3	590.5	591.4	594.0	-03.4	-01.2	-00.4	-01.4	-00.4	-11.8	-	03.5	04.2	03.6	97	95	81	92	N	11	N	15	M	3
4	592.6	593.8	594.8	-00.4	01.2	02.6	01.5	03.4	-01.5	-	03.3	03.3	02.3	73	65	42	60	N	8	N	8	NW	2
5	594.2	595.3	596.3	-01.0	-02.4	-02.8	-02.3	02.6	-03.3	-	03.7	03.5	01.9	86	91	51	76	NW	6	NW	7	NW	9
6	596.7	597.5	598.1	-02.0	00.6	00.6	00.0	01.4	-03.2	-	01.8	02.0	02.0	44	42	41	42	SW	8	SW	8	NW	6
7	598.6	600.0	601.0	-00.4	-00.1	-03.6	-01.9	01.6	-03.6	-	02.3	03.5	03.4	52	76	57	75	NNW	5	N	3	N	5
8	603.8	605.2	605.9	03.6	02.8	01.1	02.2	04.0	-04.2	-	06.9	03.5	04.1	16	62	83	54	ENE	4	-	0	S	1
9	603.0	602.0	600.3	00.6	01.1	00.5	00.7	01.4	00.0	-	03.5	04.0	04.7	72	81	98	84	SSW	7	SW	5	WNW	5
10	596.9	595.9	594.7	00.9	00.7	-06.5	00.2	02.5	-00.7	-	04.4	04.8	04.4	91	100	100	97	NNW	5	N	5	-	0
11	593.4	593.1	592.0	-00.8	00.6	-00.2	-00.2	00.9	-01.1	-	04.3	04.2	04.1	100	88	91	93	WSW	4	SSW	8	SSW	9
12	589.8	589.6	588.5	-02.2	-01.7	00.0	-01.0	00.0	-02.7	-	03.8	04.0	04.6	98	98	103	99	SSW	12	SSW	10	SSW	10
13	585.6	587.2	588.4	-02.3	-01.0	-04.8	-03.2	00.0	-04.8	-	03.8	04.3	03.1	98	100	95	98	S	11	SSW	8	N	8
14	590.1	594.4	595.4	-05.7	-03.6	-04.3	-04.5	-03.5	-05.7	-	02.8	03.4	03.2	95	97	96	96	N	13	N	7	N	7
15	596.0	597.2	597.7	-04.9	-03.7	-04.4	-04.4	-03.3	-05.4	-	03.0	03.4	03.2	93	96	96	95	N	9	N	8	N	9
16	597.9	599.8	599.8	-05.2	-04.7	-04.7	-04.8	-04.2	-05.2	-	03.0	03.1	03.1	95	95	95	95	N	9	N	7	N	6
17	598.7	598.8	597.5	-05.8	-02.6	-01.8	-03.0	-01.8	-07.4	-	02.6	03.2	03.6	87	84	88	86	N	5	NE	1	N	5
18	596.5	595.9	595.1	02.7	05.0	04.4	04.1	05.9	-01.8	-	02.5	02.1	02.2	45	33	34	37	NNW	5	N	5	NNW	3
19	593.4	591.3	590.9	02.7	02.4	00.8	01.7	05.1	00.8	-	02.3	03.4	03.6	42	63	75	60	SW	1	SW	7	SSW	6
20	588.6	590.7	591.2	-01.4	-00.6	-01.4	-01.2	00.8	-02.2	-	04.1	04.4	04.1	99	100	100	100	S	12	S	8	S	7
21	591.0	592.6	594.2	-00.8	-00.6	-01.4	-01.1	-00.3	-01.4	-	04.3	04.4	04.1	100	100	99	100	S	8	SSW	12	SSW	13
22	595.4	598.7	599.3	-01.0	01.4	02.2	01.2	02.3	-01.4	-	04.2	04.8	03.0	99	94	56	83	SSW	13	SSW	8	SSW	8
23	600.2	600.9	600.0	03.8	05.4	04.4	04.5	06.0	01.0	-	02.7	02.4	02.2	45	35	36	39	SW	8	SSW	7	SSW	7
24	599.5	599.0	598.4	04.2	06.1	04.5	04.8	06.3	04.0	-	02.2	02.4	02.4	35	35	38	36	S	6	S	6	SSW	6
25	597.5	597.6	597.8	04.4	05.8	05.8	05.5	06.2	03.3	-	02.8	02.3	02.4	45	34	35	38	SSE	5	SSE	6	N	4
26	597.0	596.3	595.4	03.4	05.4	03.8	04.1	05.9	03.0	-	02.9	04.0	03.1	49	59	52	53	N	3	N	5	NE	5
27	592.9	591.9	590.2	04.0	05.4	03.0	03.9	05.6	02.6	-	02.3	02.8	03.3	38	41	58	46	SW	5	SW	6	SW	6
28	588.0	587.0	586.1	01.0	02.0	00.4	01.0	03.0	-00.1	-	04.8	05.1	04.7	97	97	100	98	SW	7	SW	8	SW	7
29	586.0	587.4	589.0	-00.4	00.8	00.8	00.5	01.4	-01.2	-	04.4	04.9	04.9	100	100	100	100	SW	8	SSW	9	SSW	6
30	588.0	587.7	583.8	00.1	01.8	01.8	01.4	02.2	-00.6	-	04.6	05.2	05.2	100	100	100	100	SSW	7	S	11	SSW	13
31	588.9	590.2	592.8	-00.8	-00.8	-01.8	-01.3	02.2	-01.8	-	04.3	04.3	03.9	100	99	98	99	SSW	9	SW	12	SW	7
MES.	VRED.	593.9	594.6	594.6	-01.2	00.0	-00.6	-00.6	01.1	-02.8	-	03.1	03.6	03.3	76	79	78	78	7.6	7.4	6.5		

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1	593.6	594.1	592.7	-02.0	-02.8	01.0	-00.7	01.0	-02.8	-	03.9	03.6	04.9	98	97	100	98	SM	2	SSW	3	SSW	7
2	589.5	589.0	589.2	01.4	02.4	02.0	02.0	02.8	01.0	-	05.1	05.4	05.3	100	100	100	100	SSW	8	SSW	6	SSW	6
3	587.4	587.5	587.4	02.2	02.6	02.8	02.6	03.1	01.9	-	05.4	05.5	05.6	100	100	100	100	SW	11	SW	6	SW	8
4	590.0	591.4	592.7	-00.4	02.8	01.6	01.4	03.6	-00.8	-	04.5	04.1	04.7	100	73	91	88	SW	3	SW	5	SW	4
5	591.8	591.0	590.0	00.8	02.1	01.0	01.2	02.5	00.8	-	04.9	05.3	04.9	100	100	100	100	SW	7	SW	8	SW	5
6	589.6	591.0	590.3	-07.8	-02.1	-01.3	-03.1	01.0	-08.2	-	02.4	03.8	03.6	93	98	87	93	N	5	SSW	3	SSW	7
7	589.2	589.1	588.3	-00.8	01.3	01.2	00.7	01.9	-02.5	-	02.4	05.0	04.3	56	100	80	80	SW	8	SSW	9	SSW	8
8	584.5	585.1	583.1	01.6	04.3	01.5	02.2	04.6	00.4	-	03.3	03.3	05.1	64	54	40	73	SW	14	SSW	11	SSW	12
9	577.5	577.7	579.4	00.2	-01.0	-05.4	-02.9	01.7	-05.4	-	04.7	04.3	02.9	100	100	95	98	SSN	12	SSN	12	SSN	11
10	579.4	580.8	583.6	-06.3	-05.0	-06.3	-06.0	-04.7	-06.8	-	02.7	03.0	02.7	94	95	94	94	SSW	13	SSW	10	-	0
11	584.5	585.6	585.4	-11.1	-09.3	-10.0	-10.1	-06.3	-12.0	-	01.8	02.1	01.9	90	91	91	91	N	8	N	8	N	8
12	584.7	584.7	584.8	-12.3	-10.1	-10.5	-10.9	-10.0	-12.4	-	01.6	01.9	01.9	89	91	90	90	N	10	N	10	N	10
13	584.8	586.9	586.9	-10.8	-08.1	-07.4	-08.4	-07.4	-10.9	-	01.8	02.3	02.4	90	92	93	92	N	12	N	9	N	6
14	585.0	586.0	585.5	-03.6	-03.4	-03.6	-03.7	-03.7	-03.4	-	03.4	03.5	03.3	97	97	96	97	N	9	N	6	SSE	6
15	580.8	579.6	579.4	-04.6	-08.1	-08.6	-07.6	-03.6	-09.0	-	03.1	02.3	02.1	96	92	92	93	N	5	N	10	N	10
16	579.5	585.0	585.9	-09.8	-08.8	-08.6	-09.0	-08.4	-10.0	-	02.0	02.2	02.2	91	92	92	92	N	14	N	10	N	10
17	588.8	591.4	591.8	-11.0	-08.0	-08.6	-09.1	-07.6	-11.0	-	01.8	02.2	02.2	90	88	92	90	N	12	N	5	N	6
18	592.4	593.9	592.6	-08.7	-04.1	-04.6	-05.0	-03.4	-09.9	-	02.2	02.7	02.7	92	73	77	81	N	6	-	0	SW	1
19	594.6	595.0	595.3	-03.7	-01.6	-01.4	-02.0	-00.9	-04.3	-	02.8	03.4	03.5	81	82	84	82	S	2	SW	4	N	2
20	595.4	59																					

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 $H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Vremenska časost 0-9	Oblačnost N (0-10)					Insoljajuća broj sunca	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	1	10	08	10	*	09.3	03.3	00.2	132	V 0-24, P 0-24, T 0-530 2010 24; = 0-830, 1740 24; = 830 1740, * 2010 2330, [X]
2	0	10	*	10		02	07.3	03.2	04.7	P 0-24, T 0-410 1330; = 0-24, T 0-410 1330, * 330 1330, = 1410, 1630, [X]
3	0	10	*	10		02	07.3	00.0	141	V 0-230, 530 1330, P 0-230, 2230 24; * 530 1330, T 0-230, 530 1330, = 530 1330, [X]
4	8	09	06	06		07.0	04.6	00.0	134	P 0-230, T 0-230, 1330, [X]
5	8	06	01	02		03.0	05.5	00.0	120	P 0-24, = 730 1140, 990 980 1105, = 1140 1000, # 1350 1340, [X]
6	8	05	01	00		02.0	05.7	00.4	114	P 0-24, [X]
7	8	05	05	00		03.3	08.2	00.0	106	P 0-1030, 1530 2240; = 2005 2255, [X]
8	9	04	08	05		05.7	10.1	00.0	95	[X]
9	9	02	06	02		03.3	08.8	00.0	88	P 02024, # 5-830 [X]
10	8	01	01	00		00.7	10.5	00.0	84	P 0-1630, # 5-830, [X]
11	7	00	02	10		04.0	08.7	00.0	75	# 160-0-1730, P 0-820 24, = 2010 24, V 2130 24, [X]
12	0	10	*	10	*	10	00.0	00.0	75	P 0-24, = 0-24, V 0-230, * 330 19, # 19-2230, = 2230 24, [X]
13	1	10	*	10	*	10	00.0	00.0	82	P 0-24, = 0-24, # 0-24, 1330, * 330 1330, T 0-24, T 0-24, [X]
14	0	10	*	10		01	07.0	01.4	100	P 0-24, = 0-1430, * 0-1430, T 0-1430, = 0-1430, V 240-24, [X]
15	0	06	10	10		08.7	00.0	00.0	95	V 0-24, P 0-24, # 45-530, = 830 24, [X]
16	8	10	02	00		04.0	06.3	00.0	92	P 0-24, = 0-930, P 0-15, # 1530 1330, [X]
17	9	01	00	00		00.3	11.0	00.0	90	P 0-830, 1930 24, # 5-11, [X]
18	9	01	04	00		01.7	10.4	00.0	86	P 0-1630, # 0-1630, 1115, [X]
19	9	04	02	10		05.3	10.2	00.0	84	# 0-1630, P 0-1630, = 20-24, [X]
20	8	10	*	10	*	10	00.0	00.0	84	= 0-24, P 0-24, * 0-24, 530, 1330, V 530 11, 1330 24, T 530 9, 1530 24, [X]
21	1	10	*	10	*	10	10.0	00.0	68	= 0-24, V 0-24, P 0-24, * 0-4430, T 0-4430, 0-24, [X]
22	8	09	09	04		07.3	02.0	03.7	94	= 0-450, V 0-1430, P 0-24, T 0-24, = 0-1030, [X]
23	9	01	02	00		01.0	10.6	00.0	90	P 0-24, # 0-24, 530, 930, [X]
24	9	00	02	00		00.7	10.7	00.0	82	P 0-24, # 0-24, 530, 930, [X]
25	9	08	08	05		07.0	00.7	00.0	77	P 0-23, [X]
26	8	00	06	00		02.0	06.4	00.0	68	# 16-08 530 12, 1730 2030, P 0-820 24, * 1430 1530, [X]
27	9	00	01	08		03.0	11.1	00.5	63	P 0-24, # 1430, [X]
28	0	06	10	10	*	09.3	02.2	00.0	59	P 0-24, = 1230 1410, 1930 24, # 1230 1230, 2030 2230, * 2230 24, [X]
29	0	10	*	10	*	10	00.0	00.0	57	P 0-24, = 0-24, * 0-24, 1330, V 1330 24, # 1330 1330, [X]
30	0	10	*	10	*	10	00.0	00.0	66	= 0-1430, 2010 24, * 0-530, = 0-24, # 102330, # 2130 2230, [X]
31	0	10	*	10	*	10	00.0	00.0	61	= 0-24, P 0-24, V 530 24, [X]
PES. RED.		06.1	06.3	05.1	05.8	157.6	80.2			

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1	8	10	08	10	*	09.3	00.0	00.0	60	= 0-1330, 2030 24, V 0-1630, # 10, 1430 1730, P 0-1730 24, # 1730 24, [X]
2	0	10	*	10	*	10	00.0	00.0	57	P 0-24, = 0-24, # 0-1430, 530 1330, # 1530, 1930 24, [X]
3	0	10	*	10	*	10	00.0	00.0	51	P 0-24, = 0-24, 1330, P 0-24, T 0-24, # 530, 830, [X]
4	8	10	08	02		06.7	05.3	00.3	47	# 0-1030, P 0-230, 1330, [X]
5	8	10	*	10	*	06.7	01.3	00.0	41	P 0-230, # 0-230, 1330, # 2130 2330, * 2330 24, [X]
6	8	10	00	01		03.7	09.7	05.6	44	# 0-1430, * 0-4030, P 0-2230, 1530 24, T 0-2230, = 0230 530, V 1330 110, = 1730 1030, # 1030 1730, [X]
7	0	06	10	04		06.7	02.0	00.0	43	P 0-24, # 0-24, 530, 930, [X]
8	0	06	08	10	*	08.0	05.8	00.0	41	P 0-24, = 1830 1910, # 1930 2330, Uzeti vetro oko 220 km/has 3-5, [X]
9	0	10	*	10	*	10	00.0	00.6	42	P 0-24, # 0-24, # 3-100, # 1830 1910, # 1930 24, [X]
10	1	10	*	10	*	10	00.0	00.5	45	P 0-2030, # 0-24, * 0-24, # 7-11, 1930 2030, T 0-24, T 0-2030, V 10-12, # 12-24, [X]
11	1	10	*	10	*	10	10.0	00.0	51	P 0-24, V 0-24, * 0-24, 3-24, T 0-24, 5-24, [X]
12	2	10	*	10	*	10	10.0	02.2	51	P 0-24, V 0-24, = 0-24, T 0-24, * 0-1030, [X]
13	1	10	*	10	*	10	10.0	00.0	51	P 0-24, = 0-24, 1330, V 1330 24, [X]
14	1	10	*	10	*	10	10.0	00.6	52	P 0-1530, 2024 24, = 0-24, V 0-24, T 0-24, = 2-1130 2030, * 4-530, 1430 24, # 1430 1830, [X]
15	0	10	*	10	*	10	10.0	00.0	75	P 0-24, = 0-24, # 0-23, V 0-24, T 0-24, 0-24, [X]
16	3	10	*	10	*	10	10.0	00.0	100	P 0-24, = 0-24, V 0-24, T 0-24, * 0-24, 1330 1430, # 1430 1630, [X]
17	8	10	02	00		04.0	00.0	00.0	108	P 0-24, # 0-24, 1030, P 0-24, * 0-6, T 0-6, T 0-1230, [X]
18	9	00	02	01		01.0	11.2	00.0	107	V 0-1030, P 0-1130, # 530, 9, [X]
19	9	06	06	06		06.0	10.4	00.0	98	# 1430 1530, [X]
20	1	10	*	10	*	10	00.0	00.0	90	= 2130 24, * 2130 2330, P 0-24, V 0-24, T 0-24, 20-24, [X]
21	8	04	01	00		01.7	11.8	02.9	92	V 0-24, P 0-24, = 0-530, T 0-530, = 0-530, # 0-530, [X]
22	8	00	02	02		01.3	12.4	00.0	84	V 0-630, P 0-24, = 0-24, 1330 24, [X]
23	9	05	04	06		05.0	09.3	00.0	77	P 0-830, 1330 24, [X]
24	8	08	05	01		04.7	10.3	00.0	68	P 0-24, # 0-24, 1330, [X]
25	0	10	*	10	*	10	10.0	00.0	62	P 0-24, = 1430 1530, 2030 2330, * 3-530, V 530 24, * 530 745, T 0-530, 830, [X]
26	8	10	05	00		06.3	02.9	00.3	62	P 0-24, V 0-1430, = 630 830, V 410 1730, [X]
27	9	00	01	02		01.0	13.7	00.0	59	P 0-830, [X]
28	8	05	06	04		06.3	05.6	00.0	52	P 0-24, # 0-24, [X]
29	8	08	04	04		05.3	09.2	00.0	47	P 0-24, # 0-24, [X]
30	8	02	08	04		04.7	10.7	00.0	38	P 0-24, [X]
PES. RED.		07.8	07.0	06.2	07.6	135.0	120.5			

$\varphi = 43^{\circ} 43' N$   $\lambda = 18^{\circ} 16' E$  Gr.  $\Delta G = + 1h 13 min.$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C						Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetroa D, f (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	595.3	596.6	596.2	06.8	11.0	07.0	08.0	11.4	05.2	-	04.0	04.8	04.1	55	49	55	53	SSW	7	5	6	SSW 6
2	597.5	598.9	598.7	07.0	11.0	07.0	08.0	11.2	05.0	-	03.9	04.1	03.5	52	42	46	47	SW	3	SSW	4	S 4
3	598.2	598.2	597.5	09.4	12.4	09.6	10.3	12.5	06.4	-	03.1	05.0	04.2	35	46	47	43	SSW	2	-	0	- 0
4	596.2	596.5	595.5	10.2	12.6	09.2	10.3	13.5	07.8	-	03.8	04.2	05.0	41	38	57	45	S	8	S	5	SW 5
5	594.6	595.2	595.3	07.4	06.8	03.8	05.5	09.2	03.8	-	03.5	06.0	05.9	45	81	97	74	SSW	7	SSW	12	SSW 9
6	596.0	595.7	595.6	03.0	03.7	02.1	02.7	04.1	02.1	-	05.7	05.8	05.1	100	97	96	98	SW	3	SW	5	W 3
7	594.2	593.5	592.7	01.4	04.5	01.9	02.4	05.7	00.1	-	03.8	03.2	03.6	74	51	69	65	-	0	SW	3	SW 2
8	590.3	589.2	589.0	01.2	00.9	-00.6	00.2	03.9	-00.8	-	04.5	04.7	04.4	90	97	100	96	SSW	2	S	6	S 5
9	589.7	590.7	591.4	-01.0	01.4	-01.7	-00.8	01.7	-02.2	-	04.3	04.8	04.0	100	94	100	98	SW	4	S	6	ENE 2
10	590.8	591.9	592.0	-02.8	-01.6	-01.6	-01.9	-01.1	-02.8	-	03.6	04.0	04.0	97	98	98	98	N	6	N	7	N 10
11	592.5	594.2	594.4	-01.4	-00.1	00.0	-00.4	00.2	-02.0	-	04.1	04.6	04.4	95	100	55	98	N	6	N	6	N 5
12	593.7	593.8	592.7	00.8	04.2	03.6	03.1	05.7	-01.1	-	03.6	02.9	03.9	73	46	66	62	N	6	ENE	4	NW 3
13	591.7	591.7	591.3	03.8	06.8	04.0	04.7	07.1	02.8	-	03.1	03.3	03.5	52	45	57	51	SW	6	SSW	7	SSW 9
14	587.0	588.2	588.4	01.8	02.9	02.2	02.3	04.0	01.7	-	04.5	05.6	05.4	36	100	100	95	S	12	S	10	S 8
15	587.4	588.4	588.7	00.4	04.1	02.3	02.3	04.3	00.1	-	04.7	04.6	05.3	100	74	97	90	S	7	SSW	7	SSW 3
16	589.3	589.8	591.1	01.9	05.5	02.3	03.0	05.8	00.8	-	05.0	05.2	04.1	96	77	76	83	-	0	SSW	7	SW 7
17	593.3	596.4	598.3	02.1	05.0	05.3	04.4	05.9	C1.5	-	05.3	06.5	06.2	100	100	92	97	SSW	7	SSW	6	SSW 3
18	594.4	599.5	599.3	06.4	10.5	10.1	09.3	11.0	05.2	-	05.7	06.4	06.1	78	67	66	70	S	6	SSE	4	SSW 7
19	599.1	599.4	597.9	10.8	13.4	10.8	11.5	14.0	08.8	-	04.1	04.4	06.0	43	38	62	48	SSW	10	SSW	7	SSW 8
20	595.9	598.0	596.9	08.4	12.8	08.8	09.7	13.0	08.4	-	06.6	06.6	07.4	80	60	88	76	SSW	13	S	5	SSW 10
21	597.4	598.0	597.2	08.3	12.3	08.6	09.2	13.3	07.4	-	07.5	06.7	06.5	91	63	81	78	SSW	9	SSW	7	SSW 6
22	597.3	597.4	597.6	08.3	12.6	07.3	08.9	12.7	06.4	-	07.1	06.8	06.3	86	62	82	77	SSW	4	SW	4	- 0
23	597.3	598.2	597.8	07.1	08.0	07.5	07.5	10.3	05.2	-	03.9	08.0	07.5	51	99	96	82	W	3	NNW	1	SSW 5
24	597.0	597.7	596.8	02.9	03.8	01.8	02.6	07.5	01.8	-	05.6	06.0	05.2	100	100	100	100	N	4	NNE	4	N 4
25	595.3	596.0	595.8	03.8	08.2	06.7	06.4	08.2	00.0	-	01.8	02.1	04.1	31	26	55	37	N	3	NNW	4	NNW 5
MES.	VRED.	593.9	594.8	594.6	03.9	06.4	04.2	04.7	07.4	02.2	-	04.5	05.0	05.1	75	72	63	76	5.5	5.2	4.6	

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1	594.4	595.5	595.4	02.6	04.0	-01.2	01.1	04.2	-01.2	-	05.5	06.1	04.2	100	100	95	100	ESE	3	N	2	N 4
2	594.7	594.2	593.7	-03.4	00.0	-00.2	-01.0	00.2	-04.0	-	03.5	04.6	04.5	97	100	100	99	N	5	NE	4	E 2
3	591.8	592.2	591.0	-01.0	00.2	-00.8	-00.6	00.6	-02.0	-	04.2	04.7	04.3	99	100	59	99	N	6	N	4	N 6
4	589.3	590.0	590.0	-03.4	00.8	-01.0	-01.2	01.6	-04.0	-	03.5	03.6	04.2	97	74	97	85	N	8	N	6	N 9
5	590.6	591.6	591.7	00.0	03.0	03.6	02.3	03.7	-02.4	-	04.3	04.5	05.1	94	80	90	88	N	7	NNE	3	SW 3
6	591.0	592.5	593.2	04.9	07.2	03.6	04.9	07.3	02.2	-	05.2	05.5	04.4	80	72	73	75	WSW	3	SW	6	SSW 6
7	593.3	595.4	595.5	03.6	07.1	05.0	05.2	07.4	02.7	-	05.9	06.6	06.6	100	87	70	86	SSW	8	SSW	6	SSW 7
8	597.2	598.6	599.2	06.6	09.9	08.2	08.2	11.0	03.5	-	04.8	05.7	06.5	66	63	80	70	-	0	C	-	0
9	599.3	599.7	598.9	09.5	13.0	11.0	11.1	14.0	06.8	-	06.2	04.9	05.3	70	44	54	56	W	1	NNW	1	- 0
10	597.4	597.3	597.0	11.6	13.5	11.9	12.2	14.4	08.8	-	04.3	05.8	06.4	42	50	61	51	-	0	W	1	- 0
11	596.3	596.9	597.0	11.6	15.8	12.6	12.5	16.0	11.1	-	05.5	07.1	08.7	53	53	82	63	NNW	3	W	2	NNW 2
12	596.7	596.8	597.0	11.6	15.6	10.7	12.2	15.6	10.1	-	09.4	07.7	09.2	92	58	96	82	N	3	-	0	N 2
13	597.1	597.2	596.7	11.0	13.3	12.6	12.3	13.9	05.9	-	07.9	07.8	08.9	80	68	82	77	N	3	-	0	W 4
14	595.9	595.4	592.8	14.7	14.2	09.2	11.8	15.0	05.2	-	04.5	07.1	05.9	36	58	68	54	SW	5	SW	6	SW 8
15	593.0	593.6	593.1	09.1	12.9	08.6	09.8	13.3	06.6	-	07.0	07.1	06.3	80	64	75	73	SW	6	SSW	6	SSW 5
16	591.4	591.0	591.2	05.7	09.8	05.7	06.7	10.0	05.2	-	06.9	09.1	06.5	100	100	100	100	NE	3	S	3	N 5
17	591.8	593.3	594.7	05.0	27.2	07.6	06.6	07.8	04.7	-	06.5	07.6	07.8	100	100	100	100	N	6	N	5	N 5
18	595.8	597.0	596.5	09.0	12.2	10.6	10.7	13.6	06.8	-	08.1	09.1	08.5	94	91	87	91	E	2	E	2	SSW 5
19	596.0	596.3	595.9	10.8	13.7	10.2	11.2	14.0	08.4	-	06.5	07.6	08.0	67	64	86	72	SW	6	SW	7	SW 6
20	595.3	595.3	596.1	09.0	13.1	05.6	10.0	13.6	08.4	-	06.8	07.6	07.1	79	67	82	76	SW	3	SW	6	N 3
21	596.6	596.8	595.3	05.6	13.8	08.6	10.2	13.9	07.8	-	06.5	06.5	06.4	72	55	77	68	W	3	WSW	3	SW 7
22	594.4	593.7	593.4	09.6	11.3	07.3	08.9	12.9	07.0	-	07.0	08.0	06.8	78	80	88	82	-	0	SSW	6	SW 5
23	593.7	595.1	595.8	05.2	06.4	05.4	05.6	07.7	04.1	-	06.6	07.2	06.4	100	95	98	-	NNW	2	NW	1	
24	596.0	596.4	596.6	06.1	08.6	05.2	06.3	09.8	05.0	-	07.1	06.8	06.7	100	81	100	94	SW	4	S	2	WSW 5
25	597.4	597.0	596.3	06.0	09.8	06.0	07.0	10.0	04.1	-	06.2	07.9	07.0	89	87	100	92	N	2	S	2	SW 6
26	595.2	593.7	592.8	06.6	08.0	04.6	06.0	09.4	04.6	-	05.9	06.1	06.4	81	75	100	85	SW	3	SW	6	SW 5
27	592.1	592.5	592.6	05.2	05.8	04.0	04.6	06.8	04													

BB, ST, 138

$$H_s = 2067 \text{ m} \quad H_b = 2070,4 \text{ m} \quad h_t = 3,0 \text{ m} \quad h_r = 1,5 \text{ m}$$

B.IEL ASÉNICA

1877 Jun

1	6	10≡	10≡•	10≡•	10.0	00.0	01.6	.	≡ 0-24, #402 580, 1232 1510, 9 1012 1230, 1632 1710, □ 1512 1630, ▲ 1912 2230
2	3	10≡	10≡	10≡*	10.0	00.0	02.2	.	≡ 0-24, Y-900, □ 1502 1520, □ 1532 1610, □ 1612 1620, ▲ 2112 24, [■]
3	0	10≡	10≡	10≡	10.0	00.0	07.4	01	≡ 0-24, X-026, □ 020 900, □ 1452 24, □ 220 1020, □ 1252 44, [■]
4	e	10≡	080	04	57.3	39.5	.	.	≡ 0-86, □ 024 V-920, □ 220 1020, □ 1252 44, [■]
5	7	000	090	10	36.3	69.7	.	.	≡ 0-1130, #1102 4440
6	6	120	060	06	45.3	69.1	.	.	#14-10 2308, □ 9-24
7	7	110	100	01	07.0	92.6	.	.	≡ 0-24, #520 1230, # 1232 17, □ 1520 1345
8	8	000	090	00	03.0	45.2	00.0	.	□ 0-200 #14-10 0211, □ 220 636, 2112 24
9	8	210	060	00	02.3	15.5	.	.	□ 0-720 2332 24, # 2300
10	9	000	060	02	02.7	21.4	.	.	□ 0-5, # 2300 6
11	9	310	020	01	01.3	13.4	.	.	≤ 2112 2230, □ 2040 24
12	8	010	09	00	03.3	58.8	.	.	△ 0-500 #380 2020, □ 1615 1630, □ 1630 1645, ≡ 1640 1720, ≤ 2030 23
13	8	010	09	00	03.3	57.6	01.7	.	#14-2-1700 8-12
14	8	010	05	00	03.3	55.4	.	.	# 2306, □ 702 24, □ 2245 24
15	e	020	060	00	00.7	15.1	.	.	□ 0-245, □ 0-235, ≡ 245 430
16	1	10≡	10≡•	10≡•	10.0	01.1	.	.	≡ 020 04, □ 1415 1720, □ 1410 1710, 2020 24, ≤ 1415 1710, □ 1525 1610, □ 2015 24
17	1	10≡	10≡	10≡	10.0	01.0	25.5	.	≡ 0-24, □ 0-24, □ 0-205, 635, 1635
18	7	000	09	04	24.3	77.6	00.0	.	≡ 0-3, 820 1930, □ 0-500 1922 24, # 10-20 3-800, □ 30 445
19	8	000	050	01	72.0	11.3	.	.	≡ 0-24, □ 0-24, □ 0-24, □ 0-24
20	8	060	050	01	64.0	11.1	32.4	.	≡ 0-50, #105 1810, □ 0-515, 2112 24; □ 515 610, ≡ 1030 1910
21	8	000	09	06	35.0	46.1	.	.	△ 0-720, #1014 4530, □ 1445 1315, □ 1535 1515, ≤ 2235 24
22	8	060	060	03	57.0	16.6	04.5	.	≤ 0-315, □ 102 230 232 205, □ 1212 1245, □ 1212 24, ≡ 1812 1930
23	1	10≡•	10≡	10≡	69.7	31.6	04.8	.	≡ 0-310, #102 15 1912 2030, ≡ 1017 1700, □ 502 745, 1520 1615
24	3	08	10≡R	10≡	69.3	22.6	01.8	.	≡ 045 25, 1320 2120, # 225-5 2024, ≡ 820 1035, □ 1812 1415, □ 2012 24
25	3	060	10≡R	10≡	58.7	12.2	.	.	≡ 0-20, 1720 24, □ 0-11, □ 0-27 750, ≡ 750 205, 1212 1940, □ 930 1105, 1512 1620, □ 910 1105, □ 1415 1105, □ 1310 1610, ≡ 1310 13
26	9	310	06	04	34.3	35.7	68.0	.	≡ 0-400 □ 0-530 1110 2100, # 1412 2100, □ 1122 1140, □ 2020 224
27	0	10≡	10≡•	10≡•	10.0	02.0	01.6	.	□ 0-005, # 015 24, □ 820 900, □ 910 1100, □ 1520 205, ≡ 920 1220, □ 1320 1620, □ 2020 2200, □ 1710 24
28	8	10≡•	050	06	05.0	45.0	24.6	.	≡ 0-100, □ 0-1430, □ 0-1200, □ 002 430, □ 1912 24
29	8	000	060	06	34.0	69.5	00.2	.	□ 0-70, □ 1912 24
30	0	060	10≡	10≡R	68.7	44.0	.	.	□ 0-103, 1720 1935, □ 750 945, □ 1415 1410, □ 2015 2220, ≡ 320 1610, □ 1015 2215, □ 1210 2205

PES. 04.7 48.1 05.1 26.0 192.9 81.7  
RED.

$\varphi = 43^{\circ} 43' N \lambda = 18^{\circ} 16' E$  Gr.  $\Delta G = +1h\ 13\ min.$ 

BR. ST. 138

Dan	Vozdušni pritisak P mm			Temperatura vazduha T °C						Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	596.5	597.4	596.8	04.6	05.1	04.4	04.6	08.0	03.8	-	06.4	06.6	06.3	100	100	100	100	N	5	N	6	N	10
2	598.0	599.1	599.0	04.6	07.0	06.6	06.2	07.2	03.6	-	06.4	07.5	07.3	100	100	100	100	N	10	N	7	N	6
3	599.0	599.8	598.6	07.2	10.6	10.6	09.8	11.6	05.2	-	07.6	07.8	07.0	100	81	73	85	N	5	N	3	N	6
4	597.2	596.7	595.8	12.2	14.6	12.2	12.8	15.6	09.8	-	07.3	07.4	09.4	69	59	88	72	-	0	W	3	-	0
5	593.9	593.6	593.0	11.4	14.0	08.4	10.6	15.0	06.5	-	06.5	06.8	07.3	65	56	89	70	SW	5	S	5	WSW	5
6	592.1	593.5	594.5	06.8	08.1	06.3	06.9	08.8	05.7	-	07.4	08.1	07.2	100	100	100	100	N	5	N	2	-	0
7	595.0	596.4	596.1	08.9	14.2	10.2	10.9	14.4	05.8	-	03.1	06.1	06.4	36	50	68	51	N	6	SW	3	SM	6
8	596.0	595.7	594.9	09.9	15.0	11.6	12.0	15.6	05.0	-	06.5	07.4	06.5	71	58	63	64	SW	7	SSW	7	SSW	7
9	593.1	595.2	596.4	11.9	14.3	10.3	11.7	14.6	09.9	-	07.1	08.6	08.5	68	70	90	76	SSW	10	SSW	8	SM	4
10	596.2	596.4	595.8	10.6	14.2	06.8	09.6	14.3	05.8	-	08.0	07.9	07.4	83	65	100	83	WSW	6	SSW	6	N	7
11	595.1	595.1	594.2	06.0	06.2	05.0	05.6	07.3	04.9	-	07.0	07.1	06.5	100	100	100	100	N	5	NN	7	N	8
12	594.5	596.1	596.7	06.2	07.4	07.1	07.0	07.8	04.9	-	07.1	07.7	07.6	100	100	100	100	N	9	N	7	NNW	6
13	597.0	598.6	598.1	06.8	11.4	11.4	10.3	12.6	04.8	-	05.4	05.0	04.9	73	50	48	57	N	6	N	4	W	2
14	597.2	597.4	595.8	10.6	14.4	11.8	12.2	15.3	08.9	-	06.0	06.6	07.1	62	53	69	61	W	4	SM	5	SM	9
15	594.6	595.2	596.8	11.1	13.7	10.8	11.6	14.4	09.3	-	06.8	08.8	07.7	69	75	79	74	SSW	9	SW	6	SM	5
16	598.4	599.8	598.8	04.6	13.7	11.3	10.2	14.6	03.0	-	06.4	09.1	07.9	100	77	79	85	NW	2	SSW	3	SW	6
17	596.8	596.7	596.6	11.8	13.0	07.2	09.8	13.4	07.2	-	06.3	08.8	07.5	61	79	99	80	SW	3	WSW	5	N	4
18	596.8	597.0	596.0	10.7	13.6	10.3	11.2	14.9	07.1	-	09.0	07.4	07.2	94	63	76	78	SE	4	SM	3	SM	6
19	595.1	596.0	596.7	08.6	13.2	10.6	10.8	13.6	07.1	-	06.4	06.6	07.0	77	58	73	69	N	4	SW	4	-	0
20	596.8	597.0	596.8	10.3	14.9	12.0	12.3	15.1	08.3	-	07.3	08.2	04.9	78	64	46	63	-	0	-	0	SW	3
21	595.5	596.5	596.6	11.8	16.3	11.6	12.8	16.6	09.3	-	04.8	07.7	07.9	47	56	77	60	SW	6	SW	7	SW	4
22	596.0	595.0	594.8	09.4	14.0	06.0	08.9	14.3	04.1	-	08.8	11.5	07.0	100	96	100	99	SSW	3	SSE	2	SE	3
23	593.7	594.3	595.0	04.2	02.8	03.1	03.3	06.2	02.5	-	06.2	05.6	05.7	100	100	100	100	N	7	N	11	N	9
24	596.2	596.8	595.9	04.3	09.2	09.6	08.2	10.4	03.0	-	06.2	08.0	06.7	100	92	75	89	N	6	SE	2	SW	2
25	593.8	592.3	590.8	10.8	13.6	09.0	10.6	13.7	08.9	-	06.0	07.4	06.7	62	63	78	68	W	4	SSW	7	SW	11
31	593.1	592.8	590.2	13.2	12.2	10.0	11.4	15.3	10.0	-	04.6	08.8	08.8	40	82	96	73	SSW	10	SSW	8	SSW	12
MES.	VRED.	595.5	596.1	595.8	09.1	11.9	09.3	09.5	12.9	06.8	-	06.6	07.8	07.1	78	75	82	78	5.4	4.6	5.1		

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1	588.8	591.1	591.8	07.0	07.6	03.6	05.5	10.0	03.6	-	07.5	07.1	05.9	100	91	100	97	SW	6	N	3	N	6	
2	591.7	592.9	593.4	03.2	05.4	04.0	04.2	06.4	01.6	-	05.8	06.7	06.1	100	100	100	100	N	5	N	4	N	2	
3	594.1	595.7	596.8	06.0	10.4	08.8	08.5	11.1	04.0	-	05.3	05.8	06.8	76	62	80	73	-	0	-	0	SM	2	
4	598.3	599.9	600.1	08.8	10.6	10.0	09.9	11.8	06.4	-	05.2	06.3	05.6	61	65	61	62	-	0	NE	2	SW	2	
5	599.6	599.2	598.5	10.6	13.8	12.0	12.1	15.4	09.6	-	06.0	05.6	07.1	62	48	68	59	SW	4	S	4	S	3	
6	596.7	596.7	596.4	08.3	08.9	08.1	08.4	12.0	07.6	-	08.2	08.6	08.1	100	100	100	100	NE	4	NE	4	N	6	
7	595.8	596.5	596.0	07.8	10.7	10.0	09.6	11.5	07.2	-	07.9	07.9	09.2	100	82	100	94	N	5	NNE	4	E	3	
8	596.0	596.8	597.5	11.7	12.0	10.4	11.1	13.5	09.3	-	06.7	08.2	07.4	65	78	78	74	-	0	-	0	N	1	
9	598.2	598.7	599.0	11.2	12.8	10.9	11.5	13.4	09.5	-	06.2	06.4	06.5	62	58	67	62	NE	3	S	2	-	0	
10	598.3	598.0	598.4	12.1	13.6	11.3	12.1	14.9	10.0	-	07.1	07.7	08.0	67	66	80	71	SW	3	SW	5	SW	3	
11	597.0	596.8	596.5	11.2	14.0	08.7	10.7	14.7	08.7	-	06.0	07.3	07.8	60	61	92	71	-	0	SE	2	NE	2	
12	595.9	596.5	596.8	11.0	14.0	10.6	11.6	14.7	08.2	-	08.0	08.0	08.2	82	67	85	78	SW	2	S	4	S	4	
13	596.1	596.0	596.8	09.8	08.9	08.4	08.9	12.3	08.4	-	08.7	08.6	08.3	96	100	100	99	SW	6	SW	10	SW	6	
14	596.9	596.2	597.0	10.2	10.8	08.4	07.0	08.2	13.1	07.0	-	05.2	07.9	04.6	56	95	61	71	SW	3	SM	5	N	4
15	596.8	598.1	598.4	05.4	07.9	06.6	06.7	09.0	05.3	-	06.7	06.1	07.4	100	76	100	92	NW	4	N	4	N	3	
16	598.5	599.4	599.2	06.0	10.1	05.1	08.6	10.5	04.4	-	06.0	04.5	05.8	85	45	67	67	N	4	NE	3	N	3	
17	598.5	599.1	598.9	10.6	15.0	12.0	12.4	15.2	06.4	-	06.3	05.6	07.4	65	44	70	60	N	3	W	2	SW	2	
18	598.0	598.9	597.9	12.4	15.4	12.2	13.1	15.5	11.4	-	05.4	07.1	06.7	50	54	63	56	SW	7	SSW	7	SSW	6	
19	593.0	592.2	593.0	10.6	10.2	08.6	09.5	12.2	07.8	-	09.6	09.3	08.4	100	100	100	100	SSW	11	SSW	12	SSM	6	
20	593.4	594.1	593.3	07.0	10.8	08.0	08.5	11.2	06.2	-	07.3	07.5	08.0	98	77	100	92	SW	4	SW	6	SW	7	
21	591.2	587.5	587.0	08.4	09.2	09.0	08.9	09.8	06.8	-	08.3	08.7	08.6	100	100	100	100	SW	9	SW	15	SW	10	
22	587.0	586.3	577.6	08.4	09.8	06.8	08.0	10.4	06.0	-	08.3	06.8	07.4	100	75	100	92	SW	12	SW	13	SW	9	
23	589.3	590.5	590.5	06.6	06.6	07.2	06.9	08.4	05.7	-	07.3	06.8	07.6	100	93	100	98	SW	9	SW	6	SW	8	
24	590.9	591.4	592.3	03.8	01.7	01.9	02.3	07.2	01.3	-	06.0	05.2	05.3	100	100									

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$$H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_r = 1,5 \text{ m}$$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Imajući broj sena	Padavine R mm	Šnežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	0	02	10	10	07.3	01.5	22.0	.	212.24, 232.410, 235.24, 1212.24	
2	0	10	10	10	10	02.2	01.8	.	0-24, 0-10-16, 0-24	
3	8	06	06	01	04.3	11.7	00.4	.	0-630, 202.24, 0-410, 0211145, 2032.24	
4	8	01	05	05	03.7	12.9	.	0-240, 0-240, 2032.24		
5	8	02	09	06	05.7	08.4	.	0-330, 202.24, 0-1520, 1619051945, 1920.1920, 19151930, 1932.1935		
6	0	10	10	00	06.7	02.9	22.5	.	0-029, 332.1920, 212.24	
7	8	00	05	01	02.0	14.0	00.4	.	0-020, 002024, 0-520, 15.24	
8	8	08	09	00	05.7	09.7	.	0-350, 0-240, 2-530		
9	8	00	04	03	01.3	11.4	.	0-140, 0-140, 1930, 2032.24		
10	8	08	08	10	06.7	08.8	.	0-24, 0-170, 2-1030, 1703.24, 17175.1910, 1729.19, 1818-1810, 1815-1820		
11	0	10	10	10	10.0	01.0	16.4	.	0-30, 0-24, 15125, 1502.24	
12	3	10	10	10	10.0	01.9	00.4	.	0-24, 0-24, 0-520, 1930	
13	9	00	01	06	00.3	15.2	00.0	.	0-140, 0-140, 1930, 1935.24	
14	8	00	04	01	01.7	13.5	.	1935.24		
15	8	09	05	08	07.3	06.0	.	0-2110, 71512, 023204, 1415.1415, 1415.1510, 1720.2015, 2015.14		
16	8	10	04	00	04.7	10.8	02.2	.	0-1030, 0-025, 0-025, 14145, 2015.24	
17	8	09	06	00	05.0	02.5	.	0-180, 0-055, 0-055, 1416.16, 1416.16, 1416.16, 1416.16		
18	8	00	05	00	01.7	10.4	14.8	.	0-055, 0-055, 0-055, 1515, 1715.24	
19	8	01	06	04	03.7	12.1	.	0-530, 1515.24		
20	7	00	04	00	01.3	07.2	.	0-350, 0-520, 1510		
21	8	01	06	02	03.0	12.3	.	1901730, 10152305, 10152305, 10152305, 1323.24, 2352.24, 1215.24, 2355.24		
22	1	10	10	10	10	02.5	01.2	.	0-05, 1320.105, 0-05, 1320.105, 0-05, 1320.105, 0-05, 1320.105, 0-05, 1320.105	
23	0	10	10	10	10.0	00.0	26.0	.	0-24, 0-24, 0-24, 0-24	
24	8	10	05	01	05.3	11.7	04.1	.	0-170, 0-170, 0-170, 0-170, 0-170, 0-170	
25	9	01	02	01	01.3	13.8	.	0-340, 1515.24, 101202.00		
26	3	10	09	10	05.7	04.6	.	0-170, 502.170, 1320.24, 1815.1810, 2015.24		
27	8	10	08	02	06.7	06.1	06.0	.	0-1030, 0-05, 0-310, 14145, 10102.24	
28	8	00	06	01	02.3	11.5	.	0-180, 0-180, 1130, 1915.24		
29	8	00	08	00	02.7	08.8	.	0-730, 202.24, 910.1130		
30	9	01	02	01	01.3	12.8	.	0-770, 202.24, 10102.00, 1910.24		
31	8	05	08	05	06.0	08.2	.	0-24, 0-1130		

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1	7	16≡	05	10≡	09.7	00.3	00.8	.	
2	8	00○	09○	05	04.7	07.9	04.7	.	$\overline{\text{P}} \overline{\text{P}} -0.130, 18^{\circ} 25' \equiv 0.02 950, 11^{\circ} 12' 24' \cdot 0^{\circ} 2^{\circ} 35, 10^{\circ} 12' 20' ; 9^{\circ} 16' 20' 10'$
3	8	00○	06	02	02.7	11.1	.	.	$\equiv 0-510, 10^{\circ} 24' 40', 16^{\circ} 13' 150'; \overline{\text{P}} 4^{\circ} 12' 20', \# 1^{\circ} 5^{\circ} 2^{\circ} 9^{\circ} 20'$
4	8	00○	02	00	02.7	05.2	.	.	$\overline{\text{D}} 0^{\circ} 730, 20' 24', \# 1^{\circ} 5^{\circ} 2^{\circ} 9^{\circ} 20'$
5	8	08	06○	08	07.3	06.7	.	.	$\overline{\text{D}} 0^{\circ} 780, 24' 24', \# 1^{\circ} 5^{\circ} 2^{\circ} 9^{\circ} 20'$
6	0	10≡	10	10≡	10.0	00.0	.	.	$\equiv 0-24, \bullet 762 1120, \overline{\text{P}} 15-24$
7	7	00○	09○	10≡	09.7	06.5	18.4	.	$\overline{\text{P}} 0-110, \equiv 0-10^{\circ} 24, 16^{\circ} 24' 24', \# 1^{\circ} 4^{\circ} 10^{\circ} 25, 16^{\circ} 25'$
8	8	01○	06	02	03.0	05.5	.	.	$\equiv 0-190, \# 1^{\circ} 4^{\circ} 14' 24' 90, 13^{\circ} 11' 20', 17^{\circ} 20'$
9	8	00○	06	04	03.3	08.5	.	.	$\# 10^{\circ} 32' 830, \# 12^{\circ} 25' 165, 13^{\circ} 30'; 13^{\circ} 17' 19^{\circ} 30'$
10	8	01○	08○	02	03.7	07.5	01.5	.	$\# 10^{\circ} 32' 830, \# 12^{\circ} 25' 165, 13^{\circ} 30'; 13^{\circ} 17' 19^{\circ} 30'$
11	8	01○	08○	06	05.0	08.4	00.0	.	$\# 1^{\circ} 45-25, \# 20-1150, 13^{\circ} 17' 12' 25', \# 1^{\circ} 45-20' 10'$
12	2	01○	05≡	00	02.0	05.1	.	.	$\# 1^{\circ} 45-25, 760, \# 1^{\circ} 45-20', \# 1^{\circ} 45-24$
13	7	08○	10○	10≡	09.3	03.2	.	.	$\overline{\text{D}} 0-320, \# 1^{\circ} 45-25, 165, \# 1^{\circ} 45-24, \# 1^{\circ} 45-20, 13^{\circ} 20', 18^{\circ} 20', 23^{\circ} 15', 11^{\circ} 30', 13^{\circ} 5, \# 13^{\circ} 14' 40'$
14	8	05	10	00	05.0	04.4	00.9	.	$\# 1-550, 12^{\circ} 20', 19^{\circ} 20', \# 1^{\circ} 45-25, 165, \# 1^{\circ} 45-20, 13^{\circ} 20', 18^{\circ} 20', 23^{\circ} 15', 11^{\circ} 30', 13^{\circ} 5, \# 13^{\circ} 14' 40'$
15	8	10≡	05○	10≡	06.3	06.7	05.0	.	$\# 1^{\circ} 45-25, 580, 11^{\circ} 20', 20^{\circ} 25' 24'$
16	8	01○	02○	00	01.0	13.2	.	.	$\equiv 0-450, \# 1^{\circ} 45-20', \# 1^{\circ} 45-24$
17	9	00○	02○	00	00.7	12.2	.	.	$\overline{\text{D}} 0-620, 19^{\circ} 24', \# 1^{\circ} 45-20', 90$
18	8	04○	08○	04	05.3	06.7	.	.	$\# 0-520, \# 1^{\circ} 45-24$
19	0	10○●	10	10≡	10.0	01.2	01.8	.	$\overline{\text{P}} 0-24, \# 520, 12^{\circ} 20', 17^{\circ} 20', 01^{\circ} 20', 13^{\circ} 5, \# 145-850, 17^{\circ} 20', 22^{\circ} 30', 9^{\circ} 10^{\circ} 13^{\circ} 5, 13^{\circ} 17^{\circ} 22^{\circ} 15'$
20	8	09○	06○	00	05.0	11.0	09.4	.	$\overline{\text{P}} 0-24, \# 1^{\circ} 45-20', 90$
21	0	10≡	10○●	10○●	10.0	00.1	02.2	.	$\# 0-24, \# 45-20, 22^{\circ} 20', \# 540, 23^{\circ} 10', \# 20-22, 10', \# 1^{\circ} 23^{\circ} 22, 24$
22	8	10	05○	10≡	08.3	06.0	53.6	.	$\# 0-24, \# 1^{\circ} 45-20, 45-20, \# 20-10, 17^{\circ} 20', 24$
23	7	16≡	10○	10○●	10.0	01.1	.	.	$\equiv 0-100, \# 1^{\circ} 45-24, \# 1^{\circ} 45-25, 165, \# 1^{\circ} 45-24, 17^{\circ} 20', 21^{\circ} 20', 22^{\circ} 10', 13^{\circ} 23^{\circ} 23^{\circ} 20$
24	0	10○	10	10≡	10.0	00.0	47.0	.	$\# 0-3^{\circ}, \# 1^{\circ} 45-24, \# 1^{\circ} 45-20, 17^{\circ} 20', 21^{\circ} 20', 23^{\circ} 20', \# 17^{\circ} 16^{\circ} 17^{\circ} 18^{\circ}, 23-24; \# 13^{\circ} 24$
25	8	00≡	02○	00	00.7	12.3	03.4	.	$\equiv 0-655, \# 0-2, \# 0-130, \# 1^{\circ} 45-24, \# 1^{\circ} 45-24, \# 20-22, 20$
26	5	00○	06○	01	00.3	13.5	.	.	$\# 1^{\circ} 40-46, \# 0-20, 20^{\circ} 24', \# 21^{\circ} 22, 23$
27	9	02○	05○	00	02.3	13.3	.	.	$\# 1^{\circ} 45-56, 0-9, \# 13^{\circ} 2-24$
28	9	08	02○	01	03.7	09.9	.	.	$\# 0-9, 20^{\circ} 24$
29	9	01○	01○	00	00.7	11.9	.	.	$\# 0-8, \# 1^{\circ} 45-24$
30	8	00○	04○	02	02.0	10.4	.	.	$\# 1^{\circ} 45-18, \# 1^{\circ} 45-20, 24, \# 2-9, 13^{\circ} 15-17, \# 16^{\circ} 20, 17^{\circ} 20, \# 17-18^{\circ}, \# 17^{\circ} 20-20, \# 17^{\circ} 19^{\circ} 20, \# 17^{\circ} 20-21$
31	8	10	09	09	09.3	00.9	00.0	.	
MES.	VRED.	04.8	06.5	04.7	05.3	218.8	156.7		

MES. VRED. 04.8 06.5 04.7 05.3 218.8 158.7

$\varphi = 43^{\circ}43' N$   $\lambda = 18^{\circ}16' E$  Gr.  $\Delta G = +1h\ 13\ min.$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenog pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	596.2	597.4	597.4	08.8	11.2	10.0	10.0	11.4	08.0	-	08.5	08.0	07.9	100	80	86	89	N	5	N	2	-	0
2	596.7	596.6	596.3	10.4	10.2	07.8	09.1	13.3	07.5	-	09.2	07.5	07.9	97	80	100	92	SSW	4	NNE	2	ENE	3
3	595.1	596.2	596.5	07.1	08.5	06.2	07.0	08.9	06.0	-	07.6	08.3	07.1	100	100	100	100	NE	5	NE	5	NE	5
4	596.5	597.5	597.8	05.9	09.0	06.6	07.0	09.3	04.9	-	07.0	05.5	06.4	100	63	88	84	ENE	5	NE	5	NE	6
5	598.3	599.3	599.6	07.0	09.6	07.4	07.9	10.0	05.7	-	06.4	06.1	07.7	86	68	100	85	NE	6	NE	4	N	5
6	600.6	601.5	601.4	07.3	06.8	08.2	07.6	09.2	06.3	-	07.0	07.4	08.2	92	100	100	97	N	6	E	2	N	6
7	600.7	600.8	600.7	07.1	09.0	07.8	07.9	09.4	07.0	-	07.6	08.2	07.9	100	95	100	98	K	7	N	5	N	6
8	600.1	600.2	599.1	07.7	10.6	09.2	09.2	10.9	07.0	-	07.9	07.4	08.2	100	77	94	90	NE	5	E	2	S	2
9	596.7	596.0	595.8	10.0	11.8	06.2	05.6	12.1	06.2	-	07.2	05.6	04.7	79	54	100	78	SSW	6	S	6	N	8
10	594.9	596.3	596.8	-02.3	-00.6	-00.6	-01.0	00.2	-02.8	-	03.8	04.4	04.4	98	95	100	99	N	10	N	9	N	8
11	597.7	598.9	600.0	-00.6	05.6	06.2	04.4	06.3	-02.2	-	04.0	04.3	07.2	92	63	100	85	N	7	N	9	N	11
12	601.3	602.4	601.6	05.4	10.4	10.3	09.1	10.7	05.2	-	06.7	06.6	06.6	100	70	70	80	N	7	N	3	NNW	4
13	600.2	600.0	599.9	09.8	12.0	08.0	09.5	12.4	08.0	-	07.2	06.1	08.0	80	58	100	79	-	0	-	0	N	3
14	600.1	601.4	600.8	01.4	03.2	02.8	03.1	08.0	01.0	-	05.1	05.8	05.2	100	100	87	96	N	7	NNE	2	SSE	3
15	599.2	598.6	596.8	05.0	09.4	07.8	07.5	09.5	03.8	-	03.0	06.6	03.3	46	74	41	54	N	3	SW	2	NNW	3
16	593.7	593.5	593.7	07.4	08.0	04.5	06.1	09.2	04.5	-	03.0	05.4	06.3	35	67	100	65	NW	5	S	3	N	2
17	592.0	591.6	591.0	03.8	04.8	04.8	04.6	05.0	02.4	-	06.0	06.5	06.5	100	100	100	100	S	4	SSW	7	SSW	6
18	591.1	592.0	593.2	06.0	06.2	05.2	05.7	06.6	04.8	-	07.0	07.1	06.6	100	100	100	100	SSW	7	SSW	6	SSW	4
19	595.1	597.1	596.0	02.8	05.6	07.6	05.9	07.6	02.7	-	05.6	06.5	07.8	100	95	100	98	SW	6	SSW	6	SSW	8
20	593.5	593.8	593.8	07.6	07.4	06.2	06.9	08.2	06.0	-	07.8	07.7	07.1	100	100	100	100	SSW10	SSW	9	SSW	7	
21	592.2	593.3	594.4	03.2	02.6	02.6	02.8	07.2	02.4	-	05.8	05.5	05.5	100	100	100	100	SSW	7	SSW	8	SW	7
22	594.3	594.7	594.1	01.8	05.2	03.0	03.3	05.6	01.1	-	04.8	04.8	05.7	91	73	100	88	SW	4	SSW	4	SSW	4
23	592.6	592.2	591.9	00.4	00.6	-01.0	-00.3	03.3	-01.0	-	04.7	04.8	04.3	100	100	100	100	NE	4	NNE	3	N	3
24	590.5	591.8	593.7	-01.2	-01.1	-00.7	-00.9	-00.7	-01.7	-	04.2	04.2	04.4	99	100	100	100	N	7	N	8	N	4
25	594.2	595.3	596.6	-00.8	00.0	00.0	00.0	-01.2	-	04.3	04.6	04.6	100	100	100	100	N	2	N	4	N	4	
26	596.9	597.8	598.0	-00.8	00.0	-00.2	-00.3	00.0	-00.8	-	04.3	04.6	04.5	100	100	100	100	N	5	-	0	N	4
27	597.2	598.0	598.6	-02.6	-01.8	-02.2	-02.2	-00.2	-02.6	-	03.7	03.9	03.8	97	98	98	98	N	6	N	6	N	6
28	598.1	599.9	600.3	-05.2	-03.0	-04.5	-04.3	-02.2	-05.3	-	03.0	03.6	03.1	95	97	96	96	NNE	7	N	5	N	5
29	599.6	600.4	600.5	-07.2	-03.6	-03.4	-04.4	-03.4	-07.2	-	02.5	03.3	02.0	93	93	56	81	NE	8	N	5	N	5
30	599.9	600.6	599.9	01.6	04.8	04.5	03.9	05.6	-03.4	-	00.6	01.7	03.0	13	26	48	29	N	5	4	NNW	5	
MES.	596.5	597.2	597.2	03.6	05.4	04.2	04.4	06.4	02.2	-	05.5	05.7	05.9	90	84	92	89	5.7	4.5	4.5	4.9		
RESD.	596.5	597.2	597.2																				

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1	598.2	595.8	594.4	06.0	07.7	02.2	04.6	08.9	02.3	-	02.9	03.8	04.9	42	48	50	60	W	5	SW	8	SW	7
2	590.9	590.4	589.3	03.2	04.0	02.8	03.2	04.4	01.8	-	05.8	06.1	05.6	100	100	100	100	SSW	2	SSW	7	-	0
3	589.2	592.2	594.0	-01.7	-02.4	-04.1	-03.1	02.8	-04.1	-	04.0	03.8	03.2	98	98	94	97	N	5	N	6	N	7
4	596.5	598.4	598.7	-04.8	00.0	-00.3	-01.4	00.8	-05.4	-	02.9	04.0	03.3	92	87	74	84	N	5	-	0	NNW	5
5	596.1	598.8	598.0	01.2	05.3	02.8	03.0	05.4	-00.3	-	03.5	04.2	04.1	69	63	72	68	W	6	SW	4	SW	6
6	597.1	596.5	596.4	03.1	06.4	04.8	04.8	08.8	01.9	-	04.5	05.3	03.8	79	74	59	71	W	4	SW	7	SW	7
7	595.3	595.8	595.7	03.7	07.8	05.8	05.8	08.1	03.7	-	06.0	06.1	03.6	100	76	52	76	SW	8	SSW	6	SW	4
8	594.6	594.0	592.8	06.0	08.4	05.8	06.5	08.6	04.7	-	03.2	05.9	06.1	46	71	89	69	SSW	3	S	6	SSW	9
9	591.4	592.0	592.4	05.2	09.4	06.3	06.8	09.7	05.1	-	06.6	06.9	06.9	100	78	96	91	SSW	9	S	5	S	6
10	591.3	592.0	593.5	05.6	05.7	04.7	05.2	06.3	04.4	-	06.8	06.9	06.4	100	100	100	100	S	6	S	5	S	6
11	592.3	593.2	594.2	04.4	04.1	04.0	04.1	05.3	04.0	-	06.3	06.1	06.1	100	100	100	100	SSW	7	SW	5	SW	3
12	594.7	595.8	596.8	02.1	03.3	02.7	02.7	04.0	02.0	-	05.3	05.8	05.6	100	100	100	100	N	2	N	2	NE	5
13	597.5	597.8	598.8	02.4	03.2	02.0	02.4	03.6	02.0	-	05.4	05.8	05.3	100	100	100	100	NE	5	N	4	N	4
14	597.0	596.7	596.5	01.0	03.0	02.6	02.3	03.3	00.8	-	04.9	05.7	05.5	100	100	100	100	NE	5	NNE	6	NNE	7
15	596.2	596.8	597.0	01.4	02.6	01.6	01.8	02.9	01.2	-	05.1	05.5	05.1	100	100	100	100	NNE	7	NNE	4	NNE	3
16	596.8	597.3	597.5	-00.8	00.1	-01.0	-00.7	01.6	-01.0	-	04.3	04.0	04.2	99	100	99	99	N	7	N	3	N	4
17	597.5	598.1	598.7	02.0	01.8	01.8	01.9	03.2	-01.3	-	04.9	03.7	03.9	35	71	75	60	N	3	N	1	-	0
18	599.7	600.8	601.6	05.0	05.8	04.0	04.7	06.4	01.6	-	01.1	03.6	03.1	17	52	51	40	-	0	S	4	SW	4
19	601.4	601.5	601.7	06.0	08.0	08.0	07.5	08.2	03.8	-	02.2	03.7	02.1	31	46	26	34	SW	3	W	2	NW	6
20	601.0	601.7	601.8	07.0	07.8	05.2	07.0	08.0	05.6	-	01.8	03.8	03.										

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$$H_s = 2067 \text{ m} \quad H_b = 2070.4 \text{ m} \quad h_t = 3.0 \text{ m} \quad h_r = 1.5 \text{ m}$$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Imokanje broj sati	Padavine R mm	Šnežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	10	08○	00	06.0	05.9	03.3	•	+	05-18 0-280 782 24; = 282 750, □ 3-30, △ 182 24
2	0	10	10=○	10=○	10.0	03.0	•	•	•	△ 0-5, # 0-12= 0-5, = 5-710, R 02 23 80, △ 142 110, □ 112 23, T 122 13, R 13-10, ▲ 182 20
3	1	09○	10	10	06.7	02.9	09.0	•	•	= 0-2, 19 0-280, 0-100, 0-26, 0-170, 0-24, □ 162 20, ▲ 172 21, △ 172 21
4	8	10	06○	00	05.3	05.9	06.4	•	•	# 0-1100, = 282 1130, □ 182 24, △ 202 24
5	8	01○	06○	10	05.7	10.0	•	•	•	□ 0-1140, 192 24, □ 0-780, # 0-282 580, □ 182 24
6	7	08○	10=○	10	09.3	05.7	•	•	•	□ 0-24, = 0-510, 122 24, # 14-15 510 12, □ 132 14, △ 132 14
7	7	10	05	10	08.3	03.4	03.7	•	•	□ 0-24, = 0-24, # 0-132 600
8	8	10	04○	00	04.7	06.6	•	•	•	□ 0-100, 23 24, = 0-435, 182 1930, # 2-25, 10-515, □ 202 24
9	8	00○	04○	10=○	04.7	09.4	•	•	•	□ 0-24, □ 0-630, # 10 50 630, = 162 24, □ 182 23, △ 23 25
10	0	10	10	10	10.0	00.6	03.3	•	•	□ 0-24, = 0-282, * 0-282 24, V 182 24
11	8	09	.05○	10	08.0	06.8	•	•	•	□ □ 0-24, V 0-915, # 10 50 0 10, = 182 24, □ 23 22 24
12	2	10	01○	00	03.7	10.7	00.9	•	•	= 0-705, □ 0-1115, □ 0-130, # 10-5 705 4, □ 192 24
13	9	01○	06	10	05.7	08.5	•	•	•	△ 0-8, # 16 32 9, = 20 12 24, □ 20 22 24
14	3	10=○	01	00	03.7	07.2	02.6	•	•	= 0-170, □ 0-110, □ 12 8, # 14 22 24, □ 17 22 24, □ 19 22 24
15	8	01○	01○	00	00.7	12.1	00.2	•	•	□ 0-745, # 16-16 0-110, □ 19 22 24
16	8	06○	05○	10	05.0	10.5	•	•	•	□ 52 815, = 20 815, □ 20 815
17	0	10=○	10=○	10=○	10.0	00.0	04.8	•	•	= 0-24, □ 12 50 5, 0-17 10 20, □ 10 20 25, □ 5 12 16 10 22 15, □ 17 12 24
18	0	10=○	10	10=○	10.0	00.0	50.4	•	•	= 0-24, □ 0-210, □ 0-510, 8 33, □ 17 10 23, □ 9 32 8 30, □ 14 25 15, □ 13 15 20
19	8	10	10	10=○	10.0	01.8	35.5	•	•	= 0-10 3, 15 9, 14 24, 9 32 6, □ 16 20 23, □ 5 24 15, # 9 16 10, □ 23 24, □ 23 25
20	0	10=○	10=○	10=○	10.0	00.0	33.2	•	•	= 0-24, □ 0-24, □ 0-810, 12 23 23, □ 13 12 24, □ 14 22 24, □ 12 25
21	0	10	10=○	10=○	10.0	00.0	33.4	•	•	= 0-24, □ 0-24, □ 14 22 24, □ 14 22 24
22	8	02○	08○	10=○	06.7	05.3	05.2	•	•	= 0-05, 17 22 24, □ 17 22 24, □ 14 22 24, □ 15 22 24
23	0	10	* 10=○	10=*	10.0	00.0	07.2	•	•	= 0-24, □ 0-230, 14 32 120, □ 24 610 8 15, * 16 28 15, □ 15 24, □ 15 24
24	0	10	10	10=○	10.0	00.0	09.1	01	•	* 14-24, □ 0-24, □ 12 17 20, □ 13 12 20, □ 14 22 24
25	0	10	10=○	10=○	10.0	00.0	00.0	01	•	= 0-24, □ 11-150, □ 16 22 17 30, □ 18 22 23, □ 17 22 24, □ 17 22 24
26	3	10	10	10	10.0	30.1	02.6	01	•	= 0-24, V 18 22 24
27	0	10	10	10	10.0	00.0	•	•	•	= 0-24, V 0-24, □ 32 24
28	8	10	06○	10	08.7	04.9	•	•	•	= 0-111, 17 22 24, V 0-24, □ 0-24
29	8	00○	01○	05	02.0	11.8	•	•	•	= 0-410, □ 0-24, V 0-230, # 16 28 15, □ 14 22 24
30	9	00○	04○	00	01.3	11.0	•	•	•	= 0-11, 18-23, # 15-14 0-30

BALI AENICA

1977 OKTOBAR

MES.  
VRED. 04.4 04.6 03.3 04.1 217.7 75.8

$\gamma = 43^{\circ}43' N$   $\lambda = 18^{\circ}16' E$  Gr.  $\Delta G = +1h\ 13\ min.$ 

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D	Vazdušni pritisak P mm			Temperatura vazduha T °C						Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Mjn	Min 5 cm	7	14	21	Sred. Dies	7	14	21				
1	593.8	592.6	592.0	02.0	02.2	01.2	01.7	03.4	01.2	-	05.3	05.4	05.0	100	100	100	SSW 7	SSW 7	SSW 5		
2	591.6	592.4	593.3	-01.0	-01.3	00.6	-00.3	01.2	-01.6	-	04.3	04.1	04.8	100	99	100	100	SSW 3	NW 3	SE 3	
3	593.6	595.6	596.4	02.0	06.8	06.0	05.2	07.7	00.0	-	01.9	03.9	03.6	35	52	51	46	NNW 5	NNW 5	SW 6	
4	595.6	595.8	596.5	05.1	05.4	03.8	04.5	06.9	03.8	-	04.3	06.0	06.0	66	89	100	85	SW 7	SW 7	SW 8	
5	597.4	597.4	598.0	04.6	04.7	04.1	04.4	05.3	03.0	-	06.4	06.4	06.1	100	100	100	100	SW 5	SW 6	SW 6	
6	597.3	597.7	597.6	04.0	05.2	04.5	04.6	05.6	04.0	-	06.1	06.6	06.3	100	100	100	100	SW 6	SSW 5	SW 7	
7	598.7	599.6	600.2	02.6	04.6	02.6	03.1	04.9	02.6	-	04.8	06.1	04.7	87	96	84	89	N 2	-	0	
8	600.4	600.6	601.0	02.2	04.5	02.8	03.1	04.7	02.2	-	05.2	05.2	04.9	96	83	87	89	NE 2	-	0	
9	600.8	601.0	601.0	02.4	03.7	06.2	04.6	06.2	02.4	-	02.5	04.2	02.1	45	70	30	48	N 3	N 3	N 3	
10	599.5	600.0	599.6	05.7	05.7	02.9	04.3	06.6	02.9	-	02.7	03.8	05.5	39	56	97	64	N 6	N 7	N 9	
11	600.8	602.1	602.6	03.0	07.3	07.0	06.1	07.6	02.4	-	05.1	03.2	03.3	90	41	44	58	N 8	N 5	WSW 5	
12	600.1	597.4	594.2	05.4	07.8	04.2	05.4	07.8	04.2	-	03.2	03.4	03.5	47	43	57	49	W 6	SW 8	SW 11	
13	590.8	589.4	585.8	02.4	02.6	02.4	02.5	04.7	02.0	-	05.4	05.5	05.4	100	100	100	100	SW 12	SSW 7	SSW 9	
14	585.3	585.3	585.1	02.4	01.2	00.8	01.3	02.8	-02.2	-	05.4	05.0	04.9	90	100	100	100	SSW 8	S 3	SW 10	
15	582.4	583.5	584.8	01.4	00.8	00.7	00.9	01.5	00.0	-	05.1	04.9	04.8	100	100	100	100	SSW 15	SSW 10	SW 9	
16	580.7	578.7	578.6	01.0	-00.8	-03.4	-01.7	02.1	-03.4	-	04.9	04.3	03.5	100	99	97	99	SSW 14	SSW 8	SW 5	
17	579.7	581.1	580.0	-05.0	-03.2	-02.4	-03.3	-02.1	-05.0	-	03.0	03.5	03.8	95	97	98	97	SW 2	SW 8	SW 10	
18	583.1	585.4	587.2	-01.6	-04.0	-02.0	-02.4	-00.9	-04.2	-	04.0	03.3	03.9	98	96	98	97	SW 7	SW 3	SW 1	
19	587.4	589.0	591.0	-07.0	-09.3	-09.6	-08.9	-02.0	-05.6	-	02.5	02.1	02.0	93	91	92	92	SW 2	N 7	E 7	
20	590.5	589.5	589.2	-05.6	-01.3	-05.7	-04.6	-00.6	-09.6	-	02.9	03.8	01.1	95	91	37	74	ESE 6	SE 2	NW 1	
21	588.3	585.3	583.0	-02.1	-04.0	-04.2	-03.6	-02.0	-05.8	-	03.1	02.2	03.2	80	63	96	80	SW 7	SW 10	SSW 11	
22	584.0	585.2	587.0	01.0	02.1	00.7	01.1	02.5	-04.2	-	04.9	05.3	04.8	100	100	100	100	SSW 11	SSW 10	SSW 5	
23	586.4	588.5	589.9	-00.5	-05.1	-08.2	-05.5	00.7	-08.3	-	04.4	03.0	02.3	100	95	92	96	NW 5	N 5	N 5	
24	591.3	590.3	588.7	-10.3	-02.2	-04.7	-05.5	-02.0	-10.3	-	01.9	03.7	02.7	90	94	83	89	N 3	SSW 7	SSW 8	
25	587.0	586.1	584.1	-04.0	-02.8	-02.6	-03.0	-02.1	-05.6	-	01.9	03.6	03.6	57	97	94	83	SSW 10	SSW 7	SSW 5	
26	576.1	574.4	576.1	-07.4	-04.4	-07.0	-06.5	-01.1	-08.6	-	02.4	03.2	02.5	93	96	93	94	NNW 4	SSW 7	S 7	
27	578.2	580.6	583.3	-10.4	-09.0	-10.4	-10.1	-05.3	-10.6	-	01.9	02.1	01.9	90	92	90	91	NNW 3	NNW 4	NNW 8	
28	587.6	589.7	590.1	-11.5	-08.4	-05.0	-07.5	-05.0	-11.5	-	01.7	02.2	03.0	85	92	95	92	N 7	-	0	
29	590.7	590.7	590.6	-10.0	-02.4	-02.9	-04.6	-02.2	-10.0	-	01.9	03.8	03.3	91	98	90	93	E 5	SSW 7	SSW 7	
30	589.0	587.3	587.7	-02.4	-01.5	-01.5	-01.7	-01.4	-03.2	-	03.8	04.0	04.0	98	99	99	99	SSW 9	SSW 9	SSW 7	
MES.	VRED.	590.3	590.4	590.5	-01.0	00.2	-00.6	-00.5	01.8	-02.8	-	03.8	04.1	03.9	86	86	87	87	6.5	5.7	6.2

## 1977 DECEMBER

## BJELAŠNICA

1	587.4	586.3	585.6	-01.4	-01.2	-02.1	-01.7	-01.2	-02.1	-	04.1	04.2	03.8	99	99	98	99	SSW 6	SSW 6	SSW 8
2	583.3	583.0	583.0	-01.9	-14.0	-14.0	-11.0	-01.8	-14.0	-	03.9	01.4	01.4	98	87	87	91	SSW 5	N 5	N 11
3	583.2	587.4	590.9	-16.2	-14.6	-12.6	-14.0	-12.6	-16.3	-	01.1	01.3	01.5	85	88	87	87	N 12	N 10	N 11
4	591.2	590.4	591.2	-14.0	-15.6	-15.6	-15.2	-11.6	-16.0	-	01.4	01.2	01.2	87	86	86	86	N 11	N 11	N 10
5	590.7	590.0	589.1	-15.4	-11.2	-09.3	-11.3	-09.2	-16.6	-	01.2	01.8	02.1	86	90	91	89	N 8	2	WNW 6
6	587.4	583.8	583.6	-07.9	-06.2	-05.1	-06.1	-05.1	-10.3	-	02.3	02.7	03.0	93	94	95	94	SW 9	SW 11	SW 11
7	583.8	587.1	590.1	-04.7	-04.4	-05.2	-04.9	-03.3	-05.2	-	03.1	03.2	03.0	95	96	95	95	SW 9	SW 8	NNW 6
8	592.5	592.3	592.3	-03.4	-03.1	-02.8	-03.0	-02.4	-05.2	-	02.7	03.5	03.6	76	97	97	90	NW 2	SW 4	SW 5
9	588.8	588.7	588.0	-02.4	-00.9	-00.7	-01.2	-00.7	-02.9	-	03.8	04.3	04.3	98	99	99	99	SW 9	SW 9	SSM 9
10	588.7	589.8	592.0	-00.4	00.2	-03.0	-01.6	00.3	-03.0	-	04.5	04.7	03.6	100	100	97	99	S 6	E 3	N 5
11	594.8	596.3	597.0	-04.8	-03.9	-06.6	-05.5	-03.0	-06.6	-	03.1	03.3	02.6	95	96	94	95	N 4	N 5	E 6
12	597.2	597.6	598.5	-09.6	-10.0	-06.6	-08.2	-04.8	-10.1	-	02.0	01.9	02.4	91	88	86	88	NE 6	E 7	E 7
13	597.8	597.5	597.2	-04.7	-03.6	-04.0	-04.1	-02.3	-06.6	-	02.2	02.4	02.1	68	67	63	66	ESE 5	ESE 5	ESE 5
14	597.3	597.7	597.9	-08.4	-05.2	-06.5	-06.7	-04.0	-08.4	-	00.5	00.6	00.8	21	20	29	23	E 6	NE 4	N 4
15	595.3	593.8	593.0	-08.7	-08.2	-06.4	-08.4	-05.0	-08.7	-	02.2	02.3	02.2	92	92	92	92	N 8	N 9	N 10
16	595.8	596.2	596.3	-12.0	-10.8	-11.2	-11.3	-08.4	-12.0	-	01.6	01.8	01.8	89	90	90	90	N 8	N 9	N 8
17	593.1	594.4	596.4	-11.7	-12.8	-13.6	-12.9	-09.7	-13.6	-	01.7	01.5	01.4	89	88	88	88	N 12	N 9	N 6
18	595.4	595.2	595.7	-11.6	-08.7	-06.0	-08.1	-05.6	-13.6	-	01.7	02.2	01.3	89	92	43	75	N 7	N 5	N 5
19	594.7	594.8	595.9	-05.7	-05.8	-05.0	-05.4	-05.0	-06.4	-	01.1	02.4	01.7	37	81	53	57	NE 5	ESE 6	ESE 6
20	595.7	596.0	596.3	-03.0	-02.6	-03.9	-03.4	-02.1	-05.8	-	01.3	01.0	01.0	35	29	29	31	NE 3	N 3	NNE 5
21	596.2	596.3	596.6	-02.2	-00.8	-01.6	-01.6	-00.6	-03.9	-	01.0	00.9	00.6	26	20	14	20	ENE 3	-	0
22	597.0	598.2	599.4	-02.1	-00.3	-02.4	-01.8	00.5	-02.6	-	00.9	00.8	01.1	22	18	28	23	N 2	NE 2	NE 2
23	599.4	599.6	600.1	-01.6	-01.0	-01.4	-01.4	-00.4	-02.6	-	01.0	01.5	00.9	25	36	21	27	NE 2	SW 3	SW 2
24	600.1	599.6	598.5	-00.1	03.0	03.0	02.2	04.5	-02.0	-	02.5	02.2	04.9	54	38	86	59	NNW 4	NW 5	SW 5
25																				

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 $H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$ 

Dan	Visinost 0-9	Oblačnost N (0-10)					Insolacij R broj sati	Padavine R mm	Snežni polkrivac h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	0	10	*	10	*	10	*	10.0	00.0	00.6	.
2	0	10	*	10	*	00	*	06.7	00.0	08.8	35
3	8	08	06	0	00	04.7	05.3	00.2	.	.	.
4	8	02	04	0	10	06.0	08.2	.	.	.	.
5	0	10	*	10	*	10	*	10.0	00.0	.	.
6	0	10	*	10	*	10	*	10.0	00.0	01.4	.
7	7	08	08	0	00	05.3	01.3	.	.	.	.
8	8	01	02	0	00	01.0	08.9	.	.	.	.
9	8	00	04	0	02	02.0	09.0	.	.	.	.
10	8	08	10	0	04	07.3	01.4	.	.	.	.
11	8	02	01	0	00	01.0	08.3	.	.	.	.
12	9	00	00	0	00	00.0	08.9	.	.	.	.
13	0	10	*	10	*	10	*	10.0	00.0	.	.
14	1	10	*	10	*	10	*	10.0	00.0	01.7	.
15	0	10	*	10	*	10	*	10.0	00.0	28.6	.
16	0	10	*	10	*	10	*	10.0	00.0	03.2	.
17	1	10	*	10	*	10	*	10.0	02.4	27.5	20
18	0	10	*	10	*	10	*	10.0	00.4	09.2	28
19	0	10	*	10	*	10	*	10.0	00.0	10.2	36
20	8	10	*	00	00	03.3	07.8	01.6	40	.	.
21	8	02	08	0	10	06.7	03.0	.	40	VV 0-24, 3-24, 10-24, 14-24, 18-24, 22-24, 26-24, 30-24, 34-24, 38-24, 42-24, 46-24, 50-24, 54-24, 58-24, 62-24, 66-24, 70-24, 74-24, 78-24, 82-24, 86-24, 90-24, 94-24, 98-24, 102-24, 106-24, 110-24, 114-24, 118-24, 122-24, 126-24, 130-24, 134-24, 138-24, 142-24, 146-24, 150-24, 154-24, 158-24, 162-24, 166-24, 170-24, 174-24, 178-24, 182-24, 186-24, 190-24, 194-24, 198-24, 202-24, 206-24, 210-24, 214-24, 218-24, 222-24, 226-24, 230-24, 234-24, 238-24, 242-24, 246-24, 250-24, 254-24, 258-24, 262-24, 266-24, 270-24, 274-24, 278-24, 282-24, 286-24, 290-24, 294-24, 298-24, 302-24, 306-24, 310-24, 314-24, 318-24, 322-24, 326-24, 330-24, 334-24, 338-24, 342-24, 346-24, 350-24, 354-24, 358-24, 362-24, 366-24, 370-24, 374-24, 378-24, 382-24, 386-24, 390-24, 394-24, 398-24, 402-24, 406-24, 410-24, 414-24, 418-24, 422-24, 426-24, 430-24, 434-24, 438-24, 442-24, 446-24, 450-24, 454-24, 458-24, 462-24, 466-24, 470-24, 474-24, 478-24, 482-24, 486-24, 490-24, 494-24, 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$\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$  Gr.  $\Delta G = +1h\ 14\ min.$ 

BR. ST. 140

5 8	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina vetra D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
	1	710.7	708.8	706.4	-08.0	-03.6	-05.4	-05.6	-03.0	-08.2	-08.0	02.3	03.4	02.9	92	96	95	94	-	0	0
2	708.1	708.2	710.6	-02.6	06.5	03.0	02.5	06.6	-05.6	-07.0	03.5	04.5	05.3	92	62	94	83	-	0	S 1 ESE 2	
3	712.7	713.1	714.2	01.4	05.0	02.9	03.1	05.0	01.0	00.0	04.9	05.6	05.0	97	86	89	91	ESE 3	-	0	
4	714.3	716.2	718.5	02.1	05.0	02.4	03.0	06.0	01.8	01.0	05.0	05.6	05.1	94	86	94	91	SE 1	SSE 1	SW 1	
5	719.9	719.9	720.0	00.8	03.8	02.2	02.3	04.0	00.5	-00.6	04.5	05.1	05.2	93	85	97	92	ESE 1	SSW 2	-	
6	719.8	718.2	717.7	01.0	04.7	03.4	03.1	05.0	01.0	01.0	04.8	05.7	05.5	98	89	94	94	-	0	SW 1	
7	716.4	714.4	712.6	02.2	04.4	03.4	03.4	05.0	02.0	01.1	05.2	05.9	05.7	97	94	97	96	-	0	-	
8	711.4	712.0	710.9	01.6	01.6	-03.6	-01.0	01.0	03.5	-03.6	01.5	04.9	03.3	02.9	95	64	81	80	SE 3	SE 4 ESE 2	
9	709.9	707.7	707.3	-06.0	01.6	-03.0	-02.6	02.3	-06.8	-08.0	02.5	03.4	02.8	86	65	76	SSE 1	SW 1	SE 3		
10	704.8	702.8	702.9	-02.8	04.8	03.4	02.2	06.6	-03.6	-04.1	02.8	03.4	04.3	75	53	74	67	ESE 3	S 1	-	
11	702.4	700.6	699.4	07.8	10.0	08.6	08.8	10.0	03.2	00.9	04.5	05.2	05.1	57	56	61	58	S 5	S 6	W 3	
12	697.2	696.6	697.4	08.8	08.8	01.2	04.7	10.2	01.0	05.0	05.8	05.8	04.8	75	69	97	80	S 4	SW 3	ESE 2	
13	695.8	695.6	700.0	03.0	06.2	03.2	03.9	06.7	00.8	00.7	04.8	05.4	03.8	85	77	65	76	ESE 2	W 2	WSW 2	
14	703.8	703.9	704.9	00.0	07.2	00.6	02.1	07.2	00.0	-00.7	03.9	03.5	03.0	84	45	64	64	-	0	W 4 ESE 2	
15	702.7	700.2	701.5	02.4	07.6	03.0	04.0	08.7	-00.6	-02.7	03.9	05.3	05.3	72	68	94	78	SW 2	W 2		
16	702.3	702.8	704.0	00.4	00.8	-00.6	00.0	03.0	-01.0	-01.0	04.5	04.7	03.5	95	97	79	90	-	0	-	
17	704.2	704.0	705.3	-02.0	-01.2	-02.2	-01.9	-00.5	-02.2	-01.8	03.6	03.7	03.5	91	89	91	90	-	0	W 3 WSW 1	
18	706.4	706.1	708.1	-02.6	01.6	-04.8	-03.5	-01.0	-05.0	-02.8	03.3	03.4	02.5	88	84	79	84	NW 1	NW 2	E 2	
19	707.5	706.4	706.4	-09.2	01.0	-04.8	-04.5	01.5	-09.2	-10.8	01.9	02.9	02.4	81	58	75	71	ESE 2	SSW 1	ESE 3	
20	707.1	707.0	706.9	-06.4	02.4	02.5	00.3	02.9	-06.5	-08.0	02.5	03.5	04.1	90	63	74	76	SE 1	-	0 WNW 1	
21	707.5	707.6	708.7	01.6	06.0	03.4	03.6	06.0	01.0	00.5	04.6	05.2	04.8	90	74	82	82	-	0	0 ENE 1	
22	709.8	709.4	710.0	01.4	11.1	02.4	04.3	11.2	01.4	-00.6	04.5	04.6	04.3	89	47	78	71	ESE 2	SW 2	SE 1	
23	708.5	706.6	704.8	-00.2	08.6	04.3	04.3	08.6	-00.2	-01.8	03.9	04.9	04.6	86	58	73	72	SE 2	-	0 ESE 3	
24	702.2	702.1	704.2	02.7	05.8	05.0	04.6	06.2	02.6	02.0	05.3	06.3	06.2	95	91	94	93	-	0	-	
25	706.4	705.1	704.8	04.0	09.4	04.0	05.4	10.2	04.0	03.6	05.9	06.4	05.2	97	72	85	85	-	0	SSW 1 ESE 4	
26	704.0	702.3	701.4	01.6	10.7	08.4	07.3	10.7	00.9	-01.0	04.4	05.2	05.7	86	54	69	70	SE 1	S 4	S 3	
27	699.7	699.3	701.7	09.4	12.2	05.4	08.1	12.2	05.2	07.0	05.6	06.1	05.6	64	57	84	68	SW 3	W 5	NW 2	
28	705.1	704.6	704.1	03.4	10.4	06.4	06.7	11.4	03.4	01.0	05.5	04.9	04.6	94	52	64	70	SE 2	SSE 1	ESE 2	
29	699.9	695.5	697.2	10.0	12.0	07.7	09.4	14.8	05.8	05.6	06.1	06.6	06.7	67	63	85	72	S 3	S 5	WSW 1	
30	701.0	702.5	704.1	07.6	09.6	07.2	07.9	11.4	04.0	02.3	04.4	04.8	05.5	56	54	72	61	S 5	S 5	S 3	
31	705.1	704.2	702.1	03.4	08.8	06.0	06.1	09.0	02.6	00.5	05.0	05.7	05.5	85	67	79	77	ESE 2	SSE 1	ESE 3	
MES.	VRED.	706.7	705.9	706.4	01.1	05.8	02.4	03.0	06.5	-00.3	-00.8	04.3	04.8	04.6	85	70	82	79	1.6	1.9	1.6

## 1977 FEBRUAR

1	699.1	699.6	700.9	06.1	07.8	02.6	04.8	08.3	02.6	03.8	06.2	06.4	05.0	88	80	91	86	SSW 2	ESE 2	NNW 2
2	701.2	702.1	704.6	-00.8	-00.4	-02.6	-01.6	02.6	-02.6	-00.5	04.2	04.3	03.4	96	96	90	94	NNW 1	-	0 NW 1
3	705.5	705.9	706.3	-03.0	-01.2	-03.0	-02.6	-01.1	-03.5	-03.0	03.6	03.6	03.3	97	85	90	91	-	0	W 1 WNW 1
4	706.8	708.3	709.3	-03.4	-01.4	-04.6	-03.5	-00.4	-05.0	-03.5	03.3	03.4	03.0	93	82	92	89	-	0	ENE 1 E 1
5	708.2	707.9	709.1	-04.3	04.4	01.6	00.8	05.5	-05.0	-16.0	03.1	03.9	04.8	94	62	94	83	ESE 2	-	0 -
6	708.0	704.8	705.7	00.4	04.8	03.4	03.0	05.2	-00.4	-01.5	04.4	05.4	05.8	93	83	98	91	-	0	S 1 -
7	707.5	709.1	709.2	01.2	06.2	02.2	03.0	08.3	00.8	00.1	04.9	05.1	04.2	98	71	78	82	-	0	SE 2 ESE 3
8	707.6	705.1	704.0	-00.4	13.8	07.5	07.1	14.0	-00.6	-02.5	03.8	04.5	04.6	86	38	60	61	ESE 2	W 2	W 2
9	703.2	702.7	703.7	05.1	10.8	07.6	07.8	10.8	05.0	02.8	05.2	05.0	05.3	79	51	68	66	-	0	N 1 WNW 1
10	702.7	701.6	698.9	05.6	11.4	11.8	10.2	12.2	05.2	05.0	06.3	05.9	06.0	92	58	58	69	-	0	S 4 S 4
11	696.2	698.3	699.5	12.4	06.5	08.2	08.8	12.5	06.0	10.4	06.1	06.8	05.1	97	62	71	71	SW 3	-	0 W 2
12	696.8	696.3	698.5	10.8	11.4	07.0	09.1	14.4	06.1	04.0	06.6	06.3	05.8	68	62	77	69	S 3	S 3	WSW 1
13	702.7	703.4	702.8	05.9	12.2	07.4	08.2	13.0	05.6	04.0	05.3	04.6	04.9	76	43	63	61	-	0	SW 2 ESE 3
14	700.2	697.2	699.1	03.2	01.2	00.5	01.4	07.5	05.6	04.0	05.4	04.8	04.7	94	97	98	96	ENE 2	ENE 1	-
15	701.2	701.2	702.1	00.8	08.8	02.4	03.6	09.0	00.5	00.5	04.8	04.6	04.8	98	54	68	80	-	0	NW 2 ESE 2
16	702.8	702.2	703.2	-00.8	10.0	03.2	03.9	10.3	-01.2	-02.1	03.9	04.2	05.2	89	46	91	75	ESE 2	SSW 2	ESE 2
17	704.2	705.6	708.4	01.5	04.2	03.2	03.0	04.8	01.5	00.5	04.9	05.3	04.4	97	86	76	86	E 1	SW 1	-
18	709.5	708.7	711.2	-02.0	10.2	02.2	03.2	11.0	-02.5	-03.4	03.7	04.5	04.1	92	48	77	72	ESE 3	W 2	NW 1
19	711.8	710.3	710.0	01.2	10.3	09.0	07.4	12.0	00.4	-01.6	04.2	05.6	05.4	84	59	63	69	ESE 1	S 2	S 3
20	708.7	708.7	707.0	07.6	12.4	10.8	13.5	06.4	05.5	05.7	05.8	05.1	73	53	53	60	WNW 1	SW 3	S 4	
21	704.0	701.9	702.6	10.8	11.6	11.2	11.2	12.5	10.2	09.1	05.5	05.4	06.5	57	53	66	59	SW 4	SS 4	S 3
22	704.2	705.1	706.0	12.4	14.2	14.0	13.7	15.4	10.5	09.8	07.0	07.5	07.3	65	61	62	62	SSW 2	S 2	S 4
23	704.9	706.7	711.1	13.4	17.9	10.0	12													

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrem.	Oblačnost N (0-10)					Insekticij broj seti	Padavine R mm	Šnežni pokrivac h cm	Razvoj vremena	
		14	7	14	21	Sred Dnes				7	7
1	6	10	04	08.0	00.0	.	06	0-730	730-24, [X]		
2	5	09	07	09	08.3	03.5	04	0-130	[X]		
3	6	09	10	10	09.7	00.0	03	830-24, [X]			
4	5	08	10	04	07.3	00.0	03	0-24, 0-1630-1310 i, [X]			
5	4	10	09	10	09.7	01.6	00.2	0-24, 0-1830-2030			
6	3	10	04	10	10.0	00.0	00.4	0-230, 15-84; 0-0-3	230-12, 12-15		
7	3	10	04	10	10.0	00.0	00.4	0-130, 20-24; 440-20, 0-130-24, 0-2130-24			
8	7	10*	10	00	06.7	00.0	05.7	0-12, 0-630, 0-24, 0-620, X, 620-90, X, 730-90, 20-24			
9	7	04	01	00	01.7	05.6	01.2	0-11, 2030-24			
10	6	05	05	04	04.7	02.3	00.3	0-9, 0-15, 23-87			
11	8	06	09	07	07.3	00.2	00.2	0-346, 945-1350, 1310-24, 0-12-94			
12	7	10	10	10	10.0	00.5	07.6	0-230, 0-114, 0-1445, 0-1755-1930			
13	7	10	10	03	07.7	00.0	37.9	0-140, 1630			
14	8	10*	01	00	03.7	07.2	01.4	230-24, X, 350-730			
15	8	09	09	10	09.3	00.1	00.0	0-1830-24, 0-2130-24, 0-2330-24, X, 2130-2330, [X]			
16	5	10	10	09	09.7	00.0	14.3	0-1, 0-1030; 530-24, X, 1030-1330			
17	6	10*	10*	09*	09.7	00.0	03.3	0-04, X, 2-24, [X]			
18	6	10*	10*	00	06.7	00.0	01.2	0-130, X, 0-164, [X]			
19	6	00	01	00	00.3	07.8	00.0	9-1630, [X]			
20	5	01	10	10	07.0	02.5	00.3	3-830, 12-24, [X]			
21	7	10	10	07	09.0	00.1	00.0	0-140, 0-15300, 6-11, [X]			
22	6	03	02	00	01.7	07.0	00.3	1030-15			
23	7	00	09	10	06.3	03.9	00.3	3-9, 0-2130-24			
24	5	10	10	10	10.0	00.0	01.4	0-30, 530-630, 11-2330, =0-24			
25	7	10	05	00	05.0	02.4	03.1	0-11			
26	8	03	07	10	06.7	00.4	00.4	3-830, 1310-1030, 21-24, 0-1930-2130			
27	8	10	10	05	08.3	04.9	01.1	0-40, 0-62640			
28	8	07	08	09	08.0	00.5	00.5	0-8			
29	7	10	10	10	10.0	01.9	00.0	330-410, 1030-24, 1040-1330, 0-1730-1935			
30	8	07	10	09	08.7	01.4	05.5	0-04, 630-930, 0-20, 1030, 0-020-045			
31	8	08	09	10	09.0	00.3	00.0	0-19			
MES. VRED.		07.7	08.1	06.4	07.4	54.1	88.6				

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1	8	10	07	10	09.0	00.2	03.2	• 0-1130, 1410-1630, 2110-24, X, 2130			
2	6	10*	10*	10	10.0	00.0	11.6	08	• 0-130, X, 1030-1730, =17-24, [X]		
3	6	10	10	10	10.0	00.0	04.1	07	=0-24, 0-32-10, [X]		
4	6	10	09	00	06.3	00.2	00.4	0-24, [X]			
5	6	04	03	00	02.3	06.1	00.3	0-24, [X]			
6	6	10	10	07	09.0	00.0	00.4	0-23, 0-1350-1830, =23-24			
7	6	15	09	00	06.3	02.6	06.6	0-930, 0-450-1530, X, 730-810, =930-15			
8	7	00	08	03	03.7	08.4	60.8	2-8, 0-490-930			
9	8	10	10	10	10.0	00.1	00.3	0-1030, 0-2030, 11-2045			
10	8	10	09	07	08.7	02.9	00.7	0-1030, 0-2030, 1350-14, 18-2045			
11	7	10	09	00	06.3	01.6	00.0	0-0, 0-1350-320, 0-320-1350, 0-1330, 1410			
12	7	10	09	10	09.7	03.1	20.2	3-5, 0-1930-2030, 0-1930-2130, 0-2030			
13	8	09	07	09	08.3	04.4	04.6	0-1930			
14	5	10	10	10	10.0	00.0	07.7	0-1030, X, 1030-24, 0-1730-1935, [X]			
15	8	08	08	05	07.0	05.6	19.5	*0-40, =0-1130, 0-1730-1935, [X]			
16	8	00	06	09	05.0	07.6	00.0	3-8, 0-1830-2030			
17	6	10	10	09	09.7	00.2	00.6	0-24, 0-1730-1930			
18	8	00	05	03	02.7	06.3	00.3	0-6, 0-9			
19	8	04	08	08	06.7	04.5	00.3	0-8, 0-1630-2230			
20	8	05	09	08	07.3	04.9	00.3	0-02-210, 11-15-1330, 1915-24			
21	8	09	09	10	09.3	00.2	00.3	0-1730-2130-2330, 0-1430-2230			
22	8	09	09	06	08.0	01.3	00.0	0-1330-2030			
23	8	10	02	00	04.0	35.9	00.0	0-0, 0-1230-1530, 0-630-1130			
24	8	05	10	09	08.0	01.6	00.0	0-1730-2130, 0-1530-1930			
25	8	09	09	10	09.3	04.0	00.3	0-0, 0-1630-1930, 0-1530-2130, =2030-2130			
26	8	09	09	07	08.3	05.0	03.4	0-2030-24			
27	7	10	09	04	07.7	02.9	06.7	0-0, 0-2030-2230, 0-1630-2030, =1-1330			
28	7	10	09	09*	09.3	02.8	00.9	*0-2030-24, 0-1330-1330, 0-2030-2130, [X]			
MES. VRED.		07.9	08.3	06.5	07.6	82.4	91.3				

$\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$  Gr.  $\Delta G = +1h\ 14min.$ 

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Dn	Vozdušni pritisak P mm			Temperatura vazduha T °C						Napon vodené pare e mm			Relativna vlažnosť v %			Pravac i jačina vetro D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	714.0	712.8	713.8	-05.0	00.0	-00.4	-01.5	01.2	-05.4	-05.4	02.1	02.3	02.4	66	51	53	57	NNW 2	E 1	N 1	
2	713.9	713.9	712.8	-01.6	03.1	-02.2	-00.7	03.4	-02.2	-02.0	03.1	03.1	02.4	77	55	62	65	- 0	W 2	ESE 1	
3	710.8	709.6	708.2	-01.4	04.0	03.4	02.4	05.5	-03.0	-04.5	02.9	04.9	05.0	71	80	85	79	SSW 1	- 0	- 0	
4	708.9	707.8	707.6	02.0	12.0	07.7	07.4	13.1	01.6	01.2	04.9	06.2	05.8	92	59	74	75	ENE 1	ESE 3	ESE 3	
5	709.6	711.7	713.3	04.2	10.4	04.6	06.0	11.2	04.2	01.5	05.3	04.9	04.6	86	52	72	70	- 0	SW 1	ESE 4	
6	712.4	710.9	712.3	01.4	17.5	07.8	08.6	17.9	00.7	-00.8	03.9	03.4	03.4	77	23	43	48	ESE 2	W 4	ESE 2	
7	715.0	715.0	718.3	01.4	15.0	05.8	07.0	15.4	01.4	-00.6	04.2	05.1	04.3	84	40	63	62	ESE 2	MSW 2	SE 4	
8	720.6	720.0	721.0	01.7	15.8	06.3	07.5	16.4	00.5	-01.0	04.1	04.3	03.9	79	32	55	55	ESE 3	MSW 1	E 2	
9	719.3	715.9	714.5	00.7	18.0	08.6	09.0	18.5	00.2	-02.1	03.3	02.7	03.1	68	18	36	41	ESE 3	W 2	SE 1	
10	712.5	709.5	708.7	02.2	16.4	09.0	09.2	17.1	02.0	00.0	04.1	05.6	05.0	77	40	58	58	ESE 2	WNW 2	E 4	
11	707.8	706.2	706.8	03.2	17.3	10.6	10.4	17.4	02.0	01.5	04.6	05.1	04.9	81	35	51	56	E 2	WNW 2	S 2	
12	706.0	704.9	703.7	09.6	10.6	09.8	10.0	13.0	09.0	06.9	05.7	07.9	06.7	64	82	74	73	- 0	S 1	ESE 2	
13	700.4	700.4	705.7	08.5	11.7	04.4	07.3	12.0	04.0	06.7	05.9	05.4	05.9	70	52	94	72	ESE 1	SW 1	W 3	
14	709.9	710.1	711.3	04.4	10.6	05.6	06.6	11.6	03.0	03.0	05.7	05.0	04.2	91	53	62	69	- 0	W 2	ESE 3	
15	713.7	715.5	715.6	00.7	06.0	04.4	03.9	07.5	00.5	-01.0	04.4	06.1	05.0	92	87	80	86	E 1	- 0	- 0	
16	717.6	716.5	716.2	00.6	13.0	05.2	06.0	13.3	00.2	-01.3	04.5	04.7	04.2	93	42	64	66	ESE 1	W 2	ESE 3	
17	714.7	711.8	711.1	01.1	17.6	08.6	09.0	18.5	00.2	-01.5	03.7	03.3	03.8	75	22	45	47	SE 2	SSW 1	ESE 3	
18	710.2	707.2	706.9	02.8	20.0	11.0	11.2	21.0	02.0	00.5	04.1	04.9	04.7	73	28	47	49	E 3	WSW 2	ESE 2	
19	705.9	703.1	703.2	04.8	19.0	13.2	12.6	20.4	04.8	03.0	05.1	05.4	05.0	79	33	44	52	ESE 2	WSW 2	S 3	
20	703.6	704.7	705.8	08.8	14.2	09.3	10.4	14.4	08.4	07.2	06.7	04.8	05.7	78	40	64	61	E 2	W 2	ESE 3	
21	706.5	708.0	710.4	07.2	14.0	10.4	10.5	14.6	07.2	06.4	07.1	05.3	05.0	94	44	53	64	E 1	S 3	NW 1	
22	710.7	711.2	712.3	09.4	18.2	12.4	13.1	19.7	07.0	04.9	05.6	05.8	04.8	63	37	44	48	ESE 3	SW 2	SE 1	
23	713.0	711.7	712.2	07.4	25.7	13.6	15.1	25.7	07.3	04.0	04.2	04.8	04.8	55	19	41	38	SE 3	MSW 3	ESE 2	
24	712.1	709.8	709.8	08.2	25.6	14.4	15.7	25.8	07.8	05.8	05.0	04.0	05.2	62	16	43	40	SE 3	MSW 3	ESE 3	
25	709.6	708.7	709.8	09.0	21.4	13.6	14.4	23.3	08.2	05.6	05.4	07.0	05.4	63	37	46	49	SE 1	WNW 1	SE 3	
MES.	VRED.	709.7	708.9	709.4	04.0	14.3	08.0	08.6	15.3	03.1	01.9	04.8	05.1	04.8	78	45	61	61	1.5	1.9	2.0

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1	708.9	709.1	707.5	04.4	09.6	06.9	07.0	10.2	04.2	02.8	05.7	06.3	06.0	91	70	81	81	- 0	- 0	- 0
2	703.3	702.1	702.0	05.8	10.8	09.4	08.9	11.5	05.6	02.6	06.5	07.6	08.2	95	78	93	89	- 0	SSW 1	- 0
3	700.4	698.9	699.7	08.8	15.0	11.4	11.7	16.6	08.5	09.0	08.1	10.3	07.8	95	81	77	84	SSW 1	MSW 2	- 0
4	703.0	703.4	705.4	08.0	17.9	12.4	12.7	18.6	07.3	04.5	07.2	06.3	06.4	90	41	59	63	- 0	MSW 2	- 0
5	704.9	703.6	703.6	11.4	16.4	06.9	10.4	17.6	06.9	06.2	06.4	06.2	05.8	64	44	78	62	SSE 1	SW 2	M 1
6	707.4	705.5	703.9	01.4	12.0	06.4	06.6	13.3	00.2	00.5	04.8	04.6	05.5	95	44	77	72	- 0	SSE 1	ESE 3
7	703.4	701.3	700.6	03.4	16.6	13.2	11.6	17.5	1.8	00.1	04.6	06.2	05.1	79	44	44	56	SE 1	W 2	ESE 1
8	697.5	695.6	695.7	15.0	20.4	14.4	16.1	22.0	10.5	06.0	02.9	05.1	06.1	22	28	50	33	S 4	SW 2	SE 3
9	691.0	691.1	694.5	10.8	15.4	08.0	10.6	16.0	08.0	07.5	06.6	05.3	03.9	68	40	49	52	W 2	SSW 5	SW 4
10	695.0	696.0	699.8	06.0	10.3	02.8	05.5	11.5	02.8	04.0	04.3	04.5	05.3	61	48	94	68	NW 2	SSW 2	NW 1
11	703.2	702.7	703.7	00.8	04.4	02.2	02.4	05.6	00.0	00.7	03.4	03.0	02.8	70	48	51	56	NNW 2	NE 2	E 3
12	703.9	702.6	702.4	-01.2	05.6	00.6	01.4	06.0	-01.3	-03.6	02.8	02.8	03.8	66	42	80	63	N 1	ENE 3	- 0
13	704.9	704.0	703.2	-00.0	06.8	03.9	03.7	07.0	-01.5	-01.5	04.3	03.2	04.0	93	43	66	67	- 0	WNW 2	ESE 2
14	701.8	701.2	699.8	01.9	07.6	06.6	05.7	09.0	01.7	00.7	04.9	05.5	05.6	94	71	77	81	- 0	W 1	- 0
15	696.0	696.1	699.1	00.8	01.2	00.2	00.6	06.6	00.2	00.6	04.5	04.8	04.6	93	97	98	96	WNW 1	W 1	W 3
16	701.1	702.7	706.0	00.2	05.0	00.8	01.7	05.0	00.1	00.8	04.6	04.1	04.7	98	62	97	86	W 2	WNW 2	WSW 1
17	708.6	707.8	708.4	01.2	09.8	01.8	03.7	09.8	-00.4	00.7	03.5	03.4	03.4	71	37	65	58	W 3	WNW 2	- 0
18	708.5	707.3	708.6	-00.7	15.6	06.8	07.1	16.5	-02.9	-04.0	03.3	01.6	03.0	75	12	41	43	ESE 2	SW 2	ESE 3
19	709.9	708.4	709.5	03.4	16.2	10.6	10.2	17.7	01.4	-00.5	04.1	03.6	04.0	71	26	42	46	ESE 2	W 1	- 0
20	711.1	713.9	713.5	06.0	04.4	04.8	10.6	04.2	02.5	05.9	05.5	05.6	84	87	89	87	- 0	- 0	- 0	
21	713.4	711.6	712.2	02.6	12.6	04.8	06.2	13.0	01.3	-01.8	04.0	02.2	03.7	73	20	58	50	- 0	NE 3	SE 2
22	712.3	709.5	709.2	01.1	16.4	08.8	08.8	17.0	-01.0	-03.0	03.7	03.4	03.0	74	24	35	44	ESE 1	NW 2	ESE 2
23	708.2	704.5	704.6	06.4	22.4	16.0	15.2	23.0	03.5	01.7	05.0	05.2	04.9	69	25	36	43	SE 2	NNE 1	NNW 1
24	703.3	701.4	701.4	13.2	21.5	14.8	16.1	22.0	10.5	0.9	06.4	05.6	06.8	56	29	54	46	WNW 1	WSW 5	NW 2
25	708.2	708.4	709.0	01.4	11.0	05.8	06.0	14.8	01.4	01.0	04.9	03.7	04.4	97	38	63	66	- 0	NNW 2	ESE 2
26	710.6	709.3	708.8	03.7	15.0	09.4	09.4	15.5	01.3	00.2	04.7	04.6	04.8	78	36	55	56	- 0	- 0	ESE 1
27	708.6	706.0	706.9	05.8	23.6	15.4	15.1	24.1	03.3	02.3	05.3	04.8	06.5	76	22	49	49	ESE 2	WSW 2	SE 2
28	708.8	707.3	707.6	11.4	24.5	15.6	16.8	24.5	11.0	0.9	07.7	08.3	08.6	76	36	65	59	- 0		

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vremenska časost 0-9	Oblačnost N (0-10)					Insektocija broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena	
		14	7	14	21	Sred Dnes				7	7
1	7	09*	07	08	08.0	02.9	01.2	01	*	0-9 <sup>30</sup> , $\square$	
2	6	10*	07○	00	05.7	04.0	00.2	•	*	0-9 <sup>30</sup> , $\square$ = 7 <sup>30</sup> 24, $\square$	
3	6	10*	00	05	05.0	00.0	00.8	•	=	0-24, $\square$ 6 <sup>30</sup> 9, ● 12-13 <sup>30</sup> , 17 <sup>40</sup> 18 <sup>10</sup>	
4	7	09	09	09	09.0	01.2	01.2	•	=	2 <sup>30</sup> 19 <sup>10</sup>	
5	7	09	06○	00	05.0	04.5	•	•	△	0-8 <sup>30</sup> , ● 8 <sup>30</sup> 11, = 9-11	
6	8	06	02○	00	02.7	10.3	00.1	•			
7	6	04	07○	02	04.3	07.1	•	•	△	5-10, = 8-15	
8	8	08	05○	00	04.3	09.5	•	•	△	0-5 <sup>30</sup> , 19-24, $\square$ 15 <sup>30</sup> 7 <sup>30</sup> , = 6 <sup>30</sup> 10 <sup>30</sup>	
9	8	02○	07○	00	03.0	08.9	•	•	△	0-5 <sup>30</sup> , 5-8	
10	8	00○	01○	00	00.3	10.1	•	•	△	0-5 <sup>30</sup> , $\square$ 5 <sup>30</sup> 8	
11	7	00○	02○	05	02.3	09.4	•	•	△	3-10, = 9-12, $\square$ 22 <sup>30</sup> 23 <sup>30</sup>	
12	7	09	10○	09○	09.3	00.6	•	•	●	12 <sup>30</sup> 24, $\square$ 3 <sup>30</sup>	
13	8	10	10	10	10.0	00.1	10.2	•	●	0-3 <sup>30</sup> , 14 <sup>30</sup> 24, $\square$ 3 <sup>30</sup> 4, = 18 <sup>30</sup> 24	
14	7	10	08	04	07.3	03.0	09.4	•	●	0-3 <sup>30</sup> , = 3-8 <sup>30</sup>	
15	6	04	10○	04	06.0	01.1	•	•	△	3-4 <sup>30</sup> , $\square$ 4 <sup>30</sup> 8, = 8-15, ● 9 <sup>30</sup> 14 <sup>30</sup>	
16	7	01○	05○	00	02.0	09.5	01.1	•	■	3-8, = 6-9 <sup>30</sup> , △ 19-24	
17	8	01○	00○	00	00.3	10.5	•	•	△	0-5, $\square$ 5-7 <sup>30</sup>	
18	8	00○	01○	01	00.7	10.4	•	•	△	3-10, $\square$ 19 <sup>30</sup> 20 <sup>30</sup> , 22 <sup>30</sup>	
19	8	03	06○	05	04.7	09.4	•	•	●	3-5, $\square$ 2 <sup>30</sup> 23 <sup>30</sup>	
20	7	09	08	10	09.0	01.9	00.5	•	●		
21	8	09○	10	00	06.3	00.4	03.3	•	●	0-6 <sup>30</sup> , △ 20 <sup>30</sup> 24	
22	8	09	09	01	06.3	00.4	00.1	•	△	0-9, 20 <sup>30</sup> 24	
23	8	00○	03○	00	01.0	10.5	•	•	△	0-7 <sup>30</sup>	
24	8	00○	02○	04	02.0	10.5	•	•	△	22-24	
25	8	08	08○	08	08.0	02.9	•	•	△	0-9	
26	8	00○	08	03	03.7	06.8	•	•	△	0-8, $\square$ 14 <sup>30</sup> 15 <sup>30</sup> , ● 14 <sup>30</sup> 14 <sup>30</sup> , 19 <sup>30</sup> 18 <sup>30</sup>	
27	8	00○	02○	05	02.3	10.2	00.3	•	△	0-9, 14 <sup>30</sup> 24, = 0-24	
28	7	04○	09	10	07.7	05.4	•	•	△	0-8, $\square$ 13-13 <sup>30</sup> , ● 23 <sup>30</sup> 24	
29	7	10○	08	10○	09.3	00.5	00.0	•	●	0-0 <sup>30</sup> , 5-8 <sup>30</sup>	
30	6	10*	10○	10○	10.0	00.0	14.8	10	*	0-6 <sup>30</sup> , = 0-24, ● 13 <sup>30</sup> 24, $\square$	
31	8	09	10	09	09.3	00.0	21.4	02	●	0-3, = 0-11, $\square$	
MES- VRED.		05.6	06.1	04.3	05.3	162.0	64.6				

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1	6	07	06	06	06.3	00.0	•	•	△	0-9, 21-22 <sup>30</sup> , = 9-24, ● 22 <sup>30</sup> 24	
2	6	10	10	10○	10.0	00.1	00.7	•	●	0-11, 14 <sup>30</sup> 24, = 0-24	
3	7	10	=	09	06.3	00.8	01.4	•	≡	0-8, ● 0-0 <sup>30</sup> , = 8-13 <sup>30</sup> , △ 19 <sup>30</sup> 24	
4	7	09	08○	08	08.3	06.0	•	•	△	0-10, = 8-11	
5	8	08○	09	10○	09.0	03.4	•	•	△	0-8, ● 20 <sup>30</sup> 22 <sup>30</sup> , $\square$ 22 <sup>30</sup> 22 <sup>30</sup> , * 22 <sup>30</sup> 24	
6	7	10	02○	00	04.0	06.4	14.7	03	*	0-4 <sup>30</sup> , = 0 <sup>30</sup> 11, $\square$	
7	8	00○	10	07	05.7	04.2	•	•	△	0-8	
8	8	04○	09	08	07.0	03.9	•	•	≡	0-23 <sup>30</sup>	
9	8	08○	03○	10	07.0	07.5	02.4	•	≡	0-8, 10 <sup>30</sup> 45 <sup>30</sup> 6 <sup>45</sup> 10 <sup>30</sup> 14 <sup>30</sup> ; ● 21 <sup>30</sup> 6 <sup>30</sup> 11 <sup>30</sup> , 10 <sup>30</sup> 10 <sup>30</sup> , $\square$ 10 <sup>30</sup> 15 <sup>30</sup>	
10	8	09	06○	05	06.7	02.6	00.0	•	●	10 <sup>30</sup> 14 <sup>30</sup> , 15 <sup>30</sup> 20 <sup>30</sup> , $\square$ 10 <sup>30</sup> 10 <sup>30</sup> , $\square$ 15 <sup>30</sup> 15 <sup>30</sup>	
11	7	10*	08	10	09.3	01.4	01.3	•	*	5 <sup>30</sup> 8	
12	8	06	08○	09	07.7	04.0	00.0	•	△	0-4, $\square$ 4-8, * 8 <sup>30</sup> 9 <sup>30</sup> , 12 <sup>30</sup> 15, 18-20	
13	7	10*	09	10	09.7	02.2	00.5	•	×	19 <sup>30</sup> 10	
14	6	10*	* 09	10	09.7	00.6	01.1	•	●	14 <sup>30</sup> , = 3-15, 20 <sup>30</sup> 24, $\square$ 5 <sup>30</sup> 9	
15	5	10*	10*	10*	10.0	00.0	14.4	02	●	0-4 <sup>30</sup> , = 0-24, $\square$ 4 <sup>30</sup> 5 <sup>30</sup> , $\square$ 5 <sup>30</sup> 24, $\square$	
16	8	10*	10*	10*	10.0	03.3	17.6	06	*	0-8 <sup>30</sup> 11-24; = 0-8, $\square$ 4 <sup>30</sup> 16 <sup>30</sup> , $\square$	
17	7	10	05○	00	05.0	10.0	05.0	02	=	0-8 <sup>30</sup> * 5 <sup>30</sup> 6 <sup>30</sup> , 10 <sup>30</sup> 24, $\square$	
18	8	00○	02○	00	00.7	12.6	•	•	△	0-8 <sup>30</sup> , $\square$ 10 <sup>30</sup> 24	
19	8	05○	08	06	06.3	09.4	•	•	△	0-8 <sup>30</sup> , $\square$ 6 <sup>30</sup> 4 <sup>30</sup> , = 8-24, $\square$	
20	6	10○	10○	10	10.0	00.0	00.0	•	△	0-6 <sup>30</sup> , ● 6 <sup>30</sup> 4 <sup>30</sup> , = 8-24, $\square$ 4 <sup>30</sup> 16 <sup>30</sup>	
21	8	00○	00○	00	00.0	12.5	02.2	•	≡	0-3, $\square$ 10-24	
22	8	00○	01○	05	02.0	12.4	•	•	△	0-3, $\square$ 3-9, = 6-9	
23	8	09	05○	04	06.0	09.5	•	•	△	0-8	
24	8	07○	06○	00	04.3	09.3	•	•	△	0-8 <sup>30</sup>	
25	7	10*	06○	00	05.3	07.2	04.8	•	△	0-3 <sup>30</sup> , 21-24; ● 3 <sup>30</sup> 5 <sup>30</sup> 9 <sup>30</sup> 7 <sup>30</sup> , * 5 <sup>30</sup> 7 <sup>15</sup> , $\square$ 3 <sup>30</sup> 3 <sup>40</sup>	
26	8	08○	07○	00	05.0	06.5	00.8	•	△	0-9 <sup>30</sup>	
27	8	00○	00○	03	01.0	13.2	•	•	△	0-8	
28	8	10	08○	01	06.3	05.3	•	•	△	0-8	
29	8	07	06○	00	04.3	09.0	•	•	△	0-8, 20-24	
30	8	04○	08○	09	07.0	10.3	•	•	△	0-8 <sup>30</sup>	
MES- VRED.		07.0	06.6	05.4	06.3	173.6	66.9				

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 $\varphi = 43^{\circ}52' N$   $\lambda = 18^{\circ}26' E$  Gr.  $\Delta G = +1h\ 14\ min.$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	706.7	705.9	707.6	14.8	27.0	17.4	19.2	27.0	12.0	11.5	08.2	06.6	07.8	65	25	52	47	ESE 3	WSW 2	- 0	
2	709.6	708.9	709.7	11.2	24.6	15.5	16.7	25.3	10.0	08.2	07.6	06.3	09.6	76	27	73	59	ESE 1	WNW 2	ESE 3	
3	709.6	708.1	707.0	11.4	27.0	17.6	18.4	27.0	10.2	07.8	08.4	07.2	10.0	84	27	67	59	- 0	- 0	ESE 2	
4	707.1	705.5	705.1	13.1	28.0	19.0	19.8	28.2	11.2	09.9	08.4	06.7	07.2	74	24	44	47	- 0	WNW 2	ESE 2	
5	705.8	707.1	708.1	16.4	16.4	13.0	14.7	23.6	13.0	13.7	08.7	10.1	09.8	62	72	87	74	ESE 3	SSE 2	ESE 3	
6	709.3	708.6	708.5	11.0	12.9	10.2	11.1	13.2	10.0	08.2	09.5	10.1	08.7	97	90	93	93	- 0	SE 2	- 0	
7	708.0	705.4	705.0	09.2	18.4	12.6	13.2	19.0	08.5	07.4	08.1	05.3	07.7	93	33	70	65	SE 2	W 2	SE 2	
8	703.5	701.4	703.6	09.8	15.2	07.8	10.2	16.3	07.6	07.3	07.4	06.4	07.5	81	49	95	75	NE 1	W 2	- 0	
9	703.8	703.5	705.9	06.2	14.0	08.6	09.4	15.3	04.4	03.7	06.7	07.3	07.8	95	61	93	83	ESE 1	ESE 1	NNW 1	
10	706.2	707.0	707.7	05.6	08.6	07.6	07.4	11.0	05.5	06.3	06.5	07.2	07.2	96	85	92	91	- 0	- 0	- 0	
11	708.4	707.2	707.8	06.8	16.4	08.6	10.1	17.1	06.4	07.1	07.0	07.1	06.8	95	51	81	76	- 0	WSW 1	ESE 2	
12	707.6	704.8	703.8	06.4	20.6	12.4	13.0	21.0	03.7	03.0	06.0	04.3	05.8	83	24	53	53	SE 1	WSW 1	S 1	
13	703.5	701.7	702.4	09.8	23.0	16.6	16.5	23.2	06.0	05.2	06.8	07.9	04.5	75	37	32	48	SE 1	W 2	S 3	
14	701.2	700.8	701.0	13.4	16.0	13.2	14.0	17.4	11.0	09.0	05.6	07.3	08.0	48	54	70	57	WNW 1	S 1	ESE 3	
15	700.0	695.5	700.5	11.4	19.6	12.8	14.2	19.6	11.0	10.6	07.9	06.6	07.3	78	38	66	61	- 0	S 2	- 0	
16	701.6	701.2	703.9	10.0	19.0	11.4	13.0	19.5	09.0	07.6	07.6	07.3	07.7	83	44	76	68	- 0	W 3	NNW 1	
17	706.3	708.2	710.4	12.2	20.0	14.2	15.2	20.3	09.0	08.0	08.8	08.2	08.8	83	47	72	67	ESE 1	W 1	ESE 2	
18	712.0	710.0	710.3	11.8	22.7	17.6	17.4	23.0	10.0	08.5	08.9	12.4	12.4	86	60	82	76	- 0	W 1	- 0	
19	709.8	708.4	707.9	14.4	28.2	21.4	21.4	29.0	14.0	12.5	11.8	11.9	10.6	96	41	55	64	- 0	WSW 1	SE 1	
20	707.7	707.4	707.9	21.0	26.0	21.2	22.4	26.4	19.1	16.1	09.0	08.9	07.4	48	35	39	41	ESE 1	S 3	WSW 1	
21	708.5	707.4	708.4	20.4	25.8	20.8	22.0	26.6	18.4	15.5	08.5	08.0	06.9	47	32	37	39	WSW 1	SW 2	S 3	
22	708.7	707.0	708.8	14.6	25.6	17.4	18.8	26.5	12.5	10.2	08.8	07.3	09.2	71	30	61	54	- 0	WSW 1	NE 1	
23	709.9	709.1	709.9	13.2	22.0	13.6	15.6	23.0	13.0	12.5	09.7	09.5	09.3	85	48	80	71	NW 1	W 2	WSW 1	
24	710.9	710.6	710.5	11.0	17.6	12.6	13.5	18.2	10.9	11.2	09.2	08.1	06.3	93	54	58	68	SSE 1	W 1	ESE 3	
25	709.6	706.9	706.9	08.4	21.8	14.4	18.8	22.2	05.6	04.6	06.9	07.1	06.1	83	36	49	56	S 1	W 2	E 2	
26	707.7	706.3	706.9	09.4	23.0	15.0	15.6	23.8	07.2	06.0	07.0	08.3	08.9	79	39	69	62	SE 1	ESE 2	ESE 3	
27	706.4	708.0	709.1	11.6	09.8	07.3	09.0	15.0	07.0	11.5	09.8	08.4	06.7	96	93	87	92	ENE 1	ESE 3	ESE 3	
28	708.8	709.0	708.8	05.5	09.6	06.8	07.2	10.5	05.3	05.8	05.8	05.9	06.4	86	66	87	80	ESE 2	- 0	S 1	
29	708.3	706.7	707.1	04.2	15.4	10.2	10.0	16.5	01.6	01.0	05.7	03.8	05.7	91	29	61	60	ESE 1	NNW 2	E 2	
30	706.9	705.2	705.0	06.8	21.6	14.2	14.2	21.6	04.5	03.7	05.9	04.9	07.5	79	25	61	55	SE 1	NW 2	W 1	
31	705.9	705.6	706.9	11.2	22.2	14.2	15.5	23.2	08.3	07.5	07.6	07.2	08.9	76	36	73	62	SE 1	WSW 2	E 2	
MES.	VRED.	707.1	706.2	706.8	11.0	19.9	13.7	14.6	21.0	09.2	08.4	07.9	07.5	07.9	80	46	68	65	0.9	1.6	1.6

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1	709.6	710.2	710.5	08.6	09.4	08.8	08.9	14.2	08.3	09.0	06.7	07.3	06.9	80	82	81	81	ESE 1	WSW 1	SSE 2
2	709.5	707.7	707.9	08.8	13.4	08.7	09.9	14.5	07.3	07.3	06.9	06.5	07.4	81	57	88	75	- 0	SE 3	SSW 2
3	706.6	704.5	704.7	08.5	16.8	10.2	11.4	17.0	07.7	07.8	07.7	07.3	05.6	93	51	60	68	- 0	SE 3	ESE 3
4	704.4	703.5	704.2	07.4	16.3	10.2	11.0	17.6	04.9	04.8	06.0	04.4	04.9	77	31	52	53	- 0	N 2	ENE 1
5	704.6	703.6	703.7	07.0	16.9	11.6	11.8	18.4	04.5	04.0	05.2	06.3	06.6	70	44	64	59	- 0	WNW 1	E 1
6	703.0	703.2	705.2	09.6	18.4	15.6	14.8	22.2	06.4	05.4	06.7	06.8	07.3	75	43	55	58	ESE 2	NW 2	- 0
7	706.4	706.6	707.0	13.0	20.8	15.8	16.4	21.4	10.9	08.8	07.6	08.1	06.3	68	44	47	53	SE 1	S 2	SSE 1
8	709.2	708.9	709.9	11.8	24.7	17.6	17.9	25.0	08.4	06.5	07.3	07.2	09.6	70	31	63	55	ESE 1	SSW 1	SW 1
9	710.5	708.6	708.2	14.1	27.6	18.8	19.8	28.0	10.8	06.4	09.1	07.7	09.1	75	28	56	53	SE 1	N 1	E 1
10	707.4	705.7	705.2	15.1	28.4	20.8	21.3	26.5	12.3	11.0	09.3	07.7	10.3	72	26	56	51	SE 1	W 2	ENE 1
11	705.2	704.7	705.6	16.0	29.2	22.0	22.3	29.4	14.0	12.9	10.3	08.8	10.0	76	29	51	52	SE 1	W 2	E 2
12	706.3	704.8	707.2	17.8	28.8	16.8	20.1	28.8	15.4	12.8	11.3	12.2	12.6	74	41	88	68	ESE 2	W 1	SE 2
13	707.2	705.5	705.7	15.3	27.2	20.0	20.6	28.2	13.2	12.5	10.9	11.2	11.8	83	41	67	64	- 0	WSW 2	ESE 1
14	704.3	703.7	703.8	17.2	30.5	20.2	22.0	30.6	14.6	13.7	11.2	10.2	10.7	76	31	38	48	SE 1	S 3	W 1
15	703.5	702.5	702.6	16.2	25.3	18.2	19.5	26.9	12.3	11.0	09.0	08.6	08.4	65	36	54	52	SE 1	WSW 2	- 0
16	702.2	700.3	702.4	14.9	19.2	15.2	16.1	20.7	13.6	11.0	10.8	12.4	10.9	85	74	84	81	SSE 1	W 2	SW 1
17	703.6	704.1	705.3	14.6	19.7	15.8	16.5	20.0	13.6	13.2	10.8	11.5	11.4	87	67	85	80	SW 1	SSW 2	S 2
18	706.2	705.0	705.5	15.4	26.8	20.6	20.9	26.9	14.4	12.9	11.3	09.9	12.0	86	38	66	63	E 1	W 2	- 0
19	706.0	704.8	705.1	17.2	28.0	20.8	21.7	28.2	13.8	12.5	11.2	09.4	09.4	76	33	51	53	SE 1	W 3	SSW 1
20	705.3	703.6	706.3	16.7	25.8	20.0	20.6	27.8	14.0	12.7	10.7	10.4	09.9	75	42	57	58	ESE 1	WNW 1	- 0
21	707.1	705.8	705.1	14.5	26.2	18.4	19.4	27.0	12.2	11.0	09.6	08.3	10.2	77	33	64	58	- 0	NW 2	ESE 1
22	704.7	703.3	704.4	15.8	20.0	13.9	15.9	23.5	13.8	13.5	10.6	11.2	10.5	79	64	88	77	-		

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Inzidični broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	08	03○	01	04.0	11.4	.	.	.	
2	8	04○	09	00	04.3	08.3	.	.	.	$\square 0-9, 11-24, \bullet 16^{\circ} 17^{\circ}$
3	8	03○	06○	06	05.0	12.1	00.0	.	.	$\square 0-8, 20^{\circ} 24$
4	8	06○	08	08	07.3	10.0	.	.	.	$\square 0-8$
5	8	09	10○	08	09.0	00.8	00.0	.	.	$\bullet 5^{\circ} 2.5^{\circ}, 12^{\circ} 2^{\circ} 17^{\circ} 30$
6	7	10○	10○	09	09.7	00.4	03.2	.	.	$\square 0-6^{\circ}, \bullet 6^{\circ} 10^{\circ}, = 7^{\circ} 13^{\circ}, \square 12^{\circ} 13$
7	8	09	08○	09	08.7	07.1	08.9	.	.	$\bullet 2^{\circ} 3^{\circ} 22$
8	8	09	10	09	09.3	04.4	00.0	.	.	$\square 2-8, \bullet 10^{\circ} 12^{\circ} 13^{\circ} 10^{\circ}, \square 14^{\circ} 15^{\circ}, = 15-20$
9	7	08○	09○	10○	09.0	05.1	02.4	.	.	$= 0-8, \bullet 12^{\circ} 13^{\circ} 13^{\circ} 10^{\circ}, 16-24$
10	7	10○	10	10	10.0	00.4	13.2	.	.	$\bullet 0-13^{\circ}, 16^{\circ} 17^{\circ} 17^{\circ}, = 2-12$
11	7	10	08	00	06.0	04.8	04.2	.	.	$= 6-11, \bullet 15^{\circ} 16^{\circ}, \square 20-24$
12	8	00○	04○	00	01.3	13.2	00.0	.	.	$\square 0-9, = 5-8^{\circ}$
13	8	03○	05○	01	03.0	12.7	.	.	.	$\square 0-8$
14	8	10	09	10○	09.7	00.6	.	.	.	$\bullet 15^{\circ} 16^{\circ} 20^{\circ} 21^{\circ}, \square 12^{\circ} 14^{\circ}$
15	8	10	08○	07	08.3	04.0	00.1	.	.	$\square 22-24$
16	8	09	08	01	06.0	04.6	.	.	.	$\square 0-8^{\circ}, 23-24, \bullet 14^{\circ} 16^{\circ}$
17	8	06○	10	05	07.0	04.3	02.6	.	.	$\square 0-8$
18	7	10	08○	00	06.0	02.1	.	.	.	$\square 0-8$
19	7	10=	10	10	10.0	05.4	.	.	.	$\square 0-9, 22-24, = 6^{\circ} 10^{\circ}, \square 12^{\circ} 13^{\circ}$
20	8	09	10	06	08.3	00.4	.	.	.	$\square 0-8, \square 10^{\circ} 11^{\circ}, \square 14^{\circ} 15^{\circ}, 16^{\circ} 17^{\circ}$
21	8	10	08	05	07.7	03.5	.	.	.	$\square 3-8$
22	8	04○	05○	04	04.3	11.3	.	.	.	$\square 3-7^{\circ}, \square 13^{\circ} 14^{\circ}, 17^{\circ} 18^{\circ}, \square 17^{\circ} 18^{\circ}, \bullet 17^{\circ} 18^{\circ}$
23	7	10	08○	07	08.3	07.3	.	.	.	$\bullet 0-2, 4^{\circ} 5^{\circ}, = 6-10^{\circ}$
24	7	10○	07	08	08.3	03.1	00.5	.	.	
25	8	00○	01○	00	00.3	12.6	00.0	.	.	$\square 0-8$
MES.	VRED.	06.7	07.7	05.4	06.6	191.0	55.7			

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1	6	10	10○	10	10.0	00.3	00.4	.	.	$\bullet 0^{\circ} 1, 10^{\circ} 16^{\circ}, = 7^{\circ} 18$
2	8	09	10	10○	09.7	00.0	00.1	.	.	$\bullet 16^{\circ} 24$
3	8	10	09	04	07.6	01.7	02.3	.	.	$\bullet 0-3^{\circ}$
4	8	08	08	07	07.7	10.2	.	.	.	$\square 0-7^{\circ}, 22-24$
5	7	08	08○	02	06.0	08.1	.	.	.	$\square 0-8^{\circ}$
6	8	01○	08	10	06.3	08.9	.	.	.	$\square 13^{\circ} 13^{\circ}, \bullet 13^{\circ} 15^{\circ}$
7	8	10	08	00	06.0	03.4	00.0	.	.	$\square 0-7^{\circ}, \square 14^{\circ} 17^{\circ}, \bullet 14^{\circ} 17^{\circ}, \square 16^{\circ} 17^{\circ}, \square 18^{\circ} 22$
8	8	00○	04○	00	01.3	12.9	.	.	.	$\square 0-8$
9	8	01○	05○	00	02.0	13.1	.	.	.	$\square 20^{\circ} 24$
10	8	00○	02○	00	00.7	13.9	.	.	.	$\square 0-7^{\circ}, 24-24$
11	8	00○	01○	02	01.0	13.4	.	.	.	$\square 0-8, 21^{\circ} 24$
12	8	00○	08	02	03.3	09.1	.	.	.	$\square 0-7^{\circ}, \square 14^{\circ} 17^{\circ}, \bullet 14^{\circ} 17^{\circ}, \square 16^{\circ} 17^{\circ}, \square 18^{\circ} 22$
13	7	01○	09	00	03.3	08.5	02.4	.	.	$\square 0-8^{\circ}, = 6-11$
14	8	01○	06○	01	02.7	11.8	.	.	.	$\square 0-7$
15	8	00○	06○	00	02.0	11.7	.	.	.	$\square 0^{\circ} 7$
16	7	09	09	10	09.3	01.6	00.3	.	.	$\bullet 14^{\circ} 14^{\circ}, 13^{\circ} 13^{\circ}, 16^{\circ} 17^{\circ}, \square 13^{\circ} 13^{\circ}, \triangle 13^{\circ} 13^{\circ}, \triangle 13^{\circ} 13^{\circ}$
17	7	10	10	05	08.3	00.3	02.6	.	.	$= 6-8^{\circ}$
18	7	05○	02○	04	03.7	11.0	.	.	.	
19	8	00○	05○	01	02.0	10.5	.	.	.	
20	8	05○	08○	08	07.0	10.0	00.0	.	.	$\square 0^{\circ} 7, \square 12^{\circ} 12^{\circ}, \square 12^{\circ} 12^{\circ}, \square 12^{\circ} 12^{\circ}$
21	8	00○	10	05	05.0	08.5	00.0	.	.	$\square 0-7^{\circ}, \bullet 16^{\circ} 16^{\circ}$
22	8	04○	07	04	05.0	06.3	00.1	.	.	$\bullet 16^{\circ} 16^{\circ}, \square 12^{\circ} 12^{\circ}, \square 13^{\circ} 13^{\circ}, \square 16^{\circ} 17^{\circ}, \square 18^{\circ} 18^{\circ}, \triangle 16^{\circ} 17^{\circ}, \triangle 16^{\circ} 17^{\circ}$
23	8	09○	09	09	09.0	03.1	23.4	.	.	$\square 0^{\circ} 9, \square 14^{\circ} 14^{\circ}, 6^{\circ} 7^{\circ}, 15-16^{\circ}$
24	7	09	10○	10	09.7	04.7	00.4	.	.	$\square 12^{\circ} 14^{\circ}, \square 13^{\circ} 13^{\circ}$
25	7	10	09	04	07.7	02.4	02.6	.	.	$= 3-11, \square 14^{\circ} 16^{\circ}, \bullet 14^{\circ} 16^{\circ}, \square 14^{\circ} 16^{\circ}$
26	8	08	09○	08	08.3	08.5	01.3	.	.	$= 6-8^{\circ}, \bullet 14^{\circ} 14^{\circ}$
27	7	09	10○	10	05.7	01.3	01.5	.	.	$\bullet 14^{\circ} 14^{\circ}, \square 14^{\circ} 14^{\circ}, 15^{\circ} 16^{\circ}$
28	8	08	08	00	05.3	09.6	15.8	.	.	$\bullet 14^{\circ} 14^{\circ}, \square 22-24$
29	8	00○	03○	00	01.0	13.9	.	.	.	$\square 0-7^{\circ}, \square 22-24$
30	7	01○	10○	10	07.0	04.1	.	.	.	$\square 0-8, \bullet 9^{\circ} 16^{\circ}, \square 11^{\circ} 24$
MES.	VRED.	04.9	07.4	04.5	05.6	222.8	59.2			

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 $\varphi = 43^{\circ}52'$  N  $\lambda = 18^{\circ}26'$  E Gr.  $\Delta G = +1\text{h }14\text{ min.}$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C						Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	709.5	710.3	711.5	13.4	17.0	13.8	14.5	17.1	12.4	10.6	10.6	10.0	09.7	92	69	82	81	-	0	W	2	- 0
2	711.4	711.0	711.3	13.6	20.0	15.7	16.3	22.1	12.9	13.5	10.7	09.2	09.7	92	52	73	72	-	0	WSW	2	ENE 2
3	711.4	710.0	708.2	12.0	25.5	18.8	18.8	26.2	10.8	10.3	09.0	11.1	11.0	86	45	68	66	-	0	W	2	S 1
4	706.6	704.1	704.5	14.8	30.0	21.4	21.9	30.0	12.6	10.4	10.1	09.8	12.5	80	31	65	59	SE 2	2	W	1	ESE 3
5	703.3	701.3	703.3	17.7	27.1	14.8	18.6	27.6	14.6	14.7	12.3	10.0	12.1	81	37	96	71	ESE 1	WWN	2	E	2
6	703.2	703.3	705.5	14.2	22.3	15.6	16.9	22.7	13.7	14.0	11.6	10.9	08.1	96	54	61	70	-	0	WSW	2	ENE 1
7	706.5	704.9	705.7	12.0	27.8	19.8	19.9	27.8	9.8	9.0	08.7	08.1	10.4	83	29	60	57	ESE 1	SW 2	-	0	
8	706.2	703.9	703.9	16.5	29.6	24.0	23.5	29.6	13.2	12.2	10.3	09.7	08.8	73	31	39	48	W 1	S 3	SW 1		
9	703.1	703.6	705.9	23.6	29.6	21.6	24.1	29.6	21.6	18.0	08.0	09.6	09.7	37	31	50	39	W 2	W 3	-	0	
10	706.6	705.3	707.0	17.2	26.0	16.2	18.9	27.0	16.0	14.5	11.2	11.2	13.0	76	44	94	71	SE 1	NW 1	-	0	
11	707.3	707.3	708.0	14.8	20.2	16.6	17.1	21.5	14.0	14.5	11.9	10.0	07.8	94	56	55	68	SW 1	W	2	- 0	
12	707.5	706.9	708.0	13.2	22.6	16.8	17.4	23.2	12.0	11.4	10.0	10.4	09.4	87	51	66	68	-	0	NNW	2	E 1
13	709.2	708.5	707.3	13.1	25.6	17.8	18.6	26.0	10.5	10.2	09.3	08.1	09.8	82	33	64	60	ESE 1	NW 2	ESE 1		
14	707.0	705.5	705.7	14.6	29.6	22.4	22.3	29.6	12.1	11.2	09.1	10.3	08.0	73	33	40	49	SE 1	W 3	W 1		
15	704.1	703.9	705.9	21.8	27.2	16.0	21.3	27.2	18.0	15.4	08.7	11.6	11.4	44	43	74	54	S 1	SW 1	ESE 2		
16	711.9	709.9	708.6	14.4	24.2	19.0	19.2	25.5	13.6	13.8	09.9	09.1	11.6	80	40	70	63	SSW 1	NW 1	ESE 1		
17	706.9	706.0	707.9	16.4	22.8	16.2	17.9	24.0	15.2	14.0	11.9	12.7	13.1	85	61	95	80	NW 1	SE 1	- 0		
18	708.2	706.0	705.0	15.0	27.0	21.0	21.0	27.4	14.5	14.0	12.2	10.8	10.8	95	40	58	64	-	0	NW 1	S 1	
19	705.4	704.6	706.5	15.4	27.2	20.1	20.7	27.6	13.4	11.6	10.3	10.0	12.5	79	37	71	62	ESE 2	NW 2	ESE 2		
20	707.2	705.4	705.4	19.0	28.0	20.8	22.2	28.0	17.4	16.5	12.6	10.8	12.2	77	38	66	60	ESE 2	-	0	ESE 2	
21	705.4	704.0	706.9	16.4	20.2	18.6	21.0	20.2	13.2	13.0	11.4	11.2	14.5	81	35	90	69	SE 2	SW 2	SW 1		
22	706.4	706.2	707.0	15.0	15.0	12.0	13.5	18.6	11.8	15.5	11.4	11.3	10.1	89	88	96	91	W 1	S 1	ESE 3		
23	706.8	708.6	709.1	12.0	12.2	12.5	12.3	13.4	11.8	11.9	10.1	10.0	10.1	96	93	92	94	N 1	WSW 2	WSW 1		
24	709.1	706.6	705.0	11.4	23.6	16.8	17.2	24.0	10.2	12.0	09.7	10.1	10.7	96	46	74	72	SSE 1	SW 2	ESE 2		
25	703.2	700.0	700.4	14.0	28.6	21.4	21.4	28.6	11.4	11.0	10.3	09.8	07.6	86	33	40	53	E 1	SW 1	NW 1		
MES.	VRED.	706.5	705.5	706.2	15.4	25.0	18.2	19.2	25.7	13.5	12.9	10.4	10.2	10.7	81	45	70	65	0.9	1.7	1.3	

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1	699.3	701.5	704.3	15.2	18.4	14.6	15.7	22.8	14.3	13.5	11.9	10.0	09.3	92	63	75	77	NE 1	WW 2	- 0	
2	704.3	703.8	705.4	13.1	19.4	14.4	15.3	21.0	12.7	12.4	09.9	08.5	09.2	87	50	74	70	-	0	NW 1	ESE 2
3	706.0	706.1	706.8	10.2	24.0	16.0	16.6	24.1	09.0	08.7	08.4	08.6	09.6	90	38	70	66	-	0	W	2 ESE 2
4	709.7	709.7	710.4	12.8	26.9	16.8	19.3	27.0	10.8	10.8	09.2	07.6	09.7	83	29	60	57	SE 1	WSW 2	ESE 2	
5	710.3	708.0	707.3	14.8	27.8	20.4	20.9	27.9	13.0	13.4	10.1	09.6	12.4	80	34	69	61	-	0	NW 2	- 0
6	707.3	707.1	707.6	17.2	21.0	17.2	18.2	22.0	16.7	16.6	13.6	13.8	11.8	92	74	80	82	ESE 1	W 1	- 0	
7	707.2	705.6	705.5	15.0	26.0	19.4	19.5	26.2	11.8	11.7	10.6	12.0	12.3	95	48	73	72	E 1	W 1	E 1	
8	705.8	705.5	707.3	14.6	22.4	18.0	18.3	27.8	14.3	13.0	11.2	11.2	12.7	90	55	82	76	-	0	E 3	E 1
9	708.6	707.3	708.5	14.4	29.0	17.6	19.7	29.0	12.5	12.4	10.6	08.8	12.4	86	29	82	66	ESE 1	W 2	N 1	
10	708.6	707.6	708.0	14.7	24.2	18.4	18.9	28.6	12.9	12.3	10.4	10.9	11.5	83	48	72	68	ESE 2	WWN 2	ESE 2	
11	707.1	705.5	706.7	13.2	27.0	15.8	18.0	27.2	12.5	11.2	10.3	09.8	12.7	91	37	94	74	SE 1	W 1	N 1	
12	706.9	706.7	706.7	14.0	22.9	18.4	24.0	13.9	13.6	11.5	13.0	14.7	96	62	93	84	E 2	WSW 2	E 3		
13	706.5	706.8	707.3	14.6	21.0	15.0	16.4	23.8	13.2	12.2	11.2	11.4	11.3	90	61	88	80	ESE 2	NW 1	ESE 1	
14	707.8	706.8	708.7	13.6	18.6	12.8	14.5	25.2	12.0	11.4	10.6	11.9	10.5	91	74	95	87	-	0	N 3	- 0
15	709.2	709.2	710.0	11.4	23.4	15.6	16.5	23.4	10.5	09.9	09.7	08.8	09.8	96	41	74	70	S 1	W 2	E 1	
16	710.0	709.7	709.8	12.2	25.4	17.4	18.1	25.4	10.8	09.8	09.5	11.0	09.9	89	45	66	67	SE 2	W 2	ESE 2	
17	709.2	707.9	708.1	13.0	28.4	19.0	19.9	28.5	11.6	10.3	10.1	08.5	12.2	89	29	74	64	SE 1	WSW 1	ESE 1	
18	707.7	707.6	706.4	15.9	27.8	23.4	22.6	28.0	14.1	13.0	10.8	12.0	09.8	80	43	45	56	ESE 3	S 1	E 1	
19	702.9	703.0	703.2	22.6	23.6	16.0	19.6	24.5	16.0	18.5	09.9	11.4	12.3	48	52	90	63	S 3	S 3	SE 2	
20	703.9	703.6	704.2	13.0	25.6	17.4	18.4	25.6	11.6	10.6	10.5	09.0	09.7	94	36	65	65	ESE 3	W 3	ESE 1	
21	701.2	699.5	696.2	18.2	22.0	14.8	17.5	23.7	14.5	12.2	10.1	10.2	12.0	64	52	95	70	SE 2	S 3	SE 3	
22	696.4	696.0	698.3	20.5	25.4	17.6	20.3	26.0	14.8	13.6	09.0	08.5	08.5	50	35	56	47	W 1	SW 4	- 0	
23	699.7	700.9	701.9	13.0	20.6	14.6	15.7	22.5	11.5	10.0	09.4	09.0	11.2	83	49	90	74	WSW 1	S 2	ESE 2	
24	702.9	704.9	706.4	12.2	10.8	11.2	11.4	14.6	10.5	11.0	10.0	09.1	09.3	93	93	93	93	-	0	W 1	- 0
25	708.1	708.2	709.3	10.0	19.0	11.1	12.8	19.4	09.4	08.0	08.6	06.9	07.5	93	36	76	68	-	0	W 3	SE 2
26	709.5	708.0	709.0	07.6	23.0	14.0	14.7	23.5	06.2	04.8	06.6	09.3	09.3	84	44	78	69	ESE 1	W 1	W 1	
27	710.3	709.8	709.8	09.8	26.4	16.4	17.3	26.5	05.0	07.3	07.9	09.8	10.4	87	38	74	66	ESE 1	W 1	1 S 1	
28	710.0	708.8	709.1	14.4	21.0	20.6	21.7</td														

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vremenska redoslijed O-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Šnežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	06	10	10	08.7	00.7	16.4	.	• 20-540	
2	7	10	09	00	06.3	02.5	00.0	.	• 0-1, = 342-1310	
3	7	010	040	00	01.7	12.7	.	.	△ 0-9, 2492-24	
4	8	000	040	02	02.0	12.0	.	.	△ 0-9, 22-24	
5	8	020	10	080	06.7	07.8	.	.	△ 0-750, □ 15-1520, • 1040-24, □ 16-23	
6	7	100	050	02	05.7	05.3	16.2	.	• 0-7, 8-102-100, = 2-11, △ 21-24	
7	8	000	040	00	01.3	13.7	00.0	.	△ 0-9, 20-24	
8	8	050	060	00	03.7	09.6	.	.	△ 0-750, □ 5-1310	
9	8	000	040	00	01.3	12.4	.	.	△ 0-8, = 3-8	
10	8	000	080	10	06.0	07.7	.	.	△ 0-8, • 10-1920, □ 17-25-1730, ♦ 17-21-1740, □ 17-22-1740	
11	7	10	070	07	08.0	03.6	15.9	.	= 0-120, • 10-2410	
12	8	100	07	01	06.0	05.6	02.7	.	△ 0-650, □ 6-26-610, • 6-107	
13	8	000	010	00	00.3	13.5	00.0	.	△ 0-8, 20-24; = 3-02-8	
14	8	000	040	00	01.3	13.0	.	.	△ 0-750	
15	8	08	050	10	07.7	03.4	.	.	△ 0-6, • 8-10, □ 1115, 2310-2335	
16	8	10	010	00	03.7	11.5	00.2	.	△ 0-730, 20-24	
17	7	09	090	08	08.7	03.5	.	.	△ 0-850, 20-24, □ 4-2445, 8-920, 12-42-430, • 8-900, 12-42-1650	
18	7	070	020	00	03.0	12.0	03.8	.	△ 0-8, = 3-8	
19	8	000	020	05	02.3	13.5	.	.	△ 0-9	
20	7	010	040	00	01.7	11.2	.	.	△ 3-92-730	
21	8	010	040	09	04.7	10.5	.	.	△ 0-8, • 1645-18, □ 17-1730	
22	6	10	10	100	10.0	00.2	02.8	.	□ 0-130, 1642-1920, • 0-170, 44-45-2220, 95-6, = 12-24, □ 1704	
23	6	100	10	06	08.7	00.0	33.3	.	= 0-1420, 22-24, ♦ 5-92-1130, • 16-2-1510	
24	7	10	040	00	04.7	10.3	01.9	.	= 0-1130, □ 16-2-1510	
25	7	010	030	00	01.3	13.3	.	.	△ 0-8, = 7-1310	
26	8	040	09	100	07.7	06.3	.	.	△ 0-8, • 8-24	
27	7	10	08	10	09.3	03.6	17.4	.	• 0-8, = 9-2-1030	
28	8	000	030	03	02.0	12.1	00.0	.	△ 0-7	
29	8	000	040	00	01.3	12.8	.	.	△ 0-8, 20-204	
30	8	000	030	00	01.0	11.8	.	.	△ 0-7, 20-2024, = 4-20-730	
31	8	010	050	03	03.0	12.8	.	.	△ 0-7, □ 104	
MES. VRED.		04.4	05.5	03.7	04.5	268.9	110.6			

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1	8	09	09	10	09.3	01.6	04.0	.	□ 1056, ♦ 5-92-530, • 14-1510
2	8	050	08	04	05.7	05.8	00.0	.	△ 2-3, 22-24
3	8	000	030	00	01.0	11.4	.	.	△ 0-8, 21-22-24
4	7	000	010	00	00.3	13.0	.	.	△ 0-8
5	8	09	050	07	07.0	05.9	.	.	△ 0-8, • 15-16, 22-24; □ 22-2320, □ 23-24
6	7	10	10	00	06.7	02.4	03.9	.	□ 0-05, • 0-02, 6-2645, 8-92-1030; □ 0-220, □ 21-24
7	7	09	060	00	05.0	06.0	00.3	.	△ 0-8, = 5-1210
8	6	000	08	10	06.0	07.6	.	.	△ 0-8, = 5-261020, □ 12-24-1535, • 13-14
9	7	000	08	00	02.7	09.7	00.0	.	△ 0-8, • 14-1610, □ 14-1615, □ 15-1510
10	7	000	10K	03	04.0	08.4	05.1	.	△ 0-8, 22-24; = 4-20-1330, □ 1330, □ 13-1510
11	8	010	08	04	04.3	08.2	.	.	△ 0-8, • 14-2-1920, □ 15-2-1920, □ 15-2-1920, ♦ 17-2-1810
12	6	10	030	09	07.3	05.6	11.6	.	□ 1056, □ 1056, □ 1056
13	8	08	10	01	06.3	05.6	01.0	.	□ 1056, □ 1056, □ 1056
14	7	030	10K	00	04.3	06.7	00.8	.	□ 0-8, 24-24; = 4-20-820, • 13-1340, 16-20-1710, □ 13-1430
15	7	10	08	04	07.3	10.0	01.7	.	△ 0-9, 20-24; = 0-830
16	6	08	030	00	03.7	12.5	.	.	△ 0-830, = 7-1410
17	8	000	020	00	00.7	12.7	.	.	△ 0-730, 20-2024; = 4-20-8
18	8	020	08	08	06.0	04.5	.	.	△ 0-730
19	7	09	09	08	08.7	02.2	.	.	• 7-20-1330, 10-20-2310; □ 9-13, 14-15, 15-15, □ 18-22-23
20	8	010	010	00	00.7	12.6	14.4	.	.
21	8	10	09	07K	08.7	00.9	.	.	△ 0-8, • 0-830, 16-2330, □ 10-8-1520, □ 16-162-2300
22	6	050	040	03	04.0	12.3	22.3	.	□ 1056, □ 1056, □ 1056
23	8	08	09	10	09.0	02.1	.	.	△ 0-8, = 0-8224-6
24	7	10	100	10	10.0	00.0	22.6	.	• 0-100, 0-100, 20-24; = 0-830
25	8	08	040	00	04.0	10.5	01.9	.	• 0-200, = 6-20-8, □ 19-22-24
26	8	000	000	00	00.0	12.1	.	.	△ 0-830, 20-24; = 5-830
27	8	000	030	00	01.0	11.8	.	.	△ 0-9, 19-22-24
28	8	080	030	03	04.7	08.6	.	.	△ 0-9, 20-24
29	8	000	000	00	00.0	10.8	.	.	△ 0-8, 20-24
30	8	10	040	02	05.3	07.6	.	.	△ 0-830, 20-24; = 6-8, • 14-2-1520, 18-25-1830, □ 15-1510
31	8	10	08	13	09.3	01.3	00.0	.	△ 0-9, 20-24, □ 17-22-20
MES. VRED.		05.3	05.9	03.6	04.9	231.4	89.6		

$\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$  Gr.  $\Delta G = +1h\ 14\ min.$ 

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D 5	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost v %			Pravac i jačina vetra D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
	1	707.0	706.4	707.8	17.2	26.8	18.6	20.3	26.8	17.0	15.5	13.3	11.1	13.8	91	42	86	73	-	0	W	1	ESE 1
2	707.6	706.0	707.6	15.4	21.2	15.4	16.9	25.2	14.2	13.4	12.1	16.2	12.6	92	86	96	91	-	0	-	0	-	0
3	706.2	706.1	707.9	15.8	21.2	14.8	16.7	23.0	14.6	15.0	12.7	12.6	11.6	94	66	92	84	-	0	E	3	WSW	1
4	708.8	708.1	709.1	12.2	22.8	15.4	16.5	24.3	11.4	10.5	09.5	09.1	09.6	89	44	73	69	E	1	ESE	3	-	0
5	710.2	709.4	711.2	13.2	23.3	16.8	17.0	24.5	10.0	09.5	08.9	12.6	11.9	89	59	83	77	ESE	2	W	1	S	1
6	712.8	712.1	713.1	11.8	20.6	15.2	15.7	22.0	10.8	10.2	09.7	11.7	11.2	93	65	86	81	SE	2	NW	1	ESE	1
7	713.1	711.6	712.1	12.4	23.0	16.4	17.1	23.5	11.9	11.2	10.3	11.7	11.5	96	56	82	78	-	0	SW	1	SE	1
8	711.9	709.9	709.0	11.6	24.6	16.6	17.4	25.2	11.2	10.5	09.8	13.9	10.5	96	60	74	77	SE	2	W	1	ESE	2
9	706.6	704.6	711.8	13.4	27.4	11.0	15.7	27.4	10.8	10.5	10.8	09.9	08.7	94	36	89	73	-	0	W	2	W	2
10	712.3	711.6	713.0	07.8	14.6	08.6	09.9	15.6	07.4	07.2	07.5	04.9	06.4	95	40	78	71	-	0	N	2	-	0
11	712.6	712.0	714.2	08.2	19.6	13.8	13.9	20.1	06.7	06.0	06.9	07.4	09.4	84	43	80	69	E	1	WSW	2	-	0
12	714.7	712.8	712.0	09.4	24.6	15.4	16.2	24.6	08.7	07.6	08.3	10.7	10.6	94	46	81	74	SE	2	W	1	ESE	2
13	710.9	708.9	711.5	12.2	26.8	18.2	18.9	27.6	08.6	07.6	09.2	12.5	12.6	86	47	80	71	SE	2	SW	1	SSW	2
14	715.9	716.1	715.2	10.4	11.8	11.0	11.1	18.2	09.6	10.0	08.6	07.4	08.1	91	71	82	81	NNW	1	-	0	-	0
15	713.0	710.4	708.2	10.1	20.3	09.8	12.5	20.6	09.8	10.2	08.5	04.8	06.2	92	27	68	62	-	0	NW	2	ESE	2
16	705.4	703.4	705.1	06.6	22.6	14.6	14.6	22.6	06.0	05.1	06.4	07.5	08.6	88	36	69	64	ESE	2	WNW	2	E	2
17	705.7	705.5	705.1	08.1	07.9	07.8	07.9	14.6	07.6	05.2	07.8	07.6	07.3	96	95	92	94	W	1	NW	2	W	1
18	704.7	704.8	707.1	05.8	09.2	07.4	07.5	09.6	05.6	06.0	06.5	07.8	07.4	95	89	96	93	NW	2	W	1	W	1
19	709.7	710.0	709.5	07.0	10.2	09.2	08.9	11.0	06.1	05.2	07.3	08.0	08.5	97	86	98	94	-	0	WNW	1	-	0
20	704.5	706.2	706.1	16.2	13.0	09.4	12.0	18.0	08.5	08.6	10.0	10.3	08.4	72	92	95	86	SSE	1	-	0	-	0
21	705.3	706.2	707.4	08.4	14.8	11.0	11.3	20.0	08.0	08.3	07.9	09.5	09.2	95	67	93	85	NW	1	SW	3	-	0
22	708.1	706.7	707.0	07.4	18.0	12.6	12.8	19.5	06.7	05.6	07.3	05.9	09.1	95	37	83	72	-	0	WSW	2	-	0
23	706.4	705.9	706.4	09.4	10.0	07.7	08.7	12.6	07.7	09.5	08.3	08.1	07.7	94	88	97	93	NW	2	SE	2	-	0
24	706.3	707.1	708.7	07.2	10.4	08.4	08.6	10.5	06.8	07.1	07.4	08.0	07.9	97	84	95	92	NW	1	-	0	-	0
25	708.9	710.1	711.9	08.0	10.3	09.6	09.4	10.5	07.8	07.7	07.6	08.4	08.1	95	90	91	92	NW	1	-	0	-	0
26	712.7	712.3	713.3	07.3	13.0	08.5	09.3	13.0	07.3	07.5	06.8	07.4	06.5	88	66	78	77	NNE	2	-	0	E	2
27	713.7	713.4	715.5	05.8	11.0	08.4	08.4	11.5	05.2	04.0	06.4	07.0	05.9	93	72	71	79	-	0	SSW	2	ESE	3
28	716.5	715.2	717.9	03.3	13.9	04.4	06.5	14.7	02.6	01.4	05.0	04.8	04.8	87	40	77	68	-	0	ENE	2	SE	1
29	718.3	716.1	716.0	00.4	14.1	04.2	05.7	14.6	-00.2	-01.3	04.6	04.6	04.7	97	38	76	70	-	0	NW	2	ESE	2
30	716.4	714.3	713.3	01.2	17.0	07.2	08.2	17.6	-00.6	-01.5	04.2	03.0	05.3	84	21	70	58	SE	2	W	2	ESE	3
MES.	VRED.	710.2	709.4	710.5	09.4	17.5	11.6	12.5	19.0	08.3	07.8	08.3	08.8	08.8	92	60	84	78	0.9	1.4	1.0		

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1	711.0	707.7	707.1	04.4	22.2	13.4	13.4	23.4	02.8	11.5	05.2	05.5	06.5	83	27	57	56	SE	2	W	4	WSW	2
2	704.3	704.7	704.1	14.6	06.2	05.0	07.7	14.6	05.0	11.2	07.6	06.7	06.4	61	95	97	84	WSW	2	NNW	2	-	0
3	704.5	706.8	710.8	04.0	11.7	04.0	05.9	13.4	03.8	04.0	05.9	06.2	05.2	97	60	85	81	-	0	W	1	E	2
4	713.7	712.4	712.2	00.3	16.1	05.2	06.7	16.5	-00.2	-01.0	04.4	03.6	05.1	95	26	77	66	-	0	-	0	-	0
5	712.2	711.3	711.4	03.4	19.0	08.2	09.7	19.9	01.9	00.6	04.5	06.5	06.9	76	40	84	67	SE	3	WSW	3	-	0
6	710.6	708.5	708.4	04.4	21.4	10.2	11.6	22.0	04.1	03.0	05.6	06.9	07.4	90	36	80	69	ESE	2	WSW	2	ESE	1
7	708.4	706.2	706.7	06.0	25.5	11.5	12.6	22.3	06.0	04.0	06.3	08.6	08.3	89	45	81	72	SE	3	W	1	W	1
8	706.5	704.0	703.6	07.2	23.4	12.1	13.7	23.6	06.2	05.2	06.6	07.2	08.2	87	33	78	66	SE	3	SW	1	SW	1
9	703.0	701.3	703.2	09.4	25.3	14.4	15.9	25.4	09.2	07.7	07.8	09.1	10.0	88	38	81	69	-	0	SW	2	SE	2
10	703.6	703.6	705.2	11.8	16.4	14.2	14.2	16.4	11.4	10.9	10.0	11.9	10.0	97	85	82	88	-	0	-	0	-	0
11	704.4	704.9	706.7	12.2	13.6	11.0	12.0	14.3	11.0	10.6	10.2	12.0	10.6	88	96	92	92	NNE	1	ESE	2	ESE	1
12	707.8	708.8	710.2	10.4	13.0	11.2	11.5	13.6	10.3	10.2	08.9	09.6	09.5	94	85	96	92	-	0	SW	1	-	0
13	711.0	710.6	712.0	10.8	13.8	10.8	11.6	14.0	10.7	10.2	09.4	09.9	08.9	97	84	92	91	-	0	-	0	ESE	2
14	711.6	710.7	710.6	08.6	12.7	11.4	11.0	13.0	08.2	07.0	08.1	08.7	09.2	96	79	91	89	-	0	-	0	-	0
15	710.1	710.0	711.1	10.4	13.9	10.0	11.1	15.0	10.0	09.5	09.0	09.6	07.5	95	81	82	86	-	0	-	0	ESE	2
16	712.0	711.5	712.9	07.6	15.8	07.0	09.4	16.0	07.0	05.9	07.0	05.2	05.8	90	39	77	69	-	0	WSW	2	E	2
17	713.4	712.0	713.5	01.5	14.4	05.8	06.9	14.6	01.5	00.5	04.9	07.1	04.9	95	58	71	75	-	0	WSW	1	ESE	3
18	714.6	713.6	715.0	01.7	17.6	07.4	08.5	17.9	01.5	00.9	04.8	06.3	05.4	94	42	70	69	SE	1	-	0	ESE	3
19	715.2	713.3	714.4	02.4	21.7	08.0	10.0	21.7	02.2	02.0	04.8	05.4	05.1	88	28	64	60	SE	2	WNW	1	ESE	1
20	715.5	713.4	715.3	02.9	19.2	08.8	09.9	19.2	02.7														

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacija broj sjeni	Padavine R mm	Snožni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	7	10	01○	04	05.0	07.5	00.0	•	△ 0-4 <sup>10</sup> , ● 14 <sup>25</sup>		
2	7	08	10○	10●	09.3	03.9	•	•	△ 0-8, ● 12 <sup>55</sup> 13 <sup>45</sup> , 19-24; △ 13 <sup>25</sup> 19		
3	7	10	10○	03	07.7	03.8	34.0	•	● 0-1, 13 <sup>25</sup> 14 <sup>45</sup> ; = 2-B, 13 <sup>45</sup> 15 <sup>30</sup>		
4	8	09	08	00	05.7	07.7	00.0	•	△ 13 <sup>25</sup> 14 <sup>45</sup>		
5	7	01○	05○	08	04.7	08.7	•	•	△ 0-9, △ 15 <sup>25</sup> 15 <sup>35</sup>		
6	7	00○	09	01	03.3	07.4	02.0	•	△ 0-10 <sup>30</sup> , 21-24; ● 12 <sup>55</sup> 16 <sup>30</sup>		
7	7	10	06	00	05.3	04.2	00.2	•	△ 0-0 <sup>30</sup> , 19 <sup>25</sup> 24; ● 0 <sup>25</sup> 1, = 3-13 <sup>45</sup>		
8	8	00○	06	00	02.0	06.9	•	•	△ 0-9, = 4 <sup>25</sup> 12 <sup>30</sup>		
9	8	00○	= 03○	09	04.0	09.8	•	•	△ 0-9, = 6 <sup>25</sup> 9, = 9-11, □ 17 <sup>25</sup> , ● 1710, 18 <sup>40</sup> , 22 <sup>25</sup> 24		
10	7	09	08	00	05.7	03.1	04.3	•	● 0-1, □ 19-24		
11	8	09	00○	07	05.3	06.5	•	•	△ 0-8 <sup>30</sup> , 20-24; = 5-9 <sup>45</sup>		
12	8	00○	01○	00	00.3	10.9	•	•	△ 0-9, 20 <sup>25</sup> 24		
13	8	00○	06○	10●	05.3	10.3	•	•	△ 0-9, ● 15 <sup>25</sup> 16, 18 <sup>25</sup> 21 <sup>45</sup> ; △ 21 <sup>45</sup> 22 <sup>45</sup> , □ 21 <sup>25</sup> 22 <sup>30</sup>		
14	7	10	10	10	10.0	00.0	18.2	•	•		
15	7	08	00○	00	02.7	08.4	•	•	= 6 <sup>25</sup> , □ 20-24		
16	8	00○	05○	10	05.0	09.9	•	•	△ 0-9		
17	6	10●	10●	10	10.0	00.0	00.6	•	● 5 <sup>25</sup> 19 <sup>25</sup> 22 <sup>45</sup> 24; = 6-24		
18	6	10●	10●	10●	10.0	00.0	26.8	•	= 0-24, ● 0-22, □ 18 <sup>25</sup> 20		
19	6	10●*	10●	10●	10.0	00.0	16.0	•	= 0-24, ● 5-6 <sup>25</sup> 17 <sup>25</sup> 18, ● 19 <sup>25</sup> 24		
20	6	10●	10●	10●	10.0	00.0	07.6	•	= 0-24, ● 0-10 <sup>30</sup> , 18 <sup>25</sup> 24; □ 0 <sup>25</sup> 8 <sup>30</sup> , 13 <sup>50</sup> 14 <sup>30</sup> , □ 34 <sup>25</sup> 4 <sup>40</sup>		
21	7	10	09●	10	09.7	03.3	15.3	•	= 0-H, ● 13 <sup>25</sup> 17 <sup>30</sup>		
22	7	10	05○	10●	08.3	05.6	00.4	•	= 2 <sup>25</sup> 4 <sup>30</sup> , ● 13 <sup>25</sup> 24		
23	7	10●	10●	10●	10.0	00.0	06.7	•	● 0-24, = 3-13 <sup>25</sup> , 17 <sup>25</sup> 24		
24	7	10●	10	10	10.0	00.0	04.9	•	= 0-H, 16 <sup>25</sup> 24; ● 0-4 <sup>10</sup> , ● 4 <sup>25</sup> 8 <sup>30</sup> , 18 <sup>25</sup> 20 <sup>30</sup>		
25	6	10	10	10	10.0	00.0	00.9	•	= 0-24, ● 8-9		
26	6	10	09	09	09.3	01.0	00.1	•	= 0-15 <sup>20</sup>		
27	7	09	09	10	09.3	00.2	•	•	△ 2-8, 23-24; = 3-9		
28	7	02○	05○	00	02.3	07.0	•	•	□ 19 <sup>25</sup> , □ 18 <sup>25</sup> 24		
29	7	00○	00○	01	00.3	08.1	•	•	□ 0-7 <sup>30</sup> , = 6-H, □ 7 <sup>25</sup> 10, 18 <sup>45</sup> 24		
30	6	00○	00○	00	00.0	09.2	•	•	□ 0-3 <sup>30</sup> , 18 <sup>25</sup> 24; □ 3 <sup>25</sup> 7 <sup>20</sup> , = 6-19		
MES.	VRED.	06.5	06.5	06.1	06.4	143.8	138.0				

1	7	04○	01○	07	04.0	08.7	•	•	△ 0-8 <sup>30</sup>		
2	7	10	10●	10●	10.0	00.0	00.0	•	● 3 <sup>25</sup> 4 <sup>30</sup> , 8 <sup>25</sup> 24		
3	7	10	05○	00	05.0	03.5	31.0	•	● 0-5, 15 <sup>25</sup> 16; = 5 <sup>25</sup> 21, □ 20 <sup>25</sup> 24		
4	8	05=	01○	00	02.0	07.0	00.0	•	△ 0-3, 20-24; □ 3-7 <sup>20</sup> = 5 <sup>25</sup> 6 <sup>30</sup> , 10 <sup>15</sup> H; = 6 <sup>25</sup> 10 <sup>15</sup>		
5	8	00○	05○	00	01.7	08.4	•	•	△ 0-4, 20-24; □ 4-7 <sup>20</sup>		
6	7	00○	00○	00	00.0	09.2	•	•	△ 0-8 <sup>30</sup> , 18 <sup>25</sup> 24; = 7-10 <sup>20</sup>		
7	7	08	09○	00	05.7	06.6	•	•	△ 0-4, 19-24; = 9-11		
8	8	00○	00○	00	00.0	09.2	•	•	△ 0-8, 19-24		
9	7	09	05○	08	07.3	07.2	•	•	△ 0-9, 21-24		
10	7	10●	10●	10	10.0	00.4	03.6	•	△ 0-9 <sup>35</sup> , ● 0 <sup>25</sup> 19 <sup>20</sup> , = 9-11 <sup>30</sup> , □ 14 <sup>25</sup> 15 <sup>15</sup>		
11	7	10●	10	08	09.3	00.0	27.6	•	● 2 <sup>25</sup> 13 <sup>25</sup> , 18 <sup>25</sup> 24		
12	7	10	10	10	10.0	00.1	15.3	•	● 0-16 <sup>25</sup> , = 9-13 <sup>30</sup> , 17 <sup>25</sup> 24		
13	7	10	10	08	09.3	00.0	02.2	•	= 0-H, □ 10 <sup>25</sup> 24		
14	4	10	10	08	09.3	00.0	•	•	△ 0-9 <sup>25</sup> , = 0-24		
15	6	10	10	06	08.7	00.3	00.0	•	= 0-19, ● 4 <sup>25</sup> 5, □ 20-24		
16	7	01○	03○	00	01.3	06.1	•	•	△ 0-11, 18 <sup>25</sup> 24; = 5-12		
17	7	00○	00○	03	00.0	08.0	•	•	△ 0-5, 18 <sup>25</sup> 24; □ 5-7, = 5-11		
18	6	00	02○	00	00.7	09.4	•	•	△ 0-9, 18 <sup>25</sup> 24; = 7-24		
19	7	00○	00○	00	00.0	09.7	•	•	△ 0-10, 18-24		
20	6	00○	00○	00	00.0	09.6	•	•	△ 0-9, 18-24; = 6 <sup>25</sup> 19		
21	7	04	00○	00	01.3	09.4	•	•	△ 0-9, 18 <sup>25</sup> 24; = 6-9		
22	7	00○	02○	00	00.7	09.5	•	•	△ 0-9 <sup>25</sup> , 18-24; = 7-11		
23	7	00	02○	02	01.3	09.4	•	•	△ 0-10, 18-24		
24	6	03	00○	00	01.0	09.1	•	•	△ 0-9, 18-24; = 7 <sup>25</sup> 14 <sup>30</sup>		
25	7	10	09	10	09.7	01.4	•	•	△ 0-9, = 3-12		
26	6	10	03○	00	04.3	06.6	•	•	△ 0-9, 17 <sup>25</sup> 24; = 0-20		
27	6	00	00○	00	00.0	08.7	•	•	△ 0-10, 18 <sup>25</sup> 24; = 7 <sup>25</sup> 24		
28	7	03	00○	00	01.0	08.2	•	•	△ 0-9, 19-24; = 0-5		
29	8	01	01○	00	00.7	08.4	•	•	△ 0-9, 19-24		
30	6	01	05○	04	03.3	06.8	•	•	△ 0-9, 18-24; = 9-16 <sup>30</sup>		
31	6	00	06	00	02.0	03.4	•	•	△ 0-10, 20-24; = 5 <sup>25</sup> 24, ● 17 <sup>25</sup> 18 <sup>45</sup>		
MES.	VRED.	04.5	04.2	02.9	03.9	184.3	79.7				

1977 NOVEMBAR

SARAJEVO

 $\varphi = 43^{\circ}52' N$   $\lambda = 18^{\circ}26' E$  Gr.  $\Delta G = +1h\ 14min.$ 

BR. ST. 140

D B	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost % %				Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	Sred Dnes	7	14	21	Sred Dnes	7	14	21	
1	707.6	705.9	704.9	04.8	11.2	09.6	08.8	11.4	04.8	04.0	06.3	09.1	08.5	97	91	95	94	SE	1	WSW	1	ESE 2
2	706.0	706.4	708.0	07.7	07.8	07.2	07.5	09.9	07.2	08.0	07.5	07.1	06.8	95	90	92	92	W	1	WSW	2	- 0
3	707.8	707.0	708.0	04.0	14.0	08.0	08.5	14.2	03.8	03.8	05.7	06.7	06.8	94	56	85	78	ESE 2	2	SW	1	ESE 3
4	708.0	707.6	709.3	04.4	19.9	10.6	11.4	20.0	04.4	03.7	05.9	06.9	06.9	94	40	72	69	SE	1	W	2	ESE 2
5	709.5	709.7	710.4	07.8	17.4	10.8	11.7	19.0	07.7	05.5	07.2	08.9	08.0	91	60	82	78	ESE 1	1	WNW	1	SE 2
6	710.8	709.5	710.8	07.6	17.2	11.0	11.7	17.5	07.6	06.0	07.0	09.2	09.0	90	63	91	81	SSE 2	2	WSW	1	- 0
7	712.0	712.1	713.7	07.0	17.2	10.0	11.1	17.3	06.7	05.5	06.9	08.5	07.7	92	58	84	78	ESE 1	-	0	ESE 2	
8	714.5	713.9	715.4	05.8	15.4	07.6	09.1	15.7	05.8	04.5	06.5	07.9	06.8	95	60	87	81	ESE 2	2	SE	1	ESE 3
9	715.8	715.9	714.6	05.6	10.0	05.0	06.4	10.4	04.1	03.0	06.1	07.3	06.2	83	79	94	87	ESE 2	2	W	1	ESE 2
10	713.6	712.8	714.9	02.3	09.2	07.6	06.7	09.4	02.1	01.0	05.2	06.5	07.2	95	74	92	87	ESE 1	-	0	WSW 1	
11	715.7	714.2	714.2	04.0	18.2	10.0	10.6	18.2	02.8	02.2	05.7	06.7	06.1	94	43	66	68	SW	1	SW	1	ESE 3
12	712.4	708.6	706.4	04.6	22.7	15.2	14.4	22.7	04.6	03.1	05.5	06.0	04.7	86	29	36	50	ESE 3	2	W	2	WNW 1
13	703.2	701.2	697.5	13.2	15.6	14.2	14.3	16.0	13.2	11.4	05.8	06.9	07.3	51	52	60	54	WNW 1	1	SW	3	
14	699.5	700.1	699.0	02.2	01.8	01.2	01.6	14.6	00.9	02.1	05.3	04.9	04.8	98	94	97	96	W	2	WNW	1	SW 1
15	696.0	696.2	696.5	00.2	14.2	11.1	09.2	15.8	00.0	00.0	04.5	05.8	06.2	97	48	63	69	SSW 1	1	SW	3	
16	692.4	690.5	691.3	11.2	09.0	04.8	07.5	15.5	04.8	08.6	06.6	07.6	06.1	66	88	94	83	SE	2	NW	2	- 0
17	695.1	696.4	695.0	00.6	05.0	04.8	03.8	06.5	00.4	00.3	04.0	04.9	05.5	97	75	85	86	WNW 1	1	SE	1	
18	697.9	700.3	703.0	03.4	04.2	01.9	02.4	05.7	01.0	01.7	05.3	05.5	04.3	91	89	87	89	WSW 1	1	ESE 2		
19	704.1	706.8	708.8	00.4	01.2	-00.9	-00.1	01.6	-01.0	00.4	04.4	04.8	03.6	93	95	84	91	NW 2	2	NW	1	- 0
20	708.9	706.0	705.5	-03.9	03.1	-02.5	-01.5	03.5	-04.1	-05.4	02.8	03.6	03.3	83	63	86	77	ESE 2	2	SW	2	ESE 2
21	704.2	702.2	700.5	-05.4	02.0	07.4	02.9	07.5	-05.5	-06.6	02.8	03.7	04.1	93	69	53	72	SE	2	-	0	NW 4
22	697.4	697.1	700.4	13.2	14.0	09.4	11.5	14.9	05.6	03.5	07.1	08.4	08.2	62	70	93	75	SSW 4	2	NW	3	WNW 1
23	700.6	705.2	707.9	06.6	00.6	00.5	02.1	09.4	00.4	05.0	06.6	04.6	04.5	95	97	95	96	NNW 2	2	SW	2	- 0
24	709.4	707.3	705.5	-01.6	02.7	-00.8	-00.1	03.9	-01.6	-01.5	03.8	04.3	04.1	92	77	95	88	SE	2	E	2	ESE 2
25	703.1	701.5	698.5	-04.0	00.4	00.4	-00.7	00.5	-04.0	-05.5	02.8	04.2	04.6	82	90	97	90	SE	3	WNW	1	NW 1
26	690.8	689.2	692.0	-00.6	-00.4	-01.0	-00.8	00.5	-01.1	00.0	04.3	04.0	04.0	98	90	93	94	-	0	W	2	W 1
27	694.8	697.0	701.5	-01.6	02.4	-00.5	-00.1	03.2	-01.8	-02.0	03.9	03.6	04.2	96	67	95	86	W	1	W	1	- 0
28	705.8	707.7	708.4	-01.6	04.6	-02.2	-00.4	04.7	-02.4	-02.2	03.9	03.5	03.3	96	55	85	79	-	0	S	2	ESE 1
29	709.2	709.1	708.1	-02.6	00.6	-00.6	-00.8	00.6	-03.4	-04.5	03.6	04.7	03.7	96	87	84	89	-	0	-	0	SE 2
30	705.3	703.2	702.8	-02.3	01.8	01.6	00.7	02.0	-02.6	-04.9	03.6	04.1	03.9	94	78	94	89	-	0	WSW 1	SSE 1	
MES. VRED.	705.1	704.7	705.1	03.1	08.8	05.4	05.6	10.4	02.0	01.7	05.2	01.1	05.7	90	71	84	82	1.5	1.2	1.2	1.5	

1977 DECEMBAR

SARAJEVO

1	702.2	702.1	702.2	01.4	00.6	-00.9	00.1	02.4	-01.0	00.5	04.7	04.3	04.0	94	90	93	92	ENE	3	NW	2	NW 2
2	701.7	703.3	705.3	-03.8	03.2	-03.4	-03.5	-00.9	-04.6	-02.0	03.1	03.1	03.3	90	85	93	89	NW	1	WNW	2	WNW 2
3	708.2	710.5	713.5	-05.4	03.6	-04.2	-04.4	-03.4	-05.4	-05.4	02.8	03.0	03.2	93	85	94	91	NNW	2	WNW	2	SW 1
4	714.8	714.2	714.9	-03.9	02.2	-11.1	-07.1	-00.8	-11.1	-04.9	02.8	02.1	01.7	80	55	84	73	NNW	2	NNE	1	NNE 1
5	712.5	709.0	706.9	-14.2	-04.7	-10.4	-09.9	-9.4	-14.2	-16.6	01.3	02.0	01.9	84	62	90	79	SE	2	-	0	0
6	705.1	701.4	700.5	-13.2	05.9	04.8	00.6	06.0	-13.2	-16.5	01.5	03.9	03.8	88	56	59	68	-	0	S	4	- 0
7	699.4	702.7	706.6	03.3	05.4	02.7	03.5	06.3	02.7	02.2	05.4	05.3	04.7	93	78	85	85	NNW	1	-	0	SE 1
8	707.8	706.8	706.6	00.0	01.6	-00.4	00.2	02.7	-00.5	-02.0	04.1	04.6	04.3	90	90	96	92	ESE	2	-	0	SE 1
9	704.0	702.9	702.1	03.6	06.5	03.6	04.3	08.2	-00.8	-01.0	04.5	05.3	05.4	77	73	91	80	ESE	2	-	0	0
10	702.8	704.8	708.9	01.8	03.0	01.0	01.7	03.6	01.0	01.0	04.9	05.0	04.7	94	88	95	92	NE	1	NNE	1	
11	712.7	714.6	716.7	00.2	01.4	-01.0	-00.1	01.5	-01.1	00.2	04.5	04.4	03.6	97	87	84	89	-	0	-	0	NNE 1
12	717.5	717.2	718.8	-01.9	02.0	-03.8	-01.9	03.5	-04.0	-02.0	03.3	03.6	02.7	82	69	77	76	NNE	1	5	1	ESE 4
13	717.1	716.3	717.0	-07.6	-01.8	-07.2	-06.0	-01.6	-07.6	-08.5	02.2	02.8	02.5	83	70	93	82	-	0	-	0	
14	717.6	716.8	717.4	-06.8	-02.8	-07.8	-06.3	-01.6	-07.8	-06.9	02.5	02.4	02.3	89	64	90	81	SE	1	-	0	
15	716.5	714.5	713.8	-06.4	-03.8	-03.0	-04.1	-03.0	-08.5	-08.6	02.7	03.2	03.4	94	92	93	93	-	0	-	0	
16	718.0	718.8	718.8	-02.3	-01.0	-02.6	-02.1	00.5	-03.5	-04.8	03.3	03.5	03.4	85	82	90	86	ESE	1	W	3	- 0
17	716.6	716.0	717.3	-02.0	-00.2	-05.4	-03.3	00.9	-05.5	-02.0	03.8	02.3	02.4	96	50	78	75	-	0	NE	3	E 2
18	716.4	714.8	714.9	-10.6	-04.0	-08.0	-07.7	-04.0	-11.0	-11.0	01.8	02.5	02.4	90	74	95	86	-	0	-	0	
19	714.0	713.3	714.2	-11.0	-05.0	-08.6	-08.3	-04.5	-11.0	-11.2	01.9	02.4	02.2	96	74	92	87	-	0	-	0	
20	713.9	713.3	714.5	-11.4	-02.4																	

BR. ST. 140

 $H_s = 630 \text{ m}$   $H_b = 637.0 \text{ m}$   $h_t = 2.0 \text{ m}$   $h_r = 1.0 \text{ m}$ 

Den	Vrijeme G. G.	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	6 08	10●	10●	09.3	00.0	00.6	.			= 0-70, 12-24; □ 0-85, = 730 1230, 885 9, ● 1332 24	
2	7 10●	10	10	10.0	00.0	10.5	.			● 0-10, = 0-12	
3	6 08	08○	00	05.3	03.3	00.1	.			□ 0-13, 18-24; = 0-1430	
4	8 05	08○	09	07.3	07.3	.	.			□ 0-10, 21-24	
5	7 08	09	00	05.7	04.2	.	.			□ 0-8, 20-24	
6	8 06	08	00	04.7	05.4	.	.			□ 0-9, 20-24	
7	6 09	02○	00	03.7	04.8	.	.			□ 0-9, 18-24; = 885 1530	
8	6 10	05○	00	05.0	02.5	.	.			□ 0-13, 18-24; = 730 1530	
9	6 10	06○	00	05.3	00.4	.	.			□ 0-8, 18-24; = 685 24	
10	6 10	10	10	10.0	02.3	.	.			= 0-24, □ 0-9, 20-24	
11	6 01	00○	00	00.3	06.3	.	.			□ 0-130, 18-24; = 0-1610 i, = 885 845, = 845 945	
12	7 00	00○	00	00.0	08.5	.	.			□ 0-10, = 8-13, = 23-2330	
13	8 06	10	10●	08.7	00.3	.	.			□ 0-85 50, 105 1905 2145, 0-2045 23	
14	4 10●*	10*	10	10.0	00.0	09.0	.			□ 6 085 10 085 630, □ 6 20705 = 645 930, 1330 24, * 705 1515, = 730 1530, □	
15	8 00	07	01	02.7	05.5	12.6	02			= 0-6, □ 610 730, □ 10 20 1116, 1605, □	
16	7 08	10●	10●	09.3	01.5	00.1	.			□ 24410, 1135 1140; ● 585 60, 11-2110; * 2112 2330	
17	7 10*	10	09●	09.7	01.8	23.7	03			* 0-9, 645, = 5-11, ● 1702 2145, □	
18	7 10	10●	09	09.7	00.0	00.8	.			● 102 1510	
19	6 10*	10*	01	07.0	00.0	04.5	.			= 0-1710, * 140 310, 582 1610; □ 19-24	
20	6 01	04○	01	02.0	07.7	02.1	.			□ 0-10, 18-24; = 0-24	
21	6 04	10	01	05.0	04.2	.	.			= 0-180, 620 17; □ 0-11, □ 1610 2330	
22	6 08	09●	10	09.0	00.5	.	.			□ 0-24, 0-20 12, ● 245 1930	
23	5 10●	10*	10	10.0	05.2	10.7	.			● 585 450, = 6-24, * 1402 1210, * 1210 1610, □	
24	7 09	04○	03	05.3	00.1	23.6	02			= 0-18; □ 18-24, □	
25	6 04	10	10*	08.0	00.0	.	.			□ 0-11, = 730 24, * 19-24, □	
26	5 10*	10	10*	10.0	00.0	33.2	21			* 0-24, = 0-24, □	
27	7 10	09	10*	05.7	01.0	12.0	31			* 0-24, 0-285 1625 24; = 0-1210, 18-24; □	
28	6 10*	04○	10	08.0	05.3	03.4	31			* 0-9, 2112 24; = 0-15, □	
29	6 10*	10	09	09.7	00.0	05.7	37			* 0-730 = 0-24, □	
30	5 09	08	10	09.0	00.7	00.1	31			= 0-24, * 185 230, ● 2112 2330, □	
MES. WRED.		07.5	07.7	05.8	07.0	78.8	162.7				

1	6 10●	10	10	10●	10.0	.	10.6	20		= 0-24, ● 3-8, 1110 520, * 17-24, □	
2	5 10*	10*	10*	10*	10.0	.	16.9	29		= 0-24, * 0-24, □	
3	6 10*	10*	10*	10*	10.0	.	11.7	47		= 0-24, * 0-24, □	
4	7 10	04	00	04.7	03.8	02.1	43			= 0-9, * 0-3, □	
5	6 00	00○	00	00.0	06.5	.	36			= 685 24, □	
6	7 00	03○	05	02.7	03.7	.	36			= 0-1315 i, = 9-11, □ 1312 1910, □	
7	7 08	10	09	09.0	00.1	03.4	18			● 002 500, 12 2430, □	
8	5 06	08	00	04.7	02.0	00.0	13			= 3-24 i, = 0120 2130, □	
9	7 10	10	10	10.0	.	00.8	12			= 0-730, 1610 24, * 3-6, 1415 1620, □	
10	6 10	10	10●	10.0	.	02.4	08			= 0-430, 9-24; ● 192 20, = 410 9, ● 17-24, □	
11	6 10●	10	10	10●	10.0	.	00.8	05		* 0-70, = 0-24, □	
12	7 10	08	08	08.7	03.3	00.0	05			= 0-9, □	
13	6 00	00○	10	03.3	05.0	.	04			= 1312 1810, = 0030 24, □	
14	5 10	00○	00	03.3	04.7	.	04			= 0-230, = 2324, □	
15	5 10	10	10	10●	10.0	.	00.4	03		= 0-24, □ 5227, * 9-13, 20-23, □ 1312 20, □	
16	7 08	10	10	09.3	00.9	02.8	05			= 0-11, 2130 24, □	
17	8 10	02	00	04.0	01.5	.	05			= 0-110, * 955 1320, □	
18	5 00	00○	00	00.0	03.3	00.0	05			= 8-24, □	
19	5 10	00	00	03.3	00.0	.	05			= 0-730, = 730 1030, = 1030 24, □	
20	5 00	05	00	01.7	00.6	.	05			= 0-24, V 0-11, □, = 410 9, ● 17-24, □	
21	5 00	00	00	00.0	.	.	05			= 0-24, V 0-1520, □	
22	3 10	10●	10	10.0	.	.	05			= 0-230, 17-24; V 0-24, = 2321 17, □	
23	5 00	00	00	00.0	00.0	00.0	04			= 0-24, V 0-5, □	
24	5 10	00	00	03.3	00.0	.	04			= 0-430, 820 24, V 0-1120, = 402 24, □	
25	6 10	10●	10	10.0	.	.	04			= 0-24, ● 850 13, □	
26	6 10●	10●	05	08.3	.	16.1	02			= 0-2310 i, = 0320 280, ● 1220 1520 i, * 920 9, □	
27	7 00	04○	01	01.7	06.5	02.7	02			V 0-8, □	
28	8 09	08	09	08.7	00.4	.	02			□ 820 1520, □	
29	4 09	10●	10●	05.7	00.7	.	01			□ 102 1420, ● 1320 24, = 1030 1410, 18-24; = 1110 18	
30	8 10●	10	07	09.0	02.7	19.5	.			● 0-8, = 0-12	
31	7 10*	08	09	09.0	03.0	02.3	01			● 302 4, * 4-415, * 415 9, 2112 2220, = 1032 12, □	
MES. WRED.		07.1	06.1	05.6	06.3	48.8	92.5				

$\varphi = 44^{\circ}48' N$   $\lambda = 20^{\circ}28' E$  Gr.  $\Delta G = +1h\ 22\ min.$

BR. ST. 170

D S	Vazdušni pritisak P mm			Temperatura vazduha T °C						Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	753.9	752.6	752.7	-04.5	04.7	02.6	01.4	04.7	-04.6	-08.4	02.9	02.4	02.2	89	37	40	55	ESE 4	SE 4	SE 4	
2	752.3	753.1	756.0	01.9	05.1	01.9	02.7	05.1	01.2	00.0	03.2	03.7	03.7	61	57	71	63	SE 5	SE 5	SE 4	
3	758.4	759.3	761.2	00.9	04.8	01.3	02.1	05.6	00.9	00.2	03.7	03.8	03.5	76	59	70	68	ESE 5	ESE 4	ESE 5	
4	763.0	764.6	766.4	-00.6	01.9	-01.6	-00.5	02.1	-01.6	-01.5	03.3	02.7	02.4	76	52	59	62	ESE 4	SE 3	SE 4	
5	767.8	767.1	766.6	-03.5	02.7	-03.2	-01.8	02.8	-03.6	-04.8	02.0	02.4	01.8	55	43	49	49	ESE 4	ESE 4	ESE 4	
6	765.4	763.8	763.1	-03.2	02.3	01.8	00.7	02.6	-04.1	-05.4	02.1	03.0	03.0	58	56	58	57	ESE 3	NNW 1	- 0	
7	761.2	760.3	759.4	02.4	02.4	00.5	01.5	02.8	00.3	00.6	03.4	03.5	03.8	62	64	81	69	NNW 1	NNW 2	N 2	
8	757.9	757.2	755.8	-00.4	03.6	-01.3	00.2	04.0	-01.3	-00.6	04.0	03.4	03.5	89	57	83	76	WSW 2	NW 3	WSW 2	
9	754.0	754.2	753.3	-01.8	01.8	-01.8	-00.9	02.4	-02.9	-06.8	03.0	03.2	03.1	74	61	78	71	WSW 3	W 2	SE 2	
10	749.6	747.5	747.8	-01.1	06.0	01.8	02.1	06.4	-01.9	-06.9	03.1	03.4	03.1	74	48	60	61	ESE 3	ESE 4	ESE 4	
11	747.1	745.7	744.8	02.5	07.0	05.7	05.2	07.2	01.6	00.2	03.8	04.8	04.8	70	64	70	68	ESE 3	ESE 4	ESE 3	
12	742.3	740.9	741.2	09.5	14.8	07.8	10.0	15.1	05.6	04.4	05.6	06.1	05.1	62	49	65	59	SE 4	SE 5	ESE 4	
13	738.9	739.2	742.7	05.6	08.7	04.5	05.8	09.2	04.1	01.9	05.4	06.8	05.8	79	80	91	83	- 0	ESE 3	WSW 3	
14	748.6	749.3	749.6	02.2	06.6	02.0	03.2	06.8	01.6	00.3	04.2	04.2	04.3	79	57	82	73	SSW 1	ESE 3	ESE 3	
15	748.4	746.2	745.4	01.9	06.4	02.8	03.5	07.2	01.2	-01.3	04.0	04.3	04.9	76	59	87	74	ESE 4	ESE 4	ESE 6	
16	747.0	748.2	749.4	00.2	00.8	00.3	00.4	02.8	00.2	00.0	04.4	04.4	04.2	95	91	89	92	ESE 3	ESE 2	NW 2	
17	750.0	749.7	750.6	-00.8	-00.3	00.0	-00.3	00.6	-00.8	-00.9	04.0	04.2	04.3	92	93	93	93	N 2	N 2	N 3	
18	751.6	752.7	754.0	-01.9	-01.1	-02.8	-02.2	00.3	-02.8	-02.4	03.8	03.6	03.4	94	86	91	90	NNW 3	NNW 2	SW 1	
19	754.6	753.9	752.0	-06.4	00.0	-03.0	-03.1	00.6	-06.6	-15.6	02.7	03.2	02.2	94	70	59	74	ESE 2	ESE 2	E 3	
20	752.4	751.8	751.7	-05.0	02.0	01.2	-00.2	02.7	-05.6	-09.6	02.2	03.6	03.5	70	68	70	69	SE 2	ESE 2	ESE 1	
21	751.8	751.8	752.5	01.2	04.3	03.5	03.1	04.4	00.3	-00.1	04.5	05.8	05.6	90	93	95	93	NNW 1	SE 1	SW 1	
22	754.3	753.9	753.2	01.6	03.9	05.7	04.2	05.7	01.2	00.6	04.8	05.2	05.1	93	86	74	84	E 1	ESE 3	ESE 3	
23	752.2	751.0	749.4	02.7	08.1	03.3	04.4	08.6	02.7	-01.0	04.4	05.0	04.6	79	62	80	74	ESE 2	ESE 3	ESE 3	
24	746.9	746.1	747.9	04.6	05.9	04.9	05.2	06.5	02.9	01.9	04.8	06.3	06.0	75	90	93	86	ESE 3	SE 3	W 2	
25	750.2	749.7	748.4	03.0	06.1	04.6	04.6	06.9	02.9	02.6	05.5	05.9	05.8	97	84	91	91	SW 1	- 0	ESE 3	
26	746.5	744.9	743.6	03.4	12.1	10.4	09.1	12.1	03.0	-01.2	05.2	05.8	05.8	89	55	61	68	- 0	ESE 3	SSE 2	
27	743.3	742.0	745.8	08.4	09.6	06.8	07.9	10.4	06.7	06.9	07.4	07.9	06.7	90	88	91	90	SE 2	N 2	WSW 2	
28	749.5	749.9	748.6	03.4	11.9	07.8	07.7	12.2	03.2	00.6	05.5	06.8	05.4	94	65	68	76	SSW 2	ESE 2	ESE 3	
29	743.8	740.0	739.0	07.8	12.8	09.2	09.8	13.3	07.1	04.9	05.4	06.8	06.7	68	62	77	69	ESE 3	ESE 4	ESE 3	
30	743.5	745.0	747.6	10.0	14.7	09.4	10.9	16.3	08.8	06.2	05.1	04.9	05.7	56	39	65	53	SSW 2	SW 3	NNE 3	
31	748.9	749.3	747.9	05.3	09.0	07.8	07.5	09.8	03.7	00.3	05.7	06.4	06.3	86	74	80	80	NNE 1	NNE 2	ESE 2	
MES.	VRED.	751.5	751.0	751.2	01.6	05.8	03.0	03.4	06.4	00.8	-01.1	04.2	04.6	04.4	79	66	75	73	2.5	2.8	2.8

## 1977 FEBRUAR

## BEOGRAD

1	743.3	744.1	746.6	07.6	07.1	02.1	04.7	10.6	02.0	00.4	05.7	06.9	05.0	73	91	93	86	ESE 3	NNW 3	W 3
2	747.6	748.3	750.4	00.0	00.1	-06.6	-00.3	02.1	-00.6	-00.1	04.4	04.4	04.1	96	95	93	95	NNW 2	NNW 2	NN 2
3	751.8	752.5	752.5	-01.7	-00.4	-01.5	-01.3	-00.3	-01.8	-01.9	03.7	03.6	03.6	91	80	87	86	NW 3	NNW 2	WSW 2
4	752.9	753.7	754.4	-03.8	00.6	-01.5	-01.6	00.8	-04.6	-05.1	03.1	03.2	03.5	88	67	86	80	WSW 2	WSW 2	SSE 2
5	753.8	753.4	752.7	-01.8	06.0	03.5	02.8	06.7	-02.5	-05.0	03.3	03.7	04.5	83	53	77	71	ESE 2	ESE 2	ESE 3
6	752.1	749.2	748.6	03.1	07.4	03.1	04.2	08.8	02.8	00.2	05.1	05.9	05.5	89	77	95	87	SSW 1	ESE 2	NW 2
7	751.3	752.6	753.0	02.8	08.4	04.6	05.1	09.0	02.2	01.9	05.3	06.3	05.7	95	76	90	87	W 3	NNW 3	ESE 2
8	750.7	747.4	745.3	02.9	16.5	11.3	10.5	16.7	02.9	-01.1	04.8	05.7	05.4	84	41	53	59	ESE 1	S 2	SW 2
9	746.9	747.6	747.6	07.8	09.3	06.4	07.5	11.3	05.9	04.0	07.0	06.3	06.2	88	71	86	82	N 2	SSW 2	ESE 1
10	746.5	745.0	745.8	05.4	17.0	13.9	12.6	17.6	04.8	01.4	06.2	07.7	06.4	93	53	54	67	ESE 3	SSE 2	SSE 3
11	738.1	739.2	741.4	13.3	10.7	08.5	10.3	14.3	08.5	10.6	07.2	08.4	06.1	63	87	73	74	S 3	SW 2	S 3
12	740.0	738.2	740.5	09.6	18.5	12.5	13.3	19.2	08.5	04.0	07.5	07.2	05.7	73	45	52	60	ESE 2	S 3	S 3
13	744.0	747.4	747.6	10.7	14.1	10.8	11.6	15.0	10.4	06.4	04.9	06.4	05.7	50	53	59	54	NN 2	ESE 2	E 2
14	744.5	741.0	740.8	07.0	07.2	05.5	06.3	10.8	05.5	06.4	06.8	06.8	06.5	91	89	96	92	ESE 3	N 3	NNW 2
15	744.3	745.0	745.8	04.1	09.6	07.2	07.0	10.6	03.0	02.6	05.8	06.1	05.9	94	68	78	80	WSW 3	WSW 2	ESE 2
16	746.0	747.0	747.6	03.3	10.9	08.4	07.8	11.7	02.9	-00.4	05.5	05.7	06.1	95	58	74	76	- 0	NNE 2	E 2
17	748.6	750.3	752.6	04.3	05.0	04.1	04.6	08.4	03.2	02.6	05.0	05.7	05.4	81	87	88	85	WSW 2	W 3	WSW 2
18	753.7	753.5	754.5	01.9	11.4	09.2	07.9	12.4	01.9	-02.0	04.9	05.0	04.3	93	50	50	64	ESE 1	W 2	SE 1
19	755.6	753.6	753.2	04.7	15.7	12.2	11.2	16.2	04.2	-00.6	04.7	05.9	06.5	73	44	61	59	SSE 1	SSE 2	SSE 2
20	752.3	750.7	749.3	10.5	18.2	13.1	13.7	18.8	10.4	08.4	05.8	06.7	06.0	61	43	53	52	SSE 3	SSE 3	S 2
21	746.6	744.0	744.1	10.1	17.5	15.4	14.6	19.5	10.1	07.2	05.4	06.9	06.3	58	46	48	51	SE 3	ESE 3	SSE 4
22	748.4	750.2	749.0	10.8	11.2	10.4	10.7	16.0	10.0	10.2	09.1	08.								

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 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vrijnost 0-9	Oblačnost N (0-10)					Imotno broj	Padavina R mm	Snežni pokriven h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	7	03	10	04	05.7	04.7	.	.	01	$\overline{\square}^0 0-730, \overline{\square}^0 5^0-14, \overline{\square}^0 12^0-24 i, \boxed{\square}$	
2	8	09	04○	09	07.3	05.0	.	.	.	$\overline{\square}^0 0-24 i, \overline{\square}^0 10-17, \overline{\square}^0 12^0-24$	
3	8	00	05	07	04.0	01.2	.	.	.	$\overline{\square}^0 0-24 i, \overline{\square}^0 12^0-24$	
4	8	10	09	03	07.3	00.0	00.4	.	.	$\overline{\square}^0 0-24 i, \overline{\square}^0 0-12^0, \overline{\square}^0 0-14^0-5^0 i, \boxed{\square} 400-120$	
5	8	00	03○	01	01.3	07.0	.	.	.	$\overline{\square}^0 0-24 i, \overline{\square}^0 0-14^0 i, \overline{\square}^0 0-16^0 i, \overline{\square}^0 0-24 i$	
6	8	04	09	09	07.3	00.0	.	.	.	$\overline{\square}^0 0-320, \overline{\square}^0 0-22, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
7	7	10	10	10*	10.0	00.3	.	.	01	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
8	7	10	09	00	06.3	01.4	00.6	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
9	7	06	03○	01	03.3	04.8	00.0	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
10	7	00	05○	00	01.7	05.2	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
11	7	02	10	09	07.0	00.2	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
12	8	07	05○	10	07.3	05.5	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
13	7	10	10*	10*	10.0	00.0	01.2	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
14	7	10	00○	00	03.3	06.1	04.0	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
15	8	03	07	10*	06.7	02.8	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
16	5	10*	10*	10	10.0	00.0	10.6	01	.	$\bullet^0 0-320, \overline{\square}^0 1-300, 5^0-6^0, \overline{\square}^0 300, 0-100, \overline{\square}^0 100, 0-1730 i, \boxed{\square}$	
17	5	10*	10*	10*	10.0	00.0	05.7	12	.	$\times^0 200, \boxed{\square}$	
18	6	10	10	04	08.0	02.0	10.0	20	.	$\times^0 0-020, \overline{\square}^0 0-020, \boxed{\square}$	
19	7	00	00○	00	00.0	07.8	.	15	.	$\overline{\square}^0 0-020, \overline{\square}^0 0-020, \overline{\square}^0 13-2330$	
20	7	03	08	10	07.0	03.9	.	12	.	$\overline{\square}^0 0-020, \overline{\square}^0 0-020, \boxed{\square}$	
21	6	10	10*	10*	10.0	00.0	01.2	09	.	$\times^0 0-320, \overline{\square}^0 0-220, \overline{\square}^0 12^0-24, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
22	6	10	10	09	09.7	00.0	04.9	06	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \boxed{\square}$	
23	7	00	03○	03	02.0	06.6	.	01	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
24	7	10	10*	10	10.0	00.0	00.0	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
25	7	10	09	00	06.3	00.3	00.2	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
26	7	06	09	10	08.3	01.0	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
27	7	10*	10*	10	10.0	00.0	03.9	.	.	$\bullet^0 0-160, \boxed{\square}$	
28	7	10	00○	00	03.3	06.6	00.8	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
29	8	09	09○	10*	09.3	00.6	.	.	.	$\overline{\square}^0 0-630, \overline{\square}^0 0-10^0, \overline{\square}^0 18^0-2330 i$	
30	8	03	09	06	06.0	04.6	00.6	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
31	7	06	04○	06	05.3	03.3	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24$	
MES.	VRED.	06.5	07.1	06.2	06.6	80.9	44.1				

1	6	06	10*	10*	08.7	00.0	00.0	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
2	7	10*	10*	10*	10.0	00.0	03.6	01	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
3	6	10*	10	09	09.7	00.0	03.8	05	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
4	6	06	02○	02	03.3	04.5	00.6	02	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
5	7	07	09○	10	08.7	04.5	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
6	6	10	10*	10*	10.0	01.1	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
7	7	10	09	02	07.0	02.6	14.6	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
8	7	03	06○	00	03.0	05.7	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
9	8	10*	09	08	09.0	00.5	04.6	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
10	8	06	00○	10	05.3	05.2	06.3	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
11	7	10	10*	00	06.7	00.0	01.0	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
12	8	10*	05○	03	06.0	03.7	09.7	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
13	8	03	05○	10	06.0	06.6	00.0	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
14	7	10*	10	10*	10.0	00.0	04.3	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
15	7	10*	04○	05	06.3	05.4	26.8	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
16	7	06	05○	00	03.7	05.9	00.1	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
17	6	10	10*	10	10.0	00.0	00.4	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
18	7	00	05○	05	03.3	09.3	00.8	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
19	7	02	03○	09	04.7	03.3	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
20	8	03	05○	00	02.7	06.9	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
21	8	06	09○	08	07.7	01.2	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
22	8	10	10*	10	10.0	00.0	00.0	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
23	8	10	05○	00	05.0	06.1	05.4	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
24	8	08	07○	05	06.7	03.9	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
25	7	09	10	10*	09.7	00.0	.	.	.	$\overline{\square}^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
26	8	10	06○	10*	08.7	02.4	05.1	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
27	7	10*	10	10	10.0	00.8	17.7	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
28	7	09	06○	02	05.7	06.0	00.7	.	.	$\bullet^0 0-220, \overline{\square}^0 0-24^0, \overline{\square}^0 13-24 i, \overline{\square}^0 0-22^0-24, \boxed{\square}$	
MES.	VRED.	07.6	07.1	06.4	07.1	85.6	105.5				

1977 MART

BEOGRAD

 $\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$  Gr.  $\Delta G = + 1h 22 min.$ 

BR. ST. 170

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost U %			Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	758.9	757.3	757.2	-04.2	01.5	02.3	00.5	02.7	-04.2	-05.7	02.9	03.1	03.9	88	61	73	74	WSW 2	WNW 2	NW 3	
2	758.9	758.6	757.1	00.0	04.0	01.2	01.6	04.9	00.0	-00.6	04.2	03.9	03.3	91	65	66	74	NW 3	WSW 3	SSE 2	
3	754.0	752.5	749.7	03.0	05.3	07.2	05.7	07.2	00.5	-03.4	03.3	06.2	07.2	59	93	95	82	WSW 1	W 3	S 2	
4	751.2	751.9	750.0	07.7	11.3	09.7	09.6	11.9	07.0	06.0	07.5	07.1	06.7	95	71	74	80	WSW 4	WSW 3	ESE 2	
5	752.6	755.6	756.8	08.0	11.0	09.0	09.3	11.7	07.6	06.5	06.0	04.2	04.7	75	43	55	58	NW 3	WNW 3	W 2	
6	754.6	754.4	757.0	05.3	14.5	09.6	09.8	15.9	04.4	00.6	04.5	05.2	05.0	68	42	56	55	SE 2	NW 3	NW 2	
7	759.3	761.0	764.2	05.5	12.0	07.6	08.2	12.3	05.2	02.0	04.4	05.0	04.4	65	48	56	56	WNW 2	N 2	NNE 2	
8	766.7	765.7	765.2	02.6	13.6	08.0	08.1	14.4	02.0	-02.4	04.4	04.4	05.1	79	38	64	60	ESE 3	ESE 3	ESE 3	
9	762.6	759.8	757.7	04.5	16.8	11.2	10.9	17.3	03.3	-01.5	05.1	05.5	06.6	81	38	66	62	- 0	SW 2	ENE 1	
10	756.2	755.2	754.5	06.2	16.0	09.4	10.3	16.4	05.3	01.1	05.8	05.2	04.8	81	38	55	58	NW 2	ESE 1	ESE 3	
11	753.2	751.1	750.7	05.3	15.8	09.8	10.2	15.9	05.2	03.0	04.4	04.4	04.3	65	32	48	48	ESE 4	SE 4	ESE 4	
12	750.4	749.5	748.8	07.1	15.8	10.5	11.0	16.6	07.1	05.4	04.2	05.3	06.4	55	40	67	54	ESE 3	ESE 3	ESE 3	
13	746.1	745.2	747.0	09.1	10.6	07.4	08.6	11.1	07.3	08.0	06.8	06.9	06.5	78	71	84	78	ESE 4	ESE 4	SE 3	
14	751.8	753.4	754.9	06.6	10.6	08.0	08.3	12.6	06.5	06.4	06.9	07.0	06.9	95	73	86	85	WNW 3	NW 2	S 1	
15	756.9	758.1	759.0	05.5	11.2	09.0	08.7	13.2	05.1	01.3	05.5	07.0	07.3	82	70	85	79	WSW 2	W 2	W 2	
16	761.3	761.3	760.9	04.0	13.1	08.4	08.5	14.2	03.6	00.0	05.2	05.0	05.5	85	44	67	65	WSW 2	NW 2	S 1	
17	759.0	757.4	756.3	05.8	16.0	09.0	10.0	16.6	04.3	-00.7	05.2	05.1	05.5	75	37	64	59	ESE 2	E 2	ESE 4	
18	756.6	752.6	751.4	05.8	16.0	08.4	09.7	16.6	05.1	03.4	04.7	04.9	04.8	69	36	59	55	ESE 4	ESE 3	ESE 4	
19	749.7	747.8	746.7	06.7	16.8	10.6	11.2	17.6	06.0	04.4	04.4	05.4	05.9	60	37	62	53	ESE 4	ESE 3	ESE 4	
20	747.9	748.5	749.3	09.7	15.7	13.6	13.2	16.2	09.3	08.0	05.9	07.7	07.1	65	58	61	61	ESE 3	SE 4	ESE 3	
21	750.6	751.8	752.7	09.9	15.8	12.3	12.6	16.7	09.6	08.7	07.9	07.9	08.6	87	59	80	75	ESE 3	SE 2	ESE 1	
22	754.0	753.9	753.9	11.6	21.8	17.8	17.3	22.6	09.5	03.3	05.8	06.3	06.6	57	32	43	44	ESE 1	WSW 2	ESE 2	
23	755.5	754.9	754.2	13.1	28.3	18.8	19.8	28.9	11.4	06.0	06.9	05.0	05.9	61	17	37	38	ESE 2	WNW 2	ESE 2	
24	753.8	753.0	752.5	13.0	27.0	20.3	20.2	27.6	12.0	06.0	06.6	06.9	07.1	59	26	40	42	E 1	NNE 2	ESE 3	
25	753.1	752.7	753.1	12.5	22.0	14.4	15.8	22.1	12.5	10.8	06.6	08.0	06.3	61	40	52	51	ESE 5	ESE 4	ESE 4	
MES.	VRED.	753.5	753.1	753.1	07.1	14.7	10.2	10.6	15.7	06.2	03.7	05.7	05.9	06.0	74	50	65	63	2.5	2.6	2.5

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1	754.8	754.4	752.8	03.7	08.4	06.8	06.4	09.0	03.4	03.0	04.5	05.4	06.2	76	66	84	75	ENE 2	WNW 2	ESE 2
2	748.1	746.4	746.4	08.0	13.4	11.3	11.0	13.8	06.4	02.9	07.4	09.1	09.2	92	79	92	88	ESE 3	ESE 2	WSW 1
3	744.5	743.1	742.4	10.2	12.4	12.3	11.8	13.8	09.6	09.5	09.0	09.7	10.1	96	90	94	93	WSW 1	WNW 2	WSW 1
4	746.6	748.8	749.3	10.0	13.0	10.6	11.1	14.7	09.9	09.3	08.8	06.9	08.0	95	62	84	80	WNW 2	W 2	SE 1
5	748.1	745.4	749.1	11.7	19.0	06.4	10.9	21.4	06.4	03.3	08.1	08.1	07.0	79	49	97	75	ESE 2	NW 2	NW 3
6	750.7	749.9	748.1	05.7	12.7	08.1	08.7	13.0	05.6	05.0	06.4	05.1	05.4	93	46	66	68	WSW 3	WSW 2	ESE 3
7	745.9	744.4	743.2	09.3	19.8	15.4	15.0	20.9	05.4	00.0	05.5	05.9	07.2	62	34	55	50	ESE 2	S 1	ESE 3
8	741.1	730.0	737.4	13.9	22.0	18.4	16.2	22.4	12.4	07.1	07.2	08.2	07.9	60	42	59	51	ESE 3	ESF 3	SSE 3
9	735.0	732.3	737.4	16.2	21.3	06.6	12.7	22.8	06.3	12.5	07.4	08.1	06.3	53	43	86	61	SE 3	WNW 3	W 3
10	740.4	740.7	743.5	05.3	09.2	07.1	07.2	09.4	04.8	04.5	05.2	06.2	06.5	77	71	85	78	WNW 2	NNE 2	NNE 3
11	747.5	746.7	747.4	03.1	08.8	05.2	05.6	09.8	02.4	01.8	03.9	03.5	03.1	68	41	47	52	WNW 3	NW 3	NW 3
12	747.6	747.5	747.7	01.1	07.1	05.5	04.8	08.3	00.2	-02.7	04.0	03.8	04.0	60	50	59	63	WSW 3	N 2	WNW 2
13	749.2	748.2	747.4	02.1	09.0	05.2	05.4	09.4	00.0	-03.0	04.6	04.1	05.4	85	47	81	71	W 2	NW 3	WSW 2
14	745.3	744.0	743.4	05.1	10.3	09.0	08.4	12.6	04.2	01.2	05.6	06.8	04.1	84	72	47	68	W 2	WSW 3	NW 2
15	741.5	740.6	740.2	05.2	04.8	04.0	04.5	09.0	03.7	-00.6	06.1	06.0	05.9	91	93	97	94	- 0	ENE 2	NW 3
16	740.5	742.8	746.3	03.4	07.9	04.8	05.2	08.4	02.2	02.1	05.5	04.8	05.7	74	60	88	81	WNW 4	WNW 4	NW 4
17	750.1	750.5	751.4	04.4	11.4	07.2	07.6	12.1	03.9	03.2	04.9	04.4	04.7	78	44	62	61	WNW 3	NW 4	WNW 2
18	751.7	751.4	751.8	05.7	15.7	10.9	10.8	17.2	01.8	-03.7	04.6	03.4	04.9	58	32	50	47	WSW 2	SE 2	SE 2
19	752.8	752.4	752.2	09.2	18.6	14.6	14.3	19.7	04.4	-03.4	04.6	04.7	06.7	53	29	54	45	WSW 1	ENE 2	NNE 2
20	755.2	757.4	756.0	09.3	11.3	07.4	08.9	14.6	07.4	05.8	07.1	07.1	04.0	81	71	52	68	NW 2	WNW 3	N 3
21	758.9	757.7	757.0	03.8	13.4	08.0	08.3	13.7	02.6	-00.1	04.0	04.6	04.9	67	40	61	56	WSW 1	ESE 2	NNE 1
22	756.2	754.0	751.8	07.2	16.8	11.0	11.5	17.4	02.6	-01.2	04.7	04.9	04.2	62	34	43	46	S 1	WSW 2	WSW 1
23	749.3	747.9	746.0	13.2	22.0	17.6	17.6	22.7	09.4	04.9	05.3	06.7	08.6	47	34	57	46	WSW 2	NW 3	ENE 2
24	744.9	744.3	744.4	15.5	20.9	11.7	15.0	21.3	10.8	10.1	07.9	08.3	09.3	60	45	90	65	SSW 2	NNE 2	NNE 3
25	750.4	751.1	752.5	05.6	12.2	09.0	09.0	13.3	04.7	05.4	06.4	05.9	05.2	94	56	61	70	WSW 4	NW 3	WNW 2
26	753.6	752.8	752.4	07.9	15.3	10.2	10.9	16.1	03.6	01.3	05.4	05.6	06.7	67	43	72	61	WN 2	NM 3	SSW 1
27	752.1	750.7	750.0	11.1	20.5	14.8	15.3	22.4	04.4	00.6	06.3									

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$$H_s = 132 \text{ m} \quad H_b = 132.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

BENGRAD

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1	7	10	10	09	09.7	00.0	.	$\Delta^{\pm 1} 20^{\pm 24}$
2	7	100	10	100	10.0	00.0	02.6	$\Delta^{\pm 1} 0-0^{\pm 6}$ , $\bullet^{\pm 1} 045^{\pm 730}, 14^{\pm 5} 1515, \square^{\pm 1} 712, =^{\pm 1} 1702-24$
3	6	100	10	100	10.0	00.0	01.9	$\square^{\pm 1} 0-24, \bullet^{\pm 1} 020^{\pm 240}, 0^{\pm 1} 020^{\pm 1030}, 1214, 2143, 4$
4	7	10	08	06	08.0	02.4	02.1	$=^{\pm 1} 0-6^{\pm 20}, 20^{\pm 24}, \bullet^{\pm 1} 530, \square^{\pm 1} 23^{\pm 24}$
5	7	07	090	100	08.7	04.6	.	$\Delta^{\pm 1} 0-9^{\pm 3}, =^{\pm 1} 0-730, \bullet^{\pm 1} 13^{\pm 24}, \square^{\pm 1} 44^{\pm 1534}, =^{\pm 1} 1446$
6	7	10	060	00	05.3	06.4	06.0	$\square^{\pm 1} 0-0^{\pm 4}, \bullet^{\pm 1} 0-1^{\pm 5}, \Delta^{\pm 1} 19^{\pm 24}$
7	7	020	08	01	03.7	07.5	.	$\square^{\pm 1} 0-10^{\pm 30}$
8	7	10	090	10	05.7	01.8	00.0	$=^{\pm 1} 28^{\pm 1937}, \bullet^{\pm 1} 0-510^{\pm 550}$
9	7	09	09	09	09.0	03.2	.	$\square^{\pm 1} 152^{\pm 2143}, \bullet^{\pm 1} 144^{\pm 1515}, \bullet^{\pm 1} 0-14^{\pm 1515}, i, 18^{\pm 10-20\%}, \checkmark^{\pm 1} 15^{\pm 5} 15^{\pm 5}$
10	7	10	10	100	10.0	01.3	05.5	$\bullet^{\pm 1} 1130-120, \square^{\pm 1} 142^{\pm 1535}, 1355, 21100, 2232, 24$
11	7	060	060	00	04.0	10.0	04.4	.
12	7	03	06	06	05.0	03.6	.	$\bullet^{\pm 1} 0-10^{\pm 6}, \square^{\pm 1} 208^{\pm 219}, 74^{\pm 1} 1933, \times^{\pm 1} 33^{\pm 45}$
13	7	05	07	10	07.3	05.1	.	$\square^{\pm 1} 190, 415^{\pm 2140}, \square^{\pm 1} 0-4^{\pm 6}, \square^{\pm 1} 123^{\pm 18}$
14	7	100	07	06	07.7	01.6	00.3	$\square^{\pm 1} 0-4^{\pm 8}, \square^{\pm 1} 14^{\pm 720}, \square^{\pm 1} 0-4^{\pm 2} 1515, 1635-1715, \square^{\pm 1} 15^{\pm 6}-16^{\pm 5} i$
15	6	10	100	100	10.0	00.0	01.6	$\square^{\pm 1} 0-5^{\pm 12}, \square^{\pm 1} 0-22^{\pm 24}, \square^{\pm 1} 0-3^{\pm 6}, =^{\pm 1} 0-5^{\pm 30}, \bullet^{\pm 1} 0-2^{\pm 24}, \square^{\pm 1} 21^{\pm 2358}$
16	7	100	10	100	10.0	00.0	39.4	.
17	7	090	060	00	05.0	06.0	10.9	.
18	7	000	030	02	01.7	11.8	.	$\bullet^{\pm 1} 0-4^{\pm 10}, \square^{\pm 1} 16^{\pm 25}, \square^{\pm 1} 0^{\pm 15}, 8^{\pm 2} 8^{\pm 10}, \square^{\pm 1} 0-20^{\pm 24}$
19	7	000	050	10	05.0	11.0	.	$\square^{\pm 1} 0-230, 19^{\pm 24}, \square^{\pm 1} 0-22^{\pm 280}$
20	7	06	06	00	04.0	01.1	.	$\square^{\pm 1} 0-3^{\pm 6}, \square^{\pm 1} 10^{\pm 12}, \square^{\pm 1} 1630-1655, \square^{\pm 1} 0-80^{\pm 24}$
21	7	000	030	00	01.0	12.2	00.7	.
22	7	010	020	00	01.0	11.4	.	$\square^{\pm 1} 0-6^{\pm 10}, 20^{\pm 24}, \square^{\pm 1} 6^{\pm 2} 6^{\pm 0}$
23	7	06	080	10	08.0	06.2	.	$\square^{\pm 1} 0-4^{\pm 10}, 20^{\pm 24}, \square^{\pm 1} 4^{\pm 2} 8^{\pm 0}, \square^{\pm 1} 0-10^{\pm 10}$
24	7	10	10	10	10.0	02.1	.	$\square^{\pm 1} 0-7^{\pm 8}, 24^{\pm 24}$
25	7	100	080	03	07.0	06.2	11.0	$\square^{\pm 1} 0-3^{\pm 6}, \square^{\pm 1} 17^{\pm 20}, 19^{\pm 50}, 23^{\pm 24}, \square^{\pm 1} 1700-1954, i$
26	8	040	060	02	04.0	10.4	00.1	$\square^{\pm 1} 0-8^{\pm 10}, 20^{\pm 24}, \square^{\pm 1} 9^{\pm 2} 15$
27	8	000	000	00	00.0	12.5	.	$\square^{\pm 1} 0-8^{\pm 10}, 20^{\pm 24}, \square^{\pm 1} 10^{\pm 20}$
28	7	070	070	04	06.0	06.4	.	$\square^{\pm 1} 0-7^{\pm 4}, \square^{\pm 1} 23^{\pm 24}$
29	7	040	030	02	03.0	12.2	.	$\square^{\pm 1} 0-3^{\pm 4}, \square^{\pm 1} 17^{\pm 20}, \square^{\pm 1} 10^{\pm 20}$
30	8	000	080	04	04.0	10.6	.	$\square^{\pm 1} 0-2^{\pm 4}, \square^{\pm 1} 19^{\pm 25}, \square^{\pm 1} 13^{\pm 20}, \square^{\pm 1} 20^{\pm 2230}$

1977 MAJ

BEOGRAD

 $\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$  Gr.  $\Delta G = + 1h 22 min.$ 

BR. ST. 170

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost U %			Provac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	749.9	749.6	749.6	18.7	27.5	20.9	22.0	27.7	16.9	15.4	09.4	08.4	08.3	58	31	45	45	ESE 4	ESE 4	ESE 3	
2	751.8	752.0	752.2	18.6	26.1	20.5	21.4	26.8	15.7	10.4	08.3	09.8	11.1	52	39	61	51	ESE 2	WSW 2	ESE 2	
3	752.1	751.1	750.2	19.0	28.2	19.6	21.6	28.6	13.7	09.2	10.8	08.5	08.8	65	30	51	49	- 0	ESE 2	ENE 1	
4	749.8	748.9	748.1	19.4	29.5	22.3	23.4	30.1	16.4	10.3	08.2	07.3	07.7	48	24	38	37	ESE 3	ESE 4	ESE 3	
5	749.0	749.3	751.7	22.5	26.3	16.4	20.4	27.8	16.4	16.4	08.1	09.0	12.9	40	35	92	56	ESE 4	ESE 4	ESE 2	
6	752.9	751.5	752.1	12.4	20.8	14.4	15.5	23.0	12.2	11.5	09.1	08.6	11.8	85	47	96	76	ESE 3	ESE 2	SSE 3	
7	750.6	749.4	748.8	13.6	19.5	15.2	15.9	19.9	12.6	10.7	11.1	09.1	09.5	95	54	73	74	WSW 2	NNW 2	SW 2	
8	747.5	746.0	746.2	11.9	16.2	11.7	12.9	17.6	11.2	10.6	08.0	07.5	09.5	77	54	92	74	N 2	NE 2	SSE 1	
9	746.8	747.9	749.3	11.7	14.0	13.3	13.1	17.5	10.4	07.4	09.4	08.2	09.0	91	69	79	80	WSW 2	NW 3	S 2	
10	749.5	749.9	750.1	10.8	11.9	11.2	11.3	15.4	10.7	10.1	09.0	08.8	09.1	93	84	91	89	WSW 2	NW 2	WSW 2	
11	750.9	750.0	750.3	10.8	19.6	12.6	13.9	20.1	09.0	05.0	08.3	07.0	08.6	85	41	78	68	SW 2	NW 3	WSW 1	
12	750.1	748.3	746.5	13.3	21.7	14.5	16.0	22.0	08.7	04.6	08.1	07.0	07.8	71	36	63	57	SE 1	NW 2	ESE 2	
13	745.4	744.3	743.5	15.8	24.9	20.4	20.4	25.9	11.9	07.0	08.0	07.7	09.3	60	33	52	48	ESE 3	SSE 2	ESE 2	
14	752.8	743.3	742.9	18.1	23.1	19.2	19.9	24.2	16.4	10.7	07.6	07.8	08.0	49	37	48	45	SE 3	WSW 2	S 3	
15	743.4	743.1	742.8	14.8	20.8	16.6	17.2	21.9	13.2	11.1	11.0	09.1	09.4	87	49	67	68	SSW 2	S 3	NNE 2	
16	744.2	745.0	746.3	13.2	16.4	15.0	14.9	19.6	12.5	11.7	10.9	11.2	10.7	96	80	84	87	W 2	W 2	NNE 2	
17	749.6	751.0	753.3	16.4	23.7	18.4	19.2	24.2	10.8	07.4	10.8	08.7	11.5	77	40	72	63	SE 2	SW 2	- 0	
18	755.4	754.6	754.3	18.2	24.4	21.3	21.3	24.9	12.9	09.7	11.6	10.3	11.0	74	45	58	59	NNE 1	ENE 3	ENE 2	
19	753.0	751.9	750.9	19.6	27.0	22.6	23.0	27.4	18.6	15.4	12.5	13.3	11.5	73	50	56	60	ESE 3	ESE 4	ESE 4	
20	750.4	749.6	749.0	21.4	29.1	24.4	24.8	29.1	19.8	18.0	12.3	15.8	15.0	65	52	66	61	SE 4	SE 3	SE 3	
21	750.7	749.7	748.7	21.8	28.6	23.4	24.3	29.1	18.8	14.8	13.9	15.5	15.1	71	53	70	65	SE 1	WSW 1	SSW 1	
22	750.1	749.9	751.3	20.8	26.7	19.8	21.8	27.2	19.2	17.3	12.4	09.7	10.8	67	37	62	55	WSW 2	W 2	NW 3	
23	754.4	753.7	754.0	13.3	20.0	15.8	16.2	20.7	11.7	09.6	08.2	08.1	07.7	72	46	57	58	NW 2	WNW 2	NW 3	
24	754.7	754.2	754.1	13.3	19.6	15.1	15.8	20.0	11.8	11.5	08.8	07.2	06.6	77	42	51	57	WSW 2	NW 3	NNE 2	
25	753.2	750.9	749.8	14.8	21.2	15.6	16.8	21.8	08.3	04.7	06.1	06.9	08.6	49	36	65	50	SE 1	NNW 2	WSW 1	
MES.	VRED.	750.1	749.6	749.7	15.5	21.9	16.8	17.8	23.0	12.8	10.0	09.3	08.8	09.5	70	46	66	61	2.1	2.4	2.1

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1	753.5	754.5	754.5	10.2	13.8	10.9	11.5	14.4	10.0	09.9	08.2	07.2	08.0	88	61	82	77	WNW 2	WNW 1	WSW 2
2	754.0	752.3	751.4	11.2	19.5	13.6	14.5	20.6	06.6	03.5	07.6	05.6	08.3	76	33	71	60	SSW 1	ESE 2	SE 3
3	749.2	748.7	749.1	13.2	17.5	12.8	14.1	19.0	10.4	08.1	08.5	06.6	06.4	75	44	58	59	SSE 2	NNW 3	NNE 3
4	748.3	747.1	747.0	10.6	18.2	14.5	14.5	19.0	06.2	02.7	06.9	06.2	05.1	71	40	41	51	W 1	2	NNE 2
5	747.4	746.6	746.0	13.2	19.9	15.3	15.9	20.9	07.3	03.6	06.9	07.4	09.1	61	43	70	58	WSW 2	W 2	WSW 1
6	745.9	745.7	747.1	17.2	24.5	16.7	18.8	25.3	11.0	07.0	07.7	07.4	10.0	52	32	70	51	SSE 1	SSW 2	SSE 1
7	748.5	749.0	749.4	18.8	25.8	21.0	21.7	26.0	14.0	09.5	10.2	08.3	10.1	63	33	54	50	SSE 1	W 3	SE 2
8	751.4	751.0	751.7	19.7	27.6	20.8	22.2	28.4	16.0	12.3	11.2	08.5	09.1	65	31	49	48	SSW 2	WSW 2	SSW 1
9	752.3	751.5	750.0	20.5	29.5	21.7	23.4	30.2	15.4	10.4	11.4	08.4	10.7	63	27	55	48	W 1	NW 2	ESE 2
10	749.4	747.6	747.0	22.8	30.7	23.1	24.9	31.4	16.2	11.6	11.2	08.5	10.5	54	26	50	43	NE 1	NW 2	SSE 1
11	746.7	746.3	746.2	23.8	30.7	24.0	25.6	31.3	17.0	12.5	10.3	11.2	14.0	47	34	62	48	- 0	NNW 2	SSM 1
12	747.1	746.9	747.9	21.6	29.8	24.0	24.9	29.9	17.8	14.3	13.5	12.3	11.0	70	39	49	53	WNW 1	NNW 2	NNW 1
13	748.8	747.7	746.5	21.5	28.9	23.7	24.5	29.8	17.6	14.1	13.3	09.6	12.0	69	32	55	52	WNW 1	N	NNE 1
14	746.0	744.7	743.2	24.6	32.9	27.6	28.2	33.5	18.4	14.3	12.9	11.7	11.9	56	31	43	43	ESE 1	ESE 2	WSW 2
15	745.3	744.4	744.0	22.2	28.4	24.2	24.8	29.7	20.8	18.8	09.2	10.6	10.7	46	36	47	43	WSW 3	WSW 2	N 2
16	744.1	742.7	744.0	20.3	25.5	15.8	19.4	26.8	15.8	17.5	13.2	13.7	12.0	74	56	89	73	W 2	NW 3	WSM 2
17	745.6	746.6	747.3	16.2	22.9	20.4	20.0	23.9	15.6	14.8	12.5	12.7	14.0	90	61	78	76	SSW 2	WNW 2	WSM 1
18	748.7	747.9	747.0	19.5	27.7	22.4	23.0	28.4	17.0	14.1	14.7	13.5	14.0	87	49	69	68	WSM 2	WSW 2	W 1
19	746.5	745.3	745.7	23.3	31.0	24.4	25.8	31.4	18.9	15.6	15.3	11.1	10.8	71	33	47	50	SE 1	WSW 3	- 0
20	746.7	745.9	747.0	22.4	28.7	21.4	23.5	29.4	18.0	14.0	10.4	10.9	13.3	51	37	70	53	WSW 2	NW 2	SM 1
21	749.0	748.5	747.3	19.0	26.6	22.7	22.8	27.3	16.3	13.3	11.6	10.5	11.0	70	40	53	54	W 2	NNW 2	WNW 1
22	747.6	746.5	746.6	18.7	24.6	18.3	20.0	24.8	16.9	13.4	13.3	12.9	12.5	82	56	79	72	WSW 3	NNW 3	NNE 2
23	748.0	748.6	749.7	16.0	21.9	17.3	18.1	22.0	15.4	14.6	12.8	11.2	13.4	94	57	90	80	W 2	NNW 3	SSW 1
24	750.3	749.6	750.8	19.0	24.7	16.4	19.1	25.4	15.5	13.7	12.6	11.8	11.2	76	51	80	69	W 2	W 3	SSW 2
25	751.9	750.4	749.9	18.3	25.8	20.3	21.2	26.8	12.9	10.6	11.0	10.7	13.0	70	43	73	62	- 0	ESE 1	SSE 1
26	749.2	746.5	745.7	19.3	26.6	19.8	21.4	26.6	15.2	12.9	11.4	12.1	10.7	68	46	62	59	E 1	ESE 2	W 2
27	745.5	745.1	747.6	17.0	20.5	16.4	17.6	21.4	15.8	14.4	12.3	12.9	12.9	85	71	92	83	E 2	NW 3	WNW 1
28	750.1	750.2	750.3	15.7	21.6	17.0	17.8	22.6	15.6											

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 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vrhivost 0-9	Oblačnost N (0-10)					Insolacije broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremene w
		14	7	14	21	Sred Dnes				
1	7	10	020	00	04.0	10.5	.	.	.	$\overline{\text{FSE}} 0-19^{\circ}$
2	7	030	030	04	03.3	10.6	.	.	.	$\overline{\text{T}} 24^{\circ}-31^{\circ}, \bullet 0^{\circ} 22^{\circ}-22^{\circ}$
3	8	010	030	00	01.3	11.0	00.0	.	.	.
4	8	000	000	00	00.0	13.0	.	.	.	$\overline{\Delta^{\circ} 2^{\circ}-7^{\circ}}, \overline{\text{FSE}} 0^{\circ}-24^{\circ}$
5	8	070	040	100	07.0	07.4	.	.	.	$\overline{\text{FSE}} 0-17^{\circ}, \overline{\text{R}} 48^{\circ}-20^{\circ}, \nabla^{\circ} 10^{\circ}-10^{\circ}, \bullet 0^{\circ} 18^{\circ}-23^{\circ}$
6	7	100	080	100	09.3	02.9	04.1	.	.	$\bullet 0^{\circ} 35^{\circ}-9^{\circ}, 10^{\circ}-23^{\circ}, \overline{\text{FSE}} 4^{\circ}-6^{\circ}, 17^{\circ}-18^{\circ}, \overline{\text{R}} 0^{\circ}-20^{\circ}$
7	7	100	06	100	08.7	07.1	05.2	.	.	$\bullet 0^{\circ} 6^{\circ}-8^{\circ}, \overline{\text{I}}, 19^{\circ}-24^{\circ}$
8	7	08	050	100	07.7	03.2	00.8	.	.	$\bullet 0^{\circ}-0^{\circ}, 17^{\circ}-22^{\circ}, \nabla^{\circ} 17^{\circ}-18^{\circ}$
9	7	06	09	07	07.3	05.3	05.0	.	.	$\overline{\Delta^{\circ} 0^{\circ}-6^{\circ}}, \overline{\text{R}} 12^{\circ}-14^{\circ}, \bullet 12^{\circ}-13^{\circ}, 21^{\circ}-24^{\circ}$
10	7	100	100	10	10.0	09.7	06.4	.	.	$\bullet 0^{\circ} 0-15^{\circ}$
11	7	000	050	02	02.3	09.9	03.1	.	.	$\overline{\Delta^{\circ} 1^{\circ}-2^{\circ}}, 19^{\circ}-24^{\circ}, \overline{\Delta^{\circ} 4^{\circ}-9^{\circ}}$
12	7	040	040	00	02.7	11.8	.	.	.	$\overline{\Delta^{\circ} 4^{\circ}-9^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
13	8	000	040	09	04.3	10.2	.	.	.	$\overline{\Delta^{\circ} 0-3^{\circ}}, \bullet 21^{\circ}-22^{\circ}, \overline{\text{I}}$
14	8	040	10	05	06.3	06.7	00.0	.	.	.
15	7	100	060	04	06.7	05.4	00.4	.	.	$\bullet 0^{\circ} 35^{\circ}-9^{\circ}, \overline{\text{I}}$
16	7	100	10	10	10.0	03.0	03.7	.	.	$\bullet 0^{\circ} 2^{\circ}-12^{\circ}, 21^{\circ}-23^{\circ}, \overline{\Delta^{\circ} 19^{\circ}-24^{\circ}}$
17	8	030	060	04	04.3	10.1	04.1	.	.	$\overline{\Delta^{\circ} 0^{\circ}-2^{\circ}}, \overline{\Delta^{\circ} 10^{\circ}-24^{\circ}}$
18	7	040	10	09	07.7	05.3	.	.	.	$\overline{\Delta^{\circ} 0-9^{\circ}}, \bullet 0^{\circ} 13^{\circ}-13^{\circ}, 17^{\circ}-17^{\circ}$
19	8	08	060	09	07.7	06.7	00.0	.	.	$\overline{\text{FSE}} 6^{\circ}-24^{\circ}$
20	7	10	10	05	08.3	05.3	.	.	.	$\overline{\Delta^{\circ} 0-16^{\circ}}, 19^{\circ}-24^{\circ}, \overline{\Delta^{\circ} 23^{\circ}-24^{\circ}}$
21	6	09	10	06	08.3	03.1	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 12^{\circ}-15^{\circ}}$
22	7	040	030	10	05.7	11.2	.	.	.	$\overline{\Delta^{\circ} 0-3^{\circ}}, \overline{\Delta^{\circ} 18^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 22-22^{\circ}}$
23	7	080	020	10	06.7	06.9	00.0	.	.	$\bullet 0^{\circ} 23^{\circ}-24^{\circ}, \overline{\text{I}}$
24	8	03	040	03	03.3	11.0	00.2	.	.	$\bullet 0^{\circ}-1^{\circ}, \overline{\Delta^{\circ} 23^{\circ}-24^{\circ}}$
25	8	000	020	00	00.7	12.7	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
26	8	000	01	09	03.3	10.5	.	.	.	$\overline{\Delta^{\circ} 0-9^{\circ}}, \overline{\text{FSE}} 10^{\circ}-14^{\circ}$
27	8	10	10	10	10.0	00.6	.	.	.	$\bullet 0^{\circ} 10^{\circ}-14^{\circ}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
28	7	10	100	05	08.3	02.0	00.0	.	.	$\bullet 0^{\circ} 0^{\circ}-6^{\circ}, \overline{\Delta^{\circ} 10^{\circ}-14^{\circ}}$
29	8	080	07	07	07.3	05.8	00.4	.	.	$\overline{\Delta^{\circ} 18^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 19^{\circ}-19^{\circ}}$
30	8	000	010	00	00.3	13.6	00.0	.	.	$\overline{\Delta^{\circ} 0^{\circ}-2^{\circ}}, \overline{\Delta^{\circ} 10^{\circ}-14^{\circ}}$
31	8	000	050	10	05.0	10.2	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\text{FSE}} 14^{\circ}-14^{\circ}, \overline{\Delta^{\circ} 17^{\circ}-17^{\circ}}, \overline{\Delta^{\circ} 17^{\circ}-17^{\circ}}, \overline{\Delta^{\circ} 17^{\circ}-17^{\circ}}, \overline{\Delta^{\circ} 19^{\circ}-19^{\circ}}$
MES.	VRED.	05.5	05.7	06.1	05.7	233.1	33.4			

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1	7	10	10	05	08.3	00.0	10.1	.	.	$\bullet 0^{\circ} 0^{\circ}-3^{\circ}, \overline{\text{FSE}} 10^{\circ}-14^{\circ}, \overline{\Delta^{\circ} 12^{\circ}-15^{\circ}}, \overline{\Delta^{\circ} 2^{\circ}-20^{\circ}}$
2	7	020	060	07	05.0	09.6	00.4	.	.	$\bullet 0^{\circ} 10^{\circ}-14^{\circ}, \overline{\text{FSE}} 20^{\circ}-24^{\circ}$
3	7	08	080	00	05.3	05.5	.	.	.	$\bullet 0^{\circ} 14^{\circ}-14^{\circ}, \overline{\Delta^{\circ} 13^{\circ}-14^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
4	7	050	030	02	03.3	12.5	00.0	.	.	$\overline{\Delta^{\circ} 0^{\circ}-1^{\circ}}, \overline{\Delta^{\circ} 2^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 22-24^{\circ}}$
5	7	04	060	09	06.3	07.6	.	.	.	$\overline{\Delta^{\circ} 0-8^{\circ}}, \overline{\Delta^{\circ} 19^{\circ}-24^{\circ}}$
6	7	000	040	07	03.7	12.1	.	.	.	$\overline{\Delta^{\circ} 0-8^{\circ}}, \overline{\Delta^{\circ} 10^{\circ}-12^{\circ}}, \overline{\Delta^{\circ} 18^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 18^{\circ}-24^{\circ}}$
7	7	000	040	10	04.7	10.6	.	.	.	$\overline{\Delta^{\circ} 0-8^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
8	8	000	020	00	06.7	13.1	.	.	.	$\overline{\Delta^{\circ} 0-8^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
9	8	000	030	00	01.0	13.9	.	.	.	$\overline{\Delta^{\circ} 0-8^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
10	8	000	010	00	00.3	13.4	.	.	.	$\overline{\Delta^{\circ} 0-8^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
11	7	000	040	00	01.3	11.0	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 24^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 16^{\circ}-16^{\circ}}, \bullet 0^{\circ} 16^{\circ}-16^{\circ}$
12	8	020	050	00	02.3	11.1	00.0	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 24^{\circ}-24^{\circ}}$
13	8	000	010	00	00.3	13.0	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 24^{\circ}-24^{\circ}}$
14	8	000	010	07	02.7	11.1	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-22^{\circ}}$
15	7	050	030	02	03.3	12.0	.	.	.	.
16	8	030	10	09	07.3	05.8	00.2	.	.	$\bullet 0^{\circ} 3^{\circ}-3^{\circ}, 14^{\circ}-16^{\circ}, \overline{\Delta^{\circ} 16^{\circ}-16^{\circ}}, \nabla^{\circ} 0^{\circ}-15^{\circ}-15^{\circ}, \overline{\Delta^{\circ} 15^{\circ}-19^{\circ}}$
17	7	100	08	03	07.0	04.2	05.4	.	.	$\bullet 0^{\circ} 4^{\circ}-9^{\circ}, \overline{\Delta^{\circ} 19^{\circ}-24^{\circ}}$
18	6	07	030	00	03.3	09.1	00.6	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 23^{\circ}-24^{\circ}}$
19	7	010	040	04	03.0	11.4	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 23^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 16^{\circ}-16^{\circ}}, \overline{\Delta^{\circ} 16^{\circ}-16^{\circ}}$
20	8	030	050	00	02.7	11.9	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 23^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 16^{\circ}-16^{\circ}}, \bullet 0^{\circ} 16^{\circ}-16^{\circ}$
21	8	000	060	08	04.7	10.7	00.0	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 12^{\circ}-16^{\circ}}, \bullet 0^{\circ} 23^{\circ}-24^{\circ}$
22	7	100	10	100	08.0	03.8	00.3	.	.	$\bullet 0^{\circ} 0^{\circ}-6^{\circ}, \overline{\Delta^{\circ} 18^{\circ}-24^{\circ}}, \overline{\Delta^{\circ} 6^{\circ}-7^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-20^{\circ}}$
23	7	100	07	10	09.0	02.2	12.5	.	.	$\bullet 0^{\circ} 3^{\circ}-15^{\circ}, \overline{\Delta^{\circ} 15^{\circ}-15^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-20^{\circ}}, \overline{\Delta^{\circ} 0^{\circ}-15^{\circ}-15^{\circ}}$
24	7	010	060	04	03.7	07.2	02.0	.	.	$\bullet 0^{\circ} 16^{\circ}-16^{\circ}, \overline{\Delta^{\circ} 14^{\circ}-14^{\circ}}, \overline{\Delta^{\circ} 16^{\circ}-16^{\circ}}$
25	7	000	060	090	05.0	08.8	00.4	.	.	$\overline{\Delta^{\circ} 0-6^{\circ}}, \overline{\Delta^{\circ} 10^{\circ}-18^{\circ}}, \bullet 0^{\circ} 16^{\circ}-17^{\circ}, \overline{\Delta^{\circ} 16^{\circ}-16^{\circ}}, \overline{\Delta^{\circ} 23^{\circ}-24^{\circ}}$
26	7	000	040	07	03.7	09.7	00.1	.	.	$\bullet 0^{\circ} 0^{\circ}-6^{\circ}, \overline{\Delta^{\circ} 17^{\circ}-17^{\circ}}$
27	7	100	100	10	16.0	00.0	01.0	.	.	$\bullet 0^{\circ} 3^{\circ}-10^{\circ}, \overline{\Delta^{\circ} 5^{\circ}-16^{\circ}}, \overline{\Delta^{\circ} 7^{\circ}-17^{\circ}}, \overline{\Delta^{\circ} 11^{\circ}-11^{\circ}}, \overline{\Delta^{\circ} 13^{\circ}-13^{\circ}}, \overline{\Delta^{\circ} 13^{\circ}-16^{\circ}}$
28	8	08	050	00	04.3	10.0	16.9	.	.	$\overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
29	8	000	040	00	01.3	13.8	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 20^{\circ}-24^{\circ}}$
30	7	050	09	07	07.0	06.3	.	.	.	$\overline{\Delta^{\circ} 0-7^{\circ}}, \overline{\Delta^{\circ} 12^{\circ}-13^{\circ}}, \bullet 0^{\circ} 15^{\circ}-21^{\circ}$
MES.	VRED.	03.5	05.3	04.3	04.4	271.4	49.9			

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 $\varphi = 44^{\circ}48'$  N  $\lambda = 20^{\circ}28'$  E Gr.  $\Delta G = +1h\ 22\ min.$ 

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58	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog paru e mm			Relativna vlažnost % 1			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	751.7	752.5	752.9	17.2	19.4	17.2	17.8	19.7	16.7	16.0	13.2	12.1	12.2	90	71	83	81	WSW 2	WNW 3	W 3			
2	753.0	752.9	752.5	16.6	25.8	21.6	21.4	25.9	15.2	14.3	12.4	12.8	10.2	87	51	52	63	W 2	NW 3	WNW 2			
3	752.7	751.9	750.2	19.1	27.3	21.6	22.4	27.7	16.0	13.4	12.2	10.7	12.5	74	39	65	59	WSW 2	NW 3	WSW 1			
4	748.0	745.8	745.5	22.4	29.6	24.2	25.1	30.7	17.9	16.3	12.8	12.0	12.1	63	38	53	51	SE 1	WNW 3	N 2			
5	745.9	745.4	743.6	18.2	23.6	21.0	21.0	24.6	16.4	13.2	12.3	11.8	14.1	78	54	76	69	WNW 1	WSW 2	WNW 1			
6	745.2	746.1	747.2	16.4	22.0	18.2	18.7	23.0	15.9	16.2	12.8	11.8	10.4	91	59	66	72	NW 3	NW 2	WSM 1			
7	748.0	747.4	746.8	19.2	27.9	23.9	23.7	28.8	13.8	10.7	10.7	10.5	11.7	64	37	52	51	S 1	S 2	S 3			
8	747.2	746.0	744.0	22.2	31.9	26.9	27.0	32.4	17.2	14.5	13.2	13.0	15.2	66	37	57	53	ESE 1	SSN 1	S 3			
9	744.2	744.4	747.0	27.0	32.1	23.3	26.4	32.3	23.3	20.0	9.9	9.8	12.0	12.5	37	33	58	43	SSW 2	WSW 3	NW 2		
10	748.3	748.4	747.6	20.6	25.1	22.9	22.9	25.7	19.3	16.7	13.6	13.7	12.4	75	57	59	64	W 1	NW 3	WNW 3			
11	747.8	747.5	748.0	18.2	21.7	20.7	20.3	22.9	17.2	16.2	13.1	11.5	10.3	84	59	56	66	W 3	W 3	W 3			
12	748.3	748.3	749.4	16.9	25.1	21.6	21.3	26.0	14.2	10.5	10.5	09.1	09.5	73	38	49	53	W 2	NW 3	NNE 2			
13	751.1	750.4	749.2	17.8	26.6	21.1	21.7	27.6	13.5	10.1	10.1	9.9	10.8	66	36	58	53	WSW 2	NNE 2	ESE 2			
14	748.0	747.1	746.0	22.5	31.8	25.2	26.2	32.6	17.3	12.4	11.2	11.0	11.3	55	31	47	44	ESE 2	SW 3	N 2			
15	746.5	745.9	751.0	20.8	26.8	16.4	20.1	27.4	16.3	16.2	14.1	12.9	12.8	76	49	91	72	N 2	WSW 3	W 3			
16	754.7	754.6	752.3	15.9	22.4	19.2	19.2	23.4	15.4	14.8	12.1	9.8	9.0	89	42	54	62	W 2	WSW 1	ESE 2			
17	749.2	749.1	749.4	16.3	23.6	21.3	20.6	25.0	15.5	13.8	10.1	13.1	12.7	73	60	67	67	SE 2	WNW 2	NW 2			
18	751.3	749.7	747.6	18.3	26.6	21.8	22.1	27.5	14.0	11.6	11.9	10.6	11.2	76	41	57	58	WSW 2	NNE 2	ESE 2			
19	746.9	746.8	749.4	20.9	27.6	19.5	21.9	28.4	17.9	15.3	12.6	13.0	12.2	68	47	72	62	ESE 1	WSW 1	NNW 1			
20	750.6	749.5	748.7	18.7	27.4	21.2	22.3	28.4	14.8	12.5	12.2	11.4	13.2	75	42	70	62	- 0	NE 2	ESE 2			
21	747.0	745.8	749.8	21.0	31.8	19.3	22.9	32.2	19.0	16.3	11.7	11.8	15.4	63	33	92	63	ESE 2	WSW 2	W 3			
22	750.6	749.8	749.6	16.1	21.9	16.7	17.9	22.5	15.6	15.4	12.6	11.4	13.6	92	58	95	82	WNW 2	NNE 2	WSW 2			
23	748.6	750.4	750.6	16.0	15.4	16.9	16.3	17.0	15.2	15.4	12.8	12.6	13.2	94	96	91	94	SSW 1	WNW 3	WSW 2			
24	750.7	749.7	747.8	15.5	25.5	19.0	19.8	26.2	13.5	11.2	11.6	10.3	12.7	88	42	77	69	WSW 2	WNW 2	SE 1			
25	745.1	742.3	740.7	20.0	29.4	24.5	24.6	30.2	17.9	14.6	12.5	13.8	14.7	71	45	64	60	SE 3	S 3	SE 3			
26	742.3	741.8	746.0	22.7	30.6	15.4	21.0	31.2	15.3	15.3	12.4	11.3	11.5	60	34	88	61	SE 1	SSE 3	WNW 3			
27	747.6	749.7	750.9	14.4	19.1	15.9	16.3	19.6	14.0	13.5	11.3	11.3	11.9	92	68	88	83	WNW 2	WNW 2	SSW 2			
28	750.1	748.9	749.0	16.8	24.6	19.4	20.1	25.4	12.6	9.6	11.8	11.3	13.2	82	49	78	79	ESE 2	NNE 2	E 1			
29	750.0	749.8	749.5	18.6	27.1	21.5	22.2	27.8	14.8	12.2	12.2	11.8	12.0	76	44	73	64	ESE 1	NNE 2	E 2			
30	749.3	748.3	746.6	20.5	30.0	24.0	24.6	31.0	16.3	13.6	13.2	11.6	15.1	73	36	67	59	ESE 2	E 2	ESE 2			
31	743.0	740.1	741.0	24.4	32.7	25.3	26.9	34.4	22.0	19.1	14.2	16.8	15.4	62	45	64	57	ESE 3	SSE 3	NNW 2			
MES.	RED.			748.5	747.9	748.0	19.1	26.2	20.9	21.8	27.0	16.2	14.2	12.2	11.8	12.5	75	47	68	63	1.8	2.4	2.1

1977 AVGUST

BEOGRAD

1	740.8	742.3	745.9	16.6	20.4	17.2	17.9	25.3	15.6	15.5	13.1	12.6	10.9	92	70	74	79	ESE 2	WSW 3	W 2
2	746.2	746.4	747.5	16.0	17.5	15.7	16.2	20.2	15.2	15.0	09.5	09.7	11.4	70	65	85	73	WSW 3	W 4	WSW 2
3	748.3	748.7	749.5	16.1	23.7	17.8	18.9	24.3	13.2	10.9	10.2	09.5	12.2	74	43	80	66	SW 1	W 2	E 2
4	751.9	752.7	752.6	18.3	26.3	20.0	21.2	26.8	15.4	15.0	11.9	10.5	12.6	76	41	72	63	- 0	WNW 2	ESE 1
5	752.5	751.2	750.0	19.1	28.6	22.7	23.3	28.9	15.2	12.6	12.4	12.1	12.0	75	41	58	58	ESE 1	E 2	ENE 2
6	749.7	748.9	748.7	20.2	27.6	22.7	23.3	28.9	18.7	18.2	15.1	12.3	13.4	85	45	65	65	WNW 1	N 2	NNE 2
7	748.8	748.2	747.8	18.4	27.1	22.1	22.4	28.1	16.8	14.4	13.7	14.0	14.0	86	52	70	69	WSW 1	WNW 2	ESE 2
8	748.4	748.0	748.9	20.4	29.7	23.3	24.2	29.9	16.2	14.6	12.6	13.5	14.2	70	43	66	60	ESE 3	E 3	ESE 2
9	750.3	749.8	750.1	21.3	29.8	23.2	24.4	30.4	19.5	16.0	13.5	13.0	13.6	71	41	64	59	SE 2	SE 2	ESE 1
10	749.9	749.1	748.8	21.8	29.1	22.8	24.1	30.6	18.7	15.3	14.2	14.3	14.7	72	47	71	63	WNW 1	S 1	ESE 1
11	748.9	748.9	748.9	20.9	24.5	19.7	21.2	25.0	19.5	18.0	15.1	15.6	16.0	81	68	93	81	WSW 2	NNE 2	WSW 2
12	749.6	749.5	749.4	17.6	24.0	19.3	20.1	25.6	16.2	14.9	13.4	13.8	14.5	89	62	87	79	WSW 2	NNE 2	ENE 1
13	748.7	747.8	749.3	19.8	29.2	19.6	22.1	29.4	17.2	14.5	14.1	15.2	15.7	82	50	92	75	ESE 3	ESE 2	WSW 1
14	749.5	748.7	749.8	19.0	26.8	17.3	20.1	27.0	16.5	14.0	14.0	13.7	13.7	85	52	92	76	SW 2	NNE 2	WNW 2
15	751.6	750.7	751.4	16.6	23.8	19.8	20.0	24.4	16.0	15.1	12.9	12.6	12.6	91	57	73	74	WSW 3	W 3	W 2
16	752.4	752.3	752.1	16.6	25.1	18.2	19.5	25.1	14.9	12.7	11.9	10.3	12.3	84	43	78	68	WSW 1	NW 3	SSW 1
17	751.6	751.2	750.9	17.0	25.3	19.5	20.3	25.8	14.1	11.0	11.3	11.7	10.5	78	48	62	63	E 1	NNE 2	E 2
18	749.1	748.2	746.7	19.4	28.8	25.4	24.8	29.7	17.5	14.3	11.9	14.8	15.8	71	50	65	62	ESE 3	ESE 3	ESE 3
19	744.5	744.0	745.4	21.4	25.4	16.9	20.2	26.8	16.9	19.6	15.3	15.0	13.5	80	62	93	78	ESE 2	SSE 2	SW 2
20	745.3	745.4	745.4	18.4	26.2	19.6	21.0	26.9	14.6	12.6	13.0	11.4	13.0	82	45	76	68	SW 2	W 2	ESE 2
21	743.5	740.9	740.9	20.4	24.8	18.9	20.8	25.6	18.4	13.9	10.2	12.7	15.0	57	54	92	68	SSE 2	ESE 3	ESE 2
22	738.1	737.1	740.0	19.2	24.8</															

BR. ST. 170

 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vreme Op.	Oblačnost N (0-10)				Insekt. broj sen	Padavine R mm	Snežni pokrivač h cm	Resanj vremena w
		14	7	14	21	Sred Dies			
1	6	09	10	10	09.7	00.0	00.2	.	$\square^o 6^o 2^o 8^o 12^o 24^o ; \bullet^o 8^o 9^o 19^o 5^o 23^o ; \overline{\text{SW}} 12^o 2^o 14^o 2^o$
2	6	09	04	00	04.3	09.1	01.3	.	$\square^o 0^o 1^o 1^o 1^o$
3	8	00	04	00	01.3	12.8	.	.	$\square^o 2^o 8^o 20^o 24^o ; \square^o 5^o 6^o 15^o ; \overline{\text{W}} 11^o 13^o$
4	8	00	06	03	03.0	09.4	.	.	$\square^o 0^o 8^o 20^o 24^o ; \square^o 1^o 1^o 1^o$
5	7	10	07	09	06.7	03.5	00.5	.	$\square^o 0^o 4^o 1^o 4^o 1^o 1^o ; \square^o 1^o 1^o 1^o$
6	7	10	05	02	05.7	04.8	07.4	.	$\bullet^o 0^o 1^o 7^o 1^o 8^o 10^o 1^o 1^o ; \square^o 5^o 10^o ; \bullet^o 6^o 8^o 7^o 1^o$
7	8	00	01	10	03	03.7	12.5	00.3	$\square^o 1^o 0^o 7^o 1^o 20^o 21^o 1^o 1^o$
8	7	00	00	00	00.0	11.6	00.0	.	.
9	7	00	03	04	02.3	10.2	.	.	$\square^o H^o 15^o 16^o 16^o 15^o$
10	8	02	08	10	06.7	07.7	03.4	.	$\square^o 20^o 21^o 22^o 23^o$
11	7	09	07	03	06.3	01.0	00.1	.	$\overline{\text{W}} 7^o 18^o 1^o ; \bullet^o 12^o 12^o$
12	8	01	03	02	02.0	12.7	00.0	.	.
13	8	00	01	00	00.3	13.1	.	.	$\square^o 3^o 2^o 7^o 1^o$
14	8	00	03	10	04.3	12.0	.	.	$\square^o 19^o 20^o 21^o 24^o 1^o 1^o 1^o 1^o$
15	7	09	06	10	08.3	04.0	00.0	.	$\bullet^o 13^o 14^o 15^o 16^o 17^o 18^o 19^o 1^o$
16	7	08	03	00	03.7	11.3	09.4	.	$\square^o 6^o 8^o 10^o 12^o 14^o 16^o 18^o 1^o$
17	7	10	05	03	06.0	06.2	00.5	.	$\square^o 6^o 8^o 10^o 12^o 14^o 16^o 18^o 1^o$
18	7	00	03	00	01.0	12.5	00.9	.	$\square^o 1^o 3^o 5^o 7^o 9^o 11^o 13^o 1^o$
19	7	08	03	00	03.7	07.7	00.0	.	$\square^o 15^o 16^o 17^o 18^o 19^o 1^o 1^o$
20	8	00	00	01	00.3	13.1	08.6	.	$\square^o 22^o 24^o$
21	8	03	10	05	05.3	09.2	00.0	.	$\square^o 0^o 2^o 3^o 5^o 7^o 9^o 11^o 1^o$
22	8	10	09	10	09.7	03.8	10.5	.	$\bullet^o 6^o 11^o 16^o 21^o 1^o 1^o 1^o$
23	5	10	10	10	10.0	00.0	<u>21.8</u>	.	$\bullet^o 6^o 10^o 15^o 17^o 19^o 1^o 1^o$
24	6	00	01	00	00.3	12.0	06.6	.	$\square^o 20^o 22^o 24^o$
25	8	00	03	04	02.3	12.0	.	.	$\square^o 0^o 8^o 10^o 12^o 14^o 16^o 18^o$
26	8	00	05	10	05.0	13.8	.	.	$\square^o 0^o 5^o 7^o 10^o 12^o 14^o 16^o 1^o$
27	7	10	06	00	05.3	02.6	04.3	.	$\bullet^o 0^o 10^o 12^o 14^o 16^o 18^o 20^o 24^o$
28	6	00	04	00	01.3	12.7	06.8	.	$\square^o 1^o 3^o 5^o 7^o 9^o 11^o 13^o 1^o$
29	8	00	03	00	01.0	12.6	.	.	$\square^o 1^o 3^o 5^o 7^o 9^o 11^o 13^o 1^o$
30	8	00	01	03	01.3	12.5	.	.	$\square^o 1^o 3^o 5^o 7^o 9^o 11^o 13^o 1^o$
31	7	08	05	00	04.3	09.8	00.0	.	$\square^o 0^o 6^o 8^o 10^o 12^o 14^o 16^o 1^o$
MES. VRED.		04.1	04.3	04.0	04.1	273.6	82.6		

1	7	09	08	10	09.0	03.7	20.4	.	$\bullet^o 0^o 1^o 8^o 9^o 10^o 11^o 12^o 1^o$
2	7	10	10	10	10.0	00.3	02.6	.	$\bullet^o 8^o 9^o 10^o 11^o 12^o 1^o$
3	8	02	06	00	02.7	07.2	00.0	.	$\square^o 1^o 2^o 24^o$
4	7	00	04	00	01.3	10.4	.	.	$\square^o 0^o 1^o 5^o 10^o 14^o 18^o 22^o 24^o$
5	7	06	06	05	05.7	09.7	.	.	$\square^o 1^o 2^o 8^o 10^o 12^o 14^o 16^o 18^o$
6	8	08	04	00	04.0	09.0	00.3	.	$\square^o 0^o 2^o 3^o 5^o 7^o 9^o 11^o 1^o$
7	7	00	01	00	00.3	11.0	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
8	7	00	00	00	00.0	11.4	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
9	7	00	02	00	00.7	10.6	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
10	8	06	08	03	05.7	09.2	.	.	$\square^o 1^o 2^o 3^o 5^o 7^o 9^o 11^o 1^o$
11	7	06	10	06	07.3	03.5	00.0	.	$\square^o 0^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
12	7	10	06	00	05.3	06.6	17.4	.	$\bullet^o 0^o 1^o 4^o 6^o 8^o 10^o 12^o 1^o$
13	7	05	04	09	06.0	06.3	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
14	7	03	03	10	05.3	08.7	01.4	.	$\bullet^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
15	7	10	06	03	06.3	06.5	01.0	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
16	6	00	01	00	00.3	10.9	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
17	7	00	01	00	00.3	09.4	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
18	7	00	09	04	04.3	07.9	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
19	7	10	09	10	09.7	02.6	00.3	.	$\bullet^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
20	8	01	03	00	01.3	12.3	<u>35.3</u>	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
21	8	08	08	10	06.7	01.2	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
22	7	04	06	05	05.0	07.9	02.2	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
23	8	02	05	10	05.7	08.1	00.8	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
24	7	10	10	10	10.0	00.0	02.0	.	$\bullet^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
25	7	06	07	08	07.0	04.2	00.1	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
26	8	00	01	00	00.3	11.4	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
27	8	00	00	00	00.0	12.0	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
28	8	01	01	05	02.3	10.8	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
29	6	00	00	00	00.0	10.1	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
30	8	00	00	00	00.0	10.9	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
31	8	00	00	05	01.7	10.5	.	.	$\square^o 1^o 2^o 4^o 6^o 8^o 10^o 12^o 1^o$
MES. VRED.		03.8	04.5	04.0	04.1	244.7	83.8		

$\varphi = 44^{\circ}48' N$   $\lambda = 20^{\circ}28' E$  Gr.  $\Delta G = +1h\ 22\ min.$

BR. ST. 170

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C						Napon vodenog pare e mm			Relativna vlažnost v %			Pravac i jačina veta D, f (0—12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	750.5	750.5	751.0	18.4	26.0	20.2	21.2	26.7	16.8	13.7	10.6	09.9	11.3	67	39	63	56	ESE 4	ESE 3	ESE 3	
2	750.7	749.9	750.0	18.4	28.0	19.7	21.5	28.0	16.2	12.6	11.6	09.6	10.2	73	34	59	55	ESE 4	E 3	E 2	
3	749.9	750.1	750.3	19.5	25.7	18.3	20.5	25.8	18.2	13.3	08.4	08.8	11.1	49	35	71	52	E 3	ESE 4	NNE 1	
4	751.2	750.6	751.1	16.0	27.8	19.4	20.7	28.5	15.0	11.4	10.1	10.3	10.5	74	37	62	58	- 0	N 2	ESE 2	
5	752.2	751.5	752.1	16.6	28.4	20.0	21.3	28.6	13.7	10.0	10.9	10.6	11.9	77	36	68	60	SW 1	NW 3	E 1	
6	754.0	753.9	754.4	16.4	27.2	19.8	20.8	27.7	15.4	11.8	11.8	12.1	12.6	85	45	73	68	WSW 2	NNW 2	W 2	
7	754.5	753.3	753.4	17.3	27.0	20.2	21.4	28.0	16.5	12.4	12.6	12.7	13.5	85	45	76	69	WSW 2	NNW 2	WSW 1	
8	753.7	752.7	751.2	17.2	27.2	19.8	21.0	28.1	15.8	11.9	12.5	11.3	12.3	85	42	71	66	WSW 2	NW 2	SE 2	
9	747.8	745.9	753.8	19.6	30.6	13.1	19.1	30.6	13.0	11.3	11.3	09.8	08.8	66	30	78	58	ESE 2	WSW 3	W 3	
10	754.5	754.0	755.3	11.0	17.9	14.7	14.6	19.4	10.6	10.6	08.2	06.6	06.1	83	43	49	58	W 3	NW 3	W 3	
11	755.5	754.9	756.0	12.5	19.1	18.0	16.9	20.4	10.7	09.6	07.5	07.3	09.2	69	44	60	58	SW 2	NNW 3	NNW 2	
12	757.2	756.1	754.5	15.9	25.3	17.7	19.2	25.6	14.6	11.4	09.7	10.1	11.6	71	42	76	63	WSW 1	W 2	ESE 2	
13	752.9	752.3	754.0	17.4	27.8	19.7	21.2	29.2	13.8	10.8	10.8	10.6	12.1	72	38	70	60	ESE 2	NNE 2	N 3	
14	759.9	760.0	759.1	11.4	18.0	10.2	12.5	19.7	10.2	09.8	06.7	05.0	06.6	66	32	71	56	NW 3	NNW 4	SSW 2	
15	756.7	753.0	749.6	08.6	20.6	13.4	14.0	20.8	06.3	03.3	06.7	07.2	09.1	80	39	79	66	ESE 1	WSW 2	SE 1	
16	747.4	748.1	749.9	11.5	19.2	14.4	14.9	21.2	09.4	06.0	07.7	08.5	06.1	76	51	50	59	WSW 2	N 3	N 3	
17	750.7	750.6	750.7	10.8	09.8	07.9	09.1	14.4	07.8	10.0	05.4	07.3	07.3	56	80	91	76	N 3	N 3	NNE 2	
18	748.7	749.3	750.4	08.4	09.6	09.6	09.3	10.2	07.8	07.4	07.8	08.3	08.7	95	93	98	95	WSW 2	WSW 1	W 3	
19	753.6	755.5	755.4	09.3	12.8	11.8	11.4	13.1	09.0	08.7	08.1	07.9	08.8	93	71	84	83	W 2	NNE 1	NE 1	
20	748.8	750.6	750.5	12.1	12.6	10.9	11.6	14.0	10.6	08.8	10.0	10.1	09.4	94	92	96	94	ESE 3	W 2	W 2	
21	748.2	750.0	751.2	10.6	13.7	12.0	12.1	14.4	10.3	10.4	09.5	10.2	09.8	99	86	93	93	WSW 2	- 0	SSW 2	
22	751.5	751.0	750.7	10.4	17.0	13.7	13.7	18.2	09.5	06.0	09.2	09.0	09.9	98	62	84	81	SSE 1	NNE 2	NNW 1	
23	750.7	750.6	749.9	12.1	15.5	12.4	13.1	16.0	11.6	10.5	08.4	07.4	09.5	79	56	88	74	NNE 2	NNW 3	WSW 1	
24	749.7	750.3	751.9	10.1	11.4	11.2	11.0	12.4	09.7	10.0	08.5	09.8	09.7	92	97	98	96	N 2	NE 1	ESE 1	
25	752.8	754.5	756.4	11.0	13.1	10.6	11.3	13.3	10.5	10.5	09.5	09.3	08.5	96	82	88	89	- 0	N 2	ESE 2	
26	757.4	757.6	758.3	08.6	16.1	09.4	10.9	16.6	08.4	06.0	06.5	06.2	05.6	78	45	63	62	ESE 3	ESE 2	ESE 3	
27	758.8	756.6	761.0	07.8	14.0	09.0	10.0	14.5	07.6	07.0	05.7	05.6	06.9	72	46	80	66	SE 3	ENE 2	E 1	
28	762.2	762.6	763.5	05.8	13.8	08.0	08.9	14.4	04.4	01.5	05.2	04.3	05.0	75	36	63	58	SE 2	ESE 2	ESE 3	
29	764.3	763.0	762.1	05.3	13.4	07.6	08.5	14.0	04.6	01.3	04.5	04.3	04.6	68	37	59	55	ESE 3	SE 3	ESE 3	
30	760.4	758.1	756.0	04.8	17.6	08.8	10.0	18.0	03.9	-00.5	04.2	04.7	06.9	64	31	71	55	ESE 3	S 2	SE 1	
MES.	VRED.	753.5	753.3	753.8	12.5	19.6	14.0	15.0	20.4	11.1	08.9	08.6	08.5	09.1	78	52	74	68	2.2	2.3	2.0

## 1977 OKTOBAR

## BEOGRAD

1	752.6	749.6	747.7	08.6	24.6	14.3	15.5	25.4	05.9	02.2	05.8	07.9	09.5	69	34	78	60	SE 1	N 1	SSE 2
2	749.2	749.9	749.1	10.2	08.7	06.7	08.1	17.0	06.6	08.5	07.3	07.5	07.0	78	89	95	87	N 3	WSW 2	NNW 2
3	748.9	751.3	753.6	06.9	09.4	08.0	08.1	11.1	06.3	06.0	07.2	07.1	07.2	96	81	90	89	NW 1	WSW 2	WSW 2
4	756.7	756.4	755.0	04.9	16.5	10.4	10.6	16.6	04.3	01.6	06.0	04.9	06.1	93	35	65	64	SW 2	WSW 2	ESE 2
5	754.6	754.1	753.8	09.6	21.0	12.0	13.7	21.7	07.4	01.5	05.4	05.7	07.8	60	30	74	55	ESE 2	WSW 2	SE 2
6	752.6	751.6	750.6	10.9	23.5	14.2	15.7	23.5	09.1	03.6	07.2	07.2	07.9	74	33	65	57	SE 2	S 2	ESE 2
7	750.0	749.2	748.7	10.2	21.6	15.6	15.8	24.2	09.0	04.5	07.8	09.0	09.2	84	46	69	66	SE 1	N 1	ESE 2
8	748.1	747.1	745.9	14.3	25.2	16.5	18.1	25.5	10.6	05.1	08.8	08.9	08.0	72	37	57	55	ESE 3	SSE 3	SE 3
9	746.1	745.3	746.4	15.2	24.2	18.3	19.0	24.6	14.5	11.7	07.4	09.5	08.1	57	42	51	50	SE 3	ESE 3	ESE 4
10	747.3	748.1	748.5	14.4	16.8	13.8	14.7	19.0	13.0	12.2	10.0	09.0	09.7	82	62	82	75	ESE 4	ESE 4	ESE 4
11	748.3	748.9	750.3	13.6	16.6	13.4	14.3	17.9	13.2	12.0	09.2	09.4	09.6	79	67	83	76	ESE 5	ESE 4	ESE 4
12	751.8	752.5	754.1	12.4	19.8	15.0	15.6	20.0	11.8	11.0	08.5	08.8	08.8	78	51	69	66	ESE 3	NE 2	ESE 3
13	755.4	755.0	755.6	11.4	17.3	14.0	14.2	18.2	11.2	08.7	07.8	08.0	08.6	78	54	72	68	ESE 2	NNE 2	ESE 1
14	754.6	754.0	753.9	13.4	17.1	14.7	15.0	18.1	13.0	11.5	09.0	10.2	10.9	78	70	87	78	WSW 2	W 2	W 2
15	754.0	754.2	755.1	10.8	16.4	12.5	13.1	17.0	10.6	07.9	08.3	07.6	07.0	85	54	64	68	WNW 2	N 2	N 1
16	756.3	756.7	757.5	07.4	15.3	09.7	10.5	15.6	06.3	02.8	05.8	06.3	07.0	75	49	77	67	NNE 2	NNW 2	ESE 3
17	758.8	757.5	757.4	06.5	15.2	07.8	09.3	15.4	06.1	04.3	05.1	05.6	05.0	71	43	62	59	SE 3	ESE 2	ESE 2
18	758.3	758.3	758.3	04.0	16.8	09.4	09.9	16.9	03.5	-00.6	05.3	06.3	06.1	86	44	69	66	- 0	NNE 2	ESE 2
19	757.4	756.9	756.9	05.0	20.0	10.6	11.6	20.8	04.5	00.0	05.7	06.0	07.1	87	34	74	65	SE 1	MNW 2	SSE 2
20	758.3	758.0	758.5	07.4	18.4	10.2	11.6	19.0	06.4	01.9	06.4	07.8	07.9	83	49	85	72	SW 2	NNE 2	E 1
21	759.3	759.1	759.6	08.6	17.5	10.6	11.8	17.6	07.5	02.9	07.0	06.5	06.0	84	43	63	63	ESE 4	ESE 4	ESE 4
22	759.0	758.2	758.6	09.4	18.6	10.4	12.2	18.9	07.8	06.8	06.0	07.5	06.2	69	46	66	60	ESE 4	ESE 3	SE 3
23	757.7	757.7	757.9	10.0	20.6	12.6	14.0	21.7	09.4	07.5	06.8	07.2	08.							

BR. ST. 170

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijnost 0-9	Oblakost N (0-10)					Insekcija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	7 08	020	00	03.3	08.5	.	.	—	—	—	—
2	8 010	010	00	00.7	10.8	.	.	—	—	—	—
3	7 050	060	00	03.7	08.6	.	.	—	—	—	—
4	7 00	030	03	02.0	10.3	.	.	—	—	—	—
5	8 010	000	00	00.3	10.9	.	.	—	—	—	—
6	8 000	000	00	00.0	10.4	.	.	—	—	—	—
7	8 000	010	00	00.3	09.8	.	.	—	—	—	—
8	7 03	030	00	02.0	10.0	.	.	—	—	—	—
9	8 000	000	10	03.3	08.8	.	.	—	—	—	—
10	7 10	10	06	07.3	06.3	01.4	.	—	—	—	—
11	7 10	10	09	09.7	03.7	.	.	—	—	—	—
12	7 000	040	00	01.3	10.8	.	.	—	—	—	—
13	6 010	040	08	04.3	10.6	.	.	—	—	—	—
14	8 10	000	00	03.3	08.7	13.0	.	—	—	—	—
15	8 000	000	00	00.0	11.2	.	.	—	—	—	—
16	8 000	050	10	05.0	08.7	.	.	—	—	—	—
17	7 100	100	10	10.0	00.0	00.2	.	—	—	—	—
18	6 10	100	100	10.0	00.0	18.7	.	—	—	—	—
19	7 10	10	10	10.0	00.0	07.3	.	—	—	—	—
20	7 080	10	100	09.3	00.0	04.0	.	—	—	—	—
21	6 100	10	08	09.3	00.2	19.8	.	—	—	—	—
22	7 04	09	10	07.7	03.7	01.0	.	—	—	—	—
23	7 09	09	10	09.3	00.2	00.2	.	—	—	—	—
24	6 100	100	10	10.0	00.0	00.0	.	—	—	—	—
25	7 100	10	03	07.7	00.0	06.8	.	—	—	—	—
26	7 04	040	05	04.3	07.2	00.1	.	—	—	—	—
27	7 10	09	09	09.3	00.9	.	.	—	—	—	—
28	7 03	040	00	02.3	08.5	.	.	—	—	—	—
29	8 000	000	00	00.0	10.2	.	.	—	—	—	—
30	8 010	030	00	01.3	10.3	.	.	—	—	—	—
MES. VRED.	04.9	05.1	04.7	04.9	189.3	72.5					

## BEOGRAD

1977 OKTOBAR

1	7 050	020	05	04.0	10.4	.	.	—	—	—	—
2	6 10	100	100	10.0	00.0	00.0	.	—	—	—	—
3	6 10	10	03	07.7	02.2	11.2	.	—	—	—	—
4	8 03	020	00	01.7	09.7	.	.	—	—	—	—
5	8 020	010	00	01.0	10.4	.	.	—	—	—	—
6	8 000	000	00	00.0	10.0	.	.	—	—	—	—
7	7 000	040	00	01.3	08.2	.	.	—	—	—	—
8	8 000	000	00	00.0	10.1	.	.	—	—	—	—
9	8 000	060	03	03.0	07.6	.	.	—	—	—	—
10	8 10	08	06	08.0	03.8	00.4	.	—	—	—	—
11	8 10	09	08	09.0	00.0	00.5	.	—	—	—	—
12	8 05	080	06	06.3	06.5	01.2	.	—	—	—	—
13	7 04	07	10	07.0	03.6	.	.	—	—	—	—
14	7 06	10	10	08.7	00.1	.	.	—	—	—	—
15	6 08	08	04	06.7	01.0	.	.	—	—	—	—
16	7 09	000	00	03.0	06.3	.	.	—	—	—	—
17	7 00	000	00	00.0	05.0	.	.	—	—	—	—
18	7 00	000	00	00.0	09.0	.	.	—	—	—	—
19	7 00	000	00	00.0	09.3	.	.	—	—	—	—
20	7 000	000	00	00.0	08.2	.	.	—	—	—	—
21	6 32	020	00	01.3	08.3	.	.	—	—	—	—
22	7 000	000	00	00.0	08.0	.	.	—	—	—	—
23	7 08	000	00	02.7	05.7	.	.	—	—	—	—
24	7 00	000	00	00.0	06.9	.	.	—	—	—	—
25	6 10	07	00	05.7	01.3	.	.	—	—	—	—
26	6 00	010	00	00.3	05.7	.	.	—	—	—	—
27	6 00	000	00	00.0	06.8	.	.	—	—	—	—
28	7 05	000	08	04.3	06.1	.	.	—	—	—	—
29	1 10	10	10	10.0	00.0	.	.	—	—	—	—
30	5 10	10	10	10.0	00.0	.	.	—	—	—	—
31	5 10	10	03	07.7	00.0	00.3	.	—	—	—	—
MES. VRED.	04.4	04.0	03.1	03.9	174.2	13.6					

$\varphi = 44^{\circ} 48' N$   $\lambda = 20^{\circ} 28' E$  Gr.  $\Delta G = +1h 22min.$

BR. ST. 170

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenog pare e mm			Relativna vlažnost u %			Pravac i jačina vetra D, f (0-12)				
				7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	7	14	21	Sred. Dies	7	14	21	7	14	21	
		7	14	21		7	14	21														
1	751.0	749.3	749.7	08.9	17.2	11.0	12.0	17.5	07.9	04.4	07.9	08.3	08.3	92	56	84	77	-	0	ESE 3	ESE 3	
2	749.6	750.2	751.4	11.1	18.4	09.6	10.2	11.1	09.6	09.0	08.0	08.9	08.4	81	94	94	90	SE 2	SSW 2	W 3		
3	751.0	750.0	750.5	07.4	14.2	11.4	11.1	14.5	07.0	02.9	07.3	07.2	06.3	95	59	63	72	SE 2	SSW 2	SE 1		
4	750.4	750.1	750.4	07.6	21.2	16.8	15.6	21.7	07.1	03.2	07.0	06.8	07.3	90	36	51	59	N 1	S 2	S 2		
5	752.9	753.8	754.4	14.3	14.3	12.2	13.3	17.0	12.2	10.5	09.0	09.3	09.4	74	76	88	79	N 1	N 3	NW 1		
6	754.7	753.3	753.2	08.8	18.3	16.0	14.8	19.0	08.0	04.5	08.2	09.5	09.6	96	60	70	75	ENE 1	ESE 2	ESE 2		
7	755.3	756.1	757.8	11.6	16.8	12.8	13.5	18.6	11.4	08.3	09.8	11.2	10.4	95	78	93	89	SSE 1	WNW 1	NNE 1		
8	759.0	759.3	759.9	11.0	11.8	10.0	10.7	13.2	10.0	10.8	08.9	09.0	08.2	91	87	89	89	N 1	NNE 2	NNE 1		
9	760.3	759.2	757.2	09.5	13.7	10.0	10.8	14.4	09.1	08.2	08.0	07.9	06.0	90	67	87	81	NE 1	WSW 2	SE 2		
10	754.5	754.3	756.0	09.9	16.6	13.8	13.5	16.7	08.5	04.6	07.7	08.0	08.4	84	56	71	70	WSW 2	WSW 1	WNW 1		
11	758.1	756.9	755.8	12.2	20.8	14.0	15.3	21.0	13.6	08.4	08.8	09.1	09.6	82	49	80	70	SW 1	WNW 2	ESE 2		
12	754.0	750.7	746.6	09.4	23.5	17.3	16.9	23.7	09.2	04.4	07.7	07.6	06.2	87	35	42	55	-	ESE 2	SSE 3		
13	745.6	745.0	741.6	12.2	12.4	08.0	10.2	17.3	08.0	06.6	06.4	06.2	05.8	60	57	72	63	ESE 2	N 4	NNE 2		
14	743.2	744.7	742.9	05.8	06.9	05.3	05.8	08.2	05.1	05.4	06.5	06.2	06.1	94	83	91	89	WNW 2	WSW 1	SE 1		
15	738.0	738.9	740.1	05.6	13.8	07.4	08.6	20.2	03.9	00.6	05.9	07.2	05.9	86	61	77	75	ESE 2	N 3	ENE 3		
16	735.3	734.4	734.8	06.3	12.5	06.4	07.9	14.5	05.7	02.0	06.5	07.8	06.7	90	72	93	85	WNW 1	WNW 2	NW 3		
17	737.9	739.9	739.8	04.5	08.3	06.6	06.5	08.7	04.3	03.7	05.7	05.2	05.6	90	63	76	76	WSW 3	WSW 1	- 0		
18	742.3	745.2	748.0	04.7	05.4	02.6	03.8	07.0	02.4	04.1	06.0	05.0	05.2	94	75	94	88	WNW 2	SE 1	- 0		
19	749.7	752.0	754.6	01.4	04.4	01.8	02.4	05.2	00.6	03.2	04.7	05.6	05.0	93	90	97	93	ESE 1	W 1	SW 1		
20	754.3	752.3	750.9	-00.6	04.3	-00.2	00.8	06.9	-01.4	-05.0	04.2	05.3	04.4	96	85	96	92	ESE 1	NE 2	ESE 3		
21	748.2	745.9	743.6	00.7	08.8	05.4	05.1	09.1	-00.6	-03.7	04.4	05.0	04.5	91	59	67	72	ESE 3	ESE 3	ESE 3		
22	741.6	740.1	744.0	06.9	12.7	08.0	08.9	13.4	05.0	03.0	04.6	06.1	07.7	61	56	96	71	ESE 4	SE 4	WNW 2		
23	745.6	749.2	752.3	07.1	00.6	00.8	02.3	08.5	00.5	06.7	07.4	04.6	04.7	97	96	97	97	NE 1	W 2	WSW 2		
24	754.0	752.7	749.5	-00.4	05.0	02.8	02.6	05.9	-00.4	-00.4	04.5	05.2	04.6	100	80	83	88	SSW 1	ESE 2	ESE 3		
25	747.0	745.4	744.0	01.4	07.4	05.7	05.1	07.8	-00.5	-04.1	03.8	05.2	05.3	75	68	76	73	ESE 3	E 2	ESE 3		
26	736.5	732.0	734.7	04.0	04.6	01.4	02.9	09.4	01.3	03.4	05.7	05.6	04.8	94	88	95	92	NNE 2	WSW 3	WSW 4		
27	737.8	740.3	743.9	02.6	03.6	01.7	02.4	03.7	01.4	01.3	04.3	04.5	04.8	78	76	92	82	SW 3	WSW 3	WSW 3		
28	749.8	752.7	755.1	01.7	04.2	01.8	02.4	04.4	00.5	00.1	04.9	04.5	03.9	95	72	74	80	W 3	W 3	N 2		
29	756.1	755.7	755.1	-00.8	02.4	-01.6	-00.4	03.6	-01.6	-03.3	03.4	03.1	03.6	78	58	87	74	NNE 2	WNW 3	NE 1		
30	751.6	748.2	747.8	-01.7	02.6	00.4	00.4	03.8	-02.6	-26.0	03.5	04.3	04.5	85	78	95	86	ESE 2	SE 2	N 2		
MES.	VRED.	748.8	748.6	748.8	06.1	10.6	07.3	07.8	12.2	04.8	03.0	06.4	06.6	06.4	87	69	82	79	1.7	2.2	2.0	

## 1977 DECEMBAR

## BEOGRAD

1	747.9	749.1	749.2	-00.5	-01.3	-01.7	-01.3	01.3	-01.9	-00.4	04.3	03.9	03.8	96	93	93	94	NNW 2	WNW 2	NNE 2		
2	747.3	747.8	749.9	-02.5	-01.8	-01.1	-01.6	-01.0	-03.0	-03.2	03.6	03.9	04.1	94	96	97	96	NNW 2	NNW 3	NN 3		
3	753.2	755.3	757.3	-02.6	-01.9	-00.5	-01.4	-00.4	-02.6	-02.9	03.5	03.7	03.8	94	92	87	91	NNW 3	NNW 2	NN 3		
4	759.9	760.4	760.0	-06.0	-03.2	-06.6	-05.6	-00.4	-07.0	-06.6	02.5	02.6	02.5	85	71	89	82	NNW 3	NNW 2	NN 2		
5	758.0	755.8	752.4	-06.2	-02.6	-06.0	-05.2	-00.4	-07.7	-12.0	02.5	02.4	02.5	85	63	85	78	W 2	WSW 2	ESE 3		
6	749.1	746.9	745.5	-07.2	02.0	01.9	-00.4	03.0	-07.6	-14.0	02.1	03.1	03.3	79	58	63	67	ESE 1	ESE 3	ESE 4		
7	743.6	746.5	751.2	02.0	04.0	00.6	01.8	05.7	00.6	-00.1	04.8	05.5	04.7	90	89	98	92	SE 4	SE 2	WSW 3		
8	753.3	751.9	751.4	01.1	05.2	03.6	03.4	05.7	00.5	00.0	04.7	05.2	04.4	95	79	74	83	S 1	ESE 3	ESE 4		
9	749.3	748.8	748.2	03.6	03.9	03.6	03.7	04.8	03.0	02.2	04.5	05.0	04.8	76	82	82	80	ESE 5	ESE 4	ESE 5		
10	749.0	751.8	757.0	03.0	00.5	-01.4	00.2	03.8	-01.8	02.1	04.9	05.2	03.2	86	88	77	84	ESE 4	ESE 5	ESE 5		
11	762.1	764.2	765.8	-01.9	-01.5	-03.4	-02.6	-01.3	-03.4	-02.2	02.7	02.7	02.7	67	66	75	69	ESE 5	ESE 5	ESE 5		
12	767.7	767.7	767.2	-05.0	-01.2	-04.9	-04.0	-01.2	-05.3	-06.5	02.1	02.4	02.1	68	58	66	64	ESE 3	E 3	ESE 3		
13	764.9	763.7	763.8	-06.2	00.1	-03.6	-03.3	00.5	-06.6	-08.9	02.1	02.4	03.0	74	52	84	70	ESE 2	E 2	WNW 1		
14	764.8	764.3	763.1	-07.7	-05.2	-06.3	-06.4	-03.6	-07.9	-08.8	02.4	02.8	02.8	95	88	96	93	WSW 2	NW 2	SE 2		
15	761.1	759.5	760.8	-02.8	-01.6	-03.0	-02.6	-01.1	-06.6	-09.5	03.0	03.9	03.3	82	97	89	89	WSW 2	W 1	NNE 2		
16	764.8	764.3	763.5	-04.7	-02.4	-00.6	-02.1	-00.5	-05.2	-05.0	03.1	03.3	04.1	95	86	94	92	WNW 3	WNW 2	WNW 2		
17	763.1	764.1	765.1	-02.3	-02.6	-02.9	-02.7	-00.4	-03.0	-02.6	03.6	03.4	03.2	92	90	87	90	N 3	ENE 1	SSW 1		
18	763.7	762.2	762.3	-03.6	-04.0	-04.4	-04.1	-02.8	-04.7	-03.6	03.1	03.0	03.0	88	88	89	88	N 1	NNE 2	- 0		
19	761.0	760.9	761.1	-05.1	-04.0	-04.4	-04.5	-03.8	-05.3	-05.0	02.9	02.9	03.0	91	84	89	88	SSE 2	E 2	SSE 1		
20	761.0	761.0	761.6	-05.5	-05.3	-05.3	-05.4	-04.2	-05.6	-05.7	02.9	02.9	02.9	95	95	95	95	- 0	WNW 2	NW 2		
21	762.0	761.4	761.8</																			

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 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vrijednost O <sub>9</sub>	Oblačnost N (0-10)					Insolacija R mm	Padavine mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7	06	09	10	08.3	01.4	00.2	.	.	$\Delta^0 0-830$ , $\overline{\Delta} 0-215$ , $\overline{H} 0-930$ , $\overline{R} 0-1032$ , $\overline{H} 0-1130$ , $\overline{L} 0-1532$ , $\overline{H} 0-1730$ , $\bullet^0 1832$ , $\overline{2230}$ , $\Delta^0 2230$	
2	6	10*	10*	10*	10.0	00.0	01.8	.	.	$\bullet^0 620$ , $\overline{H} 0-1430$ , $\overline{H} 0-1930$ , $\overline{R} 0-2230$ , $\bullet^0 1430$ , $\overline{H} 0-1930$ , $\overline{L} 0-2230$ , $\Delta^0 2230$	
3	7	07	10	05	37.3	03.7	05.5	.	.	$\overline{\Delta} 0-1230$ , $\overline{\Delta} 0-1230$ , $\overline{\Delta} 0-1230$ , $\Delta^0 2030$	
4	7	03	02*	06	03.7	07.3	.	.	.	$\overline{\Delta} 0-2$ , $\overline{H} 0-830$ , $\overline{R} 0-630$ , $\Delta^0 2030$	
5	7	09	09	08	08.7	06.5	.	.	.	$\overline{\Delta} 0-2330$	
6	6	04	01*	09	04.7	06.5	.	.	.	$\Delta^0 0-1030$ , $\overline{\Delta} 0-2$ , $\overline{H} 0-930$	
7	6	07	08*	10	08.3	03.2	03.0	.	.	$\overline{\Delta} 0-1030$ , $\bullet^0 1530$ , $\overline{R} 0-1930$	
8	4	10	10	08	09.3	00.0	.	.	.	$\Delta^0 0-930$ , $\overline{\Delta} 0-2$ , $\overline{H} 0-930$	
9	7	10	06*	00	05.3	03.7	00.0	.	.	$\overline{\Delta} 0-1030$ , $\overline{H} 0-1330$	
10	7	10	10	09	09.7	00.4	.	.	.	$\overline{\Delta} 0-030$ , $\overline{H} 0-1330$ , $\bullet^0 1430$ , $\overline{H} 0-1330$	
11	7	10	00*	00	03.3	07.3	00.0	.	.	$\Delta^0 0-930$ , $\overline{H} 0-1930$	
12	7	00	00*	00	00.0	08.7	.	.	.	$\overline{\Delta} 0-030$	
13	8	03	08	10	07.0	01.6	.	.	.	$\overline{H} 0-1330$ , $\overline{H} 0-1330$	
14	7	10*	10	00	06.7	00.0	02.6	.	.	$\bullet^0 0-1330$ , $310$ , $\overline{H} 0-1330$ , $\overline{R} 0-3445$ , $\overline{H} 0-2230$ , $\Delta^0 1930$	
15	7	00	10	02	04.0	04.8	02.6	.	.	$\overline{\Delta} 0-030$ , $2230$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$ , $\bullet^0 1430$ , $\overline{H} 0-1430$	
16	7	05	10*	10*	08.3	02.4	00.0	.	.	$\overline{\Delta} 0-030$ , $2430$ , $\overline{H} 0-1330$	
17	7	10	03*	10*	07.7	02.5	24.7	.	.	$\bullet^0 0-530$ , $1930$ , $\overline{H} 0-1330$	
18	6	10*	06	00	06.0	01.1	02.0	.	.	$\bullet^0 0-1230$ , $\overline{H} 0-1330$ , $\overline{R} 0-1430$ , $\overline{H} 0-2030$	
19	6	07	10	08	08.3	00.0	01.0	.	.	$\overline{\Delta} 0-030$ , $930$ , $\overline{H} 0-1930$ , $\overline{R} 0-1330$ , $\bullet^0 1030$ , $1830$ , $\overline{H} 0-1930$ , $\overline{R} 0-1930$	
20	6	00	00*	00	00.0	06.2	.	.	.	$\overline{\Delta} 0-330$ , $830$ , $\overline{H} 0-2430$ , $\overline{R} 0-2430$ , $\bullet^0 930$ , $\overline{H} 0-1030$	
21	7	03	06*	04	04.3	07.1	.	.	.	$\overline{\Delta} 0-330$ , $\overline{H} 0-1330$ , $\overline{R} 0-1030$	
22	7	00	10	10*	06.7	01.5	.	.	.	$\overline{\Delta} 0-030$ , $1530$ , $\overline{H} 0-2430$	
23	4	10	10*	10*	10.0	00.0	05.1	.	.	$\bullet^0 0-1330$ , $630$ , $\overline{H} 0-1330$ , $\overline{R} 0-1430$ , $\overline{H} 0-1430$ , $\overline{R} 0-1430$	
24	6	10	00*	00	03.3	05.6	14.0	02	.	$\overline{\Delta} 0-030$ , $1030$ , $\overline{H} 0-1030$ , $\overline{R} 0-1030$ , $\bullet^0 1030$ , $1030$ , $\overline{H} 0-1030$ , $\overline{R} 0-1030$	
25	7	00	09	10	06.3	04.4	.	.	.	$\overline{\Delta} 0-330$ , $2430$ , $\overline{H} 0-2230$ , $\overline{R} 0-2230$	
26	7	10	10	10	10.0	01.9	09.7	.	.	$\bullet^0 0-330$ , $1830$ , $\overline{H} 0-1930$	
27	7	10	10	10*	10.0	00.2	01.0	.	.	$\overline{H} 0-930$ , $1030$ , $\overline{R} 0-2330$	
28	7	10	08*	03	07.0	00.8	03.5	.	.	$\overline{\Delta} 0-030$ , $1030$ , $\overline{H} 0-1030$ , $\overline{R} 0-1030$	
29	7	04	05	04	04.3	05.9	00.3	.	.	$\overline{\Delta} 0-330$	
30	5	06	10	10*	08.7	02.1	.	.	.	$\overline{\Delta} 0-1030$ , $\overline{H} 0-1030$ , $\overline{R} 0-1530$ , $\bullet^0 1430$ , $\overline{H} 0-1430$	
MES. VRED.					06.5	07.1	06.2	06.6	87.8	77.0	

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1	5	10*	10*	10*	10.0	00.0	09.0	03	.	$\overline{\Delta} 0-030$ , $\bullet^0 0-330$ , $\overline{H} 0-330$ , $\overline{R} 0-430$ , $\bullet^0 430$ , $\overline{H} 0-430$ , $\overline{R} 0-430$	
2	5	10*	10*	10*	10.0	00.0	11.2	15	.	$\bullet^0 0-24$ , $\overline{H} 0-24$	
3	5	10*	10*	10	10.0	00.0	19.4	15	.	$\bullet^0 0-1530$ , $\overline{H} 0-1530$	
4	7	04	03*	00	02.3	04.5	02.2	23	.	$\overline{\Delta} 0-030$ , $\overline{H} 0-2530$	
5	7	03	01*	00	01.3	06.7	.	22	.	$\overline{H} 0-2530$	
6	8	02	02*	10	04.7	07.6	.	20	.	$\overline{\Delta} 0-330$ , $\overline{H} 0-1330$	
7	6	10*	10*	10*	10.0	01.3	05.8	.	.	$\overline{\Delta} 0-1130$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$	
8	7	10	00*	00	03.3	03.9	02.7	09	.	$\overline{\Delta} 0-1230$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$	
9	7	10	10*	09	09.7	00.0	*	03	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-24$ , $\overline{R} 0-24$	
10	6	10*	10*	10*	10.0	00.0	02.9	.	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-24$ , $\overline{R} 0-24$	
11	7	10	10	01	07.0	00.0	00.5	.	.	$\overline{\Delta} 0-530$ , $\overline{H} 0-1330$	
12	8	00	00*	00	00.0	07.6	.	.	.	$\overline{\Delta} 0-1330$ , $\overline{H} 0-430$	
13	8	00	00*	00	00.0	07.7	.	.	.	$\overline{H} 0-1330$	
14	6	97	03*	00	03.3	04.6	.	.	.	$\overline{\Delta} 0-030$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$	
15	4	10*	10	08	09.3	00.0	00.0	.	.	$\overline{\Delta} 0-630$ , $\overline{H} 0-1530$ , $\overline{R} 0-1530$	
16	4	10	10	10	10.0	00.0	01.0	02	.	$\overline{\Delta} 0-330$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$	
17	1	10	10	10	10.0	00.0	00.0	01	.	$\overline{\Delta} 0-030$ , $\overline{H} 0-430$ , $\overline{R} 0-430$	
18	5	10*	10	10*	10.0	00.0	00.0	01	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$	
19	5	10	10*	10*	10.0	00.0	00.0	01	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$	
20	4	10*	10	10	10.0	00.0	00.0	01	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-1330$ , $\overline{R} 0-1330$	
21	4	10*	10*	10*	10.0	00.0	00.0	01	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-1330$	
22	5	10*	10	10	10.0	00.0	00.1	01	.	$\overline{\Delta} 0-1030$ , $\overline{H} 0-2430$	
23	6	10	10	10*	10.0	00.0	00.0	01	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-1930$ , $\overline{R} 0-1930$	
24	5	10	07*	06	07.7	03.2	00.0	01	.	$\overline{\Delta} 0-1030$ , $\overline{H} 0-2430$	
25	6	10*	10	05	08.3	00.0	02.4	.	.	$\overline{\Delta} 0-430$ , $\overline{H} 0-2230$ , $\overline{R} 0-2230$	
26	7	10	06	07	07.7	02.6	07.9	.	.	$\overline{\Delta} 0-630$ , $\overline{H} 0-2430$	
27	7	00	05	00	01.7	05.9	.	.	.	$\overline{\Delta} 0-030$ , $\overline{H} 0-2430$	
28	7	05	08	10	07.7	02.6	.	.	.	$\overline{\Delta} 0-630$ , $\overline{H} 0-2430$	
29	4	10	10*	10*	10.0	00.0	00.0	.	.	$\overline{\Delta} 0-630$ , $\overline{H} 0-2430$	
30	7	10*	10	09	09.7	02.9	15.4	.	.	$\overline{\Delta} 0-930$ , $\overline{H} 0-2430$	
31	7	10	06	10*	08.7	00.5	00.0	.	.	$\overline{\Delta} 0-24$ , $\overline{H} 0-2430$ , $\overline{R} 0-2430$	
MES. VRED.					08.1	07.5	06.9	07.5	61.6	80.5	

$\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$  Gr.  $\Delta G = +1h\ 17\ min.$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	762.3	761.5	762.0	-01.2	08.0	01.0	02.2	08.0	-01.2	-03.5	03.7	04.5	04.6	88	56	93	79	-	0	SE 2 - 0	
2	762.3	761.4	763.5	02.2	07.2	06.2	05.5	07.5	01.0	02.0	04.7	05.4	05.9	87	71	84	81	-	0	E 1 N 1	
3	764.7	765.0	766.4	04.8	09.8	07.0	07.2	10.4	03.4	01.0	05.8	06.3	06.5	90	70	87	82	-	0	- 0 - 0	
4	768.0	768.6	770.6	06.2	11.4	06.2	07.5	11.5	05.7	03.0	06.5	06.3	05.9	92	63	84	80	-	0	- 0 - 0	
5	772.7	771.7	772.8	01.8	10.8	03.2	04.8	13.2	01.5	-00.5	05.0	06.0	05.4	97	62	94	84	-	0	- 0 - 0	
6	772.4	770.4	769.8	00.0	10.2	02.4	03.8	12.2	00.0	-02.4	04.4	05.9	05.1	96	63	94	84	-	0	SSE 1 - 0	
7	769.4	766.4	765.5	-00.4	12.2	06.0	06.0	12.4	-00.7	-02.5	04.3	06.2	06.2	96	58	89	81	-	0	SE 2 - 0	
8	761.2	762.5	760.2	05.0	06.0	03.4	04.5	07.0	-03.6	02.5	06.2	06.4	05.5	94	92	94	93	-	0	NW 1 - 0	
9	761.3	759.7	758.9	-01.0	08.0	00.4	02.0	08.6	-01.0	-02.8	03.8	04.5	04.6	89	56	96	80	WW 1	SSE 1 - 0		
10	757.6	756.3	757.9	-01.8	08.6	04.0	03.7	09.7	-01.8	-04.2	03.6	03.8	04.6	91	45	76	71	N 1	SE 1 S 1		
11	757.4	756.2	754.9	04.0	06.2	09.0	07.1	11.0	04.0	-03.7	05.9	06.9	06.0	97	97	93	96	-	0	NW 2 S 6	
12	751.9	750.9	750.1	10.8	11.0	07.0	09.0	12.0	07.0	03.8	08.4	08.5	06.9	86	82	92	88	SE 5 N 3	SE 5 N 3		
13	748.9	749.9	753.4	06.6	06.8	05.6	06.2	11.5	00.5	00.5	07.1	07.0	06.6	97	95	97	96	W 2 W 1	SE 1		
14	756.6	757.7	759.5	02.0	08.4	03.6	04.4	09.6	01.5	00.0	05.1	05.8	05.4	97	70	91	86	N 2	SE 2 NW 2		
15	758.8	756.7	754.2	04.2	05.4	04.8	04.8	06.2	02.4	-00.4	04.9	06.2	06.3	79	91	97	89	N 2	SSW 2		
16	753.7	753.0	752.5	05.4	09.8	03.8	05.7	11.4	03.5	03.8	06.5	06.5	05.6	97	72	94	88	N 1	N 3 NW 3		
17	751.5	752.1	752.2	04.4	07.8	04.6	05.4	07.8	03.5	02.0	03.1	03.3	03.0	49	41	46	45	N 5 N 1	N 1 N 1		
18	751.9	754.7	756.6	04.8	08.2	04.6	05.6	08.6	04.4	02.8	02.9	03.1	02.6	44	38	41	41	N 5 N 5	SE 1		
19	757.4	758.1	759.6	03.0	08.4	00.4	03.1	09.5	-00.5	-00.6	02.8	03.4	03.4	48	41	72	54	N 2 S 2	SE 1		
20	761.1	760.5	761.0	-00.8	07.2	03.8	03.5	08.5	-01.8	-04.6	03.4	03.8	03.7	78	49	61	63	N 2	SE 1 - 0		
21	760.7	760.4	762.1	03.6	10.6	02.4	04.8	10.6	02.4	-02.0	05.0	05.9	05.1	85	62	94	80	-	0	SSW 2 - 0	
22	763.1	762.8	763.2	03.4	10.4	04.2	05.6	11.3	01.8	-01.2	05.5	05.8	05.4	94	61	88	81	-	0	E 1 E 2	
23	761.7	758.7	755.1	02.2	09.6	05.4	05.7	09.6	00.5	-02.2	04.7	06.2	06.3	87	69	94	83	-	0	- 0 - 0	
24	753.4	752.7	754.1	06.2	08.6	07.8	07.6	08.8	05.4	00.0	06.9	08.2	07.7	97	97	97	97	-	0	- 0 - 0	
25	755.8	755.6	757.2	06.2	13.8	06.6	08.3	14.5	05.8	00.6	06.9	07.8	07.3	97	66	100	88	-	0	SW 1 W 1	
26	758.4	756.8	755.9	03.4	11.6	08.0	07.8	12.8	03.2	00.8	05.5	05.7	07.4	94	73	92	86	-	0	- 0 - 0	
27	753.3	752.7	752.7	09.2	10.3	10.4	10.1	10.8	06.6	00.8	08.5	09.1	09.0	98	96	95	96	SSW 1 W 2 NW 2	ESE 2		
28	755.9	757.0	756.9	05.4	13.2	09.2	09.3	14.0	05.4	04.2	06.5	07.8	07.9	97	69	90	85	NNW 1 -	0 ESE 2		
29	752.3	748.6	749.4	08.4	14.6	12.8	12.2	15.8	07.5	03.0	07.4	08.5	08.3	90	68	74	77	-	0	S 1 S 2	
30	754.8	755.7	756.8	09.8	14.0	09.4	10.7	14.6	09.2	02.8	08.2	07.4	07.8	90	62	88	80	SE 1 S 2	SE 1 S 1		
31	757.7	755.5	754.7	07.4	13.2	08.8	09.6	14.2	07.0	04.6	07.5	08.1	07.6	97	71	90	86	NW 1 S 2 W 2			
MES.	VRED.	759.0	758.4	758.7	04.0	09.7	05.5	06.2	10.8	02.7	00.2	05.5	06.2	06.0	88	68	86	81	1.1	1.4	1.2

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1	752.5	751.0	752.4	07.6	10.4	08.2	08.6	10.5	07.4	06.2	07.4	09.0	07.9	95	95	97	96	-	0	WW 1 NE 2
2	751.6	752.8	753.2	07.8	09.8	07.4	08.1	12.0	07.3	06.5	07.7	08.6	07.3	97	95	95	96	W 1 W 1	- 0	
3	753.0	754.2	755.6	07.0	11.0	07.2	08.1	12.6	06.0	04.0	05.7	09.6	00.5	92	64	64	64	NW 3 SSE 2	N 2 N 3	
4	756.3	756.0	758.4	05.0	11.0	08.2	08.1	12.0	04.4	01.4	03.8	04.5	03.6	58	46	45	50	NNW 2 N 1	N 1 N 4	
5	760.0	760.1	760.8	01.0	13.6	04.8	06.1	14.1	00.8	-01.4	04.8	05.1	06.0	97	44	93	78	N 1 S 2 S 1		
6	760.4	758.3	756.9	03.8	10.8	07.0	07.2	11.6	03.0	00.2	05.5	06.2	06.5	91	64	87	81	-	0	SSW 2 WNW 2
7	757.8	758.1	759.2	04.4	16.4	09.8	10.1	16.7	03.5	01.0	06.1	05.1	04.3	97	37	48	61	-	0	NM 4 N 3
8	761.6	760.0	758.1	04.8	15.0	09.0	09.5	15.2	03.4	00.5	05.2	06.8	07.4	80	53	86	73	N 2 S 1	NE 1	
9	757.2	755.3	755.1	08.6	14.8	11.0	11.4	15.0	08.0	02.0	07.5	08.6	08.5	90	68	86	81	-	0	SSE 2 - 0
10	754.1	754.1	752.5	09.4	09.8	09.8	09.7	11.5	09.0	07.5	08.4	08.9	09.1	95	98	100	98	-	0	- 0 - 0
11	750.1	751.7	752.1	12.8	13.8	10.4	11.9	14.0	05.8	0.8	10.7	10.9	09.0	97	90	95	94	SE 4 ESE 4	WW 1	
12	750.4	750.1	750.0	13.0	13.4	13.0	13.1	14.4	10.2	08.4	09.9	10.5	09.1	86	91	81	87	SE 4 SSE 3		
13	753.1	753.3	751.6	09.4	14.4	09.4	10.7	14.8	09.0	07.2	07.8	08.4	07.8	88	68	88	81	-	0	N 3
14	746.7	745.6	749.1	08.2	11.0	09.4	09.5	11.1	08.0	07.3	07.8	08.8	08.0	96	90	92	92	NE 2 SE 2	S 2 S 4	
15	753.3	753.8	754.7	06.6	11.8	06.6	07.9	12.0	06.0	04.6	06.7	06.6	06.9	92	74	95	87	-	0	NNW 2 W
16	754.2	753.8	754.3	05.2	11.2	07.0	07.6	12.5	05.0	03.5	06.4	07.7	06.5	97	77	87	87	-	0	E 3 N 2
17	755.3	755.0	759.3	06.0	11.4	06.4	07.6	11.7	05.6	04.3	06.9	06.7	06.9	99	66	96	87	WW 2 S 2	- 0	
18	762.3	762.9	764.1	02.2	12.7	08.6	08.0	13.6	02.0	00.0	05.2	06.3	07.0	97	57	84	79	-	0	SE 2 - 0
19	764.4	764.3	764.0	05.6	12.4	09.6	09.3	13.5	02.5	01.0	06.4	06.9	07.5	94	64	83	80	-	0	- 0 - 0
20	763.5	763.1	762.0	08.0	09.8	08.2	08.6	10.6	07.6	05.6	07.9	08.9	08.2	99	98	100	99	-	0	W 1 N 1
21	759.5	758.6	757.8	09.8	12.8	12.2	11.8	13.4	08.0	06.2	08.6	08.3	09.2	95	74	87	85	WW 2 SE 3 SE 4		
22	758.6	759.6	760.7	13.4	13.8	12.0	12.8	14.2	12.0	09.5	08.9	08.9	09.6	77	75	91	81	S 4 S 4	- 0	
23	760.3	760.6	763.0	09.6	19.0	10.0	12.2	19.0	09.4	08.4	08.9	09.5	08.5							

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8 03	05○	02	03.3	06.2	.	.	.	.	└' n-10	.
2	8 10	10	04	06.0	00.0	.	.	.	.	.	.
3	8 08	10	10	09.3	00.0	.	.	.	.	.	.
4	7 10	08	06	08.0	01.2	.	.	.	.	.	.
5	7 03	06	04	04.3	04.8	.	.	.	.	└' n-10, └' 08○ H	.
6	8 01	00○	00	00.3	07.6	.	.	.	.	└' n-10, └' 19-n	.
7	8 00	00○	02	00.7	07.1	.	.	.	.	└' n-10, └' 0-10○	.
8	7 10○	10	02	07.3	00.0	03.1	.	.	.	●' n-H, └' n-11○, └' 14-1555	.
9	8 01	04○	00	01.7	08.3	01.6	.	.	.	└' n-9○, └' 9○ 24	.
10	8 03	06	08	05.7	05.7	.	.	.	.	└' n-9○, └' 19○ 24	.
11	6 10○	10○	10○	10.0	00.0	02.6	.	.	.	●' n-16, 0855 n, └' n-10, └' 10-1200, └' 1850 24	.
12	7 10○K	10○	10○K	10.0	00.0	29.0	.	.	.	└' 0-24, └' n-KV i, └' 16-20, └' 9○ i, 16-KV; └' n-9, └' 1950 1945	.
13	7 10○	10○	10○	10.0	00.0	70.7	.	.	.	●' n-10, └' n-KV i, └' 16-20	.
14	8 10	08	00	06.0	06.5	34.4	.	.	.	└' 20-n, └' n	.
15	7 10	10○	10○	10.0	00.0	01.0	.	.	.	└' 12-n, └' 19○ n	.
16	8 10	08○	10	09.3	03.6	36.4	.	.	.	●' n-450, 1450 2050; └' n n-210	.
17	8 03	06○	10	06.3	03.6	04.5	.	.	.	●' n-24, └' n	.
18	8 04	02○	00	02.0	07.1	.	.	.	.	└' n-550	.
19	8 00	00○	00	00.0	08.9	.	.	.	.	└' n-11	.
20	8 04	08	00	04.0	02.8	.	.	.	.	└' 0-14○, └' 19○ n i	.
21	8 10	08	00	06.0	02.9	.	.	.	.	└' 20-n	.
22	8 10	04○	06	06.7	03.4	.	.	.	.	└' 19○ n	.
23	7 05	10	10	08.3	00.0	.	.	.	.	└' n-9○	.
24	6 10○	10○	10○	10.0	00.0	13.4	.	.	.	●' n-10 i, └' n-16, └' 16-n i	.
25	6 10○	02○	10○	07.3	06.9	02.6	.	.	.	└' 0-14○, └' 19○ n i	.
26	8 01	08	10	06.3	03.6	.	.	.	.	└' n-9	.
27	3 10○	10○	10	10.0	00.0	10.0	.	.	.	●' 0-12, 1450 1550; └' n-1650, └' 1650 1750, └' 2250 24	.
28	8 01	10	08	06.3	05.6	13.0	.	.	.	●' 0-3	.
29	7 10	10	10○K	10.0	00.0	.	.	.	.	└' 19○ 1650, └' 1550 1850, └' 1650 n i, └' 2050 n	.
30	8 10○	08○	18	12.0	02.6	12.6	.	.	.	●' n-750, └' 1750, └' 1950 2150	.
31	8 10	10	10	10.0	02.9	00.3	.	.	.	●' 7-1850, └' 2250 24	.
MES. WRED.		06.7	07.1	06.5	06.7	101.5	234.2				

1	8 10	10○K	10○K	10.0	00.0	14.2	.	.	.	●' 0-17 i, 19-23; └' 102 1450 1050 1650, 1350 KV i	.
2	7 10○	10○	04	08.0	02.2	38.7	.	.	.	●' n-9○, └' 13-14○	.
3	8 04	08	06	06.0	05.3	07.5	.	.	.	●' n-9○	.
4	8 01	00○	00	00.3	05.4	.	.	.	.	└' n 9○ 1650	.
5	8 04	02○	02	02.7	08.5	.	.	.	.	●' n-9○	.
6	8 08	08	10○	08.7	00.2	.	.	.	.	●' 1750 2050	.
7	8 08	04○	00	04.0	09.1	03.3	.	.	.	●' 0-12, 1450 1550; └' n-1650, └' 1650 1750, └' 2250 24	.
8	8 03	03○	10	05.3	09.4	.	.	.	.	●' 0-3	.
9	8 10	08	10	09.3	01.3	.	.	.	.	└' 19○ 1650, └' 1550 1850, └' 1650 n i, └' 2050 n	.
10	7 10○	10○	10	10.0	00.0	.	.	.	.	●' 7-1850, └' 2250 24	.
11	7 10	10○	10	10.0	00.0	35.2	.	.	.	└' 0-1200, └' 1750 24, └' 1450 15, └' 1750 1850	.
12	7 10○	10○	06	08.7	00.0	33.6	.	.	.	●' 0-12, 1450 1550; └' 13-14○	.
13	8 08	10	10○	09.3	00.0	15.7	.	.	.	●' 1650 1450, └' 2250 24	.
14	8 10	10○	10	10.0	00.0	13.9	.	.	.	●' 0-6, 1350 18	.
15	8 10	04○	10○	08.0	01.7	02.6	.	.	.	●' 1750 1750, └' 1950 2150	.
16	8 08	08	08	08.0	04.3	03.8	.	.	.	└' 9○ 1050, 20-21; └' 1550 1250, 2350 24	.
17	8 10○	04○	08	07.3	05.7	07.9	.	.	.	●' 0-8	.
18	8 00	06○	08	04.7	09.0	00.4	.	.	.	└' n-9○	.
19	8 08	10	10○	09.3	01.0	.	.	.	.	●' 21-24	.
20	7 10	10○	05	08.3	00.0	02.6	.	.	.	●' 0-2, 9○ 15 i	.
21	7 10○	10○	10○	10.0	00.0	03.4	.	.	.	●' 18○ 24 i, └' 9○ n	.
22	8 10○	10	10	10.0	00.0	07.4	.	.	.	●' 0-7, └' n-10○	.
23	8 10	10	00	06.7	02.6	00.0	.	.	.	└' 12-16	.
24	8 03	06○	00	03.0	06.2	.	.	.	.	└' 1950 24	.
25	8 06	10	08	08.0	05.3	.	.	.	.	└' 0-950, └' 1050 1650, └' 1850 2350-24	.
26	8 03	05○	02	03.3	09.2	00.6	.	.	.	●' 1-1	.
27	8 08	08○K	00	05.3	06.5	05.0	.	.	.	└' n-650, └' 1050 1450, └' 1550 1650, └' 1750 1850, └' 1950 2150	.
28	8 10○	07	02	06.3	02.6	04.6	.	.	.	●' 4-8, └' 8○ 24	.
MES. WRED.		07.6	07.5	06.4	07.2	59.5	264.8				

$\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$  Gr.  $\Delta G = +1h\ 17\ min.$ 

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d	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21				
1	764.7	763.9	764.9	06.4	07.0	03.4	03.6	07.2	00.4	-01.2	02.0	02.8	03.3	42	37	56	45	N	4	N	4	N	1	
2	765.1	764.9	765.4	02.0	09.2	04.4	05.0	09.6	01.0	-02.7	03.3	02.4	02.6	61	28	41	43	NNW	1	N	3	N	2	
3	764.3	763.4	763.1	02.6	07.2	04.8	04.9	14.2	02.5	00.0	03.6	03.4	04.2	65	45	66	59	-	0	-	0	-	0	
4	762.0	761.6	761.2	04.0	12.2	06.4	07.3	12.5	02.1	00.0	04.3	06.2	06.8	70	58	94	74	N	2	S	1	-	0	
5	762.1	762.3	764.2	06.6	15.2	08.1	09.5	16.0	03.6	01.4	06.5	06.9	06.9	89	54	85	76	-	0	SSE	2	-	0	
6	765.3	763.7	764.7	03.8	16.4	08.2	09.2	17.5	03.5	01.0	05.6	06.9	06.9	94	49	85	76	-	0	E	3	-	0	
7	765.6	765.2	767.1	05.0	19.0	10.4	11.2	19.0	04.4	01.5	04.9	06.1	06.8	74	37	72	61	-	0	S	2	-	0	
8	771.1	771.3	772.1	10.4	18.6	10.4	12.5	18.6	08.8	02.8	03.8	06.0	05.7	41	38	60	46	NE	2	SSE	2	-	0	
9	771.9	768.9	767.1	05.0	17.2	09.4	10.3	18.0	05.0	00.6	05.0	04.7	07.1	77	32	81	63	-	0	S	2	-	0	
10	764.4	760.6	760.0	04.4	17.0	09.0	09.9	19.3	04.4	01.5	05.4	06.2	08.0	85	42	92	73	-	0	S	2	-	0	
11	760.4	759.8	760.0	05.8	17.4	05.6	10.6	18.0	04.4	01.9	04.3	05.5	07.5	92	37	83	71	-	0	SSE	3	-	0	
12	759.3	758.6	757.5	09.8	09.4	11.2	10.4	11.7	09.0	03.2	07.9	08.6	09.7	87	98	98	94	-	0	W	1	S	2	
13	753.0	753.5	754.7	10.6	09.0	08.4	09.1	12.6	08.1	08.0	09.4	08.2	07.8	98	95	95	96	W	3	N	3	N	3	
14	758.7	759.9	761.6	08.0	15.9	11.2	11.6	16.6	07.5	05.4	07.2	05.2	05.6	90	38	56	61	SE	3	N	4	N	2	
15	764.1	763.9	765.7	08.2	17.8	11.8	12.4	18.6	06.8	03.0	01.5	05.5	05.1	63	36	49	49	N	2	N	3	NNW	2	
16	767.0	766.5	767.0	11.0	18.0	10.8	12.7	18.0	07.7	04.8	04.9	05.0	05.0	50	32	52	45	NNN	2	N	5	N	2	
17	766.5	763.4	762.7	05.4	17.8	08.0	09.8	18.8	03.6	00.7	05.4	05.5	07.1	80	36	88	68	-	0	SSE	2	-	0	
18	762.3	759.6	758.4	06.2	18.2	09.2	10.7	18.6	04.5	01.6	05.2	05.8	07.0	73	37	81	64	-	0	S	5	-	0	
19	758.8	757.0	756.8	07.0	17.8	10.2	11.3	17.8	05.7	03.0	05.7	06.9	08.0	76	45	86	69	-	0	S	3	-	0	
20	756.9	758.1	759.0	12.0	11.4	12.2	12.0	13.8	09.8	06.8	08.9	09.6	09.7	84	95	91	90	ESE	3	WSW	2	SE	4	
21	759.8	761.4	763.0	13.4	14.4	13.2	13.6	16.0	07.0	07.0	08.6	10.5	10.4	75	86	91	84	SE	4	S	6	-	0	
22	763.9	763.0	763.8	06.4	22.4	12.4	13.9	23.0	08.3	06.0	08.1	09.4	09.1	97	46	85	76	-	0	S	1	-	0	
23	764.0	761.9	761.8	09.9	25.8	14.0	15.9	26.4	08.0	05.2	08.1	09.6	09.0	88	38	75	67	-	0	SSE	2	-	0	
24	761.8	759.8	759.2	11.8	27.0	14.8	17.1	27.2	09.5	06.2	08.1	07.9	09.8	78	29	78	62	-	0	S	2	-	0	
25	759.3	759.0	758.7	13.4	24.0	15.6	17.2	24.6	12.0	07.5	07.3	07.8	09.4	63	35	71	56	-	0	-	0	-	0	
MES.	VRED.	761.1	760.3	760.7	08.5	16.8	10.9	11.8	17.9	07.1	04.4	06.7	07.1	07.5	77	51	76	68	1.2	2.5	0.9			

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## TITCGPAC

1	759.0	757.9	756.3	12.4	14.0	13.6	13.4	14.4	12.0	11.0	10.6	10.5	10.7	98	87	91	92	-	0	NW	3	NNW	2
2	753.5	752.6	752.7	12.6	14.6	13.6	13.6	15.0	12.5	12.0	10.7	11.9	11.4	98	96	98	97	-	0	NNW	1	NW	1
3	750.6	748.7	750.4	13.2	20.6	13.6	15.3	20.8	12.7	12.2	11.1	12.6	12.2	98	67	96	87	NNW	2	ESE	2	-	0
4	753.4	754.3	756.2	12.4	20.0	13.4	14.8	20.4	10.2	08.0	10.6	11.9	10.8	98	68	94	87	-	0	SSE	2	-	0
5	757.4	755.7	754.7	12.4	20.4	15.8	16.1	21.0	09.5	07.5	10.3	10.4	09.6	96	58	71	75	-	0	S	4	-	0
6	755.1	756.1	755.4	12.2	16.8	11.4	13.5	18.8	10.5	07.5	04.9	08.1	09.1	46	50	90	62	NNW	4	S	4	-	0
7	755.6	754.4	753.6	10.4	18.6	12.2	13.4	19.0	08.2	04.7	08.1	08.2	09.2	86	51	87	75	-	0	S	4	-	0
8	751.3	747.7	745.8	12.4	24.2	18.0	18.2	24.5	09.5	07.5	08.7	04.9	07.5	80	22	49	50	S	3	S	3	NW	2
9	743.9	741.2	745.9	16.2	15.2	10.8	13.3	19.2	05.6	08.5	08.5	09.0	07.6	64	51	78	64	SE	6	SSW	3	SE	3
10	746.0	748.8	749.9	10.6	10.4	09.6	10.1	14.0	07.6	07.6	07.8	08.3	07.9	81	88	86	86	SE	3	S	4	-	0
11	750.0	749.9	750.9	09.6	14.2	05.6	10.8	14.4	06.1	04.5	05.9	04.0	03.8	66	34	42	47	N	3	N	7	N	6
12	771.1	750.5	751.1	08.8	14.6	05.2	10.5	15.4	07.2	05.5	03.5	04.1	03.3	41	33	38	37	N	5	NNE	3	NNE	5
13	753.1	752.5	753.3	08.6	13.6	05.8	10.5	14.5	07.0	02.0	02.9	03.2	03.2	34	28	35	32	NNE	5	NW	5	N	3
14	752.8	751.3	750.3	07.0	16.0	11.2	11.4	16.5	04.6	02.0	04.6	06.4	06.9	61	47	69	59	-	0	S	2	-	0
15	746.0	744.7	747.2	08.2	08.2	06.2	11.5	16.0	06.0	05.4	07.7	07.9	06.3	95	97	89	94	S	2	SE	3	S	2
16	749.3	752.5	755.7	06.0	13.4	08.2	09.0	14.0	04.2	04.0	05.9	03.9	04.0	82	34	49	55	-	0	NW	4	WNW	3
17	757.6	758.7	758.7	08.6	15.8	08.8	10.5	16.5	03.5	04.6	04.6	05.4	05.4	52	34	64	50	NW	3	N	2	-	0
18	759.7	759.0	759.9	08.6	16.6	08.8	10.7	16.9	05.0	03.5	03.8	05.4	07.3	45	40	86	57	N	2	S	3	-	0
19	761.3	760.1	760.6	11.0	17.4	10.2	12.2	18.3	04.8	01.8	05.9	07.3	07.6	60	49	81	62	NNE	1	NNW	4	-	0
20	760.4	759.2	760.2	10.2	18.8	13.0	13.8	19.5	06.6	06.4	06.7	07.0	07.4	72	45	46	54	-	0	S	2	N	8
21	760.6	758.5	760.2	10.6	18.4	12.6	13.6	18.6	10.0	06.4	03.2	03.9	03.5	33	25	32	30	N	2	N	7	N	6
22	760.9	758.8	758.3	12.4	19.4	11.5	13.7	19.5	10.0	07.5	03.8	05.4	06.5	35	32	64	44	N	5	S	2	NE	1
23	757.8	756.7	756.2	12.0	21.8	15.4	16.2	22.5	06.5	03.5	07.5	07.6	08.8	72	39	67	59	-	0	SSE	4	-	0
24	755.8	754.4	753.2	12.8	21.2	15.2	16.1	22.2	06.6	03.6	08.3	10.0	08.2	74	53	63	63	-	0	SSE	3	-	0
25	752.8	755.5	758.7	13.4	17.4	13.6	14.5	18.0	10.0	06.0	03.6	07.5	04.4	03.4	65	30	29	41	NN				

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 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacije broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred. Dies				
1	8 02	03○	08	04.3	08.7	.	.	■ 0-16 <sup>20</sup>		
2	8 05	02○	00	02.3	05.7	.	.	■ 11-16 <sup>20</sup>		
3	8 07	10	04	07.0	00.5	.	.			
4	8 10	05○	06	07.0	08.5	.	.			
5	8 04	00○	00	01.3	03.7	.	.	△ 20-24		
6	8 01○	00○	00	00.3	10.8	.	.	△ 0-8		
7	8 04○	04○	08	05.3	10.0	.	.	△ 11-8 <sup>20</sup> ■ 22-24		
8	8 01○	00○	01	06.7	10.3	.	.	■ 0-5 △ 11-20 <sup>20</sup> 24		
9	8 02	03	00	01.7	05.7	.	.	△ 0-7 <sup>30</sup>		
10	8 00○	00○	00	00.0	10.2	.	.	△ 11-8 <sup>20</sup> 20-24		
11	8 00	00○	00	00.0	10.0	.	.	△ 11-0-8 <sup>20</sup> 20-24		
12	7 10	10○	10○	10.0	00.0	.	.	● 0-14 7 <sup>30</sup> 24 4		
13	8 10 <sup>E</sup> ●	10○	10	10.0	00.0	60.6	.	● 0-12 0-13 <sup>20</sup> 22 <sup>20</sup> 24; ■ 54.8, □ 64.9		
14	8 08	06	03	04.7	09.7	26.8	.	● 0-1 11 <sup>50</sup> 17		
15	8 02	03○	00	01.7	05.7	.	.	■ 11-12 <sup>20</sup>		
16	8 02○	01○	00	01.0	11.2	.	.	■ 8 <sup>20</sup> 15		
17	8 00○	00○	00	00.0	11.1	.	.	△ 0-1 0-8 <sup>10</sup> , 19 <sup>20</sup> 24		
18	8 00○	02○	00	00.7	11.1	.	.	△ 0-8 <sup>20</sup>		
19	8 04	00○	06	03.3	10.1	.	.	△ 11-7 <sup>30</sup>		
20	7 10	10○	10○	10.0	00.0	.	.	● 0-13 7 <sup>20</sup> 11, ■ 7 <sup>20</sup> 22		
21	7 10	10○	08	05.3	01.2	31.4	.	● 0-12 0-10 <sup>20</sup> 8 <sup>20</sup> 13 <sup>50</sup> 4, ■ 2 <sup>20</sup> 15 <sup>50</sup> 4		
22	8 06	00○	00	02.0	09.4	03.9	.	△ 0-1 0-8 <sup>20</sup> 20-24		
23	8 00○	01○	00	00.3	11.2	.	.	△ 11-0-8 <sup>20</sup> , 18 <sup>20</sup> 24		
24	8 00○	01○	00	00.3	11.0	.	.	△ 0-8 <sup>20</sup>		
25	8 06	10	08	08.0	03.9	.	.	■ 17 <sup>20</sup> , △ 20 <sup>20</sup> 24		
26	8 02	02○	00	01.3	10.1	.	.	△ 1-2 0-8 <sup>20</sup>		
27	8 00○	00○	00	00.0	11.0	.	.	■ 10 <sup>20</sup>		
28	8 08	04○	07	06.3	08.6	00.3	.	● 0-3 <sup>20</sup> 3 <sup>20</sup> 22 <sup>20</sup> 24, ■ 11 <sup>20</sup> 19 <sup>40</sup> 4		
29	7 10○	08	10○	09.3	00.0	02.9	.	■ 18 <sup>20</sup> , ● 0-1 10 <sup>20</sup> 24 4		
30	7 10○	10	10	10.0	00.0	12.7	.	● 0-9 4 <sup>20</sup> , ■ 9 <sup>20</sup> 10 <sup>20</sup> 4		
31	8 10○	10○	10○	10.0	00.0	14.8	.	■ 05 <sup>20</sup> 9 <sup>40</sup> 4 <sup>20</sup> , ● 0-1 19 <sup>20</sup> 24 4		
MES.	VRED.	04.6	04.0	03.7	04.1	220.9	153.6			

1	8 10●	10	10●	10.0	00.0	37.1	.	● 0-1 0-13 <sup>20</sup> 4, 19 <sup>20</sup> 24		
2	8 10	10●	10●	10.0	00.0	18.6	.	● 0-1 0-17 4, 19 <sup>20</sup> 24 4		
3	8 10●	08●	00	06.0	03.8	07.5	.	● 0-0 5 <sup>20</sup> 3 <sup>20</sup> 24 <sup>20</sup> , △ 1-2 19 <sup>20</sup> 24		
4	8 00	02○	00	00.7	06.1	00.3	.	△ 1-2 0-9 <sup>20</sup> , 18 <sup>20</sup> 24		
5	8 10	02○	00	04.0	08.4	.	.	△ 0-9, ■ 14 <sup>20</sup> 6 <sup>20</sup>		
6	8 02	02○	00	01.3	12.1	02.1	.	● 0-2 <sup>20</sup> 4, ■ 15 <sup>20</sup> 10 <sup>20</sup> , △ 1-2 19 <sup>20</sup> 24		
7	8 04○	08	00	04.0	07.8	.	.	△ 1-2 0-8 <sup>20</sup>		
8	8 07○	06	10	07.7	07.5	.	.			
9	8 10	08	08	06.7	01.3	.	.	■ 3 <sup>20</sup> 4 <sup>20</sup> , 14-14 <sup>25</sup> , ■ 6 <sup>20</sup> 14 <sup>40</sup> , ■ 0-12 <sup>20</sup> 12 <sup>55</sup> , 15 <sup>20</sup> 15 <sup>45</sup> , 21 <sup>20</sup> 02 <sup>25</sup>		
10	8 10	10●	09	09.7	04.3	00.8	.	T 6 <sup>20</sup> 7 <sup>20</sup> , 12-12 <sup>25</sup> , ● 1-2 7 <sup>20</sup> 10 <sup>20</sup> , 13 <sup>20</sup> 14 <sup>40</sup> , 21 <sup>20</sup> 22, ■ 8 <sup>20</sup> 9 <sup>20</sup> , ■ 12 <sup>20</sup> 13 <sup>20</sup> , △ 19 <sup>20</sup> 21		
11	8 02	02	00	01.3	12.0	05.2	.	■ 8 <sup>20</sup> 24		
12	8 02	04	02	02.7	12.2	.	.	■ 0-24 4		
13	8 00	02	00	00.7	11.1	.	.	■ 0-19 <sup>25</sup>		
14	8 10	08○	10	09.3	06.4	.	.			
15	7 10 <sup>E</sup> ●	10●	10●	10.0	00.1	20.2	.	● 0-0 17 <sup>35</sup> 4, 20 <sup>20</sup> 24 <sup>10</sup> ; ■ 11 <sup>20</sup> 12 <sup>20</sup> , ■ 7 <sup>20</sup> 8 <sup>20</sup> 4, 22 <sup>20</sup> 23 <sup>20</sup>		
16	8 06	03○	00	03.0	07.7	51.0	.	■ 8 <sup>20</sup> 17 <sup>40</sup>		
17	8 02○	02○	00	01.3	11.7	.	.	■ 3 <sup>20</sup> 5 <sup>20</sup>		
18	8 00○	00○	00	00.0	12.7	.	.	△ 1-2 20 <sup>20</sup> 24		
19	8 04○	02	00	02.3	06.7	.	.	△ 1-2 0-8 <sup>20</sup>		
20	8 06	10	03	00.3	06.4	.	.	■ 16 <sup>20</sup> 24		
21	8 02○	04○	00	02.0	12.1	.	.	■ 0-24		
22	8 02○	02○	00	01.3	12.7	.	.	■ 0-4 <sup>20</sup> , ■ 7 <sup>20</sup> 11		
23	8 07○	02○	02	03.7	10.8	.	.			
24	8 02	01○	00	01.0	11.1	.	.	■ 10 <sup>20</sup> 4 <sup>20</sup>		
25	8 10●	02○	00	04.0	07.6	00.3	.	● 0-6 <sup>20</sup> 8 <sup>20</sup> , ■ 6 <sup>20</sup> 17 <sup>20</sup> , ■ 19 <sup>20</sup> 21		
26	8 00○	00○	00	00.0	12.6	00.0	.	■ 6 <sup>20</sup> 18		
27	8 00○	00○	00	00.0	12.8	.	.			
28	8 10	02○	00	04.0	06.9	.	.			
29	8 04○	00○	00	01.3	12.6	.	.			
30	8 00○	01○	00	00.3	12.8	.	.			
MES.	VRED.	05.1	04.1	02.5	03.9	249.9	143.2			

$\gamma = 42^\circ 26' N \lambda = 19^\circ 17' E$  Gr.  $\Delta G = + 1h 17 min.$ 

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D	Vazdušni pritisak P mm			Temperatura vozduha T °C							Napon vodene pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	757.2	756.4	757.4	18.8	27.8	19.2	21.3	28.4	14.2	10.6	09.6	09.1	09.9	59	33	59	50	NNW	2	SE	2	WNW	1	
2	759.7	758.6	758.6	19.2	27.0	18.2	20.7	27.5	13.0	09.6	10.2	10.1	11.5	61	38	73	57	NNW	1	E	2	-	0	
3	759.1	757.1	756.3	17.6	28.2	18.2	20.6	29.2	14.0	09.5	09.2	09.2	11.5	61	32	73	55	-	0	S	2	-	0	
4	756.1	755.4	755.8	19.7	28.2	19.2	21.6	29.6	12.4	10.5	09.4	10.4	11.2	55	36	67	53	S	2	SSE	2	-	0	
5	756.1	759.1	759.2	18.0	18.4	16.4	17.3	21.6	16.3	13.6	10.2	13.3	12.9	66	84	92	81	E	2	NNW	2	-	0	
6	759.3	758.1	758.4	16.8	23.2	17.2	18.6	24.5	14.5	12.3	12.7	11.4	12.0	88	54	81	74	-	0	S	5	S	3	
7	757.6	755.8	756.5	16.4	21.4	15.8	17.4	24.5	13.4	11.5	11.8	10.4	10.3	85	54	65	69	-	0	W	5	-	0	
8	753.9	752.7	753.4	16.0	18.6	14.8	16.1	21.0	12.0	09.0	08.8	08.7	09.4	64	54	74	64	-	0	NNW	3	ESE	1	
9	755.4	757.0	756.4	11.6	18.2	10.6	12.8	20.0	10.4	09.0	09.3	09.9	09.4	91	63	98	84	NN	1	S	3	N	5	
10	756.8	756.9	757.3	11.6	13.4	11.2	11.9	16.5	10.0	09.5	09.8	08.9	07.9	95	77	80	84	NNW	2	NNW	4	1		
11	757.7	755.5	757.1	12.6	23.3	14.2	16.1	24.6	08.3	06.0	08.8	10.7	10.9	81	50	90	74	-	0	N	4	-	0	
12	756.8	750.9	754.9	15.8	22.4	15.0	17.1	23.4	11.8	09.3	09.3	08.6	10.7	69	42	84	65	N	2	SE	3	-	0	
13	755.4	754.1	754.4	15.8	23.0	15.4	17.4	23.0	10.6	09.0	09.1	09.3	10.5	68	44	80	64	NNE	1	S	4	S	2	
14	753.8	753.9	753.5	16.0	17.6	14.4	15.6	21.6	11.5	08.8	09.1	10.2	12.3	67	67	100	78	N	2	S	4	-	0	
15	753.1	750.9	751.1	13.2	16.8	13.0	14.0	18.2	12.5	12.0	10.2	10.3	10.7	89	72	96	86	-	0	NNW	3	-	0	
16	752.3	753.0	754.5	13.8	20.8	16.0	16.7	21.6	10.6	09.2	10.2	11.9	10.2	86	65	75	75	-	0	SSE	3	SE	2	
17	757.8	759.0	759.7	16.4	23.8	18.6	19.4	24.6	14.2	12.0	15.5	10.0	12.9	75	45	80	67	-	0	SE	2	S	1	
18	760.4	758.4	759.1	18.4	29.4	22.4	23.2	31.0	16.5	15.6	12.7	13.5	16.3	80	44	80	68	NW	2	-	0	-	0	
19	760.0	757.7	757.2	23.2	31.4	25.0	26.2	32.3	19.5	17.0	13.2	11.7	18.7	62	34	79	58	-	0	-	0	-	0	
20	758.7	759.4	760.2	21.2	30.2	22.8	24.3	30.4	18.6	16.6	16.3	14.4	16.1	86	45	78	70	-	0	SE	2	-	0	
21	759.4	758.7	758.4	23.2	23.6	20.2	21.8	26.5	19.1	16.2	13.5	16.4	13.5	63	75	76	71	NNW	2	NW	4	-	0	
22	757.4	757.3	758.1	20.0	27.2	18.6	21.2	28.5	17.2	14.9	12.2	12.1	13.9	70	45	86	67	N	4	S	5	6	-	0
23	758.4	757.0	757.0	20.2	28.4	23.0	23.7	29.2	14.6	11.8	11.8	11.0	12.7	67	38	60	55	-	0	S	4	N	5	
24	757.4	756.3	756.4	21.8	29.6	21.8	23.8	30.0	18.6	11.7	11.3	11.8	08.9	58	38	45	47	NW	3	SSE	2	NNE	4	
25	757.6	755.2	755.1	20.4	26.8	19.4	21.5	27.1	15.0	15.2	08.3	09.9	13.9	46	36	82	55	N	3	S	4	SE	1	
MES.	VRED.	756.9	756.0	756.4	17.4	23.7	17.5	19.1	25.1	14.0	11.5	10.5	10.8	11.7	71	50	78	66	1.5	3.0	1.2			

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1	755.8	756.8	756.9	16.4	23.6	18.0	19.0	24.8	12.0	08.7	11.6	08.8	06.7	83	40	56	60	-	0	W	2	NNW	6
2	757.0	757.2	756.5	17.2	17.4	14.0	15.7	19.2	14.0	13.0	07.7	10.0	11.5	52	72	96	73	N	5	N	1	-	0
3	755.1	753.5	752.8	14.0	17.6	16.2	19.2	21.8	12.0	05.8	13.1	11.5	81	87	84	84	-	0	S	2	-	0	
4	751.3	750.3	751.3	16.2	20.2	17.8	18.0	22.6	14.2	11.5	08.1	09.4	05.8	58	53	38	50	N	5	SSE	3	NNE	4
5	752.6	751.8	752.4	18.2	22.8	17.0	18.8	24.0	15.0	12.0	05.8	07.1	06.7	37	34	60	44	NNE	3	S	3	-	0
6	754.8	754.1	755.3	16.4	23.4	17.6	18.9	24.0	13.2	09.0	08.8	13.4	13.3	63	62	87	71	-	0	S	3	N	2
7	757.7	757.5	758.6	18.0	25.4	18.8	20.3	26.4	13.6	10.0	09.5	11.2	10.9	61	46	67	58	NNW	2	SSE	2	-	0
8	759.7	758.8	759.2	19.0	27.8	20.2	21.8	28.0	13.6	10.0	09.7	08.9	10.2	59	32	57	45	NW	2	S	3	-	0
9	760.0	758.0	757.0	20.8	30.8	22.0	23.9	31.2	15.0	11.0	10.7	11.2	11.8	58	34	59	50	NNE	2	SSW	3	-	0
10	756.9	753.8	754.2	22.8	32.0	24.0	25.7	32.2	16.6	13.0	11.4	16.2	17.5	55	45	78	59	NNW	2	S	3	-	0
11	754.1	753.4	754.7	23.6	31.0	22.0	24.7	31.5	19.0	16.4	13.0	13.0	12.6	59	35	64	54	-	0	S	5	N	6
12	755.2	754.0	754.7	24.4	28.6	23.2	24.9	31.0	19.2	17.2	14.4	14.5	13.8	63	49	65	59	NNE	1	SSE	2	NNE	2
13	755.2	754.0	755.3	23.4	31.8	24.0	25.8	32.2	19.4	17.2	17.5	17.8	18.8	81	50	84	72	N	2	S	2	-	0
14	754.5	754.3	752.6	24.4	31.6	24.8	26.4	32.5	20.0	19.4	13.8	12.4	13.0	60	35	55	50	N	2	S	5	-	0
15	753.3	751.9	751.9	23.6	30.0	22.0	24.4	30.4	18.6	16.0	12.1	12.2	13.8	55	38	69	54	WNW	1	SSE	4	SE	1
16	750.9	749.2	745.6	24.0	28.3	21.4	23.8	28.8	17.2	14.7	16.2	15.7	14.1	72	54	74	71	N	2	S	5	N	3
17	751.4	751.0	753.3	20.8	27.2	21.2	22.6	28.0	18.5	17.5	13.2	11.5	14.2	72	42	75	63	N	2	S	4	-	0
18	754.9	754.0	754.2	24.0	32.0	24.4	26.2	32.2	19.2	16.0	12.5	12.5	13.5	56	35	59	50	NNW	1	SSE	3	-	0
19	755.4	754.2	753.4	23.8	31.8	25.4	26.6	32.2	18.2	16.0	13.9	13.2	13.6	63	35	56	51	-	0	S	4	-	0
20	753.8	753.1	754.6	24.4	30.2	22.8	25.1	31.6	20.0	19.2	13.8	12.1	16.1	60	38	76	59	-	0	S	5	-	0
21	756.3	754.6	753.8	22.8	30.8	24.8	25.8	31.2	16.8	16.2	14.0	12.8	15.1	67	38	64	56	NNW	1	SSE	3	-	0
22	752.6	751.5	752.3	24.2	30.8	23.4	25.5	31.8	21.0	19.0	14.2	11.5	14.3	62	35	66	55	-	0	S	3	-	0
23	754.0	754.3	755.1	22.6	26.2	21.4	22.9	28.2	19.0	17.2	12.0	10.2	12.6	58	40	66	55	-	0	S	4	-	0
24	757.9	756.7	758.1	22.2	22.6	19.8	21.1	28.0	18.4	16.8	13.7	12.6	11.3	68	61	65	65	NNW	1	N	4	N	3
25	759.0	757.5	756.9	19.0	27.6	21.2	22.3	28.5	16.2	14.6	11.6	11.9	10.8	70	43	57	57	N	2</				

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijeme O	Oblačnost N (0-10)					Inobuduć broj	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 040	010	03	02.7	12.5	.	.	.	.	.
2	8 000	060	02	02.7	11.1	.	.	.	.	.
3	8 000	030	02	01.7	12.3	.	.	.	.	.
4	8 020	06	04	04.0	09.3	.	.	.	.	.
5	8 10	100	10	16.0	00.0	.	.	.	• <sup>0</sup> 932 1530	.
6	8 10	08	04	07.3	67.5	02.8	.	.	.	.
7	8 060	000	02	02.7	10.6	.	.	.	■ 1330 1430	.
8	8 050	060	100	07.0	68.9	.	.	.	■ 1530 1313, T' 1230, 1310, L' 14-20, R' 20-2030, • <sup>0</sup> 2030 2330	.
9	8 10	040	1040	08.0	03.9	02.8	.	.	• <sup>0</sup> 1442 430, 710 930, 1633 9330, 14 1630 24, ■ 1637	.
10	8 080	060	02	05.3	02.5	2531	.	.	• <sup>0</sup> 032 2, 142 740, 1032 1235, 14 932 1035, ■ 938	.
11	8 010	030	00	01.3	12.5	04.4	.	.	■ 932 1130	.
12	8 000	040	00	01.3	10.8	.	.	.	.	.
13	8 000	000	00	00.0	13.2	.	.	.	.	.
14	8 07	10	100	09.0	02.4	.	.	.	• <sup>0</sup> 2030 94	.
15	7 10	10	10	10.0	00.0	05.6	.	.	• <sup>0</sup> 032 635, 1512 20	.
16	8 030	020	02	02.3	12.2	05.6	.	.	.	.
17	8 10	060	07	07.7	04.8	.	.	.	.	.
18	8 08	040	02	04.7	08.0	00.1	.	.	• <sup>0</sup> 610 630	.
19	8 060	020	00	02.7	11.6	.	.	.	.	.
20	8 040	060	02	04.0	09.0	.	.	.	.	.
21	8 08	08	00	05.3	04.7	.	.	.	• <sup>0</sup> 1230 1230	.
22	8 030	040	04	03.7	11.5	00.0	.	.	■ 032 1630	.
23	8 020	020	00	01.3	12.7	.	.	.	■ 1330 24	.
24	8 020	020	00	01.3	12.7	.	.	.	■ 0-1, 1430 2330	.
25	8 000	000	00	00.0	13.7	.	.	.	■ 032 330	.
26	8 000	030	06	03.0	13.0	.	.	.	L' 21-24	.
27	8 07	08	08	07.7	01.5	00.1	.	.	• <sup>0</sup> 2-2, 032 130, 1032 1215, 1532 1630, ■ 2232 24	.
28	8 100	10	100	10.0	01.4	08.7	.	.	■ 0-730, 1032 21, • <sup>0</sup> 2-332 830, 1532 1630, 2032 2130, ■ 2232 432 630	.
29	8 030	030	04	03.3	13.0	02.7	.	.	.	.
30	8 020	020	02	01.2	14.0	.	.	.	.	.
31	8 000	000	00	00.0	14.0	.	.	.	.	.
MES. VRED.	04.5	04.5	03.8	04.4	275.7	61.9				

1	8 08	08	07	07.7	00.8	.	.	.	■ 14-1435, 0730 2130; • <sup>0</sup> 1430 1435, 2030 2030	.
2	8 10	100	100	10.0	00.0	00.0	.	.	■ 04-730, • <sup>0</sup> 1312 1530, 1932 2130	.
3	8 10	08	08	08.7	00.9	03.6	.	.	• <sup>0</sup> 1312 430, 2332 24	.
4	8 08	08	06	05.3	09.0	00.3	.	.	• <sup>0</sup> 083, ■ 041, 10-24	.
5	8 000	020	00	00.7	13.9	.	.	.	■ 0-5	.
6	8 040	08	03	05.0	09.6	.	.	.	.	.
7	8 020	020	00	01.3	13.5	.	.	.	.	.
8	8 000	020	00	00.7	13.7	.	.	.	.	.
10	8 000	000	00	00.0	13.9	.	.	.	.	.
11	8 020	030	06	03.7	12.9	.	.	.	■ 15-2330, ■ 1710 1915 i	.
12	8 010	08	00	33.0	08.6	.	.	.	■ 024	.
13	8 000	010	00	00.3	12.3	.	.	.	• <sup>0</sup> 1712 1735	.
14	8 000	060	00	02.0	13.4	00.0	.	.	.	.
15	8 010	030	00	01.3	14.0	.	.	.	.	.
16	8 08	030	00	03.7	13.3	.	.	.	.	.
17	7 10	060	00	05.3	08.5	.	.	.	• <sup>0</sup> 1532 1630	.
18	8 000	020	00	00.7	14.3	00.1	.	.	.	.
19	8 000	010	02	01.0	13.5	.	.	.	.	.
20	8 040	020	00	02.0	12.8	.	.	.	■ 1032 16, ■ 1532 1535, • <sup>0</sup> 1512 1530	.
21	8 000	040	00	01.3	12.1	00.3	.	.	.	.
22	8 010	000	00	00.3	13.8	.	.	.	.	.
23	7 070	050	00	04.0	10.2	.	.	.	■ 1230 1430	.
24	8 040	08	00	04.0	09.9	.	.	.	■ 1130 1215, T' 1215 1315, ■ 1332 1530, 1730	.
25	8 000	040	00	01.3	13.1	.	.	.	.	.
26	8 07	050	00	04.0	07.5	00.7	.	.	• <sup>0</sup> 132, 020, 1432, 5, 1432-1532	.
27	8 020	10	03	05.0	05.7	02.4	.	.	T' 1032 1332 i, • <sup>0</sup> 1232 1335	.
28	8 010	030	00	01.3	13.3	00.6	.	.	■ 732 1430	.
29	8 000	000	00	00.0	13.3	.	.	.	.	.
30	8 010	08	06	05.0	10.0	.	.	.	■ 2135 23, • <sup>0</sup> 2332 24, ■ 2336	.
MES. VRED.	03.0	04.4	01.5	03.0	321.1	08.0				

$\varphi = 42^{\circ}26'$ ,  $N$   $\lambda = 19^{\circ}17'$  E Gr.  $\Delta G = +1h\ 17\ min.$

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D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0—12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	758.2	757.1	758.2	20.2	26.0	21.4	22.3	28.7	20.0	17.0	13.2	13.0	11.5	74	51	60	62	W	2	N	5	NW	3
2	758.3	756.6	757.8	21.8	28.5	24.4	24.8	30.2	19.4	17.0	10.9	10.8	11.4	56	37	50	48	N	3	NNW	5	N	2
3	758.6	757.2	756.3	25.0	31.8	24.8	26.6	33.0	22.4	19.5	10.5	11.0	13.6	44	31	58	44	NW	2	N	5	-	0
4	755.8	753.5	753.0	25.2	31.2	25.0	26.6	32.6	21.0	19.2	12.2	13.2	13.8	51	39	58	49	NNW	2	SSE	4	SSW	1
5	752.8	751.4	750.7	24.0	31.0	25.3	26.4	31.5	19.5	17.2	13.5	12.0	12.6	60	36	52	49	W	1	S	4	S	3
6	750.6	751.4	752.9	22.2	24.2	21.6	22.4	27.0	18.7	18.3	14.6	15.8	16.4	73	70	85	76	-	0	-	0	-	0
7	755.0	754.0	755.0	23.0	30.0	24.0	25.3	30.5	18.1	15.9	12.4	13.3	16.5	59	42	74	58	N	3	S	4	S	2
8	754.9	755.0	754.6	22.8	32.0	24.6	26.0	32.6	19.0	17.4	13.7	10.9	13.4	66	31	58	52	N	2	SSE	2	E	2
9	754.7	754.4	754.9	24.4	31.2	25.6	26.7	32.3	20.7	18.2	14.7	12.9	16.0	64	38	65	56	-	0	S	5	S	2
10	755.4	754.8	754.4	25.9	31.0	25.6	27.0	31.2	22.8	20.4	16.0	17.6	16.0	64	52	65	60	-	0	S	4	S	3
11	754.7	753.3	753.6	25.2	31.0	24.8	26.5	32.5	20.0	17.5	11.0	10.2	0.9.2	46	30	39	38	NW	3	NE	2	N	5
12	755.1	754.0	754.9	23.8	30.2	25.2	26.1	31.5	21.0	19.2	10.3	0.8.2	10.4	47	26	43	39	NW	2	N	4	N	5
13	757.1	755.7	755.8	24.6	31.4	23.8	25.9	32.2	19.8	19.4	0.9.9	10.3	12.0	43	30	54	42	NNW	2	SSE	3	-	0
14	756.5	755.5	755.8	25.0	32.2	25.0	26.8	32.5	20.3	17.0	11.5	12.4	11.1	49	34	47	43	-	0	S	3	-	0
15	755.7	754.6	755.2	24.6	31.6	26.4	27.3	33.2	19.0	16.5	10.5	10.5	12.5	45	30	48	41	N	1	S	5	S	2
16	757.6	757.5	756.9	26.0	32.0	27.6	28.3	32.6	23.0	22.0	13.6	15.5	16.0	54	44	58	52	NNE	2	S	4	SSE	3
17	755.0	754.3	755.2	25.2	31.2	24.2	26.2	32.5	23.0	21.0	15.3	16.6	12.7	63	49	56	56	N	2	SSE	6	NW	3
18	756.5	754.2	753.9	22.4	31.8	24.8	26.0	32.4	20.5	20.0	11.8	11.3	15.5	58	32	66	52	NW	2	SSE	3	SSE	1
19	754.9	753.1	753.9	23.8	31.8	25.6	26.7	33.0	21.6	17.5	13.2	12.6	12.6	60	36	51	49	N	2	SSE	3	-	0
20	755.0	753.5	754.1	25.6	33.5	27.0	28.3	34.2	21.0	19.6	13.2	11.1	13.7	54	29	51	45	NNW	2	SSE	4	-	0
21	755.0	753.8	753.9	25.6	33.0	26.7	28.0	33.5	21.4	19.1	13.3	10.7	13.1	54	28	50	44	N	2	SSE	3	S	2
22	753.9	752.3	753.8	25.8	33.4	18.2	23.9	34.6	18.0	20.5	14.3	10.2	15.4	57	26	98	60	N	3	SSE	5	N	3
23	753.8	753.3	754.8	20.2	27.6	21.4	22.7	28.7	18.1	17.5	13.2	10.7	0.9.6	74	35	50	54	NW	3	NNW	4	NNE	6
24	755.0	753.8	752.9	24.8	30.8	25.6	26.7	30.8	16.7	16.2	0.9.0	10.7	11.8	38	32	48	39	NNW	4	N	6	NE	2
25	752.7	749.8	749.8	24.9	30.8	25.4	26.6	31.5	20.0	17.0	11.4	12.1	12.8	48	36	53	46	NNW	2	SSE	5	SE	4
26	751.5	751.6	751.9	24.0	28.4	25.2	25.7	30.0	19.0	16.8	13.4	14.3	16.2	60	49	67	59	NW	2	SSM	5	S	3
27	753.0	753.9	755.5	18.4	28.6	22.4	23.0	29.5	18.2	18.0	15.9	12.3	15.4	100	42	76	73	NW	2	SSE	4	-	0
28	755.7	754.5	754.9	22.2	30.8	23.6	25.1	31.2	18.6	16.2	13.1	13.1	13.9	65	39	64	56	NNW	2	SSW	2	-	0
29	755.5	754.1	753.8	24.3	33.6	25.6	27.3	33.8	18.9	18.4	13.7	11.4	13.8	60	29	56	48	N	2	S	2	N	2
30	754.7	753.1	752.9	26.2	35.5	27.2	29.0	35.8	21.0	18.4	13.5	11.1	13.3	53	26	49	43	N	3	-	0	-	0
31	752.2	751.1	750.2	25.8	31.8	26.6	27.7	33.6	22.5	20.0	13.7	12.6	11.8	55	36	45	45	-	0	SE	6	S	5
MES.	VRED.	755.0	753.9	754.2	24.0	30.9	24.7	26.1	31.9	20.1	18.3	12.8	12.2	13.4	58	37	58	51	1.9	3.8	2.1		

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1	749.2	750.7	751.7	23.4	26.2	19.4	22.1	27.4	18.6	18.0	12.5	12.6	13.3	58	49	79	62	SSE	3	SSE	4	NNW	1
2	751.8	751.8	752.8	22.0	27.9	22.1	23.5	28.4	18.1	15.8	11.2	12.3	12.7	56	44	64	55	S	2	S	4	NNW	3
3	755.4	755.5	756.6	19.0	26.1	21.8	22.2	28.0	18.0	15.0	14.1	13.2	13.6	86	52	69	69	-	0	SSW	2	-	0
4	758.8	758.0	758.6	21.6	30.6	23.8	25.0	30.8	18.0	15.4	12.2	12.2	13.5	63	37	61	54	NNW	1	SSE	2	-	0
5	758.7	757.4	755.2	23.3	32.8	25.3	26.7	33.1	19.8	16.9	13.3	13.4	15.2	62	36	63	54	N	2	SSE	3	-	0
6	753.9	753.9	753.0	25.2	31.8	24.8	26.7	32.2	18.2	14.2	13.8	16.3	13.0	58	46	55	53	-	0	N	2	N	4
7	752.8	751.9	752.7	25.6	32.4	27.2	28.1	32.6	24.4	21.0	11.7	13.6	11.5	47	37	42	42	NNE	4	SSE	3	NNE	3
8	754.1	754.1	756.0	24.0	32.0	22.8	25.4	32.0	22.2	20.3	12.0	13.8	14.1	54	39	68	54	SW	3	S	3	W	2
9	757.0	755.8	757.0	20.7	31.6	22.8	24.5	32.0	19.5	17.4	12.4	13.5	14.9	68	39	72	60	N	2	S	3	-	0
10	757.5	755.6	755.4	23.0	32.0	24.0	25.8	32.6	20.4	17.0	13.6	14.2	15.2	64	40	68	57	NNW	1	SSE	2	-	0
11	755.6	754.2	754.1	23.2	32.8	24.5	26.3	32.9	19.9	16.9	14.8	12.8	14.2	70	34	62	55	W	3	S	4	S	2
12	754.4	753.5	754.5	23.8	32.6	25.2	26.7	33.0	21.0	19.4	13.5	16.1	15.3	61	44	63	56	N	5	S	4	N	2
13	755.0	755.7	756.1	22.4	30.4	23.6	25.0	32.0	20.0	16.6	12.7	13.3	14.8	62	41	68	57	NNW	2	SSM	3	NNW	2
14	756.6	755.4	756.5	22.9	29.0	19.2	22.6	30.1	17.8	16.6	15.9	12.4	11.8	71	41	70	62	N	4	NW	4	N	4
15	757.6	756.5	757.5	19.2	28.8	22.8	23.4	29.4	16.8	14.6	10.4	13.1	16.1	62	44	78	61	N	3	S	5	-	0
16	762.0	756.6	757.6	22.8	31.2	25.8	26.4	31.8	18.8	15.4	11.4	12.3	0.9.6	55	36	38	43	NNW	1	NNE	2	NNE	3
17	757.8	756.3	756.3	22.6	32.4	24.8	26.2	32.0	20.8	17.4	11.9	12.6	14.0	58	35	60	51	N	3	S	3	W	2
18	757.7	756.2	756.3	24.6	34.0	24.0	26.7	34.4	20.8	17.0	13.1	11.8	12.5	56	30	56	47	NW	2	SSE	3	-	0
19	755.2	753.3	752.5	24.2	30.4	25.4	26.4	31.2	19.8	16.8	12.4												

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 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vremens O.	Oblačnost N (0-10)					Insolacije broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	020	060	08	05.3	07.8	03.1	.	$\bullet^{\circ} 0-0^{\circ}, \overline{F}_{NNW} 13^{\circ}-15^{\circ}$	.
2	8	060	040	00	03.3	13.0	.	.	$\overline{F}_{NNW} 8^{\circ}-10^{\circ}$	.
3	8	000	020	00	00.7	13.6	.	.	.	.
4	8	000	060	00	02.0	13.1	.	.	.	.
5	8	000	040	04	02.7	10.3	.	.	.	.
6	8	08	06	00	04.7	04.0	.	.	$R_{\Delta} 7^{\circ}-12^{\circ}, \bullet^{+4} 7^{\circ}-12^{\circ}$	.
7	8	000	000	00	00.0	14.0	10.7	.	.	.
8	8	000	060	00	02.0	05.0	.	.	$\overline{F}_{SSW} 8-10^{\circ}$	.
9	8	080	000	01	03.0	12.2	.	.	.	.
10	8	05	020	00	02.3	09.0	.	.	.	.
11	8	010	050	00	02.0	11.9	.	.	$\overline{F}_{NNW} 14^{\circ}-17^{\circ}$	.
12	8	030	040	00	02.3	12.6	.	.	$\overline{F}_{NNW} 10^{\circ}-17^{\circ}$	.
13	8	000	000	00	00.0	14.0	.	.	.	.
14	8	000	010	00	00.3	13.5	.	.	.	.
15	8	000	070	07	04.7	09.6	.	.	$\overline{F}_{SSW} 14^{\circ}-19^{\circ}$	.
16	8	08	010	00	03.0	11.8	.	.	.	.
17	8	000	040	00	01.3	11.3	.	.	$\overline{F}_{SSW} 10-19^{\circ}, R_{\Delta} 16^{\circ}-19^{\circ}$	.
18	8	000	020	00	00.7	13.6	.	.	.	.
19	8	020	030	00	01.7	13.1	.	.	.	.
20	8	010	020	00	01.0	13.3	.	.	.	.
21	8	000	020	00	00.7	12.5	.	.	.	.
22	8	020	040	08	04.7	07.4	.	.	$\overline{F}_{SW} 12^{\circ}-20^{\circ}, R_{\Delta} 15^{\circ}-20^{\circ}, \bullet^{+4} 15^{\circ}-19^{\circ}$	.
23	7	07	050	00	04.0	05.4	08.7	.	$\overline{F}_{NNW} 11^{\circ}-14^{\circ}, \overline{F}_{NNW} 12^{\circ}-24^{\circ}$	.
24	8	020	020	00	01.3	13.4	00.2	.	$\overline{F}_{NNW} 0-16^{\circ}$	.
25	8	000	010	00	00.3	13.4	.	.	.	.
26	8	040	050	03	04.0	12.3	.	.	.	.
27	8	080	020	00	03.3	09.6	13.2	.	$\bullet^{+4} 15^{\circ}-17^{\circ}, \square 21^{\circ}-24^{\circ}$	.
28	8	000	020	00	00.7	13.5	00.7	.	$\square 0-9^{\circ}$	.
29	8	000	000	00	00.0	13.7	.	.	.	.
30	8	000	000	00	00.0	13.3	.	.	.	.
31	7	040	060	02	04.0	11.3	.	.	$\overline{F}_{SSW} 0-0^{\circ}, 9^{\circ}-24^{\circ}$	.
MES. VRED.		02.3	03.0	01.1	02.1	356.9	36.6			

1	8	06	040	02	04.7	05.2	03.4	.	$\overline{F}_{NNW} 2^{\circ}, 7^{\circ}-11^{\circ}, 15^{\circ}-18^{\circ}, R_{\Delta} 15^{\circ}-2, \overline{F}_{S} 12^{\circ}-14^{\circ}$	.
2	8	020	040	08	04.7	11.2	03.8	.	$\overline{F}_{NNW} 3^{\circ}-5^{\circ}, \overline{F}_{NNW} 22^{\circ}-23^{\circ}, \bullet^{+4} 0^{\circ}-2^{\circ}, \overline{F}_{S} 1-10^{\circ}$	.
3	8	010	060	00	02.3	11.8	07.8	.	.	.
4	8	000	020	00	00.7	13.3	.	.	.	.
5	8	020	040	00	02.0	11.7	.	.	.	.
6	8	020	050	00	02.3	06.9	.	.	$R_{\Delta} 14^{\circ}-15^{\circ}, \overline{F}_{NNW} 14^{\circ}-14.5^{\circ}, \triangle 14^{\circ}-14.5^{\circ}, \nabla^{+4} 14^{\circ}-15^{\circ}$	.
7	8	000	040	00	01.3	12.4	16.3	.	$\overline{F}_{NNW} 0-11^{\circ}, 20^{\circ}-24^{\circ}, 0-13^{\circ}, \square 18^{\circ}-19^{\circ}$	.
8	8	08	060	04	06.0	06.1	.	.	$\overline{F}_{NNW} 19^{\circ}-21^{\circ}, \bullet^{+4} 17^{\circ}-18^{\circ}, \overline{F}_{SSW} 17^{\circ}-18^{\circ}$	.
10	8	020	040	00	02.0	11.0	.	.	.	.
11	8	000	020	00	00.7	11.4	.	.	.	.
12	8	020	000	00	00.7	12.7	.	.	.	.
13	8	08	10	00	06.0	06.2	.	.	$\overline{F}_{NNW} 14^{\circ}-16^{\circ}, \overline{F}_{NNW} 10^{\circ}-17^{\circ}, \overline{F}_{NNW} 10^{\circ}-16^{\circ}, \bullet^{+4} 10^{\circ}-10.5^{\circ}, 14^{\circ}-16.5^{\circ}$	.
14	8	060	060	00	04.0	06.6	.	.	$\overline{F}_{NNW} 14^{\circ}-16^{\circ}, \overline{F}_{NNW} 10^{\circ}-17^{\circ}, \overline{F}_{NNW} 10^{\circ}-16^{\circ}, \bullet^{+4} 10^{\circ}-10.5^{\circ}, 14^{\circ}-16.5^{\circ}$	.
15	8	000	010	00	00.3	12.7	06.0	.	.	.
16	8	000	020	00	00.7	12.1	.	.	$\overline{F}_{S} 15^{\circ}-15.5^{\circ}$	.
17	8	000	000	00	00.0	12.8	.	.	.	.
18	8	030	040	00	02.3	11.9	.	.	.	.
19	8	050	060	08	06.3	06.8	.	.	$\overline{F}_{NNW} 8^{\circ}-20^{\circ}, \bullet^{+4} 10^{\circ}, \square 10-23^{\circ}$	.
20	8	020	030	00	01.7	12.1	00.0	.	$\overline{F}_{S} 14^{\circ}-21^{\circ}, \bullet^{+4} 10^{\circ}, \square 10-23^{\circ}$	.
21	8	08	06	08	07.3	04.0	.	.	$\bullet^{+4} 7^{\circ}-10^{\circ}, \overline{F}_{SSW} 23-24^{\circ}$	.
22	7	10	10	08	09.3	02.6	00.3	.	$\overline{F}_{NNW} 0^{\circ}-13^{\circ}, \bullet^{+4} 20^{\circ}-35^{\circ}, 0-20^{\circ}, 10-22^{\circ}, 10-10^{\circ}, T 12^{\circ}-14^{\circ}, \nabla^{+4} 13^{\circ}-14^{\circ}, 10-18^{\circ}, \square 19^{\circ}-20^{\circ}$	.
23	8	040	060	10	06.7	08.7	10.0	.	$\overline{F}_{NNW} 14^{\circ}-15^{\circ}, \overline{F}_{NNW} 20^{\circ}-22^{\circ}, \square 18^{\circ}-20^{\circ}, \triangle 18^{\circ}-20^{\circ}$	.
24	7	10	100	04	08.0	05.0	28.2	.	$\overline{F}_{NNW} 3^{\circ}-5^{\circ}, \nabla^{+4} 4^{\circ}-6^{\circ}, \triangle 4^{\circ}-4.5^{\circ}, \overline{F}_{NNW} 4^{\circ}-4.5^{\circ}, 12^{\circ}-23^{\circ}, \bullet^{+4} 5^{\circ}-6^{\circ}, \overline{F}_{NNW} 5^{\circ}-6^{\circ}, 12^{\circ}-23^{\circ}, T 12^{\circ}-14^{\circ}$	.
25	8	000	010	00	00.3	12.6	02.8	.	$\overline{F}_{S} 9^{\circ}, 10^{\circ}$	.
26	8	000	000	00	00.0	12.7	.	.	.	.
27	8	000	000	00	00.0	12.6	.	.	.	.
28	8	000	000	00	00.0	12.0	.	.	.	.
29	8	000	000	00	00.0	12.3	.	.	.	.
30	8	000	010	01	00.7	12.2	.	.	$\overline{F}_{NNW} 20^{\circ}-21^{\circ}, \overline{F}_{NNW} 22^{\circ}-23^{\circ}$	.
31	8	08	040	10	07.3	08.8	.	.	$\overline{F}_{NNW} 14^{\circ}-16^{\circ}, \overline{F}_{NNW} 15^{\circ}-17^{\circ}, \nabla^{+4} 16^{\circ}-18^{\circ}, \square 18-23^{\circ}$	.
MES. VRED.		03.0	03.7	02.0	02.9	308.6	78.6			

$\varphi = 42^{\circ}26'$  N  $\lambda = 19^{\circ}17'$  E Gr.  $\Delta G = +1$  h 17 min.

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5	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina vetrova D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	755.0	755.1	755.2	22.6	31.2	24.4	25.7	31.8	20.8	20.0	15.3	12.9	16.8	74	38	73	62	W	3	ESE	4 - 0		
2	755.7	754.1	754.8	22.8	30.2	20.4	23.5	31.0	19.0	17.2	14.7	13.4	14.4	71	42	80	64	NNW	2	SSW	3 NW 1		
3	754.1	753.8	754.8	20.3	25.4	23.4	23.1	27.6	19.4	18.0	14.9	14.5	11.5	84	60	53	66	SE	2	SE	4 NE 2		
4	755.1	754.1	755.6	21.6	30.8	25.4	25.8	30.8	19.9	17.3	10.6	09.8	09.2	55	29	38	41	-	0	N	5 N 5		
5	757.2	756.0	757.8	23.2	32.0	25.0	26.3	32.0	21.0	18.0	10.0	10.0	12.9	47	28	54	43	NW	3	NE	3 N 1		
6	759.7	759.0	760.2	24.0	31.4	25.2	26.5	32.0	21.0	14.9	11.3	11.8	10.4	51	34	43	43	N	5	N	3 N 2		
7	760.5	758.6	759.0	24.2	30.4	25.6	26.5	32.0	21.5	19.0	10.9	11.6	11.1	48	35	45	43	NW	3	NNW	3 N 3		
8	755.7	758.3	756.6	23.8	31.6	25.4	26.6	32.5	21.6	18.4	15.2	11.1	12.1	60	32	50	47	-	0	S	5 N 4		
9	756.1	753.8	755.3	22.2	30.2	22.6	24.4	31.0	21.2	19.2	11.1	11.2	14.1	55	35	68	53	N	3	S	3 - 0		
10	759.2	759.5	760.9	17.0	22.2	18.1	18.9	23.4	13.5	11.8	06.8	06.4	06.3	47	32	40	40	N	8	N	7 N 5		
11	761.2	760.6	762.3	18.0	25.2	18.0	19.8	25.6	17.2	13.3	05.4	07.7	08.9	35	32	57	41	N	5	SSE	4 - 0		
12	763.0	760.9	760.5	17.8	29.2	20.8	22.2	29.4	14.3	11.4	10.3	13.6	12.4	68	45	67	60	-	0	S	4 - 0		
13	759.7	757.7	758.6	20.0	30.8	21.6	23.5	31.0	16.5	13.0	10.3	10.3	12.5	59	31	65	52	-	0	S	3 - 0		
14	760.6	761.5	763.2	23.3	26.8	20.1	22.6	27.2	17.5	14.5	12.5	10.5	09.3	58	40	53	50	N	6	N	8 N 5		
15	761.7	759.1	758.1	17.8	26.4	19.4	20.8	26.8	15.0	13.4	09.6	11.6	11.0	63	45	65	58	NW	2	SSE	4 S 1		
16	755.8	753.9	753.8	16.7	26.0	20.8	21.1	26.2	14.5	11.0	11.4	12.1	13.2	80	48	72	67	N	1	N	3 - 0		
17	753.5	752.9	752.9	17.4	25.2	22.2	23.8	26.5	15.0	12.0	11.6	08.2	12.5	78	34	62	58	-	0	S	5 S SE 6		
18	754.0	756.1	755.2	17.4	22.7	18.5	19.3	23.7	17.3	14.4	14.9	14.9	15.5	100	72	97	90	E	3	S	5 S 5		
19	758.9	758.9	758.5	17.9	26.5	20.8	21.5	26.7	16.2	14.4	13.5	15.7	93	52	85	77	-	0	S	3 - 0			
20	756.7	754.8	755.9	18.6	23.4	17.8	19.4	23.6	17.6	17.5	15.5	17.1	14.1	96	79	92	89	WNW	2	NW	2 N 4		
21	755.7	757.7	757.5	18.2	24.8	17.0	19.3	25.0	17.0	15.6	14.5	09.5	12.3	93	40	85	73	-	0	S	3 - 0		
22	758.1	758.3	758.3	15.4	23.0	16.0	17.6	23.0	14.2	13.1	12.6	13.0	12.7	96	62	93	84	-	0	S	4 W 2		
23	755.0	754.0	754.4	15.8	19.7	16.4	17.1	21.7	15.2	13.7	12.1	12.8	13.3	90	74	95	86	W	2	W	2 N 2		
24	753.4	753.8	757.9	14.4	20.2	15.4	16.4	20.5	13.8	13.4	11.5	11.3	07.9	94	63	60	72	E	2	-	0 N N 2		
25	759.5	759.1	760.0	10.8	20.0	16.2	15.8	20.8	09.0	07.0	08.4	09.0	08.7	86	51	63	67	-	0	S	1 N 2		
26	761.0	761.0	762.1	15.8	22.0	17.5	18.2	22.6	14.6	12.9	07.8	09.6	07.8	58	48	52	53	WNW	3	S	3 N E 4		
27	762.3	762.1	763.4	14.7	22.0	15.7	17.0	23.2	13.6	10.4	07.5	06.7	05.6	60	34	42	45	W	3	N	5 N 6		
28	764.9	765.1	766.4	12.9	19.2	13.8	14.9	19.5	12.0	10.2	05.8	07.6	05.6	52	46	47	48	N	7	N	7 N 6		
29	769.2	766.8	766.9	10.8	17.4	10.2	12.2	17.6	10.0	07.5	03.8	06.4	06.1	39	43	66	49	N	4	E	3 - 0		
30	767.0	765.1	764.1	07.7	19.8	11.6	12.7	20.1	06.0	01.8	06.3	06.6	08.0	79	38	78	65	-	0	S	2 - 0		
MES.	RED.			758.6	758.0	758.6	18.1	25.5	19.5	20.7	26.2	16.2	13.9	10.8	10.8	11.1	69	45	65	60	2.3	3.7	2.3

## 1977 OKTOBAR

## TITOGRAD

1	763.6	760.9	760.1	10.3	20.8	12.3	13.9	21.5	08.4	04.2	06.2	08.0	09.9	66	43	92	67	NNW	2	SSE	2 - 0
2	757.0	754.9	752.2	13.5	14.5	15.0	14.5	16.5	10.8	07.8	09.1	11.5	12.5	78	93	98	90	-	0	-	0
3	753.0	754.6	759.9	11.8	18.6	12.6	13.9	19.2	11.0	10.2	10.1	07.2	05.7	98	45	53	65	NW	6	N	7 N 5
4	764.7	763.7	764.3	11.6	18.8	11.0	13.1	19.4	09.4	04.8	05.4	06.2	06.8	53	38	69	53	-	0	SE	3 N 2
5	764.7	763.3	763.0	10.2	20.6	10.8	13.1	20.8	08.0	03.2	05.9	07.4	07.3	63	41	75	60	NNW	3	SSE	2 NNE 2
6	762.2	760.0	759.8	11.2	21.6	14.5	15.5	22.1	09.0	04.2	06.2	09.1	09.5	63	47	77	62	NNW	2	SSE	3 - 0
7	759.0	767.8	757.5	13.6	23.0	15.2	16.8	23.6	11.4	07.8	09.0	11.3	11.6	77	53	90	73	N	2	-	0
8	756.8	755.0	754.3	13.8	24.0	15.0	17.0	25.0	12.5	08.5	09.1	11.0	11.0	77	49	86	71	-	0	SE	1 - 0
9	752.9	751.4	752.5	14.0	24.8	17.4	18.4	26.4	12.1	09.8	11.1	13.1	14.1	93	56	94	81	-	0	SSE	2 ESE 1
10	753.9	754.9	756.9	15.4	21.6	17.4	18.0	22.2	15.0	11.4	12.9	15.2	14.6	98	78	98	91	NNE	1	SE	3 - 0
11	754.1	756.3	757.4	16.6	15.4	13.8	14.9	18.1	13.8	12.7	13.9	12.7	11.8	98	97	100	98	W	4	WNW	1 WNW 2
12	758.1	758.0	758.2	13.9	20.2	13.9	15.5	21.2	12.7	10.4	11.5	11.3	11.3	97	63	95	85	NN	1	-	0
13	758.6	758.3	759.4	14.8	21.2	17.8	17.9	23.0	13.2	10.6	10.3	11.6	09.1	82	61	59	67	-	0	E	2 N 1
14	758.9	756.9	758.9	17.4	23.6	18.9	19.7	24.0	17.0	12.7	07.1	08.2	07.3	48	38	45	44	N	4	N	5 NNE 6
15	758.0	757.9	759.4	15.4	23.2	17.2	18.3	23.6	15.0	10.6	07.0	09.5	08.9	53	44	60	52	NNW	2	SSE	2 NNW 1
16	760.6	760.0	761.5	16.0	22.6	16.2	17.8	22.7	13.4	08.4	07.3	07.7	06.1	54	37	44	45	WNW	1	NNE	4 N 3
17	763.3	762.0	763.4	12.3	19.6	11.4	13.7	19.8	10.8	09.0	05.7	07.1	07.1	53	41	70	55	S	2	S	2 - 0
18	765.3	764.7	766.0	09.8	20.8	12.4	13.9	21.4	08.0	04.0	06.1	07.8	07.3	67	42	68	59	-	0	SE	1 - 0
19	766.8	765.9	765.9	10.2	20.2	11.2	13.2	21.0	09.0	04.6	06.5	09.3	09.2	70	52	92	71	N	2	-	0
20	766.3	765.0	765.7	09.6	20.2	11.8	13.4	21.6	08.4	05.2	07.9	10.5	09.7	88	59	93	80	-	0	SSE	2 - 0
21	765.7	764.5	765.6	08.7	23.2	13.2	14.6	23.2	07.2	04.2	08.3	07.9	07.2	99	37	63	66	-	0	-	0 NNE 2
22	766.4	765.5	766.8	10.0	22.4	11.4	13.8	22.4	08.5	05.0	06.7	08.0	08.3	73	40	82	65	N	3		

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 $H_s = 49m H_b = 50.6 m h_t = 2.0 m h_r = 1.2 m$ 

Dan	Vr. Mj.	Oblačnost N (0-10)				Insečija bez sen.	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21				
1	8	000	020	01	01.0	11.6	06.4	.	
2	8	000	060	02	02.7	09.9	.		
3	8	08	10	07	08.3	01.8	00.5	.	
4	8	000	000	02	00.7	10.4	00.5	.	
5	8	000	040	00	01.3	11.6	.		
6	8	020	060	00	02.7	11.0	.		
7	8	000	030	00	01.0	11.1	.		
8	8	000	000	00	00.0	11.4	.		
9	8	000	020	00	00.7	10.5	.		
10	8	020	020	00	01.3	11.6	00.4	.	
11	8	10	030	00	04.3	06.5	.		
12	8	000	000	00	00.0	12.0	.		
13	8	000	030	00	01.0	11.4	.		
14	8	000	010	02	01.0	11.3	.		
15	8	000	020	00	00.7	11.3	.		
16	8	000	010	00	00.3	11.2	.		
17	7	040	070	08	06.3	06.2	.		
18	8	10	080	100	09.3	03.0	67.0	.	
19	8	08	040	06	06.0	07.4	27.6	.	
20	8	100	09	100	09.7	00.1	02.3	.	
21	7	020	060	06	04.7	08.1	10.5	.	
22	8	060	080	10	08.0	03.7	00.5	.	
23	8	10	10	10	10.0	03.0	05.1	.	
24	8	10	020	00	04.0	04.8	05.9	.	
25	8	060	060	00	04.0	04.2	.		
26	8	060	040	10	06.7	08.6	.		
27	8	010	040	02	02.3	10.6	.		
28	8	020	000	00	00.7	11.1	.		
29	8	000	000	00	00.0	11.1	.		
30	8	000	000	00	00.0	10.9	.		
MES. VRED.		03.2	03.8	02.9	03.3	257.4	126.7		

## TITOGRAD

1977 OKTOBAR

1	8	000	000	00	00.0	10.7	.		
2	8	10	10	100	10.0	00.0	.		
3	8	080	060	00	04.7	05.8	17.9	.	
4	8	000	010	00	00.3	11.0	02.5	.	
5	8	000	000	00	00.0	11.1	.		
6	8	020	000	00	00.7	10.8	.		
7	8	020	040	00	02.0	10.2	.		
8	8	000	000	00	00.0	10.3	.		
9	8	020	080	100	06.7	06.8	.		
10	8	100	040	100	08.0	03.3	14.5	.	
11	7	060	100	100	10.0	00.0	23.3	.	
12	8	06	07	00	04.3	05.2	38.0	.	
13	8	070	060	00	04.3	04.4	.		
14	8	010	000	00	00.3	09.8	.		
15	8	000	030	00	01.0	09.5	.		
16	8	000	010	00	00.3	09.6	.		
17	8	000	000	00	00.0	09.7	.		
18	8	000	000	00	00.0	09.7	.		
19	8	000	000	00	00.0	09.8	.		
20	8	04	000	00	01.3	09.7	.		
21	8	000	000	00	00.0	09.9	.		
22	8	000	000	00	00.0	09.8	.		
23	8	000	000	00	00.0	09.4	.		
24	8	000	000	00	00.0	09.1	.		
25	8	020	020	00	01.3	08.8	.		
26	8	000	000	00	00.0	09.0	.		
27	8	000	000	00	00.0	09.3	.		
28	8	000	020	02	01.3	09.2	.		
29	8	000	000	00	00.0	09.5	.		
30	8	000	000	00	00.0	08.8	.		
31	8	040	030	00	02.3	06.1	.		
MES. VRED.		02.2	02.2	01.4	01.9	256.3	96.2		

$\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$  Gr.  $\Delta G = + 1h 17 min.$ 

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DEN	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max.	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	758.8	758.0	756.4	11.4	18.5	13.4	14.2	19.0	11.0	07.5	08.1	10.5	11.3	80	66	98	81	-	0	S 1 - 0	
2	756.9	756.0	757.1	11.2	15.9	13.0	13.3	16.0	10.4	07.0	09.5	10.7	11.0	95	79	98	91	N	2	- 0 - 0	
3	758.5	759.2	760.9	09.5	17.8	10.6	12.1	22.8	09.0	06.8	08.6	09.8	09.1	96	64	95	85	-	0	SSE 1 - 0	
4	761.8	760.4	761.7	09.0	20.2	12.1	13.4	20.2	09.0	06.0	08.2	10.2	10.2	95	57	97	83	NNW 1	SSE 1 - 0		
5	762.0	761.4	762.2	12.2	17.2	12.4	13.6	17.2	12.0	07.5	08.8	10.4	10.3	82	71	96	83	-	0	- 0 - 0	
6	761.9	762.2	761.7	12.6	18.6	15.0	15.3	18.7	12.3	09.5	10.2	13.0	11.7	93	81	92	89	-	0	N 2 - 0	
7	762.0	762.2	763.5	13.4	21.0	13.6	15.4	21.2	13.0	11.5	11.3	12.8	10.8	98	69	93	87	-	0	SE 2 - 0	
8	764.3	763.9	764.4	09.4	21.6	12.2	13.9	22.0	09.0	07.0	08.6	12.0	10.2	98	62	96	85	-	0	- 0 - 0	
9	765.6	765.4	764.5	09.0	20.7	11.0	12.9	20.8	09.0	07.0	08.0	10.5	09.4	93	57	95	82	-	0	S 2 - 0	
10	763.6	762.6	763.6	09.8	18.0	12.0	13.0	18.4	09.4	06.4	06.9	09.0	09.3	76	58	89	74	N	3	E 1 - 0	
11	764.0	763.8	764.6	12.4	22.4	12.4	14.9	23.8	12.0	07.0	08.5	09.6	09.4	78	47	87	71	N	2	S 3 - 0	
12	763.7	762.4	760.3	09.8	21.1	12.2	13.8	21.4	09.0	06.5	07.1	09.7	09.9	79	52	93	75	-	0	S 2 - 0	
13	756.8	753.5	750.8	10.8	16.2	14.5	14.0	16.7	10.6	06.7	08.5	10.6	12.3	87	77	99	88	-	0	- 0 - 0	
14	747.9	748.5	748.8	16.2	14.4	13.2	14.5	18.0	13.0	08.6	11.4	10.5	09.9	83	86	87	85	E	4	- 0 - 0	
15	749.1	748.8	748.5	11.8	16.6	13.2	13.7	17.4	11.4	10.5	09.9	11.5	11.1	95	81	98	91	-	0	SSE 2 - 0	
16	746.6	742.9	742.6	14.8	13.8	13.0	13.7	18.0	12.6	11.0	11.3	16.8	08.2	90	92	73	85	SSE 1	SSE 3 SSE 4		
17	746.2	749.2	757.2	07.0	15.2	08.9	10.0	16.0	07.0	05.4	07.3	10.9	07.6	97	84	89	90	NW 1	S 3 S 5		
18	757.4	750.0	752.7	10.2	11.8	09.8	10.4	15.2	08.9	07.0	09.1	09.4	07.4	98	91	81	90	-	0	NW 3	
19	754.6	756.0	758.6	07.8	09.4	08.4	08.5	10.6	07.8	07.5	07.7	07.6	04.7	97	85	56	79	WNW 1	WNW 1 NNW 4		
20	758.5	755.9	756.7	07.2	11.8	05.2	07.4	13.5	05.0	05.0	04.5	05.5	04.8	59	53	72	61	WNW 2	SE 3 N 3		
21	758.0	756.2	756.0	02.4	09.2	06.6	06.2	10.6	02.0	00.0	04.2	05.6	05.7	78	64	79	74	-	0	SSE 1 - 0	
22	753.1	750.2	751.1	07.0	14.0	12.6	11.6	15.0	07.0	00.0	07.3	11.7	10.9	97	98	100	98	SSE 1	S 8 - 0		
23	752.9	752.8	757.1	12.0	13.6	09.0	10.9	14.0	09.0	01.5	10.3	11.4	07.3	98	88	94	-	0	NNW 1 NNW 3		
24	759.5	758.5	757.6	07.2	13.0	06.2	08.2	14.0	06.0	03.2	05.1	05.5	06.3	66	49	89	68	NNE 1	- 0 - 0		
25	754.7	752.0	747.4	06.2	06.4	06.8	06.6	08.6	06.0	03.5	05.2	06.6	07.2	73	92	97	87	-	0	NNW 3 NNW 3	
26	736.2	738.9	741.3	13.4	09.2	08.5	09.9	15.3	08.0	05.0	08.9	08.7	07.8	77	100	94	96	SE 6	S 2 WNW 2		
27	744.4	749.0	753.3	05.9	08.0	04.5	05.7	09.5	04.2	03.5	06.7	06.4	06.1	96	80	97	91	NW 3	- 0 - 0		
28	758.5	759.2	759.2	02.2	10.4	06.8	06.6	11.2	02.0	-01.8	04.0	03.8	04.2	74	41	56	57	NW 3	- 0 - 0		
29	759.2	759.5	759.0	04.4	09.6	06.2	06.6	10.4	04.2	00.5	06.1	06.2	06.4	97	69	90	85	-	0	- 0 - 0	
30	757.5	756.7	755.0	05.6	11.7	06.7	07.7	12.8	05.2	03.3	06.4	07.9	07.2	94	77	97	89	-	0	- 0 - 0	
MES.	VRED.	756.5	755.8	756.5	09.4	14.9	10.3	11.3	16.3	08.5	05.7	07.9	09.3	08.6	87	73	89	83	1.0	1.4	1.2

## 1977 DECEMBAR

## TITOGRAD

1	752.5	751.6	751.8	07.5	14.4	09.2	10.1	15.5	05.2	03.6	07.4	09.4	08.5	95	77	98	90	-	0	- 0 - 0
2	748.9	747.6	751.2	09.6	09.2	03.4	06.4	10.0	03.0	02.0	08.7	08.3	03.6	98	95	61	85	W	1	N 2 - 5
3	753.6	756.0	759.0	03.8	04.8	05.8	05.1	06.4	03.4	00.5	02.0	02.7	03.0	34	42	44	40	N	8	N 7 6
4	760.9	760.8	762.0	06.0	08.1	03.2	05.1	08.8	03.0	02.0	03.1	02.8	01.8	44	34	30	36	N	6	N 8 8
5	762.0	760.1	760.1	01.6	07.0	-01.4	01.5	08.0	-01.6	-02.0	01.8	03.0	03.7	36	40	90	55	N	7	S 4 - 0
6	759.4	758.4	755.5	01.8	04.8	03.6	03.5	05.4	-01.4	-04.6	03.4	03.9	04.7	66	60	79	68	-	0	N 2 - 0
7	753.3	754.3	757.2	05.8	12.8	06.6	08.0	14.3	02.6	-01.0	06.3	09.2	07.2	92	83	99	91	W	1	W 1 - 0
8	759.5	758.6	758.8	03.8	13.4	04.8	06.7	13.6	03.0	00.4	05.6	07.1	06.3	92	61	97	83	W	3	WSW 1 - 0
9	757.3	755.1	754.5	06.0	08.0	07.5	07.3	08.3	04.7	00.6	06.4	07.7	07.7	92	96	99	96	-	0	- 0 - 0
10	752.7	753.8	755.8	07.8	10.6	08.0	08.6	11.5	07.0	04.5	07.8	09.0	08.0	99	94	100	98	-	0	- 0 - 0
11	760.3	761.9	765.5	06.0	12.8	08.2	08.8	14.4	05.0	04.0	06.4	06.1	04.6	92	55	56	68	-	0	NNE 5 NNE 5
12	766.6	766.3	767.9	06.4	10.4	05.6	07.0	11.2	04.6	02.6	04.2	03.8	02.9	58	41	42	47	NNW 2	SSE 3 N 5	
13	767.7	765.9	765.7	-02.2	08.3	-01.4	00.8	08.6	-03.2	-06.0	03.5	04.0	03.8	90	48	92	77	-	0	- 0 - 0
14	766.1	766.0	767.0	-02.8	09.3	-01.0	00.9	09.8	-04.5	-06.6	03.4	04.6	04.1	98	52	96	82	-	0	- 0 - 0
15	766.8	763.7	763.6	-01.0	12.4	07.2	06.5	12.8	-01.6	-06.5	03.8	05.2	04.1	88	48	54	63	-	0	N 3 N NW 2
16	767.0	766.7	766.6	05.8	09.4	07.4	07.5	10.2	05.1	-02.0	03.2	03.4	03.0	47	38	39	41	N	4	N 6 N 7
17	766.0	765.6	766.7	05.7	07.6	04.6	05.6	08.0	04.0	04.0	02.9	02.4	02.5	43	38	37	39	N	3	N 5 NNE 7
18	765.2	762.8	763.8	04.0	07.6	04.8	05.3	09.5	02.5	01.0	02.6	03.2	02.7	42	41	42	42	NNW 3	SE 5 N 6	
19	762.9	762.0	763.6	-02.6	10.8	00.2	02.2	11.4	-02.6	-05.5	03.1	04.0	04.3	82	41	93	72	-	0	WSW 2 - 0
20	763.6	762.6	763.2	-01.6	11.3	01.2	03.0	11.9	-02.8	-05.2	03.8	04.5	04.6	92	44	91	76	-	0	SSE 2 - 0
21	764.0	763.0	764.4	-01.6	11.7	00.5	02.8	11.7	-03.0	-05.4	03.9	04.2	04.3	96	40	89	75	-	0	- 0 - 0
22	765.9	765.7	767.9	-02.2	09.4	-00.8	01.4	10.0	-03.5	-06.5	03.7	04.5	03.4	95	51	80	75	-	0	- 0 - 0
23	769.4	768.8	770.6	-03.6	09.2	-00.6	01.1	09.6	-04.0	-07.5	03.4	04.3	04.1	97	49	93	80	-	0	SE 1 - 0
24	770.6	768.7	767.7	-03.0	09.4	02.0	02.6	09.8	-03.2	-06.8	03.4	04.3								

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 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$ 

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	07	080	080	07.7	00.8	.	.	.	$\bullet^4 17^{\circ} 24^{\circ} i, T 18^{\circ} 19^{\circ}, \Delta 19^{\circ} 20^{\circ}$
2	7	100	10	04	08.0	00.2	48.6	.	.	$\bullet^8 0-8^{\circ} 0$
3	8	06	060	00	04.0	06.7	03.7	.	.	$\square^4 20-24$
4	8	000	060	00	02.0	08.4	.	.	.	$\square^4 0-8^{\circ} 0, 20-24$
5	8	08	10	06	08.0	00.0	.	.	.	$\square^4 0-8$
6	8	10	08	06	08.0	00.1	.	.	.	$\square^4 19^{\circ} 24$
7	8	04	030	00	02.3	07.8	.	.	.	$\square^4 0-8, 20-24$
8	7	040	020	00	02.0	08.4	.	.	.	$\square^4 0-8^{\circ} 0 = 0-15^{\circ} 0$
9	8	02	020	00	01.3	08.6	.	.	.	$\square^4 0-8^{\circ} 0$
10	8	06	06	00	04.6	04.0	.	.	.	$\square^4 0-8^{\circ} 0, 20-24$
11	8	08	000	00	02.7	08.1	.	.	.	$\square^4 0-8$
12	8	00	030	00	00.0	09.1	.	.	.	$\square^4 20-24$
13	8	08	080	100	08.7	00.3	.	.	.	$\square^4 0-7^{\circ} 0, \bullet^4 16^{\circ} 24$
14	8	10	10	10	10.0	00.0	05.1	.	.	$\square^4 0-130, \square^4 10^{\circ} 30, \bullet^4 12^{\circ} 20, 10-13^{\circ} 0$
15	8	10	08	100	09.3	02.3	04.7	.	.	$\bullet^4 0-12^{\circ} 0$
16	7	10	100	10	10.0	00.0	02.4	.	.	$\square^4 08^{\circ} 10^{\circ} 5-5^{\circ} 0 9-9^{\circ} 0 12^{\circ} 16, 22^{\circ} 23^{\circ}, \square^4 10^{\circ} 22^{\circ}, \square^4 16-18, T 19^{\circ} 20^{\circ}$
17	8	06	040	10	06.7	06.6	15.6	.	.	$T 0-4, \square^4 0-8^{\circ} 0, 20-22^{\circ}, \bullet^4 4-6^{\circ} 0$
18	7	08	10	10	09.3	01.4	22.0	.	.	$\bullet^4 12-5^{\circ} 0$
19	7	100	10	10	10.0	00.0	08.2	.	.	$\bullet^4 14-50^{\circ} 110^{\circ} i, \square^4 16^{\circ} 20^{\circ} n$
20	8	10	020	00	04.0	06.7	09.6	.	.	$\square^4 0-10^{\circ} 1, \square^4 20-24$
21	8	00	10	10	06.7	04.9	.	.	.	$\square^4 10-8^{\circ} 0, \bullet^4 16^{\circ} 23^{\circ} 0$
22	7	100	100	100	10.0	00.0	08.2	.	.	$\bullet^4 1-10^{\circ} 0, \square^4 14^{\circ} 21-22^{\circ}, \square^4 12^{\circ} 20-19^{\circ} 0$
23	7	10	100	10	10.0	08.0	39.2	.	.	$\bullet^4 10^{\circ} 24^{\circ} 0$
24	8	06	02	06	04.7	00.0	10.9	.	.	.
25	7	10	100	100	10.0	00.5	.	.	.	$\bullet^4 10^{\circ} 21^{\circ} 0$
26	7	100	100	08	09.3	00.0	13.6	.	.	$\equiv 3^{\circ} 5^{\circ} 5^{\circ} 7^{\circ} 10^{\circ} 15-15^{\circ} 0, \bullet^4 4-5^{\circ} 10^{\circ} 0, \square^4 6^{\circ} 2^{\circ} 9$
27	7	100	060	02	06.0	01.1	35.4	.	.	$\bullet^4 1-10^{\circ} 0, \square^4 9^{\circ} 2^{\circ} 9^{\circ} 0, \square^4 20-24$
28	8	02	020	10	04.7	07.3	06.4	.	.	$\square^4 0-7^{\circ} 0, \bullet^4 23^{\circ} 24$
29	7	100	10	10	10.0	00.1	01.6	.	.	$\bullet^4 0-140, 6^{\circ} 4^{\circ} 7^{\circ} 0$
30	8	10	080	03	07.0	03.3	00.4	.	.	$\bullet^4 10^{\circ} 15^{\circ} 0$
MES. VRED.					07.2	06.7	05.8	06.5	105.1	235.6

1	8	08	06	04	06.0	02.9	00.3	.	$\bullet^4 2^{\circ} 5^{\circ} 15^{\circ} 10^{\circ}, \square^4 14^{\circ} 15^{\circ} 0$	
2	7	100	100	10	10.0	00.0	15.9	.	$\bullet^4 1-10^{\circ} 0, \square^4 15^{\circ} 24^{\circ}$	
3	8	10	10	10	10.0	00.0	22.4	.	$\square^4 0-24^{\circ} 0$	
4	8	04	000	00	01.3	08.6	.	.	$\square^4 0-24^{\circ} 0$	
5	8	00	000	00	00.0	08.6	.	.	$\square^4 0-8^{\circ} 0, \square^4 20-24$	
6	8	10	10	10	10.0	00.0	.	.	$\square^4 1-8^{\circ} 0, \bullet^4 21-24$	
7	8	100	050	03	06.0	03.1	39.4	.	$\bullet^4 0-3^{\circ} 0, \square^4 10^{\circ} 11^{\circ} 0, \square^4 9^{\circ} 5^{\circ} 9^{\circ} 0, \square^4 9^{\circ} 5^{\circ} 10^{\circ} 0$	
8	8	00	040	00	01.3	07.3	08.1	.	$\square^4 19^{\circ} 24$	
9	7	100	10	100	10.0	00.0	00.5	.	$\square^4 0-3^{\circ} 0, \bullet^4 23^{\circ} 22^{\circ} 0$	
10	7	10	10	10	10.0	00.0	14.4	.	$\bullet^4 3-6$	
11	8	02	010	00	01.0	08.1	.	.	$\square^4 11^{\circ} 22^{\circ} 0$	
12	8	08	000	00	02.7	08.4	.	.	$\square^4 11^{\circ} 6^{\circ} 10^{\circ} 22^{\circ} 0$	
13	8	00	000	00	00.0	08.2	.	.	$\square^4 0-8^{\circ} 0, 20-24^{\circ} 0$	
14	8	00	010	00	00.3	07.0	.	.	$\square^4 0-9^{\circ} 0, 24^{\circ} 0, \square^4 11^{\circ} 20^{\circ} 0$	
15	8	07	040	08	06.3	07.1	.	.	$\square^4 0-9^{\circ} 0, \square^4 11^{\circ} 20^{\circ} 0$	
16	8	00	020	01	01.0	07.6	.	.	$\square^4 010^{\circ} 24^{\circ} 0$	
17	8	03	030	00	02.0	08.4	.	.	$\square^4 0-24^{\circ} 0$	
18	8	02	000	00	00.7	08.4	.	.	$\square^4 0-13^{\circ} 0, \square^4 21^{\circ} 24$	
19	8	02	000	00	00.7	08.6	.	.	$\square^4 0-9^{\circ} 0, 20^{\circ} 24$	
20	8	00	000	00	00.0	08.4	.	.	$\square^4 0-2-9^{\circ} 0, 20^{\circ} 24$	
21	8	04	020	00	02.0	07.4	.	.	$\square^4 1-2-0-9^{\circ} 0, 20^{\circ} 24$	
22	8	00	000	00	00.0	08.3	.	.	$\square^4 0-9^{\circ} 0, 20-24$	
23	8	00	000	00	00.0	06.9	.	.	$\square^4 0-8^{\circ} 0, 20^{\circ} 24$	
24	8	00	060	00	02.0	08.0	.	.	$\square^4 0-8^{\circ} 0, 20^{\circ} 24$	
25	7	10	100	100	10.0	09.0	.	.	$\square^4 0-8^{\circ} 0, \bullet^4 10^{\circ} 18^{\circ} 0, \square^4 11^{\circ} 24^{\circ} 0$	
26	8	05	020	02	03.0	07.8	11.9	.	$\square^4 10^{\circ} 24^{\circ} 0$	
27	8	02	000	00	00.7	08.5	.	.	$\square^4 0-1, \square^4 20-24$	
28	8	08	10	10	09.3	00.0	.	.	$\square^4 0-1^{\circ} 0, \square^4 21^{\circ} 24$	
29	7	100	100	100	10.0	00.0	16.5	.	$\square^4 0-24^{\circ} 0, \square^4 12-13^{\circ} 0$	
30	7	10	10	10	10.0	00.0	56.5	.	$\bullet^4 0-12^{\circ} 0, \square^4 18^{\circ} 24^{\circ} 0, T 9^{\circ} 10^{\circ} 0$	
31	8	080	060	00	04.7	03.5	42.4	.	$\bullet^4 0-9^{\circ} 0, \square^4 18^{\circ} 15^{\circ} 0$	
MES. VRED.					04.9	04.3	03.5	04.2	161.1	228.3

$\varphi = 41^{\circ}58' N$   $\lambda = 21^{\circ}39' E$  Gr.  $\Delta G = +1h\ 27\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	746.4	746.2	746.7	00.2	00.4	-00.4	-00.1	01.2	-00.5	-	04.0	03.7	03.8	86	79	85	83	-	0	MNW	2	NW	2	
2	746.9	746.6	748.5	-02.0	01.2	-00.6	-00.5	02.3	-02.3	-	03.5	04.3	04.1	88	86	93	89	-	0	-	0	-	0	
3	749.7	751.1	752.1	-00.4	02.8	01.8	01.5	03.3	-01.4	-	04.1	04.4	04.7	93	78	90	87	-	0	MNW	1	-	0	
4	754.0	754.8	756.3	02.0	07.4	-01.6	01.6	07.8	-02.0	-	04.9	04.8	03.8	93	62	92	82	-	0	S	3	-	0	
5	758.4	758.2	758.3	-05.6	03.9	-04.6	-02.7	04.4	-06.6	-	02.9	04.2	03.0	95	69	91	85	-	0	MNW	3	-	0	
6	757.5	755.5	754.8	-03.8	-01.8	-02.8	-02.8	-01.5	-07.8	-	03.3	03.6	03.3	96	91	89	92	S	1	W	2	-	0	
7	753.4	750.9	749.0	-04.2	-02.8	-04.2	-03.9	-02.0	-05.4	-	03.1	03.0	03.1	92	82	92	89	NNW	2	SW	1	SSE	2	
8	745.5	746.3	745.7	-04.4	00.4	-01.0	-01.5	01.3	-05.3	-	03.0	04.4	04.3	92	93	100	95	-	0	-	0	-	0	
9	744.6	744.0	743.2	-03.8	02.6	-04.0	-02.3	03.0	-04.4	-	03.2	04.0	03.0	92	88	84	-	0	W	2	ESE	1		
10	742.3	741.0	742.2	-04.8	02.6	-03.1	-02.1	03.0	-07.5	-	02.9	03.2	03.6	91	58	98	82	-	0	NW	2	-	0	
11	742.5	740.7	739.9	-01.8	02.4	00.8	00.6	03.2	-04.1	-	03.8	04.4	04.5	94	81	93	89	-	0	NW	1	WSW	2	
12	738.1	736.3	735.2	06.6	11.4	09.0	09.0	13.0	00.4	-	06.7	07.7	06.9	92	77	80	83	SW	3	SSE	5	SSE	3	
13	731.4	731.7	735.1	04.4	09.4	03.0	05.0	11.0	03.0	-	06.3	06.9	04.6	100	78	81	86	ENE	2	ESE	1	WSW	1	
14	737.4	738.9	740.7	01.3	08.6	00.7	02.8	09.3	-00.8	-	04.4	05.5	04.6	88	66	95	83	SE	2	ESE	2	SE	1	
15	741.9	740.8	740.0	-03.2	-00.4	00.6	-00.6	00.7	-04.2	-	03.4	04.4	04.8	93	100	100	98	ESE	1	-	0	-	0	
16	737.3	736.6	735.3	01.8	03.6	03.5	03.1	04.2	00.0	-	05.0	05.8	05.8	97	97	98	97	-	0	-	0	WNW	2	
17	734.9	734.1	735.1	00.6	02.2	00.4	00.9	04.0	00.4	-	04.3	04.0	03.2	89	74	67	77	SW	2	NW	2	NNE	5	
18	736.9	737.8	739.8	-01.2	02.2	-01.0	-00.3	03.6	-01.4	-	03.1	03.2	02.4	74	59	57	63	NW	5	N	6	N	6	
19	742.8	742.8	744.2	-07.2	02.3	-05.4	-03.9	03.0	-07.6	-	02.2	03.8	02.6	84	70	86	80	NNE	1	NNW	2	-	0	
20	745.1	743.8	743.9	-09.6	03.0	-04.8	-04.1	04.0	-10.6	-	02.0	03.6	02.8	91	63	87	80	-	0	-	0	-	0	
21	743.8	743.7	744.3	-04.4	03.6	-03.2	-01.8	04.6	-07.1	-	03.2	04.1	03.5	96	70	96	87	NE	1	NE	1	-	0	
22	746.0	745.6	746.2	-07.2	06.4	-02.8	-01.6	07.2	-07.6	-	02.5	04.4	03.3	93	60	88	80	ENE	2	WNW	1	-	0	
23	746.3	744.4	743.0	-05.4	03.2	01.7	00.3	04.2	-06.1	-	02.9	04.3	04.8	95	75	92	87	-	0	-	0	-	0	
24	739.1	737.0	737.0	01.6	04.6	03.0	03.1	05.2	01.0	-	05.0	05.9	05.5	97	93	97	96	-	0	-	0	-	0	
25	738.5	739.2	740.3	02.0	10.2	00.8	03.5	10.4	00.7	-	05.3	07.2	04.5	100	77	93	90	-	0	NE	3	SSE	1	
26	740.1	739.0	738.3	-00.6	03.2	03.4	02.4	04.5	-03.2	-	04.4	05.6	05.5	99	97	94	97	ESE	2	-	0	-	0	
27	736.3	734.8	735.1	02.6	07.4	04.2	04.6	08.6	02.4	-	05.5	06.5	06.0	100	84	97	94	-	0	-	0	NE	3	
28	738.3	740.2	741.1	04.6	12.1	02.8	05.6	12.3	02.8	-	06.2	07.3	05.4	97	69	97	88	S	1	SSW	2	-	0	
29	739.5	734.8	734.0	01.8	13.0	06.7	07.1	13.2	00.9	-	05.2	07.7	06.7	100	69	91	87	-	0	SSE	6	WNW	2	
30	736.6	737.4	737.9	02.0	13.4	06.4	07.1	14.0	00.4	-	04.9	08.2	06.2	93	71	86	83	WNW	1	SSW	1	ESE	2	
31	740.4	739.3	738.8	01.4	15.6	04.0	06.3	16.0	01.2	-	04.7	07.3	05.6	93	52	91	80	ENE	1	NNN	1	ESE	1	
MES.	VRED.	743.0	742.4	742.6	-01.2	05.0	00.4	01.2	05.8	-02.7	-	04.1	05.1	04.4	93	76	90	86	0.9	1.6	1.6	1.6	1.6	1.6

## 1977 FEBRUAR

## SKOPJE-PETROVAC

1	737.1	735.1	735.4	05.6	12.4	06.8	07.9	13.4	03.4	-	06.4	07.8	06.6	94	72	89	85	NW	2	NW	2	S	1
2	735.0	735.6	735.6	06.8	09.1	06.8	07.4	09.4	05.6	-	07.0	07.4	07.2	95	85	97	92	ESE	1	NNW	2	NW	1
3	736.2	738.0	739.4	03.6	03.4	00.2	01.9	06.8	00.0	-	04.7	03.9	03.7	79	67	80	75	N	4	NNE	6	NE	5
4	739.0	740.5	742.5	-00.2	04.6	00.6	01.4	04.9	-00.9	-	03.9	04.3	03.6	85	68	76	76	NE	3	NNE	5	NE	7
5	743.3	742.8	743.0	-02.2	08.2	-00.2	01.4	09.5	-02.6	-	03.4	05.1	04.0	88	63	89	80	WNW	1	WNW	2	ESE	2
6	743.4	739.7	737.6	-00.6	11.0	06.8	06.0	11.4	-01.9	-	04.2	05.9	06.2	96	60	84	80	-	0	NE	2	N	2
7	739.1	741.2	743.9	05.2	08.7	04.4	05.7	10.9	01.8	-	05.9	05.8	05.2	89	68	82	80	NNE	4	NE	5	NE	1
8	744.4	741.8	740.0	-02.6	11.5	01.6	03.0	12.3	-03.0	-	03.6	05.3	04.4	96	52	85	78	-	0	SSW	2	NE	2
9	738.5	736.9	737.0	00.8	13.0	06.6	06.8	14.1	-01.0	-	04.7	06.4	06.1	97	57	84	79	-	0	NE	2	ESE	1
10	737.8	736.3	735.4	05.2	16.2	06.8	05.8	17.4	04.9	-	06.1	07.0	06.6	91	51	78	73	-	0	ENE	1	-	0
11	732.5	730.4	733.2	11.2	18.4	13.6	14.2	20.2	06.2	-	07.9	08.3	06.3	80	52	54	62	S	4	SE	3	SE	2
12	734.5	733.0	735.7	10.6	19.4	14.4	12.7	19.6	04.6	-	08.2	07.5	09.2	86	45	98	76	S	3	SSW	3	SE	2
13	737.1	737.9	737.6	07.9	10.6	07.2	08.2	12.6	06.9	-	06.1	08.2	07.2	76	86	95	86	-	0	NNE	5	NNE	2
14	732.2	727.4	728.8	04.8	10.4	08.2	07.9	13.0	03.8	-	06.3	09.0	07.3	97	95	90	94	NNE	2	WNW	3	S	2
15	735.0	736.1	736.6	01.8	14.2	07.4	07.7	14.6	01.6	-	05.0	05.4	06.1	97	44	79	73	-	0	WNW	1	-	0
16	737.7	736.8	737.9	03.0	12.0	06.6	07.1	12.8	01.6	-	05.5	07.1	06.3	97	68	86	84	-	0	NW	1	SE	1
17	738.4	737.1	740.7	00.2	10.8	07.2	06.4	11.8	-00.4	-	04.5	06.0	06.2	96	62	82	80	-	0	NW	2	NNW	5
18	744.3	744.0	745.9	01.6	11.6	03.2	04.9	13.2	01.2	-	04.6	05.2	05.2	90	51	91	77	SE	1	NW	2	E	1
19	747.8	746.0	745.7	-01.2	13.4	06.8	06.5	14.7	-01.8	-	04.0	08.8	05.5	96	59	74	76	-	0	-	0	ENE	2
20	746.4	744.6	744.4	00.8	13.4	05.6	06.4	1															

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 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolicijski broj sati	Padavina R mm	Snožni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10	10	10	10.0	-	.	.	.	$\equiv^0 0-10^{20}, 10^{20}-24; \star^0 8^{40} 9^{30}$
2	6	10	10	09	05.7	-	CO-C	.	.	$\equiv^0 0-24$
3	6	10	10	10	10.0	-	.	.	.	$\equiv^0 0-24$
4	7	10	09	09	04.3	-	.	.	.	$\equiv^0 0-24$
5	6	09	05	00	04.7	-	.	.	.	$\equiv^0 0-10^{20}, 10^{20}-24; \equiv^0 6^{40} 15^{20}, 19^{20}-24$
6	5	10	10	10	10.0	-	.	.	.	$\equiv^0 0-14^{30}, \equiv^0 0-4^{10}, 10^{15}-24; \equiv^0 4^{10} 10^{15} i, \equiv^0 5^{20} 10^{15}, V^0 6-14^{10}$
7	5	10	10	08	09.3	-	.	.	.	$\equiv^0 0-24 \leftarrow^0 4^{10} 9^{40}, \equiv^0 10^{15}-24$
8	3	10	10	00	06.7	-	CO-C	.	.	$\equiv^0 0-10^{20}, 10^{20}-24; \equiv^0 0-10^{20}, 10^{20}-24$
9	6	06	02	03	03.7	-	CO-C	.	.	$\equiv^0 0-0^{20}, \equiv^0 0-0^{25}, 6^{20} 7^{30}, 9^{40} 10^{20}; \equiv^0 10^{40} 14^{20} 22^{25} 24; \equiv^0 10^{30} 24^{40}, \bullet^0 14^{10} 15^{35}$
10	6	10	08	00	06.0	-	.	.	.	$\equiv^0 0-24, \equiv^0 0-11^{10}, \equiv^0 6^{40} 15^{20}, 19^{20}-24; \equiv^0 2^{20} 6^{40}, \equiv^0 10^{30} 24^{40}, \equiv^0 14^{10} 15^{35}$
11	5	10	10	04	08.0	-	.	.	.	$\equiv^0 0-20^{30}, \equiv^0 10^{30}-24$
12	7	05	09	02	06.7	-	00.2	.	.	$\equiv^0 0-24, \bullet^0 4^{10} 9^{40}, \equiv^0 10^{15}-24$
13	7	10	05	00	05.0	-	05.5	.	.	$\bullet^0 5^{20} 6^{40}$
14	7	10	04	00	04.7	-	01.8	.	.	$\equiv^0 0-11^{10}, \equiv^0 3^{20} 9^{40} i, 15^{30} 22^{30}; \equiv^0 8^{10} 15^{30} i, \equiv^0 2^{20} 8^{40}-24$
15	2	06	10	10	06.7	-	.	.	.	.
16	4	10	10	10	10.0	-	00.6	.	.	$\equiv^0 0-0^{20}, \equiv^0 0-0^{25}, 10^{20} 11^{30}; \equiv^0 3^{35} 11^{20} i, \equiv^0 5^{25} 6^{10}$
17	6	10	10	10	10.0	-	01.3	.	.	.
18	7	10	10	00	06.7	-	00.4	.	.	$\equiv^0 0-24, \equiv^0 3^{20} 9^{40} i, 15^{30} 22^{30}; \equiv^0 8^{10} 15^{30} i, \equiv^0 2^{20} 8^{40}-24$
19	7	00	00	00	00.0	-	.	.	.	.
20	6	00	01	00	00.3	-	.	.	.	$\equiv^0 0-11, 21^{30} 24; \equiv^0 8^{45} 14^{30}$
21	6	05	09	03	06.0	-	.	.	.	$\equiv^0 0-10^{20}, 20^{20}-24; \equiv^0 8^{20} 16^{20}$
22	6	00	06	00	06.0	-	.	.	.	$\equiv^0 0-10^{10}, 21^{20}-24; \equiv^0 6^{20} 24$
23	5	00	09	10	06.3	-	.	.	.	$\equiv^0 0-24, \bullet^0 10^{20}, \bullet^0 20^{20}, 23^{20}$
24	4	10	10	10	10.0	-	02.0	.	.	$\equiv^0 0-0^{20}, 8^{20} 16^{20}, \equiv^0 10^{20} 8^{40}, 16^{20} 20^{20}, \bullet^0 6^{10} 7^{15} 10^{25} 12^{30}, 15^{40} 17^{15}; \equiv^0 20^{20}-24$
25	6	10	08	00	06.0	-	00.9	.	.	$\equiv^0 0-10^{20}, \bullet^0 10^{20}, 24^{20}, 10^{20}-10^{25}, \equiv^0 10^{15} 14^{30}, 20^{20}-24, \equiv^0 22^{30}-24$
26	4	10	10	10	10.0	-	.	.	.	$\equiv^0 0-8^{30}, \equiv^0 4-35, 12^{35} 24; \equiv^0 8^{20} 16^{20}$
27	6	10	05	09	06.0	-	.	.	.	$\equiv^0 0-3^{10} 6^{20} 6^{40} 8^{20} 17^{20}; \equiv^0 3^{10} 5^{20}, \equiv^0 5^{20} 8^{40} i, \bullet^0 20^{55} 23^{55}$
28	7	08	08	00	05.3	-	12.2	.	.	$\equiv^0 0-24, \bullet^0 25^{50} 5^{10}$
29	7	10	06	09	06.3	-	.	.	.	$\equiv^0 0-24, \bullet^0 12^{25}, \bullet^0 12^{20}-14$
30	6	06	08	10	06.0	-	.	.	.	$\equiv^0 0-8^{30}, \bullet^0 15^{30} 16, \cap 15^{40}-16$
31	7	01	04	00	03.0	-	.	.	.	.
MES. VRED.	07.9	07.4	04.8	06.7	-	24.9				

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1	7	09	07	03	06.3	-	02.2	.	.	$\bullet^0 8^{20} 4^{40}, \equiv^0 8^{20} 12^{20}$
2	7	10	10	10	10.0	-	00.2	.	.	$\bullet^0 5^{20} 12^{20}, \bullet^0 20^{20}-23^{20}, \bullet^0 6^{10} 11^{20}, T 21^{20}-21^{30}, R 21^{20}-22^{20}$
3	7	10	10	09	05.7	-	16.5	.	.	$\bullet^0 20^{20} 9^{20}, \text{NE}, N 005, 250, 12^{20}-20$
4	7	09	03	03	05.0	-	00.0	.	.	$\text{FNE} 13^{20}, 17^{20}$
5	6	03	02	00	01.7	-	.	.	.	$\equiv^0 0-3^{20}, \equiv^0 6^{15} 16^{15}$
6	7	04	09	10	07.7	-	.	.	.	$\equiv^0 6^{15} 8^{30}, \equiv^0 10^{20} 16^{20}, \bullet^0 20^{20}-23^{20}$
7	7	09	09	01	06.3	-	01.0	.	.	$\equiv^0 12^{20}-3^{20}, \text{NE} 12^{20}, 14^{20}$
8	7	01	04	00	01.7	-	.	.	.	$\equiv^0 0-9^{20}, \bullet^0 12^{25}$
9	7	08	04	08	06.7	-	.	.	.	$\equiv^0 0-8^{20}, \equiv^0 7^{20}, 13^{20}$
10	7	10	05	04	06.2	-	.	.	.	.
11	8	10	06	00	05.2	-	.	.	.	$\text{FNE} 14^{20}, 15^{20}$
12	8	10	10	10	10.0	-	.	.	.	$\bullet^0 8^{20} 2^{40}, 12^{20}, 13^{20}, 15^{20}, 22^{20}, \text{FNE} 8^{20} 9^{20}$
13	7	10	10	09	05.7	-	04.4	.	.	$\bullet^0 14^{20}, 20^{20}, \bullet^0 12^{25}, 19^{20}$
14	5	09	09	10	05.3	-	00.3	.	.	$\equiv^0 6^{20} 19^{20}, \bullet^0 12^{25}, 19^{20}$
15	8	04	05	09	06.0	-	15.0	.	.	$\equiv^0 5^{20} 7^{20}, \bullet^0 17^{20}, 18^{25}$
16	7	09	07	02	06.0	-	CO-C	.	.	$\bullet^0 132, 305$
17	6	05	09	10	08.0	-	.	.	.	$\bullet^0 132, 4^{40}, \equiv^0 4^{20} 8^{40}, \equiv^0 11^{25}, 14^{25}, \bullet^0 17^{20}, \text{FNE} 17^{20}, 18^{20}$
18	8	01	01	00	00.7	-	02.6	.	.	$\equiv^0 0-8^{20}, \bullet^0 12^{20}, \bullet^0 12^{20}-24$
19	7	01	03	00	01.2	-	.	.	.	$\bullet^0 0-2^{20}, \bullet^0 2^{20}, 8^{40}, \equiv^0 5^{20}, 13^{20}$
20	7	05	02	00	03.7	-	.	.	.	$\bullet^0 132, 8^{40}, \bullet^0 6^{20} 17^{20}$
21	6	10	05	10	08.3	-	.	.	.	$\equiv^0 132, 8^{40}, \bullet^0 6^{20} 17^{20}$
22	7	05	09	04	07.3	-	.	.	.	$\equiv^0 132, 8^{40}, \bullet^0 6^{20} 17^{20}$
23	7	09	02	07	06.0	-	.	.	.	$\equiv^0 14^{20}, 12^{20}, \bullet^0 3^{20}, 9^{40}, \equiv^0 8^{20} 9^{40}$
24	7	03	09	08	06.7	-	.	.	.	.
25	7	07	06	04	05.7	-	.	.	.	$\bullet^0 132, 9^{40}, \equiv^0 6^{20} 11^{15}$
26	7	05	09	02	05.3	-	.	.	.	$\bullet^0 132, 8^{40}, \bullet^0 6^{20} 13^{20}, \bullet^0 11^{25}, 13^{25}, \text{FNE} 15^{45}, 20^{20}$
27	8	04	05	10	06.3	-	00.2	.	.	$\equiv^0 8^{20}, 24, \bullet^0 9^{20}, 17^{20}$
28	7	05	10	10	09.7	-	.	.	.	.
MES. VRED.	07.0	06.4	05.5	06.3	-	42.4				

$\varphi = 41^{\circ}58' N \lambda = 21^{\circ}39' E$  Gr.  $\Delta G = +1h 27 min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	745.8	744.9	745.9	-02.2	02.2	-01.4	-00.7	03.3	-03.0	-	02.2	02.5	03.3	57	47	81	62	NW	3	N	4	NE	3
2	746.1	746.6	747.6	-03.8	04.0	-02.0	-01.0	05.6	-06.0	-	02.8	03.1	03.0	80	51	76	69	N	3	NE	4	NE	1
3	746.2	746.0	742.9	-05.4	03.6	01.0	00.1	04.2	-07.0	-	02.9	03.5	04.6	95	58	93	82	-	0	NE	1	NE	1
4	741.3	742.1	742.1	00.4	11.6	08.6	07.3	13.3	-00.8	-	04.6	06.7	06.5	96	65	78	80	-	0	ESE	3	-	0
5	741.9	745.4	747.5	04.0	09.2	04.8	05.7	13.2	04.0	-	05.7	04.8	04.6	94	55	71	73	NNE	2	NNE	7	NNE	1
6	747.3	744.2	743.8	-01.4	16.2	05.8	06.6	18.6	-03.5	-	04.0	05.9	05.2	96	43	75	71	-	0	W	2	NE	2
7	748.7	747.7	751.6	00.2	16.8	09.4	09.0	17.4	-06.9	-	04.2	05.6	05.3	89	39	60	63	-	0	WNW	1	NNE	5
8	756.8	755.6	756.0	00.1	14.8	04.0	05.7	15.8	-01.1	-	03.9	04.9	03.6	84	38	59	60	-	0	-	0	-	0
9	755.4	756.6	747.8	-01.4	13.6	03.2	04.7	16.9	-02.2	-	04.0	05.5	04.2	96	47	72	72	NE	2	-	0	SE	2
10	745.5	742.1	744.6	01.6	17.0	07.0	08.2	18.3	-01.0	-	04.5	05.7	04.3	87	39	58	61	-	0	NE	6	ENE	3
11	745.2	742.8	743.3	-01.4	14.7	07.2	06.9	15.4	-02.6	-	03.8	05.8	05.4	92	46	71	70	-	0	S	3	S	1
12	744.7	742.6	743.0	01.0	14.0	09.2	08.4	14.8	00.5	-	04.6	06.1	05.6	93	51	64	69	-	0	SSE	3	SE	2
13	740.5	736.1	736.3	08.0	13.2	08.2	09.4	13.8	06.0	-	06.8	06.9	07.9	85	61	97	81	-	0	SE	6	SSW	1
14	740.2	742.2	744.4	06.8	09.1	06.8	07.4	09.6	06.8	-	06.2	06.9	06.4	84	79	87	83	NNE	4	NE	5	NE	4
15	745.7	746.5	747.6	06.0	11.1	07.4	08.0	12.6	05.9	-	06.6	07.5	07.0	94	75	91	87	-	0	NNE	4	NE	3
16	748.4	748.4	749.6	08.8	13.0	06.2	08.6	14.8	05.6	-	06.0	05.5	05.8	71	49	81	67	NW	3	N	4	NE	3
17	749.4	746.6	746.4	01.2	14.4	07.6	07.7	16.0	00.3	-	04.6	05.5	05.2	91	45	67	68	NE	1	WNW	2	NE	3
18	746.7	742.1	741.3	-00.2	16.6	07.4	07.8	18.0	-02.6	-	04.0	06.1	05.5	89	43	72	68	E	1	ESE	2	SE	2
19	742.2	739.6	739.5	03.6	15.2	08.4	08.9	16.4	02.1	-	05.8	07.3	06.7	97	56	81	78	-	0	SSW	1	SE	4
20	741.3	741.1	742.7	05.8	15.8	09.6	10.2	16.1	03.0	-	06.5	07.4	07.5	94	55	83	77	-	0	SSW	4	NE	2
21	743.6	742.2	744.3	05.2	19.6	10.4	11.4	20.3	03.0	-	06.3	07.4	07.3	94	44	77	72	N	1	S	4	E	1
22	746.7	745.2	745.8	04.6	22.0	11.2	12.3	24.4	02.1	-	06.2	09.0	07.1	97	46	71	71	ENE	2	SSE	2	ESE	1
23	747.6	745.0	744.1	05.4	25.2	13.0	14.2	28.0	03.4	-	06.3	09.0	06.4	94	38	57	63	ENE	1	S	1	S	1
24	746.2	742.3	743.6	07.0	26.6	14.0	15.4	27.6	04.2	-	06.5	09.5	06.8	87	36	56	60	-	0	SW	1	NE	3
25	744.6	742.4	743.0	06.9	22.8	14.0	14.4	23.8	03.2	-	06.0	08.6	07.9	80	41	66	62	-	0	SSE	4	ESE	3
26	742.1	738.8	738.5	07.2	21.8	13.2	13.9	22.8	05.8	-	07.0	08.1	07.4	92	41	65	66	-	0	ESE	2	S	2
27	739.4	736.4	735.8	04.6	22.0	13.4	13.4	23.2	02.6	-	05.8	06.5	06.2	91	33	71	65	-	0	S	2	SE	1
28	736.6	732.9	733.0	07.2	21.0	14.0	14.1	22.0	04.3	-	06.8	08.2	08.3	89	44	70	68	-	0	S	3	SE	3
29	735.0	735.0	737.0	10.6	19.1	14.2	14.5	19.9	08.4	-	08.0	09.1	09.1	84	55	75	71	-	0	S	3	SSE	5
30	738.1	737.6	738.6	12.4	17.2	14.6	14.7	18.4	11.8	-	09.4	09.4	09.1	87	64	73	75	SSE	5	SE	6	SE	5
31	740.0	740.7	740.3	12.4	15.8	11.6	12.9	16.1	11.4	-	08.9	09.6	08.9	83	71	86	80	-	0	-	0	-	0
MES. VRED.	744.5	742.9	743.5	03.7	15.4	08.4	09.0	16.8	02.0	-	05.5	06.7	06.3	88	50	74	71	0.9	2.9	2.2			

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1	742.0	740.3	740.8	10.6	17.2	11.6	12.8	18.7	07.4	-	08.7	10.1	08.2	91	65	80	80	ESE	2	-	C	NE	5
2	739.0	737.8	736.8	09.0	14.0	12.0	11.8	14.0	07.6	-	08.0	10.1	10.3	93	90	98	94	S	1	SE	2	NW	2
3	734.5	733.3	733.3	11.4	16.9	12.4	13.3	17.7	10.9	-	10.1	11.8	10.7	100	82	99	94	-	0	-	0	-	0
4	735.3	734.8	737.3	08.4	23.0	15.0	15.4	24.0	06.7	-	08.3	10.8	09.7	100	51	76	76	-	0	H	2	NE	5
5	739.3	736.4	735.2	09.6	23.2	17.2	16.8	24.1	06.0	-	08.5	10.3	07.6	95	48	51	65	-	0	SSW	2	NW	2
6	738.1	738.4	738.7	07.8	15.0	08.0	05.7	16.6	06.9	-	06.1	07.4	06.2	77	58	77	71	N	5	NE	6	ESE	2
7	739.4	736.5	736.6	04.2	19.6	13.6	12.8	20.6	03.3	-	05.4	09.2	08.5	88	54	73	72	-	0	SSE	3	ESE	3
8	735.6	732.1	731.4	08.6	22.8	15.4	15.6	23.4	06.4	-	07.7	09.7	08.3	92	47	64	68	-	0	SSE	4	SSE	4
9	729.7	726.2	727.9	12.4	19.2	11.0	13.4	20.6	11.0	-	08.0	08.6	06.9	74	52	98	75	E	2	SSE	7	SE	1
10	730.0	729.2	732.0	07.5	16.9	07.0	09.6	18.9	05.2	-	07.7	07.2	06.9	99	50	92	80	-	0	-	0	SE	1
11	733.8	733.4	735.3	03.2	10.6	04.2	05.6	11.4	00.2	-	05.6	06.3	04.2	97	66	68	77	WSW	1	NNE	6	NNE	5
12	735.9	733.7	735.6	05.0	11.4	05.4	06.8	11.9	00.4	-	03.9	04.9	03.9	59	49	59	56	NNE	4	NNE	6	NNE	6
13	737.2	736.0	736.5	03.8	10.4	06.0	06.6	12.0	00.2	-	04.4	04.2	04.2	73	45	60	59	-	0	NNE	4	NNE	4
14	736.1	734.2	734.2	01.6	12.0	08.4	08.1	13.7	-03.0	-	03.9	04.8	05.5	77	46	62	62	NNE	2	N	1	ESE	2
15	732.4	728.4	728.7	05.8	15.4	08.0	09.3	16.6	03.0	-	05.6	07.0	07.6	81	53	95	76	-	0	SSE	6	SW	1
16	730.5	733.0	735.7	05.1	09.6	05.6	06.5	11.5	03.5	-	05.7	04.4	04.4	87	49	64	67	-	0	NW	4	NW	3
17	737.9	739.2	741.0	07.7	12.7	08.2	09.2	14.0	03.4	-	04.6	04.1	03.6	59	37	45	47	NW	5	NNW	6	NW	3
18	742.4	740.8	741.7	03.4	16.0	07.8	08.8	17.7	-02.5	-	04.1	05.1	04.8	70	37	60	56	S	1	-	0	ESE	1
19	744.3	742.0	742.1	03.8	20.0	12.8	12.9	20.8	-06.7	-	04.6	06.5	05.6	76	37	47	53	-	0	ESE	3	ESE	3
20	742.9	741.7	744.0	06.4	18.4	10.6	12.0	19.0	04.6	-	06.2	06.6	06.1	7									

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 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } H_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Den	Vrijnost 0-9	Obločnost N (0-10)					Insolacij broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	- 7	14	21	Sred Dnes				7	7
1	7	03	06	06	05.0	-	00.0	.	$\overline{\square}^{\circ} 0-11^{55}$		
2	7	03	06	06*	03.3	-	00.3	.	$\times^{\circ} 0-02^{15}, \overline{\square}^{\circ} 13-14^{10}, \overline{\square}^{\circ} N 13^{25}-16^{30}$		
3	7	10	10	10	10.0	-	00.0	.	$\overline{\square}^{\circ} 0-30^{10}, \overline{\square}^{\circ} 20^{20}, \overline{\square}^{\circ} 035, \times^{\circ} 21^{25}-22^{45}, \equiv^{\circ} 22^{30}-24$		
4	7	10	09	09	09.3	-	00.0	.	$\overline{\square}^{\circ} 0-11^{50}, \overline{\square}^{\circ} 035-14^{55}, \times^{\circ} 21^{25}-22^{45}, \equiv^{\circ} 22^{30}-24$		
5	8	05	09	06	04.7	-	0.	.	$\overline{\square}^{\circ} NNE 10^{30}, \overline{\square}^{\circ} 16^{30}$		
6	7	07	01	00	02.7	-	.	.	$\overline{\square}^{\circ} 11^{10}-8$		
7	7	02	06	04	04.0	-	.	.	$\overline{\square}^{\circ} 0-02^{10}, \oplus 13^{20}-15^{10}, \overline{\square}^{\circ} NNE 16^{45}-18^{30}, 20^{50}-23^{10}$		
8	7	00	00	00	00.0	-	.	.	$\overline{\square}^{\circ} 0-5-8^{30}$		
9	7	08	08	00	05.3	-	.	.	$\overline{\square}^{\circ} 0-54^{20}, \equiv^{\circ} 13^{20}-14^{35}$		
10	7	08	06	00	04.7	-	.	.	$\overline{\square}^{\circ} 0-02^{10}, \equiv^{\circ} 53^{20}-8^{30}, \overline{\square}^{\circ} NE 12-18$		
11	7	06	00	00	00.0	-	.	.	$\overline{\square}^{\circ} 13^{10}-7^{40}$		
12	7	06	07	03	05.3	-	.	.	$\overline{\square}^{\circ} 3^{40}-5^{15}, \overline{\square}^{\circ} 3^{30}-7^{45}, \equiv^{\circ} 5^{40}-10^{30}$		
13	7	10	09	10	09.7	-	.	.	$\overline{\square}^{\circ} 0-02^{10}, \oplus 15^{20}, \overline{\square}^{\circ} 15^{20}-24^{15}$		
14	7	10	10	10	10.0	-	<u>12.2</u>	.	$\bullet^{\circ} 0-54^{15}$		
15	7	09	10	10	05.7	-	.	.	$\bullet^{\circ} 13^{20}-16^{20}, 21^{45}-23^{20}$		
16	7	05	06	02	06.3	-	00.3	.	$\bullet^{\circ} 6^{02}-6^{15}$		
17	8	00	03	00	01.0	-	.	.	$\overline{\square}^{\circ} 1-0-4^{30}, \overline{\square}^{\circ} 4-50-7^{30}$		
18	7	00	00	00	00.0	-	.	.	$\overline{\square}^{\circ} 0-2^{10}, \overline{\square}^{\circ} 23^{20}-7^{40}, \equiv^{\circ} 5^{15}-6^{10}$		
19	7	09	01	00	03.3	-	.	.	$\equiv^{\circ} 0-30-11^{40}$		
20	7	10	07	05	07.3	-	.	.	$\equiv^{\circ} 5^{20}-12^{45}$		
21	7	09	06	00	05.0	-	.	.	$\overline{\square}^{\circ} 0-02-8^{40}, 22-24, \equiv^{\circ} 5^{30}-12^{40}$		
22	7	01	01	00	00.7	-	.	.	$\overline{\square}^{\circ} 1-0-9^{10}, \equiv^{\circ} 5^{40}-10^{30}$		
23	7	00	01	00	06.3	-	.	.	$\overline{\square}^{\circ} 0-02-8^{30}$		
24	8	00	02	00	00.7	-	.	.	$\overline{\square}^{\circ} 3^{02}-8^{15}$		
25	8	00	07	09	05.3	-	.	.	$\overline{\square}^{\circ} 1-0-9^{15}$		
26	7	07	03	00	03.3	-	.	.	$\equiv^{\circ} 1-54^{20}-11^{40}$		
27	7	00	00	00	00.0	-	.	.	$\overline{\square}^{\circ} 1-0-8^{15}, \equiv^{\circ} 0-5^{15}-6^{40}$		
28	7	09	04	05	06.0	-	.	.	$\equiv^{\circ} 5^{10}-11^{45}, \overline{\square}^{\circ} 5^{20}-7^{40}, \overline{\square}^{\circ} SSE 17^{40}-19^{20} i, \bullet^{\circ} 18^{02}-18^{20}$		
29	7	10	05	10	08.3	-	00.0	.	$\bullet^{\circ} 0-02-22^{45}$		
30	7	10	10	10	10.4	-	00.3	.	$\bullet^{\circ} 3^{30}-5^{40}, 10^{40}-11^{40}, \overline{\square}^{\circ} SSE 9^{10}-21^{30}$		
31	6	10	10	10	10.0	-	00.0	.	$\overline{\square}^{\circ} 0-1^{10}, \equiv^{\circ} 10^{45}-24^{24}$		
MES. RED.		05.6	05.3	03.7	04.9	-	13.1				

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1	6	10	10	10	10.0	-	00.0	.	$\equiv^{\circ} 0-18^{15}$		
2	6	09	10	10	05.7	-	00.0	.	$\equiv^{\circ} 5^{40}-14^{30}, \bullet^{\circ} 6^{15}-6^{25}, 8^{02}-24^{15}$		
3	6	10	09	05	08.0	-	09.9	.	$\bullet^{\circ} 0-6^{15}, \overline{\square}^{\circ} 3^{20}-16^{25}$		
4	7	10	01	02	04.3	-	.	.	$\overline{\square}^{\circ} 0-10^{20}, \equiv^{\circ} 0-32^{20}, 8^{15}-10^{40}, \equiv^{\circ} 3^{20}-8^{15} i, \equiv^{\circ} 16^{20}-7^{30}, \overline{\square}^{\circ} NE 18^{20}-19$		
5	7	00	02	04	02.0	-	.	.	$\overline{\square}^{\circ} 0-9^{10}, \equiv^{\circ} 5^{20}-11^{45}$		
6	7	09	02	00	03.7	-	02.2	.	$\bullet^{\circ} 3^{50}-5^{20}, \overline{\square}^{\circ} NNE 4^{20}-14^{30} i, \overline{\square}^{\circ} 4^{45}-5^{20}$		
7	7	01	06	00	02.3	-	.	.	$\overline{\square}^{\circ} 0-02-8^{30}$		
8	7	09	05	01	05.4	-	.	.	$\equiv^{\circ} 0-50-16^{15}, \bullet^{\circ} 15^{02}-18^{10}, T 15^{40}-15^{20}, \equiv^{\circ} 20^{15}-23^{30}$		
9	8	08	05	10	07.7	-	.	.	$\overline{\square}^{\circ} 0-02-16^{15}, \bullet^{\circ} 14^{20}-20^{25}, \equiv^{\circ} 23^{30}-24$		
10	7	04	05	06	04.3	-	02.8	.	$\bullet^{\circ} 14^{20}-17^{15}$		
11	7	03	06	00	03.0	-	00.5	.	$\overline{\square}^{\circ} 0-035, \overline{\square}^{\circ} 4^{35}-6^{15}, \overline{\square}^{\circ} N 8^{20}-20^{20}$		
12	7	03	02	00	01.7	-	.	.	$\overline{\square}^{\circ} NNE 10^{15}-13^{15}, \overline{\square}^{\circ} 8^{12}-24^{15}$		
13	7	05	05	01	03.7	-	.	.	$\overline{\square}^{\circ} 10^{02}-10^{02}$		
14	7	01	05	05	06.3	-	.	.	$\overline{\square}^{\circ} 0-20-7^{30}$		
15	7	10	10	10	10.0	-	.	.	$\overline{\square}^{\circ} 8^{02}-16^{20} i, \bullet^{\circ} 14^{20}-20^{25}, \equiv^{\circ} 23^{30}-24$		
16	7	10	10	00	06.7	-	04.7	.	$\equiv^{\circ} 0-035, \bullet^{\circ} 4^{05}-5^{20}, \overline{\square}^{\circ} NW 11^{50}-16^{10} i$		
17	8	09	05	00	04.7	-	.	.	$\overline{\square}^{\circ} NW 5-10^{15} i$		
18	7	00	00	00	06.0	-	.	.	$\overline{\square}^{\circ} 0-20-6^{15}$		
19	8	01	08	09	06.0	-	.	.	$\overline{\square}^{\circ} 0-05-8^{20}$		
20	7	09	10	10	09.7	-	.	.	$\oplus 8^{15}-10^{40}, \overline{\square}^{\circ} 16^{05}-24^{15}$		
21	7	05	10	10	09.7	-	.	.	$\overline{\square}^{\circ} NNE 0-4-6$		
22	8	00	02	00	06.7	-	.	.	$\overline{\square}^{\circ} 3^{40}-7^{05}$		
23	7	02	05	06	04.3	-	.	.			
24	8	05	06	06	05.7	-	.	.			
25	7	06	09	01	05.3	-	.	.			
26	8	01	05	00	02.0	-	00.2	.	$\overline{\square}^{\circ} 7^{45}-11^{40} i$		
27	7	05	00	00	01.7	-	.	.	$\overline{\square}^{\circ} 2^{20}-8^{15}$		
28	7	07	05	00	05.3	-	.	.			
29	8	00	06	06	04.0	-	.	.	$\oplus 0-11^{30}-12^{45}, \overline{\square}^{\circ} 19^{30}-21^{40}$		
30	8	03	04	02	03.0	-	.	.			
MES. RED.		05.3	06.0	03.7	05.0	-	20.7				

$\varphi = 41^{\circ}58' N$   $\lambda = 21^{\circ}39' E$  Gr.  $\Delta G = +1h 27 min.$

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D S	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	741.9	739.4	739.6	13.6	27.2	16.0	18.2	27.6	06.1	-	09.2	11.2	08.5	79	41	62	61	-	0	SE 3	NE 2	
2	742.6	740.7	741.0	14.3	28.3	20.8	21.1	29.6	09.7	-	09.4	10.6	10.2	77	37	55	56	-	0	WNW 2	NE 3	
3	742.3	739.9	739.6	15.6	28.8	20.2	21.2	29.8	11.7	-	09.9	11.0	09.4	75	37	53	55	-	0	S 2		
4	741.3	739.1	738.9	14.7	28.2	21.9	21.7	29.0	09.2	-	09.4	11.9	10.4	75	41	53	56	-	0	ESE 2	SW 3	
5	740.6	740.7	740.9	17.4	21.6	15.0	19.3	23.8	12.6	-	10.7	11.7	09.9	72	60	60	64	WNW 2	WNW 4	WSW 2		
6	742.9	741.4	741.0	15.4	21.6	15.8	17.2	23.0	14.8	-	11.5	12.2	10.6	88	63	79	77	ENE 2	ESE 2	SE 2		
7	741.0	737.9	738.0	13.2	21.6	15.2	16.3	22.7	10.0	-	10.2	10.8	10.5	89	56	81	75	WNW 1	SW 4	-	0	
8	737.2	735.0	736.4	12.4	16.4	12.0	13.2	20.0	09.1	-	09.6	09.3	10.3	89	66	98	84	SW 1	NE 4	-	0	
9	737.8	737.7	738.7	10.2	19.0	12.3	13.5	21.1	06.4	-	09.1	08.0	05.0	98	48	84	77	SSE 1	ESE 1	ENE 2		
10	738.9	738.3	738.5	12.0	16.0	10.6	12.3	17.3	09.0	-	09.1	09.0	08.7	87	66	91	81	-	0	NNE 2	NE 2	
11	738.8	738.9	739.5	13.6	16.6	10.6	12.9	19.2	07.2	-	08.5	07.3	07.8	73	51	81	68	NW 3	N 5	NE 1		
12	740.0	737.3	737.6	12.4	21.4	13.6	15.3	22.6	05.0	-	08.5	07.8	07.6	78	41	65	61	NE 1	NW 2	SSE 1		
13	737.9	735.4	735.8	10.6	24.4	16.6	17.1	26.0	04.2	-	08.2	08.9	09.4	86	39	67	64	NNE 1	W 2	-	0	
14	736.9	733.8	734.8	12.9	26.1	15.7	19.6	26.6	07.4	-	09.4	09.1	08.1	84	36	47	56	-	0	SE 3	SE 4	
15	734.5	732.8	733.0	17.6	21.0	14.4	16.9	22.8	14.0	-	11.5	10.2	11.2	76	55	91	74	S 2	SSE 5	S 4		
16	733.4	734.1	736.0	14.6	22.2	15.0	16.7	24.0	12.2	-	11.7	10.8	11.0	94	54	86	78	WNW 2	WNW 2	-	0	
17	740.5	741.0	742.4	14.2	24.6	18.4	18.9	26.0	08.0	-	09.7	10.2	11.6	80	44	73	66	-	0	WNW 1	S 2	
18	745.9	743.5	743.7	18.0	28.2	23.6	23.4	29.4	14.0	-	11.6	12.5	12.4	75	44	57	59	NNE 1	SE 3	ESE 2		
19	744.9	742.9	743.3	20.6	28.6	21.4	23.0	29.0	15.8	-	11.9	13.2	11.8	65	45	62	57	SE 3	S 4	SE 3		
20	743.3	741.7	741.8	19.4	28.2	22.2	23.0	29.3	13.5	-	11.9	14.7	12.5	71	51	62	61	S 3	S 3	SE 2		
21	742.6	741.4	740.4	18.6	27.4	21.4	22.2	29.4	15.5	-	12.3	14.8	15.3	77	54	80	70	-	0	WNW 2	-	0
22	741.2	739.1	739.0	19.4	27.5	22.4	22.9	30.2	14.9	-	13.3	16.1	10.2	79	58	50	62	W 1	SSE 2	-	0	
23	741.7	740.3	742.5	20.4	27.2	21.0	22.4	30.2	13.6	-	12.3	13.0	11.7	68	48	63	60	N 3	NNE 4	WNW 2		
24	742.6	741.0	742.6	16.6	23.9	16.6	18.4	24.6	10.7	-	10.7	11.4	08.2	75	51	58	61	SW 1	NE 5	NE 5		
25	742.1	738.6	738.7	14.6	22.6	16.6	17.6	24.4	10.2	-	08.3	10.3	08.5	66	50	60	59	NE 3	SW 2	S 2		
26	739.8	738.1	738.8	14.2	26.0	20.0	20.1	26.4	06.7	-	08.7	10.3	05.5	72	41	48	54	-	0	N 2	-	0
27	739.8	738.8	741.0	16.6	21.2	13.0	16.0	23.4	12.6	-	10.7	11.3	08.6	75	60	77	71	NE 3	NE 6	NE 5		
28	740.3	740.6	741.1	11.2	11.6	11.4	11.4	13.9	10.6	-	09.5	09.5	08.3	95	93	82	90	-	0	NNE 3	WNW 2	
29	740.3	739.5	740.0	11.6	18.0	12.9	13.9	20.4	10.2	-	08.2	07.5	07.8	80	49	70	66	WNW 1	WNW 2	NE 3		
30	740.5	738.4	737.8	11.2	22.6	14.4	15.7	23.4	04.3	-	08.2	09.0	08.6	82	44	70	65	-	0	E 1	-	0
31	739.7	737.8	737.6	13.6	26.4	18.0	19.0	27.0	06.2	-	08.8	12.2	10.2	75	47	66	63	SSE 1	S 1	-	0	
MES.	VRED.	740.4	738.9	739.4	14.9	23.4	17.0	18.1	24.9	16.2	-	10.1	10.8	09.9	79	51	69	66	1.2	2.7	1.8	

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1	740.5	740.3	742.3	17.0	19.5	13.7	16.1	23.8	10.1	-	10.2	11.0	09.1	70	63	77	70	-	0	NNE 5	NE 5	
2	742.1	741.2	740.2	14.0	16.8	11.4	13.4	17.3	11.0	-	08.8	08.8	08.2	73	62	91	75	WNW 2	WSW 1	NE 3		
3	738.6	738.5	737.3	12.6	14.4	13.2	13.4	15.1	11.0	-	09.5	10.8	10.2	87	72	89	83	-	0	NW 3	-	0
4	736.4	735.8	735.5	10.8	12.8	11.6	11.7	14.4	10.2	-	09.0	07.4	08.2	93	66	80	80	N 3	NW 4	NM 1		
5	736.6	735.7	735.8	14.0	20.8	13.0	15.2	22.6	06.9	-	07.4	06.6	07.9	62	36	71	56	NNW 2	S 2	-	0	
6	737.8	736.9	738.1	12.9	22.6	15.2	16.5	24.0	06.2	-	08.7	07.4	09.0	78	36	70	61	WSW 2	W 2	SSE 2		
7	740.6	739.4	739.8	14.2	26.0	21.2	20.7	27.0	08.6	-	09.2	08.6	09.4	76	34	50	53	-	0	SE 3	E 2	
8	742.6	740.9	742.6	15.8	28.2	19.2	20.6	29.3	13.6	-	10.3	11.9	12.3	77	41	74	64	-	0	SE 2	SE 3	
9	743.1	740.6	740.0	17.4	29.0	21.2	22.2	30.3	11.8	-	11.6	10.3	11.0	78	34	58	57	-	0	SW 3	S 2	
10	740.3	737.0	737.3	17.6	30.0	21.8	22.8	31.6	11.2	-	10.7	10.7	10.7	71	34	55	53	-	0	W 3	-	0
11	738.0	735.9	737.1	19.4	31.5	22.2	23.8	32.2	12.9	-	11.9	10.8	12.5	71	31	62	55	-	0	NW 3	-	0
12	738.0	735.9	738.0	21.4	32.0	18.6	22.7	32.9	13.3	-	11.5	12.8	14.9	60	36	93	63	-	0	N 2	SE 1	
13	738.9	737.0	736.9	18.2	31.0	25.4	25.0	31.6	13.5	-	13.9	13.3	13.6	85	40	56	62	NE 1	WNW 3	NNE 5		
14	737.0	735.5	734.6	18.6	31.2	24.4	24.7	33.4	14.5	-	14.6	15.9	17.6	91	47	77	72	-	0	S 2	SSE 1	
15	735.9	732.8	732.8	20.8	32.6	24.8	25.8	34.4	15.6	-	13.2	11.9	11.2	72	32	48	51	-	0	SE 2	NE 3	
16	733.1	730.6	732.1	20.8	30.0	19.4	22.5	31.3	13.8	-	11.2	11.0	14.4	61	34	84	60	-	0	SW 2	SSW 2	
17	734.4	736.0	736.8	16.4	18.8	15.6	21.6	15.4	-	12.6	12.5	12.2	90	77	92	86	NNE 3	NW 3	-	0		
18	737.0	737.2	736.8	19.4	28.8	22.8	23.5	30.0	13.9	-	13.3	13.6	14.3	79	46	69	65	NNE 3	NW 2	S 2		
19	737.5	736.1	736.1	20.0	32.2	24.4	25.3	33.4	15.6	-	14.8	13.1	12.6	84	36	55	58	-	0	W 3	-	0
20	737.2	734.8	736.4	21.0	32.4	22.8	24.8	33.4	14.9	-	12.3	12.0	11.4	66	33	55	51	-	0	SW 2	NE 4	
21	738.6	737.0	736.2	20.8	31.9	24.6	25.5	31.9	14.4	-	12.4	10.6	10.7	67	30	46	48	-	0	NW 3	NE 2	
22	736.6	733.5	734.0	21.2	31.2	22.8	24.5	33.1	15.8	-	13.0	11.8	1									

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 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Dan	Vreme 0-9	Obločnost N (0-10)					Iskoljenje bez snij.	Padavine R mm	Snežni pokrivali h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7	060	090	02	05.7	-	-	-	-	-
2	7	030	040	09	05.3	-	-	-	-	-
3	8	010	020	04	02.3	-	-	-	-	-
4	7	010	020	05	02.7	-	-	-	-	-
5	7	10	09	10	09.7	-	-	-	-	-
6	7	10	080	10	09.3	-	00.0	-	-	-
7	7	09	06	10	08.3	-	01.4	-	-	-
8	8	060	060	10	07.3	-	-	-	-	-
9	7	040	060	01	03.7	-	06.6	-	-	-
10	7	08	09	09	08.7	-	00.0	-	-	-
11	7	10	10	00	06.7	-	04.6	-	-	-
12	7	020	040	00	02.0	-	-	-	-	-
13	8	010	05	02	02.7	-	-	-	-	-
14	7	000	070	10	05.7	-	-	-	-	-
15	7	08	10	10	09.3	-	-	-	-	-
16	7	10	030	00	04.3	-	05.9	-	-	-
17	7	020	090	04	05.0	-	00.0	-	-	-
18	8	07	070	07	07.0	-	-	-	-	-
19	7	09	01	00	03.3	-	-	-	-	-
20	7	030	060	00	03.0	-	-	-	-	-
21	7	060	090	06	07.0	-	-	-	-	-
22	7	10	09	07	08.7	-	00.0	-	-	-
23	8	000	020	04	02.0	-	-	-	-	-
24	7	000	040	04	02.7	-	-	-	-	-
25	7	10	010	00	03.7	-	-	-	-	-
26	7	000	020	02	01.3	-	-	-	-	-
27	7	040	090	05	07.3	-	00.4	-	-	-
28	7	100	100	09	09.7	-	01.7	-	-	-
29	7	10	08	01	06.3	-	03.8	-	-	-
30	7	020	020	01	01.7	-	-	-	-	-
31	7	000	020	05	02.3	-	-	-	-	-
MES. VR ED.		05.2	05.8	04.9	05.3	-	24.4			

1	7	04	10	10	08.0	-	-	-	-	-
2	7	10	10	10	10.0	-	00.8	-	-	-
3	7	10	100	100	10.0	-	04.8	-	-	-
4	7	100	10	10	10.0	-	04.9	-	-	-
5	7	020	040	00	02.0	-	00.0	-	-	-
6	7	050	080	00	04.3	-	-	-	-	-
7	8	000	030	05	02.7	-	-	-	-	-
8	7	020	030	090	04.7	-	-	-	-	-
9	7	000	030	00	01.0	-	00.8	-	-	-
10	7	000	030	02	01.7	-	-	-	-	-
11	7	000	040	01	01.7	-	-	-	-	-
12	8	050	050	04	04.7	-	-	-	-	-
13	7	010	030	09	04.3	-	01.6	-	-	-
14	7	000	010	03	01.3	-	05.4	-	-	-
15	7	020	020	00	01.3	-	-	-	-	-
16	7	060	050	10	07.0	-	-	-	-	-
17	7	100	09	00	06.3	-	02.2	-	-	-
18	7	020	030	00	01.7	-	05.4	-	-	-
19	7	010	010	02	01.3	-	-	-	-	-
20	7	030	040	01	02.7	-	-	-	-	-
21	7	010	020	00	01.0	-	-	-	-	-
22	7	030	020	01	02.0	-	-	-	-	-
23	7	010	06	02	03.0	-	-	-	-	-
24	8	030	030	02	02.7	-	-	-	-	-
25	7	000	030	02	01.7	-	00.0	-	-	-
26	7	060	09	040	06.3	-	-	-	-	-
27	7	09	06	100	08.3	-	00.5	-	-	-
28	7	10	060	01	05.7	-	02.5	-	-	-
29	7	000	010	02	01.0	-	-	-	-	-
30	7	040	05	06	05.0	-	-	-	-	-
MES. VR ED.		03.7	04.8	03.9	04.1	-	29.3			

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 $\varphi = 41^{\circ}58'$  N  $\lambda = 21^{\circ}39'$  E Gr.  $\Delta G = + 1h 27 min.$ 

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	740.0	739.8	741.8	20.4	22.9	16.4	19.0	27.6	16.4	-	12.6	12.2	12.9	70	58	92	73	NW	2	NE	5	NNW	2	
2	741.7	741.3	741.0	17.9	25.6	20.4	21.1	26.6	16.0	-	11.9	08.0	12.0	77	33	67	59	NNW	2	NNE	4	NNE	3	
3	742.5	741.0	740.6	20.4	28.8	20.4	22.5	29.0	15.0	-	12.8	11.3	12.3	71	38	68	59	NW	1	N	5	-	0	
4	739.5	735.0	735.0	19.6	31.0	24.2	24.8	32.5	12.6	-	12.7	12.0	13.6	74	36	60	57	-	0	NW	2	-	0	
5	735.9	733.1	734.4	20.9	31.4	24.1	25.1	32.9	16.4	-	12.6	13.8	13.3	68	40	59	56	-	0	NNW	2	ESE	1	
6	733.8	732.8	736.2	20.9	25.4	20.8	22.0	28.4	17.6	-	13.9	14.8	13.2	75	61	72	69	-	0	NNE	6	NNE	4	
7	738.7	737.5	737.8	19.4	28.6	21.7	22.9	30.3	14.4	-	12.5	11.7	11.9	74	40	61	58	-	0	NW	2	S	2	
8	739.0	737.3	737.6	18.8	32.8	26.6	26.2	33.8	13.1	-	11.7	13.9	14.9	72	37	57	55	-	0	SE	4	SE	2	
9	737.7	735.0	736.3	21.5	36.6	26.2	27.6	38.6	17.2	-	13.4	15.4	11.7	70	33	46	50	NE	1	S	2	NE	4	
10	737.4	735.4	733.9	22.6	34.0	26.4	27.4	34.8	16.4	-	12.3	12.8	14.3	60	32	56	49	-	0	NE	3	NE	5	
11	737.6	736.3	737.8	23.0	27.3	22.1	23.6	29.4	17.6	-	12.4	11.4	10.9	59	42	54	52	-	0	NNW	5	N	4	
12	736.9	736.1	738.7	21.7	21.8	21.0	22.8	28.2	18.2	-	11.2	10.7	11.7	58	39	63	53	NNW	4	N	5	NW	2	
13	740.3	739.3	739.8	21.2	28.0	21.6	23.1	29.6	15.3	-	11.6	10.5	11.4	58	37	59	51	NNW	2	N	4	NE	1	
14	741.0	738.1	736.9	18.6	31.7	25.8	25.5	32.8	12.2	-	11.5	12.3	13.5	72	35	54	54	-	0	NNW	3	-	0	
15	739.8	736.3	736.0	19.6	33.8	26.6	26.8	35.6	14.4	-	11.6	13.9	13.0	68	35	49	51	-	0	S	3	S	2	
16	742.0	742.6	741.5	20.2	27.4	22.3	23.1	28.6	18.0	-	12.7	12.9	12.5	71	47	62	60	NE	5	NNE	4	-	0	
17	740.2	736.3	738.1	19.9	31.8	22.2	24.0	33.8	12.6	-	12.8	18.5	12.8	73	52	64	63	H	2	ESE	5	NE	3	
18	740.6	738.6	737.4	20.2	29.2	23.2	24.0	30.2	15.0	-	13.5	13.6	11.4	76	45	54	58	-	0	NNE	4	SSW	1	
19	736.6	735.7	736.2	19.4	31.8	25.0	25.3	33.0	13.8	-	11.4	14.9	12.6	67	42	53	54	-	0	W	2	S	2	
20	738.6	737.0	737.9	23.6	31.2	26.6	27.0	32.3	16.9	-	15.7	11.5	11.5	72	34	44	50	N	3	S	3	NE	4	
21	738.4	735.8	736.3	22.4	33.0	24.4	26.1	34.0	18.4	-	13.3	14.0	12.6	65	37	55	52	NNW	1	SE	2	NE	2	
22	739.3	735.8	737.8	22.2	30.7	20.4	23.4	32.1	18.6	-	13.1	14.5	14.3	65	44	75	63	NNW	2	NW	3	E	1	
23	736.3	736.0	738.8	18.4	22.0	18.6	19.4	28.5	16.0	-	14.7	14.4	12.6	93	72	78	81	NNW	1	W	3	WSW	2	
24	738.9	738.8	738.8	17.2	22.8	18.8	19.4	25.3	16.4	-	13.0	12.8	14.8	89	61	91	80	NW	3	WSW	2	NE	2	
25	737.2	733.4	731.8	17.4	30.4	24.4	24.2	31.1	13.0	-	12.9	11.7	12.3	87	36	54	59	-	0	SE	2	ESE	1	
MES.	VRED.	738.5	736.7	737.2	20.4	30.0	23.4	24.3	31.7	16.0	-	12.8	13.1	12.9	72	42	61	56	1.1	3.2	2.3			

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1	731.8	731.5	733.1	23.8	31.0	23.5	25.5	31.6	17.6	-	12.6	09.6	09.6	57	28	44	43	S	2	WSW	5	N	5
2	736.1	735.1	735.8	16.9	25.6	21.6	21.4	26.6	16.2	-	11.6	11.2	10.6	80	46	55	60	NNW	2	E	2	NNE	4
3	738.8	737.4	738.7	16.4	28.2	21.8	22.1	29.3	16.2	-	12.9	12.2	10.7	92	42	55	63	N	2	N	1	NNE	2
4	741.6	741.1	742.1	17.4	30.2	24.4	24.1	31.0	14.0	-	11.9	12.4	10.8	80	39	47	55	-	0	NW	2	NNE	5
5	743.3	740.3	738.8	18.8	31.6	25.2	25.2	32.6	14.9	-	10.6	11.1	11.0	65	32	46	48	-	0	NNW	2	S	2
6	739.0	736.0	738.6	20.4	31.7	19.0	22.5	32.4	16.3	-	11.4	13.3	15.9	64	38	96	66	N	1	N	3	NW	2
7	738.2	737.7	737.9	18.4	25.4	21.6	21.8	27.2	17.6	-	15.0	14.8	14.0	94	61	72	76	-	0	SSE	1	NE	2
8	738.6	737.5	739.1	18.6	28.8	19.6	21.7	29.6	16.3	-	14.3	15.1	14.1	89	51	82	74	-	0	NW	2	S	2
9	741.0	739.8	740.4	17.6	29.1	20.3	21.8	30.7	14.4	-	13.4	14.3	15.2	89	47	85	74	SSE	1	SSE	2	S	3
10	741.2	738.9	739.0	18.2	30.6	23.4	23.9	31.4	14.8	-	13.1	13.7	14.3	84	42	66	64	-	0	SE	3	SW	2
11	739.5	737.1	737.6	18.4	29.6	26.4	22.2	31.2	16.0	-	14.1	14.4	14.6	89	46	81	72	-	0	S	2	S	2
12	738.6	737.5	738.9	19.2	30.4	22.8	23.8	31.1	15.8	-	15.2	16.0	14.9	91	49	72	71	-	0	NE	3	-	0
13	740.0	737.9	738.8	18.6	31.4	22.4	23.7	32.0	15.4	-	14.3	16.5	12.8	89	48	62	67	-	0	ENE	1	NE	5
14	739.8	738.1	740.3	19.2	27.0	16.6	20.9	30.1	15.4	-	13.4	13.4	11.3	80	50	70	67	-	0	W	7	ENE	3
15	740.5	739.5	740.8	15.6	27.6	22.0	21.8	29.2	11.6	-	11.4	12.0	11.2	86	43	56	62	-	0	W	2	NNE	5
16	742.0	741.1	741.2	19.2	27.8	21.2	22.4	28.2	15.8	-	11.8	10.6	11.6	70	38	61	56	-	0	N	3	SW	2
17	742.2	740.9	740.9	17.8	27.8	20.9	21.9	29.9	12.6	-	11.4	11.5	10.6	75	41	57	58	NE	3	WNN	2	S	2
18	741.8	739.9	739.4	16.4	31.1	25.2	24.5	32.7	12.8	-	10.8	12.6	14.9	77	37	62	59	-	0	S	3	SSE	3
19	738.9	739.5	734.6	20.2	32.6	26.4	26.4	35.1	18.0	-	15.3	14.9	10.1	86	40	39	55	NW	2	WNN	3	S	2
20	736.3	735.2	735.5	21.2	31.6	24.2	25.3	32.2	17.9	-	11.9	11.1	10.1	63	32	45	47	-	0	SW	4	NNM	4
21	736.9	733.6	731.4	17.2	32.4	27.1	26.0	34.7	12.2	-	09.4	12.3	10.3	64	34	38	45	ESE	1	NE	1	S	2
22	730.6	727.3	728.7	26.0	38.0	26.7	30.4	38.6	22.0	-	11.5	10.2	11.6	46	20	39	35	SE	3	SSW	6	WSW	3
23	731.9	731.7	733.6	22.7	31.4	22.8	24.9	33.0	19.4	-	13.1	12.5	09.7	63	36	47	49	S	3	-	0	NNW	2
24	733.2	734.6	736.5	19.2	15.4	15.6	16.5	20.3	14.4	-	10.3	11.8	10.4	62	90	78	77	NE	2	W	2	N	3
25	737.5	738.9	741.3	16.0	20.8	16.6	17.6	23.2	11.6	-	09.5	09.4	09.1	70	51								

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 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Dan	Vrijnost 0.9	Oblačnost N (0-10)				Insolicijski broj sunca	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies			
1	7	010	07	07	05.0	-	.	.	$\zeta 2-3^{\circ} 10^{\circ} 14^{\circ} 15^{\circ} 17^{\circ} 18^{\circ} 19^{\circ} 10^{\circ}; T 12^{\circ} 15^{\circ} 10^{\circ} i, \bullet 12^{\circ} 15^{\circ} 10^{\circ} i, 19^{\circ} 21^{\circ}$
2	7	10	05	03	06.0	-	01.0	.	$\overline{\bullet} 3^{\circ} 10^{\circ} 14^{\circ} \overline{F} NNE 9^{\circ} 13^{\circ}$
3	7	000	040	00	01.3	-	.	.	$\overline{\bullet} 3^{\circ} 10^{\circ} 14^{\circ} \overline{F} NNE 9^{\circ} 15^{\circ}$
4	7	000	010	00	00.3	-	.	.	
5	7	070	07K	04	06.0	-	.	.	$T 13^{\circ} 10^{\circ} 14^{\circ} i, \overline{\bullet} 14^{\circ} 15^{\circ} 15^{\circ}, \overline{\bullet} 20^{\circ} 21^{\circ} 15^{\circ}$
6	7	020	10K	06	06.0	-	00.5	.	$T^1 H^{\circ} H^{\circ} 13^{\circ} 14^{\circ} 15^{\circ}, \overline{\bullet} 14^{\circ} 15^{\circ} 15^{\circ}, \overline{\bullet} 14^{\circ} 15^{\circ} 16^{\circ}$
7	7	000	010	00	00.3	-	05.0	.	
8	7	000	030	01	01.3	-	.	.	
9	7	020	000	00	00.7	-	.	.	
10	7	000	030	04	02.3	-	.	.	$\zeta 20^{\circ} 24$
11	7	060	040	10	06.7	-	.	.	$\zeta 0-10^{\circ} NNE, NW 8^{\circ} 10^{\circ}, 13^{\circ} 19^{\circ} 20^{\circ}$
12	7	030	040	02	03.0	-	.	.	$\overline{F} 9^{\circ} 17^{\circ} 22^{\circ}$
13	7	010	030	00	01.3	-	.	.	$\overline{F} 9^{\circ} 10^{\circ}$
14	7	000	020	00	00.7	-	.	.	
15	7	000	000	01	00.3	-	.	.	
16	7	020	000	00	00.7	-	.	.	$F_{NE} 0-130$
17	7	060	090	03	06.0	-	.	.	$F_{S,NW} 12-13, 16^{\circ} 22^{\circ} 19^{\circ} 20^{\circ}, \overline{F}_{NE} 17^{\circ} 20^{\circ} 17^{\circ} 22^{\circ}$
18	7	020	010	00	01.0	-	.	.	
19	7	020	020	00	01.3	-	.	.	
20	7	060	030	03	04.0	-	.	.	
21	7	000	030	00	01.0	-	.	.	$T 16^{\circ} 17^{\circ} 20^{\circ}, \bullet 17^{\circ} 20^{\circ} 17^{\circ} 25^{\circ}$
22	7	020	060	09	05.7	-	00.0	.	$T^1 13^{\circ} 16^{\circ} i, 19^{\circ} 20^{\circ} 22^{\circ}, R^1 15-18^{\circ} i, \bullet 15-16^{\circ} i, 18-19^{\circ} 21^{\circ}, \overline{\bullet} 17^{\circ} 20^{\circ} 18^{\circ}$
23	6	020	10K	09	07.0	-	01.4	.	
24	7	10	08	00	06.0	-	02.3	.	$\overline{\bullet} 2^{\circ} 5^{\circ} 10^{\circ} 17^{\circ} 20^{\circ}, \overline{\bullet} 8^{\circ} 12^{\circ} 15^{\circ} 18^{\circ}, \overline{F}_S 13^{\circ} 12^{\circ} 14^{\circ} 15^{\circ} i$
25	7	000	010	02	01.0	-	06.2	.	$\overline{\Delta} 0-3^{\circ}, \overline{\bullet} 4^{\circ} 8^{\circ} 9^{\circ}$
26	7	000	020	01	01.0	-	.	.	
27	7	07	04	00	03.7	-	.	.	$F_{NE} 18^{\circ} 22^{\circ} 24$
28	7	000	010	01	00.7	-	.	.	
29	7	07	020	00	02.0	-	.	.	
30	7	000	010	00	00.3	-	.	.	
31	7	040	000	00	01.3	-	.	.	$F_S 13^{\circ} 19^{\circ} 20^{\circ} i$
MES.	VRED.	02.6	03.5	02.1	02.7	-	10.4		

1	8	050	040	02	03.7	-	.	.	$F_{NW, N} 5^{\circ} 15^{\circ} 21^{\circ} 24^{\circ}$
2	7	100	050	03	06.0	-	00.0	.	$\bullet 0-10^{\circ}, \overline{\bullet} 5^{\circ} 10^{\circ}$
3	7	09	020	02	04.3	-	00.5	.	$\bullet 5^{\circ} 6^{\circ} 10^{\circ}$
4	7	030	030	00	02.0	-	.	.	$\overline{F} 17^{\circ} 20^{\circ} 17^{\circ} 24^{\circ}$
5	8	000	010	00	00.3	-	.	.	
6	7	020	030	10K	05.0	-	.	.	
7	7	100	020	09	07.0	-	31.8	.	
8	7	010	040	00	01.7	-	00.4	.	
9	7	000	030K	00	01.0	-	01.2	.	
10	7	000	020	10	04.0	-	.	.	
11	7	030	05K	04K	05.3	-	.	.	$\overline{\Delta} 4^{\circ} 8^{\circ} 10^{\circ} T 13^{\circ} 15^{\circ} 17^{\circ} 20^{\circ}, \overline{\bullet} 14^{\circ} 15^{\circ} 15^{\circ} i, \overline{\bullet} 15^{\circ} 16^{\circ} 17^{\circ} 24^{\circ}, \overline{\bullet} 15^{\circ} 16^{\circ} 17^{\circ} 24^{\circ}, \overline{\bullet} 15^{\circ} 16^{\circ} 17^{\circ} 24^{\circ}$
12	7	030	060	00	03.0	-	00.6	.	$T 0-10^{\circ} 14^{\circ} 16^{\circ} i, \overline{\Delta} 0^{\circ} 3^{\circ} 5^{\circ} 10^{\circ} \overline{F} 15-16^{\circ} 20^{\circ}$
13	7	040	040	01	03.0	-	.	.	$\overline{\Delta} 5^{\circ} 7^{\circ} 9^{\circ} 11^{\circ} \overline{F} 10^{\circ} 12^{\circ} 14^{\circ} 16^{\circ} \overline{\bullet} 14^{\circ} 15^{\circ} 15^{\circ} i, \overline{\bullet} 15^{\circ} 16^{\circ} 16^{\circ} 17^{\circ} i$
14	7	000	08K	04	04.0	-	.	.	$\overline{\Delta} 1^{\circ} 4^{\circ} 8^{\circ} 10^{\circ} T 10^{\circ} 12^{\circ} 14^{\circ} 16^{\circ} i, \overline{\bullet} 13^{\circ} 14^{\circ} 15^{\circ} i, \overline{\bullet} 14^{\circ} 15^{\circ} 15^{\circ} i, \overline{\bullet} 15^{\circ} 16^{\circ} 16^{\circ} 17^{\circ} i$
15	7	000	030	03	02.0	-	00.4	.	$\overline{\Delta} 0-8^{\circ}, \overline{\bullet} 4^{\circ} 8^{\circ} 10^{\circ}, \overline{F} 23^{\circ} 24^{\circ}$
16	7	000	050	00	01.7	-	.	.	
17	7	000	010	00	00.3	-	.	.	
18	7	000	020	00	00.7	-	.	.	
19	7	010	03	02	02.0	-	.	.	$\zeta 20^{\circ} 21^{\circ} 30^{\circ}$
20	8	010	030	00	01.3	-	.	.	
21	7	000	020	00	00.7	-	.	.	
22	8	000	040	03	02.3	-	.	.	$\overline{F} 9^{\circ} 16^{\circ} i$
23	7	020	030	02	02.3	-	.	.	
24	6	09	10K	06	08.3	-	00.0	.	$\bullet 4^{\circ} 8^{\circ} 10^{\circ} 12^{\circ} 14^{\circ} 16^{\circ}, \overline{\bullet} 13^{\circ} 15^{\circ} 15^{\circ}, \overline{\bullet} 19^{\circ} 20^{\circ} 20^{\circ} i$
25	7	060	09	00	05.0	-	07.5	.	$\overline{\bullet} NW 7^{\circ} 10^{\circ} \overline{F} 23^{\circ} 24^{\circ}$
26	7	000	000	00	00.0	-	.	.	$\overline{\Delta} 0-7^{\circ} \overline{\bullet} 0^{\circ} 2^{\circ} 10^{\circ}$
27	7	000	010	00	00.3	-	.	.	$\overline{\Delta} 0-7^{\circ} \overline{\bullet} 0^{\circ} 4^{\circ} 6^{\circ} 8^{\circ} 20^{\circ}$
28	7	000	000	00	00.0	-	.	.	
29	7	000	000	00	00.0	-	.	.	$\overline{\Delta} 0^{\circ} 4^{\circ} 7^{\circ} 10^{\circ}$
30	7	000	010	00	00.3	-	.	.	$\overline{= 5^{\circ} 9^{\circ} 10^{\circ} T 19^{\circ} 21^{\circ} 25^{\circ}}$
31	7	10	020	10K	07.3	-	.	.	
MES.	VRED.	02.5	03.4	02.3	32.7	-	42.4		

$\varphi = 41^{\circ}58' N \lambda = 21^{\circ}39' E$  Gr.  $\Delta G = + 1h 27 min.$

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D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenje pare e mm			Relativna vlažnost v %			Pravac i jačina vetra D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	739.8	739.0	740.2	19.6	27.4	24.0	23.8	29.2	15.0	-	11.8	12.9	10.2	65	47	46	54	NE	2	-	0	NE	4
2	740.6	738.3	738.0	17.6	29.6	23.2	23.4	30.4	13.4	-	11.5	11.2	12.9	76	36	60	57	-	0	SW	2	WWN	3
3	738.0	736.0	737.8	20.0	27.8	19.6	21.8	29.2	18.4	-	13.0	11.8	13.5	74	42	79	65	-	0	N	2	S	2
4	739.0	737.7	739.7	16.7	29.1	23.6	23.3	29.7	12.7	-	14.3	09.8	11.2	100	32	51	61	-	0	N	2	NNW	2
5	741.4	739.7	741.3	17.0	29.8	21.6	22.5	30.4	12.9	-	10.7	11.1	10.3	74	35	53	54	E	1	N	3	-	0
6	743.3	742.1	743.7	15.6	25.6	21.1	20.9	30.1	12.1	-	09.9	10.2	11.0	75	42	58	58	ENE	1	NW	4	SSE	2
7	743.5	741.4	742.8	18.3	25.9	19.8	21.0	28.4	14.9	-	10.9	12.7	13.4	69	51	77	66	-	0	NW	3	-	0
8	743.0	740.7	740.7	16.6	29.4	22.4	22.7	30.0	13.2	-	11.5	09.8	10.4	81	32	51	55	-	0	N	2	SSE	1
9	740.0	737.9	735.9	15.4	30.2	19.2	21.0	31.4	11.6	-	10.5	08.9	09.9	80	28	59	56	S	1	N	1	SSW	1
10	742.3	742.5	743.4	11.8	14.8	13.6	13.5	22.0	10.9	-	08.4	07.3	07.9	81	57	67	68	W	1	N	4	NNE	3
11	744.5	743.9	746.1	14.1	20.7	15.2	16.3	21.6	13.2	-	05.5	06.1	06.3	46	33	48	42	N	4	N	4	NNE	1
12	747.4	745.8	746.6	12.7	24.2	18.2	18.3	25.5	09.8	-	07.1	09.4	08.0	64	41	51	52	-	0	W	3	ENE	1
13	744.5	741.7	741.5	12.1	27.9	17.3	18.7	29.2	08.2	-	08.0	09.4	08.1	76	33	55	55	-	0	NNW	2	ESE	1
14	745.1	746.8	747.9	14.0	20.8	14.4	15.9	21.0	10.0	-	08.6	09.2	06.8	72	50	55	59	NW	1	N	6	N	4
15	746.0	742.3	740.1	09.6	23.9	14.6	15.7	24.8	05.1	-	06.1	08.1	07.8	68	36	63	56	-	0	-	0	-	0
16	737.8	734.8	736.5	11.1	27.1	20.9	20.0	28.0	07.7	-	06.5	08.0	08.2	66	30	44	47	-	0	ESE	1	N	4
17	738.1	736.3	737.4	14.2	26.0	20.4	20.3	26.8	14.0	-	08.2	08.6	10.1	68	34	56	53	S	1	SSE	2	SSE	3
18	738.8	738.8	739.3	17.8	18.2	17.5	17.8	20.4	15.0	-	10.3	12.8	11.4	68	82	76	75	-	0	NNW	1	NW	1
19	742.5	741.4	742.0	14.8	28.2	20.4	21.0	30.0	09.0	-	11.6	11.1	12.0	92	39	67	66	-	0	NE	2	E	1
20	742.2	740.3	739.0	15.2	27.2	21.4	21.3	27.6	13.6	-	10.8	11.6	12.8	83	43	67	64	-	0	SE	4	NE	2
21	737.5	736.8	739.0	16.6	29.8	21.2	22.2	30.3	15.2	-	12.0	07.7	08.0	85	24	42	50	-	0	W	4	-	0
22	740.4	739.4	739.4	13.8	27.2	21.2	20.9	27.4	11.8	-	07.5	07.9	06.6	64	29	35	43	-	0	ESE	2	NW	3
23	739.2	738.7	738.6	16.6	16.6	15.1	15.9	21.6	15.0	-	09.3	11.2	09.1	66	79	71	72	NW	2	NN	3	NNE	3
24	737.0	737.2	740.7	13.1	12.4	11.6	12.2	15.4	11.6	-	08.1	08.7	08.1	72	80	79	77	NNW	2	NW	3	MNW	3
25	743.6	743.4	744.5	09.6	19.0	13.1	13.7	20.2	07.6	-	07.1	06.2	07.6	80	38	67	62	-	0	NE	2	NE	2
26	746.1	746.8	748.0	12.4	13.4	12.2	12.6	14.4	09.9	-	07.8	08.0	07.9	72	69	74	72	NE	2	SE	2	-	0
27	747.9	748.4	749.4	11.0	11.8	11.1	11.3	12.6	10.0	-	08.5	08.1	08.7	86	78	87	84	NE	2	NE	3	-	0
28	750.1	749.7	751.7	09.8	15.1	08.0	10.2	16.0	07.4	-	06.3	04.4	04.1	70	34	51	52	-	0	NNW	4	NNE	2
29	753.4	751.4	751.1	01.8	14.8	06.0	07.2	15.4	-01.1	-	04.0	02.4	04.2	77	27	60	55	-	0	W	2	-	0
30	751.4	748.5	748.1	00.9	16.7	05.8	07.3	18.0	-02.3	-	03.6	04.1	04.6	73	29	67	56	ESE	1	NE	1	-	0
MES.	RED.			742.8	741.6	742.3	13.7	23.0	17.1	17.8	24.6	10.9	-	09.0	09.0	09.0	74	44	60	60	0.7	2.5	1.6

1	747.3	742.6	741.9	02.4	21.8	16.5	11.5	23.6	-01.6	-	04.2	04.9	04.6	78	25	47	50	-	0	-	0	E	1
2	740.8	736.9	736.0	04.2	24.8	16.9	15.7	25.4	01.8	-	04.3	06.6	08.2	65	28	57	51	-	0	-	0	NW	1
3	734.6	740.0	743.8	11.9	10.4	07.6	09.4	17.0	07.6	-	07.7	08.0	05.8	74	85	74	78	NNE	5	N	3	NW	2
4	747.7	747.0	747.9	02.4	16.4	07.2	08.3	17.4	00.6	-	04.9	05.3	05.3	90	38	70	66	NE	1	ENE	1	-	0
5	748.7	746.2	746.5	01.0	19.8	08.7	09.6	20.9	-00.8	-	03.8	04.8	04.8	78	27	57	54	-	0	-	0	NE	1
6	746.3	743.3	743.3	02.0	21.4	10.0	10.9	22.8	-00.4	-	03.6	05.0	05.8	68	26	63	52	-	0	SM	2	-	0
7	743.8	741.0	741.3	04.8	24.2	10.7	12.6	24.3	01.4	-	04.5	06.3	06.6	70	28	68	55	-	0	-	0	0	0
8	741.7	739.1	739.3	06.6	24.0	15.9	15.6	25.2	02.3	-	05.4	07.0	06.9	73	31	51	52	-	0	S	3	ESE	2
9	739.3	736.7	737.9	10.1	23.7	17.8	17.4	24.4	07.4	-	06.7	08.7	08.6	72	40	56	56	-	0	SSE	3	SE	1
10	739.4	739.6	740.8	11.4	22.2	17.1	17.0	23.4	10.8	-	08.1	10.0	09.7	80	50	66	65	-	0	WSW	2	S	2
11	741.3	740.3	742.1	11.9	21.7	13.8	15.3	21.8	05.2	-	08.6	10.9	10.7	82	56	90	76	-	0	SE	3	-	0
12	742.2	742.9	743.1	13.1	18.6	14.8	15.3	20.2	13.0	-	10.6	10.2	10.6	94	63	84	80	-	0	ESE	2	-	0
13	743.6	743.7	744.8	14.1	18.7	13.7	15.1	19.4	13.6	-	10.2	14.0	05.6	84	62	81	76	NE	2	SSE	1	-	0
14	744.2	742.0	742.9	09.8	19.4	13.9	14.3	20.8	07.8	-	07.7	06.8	06.6	84	40	55	60	-	0	WSW	2	W	1
15	743.6	742.2	743.6	07.1	19.9	15.2	14.4	20.8	05.2	-	06.7	07.9	08.7	88	45	67	67	-	0	NNE	3	-	0
16	745.0	744.9	746.1	12.8	17.0	11.6	13.3	18.0	11.6	-	07.6	05.3	06.0	68	36	59	54	N	3	NNW	2	NE	3
17	749.0	747.7	748.6	06.1	15.9	06.1	08.6	17.0	04.0	-	05.5	03.7	04.6	78	27	65	57	E	1	-	0	E	1
18	750.0	747.9	749.6	01.1	17.6	07.6	08.5	19.4	-00.5	-	03.9	03.5	05.2	78	23	67	56	-	0	C	-	0	0
19	750.6	748.5	748.2	02.2	20.8	08.2	09.9	21.4	-00.4	-	04.0	03.9	05.2	74	21	64	53	-	0	-	0	0	0
20	749.4	747.3	748.0	01.8	21.8	14.8	13.3	23.1	-00.2	-	04.1	05.3	05.1	79	27	40	49	-	0	SW	1	-	0
21	750.5	749.0	750.6	03.9	20.9	12.7	12.6	21.0	01.9	-	04.8	05.2											

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 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Dan	Visina 0-9	Oblačnost N (0-10)					Insolj. broj sat	Padavine R mm	Snežni pokrivač h cm	Rozvoj vremena w
		14	7	14	21	Sred Dnes				
1	7	060	030	10	06.3	-	-	-	-	$\oplus 030-140$
2	7	060	020	10	06.0	-	-	-	-	$= 60-940$
3	7	09	060	10	06.3	-	-	-	-	$\ominus 0^{\circ} 1845-1945$
4	7	07	040	03	04.7	-	00.1	-	-	-
5	7	000	040	01	01.7	-	-	-	-	-
6	7	010	084	00	03.0	-	-	-	-	$T^{\circ} 13^{\circ} 14^{\circ} 0$
7	7	010	034	10	04.7	-	-	-	-	$T^{\circ} 13^{\circ} 17^{\circ} 5^{\circ} i, \Delta^{\circ} 13^{\circ} 16^{\circ} 5^{\circ} i$
8	7	06	040	00	03.3	-	03.3	-	-	$\Delta^{\circ} 13^{\circ} 8^{\circ} 0$
9	7	000	010	02	01.0	-	-	-	-	$\Delta^{\circ} 0-740, \text{NNW } 2140-24$
10	7	100	090	10	09.7	-	00.7	-	-	$\overline{F_N} 0-6, \Delta^{\circ} 6^{\circ} 8, 13^{\circ} 14^{\circ} 0$
11	7	10	08	02	06.7	-	00.0	-	-	-
12	7	09	020	00	03.7	-	-	-	-	$= 60-945$
13	7	000	010	00	00.3	-	-	-	-	$\Delta^{\circ} 0-720$
14	7	03	000	00	01.0	-	-	-	-	$\overline{F_N} 8^{\circ} 10^{\circ} 0$
15	7	000	010	00	00.3	-	-	-	-	-
16	7	00	030	10	04.3	-	-	-	-	-
17	7	06	040	00	03.3	-	-	-	-	-
18	6	10	10	06	06.7	-	-	-	-	$\oplus 0^{\circ} 845-1120 = 10^{\circ} 24$
19	7	05	060	03	04.7	-	01.6	-	-	$\overline{F_N} 0-945 = 0^{\circ} 35^{\circ} 510$
20	7	06	09	100	08.3	-	-	-	-	$\oplus 0^{\circ} 1045-1140, 1942-2140, \overline{F_N} 16^{\circ} 16^{\circ} 2$
21	8	07	030	05	05.0	-	00.0	-	-	-
22	8	020	040	10	05.3	-	-	-	-	-
23	7	100	100	10	10.0	-	00.0	-	-	$\bullet^{\circ} 6^{\circ} 8^{\circ} 12^{\circ} 4^{\circ} 5^{\circ} 20$
24	6	10	100	10	10.0	-	00.6	-	-	$\bullet^{\circ} 6^{\circ} 8^{\circ} 15^{\circ} 10^{\circ}, 1840-2020$
25	7	030	07	05	05.0	-	03.6	-	-	-
26	7	10	10	10	10.0	-	-	-	-	$\bullet^{\circ} 14^{\circ} 10^{\circ} 0$
27	7	10	10	10	10.0	-	00.0	-	-	$\bullet^{\circ} 13^{\circ} 15^{\circ} 4^{\circ}, = 20^{\circ} 24$
28	7	10	08	00	06.0	-	02.0	-	-	$= 0-840$
29	7	000	010	00	00.3	-	-	-	-	$\overline{F_N} 0^{\circ} 6^{\circ} 4^{\circ} 0$
30	7	000	000	00	00.0	-	-	-	-	$\overline{F_N} 0^{\circ} 2^{\circ} 7^{\circ} 0$
MES. VRED.		05.2	05.0	04.9	05.1	-	11.9			

1	7	030	030	00	02.0	-	-	-	-	$\overline{F_N} 0-740$
2	7	010	060	09	05.3	-	-	-	-	-
3	7	09	100	00	06.3	-	-	-	-	$\overline{F_N} 5^{\circ} 10^{\circ} 7^{\circ} 6, \bullet^{\circ} 8-940, 10^{\circ} 11^{\circ} 14^{\circ} 0$
4	7	020	020	00	01.3	-	02.3	-	-	$\Delta^{\circ} 4-5^{\circ} 10^{\circ} = 0^{\circ} 510-7^{\circ} 15$
5	7	00	000	00	00.0	-	-	-	-	$\overline{F_N} 0-740 = 0^{\circ} 510-7^{\circ} 15$
6	7	000	000	00	00.0	-	-	-	-	-
7	7	010	020	00	01.0	-	-	-	-	-
8	7	000	000	00	00.0	-	-	-	-	-
9	7	07	050	05	07.0	-	-	-	-	-
10	7	06	08	05	06.3	-	-	-	-	$\bullet^{\circ} 10^{\circ} 20^{\circ} 5$
11	7	08	06	10	08.0	-	00.1	-	-	$= 5^{\circ} 10^{\circ} 10^{\circ} 5, \bullet^{\circ} 8^{\circ} 11^{\circ} 14^{\circ} 1, 170^{\circ} 23^{\circ} 4^{\circ}, T 17^{\circ} 20^{\circ} 2^{\circ} 4^{\circ}, \overline{F_N} 17^{\circ} 22^{\circ} 17^{\circ} 40$
12	7	100	07	10	09.0	-	09.6	-	-	$\bullet^{\circ} 10^{\circ} 10^{\circ} 5, \overline{F_N} 9^{\circ} 10^{\circ} 2^{\circ} 3^{\circ} 0, = 5^{\circ} 10^{\circ} 12^{\circ} 4^{\circ}, \bullet^{\circ} 6^{\circ} 5^{\circ} 7^{\circ} 15$
13	7	10	060	05	07.6	-	01.7	-	-	$\bullet^{\circ} 5^{\circ} 6^{\circ} 10^{\circ} = 5^{\circ} 3^{\circ} 11^{\circ} 30$
14	7	040	000	00	01.3	-	-	-	-	$= 0^{\circ} 50^{\circ} 10^{\circ} 30$
15	7	000	040	07	03.7	-	-	-	-	$= 0^{\circ} 40^{\circ} 11^{\circ} 35$
16	6	10	090	10	05.7	-	-	-	-	$= 0^{\circ} 50^{\circ} 13^{\circ} 45$
17	7	010	000	00	00.3	-	-	-	-	-
18	6	06	000	00	02.0	-	-	-	-	$\overline{F_N} 0-930 = 0^{\circ} 43^{\circ} 15^{\circ} 30$
19	7	040	000	00	01.3	-	-	-	-	$\overline{F_N} 0-730$
20	7	000	000	00	00.0	-	-	-	-	$\overline{F_N} 0^{\circ} 40^{\circ} 8$
21	7	000	020	00	00.7	-	-	-	-	$\overline{F_N} 3^{\circ} 10^{\circ} 0, = 0^{\circ} 3^{\circ} 10^{\circ} 13^{\circ} 0$
22	7	03	000	00	01.0	-	-	-	-	$\Delta^{\circ} 3^{\circ} 10^{\circ} 0 = 0^{\circ} 5^{\circ} 24^{\circ} 4^{\circ}, = 0^{\circ} 6^{\circ} 7^{\circ} 05$
23	6	000	000	00	00.0	-	-	-	-	$= 0^{\circ} 0^{\circ} 14^{\circ} 15^{\circ}$
24	6	000	040	00	01.3	-	-	-	-	$= 0^{\circ} 50^{\circ} 12^{\circ} 30$
25	7	010	010	03	01.7	-	-	-	-	-
26	6	00	000	00	00.0	-	-	-	-	$= 0^{\circ} 0^{\circ} 17^{\circ} 30$
27	5	000	000	00	00.0	-	-	-	-	$\overline{F_N} 2^{\circ} 40^{\circ} 3^{\circ} 30, = 0^{\circ} 3^{\circ} 24^{\circ} 4^{\circ}, = 0^{\circ} 5^{\circ} 2^{\circ} 15^{\circ}$
28	6	030	040	00	02.3	-	-	-	-	$= 0^{\circ} 0^{\circ} 14^{\circ} 15^{\circ}, \overline{F_N} 4^{\circ} 45^{\circ} 7^{\circ} 35$
29	6	000	000	00	00.0	-	-	-	-	$= 0^{\circ} 6^{\circ} 14^{\circ} 15^{\circ}, \overline{F_N} 3^{\circ} 24^{\circ} 4^{\circ}$
30	6	00	000	00	00.0	-	-	-	-	$= 0^{\circ} 0^{\circ} 15^{\circ} 30^{\circ}, \overline{F_N} 1^{\circ} 8^{\circ} 30^{\circ}$
31	5	10	000	00	03.3	-	-	-	-	$= 0^{\circ} 3^{\circ} 24^{\circ} 4^{\circ}, \overline{F_N} 5^{\circ} 2^{\circ} 940$
MES. VRED.		03.2	02.7	02.1	02.6	-	13.7			

$\varphi = 41^{\circ}58' N$   $\lambda = 21^{\circ}39' E$  Gr.  $\Delta G = +1h 27 min.$

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D O	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21	
1	743.8	741.8	741.0	10.2	19.0	13.4	14.0	20.0	05.2	-	05.9	07.0	06.4	63	43	56	54	-	0	ESE 1	- 0
2	740.7	740.1	741.0	12.0	14.7	12.6	13.0	14.8	10.3	-	07.7	07.5	07.5	73	60	68	67	SE 2	SSE 4	- 0	0
3	741.8	742.1	743.3	13.0	18.0	10.0	12.8	18.4	10.0	-	07.9	07.5	06.7	71	49	73	64	NNE 2	- 0	0	0
4	744.0	742.3	743.3	04.8	18.8	11.3	11.6	20.4	01.8	-	04.6	12.8	06.7	71	79	67	72	- 0	- 0	0	0
5	745.3	743.3	744.2	03.6	21.2	13.2	12.8	22.0	02.8	-	05.4	06.9	06.5	91	36	57	61	- 0	NN 1	SE 1	0
6	745.6	744.1	744.5	06.6	21.4	10.6	12.4	22.2	05.4	-	07.1	08.8	07.3	97	46	75	73	- 0	- 0	0	0
7	746.3	745.6	746.7	06.8	18.6	12.6	12.7	18.8	04.4	-	04.9	05.7	08.4	66	50	76	67	- 0	- 0	SE 1	0
8	748.6	747.7	748.9	06.6	20.0	12.0	12.7	20.2	05.8	-	06.9	09.0	08.4	95	51	80	75	- 0	SW 1	NNE 2	0
9	749.6	748.7	748.8	05.8	15.8	09.0	09.9	17.0	05.0	-	06.7	08.9	07.1	97	66	83	82	- 0	- 0	0	0
10	747.4	745.2	746.3	02.2	15.7	10.8	09.9	16.6	00.3	-	05.2	07.0	08.4	97	53	86	79	- 0	- 0	0	0
11	748.0	748.2	748.7	15.4	21.2	11.2	14.8	21.4	09.9	-	09.1	08.9	07.3	69	47	73	63	NE 3	N 2	SE 1	1
12	748.7	744.4	742.8	01.4	19.4	07.9	05.2	20.8	01.4	-	05.1	06.8	05.9	100	40	73	71	- 0	- 0	E 1	1
13	740.3	733.8	735.1	00.2	17.0	08.2	08.4	19.4	-00.3	-	04.3	06.8	07.1	93	47	87	76	- 0	- 0	0	0
14	733.3	732.5	733.2	10.9	14.0	09.0	10.7	15.6	04.8	-	07.7	08.6	08.0	78	72	93	81	ESE 3	- 0	NNE 3	1
15	732.9	731.0	731.4	05.2	20.0	13.0	14.0	21.0	08.0	-	08.3	08.1	06.6	95	44	59	66	- 0	WNW 1	SE 2	2
16	730.8	726.7	725.4	08.2	19.8	16.6	15.3	20.6	05.4	-	07.5	07.1	08.0	92	41	56	63	ESE 1	SE 5	E 2	2
17	727.6	730.4	731.9	07.0	14.4	10.2	10.5	16.7	06.6	-	06.5	03.8	04.6	87	31	50	56	N 2	WNW 4	S 1	1
18	730.5	731.7	736.2	11.0	17.2	06.8	10.5	17.6	05.8	-	06.8	07.6	04.8	69	51	65	62	SE 2	WNW 2	NNE 4	3
19	738.3	738.8	743.6	06.0	10.0	05.4	06.7	10.4	05.4	-	05.6	06.4	04.5	79	70	67	72	N 1	NNE 2	N 3	3
20	744.1	742.3	741.1	00.8	01.1	00.1	00.5	05.4	00.1	-	04.9	04.9	04.6	100	98	100	95	NN 1	- 0	0	0
21	740.1	739.6	739.9	00.6	05.6	01.2	02.2	06.0	-00.2	-	04.1	04.6	04.5	86	70	90	82	S 1	SE 1	- 0	0
22	739.6	738.1	737.3	-01.2	04.4	06.0	03.8	06.0	-02.0	-	04.1	05.2	06.4	98	82	92	91	- 0	ESE 2	- 0	0
23	737.9	736.0	739.3	06.0	12.2	04.2	06.7	12.2	04.2	-	06.8	08.6	05.6	97	91	89	- 0	W 2	NNE 6	6	6
24	744.3	744.0	742.9	02.6	08.2	01.6	03.5	08.2	01.0	-	05.3	04.9	04.6	95	61	90	82	N 2	NW 2	- 0	0
25	739.9	738.9	735.1	02.6	07.6	06.8	06.0	07.6	-00.3	-	05.3	06.2	06.7	97	79	91	89	- 0	0	NN 1	1
26	726.1	720.7	725.1	11.2	12.0	08.2	09.9	14.4	05.4	-	08.8	08.8	07.3	89	82	90	87	SE 4	NW 2	SW 2	2
27	727.8	729.5	734.7	06.2	11.4	07.2	08.0	12.6	05.7	-	05.9	05.7	05.1	84	57	66	69	SSW 2	SE 2	SW 2	2
28	740.1	742.0	744.2	00.9	08.9	01.6	03.3	10.0	00.3	-	04.6	04.4	04.0	93	51	77	74	- 0	NNE 1	SE 2	2
29	744.7	743.8	744.6	00.2	03.8	02.6	02.3	03.8	00.0	-	04.7	05.5	04.8	130	91	87	93	- 0	- 0	NNE 2	2
30	742.8	741.3	740.3	02.6	05.2	05.2	04.6	06.4	02.0	-	05.1	05.5	06.1	92	83	91	89	S 1	- 0	W 1	1
MES. VRED.	740.4	739.2	740.0	05.6	13.9	08.3	09.1	14.9	03.8	-	06.1	07.1	06.3	87	61	77	75	0.9	1.2	1.2	1.2

## SKOPJE-PETROVAC

1	741.9	736.7	736.7	05.2	09.4	08.2	07.8	10.2	04.8	-	06.1	07.6	07.8	91	85	96	91	SE 1	NNW 1	- 0	0
2	734.5	732.5	735.6	08.0	09.4	00.8	04.8	09.7	00.5	-	07.6	08.0	04.7	95	90	97	94	- 0	- 0	N 4	4
3	738.3	740.4	744.0	00.2	00.0	00.6	00.5	01.3	-00.2	-	03.9	03.8	04.0	84	82	83	83	W 2	WNW 2	WSW 1	1
4	746.6	746.4	747.4	00.4	01.5	-02.8	-00.9	02.1	-03.0	-	04.4	03.9	02.9	93	77	78	82	NNE 3	NNE 4	NNE 5	5
5	747.1	745.4	744.4	-02.0	02.0	-03.6	-01.8	02.5	-05.1	-	02.7	03.1	02.8	68	58	80	65	WSW 2	NNE 2	ENE 2	2
6	743.8	742.1	742.2	-09.2	01.0	-03.0	-03.6	01.8	-09.7	-	02.0	03.1	03.3	86	63	85	79	- 0	- 0	S 1	1
7	739.3	739.4	740.8	-00.8	03.0	02.2	01.7	03.6	-03.7	-	04.2	04.8	04.7	96	84	87	89	- 0	WNW 1	NE 1	1
8	743.6	743.6	744.3	01.8	08.6	-00.4	02.4	09.0	-00.8	-	04.7	04.7	04.3	90	57	96	81	- 0	WSW 1	- 0	0
9	743.9	742.2	741.5	00.0	02.8	03.4	02.4	04.3	-02.6	-	04.4	05.2	05.8	96	94	98	96	- 0	S 1	- 0	0
10	739.8	740.0	742.6	04.4	07.2	07.2	06.5	08.4	-02.6	-	06.2	06.3	07.0	98	83	92	91	- 0	- 0	0	0
11	748.5	750.9	753.0	01.8	02.8	01.4	01.9	02.9	01.0	-	05.0	05.2	04.7	97	92	93	94	NE 3	NNE 2	NE 2	2
12	754.0	753.9	754.5	01.2	04.0	-01.9	00.4	04.8	-02.1	-	03.3	03.3	03.4	66	53	86	68	E 1	N 2	NNE 3	3
13	753.9	752.1	751.5	-06.6	00.8	-03.4	-03.2	02.0	-09.2	-	02.2	02.9	03.0	80	59	83	74	- 0	NW 1	NE 2	2
14	752.2	751.7	751.8	-06.4	03.4	-03.3	-02.4	03.4	-07.6	-	02.3	03.8	02.3	80	65	63	69	- 0	- 0	NNE 4	4
15	750.6	748.4	747.4	-06.2	-00.4	00.2	-01.6	00.4	-07.8	-	02.5	04.1	03.9	85	93	83	87	NNE 1	WNW 1	N 1	1
16	751.8	751.5	751.3	-05.7	01.0	-01.2	-01.8	02.6	-06.4	-	02.5	03.3	03.4	82	66	81	77	- 0	NNE 4	NÉ 4	3
17	750.8	750.1	752.1	-00.4	02.6	-01.6	-00.3	03.0	-02.6	-	03.7	03.1	03.8	82	56	80	73	N 2	N 5	NW 1	1
18	751.6	749.6	749.7	-06.6	01.8	-04.4	-03.4	01.8	-07.2	-	02.5	02.6	02.5	89	46	75	70	NNE 2	WNW 2	N 3	3
19	749.7	749.0	749.7	-03.4	-00.6	-04.0	-03.0	-00.4	-05.6	-	02.9	02.9	02.9	81	67	84	77	N 1	WSW 1	E 1	1
20	749.4	748.2	748.8	-07.0	00.4	-03.8	-03.6	01.2	-08.4	-	02.1	04.2	02.4	79	90	70	80	- 0	- 0	NE 3	3
21	750.2	749.2	749.8	-07.4	-01.4	-05.3	-04.9	-00.5	-09.4	-	02.2	03.0	02.7	83	81	86	83	NE 1	WN 1	NNE 3	3
22	751.8	752.6	754.9	-04.8	-01.1	-06.2	-04.6	-00.6	-07.6	-	02.8	02.9	02.5	87	69	85	80	- 0	WNW 1	SE 1	1
23	754.2	753.6	754.1	-04.8	-03.4	-04.6	-04.4	-03.3	-07.1	-	02.8	03.2									

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 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$ 

Dan	Vrijnost 0-9	Oblačnost N (0-10)					Insekcija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	6	10	06	0	10	08.7	-	.	.	= 0-18 <sup>10</sup> , ● 22 <sup>05-24</sup>
2	7	10*	10	10	10	10.0	-	02.0	.	● 0-030, 23 <sup>5</sup> , 7 <sup>10</sup> ; 10 <sup>05</sup> , 11 <sup>10</sup> ; = 0-142, 11 <sup>40</sup>
3	7	09	07	0	00	05.3	-	.	.	= 0-045, 5 <sup>10</sup> , □ 20 <sup>30-24</sup>
4	6	05	03	0	00	02.7	-	.	.	= 0-10 <sup>10</sup> , = 0-1340, 5 <sup>10</sup> , 10 <sup>15</sup> , 11 <sup>15</sup> , 16 <sup>30-24</sup> ; = 0-450, 7 <sup>20</sup> , 10 <sup>05</sup> , 10 <sup>15</sup> ; = 0-720, 10 <sup>05</sup>
5	6	05	07	0	10	07.3	-	.	.	= 0-14 <sup>10</sup> , □ 6-9 <sup>20</sup>
6	6	00	00	0	02	00.7	-	.	.	□ 4 <sup>20-24</sup> , = 0-5 <sup>10-24</sup>
7	6	08	07	0	05	06.7	-	.	.	= 0-13 <sup>10</sup> , 20 <sup>35-24</sup> ; □ 3-8 <sup>30</sup>
8	6	08	06	0	00	04.7	-	.	.	= 0-24, □ 2 <sup>10-8<sup>15</sup></sup>
9	5	06	05	0	00	02.7	-	.	.	= 0-17 <sup>10</sup> , □ 4-8 <sup>15</sup>
10	6	10	10	10	10	10.0	-	.	.	□ 1 <sup>20-8<sup>10</sup></sup> , = 0-340-24 <sup>10</sup> , = 0-54 <sup>10-740</sup>
11	7	09	02	0	00	03.7	-	.	.	= 0-6 <sup>20</sup>
12	7	00	00	0	00	00.0	-	.	.	= 0-6 <sup>10-10</sup>
13	7	03	06	0	00	03.0	-	.	.	= 0-5 <sup>2-12<sup>20</sup></sup>
14	6	07	10	07	08	08.0	-	.	.	= 0-6 <sup>24</sup> , ● 16 <sup>45-8<sup>10</sup></sup>
15	7	10	03	0	02	05.0	-	00.2	.	= 0-11 <sup>10</sup>
16	8	09	04	0	09	07.3	-	.	.	■ 5 <sup>10-12<sup>20</sup></sup> , 10 <sup>50</sup> , ○ 20 <sup>30-20<sup>45</sup></sup>
17	8	05	04	0	08	05.7	-	00.6	.	■ 5 <sup>10-6<sup>20</sup></sup> , □ 11 <sup>25-13<sup>20</sup></sup>
18	8	07	06	0	03	05.3	-	.	.	■ 5 <sup>10-11<sup>20</sup></sup> , 10 <sup>50</sup> , 13 <sup>20</sup>
19	7	10	10	10	10	10.0	-	.	.	○ 7 <sup>20-9<sup>20</sup></sup> , 20 <sup>35-24</sup>
20	3	10*	10*	10	10	10.0	-	03.4	.	○ 0-8 <sup>10</sup> , X <sup>10-11<sup>10</sup></sup> , X <sup>11-12<sup>10</sup></sup> , = 16 <sup>25-23<sup>30</sup></sup> , = 18 <sup>20-20<sup>15</sup></sup> , 23 <sup>30-24</sup> ; □
21	6	10	04	0	09	07.7	-	16.8	04	= 0-16 <sup>10</sup> , = 0-18 <sup>15-8<sup>10</sup></sup> , □
22	6	05	09	10	*	06.0	-	.	01	○ 0-02 <sup>10</sup> , = 0-6 <sup>24</sup> , ○ 0-13 <sup>2-24</sup> , □
23	5	10	10	10	10	10.0	-	04.2	.	○ 0-12 <sup>10</sup> , = 0-13 <sup>2-24</sup> , = 0-19 <sup>10</sup> , ■ 19 <sup>2-21<sup>35</sup></sup>
24	7	09	02	0	09	06.7	-	11.5	.	○ 0-5 <sup>10</sup>
25	5	10	10	10	10	10.0	-	.	.	= 0-11 <sup>2-24</sup>
26	7	10	10	10	05	08.3	-	00.0	.	= 0-5 <sup>20</sup> , 13 <sup>20-16<sup>15</sup></sup> , ● 5 <sup>15-10<sup>10</sup></sup> , 13 <sup>52-13<sup>10</sup></sup>
27	7	09	08	05	05	07.3	-	09.5	.	.
28	7	02	01	0	04	02.3	-	.	.	■ 5 <sup>20-9<sup>15</sup></sup> , X <sup>10-24<sup>10</sup></sup> , = 24 <sup>20-33<sup>10</sup></sup> , = 6 <sup>40-8<sup>35</sup></sup> , = 8 <sup>35-19<sup>10</sup></sup>
29	6	10*	10	10	10	10.0	-	01.2	.	.
30	6	10	10	10	10	10.0	-	00.0	.	= 0-26-17 <sup>10</sup> , 19 <sup>22-24</sup>
MES. RED.		07.5	06.3	05.9	06.6	-	49.4			

1	5	10	10	10	10	10.0	-	.	.	= 0-24, ● 17 <sup>2-10<sup>15</sup></sup>
2	7	10	10	10	*	10.0	-	02.9	.	= 0-15 <sup>10</sup> , 0, 23 <sup>5-24</sup> ; ○ 0-7 <sup>25-10<sup>5</sup></sup> , 17 <sup>20-19<sup>10</sup></sup> ; X <sup>9-19<sup>2-23<sup>15</sup></sup></sup>
3	6	10	10*	10	10	10.0	-	05.1	.	= 0-4 <sup>10</sup> , X <sup>9-12<sup>20</sup></sup> , 9 <sup>2-16<sup>10</sup></sup> , □
4	7	10	09	02	0	07.0	-	00.3	.	■ 19 <sup>2-24</sup>
5	7	10	04	00	0	04.7	-	.	.	= 0-20 <sup>10-24</sup>
6	7	00	00	0	04	01.3	-	.	.	■ 0-0-11 <sup>20</sup>
7	5	10	10	10	10	10.0	-	.	.	= 0-15 <sup>10</sup> , X <sup>9-11<sup>10</sup></sup>
8	5	10	02	0	00	04.0	-	00.0	.	= 0-0-24
9	4	10	10	10	10	10.0	-	.	.	= 0-11 <sup>10</sup> , = 0-12 <sup>14</sup> , ● 7 <sup>2-12<sup>10</sup></sup> , 10 <sup>25-10<sup>10</sup></sup> , 22 <sup>10-23<sup>10</sup></sup> ; ○ 0-10 <sup>22-22<sup>10</sup></sup>
10	5	10	*	10	10*	10.0	-	02.3	.	= 0-6 <sup>10</sup> , = 0-6 <sup>12</sup> , 9 <sup>30</sup> , = 19 <sup>2-18<sup>20</sup></sup> , ○ 18 <sup>2-24</sup>
11	6	10*	10*	10*	10*	10.0	-	01.0	.	● 0-24, 13 <sup>10-15<sup>10</sup></sup> , 19 <sup>2-20<sup>25</sup></sup> ; X <sup>9-13<sup>15</sup></sup> , 20 <sup>25-22<sup>10</sup></sup>
12	7	10*	04	0	00	04.7	-	01.4	.	X <sup>9-6<sup>35</sup></sup>
13	6	06	00	00	00	00.0	-	.	.	= 0-15 <sup>11</sup> , = 1-14 <sup>10</sup> , 16 <sup>30</sup>
14	7	00	00	0	00	00.0	-	.	.	■ 19 <sup>2-11<sup>10</sup></sup> , = 1-14 <sup>10</sup> , 12 <sup>10</sup>
15	6	10	10*	10*	10*	10.0	-	.	.	= 0-11 <sup>15</sup> , = 6 <sup>12-24</sup> , X <sup>11-14<sup>10</sup></sup> , 15 <sup>15-24</sup>
16	6	02	07	06	0	05.0	-	00.6	.	= 0-2-10 <sup>10</sup> , 6 <sup>15-17<sup>10</sup></sup> ; X <sup>9-21<sup>25-23<sup>15</sup></sup></sup>
17	7	10*	04	0	02	05.3	-	00.0	.	X <sup>9-2-24</sup> , = 0-9 <sup>25-11<sup>10</sup></sup>
18	7	00	02	0	02	01.3	-	.	.	= 0-2-24, = 0-5 <sup>15-14<sup>10</sup></sup>
19	6	09	09	00	00	06.0	-	.	.	= 0-16 <sup>11<sup>10</sup></sup> , = 0-13 <sup>12-24</sup>
20	5	04	00	0	00	01.3	-	.	.	= 0-0-12 <sup>10</sup> , = 0-5 <sup>12-16<sup>10</sup></sup>
21	6	00	00	0	00	00.0	-	.	.	■ 0-0-12 <sup>10</sup> , = 0-14 <sup>2-24</sup>
22	5	10	00	0	03	04.3	-	.	.	= 0-1-17 <sup>25-20<sup>35-24</sup>, = 0-20-24</sup>
23	5	10	10	10	10	10.0	-	.	.	= 0-0-24, = 0-14 <sup>10</sup>
24	5	10	02	0	00	04.0	-	.	.	= 0-0-24, X <sup>10-22-11<sup>15</sup></sup>
25	4	10	10*	10*	10*	10.0	-	00.0	.	= 0-0-24, = 0-12-10 <sup>25</sup> , X <sup>13-15-15<sup>15</sup></sup> , X <sup>17-25-20<sup>20</sup></sup>
26	6	09	09	10	06	06.3	-	02.2	01	= 2-0-23 <sup>5-6<sup>10</sup></sup> , 13 <sup>20</sup> , = 0-0-23 <sup>5-6<sup>10</sup></sup> , □
27	7	05	01	0	00	02.0	-	.	.	= 0-0-24, 13 <sup>15</sup>
28	6	03	09	06	06.0	-	.	.	= 1-0-24, 11 <sup>20</sup>	
29	4	10	10	10	06	06.7	-	.	.	= 0-0-24
30	4	07	10*	10*	10	09.0	-	.	.	= 0-0-24, 10 <sup>25-5-16<sup>20</sup></sup> , 11 <sup>10-2-10<sup>20</sup></sup> , = 0-10 <sup>2-10<sup>20</sup></sup> , = 0-10 <sup>2-10<sup>20</sup></sup>
31	7	10	*	10	00	06.7	-	02.4	.	= 0-0-24, 0-0-24, 10 <sup>25-10<sup>15</sup></sup> , = 0-0-24, 10 <sup>25-10<sup>15</sup></sup> , = 0-0-24, 10 <sup>25-10<sup>15</sup></sup> , = 0-0-24, 10 <sup>25-10<sup>15</sup></sup>
MES. RED.		07.4	06.2	04.9	06.1	-	18.2			

**B) Mesečni i godišnji  
pregled**

Meseč	Vrednost pritisaka Pa mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina vетра mD, fm (0-12)																			
		Tm				Max				Dat.				N		NE		E		SE		S		SW		W		NW	
		7	14	21	Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.		
<b>SR SLOVENIJA</b>																													
$\varphi = 46^{\circ}20' N \lambda = 13^{\circ}33' E$ Gr. AG = + 54 min.																													
I	-	-0.3	02.8	00.7	01.0	04.0	-01.4	09.1	30 -09.4	19	03	01.7	24	01.3	05	01.0	14	01.0	02	01.0	08	02.1	02	03.0	02	01.5	33		
II	-	01.5	06.4	02.6	03.3	07.3	-00.1	12.1	23 -06.1	03	05	01.0	27	01.4	06	01.0	05	01.0	05	01.0	12	01.6	06	01.5	09	01.2	08		
III	-	03.6	11.8	06.4	07.6	12.9	02.4	23.4	25 -05.5	01	05	01.0	22	02.0	09	01.8	08	01.6	04	01.0	13	01.9	08	01.8	12	01.2	12		
IV	-	04.6	12.3	07.6	08.1	13.6	03.0	22.1	30 -02.2	04	05	01.3	23	02.5	12	02.4	03	01.7	01	02.0	14	01.7	15	02.0	08	01.6	08		
V	-	10.2	17.5	11.6	12.6	18.6	07.5	24.1	25	03.0	28	07	01.3	10	02.2	03	01.0	01	01.0	16	02.4	20	02.0	08	01.8	15			
VI	-	13.6	21.5	15.3	16.4	22.5	10.8	29.0	13	03.8	02	04	01.3	12	02.1	07	01.4	06	02.0	09	01.0	18	02.1	08	02.3	25			
VII	-	15.4	22.0	17.1	17.9	23.9	13.2	28.0	15	09.0	23	01	02.0	16	02.0	03	01.3	05	01.2	11	01.5	11	02.2	03	02.3	34			
VIII	-	13.8	21.9	15.6	16.8	22.9	12.0	26.8	06	07.5	01	01.3	13	01.2	12	02.8	06	01.5	04	01.8	06	01.3	11	01.9	05	01.6	31		
IX	-	09.1	19.1	11.9	13.0	20.1	07.8	27.1	07	-00.1	19	01	01.0	15	02.3	10	02.1	03	01.0	10	01.7	13	02.4	03	01.7	32			
X	-	07.8	16.2	10.0	11.0	16.8	06.7	21.4	09	01.8	03	04	01.0	13	01.8	01	01.0	06	01.0	11	01.5	07	01.9	01	01.0	49			
XI	-	03.6	08.8	04.6	05.4	09.6	01.9	16.1	11	-05.6	20	03	01.0	15	02.0	12	02.3	05	01.0	05	01.0	10	01.5	02	02.0	02			
XII	-	-01.7	03.6	00.1	00.5	04.5	-02.9	11.7	25 -06.8	23	01	05.0	16	02.9	02	01.0	04	01.0	•	•	04	01.3	•	•	02	01.0	64		
GOD.	-	06.8	13.7	08.6	09.4	14.7	05.1	29.0	45.VI -05.4	49.1	46	01.3	206	01.9	101	01.6	58	01.3	37	01.1	120	01.8	113	02.0	63	01.6	351		
<b>BOVEC</b>																													
$\varphi = 46^{\circ}01' N \lambda = 13^{\circ}33' E$ Gr. AG = + 54 min.																													
<b>VEDRIJAN</b>																													
$\varphi = 46^{\circ}01' N \lambda = 13^{\circ}33' E$ Gr. AG = + 54 min.																													
I	-	04.1	06.3	04.4	04.8	07.2	02.2	13.0	24 -02.0	20	01	01.0	30	01.8	34	01.9	06	02.6	05	01.6	01	01.0	2	0	03	01.0	11		
II	-	05.3	08.7	05.9	06.5	09.5	03.6	13.8	22 -01.5	03	01	01.0	19	02.1	25	01.6	09	02.1	12	01.3	02	01.0	03	01.0	01	02.0	12		
III	-	07.8	13.2	09.2	09.9	14.0	06.1	24.0	25 -01.0	31	01	01.0	22	02.5	21	01.2	13	01.4	10	01.2	06	01.0	02	01.0	09				
IV	-	08.2	13.6	09.5	10.2	14.5	07.2	22.5	29	01.0	17	03	01.7	20	01.6	35	01.8	03	01.7	07	01.4	06	01.7	09	01.4	04	01.0	03	
V	-	13.8	19.2	14.5	15.5	20.0	11.0	25.5	19	06.5	07	01	01.0	17	02.4	37	02.1	15	01.8	04	02.0	09	01.7	04	01.3	03	01.3	03	
VI	-	16.6	22.9	17.9	18.9	23.9	14.4	30.5	13	16.0	01	01	01	18	04.8	42	01.5	09	01.4	08	02.0	06	01.3	04	01.0	03	01.0	06	
VII	-	18.5	23.8	19.8	20.5	25.2	16.4	28.5	03	13.0	27	04	01.0	18	02.3	36	01.8	08	02.1	05	01.2	05	01.0	01	01.0	08			
VIII	-	17.8	23.8	19.1	20.0	24.0	16.3	30.0	06	13.0	20	02	01.0	16	02.5	50	01.7	•	•	13	02.1	04	01.3	04	01.0	03	01.0	01	
IX	-	13.3	20.5	15.1	16.0	21.5	12.4	28.0	07	06.6	19	02	01.0	20	02.5	48	02.0	04	01.5	04	01.3	02	01.0	02	01.0	02	01.0	02	
X	-	12.4	17.5	13.4	14.3	18.4	11.3	24.5	25	-07.0	03	02	01.0	21	02.1	24	02.0	18	02.1	04	01.3	03	01.2	09	01.1	01	01.0	07	
XI	-	04.9	10.5	07.5	08.1	11.4	08.1	17.0	06	01.0	20	02	02.0	16	02.4	37	01.9	07	01.3	08	01.3	06	01.0	03	01.0	02	01.5	09	
XII	-	03.5	07.4	04.1	04.6	08.2	02.4	12.8	06	19 -03.0	23	01	05.0	31	02.9	38	02.0	09	01.4	10	01.1	•	•	01	01.0	•	•	03	
GOD.	-	10.7	15.6	11.7	12.5	16.5	09.0	30.5	42.VI -03.0	23.VII	20	01.4	244	02.3	427	01.8	95	01.6	98	01.5	56	01.3	52	01.1	25	01.1	74		
<b>RATECE-PLANICA</b>																													
$\varphi = 46^{\circ}10' N \lambda = 13^{\circ}43' E$ Gr. AG = + 54 min.																													
I	-	-04.5	00.5	-03.2	-02.7	01.2	-06.3	06.4	24 -17.7	18	•	•	•	•	06	01.3	09	01.2	•	•	03	01.0	05	01.0	01	01+0	69		
II	-	683.7	-02.6	04.7	-01.2	-00.1	05.4	-04.0	05.8	23 -12.4	04	•	•	01	02.0	04	05	01.8	•	•	05	01.3	07	01.4	01	03.0	57		
III	-	689.4	-00.3	0.9	0.7	01.6	02.0	03.0	10.6	-01.8	19.2	25	-12.1	01	02.0	07	02.0	01	01.0	07	01+3	13	01.8	•	•	57			
IV	-	685.4	-00.6	0.9	0.4	04.2	04.2	06.4	20.4	27 -07.4	17	01	01.0	04	01.3	05	01.8	05	02.4	17	01+4	04	01.2	02	01.5	60			
V	-	687.6	07.0	14.5	08.7	08.8	09.0	03.7	21.8	25 -01.7	19	•	•	06	02.0	09	01.9	08	02.0	•	•	08	01.7	08	01.7	03	02.3	53	
VI	-	687.1	16.9	19.7	12.7	14.0	20.9	07.2	28.8	13 -06.9	02	01	03.0	08	01.6	02.1	03	02.0	03	02.0	•	•	04	01.6	11	01.3	02	02.0	53
VII	-	687.2	12.2	19.8	14.2	15.1	21.3	09.1	27.4	03	03.8	02	•	•	05	01.8	12	01.9	05	02.4	01	02.0	04	01.5	09	01.3	02	01.5	57
VIII	-	687.3	10.9	19.1	12.7	13.0	20.1	08.6	24.0	04	03.1	07	01.7	05	01.6	01	01.7	05	01.6	06	01.5	08	01.5	02	01.0	01	01.0	67	
IX	-	691.3	06.0	15.8	06.3	09.6																							



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Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C							Čestina pravaca i srednja jačina veta nd, Fm (0-12)																		
		Tm			Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C							
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\gamma = 46^{\circ}23' N \lambda = 13^{\circ}51' E$ Gr. $\Delta G = +55$ min.												KREDARICA															
I	555.9	-07.5	-06.9	-07.6	-07.4	-05.1	-05.6	03.2	26 -14.8	17	12	05.7	03	04.0	02	06.5	22	04.9	09	06.7	.	.					
II	555.3	-07.6	-06.2	-07.1	-07.0	-04.2	-05.3	01.8	05 -19.1	28	*	*	*	*	01	04.0	23	03.7	03	04.7	.	.					
III	561.5	-03.2	-02.0	-03.1	-02.8	-06.1	-05.4	07.3	17 -15.4	01	04	05.5	03	03.0	03	03.7	28	04.2	06	04.5	.	.					
IV	567.5	-06.3	-03.1	-04.5	-04.5	-01.6	-07.8	07.6	27 -16.4	11	17	04.8	01	02.0	01	05.0	26	04.3	01	04.0	*	*					
V	561.6	-00.4	01.0	-00.6	-00.2	02.4	-02.6	10.0	18 -08.4	28	05	04.6	*	*	*	45	04.0	01	02.0	*	*	02	03.0	24	03.0	16	
VI	562.8	02.6	04.2	02.8	03.1	05.7	03.9	15.2	15 -05.5	01	07	04.3	03	03.3	04	02.8	24	03.0	01	04.0	*	*					
VII	563.8	04.7	06.4	02.1	05.3	06.1	02.7	13.8	03 -02.4	26	06	03.8	01	03.0	05	02.8	21	03.3	*	*	02	02.0	04	03.3	42		
VIII	563.7	04.1	05.9	04.6	04.8	07.2	02.7	12.3	29 -06.5	24	02	03.0	*	*	02	03.0	36	03.6	02	03.0	*	*	01	07.0	30	03.6	18
IX	565.4	00.6	02.8	00.9	01.3	04.5	-01.4	13.0	12 -04.3	19	03	02.7	01	02.0	*	*	15	03.1	01	04.0	*	*	43	04.3	26		
X	565.4	02.6	04.1	02.0	02.7	05.7	00.6	12.8	22 -07.2	03	06	04.3	03	03.3	01	05.0	21	03.3	*	*	02	04.5	32	04.2	28		
XI	556.9	-05.4	-04.7	-05.4	-05.2	-02.5	-06.0	11.8	11 -15.3	27	07	04.9	03	06.3	03	03.7	17	04.2	02	04.1	*	*	05	04.6	43	05.4	12
XII	560.3	-05.9	-04.7	-05.7	-05.5	-02.5	-08.1	05.6	24 -17.6	03	07	05.9	02	03.0	03	03.7	21	03.9	*	*	*	*	06	03.7	42	05.7	12
GDD	560.8	-01.7	-00.3	-01.6	-01.3	01.5	-03.8	13.8	03.VII -19.1	28.II	76	04.8	20	03.9	25	03.7	301	03.8	26	05.0	03	02.7	32	03.9	446	04.5	166
$\gamma = 46^{\circ}01' N \lambda = 13^{\circ}55' E$ Gr. $\Delta G = +56$ min.												VGJSKC															
I	-	-00.4	00.3	-00.6	-00.3	01.8	-03.5	07.3	25 -10.5	19	*	*	*	*	26	01.2	*	*	*	35	01.6	01	01.0	03	03.5	28	
II	-	00.3	02.5	00.4	00.9	03.6	-02.6	07.9	24 -05.5	02	*	*	*	*	12	01.1	*	*	*	26	02.2	03	01.0	04	02.6	39	
III	-	03.3	07.2	03.8	04.5	08.5	00.9	18.0	25 -08.0	01	01	01.0	*	*	13	01.9	*	*	*	25	01.7	01	02.0	13	01.9	40	
IV	-	03.3	06.9	03.4	04.3	07.9	00.2	17.3	29 -06.1	12	01	01.0	02	03.0	18	01.3	*	*	*	17	01.4	06	01.8	09	01.9	37	
V	-	09.2	12.1	08.1	09.4	13.1	05.8	19.7	25 01.0	28	*	*	*	*	31	01.5	03	01.0	01	01.0	19	01.9	03	02.0	04	01.5	32
VI	-	12.9	16.5	11.6	13.2	17.1	05.4	24.9	13 02.0	02	02	01.0	04	03.0	10	01.2	01	01.0	*	22	01.1	02	01.0	07	01.9	42	
VII	-	14.0	17.3	13.4	14.5	18.5	10.7	23.9	11 05.7	26	*	*	07	02.0	10	01.6	*	*	*	12	01.6	01	01.0	13	01.6	50	
VIII	-	13.2	16.4	12.6	13.7	17.3	10.0	21.3	06 07.0	24	*	*	01	02.0	10	01.2	*	*	*	15	02.0	*	*	*	10	01.5	51
IX	-	08.2	12.4	08.2	09.3	13.7	06.0	21.7	08 -01.3	18	03	02.0	11	02.5	30	01.9	*	*	*	6	01.2	*	*	*	02	01.5	38
X	-	07.5	10.8	07.1	08.5	11.9	02.1	14.1	27 -04.5	03	*	*	*	*	28	01.6	*	*	*	20	01.5	*	*	*	15	02.3	30
XI	-	02.4	04.5	02.3	02.9	05.7	-03.3	17.2	11 -07.3	29	01	01.0	*	*	28	01.8	*	*	*	27	01.7	02	01.0	06	02.7	26	
XII	-	-02.7	-01.1	-01.3	-02.1	00.1	-04.4	03.5	25 -10.3	13	02	03.5	05	03.0	30	01.7	*	*	*	17	01.2	*	*	*	04	01.8	35
GDD	-	05.9	06.8	05.7	06.6	09.9	03.2	24.9	4.VI -10.5	49.1	10	01.8	30	02.6	252	01.5	04	01.0	01	01.0	241	01.7	19	01.5	90	02.0	448
$\gamma = 46^{\circ}21' N \lambda = 14^{\circ}11' E$ Gr. $\Delta G = +57$ min.												RADCVLJICA															
I	-	-01.7	02.4	-00.3	00.6	03.1	-02.3	08.7	30 -11.2	19	17	01.1	09	01.1	*	*	05	01.9	04	01.0	03	01.0	*	15	01.3	36	
II	-	00.2	06.3	02.7	03.0	07.4	-	12.5	23	-	20	01.8	08	01.8	*	*	12	01.4	06	01.7	05	01.0	*	05	01.8	28	
III	-	02.2	12.4	06.8	07.0	13.6	-	22.7	25	-	17	01.2	09	01.4	*	*	13	01.5	09	01.4	02	02.0	*	09	02.7	34	
IV	-	03.5	12.0	07.9	07.8	13.5	-	22.9	30	-	17	01.6	11	02.4	*	*	12	01.5	09	01.2	02	02.0	*	08	03.4	31	
V	-	05.7	17.4	12.2	12.5	18.4	04.9	24.4	04 04.2	28	10	01.1	07	01.9	*	*	11	02.3	09	01.4	08	02.5	*	*	09	02.4	37
VI	-	13.7	21.5	15.8	16.7	22.8	10.5	25.7	13 02.2	02	12	01.5	6.8	02.0	*	*	14	02.6	02	01.0	03.0	02.0	*	07	02.4	44	
VII	-	14.8	21.5	16.9	17.5	23.5	12.6	29.4	12 09.0	02	10	01.2	07	01.9	*	*	18	02.3	05	01.4	08	01.4	*	*	05	01.6	40
VIII	-	13.8	20.6	15.3	16.6	22.1	12.3	27.1	06 07.0	25	09	01.2	08	01.8	*	*	11	02.3	06	01.3	06	01.3	*	*	11	02.5	42
IX	-	06.5	17.0	11.2	12.0	18.6	07.6	24.8	07 -00.5	29	08	01.1	09	02.1	*	*	12	02.0	06	01.7	06	01.7	*	*	04	01.8	45
X	-	06.6	15.6	09.4	10.3	16.4	-05.7	20.1	09 00.6	04	13	01.1	10	02.6	*	*	12	02.4	11	02.4	05	01.0	*	*	04	01.7	28
XI	-	01.8	08.3	04.3	04.4	09.7	00.4	20.3	11 -06.6	26	22	02.1	05	01.6	*	*	15	02.5	06	01.2	11	01.5	*	*	09	02.4	22
XII	-	-02.9	01.3	-01.0	-00.9	02.4	-03.3	10.4	25 -08.2	06	18	01.7	07	02.6	*	*	14	01.6	06	01.0	07	01.4	*	*	16	01.8	29
GDD	-	05.8	13.0	08.4	08.9	14.3	-	29.7	4.VI -	-	173	01.5	100	02.0	*	*	145	02.0	79	01.5	70	01.6	*	*	108	02.1	416
$\gamma = 46^{\circ}10' N \lambda = 14^{\circ}11' E$ Gr. $\Delta G = +57$ min.												JAVCRJE NAC PCLJANAMI															
I	-	00.6	02.1	01.1	01.2	03.9	-01.3	16.5	24 -04.5	19	07	01.4	19	02.1	07	01.3	04	02.3	03	03.0	27	02.8	08	02.0	09	02.0	05
II	-	01.9	06.6	03.6	04.1	07.6	00.6	18.3	23 -06.5	04	11	01.3	04	01.8	01	01.0	06	02.3	02	02.5	03	02.0	*	*	21	01.4	48
III	-	04.0	12.6	07.5	07.9	15.8	03.1	22.5	25 -06.5	01	30	01.2	03	01.0	*	*	01	01.0	*	*	*	*	*	*	17	01.5	50
IV	-	04.1	11.8	07.4	07.7	13.0	02.6	23.5	30 -02.0	01	23	01.2	12	01.6	01	03.0	01	02.0	01	01.0	02	02.0	01	03.0	12	01.4	38
V	-	10.1	17.2	12.5	13.1	18.4	07.8	25.0	12 02.5	26	10	01.1	08	01.8	02	01.5	02	02.0	05	01.6	07	01.7	07	01.9	41		
VI	-	13.6	21.2	16.5	16.9	22.6	11.2	29.5	13 03.0	02	14	01.1	05	02.0	03	02.3	09	01.4	08	01.8	02	02.0	05	01.6	43		
VII	-	14.5	21.3	17.5	17.7	22.9	12.9	26.5	03 08.5	27	14	01.1	05	02.0	03	02.3	09	01.4	08	01.8	04	02.0	05	01.5	43		
VIII	-	14.1	21.0	16.7	17.4	22.0	13.0	27.0	06 08.5	25	08	01.3	03	01.7	*	*	01	02.0	10	01.4	05	01.4	02	02.0	08	01.9	56
IX	-	09.2	16.6	11.8	12.4	17.5	08.2	26.0	08 01.0	29	13	01.1	04	02.0	01	02.0	*	*	*	*	*	*	*	*	05	01.6	66
X	-	06.3	15.4	11.2	11.5	16.5	07.4	20.5	09 01.5	03	13	01.4	02	01.0	*	*	*	*	*	*	*	*	*	20	01.5	57	
XI	-	03.2	08.4	04.6	05.																						

Mesec	Oblačnost Nm (0-10)			Inselacijs hruš sati	Vlažnost vazduha			Padavine R mm			Broj dana n s a:																													
	7	14	21		mm	7	14	21	Sred. (Dles.)	Min	mm	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	*	*	*	*	A	A	R	T	III	II										
					mm	7	14	21			mm	=	<	<	>	>	>	=	=	=	=	9	8	7	6	5	4	3	2	1	0									
<b>KREDARICA</b>																																								
<b>BR. ST. 6</b>																																								
I	7.1	6.5	6.1	6.7	083.5	02.1	83	83	85	84	25	241	042.4	12	13	29	31	.	.	.	23	12	04	13	19	18	10	•	19	.	.	02	21	31						
II	6.6	6.6	6.1	6.4	081.9	02.3	87	87	88	84	14	145	030.6	22	10	27	28	.	.	.	15	05	03	10	16	14	07	•	16	.	.	02	19	28						
III	6.3	6.6	4.6	5.8	159.5	02.4	66	67	68	67	20	141	043.2	30	04	12	29	.	.	.	22	10	05	10	12	11	05	01	12	.	01	.	02	14	31					
IV	6.8	6.2	5.6	5.6	139.3	02.5	73	75	78	76	13	156	037.6	09	13	18	28	.	.	.	23	07	04	13	16	13	05	04	15	.	01	.	02	16	30					
V	6.6	7.7	7.0	7.1	150.3	03.8	82	84	85	84	14	118	023.6	19	.	04	25	.	.	.	10	01	01	13	17	15	04	05	12	02	01	01	02	24	31					
VI	6.2	7.5	6.4	6.7	167.4	04.7	81	81	85	82	43	169	034.4	22	.	04	13	.	.	.	11	01	01	13	20	16	04	16	14	05	03	04	01	02	21	30				
VII	5.7	7.7	6.2	6.6	163.3	05.5	82	83	83	82	26	161	031.2	26	.	05	.	.	.	15	02	03	12	20	14	06	20	04	.	01	.	04	.	02	23	10				
VIII	6.5	8.0	6.0	6.9	122.0	05.2	80	80	82	81	41	312	051.8	22	.	04	.	.	.	14	03	05	12	19	19	12	18	06	02	01	03	.	07	25	.					
IX	6.2	7.7	6.2	6.3	139.2	04.2	82	84	88	81	17	083	025.0	14	.	06	17	.	.	.	16	02	05	13	11	05	03	05	07	.	.	03	19	14						
X	4.0	4.9	3.4	4.1	170.7	03.8	63	70	74	69	15	023	007.6	07	.	.	.	.	.	13	05	10	06	09	06	05	05	05	.	.	16	02	.							
XI	6.8	6.8	5.0	6.2	095.9	02.3	73	76	77	76	18	090	042.1	14	15	20	27	.	.	.	22	14	04	10	14	09	03	03	13	.	01	02	.	02	18	18				
XII	5.0	5.5	4.7	5.1	106.1	01.8	65	62	62	63	42	060	033.9	29	07	21	31	.	.	.	20	11	08	07	13	16	02	02	.	.	.	16	31	.						
GOD.	6.1	6.6	5.6	6.2	1579.1	03.4	76	77	79	77	12	1699	051.8	22.VII	62	142	248	.	.	.	156	75	50	132	186	154	61	81	136	09	08	04	18	01	37	236	256			
<b>VCJSKC</b>																																								
<b>BR. ST. 7</b>																																								
I	8.7	6.3	7.8	8.3	-	-	-	-	-	-	-	412	064.3	15	01	09	25	.	.	.	01	20	19	15	15	15	04	02	04	01	01	10	31							
II	7.8	7.2	6.6	7.3	-	-	-	-	-	-	-	415	117.3	22	.	04	22	.	.	.	09	17	15	08	12	09	03	.	01	.	02	11	28							
III	7.1	7.1	4.2	5.9	-	-	-	-	-	-	-	148	045.6	29	.	01	08	.	.	.	02	10	10	06	09	03	.	01	.	03	.	01	06	25						
IV	6.7	6.7	4.0	5.8	-	-	-	-	-	-	-	149	041.1	09	.	01	16	.	.	.	03	08	13	10	06	04	04	.	01	.	02	06	20							
V	6.5	7.4	6.2	6.7	-	-	-	-	-	-	-	164	062.7	14	.	.	.	.	.	.	04	11	16	13	06	16	.	.	.	01	.	07	08							
VI	6.1	6.2	5.5	5.9	-	-	-	-	-	-	-	114	049.8	22	.	.	.	.	.	.	02	18	16	12	03	14	.	.	.	.	08	01	.							
VII	5.7	7.0	5.7	6.1	-	-	-	-	-	-	-	322	067.0	26	.	.	.	.	.	.	03	11	19	18	11	19	.	.	.	02	01	12	05							
VIII	6.3	7.3	5.5	6.8	-	-	-	-	-	-	-	389	093.0	22	.	.	.	.	.	.	12	18	15	09	18	.	.	.	01	.	14	06								
IX	6.1	5.2	4.9	5.5	-	-	-	-	-	-	-	129	036.9	18	.	03	.	.	.	.	06	09	09	05	07	05	02	.	.	01	04	08	04							
X	7.3	6.6	4.3	6.8	-	-	-	-	-	-	-	036	012.3	30	.	01	18	.	.	.	02	13	10	05	01	01	01	.	.	01	.	12	02							
XI	7.8	7.2	5.8	6.8	-	-	-	-	-	-	-	205	081.6	22	.	04	18	.	.	.	05	14	12	10	04	08	06	.	04	.	01	16	11							
XII	6.5	5.5	5.5	6.0	-	-	-	-	-	-	-	146	050.2	28	01	14	29	.	.	.	06	12	07	04	05	04	02	.	.	.	02	.	01	14	31					
GOD.	6.9	6.8	5.7	6.5	-	-	-	-	-	-	-	2629	117.3	22.VII	02	33	122	.	.	.	34	133	166	143	77	143	51	09	11	04	10	02	52	97	140					
<b>RAEVVLJICA</b>																																								
<b>BR. ST. 8</b>																																								
I	7.0	7.2	7.7	7.8	-	-	-	-	-	-	-	04.2	83.9	93	89	87	56	255	043.3	15	.	03	19	.	.	02	02	02	17	20	18	11	14	11	02	.	02	01	13	25
II	7.4	7.0	6.4	6.9	-	-	-	-	-	-	-	04.7	85	72	85	81	40	176	051.8	22	.	01	10	.	.	06	02	01	15	14	13	07	11	03	.	.	01	.		
III	6.7	6.4	5.4	5.7	-	-	-	-	-	-	-	05.5	88	56	77	74	22	101	026.4	29	.	.	.	.	02	01	09	09	09	08	02	.	.	01	01	01				
IV	5.9	5.6	4.0	5.2	-	-	-	-	-	-	-	05.6	86	57	69	71	25	120	023.2	09	.	.	.	.	03	01	05	09	12	04	03	.	.	02	01	01				
V	5.7	6.2	6.4	6.1	-	-	-	-	-	-	-	08.6	88	62	81	77	39	388	046.5	14	.	.	.	.	03	02	02	11	14	11	01	.	.	.	01	.				
VI	5.6	5.7	4.6	5.3	-	-	-	-	-	-	-	10.5	82	76	88	85	43	106	018.0	22	.	.	.	.	04	01	06	14	10	03	14	.	.	05	.					
VII	5.6	6.0	5.9	6.1	-	-	-	-	-	-	-	11.7	82	65	77	74	36	249	084.8	26	.	.	.	.	03	02	04	10	18	14	08	.	.	06	.					
VIII	5.4	6.3	5.5	5.6	-	-	-	-	-	-	-	10.7	82	65	77	74	36	249	084.8	22	.	.	.	.	03	02	04	10	18	14	08	.	.	11	03					
IX	5.4	5.9	4.1	5.2	-	-	-	-	-	-	-	08.6	84	60	79	71	36	123	046.5	16	.	.	.	.	03	02	05	10	17	12	02	.	.	01	01					
X	5.8	6.0	5.5	5.8	-	-	-	-	-	-	-	07.6	86	67	82	75	41	137	016.5	11	.																			

Mesec	Vrsta/linijski pri istak Pm mm	Temperatura vаздуха °C								Cestina pravaca i srednja jačina vетра nD, Pm (0-12)																			
		Tm			Sred. (Dne)	Max	Min	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.							
$\gamma = 46^{\circ}13' N \lambda = 14^{\circ}29' E$ Gr. $\Delta G = + 58$ min.																													
I	726.2	-00.9	02.0	-00.5	00.0	02.9	-02.6	11.3	30	-10.9	19	07	01.1	09	01.6	06	01.2	01	01.0	06	01.2	10	01.3	19	01.6	*	35		
II	727.3	00.2	06.2	01.9	02.5	07.4	-01.4	14.3	23	-10.4	04	04	02.6	05	01.0	06	01.2	02	01.5	09	02.1	05	01.4	22	01.6	13	01.6	22	
III	732.4	00.3	12.7	03.9	05.2	14.2	-01.2	24.1	25	-08.9	01	02	02.5	03	01.3	08	01.6	05	02.1	05	04.6	03	01.7	19	04.5	18	01.3	27	
IV	736.2	03.2	12.1	05.7	06.7	13.7	00.2	24.3	17	06	02.3	03	01.3	16	01.4	10	02.3	04	01.4	10	01.5	10	01.3	31					
V	729.6	09.7	17.7	10.9	12.3	19.2	05.2	24.0	04	-01.6	04	02	02.0	*	0	10	01.5	07	01.9	06	02.2	05	02.0	16	01.6	09	01.3	37	
VI	728.6	13.6	22.1	15.2	16.6	23.1	08.8	31.2	13	-00.6	02	09	01.6	02	01.5	08	01.4	05	02.1	06	02.0	05	02.4	16	02.0	04	01.3	31	
VII	728.6	14.9	22.3	14.4	17.5	24.0	11.1	30.1	12	05.1	28	03	01.0	01	01.0	11	01.6	12	01.4	03	02.0	05	01.8	11	01.5	12	01.5	35	
VIII	726.7	13.7	21.9	15.4	16.6	23.3	11.2	27.1	06	05.2	25	05	01.8	05	01.4	12	01.8	08	01.7	05	01.0	07	02.0	16	01.3	11	01.4	26	
IX	734.1	07.7	17.7	09.9	11.3	19.0	05.6	26.4	07	-03.6	29	01	01.0	04	01.5	12	01.6	13	02.5	04	01.5	01	02.1	11	01.1	06	01.2	38	
X	734.3	05.4	15.5	09.2	16.5	15.3	03.9	21.8	08	-03.2	04	02	01.5	*	01	11	01.5	08	01.6	05	01.5	04	01.8	14	01.6	11	01.1	41	
XI	728.2	01.8	07.1	02.6	03.6	08.3	-00.6	19.6	11	-07.1	20	02	01.0	01	01.0	07	01.4	06	01.8	03	01.3	07	01.4	18	01.6	06	02.0	40	
XII	734.7	-03.0	01.0	-01.6	-01.3	01.6	-04.4	11.8	25	-13.1	06	01	02.0	06	01.0	11	01.2	06	01.8	06	01.3	02	01.5	14	01.5	06	01.7	41	
GOD.	730.3	05.6	13.2	07.3	08.4	14.5	03.0	31.2	43.VI	-12.1	06.VII	44	01.6	35	01.3	11.8	01.6	88	01.8	61	01.6	59	01.7	180	01.6	106	01.4	404	
$\gamma = 46^{\circ}24' N \lambda = 14^{\circ}30' E$ Gr. $\Delta G = + 58$ min.																													
I	-	-01.3	01.9	-00.8	-00.3	03.2	-03.6	10.2	25	-12.6	19	01	02.0	05	01.6	02	01.0	02	01.0	*	*	19	04.6	12	03.9	04	03.0	48	
II	-	00.0	05.0	05.5	01.5	05.8	-02.0	11.4	23	-10.2	04	*	*	07	01.7	03	02.7	01	03.0	*	*	16	03.8	10	03.6	10	03.5	37	
III	-	00.1	10.1	02.6	03.8	11.2	-00.8	19.8	25	-08.4	01	*	*	04	02.0	04	02.5	01	02.0	*	*	08	03.4	09	03.3	15	03.1	52	
IV	-	01.2	00.1	03.4	04.3	10.6	-00.5	19.7	30	-03.4	17	01	02.0	11	01.2	05	02.4	04	01.3	*	*	08	03.1	08	03.4	11	02.3	42	
V	-	07.5	14.6	09.1	10.1	16.0	04.3	22.3	04	-01.0	06	*	*	04	01.8	03	02.3	04	01.8	*	*	12	02.7	11	02.2	05	02.6	34	
VI	-	11.0	15.6	13.1	14.0	20.2	07.8	27.6	13	-01.1	02	01	02.0	07	01.9	05	02.3	02	02.4	*	*	07	03.0	00	02.6	05	03.0	34	
VII	-	12.3	18.3	14.9	20.9	19.4	09.4	26.2	12	04.6	28	*	*	05	01.8	02	03.5	03	03.0	*	*	14	02.6	09	02.2	13	02.8	47	
VIII	-	10.4	18.3	13.1	13.9	19.3	09.0	24.4	05	-03.4	25	*	*	04	02.5	01	03.0	04	02.5	*	*	19	02.6	04	01.8	05	02.2	56	
IX	-	05.9	14.8	07.6	09.0	16.0	04.5	24.4	07	-02.6	29	*	*	12	01.9	03	01.7	06	02.2	*	*	04	01.8	05	02.2	10	02.6	50	
X	-	04.6	13.9	06.8	08.0	14.9	03.4	19.6	25	-02.8	04	*	*	04	01.8	02	01.5	05	01.8	*	*	13	02.8	06	02.3	05	02.6	58	
XI	-	00.7	06.2	01.1	02.3	07.4	-01.4	19.1	11	-09.0	02	*	*	04	02.3	06	03.0	02	02.5	*	*	17	04.1	07	02.7	13	03.0	41	
XII	-	-03.9	01.2	-02.6	-02.1	02.5	-05.6	08.1	26	-15.0	05	*	*	09	02.4	03	02.7	04	02.3	*	*	04	02.8	03	03.7	11	03.2	59	
GOD.	-	04.1	11.1	05.6	06.6	12.4	02.6	27.6	43.VI	-15.0	05.VII	30	02.0	76	02.0	39	02.4	39	02.1	*	*	141	03.3	92	02.9	107	02.9	598	
$\gamma = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.																													
I	733.8	08.7	03.1	01.8	01.9	04.1	-00.3	11.4	30	-07.8	19	10	01.1	21	01.3	12	01.2	06	01.0	11	01.2	08	01.4	08	01.8	14	01.2	03	
II	731.7	02.3	06.4	04.4	04.5	08.1	02.2	14.9	23	-07.4	04	08	01.4	18	01.2	10	01.3	05	01.6	11	01.5	08	02.0	13	02.2	09	01.8	02	
III	736.6	02.3	12.5	08.7	08.6	14.7	02.4	24.6	25	-06.0	01	05	01.2	15	01.5	11	01.6	03	02.0	17	02.4	16	02.3	10	01.6	01			
IV	732.5	04.3	13.0	05.6	06.6	14.5	02.7	25.0	30	-03.3	17	01	02.0	16	01.3	22	01.4	06	01.5	10	01.9	20	02.3	11	02.2	04	01.3	.	
V	-	734.0	10.2	18.6	13.8	14.2	19.4	08.6	27.1	04	-02.0	29	01	01.0	14	01.4	20	01.2	10	01.7	12	01.5	16	02.2	13	02.1	06	01.7	01
VI	-	14.3	23.3	17.8	18.4	24.4	12.2	32.0	13	02.9	02	02	01.5	15	01.4	12	01.3	08	01.6	13	01.8	26	02.2	13	02.3	01	01.0	.	
VII	-	15.3	23.2	18.5	19.1	25.1	13.7	30.2	12	08.6	28	08	01.0	13	01.2	12	01.4	15	01.7	14	01.9	15	02.1	13	01.6	03	01.3	.	
VIII	-	14.0	23.0	17.7	18.2	23.8	13.3	28.1	06	05.2	02	05	01.2	19	01.3	15	01.4	05	01.7	13	01.3	14	01.9	15	01.6	03	01.3	.	
IX	-	738.2	09.2	18.6	12.4	13.1	19.8	08.2	27.5	06	-06.6	29	08	01.0	20	01.2	23	01.3	15	02.1	07	01.3	06	02.0	07	01.3	03	01.0	01
X	-	738.3	08.2	15.8	10.9	11.5	19.7	07.4	22.4	08	00.4	04	05	01.0	14	01.0	21	01.0	05	01.6	10	01.2	10	02.4	11	02.1	11	01.2	08
XI	-	732.4	03.9	07.7	04.8	03.3	08.9	02.4	16.6	11	-04.4	21	04	02.0	13	01.2	21	01.0	05	01.6	12	02.6	10	02.0	05	01.6	02	01.0	.
XII	-	738.8	-01.4	-00.2	-00.1	02.3	-02.2	08.8	23	-05.4	06	06	01.0	09	01.0	26	01.2	08	01.5	20	01.4	05	01.6	10	01.6	07	01.6	02	
GOD.	-	07.4	13.0	09.6	09.9	14.0	05.8	30.1	45.VI	-06.3	05.VII	30	01.6	24.0	02.0	56	02.0	92	02.2	91	02.1	197	02.5	187	03.2	106	02.4	96	
$\gamma = 46^{\circ}07' N \lambda = 14^{\circ}51' E$ Gr. $\Delta G = + 59$ min.																													
I	-	01.0	02.8	01.9	01.9	03.4	-00.2	10.5	24	-06.7	19	01	01.0	25	01.5	04	02.0	04	02.0	03	01.3	15	0						

Mesec	Oblačnost Nm (0-10)	Inzolacija broj sati Sred. (Dnev.)	Vlažnost vazduha % Sred. (Dnev.)	Padavine mm M Max Min Dat.	Broj dana n s s:																																
					Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	■	□																
	7	14	21	7	14	21	Speed. (Dnev.)	Min	6	8	2.0	8.0	0.1	1.0	10.0	•	△	*	Δ	○	▲	■	□														
<b>BR. ST. 11</b>																																					
<b>BRNIK-LETALISTE</b>																																					
I	9.4	8.3	7.5	6.5	0424.3	04.3	95	87	96	92	55	162	021.9	15	01	01	24	•	•	•	01	22	20	16	09	18	09	07	•	02	•	•	21	29			
II	8.0	7.9	6.6	5.7	0664.0	04.9	95	76	92	87	33	137	034.5	23	01	18	•	•	01	•	12	13	11	07	12	03	02	01	•	•	01	09	08				
III	6.3	6.5	4.0	5.7	1574.2	05.2	94	53	88	78	26	067	019.1	29	•	19	•	•	01	03	08	09	07	03	07	02	01	01	•	•	03	01	01				
IV	7.7	7.0	4.8	6.4	1594.4	05.5	92	55	80	75	22	131	050.3	09	•	14	•	•	03	02	10	14	10	03	14	05	05	•	•	•	03	06	01				
V	6.5	6.8	5.9	6.4	1904.8	06.1	89	54	85	76	31	051	012.1	14	•	•	03	01	•	02	02	09	09	02	15	•	•	•	•	08	04	•					
VI	5.0	5.8	4.9	5.3	2364.5	10.1	85	49	80	71	32	070	030.1	22	•	•	01	11	01	•	04	04	10	09	02	10	•	•	•	12	02	•					
VII	6.1	6.4	5.4	6.0	2174.1	11.8	91	59	89	79	32	205	059.3	26	•	•	13	01	•	02	03	08	17	13	05	17	•	•	•	01	15	05					
VIII	6.4	6.5	5.3	6.0	1694.1	11.7	95	61	92	82	36	223	059.9	22	•	•	08	01	•	01	05	08	15	07	15	•	•	•	•	14	04	•					
GOD.	7.1	6.6	5.8	6.6	16284.4	07.2	93	64	89	82	22	1339	059.9	22.VI	04	10	132	41	02	•	18	01	23	131	154	114	49	145	30	21	03	03	•	01	61	121	43
<b>JEZERSKO</b>																																					
BR. ST. 12																		H <sub>s</sub> = 894 m H <sub>b</sub> = - m h <sub>t</sub> = 1.9 m h <sub>r</sub> = 1.5 m																			
I	8.5	7.4	7.1	7.7	-	04.1	92	61	82	87	44	246	061.4	12	05	06	24	•	•	04	•	03	19	18	16	12	12	12	05	03	•	•	04	31			
II	7.3	6.7	5.9	6.6	-	04.4	90	70	80	82	37	269	067.1	22	01	01	19	•	•	01	•	03	11	14	12	08	12	07	04	•	•	•	01	13			
III	6.5	7.2	5.5	5.7	-	04.7	92	56	87	79	19	134	044.0	29	•	01	18	•	•	01	•	05	10	11	10	05	09	03	03	•	•	03					
IV	6.7	6.5	4.1	5.8	-	04.8	87	58	75	77	28	270	069.0	09	•	20	•	•	•	04	07	12	10	03	09	07	02	•	•	01	01	09					
V	6.4	6.7	5.3	6.2	-	07.2	89	60	85	78	36	125	038.1	14	•	•	01	•	•	06	12	16	10	04	16	•	•	•	02	•							
VI	5.1	6.8	5.4	5.7	-	09.0	88	55	83	75	39	098	027.2	22	•	•	01	05	•	•	04	06	10	12	03	12	•	•	04	•	•						
VII	6.1	6.8	6.1	6.3	-	10.0	89	62	86	79	38	204	022.1	26	•	•	03	•	•	04	10	17	14	04	17	•	•	•	05	01							
VIII	5.6	6.4	6.0	6.0	-	09.9	93	65	90	83	42	360	064.7	22	•	•	•	4	•	•	05	10	16	14	09	16	•	•	02	03	03						
GOD.	6.3	6.4	5.2	6.0	-	06.4	90	64	88	81	19	2059	087.1	22.VII	12	16	140	06	•	08	•	59	119	160	128	63	139	46	17	04	01	•	17	14	94		
<b>LJUBLJANA-BEZIGRAD</b>																							H <sub>s</sub> = 299 m H <sub>b</sub> = 297.6 m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.5 m														
BR. ST. 13																		H <sub>s</sub> = 299 m H <sub>b</sub> = 297.6 m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.5 m																			
I	9.6	8.3	8.0	8.6	0294.4	04.6	94	85	91	90	61	161	017.0	15	•	•	11	•	•	01	24	22	18	08	20	08	06	02	03	01	•	14	23				
II	9.0	7.3	6.7	7.7	0610.0	05.2	91	71	84	82	31	145	032.0	23	•	•	12	•	•	01	16	16	13	06	15	03	02	•	01	•	14	05					
III	6.7	6.5	5.3	5.7	1564.3	05.0	91	49	67	69	19	054	014.9	30	•	07	•	•	03	03	09	10	06	02	08	03	01	•	01	•	03	02					
IV	7.6	6.8	4.2	6.2	1624.0	05.6	87	50	67	68	21	147	052.1	09	•	07	01	•	01	02	08	15	10	05	15	04	03	03	01	•	03	02					
V	7.0	6.7	5.4	6.4	1864.4	08.0	67	48	71	69	26	060	012.0	15	•	•	03	•	•	02	11	14	11	02	14	•	•	•	04	07	•						
VI	5.0	5.2	4.6	5.0	2464.0	09.7	61	43	65	62	30	048	010.2	01	•	•	12	02	•	01	06	05	08	05	02	08	•	•	01	08	•						
VII	6.5	6.4	5.5	6.1	2134.1	11.7	87	54	65	72	31	144	027.3	16	•	•	16	02	•	03	04	08	17	13	07	17	•	•	•	12	04	•					
VIII	7.2	6.6	5.6	6.2	1634.8	11.8	91	57	61	76	33	192	053.2	22	•	•	11	•	•	01	01	01	10	17	12	04	17	•	•	14	09	•					
IX	8.0	5.5	4.4	6.0	1707.0	07.6	87	54	62	83	77	31	087	031.8	18	•	•	01	08	•	01	07	09	07	04	05	•	•	02	13	•						
X	7.7	5.4	5.2	6.1	0984.5	08.4	94	63	89	82	34	041	016.7	11	•	•	08	•	•	04	12	07	04	02	07	•	•	•	01	14	•						
XI	9.3	7.4	7.0	7.2	0464.6	04.0	92	77	90	86	36	113	045.2	14	•	•	08	•	•	01	20	13	07	03	12	04	02	•	01	17	01						
XII	8.8	7.9	7.7	8.2	0302.0	04.0	63	80	86	86	29	076	029.2	29	•	09	22	•	•	02	22	09	08	03	09	05	05	01	•	11	01						
GOD.	7.7	6.7	5.7	6.7	1564.0	07.4	90	60	79	76	18	1265	053.2	22.VII	04	09	68	52	04	•	12	01	24	152	157	114	50	151	25	19	02	06	02	01	47	117	34
<b>KLENIK PRI VACAH</b>																							H <sub>s</sub> = 550 m H <sub>b</sub> = - m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.5 m														
BR. ST. 14																		H <sub>s</sub> = 550 m H <sub>b</sub> = - m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.5 m																			
I	9.5	8.4	8.6	8.9	-	04.8	94	68	90	91	60	129	014.5	27	•	01	14	•	•	01	•	24	21	17	04	15	08	•	•	•	14	15					
II	8.4	7.0	6.4	7.2	-	05.3	93	72	85	83	41	123	022.6	23	•	09	•	•	01	•	16	13	15	03	02	07	•	•	02	04	04						
III	5.7	5.6	3.6	5.0	-	05.4																															

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Mesec	Vrstanini po mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vетра nD, Fm (0-12)																			
		Tm			Sred. (Gads)	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C		
		7	14	21							S.	J.	S.	J.	E.	J.													
$\gamma = 46^{\circ}04' N \lambda = 15^{\circ}11' E$ Gr. $\Delta G$ + 1h 01 min.																													
I	-	01.7	04.6	02.1	02.7	05.9	00.1	14.2	24	-06.1	19	25	01.6	04	01.8	02	01.5	.	.	11	01.2	02	01.5	11	01.7	06	03.5	32	
II	-	08.3	08.6	04.8	05.4	09.1	01.5	15.8	24	-06.4	04	29	01.7	01	02.0	.	.	.	.	09	01.6	04	01.8	11	01.4	03	02.7	25	
III	-	03.5	14.7	07.2	08.2	15.8	02.2	25.3	24	-06.6	01	31	01.6	01	03.0	01	04.0	.	.	17	01.8	01	02.0	09	01.7	09	02.3	24	
IV	-	05.1	13.7	07.0	08.6	15.3	02.3	26.7	30	-02.7	16	28	02.0	05	01.4	03	02.0	16	01.9	01	02.0	26							
V	-	11.8	19.4	12.9	14.3	20.7	07.9	28.2	04	01.6	28	32	01.6	02	03.6	02	01.5	.	.	11	02.0	.	.	02	02.5	06	02.7	38	
VI	-	15.9	23.1	16.4	18.0	24.7	11.7	31.4	13	02.5	02	37	01.6	01	02.0	01	03.0	.	.	09	01.7	.	.	04	01.8	06	02.5	32	
VII	-	14.3	24.1	17.9	19.1	26.0	13.5	31.2	12	09.4	28	30	01.5	.	.	.	.	01	02.0	12	01.9	.	.	04	02.0	05	01.8	41	
VIII	-	15.5	23.0	17.2	18.2	24.2	13.4	28.0	06	08.2	25	44	01.4	.	.	.	.	.	.	06	01.2	.	.	02	02.0	04	02.0	37	
IX	-	09.8	16.7	11.6	12.9	19.9	08.2	28.0	08	-01.0	29	38	01.6	01	02.0	.	.	.	.	04	01.5	.	.	03	01.0	.	.	44	
X	-	09.0	17.3	10.9	12.0	18.5	07.4	25.0	08	00.9	03	30	01.7	.	.	.	.	.	.	08	02.0	01	03.0	01	04.0	.	.	53	
XI	-	04.3	09.5	05.4	06.2	11.0	02.1	22.3	12	-03.6	19	30	01.8	.	.	01	02.0	.	.	06	01.5	.	.	09	02.7	04	03.8	40	
XII	-	-01.0	03.2	00.5	00.8	04.0	-02.5	12.3	25	-08.7	06	29	01.6	.	.	.	.	.	.	09	02.1	03	02.0	06	02.0	09	03.6	37	
GOD.	-	07.9	15.0	09.3	10.5	16.3	05.7	31.4	45.VI	-08.7	06.XII	383	01.7	10	02.2	07	02.1	01	02.0	116	01.7	18	01.9	78	01.9	53	02.8	429	
$\gamma = 46^{\circ}37' N \lambda = 15^{\circ}13' E$ Gr. $\Delta G$ + jh 01 min.																													
I	-	-00.7	03.3	-00.1	00.6	04.1	-02.8	12.1	23	-10.4	19	02	01.5	01	01.0	.	.	01	02.0	01	03.0	04	01.8	03	01.7	12	01.7	69	
II	-	01.3	08.3	03.3	04.1	09.3	00.2	15.0	25	-03.9	03	01	01.0	.	01	02.0	02	01.0	01	01.0	08	03.5	02	01.5	15	01.3	54		
III	-	01.6	14.9	07.0	07.6	15.6	00.2	24.6	25	-07.8	01	02	02.5	01	02.0	02	01.0	03	01.0	03	02.3	05	01.8	08	01.8	08	01.4	61	
IV	-	04.0	13.0	07.2	07.9	14.3	01.5	25.3	30	-04.7	17	01	01.0	.	.	.	.	01	01.0	04	02.3	08	01.6	'04	02.0	08	01.9	65	
V	-	10.6	18.9	13.4	14.1	20.2	07.0	27.5	21	01.6	29	01	01.0	03	01.3	01	01.0	10	01.9	04	02.3	06	01.5	03	01.3	10	01.5	55	
VI	-	14.2	22.7	17.8	24.6	10.6	31.5	13	01.0	02	02.0	02	01.0	03	01.3	08	01.5	04	01.8	05	01.3	05	01.8	08	01.8	49			
VII	-	14.9	23.1	17.9	18.4	24.3	11.7	32.3	03	08.0	24	01	01.0	.	02	01.0	02	02.3	.	.	08	01.2	06	01.2	10	01.7	62		
VIII	-	14.5	22.0	17.5	23.2	12.3	29.0	05	08.3	27	01	02.0	04	02.0	.	.	07	02.0	05	01.2	02	02.0	13	01.6	56				
IX	-	09.2	16.5	11.1	12.9	19.5	07.9	28.6	08	01.1	29	02	01.5	03	01.7	01	01.0	.	.	01	01.0	05	01.2	03	01.3	07	01.1	68	
X	-	08.2	17.1	10.8	11.7	17.9	06.7	23.5	07	-00.3	04	01	01.0	.	02	01.0	03	02.3	10	01.7	.	.	07	01.6	70				
XI	-	02.5	09.2	04.0	04.9	09.7	00.9	19.3	04	-06.7	30	01	01.0	.	01	01.0	01	01.0	08	01.3	04	01.3	09	02.1	67				
XII	-	-02.7	02.3	-01.8	-00.9	03.0	-04.2	08.7	25	-08.4	23	03	01.0	02	01.5	01	01.0	04	01.0	03	02.0	05	01.8	70					
GOD.	-	04.5	14.8	00.8	09.7	15.5	04.4	33.3	45.VII	-10.4	05.VIII	10.1	17	01.5	16	01.6	11	01.2	45	01.7	27	01.9	78	01.7	43	01.6	112	01.6	746
$\gamma = 46^{\circ}15' N \lambda = 15^{\circ}15' E$ Gr. $\Delta G$ + 1h 01 min.																													
I	-	08.8	09.7	01.4	02.0	04.7	-01.1	11.5	20	-08.4	19	01	01.0	24	01.0	.	.	07	01.1	.	.	17	02.1	01	01.0	08	01.0	35	
II	-	02.4	08.0	04.6	04.9	08.8	01.8	15.4	24	-07.2	04	01	01.0	14	01.1	.	.	03	01.0	.	.	23	02.0	01	01.0	08	01.0	33	
III	-	02.2	16.0	10.4	12.7	17.1	02.4	24.6	24	-07.0	01	01	01.0	09	01.0	01	02.0	09	01.3	01	01.0	16	01.4	41					
IV	-	04.8	13.5	08.1	08.4	14.5	02.1	27.3	30	-04.2	17	01	01.0	21	01.1	02	01.0	08	01.0	01	02.0	14	01.1	.	.	20	01.0	25	
V	-	11.4	19.1	14.4	14.8	20.6	03.6	27.8	04	06.8	28	01	01.0	16	01.1	.	.	10	01.3	.	.	22	01.4	.	.	23	01.2	21	
VI	-	16.5	24.0	16.9	25.3	31.0	31.4	31.6	13	00.8	02	01	01.1	11	01.1	01	01.0	09	01.3	01	01.0	35	01.3	02	01.0	16	01.3	14	
VII	-	16.3	23.7	19.1	19.6	25.4	13.3	31.8	13	08.6	29	01	01.0	10	01.2	04	01.8	.	.	01	02.0	21	01.5	09	01.1	22			
VIII	-	15.3	23.1	18.6	18.8	24.0	13.0	28.2	06	07.4	24	01	01.0	11	01.0	02	01.0	05	01.2	01	02.0	15	01.1	07	01.0	14	01.1	20	
IX	-	09.2	18.4	11.3	12.9	19.7	08.5	24.8	04	03.5	28	01	01.0	16	01.1	02	01.0	09	02.9	18	03.1	21	03.4	06	03.0	16	02.6	10	
X	-	09.1	14.6	11.2	11.2	17.1	21.5	08.6	00.4	03	03	03	07	01.3	12	02.6	12	03.4	17	02.5	02	02.5	09	04.0	17	04.5	06	02.2	27
XI	-	04.4	07.6	04.7	05.4	08.9	02.5	20.7	11	-04.9	21	01	01.0	01	01.0	18	02.9	21	03.2	02	02.5	09	04.0	17	04.3	06	03.0	16	
XII	-	-02.1	05.5	-01.0	-01.0	01.3	-03.0	08.9	25	-08.9	21	01	03.0	02	02.5	10	02.1	16	02.9	21	03.2	15	04.1	08	03.0	21			
GOD.	-	07.7	12.2	08.9	09.4	13.6	05.7	26.1	45.VI	-08.0	24.XII	12	02.3	52	02.8	226	03.1	162	03.3	15	02.9	72	03.5	223	04.0	115	02.8	198	
$\gamma = 46^{\circ}06' N \lambda = 15^{\circ}24' E$ Gr. $\Delta G$ + 1h 02 min.																													
I	-	00.7	02.7	01.3																									

Meseč	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana n s a:																															
					U m s			Tn			Tx			Tn			Tx			Tx			F(O-12)			Nm(0-10)		R mm		•	*	•	*	•	*	•	*	•	*	•	*	
	7	14	21			e <sub>m</sub> - mm	7	14	21	Sred(s) Min	M	Max	Dat.	7	14	21	Sred(s) Min	M	Max	Dat.	7	14	21	Sred(s) Min	M	Max	Dat.	7	14	21	Sred(s) Min	M	Max	Dat.	7	14	21	Sred(s) Min	M	Max	Dat.	
BR. ST. 16																														$H_s = 230 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$												
I 9+2 6+5 7+6 8+4	-	05+6 9+2 8+3 9+5	153 044+1	13	.	.	13	.	.	.	01	.	01	20	19	16	05	17	03	01	.	01	.	.	.	.	.	.	.	.	.	.	.	.	09 04							
II 7+7 7+6 6+5 7+2	-	05+6 87 69 87 81 39	096 019+3	23	.	.	10	.	.	.	01	.	01	13	14	12	05	13	03	01	.	.	.	.	.	.	.	.	.	.	.	.	08									
III 5+4 6+6 2+4 4+6	-	05+6 85 56 76 72 22	053 025+2	29	.	.	08	01	.	.	01	.	05	06	08	05	02	06	02	02	.	.	.	.	.	.	.	.	.	.	.	.	06 01									
IV 7+6 7+0 4+2 6+3	-	05+6 87 51 79 72 21	112 046+5	09	.	.	06	02	.	.	02	.	02	10	10	05	03	10	01	01	.	.	.	.	.	.	.	.	.	.	.	02										
V 4+5 6+8 3+8 5+2	-	08+6 82 52 61 72 29	080 036+6	15	.	.	06	.	.	.	06	.	06	09	12	04	02	12	.	.	.	.	.	.	.	.	.	.	.	.	02 05											
VI 5+1 6+3 4+2 5+2	-	11+0 79 51 81 71 33	065 015+2	22	.	.	15	03	.	.	06	.	06	07	09	03	05	07	09	03	.	.	.	.	.	.	.	.	.	.	.	01 01										
VII 5+2 7+0 5+1 5+8	-	12+3 86 54 85 75 28	118 019+9	08	.	.	18	04	.	.	01	.	04	11	15	14	04	15	.	.	.	.	.	.	.	.	.	.	.	05 02												
VIII 6+0 7+2 4+5 5+9	-	12+5 92 55 89 80 37	166 057+6	22	.	.	14	.	.	.	05	.	05	12	14	11	06	14	.	.	.	.	.	.	.	.	.	.	.	03 04												
IX 6+0 6+3 4+4 5+6	-	05+4 55 55 92 82 40	086 022+5	16	.	.	01	06	.	.	02	02	02	06	07	09	08	04	05	.	.	.	.	.	.	.	.	.	.	01 02												
X 8+8 5+9 5+4 6+5	-	08+8 94 64 93 82 32	046 012+6	02	.	.	01	.	.	.	02	.	02	12	05	02	06	02	06	.	.	.	.	.	.	.	.	.	.	16												
XI 6+9 7+0 6+5 7+5	-	06+2 89 71 88 83 39	126 064+1	14	.	.	11	.	.	.	01	.	03	19	18	08	03	06	01	.	.	.	.	.	.	.	.	.	.	01 08												
XII 8+1 7+4 7+3 7+6	-	03+9 84 70 83 75 27	044 014+5	29	.	05	24	.	.	02	.	03	20	10	08	01	08	02	.	.	.	.	.	.	.	.	.	.	07													
GOD. 6+6 6+5 5+2 6+3	-	07+5 88 61 85 78 21	1145 064+1	44.XI	05	73	65	07	.	10	02	48	146	134	107	40	129	13	06	.	01	.	.	.	.	.	.	.	.	17 70												
RADLJE CB BRAVI																															$H_s = 365 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$											
I 9+6 7+0 7+5 8+0	-	04+4 94 75 92 88 60	081 013+5	14	02	01	24	.	.	.	02	.	02	15	15	14	02	10	05	01	.	01	.	.	.	.	.	.	.	.	15 23											
II 8+7 6+2 7+3 7+4	-	05+2 91 67 88 82 39	083 021+8	23	.	.	15	.	.	.	02	.	02	11	11	10	03	04	02	.	.	.	.	.	.	.	.	.	13 64													
III 6+1 6+5 4+7 6+1	-	05+8 95 50 79 75 28	036 017+8	31	.	.	15	.	.	.	02	.	02	05	05	02	07	03	02	.	.	.	.	.	.	.	.	.	03 02													
IV 6+5 6+2 4+9 5+9	-	05+9 91 53 78 74 19	118 055+0	09	.	.	11	02	.	.	03	.	03	09	11	09	02	11	03	02	.	.	.	.	.	.	.	.	.	03 02												
V 6+5 6+5 6+7 6+7	-	08+6 86 54 77 72 29	065 021+8	23	.	.	04	.	.	.	01	.	01	11	08	03	11	.	.	.	.	.	.	.	.	.	.	.	03													
VI 5+1 5+7 5+6 5+5	-	10+7 65 54 73 71 33	105 057+8	22	.	.	13	03	.	.	04	.	04	11	10	08	03	02	01	.	.	.	.	.	.	.	.	.	03 01													
VII 6+7 5+5 5+3 6+0	-	11+8 91 55 81 76 29	162 042+5	26	.	.	15	02	.	.	03	.	03	05	15	11	06	15	.	.	.	.	.	.	.	.	.	02														
VIII 9+2 6+5 6+3 7+3	-	12+2 93 64 88 81 36	102 029+7	22	.	.	07	.	.	.	01	.	01	11	11	06	05	01	04	03	01	.	.	.	.	.	.	.	12													
IX 5+4 6+6 6+2 7+4	-	09+5 95 63 92 84 44	083 018+1	10	.	.	08	.	.	.	02	.	02	13	11	07	05	11	.	.	.	.	.	.	.	.	.	01 18														
X 5+4 4+3 5+5 6+1	-	08+6 53 65 90 83 44	043 019+0	12	.	.	01	.	.	.	02	.	02	05	04	02	06	01	06	.	.	.	.	.	.	.	.	.	19													
XI 8+3 5+5 6+2 6+6	-	05+8 63 69 91 85 51	077 025+8	14	.	.	13	.	.	.	02	.	02	09	08	07	04	05	04	01	.	.	.	.	.	.	.	.	18 08													
XII 8+0 5+2 8+3 7+2	-	02+7 54 72 92 86 49	032 020+0	07	.	04	28	.	.	.	01	.	01	11	06	05	01	04	03	01	.	.	.	.	.	.	.	.	13 26													
GOD. 7+5 5+5 6+2 6+7	-	07+7 51 62 85 79 19	996 057+8	22.VI	02	05	107	49	05	.	02	.	18	105	123	95	37	110	24	07	.	01	01	.	06	122	63	.	20													
CELJЕ-LEVEC																															$H_s = 244 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$											
I 9+0 7+6 6+2 8+3	051+6	04+5 88 79 87 84 43	112 014+4	27	.	.	18	.	.	.	01	.	01	20	17	17	05	16	06	03	.	01	.	.	.	.	.	.	.	03 12												
II 8+4 7+4 7+3 7+7	068+2	02+5 88 69 84 40 45	108 027+2	23	.	61	14	.	.	01	.	01	16	15	12	05	13	03	02	.	.	.	.	.	.	.	.	01 06														
III 6+7 5+5 5+5 6+4	144+8	05+8 52 72 75 73 19	045 015+9	29	.	01	05	.	.	01	.	01	08	05	02	07	03	02	.	.	.	.	.	.	.	.	.	01 01														
IV 7+6 7+1 5+8 6+8	152+3	05+7 84 50 83 60 20	107 039+2	05	.	09	03	.	.	01	.	01	10	12	09	04	12	.	.	.	.	.	.	.	.	.	01 03															
V 6+6 6+8 6+6 6+3	187+1	08+6 84 52 75 71 16	152 027+1	15	.	.	06	.	.	.	02	.	02	09	11	06	04	11	01	01	.	.	.	.	.	.	.	05 01														
VI 4+6 6+1 6+7 5+2	230+3	11+1 77 49 70 45 27	037 011+5	01	.	.	16	05	.	.	02	.	02	03	08	06	01	08	.	.	.	.	.	.	.	.	06															
VII 5+3 5+5 5+2 5+6	230+3	12+5 87 57 76 74 36	146 030+7	15	.	.	16	03	.	.	03	.	03	04	16	12	05	16	.	.	.	.	.	.	.	.	06 05															
VIII 6+5 7+1 6+9 6+8	171+7	12+7 89 61 86 75 37	154 062+7	22	.	.	13	.	.	.	08	.	08	14	12	04	14	.	.	.	.	.	.	.	.	.	06 05															
IX 6+5 6+5 6+6 6+6	165+6	05+6 50 51 56 51 56	068 017+2	10	.	.	01	08	.	.	03	.	03	06	07	09	07	04	05	.	.	.	.	.	.	.	.	02 10														
X 8+0 5+8 6+1 6+7	118+1	08+1 89 61 85 78 24	026 010+4	02	.	.	02	.	.	.	01	.	01	12	11	06	04	01	06	.	.	.	.	.	.	.	.	01 13														
XI 6+1 6+7 6+9 7+2	083+3	05+7 69 66 36	066 019+0	24	.	.	08	.	.	.	01	.	01	10	07	03	10	.	.	.	.	.	.	.	.	.	01 06															
XII 8+2 7+4 7+4 7+8	054+7	03+8 61 70 87 74 34	146 075+9	14	.	01	09	.	.	02	.	02	13	10	08	04	06	03	01	01	.	.	.	.	.	.	.	06 12														
GOD. 7+1 5+6 5+6 5+5	-	07+2 62 68 78 76 28	1181 075+5	44.XI	05	76	15	.	.	15	01	35	143	144	114	45	125	25	.	.	03	01	25	33	78	.	.	.	.													
KARLOCA-TEZNIC																															$H_s = 275 \text{ m } H_b = 274.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.4 \text{ m}$											
I 6+1 7+7 7+2 7+7	058+4	04+3 61 80 91 87 45	083 016+4	14	01	06	20	.	.	.	01	.	01	12	12	04	13	07	03	.	01	.	.	.	.	.	.	.	07 24													
II 6+7 7+5 7+4 7+9	195+1	05+1 87 66 73 79 36	086 017+6	23	.	62	06	.	.	01	.	01	16	15	12	04	11	03	01	.	01	.	.	.	.	.	.	01 02														
III 6+6 6+6 6+6 6+6	174+7	05+7 87 68 71 69 25	046 020+6	29	.	.	06	.	.	01	.	01	07	04	06	03	02	.	.	.	.	.	.	.	.	.	01 01															
IV 7+2 7+3 5+0 6+5	175+6	05+6 61 51 70 67 27	066 026+3	08	.	05	02	.	.																																	

Mesec	Vazdušni pritisak Fm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, Fm (0-12)																		
		Tm			Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21								8.	J.	8.														
$\varphi = 40^{\circ}24' N \lambda = 15^{\circ}39' E$ Gr. $\Delta G = +1h\ 03\ min.$																												
I	-	-00.5	03.3	-01.0	01.2	04.6	-02.3	13.2	30 -12.0	19	-	-	-	-	-	-	-	40	02.2	02	01.5	07	01.1	44				
II	-	-02.3	08.2	04.0	04.6	09.0	00.6	17.0	24 -10.5	03	-	-	03	01.3	-	-	-	47	02.3	-	-	01	02.0	33				
III	-	-03.7	14.2	06.7	07.8	15.3	01.6	24.5	24 -05.6	01	-	-	05	01.4	-	-	-	39	02.1	-	-	07	01.1	42				
IV	-	-05.1	13.4	07.4	08.4	14.3	02.2	26.0	29 -03.5	17	-	-	04	01.5	-	-	-	27	02.0	-	-	13	01.5	46				
V	-	11.7	16.0	12.5	14.0	20.4	07.8	27.0	04 00.2	28	-	-	01	02.0	-	-	-	41	01.9	-	-	04	01.8	47				
VI	-	-16.0	24.2	16.4	16.3	25.1	11.5	30.7	14 00.5	02	-	-	03	01.3	-	-	-	38	02.3	-	-	02	02.0	47				
VII	-	-15.8	23.3	17.1	18.6	25.1	12.5	29.8	12 06.6	27	-	-	-	-	-	-	-	36	01.9	-	-	02	01.5	55				
VIII	-	-14.9	23.0	16.5	17.7	23.5	12.7	26.0	06 07.6	25	-	-	-	-	05	01.6	-	26	01.5	-	-	07	01.3	53				
IX	-	05.9	18.0	11.1	12.3	19.0	07.0	28.0	08 -00.5	29	-	-	01	02.0	01	01.5	08	13	01.5	-	-	11	01.5	56				
X	-	07.8	15.6	09.5	10.6	16.4	05.5	23.0	07 -01.8	18	-	-	-	-	-	-	-	32	02.5	-	-	07	01.0	52				
XI	-	03.4	09.2	04.8	05.0	10.4	01.6	21.5	15 -05.5	20	-	-	07	01.6	-	-	-	33	02.1	-	-	-	-	47				
XII	-	-02.2	01.8	-00.5	-00.5	02.7	-03.6	10.0	25 -10.6	05	-	-	09	01.7	-	-	-	25	01.9	-	-	-	-	59				
GOD.	-	07.2	14.4	08.8	09.9	15.5	04.8	30.7	44.VI -12.0	49.1	-	-	33	01.6	01	01.0	18	01.7	-	-	399	02.1	02	01.5	61	01.4	581	
$\varphi = 40^{\circ}38' N \lambda = 16^{\circ}11' E$ Gr. $\Delta G = +1h\ 05\ min.$																												
I	744.9	-00.7	02.5	00.3	00.6	03.7	-03.5	12.0	26 -20.7	01	05	01.2	09	01.4	10	01.7	05	02.0	12	03.2	04	03.5	03	01.7	04	01.3	37	
II	742.4	01.5	07.7	03.2	03.9	08.5	-00.4	16.6	24 -14.6	03	04	01.8	06	02.0	10	01.2	04	01.5	16	02.1	13	03.8	07	01.6	06	01.7	18	
III	747.6	-02.0	04.1	04.6	07.5	14.9	00.4	24.0	24 -06.5	01	06	02.7	11	02.5	04	01.8	13	01.5	17	02.2	06	02.3	04	01.8	15	01.1	17	
IV	742.5	04.2	12.9	07.4	08.0	14.0	01.7	26.4	30 -03.4	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	744.8	11.6	19.4	12.8	14.2	20.5	07.4	27.3	04 01.1	28	08	01.6	17	02.1	05	01.8	03	01.3	11	02.4	11	02.7	05	01.2	10	01.3	23	
VI	743.2	15.8	24.0	16.5	18.2	24.6	16.9	31.2	14 -00.1	02	06	01.5	11	02.0	07	01.5	03	01.7	10	01.7	13	03.1	05	01.2	11	01.6	21	
VII	743.4	16.3	23.8	17.8	18.9	25.0	12.4	25.4	03 04.8	26	08	02.3	06	01.7	16	01.3	03	01.3	12	02.2	06	03.8	10	04.5	10	01.6	24	
VIII	742.4	15.0	23.0	16.6	18.0	23.9	12.7	27.6	04 07.1	08	01.9	02.1	05	01.8	08	01.9	01	01.9	18	02.0	12	02.3	03	02.0	18	01.7	33	
IX	745.1	08.8	17.9	10.4	12.1	18.7	06.8	27.4	05 -03.5	29	05	01.4	13	01.5	02	02.5	05	01.4	07	01.7	08	01.6	01	02.0	13	01.5	32	
X	745.0	07.4	15.2	09.2	10.2	15.6	05.6	23.3	08 -02.3	04	04	01.3	02	01.0	-	-	08	01.4	05	02.0	15	04.1	03	01.0	09	01.3	47	
XI	743.0	-02.6	09.3	04.3	05.1	10.1	00.8	26.2	04 -07.0	30	06	02.8	10	02.6	05	01.8	04	02.5	14	02.5	05	02.0	03	01.3	05	01.2	33	
XII	750.4	-02.5	01.1	-01.5	-01.1	02.1	-04.0	09.7	25 -11.1	05	05	02.4	12	01.8	05	01.0	16	01.7	02	02.0	08	02.0	04	01.5	07	01.6	34	
GOD.	745.4	08.6	14.2	08.7	09.6	15.2	04.2	31.2	44.VI -20.7	49.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 40^{\circ}28' N \lambda = 16^{\circ}12' E$ Gr. $\Delta G = +1h\ 05\ min.$																												
I	-	-00.3	02.3	01.0	01.0	03.9	-02.0	12.5	30 -09.9	15	-	-	34	02.1	01	02.0	10	01.7	04	01.8	44	02.2	-	-	-	-	-	
II	-	-0.9	07.5	04.5	04.6	08.6	01.1	16.5	24 -05.1	04	-	-	23	02.2	-	-	-	46	02.5	-	-	-	-	-	-	-		
III	-	-05.9	13.2	09.6	09.6	14.3	04.1	24.0	24 -05.0	31	-	-	26	03.5	-	-	-	35	02.0	02	01.5	04	02.3	-	-	-		
IV	-	-05.6	12.3	08.4	08.6	13.6	03.1	25.5	30 -03.5	01	03	01.7	32	02.4	05	02.0	06	34	02.0	02	01.5	07	01.7	-	-	-		
V	-	12.7	19.1	14.1	15.0	20.4	09.1	27.0	04 04.5	28	01.1	03	01.5	02	02.5	05	01.4	07	01.7	08	01.6	01	02.0	13	01.5	32		
VI	-	17.1	23.1	17.6	18.6	24.2	12.7	31.0	14 04.0	02	01	01.0	29	02.6	04	01.5	03	32	02.4	01	02.0	06	01.0	30	02.0	01		
VII	-	17.6	23.8	18.4	19.4	24.5	13.7	29.5	08 06.0	27	01	02.7	27	02.2	05	01.4	18	02.4	02	03.0	40	02.3	05	02.0	03	02.0	33	
VIII	-	16.3	22.8	17.5	18.4	23.3	13.6	27.0	05 10.0	24	03	01.7	29	02.3	03	02.4	01	34	02.4	03	01.7	09	02.3	-	-	-		
IX	-	11.0	17.2	13.0	13.6	16.7	08.4	27.5	08 02.5	29	-	-	36	02.5	06	02.3	10	02.1	-	-	33	02.1	01	02.0	04	01.8	-	
X	-	08.9	14.9	11.0	11.5	15.6	07.2	23.5	08 01.0	03	01	02.0	37	02.1	03	02.4	06	35	02.7	03	02.3	04	01.8	-	-	-		
XI	-	-0.4	06.6	05.6	06.1	10.2	01.9	21.5	11 -05.0	20	-	-	30	02.5	-	-	-	13	02.1	-	-	43	02.7	01	02.0	03	02.3	-
XII	-	-0.2	00.8	-0.1	-0.1	01.0	-0.9	10.0	25 -08.0	06	01	01.0	26	02.2	05	01.7	17	04.6	01	01.0	38	02.3	04	01.0	03	01.7	-	
GOD.	-	08.4	13.7	09.9	10.5	14.9	05.8	31.0	44.VI -05.5	49.1	11	01.6	370	02.3	23	01.9	123	02.0	15	01.9	475	02.4	25	01.7	43	01.9	-	
$\varphi = 46^{\circ}50' N \lambda = 16^{\circ}17' E$ Gr. $\Delta G = +1h\ 05\ min.$																												
I	-	-01.0	02.2	00.2	00.4	03.2	-03.0	10.5	26 -12.5	01	34	01.1	03	02.0	01	01.0	06	02.0	22	01.4	22	02.3	04	01.3	01	02.0	-	
II	-	01.4	07.5	03.9	04.2	08.2	15.5	24 -08.5	03	28	01.2	06	02.0	-	-	03	03.3	14	02.2	27	02.1	05	01.0	01	01.0	-		
III	-	03.5	13.3	07.6	08.0	14.1	01.8	23.0	24 -07.0	01	27	01.5	09	03.0	01	01.0	13	02.0	13	01.7	31	02.2	07	01.0	01	02.0	-	
IV	-	04.9	12.4	08.1	08.4	13.5	01.8	25.5	30 -06.0	01	24	01.2	20	02.2	02	01.0	01	01.0	16	01.5	20	02.1	06	01.0	01	02.0	-	
V	-	12.3	16.5	12.9	14.2	19.4	07.8	26.5	04 02.6	28	17	01.4	13	02.1	-	-	26	01.4	29</									

Mjesec	Oblačnost Nm (0-10)	Vlažnost vazduha e-m mm	Insolacija broj sati	Padavine R mm			Broj dana na sas:																			
							Tn	Tx	Tn	Tx	Tn	F(O-12)	Nm(O-10)	R mm	•	*	*	Δ	Δ	▲	▲	T	≡			
				7	14	21	Sred. (Dnev.)	mm	7	14	21	Specijal (Dnev.)	Min	Max	Dat.	10.00.0	0.025	0.020	0.0	6	8	2.0	8.0	0.1	1.0	0.0
<b>BR. ST. 21</b>																										
<b>FRANCUSKA</b>																										
I 8.3 6.5 7.0 7.3	-	04.3 85 86 85 64 54	085 021.8	14	04	02	21	*	*	*	*	01	*	02	17	13	15	04	11	05	03	*	*	*	08 11	
II 7.2 6.5 7.0 7.1	-	05.2 66 66 78 48	070 013.7	23	01	*	13	*	*	*	*	*	*	04	13	11	11	03	06	02	03	*	*	*	02 07	
III 4.6 5.0 3.6 4.4	-	06.3 88 62 80 77 35	056 018.5	31	*	*	11	*	*	*	*	*	05	07	06	04	02	05	03	01	*	*	*	*	03 02	
IV 5.4 5.1 4.3 4.9	-	06.4 87 61 82 77 34	065 023.2	09	*	*	11	03	*	*	*	*	05	09	10	09	01	10	*	*	*	*	*	*	01 01	
V 5.5 5.3 4.7 5.3	-	09.6 87 64 86 79 39	046 015.7	31	*	*	06	*	*	*	*	*	08	12	10	10	01	10	*	*	*	*	*	*	01 *	
VI 4.6 4.6 4.5 4.6	-	12.5 67 55 86 77 33	021 006.8	22	*	*	15	04	*	*	*	*	06	06	06	06	*	06	*	*	*	*	*	*	02 *	
VII 5.6 5.6 4.7 5.3	-	12.5 64 65 50 64 48	178 043.2	15	*	*	18	*	*	*	*	*	07	05	12	12	07	12	*	*	*	*	*	*	01 05 *	
VIII 5.5 6.1 5.5 5.8	-	13.8 61 55 78 95 88 61	110 029.2	22	*	*	13	*	*	*	*	*	06	13	11	11	05	11	*	*	*	*	*	*	01 01	
GOD. 6.1 5.6 5.2 5.7	-	08.3 90 69 87 82 33	829 052.4	44.xi	07	08	96	63	04	*	02	*	86	140	106	104	27	96	16	04	*	*	01	10 31 31		
<b>BR. ST. 22</b>																										
<b>MURSKA SOBOCA</b>																										
I 9.3 6.6 6.5 6.8	044.1	04.3 92 85 51 85 42	065 016.2	27	03	06	23	*	*	*	*	02	*	22	13	05	02	12	05	01	*	*	*	09 12		
II 8.5 6.5 6.7 7.6	058.4	05.2 93 68 55 62 39	056 013.6	07	03	02	16	*	*	*	*	05	*	16	11	09	02	10	03	01	*	*	*	01 06 07		
III 5.6 6.5 4.9 5.6	189.0	05.8 95 52 81 75 24	041 013.5	25	*	*	16	*	*	*	02	*	03	07	09	04	02	05	03	02	*	*	*	05 01		
IV 7.1 5.3 4.9 6.5	185.5	06.0 88 61 74 25	063 024.6	09	*	*	12	02	*	*	01	*	04	10	05	07	02	05	02	*	*	*	*	03 02 01		
V 6.3 6.9 5.0 6.0	226.2	08.5 82 51 77 30	024 009.5	24	*	*	04	*	*	*	04	*	10	09	05	*	05	*	*	*	*	*	*	03 02		
VI 4.2 6.0 5.3 5.3	287.1	10.5 77 46 76 66 32	067 025.7	16	*	01	15	02	*	*	01	*	04	05	09	06	03	*	*	*	*	*	*	01 07 *		
VII 5.8 5.5 4.5 5.3	247.4	11.9 86 54 81 74 25	100 022.7	15	*	*	16	*	*	*	01	*	04	05	11	08	04	11	*	*	*	*	*	*	04 03	
VIII 5.9 6.6 4.9 5.8	203.8	11.9 87 57 86 77 36	137 044.5	22	*	*	12	*	*	*	04	*	10	15	05	15	*	*	*	*	*	*	*	08 03		
GOD. 6.6 6.5 5.6 6.4	1905.9	07.5 86 60 84 77 24	717 045.0	44.xi	09	16	114	56	02	*	20	*	34	136	129	81	25	113	20	09	01	01	01	29 78 32		
<b>BR. ST. 23</b>																										
<b>JERUZALEM</b>																										
I 8.7 7.6 7.1 7.8	049.7	04.3 85 82 89 87 47	052 028.0	14	*	06	24	*	*	*	01	15	12	10	02	16	05	02	*	*	*	*	09 25			
II 8.5 7.3 7.3 7.7	082.8	05.1 84 65 78 77 41	059 016.3	01	*	03	09	*	*	04	*	02	16	05	08	01	07	03	01	*	*	*	01 04 07			
III 4.6 5.6 3.1 3.1	181.0	06.2 81 68 66 69 38	082 025.5	31	*	*	05	*	*	02	*	08	08	05	04	06	03	*	*	*	*	*	*	02		
IV 5.5 5.5 4.8 5.7	171.3	06.0 77 62 72 70 32	078 027.0	09	*	*	06	02	*	*	*	06	10	08	08	03	06	02	*	*	*	*	*	01 02 03		
V 5.5 6.4 3.5 5.2	229.0	08.7 78 58 67 68 34	037 013.7	15	*	*	04	*	*	01	*	08	10	09	07	01	05	*	*	*	*	*	*	04 03		
VI 5.2 5.1 3.3 3.0	275.4	11.0 73 55 76 66 40	082 040.2	23	*	*	14	02	*	*	04	*	13	05	10	07	03	10	*	*	*	*	*	*	07 *	
VII 5.6 5.4 5.2 5.6	251.5	12.0 78 60 73 71 43	115 030.4	15	*	*	15	*	*	01	*	08	04	11	05	05	11	*	*	*	*	*	*	06 *		
VIII 6.0 5.6 5.6 5.6	199.9	12.4 85 66 80 77 45	120 036.8	22	*	*	09	*	*	*	06	*	11	15	12	05	15	*	*	*	*	*	*	07 02		
IX 4.7 5.3 3.5 4.5	187.4	08.8 85 61 75 74 36	064 016.4	10	*	*	06	*	*	04	*	11	08	08	07	03	06	*	*	*	*	*	01 *			
X 6.5 4.8 4.8 4.5	136.6	06.4 52 72 85 83 27	036 015.2	12	*	*	04	*	*	04	*	09	14	05	04	02	05	*	*	*	*	*	*	06 *		
XI 7.7 6.6 6.7 7.0	190.7	05.7 83 70 75 77 26	075 052.4	14	*	*	09	*	*	04	*	04	16	10	06	01	08	04	01	*	*	*	*	04 05		
XII 6.0 6.3 6.4 7.7	149.6	03.7 90 82 87 86 46	055 015.2	07	*	10	27	*	*	04	*	04	19	11	07	02	06	07	02	*	*	*	*	10 24		
GOD. 6.2 6.2 5.1 5.9	1903.9	07.7 82 66 76 75 27	896 052.4	44.xi	*	19	80	56	02	*	20	*	80	145	116	90	32	105	24	06	*	*	*	27 48 67		
<b>BR. ST. 24</b>																										
<b>VELIKI COLENCI</b>																										
I 8.8 8.1 7.0 8.0	-	-	-	-	075	013.0	14	02	06	24	*	*	01	*	16	14	13	02	08	08	*	02	*	*	09 18	
II 6.1 7.4 5.6 7.6	05.0	96 61 79 41	058 013.5	07	*	14	*	*	02	*	01	*	11	11	05	02	01	01	01	01	*	*	*	01 02 06		
III 4.4 5.1 2.0 3.6	04.7	87 52 74 71 26	041 018.0	31	*	*	08	*	*	01	*	09	03	05	04	02	04	02	01	*	*	*	03 01			
IV 6.5 6.7 4.1 5.8	05.9	85 57 75 72 31	057 022.0	09	*	*	09	01	*	*	*	03	07	07	06	01	07	02	*	*	*	*	*	02 01		
V 5.7 6.4 4.4 5.5	09.2	84 61 79 75 27	031 007.7	06	*	*	04	*	*	02	*	04	09	07	07	02	07	*	*	*	*	*	*	03 *		
VI 4.1 5.3 5.3 4.8	11.8	84 54 82 73 42	061 017.5	27	*	*	14	03	*	02	*	03	06	06	06	02	06	06	*	*	*	*	*	01 *		
VII 5.4 5.7 5.8 5.7	14.5	85 53 82 73 37	084 015.0	15	*	*	15	01	*	04	*	04	08	09	08	05	09	*	*	*	*	*	*	03 *		
VIII 6.4 6.4 6.4 6.4	-	-	-	-	076	026.0	22	*	*	09	*	*	02	05	10	05	02	10	*	*	*	*	*	03 *		
IX 5.6 5.4 3.6 4.8	-	-	-	-	034	017.8	16	*	01	06	*	*	08	05	07	06	01	07	*	*	*	*	*	02 *		
X 5.8 4.7 3.5 4.7	-	084.4	90 70 91 84 44	010 006.0	02	*	01	*	*	02	*	02	10	05	05	02	05	*	*	*	*	*	*	09 *		
XI 6.6 7.4 6.2 6.6	05.5	68 72 85 73 35	040 032.4	14	*	01	08	*	*	02	*	03	06	06	04	01	06	02	02	*	*	*	05 01			
XII 6.4 7.6 6.4 7.4	-	03.6	91 82 89 87 42	032 010.6	07	01	-	27	*	*	01	*	01	15	09	07	01	07	04	*	*	*	*	09 10		
GOD. 6.3 6.2 5.0 5.8	-	-	-	-	603	032.4	14	01	09	04	*	11	*	47	105	98	82	18	87							





Mesec	Vrhovni Pratiljak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра nD, Fm (0-12)																					
		Fm				Sred. (Gles)				Max		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21		Max	Min	Max	Min	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
Φ = 45°34' N λ = 14°15' E Gr. ΔG = + 57 min.																									ILIRSKA BISTRICA		BR. ST. 31						
I	-	02.7	05.8	03.7	04.0	06.7	01.2	11.8	24 -06.0	19	18	01.8	.	.	04	02.5	11	03.4	27	03.3	02	04.0	01	02.0	04	02.5	26						
II	-	03.0	04.1	04.6	05.1	05.2	01.3	13.2	23 -06.5	03	11	03.0	.	.	03	03.3	07	04.6	19	03.2	01	02.0	03	02.0	04	02.0	29						
III	-	02.6	12.6	06.8	07.2	13.5	01.6	24.2	25 -05.6	02	12	03.8	02	03.5	13	03.7	03	02.3	11	03.4	04	03.0	01	02.0	04	04.5	48						
IV	-	03.4	12.8	07.5	07.8	14.0	02.0	21.1	30 -04.6	17	27	02.7	01	03.0	07	03.3	06	04.5	13	03.8	05	03.6	01	01.0	02	04.5	28						
V	-	08.8	17.7	12.2	12.7	18.9	06.5	24.5	25 00.5	06	15	02.8	02	03.5	06	03.2	06	03.7	07	02.7	08	03.4	02	02.5	04	03.5	43						
VI	-	12.4	20.7	15.5	16.1	22.4	10.4	26.8	13 02.4	03	19	02.7	.	.	09	02.9	07	03.7	15	03.3	03	02.0	01	04.0	03	04.0	33						
VII	-	14.1	22.8	17.6	16.0	24.1	12.5	25.2	13 07.9	28	23	03.2	.	.	02	02.0	06	03.3	17	03.4	03	04.0	01	03.0	02	05.0	39						
VIII	-	12.9	22.4	16.0	16.8	23.5	12.0	26.8	08 07.4	25	10.9	02.4	.	.	01	02.0	05	03.2	18	02.6	04	02.5	04	02.3	01	03.0	45						
IX	-	07.5	18.9	10.9	12.1	20.1	04.7	27.7	08 -02.6	25	23	03.3	01	03.0	02	03.0	06	02.7	10	02.3	07	03.6	03	01.3	02	02.0	36						
X	-	07.4	16.4	10.0	11.0	17.6	06.5	22.5	25 -01.0	04	13	02.3	02	03.0	04	01.5	12	03.5	09	03.4	04	03.5	01	01.0	01	04.0	47						
XI	-	03.8	10.2	05.2	06.1	11.3	01.5	20.0	11 -04.5	20	24	03.8	01	03.0	03	01.3	05	03.9	16	03.3	04	02.3	01	04.0	03	02.0	29						
XII	-	-02.2	05.4	00.3	01.0	06.5	-03.5	11.2	25 -10.9	23	27	03.6	01	01.0	05	02.2	07	03.3	08	02.1	12	05.0	05	01.2	02	02.0	36						
GOD.	-	06.4	14.5	09.2	09.8	15.6	05.0	26.8	13 VI -16.9	23 XI 22.7	03.0	10	03.0	70	02.9	85	03.6	170	03.1	45	03.4	26	C1.9	23	63.0	439							
Φ = 45°38' N λ = 14°22' E Gr. ΔG = + 57 min.																									MASUN		BR. ST. 32						
I	-	-00.4	01.3	-00.2	00.2	02.2	02.5	-03.1	06.7	25	-10.4	05	*	*	01	01.0	12	01.4	19	01.2	01	04.0	48	02.1	06	02.5	14	C1.3	*				
II	-	-06.2	02.7	00.4	00.9	03.4	03.6	-05.6	06.7	24	-12.2	04	03	01.0	11	01.2	04	01.8	04	01.5	03	01.7	39	02.3	03	01.7	15	C1.5	*				
III	-	02.0	0.9	01.3	02.7	05.7	00.1	12.4	25 10.6	01	02.0	01.0	02	01.5	14	01.6	12	01.6	32	01.6	05	01.8	04	01.5	03	01.5	*						
IV	-	01.3	07.5	02.7	03.6	08.7	-00.7	17.3	30 -08.9	17	06	01.0	20	01.4	01	02.0	11	01.5	*	*	11	01.8	17	01.4	24	C1.4	*						
V	-	08.5	12.4	07.4	08.9	13.6	04.1	26.1	04 -02.6	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	11.7	15.9	10.9	12.3	17.4	07.8	24.9	13 01.1	03	04	01.5	16	01.1	15	01.5	04	01.6	01	01.0	18	01.7	15	01.3	17	01.2	*						
VII	-	13.2	18.1	12.4	14.0	19.2	05.2	23.2	04 03.7	28	06	01.0	13	01.8	18	01.6	02	02.0	04	01.5	05	01.6	32	01.3	13	01.5	*						
VIII	-	11.5	16.9	12.0	13.1	18.2	05.1	22.4	07 03.0	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
GOD.	-	04.8	09.4	05.0	06.0	10.4	02.0	24.9	13 VI -15.2	04.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
Φ = 45°53' N λ = 14°26' E Gr. ΔG = + 58 min.																									RAKITA		BR. ST. 33						
I	-	-00.4	01.7	00.6	00.3	02.7	02.7	05.4	25 -13.1	19	10	01.7	22	02.3	08	01.6	16	02.7	07	01.9	08	02.8	11	01.6	10	02.8	01						
II	-	00.7	04.4	01.3	01.9	05.7	-01.7	10.7	24 -17.8	04	13	02.5	08	02.6	18	01.4	10	02.9	08	03.0	06	02.2	18	02.1	11	03.2	*						
III	-	02.2	09.8	04.1	05.1	11.0	-00.6	20.1	25 -10.6	04	02	01.0	09	02.3	05	03.2	05	02.1	17	01.7	13	02.5	19	02.0	18	03.2	01						
IV	-	02.7	08.9	04.0	05.1	10.5	-00.5	20.7	30 -08.7	17	03	02.0	14	02.1	15	02.0	11	02.3	12	01.4	16	02.2	10	02.6	10	02.5	04						
V	-	09.9	14.0	10.1	10.5	15.5	04.0	22.5	04 -02.9	07	07	01.6	11	02.4	13	02.5	05	02.4	14	01.6	14	02.1	20	01.6	08	02.5	01						
VI	-	13.5	17.0	12.1	14.4	19.2	07.6	27.4	13 -02.2	03	09	02.1	13	02.5	12	02.7	13	01.8	10	02.0	04	02.3	17	01.6	09	01.9	23						
VII	-	13.6	15.1	14.4	15.7	20.4	10.0	25.4	04 -02.9	02	09	01.8	12	02.1	14	02.1	06	02.1	13	02.1	09	02.6	15	01.7	13	02.5	01						
VIII	-	13.3	18.5	12.7	14.7	19.7	05.3	24.4	08 02.3	25	13	01.5	11	01.8	13	01.6	02	0.6	09	02.4	17	01.1	11	01.7	06	01.8	03						
IX	-	07.3	14.5	08.2	05.5	15.9	04.2	23.4	08 -06.8	29	10	01.6	21	02.2	17	02.4	07	02.5	02	01.2	05	01.4	05	01.8	06	02.3	04						
X	-	06.8	12.7	08.3	09.0	13.8	04.9	18.0	08 -05.7	18	08	02.3	08	02.3	11	01.5	07	02.0	18	02.2	16	02.3	15	02.3	05	02.4	05						
XI	-	02.0	0.6	02.3	03.3	03.9	-00.9	18.6	11 -12.1	28	11	01.8	13	02.1	07	01.9	16	02.1	08	02.5	14	01.9	10	03.1	06	02.1	*						
XII	-	-04.3	-00.5	-03.5	-02.9	00.9	-06.9	07.5	26 -16.5	05	16	01.8	08	02.0	19	02.3	17	02.2	02	02.0	14	02.0	09	01.7	04	01.8	02						
GOD.	-	05.4	11.6	06.5	07.5	12.8	02.4	28.6	13 VI -20.3	04.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
Φ = 45°46' N λ = 14°31' E Gr. ΔG = + 58 min.																									NEVA VAS NA BICKAF		BR. ST. 34						
I	-	00.5	02.6	00.4	01.0	03.9	-02.2	10.0	25 -11.5	20	-	-	32	02.1	*	*	01	01.0	05	04.0	05	04.2	05	03.4	23	02.9	26						
II	-	00.3	05.2	01.4	02.4	02.6	-05.1	13.3	24 -20.3	04	-	15	01.9	01	04.0	03	*	01	01.0	16	03.6	05	02.8	18	02.6	23							
III	-	01.5	10.6	03.9	05.0	11.8	-00.6	21.0	24 -09.9	01	-	16	02.4	05	01.0	02	01.5	*	01.0	14	02.4	05	03.0	22	02.5	29							
IV	-	02.1	09.9	04.6	05.3	11.3	-00.6	21.4	29 -06.5	17	-	27	01.9	*	*	07	01.9	01	03.0	04	03.0	01	04.0	25	02.6	25							
V	-	05.3	15.1	05.2																													

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha em mm	Padavine R mm	Broj dana na snazi:																						
						U m s		Tn	Tn	Tn	Tn	Tn	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ					
	7	14	21	Sred. četv.	21 Sred. (Dnes) Min	Σ	Max	Dat.	III	IV	V	VI	VI	VI	VI	VI	VI	VI	VI	VI	VI	VI						
ILIRSKA BISTRICA																												
<b>BR. ST. 31</b>																												
I 6.5 7.6 7.4 7.9	-	05.5 94 81 92 85 40	206 047.0	12	.	09	.	.	02	.	04	21	22	16	07	21	02	.	.	.	.	09	02					
II 7.6 7.6 6.9 7.3	-	05.5 85 68 75 22	164 035.2	22	.	12	.	.	01	.	02	14	15	13	05	18	01	.	01	02	06	.						
III 7.7 5.8 3.9 5.8	-	05.7 92 56 81 76 20	038 009.7	30	.	12	.	.	01	.	04	09	10	07	05	09	01	.	.	07	01	.						
IV 6.7 5.6 3.7 5.3	-	05.4 64 51 74 65 21	059 042.6	09	.	10	.	.	02	.	06	17	15	07	17	.	.	.	.	.	04	01						
V 7.1 6.6 4.6 6.1	-	08.3 93 56 79 26 29	093 019.5	14	.	09	.	.	01	.	05	12	16	12	02	16	.	.	.	.	05	09						
VI 5.9 6.0 5.9 5.9	-	10.6 92 55 80 77 36	039 008.3	22	.	07	.	.	02	.	05	13	10	13	05	13	.	.	06	05	.							
VII 6.2 6.0 4.8 5.7	-	11.6 91 57 81 77 39	130 038.2	22	.	11	.	.	01	.	05	07	16	14	04	16	.	.	11	13	.							
VIII 8.0 6.1 4.7 6.3	-	12.0 98 63 91 84 42	204 040.5	22	.	08	.	.	02	.	06	17	15	07	17	.	.	.	.	10	20	.						
IX 6.7 4.5 2.9 4.7	-	08.2 98 51 85 77 30	046 020.5	18	.	01	05	.	02	.	07	05	06	06	01	06	.	.	.	.	01	10						
X 8.3 5.7 4.4 6.2	-	08.3 94 61 84 39	074 025.4	03	.	03	.	.	02	.	09	08	05	03	03	01	.	.	.	.	01	13						
XI 6.2 6.2 6.0 6.8	-	06.2 92 47 88 82 30	112 025.9	22	.	12	.	.	04	.	02	13	14	11	04	13	02	.	.	.	03	08						
XII 4.8 4.2 4.5 4.7	-	03.9 87 63 79 76 32	108 032.4	29	03	24	.	.	04	.	09	09	07	07	03	07	.	.	.	.	08	.						
GOD. 7.1 6.1 5.0 6.1	-	07.6 91 61 83 78 20	1313 047.0	421	03	82	35	.	18	.	51	121	160	126	39	154	16	.	01	.	03	39 119	04					
PAŠUR																												
<b>BR. ST. 32</b>																												
I 6.8 8.4 7.8 8.2	-	-	-	-	-	337 064.0	12	03	06	25	.	.	.	02	22	22	21	11	17	11	02	03	02	.				
II 7.9 8.3 5.7 7.3	-	-	-	-	-	357 039.7	22	03	04	19	.	.	.	01	14	19	19	09	13	10	02	02	01	04				
III 6.2 6.2 5.1 5.6	-	-	-	-	-	091 020.2	13	01	02	15	.	.	.	02	06	13	08	05	12	03	01	.	01	06				
IV 6.3 6.3 3.7 5.4	-	-	-	-	-	137 050.2	09	01	21	.	.	.	.	04	09	12	10	04	05	05	01	.	.	02	15			
V 5.9 6.5 4.3 5.7	-	-	-	-	-	147 048.1	14	.	05	.	.	.	.	05	10	17	14	04	17	01	.	.	06	02				
VI 5.0 6.0 5.4 5.7	-	-	-	-	-	087 015.6	26	.	.	.	.	.	.	02	09	13	09	05	13	.	.	01	06	.				
VII 4.5 5.6 4.1 4.8	-	-	-	-	-	163 024.3	22	.	.	.	.	.	.	07	05	17	15	08	17	.	.	08	5.	.				
VIII 5.1 5.5 4.5 6.1	-	-	-	-	-	323 113.6	22	.	.	.	.	.	.	03	10	16	12	08	16	.	.	01	06	.				
IX 4.6 5.1 3.2 4.3	-	-	-	-	-	073 031.4	18	.	07	.	.	.	.	09	66	69	07	02	08	03	01	.	01	02	03			
X 4.5 6.0 4.1 5.4	-	-	-	-	-	075 033.0	03	.	04	.	.	.	.	06	10	09	10	07	03	10	01	.	01	07	01			
XI 7.1 6.2 5.9 6.5	-	-	-	-	-	213 051.6	22	.	05	14	.	.	.	05	12	14	12	07	10	07	01	.	01	03	12			
XII 5.9 5.5 4.5 5.4	-	-	-	-	-	147 052.8	29	06	10	29	.	.	.	08	12	09	08	03	05	01	.	01	05	31				
GOD. 6.4 6.4 4.8 5.9	-	-	-	-	-	2150 113.6	22.VII	13	26	141	.	.	.	58	127	171	142	69	144	50	10	06	04	02	.			
RAKITNA																												
<b>BR. ST. 33</b>																												
I 6.7 7.5 8.4 8.3	-	-	-	-	-	186 018.7	27	04	04	22	.	.	.	01	21	24	21	11	20	09	.	01	01	12 23				
II 7.8 7.4 6.4 7.2	-	-	-	-	-	178 037.2	23	02	02	16	.	.	.	01	11	14	14	06	14	04	01	.	.	07	07			
III 6.4 5.9 4.2 5.6	-	-	-	-	-	085 022.6	30	01	02	16	.	.	.	04	05	05	08	04	07	03	.	01	.	02	02			
IV 6.7 7.1 3.8 5.9	-	-	-	-	-	145 035.4	09	01	18	.	.	.	.	03	07	12	11	03	08	07	01	.	01	04	10			
V 5.7 6.5 4.6 5.6	-	-	-	-	-	096 030.8	08	01	03	.	.	.	.	05	09	15	11	03	15	.	.	.	05	04	.			
VI 4.6 5.9 4.6 5.0	-	-	-	-	-	062 014.4	01	01	03	.	.	.	.	06	07	14	09	01	14	.	.	06	05	.				
VII 4.8 6.2 5.0 5.4	-	-	-	-	-	237 038.4	16	.	03	.	.	.	.	06	11	16	13	09	16	.	.	01	07	03	.			
VIII 6.4 7.1 4.2 5.9	-	-	-	-	-	241 055.4	22	.	.	.	.	.	.	02	04	18	18	08	18	.	.	05	16	.				
IX 4.6 5.3 4.3 4.8	-	-	-	-	-	117 044.7	18	.	06	.	.	.	.	07	05	09	08	04	09	01	.	01	02	08	01			
X 6.6 5.0 5.0 5.9	-	-	-	-	-	048 013.0	30	.	05	.	.	.	.	06	13	08	05	02	08	.	.	01	12	.				
XI 7.4 6.5 5.3 6.4	-	-	-	-	-	164 040.6	02	02	03	17	.	.	.	01	04	13	10	06	11	06	02	.	01	09	07			
XII 6.5 6.1 5.9 6.2	-	-	-	-	-	076 026.4	29	09	13	28	.	.	.	04	12	09	04	02	07	04	.	.	01	12	26			
GOD. 6.4 6.5 5.1 6.0	-	-	-	-	-	1635 055.4	09.IV	18	24	132	06	.	.	01	.	49	124	163	126	59	147	34	06	.	01	05	35 83	76
NEVA VAS NA BLCKAH																												
<b>BR. ST. 34</b>																												
I 8.8 8.0 7.6 8.2	-	04.5 91 81 92 88 49	129 021.3	12	04	05	20	.	.	.	03	01	01	15	22	17	14	08	18	09	01	.	01	07	22			
II 7.5 7.4 5.5 6.9	-	04.6 85 75 91 85 43	134 023.1	01	03	01	15	.	.	.	03	01	01	10	17	12	05	14	04	01	.	.	.	03	08			
III 6.5 6.2 3.9 5.5	-	05.3 92 04 85 79 33	072 021.0	30	01	01	14	.	.	.	04	07	09	08	03	09	02	01	.	.	.	.	02	02				
IV 6.7 6.3 3.9 5.7	-	05.2 88 61 80 76 38	134 057.8	09	02	01	17	.	.	.	04	07	12	09	04	07	08	01	.	.	.	.	01	02	09			
V 5.7 6.6 5.6 5.8	-	08.4 87 65 90 86 39	079 020.8	27	.	05	.	.	.	03	08	16	12	03	16	.	.	.	.	01	.	.	01	06				
VI 4.6 5.2 3.8 4.9	-	09.8 82 61 82 75 40	082 025.7	23	.	01	03	.	.	.	06	05	12	10	03	12	.	.	.	.	07	.	.	01	05			
VII 4.7 4.6 4.8 5.2	-	11.1 87 67 87 80 48	176 024.0	15	.	03	04	.	.	.	07	08	18	14	08	18	.	.	.	.	07	01	.	01	04			
VIII 5.5 6.3																												

Mjesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vjetra nd, Fm (0-12)																			
		Tm			Max (Dnes)	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C		
		7	14	21							8.	15.	22.	29.	8.	15.	22.	29.	8.	15.	22.	29.	8.	15.	22.	29.	8.	15.	
$\varphi = 45^{\circ}38' N \lambda = 14^{\circ}52' E$ Gr. $\Delta G = +59$ min.																													
I	-	01.1	03.8	02.0	02.3	04.8	-00.2	10.2	26	-07.8	20	.	.	27	01.6	C4	02.6	E1	02.4	.	.	11	02.0	.	.	30	01.8	11	
II	-	01.6	03.9	03.1	03.7	07.5	00.4	14.9	24	-13.1	04	.	.	18	01.6	C3	03.0	07	02.7	.	.	12	03.2	.	.	31	01.8	13	
III	-	01.6	13.5	06.7	07.1	14.4	00.6	24.1	24	-06.5	01	01	01.0	16	02.1	E5	02.0	14	02.8	.	.	10	02.6	01	02.0	34	02.0	10	
IV	-	02.6	12.4	07.1	07.3	13.7	01.1	24.3	30	-04.9	17	01	01.0	18	02.1	O1	02.0	26	02.8	.	.	06	02.3	02	02.0	32	02.1	04	
V	-	09.0	18.0	11.6	12.7	16.8	06.7	26.3	04	00.7	28	.	.	13	01.6	C1	02.0	33	02.1	O3	02.0	07	01.6	01	01.0	19	01.6	10	
VI	-	15.0	21.1	16.3	22.7	10.3	30.6	13	01.1	02	01	02.0	13	01.6	O1	02.0	25	01.9	O1	01.0	08	02.0	.	.	31	01.7	13		
VII	-	14.1	22.8	16.8	17.6	24.0	11.4	25.7	03	07.2	18	.	.	13	02.0	O1	01.0	35	01.9	O1	01.0	08	01.4	.	.	15	01.5	30	
VIII	-	12.9	21.9	16.2	16.0	23.0	11.6	26.6	07	06.2	23	.	.	16	01.7	O1	01.0	24	01.7	O1	01.0	18	01.6	.	.	12	01.6	21	
IX	-	06.5	17.5	09.9	11.1	18.8	05.5	27.3	08	-03.1	29	.	.	27	01.6	O1	02.0	15	01.5	O1	01.0	10	01.7	.	.	20	01.8	18	
X	-	06.7	15.9	09.6	10.5	16.7	05.9	22.3	08	-06.7	18	.	.	12	02.0	.	.	22	02.0	O1	02.0	10	01.7	.	.	31	01.5	17	
XI	-	03.1	08.3	03.9	04.9	09.5	01.1	21.6	11	-07.1	20	.	.	10	02.1	.	.	20	02.3	.	.	16	01.7	.	.	27	01.7	17	
XII	-	-03.4	00.8	-01.8	-01.5	01.5	-04.9	10.2	25	-14.3	03	01	02.0	18	01.6	C1	03.0	10	02.0	.	.	12	02.2	.	.	37	01.6	14	
600.	-	05.8	13.6	08.4	05.1	14.7	04.2	30.6	43.VI	-14.3	03.XII	04	01.5	191	01.6	18	02.3	251	02.1	07	01.6	128	02.0	04	01.6	311	01.7	181	
$\varphi = 45^{\circ}48' N \lambda = 15^{\circ}11' E$ Gr. $\Delta G = +1h 01$ min.																													
I	742.3	00.5	03.5	01.6	01.9	04.5	-06.7	12.2	23	-08.0	19	05	C1.4	07	02.0	18	01.8	04	01.0	16	01.4	14	01.7	21	01.6	04	01.3	04	
II	740.9	02.2	07.8	04.1	04.7	09.1	00.5	15.9	24	-11.1	04	05	01.4	05	02.0	08	01.9	02	01.0	14	02.5	21	01.9	22	02.0	03	01.3	04	
III	746.0	02.8	08.0	04.3	08.3	08.3	15.2	01.8	23.7	23	-06.2	01	04	02.0	07	01.7	12	02.5	01	01.0	23	01.6	24	01.8	19	01.7	02	02.5	01
IV	741.7	03.7	13.1	08.3	08.3	14.5	02.2	26.9	30	-03.4	17	03	02.7	08	02.0	16	02.1	C1	02.0	23	01.6	13	01.3	18	01.6	01	01.0	05	
V	742.9	10.5	18.6	13.4	13.9	20.2	08.5	26.3	04	02.0	28	07	02.0	05	01.8	11	02.2	02	02.0	18	01.5	14	01.7	28	01.6	07	01.9	01	
VI	741.7	14.4	22.5	18.2	24.5	11.9	31.1	13	01.9	02	06	01.5	09	02.1	03	02.0	15	01.5	19	01.5	15	01.7	29	01.7	05	01.4	20	01.4	
VII	741.7	15.6	23.2	18.8	19.1	25.0	13.7	30.0	12	09.3	28	02	01.5	08	01.6	13	01.3	07	01.7	23	01.6	10	01.7	21	01.4	04	01.8	05	
VIII	741.7	14.0	22.4	17.8	18.2	23.5	13.5	26.3	18	07.6	25	02	01.5	06	01.7	12	02.1	C1	01.5	14	01.7	21	01.3	06	02.0	23	01.3	04	
IX	747.2	09.0	17.5	11.6	12.6	19.1	08.2	27.7	08	-01.0	29	03	01.0	10	02.4	20	02.1	05	01.6	20	01.1	12	01.0	17	01.1	01	01.0	02	
X	747.4	07.7	16.0	10.7	11.3	17.1	07.0	23.9	08	-06.1	18	03	01.7	11	01.4	19	01.5	02	01.5	19	01.3	21	01.4	10	01.4	04	01.8	04	
XI	741.5	03.5	08.0	05.0	05.4	09.3	02.2	21.3	11	-03.8	24	05	01.0	10	01.7	13	01.8	01	01.0	16	01.3	20	01.5	06	01.7	04	01.3	03	
XII	746.6	-01.9	01.5	-00.6	-00.4	02.5	-03.3	05.8	25	-11.4	06	06	01.7	16	01.7	15	01.8	04	01.5	12	01.5	14	01.6	19	01.3	04	01.3	03	
600.	743.7	06.9	14.0	09.8	10.1	15.4	05.5	31.1	43.VI	-11.6	06.XII	55	01.6	102	01.8	162	01.9	37	01.4	218	01.5	190	01.6	245	01.5	47	01.7	39	
$\varphi = 45^{\circ}34' N \lambda = 15^{\circ}12' E$ Gr. $\Delta G = +1h 01$ min.																													
I	-	01.0	04.3	02.0	02.3	05.3	-00.5	12.6	26	-05.2	01	20	01.7	09	01.3	06	01.5	02	01.5	07	02.0	18	02.0	15	01.1	.	.	16	
II	-	00.6	05.6	03.5	03.7	05.9	01.2	16.7	23	-11.0	04	12	01.3	10	02.0	02	03.0	.	.	08	01.9	30	02.8	10	01.4	01	02.0	11	
III	-	03.9	14.9	09.4	09.4	16.0	02.6	25.2	23	-07.6	01	09	01.7	20	01.9	04	02.0	.	.	04	02.5	24	02.8	16	01.3	01	01.5	19	
IV	-	04.2	14.5	06.6	06.9	15.1	02.7	28.0	30	-02.9	17	12	01.6	13	01.8	09	01.7	06	01.5	17	01.3	21	01.1	07	02	01.5	18		
V	-	11.3	19.6	14.0	14.8	21.0	08.7	27.6	04	01.4	28	06	01.8	13	01.8	08	02.0	07	02.0	08	02.0	18	02.6	10	01.6	.	.	28	
VI	-	15.6	23.5	18.4	18.8	24.8	13.4	31.2	11	03.0	20	07	02.0	12	01.7	10	01.8	11	02.1	08	01.4	25	01.9	03	02.3	.	.	14	
VII	-	16.0	24.5	19.0	19.7	25.6	13.9	30.9	14	06.9	25	07	01.7	17	01.9	06	02.0	10	01.8	06	01.7	12	02.7	11	02.0	01	02.0	23	
VIII	-	15.0	25.8	18.2	18.2	24.7	13.6	24.8	18	07.5	25	07	01.7	13	01.7	10	01.8	06	02.0	10	01.8	09	01.8	08	02.0	26	01.8	26	
IX	-	08.9	18.5	12.6	13.2	19.8	08.0	28.6	08	-01.8	29	08	02.0	21	02.0	07	02.0	04	02.0	06	01.8	01.0	01.0	13	01.5	02	01.5	28	
X	-	08.2	16.8	11.4	12.0	17.6	07.2	25.0	08	-00.7	18	02	01.7	12	01.8	04	01.5	05	02.0	03	01.3	19	02.5	16	01.5	02	03.0	20	
XI	-	04.3	08.5	05.9	06.2	09.8	02.9	20.6	11	-04.2	24	14	01.6	15	01.9	06	01.7	03	01.0	05	01.2	20	02.6	08	01.6	03	01.7	16	
XII	-	-02.1	02.1	-00.1	-00.4	03.1	-02.9	12.6	05	-12.8	05	09	01.4	22	01.3	13	01.7	03	01.3	06	01.7	12	01.5	12	01.4	02	01.5	08	
600.	-	07.4	15.0	10.4	10.8	16.1	05.8	31.2	43.VI	-10.4	05.XII	04	01.0	325	01.6	08	01.1	103	01.5	.	.	351	01.8	20	01.4	151	01.3	123	
SR HRVATSKA																													
$\varphi = 41^{\circ}11' N \lambda = 15^{\circ}45' E$ Gr. $\Delta G = +1h 03$ min.																													
I	-	00.4	03.0	01.2	01.4	03.5	-01.2	11.2	26	-1C.2	15	01	01.0	06	01.0	28	01.6	05	01.0	01	02.0	03	01.0	08	01.3	13			
II	-	02.0	07.1	03.9	04.2	07.7	00.8	14.3	25	-10.2	03	01	01.0	12	01.6	32	01.3	03	01.3	02	01.3	05	01						

Mjesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha mm			Padavine R mm			Broj dana na sat																									
	7	14	21		7	14	21	Sred. Min	Max	Dat.	Tn	Tw	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ									
	Sred. (Dnev.)										0.0	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	0.0	•	Δ	*	Δ	Δ	Δ								
KOCJEVJE																																				
BR. ST. 36																																				
I	9.2	8.5	8.7	8.8	-	04.8	92	80	90	88	53	180	024.0	12	01	02	16	.	.	.	.	.	22	18	17	08	17	04	01	01	.	.	.	04	14	
II	9.4	8.4	6.3	7.6	-	05.1	90	71	82	77	43	156	041.2	23	02	01	13	.	.	.	.	.	16	17	14	06	15	05	.	.	.	02	07	09		
III	5.9	5.6	3.8	5.1	-	05.6	93	55	71	75	25	068	021.4	30	01	02	17	.	.	.	.	.	04	06	07	03	08	02	.	.	.	01	04	02		
IV	8.0	8.8	4.9	6.4	-	02.0	87	57	83	78	32	122	036.3	06	01	01	13	.	.	.	.	.	02	09	17	05	16	06	03	.	.	.	01	03	05	
V	7.2	7.7	6.1	7.0	-	08.7	94	59	86	75	25	138	027.1	28	01	01	08	.	.	01	.	.	02	13	17	13	05	17	.	.	.	01	03	05		
VI	4.5	2.2	4.5	5.4	-	10.8	90	61	82	77	36	077	022.3	01	01	01	04	01	.	.	.	.	05	05	14	09	03	14	.	.	.	01	10	02		
VII	5.6	6.6	4.4	5.5	-	12.0	93	60	86	80	39	160	049.3	22	01	01	13	.	.	.	.	.	05	08	18	12	06	15	.	.	.	04	04	.		
VIII	7.4	7.7	5.8	7.0	-	12.0	97	66	89	84	40	167	070.4	22	01	01	08	.	.	.	.	.	09	17	13	05	17	.	.	.	03	08	.			
GOD.	7.3	7.0	5.9	6.7	-	07.6	93	66	87	82	25	1472	072.2	44.XI	06	16	104	39	01	01	01	25	143	168	124	55	157	30	08	01	.	.	02	30	76	45
NOVO MESTO																											$H_s = 220 \text{ m } H_b = 212.6 \text{ m } h_t = 2.2 \text{ m } h_r = 1.5 \text{ m}$									
BR. ST. 37																											.									
I	9.6	8.7	8.0	8.8	027.5	05.0	96	87	93	65	085	019.0	14	01	02	18	.	.	.	.	.	23	18	12	03	16	03	01	.	02	.	.	12	21		
II	8.6	7.8	6.8	7.7	074.9	05.3	91	70	86	82	38	076	029.7	01	01	01	14	.	.	02	.	15	14	10	02	13	03	.	.	.	04	09	.			
III	6.7	7.0	4.1	5.9	181.1	06.1	95	53	76	74	34	040	010.7	30	01	08	.	.	02	.	02	08	09	07	01	09	04	02	.	.	01	03	02			
IV	7.3	7.3	4.3	6.3	180.9	05.9	93	54	74	74	31	115	032.4	09	01	01	10	02	.	01	01	09	12	08	05	12	03	02	.	02	01					
V	6.2	7.0	6.1	6.4	201.5	08.8	91	54	80	75	24	023	008.6	23	01	01	05	.	.	.	02	11	14	07	07	14	.	.	.	07	03	.				
VI	5.0	6.3	4.7	5.3	268.7	10.9	86	52	73	71	36	062	014.3	16	01	01	17	01	.	.	05	07	10	07	03	10	.	.	.	12	.					
VII	5.1	5.8	5.4	5.5	260.5	12.2	50	57	80	76	25	172	065.2	01	01	01	17	01	.	02	03	06	15	12	05	14	.	.	07	01						
VIII	6.3	7.0	5.6	6.3	200.8	12.7	52	76	82	80	40	149	040.4	22	01	01	10	.	.	03	16	15	11	04	15	.	.	.	01	08	04					
GOD.	7.0	7.0	5.8	6.6	1829.4	07.9	93	64	85	81	24	1110	065.6	44.XI	03	13	88	57	02	01	08	33	145	157	107	35	146	21	09	01	06	02	01	42	76	45
CRACPELJ																											$H_s = 156 \text{ m } H_b = 2.0 \text{ m } h_t = 1.5 \text{ m}$									
BR. ST. 38																											.									
I	9.3	8.7	7.4	8.5	-	04.9	93	84	91	89	54	112	022.7	14	01	02	19	.	.	.	.	18	21	14	05	17	04	01	.	02	.	01	15	15		
II	8.4	7.1	7.4	8.6	-	05.5	90	68	85	74	42	001	021.4	08	02	01	14	.	.	03	.	05	17	18	11	02	16	03	01	.	.	01	05	09		
III	6.3	5.3	4.0	5.3	-	05.2	87	53	69	70	29	097	020.1	30	01	09	02	.	.	05	07	10	07	03	10	04	01	.	.	02	06	02				
IV	7.0	6.5	4.3	5.9	-	05.9	88	52	71	70	24	136	033.4	08	01	09	03	.	.	.	03	08	13	01	06	12	06	02	.	.	01	03	02			
V	5.1	6.9	5.2	5.8	-	09.0	86	53	77	72	28	084	022.5	28	01	01	06	.	.	.	04	05	14	10	03	14	.	.	.	08	01	.				
VI	4.0	5.7	4.9	4.9	-	11.1	81	53	72	69	33	079	030.8	01	01	01	14	03	.	.	08	05	12	10	02	12	02	.	.	01	11	.				
VII	4.6	4.9	4.5	4.7	-	12.7	68	57	79	75	32	144	035.6	12	01	01	20	03	.	01	09	07	15	12	04	15	.	.	01	04	.					
VIII	5.6	6.7	5.0	5.8	-	12.5	93	61	84	79	41	052	016.2	23	01	01	18	.	.	.	03	08	15	10	03	15	.	.	.	07	04	.				
IX	5.3	5.9	5.1	5.4	-	09.2	94	60	87	80	39	094	035.4	18	01	01	08	.	.	01	07	08	11	09	04	11	.	.	.	01	05	.				
X	7.3	7.0	6.4	6.0	-	08.7	94	67	87	82	37	092	035.6	02	01	01	12	01	.	01	05	11	14	06	03	10	.	.	.	02	17	.				
XI	8.6	8.2	8.2	8.4	-	08.4	92	79	86	87	38	200	051.0	14	01	01	12	01	.	.	01	09	19	21	10	06	17	02	01	.	01	03	14	81		
XII	9.0	8.6	8.3	7.6	8.3	-	04.0	90	80	80	87	30	061	014.4	29	02	09	25	.	.	.	02	21	18	08	04	11	06	03	.	.	03	12	07		
GOD.	6.7	6.7	5.7	6.4	-	08.0	89	63	81	78	24	1249	051.0	44.XI	04	11	90	75	06	.	05	49	139	183	117	45	160	26	05	05	.	03	03	43	83	36
GORNJI LENART																											$H_s = 150 \text{ m } H_b = 2.0 \text{ m } h_t = 1.5 \text{ m}$									
BR. ST. 39																											.									
I	9.1	8.4	6.9	8.1	-	04.9	93	65	54	51	59	081	023.6	14	01	01	20	.	.	.	01	19	16	09	03	14	03	.	.	.	.	06	.			
II	7.6	6.9	5.5	6.8	-	05.4</td																														

Mesec	Vazdušni Prstenski Fm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, Fm (0-12)																			
		Tm			Sred. (Dles.)	Max	Min	Max	Min	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21																									
$\varphi = 46^{\circ}18' N \lambda = 16^{\circ}23' E$ Gr. $\Delta G = + 1h 05 min.$																													
I	747.0	00.1	03.1	06.9	01.3	04.4	-02.0	13.3	30	-13.0	19	17	02.2	11	02.4	12	02.5	03	01.7	21	03.1	11	02.7	12	02.1	03	01.7	03	
II	745.5	02.0	07.9	03.6	04.6	09.1	00.3	16.4	25.2	-16.4	04.03	08	02.0	04	02.0	10	03.3	15	02.7	21	03.2	18	02.3	05	02.0	.	.	.	
III	745.7	03.7	14.2	07.6	08.2	15.2	02.1	24.0	24	-05.1	02	13	03.0	14	01.7	09	02.3	02	02.0	21	02.7	23	02.5	13	02.1	02	01.5	04	
IV	745.2	05.6	13.0	08.1	08.7	14.0	03.3	26.7	30	-02.4	21	19	02.4	09	02.9	14	01.9	03	02.3	12	02.8	15	02.5	12	01.7	03	02.3	03	
V	746.7	12.9	20.0	13.9	15.2	21.0	08.4	28.1	20	01.1	28	12	02.3	11	02.9	13	01.5	02	01.5	12	02.3	18	02.7	16	02.0	07	02.0	02	
VI	745.2	17.5	24.6	17.8	19.4	25.6	12.5	32.6	14	04.6	03	21	02.1	06	02.5	04	01.8	02	01.0	17	02.5	19	02.7	12	02.8	10	01.9	.	
VII	745.4	17.6	23.9	18.5	20.6	25.3	14.0	29.6	08	07.9	27	12	02.8	05	02.6	07	01.3	02	01.5	12	02.3	13	02.6	15	01.7	08	01.9	09	
VIII	745.5	16.1	23.4	17.4	18.6	24.4	13.6	28.6	06	08.2	25	10	02.1	12	01.8	07	01.2	01	01.5	11	02.3	16	02.2	16	01.8	11	02.1	08	
IX	751.1	10.2	18.3	11.4	12.8	19.4	07.5	29.1	08	-03.1	29	14	02.4	08	02.5	12	01.1	04	01.8	14	02.4	11	01.9	21	01.5	02	02.0	04	
X	751.1	07.6	15.7	10.2	10.9	16.6	06.2	23.7	07	-01.0	03	15	02.1	07	01.6	09	01.9	03	01.7	15	03.3	15	01.8	07	01.7	07	.		
XI	752.2	04.6	09.2	05.1	05.9	10.7	02.3	20.9	11	-05.2	20	13	02.7	06	02.3	12	02.1	01	02.0	23	02.8	20	02.6	09	02.2	04	02.8	02	
XII	752.5	-01.5	01.4	-00.7	-00.3	02.4	-03.3	10.6	25	-09.7	05	14	02.6	07	02.6	08	02.1	07	01.9	29	02.4	13	02.1	11	02.2	03	02.0	01	
GOD.	747.4	08.0	14.6	09.5	10.4	15.7	05.4	32.6	4.6V	-16.4	04.09	168	02.4	92	02.3	117	02.0	34	01.7	212	02.6	194	02.6	170	02.0	65	02.0	43	
$\varphi = 46^{\circ}02' N \lambda = 16^{\circ}33' E$ Gr. $\Delta G = + 1h 07 min.$																													
I	749.2	00.5	03.3	01.5	01.7	04.3	-01.1	13.0	26.2	-23	-11.6	01	07	02.9	30	03.0	07	02.0	06	02.2	05	02.2	17	02.1	07	02.0	14	02.0	.
II	746.7	02.0	07.7	04.2	04.5	08.8	00.6	16.0	21.2	-20	-12.5	03	11	02.9	15	02.5	04	02.0	05	02.2	10	02.5	20	03.2	04	02.0	15	02.3	.
III	751.1	04.1	13.7	08.5	08.7	14.9	02.5	24.0	24	-04.7	01	20	02.8	23	02.4	05	02.2	09	02.1	04	02.0	13	02.4	06	02.0	13	02.2	.	
IV	747.5	05.6	12.9	08.1	08.7	14.0	03.2	27.0	30	-02.2	12	14	02.6	21	03.1	03	02.3	12	02.2	12	02.1	11	02.5	03	02.3	14	02.6	.	
V	748.6	12.7	19.9	14.0	15.2	21.1	08.8	27.2	20.0	04	01.0	28	16	02.5	23	03.1	04	02.2	02	02.0	15	02.4	15	02.3	05	02.0	13	01.9	.
VI	747.1	16.6	24.0	17.8	19.0	24.8	12.2	31.0	13	02.3	02	16	03.2	18	02.9	05	02.5	05	01.6	09	02.8	20	02.8	02	02.0	18	02.3	.	
VII	747.3	17.4	25.7	17.9	18.4	24.9	13.4	29.1	03	08.0	28.27	09	03	02.0	23	02.5	05	02.2	09	02.1	08	01.9	18	02.3	01	02.0	20	02.2	.
VIII	747.3	16.0	24.0	17.8	18.9	25.1	13.5	29.0	09.6	07.8	29	09	02.7	31	02.3	02	02.2	02	02.1	14	02.1	03	02.3	20	02.3	.	.	.	
IX	752.6	10.1	18.3	11.9	13.0	19.5	07.8	28.2	08	-02.0	29	15	03.1	32	02.6	05	02.4	06	01.7	08	02.0	11	02.2	04	02.0	09	02.2	.	
X	753.2	07.1	15.6	10.0	10.7	16.6	05.9	23.7	08	-01.0	03	17	02.4	18	02.4	05	02.0	04	02.0	23	02.7	16	03.1	02	02.0	13	02.1	.	
XI	752.4	-0.4	08.0	05.7	05.9	09.5	02.5	19.6	04	-04.8	30	23	02.9	07	03.1	04	03.4	04	03.2	15	02.9	21	02.5	05	02.8	08	02.6	.	
XII	754.7	-01.6	00.6	-00.9	-00.7	01.4	-03.2	10.0	25	-10.2	05	19	03.6	11	02.8	09	02.8	04	02.0	18	02.4	16	02.1	07	02.1	09	02.6	.	
GOD.	749.5	07.8	14.3	09.7	10.4	15.4	05.5	31.0	4.6V	-12.5	08	176	02.9	252	02.7	58	02.5	68	02.0	134	02.4	192	02.5	49	02.1	166	02.2	.	
$\varphi = 46^{\circ}11' N \lambda = 16^{\circ}49' E$ Gr. $\Delta G = + 1h 07 min.$																													
I	-	00.3	03.5	01.1	11.5	04.3	-14.1	14.2	30	-08.4	19	04	02.2	28	01.6	07	02.0	13	01.8	05	02.2	22	02.0	04	02.0	10	01.4	.	
II	-	02.3	08.5	04.6	05.0	09.4	01.5	17.3	24	-15.2	03	06	01.3	13	01.7	0.	07	02.9	14	02.1	34	02.3	05	02.6	05	01.0	.		
III	-	06.8	14.6	08.3	09.8	15.4	03.9	22.5	24	-02.6	01	08	02.0	14	02.2	03	01.3	08	02.0	10	01.5	29	02.1	03	02.0	10	01.3	.	
IV	-	08.2	13.6	08.4	09.2	14.8	04.6	26.1	30	-01.1	12	10	02.0	18	02.1	04	01.5	08	01.4	10	01.8	23	02.0	05	02.2	12	02.2	.	
V	-	13.3	21.4	14.2	15.8	22.2	10.2	30.0	04	04.8	29	08	02.2	20	02.0	06	02.0	02	01.5	12	01.9	28	02.4	06	02.3	11	01.8	.	
VI	-	17.4	25.1	17.5	19.4	26.0	12.7	32.4	13	02.0	02	09	02.9	11	02.3	01	01	07	01.6	17	02.6	31	02.6	04	02.5	18	02.0	.	
VII	-	17.4	24.9	18.1	19.6	25.9	14.6	30.1	13	09.0	26	07	02.4	15	01.6	02	01.0	10	01.5	17	02.0	23	02.0	10	01.6	09	01.7	.	
VIII	-	16.4	24.9	17.6	19.3	25.7	14.4	30.1	05	09.8	25	07	02.3	18	02.2	04	01.8	04	01.5	18	02.5	25	01.9	02	02.5	19	01.8	.	
IX	-	10.7	19.1	11.6	13.2	20.0	08.3	29.5	08	-01.1	29	10	01.4	17	01.7	08	02.6	04	01.5	15	01.4	21	01.9	02	02.0	13	01.2	.	
X	-	07.3	16.3	09.6	10.7	16.8	06.3	24.9	08	00.5	18	03	11	01.0	01	03	21	02.4	08	01.2	20	02.0	29	02.4	06	01.7	07	01.3	.
XI	-	04.4	09.0	05.7	06.2	10.1	03.3	19.8	04	-04.8	30	03	01.0	13	02.1	03	02.3	10	02.0	16	02.1	35	02.3	01	01.0	09	01.6	.	
XII	-	-01.6	01.0	-00.5	-00.6	01.8	-02.2	10.8	25	-08.9	06	16	01.8	10	01.6	06	01.7	11	01.5	18	01.6	20	02.0	02	01.5	10	01.6	.	
GOD.	-	08.2	15.2	09.7	10.7	16.0	06.5	32.4	4.6V	-13.2	08	98	01.9	187	01.9	45	01.9	86	01.7	176	01.9	320	02.2	50	02.0	133	01.6	.	
$\varphi = 45^{\circ}14' N \lambda = 13^{\circ}36' E$ Gr. $\Delta G = + 55 min.$																													

Meseč	Oblačnost Nm (0-10)			Vlažnost vazduha em mm	Padavine R mm Σ 7 14 21 Sred. (Des) Min	Vlažnost vazduha U m %		Broj dana na sa:													
	7	14	21			7	14	21	Sred. (Des) Min	Σ	Max	Dat.	=	<	<	=	=	•	*		
	30.00.0	0.0250	30.020.0			6	8	2.0	8.0	0.1	1.0	0.0	05	04	03	02	01	00	01		
<b>VARAŽDIN</b>																					
BR. ST. 41																					
II 8.8 6.2 7.1 8.0	056.0	04.5	89 83 90 87 43	088 019.8	14	02	03	20	.	.	.	04	.	18	12	09	03	12	04	02	
III 6.1 7.0 5.0 6.3	089.4	05.3	90 83 81 42	065 014.7	13	03	02	10	.	.	.	08	03	13	13	10	02	10	04	01	
IV 7.3 7.2 6.1 6.9	195.1	06.0	88 53 76 73 26	044 013.1	14	.	.	11	.	.	.	04	04	09	09	05	03	03	02	04	
V 6.4 7.3 6.1 6.5	171.8	06.1	81 51 77 71 29	072 025.6	09	.	.	08	02	.	.	05	04	14	12	09	02	12	02	01	
VI 6.4 7.3 6.5 7.0	220.9	08.7	77 50 73 67 30	012 005.4	15	.	.	07	.	.	03	.	04	12	11	03	11	.	.	04	
VII 4.5 5.2 5.2 5.0	274.9	10.6	69 45 71 62 31	037 013.5	22	.	.	17	07	.	06	06	08	06	01	08	03	05	02		
VIII 5.5 5.8 5.7 5.7	265.3	12.1	88 56 77 71 38	108 030.2	16	.	.	18	.	.	03	01	04	03	10	08	05	10	.		
IX 5.5 5.8 5.7 5.7	215.3	12.6	88 59 87 78 37	076 018.9	01	.	.	14	.	.	04	.	05	07	15	11	01	15	.		
X 5.5 5.8 5.4 5.5	131.0	08.3	94 65 89 84 47	022 011.3	20	.	.	03	.	.	05	01	06	09	10	03	01	05	02		
XI 7.0 6.5 6.7 7.1	098.6	06.1	98 74 88 84 42	089 049.3	14	.	.	07	.	.	04	32	03	16	17	07	01	16	04		
XII 8.2 7.7 6.6 7.5	050.2	04.0	89 82 89 87 42	051 016.0	07	.	09	25	.	.	05	01	01	17	12	09	01	09	06		
GOD. 6.7 6.8 5.8 6.4	1962.1	07.6	85 62 82 76 26	720 049.3	44.ii	05	14	85	66	07	.	52	08	41	130	137	87	22	124		
<b>KRIZEVCI</b>																					
BR. ST. 42																					
I 9.1 6.2 8.2 8.5	041.3	04.6	90 82 89 87 56	093 027.5	03	01	02	18	.	.	04	.	21	17	11	02	12	03	01	07	
II 8.5 7.2 7.1 7.6	084.4	05.3	90 70 83 81 43	057 012.7	13	01	03	12	.	.	08	01	13	08	01	10	03	01	01	05	
III 4.5 4.0 3.8 4.1	200.6	06.0	88 54 72 71 32	043 017.7	13	.	.	07	.	.	04	08	06	06	02	04	03	01	07	03	
IV 7.6 6.2 5.4 6.4	162.8	06.1	83 55 76 71 20	055 025.2	09	.	.	06	02	.	05	04	13	11	09	01	11	01	02	01	
V 5.5 5.7 4.6 5.0	219.3	08.9	81 50 75 68 28	021 010.5	07	.	.	05	.	.	02	.	06	06	08	04	01	06	02	04	
VI 4.2 4.2 4.9 4.6	267.7	10.9	76 46 73 65 34	056 030.2	23	.	.	16	03	01	06	01	07	03	09	05	02	09	06		
VII 5.5 5.0 5.5 5.0	257.0	12.3	83 54 74 71 41	092 025.0	05	.	.	17	.	.	10	01	07	04	12	03	14	08	01		
VIII 6.0 6.8 6.3 6.7	214.5	12.5	89 56 74 72 43	031 016.1	15	.	.	17	.	.	06	02	04	06	13	01	06	02	06		
GOD. 6.8 5.8 6.0 6.2	1869.2	07.8	87 62 82 77 28	782 045.0	44.ii	03	18	82	66	03	01	55	05	48	125	146	91	26	120		
<b>KOPRIVNIKA</b>																					
BR. ST. 43																					
I 9.0 7.6 8.3 8.3	-	04.4	86 79 87 84 40	078 024.2	03	.	01	21	.	.	01	22	16	11	02	14	03	01	14	25	
II 8.1 7.5 5.9 5.2	-	05.4	85 68 81 78 39	079 022.1	01	02	03	08	.	.	01	01	12	10	02	09	03	02	12	08	
III 4.7 6.2 4.3 5.1	-	05.5	85 51 71 59 20	062 022.2	31	.	.	05	01	.	02	05	02	05	02	07	02	01	07	02	
IV 7.2 6.8 5.6 6.5	-	06.2	80 56 74 70 24	036 028.3	09	.	.	03	02	.	02	11	11	07	01	10	.	04	01		
V 5.0 6.3 5.1 5.5	-	08.8	77 46 73 65 25	013 004.6	17	.	.	08	01	.	03	10	08	04	06	08	04	01	.		
VI 4.0 6.0 4.3 4.8	-	11.1	74 45 74 64 -	038 014.2	23	.	.	16	07	01	01	03	02	07	05	02	07	01	.		
VII 5.7 5.8 4.8 5.4	-	12.3	84 51 72 32	092 029.2	01	.	.	22	01	01	02	05	15	08	04	15	.	03	01		
VIII 6.1 5.6 5.0 5.6	-	12.5	83 53 74 72 32	044 017.6	13	.	.	23	01	.	01	06	13	08	02	13	.	02	06		
IX 3.7 4.6 3.7 4.0	-	08.5	89 54 65 76 29	068 016.5	10	.	.	01	09	.	09	03	09	07	04	05	06	.	06		
X 7.0 5.1 5.6 5.9	-	08.2	92 67 89 83 40	034 025.5	02	.	.	02	.	.	01	05	11	05	04	01	05	02	22		
XI 6.0 7.2 6.6 7.3	-	06.1	88 74 86 83 46	145 053.1	14	.	01	05	.	.	01	12	17	10	05	17	02	01	09	04	
XII 7.7 8.1 7.7 7.8	-	03.7	80 79 81 80 47	033 006.6	29	.	10	24	.	.	01	19	11	09	09	05	02	.	10	13	
GOD. 6.4 6.4 5.6 6.1	-	07.8	83 60 80 74 -	742 053.1	44.ii	02	15	67	83	10	02	02	.	31	116	132	88	25	123		
<b>PCREČ</b>																					
BR. ST. 44																					
I 8.3 7.8 7.7 7.9	-	06.7	87 80 87 85 36	119 019.8	15	.	.	05	.	.	04	20	17	15	06	17	.	.	08		
II 7.1 6.1 7.0 6.7	-	06.8	86 74 86 82 31	081 016.5	12	.	.	05	.	.	04	13	13	10	03	13	.	.	03		
III 6.4 5.6 4.9 5.6	-	07.5	80 70 84 80 49	032 016.0	31	.	.	01	.	.	03	09	07	05	01	07	01	01	03		
IV 5.0 5.3 4.3 4.8	-	07.0	76 58 77 71 36	068 018.4	09	.	.	02	.	.	06	08	06	06	05	06	.	01	.		
V 5.2 4.5 4.5 4.9	-	10.3	80 65 81 75 44	052 014.5	09	.	.	01	.	.	06	06	12	09	01	12	.	02	.		
VI 3.7 3.5 3.5 4.1	-	12.6	72 61 75 63 43	016 012.5	27	.	.	15	.	.	01	11	04	07	03	01	07	.	02		
VII 3.7 2.9 2.9 3.5	-	14.9	74 64 80 73 44	107 025.3	08	.	.	27	02	.	13	02	10	10	05	10	.	01	06		
VIII 4.2 4.0 4.2 4.2	-	14.9	81 67 75 74 36	158 051.3	11	.	.	17	03	01	09	66	14	10	04	14	.	01	07		
IX 3.3 3.6 3.5 3.5	-	10.6	81 64 78 74 46	060 037.8	16	.	.	06	.	.	10	04	07	06	01	07	.	02	.		
X 5.0 4.8 4.9 5.1	-	10.5	87 74 89 83 54	023 004.2	12	.	.	05	.	.	09	05	04	04	01	05	.	01	08		
XI 6.8 7.2 6.9 7.0	-	07.8	84 71 86 80 36	066 028.4	02	.	.	02	.	.	02	14	06	05	03	04	.	01	04		
XII 5.0 5.1 3.4 3.5	-	05.4	80 68 81 77 40	059 020.8	07	.	.	16	.	.	11	08	07	06	02	07	.	.	.		
GOD. 5.4 5.0 5.1 5.2	-	09.6	81 68 82 77 31	841 051.3	MVm	.	.	31	64	03	03	03	.	88	102	111	89	32	111		
<b>PCVINJ</b>																					
BR. ST. 45																					
BR. ST. 45																					
I 6.3 7.6 8.1 8.0	066.4	J7.2	88 85 83 89 87 30	127 034.5	02	.	.	05	.	.	02	05	22	16	16	04	16	.	.	01	02
II 6.5 5.5 6.2 6.3</																					

Mjesec	Vazdušni pritisak Pn mm	Temperatura vazduha °C								Cestine pravaca i srednja jačina veta nD, Pm (0-12)																							
		Tm				Dat.				N						NE			E		SE			S		SW			W		NW		
		7	14	21	Sred. (Dnev.)	Max	Min	Max	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.				
$\varphi = 45^{\circ} 14' N \lambda = 13^{\circ} 56' E$ Gr. $\Delta G = + 56$ min.																																	
I	735.0	04.0	08.4	05.0	05.6	09.3	01.9	14.1	24 - 08.0	19	03	01.3	02	02.0	10	02.0	14	02.5	15	02.1	06	01.8	03	02.0	.	.	40						
II	732.4	03.9	10.2	05.6	06.3	11.1	02.2	14.5	11 - 07.0	03	.	.	06	01.7	04	01.8	05	02.6	16	02.2	14	02.7	04	02.5	.	.	35						
III	738.6	04.1	14.3	07.6	08.5	15.0	02.2	26.5	25 - 05.9	01	.	.	02	01.5	08	02.1	11	02.7	13	02.4	07	02.3	07	02.0	.	.	45						
IV	734.1	05.1	14.9	07.6	08.9	16.0	02.2	21.5	29 - 07.0	17	02	02.0	04	02.0	14	02.5	15	02.2	16	02.8	04	02.8	02	03.0	31								
V	735.3	10.7	20.2	13.7	14.5	21.4	07.8	26.7	25 02.0	06	01	01.0	03	02.0	09	02.3	14	02.5	10	02.6	07	02.9	09	02.3	01	05.0	39						
VI	734.8	14.0	23.5	16.8	17.8	25.2	11.0	31.7	15 03.0	02	04	01.8	01	03.0	09	02.2	09	02.6	08	02.8	09	02.6	07	02.7	04	01.2	41						
VII	734.2	15.8	25.7	19.0	19.5	27.0	15.5	32.7	13 09.5	28	.	.	05	01.8	06	02.6	02	04.0	12	02.7	13	08	03.5	11	02.5	04	02.2	43					
VIII	734.3	14.9	24.5	16.0	18.6	26.1	13.0	30.7	07 09.0	25	.	.	03	02.0	04	02.8	08	02.1	13	02.4	13	02.5	04	02.2	.	.	48						
IX	738.9	08.5	21.8	11.9	13.5	22.7	07.0	30.3	08 - 02.0	25	02	02.0	08	02.0	05	02.4	05	02.4	02	02.5	03	02.3	06	01.7	01	03.0	55						
X	739.8	08.3	18.3	12.0	19.3	26.7	10.8	25.8	23 - 04.0	04	01	02.0	03	01.3	07	01.4	10	02.4	09	03.3	06	02.3	04	01.8	01	02.0	52						
XI	739.3	05.8	12.0	06.5	07.7	13.3	02.8	19.7	11 - 06.2	20	03	01.3	05	02.8	11	02.2	05	02.6	10	02.5	10	02.1	04	01.8	02	01.5	40						
XII	739.2	-00.1	09.3	01.4	03.0	10.5	-02.6	14.7	19.15 - 08.2	22	04	02.0	12	01.6	11	01.7	06	02.5	10	02.1	04	01.8	04	02.0	03	02.0	39						
GOD.	736.0	07.9	16.9	10.4	11.4	16.1	05.6	32.7	03.vi - 08.2	22.xi	20	01.7	54	01.9	99	02.1	103	02.6	131	02.4	55	02.5	67	02.2	18	02.1	508						
$\varphi = 45^{\circ} 20' N \lambda = 14^{\circ} 27' E$ Gr. $\Delta G = + 58$ min.																																	
RIJEKA																																	
BR. ST. 47																																	
I	751.0	07.0	09.1	07.4	07.7	10.2	05.2	14.9	24 - 01.6	19	02	02.0	23	02.1	01	02.0	08	02.8	08	02.9	06	02.0	03	02.0	01	02.0	41						
II	750.3	07.3	10.5	08.0	08.4	11.4	06.0	16.3	23 - 06.6	03	02	03.0	22	02.1	02	02.4	10	02.7	07	01.7	02	01.5	01	01.0	.	.	31						
III	755.5	08.6	13.7	10.5	10.8	14.8	07.3	23.4	23 - 01.0	01	.	.	25	02.7	02	02.5	03	01.7	04	02.5	08	01.4	03	02.0	.	.	48						
IV	750.6	08.9	14.6	10.8	11.2	15.7	06.9	23.4	30 01.9	12	03	04.0	34	02.6	04	02.0	03	01.7	07	01.7	08	01.8	01	02.0	02	01.5	28						
V	751.8	15.0	19.6	15.8	16.6	21.1	12.3	25.6	19.04 08.4	06	.	.	36	02.7	03	03.3	02	01.5	05	02.6	15	01.7	04	01.8	.	.	28						
VI	751.0	18.3	23.1	19.0	19.4	24.4	15.6	30.3	18 10.0	03	01	03.0	25	02.6	01	01.0	04	02.2	06	01.7	14	01.7	05	02.4	02	01.5	32						
VII	750.4	20.0	25.0	21.4	22.0	26.3	17.6	29.8	13 13.4	27	04	02.5	32	02.9	.	04	02.0	04	01.8	18	01.7	03	02.0	01	01.0	27							
VIII	750.4	19.0	24.5	20.5	21.1	25.8	17.3	30.4	08 13.1	25	06	02.5	31	02.0	04	02.7	03	01.7	07	01.7	16	01.8	05	01.8	.	.	25						
IX	755.2	14.1	20.7	16.2	16.8	21.9	12.8	29.8	06 04.8	23	03	01.7	48	03.1	04	03.2	02	01.5	05	02.6	15	01.7	04	01.8	.	.	15						
X	756.3	12.9	18.1	14.3	14.7	19.1	11.4	25.1	09 06.3	02	03	01.6	30	02.2	03	04	03.4	04	02.0	11	01.3	03	01.0	.	.	37							
XI	756.4	08.4	12.2	09.3	09.0	15.0	06.2	17.6	07 01.8	23	04	02.2	40	02.9	03	04.4	04	02.8	07	02.0	01	01.0	01	02.0	23								
XII	754.7	04.0	09.1	05.4	06.2	10.1	02.8	14.4	19 03.5	13	06	02.0	34	02.6	09	02.2	02	02.0	06	02.3	10	01.5	.	.	03	02.3	23						
GOD.	752.4	12.0	16.7	13.2	13.8	17.8	10.2	30.4	06.vii - 03.5	13.xi	36	02.4	380	02.6	35	02.8	48	02.4	61	02.3	131	01.7	33	01.8	13	01.8	358						
$\varphi = 45^{\circ} 36' N \lambda = 14^{\circ} 38' E$ Gr. $\Delta G = + 59$ min.																																	
PARG																																	
BR. ST. 48																																	
I	686.1	01.2	02.2	00.1	02.6	05.4	25 - 08.0	02	00.2	20	02	01.0	05	01.8	02	01.0	38	01.5	21	02.0	20	02.7	01	01.0	04	02.0	.	.					
II	685.2	01.3	03.8	01.7	02.1	05.5	-01.1	10.3	24 - 10.5	03	01	01.0	01	02.0	03	01.0	27	01.7	22	01.8	24	02.6	.	.	06	02.0	.	.					
III	690.4	03.2	09.4	04.9	05.6	11.0	00.0	21.2	25 - 08.5	01	04	01.5	02	02.0	01	02.0	41	01.8	20	01.8	18	02.6	01	02.0	06	01.0	01.0	01.0					
IV	686.2	02.2	08.5	04.6	05.6	10.4	00.0	20.0	02.4 - 03.4	02	03	01.0	06	02.0	03	01.5	33	01.5	19	01.7	23	01.0	02.3	01	02.4	01	01.0	01	01.0				
V	688.1	09.2	13.8	09.4	10.4	15.8	05.0	23.3	04 - 00.4	28	01	02.0	02	01.5	02	01.0	49	01.7	23	01.8	10	03.0	.	.	05	01.8	01	01.0					
VI	687.0	12.9	17.3	13.1	14.1	19.5	08.8	28.0	13 02.2	04	03	01.3	06	01.7	03	02.0	39	01.6	23	01.9	11	02.5	.	.	07	02.3	.	.					
VII	688.2	13.9	19.0	14.5	15.5	21.1	10.3	26.5	13 05.8	28	03	01.3	04	01.8	06	01.5	46	01.6	23	01.8	09	03.1	.	.	08	01.9	.	.					
VIII	688.3	13.2	18.4	14.0	14.9	20.2	10.4	23.6	17 05.5	23	01	01.0	06	02.0	47	01.6	21	01.6	14	02.1	03	01.0	03	01.0	03	01.0	03	01.0					
IX	692.1	07.7	14.6	09.1	10.1	16																											

Mjesec	Oblačnost Nm (0-10)	Vlažnost vazduha %	Padavine R mm	Broj dana na sat																															
				Insolacija Broj sati				Tn Tx Tn Tx Tx				Tn F(0-12) Nm(0-10)				R mm				•	*	*	Δ	Δ	Δ	R	T	≡	□						
				7	14	21	Sred. (Dnev.)	mm	7	14	21	Sred. (Dnev.)	Min	M	Max	Dat.	mm	0.00.0	0.0250	0.0200	6	8	2.0	8.0	0.1	1.010.0	•	*	*	Δ	Δ	Δ	R	T	≡
PAZIN																																			
BR. ST. 46																																			
I 8.5 6.0 7.8 8.1	-	06.3 95 79 93 89 38	155 025.6	27	.	.	09	.	.	.	.	.	.	03	22	16	15	06	16	01	01	.	.	.	.	.	16	01							
II 7.5 6.5 6.8 7.3	-	06.3 95 67 91 84 28	114 026.3	22	.	.	10	.	.	.	.	.	.	04	17	12	10	05	12	.	.	.	.	.	.	.	09	.							
III 6.9 7.2 5.5 6.4	-	06.5 94 58 84 78 22	029 012.4	31	.	.	09	01	.	.	.	.	.	02	10	08	05	01	08	01	01	.	01	.	.	.	08	01							
IV 5.9 6.5 4.6 5.7	-	06.3 88 53 80 73 28	099 029.3	09	.	.	11	.	.	.	.	.	.	04	08	09	07	04	09	01	01	.	.	.	.	.	.	.	.						
V 6.2 6.3 4.5 5.7	-	09.5 93 56 81 76 39	063 013.1	16	.	.	04	.	.	.	.	.	.	05	10	12	08	02	12	.	.	.	.	.	.	02	02								
VI 4.8 5.8 4.6 5.1	-	11.3 92 54 78 74 32	086 049.8	27	.	.	16	03	.	.	.	.	.	02	06	11	08	02	11	.	.	.	.	.	.	04	01								
VII 4.3 5.6 4.4 4.8	-	13.2 92 56 81 77 41	119 022.4	10	.	.	24	03	.	.	.	.	.	07	05	13	11	05	13	.	.	.	.	.	.	11	01								
VIII 5.4 6.7 4.4 5.5	-	13.4 95 63 88 82 42	182 045.0	23	.	.	19	03	.	.	.	.	.	05	07	18	12	06	18	.	.	.	01	.	01	11	09								
IX 4.0 4.9 2.8 3.9	-	09.1 95 51 87 78 36	053 038.0	18	.	.	01	12	01	.	.	.	.	09	03	09	07	01	09	.	.	.	.	.	.	02	01								
X 6.8 6.4 5.2 6.2	-	09.1 96 66 93 85 36	040 014.6	11	.	.	01	01	.	.	.	.	.	06	12	07	05	02	10	.	.	.	.	.	.	02	11								
XI 7.8 6.8 6.4 6.9	-	06.9 89 67 88 82 28	083 023.5	22	.	.	11	.	.	.	.	.	.	02	10	10	07	03	10	.	.	.	.	.	.	01	02	18							
XII 5.1 4.9 3.4 4.5	-	04.4 89 55 84 76 15	080 029.0	29	.	.	26	.	.	.	.	.	.	01	09	07	07	03	07	.	.	.	.	.	.	04	.								
GOD. 6.1 6.4 5.0 5.8	-	06.5 92 60 85 79 15	1103 045.0	23.VIII	.	.	78	77	10	.	.	01	.	58	117	132	102	40	131	03	03	.	01	01	02	34	68	02							
RIJEKA																																			
BR. ST. 47																																			
I 8.3 8.1 7.6 8.0	062.4	046.2	80 72 78 77 32	353 099.4	03	.	01	.	.	.	.	.	.	01	01	04	22	21	17	07	21	.	.	.	.	.	01	01							
II 7.9 8.3 6.8 7.7	078.1	063.3	76 76 73 14	185 036.2	22	.	01	.	.	.	.	.	.	01	17	16	14	07	16	.	.	.	.	.	.	02	.								
III 7.9 8.5 5.1 6.8	150.9	06.4	71 57 68 65 25	040 012.4	29	.	01	.	.	.	.	.	.	03	02	01	13	08	06	01	08	01	.	.	.	02	.								
IV 6.8 6.6 4.7 6.0	197.1	06.0	65 48 64 59 24	088 036.4	09	.	.	.	.	.	.	.	.	03	01	04	11	09	06	03	09	.	.	.	.	.	02	.							
V 6.7 6.6 5.0 6.1	231.0	09.1	70 54 68 64 27	096 021.2	16	.	02	.	.	.	.	.	.	06	10	15	09	05	15	.	.	.	.	.	.	04	.								
VI 5.5 4.9 5.6 5.6	256.4	113.3	69 53 69 64 34	029 008.5	27	.	14	02	.	.	.	.	.	04	01	03	06	10	07	10	.	.	.	.	.	06	.								
VII 4.4 5.7 4.3 4.6	274.5	12.2	68 66 62 32	135 025.2	01	.	23	01	.	.	.	.	.	02	04	02	08	06	11	10	07	11	.	.	.	07	.								
VIII 5.1 5.9 4.4 5.2	232.9	12.5	74 55 72 67 35	180 060.4	22	.	20	03	02	01	01	05	11	17	13	06	17	.	.	.	.	.	.	.	11	.									
IX 4.4 4.6 3.3 4.1	227.3	08.9	69 50 63 20	049 021.1	10	.	10	.	.	.	.	.	09	03	11	05	06	05	02	06	.	.	.	.	.	01	.								
X 6.0 5.8 4.6 5.5	152.1	09.4	79 62 78 73 35	035 017.6	11	.	03	02	01	01	01	01	01	14	19	15	07	15	07	02	01	.	01	04	11	.									
XI 7.6 7.5 6.4 7.1	095.2	07.0	75 67 75 72 30	124 040.3	14	.	04	04	.	05	03	02	01	14	15	11	05	15	.	.	.	.	.	03	01	.									
XII 4.8 5.3 4.6 4.9	125.5	04.5	64 54 64 23	139 051.4	07	.	04	04	.	02	01	01	09	08	07	05	04	.	.	.	.	01	.	01	01	.									
GOD. 6.3 6.5 5.2 6.0	2083.4	08.3	71 57 70 66 14	1455 099.4	05.1	.	07	65	05	04	39	15	65	135	142	110	50	142	01	01	.	.	03	01	39	05									
PAGB																																			
BR. ST. 48																																			
I 8.4 8.0 8.0 8.3	040.3	04.2	89 86 90 89 50	239 044.7	12	.	05	22	.	.	.	.	.	02	21	21	15	08	18	10	.	02	02	.	02	09	24								
II 7.6 8.2 7.2 7.7	053.3	04.5	82 78 82 78 36	236 051.3	23	02	04	15	.	.	.	.	.	03	01	14	19	15	07	15	07	02	01	.	01	04	11								
III 6.4 6.6 4.3 5.6	196.2	04.1	61 59 23	128 039.0	29	.	02	14	.	.	.	.	.	02	04	08	11	07	04	10	02	.	.	.	02	06									
IV 7.1 7.1 5.1 5.5	161.0	04.6	76 64 74 71 28	145 048.2	09	.	19	.	.	.	.	.	.	01	02	11	11	09	05	03	09	01	01	.	01	08									
V 5.9 7.1 5.6 6.2	169.5	07.2	81 64 80 75 22	115 026.4	27	.	01	.	.	.	.	.	.	04	12	15	13	05	15	.	.	.	.	.	06	01									
VI 5.2 6.8 4.8 5.6	191.0	09.3	80 66 78 75 37	079 020.2	22	.	03	03	.	.	.	.	.	02	04	15	10	04	15	.	.	.	01	11	.										
VII 5.1 6.2 4.8 5.6	219.0	10.3	83 67 83 77 42	180 041.3	27	.	04	04	.	01	01	01	01	05	07	17	14	06	17	.	.	.	.	.	13	01									
VIII 6.1 7.2 5.7 6.6	196.6	10.6	85 72 88 62 44	250 098.8	22	.	03	03	02	02	03	03	03	01	03	11	18	14	06	18	.	.	.	.	.	11	05								
IX 5.7 5.3 3.9 5.0	187.5	07.7	88 66 86 80 24	096 039.7	18	.	02	.	.	.	.	.	01	04	03	08	08	04	08	03	03	.	.	.	02	04	02								
X 5.8 5.0 5.6 5.6	131.3	07.4	90 73 88 84 44	114 036.6	03	.	04	.	.	.	.	.	01	08	14	10	08	05	10	01	01	.	.	.	01	07	01								
XI 7.1 6.1 6.7 6.6	096.5	05.2	86 74 87 82 29	222 076.0	14	.	04	17	.	.	.	.	02	05	03	15	11	08	12	07	01	.	01	01	05	12									
XII 6.9 6.1 6.1 6.3	077.3	03.5	85 79 87 84 34	091 024.6	07	06	12	28	.	.	.	.	05	14	11	08	02	06	04	01	01	.	01	01	07	26									
GOD. 5.3 5.2 5.2 5.2	-	095.7 66 66 73 72	127 052.0	44.2	-	-	71	04	-	12	01	48	78	128	96	51	128	01	01	.	.	.	03	40	12										
ZALESINA																																			
BR. ST. 50																																			

Mjesec	Vrstdišnji pritisak Pm mm	Temperatura vazduha °C										Cestine pravaca i srednja jačina veta m/s, Fm (0-12)																		
		Tm			Max.			Min.			Dat.	N			NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnes)	Max.	Min.	Max.	Min.	Max.	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
I	-	01.8	03.1	01.7	02.1	04.3	-00.5	10.5	24	-10.0	25 -07.0	20	.	.	09	02.0	15	01.5	06	02.2	03	02.0	07	02.9	43	03.3	10	01.8		
II	-	02.8	05.8	03.4	03.9	06.7	01.3	13.5	24	-10.0	04	01	02.0	09	02.2	03	02.3	07	02.3	03	01.0	15	02.5	37	03.7	09	01.7			
III	-	04.7	11.5	07.0	07.5	12.7	03.3	23.5	24	-06.0	01	02	01.0	04	02.8	11	02.4	16	02.1	03	02.3	18	02.4	32	02.8	07	C2.1			
IV	-	04.3	10.4	06.6	07.1	12.3	02.0	22.9	30	-05.5	17	02.2	05.5	15	02.4	11	02.1	03	01.7	11	02.6	23	02.5	08	01.9	.	.			
V	-	10.0	16.3	11.5	12.4	17.5	05.3	25.0	04	00.1	29	05	02.0	08	02.4	13	02.5	12	02.4	02	02.0	16	02.1	19	02.3	18	01.8			
VI	-	13.9	19.1	14.7	15.0	21.0	02.0	21.1	13	01.0	02	03	01.7	14	01.6	09	02.7	02	01.5	03	01.7	12	02.7	29	03.0	18	01.5			
VII	-	15.4	20.7	16.7	17.3	22.5	12.5	27.0	03	07.5	28	04	01.8	17	02.4	07	02.1	16	02.4	02	01.5	08	02.0	25	02.7	14	01.6			
VIII	-	14.4	20.3	15.7	16.5	21.2	11.5	25.0	17	06.2	25	08	02.2	06	01.7	15	02.1	12	02.3	08	01.9	14	01.9	28	02.4	10	01.6			
IX	-	08.9	15.4	10.4	11.3	16.6	06.6	26.0	08	-01.8	29	04	01.2	19	02.3	14	02.7	19	02.1	03	01.0	07	01.6	08	01.8	16	01.7			
X	-	08.7	13.5	10.2	10.6	14.5	07.3	26.0	21	00.0	04.02	03	01.3	17	01.9	14	02.0	12	01.6	01	01.0	14	02.6	29	02.8	03	01.7			
XI	-	04.2	07.4	04.5	05.2	08.2	01.6	19.5	41	-05.6	29	03	01.3	14	02.1	12	02.5	06	02.2	08	01.9	19	02.0	26	03.5	10	02.0			
XII	-	-02.4	00.0	-01.6	-01.4	00.5	-04.4	08.5	25	-11.5	05	06	01.2	16	02.0	18	01.9	11	02.0	04	04.0	16	02.9	19	01.8	06	01.2			
GOD.	-	07.2	12.0	08.4	09.0	13.2	04.6	30.1	43	-11.5	05.8	41	01.7	14.8	02.1	14.2	02.2	13.0	02.2	24	01.6	16.3	02.4	31.8	02.9	12.9	€1.8			
$\gamma = 45^{\circ}25' N \lambda = 14^{\circ}55' E$ Gr. $\Delta G = +1h 00 min.$																														
$\gamma = 45^{\circ}16' N \lambda = 15^{\circ}14' E$ Gr. $\Delta G = +1h 01 min.$																														
I	732.8	02.0	04.7	03.0	03.2	06.3	00.5	12.3	25	-06.3	20	07	01.3	21	01.4	11	01.5	11	02.1	08	02.5	11	03.2	07	01.4	06	01.5	11		
II	730.7	03.6	07.8	04.5	05.5	09.6	02.4	17.2	24	-10.4	04	04	02.2	10	01.7	05	01.6	06	01.7	10	02.7	16	04.1	19	02.3	14	01.8	.		
III	735.9	04.9	13.7	08.6	08.9	14.9	03.3	24.6	23	-07.5	01	05	01.2	11	02.4	06	02.3	05	01.4	06	02.2	18	04.3	27	02.4	13	01.8	01		
IV	731.6	04.7	13.0	08.1	08.5	14.5	02.6	26.9	29	-03.2	17	02	01.5	11	02.1	10	01.8	08	02.2	05	03.4	19	01.9	17	01.6	06	.			
V	733.1	11.3	18.3	13.0	13.9	19.6	08.3	26.8	04	01.8	28	07	01.6	13	01.8	09	02.3	07	02.3	08	02.8	08	03.6	27	01.9	13	01.7	01		
VI	732.1	15.4	22.0	17.6	17.8	23.0	12.0	31.1	13	02.1	02	08	01.8	06	01.7	06	01.8	07	01.7	04	02.0	18	03.5	27	02.2	13	01.6	01		
VII	732.1	16.8	22.4	18.0	18.8	24.5	13.3	30.0	13	08.2	26	08	01.5	10	02.1	05	01.8	08	01.6	06	02.2	09	03.1	26	02.0	17	01.6	04		
VIII	732.0	15.0	22.7	18.3	18.1	23.6	13.3	28.0	17	07.0	25	07	01.9	08	01.5	10	01.5	05	01.6	06	02.5	08	02.9	26	01.7	20	01.5	03		
IX	732.2	09.2	17.2	11.6	12.4	18.7	07.7	27.6	08	-01.5	29	12	02.4	14	02.2	10	02.0	06	02.0	02	02.0	07	.	.	21	01.5	21	01.4	04	
X	732.4	08.6	16.1	11.5	12.7	17.2	07.4	24.6	08	00.1	04	06	01.2	24	01.6	07	01.1	08	02.0	12	01.9	07	03.4	17	02.2	06	01.8	06		
XI	731.4	05.0	09.1	05.8	06.4	16.3	02.5	24.7	11	-06.1	20	09	02.4	09	01.8	05	01.4	07	01.7	07	02.4	11	03.2	13	01.8	11	.			
XII	738.0	-02.2	01.9	-00.8	-00.4	02.7	-03.8	11.1	25.2	-16.2	06	07	01.7	22	01.5	11	02.1	05	01.6	06	02.5	06	02.7	12	02.4	08	01.6	12		
GOD.	733.7	07.9	14.1	09.8	10.4	15.5	05.8	31.1	43	-16.2	06.8	83	01.8	159	01.8	95	01.7	91	01.8	83	02.3	117	03.5	246	02.0	161	01.6	60		
$\gamma = 45^{\circ}30' N \lambda = 15^{\circ}33' E$ Gr. $\Delta G = +1h 02 min.$																														
$\gamma = 45^{\circ}20' N \lambda = 15^{\circ}33' E$ Gr. $\Delta G = +1h 02 min.$																														
I	751.9	01.7	04.4	02.6	02.8	05.7	00.2	13.7	30	-07.5	01	07	01.0	35	01.2	*	*	*	01	02.0	05	01.9	01	02.0	01	01.0	39			
II	749.5	03.2	09.5	05.5	05.8	10.3	02.4	17.5	23	-05.7	04	03	01.0	23	01.1	*	*	*	02	03.0	16	02.0	01	01.0	02	01.0	37			
III	754.6	04.1	15.6	09.8	09.8	16.9	03.4	26.5	24	-05.6	01	04	01.5	24	01.2	*	*	*	01	02.0	17	01.8	02	03.5	01	01.0	45			
IV	750.2	04.7	14.0	09.7	09.7	16.3	03.6	28.5	20.9	-01.4	17	07	01.4	29	01.4	01	01.0	01	01.0	16	01.3	*	*	*	*	35				
V	751.2	11.9	21.0	15.5	16.0	22.3	10.0	29.3	01	02.6	28	04	01.5	24	01.4	01	01.0	02	01.0	19	01.6	03	01.3	02	01.0	37				
VI	749.9	16.0	24.8	19.2	19.6	25.9	13.3	32.6	13	04.2	02	01	01.0	23	01.3	C2	01.0	*	*	03	02.0	23	01.7	01	01.0	31				
VII	749.8	17.1	22.5	20.5	20.8	26.6	15.0	32.1	14	10.4	28	08	01.6	26	01.3	*	*	*	02	01.0	17	01.8	01	02.0	05	01.0	38			
VIII	745.8	15.7	24.6	19.4	19.8	25.7	14.6	26.2	08	09.0	25	04	01.2	25	01.1	*	*	*	01	01.0	16	01.4	*	*	*	*	46			
IX	755.3	09.9	19.1	13.5	14.0	20.5	09.6	25.1	08	-01.1	29	03	01.0	29	01.5	04	01.2	02	01.5	*	*	04	01.2	*	*	47				
X	755.7	08.2	16.8	11.6	12.1	17.7	07.5	25.4	08	00.6	18	02	01.0	20	01.2	01	01.0	*	*	*	19	01.9	*	*	01	01.0	50			
XI	750.0	05.0	09.2	06.7	06.9	10.5	03.5	21.6	12	-03.1	24	05	01.0	35	01.3	*	*	*	15	01.8	01	02.0	*	*	34					
XII	757.3	-01.3	01.3	00.0	02.7	-02.5	12.7	25	-11.9	05	03	02.0	44	01.0	21	01.0	01	01.0	*	03	01.0	*	*	*	*	41				
GOD.	752.1	08.0	15.5	11.2	11.5	16.8	06.7	32.6	03	-11.5	05.8	51	01.2	337	01.3	10	01.1	08	01.1	09	01.9	170								



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Mjesec	Vrijednost Pritisak Pa mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina vjetra m/s, Pm (O-12)																				
		Tm				Min				N						NE			E		SE		S		SW		W		NW	
		7	14	21	Sred. (Dnev.)	IM	MIN	MAX	Dat.	MIN	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	
$\varphi = 45^{\circ}56' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$																														
I	-	01.0	02.7	01.6	01.7	04.3	-01.0	11.4	25 -07.6	20	03	01.0	20	02.0	.	.	13	02.2	01	01.0	35	03.8	09	01.4	07	01.9	05			
II	-	03.0	05.7	03.7	04.0	06.8	01.5	13.2	25 -06.4	03	03	02.8	09	01.9	03	01.0	15	03.1	.	.	25	03.0	13	01.8	10	02.6	06			
III	-	05.9	11.0	07.6	06.0	12.2	04.6	21.6	24 -05.8	01	07	01.0	13	03.0	02.8	01.8	12	02.0	.	.	29	02.9	07	01.4	16	02.2	01			
IV	-	05.5	10.2	06.8	07.3	11.3	03.3	22.6	30.29 -03.5	11	04	02.5	16	02.0	01	01.0	16	02.4	01	02.0	16	02.2	03							
V	-	12.5	16.1	12.2	13.3	17.4	09.5	24.2	04 04.4	28	02	01.0	26	02.0	02	01.5	14	02.2	07	01.6	14	02.6	08	01.4	13	02.4	07			
VI	-	15.8	20.3	15.6	16.9	21.3	13.0	27.6	13 04.2	01	08	01.4	11	01.7	05	02.0	11	02.5	05	02.2	24	03.0	08	02.5	15	03.1	03			
VII	-	16.6	20.3	17.5	17.9	21.9	14.0	25.8	03 06.2	21	02	02.5	16	02.1	09	01.8	16	02.5	07	02.1	18	02.8	05	01.8	18	01.8	02			
VIII	-	16.5	20.4	16.5	17.5	21.1	13.9	24.8	18.08 16.0	25	01	01.0	17	01.6	08	01.8	09	02.4	06	01.5	17	03.0	09	02.3	22	02.3	06			
IX	-	11.2	15.2	11.3	12.2	16.2	08.8	24.6	08 02.5	20	03	01.3	31	02.4	11	01.5	18	02.2	03	01.7	07	01.4	01	04.0	10	02.0	06			
X	-	09.5	13.6	10.3	11.1	14.5	08.4	21.2	08 01.0	03	04	01.0	10	02.0	17	01.4	08	01.9	01	01.0	19	04.1	10	02.3	12	01.9	12			
XI	-	05.1	06.6	04.9	05.6	08.4	02.8	20.2	11 -06.2	30.29	02	02.5	10	02.6	03	01.0	18	02.4	02	03.0	26	03.1	05	01.4	15	02.5	09			
XII	-	-02.3	-00.5	-01.7	-01.5	00.6	-03.8	07.4	25 -09.8	21.20	03	02.3	15	02.3	13	01.1	05	02.0	02	05.0	11	03.3	03	01.3	15	02.0	21			
GOD.	-	08.4	11.8	08.5	09.5	13.0	06.2	27.6	05.VI -06.8	24.00	42	01.4	203	02.1	87	01.5	155	02.3	35	02.0	244	03.1	79	01.9	169	02.2	81			
$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$																														
I	747.7	02.2	04.2	03.2	03.2	05.3	01.0	12.7	23 -05.8	01	04	01.8	28	01.5	18	01.3	09	01.1	08	01.1	10	01.7	14	02.0	01	01.0	01			
II	745.3	04.5	08.6	06.1	08.3	09.5	03.8	15.5	21 -02.5	04	04	02.0	10	01.3	14	01.6	03	01.0	08	01.6	17	02.3	16	02.0	09	01.7	01			
III	750.4	07.0	14.4	11.2	11.0	15.4	04.6	24.0	24 -02.8	01	05	01.6	19	01.7	13	01.9	04	01.8	07	01.7	12	02.1	16	02.2	11	01.9	06			
IV	746.1	06.9	13.8	10.5	10.4	14.7	06.0	26.7	29 00.1	01	05	02.0	19	01.8	17	01.6	05	01.6	09	01.7	14	02.0	11	01.7	05	01.6	05			
V	747.3	13.7	20.1	15.5	16.4	21.3	11.5	27.1	20 06.3	28	12	01.5	21	01.5	12	01.7	05	01.4	10	01.5	10	01.8	12	01.8	08	01.9	03			
VI	745.9	17.5	24.4	19.0	20.3	25.3	15.4	31.5	13 06.5	03	07	01.9	18	01.4	08	02.5	02	01.8	08	01.9	12	02.2	16	02.1	11	01.3	05			
VII	746.0	16.4	24.1	20.7	25.6	16.2	30.4	13 11.5	27	16	01.5	23	01.5	14	01.4	08	01.4	13	01.8	10	02.2	07	01.6	08	01.4	04				
VIII	746.0	17.3	24.1	19.7	20.2	24.6	16.0	28.6	08.05 11.9	25	07	01.7	26	01.5	14	01.6	05	01.0	07	01.6	10	02.1	13	01.5	10	01.5	01			
GOD.	748.1	05.5	14.8	11.7	12.1	15.6	08.4	31.5	05.VI -06.8	06.00	73	01.6	261	01.6	176	01.6	67	01.4	115	01.5	135	02.0	162	01.9	80	01.6	26			
$\varphi = 45^{\circ}18' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$																														
I	-	01.7	05.6	03.3	03.5	06.6	-01.2	14.5	23 -09.5	01	33	01.5	06	02.7	13	01.7	.	.	19	02.2	10	03.2	07	01.4	03	01.7	02			
II	-	03.2	09.8	05.6	10.6	10.4	00.4	17.0	25 -12.0	04	17	02.4	06	02.0	03	01.7	.	.	21	03.6	15	03.1	15	01.8	06	01.5	01			
III	-	04.2	16.1	08.2	09.3	16.8	01.4	25.5	24.23 -06.0	01	12	03.5	15	02.2	11	02.2	02	02.0	15	02.3	16	02.4	14	01.3	08	01.8	00			
IV	-	06.2	14.8	08.6	09.6	16.2	01.7	28.5	29 -03.0	12	21	02.8	11	03.0	02.3	13	01.6	02	02.5	10	01.4	08	02.5	05	01.6	05				
V	-	13.3	21.3	14.1	15.7	22.1	07.8	29.0	01 01.5	29	11	03.4	06	02.7	07	02.2	04	02.2	29	01.9	07	02.7	17	01.9	12	02.7	.			
VI	-	16.7	25.0	13.1	19.0	25.7	10.4	32.0	13 01.2	20	13	01.2	02	03	01.2	03	01.2	08	01.8	19	02.6	27	02.6	14	02.1	05	01.4	.		
VII	-	17.1	25.5	17.9	19.6	26.4	12.5	32.2	08 08.0	28	13	02.4	08	02.7	07	02.7	04	02.4	13	01.1	13	01.7	20	01.9	03	01.7	.			
VIII	-	16.3	25.5	19.6	26.2	12.4	29.5	14 05.5	25	14	02.0	05	01.0	08	01.8	11	02.1	14	01.4	11	02.5	27	02.4	07	01.0	04				
IX	-	10.3	19.9	11.5	13.3	20.6	06.9	29.5	12 -03.0	29	27	02.8	12	02.0	02	03.0	09	02.6	66	01.2	06	01.7	17	01.7	10	01.7	01			
X	-	08.2	17.8	10.2	11.6	18.4	05.6	26.2	07 -01.0	04	24	01.8	17	02.2	04	01.8	03	02.7	17	02.2	10	02.0	12	02.1	06	02.0	.			
XI	-	05.1	10.4	04.3	07.0	11.4	01.8	25.0	11 -05.0	30	18	02.8	16	02.2	03	01.3	01.5	01.2	08	02.8	13	01.9	14	01.8	02	01.0	01			
XII	-	-01.6	01.8	-00.6	-00.2	02.9	-04.1	13.6	28 -17.0	06	28	02.0	09	01.9	66	02.2	04	01.8	10	02.1	14	02.3	11	01.6	10	01.6	01			
GOD.	-	08.4	16.1	10.1	11.2	17.0	04.6	33.0	05.VI -17.0	06.00	222	02.4	109	02.3	69	02.0	200	02.3	154	02.5	183	01.8	96	01.9	08					
$\varphi = 45^{\circ}49' N \lambda = 16^{\circ}02' E$ Gr. $\Delta G = + 1h 05 min.$																														
I	-	01.8	03.2	01.7	02.1	04.5	-00.7	13.4	26 -12.6	01	18	02.4	21	02.3	07	02.1	06	01.8	06	02.5	15	02.4	13	02.9	07	01.7	.			
II	-	03.9	08.4	05.4	06.5	09.5	01.5	16.6	11 -08.8	03	28	01.5	06	02.2	08	01.2	06	01.3	08	02.4	16	02.4	07	01.9	01	01.0	04			
III	-	04.4	14.5	08.3	08.9	15.8	02.9	24.6	24 -04.5	01	43	01.6	02	02.0	04	02.0														

Meseč	Oblačnost Nm (0-10)	Sred. (Dies) Broj sati	Vlažnost vazduha U m % mm.	Padavine R mm mm.	Broj dana na sat																																					
					Tn	Tk	Tn	Tk	Tk	Th	F(O-12)	Nm(O-10)	R mm	•	*	*	X	o	A	▲	■	□																				
					7	14	21	Sred.	Nm	M	Max	Dat.	30.00.0	0.0250	30.020.0	6	6	2.0	8.0	0.1	1.010.0																					
<b>STLBIČKA GORA</b>																																										
<b>BR. ST. 56</b>																																										
I	7.7	7.3	6.5	7.3	-	04.5	86	83	86	85	50	114	024+2	03	•	04	17	•	•	05	•	01	15	13	11	06	11	05	02	•	•	•	•	06	12							
II	7.7	6.5	5.3	7.1	-	05.1	82	77	82	80	45	108	036+3	01	•	02	07	•	•	02	•	02	12	10	04	08	04	04	•	•	•	•	01	09								
III	4.1	5.7	3.2	4.3	-	05.4	74	64	72	70	36	093	033+2	31	•	02	05	•	•	01	•	05	06	06	04	04	03	02	•	•	•	•	01	04	05							
IV	5.9	6.7	3.7	5.5	-	05.4	73	62	71	69	29	103	035+8	09	•	•	07	•	•	07	03	13	08	04	09	06	01	•	•	•	•	03	06									
V	5.5	7.0	4.0	5.5	-	06.0	73	63	69	68	17	040	011+2	17	•	•	•	•	•	01	•	06	07	11	06	02	11	•	•	•	•	01	03	•								
VI	4.0	5.4	3.7	4.4	-	06.7	70	56	68	65	33	095	026+3	23	•	•	07	•	•	01	•	07	04	07	07	•	•	•	•	04	•	•										
VII	5.2	5.4	3.4	4.7	-	10.7	74	64	70	69	45	145	028+8	11	•	•	04	•	•	07	05	13	13	06	13	•	•	•	•	04	01	•										
VIII	5.0	7.0	3.6	5.5	9.5	-	11.6	80	65	78	76	54	098	020+7	01	•	•	•	•	•	04	08	13	11	04	13	•	•	•	•	05	•	•									
IX	4.4	5.5	3.9	4.6	-	08.1	78	67	76	74	32	108	033+8	18	•	•	•	•	•	08	07	10	08	03	10	•	•	•	•	01	04	•										
X	3.7	5.4	3.6	4.2	-	08.1	85	75	83	81	43	066	032+4	02	•	•	•	•	•	03	13	05	04	04	02	04	•	•	•	•	18	•										
XI	6.8	8.8	5.5	6.4	-	05.5	78	76	79	78	34	216	066+8	14	•	03	10	•	•	01	01	07	13	10	10	07	08	04	02	•	•	01	18	04								
XII	6.1	8.4	7.2	7.9	-	03.6	64	84	84	85	53	073	028+2	29	•	16	25	•	•	02	•	02	17	12	10	03	06	07	•	•	•	•	18	24								
GOD.	5.7	6.6	4.5	5.6	-	07.2	78	70	76	74	17	1258	066+8	44.XI	•	27	71	11	•	•	16	01	73	111	124	106	49	103	29	05	•	•	01	15	59	42						
<b>ZAGREB-GRCIC</b>																																										
<b>BR. ST. 57</b>																																										
I	8.7	8.5	7.6	8.4	033+9	04.9	86	81	84	84	49	080	022+4	03	•	01	13	•	•	02	•	20	16	11	02	14	04	02	•	•	•	01	18	06								
II	7.9	7.9	6.0	7.3	079+5	05.4	81	67	74	74	40	067	017+9	01	•	01	06	•	•	09	•	01	14	12	08	03	10	04	02	•	•	02	08	02								
III	6.0	7.1	4.2	5.8	178+9	05.8	75	49	57	60	21	054	022+9	13	•	•	04	•	•	05	•	03	07	08	06	02	07	02	01	•	•	01	02	02								
IV	7.6	7.1	5.1	6.6	164+4	05.9	75	52	63	63	30	091	027+6	09	•	•	02	•	•	01	•	03	12	10	07	04	09	01	•	•	•	•	02	03	01							
V	6.3	6.9	5.1	6.1	212+8	08.5	74	50	61	62	29	028	006+5	06	•	•	06	•	•	03	•	07	12	12	06	02	12	06	02	•	•	02	•	•	02	•						
VI	5.1	6.6	3.5	5.5	246+6	16.6	70	46	61	59	33	066	030+2	23	•	•	17	04	03	05	•	06	08	08	06	02	08	06	•	•	08	•	•	08	•							
VII	5.2	6.1	3.9	5.1	247+6	12.0	76	53	70	66	35	110	024+7	16	•	•	20	01	•	01	•	02	05	12	11	04	12	06	05	•	•	05	•	05	05							
VIII	5.5	6.5	6.8	6.0	213+4	12.2	76	52	73	70	38	105	040+9	24	•	•	15	•	•	01	•	03	07	12	10	02	12	06	05	•	•	01	08	•	•	01	08	•	•			
IX	5.4	5.9	4.6	5.3	175+2	08.6	81	57	71	70	38	090	023+2	15	•	•	08	•	•	01	•	06	05	10	08	04	10	04	02	•	•	01	01	•	•	01	01	•	•			
X	5.6	5.5	5.2	5.5	132+7	08.7	89	70	63	63	45	046	037+9	02	•	•	04	•	•	01	•	08	11	06	04	02	06	05	•	•	01	16	•	•	01	16	•	•	01	16	•	•
XI	8.7	8.7	8.2	8.5	053+5	06.5	89	79	84	84	48	159	046+3	14	•	•	05	•	•	01	•	19	16	09	05	16	03	05	03	•	•	01	16	03	•	07	02					
GOD.	6.7	7.2	5.6	6.5	1770+6	07.8	80	61	71	71	21	963	046+3	44.XI	•	11	47	66	05	03	33	01	40	140	134	96	31	127	16	08	•	•	01	32	51	13						
<b>TOPUSKO</b>																						<b>H<sub>s</sub> = 129 m H<sub>b</sub> = 2.0 m h<sub>t</sub> = 1.0 m</b>																				
<b>BR. ST. 58</b>																						<b>H<sub>s</sub> = 129 m H<sub>b</sub> = 2.0 m h<sub>t</sub> = 2.0 m</b>																				
I	8.4	7.5	5.6	7.2	-	05.1	90	82	86	86	49	084	016+5	13	•	20	•	•	01	•	02	14	13	13	02	12	03	02	•	•	•	10	11	04								
II	6.3	6.6	4.4	5.8	-	05.7	79	71	82	81	27	076	015+8	01	02	12	02	•	•	05	•	05	04	04	06	02	03	01	•	•	04	04										
III	3.0	3.2	1.9	2.7	-	06.1	91	48	74	71	25	066	022+4	31	•	09	02	•	01	•	18	04	06	06	02	05	02	02	•	•	03	02	02									
IV	4.9	4.2	3.7	4.3	-	06.4	86	53	73	72	28	133	034+5	15	•	09	03	•	•	09	05	10	10	06	09	01	•	•	•	01	01	01										
V	5.1	5.6	4.4	5.0	-	09.3	82	50	75	69	29	082	022+1	15	•	•	09	•	•	01	•	08	10	10	03	10	04	02	•	•	01	01	•									
VI	5.3	4.0	3.0	3.5	-	11.2	79	46	76	67	33	038	013+0	27	•	•	16	05	•	•	13	03	08	07	01	08	06	•	•	02	02	•										
VII	3.7	3.7	2.9	3.5	-	12.7	88	52	84	75	27	140	051+4	27	•	•	23	06	•	•	11	03	08	08	06	08	08	•	•	01	01	•										
VIII	5.0	5.4	3.4	3.4	-	13.0	90	54	82	76	33	046	008+1	19	•	•	22	•	•	09	03	10	10	01	08	08	08	•	•	08	•	•	08									
IX	5.9	4.6	3.7	4.7	-	05.4	93	59	87	80	35	082	026+8	20	•	•	01	12	•	•	01	•	10	08	06	06	03	06	•	•	•											

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Mesec	Vrednost Pritisaka Pm mm	Temperatura vazduha °C						Čestina pravaca i srednja jačina vjetra mD, Pm (G-12)																					
		Tm			Sred. (Des)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21							E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.			
$\varphi = 45^{\circ}30' N \lambda = 16^{\circ}22' E$ Gr. $\Delta G = + 1h 06 min.$																													
I	752.8	01.5	64.4	02.8	02.8	06.0	-00.4	14.7	26	-05.4	19	10	01.4	12	01.2	12	01.2	06	01.0	01	02.0	05	01.4	01	01.0	39			
II	750.6	03.7	68.9	05.9	06.1	10.2	02.2	17.4	25.2	-06.6	04	04	01.8	09	01.7	07	01.1	04	01.0	03	02.3	04	03.0	03	01.0	39			
III	755.5	05.0	15.2	05.6	09.8	16.7	03.3	25.6	24	-04.9	01	08	01.6	05	02.0	07	01.1	01	01.0	04	01.2	01	01.3	09	01.6	03	01.0	49	
IV	751.2	06.3	10.0	05.8	10.3	03.6	26.8	30	-01.4	01	06	02.8	12	02.5	05	01.2	02	01.5	05	01.2	10	01.2	04	01.2	42				
V	752.3	13.4	20.4	15.2	16.2	22.7	09.6	28.9	20	02.7	28	07	02.1	08	01.6	12	01.5	03	01.7	03	03.7	06	02.0	10	01.5	03	02.3	41	
VI	751.0	17.5	24.4	18.9	19.9	25.6	12.6	32.0	14	03.0	02	10	02.4	06	02.2	05	02.0	04	01.3	02	01.0	13	02.2	03	01.7	32			
VII	750.9	17.9	24.9	19.7	20.5	26.6	14.1	32.7	14	05.6	28	07	02.0	14	02.0	04	01.8	06	01.5	02	01.0	04	02.2	12	01.7	02	02.0	42	
VIII	750.9	16.7	25.2	19.2	20.0	26.6	13.8	29.9	09.05	08.7	25	08	01.8	09	01.8	05	01.4	04	01.5	02	01.3	06	02.2	09	01.8	05	01.4	45	
IX	754.6	10.3	19.2	15.5	13.6	20.5	08.3	30.1	08	-01.6	29	06	02.6	18	02.2	07	01.0	06	01.0	04	01.0	03	01.3	46					
X	757.0	07.9	16.2	10.9	11.5	17.5	06.2	25.1	07	-00.1	18	01	01.0	15	01.4	05	01.2	03	01.2	04	02.5	05	02.8	01	01.0	56			
XI	751.3	04.9	05.0	06.0	06.5	10.2	02.9	21.3	12	-04.3	30	12	01.7	10	01.7	06	01.3	03	01.7	02	01.0	08	01.4	07	01.3	06	01.0	36	
XII	758.6	-01.4	01.3	00.0	00.0	02.7	-03.1	12.1	25	-13.7	06	08	01.5	08	01.4	14	01.1	03	01.0	01	01.0	02	01.0	01	01.0	54			
GOD.	753.2	08.6	15.3	10.9	11.4	16.8	06.1	32.7	04.VI	-15.7	06.XI	67	01.9	126	01.8	89	01.3	44	01.3	31	01.5	73	02.0	90	01.7	34	01.3	521	
$\varphi = 45^{\circ}30' N \lambda = 16^{\circ}23' E$ Gr. $\Delta G = + 1h 06 min.$																													
V	-	12.7	20.6	16.2	16.4	21.7	05.4	28.4	04	01.8	28	15	02.1	10	01.8	04	01.5	19	02.2	17	01.9	07	02.0	21	01.4	04	01.4	00	
VI	-	16.7	24.8	21.0	20.9	25.5	12.7	32.5	12	03.1	03	12	02.2	14	01.6	02	03.0	01	02.0	05	02.4	33	02.2	07	02.1	16	01.8	00	
VII	-	17.5	24.9	21.2	21.2	26.1	14.0	30.5	14	06.6	28	15	01.8	08	01.7	04	02.6	06	01.8	24	02.1	04	01.5	11	01.5	00			
VIII	-	16.1	20.1	20.4	26.2	13.7	29.6	30	07.2	15	01.4	16	01.8	03	02.0	05	01.6	02	02.0	29	02.0	06	01.7	17	01.5	00			
IX	-	10.2	19.8	14.8	14.9	20.5	07.9	30.2	07	-02.2	29	22	01.4	22	01.9	05	02.0	02	01.5	04	02.2	16	01.6	07	01.7	12	01.3	00	
X	-	04.1	16.4	12.6	12.4	17.2	06.8	25.6	08	-01.1	18	11	01.7	21	01.5	06	02.0	03	01.3	10	02.0	25	01.8	09	01.7	07	01.3	00	
XI	-	04.6	08.8	06.7	06.7	10.3	03.4	20.6	11	-04.4	29	10	02.0	12	02.0	03	01.7	04	01.8	08	02.6	31	02.0	11	01.5	11	01.4	00	
XII	-	-02.0	01.3	00.0	-00.2	02.0	-03.2	12.2	25	-12.2	06.05	11	01.9	23	01.7	09	01.7	08	01.5	08	01.6	24	01.6	07	01.3	03	01.7	00	
GOD.	-	08.2	15.3	11.4	11.6	16.3	06.1	32.5	05.VI	-12.2	06.05	178	01.8	201	01.7	52	01.9	55	01.6	91	02.2	304	02.0	73	01.7	141	01.5	00	
$\varphi = 45^{\circ}54' N \lambda = 16^{\circ}51' E$ Gr. $\Delta G = + 1h 07 min.$																													
V	748.9	13.1	21.1	14.9	16.0	22.1	08.6	29.3	04	01.2	28	09	01.9	21	01.7	11	01.1	13	01.0	11	01.8	07	01.7	11	01.1	01	01.1	00	
VI	747.5	17.0	24.6	17.8	19.3	25.4	11.9	31.5	13	02.0	02	02	02.0	15	01.3	08	01.0	10	01.0	08	01.1	28	01.0	04	01.0	14	01.6	01	
VII	747.8	17.8	24.9	18.4	19.8	25.7	13.1	30.0	08	09.2	27	07	01.6	21	01.3	11	01.0	08	01.1	18	01.2	07	01.0	18	01.2	00			
VIII	747.7	16.2	23.4	18.6	19.4	26.1	13.3	30.0	30	06.0	25	07	01.6	12	01.2	18	01.0	09	01.2	04	01.0	16	01.6	17	01.0	10	01.4	00	
IX	753.3	09.9	19.4	11.7	13.1	20.4	07.4	29.6	04	-02.0	29	15	01.6	25	01.3	17	01.4	07	01.0	04	01.0	09	01.3	09	01.1	04	01.0	00	
X	753.5	07.1	16.9	10.3	11.1	17.7	05.6	26.5	18	04	01.2	23	01.2	12	01.0	16	01.0	03	01.0	28	01.6	04	01.0	03	01.0	00			
XI	747.6	04.2	09.6	05.8	06.4	10.9	08.2	22.8	11	-07.6	30	06	02.5	10	01.7	09	01.2	16	01.1	12	01.4	22	01.4	06	01.0	06	01.0	01	
XII	754.9	-02.0	01.0	-01.0	-00.7	01.6	-03.8	10.8	26	-13.8	06	11	01.3	18	01.3	10	01.1	09	01.0	22	01.0	06	01.0	04	01.0	00			
GOD.	749.8	08.0	15.4	10.0	10.8	16.4	05.2	31.5	04.VI	-13.8	06.XI	122	01.8	204	01.3	153	01.1	143	01.0	82	01.3	214	01.6	82	01.1	93	01.2	02	
$\varphi = 45^{\circ}22' N \lambda = 16^{\circ}58' E$ Gr. $\Delta G = + 1h 08 min.$																													
V	-	13.3	21.1	14.8	16.0	23.2	05.8	29.6	04	03.6	28	10	02.2	29	01.5	09	01.4	17	01.6	02.0	03.0	01.0	09	01.0	09	01.0	01	01.0	00
VI	-	16.7	24.2	17.9	19.2	25.2	12.6	32.0	14.12	03.5	02	07	02.1	21	01.3	03	01.3	18	02.0	05	01.9	11	01.9	06	03.5	16	01.9	03	
VII	-	17.6	24.8	18.5	19.9	26.1	14.3	31.5	08	08.5	28	04	02.2	16	01.2	08	02.1	17	01.4	10	01.3	12	01.4	04	02.5	15	01.7	07	
VIII	-	16.6	25.0	18.5	19.7	26.1	14.2	36.0	30.09	06.5	26	11	01.3	22	01.2	05	02.0	11	02.1	14	01.9	01	01.0	07	02.0	09	01.7	09	
IX	-	10.4	19.4	12.8	13.9	20.5	06.3	29.0	08	-01.0	29	13	01.5	20	01.3	03	01.7	17	01.5	10	01.4	06	01.3	04	01.8	09	01.3	08	
X	-	07.9	17.2	11.4	11.9	18.3	05.5	25.6	08	-00.5	04	04	02.2	18	01.2	04	01.5	29	01.3	08	01.0	09	01.6	03	01.0	13	01.2	05	
XI	-	04.5	09.3	06.1	06.5	10.8	02.8	22.0	12	-05.0	30	07	02.0	14	01.1	12	01.4	33	01.7										



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Mjesec	Vruditni Pritisak Pm mm	Temperatura vazduha °C							Cestina pravaca i srednja jačina vjetra nD, Pm (0-12)																					
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Max	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.									
$\varphi = 45^{\circ}36' N \lambda = 17^{\circ}14' E$ Gr. $\Delta G = + 1h\ 09\ min.$																														
I	746.1	02.0	05.7	02.6	03.2	06.7	00.1	14.8	29 -08.1	01	16	01.6	08	02.1	04	02.2	13	02.6	09	02.2	04	02.0	06	01.3	12	01.4	21			
II	745.8	04.1	09.5	05.5	06.1	10.6	02.7	17.6	25 -08.5	04	14	02.4	07	01.9	05	01.8	16	02.7	07	03.0	08	02.5	06	01.5	16					
III	750.8	05.3	15.2	09.2	09.7	16.4	04.1	27.0	24 -04.4	01	17	02.4	06	01.5	11	01.1	10	01.4	07	01.7	07	02.1	05	01.8	05	01.6	25			
IV	746.4	06.5	14.4	08.9	09.7	15.9	04.2	30.2	29 -01.6	12	17	02.4	05	02.1	05	01.2	10	01.2	10	01.5	09	01.8	10	01.4	10	01.8	16			
V	747.6	13.8	21.4	14.8	16.2	22.6	10.0	30.1	04	03.5	29	17	01.9	09	02.0	06	01.0	17	01.4	07	02.0	06	01.8	08	01.2	02	01.0	21		
VI	746.3	17.4	24.8	16.2	19.6	25.8	13.0	32.4	14	02.4	02	10	02.1	06	01.7	05	01.4	16	01.5	09	02.3	12	01.9	05	02.0	15				
VII	746.3	17.7	25.2	20.1	16.4	26.8	14.0	31.8	08 -06.5	28	17	02.2	07	01.4	06	00.8	10	01.5	10	01.4	06	02.0	08	01.5	05	01.2	26			
VIII	746.3	16.7	25.2	18.6	19.8	26.4	14.2	30.3	30 -07.2	25	09	02.2	09	01.7	07	01.0	13	01.8	15	01.7	04	01.8	08	01.5	04	02.2	24			
IX	751.7	10.2	19.3	12.0	13.4	20.7	07.8	29.4	12 -01.7	29	16	01.9	08	01.3	03	01.2	03	01.0	05	01.2	03	01.3	04	01.2	26					
X	752.2	08.2	17.1	10.7	11.7	17.9	06.7	26.8	24 -04.0	01	18	01.4	11	01.2	03	01.3	02	01.0	01	01.0	09	01.0	29	01.1	20	01.1				
XI	746.4	04.8	09.5	06.0	06.5	10.9	03.0	23.5	11 -08.8	30	11	01.5	09	02.1	05	01.6	10	01.5	17	02.2	05	02.4	10	01.3	08	01.9	15			
XII	753.6	-02.0	01.4	-00.4	-00.3	02.3	-03.1	12.4	28 -16.5	06	21	01.4	13	01.5	06	01.2	13	01.5	14	01.8	03	01.3	00	01.0	05	01.2	12			
GOD.	748.5	08.7	15.7	10.4	11.3	16.9	06.4	32.4	44.VI -16.5	06.XII	173	02.0	111	01.8	73	01.3	132	01.6	122	02.0	72	02.0	87	01.6	76	01.6	249			
$\varphi = 45^{\circ}20' N \lambda = 17^{\circ}41' E$ Gr. $\Delta G = + 1h\ 11\ min.$																						SLAVONSKA POZEGA		BR. ST. 67						
I	-	-00.4	04.4	02.3	02.1	05.3	-01.3	13.7	26 -10.1	01	23	01.1	19	01.2	07	01.1	03	01.0	05	01.2	07	01.3	14	01.1	15	01.1	.			
II	-	02.8	09.9	06.1	06.2	11.1	01.5	20.1	25 -11.8	04	19	01.4	06	01.2	04	01.2	05	01.0	03	01.3	13	02.0	16	01.6	18	01.1	.			
III	-	04.2	15.5	09.7	09.8	16.5	02.8	26.6	24 -04.0	01	18	01.4	11	01.2	03	01.3	02	01.0	01	01.0	09	01.0	29	01.1	20	01.1	.			
IV	-	06.7	14.9	10.4	10.6	16.2	03.9	28.6	29 -02.0	18	22	01.8	09	01.6	07	01.3	02	01.5	07	01.0	14	01.1	14	01.6	15	01.2	.			
V	-	13.2	21.3	15.5	16.4	22.2	09.7	30.1	04	03.3	28	14	01.1	11	01.2	07	01.4	-	-	10	01.3	18	01.1	13	01.1	20	01.0	.		
VI	-	16.7	24.3	19.2	19.9	25.3	11.9	32.5	14	02.5	02	09	01.1	03	01.0	03	02.0	01	01.0	08	01.1	15	01.3	28	01.1	23	01.3	.		
VII	-	17.5	24.9	19.6	20.4	26.3	13.4	31.2	14	08.2	28	14	01.4	06	02.8	01	02.0	03	01.7	11	01.2	20	01.4	21	01.0	16	01.2	.		
VIII	-	16.4	25.3	19.6	19.9	26.0	13.0	30.0	09	06.8	26	09	01.0	08	01.1	03	02.0	01	02.5	07	01.0	14	01.1	26	01.2	21	01.0	11	01.0	.
GOD.	-	07.9	15.7	11.3	11.5	16.7	05.5	32.5	44.VI -20.2	05.XII	198	01.3	109	01.3	80	01.4	36	01.2	82	01.2	175	01.2	215	01.2	200	01.1	1	.		
$\varphi = 45^{\circ}10' N \lambda = 18^{\circ}00' E$ Gr. $\Delta G = + 1h\ 12\ min.$																						SLAVONSKI BROD		BR. ST. 68						
I	754.8	00.3	04.3	02.0	02.2	05.4	-01.8	14.5	12 -10.4	01	02	02.0	32	02.1	15	02.1	-	04	02.5	09	01.8	08	02.0	07	01.7	16				
II	752.3	03.2	09.5	05.1	05.7	11.0	06.7	21.2	25 -12.2	04	11	02.1	13	02.0	05	01.8	05	01.0	03	02.0	15	02.0	16	02.2	03	01.0	14			
III	757.1	04.5	16.9	08.8	09.2	16.2	02.1	27.4	23 -05.4	01	09	03.0	22	02.0	17	01.9	06	01.2	01	02.0	12	02.3	15	02.0	05	02.2	06			
IV	752.6	06.3	14.4	09.8	10.1	15.9	03.2	27.8	29 -04.4	18	11	02.6	17	02.1	14	01.6	05	02.0	01	01.0	07	02.0	13	01.8	10	03.3	12			
V	-	13.1	21.0	15.5	16.3	22.2	08.8	29.6	05 -04.2	28	12	01.9	20	01.9	10	01.9	06	02.0	08	01.6	14	01.6	16	01.6	02	01.0	05			
VI	752.3	16.1	23.9	18.2	19.1	25.2	10.8	33.3	14	01.7	04	11	01.8	04	01.8	07	01.7	04	02.0	03	02.0	23	01.6	18	01.6	07	02.1	11		
VII	752.4	17.0	24.5	18.9	19.8	26.1	12.3	31.3	14	06.4	28	13	09	02.4	18	01.9	08	01.8	03	01.3	07	14	01.9	21	01.7	08	02.1	07		
VIII	752.4	15.9	24.9	18.8	19.6	26.0	12.4	29.9	09	05.3	26	05	01.4	14	02.1	10	02.0	04	02.0	09	01.3	14	01.9	16	01.6	05	01.4	12		
IX	757.9	09.5	19.3	12.5	13.5	20.4	06.9	26.5	08 -02.0	29	07	03.0	28	01.9	13	02.2	02	01.5	03	01.7	12	01.9	12	01.2	02	01.0	11			
X	758.6	06.4	17.1	10.3	11.0	18.0	04.4	25.6	07 -02.9	18	03	01.3	17	01.5	18	01.7	06	01.2	04	01.5	14	01.6	11	01.6	01	01.0	19			
XI	752.9	03.4	08.9	05.1	05.6	10.2	01.4	24.0	11 -08.0	25	02	01.5	16	01.8	06	01.9	05	01.4	01	01.0	17	01.4	24	01.9	02	01.0	07			
XII	760.3	-02.3	00.4	-01.9	-01.4	01.3	-04.6	10.7	25 -14.5	05	07	02.0	18	01.9	20	01.9	05	01.4	07	01.1	16	01.6	12	01.8	03	01.3	05			
GOD.	754.8	07.8	15.3	10.2	10.9	16.5	04.7	33.3	44.VI -16.5	05.XII	89	02.2	221	01.9	153	01.9	51	01.5	47	01.6	169	01.8	85	01.8	59	01.9	121			
$\varphi = 45^{\circ}46' N \lambda = 18^{\circ}00' E$ Gr. $\Delta G = + 1h\ 13\ min.$																						DONJI MINGLJAC		BR. ST. 69						
I	-	00.1	04.0	01.5	01.6	04.8	-01.2	13.8	30 -05.5	01	03	02.7	07	02.7	20	02.6	31	02.5	02	02.0	05	02.2	07	02.6	18	02.5	.			
II	-	03.4	09.2	04.7	05.5	10.0	01.7	18.6	20 -10.0	03	03	03.7	03	02.7	04	02.6	16	02.3	06	01.8	25	02.8	10	03.9	17	02.8	.			
III	-	05.6	14.8	07.7	09.0	15.6	04.0	26.5	23 -03.8	02.1	03	02.7	06	02.2	09	02.3	29	02.5	13	02.5	09	02.2	05	02.2	30	02.7	.			
IV	-	07.0	14.5	08.7	09.7	15.6	04.4</td																							

Mjesec	Oblačnost Nm (0-10)	Sred. (Dnev.)	Insolacija hrčj sati	Vlažnost vazduha				Padavine R mm												Broj dana na sata:																	
								Tn	Tx	Tn	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	□	□	□	□	□	□	□	□	□						
				mm	7	14	21	Sred. (Dnev.)	Min	Σ	Max	Dat.	10.00.0	0.0250.0	0.020.0	6	8	2.0	8.0	0.1	1.010.0	9	Δ	*	Δ	▲	▲	□	□	□	□						
<b>DARUVAR</b>																																					
<b>BR. ST. 66</b>																																					
I	8.0	6.1	7.8	8.0	047.8	04.7	85	72	87	81	35	067	014.9	16	.	01	13	.	.	.	01	20	15	09	03	13	05	.	01	.	08	10					
II	7.6	5.7	7.0	8.0	089.7	05.4	85	60	80	73	24	044	010.4	01	.	01	09	.	.	.	02	02	10	18	12	01	15	04	01	.	09	05					
III	5.7	5.5	4.4	5.2	194.6	05.5	85	45	71	67	22	049	017.8	31	.	.	04	02	.	.	01	05	08	09	07	03	02	01	01	.	02	01					
IV	7.3	6.5	5.1	6.3	171.1	06.2	81	49	76	65	24	054	016.1	04	.	.	06	03	01	02	02	12	11	05	02	12	02	02	01	02	.	01	01				
V	5.0	6.5	4.8	5.4	213.4	06.2	76	47	76	67	20	045	017.1	15	.	.	10	01	.	.	06	08	15	10	01	15	.	.	.	.	06	.					
VI	3.8	3.4	3.7	4.3	265.2	10.9	72	45	72	63	29	091	027.5	17	.	.	16	07	01	.	11	05	11	04	04	11	.	.	.	.	09	.					
VII	5.7	4.7	3.3	4.6	259.8	12.6	83	52	83	72	35	123	022.7	05	.	.	22	04	.	.	03	14	10	07	14	.	.	.	.	06	.						
VIII	5.2	5.2	4.1	4.9	233.8	12.8	89	53	82	75	37	036	014.2	14	.	.	24	01	.	.	05	04	13	06	01	13	.	.	.	.	06	.					
IX	5.8	5.8	4.1	4.9	194.3	06.0	93	54	87	78	29	044	014.9	18	.	.	01	10	.	.	01	07	09	07	02	09	.	.	.	.	02	01					
X	5.2	4.5	4.3	4.7	153.8	08.7	93	65	94	83	34	050	022.3	03	.	.	01	01	.	.	11	09	08	04	02	06	.	.	.	.	11	.					
XI	7.6	7.6	7.0	7.4	066.2	06.4	92	78	93	87	43	158	027.0	06	.	01	07	.	.	01	17	17	12	06	13	04	01	.	01	01	03	05	04				
XII	8.3	7.9	8.8	8.4	045.8	04.2	55	84	92	90	53	065	009.2	02	02	09	21	.	.	01	01	20	16	14	11	06	01	.	.	01	04	10					
GOD.	6.2	6.3	5.3	5.9	1935.5	06.0	85	58	82	75	20	826	027.9	47.VI	02	12	61	88	14	.	09	02	55	123	156	106	32	142	22	06	01	02	03	.	38	33	32
<b>SLAVONSKA POZEGA</b>																																					
<b>BR. ST. 67</b>																																					
I	6.2	7.8	6.3	6.8	-	04.8	92	81	50	88	59	064	017.8	27	01	.	21	.	.	02	12	12	08	03	10	03	01	.	.	01	08	04					
II	6.3	7.0	4.2	5.8	-	06.2	89	74	89	74	43	073	016.6	01	01	.	10	.	.	02	01	07	17	14	03	15	03	01	.	01	03	02					
III	4.6	5.1	3.4	4.4	-	07.1	51	59	84	78	24	030	016.4	30	.	.	06	03	.	.	06	06	08	05	02	07	02	.	.	.	02	01					
IV	5.2	5.8	4.2	5.1	-	07.6	88	61	86	78	36	033	005.2	06	.	.	05	03	.	.	01	05	04	09	08	09	01	.	.	01	03						
V	4.2	6.3	3.9	5.0	-	11.0	88	60	86	78	37	105	033.8	17	.	.	08	01	.	.	08	05	14	11	04	14	.	.	.	06	.						
VI	4.0	5.6	3.5	4.4	-	12.9	83	57	80	73	42	097	026.7	22	.	.	16	06	.	.	06	02	12	09	03	12	.	.	.	06	.						
VII	4.5	5.3	2.5	4.1	-	14.1	88	60	86	78	39	125	035.6	05	.	.	22	04	.	.	07	03	14	10	04	14	.	.	.	08	.						
VIII	4.5	5.8	4.2	4.6	-	13.8	51	84	87	75	42	062	026.8	12	.	.	24	01	.	.	04	04	11	07	11	11	.	.	.	01	03						
IX	4.1	5.2	3.4	4.4	-	05.9	51	60	87	79	34	056	020.6	20	.	.	01	11	.	.	01	07	08	07	02	06	.	.	.	03	01						
X	6.0	4.9	4.3	5.1	-	08.9	92	65	88	82	41	043	020.2	03	.	.	02	01	.	.	07	03	07	05	01	07	.	.	.	01	12						
XI	7.1	7.5	5.5	6.7	-	06.7	91	77	85	84	48	120	018.5	17	.	.	09	.	.	.	03	11	14	12	07	13	03	02	.	.	02	03					
XII	7.3	6.1	6.1	7.6	-	04.0	87	89	91	85	48	080	031.1	02	05	12	24	.	.	01	03	19	14	12	02	10	04	.	.	.	07	09					
GOD.	5.4	6.4	4.3	5.3	-	06.5	89	66	86	80	24	896	035.8	05.VI	07	12	78	87	12	.	06	.	57	86	140	108	33	130	15	04	.	.	.	29	40	16	
<b>SLAVONSKI BROD</b>																																					
<b>BR. ST. 68</b>																																					
I	8.8	8.8	8.2	8.6	042.0	04.6	94	80	81	56	46	042	011.5	27	01	01	21	.	.	.	07	04	15	16	13	03	01	.	.	.	16	04					
II	8.6	7.7	6.1	7.5	089.1	05.8	93	88	83	35	057	008.2	27	01	01	10	.	.	.	01	07	14	17	14	03	01	.	.	.	01	10	06					
III	6.2	7.6	4.0	5.7	176.9	06.3	53	51	78	74	22	035	012.2	30	.	.	11	03	.	.	01	06	07	12	09	01	12	02	.	.	03	01					
IV	7.3	7.3	5.2	6.6	182.6	06.6	91	50	77	73	24	034	010.5	06	.	.	04	02	.	.	06	03	01	10	08	01	10	01	.	.	01	01					
V	6.5	7.5	6.7	6.7	198.9	05.9	89	51	77	72	28	062	025.0	06	.	.	08	.	.	.	01	07	08	07	05	03	07	.	.	.	01	05					
VI	4.4	6.3	5.3	5.3	249.4	11.0	89	49	81	73	30	097	024.4	17	.	.	14	04	.	.	02	01	04	06	12	09	12	.	.	.	10	06					
VII	5.2	5.9	4.1	5.1	271.2	13.3	53	54	86	78	34	181	039.8	06	.	.	21	02	.	.	07	02	07	08	15	12	05	15	.	.	01	08	13				
VIII	5.4	5.8	5.5	5.4	225.5	13.4	97	54	88	80	37	074	022.4	24	.	.	26	04	.	.	02	01	06	07	11	08	03	11	.	.	01	07	14				
IX	5.8	5.6	5.1	5.5	208.5	08.0	95	51	87	78	28	046	014.1	18	.	.	02	11	.	.	01	01	07	08	07	05	03	07	.	.	02	15					
X	3.7	5.6	3.6	3.8	11.6	77	45	84	69	30	075	034.6	17	.	.	21	07	.	.	12	04	10	10	03	10	07	.	.	.	06	01						
XI	8.4	8.4	6.8	7.9	053																																

Mesec	Vazdušni Pritisak Fm mm	Temperatura vazduha °C						Čestina pravaca i srednja jačina veta nD, Fm (0-12)																				
		Tm	7	14	21	Sred. (Globus)	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		8.	3.	8.	J.	8.	3.	8.	J.	8.	J.	8.	3.	8.	3.	8.	3.	8.	3.									
$\gamma = 45^{\circ}42' N \lambda = 18^{\circ}44' E$ Gr. $\Delta G = + 1h 15 min.$																												
BRESTOVAC-BELJE																												
I	754.6	-00.2	04.2	01.5	01.8	04.7	-01.2	13.4	30	-16.9	01	09	01.7	08	01.0	25	01.1	14	01.7	17	01.2	08	01.4	06	02.0	06	01.5	.
II	752.8	03.1	09.2	02.3	05.7	10.3	02.0	20.0	25	-03.0	04	14	02.4	11	01.6	04	01.0	03	01.0	18	01.1	17	01.8	14	01.7	03	02.0	.
III	757.3	04.8	14.6	07.6	08.8	15.4	03.1	25.9	23	-03.5	01	11	02.5	16	01.3	14	01.0	08	01.1	11	02.1	07	01.1	10	01.4	16	01.8	.
IV	752.9	07.2	14.2	09.0	09.9	15.2	03.9	27.5	29	-01.4	16	12	02.8	17	01.6	09	01.7	06	01.3	06	01.0	05	01.4	14	01.7	21	02.9	.
V	754.0	14.8	21.4	15.1	16.6	22.1	10.7	30.1	04	03.9	26	17	02.0	12	01.5	18	01.3	16	02.4	09	01.2	08	01.4	16	01.6	03	01.0	.
VI	752.8	17.8	25.1	17.6	19.5	25.6	12.3	33.5	14	03.4	04	12	02.0	07	01.0	09	01.1	07	01.2	10	01.4	17	01.6	14	01.4	14	01.4	.
VII	752.9	18.3	24.4	18.5	19.9	25.7	14.2	30.8	08	05.7	28	16	02.1	10	01.3	11	01.1	07	01.4	03	01.3	02	01.0	27	01.1	16	01.9	.
VIII	752.9	17.2	25.8	18.0	20.1	26.4	14.3	31.1	09	07.5	26	10	01.8	09	01.7	14	01.4	11	01.0	08	01.9	17	01.6	11	01.6	.		
GOD.	755.0	08.6	15.5	10.0	11.0	16.2	04.1	38.5	44.VI	-17.6	06.XII	155	02.0	131	01.3	149	01.3	97	01.5	127	01.1	107	01.4	177	01.4	130	01.8	02
$\gamma = 45^{\circ}32' N \lambda = 18^{\circ}44' E$ Gr. $\Delta G = + 1h 15 min.$																												
CSIJEM																												
BR. ST. 72																												
I	754.6	-00.1	04.1	01.4	01.7	04.5	-01.0	15.4	30	-08.4	01	13	02.0	05	01.8	26	02.1	06	02.2	06	01.8	05	01.6	08	02.0	.		
II	751.8	03.3	09.5	02.3	05.9	10.5	03.1	20.1	25	-08.7	04	12	02.5	04	01.5	03	02.0	20	02.2	16	02.2	12	07	01.7	10	02.3	.	
III	754.8	04.8	14.9	06.6	09.2	16.0	03.4	26.9	24	-03.6	01	12	01.9	09	01.4	19	01.7	19	02.2	06	02.0	10	01.9	09	02.1	13	02.5	.
IV	752.0	07.1	14.6	09.2	10.0	15.9	04.2	28.2	29	-01.7	18	16	02.7	08	02.2	07	02.6	17	02.2	03	01.0	13	01.5	06	02.7	20	02.8	.
V	753.4	14.6	21.9	15.7	17.0	22.9	11.0	31.4	04	05.3	28	08	02.0	17	02.0	07	02.1	17	02.1	11	01.5	09	01.6	10	01.3	14	02.1	.
VI	751.8	17.6	24.8	18.2	19.7	26.0	12.9	33.1	14	04.9	02	10	01.7	11	01.6	05	01.0	08	01.1	13	01.7	15	01.6	09	01.4	19	01.9	.
VII	751.6	17.8	25.2	18.6	20.2	26.4	14.3	31.8	14	10.4	28	10	01.7	04	01.2	14	01.7	11	01.8	11	01.7	07	01.7	20	01.5	16	02.0	.
VIII	752.5	16.7	25.6	19.1	20.1	26.8	14.5	31.8	29	08.1	26	18	01.3	11	01.3	12	01.7	10	01.5	14	02.1	04	01.8	18	02.0	06	01.8	.
GOD.	754.4	08.3	15.6	10.3	11.1	16.7	06.2	39.1	44.VI	-20.1	06.XII	158	01.6	108	01.6	141	01.6	185	01.9	123	01.8	103	01.7	139	01.6	138	02.1	.
$\gamma = 45^{\circ}13' N \lambda = 19^{\circ}22' E$ Gr. $\Delta G = + 1h 18 min.$																												
ILCK																												
ER. ST. 73																												
I	-	02.0	05.7	02.4	03.2	05.5	-00.1	14.4	12	-04.8	20	06	01.2	01	01.0	10	01.5	26	01.0	10	02.1	11	01.4	07	01.6	15	01.5	07
II	-	05.1	09.8	06.1	04.8	10.5	03.2	19.0	23	-07.8	04	02	01.5	07	01.1	02	01.0	13	02.5	20	02.2	09	02.3	09	01.7	15	01.4	07
III	-	07.2	15.4	09.4	10.3	16.0	05.3	28.2	24	-04.6	01	06	01.7	04	01.0	01	01.3	14	01.6	14	01.5	19	01.6	06	02.1	14	01.5	06
IV	-	07.3	15.6	09.5	10.5	16.3	04.6	28.1	25	-02.5	01	05	01.6	11	01.3	08	01.4	14	01.6	14	01.7	10	01.5	10	01.2	04	01.4	.
V	-	07.3	15.6	09.5	10.5	16.3	04.6	29.1	19	04.7	05	03	02.0	21	01.2	13	01.5	24	01.3	15	01.5	07	01.6	03	01.2	*	*	07
VI	-	16.2	24.1	17.1	18.6	24.4	13.2	31.7	11	05.2	02	18	01.4	05	01.3	11	01.5	16	01.4	12	01.3	10	01.5	03	01.3	06	01.8	09
VII	-	18.5	25.2	18.4	20.1	25.9	15.0	33.4	31	10.1	27	04	01.2	10	01.2	07	01.3	08	01.4	08	01.4	12	01.5	26	01.5	11	01.5	11
VIII	-	19.1	25.9	18.3	20.4	26.8	14.3	31.5	09.0	07.6	26	08	01.0	14	01.8	08	01.5	15	01.3	12	01.5	14	02.1	09	01.6	02	02.1	.
IX	-	13.9	20.6	12.5	14.9	21.2	08.6	30.4	05	01.9	28	10	01.6	14	01.3	04	01.5	04	01.5	11	01.3	05	01.6	10	01.5	23	01.4	05
X	-	10.0	18.7	09.7	12.0	19.1	05.2	25.5	09.6	-02.2	16	07	01.0	14	01.1	05	01.0	12	01.8	10	01.6	08	01.5	10	01.5	10	01.7	05
XI	-	04.9	09.6	05.9	06.6	10.5	02.6	22.5	12	-05.1	30	05	01.0	07	01.3	*	*	11	02.0	16	01.6	16	01.1	07	01.9	10	01.3	16
XII	-	-01.3	01.4	-00.7	-00.3	02.1	-03.4	10.3	28	-16.8	03	09	01.0	11	01.3	08	01.6	17	01.9	07	02.4	05	01.4	15	01.8	07	01.6	14
GOD.	-	09.2	15.6	09.8	11.1	16.2	06.1	33.4	34.VI	-10.8	05.0	23	10	01.2	77	01.4	179	01.7	155	01.7	119	01.5	114	01.6	150	01.5	99	.
$\gamma = 44^{\circ}52' N \lambda = 13^{\circ}51' E$ Gr. $\Delta G = + 55 min.$																												
PULJA																												
BR. ST. 74																												
I	-	07.0	09.3	07.5	07.8	10.5	04.8	13.2	29	-00.6	20.19	02	03.0	14	02.5	10	02.1	13	03.7	10	03.1	02	04.5	*	*	11	02.7	31
II	-	06.8	10.7	07.8	08.2	11.6	05.3	15.3	20	-00.7	04	02	01.0	15	02.9	08	02.0	22	02.5	02	01.5	04	03.2	01	01.0	07	02.6	29
III	-	07.7	13.0	09.1	09.7	14.3	05.9	19.0	22	-01.6	01	03	01.0	11	04.1	06	01.8	30	02.3	03	02.3	03	02.0	*	*	05	02.8	32
V	-	15.5	19.5	15.2	16.3	20.9	11.6	24.7	21	06.9	11	01	0.0	64	03.0	19	04.2	28	02.1	*	*	01	02.4	20	02.3	20	02.0	21
VI	-	13.8	23.8	19.6	20.4	24.9	15.6	30.6	13	10.1	04	03	00.9	15	04.0	12	02.4	17	02.2	03	02.0	10	02					



Mesec	Vazdušni pritisak Pn mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nd, Fm (0-12)																								
		Tm				Max.				Min.				Dat.				N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (dies)	Max	Min	Max	Dat.	Min	Dat.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.				
$\varphi = 44^{\circ}32' N \lambda = 14^{\circ}28' E$ Gr. $\Delta G = + 58$ min.																		MALI LOSINJ												BR. ST. 76				
I	756.6	08.8	10.1	09.2	09.3	11.1	07.6	14.3	12	02.7	19	16	02.9	07	04.1	01	03.0	34	03.6	08	03.2	10	03.4	06	02.5	03	02.0	08						
II	755.1	05.1	11.3	09.6	09.9	12.3	08.2	16.5	24	03.3	28	13	03.4	11	03.4	05	02.4	09	03.6	24	03.0	14	02.9	01	01.0	03	01.3	04						
III	760.1	10.3	13.9	11.4	11.8	14.5	09.4	20.3	23	02.4	01	06	02.0	16	02.8	09	02.4	18	03.2	13	02.5	13	02.5	06	02.3	02	02.0	10						
IV	755.3	11.3	15.1	12.0	12.6	15.9	09.6	21.2	29	05.3	10	10	04.1	12	03.1	07	02.3	16	02.9	25	02.9	10	02.6	06	02.0	02	03.5	02						
V	756.3	15.9	19.5	16.4	17.1	21.2	14.1	24.6	26	16.0	09	09	03.3	17	02.6	18	02.4	08	03.0	19	02.9	05	02.4	14	02.7	01	02.0	04						
VI	755.6	15.8	24.1	20.0	21.0	25.9	17.8	30.7	02	13	02.3	01	11	02.5	19	02.5	05	01.8	01	03.0	22	03.0	14	02.2	14	02.7	04	02.0	04					
VII	754.9	22.0	26.5	22.5	23.4	28.0	15.9	32.6	13	15.8	27	14	02.2	20	02.3	09	01.7	05	03.0	20	02.1	10	02.4	12	01.9	02	02.0	01						
VIII	754.9	21.2	25.5	22.1	22.7	26.4	19.7	29.8	08	15.5	24	17	02.1	19	01.6	09	01.7	04	02.5	14	03.4	14	02.4	11	01.7	05	02.2	.						
IX	759.3	17.4	21.3	17.8	18.6	22.3	16.0	26.7	05	16.3	18	40	02.6	19	02.5	06	02.5	02	02.5	03	02.0	07	02.0	09	02.3	04	02.0	.						
X	760.8	15.2	19.2	16.0	16.6	19.9	14.5	23.0	08	11.7	03	23	02.0	13	02.2	09	01.9	12	02.7	14	03.2	06	01.8	14	01.9	02	02.0	.						
XI	761.7	11.7	13.2	11.9	12.2	14.7	10.1	18.7	05	05.1	27	18	02.9	15	03.5	06	02.8	08	03.6	19	03.1	04	02.8	13	02.5	07	02.4	.						
XII	760.4	07.9	09.6	08.1	08.4	10.5	06.6	13.9	03	35	03.5	19	04.3	05	03.2	05	02.6	02	01.5	06	02.3	11	01.5	07	02.5	.								
GOD.	757.0	14.2	17.4	14.8	15.3	18.6	12.8	32.6	19.VII	00.4	04	212	02.8	187	02.8	89	02.3	125	03.2	186	02.9	105	02.4	112	02.3	46	02.2	33						
$\varphi = 44^{\circ}45' N \lambda = 14^{\circ}46' E$ Gr. $\Delta G = + 59$ min.																													BR. ST. 77					
I	759.5	08.6	10.5	08.9	09.2	11.6	06.8	15.2	29	00.5	19	12	01.6	07	02.3	01	01.0	47	04.6	09	02.6	02	0.5	01.7	01.3	01.3	01	01.3	11					
II	758.0	08.7	11.9	09.2	09.8	13.3	07.3	23.0	09	01.0	04	09	01.9	11	01.7	04	01.2	40	03.6	02	0.5	01.7	01.3	01.3	01.3	01.3	01.3	01.3	01.3	01.3	01.3			
III	763.0	09.6	14.9	10.8	11.5	15.7	08.0	23.1	26	00.7	01	11	01.6	14	01.6	08	01.9	19	03.3	10	01.9	06	01.3	03	01.3	01.3	01.3	01.3	01.3	01.3				
IV	758.2	10.8	15.5	11.4	12.3	16.7	08.4	22.6	30	02.1	12	01.8	02.3	05	02.3	12	03.1	11	02.0	08	02.2	03	01.8	01.8	01.8	01.8	01.8	01.8	01.8	01.8	01.8			
V	758.9	16.1	20.8	16.5	17.5	22.1	13.4	26.0	02	08.8	09	10	01.7	09	02.3	04	02.5	15	02.8	07	02.6	08	02.1	09	02.0	10	01.5	18						
VI	756.3	24.2	24.2	20.0	21.0	25.1	17.1	29.2	13	12.1	03	12	02.6	04	04.5	07	02.4	20	02.4	05	02.4	12	01.9	06	02.3	07	02.1	17						
VII	757.6	21.6	26.6	22.2	23.2	26.0	19.1	31.9	13	14.7	27	15	02.1	09	02.1	06	01.8	23	02.6	09	02.6	09	02.1	05	02.4	09	02.7	08						
VIII	757.7	20.3	26.1	21.1	22.2	27.1	16.3	32.1	29	14.3	25	17	01.8	11	01.2	05	01.6	16	03.2	05	02.8	08	02.0	06	02.2	08	01.8	17						
IX	762.1	14.6	22.9	17.1	18.4	23.7	14.7	30.9	06	07.7	29	07	01.7	27	01.6	13	02.8	06	02.8	08	02.0	08	01.5	09	01.9	09	01.6	09						
X	763.6	14.4	20.0	15.2	16.2	20.7	13.2	24.0	13	08.7	03	11	01.5	15	03.0	07	01.7	21	03.6	04	02.5	08	01.4	06	01.5	04	01.8	17						
XI	757.8	10.6	14.0	10.9	11.6	15.1	08.6	20.0	07	03.0	29	14	02.1	20	02.5	06	02.0	26	04.4	03	02.3	01	01.0	05	02.4	08	01.6	07						
XII	763.1	06.5	11.0	07.0	07.8	12.0	04.9	16.5	23	14	01.4	23	16	02.1	24	02.4	05	01.2	24	04.0	05	01.4	02	01.0	04	01.8	15	02.0	02					
GOD.	759.8	13.7	17.3	16.2	14.2	15.1	19.3	11.6	32.1	29.VII	00.5	49	151	01.9	164	02.0	71	02.1	274	03.6	77	02.3	70	01.8	61	02.0	93	01.2	134					
$\varphi = 44^{\circ}59' N \lambda = 14^{\circ}54' E$ Gr. $\Delta G = + 1h 00$ min.																			SENJ		BR. ST. 78													
I	758.9	08.3	09.8	08.5	08.6	11.3	06.4	17.2	29	00.5	19	02	02.0	14	04.7	24	03.8	15	02.9	15	03.3	07	03.4	03	02.7	08	01.6	05	01.5	05				
II	757.3	08.4	11.0	09.1	09.4	12.4	07.1	18.7	23	00.4	03	03	02.0	13	04.9	19	03.9	18	02.8	13	03.0	06	03.2	01	02.0	05	02.2	06	01.2	06				
III	762.5	10.0	14.0	10.4	11.5	15.5	08.1	24.0	26	-01.3	31	06	02.0	10	05.3	23	03.9	20	02.0	06	02.4	05	01.5	05	01.2	06	01.1	01	01.1	11				
IV	757.6	10.0	15.1	11.4	12.0	16.5	08.0	23.8	30.9	03.5	12	01.3	03.0	01	03.0	28	04.1	07	04.0	08	03.4	06	03.3	26	03.2	04	02.2	04						
V	758.5	15.7	19.8	16.7	17.2	21.5	13.5	26.0	20	08.0	09	04	01.8	10	07.3	30	03.8	16	02.2	06	02.7	05	02.0	04	01.2	11	01.9	05						
VI	757.4	19.4	24.1	20.3	21.1	25.2	17.4	30.3	12	10.6	01	04	02.0	12	03.8	19	03.9	18	02.8	13	03.0	08	02.4	07	01.9	13	01.7	05						
VII	757.1	21.3	25.9	22.6	23.1	27.4	19.1	30.9	13	14.2	27	02	02.0	18	04.4	27	03.8	20	02.6	07	02.4	09	02.1	03	10	02.2	02	02	02					
VIII	757.1	26.0	22.0	22.7	23.0	27.0	19.1	31.0	07	15.5	25.4	04	02.6	11	05.3	30	03.2	19	02.2	09	02.2	09	01.7	04	01.8	05	01.8	05						
IX	761.6	14.1	21.4	17.1	17.9	22.3	14.7	30.5	07	06.7	18	01	02.0	29	05.6	41	04.8	08	02.6	04	01.0	02	01.5	03	01.7	03	01.7	02						
X	762.1	15.8	19.2	15.8	16.4	20.2	13.6	23.2	09	07.0	02	05	02.4	19	04.6	23	03.8	12	02.1	10	02.6	05	03.0	02	01.0	06	02.3	06						
XI	757.																																	

Meseč	Oblačnost Nm (0-10)			Vlažnost vazduha % mm	Padavine R mm	Broj dana na sat																					
	7	14	21			Tn	Tx	Tx	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	A	A	R	T	III	II				
	Sred. (Dnev.)	Sred. (Dnev.)	Sred. (Dnev.)			7	14	21	Sred. Min	Max	Dat.	IV	IV	IV	IV	V	VI	VI	VI	VI	VI	VI	VI				
<b>MALI LESINJ</b>																											
BR. ST. 76																											
I	8.0	8.0	7.3	7.8	062.0	07.0	83	74	78	75	46	138	025.1	03	.	.	.	.	.	04	20	17	16	05	17		
II	7.2	6.7	6.6	6.9	109.5	07.4	82	72	72	72	39	134	038.5	22	.	.	.	.	.	05	03	12	16	13	04	16	
III	6.3	6.6	4.9	6.0	145.5	07.9	80	68	72	73	39	040	021.0	31	.	.	.	.	.	05	09	08	04	01	08	.	
IV	5.9	5.9	4.1	5.3	240.1	07.1	65	67	64	28	115	066.0	09	.	.	.	.	.	.	07	08	05	03	06	.	03	
V	5.9	5.4	4.7	5.4	273.5	10.1	75	55	74	69	29	043	014.0	06	.	.	.	.	.	02	07	09	12	09	01	12	
VI	5.0	4.1	3.7	4.3	318.0	12.2	72	72	71	64	21	014	006.0	27	.	.	.	.	.	02	04	04	02	00	.	02	
VII	3.7	3.0	2.6	3.1	345.4	14.1	72	52	50	65	27	046	011.4	27	.	.	.	.	.	04	16	12	02	09	09	01	
VIII	4.7	4.7	3.8	4.4	265.0	14.2	76	56	73	69	38	066	015.5	14	.	.	.	.	.	06	07	05	11	09	03	11	
IX	3.6	2.5	3.3	3.3	248.8	10.6	70	52	73	65	31	071	019.4	18	.	.	.	.	.	06	03	17	05	06	03	06	
X	5.2	4.7	2.7	4.2	180.6	11.0	82	67	83	77	38	038	016.2	11	.	.	.	.	.	09	03	05	04	02	05	.	
XI	6.8	7.0	6.8	6.9	098.2	07.8	72	70	75	35	096	029.7	17	.	.	.	.	.	02	01	02	14	11	09	04		
XII	5.0	5.2	4.1	4.7	138.6	05.8	68	64	72	68	32	131	047.5	29	.	.	.	.	.	09	03	08	08	04	08	.	
GOD.	5.6	5.4	4.5	5.2	2420.0	05.6	75	61	74	69	21	932	066.0	09.IV	.	.	.	.	.	81	06	41	40	05	91	96	
<b>RAB</b>																											
BR. ST. 77																											
I	8.1	8.1	6.8	7.7	066.3	04.5	83	72	78	77	24	131	018.3	13	.	.	.	.	.	11	08	03	20	19	17	07	
II	7.7	7.2	6.8	7.2	107.4	06.8	79	65	75	73	-	117	032.2	01	.	.	.	.	.	07	03	02	16	13	03	13	
III	6.5	6.0	5.1	6.4	161.8	07.4	80	60	76	72	30	091	038.3	13	.	.	.	.	.	02	01	03	10	06	05	04	
IV	6.1	5.9	3.5	5.2	235.3	03.6	73	61	68	61	29	126	071.1	06	.	.	.	.	.	02	07	05	08	06	04	08	
V	5.8	5.8	4.2	5.3	261.1	09.8	74	55	67	65	31	032	014.2	09	.	.	.	.	.	02	03	01	05	07	05	02	
VI	5.8	4.7	3.8	4.4	298.0	11.7	68	62	65	62	29	025	016.3	27	.	.	.	.	.	16	01	01	03	07	04	01	
VII	3.9	3.5	3.1	3.6	321.6	13.3	69	53	65	62	26	174	077.2	26	.	.	.	.	.	28	04	08	04	11	03	12	
VIII	5.1	5.8	3.8	4.7	268.8	13.8	78	55	72	68	37	160	045.4	23	.	.	.	.	.	25	03	06	02	01	09	12	
IX	4.2	4.0	2.9	3.7	242.3	09.7	67	46	63	59	28	048	019.4	18	.	.	.	.	.	11	03	02	14	06	07	04	
X	5.8	4.7	2.1	4.2	196.7	10.3	81	62	78	74	25	065	038.4	03	.	.	.	.	.	03	09	02	07	04	02	07	
XI	7.0	6.6	6.6	6.8	103.3	07.6	74	63	75	70	29	117	033.6	02	.	.	.	.	.	06	05	02	12	10	08	16	
XII	5.1	5.4	3.9	4.8	149.5	05.3	71	57	67	65	22	112	035.0	29	.	.	.	.	.	06	04	12	09	10	07	04	
GOD.	5.6	5.7	4.4	5.3	2412.1	05.1	73	57	70	67	-	-	1198	077.2	26.VN	.	.	.	.	.	83	12	17	47	23	84	100
<b>SENIJ</b>																											
BR. ST. 78																											
I	8.3	8.1	7.5	7.9	059.0	06.1	73	64	70	70	41	105	015.6	13	.	.	.	.	.	12	02	02	20	17	14	04	
II	8.2	6.6	6.5	7.7	085.9	06.2	71	63	68	67	24	118	028.8	01	.	.	.	.	.	06	04	02	11	15	13	05	
III	7.1	7.0	4.8	6.3	154.6	06.5	65	56	66	64	27	066	028.7	30	.	.	.	.	.	04	03	05	02	05	02	01	
IV	6.6	6.3	4.2	5.7	202.0	06.0	62	45	60	56	22	174	045.4	09	.	.	.	.	.	10	03	04	16	10	06	05	
V	5.8	6.3	4.0	5.4	222.1	08.7	65	51	60	55	22	034	016.2	09	.	.	.	.	.	02	10	06	07	10	07	01	
VI	4.7	5.2	4.9	4.9	262.8	11.0	65	48	61	58	26	055	026.4	26	.	.	.	.	.	14	02	05	05	01	07	08	
VII	4.1	4.1	3.1	3.8	289.1	12.1	61	45	59	58	32	114	033.2	27	.	.	.	.	.	26	03	09	08	02	17	04	
VIII	4.6	5.0	3.8	4.6	254.1	12.9	71	50	67	63	31	125	030.4	19	.	.	.	.	.	24	03	11	07	10	09	12	
IX	4.2	4.3	3.2	3.9	230.1	08.9	63	47	51	56	27	047	016.5	18	.	.	.	.	.	11	01	08	17	08	06	08	
X	5.5	5.3	3.6	4.8	172.4	09.3	72	52	66	67	27	028	011.6	03	.	.	.	.	.	11	01	08	10	07	04	01	
XI	7.0	6.8	6.8	7.1	097.0	07.0	70	63	71	68	30	275	012.1	06	.	.	.	.	.	15	05	03	15	11	11	06	
XII	5.2	5.7	5.2	5.3	120.8	04.4	61	58	61	60	24	118	037.6	29	.	.	.	.	.	18	12	09	10	11	10	04	
GOD.	6.0	6.1	4.8	5.6	2149.6	08.8	63	54	64	62	22	1260	112.1	06.XI	.	.	.	.	.	09	09	33	124	47	81	123	
<b>ZAVIŽAN</b>																											
BR. ST. 79																											
I	8.5	6.5	8.1	8.6	049.6	03.6	95	55	53	54	49	173	027.7	04	02	12	29	.	.	11	01	01	23	27	21	06	
II	8.8	8.5	7.9	8.4	053.3	03.6	91	90	86	90	24	128	028.8	01	03	10	24	.	.	12	03	01	20	19	16	04	
III	6.6	6.1	4.6	5.6	164.3	03.5	72	63	70	66	22	113	035.6	31	04	04	17	.	.	02	01	04	08	09	08	04	
IV	5.7	6.7	4.9	5.4	196.6	03.8	81	72	65	76	29	160	042.2	10	.	05	20	.	.	06	02	08	13	05	04	11	
V	6.5	7.1	5.4	6.3	206.8	05.5	77	72	76	75	27	067	013.5	06	.	.	.	.	.	05	03	11	01	02	04	02	
VI	4.7	4.6	3.9	4.4	255.0	10.1	67	52	66																		

Mjesec	Vruditni Pm mm	Temperatura vazduha °C						Cestina pravaca i srednja jačina vетра mB, Fm (0-12)																							
		Tm			Sred. (Dnev)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW						
		7	14	21							8.	3.	8.	3.	8.	3.	8.	3.	8.	3.	8.	3.	8.	3.	8.	3.					
$\varphi = 44^{\circ}08' N \lambda = 15^{\circ}13' E$ Gr. $\Delta G = +1h\ 01\ min.$																															
I	761.1	08.0	10.9	08.6	09.0	11.6	06.3	14.8	29 -00.1	19 05	01.6	04	01.8	14	01.6	44	02.5	06	03.5	02	02.0	01	03.0	08	02.9	09					
II	759.5	08.4	11.9	09.3	08.8	13.1	07.2	16.6	11 06.0	04	08	02.1	09	02.2	03	01.3	31	02.7	06	03.2	01	02.0	04	02.8	07	02.3	15				
III	764.2	09.3	14.6	10.5	11.4	15.3	08.3	22.0	23 00.2	01	02	01.0	05	03.6	06	02.3	20	02.5	05	02.1	01	02.4	03	01.7	17	02.2	34				
IV	759.6	10.8	15.5	11.7	12.4	16.3	04.5	22.0	29 02.4	04	02.0	03	01.3	23	01.9	05	03.0	01	02.0	02	02.0	19	02.4	19							
V	760.3	14.3	20.1	16.4	17.3	21.4	13.0	25.3	18 05.4	06	02	01.5	05	01.8	04	02.0	16	02.4	02	01	02.0	*	*	*	10	02.3	31				
VI	759.5	19.6	23.7	19.6	20.6	24.9	14.2	24.8	13 16.7	02	07	01.6	04	01.5	04	01.0	14	02.1	05	02.7	02	02.5	03	02.0	25	02.6	26				
VII	758.8	22.1	24.1	21.8	23.0	27.5	16.7	31.3	13 18.4	22	09	01.9	05	03.0	02.0	01.9	03	01.7	*	*	*	06	01.8	24	02.3	29					
VIII	758.8	20.9	25.4	21.5	22.3	26.5	16.7	30.4	14 04.3	24	05	02.0	04	02.5	04	02.0	15	02.6	05	03.0	*	*	*	08	02.2	20	02.4	32			
IX	762.1	15.7	21.8	17.1	17.9	22.9	14.1	29.2	05 08.0	29	06	01.8	07	02.4	12	01.4	12	01.5	02	01.5	*	*	*	03	03.0	18	02.6	30			
X	764.8	13.8	19.5	15.0	16.0	20.2	12.7	24.5	13 05.5	17	01	02.0	01	02.0	09	01.8	11	02.8	07	03.4	*	*	*	04	01.8	13	02.0	47			
XI	755.2	10.1	14.1	11.1	11.6	15.4	08.4	21.0	06 02.8	29	10	02.9	12	02.3	09	02.1	16	02.6	06	03.2	*	*	*	03	02.3	15	02.1	19			
XII	764.4	05.9	11.1	07.0	07.8	12.1	04.4	14.6	20.9	00.0	23	09	02.3	10	02.1	14	01.5	21	02.8	02	02.0	*	*	*	02	02.0	11	02.5	24		
GOD.	761.1	13.4	17.9	14.2	14.9	18.9	11.4	31.3	15.VII -00.1	49.1	76	02.1	65	02.2	85	01.7	244	02.4	68	02.7	08	02.1	39	02.2	195	02.4	315				
$\varphi = 44^{\circ}48' N \lambda = 15^{\circ}19' E$ Gr. $\Delta G = +1h\ 01\ min.$																															
V	-	02.9	05.1	03.1	03.6	06.6	00.3	13.3	29 -12.1	01	06	01.2	05	01.6	01	01.0	15	02.5	20	03.2	12	02.0	01	01.0	24	01.2	69				
II	-	03.3	07.4	04.2	04.8	08.5	01.0	16.0	24 -11.9	03	09	01.3	01	01.0	*	*	10	02.2	21	02.7	08	02.0	04	02.0	19	01.5	12				
III	-	02.5	13.6	05.6	06.8	14.6	00.2	24.3	23 -07.5	01	12	01.4	01	01.0	01	02.0	08	01.5	13	02.3	05	02.0	02	01.0	28	01.4	23				
IV	-	04.3	13.3	06.3	07.5	14.6	01.2	25.2	30 -04.8	01	14	01.6	01	01.3	01	01.0	12	01.4	08	01.8	10	01.4	02	01.0	26	01.4	11				
V	-	10.1	15.0	09.8	12.2	20.1	05.5	25.8	04 -00.6	29.0	06	01.8	05	01.4	01	01.0	04	01.5	13	02.3	12	01.4	07	01.0	28	01.2	15				
VI	-	13.8	22.2	13.2	15.6	23.6	08.4	31.1	13 -00.1	04.0	10	01.7	09	01.4	04	01.0	06	01.7	06	01.3	10	01.3	20	01.2	15						
VII	-	15.7	23.8	14.5	17.1	25.4	10.2	30.1	14 06.4	04	13	01.4	06	01.0	01	00.6	02.0	01.1	06	02.2	11	02.5	04	01.2	27	01.4	20				
VIII	-	14.6	23.6	14.3	16.7	24.7	11.0	27.4	17 04.1	23	14	01.2	05	01.2	06	02.0	02	03.1	13	01.4	07	01.0	18	01.3	21						
IX	-	08.6	18.1	09.6	11.1	18.9	05.7	26.6	08 -02.9	25	14	01.7	05	02.0	03	02.0	*	*	02	01.0	01	02.0	02	01.0	38	01.1	25				
X	-	07.1	16.2	08.4	10.0	17.1	04.6	22.6	07 -02.1	19.0	12	01.2	05	01.8	01	01.0	07	01.3	10	02.6	07	02.3	02	01.0	17	01.3	32				
XI	-	03.4	08.0	03.8	04.7	09.0	00.5	21.0	12 -11.8	28	09	01.3	01	01.0	*	*	13	02.2	13	02.0	11	02.0	02	01.0	25	01.3	16				
XII	-	-C3.0	01.4	-02.0	-01.4	02.2	-05.2	10.5	25 -18.4	06	12	01.5	03	02.3	01	01.0	C1	01.0	13	02.5	03	01.0	03	01.0	36	01.4	21				
GOD.	-	06.9	14.3	07.5	09.1	15.4	03.5	31.1	15.VII -18.4	06.xv	133	01.4	52	01.6	24	01.2	79	01.9	132	02.5	103	01.9	46	01.2	306	01.3	220				
$\varphi = 44^{\circ}33' N \lambda = 15^{\circ}22' E$ Gr. $\Delta G = +1h\ 02\ min.$																															
V	-	09.4	17.7	11.7	12.6	18.6	05.7	24.6	04 -01.0	06	16	02.1	02	01.5	03	02.0	09	01.6	09	02.2	08	02.3	07	02.3	08	01.9	31				
VI	711.8	12.8	23.0	16.7	17.7	24.3	10.4	28.7	30 05.0	28	13	02.3	04	03.0	02.0	02.0	14	02.8	05	01.6	15	02.4	04	02.5	05	02.2	36				
VII	711.8	14.3	23.0	16.2	17.7	24.3	10.4	28.7	30 05.0	28	13	02.3	04	03.0	01	01.0	01	02.0	08	01.6	13	02.4	04	02.5	05	02.2	36				
VIII	711.7	13.1	22.8	16.4	17.0	23.7	10.6	28.6	30 03.0	25	09	01.7	05	01.8	02	01.5	01	02.0	07	02.3	18	01.9	07	01.9	03	01.3	40				
IX	-	08.6	17.7	11.7	12.6	18.2	05.0	25.7	08 -04.9	29	25	02.4	05	03.4	*	*	01	01.0	02	01.5	03	01.7	07	01.1	36						
X	716.5	05.2	15.7	08.7	16.6	19.6	03.4	21.0	04 11	01.9	03	02.7	01	02.0	04	01.8	07	01.0	05	01.9	18	01.9	08	01.2	05	01.3	33				
XI	-	02.8	07.5	04.0	04.6	09.2	00.2	20.2	11 -11.7	28	15	01.7	03	01.3	01	02.0	14	02.0	08	02.5	11	02.4	04	02.8	06	02.2	28				
XII	-03.8	01.4	-02.2	-01.7	02.4	-06.1	03.1	29 -18.3	05	23	02.4	06	01.7	*	*	15	03.6	02	02.5	04	01.8	02	02.0	18	01.6	33					
GOD.	-	06.6	14.0	09.4	09.8	15.4	04.4	30.2	30.VIII -13.5	06.xv	195	01.8	27	01.2	47	01.1	122	01.7	50	02.7	125	01.6	149	01.3	90	01.3	246				
$\varphi = 44^{\circ}18' N \lambda = 15^{\circ}51' E$ Gr. $\Delta G = +1h\ 05\ min.$																															
I	-	02.3	04.9	03.5	03.6	06.2	00.5	11.6	27 -04.5	19	09	02.1	14	02.5	02	02.0	11	02.1	16	02.1	*	*	*	*	06	02.3	35				
II	-	02.9	06.8	04.5	04.7	08.6	01.3	15.5	25 -13.0	04	09	01.6	03	02.0	04	01.0	12	01.2	16	03.6	10	02.5	11	01.4	07	01.1	14				
III	-	03.3	13.0	07.9	08.0	14.3	01.9	22.6	26 -04.3	01	13	01.5	02.0	01.0	05	01.0															

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha e <sub>m</sub> mm	Padavine R mm	Broj dana na sat														•	*	*	Δ	∞	▲	■	T	≡	█							
						L m %			Tn Tx Tn Tx Tx			F(0-12) Nm(0-10)			R mm			•	*	*	Δ	∞	▲	■	T	≡	█									
	7	14	21	Sred. (Dnes)	Sred. (Dnes)	Min	Σ	Max	Dat.	30.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.010.0	•	Δ	*	Δ	∞	▲	■	T	≡	█								
<b>ZADAR</b>																																				
<b>BR. St. 81</b>																																				
I	7.8	8.0	6.4	7.4	052.8	07.3	65	78	82	43	077	015.3	27	•	•	01	•	•	04	16	15	14	03	15	•	•	•	02								
II	7.4	6.8	4.9	6.4	114.3	07.7	77	75	65	62	26	078	024.6	16	•	•	•	•	01	11	13	11	02	13	•	•	•	03								
III	5.7	5.6	3.8	5.1	172.7	08.4	86	73	85	81	57	042	014.4	13	•	•	•	•	01	07	06	05	02	06	•	•	•	02								
IV	5.4	5.2	3.9	4.8	242.0	07.9	76	62	76	72	34	055	015.8	09	•	•	•	•	05	04	07	07	03	07	•	•	•	01								
V	4.8	5.1	3.5	4.5	266.2	11.5	81	65	80	77	40	052	019.0	27	•	•	02	•	01	09	04	11	08	01	11	•	•	•	06							
VI	3.7	4.8	3.8	4.1	274.7	13.8	75	63	80	74	45	014	007.2	26	•	•	17	•	03	09	03	06	04	06	•	•	•	04								
VII	3.6	2.6	2.5	2.9	352.2	16.3	76	65	84	74	44	077	031.0	27	•	•	28	01	08	12	06	04	03	06	•	•	01	05								
VIII	4.5	4.5	2.5	3.8	257.2	15.8	83	66	83	77	42	046	012.4	24	•	•	24	01	10	02	•	03	04	13	09	01	13	•	05							
IX	3.5	3.8	2.6	3.3	239.6	11.7	78	63	77	73	27	068	023.6	03	•	•	08	•	01	13	04	07	07	02	07	•	•	•	01							
X	3.5	3.7	2.3	3.2	207.5	11.5	86	76	87	83	51	077	036.1	11	•	•	•	•	02	04	10	03	05	06	•	•	03	03								
XI	6.7	6.5	5.1	6.1	161.3	08.2	73	76	76	73	23	022.7	02	•	•	•	•	02	03	08	11	11	04	11	•	•	01	01								
XII	4.3	4.5	3.3	4.0	152.8	05.6	71	62	70	67	26	051	027.2	29	•	•	•	•	03	14	06	10	03	10	•	•	•	•								
GOD.	5.1	5.1	3.7	4.6	2423.3	10.5	80	68	80	76	28	776	036.1	44x	•	•	01	79	02	19	14	•	95	68	111	93	27	111	•	•	01	31	07			
<b>LITKOV LESJE</b>																																				
<b>BR. St. 82</b>																																				
I	6.4	6.5	7.4	8.1	-	35.0	85	79	83	80	60	146	030.6	13	01	•	18	•	07	•	20	23	16	05	20	05	01	02	01	•	02	05				
II	6.2	7.3	7.1	7.5	-	35.2	80	71	83	78	44	136	031.8	22	02	03	13	•	02	12	19	14	05	18	03	•	•	•	04	08	05					
III	5.8	4.6	3.5	4.6	-	35.4	85	50	82	72	22	073	019.9	13	•	17	•	01	07	05	09	06	03	09	02	•	•	06	02	•	•					
IV	6.0	5.6	4.3	5.3	-	35.5	79	52	79	70	26	105	035.4	06	•	14	01	•	•	07	07	10	08	04	08	06	02	•	01	05	05					
V	6.4	6.3	4.4	5.7	-	38.2	84	56	82	74	28	042	009.3	15	•	02	04	•	02	03	06	12	08	•	12	•	•	03	12	•	•	03	12			
VI	4.6	4.9	3.1	4.2	-	39.3	80	47	60	69	28	048	017.5	27	•	02	14	01	•	03	05	13	10	04	22	06	02	10	•	01	06	06				
VII	6.5	6.5	3.4	4.8	-	10.9	82	53	73	83	32	142	055.5	27	•	03	19	01	•	03	05	13	10	04	13	•	•	01	11	18	•	•				
VIII	7.7	7.4	4.2	5.6	-	11.4	90	55	50	78	39	114	027.0	23	•	16	•	02	•	02	15	11	05	15	•	•	01	08	13	•	•					
IX	9.1	4.9	3.7	5.5	-	38.4	90	42	90	80	29	071	035.5	20	•	03	06	•	01	02	09	05	05	02	06	•	•	01	15	•	•	01	15			
X	8.2	5.0	3.4	5.7	-	37.7	89	65	87	80	34	062	022.5	03	•	06	•	•	02	01	01	09	07	06	03	07	•	•	01	15	•	•	01	15		
XI	8.3	7.4	6.5	7.4	-	35.7	84	71	90	83	48	144	039.5	14	01	01	15	•	02	13	16	12	04	11	09	03	02	•	02	11	05					
XII	7.6	6.3	6.8	6.9	-	33.8	86	82	87	85	64	119	034.3	29	06	09	26	•	02	04	17	14	09	05	11	01	01	01	10	09	09					
GOD.	7.2	5.8	4.5	6.0	-	37.2	84	64	84	77	22	1202	055.5	27.VII	10	13	116	60	02	•	22	01	39	105	157	111	44	143	34	07	02	04	03	39	116	31
<b>CCSPIC</b>																																				
<b>BR. St. 83</b>																																				
I	9.0	8.2	7.5	8.5	-	035.3	05.0	93	85	91	90	62	133	025.5	12	•	01	19	•	04	•	01	22	16	05	16	02	01	•	01	02	09	10			
II	8.9	6.1	6.9	8.0	-	066.6	05.1	87	73	85	62	42	159	038.9	01	02	03	14	•	05	•	01	17	16	14	05	15	03	02	•	01	05	08	09		
III	6.8	6.5	4.2	5.8	-	174.0	05.3	94	50	79	74	22	104	026.6	30	•	17	•	•	03	05	09	07	04	08	02	02	02	04	08	02	02				
IV	6.1	6.1	4.4	5.9	-	195.7	05.3	86	62	66	26	148	022.3	15	•	13	•	•	01	04	05	09	10	08	04	07	02	01	01	01	05	05				
V	5.7	6.9	5.0	5.9	-	221.4	07.9	88	52	78	73	27	119	077.6	15	•	03	•	•	02	04	08	11	08	03	11	•	•	01	02	01	01	01	01		
VI	4.5	5.8	4.6	5.0	-	261.7	09.3	85	51	72	65	35	040	015.3	26	•	03	•	01	05	01	08	06	06	08	01	00	10	08	01	00	08	08			
VII	5.0	4.9	3.5	4.5	-	291.8	10.6	86	50	79	72	34	141	052.2	27	•	03	16	•	06	04	09	06	03	09	07	01	01	08	09	05	04	07	08		
VIII	6.0	5.5	3.2	4.9	-	238.3	11.0	93	52	84	77	34	110	038.0	21	•	12	•	•	02	06	04	14	11	06	04	11	•	•	07	10	08	04	05	04	
IX	5.8	5.1	4.4	5.1	-	06.4	93	61	80	78	26	141	059.7	20	•	02	06	•	•	08	09	09	06	05	09	•	•	01	02	03	03	01	01			
X	6.0	5.2	3.8	5.1	-	08.0	85	57	68	82	31	114	043.9	11	•	04	•	•	04	06	08	07	07	08	06	08	07	01	01	02	03	01	01			
XI	6.1	7.0	6.6	7.2	-	06.1	89	68	84	77	25</																									

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Mesec	Vazduhni prstenski Pm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, Pm (0-12)																	
		Tm			Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C							
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\varphi = 43^{\circ}44' N \lambda = 15^{\circ}55' E$ Gr. $\Delta G = + 1h 04 min.$																											
I	755.0	08.0	11.0	08.7	09.1	12.0	06.0	15.8	27 -00.1	19	13	04.2	05	01.6	14	03.4	29	03.9	09	03.6	01	04.0	.	.	.	.	22
II	753.4	08.6	12.4	09.4	10.0	13.5	06.4	18.0	23 -00.6	03	15	03.9	06	03.0	15	04.5	11	03.9	03	01.0	05	01.6	02	01.5	20		
III	756.1	09.6	15.8	12.2	12.5	17.0	08.0	26.2	23 -00.4	01	06	03.5	05	05.6	01	02.0	17	04.3	06	03.7	05	01.6	10	02.2	03	03.0	38
IV	753.2	10.7	16.1	12.7	12.7	17.5	08.0	26.6	29 04.1	12	22	03.9	11	03.9	10	02.0	10	05.1	03	04.0	08	02.4	07	02.6	.	.	28
V	754.2	17.1	21.9	17.4	18.4	23.4	13.4	25.0	19 09.1	07	15	02.9	13	03.5	06	03.2	06	03.6	13	03.3	05	03.0	09	02.7	.	.	24
VI	753.2	19.9	24.8	20.6	21.5	26.4	14.5	30.3	19 14.1	12.1	03	19	02.9	07	03.4	01	04.0	02	03.2	09	02.4	11	02.4	02	02.0	34	
VII	752.6	22.6	27.6	23.2	24.2	29.0	19.2	32.4	15 13.4	22	16	03.1	11	03.5	02	05.0	01	03.0	09	03.4	07	03.1	14	02.6	03	02.0	30
VIII	752.9	21.4	26.8	22.4	23.3	28.5	18.8	35.4	29 14.3	25	15	02.8	08	02.2	03	03.0	05	03.0	09	02.7	08	02.2	09	02.3	01	05.0	35
IX	756.5	16.0	22.7	17.4	18.4	23.7	13.9	30.4	06 07.4	29	19	03.9	21	03.2	02	03.0	.	.	01	02.0	05	02.6	10	01.8	01	03.0	31
X	758.8	20.6	26.4	21.3	21.2	24.7	13	08.7	19	02.8	09	02.8	05	02.6	10	03.7	08	03.2	06	01.8	07	01.3	01	03.0	38		
XI	753.1	09.4	13.9	10.7	11.2	15.3	07.3	20.7	05 01.0	29	16	03.8	14	02.6	09	03.1	17	03.5	03	02.3	02	02.0	03	01.3	02	02.5	24
XII	757.9	05.5	10.1	06.4	07.3	10.9	03.2	16.6	23 01.0	23	24	04.8	05	04.4	07	02.3	11	04.8	01	07.0	.	.	.	.	02	03.0	24
God.	755.0	13.6	18.6	14.7	15.4	19.6	11.1	35.4	29.VM -01.0	25	VM 190	03.6	135	03.4	58	03.1	125	04.1	78	03.4	59	02.3	65	02.2	17	02.6	348
$\varphi = 43^{\circ}03' N \lambda = 16^{\circ}05' E$ Gr. $\Delta G = + 1h 04 min.$																						KOMIZA	BR. ST. 87				
I	-	09.0	12.3	09.4	10.0	12.7	07.0	17.1	30 00.2	19	11	02.9	01	02.0	11	03.1	50	03.3	04	06.0	02	01.5	07	02.3	04	02.0	03
II	-	10.6	13.4	10.6	11.3	14.0	06.2	19.3	23 03.6	28	14	03.2	02	01.5	03	03.7	30	03.7	03	05.3	05	03.6	05	01.4	15	02.4	03
III	-	11.8	15.9	11.6	12.7	16.4	08.8	22.2	24 01.6	01	18	02.6	.	06	03.7	36	02.7	03	03.0	03	01.0	06	01.8	12	02.6	09	
IV	-	12.3	16.8	12.4	13.5	17.4	09.2	24.2	30 01.2	11	25	03.4	04	04.2	06	03.5	25	03.3	01	03.0	02	02.0	04	02.0	13	02.8	10
V	-	10.4	21.6	17.4	18.7	22.4	13.6	28.7	19 09.8	31	15	02.7	.	.	04	03.5	43	02.8	04	02.0	02	01.0	01	01.0	16	02.3	08
VI	-	21.2	24.7	20.3	21.8	25.1	16.7	26.7	13 12.4	03	12	02.7	.	.	.	27	02.0	04	01.0	.	08	01.4	25	02.5	13		
VII	-	23.9	27.9	22.7	24.3	28.4	19.2	31.1	13 15.2	08	16	02.6	02	02.5	23	02.8	02	02.0	03	01.0	15	01.6	20	02.6	10		
VIII	-	23.6	26.1	22.2	23.9	26.8	16.3	32.6	29 15.2	27.24	17	02.0	.	03	03.0	20	03.4	25	02.5	03	01.3	17	01.6	19	02.2	12	
IX	-	18.5	24.2	18.4	19.9	24.6	15.2	25.0	08 09.0	30	37	02.7	01	04.0	02	04.5	05	02.8	01	01.0	02	01.0	13	01.3	21	02.7	08
X	-	16.4	22.2	16.4	17.8	22.5	12.9	24.6	08 10.2	19	10	01.9	03	01.7	03	03.3	23	03.3	01	02.3	03	01.3	17	01.5	13	01.7	12
XI	-	12.0	16.2	12.8	13.5	16.6	10.0	21.7	12 02.6	20	11	02.6	02	03.0	04	02.8	26	02.7	08	02.8	03	02.7	05	03.8	27	03.1	04
XII	-	08.3	13.0	08.5	09.6	13.3	05.7	16.3	01 02.0	19	32	03.2	04	05.8	01	02.0	17	03.7	01	01.0	01	01.0	08	01.1	28	02.6	01
God.	-	15.5	19.7	15.2	16.4	20.2	12.1	32.6	29.VM 00.2	49	VM 228	02.8	19	03.4	43	03.3	325	03.0	34	02.9	29	01.9	107	01.7	217	02.5	93
$\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$																						SPLIT-PARJAN	BR. ST. 88				
I	750.4	10.4	09.1	09.2	11.2	07.2	14.2	24	10.0	05	05	02.6	14	02.5	08	01.9	28	03.6	10	02.4	02	02.0	03	01.3	02	01.0	05
II	749.0	09.2	11.5	09.9	10.1	13.6	07.5	17.9	23 01.5	28	09	02.9	22	02.2	16	03.6	23	04.3	01	04.0	05	01.8	05	01.6	03	02.0	.
III	753.5	10.9	15.6	13.0	13.1	16.2	10.0	23.2	23 00.2	01	04	02.0	17	01.8	06	03.0	26	03.7	11	01.9	17	02.0	06	01.7	04	02.2	.
IV	748.5	11.7	15.8	13.0	13.4	16.5	09.9	24.8	30 05.1	10	10	02.1	25	03.2	05	03.2	21	03.6	06	02.3	14	01.7	04	02.2	05	02.8	.
V	749.7	17.7	22.4	10.3	19.2	25.1	15.5	28.1	24 10.0	10	05	02.6	14	02.5	08	01.9	28	03.6	10	02.4	02	02.0	06	02.0	06	02.0	01
VI	748.8	20.9	25.4	21.4	22.3	26.9	16.4	30.9	19 13.4	03	07	01.4	14	02.5	06	02.4	12	02.4	10	01.5	23	02.4	08	02.0	09	01.7	01
VII	746.2	23.6	26.2	24.4	25.9	29.4	21.4	32.1	30 16.1	06	01	01.8	21	02.0	06	02.5	17	03.1	05	01.8	22	02.5	07	02.1	08	02.2	01
VIII	748.5	22.8	27.3	23.7	24.3	28.8	20.7	32.5	27 05.6	23	04	02.5	22	02.3	15	01.6	14	02.7	07	01.7	18	02.6	04	01.2	09	02.2	.
IX	752.1	17.7	23.0	19.1	19.7	23.7	16.5	30.5	06 10.1	25	02	03.0	38	03.5	09	02.2	05	02.4	04	01.8	20	02.0	07	01.7	04	01.2	01
X	754.0	15.0	19.6	16.6	16.9	20.1	14.2	22.7	14 11.8	05	03	02.0	24	02.7	05	01.5	21	03.2	08	01.4	16	01.7	03	01.7	07	01.7	.
XI	748.4	16.6	18.8	12.0	12.5	14.9	09.4	20.0	06 03.0	27	24	02.7	28	02.7	12	02.7	18	03.4	10	02.8	05	01.6	05	01.6	07	02.0	02
XII	753.0	07.1	10.1	08.5	11.0	06.1	14.0	14.0	01 02.5	31	03	02.2	41	03.3	10	02.7	15	04.1	08	02.0	06	01.2	03	01.7	06	02.0	.
God.	750.4	14.6	18.6	15.7	16.2	19.6	13.1	32.5	07.VM 00.2	49	VM 64	02.4	284	02.7	126	02.7	224	03.5	88	02.1	167	02.1	59	01.8	72	02.0	11
$\varphi = 43^{\circ}10' N \lambda = 16^{\circ}27' E$ Gr. $\Delta G = + 1h 07 min.$																						SINJ	BR. ST. 90				
I	-	03.3	08.3	05.4	05.6	08.9	01.4	14.7	25 -07.6	19	07	03.1	06	03.3	01	02.0	14	02.2	23	01.8	06	01.0	.	.	.	.	36
II	-	05.0	10.1	06.7	07.1	11.																					



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Mjesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nD, Fm (0-12)																		
		Tm		Sred. (dnev.)	Max.	Min.	Max.	Dat.	Min.	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		7	14	21							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\varphi = 43^{\circ}18' N \lambda = 17^{\circ}01' E$ Gr. $\Delta G = +1h\ 08\ min.$																												
I	-	06.3	12.3	18.6	09.4	12.9	06.0	16.0	30	00.0	09	11	01.2	20	01.8	21	01.2	20	01.6	12	01.4	03	01.0	02	01.0	04		
II	-	09.7	13.2	19.5	10.7	14.0	07.5	20.0	24	08.0	04	12	01.1	17	01.5	18	01.4	13	01.2	06	01.2	06	01.2	02	01.2	03		
III	-	10.4	16.5	19.5	12.2	17.1	06.3	26.0	24	02.0	01	09	01.0	28	01.4	15	01.7	11	01.6	07	01.3	02	01.0	14	01.2	05	01.4	
IV	-	17.4	11.8	19.2	13.2	17.5	05.2	24.0	30	05.5	13	12	01.4	24	01.6	11	01.6	11	01.0	05	01.2	11	01.2	01	01.2	01		
V	-	17.9	22.7	19.4	23.4	15.5	32.0	19	10.0	10	14	01.0	20	01.4	12	01.3	13	01.8	11	01.7	02	01.4	13	01.0	08	01.1		
VI	-	20.8	25.3	21.3	22.2	26.0	16.5	36.2	19	05.0	02	12	01.2	12	01.2	12	01.2	02	01.5	02	01.0	12	01.0	13	01.1	01		
VII	-	23.2	28.4	23.7	24.8	29.1	20.0	32.0	31	17.0	28	09	01.0	13	01.8	18	01.7	05	01.2	04	01.2	29	01.1	07	01.1	01		
VIII	-	21.9	28.1	22.4	23.7	28.7	19.9	32.5	30.0	16.0	24	20	01.0	23	01.2	11	01.2	04	02.2	08	01.1	02	01.0	18	01.1	07	01.0	
IX	-	16.6	24.1	19.1	20.2	24.8	16.1	30.5	07	16.5	30	18	01.1	13	01.7	20	01.2	04	01.0	07	01.0	03	01.0	20	01.0	05	01.0	
X	-	15.5	21.1	16.0	17.2	21.6	13.1	24.0	09.8	16.0	27.7	12	01.0	11	01.1	25	01.1	07	01.1	16	01.1	05	01.2	13	01.1	04	01.2	
XI	-	11.8	16.5	12.3	13.3	17.0	09.4	23.0	05	03.5	21	13	01.0	18	01.2	25	01.2	08	01.4	13	01.2	04	01.5	07	01.0	02	01.5	
XII	-	07.4	12.6	08.2	09.1	13.2	04.4	18.0	10	06.0	23.13	16	01.2	28	01.8	21	01.7	09	02.1	03	01.0	09	01.1	07	01.6	01		
GOD.	-	14.8	19.8	15.2	16.3	20.5	12.4	32.5	30.0	00.0	05.0	165	01.1	237	01.5	218	01.4	120	01.7	53	01.2	27	01.1	151	01.1	77	01.2	07
$\varphi = 43^{\circ}01' N \lambda = 17^{\circ}34' E$ Gr. $\Delta G = +1h\ 10\ min.$																							CROATIA		BR. ST. 91			
I	-	06.6	10.8	08.2	08.4	11.6	04.6	16.7	30	-01.1	01	05	03.6	01	04.0	22	02.2	58	02.3	04	02.8	03	02.0	0.	0.	0.		
II	-	08.7	13.2	10.6	10.8	14.3	06.5	16.7	23	00.6	04	04	03.2	03	02.7	07	02.4	35	02.6	21	03.8	12	01.8	02	03.0	0.		
III	-	09.7	17.4	12.9	13.2	18.0	07.8	26.0	24	06.3	01	0.	0.	0.	08	02.1	40	02.6	11	03.2	26	02.4	05	02.6	03	02.0		
IV	-	11.1	17.6	14.0	14.2	18.4	06.6	27.6	30	03.8	18	09	03.6	15	02.7	02	02.5	30	02.6	03	03.9	16	02.2	02	02.5	0.		
V	-	17.1	23.4	19.1	19.7	24.2	12.9	32.1	19	08.3	11	03	03.0	01	01.0	07	02.4	43	02.6	14	02.7	14	02.6	11	02.6	0.	0.	
VI	-	20.3	25.6	22.2	22.6	26.5	15.0	30.4	19	08.6	05	07	02.6	01	05.0	09	01.4	24	02.3	61	03.0	16	02.1	27	02.4	05	02.6	
VII	-	22.9	29.5	24.5	25.5	30.3	17.6	33.8	31	14.5	28	04	02.5	03	02.7	07	02.0	21	02.3	07	03.0	16	02.1	32	02.3	03	02.7	
VIII	-	20.6	28.0	23.3	23.9	29.0	17.0	35.1	30	12.7	25	0.	0.	0.	13	02.4	19	02.2	06	02.8	16	01.6	39	01.9	0.	0.		
IX	-	16.7	23.5	19.8	19.9	24.7	13.6	31.0	06	10.4	30	05	03.4	02	03.0	16	02.4	40	02.2	02	02.0	09	02.4	14	01.8	02	01.5	
X	-	22.2	21.1	16.0	16.3	22.3	10.1	24.5	08	05.6	05	01	01.0	01	02.0	27	02.4	45	02.1	0.	0.	02.5	07	01.9	0.	0.		
XI	-	09.4	15.0	12.7	12.4	16.0	06.9	22.0	11	00.2	28	0.	0.	0.	02.5	24	02.1	36	02.1	07	02.1	13	02.0	04	02.0	02	01.5	
XII	-	04.9	10.8	07.1	07.4	12.1	02.6	16.6	10	-02.1	06	07	03.3	20	02.4	21	02.3	38	01.9	05	01.2	0.	0.	0.	02	02.0	0.	
GOD.	-	13.4	19.7	15.9	16.2	20.6	10.3	35.1	30.0	-02.1	06.0	45	03.1	51	02.6	173	02.2	429	02.3	81	02.9	143	02.2	154	02.2	19	02.2	
$\varphi = 42^{\circ}24' N \lambda = 16^{\circ}16' E$ Gr. $\Delta G = +1h\ 05\ min.$																							PALAGRUZ		BR. ST. 93			
I	752.8	10.0	11.5	10.4	10.6	12.0	06.3	15.3	29	04.5	14	14	04.4	01	04.0	04	04.0	15	05.5	29	04.5	08	04.4	06	03.5	05	03.4	01
II	751.3	10.9	13.1	11.1	11.5	13.5	09.4	17.4	22	03.7	28	06	05.0	05	03.0	04	03.0	08	04.1	28	04.4	10	04.5	02	03.0	21	05.0	0.
III	755.9	11.4	14.7	12.2	12.6	15.3	12.2	18.4	27	02.3	01	14	03.7	0.	0.	03	0.7	16	04.5	23	04.2	05	02.5	01	02.0	26	03.9	04
IV	750.8	12.4	15.2	12.6	13.2	16.0	10.3	19.8	04	03.3	13	20	04.9	06	04.0	04	03.0	12	05.6	20	04.3	05	04.0	04	03.2	16	04.3	03
V	752.0	16.7	19.6	16.6	17.4	20.4	14.4	25.4	23	10.2	10	13	02.8	03	01.7	02	02.5	20	04.3	22	03.9	04	02.8	05	02.6	22	03.5	02
VI	751.6	20.5	23.9	20.9	24.4	27.7	17.7	26.2	13	12.5	03	13	02.8	08	01.9	01	01.0	06	04.7	13	02.6	05	02.2	07	03.0	34	03.1	03
VII	750.7	22.3	26.9	23.1	24.1	27.7	21.1	31.6	26	16.0	01	12	03.5	10	01.9	01	01.0	06	04.6	16	03.8	07	02.6	04	02.5	32	03.6	03
VIII	751.0	22.6	26.4	22.9	23.7	27.2	20.7	30.2	17	13.0	24	10	02.7	06	01.3	02	04.5	13	03.4	20	03.2	04	02.7	04	02.9	30	02.9	02
IX	754.6	18.8	22.9	19.3	20.1	23.4	17.3	28.2	06	12.4	16	15	03.2	09	02.6	02	02.5	02	02.5	22	03.9	04	02.8	05	02.6	22	03.5	02
X	756.6	16.5	19.6	17.6	18.2	20.4	14.9	22.8	09	11.2	14	16	02.1	02	02.5	05	02.4	02	02.5	22	03.9	06	03.0	04	02.5	32	03.6	04
XI	750.8	13.2	19.5	12.7	13.9	15.9	10.6	20.4	04	-0.4	27	06	03.3	03	02.3	*	0.	02.5	32	02.2	08	02.4	05	02.3	33	04.1	01	
XII	752.2	10.0	11.7	10.1	10.5	12.4	08.4	15.1	11	05.0	03	22	03.5	11	02.6	01	02.6	01	05.0	17	04.4	03	01.7	07	03.0	29	03.2	0.
GOD.	752.8	15.5	18.4	15.7	16.3	19.0	13.7	31.6	29	14.4	26	07	02.3	02	02.0	23	01.1	29	02.2	06	02.2	01	02.8	11	02.5	01		
$\varphi = 42^{\circ}58' N \lambda = 16^{\circ}43' E$ Gr. $\Delta G = +1h\ 07\ min.$																							VELA LUKA		BR. ST. 94			
I	-	07.5	11.8	08.7	09.2	12.4	05.7	16.4	29	-02.3	19	06	03.2	*	*	20	01.3	57	02.7	04	02.2	*	*	02	02.0	04	02.5	*
II	-	08.6	12.8	0																								

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha em mm	Padavine R mm	Broj dana na sat																					
	Inhalacija broj sati			L m s			Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	★	♦	▲	■	□								
	7	14	21	Sred. (Dles)	Σ	Max	Dat.	30.00.0	0.0250	30.020.0	6	8	2.0	8.0	0.1	1.0	10.0	.										
MAKARSKA																												
BR. ST. 91																												
I 8.3 7.8 7.0 7.7	-	06.5	73	76	73	74	44	120	052.5	16	.	.	.	.	01	03	20	18	14	03	17	01	.					
II 7.4 6.4 6.4 7.1	-	07.6	77	75	75	75	46	113	C19.1	12	.	.	.	.	01	04	15	14	12	04	14	.	.					
III 6.2 5.4 5.4 5.7	-	07.8	71	68	69	69	42	047	014.6	14	.	.	.	.	02	05	11	08	08	02	08	.	.					
IV 5.2 4.6 3.8 4.7	-	08.0	68	66	66	67	42	041	010.3	15	.	.	.	.	02	07	09	09	01	08	.	.						
V 5.2 5.1 4.5 5.0	-	12.6	74	70	72	72	48	028	012.0	15	.	.	.	.	10	02	03	.	08	09	04	01	04	.				
VI 5.9 4.1 4.4 4.1	-	14.2	71	67	68	69	37	049	019.1	26	.	.	.	.	21	03	09	.	10	05	06	02	06	.				
VII 5.6 3.2 2.3 2.8	-	16.1	71	63	68	67	40	084	068.0	23	.	.	.	.	31	12	20	.	14	01	05	02	05	.				
VIII 5.2 4.0 3.2 4.1	-	15.5	71	64	69	69	47	044	018.7	24	.	.	.	.	30	13	20	.	10	06	04	02	04	.				
IX 3.2 2.5 3.1 2.9	-	12.3	68	65	65	65	48	066	028.2	04	.	.	.	.	15	02	04	.	16	03	07	07	02	07	.			
X 3.5 3.0 2.4 3.0	-	10.3	66	69	65	67	35	038	020.9	10	.	.	.	.	17	03	02	.	02	03	.	.	01	.				
XI 6.7 6.4 6.8 6.5	-	08.0	65	63	60	65	32	129	025.7	02	.	.	.	.	01	12	13	10	05	13	.	.	02	.				
XII 5.4 4.2 4.5 4.7	-	05.6	61	66	57	62	21	171	039.3	30	.	.	.	.	02	10	08	06	09	06	09	.	.					
GOD. 5.2 4.0 4.5 4.9	-	10.4	65	66	67	68	21	924	068.0	25.ii	.	.	.	.	111	32	56	04	105	100	100	88	32	98	01	.		
CPUZEN																												
BR. ST. 92																												
I 8.3 6.1 8.3 6.2	-	06.6	85	72	70	77	82	42	167	041.2	16	.	.	.	04	02	22	20	18	05	20	.	.					
II 7.0 7.6 6.9 7.9	-	07.5	80	70	77	76	49	080	015.3	02	.	.	.	.	02	12	14	12	02	14	.	.	04	01				
III 5.7 4.4 5.3 5.1	-	08.6	81	63	78	74	43	043	023.1	13	.	.	.	.	01	03	06	04	05	01	06	.	.					
IV 5.7 4.4 5.3 5.1	-	08.1	72	56	66	69	24	043	016.2	09	.	.	.	.	02	07	09	07	02	09	.	.	02					
V 4.3 5.1 5.4 4.9	-	11.4	72	55	71	66	32	032	014.8	28	.	.	.	.	13	01	01	.	11	09	05	02	06	.				
VI 2.4 3.2 2.6 2.8	-	12.3	72	48	62	60	29	016	014.3	03	.	.	.	.	21	03	05	.	15	01	02	02	01	.				
VII 2.2 2.2 2.2 2.3	-	12.1	66	34	51	50	24	028	025.4	23	.	.	.	.	31	18	03	.	18	01	04	02	01	.				
VIII 3.2 3.4 3.2 3.3	-	13.2	70	65	61	61	26	156	055.2	22	.	.	.	.	29	13	02	.	16	02	11	10	04	11	.			
IX 3.7 4.1 4.7 4.2	-	12.3	70	61	73	71	36	210	050.3	18	.	.	.	.	12	02	04	.	13	08	12	09	05	12	.			
X 2.6 1.5 2.2 2.1	-	10.2	85	60	74	72	42	104	081.7	10	.	.	.	.	20	03	02	.	02	02	02	.	03	02				
XI 6.1 6.3 6.2 6.2	-	08.6	88	70	77	78	49	260	055.6	26	.	.	.	.	06	13	14	12	07	14	.	.	01	04	02			
XII 4.7 4.5 4.3 4.5	-	05.2	70	52	65	65	36	115	035.2	10	.	.	.	.	12	02	04	.	13	08	12	10	03	12	.			
GOD. 4.6 4.6 4.7 4.6	-	09.7	77	57	69	68	24	1258	081.7	40.x	.	.	.	.	16	110	36	06	04	136	94	112	94	35	112	.		
PALAGRAZ																												
BR. ST. 93																												
I 7.4 7.7 6.7 7.3	086.0	074.6	E3	72	78	77	45	039	013.5	05	.	.	.	.	16	.	11	09	06	02	09	.	.	01	.			
II 7.2 6.7 5.0 6.3	122.5	078.8	80	68	60	46	018	013.7	02	.	.	.	.	04	02	14	04	05	02	04	01	.	.	02				
III 6.2 6.4 3.8 5.4	226.1	087.4	85	65	61	73	33	003	018.8	30	.	.	.	.	07	01	04	05	02	02	02	.	.	03				
IV 5.6 5.4 4.7 5.3	263.4	075.6	65	57	70	65	36	021	020.0	15	.	.	.	.	14	01	05	06	02	01	01	.	.	01				
V 5.0 5.7 5.1 5.3	273.7	11.1	80	65	78	74	38	028	014.6	10	.	.	.	.	02	07	01	06	05	06	01	.	.	01				
VI 4.0 4.0 4.9 4.3	316.2	13.3	73	55	79	70	43	011	004.3	10	.	.	.	.	15	06	02	07	03	07	03	.	.	03				
VII 2.5 2.9 1.5 2.3	364.4	16.1	77	59	77	71	35	026	012.5	23	.	.	.	.	29	04	27	09	17	02	04	04	01	03				
VIII 4.3 4.1 2.6 3.7	307.8	15.7	77	60	76	71	40	037	016.5	22	.	.	.	.	28	02	22	08	11	01	05	04	02	.				
IX 5.3 4.2 3.6 4.4	268.2	12.7	77	57	76	70	28	021	012.6	20	.	.	.	.	11	06	07	07	06	03	02	01	03	.				
X 4.3 2.7 3.7 3.6	223.6	11.9	85	67	64	79	24	000	006.0	03	.	.	.	.	06	10	01	06	07	07	07	.	.	02				
XI 6.6 6.5 5.3 6.1	106.7	09.1	78	70	75	74	46	026	006.3	17	.	.	.	.	11	01	06	07	07	07	07	.	.	02				
XII 5.1 5.0 3.5 4.5	124.2	36.7	72	64	71	65	32	025	013.8	10	.	.	.	.	10	03	07	03	07	05	01	07	.	.				
GOD. 5.3 5.2 4.1 4.9	2682.8	10.7	77	63	73	72	28	255	020.0	45.IV	.	.	.	.	86	06	61	115	11	75	53	56	42	10	55	.		
VELA LUKA																												
BR. ST. 94																												
I 8.2 7.7 6.9 7.6	-	07.1	85	71	81	75	42	084	026.2	16	.	.	.	.	02	03	03	03	16	14	12	02	14	.	.	02	02	
II 8.5 6.8 6.8 7.4	-	07.5	65	68	70	78	24	026	017.6	17	.	.	.	.	01	04	02	13	11	13	11	07	02	11	.	.	01	01
III 5.6 5.6 5.4 5.9	-	07.8	79	61	78	73	17	010	010.6	14	.	.	.	.	01	03	04	07	14	04	03	04	.	.	01	.		
IV 5.6 4.8 5.3 5.2	-	07.0	66	52	66	61	23	042	024.5	15	.	.	.	.	01	08	09	10	06	01	10	.	.	02	.	.		
V 5.6 5.6 6.6 6.0	-	10.0	66	62	68	62	26	020	007.6	28	.	.	.	.	12	02	01	06	05	07	05	07	.	.	04	.		
VI 4.0 3.9 5.6 4.5	-	12.5	70	55	72	65	39	030	016.7	03	.	.	.	.	19	01	02	06	10	06	03	01	06	.	.	05		
VII 2.4 2.6 3.2 3.4	-	13.8	60	49	64	60	20	007	004.3	23	.	.	.	.	31	08	16	01	15	05	04	02	06	.	.	01	01	
VIII 4.4 3.3 3.4 3.7	-	13.9	70	51	69	63	22	046	022.5	22	.	.	.	.	20	09	09	01	13	03	05	04	03	05	.	.	07	
IX 4.2 3.2 3.3 3.7	-	11.4	75	52	73	66	26	026	008.6	20	.	.	.	.	01	14	06	07	05	06	01	07	.</					

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Mesec	Vazdušni Pritisak Fm mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta m/s, Fm (0-12)																							
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW							
		7	14	21	Sred. (Dnes)							8.	9.	10.	11.	12.	13.	8.	9.	10.	11.	12.	13.	8.	9.	10.	11.						
γ = 42°58' N λ = 17°09' E Gr. ΔG = + 1h 12 min.																																	
I	-	09.1	11.1	09.5	09.8	12.2	07.1	15.7	30	02.8	09	01	03.0	02	02.5	36	02.5	28	02.2	06	01.2	11	01.2	04	01.2	04	01.0	01					
II	-	10.0	12.4	10.2	10.7	13.5	08.3	17.2	12	02.0	04	02	04.5	03	03.1	14	01.6	01	03.0	13	01.4	11	01.9	06	02.0	01	01.9	06	02.0	01			
III	-	11.9	15.1	12.2	12.9	16.1	09.8	21.5	24	01.5	01	01	01.0	01	01.0	21	03.2	27	01.7	-	-	20	01.4	09	01.6	11	02.2	03					
IV	-	13.1	16.0	12.8	13.7	-	09.9	-	11	03.1	07.6	06	03.7	21	03.1	11	01.6	06	01.7	10	01.7	10	02.4	02	-	-	-	-	-				
V	-	18.3	20.4	17.4	18.4	21.5	15.1	25.9	24	10.5	10	*	*	*	*	30	02.8	28	02.6	04	01.5	06	02.2	18	01.7	04	01.8	01	-	-	-	-	
VI	-	21.7	23.2	19.9	21.2	24.2	17.6	24.9	12	12.9	03	03	01.7	04	02.8	20	02.6	14	01.5	*	*	14	02.0	13	01.2	18	01.8	04	-	-	-		
VII	-	24.7	26.6	23.1	24.4	27.3	20.1	30.4	16	17.4	02	*	03	01.7	04	03.2	25	02.5	15	01.5	03	01.3	12	01.8	14	01.2	15	01.6	02	-	-	-	-
VIII	-	23.9	26.5	22.8	24.0	27.3	19.6	30.9	29	15.5	24	01	01.0	04	01.5	11	02.4	29	02.0	02	03.0	18	01.2	14	01.1	13	01.6	01	-	-	-	-	
IX	-	19.6	22.9	19.3	20.3	23.6	16.2	29.6	06	09.6	29	*	*	*	*	06	03.8	09	02.7	20	02.4	06	01.2	28	01.5	06	01.2	14	01.6	01	-	-	-
X	-	16.1	20.1	16.4	17.3	20.5	14.6	23.6	15	11.6	01	*	*	*	*	03	01.7	14	02.6	31	02.3	*	*	27	01.3	03	01.3	12	01.6	03	-	-	-
XI	-	12.5	14.9	13.0	13.4	15.7	10.8	19.7	11	03.9	28	*	*	*	*	03	03.7	08	02.4	38	01.9	04	01.5	23	01.4	04	02.2	09	01.7	01	-	-	-
XII	-	08.5	10.9	09.0	09.3	11.9	06.8	14.9	01	03.2	05	01	01.0	12	03.2	08	03.6	29	02.3	03	01.3	33	01.1	01	01.0	06	01.7	0.	-	-	-	-	
GOD.	-	15.8	18.3	15.5	16.3	-	13.0	-	01.5	04.3	15	02.0	45	03.0	239	02.8	284	02.0	35	01.5	225	01.4	108	01.5	124	01.8	20	-	-	-	-		
γ = 42°58' N λ = 17°10' E Gr. ΔG = + 1h 09 min.																																	
I	-	08.8	11.5	09.2	09.7	12.3	06.3	19.0	29	00.6	01	13	01.7	12	02.9	09	03.2	43	02.7	01	03.0	01	03.0	02	02.5	03	01.0	00	-	-	-		
II	-	10.0	12.9	09.6	10.5	13.5	07.5	17.9	23	00.8	04	*	*	*	*	*	*	*	*	*	*	*	*	09	02.8	10	03.0	07	01.6	06	-	-	-
III	-	11.2	15.8	10.9	12.2	16.5	08.4	22.7	27	01.8	01	16	01.4	08	02.4	04	02.0	33	02.9	*	*	09	02.8	10	03.0	07	01.6	06	-	-	-		
IV	-	12.2	17.0	12.0	13.3	17.6	08.9	22.5	30.9	03.8	18	12	02.0	19	02.9	02	02.0	20	02.4	02	02.0	13	03.0	14	02.7	06	01.7	02	-	-	-		
V	-	18.4	22.0	16.5	18.4	22.9	13.7	28.5	19	08.4	11	14	01.6	23	02.0	03	03.0	29	02.5	01	02.0	08	02.4	08	02.9	05	02.2	02	-	-	-		
VI	-	21.2	24.5	18.9	20.9	25.5	16.0	30.2	20	12.6	06	14	01.4	12	02.4	02	03.5	22	02.4	02	02.0	13	03.2	20	02.8	01	02.0	04	-	-	-		
VII	-	24.0	28.0	22.4	24.2	26.7	18.9	31.7	16	15.0	28	13	01.5	16	02.4	04	02.5	25	02.3	03	01.7	10	03.4	14	03.1	07	03.5	01	-	-	-		
VIII	-	22.6	27.5	21.6	23.3	26.8	18.7	33.1	07	14.4	26	17	01.5	13	02.5	03	01.0	28	02.3	03	02.3	08	02.0	11	02.7	06	01.2	04	-	-	-		
IX	-	18.4	24.0	18.0	19.6	24.9	15.7	31.5	06	09.0	30	10	01.8	32	02.7	*	*	16	02.1	01	02.0	14	02.2	06	02.8	07	01.6	04	-	-	-		
X	-	15.2	21.1	14.8	16.5	21.7	12.7	24.8	13	09.0	19	28	01.5	12	02.2	06	02.7	19	02.3	03	01.3	04	02.8	08	02.1	10	01.4	03	-	-	-		
XI	-	11.9	15.6	12.1	12.9	16.6	09.6	21.2	11	02.1	21	21	01.6	18	02.2	02	02.5	20	03.0	03	02.3	04	02.8	09	02.7	09	01.6	04	-	-	-		
XII	-	07.3	12.0	07.6	08.7	13.0	04.7	17.0	01	00.3	23	18	01.5	31	02.9	03	03.3	10	03.5	05	01.6	04	02.5	09	02.4	10	01.5	03	-	-	-		
GOD.	-	15.1	19.3	14.5	15.8	20.1	11.8	33.1	30.VII	00.3	23	3X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
γ = 42°50' N λ = 17°42' E Gr. ΔG = + 1h 11 min.																																	
I	-	07.7	11.0	07.9	08.6	12.0	04.1	16.2	25	-03.0	20	19	01.9	02	01.5	06	02.7	24	04.0	04	03.8	*	01	01.0	02	02.0	03	01.0	02	02.7	34		
II	-	08.6	12.5	08.8	09.7	14.0	05.3	18.0	25	-00.5	08	18	02.2	03	01.2	02	03.5	31	03.9	02	04.0	06	02.0	02	01.0	03	01.3	22					
III	-	07.7	15.7	09.1	10.4	16.5	05.0	24.7	26	-02.0	05	03	13	01.6	03	02.7	03	03.5	33	03.4	04	01.2	01	03.0	02	02.0	03	01.9	05	02.8	26		
IV	-	10.4	16.6	10.8	12.2	17.4	06.9	23.0	30	01.3	18	27	02.9	03	03.3	09	03.2	09	03.8	*	*	08	01.9	05	01.9	05	02.8	26					
V	-	16.6	21.7	15.5	17.4	23.0	11.1	30.5	19	06.7	09	17	02.0	04	06	02.5	21	03.7	09	02.3	01	01.0	02	02.0	03	02.7	34						
VI	-	19.9	24.3	18.0	20.0	25.6	13.4	30.0	22	09.0	06.0	13	01.5	02	01.5	04	02.0	14	02.2	03	01.3	06	02.6	02	02.5	04	01.8	42					
VII	-	23.3	28.2	22.3	24.0	29.2	17.0	32.0	30	12	12.0	23	26	01.7	01	02.0	03	02.0	18	03.0	04	02.2	08	02.0	02	02.0	02	02.0	28				
VIII	-	21.2	27.1	20.5	22.3	28.2	16.2	32.5	30	11.7	12	18	01.7	03	01.7	02	02.5	17	02.8	*	*	08	02.4	10	01.7	*	*	35					
IX	-	17.4	23.5	17.1	18.8	24.3	13.7	31.0	07.06	03.5	30	40	01.8	01	01.0	*	14	02.5	02	02.5	05	02.2	02	02.0	02	01.5	24						
X	-	12.0	20.2	12.7	14.4	21.0	08.7	24.2	13	04.2	05	15	01.5	03	02.0	01	01.0	15	02.6	07	01.3	02	01.5	04	01.2	02	02.0	44					
XI	-	10.1	15.4	10.8	11.8	16.5	07.3	21.6	07	-01.5	21	25	01.6	01	02.0	*	20	02.7	03	03.0	*	04	01.8	02	01.5	35							
XII	-	05.7	11.2	05.6	07.0	12.5	01.7	16.5	01</																								

Mjesec	Oblažnost Nm (0-10)			Inzulacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sa:																			
	7	14	21		S_m			Tn Tx Tx Tx Tx Tx			F(0-12) Nm(0-10)			R mm			•	*	*	Δ	Δ	Δ	Δ	R	T	III				
					mm	7	14	21	Srednji (Srednji)	Min	Max	Dat.	IV	V	VI	IV	V	VI	IV	V	VI	IV	V	VI	IV	V	VI			
BR. ST. 96	KORČULA																													
I 7+5 6+9 6+9 7+4	-	07+2 78 74 78 77 39	134 052.0	16	.	.	.	.	.	.	.	.	01	03	15	16	15	03	16	.	.	01	01	.	01	01	01	01	01	
II 7+4 7+1 5+9 6+7	-	08+0 82 77 80 80 33	066 011.4	27	.	.	.	.	.	.	.	.	01	02	12	16	13	01	16	01	01	01	01	02	06	06	06	06	06	
III 5+4 5+6 4+8 5+3	-	08+4 77 67 77 73 34	031 012.2	13	.	.	.	.	.	.	.	.	08	10	06	06	01	06	01	06	.	.	01	01	01	01	01	01	01	
IV 5+0 5+9 3+3 4+1	-	07+4 65 57 66 62 27	041 015.0	15	.	.	.	.	.	.	.	.	03	10	05	06	06	06	01	06	.	.	01	01	01	01	01	01	01	
V 4+5 5+2 3+4 4+3	-	12+2 76 71 77 75 44	037 014.0	28	.	.	.	.	05	.	.	01	11	06	05	05	02	05	.	.	05	.	.	.	.	.	05	.	.	
VI 3+4 3+9 7+3 3+2	-	14+8 73 74 82 76 46	053 025.3	27	.	.	.	.	12	.	02	.	13	03	04	03	03	04	.	.	03	.	03	.	03	.	03	.	03	
VII 2+3 3+4 1+3 2+5	-	16+9 72 68 77 72 51	046 027.0	23	.	.	.	.	31	02	19	.	17	02	05	03	01	05	.	.	03	.	03	.	03	.	03	.		
VIII 4+0 3+6 2+0 3+1	-	17+0 75 68 80 74 47	203 070.9	14	.	.	.	.	28	03	14	.	15	02	08	05	05	08	.	.	02	07	.	.	.	02	07	.		
IX 3+6 4+0 3+5 3+6	-	13+8 78 68 79 75 45	106 029.3	19	.	.	.	.	11	.	06	04	15	07	09	08	05	09	.	.	06	.	06	.	06	.	06	.		
X 3+6 3+3 2+2 3+0	-	12+6 85 76 87 82 47	019 008.0	20	.	.	.	.	10	.	05	04	15	08	04	04	04	04	.	.	04	.	04	.	04	.	04	.		
XI 5+5 7+0 5+7 6+1	-	10+0 85 79 87 84 55	170 038.4	29	.	.	.	.	01	.	06	10	15	13	05	15	.	.	01	01	01	01	01	01	01	01	01			
XII 4+1 3+6 3+0 3+6	-	06+9 78 68 80 75 46	170 074.6	10	.	.	.	.	02	.	16	05	10	08	06	10	.	.	02	.	02	.	02	.	02	.	02			
GOD. 4+0 4+9 3+7 4+4	-	11+3 77 70 79 75 27	1072 074.6	40.XII	.	.	.	.	41	13	.	131	77	104	89	33	104	01	01	.	.	04	03	43	.	.	.	.		
BR. ST. 97	OREBIC																													
I 7+3 8+0 7+5 7+6	-	07+9 79 72 79 77 32	134 054.1	16	.	.	.	.	.	.	.	.	04	19	19	15	03	19	.	.	02	02	02	02	02	02	02	02		
II 7+7 6+8 5+8 6+8	-	07+8 86 72 81 79 32	070 010.3	17	.	.	.	.	.	.	.	.	02	11	13	11	02	13	.	.	01	01	01	01	01	01	01	01		
III 4+9 4+2 4+9 4+9	-	08+1 77 64 74 79 30	037 021.4	13	.	.	.	.	.	.	.	.	10	09	06	04	01	06	.	.	01	01	01	01	01	01	01	01		
IV 4+5 3+6 3+6 4+0	-	07+8 67 51 66 15	041 013.8	15	.	.	.	.	.	.	.	.	01	11	05	07	06	01	07	.	.	01	05	05	05	05	05	05	05	
V 4+3 4+3 3+9 4+1	-	10+5 66 58 68 64 33	036 015.7	28	.	.	.	.	08	.	01	.	11	06	04	03	02	04	.	.	02	.	02	.	02	.	02	.		
VI 3+4 3+8 3+6 3+5	-	12+4 64 57 72 64 25	030 013.3	03	.	.	.	.	20	.	01	.	13	03	03	02	03	03	.	.	03	.	03	.	03	.	03	.		
VII 2+6 2+8 1+8 2+4	-	14+4 65 54 65 62 34	038 023.3	23	.	.	.	.	31	05	04	.	18	03	04	03	05	05	.	.	01	01	01	01	01	01	01	01		
VIII 3+4 3+0 3+0 3+1	-	14+2 70 55 68 64 33	191 069.1	24	.	.	.	.	31	04	10	.	16	03	07	03	04	07	.	.	01	05	05	05	05	05	05	05		
IX 3+2 3+8 3+6 3+5	-	11+2 69 53 68 63 30	086 020.8	19	.	.	.	.	13	03	03	.	16	04	11	09	04	11	.	.	06	.	06	.	06	.	06	.		
X 3+1 2+5 2+3 2+6	-	10+6 81 61 80 74 30	026 011.4	10	.	.	.	.	20	.	01	.	14	03	04	04	01	04	.	.	02	.	02	.	02	.	02	.		
XI 5+4 6+5 5+8 5+9	-	09+4 80 75 83 79 40	214 042.0	02	.	.	.	.	07	.	09	.	14	11	06	14	06	14	.	.	04	.	04	.	04	.	04	.		
XII 3+7 3+8 3+2 3+6	-	05+7 68 56 67 64 22	156 049.1	10	.	.	.	.	08	.	09	.	16	05	09	08	06	09	.	.	02	.	02	.	02	.	02	.		
GOD. 4+0 4+5 4+1 4+4	-	09+9 72 60 73 68 15	1059 069.6	24.XII	.	.	.	.	103	13	21	01	138	80	102	83	33	102	.	.	02	01	28	01	.	.	.	.		
BR. ST. 98	STON																													
I 7+2 6+9 7+0 7+0	-	07+6 94 84 86 88 51	202 060.4	13	.	.	.	.	05	.	.	04	04	18	16	14	05	16	.	.	01	01	.	01	01	01	01	01		
II 6+4 6+5 5+5 6+1	-	08+2 93 81 86 87 39	078 016.5	13	.	.	.	.	01	.	.	04	03	09	14	13	02	14	.	.	01	01	.	01	01	01	01	01		
III 4+1 3+9 3+8 3+9	-	08+5 94 74 90 86 46	045 020.8	13	.	.	.	.	02	.	.	02	16	07	06	05	02	06	.	.	01	01	.	01	01	01	01	01		
IV 4+6 2+9 2+9 3+5	-	08+5 88 64 80 77 34	068 034.6	15	.	.	.	.	01	.	.	01	01	12	04	08	08	01	08	.	.	01	01	.	01	01	01	01	01	
V 3+6 3+5 3+4 3+5	-	11+7 86 64 81 77 46	070 020.0	10	.	.	.	.	08	01	01	01	12	02	09	05	04	09	.	.	02	.	02	.	02	.	02	.		
VI 2+4 3+1 1+5 2+3	-	13+6 83 60 80 74 36	028 019.7	03	.	.	.	.	20	.	01	.	17	01	03	03	01	03	.	.	01	01	.	01	01	01	01	01		
VII 1+9 2+1 1+3 1+8	-	13+6 67 47 66 60 27	028 026.0	23	.	.	.	.	31	11	04	04	21	01	04	02	01	04	.	.	01	01	.	01	01	01	01	01		
VIII 2+8 2+7 1+6 2+4	-	14+2 77 55 75 69 33	105 052.0	15	.	.	.	.	30	07	07	03	18	01	07	07	03	07	.	.	01	01	.	01	01	01	01	01		
IX 3+1 2+6 3+1 3+0	-	11+6 77 56 76 70 29	197 053.3	23	.	.	.	.	12	03	01	01	17	05	10	10	06	10	.	.	04	.	04	.	04	.	04	.		
X 2+7 3+2 1+5 2+5	-	09+9 88 64 84 79 36	042 023.0	10	.	.	.	.	01	.	.	20	03	03	03	02	03	.	.	01	01	.	01	01	01	01	01			
XI 4+6 5+7 5+0 5+1	-	09+7 93 83 80 88 50	216 070.6	26	.	.	.	.	01	.	.	02	08	09	14	13	05	14	.	.	01	02	.	01	02	.	01	02		
XII 4+1 3+9 3+2 3+7	-	05+7 78 59 74 70 29	155 050.1	10	.	.	.	.	12	05	07	07	15	07	10	10	06	10	.	.	01	01	.	01	01	01	01	01		
GOD. 4+0 3+8 3+3 3+7	-	10+2 84 65 80 77 27	1234 070.0	26.XI	.	.	.	.	21	101	23	07	21	01	163	66	104	93	38	104	.	.	04	21	06	.	.	07	04	68
BR. ST. 99	DUBROVNIK																													
I 7+2 7+3 6+7 7+1	-	06+5 68 67 70 69 24	146 044.2	16	.	.	.	.	.	.	.	06	01	07	17	15	06	17	.	.	01	05	.	01	05	.	01	05		
II 7+0 6+8 5+9 6+7	-	07+6 77 70 77 75 30	105 013.6	14	.	.	.	.	.	.	.	06	01	07	17	15	06	17	.	.	03	06	.	03	06	.	03	06		
III 4+7 4+6 4+6 4+8	-	07+8 65 67 73 69 25	041 019.9	13	.	.	.	.	.	.	.	06	01	07	05	07	05	01	07	.	.	01	05	.	01	05	.	01	05	
IV 5+0 4+3 4+6 4+6	-	07+2 59 58 62 60 23	046.009.8	15	.	.	.	.	.	.	.	12	03	07	06	09	07	09	07	.	.	01	04	.	01	04	.	01	04	
V 4+3 4+6 4+6 4+4	-	10+6 62 64 67 64 37	068 033.6	10	.	.	.	.	04	.	02	07	09	05	13	04	02	13	.	.	01	04	.	01	04	.	01	04		
VI 2+9 3+7 2+9 3+5	-	13+3 65 66 69 70 24	026 013.7	03	.	.	.	.	15	.	03	.	13	03	05	03	02	05	.	.	01	05	.	01	05	.	01	05		
VII 1+9 2+5 2+5 2+3	-	14+4 57 63 65 62 31	010 002.9	06	.	.	.	.	30	03	23	07	20	.	05	04	05	03	.	.	01	04	.	01	04	.	01	04</		

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Meseč	Vrednost Precipit. Pm mm	Temperatura vazduha °C				Čestina pravaca i srednja jačina vетра nD, Pm (0-12)																								
						N	NE	E	SE	S	SW	W	NW	C	8.	J.	8.	J.	8.	J.										
		7	14	21	Sred. (Dana)	Min	Max	Dat.	Min	Dat.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.										
$\varphi = 45^{\circ}13' N \lambda = 16^{\circ}54' E$ Gr. $\Delta G = + 1h 08 min.$																														
I	-	00.6	04.5	01.6	02.1	05.4	-00.9	14.5	30	-06.0	19	14	01.9	07	01.6	25	01.4	.	01	02.0	05	02.2	02	02.0	06	01.7	33			
II	-	02.8	05.5	04.6	05.4	10.5	00.8	20.0	25	-15.0	04	14	02.1	02	01.5	04	03.0	01	01.0	12	02.8	06	02.0	03	02.0	37				
III	-	04.2	15.3	08.5	09.1	16.7	02.7	26.0	23	-05.0	01	19	02.0	05	01.4	17	01.5	06	01.3	11	01.3	02	01.5	02	01.0	29				
IV	-	06.2	14.6	09.1	09.7	16.0	03.5	29.5	30	-01.6	12	29	02.3	09	01.7	15	01.4	.	07	01.4	05	01.8	.	.	04	01.0	21			
V	-	13.0	21.3	14.5	16.0	22.9	09.1	32.5	04	03.5	29	21	02.0	08	01.8	11	01.2	01	01.0	05	01.6	04	01.2	06	02.2	31				
VI	-	17.0	24.5	17.4	19.1	25.7	11.9	33.4	14	03.0	04	23	01.8	07	01.4	04	01.8	02	02.0	07	01.3	12	01.6	05	01.4	22				
VII	-	17.4	24.9	18.2	19.7	26.2	13.3	31.0	14.0	08.5	28	22	01.4	14	01.5	16	01.2	05	01.4	08	01.6	01	01.0	05	02.2	22				
VIII	-	16.4	24.9	18.0	19.3	26.0	13.5	29.2	09	07.5	26	14	01.4	11	01.3	24	01.3	06	01.3	16	01.4	01	01.0	05	01.0	21				
IX	-	09.7	19.5	11.6	13.1	20.8	07.5	29.0	12	-02.0	29	17	01.6	08	01.5	20	01.2	08	01.8	05	01.6	01	02.0	05	01.2	31				
X	-	06.9	17.4	11.4	18.4	20.5	05.5	24.8	07	-01.5	18	09	01.4	08	01.2	18	01.2	05	01.2	06	01.7	02	02.0	01	02.0	39				
XI	-	04.1	04.4	05.3	06.0	10.7	02.2	23.5	12.0	-04.5	25	11	01.5	08	01.2	23	01.6	06	01.3	05	01.4	01	03.0	01	02.0	34				
XII	-	-02.2	01.0	-01.3	-00.9	02.0	-03.3	11.5	25	-17.5	06	12	01.5	05	01.2	27	01.5	01	01.0	04	01.5	.	.	01	01.0	43				
GOD.	-	08.0	15.6	09.9	10.8	16.8	05.5	33.4	4	VI	-17.5	06.6	20.5	01.8	92	01.5	204	01.4	45	01.	81	01.4	47	02.0	22	01.6	36	01.9	363	
$\varphi = 45^{\circ}00' N \lambda = 17^{\circ}05' E$ Gr. $\Delta G = + 1h 12 min.$																						DERVENTA		BR. ST. 102						
I	-	-00.1	04.7	01.4	01.6	05.4	-01.7	16.2	12	-11.0	01	*	*	05	02.0	14	01.5	02	04.0	*	*	01	03.0	04	02.8	67				
II	-	02.3	10.3	04.6	05.7	11.1	01.3	20.0	25	-12.5	04	01	04.0	07	01.9	08	02.1	01	02.0	*	*	01	04.0	06	03.5	56				
III	-	04.4	15.1	07.8	08.9	16.5	02.4	24.8	24	-04.0	01	02	01.5	08	02.6	12	02.0	01	02.0	*	*	08	01.8	05	02.0	57				
IV	-	06.6	15.4	08.9	10.0	16.4	03.9	28.0	29	-02.0	12	01	04.0	11	02.2	15	01.7	*	*	*	*	04	01.8	10	03.2	49				
V	-	13.8	21.9	14.5	16.2	22.6	10.1	29.8	04	05.0	11	*	*	08	02.1	24	01.5	*	*	*	01	03.0	06	01.5	01	02.0	53			
VI	-	17.5	25.2	17.9	19.6	25.9	12.3	33.4	14	03.0	04	*	*	13	01.8	13	01.5	02	01.5	*	*	08	01.2	08	01.6	46				
VII	-	17.8	25.8	18.4	20.1	26.8	14.1	33.0	14	04.5	28	01	02.0	07	02.4	17	01.8	*	*	*	*	03	02.7	04	03.5	61				
VIII	-	16.4	25.7	18.0	19.6	26.5	13.8	30.0	18.0	09.0	26	*	*	02	02.0	15	01.5	02	03.0	*	*	04	01.8	05	02.8	64				
IX	-	10.4	20.1	11.7	13.5	20.7	08.0	29.0	08	-01.0	29	01	04.0	03	02.3	17	01.8	01	01.0	*	*	*	04	01.8	02	01.5	42			
X	-	07.6	18.0	10.1	11.5	18.4	06.1	26.4	07	-01.0	04	*	*	01	02.0	10	01.0	01	01.0	*	*	04	01.2	02	02.0	75				
XI	-	03.7	09.4	05.1	05.9	10.4	02.0	23.4	11.0	-04.5	25	*	*	04	01.5	13	02.0	*	*	*	*	04	02.0	*	*	68				
XII	-	-02.7	00.4	-01.6	01.4	02.4	-04.0	08.2	26	-17.5	06	*	*	01	01.0	10	01.5	*	*	*	*	04	01.2	*	*	79				
GOD.	-	08.2	16.0	09.7	11.0	16.8	05.7	33.4	4	VI	-17.5	06.6	02.8	69	02.1	168	01.7	11	02.3	*	*	02	03.5	56	01.9	45	02.4	737		
$\varphi = 44^{\circ}49' N \lambda = 15^{\circ}53' E$ Gr. $\Delta G = + 1h 04 min.$																						BIHAC		BR. ST. 103						
I	735.9	04.1	06.3	04.0	05.0	08.1	01.5	17.0	29	-06.8	20	04	02.0	03	02.7	02	01.0	17	03.8	17	03.7	06	02.2	11	01.5	29	01.6	04		
II	737.9	04.7	09.1	06.2	06.6	10.8	02.5	19.0	25	-15.2	04	06	01.8	06	02.5	09	02.8	20	03.4	10	03.3	12	02.5	15	02.0	01	01.0	05		
III	742.8	05.6	15.6	09.8	10.2	16.9	03.4	27.2	23	-04.6	03	02	02.0	12	02.2	16	02.8	19	02.3	14	02.0	15	01.8	06	01.5	05	02.0	04		
IV	738.5	05.8	13.9	09.5	09.6	16.6	03.2	28.2	30	-03.6	01	02	02.0	20	02.0	10	02.0	20	02.0	13	02.1	14	01.8	08	01.8	08	01.8	08		
V	735.8	11.9	19.8	14.5	15.1	21.2	08.6	28.8	04	01.6	29	06	01.2	07	01.7	15	01.6	19	01.8	06	02.2	13	02.2	11	01.5	13	01.8	07		
VI	738.8	15.7	23.4	18.0	19.4	24.7	12.3	32.2	13	02.6	02	03	03.3	04	01.8	15	01.5	14	02.0	09	02.0	19	01.7	13	01.5	06	01.5	05		
VII	738.8	16.5	24.0	19.1	19.6	26.3	13.3	32.4	14	01.6	28	04	01.8	03	02.0	09	01.3	12	01.5	18	02.2	09	01.8	18	01.7	09	01.6	11		
VIII	738.8	16.2	23.8	19.2	23.3	13.6	30.0	18	05.6	25	02	01.5	03	02.3	03	02.8	15	01.5	22	02.2	10	01.7	17	01.5	14	01.4	10	01.7	07	
IX	743.8	09.6	18.6	13.2	13.0	19.5	08.0	29.2	09	-01.4	29	06	01.8	10	01.9	17	01.3	07	01.4	01	01.0	09	01.0	13	01.4	20	01.6	07		
X	744.3	09.3	17.4	12.0	12.7	16.5	07.8	25.2	28	-01.0	04	01	01.0	03	01.7	08	01.8	18	02.3	16	02.1	19	01.9	14	01.4	16	01.4	04		
XI	738.3	05.7	10.7	06.6	07.4	12.1	02.8	25.6	11	-06.2	20	02	02.0	01	01.0	10	02.2	16	02.8	16	02.5	19	01.6	14	02.0	05				
XII	745.1	-01.5	02.0	00.0	00.1	03.0	-03.3	13.4	28	-14.6	06	02	01.0	07	01.1	07	02.1	10	03.3	04	03.0	17	01.3	28	01.6	12	01.4	06		
GOD.	740.6	08.6	15.4	10.9	11.4	16.9	06.2	32.2	4	VI	-15.2	04.6	08.0	00.0	01.9	01	01.0	02	01.0	03	02.0	03	02.0	07	01.6	01	01.0	05	01.6	815
$\varphi = 44^{\circ}53' N \lambda = 16^{\circ}10' E$ Gr. $\Delta G = + 1h 05 min.$																						DRVAR		BR. ST. 105						
I	718.3	01.0	05.5	02.4	02.8	06.8	-01.1	14.6	25	-11.6	01	08	04.1	01	02.0	07	01.9	03	01.7	04	02.0	06	02.4	01	02.0	05	02.6	56		
II	717.0	02.9	07.7	04.2	04.8	09.2	00.7	18.4	24	-11.2	04	07	04.6	01	03.0	01	03.0	05	02.4	16	04.7	02	04.5	07	02.1	45				
III	721.9	02.2	14.8	07.3	07.9	16.0	01.2	24.6	23	-05.0	01	07</																		

Mesec	Oblačnost Nm (0-10)	Inkolacijs broj sati (dies)	Vlažnost vazduha			Padavine R mm			Broj dana na sat																	
			e <sub>m</sub>	U m	%	Tn	Tx	Tn	Tx	Tx	Tn	F(O-12)	Nm(O-10)	R mm	•	*	*	Δ	Δ	▲	▲	RT	III			
	7	14	21	Sred. (dies)	mm	7	14	21	Sred. (dies)	Min	Σ	Max	Dat.	=	<	<	IV	IV	IV	IV	IV	IV	IV	IV		
BR. ST. 101	BOSANSKA DUBICA																							H <sub>s</sub> = 98 m H <sub>b</sub> = - m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m		
I 9.7 8.6 8.4 8.9	-	05.1 97 89 95 94 61	058 022.4	27	.	02	20	.	.	.	.	.	.	23	10	08	01	10	.	.	.	.	.	.	11	
II 9.0 7.5 7.4 7.1	-	06.3 95 78 93 89 44	109 023.0	07	02	01	10	.	.	.	.	.	02	13	15	14	06	13	03	.	.	.	.	.	01 05	
III 4.5 3.8 3.3 3.9	-	07.3 55 62 93 83 20	066 027.2	13	.	05	02	.	.	.	.	.	12	C6	04	04	03	04	02	01	.	.	.	.	.	02
IV 6.4 5.9 5.9 5.4	-	07.6 92 63 93 82 35	062 013.5	01	.	04	03	.	.	.	.	07	10	10	09	03	10	01	.	.	.	.	.	.	03	
V 4.8 6.1 5.2 4.7	-	11.1 88 64 90 81 33	046 014.2	06	.	.	.	09	01	.	01	.	05	03	10	08	01	10	.	.	.	.	.	.	01	
VI 3.9 5.2 3.0 4.4	-	13.0 84 57 91 77 32	062 021.5	27	.	.	.	16	08	.	.	.	12	06	08	08	03	08	.	.	.	.	.	.	01	
VII 4.8 4.3 2.7 3.9	-	14.1 88 63 92 81 47	138 040.8	23	.	.	.	21	03	.	.	.	10	04	11	11	06	11	.	.	.	.	.	.	01	
VIII 5.5 5.4 5.3 4.8	-	14.9 93 67 86 85 44	073 020.0	24	.	.	.	23	.	.	.	.	08	05	08	07	03	08	04	.	.	.	.	.	03	
GOD. 6.7 6.2 5.2 6.0	-	05.1 93 71 93 85 20	930 040.8	23 VI	05	13	74	87	14	.	01	.	75	146	114	103	37	108	13	01	.	.	.	01	46	
BR. ST. 102	DERVENTA																							H <sub>s</sub> = 105 m H <sub>b</sub> = - m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m		
I 8.3 7.5 7.7 7.9	-	04.8 93 82 92 85 52	035 022.2	20	.	.	01	10	.	.	.	.	10	10	09	08	02	09	.	.	.	.	.	.	05	
II 7.6 6.5 5.8 6.6	-	06.1 93 70 90 84 37	089 015.5	15	01	01	08	.	.	03	.	02	11	16	14	02	15	03	.	.	.	.	.	.	03 06	
III 4.5 4.7 4.1 4.4	-	06.7 92 54 89 78 23	046 013.6	30	.	.	08	03	.	.	.	12	08	08	07	02	07	02	.	.	.	.	.	.	01 01	
IV 5.6 5.8 5.3 5.6	-	07.2 89 54 87 77 30	057 017.3	06	.	04	03	.	.	.	07	10	11	08	03	11	.	.	.	.	.	.	.	02		
V 5.6 6.1 6.0 5.9	-	10.5 86 58 89 78 36	061 013.5	28	.	.	11	.	.	.	.	05	11	15	10	02	15	.	.	.	.	.	.	04 02		
VI 3.7 5.3 5.0 4.7	-	12.5 81 50 85 72 32	065 025.0	17	.	.	18	07	.	.	.	-	09	07	03	05	.	.	.	.	.	.	.	02		
VII 4.1 4.4 4.1 4.2	-	14.1 87 60 89 79 40	118 042.2	23	.	.	24	06	.	01	.	11	05	10	10	04	10	.	.	.	.	.	.	03 01		
VIII 4.5 5.1 5.0 5.0	-	14.0 92 55 92 81 39	066 020.2	24	.	.	25	02	.	.	.	04	11	08	02	11	.	.	.	.	.	.	.	04		
IX 4.6 4.4 4.7 4.6	-	09.8 94 60 94 83 40	066 018.9	18	.	01	11	.	.	.	11	09	09	07	03	09	.	.	.	.	.	.	01 03			
X 5.5 5.6 5.4 4.4	-	08.8 96 64 95 85 34	058 024.0	03	.	01	03	.	.	.	11	09	06	02	06	.	.	.	.	.	.	.	03			
XI 6.1 7.7 7.0 7.6	-	06.7 96 83 94 91 48	143 024.3	02	.	13	.	.	.	.	02	16	14	13	05	13	04	01	.	.	.	.	.	13 04		
XII 6.8 6.3 6.9 8.7	-	03.9 90 86 89 88 68	103 025.1	02	04	11	27	.	.	.	24	15	13	05	11	07	.	.	.	.	.	.	.	03 26		
GOD. 5.9 5.8 5.6 5.8	-	08.8 90 65 90 82 23	908 042.2	23 VI	06	14	83	98	15	.	04	.	-	136	112	33	128	18	01	.	.	.	.	10 51 46		
BR. ST. 103	BINAC																							H <sub>s</sub> = 246 m H <sub>b</sub> = 250.4 m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.0 m		
I 8.1 6.5 6.9 7.8	046.5	04.8 79 71 74 75 39	075 016.0	13	.	01	14	.	.	.	17	17	.	17	16	15	02	13	05	.	.	.	.	.	03 02 06	
II 7.3 7.9 6.1 7.1	090.6	05.1 75 62 72 70 33	122 028.2	01	02	02	08	.	.	.	13	08	.	10	18	17	03	16	04	01	.	.	.	.	.	03 05 09
III 5.5 6.2 4.2 5.3	171.3	05.4 78 44 61 61 19	096 027.9	31	.	07	02	.	.	.	15	.	06	05	07	05	04	05	03	01	.	.	.	.	.	01 01 02
IV 6.9 6.6 5.6 5.3	169.4	05.6 80 50 65 65 23	127 032.0	15	.	09	03	.	.	.	10	.	02	09	10	07	05	10	05	04	.	.	.	.	.	01 03 05
V 5.9 7.4 5.4 6.2	184.8	08.2 79 51 70 67 23	075 046.2	15	.	08	07	.	03	.	05	08	12	08	02	12	.	.	.	.	.	.	.	01 05 02		
VI 4.2 6.0 4.4 4.9	217.7	10.7 76 48 62 62 22	085 029.2	27	.	14	05	.	06	.	05	05	11	06	04	11	11	.	.	.	.	.	.	07		
VII 4.0 5.5 3.7 4.4	251.3	11.7 82 55 73 70 32	198 059.2	23	.	21	06	01	07	01	07	02	11	07	05	11	11	10	04	.	.	.	.	.	10 04	
VIII 6.0 7.0 4.7 5.9	195.6	12.1 85 56 78 73 38	094 031.2	11	.	21	01	.	10	02	04	09	16	08	04	16	.	.	.	.	.	.	.	01 04 03		
IX 6.6 6.1 4.9 5.8	159.0	09.0 92 58 85 78 29	092 036.1	20	.	01	09	.	01	.	04	11	12	09	04	12	12	.	.	.	.	.	.	10		
X 6.1 6.0 4.6 5.6	139.1	08.2 87 59 79 75 26	097 037.2	03	.	02	03	.	08	.	06	11	06	06	03	06	.	.	.	.	.	.	.	01 07		
XI 7.4 7.4 6.0 6.9	075.8	05.9 83 64 91 76 24	180 042.0	17	.	02	09	01	.	12	04	01	11	16	14	04	13	06	01	.	.	.	.	.	01 02 08 06	
XII 6.5 8.4 7.6 8.1	035.7	03.9 88 76 82 32	094 024.2	02	02	14	23	.	07	05	01	13	11	14	10	05	10	05	04	.	.	.	.	.	01 01 04 03	
GOD. 6.4 6.9 5.3 6.2	1747.1	07.5 82 57 73 71 19	1335 059.2	23 VI	04	19	73	81	12	01	109	37	41	116	148	113	44	135	28	07	.	01	04	40	55 36	
BR. ST. 104	BOSANSKA KRUPA																							H <sub>s</sub> = 176 m H <sub>b</sub> = - m h <sub>t</sub> = 2,0 m h <sub>r</sub> = 1,0 m		
I 8.5 7.9 8.5 8.3	-	05.1 85 77 85 82 48	060 013.4	13	01	12	.	.	.	01	.	03	05	14	13	02	13	05	.	.	.	.	.	.	11 12	
II 7.5 5.2 6.8 6.5	-	06.1 84 73 83 80 44	108 021.0	01	01	01	09	.	.	01	.	03	05	14	13	03	13	03	01	.	.	.	.	.	01 09 03	
III 5.6 3.4 3.2 4.0	-	07.2 83 67 82 77 27	130 042.0	13	.	09	02	.	.	.	11	05	08	08	04	07	02	01	.	.	.	.	.	06		
IV 5.7 5.5 3.2 5.5	-	07.0 85 66 80 78 25	121 025.0	06	.	07	05	.	.	.	05	06	09	09	09	09	04	09	02	.	.	.	.	.	06 08	
V 4.9 5.5 5.2 5.2	-	10.3 83 66 80 76 19	104 033.0	15	.	08	12	.	.	.	06	06	11	11	02	11	.	.	.	.	.	.	.	03		
VI 3.3 5.4 4.5 4.4	-	11.6 88 55 81 72 30	083 034.2	27	.	15	07	.	.	.	07	07	06	05	03	06	.	.	.	.	.	.	.	03		
VII 3.9 4.9 3.1 4.0	-	13.1 86 66 80 77 35	153 035.0	27	.	23	06	.	.	.	07	03	11	10	06	11	.	.	.	.	.	.	.	03		
VIII 5.9 5.1 3.7 4.6	-	13.8 87 69 88 81 42	090 020.0	24	.	22	02	.	.	.	05	11	11	11	03	11	.	.	.	.	.	.	.	01		
IX 7.4 5.4 4.3 5.7	-	10.3 92 71 72 85 47	088 030.0	20	.	01	11	.	.	.	05	10	08	08	04	08	.	.	.	.	.	.	.	11		
X 8.0 4.9 4.6 5.8	-	08.8 90 66 86 80 27	091 031.0	12	.	04	.	.	.	05	12	06	06	04	06	.	.	.	.	.	.	.	18			
XI 6.6 7.0 7.5 7.7	-	06.7 91 74 89 95 41	162 039.4	17	.	11	01	.	.	.	01	18	16	14	05	13	07	02	.	.	.	.	.	11 06		
XII 9.5 7.8 8.6 8.6	-	04.2 90 84 87 81 40	107 030.4	02	02	09	23	.	.	.	21	12	12	04	09	05	.	.	.	.	.	.	.	07 12		
GOD. 6.5 5.7 5.4 5.9	-	06.7 86 69 84 80 19	1297 042.0	45 W	03	10	72	95	13	.	01	.	61	125	126	119	44	117	23	06	.	.	.	04 80		
BR. ST. 105	DRVAR																							H <sub>s</sub> = 485 m H <sub>b</sub> = 490.0 m h <sub>t</sub> = 2.0 m h <sub>r</sub> = 1.0 m		
I 8.5 8.6 7.5 8.2	045.9	04.9 91 77 89 86 57	107 020.2	13	02	14	.	.	.	07	07	01	21	15	12	04	13	03	.	.	.	.	.	01 03 07		
II 8.5 7.8 5.8 6.4	060.7	05.6 90 73 83 85 43	130 026.8	01	01	01	14	.	.	06	05	.	12	18	16	04	16	04	.	.	.	.	.	02 05 06		
III 4.5 5.4 3.4 4.4	173.7	06.1 93 56 78																								

Mesec	Vadudini Pratisk Fm min	Temperatura vazduha °C							Cestina pravaca i srednja jačina vetrova nD, Fm (0-12)																				
		Tm			Sred. (Gdes)	Max	Min	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21							8.	j.	8.																
$\Psi = 44^{\circ}31' N \lambda = 16^{\circ}28' E$ Gr. $\Delta G = +1h\ 06\ min.$																													
I	-	01.6	04.3	01.6	02.3	05.1	-01.3	12.5	29	-15.0	19	08	01.6	.	.	.	.	23	02.1	01	02.0	.	.	.	51				
II	-	02.5	06.8	02.6	03.6	07.8	-	19.5	25	-	-	03	03.0	.	.	.	.	33	02.3	.	.	.	.	.	48				
III	-	04.5	13.4	05.8	07.4	14.3	-	23.5	24	-	-	08	01.8	.	.	.	.	26	01.4	.	.	02	01.0	57					
IV	-	05.0	11.9	05.8	07.1	13.1	01.1	25.0	30	-04.5	16.1	12	01.5	02	02.5	.	.	30	01.6	.	.	04	01.8	43					
V	-	11.2	18.3	11.2	13.0	19.1	05.7	27.0	04	-06.5	29	19	01.5	.	.	.	.	31	01.7	01	02.0	03	01.0	.	39				
VI	-	14.3	20.8	14.0	15.8	22.0	06.7	30.0	13	00.0	02	12	01.5	.	.	.	.	37	01.7	.	.	03	01.3	.	36				
VII	-	14.9	24.0	15.4	17.4	24.7	10.0	32.0	30	05.5	28	13	01.6	.	.	.	.	37	02.0	.	.	02	02.0	.	41				
VIII	-	14.4	23.4	16.9	18.0	24.3	10.0	28.5	28	04.0	25	06	01.2	.	.	.	.	35	01.8	.	.	.	.	.	52				
IX	-	08.0	17.0	09.4	11.0	05.2	27.0	12.0	-03.0	25	32	01.6	.	.	.	.	13	01.4	.	.	.	.	.	45					
X	-	06.3	16.4	05.2	09.8	17.3	03.9	22.5	28	-03.5	17.0	04	07	01.3	.	.	.	11	01.8	.	.	.	.	.	75				
XI	-	02.6	09.8	03.7	05.0	11.1	-00.2	23.5	12	-07.5	29.0	09	01.1	.	.	.	.	22	01.6	.	.	.	.	.	59				
XII	-	-04.5	-00.1	-03.3	-02.8	01.2	-07.2	11.0	07	-17.0	05	23	01.2	.	.	.	.	15	01.7	.	.	.	.	.	55				
GOD.	-	06.7	13.8	07.4	08.9	14.8	-	32.0	30.0	00.0	151	01.5	02	02.5	.	.	.	323	01.8	02	02.0	12	01.5	02	01.0	603			
$\Psi = 44^{\circ}46' N \lambda = 16^{\circ}42' E$ Gr. $\Delta G = +1h\ 07\ min.$																						BR. ST. 106							
I	-	02.4	06.9	03.2	03.9	06.2	-00.6	17.7	25	-05.5	01	04	03.0	02	03.0	01	03.0	02	04.5	14	04.0	05	01.4	11	01.5	34			
II	-	03.8	10.0	02.2	06.1	11.4	-01.2	20.0	25	-10.2	04	05	01.8	04	02.5	02	02.5	02	01.0	11	04.6	12	02.7	11	02.1	14	01.5	24	
III	-	03.3	16.4	07.9	08.9	17.5	01.7	26.2	23	-05.0	01	06	02.7	02	02.5	02	01.0	01	01.7	08	01.2	09	01.6	17	01.8	36			
IV	-	05.2	14.9	08.4	09.2	16.8	02.4	25.6	29	-03.1	12	10	02.4	06	01.7	03	02.0	07	01.7	06	01.8	07	02.0	16	01.5	35			
V	-	11.7	20.8	13.8	15.0	22.0	08.0	30.0	20	01.4	29	08	02.2	05	02.0	02	02.0	02	01.0	02	02.0	11	01.7	11	01.2	25			
VI	-	14.9	23.9	16.0	20.4	25.4	10.6	32.5	14	01.6	04	05	01.6	.	03	01.7	03	01.0	04	02.5	13	01.1	13	01.7	17	01.9	32		
VII	-	15.9	24.9	17.8	15.1	26.7	13.0	32.3	14	05.0	02	03	02.3	04	02.5	01	02.0	01	02.0	09	01.9	11	01.6	20	01.7	42			
VIII	-	16.5	24.7	17.8	19.0	25.9	13.4	25.6	18	06.5	25	05	01.6	01	01.0	01	03.0	04	02.2	04	02.0	08	01.8	16	01.7	53			
IX	-	09.3	15.1	11.6	12.5	20.3	07.8	26.4	12	-00.6	25	09	02.9	06	02.3	01	02.0	.	01	01.0	02	01.0	03	01.0	18	01.7	50		
X	-	06.4	18.2	10.2	11.4	19.1	05.6	27.2	07	-01.1	04	04	02.2	04	01.5	.	.	02	01.5	06	02.7	07	01.3	19	01.8	51			
XI	-	04.0	11.0	06.6	06.7	12.6	02.3	25.4	12	-04.2	21	02	01.5	02	02.5	.	03	03.0	10	02.7	07	02.0	13	01.5	18	01.9	35		
XII	-	-01.9	01.4	-06.9	-00.6	02.9	-03.7	15.8	28	-16.0	06	08	01.4	06	01.3	04	01.5	03	01.7	08	02.2	07	01.0	06	01.0	11	01.5	40	
GOD.	-	07.6	16.0	09.6	10.8	17.4	05.1	32.5	44	-18.2	04	69	02.2	42	02.0	15	01.5	27	02.4	71	02.9	90	01.7	110	01.6	211	01.7	460	
$\Psi = 44^{\circ}59' N \lambda = 16^{\circ}45' E$ Gr. $\Delta G = +1h\ 07\ min.$																						PRIJEĆCR							
I	-	00.9	05.6	02.6	02.9	06.6	-00.4	16.8	12	-05.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	01.3	07.9	03.7	04.2	09.3	00.0	18.5	25	-13.0	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	04.9	15.0	11.7	10.8	17.0	03.3	26.9	30.29	-04.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	11.3	21.2	15.9	16.0	23.0	08.6	30.6	20	00.1	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	15.7	25.1	19.3	19.8	26.4	11.7	34.1	14	04.0	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	16.5	25.9	20.0	20.7	27.7	14.4	34.7	14	10.7	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	16.4	25.7	19.8	20.4	26.9	14.7	36.5	19	06.0	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IX	-	10.3	15.6	13.4	14.1	20.7	09.1	29.9	12	-00.9	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
X	-	07.8	17.8	11.9	12.4	19.2	06.9	26.4	07	01.5	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-	05.0	10.7	06.7	07.3	12.2	03.7	25.0	12	-03.4	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII	-	-01.6	00.9	-06.6	-00.5	02.2	-02.9	13.8	28	-16.4	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\Psi = 44^{\circ}16' N \lambda = 16^{\circ}52' E$ Gr. $\Delta G = +1h\ 07\ min.$																						BR. ST. 109							
I	-	-00.9	02.1	-00.7	-00.1	02.4	-04.4	08.5	25	-16.2	01	10	02.5	20	03.5	C1	09.0	09	04.7	08	02.4	08	03.2	10	02.8	09	03.7	18	
II	-	01.0	03.4	00.7	01.5	04.7	-02.2	13.0	24	-12.4	03	03	02.7	08	02.8	.	03	04.0	14	02.1	15	04.9	19	02.9	11	04.4	11		
III	-	01.7	09.9	03.7	04.7	10.5	-01.1	19.0	23	-11.4	03	03	02.0	16	02.8	08	02.0	09	03.0	12	01.9	07	02.1	07	02.7	17			
IV	-	03.4	09.0	03.5	04.8	09.8	-00.3	21.7	30	-06.4	11	02	02.5	06	03.2	01	04.0	04	02.0	25	03.0	13	02.5	12	02.4	14			
V	-	08.1	15.0	08.5	10.2	15.4	04.8	22.6	04	00.4	29	04	01.5	12	02.7	C1	05.0	07	02.4	16	01.7	09	03.2	08	02.1	11	02.8	25	
VI	-	13.5	17.6	12.0	13.7	18.4	08.0	26.8	11	00.6	02	05	02.0	12	02.8	02	02.5	07	02.6	20	02.0	04	02.2	09	02.1	09	02.3	22	
VII	-	14.8	20.8	13.3	15.5	21.2	09.5	26.4	21	06.0	02	02	0.5	22	07	02.4	02	02.0	23	03.0	15	01.9	06	03.0	11	02.8	04	01.5	25
VIII	-	14.5	19.3	13.3	15.0	20.2	09.4	26.3	30	04.8	05	02	02.5	03	02.7	C1													

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm		Broj dana naša:																									
	7	14	21		L m s			e <sub>m</sub> mm	Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	*	*	*	*	*													
					7	14	21											+	Δ	Δ	Δ														
DRINIĆ																																			
BR. ST. 106	$H_s = 730 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																		
I 6.0 7.5 6.5 7.5	-	05.1 50 69 89 90 61	114 025.6	30	01	03	18	.	.	.	.	.	.	.	01	16	14	12	04	11	04	.	.	04 16											
II 6.8 7.5 6.0 6.8	-	-	-	176 026.2	01	02	10	03	.	.	.	.	.	01	11	16	16	07	14	05	.	.	01 10												
III 4.4 5.4 4.5 4.8	-	-	-	109 045.3	13	-	-	.	.	.	.	.	.	10	08	08	07	03	05	03	.	.	02												
IV 6.1 6.6 6.0 6.2	-	06.1 83 72 78 77 30	140 036.9	15	-	12	01	.	.	.	.	.	.	03	10	11	09	05	08	08	02	.	.	01 01 07											
V 4.4 6.3 4.8 5.2	-	08.7 78 67 77 74 35	051 012.2	27	.	.	01	02	.	.	.	.	.	10	07	09	08	03	05	.	.	.	.	.											
VI 4.2 6.2 4.5 5.0	-	09.4 74 56 76 65 30	045 015.8	17	.	.	11	01	.	.	.	.	.	04	06	04	04	03	04	.	.	.	.	.											
VII 4.4 5.4 3.3 4.3	-	12.0 61 68 79 76 42	169 054.3	23	.	.	17	01	.	.	.	.	.	08	03	07	07	04	07	.	.	02	.	.											
VIII 5.8 6.6 3.7 5.3	-	12.5 66 73 86 81 49	087 026.7	24	.	.	14	.	.	.	.	.	.	07	07	12	11	03	12	.	.	.	03	.											
IX 4.6 5.2 4.0 4.6	-	09.0 89 80 88 85 64	120 045.7	20	.	.	02	04	.	.	.	.	.	11	08	11	10	04	11	.	.	.	.	.											
X 3.7 4.4 3.5 3.9	-	08.3 90 77 89 85 51	090 037.1	03	.	.	05	.	.	.	.	.	.	15	07	06	06	01	01	.	.	01 01	.	.											
XI 5.7 6.7 5.6 6.0	-	06.3 91 82 88 77 57	193 025.4	17	01	14	.	.	.	.	.	.	.	07	10	15	15	08	09	10	.	.	01	14											
XII 5.9 6.7 5.4 6.0	-	03.5 85 83 82 46 46	136 046.5	29	11	14	28	.	.	.	.	.	.	08	12	11	10	03	06	06	.	.	01 02 29												
GOD.	5.3 6.2 4.8 5.5	-	-	-	-	-	1430 054.3	25/V	-	21	-	49	02	-	.	.	87	105	124	115	52	102	37	03	.	.	06 09 78								
SANSKI MCST																																			
BR. ST. 107	$H_s = 158 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																		
I 5.1 6.3 7.0 8.1	051.0	051.1	89 73 87 83 42	044 008.2	27	.	01	14	.	.	04	.	.	19	16	13	14	02	.	.	.	.	06 07												
II 8.4 7.4 6.1 7.3	086.4	055.5	85 62 81 76 35	081 022.7	01	02	12	.	.	06	04	.	12	13	02	15	03	01	.	.	.	.	01 08 07												
III 6.6 6.1 3.9 5.5	173.3	06.0	93 44 80 73 19	082 035.0	13	.	12	02	.	.	01	04	06	10	05	03	16	02	02	.	.	.	05 02												
IV 7.2 6.4 5.2 6.2	176.8	06.6	93 52 85 77 19	098 034.8	15	.	08	04	.	02	02	08	12	09	03	12	.	.	.	.	.	.	03 01												
V 5.5 7.1 5.1 5.9	216.4	09.5	87 54 82 75 30	046 018.5	09	.	.	10	01	.	01	06	09	12	09	01	12	.	.	.	.	.	05 01												
VI 5.0 6.1 4.1 5.1	237.3	11.1	86 51 84 73 23	062 020.7	27	.	.	16	07	.	01	06	09	12	07	02	12	.	.	.	.	.	06 02												
VII 6.7 5.7 2.9 5.1	254.6	13.0	92 37 89 79 32	256 078.3	23	.	.	22	05	.	02	05	01	15	11	07	15	.	.	.	.	.	08 07												
VIII 6.1 6.5 4.3 5.4	188.1	13.5	93 60 80 81 40	079 026.9	24	.	.	23	01	05	06	12	06	03	12	.	.	.	.	.	.	04 10													
IX 8.2 6.2 4.3 6.2	168.3	05.5	97 59 93 83 32	093 030.0	20	.	.	01	05	.	01	01	02	10	11	05	04	11	.	.	.	.	01 14												
X 8.1 5.1 4.5 5.9	146.6	08.4	97 61 93 83 31	066 023.0	03	.	.	02	03	.	04	04	11	06	06	03	04	.	.	.	.	.	01 12												
XI 8.7 6.5 6.9 6.0	084.6	06.4	94 70 89 84 26	144 026.6	17	.	08	01	.	01	02	03	13	18	13	15	04	06	01	.	.	.	01 05 05												
XII 9.3 8.1 8.4 8.6	050.0	04.0	89 79 88 85 38	076 030.1	02	03	09	25	.	01	01	01	21	15	09	02	11	06	01	.	.	.	01 08 11												
GOD.	7.3 6.7 5.2 6.4	1836.8	08.2 91 60 86 79 19	1127 078.3	23/V	05	10	82	90	13	.	24	08	38	131	155	110	37	145	17	05	.	.	01 27 84 33											
PRIJEDOR																																			
BR. ST. 108	$H_s = 135 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																		
I 9.3 6.4 9.1 8.9	-	04.7 82 75 83 37	042 007.5	27	.	02	18	.	.	09	04	.	22	12	10	11	01	.	.	.	.	08 08													
II 7.2 6.1 6.5 6.6	-	04.3 83 56 70 21	072 021.7	01	01	02	15	.	.	02	10	12	12	01	03	01	.	.	.	.	.	01 03 07													
III -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.													
IV 4.5 4.1 4.9 4.5	-	-	-	-	-	-	-	080 020.7	15	.	07	04	.	01	01	11	06	09	09	03	.	.	05												
V 2.8 2.5 3.1 2.8	-	-	-	-	-	-	-	052 019.8	09	.	11	03	.	13	02	09	09	01	05	01	.	.	.												
VI 2.7 3.6 4.1 3.5	-	10.8 83 44 66 24	034 013.4	23	.	.	15	10	.	12	02	06	06	01	08	.	.	.	.	.	.	05													
VII 4.0 3.0 3.4 3.5	-	12.2 86 51 68 69 26	183 044.9	23	.	.	24	10	.	13	04	10	08	06	01	06	04	05	01	.	.	.													
VIII 4.8 3.8 3.6 4.1	-	-	-	-	-	-	-	084 046.2	24	.	04	20	.	11	03	10	06	02	10	.	.	04 11													
IX 3.8 2.6 3.2 3.2	-	-	-	-	-	-	-	108 029.0	20	.	10	.	01	01	15	04	09	08	05	04	.	.	.												
X 8.7 4.5 5.3 6.2	-	07.8 85 56 79 73 27	060 026.2	03	.	04	.	02	01	03	11	06	03	06	03	06	02	01	02	01	.	.													
XI 8.1 8.4 7.0 7.3	-	07.2 86 80 83 50	092 027.0	17	.	05	01	.	02	01	12	11	04	09	03	02	01	01	08	.	.	.													
XII 9.3 9.3 9.5 9.4	-	03.9 86 80 83 50	093 027.0	02	02	08	21	.	.	04	09	13	10	04	11	06	05	02	01	01	05	-													
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.													
MLINISTE																																			
BR. ST. 109	$H_s = 970 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																		
I 7.5 8.0 7.0 7.6	-	03.5 81 77 82 80 52	141 025.6	12	05	04	23	.	.	07	03	01	17	18	17	05	14	11	06	.	.	05													
II 7.6 7.5 6.4 7.2	-	04.0 74 73 77 75 53	224 025.1	27	04	03	14	.	.	07	03	.	14	19	15	08	15	11	07	.	.	.													
III 4.5 4.2 4.6 4.5	-	-	-	-	-	-	-	163 036.3	14	02	02	15	.	02	10	07	09	07	05	.	.	01 01													
IV 6.7 6.5 5.4 5.4	-	05.2 78 68 80 75 53	203 035.3	15	.	16	.	.	03	07	08	16	15	06	05	12	05	.	.	.	09 16														
V 4.5 5.2 5.0 5.0	-	04.5 68 61 70 66 47	006 028.8	15	.	.	.	.	.	06	07	12	10	04	12	.	.	.	.	.	.	01 08													
VI 4.6 5.5 5.7 5.2	-	07.8 61 58 67 62 44	075 030.0	17	.	05	04	.	02	01	05	06	07	06	02	10																			

1977

Mjesec	Vazdušni pritisk Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra nD, Pm (0-12)																	
		Tm			Sred. (Dies)	Max	Min	Max	Min	Dat.	Max	N	NE	E	SE	S	SW	W	NW	C									
		7	14	21								8.	1.	8.	1.	8.	1.	8.	1.	8.	1.								
$\varphi = 44^{\circ}47' N$ $\lambda = 17^{\circ}13' E$ Gr. $\Delta G = +1h\ 09\ min.$												BANJA LUKA																	
I	748.7	01.1	06.3	03.0	03.4	07.2	-00.4	16.2	25	-06.2	01	28	01.3	29	01.2	05	01.8	01	01.0	05	03.4	07	01.7	06					
II	746.6	04.7	10.2	05.7	06.5	11.6	01.9	21.2	25	-14.7	04	10	01.7	17	01.4	03	01.7	12	02.8	16	03.4	11	02.5	14					
III	751.4	04.3	16.0	08.7	09.4	17.2	02.5	25.6	23	-05.8	01	17	02.1	17	01.6	07	01.4	08	01.6	11	01.6	08	02.1	12					
IV	747.1	06.4	15.0	09.2	09.9	16.7	03.3	29.1	29	-03.2	12	15	01.1	24	01.6	04	02.2	04	01.2	07	01.1	06	02.5	15					
V	748.3	12.9	21.2	14.6	15.9	22.7	06.2	25.2	04	02.8	29	14	01.5	09	01.4	14	01.6	13	01.4	14	01.6	05	01.6	10					
VI	747.2	17.0	24.5	18.1	19.4	24.0	11.9	33.3	14.1	02.6	04	07	01.9	13	01.5	11	01.0	16	01.3	04	01.0	15	01.9	09	01.8	05			
VII	747.2	17.3	25.6	16.6	20.0	27.2	13.3	33.2	14	08.7	28	12	02.0	19	01.5	06	01.7	15	01.1	13	01.4	03	02.9	07	03.0	13	01.2	05	
VIII	747.1	16.6	25.0	18.3	19.6	26.3	13.3	30.0	18	06.8	26	10	01.6	20	01.6	13	01.2	08	01.1	13	01.5	06	01.7	11	01.5	05			
IX	752.3	10.1	19.5	11.8	13.3	20.7	07.8	29.5	09	-01.0	29	10	02.1	13	01.8	18	02.1	11	01.2	04	01.2	05	01.2	10	01.2	09	01.6	10	
X	752.8	18.2	18.0	11.3	11.7	19.1	06.0	27.2	07	-00.8	04	14	02.1	13	01.7	11	01.8	07	01.3	04	01.5	05	02.0	13	01.8	20	01.2	06	
XI	747.2	04.3	10.9	06.1	06.9	12.3	02.7	26.2	12	-04.6	25.2	12	01.7	19	01.5	13	01.3	08	01.8	08	02.8	15	02.3	06	01.2	01			
XII	754.3	-02.2	01.4	-01.3	-00.9	02.1	-03.9	13.0	28	-16.2	06	14	01.6	34	01.2	14	01.1	03	01.7	08	02.0	07	01.6	09	01.3	02			
GOD.	749.2	08.4	16.2	10.3	11.3	17.4	05.6	33.3	44.VI	-16.2	06.XI	163	01.7	227	01.5	119	01.5	54	01.2	109	01.8	75	02.4	130	02.0	122	01.5	56	
$\varphi = 44^{\circ}21' N$ $\lambda = 17^{\circ}16' E$ Gr. $\Delta G = +1h\ 09\ min.$												JAJCE										BR. ST. 112							
I	-	01.1	06.6	03.3	03.8	07.3	-00.5	14.2	29	-11.4	01	03	04.3	01	02.0	-	-	03	04.0	02	03.0	08	02.2	05	03.6	04	04.0	67	
II	-	04.1	09.1	06.1	06.4	10.8	06.9	20.8	24	-06.6	28	03	03.7	05	03.4	04	03.0	01	06.0	02	03.5	02	05.0	08	03.6	05	04.2	54	
III	-	04.0	15.5	09.3	09.5	16.7	02.1	26.4	23	-05.8	01	01	02.0	05	01.8	01	03.0	01	01.0	01	01.0	01	01.0	01	01.0	72			
IV	-	05.8	14.8	09.0	09.7	16.1	02.7	28.8	30	-02.6	18.12	-	-	05	03.8	02	02.0	-	-	03	01.0	06	02.5	06	03.3	04	02.5	64	
V	-	11.2	20.2	14.4	15.0	21.7	08.1	29.0	20	02.0	29	03	03.0	06	02.3	04	01.5	-	-	08	02.6	12	02.4	03	02.0	57			
VI	-	14.5	23.1	17.0	17.9	24.5	10.6	31.4	13	03.4	04	02	02.0	05	03.2	06	02.3	-	-	04	02.5	05	01.2	01	01.0	67			
VII	-	15.2	24.4	16.2	19.0	26.6	12.8	32.2	30	08.6	07	01	02.0	04	02.0	03	01.3	02	02.5	02	03.0	06	03.2	09	02.7	01	01.0	65	
VIII	-	15.0	24.0	17.4	18.4	25.6	12.8	25.8	30	07.0	26	01	01.5	01	01.0	00	01.0	-	-	08	03.2	04	02.8	01	02.0	76			
IX	-	09.4	18.0	12.4	13.0	19.2	08.1	28.6	29	01.0	01.0	04	03.0	01	02.0	-	-	-	06	02.0	06	02.3	-	-	72				
X	-	07.0	17.9	10.5	11.5	18.6	05.6	24.6	06	01.0	05.04	01	02.0	-	-	-	-	-	05	02.8	03	02.3	-	-	84				
XI	-	04.0	09.4	05.9	06.3	11.4	01.9	23.2	12	-05.4	21	-	-	05	03.8	02	05.0	-	01	02.0	03	01.7	04	03.2	01	01.0	75		
XII	-	-02.5	00.8	-01.5	-01.2	01.8	-04.5	12.2	29	-15.4	06	02	03.0	02	03.5	05	02.4	01	02.0	02	04.0	03	03.5	01	03.0	79			
GOD.	-	07.4	15.3	10.2	10.8	16.7	05.0	32.2	30.VII	-15.4	06.XI	19	02.8	43	02.9	29	02.3	08	03.2	13	02.2	63	02.7	73	02.7	21	03.1	826	
$\varphi = 44^{\circ}00' N$ $\lambda = 17^{\circ}17' E$ Gr. $\Delta G = +1h\ 09\ min.$												KLIPRES										BR. ST. 113							
I	-	-02.5	00.4	-01.1	-01.1	01.4	-04.6	08.0	25	-16.4	01	16	02.2	-	-	-	-	-	25	03.1	-	-	-	-	-	-	-	42	
II	-	-00.9	02.1	00.9	00.9	04.5	-02.8	12.0	24	-15.2	04	17	07.5	-	-	-	-	-	42	03.8	-	-	01	04.6	-	-	-	24	
III	-	04.4	10.1	04.6	04.5	11.1	-01.2	18.8	26	-10.2	01	21	02.5	-	-	-	-	-	30	02.3	-	-	01	02.0	-	-	-	40	
IV	-	02.1	08.5	04.2	04.7	09.7	05.8	20.5	30	-05.4	18	31	01.3	-	-	-	-	-	35	03.5	-	-	62	02.0	-	-	-	21	
V	-	10.4	15.6	10.4	10.7	16.8	03.6	23.2	04	-02.0	30	20	02.1	-	-	-	-	-	41	02.7	-	-	-	-	-	-	-	32	
VI	-	16.0	17.0	12.8	12.8	18.7	06.2	26.2	11	02.4	02	34	02.3	01	02.0	-	-	-	13	02.2	-	-	03	02.7	-	-	-	39	
VII	-	11.9	20.7	13.4	14.8	21.5	07.8	26.2	30	04.0	07	03	02.0	-	-	-	-	-	01	02.0	0.0	07	10	03.2	-	-	-	18	
VIII	-	10.7	19.4	13.5	14.3	21.0	07.3	29.2	30	01.8	26	17	02.5	01	02.0	-	-	-	37	03.2	-	-	02	02.0	-	-	-	36	
IX	-	05.7	14.1	08.8	09.3	15.3	03.6	23.8	12	-03.6	30	42	02.9	-	-	-	-	-	12	02.8	-	-	-	-	-	-	-	36	
X	-	03.0	14.1	07.5	08.0	15.2	01.2	19.2	28.4	16.0	20.8	18	02.3	-	-	-	-	-	21	02.5	-	-	05	02.4	-	-	-	49	
XI	-	-00.5	05.7	02.0	02.3	07.4	-03.1	19.0	11	-16.2	21	32	02.3	-	-	-	-	-	18	03.1	-	-	04	02.0	-	-	-	40	
XII	-	-06.0	-00.3	-04.4	-03.8	00.1	-08.0	05.2	29.0	-16.2	13	-	-	-	-	-	-	-	24	02.1	-	-	-	-	-	-	-	31	
GOD.	-	03.4	10.7	06.0	06.5	11.9	00.8	29.2	30.VII	-16.4	01.1	251	02.3	02	02.0	02	03.0	01	02.0	378	03.1	-	-	15	02.4	-	-	-	408
$\varphi = 44^{\circ}38' N$ $\lambda = 17^{\circ}23' E$ Gr. $\Delta G = +1h\ 10\ min.$												KOTOR VAROS										BR. ST. 114							
I	-	01.5	07.2	03.1	03.7	08.4	-01.1	19.0	29	-12.5	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	04.5	10.3	06.4	06.7	11.8	01.4	21.5	25	-15.0	04	02	04.0	-	-	-	-	-	27	04.9	-	-	-	-	-	-	-	55	
III	-	03.4	16.1	07.7	08.8	17.6	01.6	28.5	23	-03.5	01	08	03.2	-	-	-	-	-	01	03.0	-	-	-	-	-	-	-	84	
IV	-	05.0	15.1	08.6	09.2	16.4	02.4	29.5	29	-04.0	12	07	03.7	-	-														



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Mesec	Vrstdišni Pritisak Pm mm	Temperatura vazduha °C						Cestina pravaca i srednja jačina veta nD, Fm (0-12)																					
		Tm			Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
$\gamma = 44^{\circ}14' N \lambda = 17^{\circ}40' E$ Gr. $\Delta G = +1h\ 11min$																													
I	-	00.2	04.7	01.8	02.0	06.1	-01.5	13.2	26	-13.6	01	.	.	07	02.1	03	02.7	02	01.5	C1	03.0	06	02.8	.	.	03	C2.0	71	
II	-	02.9	08.6	04.6	05.2	09.5	00.6	15.6	24	-04.0	04	.	.	10	02.0	03	02.4	05	02.4	.	15	03.1	01	02.0	05	02.2	45		
III	-	02.9	14.0	06.8	07.6	15.2	01.4	26.0	25	-04.2	01	.	.	06	01.5	04	02.2	04	02.5	02	01.0	07	02.0	01	02.0	01	02.0	68	
IV	-	04.6	13.5	07.5	06.3	15.0	02.0	25.2	30	-04.0	18	.	.	06	01.8	01	02.0	13	02.2	02	02.0	11	01.9	02	02.5	.	.	55	
V	-	10.2	15.5	11.3	13.1	20.7	07.2	29.4	20	00.2	30	.	.	04	01.8	.	.	15	01.3	.	.	10	02.3	01	02.0	.	.	63	
VI	-	12.3	21.3	14.5	15.7	22.7	05.2	30.0	11	02.5	04	01	02.0	03	02.0	.	.	15	01.5	C1	01.0	06	02.0	.	.	01	02.0	63	
VII	-	14.1	24.4	18.3	17.8	25.8	11.5	34.5	21	08.0	07.0	03	.	04	02.5	.	.	12	01.6	05	01.0	12	02.3	01	02.0	03	02.0	56	
VIII	-	12.9	23.2	15.1	16.6	24.6	10.9	35.5	27	04.5	26	.	.	08	01.9	02	03.0	02	01.5	02	01.0	09	02.2	01	03.0	.	.	69	
IX	-	08.0	16.9	10.4	11.4	19.5	06.2	30.5	08	-02.8	30	.	.	03	02.0	.	.	08	01.6	01	01.0	05	02.0	02	02.0	.	.	71	
X	-	05.6	15.7	08.6	09.7	17.2	04.0	23.0	09	-02.0	04	.	.	01	02.0	.	.	05	01.7	*	.	08	01.6	01	02.0	.	.	74	
XI	-	02.9	07.7	03.7	04.5	09.2	00.4	19.4	04	-06.0	21	.	.	07	02.0	01	02.0	07	01.7	.	.	08	01.8	02	02.5	03	02.0	62	
XII	-	-04.5	-00.9	-03.7	-03.2	00.4	-08.6	10.0	29.8	-18.2	06	01	01.0	01	02.0	01	02.0	12	01.3	03	01.7	04	02.8	02	02.0	.	.	69	
GOD.	-	06.0	14.0	08.1	09.1	15.5	03.7	35.5	27	VIII	-18.2	06.XX	02	01.5	60	01.9	15	02.3	104	01.7	17	01.4	101	02.3	14	02.2	16	C2.1	766
$\gamma = 44^{\circ}52' N \lambda = 17^{\circ}42' E$ Gr. $\Delta G = +1h\ 11min$																									PRNJAVA		BR. ST. 117		
I	-	00.0	04.9	01.6	02.0	05.8	-01.5	16.0	12	-11.6	01	10	01.2	18	C1.3	16	01.2	05	01.0	13	01.2	24	01.7	04	01.2	03	C1.0	.	
II	-	03.5	10.1	05.4	06.1	11.4	01.4	21.0	25	-16.2	04	03	01.7	05	01.3	14	01.6	06	01.7	27	01.6	26	01.8	*	.	01	01.0	25	
III	-	04.3	15.0	08.4	09.0	16.0	02.9	26.5	23	-03.2	01	12	01.3	05	01.0	15	01.1	*	.	19	01.1	15	01.5	01	01.0	01	01.0	.	
IV	-	05.4	14.7	08.6	09.4	16.1	03.7	26.0	29	-01.8	18	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	
V	-	12.5	21.0	14.1	15.4	21.9	09.8	29.5	04	04.8	29	08	01.1	67	01.1	14	01.2	01	01.0	12	01.0	21	01.0	03	01.0	01	01.0	26	
VI	-	14.8	24.5	17.4	19.0	25.3	12.5	33.0	14	02.6	04	04	01.0	04	01.0	10	01.1	02	01.5	17	01.0	23	01.1	04	01.5	*	.	26	
VII	-	17.3	25.5	18.2	19.8	26.6	13.6	32.5	14	05.6	26	08	01.0	04	04.5	01.0	01.0	11	01.2	22	01.2	04	01.8	02	01.0	36			
VIII	-	16.0	25.1	17.9	19.2	26.0	13.5	30.0	09	06.6	26	02	01.0	04	01.0	10	01.2	17	01.1	19	01.2	*	.	.	.	.	.	36	
IX	-	10.1	19.3	11.3	13.0	20.3	07.8	29.0	09	-03.0	29	07	01.3	08	01.1	10	01.0	01	01.0	11	01.1	22	01.2	04	01.8	01	02.0	26	
X	-	17.8	20.5	10.9	18.2	05.4	25.0	08.0	-01.2	18	10	01.0	11	01.0	08	01.2	04	01.5	16	01.1	20	01.1	03	01.0	01	01.0	22		
XI	-	03.1	09.7	04.9	05.6	10.7	01.7	25.0	21	07	01.0	21	01.1	13	01.2	03	01.0	12	01.1	24	01.2	02	02.0	*	.	08			
XII	-	-02.5	00.2	-01.7	-01.4	01.0	-04.2	06.0	06	31.0	25.0	06	01.0	12	01.1	07	01.4	06	01.0	16	01.0	26	01.2	03	01.3	02	01.0	04	
GOD.	-	07.8	15.6	09.7	10.7	16.6	05.6	33.0	44.VI	-20.6	06.XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\gamma = 44^{\circ}36' N \lambda = 17^{\circ}54' E$ Gr. $\Delta G = +1h\ 11min$																									TESLIC		BR. ST. 118		
I	-	00.5	06.6	02.7	03.1	07.3	-01.3	17.4	30	-12.6	15	10	01.2	.	.	.	.	.	04	02.5	03	02.3	04	01.2	.	.	.	72	
II	-	03.2	09.9	05.0	05.8	11.2	01.6	18.4	25	-10.0	04	04	01.2	.	.	.	.	.	03	02.0	08	03.0	C5	02.0	02	02.0	.	62	
III	-	03.5	15.7	07.9	08.7	16.6	02.1	27.7	24	-05.2	01	14	01.2	01	01.0	.	.	.	.	03	02.0	06	01.3	01	01.0	68			
IV	-	04.6	14.5	07.7	08.6	15.3	02.9	29.4	30	-02.2	18.12	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.		
V	-	10.7	21.5	13.6	14.9	22.4	08.7	31.0	20	02.4	29	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.		
VI	-	14.0	23.3	15.6	17.2	24.1	12.0	33.4	14	04.0	03	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.		
VII	-	15.4	25.0	17.3	18.7	25.5	13.0	32.6	09	05.2	26	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	65		
VIII	-	14.4	24.3	17.3	18.4	25.5	12.9	32.6	26	01.2	26	04	01.2	.	.	.	.	.	01	02.0	01	01.0	02	01.0	.	.	.		
IX	-	09.4	18.4	11.4	12.7	19.3	07.5	29.0	09	-01.0	30	06	01.5	08	.	.	.	.	.	.	.	.	05	01.4	01	02.0	78		
X	-	06.1	18.0	10.5	11.5	18.6	04.6	25.6	08	-02.0	19	12	01.0	.	.	.	.	.	.	.	.	06	01.2	*	.	75			
XI	-	03.6	10.0	04.8	05.8	11.3	01.5	24.2	12	-05.6	21	26	01.4	.	.	.	.	.	C1	02.0	.	.	01	02.0	.	.	62		
XII	-	-02.9	00.5	-01.6	01.2	-04.4	10.6	28	-21.0	06	26	01.4	.	.	.	.	.	.	.	.	.	.	.	.	.	67			
GOD.	-	06.9	15.7	09.4	10.3	16.6	05.1	32.4	24.VII	-16.6	06.XT	50	02.7	08	02.2	*	*	04	03.0	33	03.0	28	02.7	04	02.2	10	C2.6	958	
$\gamma = 44^{\circ}44' N \lambda = 18^{\circ}06' E$ Gr. $\Delta G = +1h\ 12 min$																									CCBČJ		BR. ST. 120		
I	-	01.2	06.6	02.3	03.1	07.4	-00.4	16.2	25	-0.4	19	01	02.0	02	01.0	13	01.5	12	01.6	C2	02.0	03	01.3	06	02.0	10	01.3	44	
II	-	04.6	05.0	06.4	12.2	01.7	22.2	25	-11.2	04	02	01.0	04	01.8	01	02.0	06	02.0	04	02.8	08	02.6	04	02.0	08	01.8	47		
III	-	05.2	16.3	08.5	09.6	17.0	03.3	29.0	24	-0.4	01	02	02.0	04	01.5	05	01.8</td												

Meseč	Oblačnost Nm (0-10)			Insekcija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																				
	7	14	21		Sredn. Sredn. Min.	mm	m	%	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	□	■					
					mm	7	14	21	(Sredn.)	Min.	Max	Dat.		10.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.0	0.0	9	Δ	*	□	■			
<b>BR. ST. 116</b>																															
I	8.6	6.0	6.8	7.8	-	04.6	53	73	85	84	41	073	016.0	30	02	02	18	.	.	.	.	02	19	13	11	02	16	05	02		
II	7.6	7.5	7.7	7.2	-	05.2	87	65	81	78	27	114	017.4	11	.	01	15	.	.	.	.	02	16	15	05	15	03	.	.		
III	4.5	4.0	4.3	4.8	-	05.8	85	55	80	75	20	042	011.4	31	.	.	12	03	.	.	.	.	05	09	08	06	01	06	04	02	
IV	7.1	5.7	6.1	6.3	-	05.8	84	52	77	71	23	081	022.0	06	.	.	08	02	.	.	.	.	05	11	16	11	03	15	07	05	
V	5.9	6.9	6.5	6.4	-	05.2	85	45	84	73	28	048	014.5	10	.	.	08	.	.	.	.	04	15	13	06	02	11	.	.		
VI	4.1	6.1	5.5	5.2	-	09.8	89	55	79	74	23	051	012.5	26	.	.	11	01	.	.	.	.	08	05	10	09	01	16	.	.	
VII	4.6	4.7	4.4	4.6	-	11.1	50	53	83	74	25	125	020.4	11	.	.	21	02	.	.	.	.	07	06	13	10	04	13	.	.	
VIII	5.6	5.1	4.4	5.1	-	11.3	91	57	89	79	19	136	037.5	22	.	.	14	01	.	.	.	.	05	07	13	10	05	13	04	.	
IX	6.5	5.5	5.8	5.9	-	06.6	95	65	88	83	34	169	029.0	14	.	.	02	06	02	.	.	.	05	11	14	14	07	14	.	.	
X	5.1	3.7	3.8	4.2	-	07.5	95	62	88	82	31	099	033.5	11	.	04	.	.	.	.	.	14	10	05	05	03	05	.	.		
XI	5.5	5.5	5.4	5.5	-	05.9	94	79	94	89	47	157	044.0	17	01	13	.	.	.	.	.	01	15	12	12	05	10	02	.		
XII	9.4	7.5	7.4	8.1	-	03.6	95	86	90	90	56	073	019.0	01	10	14	26	.	.	.	.	01	21	12	12	03	08	05	.		
GOD.	6.3	5.5	5.5	5.9	-	07.3	90	62	84	79	19	1168	044.0	47	XI	12	18	98	67	06	.	.	.	61	144	146	119	41	127	34	11
<b>BR. ST. 117</b>																															
<b>PRAJAVCR</b>																															
I	8.9	8.4	7.6	8.3	-	04.3	83	73	82	80	26	053	018.5	28	01	02	20	.	.	.	.	20	14	13	02	12	02	.	.		
II	8.3	8.1	4.7	7.0	-	05.2	76	64	72	71	19	129	022.0	15	01	01	07	.	.	.	.	01	07	14	13	05	12	03	.		
III	6.2	5.9	3.7	5.3	-	06.0	80	51	74	69	22	048	013.5	21	.	06	02	.	.	.	.	03	08	08	01	02	08	02	.		
IV	6.3	6.1	5.0	5.8	-	06.8	80	62	79	74	36	075	019.5	06	.	.	02	02	.	.	.	03	08	11	10	03	11	.	.		
V	6.6	6.3	4.9	5.8	-	09.0	74	51	79	68	29	067	016.5	16	.	.	10	.	.	.	.	01	08	11	11	02	11	.	.		
VI	4.1	5.3	5.6	5.0	-	12.0	78	54	81	71	25	077	019.4	18	.	.	16	07	.	.	.	03	C6	13	12	03	13	.	01	12	
VII	5.4	4.9	3.7	4.7	-	13.1	90	56	81	76	35	133	045.6	23	.	.	23	06	.	.	.	04	05	11	10	05	11	.	06		
VIII	5.6	5.2	4.2	5.0	-	12.7	85	58	81	75	39	105	054.6	06	.	.	23	01	.	.	.	05	05	09	08	03	09	.	01		
IX	5.2	5.6	4.6	5.2	-	09.0	86	62	62	77	34	054	018.0	18	.	.	01	10	.	.	.	07	08	09	09	02	09	.	02		
X	6.2	5.6	5.1	5.3	-	07.5	84	61	79	75	27	064	025.0	03	.	.	02	04	.	.	.	09	10	06	05	03	06	.	01		
XI	6.7	7.0	5.8	7.2	-	06.1	92	76	89	86	39	157	028.0	02	.	.	11	01	.	.	.	01	14	14	14	06	11	04	.		
XII	8.9	6.5	8.9	8.7	-	03.7	75	85	90	85	-	116	030.6	02	03	12	26	.	.	.	02	23	17	16	05	14	04	.			
GOD.	6.7	6.3	5.3	6.1	-	08.0	82	62	80	75	-	1088	054.5	06	XVII	05	15	75	91	14	.	.	.	39	122	137	128	41	127	15	02
<b>BR. ST. 118</b>																															
<b>TESELIC</b>																															
I	7.6	7.6	8.0	7.8	-	05.2	91	82	89	88	26	035	008.8	16	03	04	19	.	.	.	.	01	17	12	09	01	11	02	.		
II	7.7	7.3	7.0	7.3	-	36.2	92	77	91	87	47	085	021.6	15	01	02	09	.	.	.	.	12	13	13	01	12	03	.	.		
III	4.6	5.4	3.4	4.6	-	04.5	52	55	90	79	15	056	016.4	14	.	.	10	02	.	.	.	10	07	10	06	02	05	03	.		
IV	5.9	5.6	5.9	6.1	-	07.3	91	72	90	84	23	119	030.6	16	.	06	04	04	.	.	.	05	11	13	05	03	13	01	.		
V	5.6	6.1	6.0	5.9	-	10.1	90	55	87	70	30	036	012.4	28	.	.	11	01	.	.	.	05	12	09	09	01	09	.	.		
VI	4.7	6.7	5.0	5.4	-	12.0	91	60	91	81	19	104	026.4	28	.	.	13	06	.	.	.	04	06	06	05	09	05	06	.		
VII	5.3	6.2	4.7	5.4	-	13.6	53	63	94	83	31	136	056.4	23	.	.	19	03	.	.	.	07	12	09	04	12	12	.	.		
VIII	4.7	5.8	5.3	5.3	-	13.0	92	61	92	82	42	056	015.4	24	.	.	23	01	.	.	.	07	36	12	07	03	12	02	.		
IX	5.5	6.4	5.2	5.7	-	10.1	53	76	92	87	41	069	021.6	15	.	02	08	.	.	.	06	12	09	09	03	12	02	.			
X	5.0	4.8	4.2	4.7	-	05.9	94	73	92	86	45	053	019.2	03	.	.	06	01	01	.	.	09	05	06	05	02	06	.	.		
XI	6.4	7.4	6.1	6.7	-	06.7	93	53	64	91	54	119	029.4	26	.	.	12	01	.	.	.	04	16	13	13	05	10	05	.		
XII	8.4	7.9	7.5	7.9	-	04.0	91	93	91	62	68	074	020.4	02	04	14	24	.	.	.	19	10	09	03	06	05	05	.			
GOD.	6.0	6.6	5.7	6.1	-	08.6	51	71	91	84	15	951	058.4	23	XVII	08	20	88	81	10	.	.	.	58	135	131	106	34	121	15	.
<b>ZENICA</b>																															
I	7.4	7.5	6.4	7.1	045.9	05.0	51	65	88	83	42	046	017.0	13	01	01	18	.	.	.	.	01	12	16	05	01	14	02	.		
II	7.5	7.2	6.4	7.0	085.5	05.5	87	60	82	76	30	055	011.3	27	.	01	12	02	.	.	.	07	10	14	13	01	12	03	.		
III	5.4	6.1	4.2	5.2	175.9	05.4	85	43	73	67	17	044	015.2	14	.	.	09	02	.	.	.	06	06	10	04	08	03	02	.		
IV	7.1	6.0	5.4	6.5	162.3	05.1	65	77	63	46	178	078.4	06	.	04	05	.	01	.	.	.	03	10	17	09	04	17	01	.		
V	6.2	6.9	4.2	5.8	168.3	05.8	61	47	77	66	23	042	010.7	10	.	.	06	01	01	01	.	02	05	12	07	01	12	02	.		
VI	4.8	6.7	4.5	5.3	182.2	10.2	59	62	50	76	69	44	22	006.6	25	.	.	13	06	.	.	.	05	09	08	06	08	06	08	.	
VII	5.4	4.8	4.9	5.4	255.4	10.2	59	62	51	71	35	116	036.9	11	.	.	25	08	.	.	.	06	03	11	11	03	11	01	.		
VIII	7.7	5.4	5.1	5.4	188.3	12.4	91	52	66	76	32																				

Mesec	Vazdušni pritisk Fm mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina vетра nD, Fm (0-12)																				
		Tm				Max.				Min.				N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dnes)	Max.	Min.	Max.	Min.	Dat.	Min.	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.		
$\varphi = 44^{\circ}39' N \lambda = 18^{\circ}18' E$ Gr. $\Delta G = +1 h 13 min.$														MEDRICA		BR. ST. 121														
I	-	00.1	04.6	01.9	02.1	05.4	-01.3	14.2	12	-11.2	01	08	01.4	05	01.2	08	01.4	10	01.4	01	01.0	05	02.0	03	01.0	11	01.5	42		
II	-	04.3	05.9	05.6	06.4	11.2	01.6	20.5	25	-16.5	04	13	01.5	04	02.0	01	01.0	04	01.6	05	01.7	12	02.0	10	01.5	10	02.0	24		
III	-	14.7	17.7	08.5	09.2	15.7	03.1	26.8	24	-04.8	01	10	01.7	10	01.7	15	02.2	09	01.9	*	*	04	01.8	11	01.5	12	01.9	32		
IV	-	07.3	14.5	09.4	10.2	15.5	04.1	27.3	29	-01.0	22	02.6	06	01.7	09	02.0	04	02.2	*	*	03	01.3	07	01.6	21	02.2	28			
V	-	14.5	21.1	15.5	16.9	21.8	09.8	30.1	04	05.7	25	10	01.5	05	01.8	05	02.6	07	01.4	02	02.0	08	01.6	11	01.5	16	01.6	27		
VI	-	18.2	24.6	18.5	20.1	25.1	11.8	32.7	14	04.2	04	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*		
VII	-	18.6	24.9	19.2	20.5	26.0	13.1	31.6	14	07.1	23	18	01.9	05	01.4	06	02.3	05	01.4	*	*	*	*	09	01.3	26	02.0	34		
VIII	-	17.2	25.2	19.4	20.3	25.5	14.1	25.6	18	07.5	04	03	01.0	06	01.8	08	01.6	01	01.0	*	*	02	01.0	18	01.3	17	01.5	38		
IX	-	11.0	19.1	13.2	14.2	19.9	08.6	28.4	08	-00.1	25	09	02.1	13	01.9	10	01.6	01	02.0	*	*	06	01.2	09	01.2	17	01.5	25		
X	-	08.4	17.3	10.2	11.4	17.6	06.2	25.8	07	06.5	18.17	09	01.4	04	01.8	14	01.6	07	01.6	05	01.4	11	01.5	36	*	*				
XI	-	03.9	09.5	05.5	06.5	10.6	02.6	23.8	11	-05.8	25	10	01.8	05	01.6	06	02.0	04	02.0	01	01.0	01	01.0	23	01.7	09	01.2	31		
XII	-	-02.6	06.3	-01.6	-01.6	00.6	-04.3	08.0	27	-20.0	04	13	01.2	01	02.0	10	01.7	11	02.0	01	01.0	05	01.2	29	01.7	03	02.3	20		
GOD.	-	08.8	15.5	10.5	11.3	14.3	05.8	32.7	44.VI	-20.0	00.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 44^{\circ}11' N \lambda = 18^{\circ}22' E$ Gr. $\Delta G = +1 h 14 min.$														PENIKVE		BR. ST. 122														
I	-	-01.4	03.1	-00.6	00.1	-	-	-	-	-	14	03.7	*	*	03	03.3	*	*	08	04.4	02	05.5	25	03.5	*	*	41			
II	-	01.2	C6.1	C1.1	02.9	07.8	-00.3	18.4	25	-11.0	04	15	03.5	*	01	03.0	*	*	12	04.4	*	*	15	04.2	*	*	41			
III	-	03.4	12.6	05.3	04.7	13.9	02.2	24.0	25	-06.6	01	10	03.6	*	05	03.0	*	*	03	03.0	*	*	16	03.5	*	*	60			
IV	-	03.2	10.9	05.0	06.0	12.2	01.2	25.0	30	-05.0	18	20	03.7	*	01	03.0	*	*	05	03.4	*	*	15	03.5	*	*	49			
V	-	09.1	16.3	10.3	11.5	17.9	07.9	26.0	20	02.5	25	08	03.4	*	*	*	*	*	*	*	*	*	22	03.8	*	*	63			
VI	-	13.3	15.3	12.4	14.3	21.8	10.6	29.4	15.11	04.6	07	03	01.3	*	01	03.0	*	*	*	*	*	*	23	02.0	*	*	64			
VII	-	14.3	23.2	16.0	16.9	24.7	13.2	25.4	10.08	09.0	02	14	01.6	06	02.0	04	02.0	01	01.0	05	01.4	21	01.2	28	*	*				
VIII	-	14.1	21.7	15.0	16.4	23.1	12.8	31.0	30	08.0	24	04	03.2	*	04	02.8	*	*	*	*	*	*	21	02.5	02	04.0	62			
IX	-	07.9	16.8	10.6	18.4	07.3	25.5	01	-04.4	29	10	02.5	*	*	01	03.0	*	*	*	*	*	*	22	03.0	*	*	57			
X	-	05.2	14.9	07.7	08.9	16.4	03.7	20.0	23	-01.8	17	05	02.2	*	02	02.5	01	01.0	*	*	14	02.4	*	*	71					
XI	-	00.3	06.0	01.0	02.1	08.1	-01.8	16.4	06.01	-12.8	21	06	01.0	05	02.0	*	01	03.0	*	*	*	*	27	01.7	01	02.0	50			
XII	-	-05.4	-02.5	-04.8	-04.4	-02.0	-08.1	07.0	28	-18.5	05	04	02.0	01	01.0	*	*	*	*	*	*	*	10	01.7	04	01.8	74			
GOD.	-	05.4	12.4	06.4	07.7	-	-	-	-	91	03.1	-	-	26	03.1	01	03.0	28	04.0	02	05.5	231	02.9	07	02.5	703				
$\varphi = 44^{\circ}19' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = +1 h 14 min.$														MAGRA		BR. ST. 123														
I	-	02.3	07.0	02.6	03.6	08.1	-00.3	17.0	29	-10.0	15	04	01.2	02	01.5	14	01.2	02	30	02.8	04	02.5	*	*	*	*	12	01.2	27	
II	-	04.6	16.9	05.5	06.3	06.3	11.9	20.2	22.0	24	-07.6	04	04	01.8	C2	01.0	11	01.6	17	02.2	17	05.3	*	*	10	01.1	23			
III	-	05.3	15.0	06.3	06.2	16.0	02.5	23.0	23	-03.8	01	06	01.7	01	01.0	26	01.6	05	03.4	*	01	04.0	05	01.4	21	01.2	28			
IV	-	06.3	14.7	07.1	08.6	15.8	03.2	25.5	29	-03.0	12	01	01.0	*	19	01.4	06	01.8	*	*	*	*	04	01.0	25	01.5	35			
V	-	13.2	20.6	12.9	14.9	22.2	09.1	30.0	04	02.4	25	03	01.0	01	01.0	24	01.4	16	02.4	02	01.0	*	*	10	01.3	11	01.1	32		
VI	-	15.7	22.6	15.1	17.1	24.1	11.4	32.5	14	03.0	04	02	01.0	02	01.5	25	03.2	02	01.5	07	01.0	15	01.2	40	*	*				
VII	-	17.1	24.9	16.5	16.7	26.2	13.2	31.5	21.08	05.6	28	03	01.3	*	20	01.6	06	02.5	01	01.0	02	02.0	04	01.0	22	01.5	37			
VIII	-	15.8	24.3	16.2	18.4	25.6	13.1	31.0	28	07.0	26	01	01.0	01	01.0	23	01.8	08	*	*	*	*	10	01.0	09	01.4	37			
IX	-	10.3	17.9	10.5	12.5	19.0	06.1	25.5	09	-00.2	29	03	01.3	01	01.0	14	01.1	11	01.5	05	01.1	15	01.1	15	01.1	42				
X	-	07.8	17.2	09.2	10.8	18.2	06.3	24.5	01	00.8	04	01	01.0	*	14	01.6	11	01.5	*	01	01.0	06	01.0	12	01.1	46				
XI	-	04.7	05.9	05.6	06.5	11.6	03.0	24.0	12	-04.8	28	*	*	01	02.0	24	01.6	06	05.2	01	05.0	*	01	01.0	17	01.1	37			
XII	-	-02.9	0.7	-01.3	-01.2	02.3	-04.6	11.5	28	-12.6	19.03	*	*	19	01.5	09	03.4	*	01	01.0	*	*	21	01.1	43	*	*			
GOD.	-	08.4	15.4	08.9	10.4	16.7	05.6	32.5	44.VI	-12.8	00.XII	28	01.4	11	01.3	229	01.5	118	02.5	04.3	05	02.0	62	01.1	190	01.2	427			
$\varphi = 44^{\circ}33' N \lambda = 18^{\circ}42' E$ Gr. $\Delta G = +1 h 15 min.$														TUZLA		BR. ST. 124														
I	735.1	01.1	07.1	02.6	03.3	08.2	-00.7	17.0	29	-10.0	19	01	01.0	14	01.6	02	01.0	04	0											

Mesec	Oblačnost Nm (O-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm		Broj dana na sat																					
	7	14	21		L m s		Srednji (Dnevni) mm	Max.	Min.	Tn	Tx	Tn	Tx	Tn	F(O-12)	Nm(O-10)	R mm	•	*	*	Δ	Δ	Δ	Δ							
					7	14	21	Srednji (Dnevni) mm	Dnevni mm	7	14	21	7	14	21	7	14	21	7	14	21	7	14								
BR. ST. 121 MODRIĆ																															
I 8.2 8.0 7.5 7.9	-	94.5	53	82	92	85	52	033	006.0	16	01	02	20	.	.	.	01	15	08	07	07	02	.	01	06	03					
II 7.5 6.9 6.4 6.9	-	06.0	68	70	89	82	34	100	016.5	15	01	08	.	.	.	01	02	12	16	14	03	03	.	01	02	03					
III 4.9 5.5 4.7 4.8	-	06.7	90	52	86	77	26	023	007.1	30	.	06	03	.	.	09	08	05	07	08	02	.	01	01	01						
IV 6.1 5.7 5.6 5.8	-	07.1	83	55	85	76	15	053	011.2	06	.	03	02	.	.	05	05	12	10	02	12	.	.	.	01	.					
V 4.9 6.0 5.0 5.3	-	10.5	81	55	84	73	18	037	010.5	06	.	.	08	01	.	.	06	05	12	05	05	01	12	.	.	08	.				
VI 2.7 4.5 5.4 4.2	-	12.0	73	54	80	68	27	051	031.5	17	.	.	14	06	.	.	08	05	09	06	01	05	.	.	04	.					
VII 4.4 4.6 4.2 4.3	-	13.7	64	55	84	75	27	153	065.8	23	.	.	20	04	.	.	08	05	12	09	05	12	.	.	05	.					
VIII 4.0 5.3 3.6 4.3	-	14.0	88	61	84	78	42	059	020.5	24	.	.	24	.	.	.	08	05	08	07	03	08	.	.	03	02					
IX 4.4 4.8 4.3 4.5	-	09.8	89	61	88	80	34	061	020.6	18	.	01	09	.	.	01	10	08	09	08	02	09	.	.	02	01					
X 5.7 3.9 3.8 4.5	-	08.7	95	66	93	85	31	042	023.4	03	.	02	.	.	.	09	08	04	04	01	06	.	.	01	06						
XI 8.4 7.6 6.4 7.5	-	06.7	55	82	94	80	47	143	021.3	02	.	11	.	.	.	01	17	14	13	06	11	04	.	.	01	06					
XII 8.9 7.7 8.3 8.3	-	04.0	92	91	94	93	60	088	022.5	02	03	13	25	.	.	01	02	22	12	12	03	10	05	11	.	06	26				
GOD. 5.8 5.9 5.4 5.7	-	08.7	87	65	87	80	15	843	065.6	24.VI	05	15	74	84	11	.	02	.	69	123	127	106	27	119	16	11	.	01	26	37	40
BR. ST. 122 PONIKVE																															
I 7.5 6.6 7.0 7.1	-	-	-	-	-	-	-	116	036.0	13	-	-	-	-	-	02	.	10	12	12	04	06	07	01	.	07	15				
II 5.3 5.6 6.0 5.6	-	04.1	79	62	82	74	11	095	016.1	15	01	02	11	.	.	05	.	03	05	13	12	04	10	06	.	.	06				
III 4.6 5.3 4.1 4.0	-	04.9	82	48	77	69	24	094	026.0	14	.	01	10	.	.	.	12	06	09	05	04	05	04	.	.	06					
IV 6.3 6.1 5.5 6.0	-	05.6	85	64	86	80	26	102	027.5	16	.	04	13	01	.	.	05	11	13	13	03	04	05	.	.	08					
V 4.9 4.8 5.2 5.0	-	07.8	80	64	81	75	30	037	009.4	10	.	.	03	.	.	.	08	07	09	09	.	09	.	.	01	05					
VI 3.2 3.1 3.0 3.4	-	09.5	77	66	77	73	35	089	015.6	28	.	.	08	.	.	.	19	05	11	16	06	11	.	.	01	03					
VII 3.9 4.4 5.0 4.4	-	11.0	82	60	82	75	35	167	023.4	01	.	.	18	.	.	.	10	08	15	15	08	15	.	.	03	03					
VIII 4.2 4.5 4.2 3.9	-	11.4	83	68	85	79	42	124	036.2	24	.	04	06	01	.	.	10	02	11	04	11	01	.	.	03	.					
IX 5.5 5.8 6.8 6.0	-	08.3	50	67	89	82	50	149	039.5	20	.	.	02	01	.	.	02	09	12	07	12	.	.	03	16						
X 3.5 3.2 3.3 3.3	-	07.4	92	69	91	84	49	072	018.3	11	.	03	.	.	.	14	04	06	05	03	04	01	.	.	04	01					
XI 6.4 6.6 6.7 7.5	-	-	-	-	-	-	-	176	040.5	26	03	03	05	.	.	04	13	13	07	05	10	.	.	04	16						
XII 6.4 5.6 5.7 5.9	-	-	-	-	-	-	-	132	019.2	03	13	16	29	.	.	10	13	13	13	06	09	.	.	02	31						
GOD. 5.2 5.6 5.3 5.1	-	-	-	-	-	-	-	1353	040.5	26.XI	-	-	-	-	-	05	.	97	99	137	133	56	100	50	03	.	01	13	35	88	
BR. ST. 123 MACA																															
I 7.3 7.1 5.9 6.8	-	04.8	82	69	86	79	23	087	024.0	13	01	01	13	.	.	01	01	02	13	14	10	04	12	03	01	.	03	07			
II 7.2 6.4 5.0 6.1	-	05.4	80	64	79	75	23	107	024.5	15	01	08	.	.	05	02	03	10	15	14	04	14	04	01	.	01	06				
III 4.5 4.5 3.4 4.2	-	05.7	81	45	63	71	14	067	020.0	14	.	03	02	.	.	01	13	05	11	07	02	10	04	.	02	.					
IV 6.4 5.9 5.5 5.9	-	06.3	80	53	86	73	23	114	043.4	16	.	04	03	.	.	04	16	13	11	03	12	05	.	.	03						
V 5.0 6.0 4.7 5.2	-	05.6	78	54	86	73	28	073	014.7	28	.	.	10	01	.	.	05	06	12	10	03	12	.	.	03	02					
VI 3.4 5.9 3.7 4.4	-	11.2	78	58	90	72	29	133	056.0	13	.	.	13	06	.	.	11	05	12	11	03	12	.	.	01	06					
VII 4.1 4.4 3.5 4.0	-	12.3	81	55	90	72	25	130	036.0	01	.	.	22	07	.	.	13	05	14	12	04	14	.	.	06	03					
VIII 2.7 4.2 2.6 3.2	-	12.5	87	61	94	80	32	124	058.6	06	.	.	22	01	.	.	15	04	10	09	03	10	.	.	04	.					
IX 5.4 5.5 5.1 5.4	-	09.4	92	65	95	84	38	153	060.2	14	.	01	09	.	.	09	10	13	12	06	13	.	.	01	05						
X 4.4 5.6 4.8 4.3	-	08.3	93	63	93	81	31	080	029.7	03	.	.	14	07	06	03	07	.	.	.	.	.	.	.	07						
XI 5.7 6.5 5.5 5.9	-	06.3	85	73	90	84	25	146	033.5	26	.	11	.	01	.	01	04	09	14	11	05	07	01	.	01	08					
XII 6.4 6.8 6.6 6.7	-	03.7	85	61	85	84	52	101	020.6	03	05	11	25	.	.	01	06	15	11	11	04	05	07	.	.	03	28				
GOD. 5.2 5.6 4.7 5.2	-	06.0	83	62	88	78	14	1315	060.2	44.IX	06	13	66	81	15	.	09	03	99	102	146	124	45	130	36	06	.	02	27	22	54
BR. ST. 124 TUZLA																															
I 8.2 7.5 7.1 7.6	059.8	04.7	87	65	84	75	34	040	008.4	16	01	02	17	.	.	01	01	16	12	05	09	05	.	01	.	05	05				
II 7.6 7.5 6.2 7.1	097.4	05.8	89	69	83	80	34	092	021.6	15	01	06	.	.	04	.	02	14	17	13	02	15	04	.	.	02	05				
III 5.8 6.3 3.8 5.3	171.1	06.1	61	62	62	77	19	043	012.8	14	.	06	02	.	.	08	08	11	07	02	05	05	.	01	01	02					
IV 6.5 6.5 5.6 6.2	165.2	06.4	62	62	76	23	071	040.4	16	.	04	03	.	.	02	12	16	09	02	15	06	04	.	.	02	01					
V 6.6 7.4 6.6 6.9	171.0	09.8	88	57	83	76	32	078	015.1	23	.	.	10	.	.	01	03	14	14	11	02	14	.	.	01	08					
VI 4.4 5.2 4.5 4.9	209.0	11.6	84	58	86	76	23	071	014.5	26	.	.	22	06	.	02	03	05	17	14	05	17	.	.	11	.					
VII 4.4 4.5 5.1 4.8	246.3	12.9	80	57	87	78	37	132	032.3	22	.	.	24	06	.	01	03	12	09	04	12	04	12	.	.	07					

Mesec	Vazdušni prstenski Pm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vatre m/s, Pm (0-12)															
		Tm			Sred. (Dnev.)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C					
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.				
$\varphi = 44^{\circ}12' N \lambda = 18^{\circ}57' E$ Gr. $\Delta G = +1h\ 16\ min.$																									
VLASENICA BR. ST. 126																									
I	-	01.2	05.4	02.7	03.0	04.3	-00.6	14.8	29 -08.8	19	03	01.7	.	.	08	01.9	*	25	01.5	*	*	10			
II	-	03.6	08.0	05.4	05.4	05.8	01.5	18.8	24 -07.8	04	07	01.3	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0				
III	-	05.5	13.1	07.8	08.5	14.2	02.5	25.4	23 -07.2	01	08	01.4	04	01.2	01.1	04	01.0	03.3	01	01.0	02	01.5			
IV	-	05.8	12.2	07.8	08.3	13.6	03.1	26.8	29 -02.0	12	02	01.0	04	01.2	01.1	01.0	02	01.0	06	01.7	28	01.3			
V	-	12.3	18.2	12.5	14.1	19.6	08.9	27.6	20 03.8	29	05	01.2	00.7	01.3	01	01.2	09	01.0	*	25	01.1	01 02.0			
VII	-	15.7	19.9	15.0	16.4	21.5	11.6	30.4	14 04.2	04	08	01.2	04	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0			
VIII	-	17.2	22.3	16.8	18.2	23.9	12.9	30.4	31 05.2	28	06	01.2	04	01.0	02	01.3	12	01.1	08	01.9	30	01.4	01 01.0		
IX	-	10.4	16.1	11.0	12.1	17.2	07.9	26.8	09 00.0	30	09	01.0	04	01.2	01	01.0	13	01.1	06	01.0	03	01.0	02		
X	-	07.9	15.7	10.6	10.9	16.7	06.5	23.4	01 01.2	04	07	01.0	05	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0			
XI	-	03.8	09.6	05.2	05.8	10.3	02.0	21.6	12 -06.2	20	*	*	*	*	*	*	28	01.5	10	01.1	12	01.0	02		
XII	-	-03.6	-00.6	-02.4	-02.3	00.8	-05.7	11.0	25 -14.0	19	19	01.0	03	01.0	17	01.0	05	01.0	02.0	*	26	01.1	06 01.0		
GOD.	-	08.0	13.5	09.0	09.8	14.8	05.2	30.4	44 VI	-14.0	9 XII	80	01.2	38	01.1	433	01.2	77	01.1	115	01.1	31	01.9	295	
BOSNA																									
VIJELJINA BR. ST. 127																									
I	-	00.3	05.5	02.0	02.5	04.5	-01.0	17.2	12 -07.8	01	04	01.0	.	.	16	01.9	07	02.4	10	01.1	17	01.5	15 01.4		
II	-	04.6	10.3	05.4	06.4	11.8	02.2	21.0	25 -23	04	02	01.0	01	03.0	06	01.3	03	02.0	07	02.4	19	02.0	13 01.2		
III	-	05.5	15.3	08.4	09.4	16.5	03.5	27.4	24 -04.1	01	02	01.0	02	02.0	09	01.4	04	02.0	12	01.2	18	01.3	01.2		
IV	-	07.4	15.4	08.5	10.1	16.1	04.5	26.3	29 -01.1	21	03	01.3	.	.	12	01.6	04	01.0	10	01.2	03	01.7	07 01.0		
V	-	14.6	22.0	15.0	16.7	23.1	10.8	36.0	06 06.2	11	03	01.0	.	.	11	01.8	03	01.3	07	01.1	14	01.4	14 01.4		
VI	-	17.3	25.3	17.6	19.4	26.5	12.9	36.1	14 03.5	04	06	01.0	03	01.0	04	01.0	04	01.5	03	01.3	40	01.4	10		
VII	-	17.5	26.8	18.6	20.2	27.8	15.1	35.1	31 11.1	28	03	01.3	.	.	04	01.5	03	01.0	10	01.4	14	01.1	11 01.2		
VIII	-	16.5	26.0	18.2	19.7	27.0	14.7	31.9	18 06.7	26	04	01.0	02	01.0	11	01.2	01	01.0	10	01.1	03	01.3	16		
IX	-	10.5	20.2	12.3	13.8	20.9	08.6	30.2	09 -06.7	29	03	01.0	.	.	05	01.0	03	01.0	08	01.0	09	01.3	11 01.1		
X	-	07.6	18.0	10.3	11.6	18.6	06.7	26.1	01 -05.5	18	05	01.0	01	01.0	04	01.2	02	01.0	11	01.1	12	01.2	19 01.0		
XI	-	04.7	10.1	06.0	06.7	11.5	03.3	25.1	12 -02.6	25	03	01.0	.	.	14	01.0	01	03.0	09	01.1	08	01.4	20 01.2		
XII	-	-02.7	00.9	-01.7	-01.3	01.7	-04.0	09.1	28 -18.7	06	*	*	*	*	*	*	*	*	*	*	*	*	-		
GOD.	-	08.7	16.3	10.1	11.3	17.4	04.5	35.1	34 VI	-16.7	06 XII	-	-	-	-	-	-	-	-	-	-	-	-		
LIVNO BR. ST. 128																									
I	698.6	01.0	05.3	01.7	02.4	06.1	-01.2	12.4	25 -11.9	01	05	02.2	01	04.0	07	02.0	17	02.1	04	02.2	01	02.0	47		
II	694.6	01.6	06.8	03.0	03.6	06.2	-00.1	14.6	24 -13.4	04	06	03.3	.	.	07	01.9	18	02.4	11	02.2	04	02.0	05	01.6	
III	701.0	02.6	13.2	06.3	07.1	14.1	01.1	21.7	23 -05.5	01	06	02.2	01	02.0	02	01.0	04	02.1	06	02.2	09	01.3	07 02.1		
IV	696.4	05.6	12.3	07.0	07.9	13.4	02.4	23.2	30 -05.3	18	20	03.0	02	02.0	02	02.5	11	02.0	08	02.2	03	01.7	07 02.1		
V	698.5	10.8	18.2	11.5	13.0	19.8	06.1	25.5	19 -00.2	29	07	02.0	.	.	06	02.0	17	02.1	06	02.5	05	01.6	09 01.4		
VI	698.0	13.6	20.8	14.4	15.8	22.6	07.9	29.2	13 01.5	02	06	02.0	05	02.2	04	01.5	06	01.3	02.5	06	02.2	12 01.8			
VII	698.1	15.4	24.5	16.4	18.5	25.7	10.9	30.2	30 06.6	07	03	02.0	.	.	01	02.4	09	01.8	08	02.4	06	02.0	19 01.7		
VIII	698.2	13.0	22.8	15.3	16.7	24.4	05.7	31.7	23 03.7	26	03	02.0	03	01.3	05	01.4	12	01.8	06	02.3	08	01.9	10 01.5		
IX	701.2	08.0	18.6	11.1	12.2	19.7	05.6	26.6	01 -04.2	29	11	02.5	08	02.1	06	02.0	*	04	01.5	05	10	01.5	01 02.0		
X	702.6	04.4	17.3	07.5	09.4	18.0	02.9	22.1	24 -02.4	04	03	02.0	03	02.0	03	01.8	06	01.9	06	02.2	05	01.6	11 01.0		
XI	698.5	02.2	09.4	04.2	05.0	10.7	00.4	22.0	11 -08.8	29	05	02.2	01	03.0	05	02.2	14	02.0	02	01.5	04	01.2	09 01.2		
XII	700.7	-02.9	03.9	-01.4	-00.5	05.3	-05.0	10.0	10 -12.4	23	13	02.0	06	02.5	05	03.2	02	03.0	04	03.0	*	05	01.4	05 01.6	
GOD.	698.8	06.4	14.4	08.2	09.3	15.7	03.4	31.7	29 VIII -13.4	04	88	02.4	30	02.2	58	02.0	126	02.1	65	02.3	56	01.7	112	01.6	
RAKITNO BR. ST. 129																									
I	-	01.3	04.0	01.9	02.3	05.3	-	11.2	25	-07.0	28	16	02.6	02	03.0	04	02.5	06	03.2	15	02.2	02	01.0	34	
II	-	02.7	05.7	02.9	03.6	07.1	00.1	14.0	25	-07.0	28	12	02.5	07	01.9	06	02.5	15	02.2	02	01.5	01	02.0	55	
III	-	04.3	12.0	06.6	07.4	-	-	-	-	-	18	03.9	05	04.6	*	03	01.3	13	01.9	*	05	01.0	01	02.0	45
V	-	11.5	16.8	11.2	12.7	-	-	-	-	-	04	03.2	07	02.1	16	02.2	01	01.0	05	02.3	*	*	*	51	
VI	-	14.8	15.2	13.2	15.1	20.9	11.5	28.0	11 05.0	06.04	16	02.6	05	03.2	02	01.5	01	02.0	*	04	01.2	*	61		
VII	-	17.1	23.5	16.4	18.4	24.4	-	29.0	30	-	-	-	08	02.0	06	02.5	05	01.5	01	03.0	10	01.8	*	46	
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41		
X	-	04.5	15.7	08.2	09.7	16.5	02.6	26.0	26 -05.0	01	02	02.8	*	*	*	07	01.6	*	*	*	*	*	*	65	
XI	-	03.3																							

Mesec	Oblakost Nm (0-10)			Inkolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																				
	7	14	21		U m a			Tn	Tx	Tn	Tx	Tx	Tr	F (0-12)	Nm (0-10)	R mm	•	*	•	*	•										
					e <sub>m</sub>	mm	mm										%	%	%	%	%	%									
					7	14	21	Sred. (Des.)	Min	M	Max	Dat.	%	%	%	%	%	%	%	%	%	%	%								
					mm	mm	mm										10.00.0	0.025	0.030	0.020	0.06	8	2.0	8.0	0.1	1.0	10.0	0.0			
<b>BR. St. 126</b>																															
<b>VLASENICA</b>																															
I	5+3	3+9	4+6	4+6	-	04+4	81	66	78	76	46	086	023+4	13	•	03	16	•	•	•	08	66	11	10	03	06	06				
II	5+2	5+0	5+1	5+1	-	05+0	79	65	75	73	30	104	014+2	14	•	01	10	•	•	11	01	07	09	12	12	05	11				
III	5+9	5+3	2+4	3+2	-	05+7	22	36	65	68	25	041	015+2	14	•	06	02	•	•	•	15	03	06	06	01	06	02				
IV	5+9	4+5	4+3	4+9	-	06+1	80	64	74	73	37	108	032+4	16	•	11	12	•	•	•	10	08	10	09	04	07	05				
V	3+2	3+7	4+0	3+6	-	08+7	80	61	75	72	35	085	015+5	06	•	•	05	•	•	13	05	09	09	04	09	•					
VI	3+6	4+7	4+5	4+3	-	10+5	77	66	77	73	31	112	035+6	23	•	•	08	01	•	•	12	07	12	10	05	12	•				
VII	3+0	3+4	3+9	3+4	-	11+7	78	64	79	74	35	140	026+7	18	•	•	14	01	•	•	16	05	10	10	04	10	•				
VIII	2+0	2+5	3+7	2+9	-	11+9	83	62	84	76	37	097	025+6	15	•	•	16	•	•	11	10	04	11	•	05	05					
IX	5+1	4+7	5+0	4+9	-	09+0	87	72	85	81	43	166	024+8	14	•	•	02	•	•	11	10	11	10	07	11	•					
X	4+2	3+6	4+0	3+9	-	08+1	86	71	83	80	41	076	036+4	03	•	•	•	•	•	17	08	05	05	03	05	•					
XI	5+5	5+4	5+8	5+6	-	06+1	92	75	88	86	28	116	032+8	24	•	13	•	•	03	06	09	12	11	07	10	03					
XII	7+0	6+5	6+3	6+6	-	03+7	87	89	90	89	71	119	025+9	30	07	15	26	•	•	04	15	12	11	05	06	07					
GOD.	4+5	4+3	4+5	4+4	-	07+6	82	68	79	76	25	1248	036+7	48+6	07	19	82	50	02	•	17	01	35	87	121	113	51	101	35	10	
<b>BR. St. 127</b>																															
<b>BIJELJINA</b>																															
I	7+1	5+5	6+5	6+3	049+8	04+8	89	80	88	86	52	042	010+6	16	•	02	20	•	•	02	07	11	07	01	10	02					
II	6+6	5+4	5+4	5+8	093+6	05+8	82	66	86	78	33	103	028+0	15	•	07	•	•	03	02	07	17	15	03	15	04					
III	6+4	4+2	3+9	4+2	163+8	06+3	61	51	82	71	24	041	017+5	14	•	06	03	•	•	13	06	13	08	01	12	02					
IV	5+9	4+9	6+1	5+6	163+2	03+8	76	52	86	70	35	062	027+8	16	•	03	03	•	•	07	08	14	08	02	13	01					
V	4+1	4+5	6+2	4+9	202+3	10+7	86	57	61	73	23	046	015+0	07	•	•	12	02	•	•	05	07	12	09	01	12	•				
VI	3+5	4+5	4+4	4+1	247+4	12+6	80	55	81	72	32	050	015+2	23	•	•	19	08	•	01	05	05	10	07	10	03					
VII	3+7	4+7	4+7	4+7	-	13+5	81	54	85	73	33	170	101+2	23	•	•	22	12	•	•	04	03	14	10	03	14	02				
VIII	3+9	3+9	3+9	3+9	226+8	13+3	84	57	68	76	33	079	016+0	01	•	•	25	06	•	01	11	05	10	07	04	10					
GOD.	5+5	5+6	5+3	5+2	-	08+5	83	62	85	77	23	868	101+2	23+6	03	15	74	99	29	•	05	•	65	87	146	102	28	136	17	01	
<b>BR. St. 128</b>																															
<b>LIVNAC</b>																															
I	8+3	8+5	7+0	7+9	058+5	04+8	87	77	87	84	44	126	031+9	12	01	•	15	•	•	11	02	03	21	17	15	04	16	02	01		
II	7+2	7+6	6+6	7+4	082+3	03+5	94	78	89	84	49	122	026+4	12	02	•	13	•	•	11	01	02	14	15	14	04	14	03	01		
III	5+4	5+3	3+8	4+8	206+6	05+8	86	59	81	76	30	130	033+1	13	•	•	14	•	•	09	01	03	08	06	07	04	07	02	01		
IV	6+6	4+7	6+0	6+0	213+4	05+7	76	56	75	69	22	068	019+3	09	•	•	09	•	•	14	02	03	08	11	09	03	03	01	02		
V	5+0	6+8	3+7	5+1	222+9	07+6	78	52	72	68	22	069	016+1	27	•	•	01	01	•	•	06	01	05	07	11	08	03	11	•	04	
VI	3+6	6+8	4+2	4+9	247+5	08+5	70	48	71	63	32	010	024+9	24	•	•	10	•	•	04	03	03	12	05	05	12	04	06	01		
VI	3+5	5+3	2+6	3+8	327+4	05+4	70	41	66	59	27	052	029+3	23	•	•	22	01	•	09	01	09	06	09	06	01	09	06	01		
VII	4+3	6+3	2+3	4+3	240+7	09+7	84	48	71	69	31	144	079+2	22	•	•	13	02	•	06	10	06	15	13	03	15	•	16	•		
IX	4+4	5+6	3+5	4+5	219+5	07+6	86	50	76	70	24	113	047+5	18	•	•	02	04	•	•	12	02	09	06	13	10	03	13	•	03	
X	4+3	4+1	2+8	3+7	228+9	06+5	92	49	82	74	31	073	021+8	11	•	•	07	•	•	04	11	06	11	05	05	04	05	02	01		
XI	7+0	5+3	6+4	6+4	115+4	05+4	69	64	84	79	33	120	027+4	17	•	•	09	•	•	08	06	13	14	11	04	11	04	04	02		
XII	5+3	5+2	3+7	4+7	135+0	03+5	83	61	77	73	33	140	029+7	10	07	01	25	•	•	12	06	11	09	12	10	06	09	04	02		
GOD.	5+5	6+2	4+2	5+3	229+6	06+7	82	56	77	72	22	1183	079+3	48+1	•	•	•	•	•	•	20	01	124	87	107	104	45	100	15	03	•
<b>BR. St. 129</b>																															
<b>RAKITNO</b>																															
I	7+0	6+2	4+8	7+6	-	04+5	83	61	81	82	63	259	113+4	12	•	01	•	•	01	•	05	19	15	15	05	14	03	•	02	02	
II	7+1	7+4	6+5	7+0	-	05+0	83	78	84	82	55	207	048+2	01	•	•	12	•	•	04	15	02	14	15	14	04	14	03	01	01	
III	4+4	4+2	4+6	4+4	-	06+1	75	68	75	73	33	213	085+1	13	•	•	14	•	•	01	13	05	05	05	06	05	04	02	01	01	
IV	5+1	5+4	4+1	4+8	-	06+0	78	68	83	76	32	120	042+4	09	•	•	02	•	•	05	01	07	09	09	04	04	01	02	01	02	
V	4+5	5+4	3+0	4+5	-	10+0	74	68	81	74	38	129	081+0	15	•	•	13	•	•	01	08	03	08	07	02	08	•	•	01	01	
VI	2+0	2+6	2+2	2+9	-	11+6	66	55	66	45	32	040	033+2	26	•	•	20	07	•	01	08	02	05	05	01	05	01	01	01	01	
VII	2+0	3+0	1+3	2+1	-	13+5	65	53	69	62																					

Meseč	Vazdušni pritisak Pm mm	Temperatura vazduha °C							Čestina pravaca i srednja jačina vетра nD, Fm (0-12)																				
		Tm			Sred. (Dnev.)	Max	Min	Dat.	N			NE		E		SE		S		SW		W		NW					
		7	14	21					8.	3.	8.	j.	8.	j.	8.	3.	8.	3.	8.	3.	8.	j.	8.	3.					
γ = 43°50' N λ = 17°38' E Gr. ΔG = + 1h 10 min.																													
I	-	-00.4	05.0	01.4	01.9	06.0	-02.4	12.4	25	-13.0	19	01	02.0	.	.	.	01	03.0	.	.	.	12	01.8	01	02.0	78			
II	-	00.9	07.4	02.1	03.1	08.8	-01.7	16.4	24	-05.8	04	03	02.7	.	.	01	03.0	.	.	.	16	01.8	03	02.0	61				
III	-	02.5	13.3	02.2	06.5	14.3	00.0	24.8	24	-07.6	01	02	02.0	.	.	01	02.0	02	02.0	.	20	01.8	04	C2.5	64				
IV	-	05.0	13.0	06.4	07.7	14.2	04.5	25.4	30	-04.2	18	05	02.2	.	.	07	02.6	.	.	02	03.5	.	.	24	02.4	27			
V	-	10.6	18.4	11.0	12.7	19.6	04.2	26.2	04	01.6	08	01	02.0	.	.	.	01	02.0	.	.	.	19	01.7	.	.	72			
VI	-	13.3	20.3	13.5	15.2	21.7	04.2	26.8	11	01.6	01	01	02.0	.	.	02	02.0	.	.	.	20	01.9	.	.	68				
VII	-	15.4	24.0	16.0	18.0	25.0	11.2	29.2	30.0	04	07.4	07	.	.	.	05	02.4	.	.	.	21	01.8	02	C2.5	65				
VIII	-	13.8	22.7	15.0	16.6	24.5	10.4	31.2	30	05.6	26	.	.	.	.	04	02.0	.	.	.	24	01.7	.	.	65				
IX	-	09.3	16.2	11.3	12.5	19.5	06.7	27.8	01	-00.4	29	.	.	.	.	06	02.2	.	.	.	26	01.4	01	C2.0	57				
X	-	05.7	16.5	08.2	09.6	17.5	03.9	22.2	24	-01.2	02	.	.	.	.	04	01.2	.	.	.	24	01.5	.	.	65				
XI	-	02.6	09.0	04.6	05.2	10.8	00.6	20.8	12.1	-07.2	21	.	.	.	.	16	02.2	.	.	.	13	01.7	.	.	61				
XII	-	-03.3	03.0	-01.6	-01.0	04.2	-05.4	08.2	29	-14.2	05	.	.	.	.	16	02.5	.	.	.	12	01.8	.	.	65				
GOD.	-	06.3	14.2	07.8	09.0	15.5	03.3	31.2	30VH	-14.2	05.KH	12	02.3	.	.	01	02.0	65	02.3	.	.	02	03.5	207	01.7	35	02.4	748	
γ = 43°05' N λ = 17°43' E Gr. ΔG = + 1h 11 min.																													
I	-	05.3	10.3	06.6	07.2	13.5	-	19.6	29	-	40	01.4	12	01.0	.	.	07	01.4	14	03.1	03	01.0	.	.	10	01.1	07		
II	-	07.8	13.1	08.5	09.5	16.9	-	23.5	25	-	48	01.6	02	01.0	.	.	03	03.0	25	03.0	02	01.5	.	.	06	01.0	09		
III	-	08.2	18.1	10.6	12.0	21.0	04.3	27.8	24	00.0	01	25	01.4	10	01.0	.	.	08	01.2	27	02.3	06	01.4	.	.	03	01.0	11	
IV	-	10.3	18.4	10.7	12.5	22.1	04.8	26.3	28	01.0	18	39	01.7	10	01.1	.	.	07	01.9	11	02.5	09	01.4	.	.	03	01.0	33	
V	-	15.8	24.2	16.0	18.0	26.5	11.4	32.5	19	06.2	11	14	01.4	07	01.0	.	.	13	01.4	12	02.2	11	01.5	.	.	12	01.4	24	
VI	-	16.6	26.5	18.2	21.0	26.5	13.3	32.2	14	06.7	05	12	01.2	01	01.0	.	.	06	01.0	25	02.4	15	01.3	.	.	04	01.5	25	
VII	-	21.9	30.7	21.9	24.1	31.6	16.0	35.0	30	12.5	07	14	01.4	13	01.1	.	.	17	01.9	13	02.7	16	01.4	.	.	12	01.2	08	
VIII	-	18.9	26.4	19.4	21.5	30.4	15.3	36.2	30	08.7	26	13	01.2	01	01.0	.	.	03	02.7	05	01.6	20	01.8	.	.	18	01.1	33	
IX	-	13.6	24.0	15.2	17.0	26.1	11.2	32.5	06	02.4	29	27	01.6	04	01.5	.	.	01	01.0	03	01.7	08	01.8	.	.	06	C1.2	41	
X	-	08.9	21.9	11.0	13.2	24.4	07.3	26.8	08	03.0	04	07	01.3	08	01.0	.	.	06	01.7	04	01.2	17	01.5	.	.	04	01.0	49	
XI	-	07.3	14.7	08.0	09.9	-	05.5	-	-02.5	21	35	01.3	03	01.0	.	.	02	02.0	09	02.3	08	01.2	.	.	09	01.2	24		
XII	-	02.3	10.1	04.2	05.2	14.1	00.7	16.8	28	-05.3	23	46	01.8	14	01.1	.	.	01	01.0	02	03.5	04	01.0	.	.	02	01.0	24	
GOD.	-	11.7	20.0	12.7	14.3	-	-	-	-	-	320	01.5	83	01.1	-	-	76	01.6	150	02.5	121	01.5	-	-	-	86	C1.2	259	
γ = 43°40' N λ = 17°46' E Gr. ΔG = + 1h 11 min.																													
JABLANICA																													
BR. ST. 132																													
I	-	03.4	07.5	04.5	04.9	08.1	02.1	15.5	25	-04.0	19	10	02.3	.	.	03	03.3	.	.	.	19	04.0	.	.	05	04.0	.	.	56
II	-	05.7	10.6	07.2	07.7	11.8	04.4	20.6	23	-02.0	04	08	02.2	.	.	06	03.2	.	.	.	10	03.6	.	.	07	04.3	.	.	53
III	-	05.4	16.1	10.0	10.4	17.6	04.8	27.0	23	-00.4	03	08	02.6	.	.	09	03.0	.	.	.	20	03.6	.	.	03	03.3	.	.	53
IV	-	08.4	16.4	10.5	11.5	17.3	06.5	28.5	30	00.0	18	14	03.1	.	.	11	03.9	.	.	.	18	03.9	.	.	10	03.4	.	.	37
V	-	13.6	22.4	15.6	16.8	22.6	11.4	32.5	19	05.0	26	10	02.3	.	.	08	02.1	.	.	.	19	03.5	.	.	03	02.7	.	.	53
VI	-	16.2	24.0	16.8	19.5	25.3	11.4	32.5	11	05.6	06	10	02.3	.	.	05	02.6	.	.	.	08	02.5	.	.	01	02.0	.	.	66
VII	-	18.6	27.7	19.0	21.1	28.6	16.8	33.5	21	12.0	24.23	11	02.8	.	.	09	02.4	.	.	.	07	03.6	.	.	07	04.3	.	.	59
VIII	-	16.9	24.7	18.2	20.2	26.4	12.1	32.0	30	01.0	24	-	-	-	.	.	.	.	.	.	.	.	.	.	.	.	.		
IX	-	11.3	20.1	12.0	13.8	21.7	05.0	29.0	01	00.5	30	10	02.4	.	.	03	04.0	.	.	.	02	03.0	.	.	02	03.0	.	.	73
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.	.	.	.	.	.	.	.	.	.	.	.	.		
XI	-	05.1	11.0	06.8	07.4	12.2	-	20.5	12	-	14	01.3	15	01.6	30	01.4	02	01.0	01	02.4	05	02.0	01	02.0	07	02.0	07	02.3	01
XII	-	00.5	03.9	00.4	01.0	05.3	-02.9	12.5	28	-10.5	06	08	01.6	26	02.0	39	02.1	01	01.0	03	03.0	02.7	02.0	07	02.3	01			
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
γ = 43°09' N λ = 17°47' E Gr. ΔG = + 1h 11 min.																													
OCMANOVICI																													
BR. ST. 134																													
I	-	05.4	09.8	04.6	07.0	10.3	03.0	15.0	30.29	-03.0	15	22	02.4	.	.	.	.	22	03.0	.	.	.	.	.	.	.	.	49	
II	-	07.2	13.1	07.6	09.0	13.4	04.8	19.0	23	-01.6	04	09	03.2	.	.	.	33	03.0	.	.	.	.	.	.	.	.	42		
III	-	07.9	17.1	10.2	11.3	-	05.7	-	-02.0	01	08	02.8	.	.	.	30	02.7	.	.	.	.	.	.	.	.	55			
IV	-	10.0	17.1	10.3	12.0	17.4	05.8	25.2	30	00.2	18	21	03.3	.	.	.	26	02.8	.	.	.	.	.	.	.	.	43		
V	-	16.3	23.1	15.8	17.8	23.6	11.0	31.0	19	05.2	11	09	02.6	.	.	.	.	38	02.8	.	.	.	.	.	.	.	.	46	
VI	-	19.8	25.2	18.2	20.4	26.3	13.3	30.4	13	04.6	05	11	02.8	.	.	.	27	03.0	.	.	.	.	.	.	.	.	52		
VII	-	22.1	29.6	21.4	23.7	30.3	16.1	33.4	30	13.4	24	15	03.1	.	.	.	31	03.0	.	.	.	.	.	.	.	.	47		
VIII	-	20.2	27.5	19.7	21.8	28.5	15.7	35.0	30	05.8	25	07	02.4	.	.	.	24	02.5	.	.	.	.</td							

Meseč	Oblačnost Nm (0-10)			Imogljivi broj sati (Dnev.)	Vlažnost vazduha			Padavine R mm		Broj dana na sa:																			
	7	14	21		mm	7	14	21	Spec. (Dnev.)	Min.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▴	▴	▴		
					mm	7	14	21	Spec. (Dnev.)	Min.	7	14	21	7	14	7	14	7	14	7	14	7	14	7	14				
PROZCR																													
BR. St. 131																													
I	7.4	7.5	6.6	7.3	-	04.2	79	73	80	77	47	077	021.2	13	02	19	-	-	-	02	15	13	11	02	11	04	-		
II	7.1	8.2	7.0	7.1	-	04.5	78	68	80	75	56	108	019.6	15	-	01	15	-	-	-	03	14	17	15	05	15	03	-	
III	4.7	4.7	3.8	4.4	-	05.6	81	61	75	72	41	118	030.2	13	-	14	-	-	-	11	09	08	06	05	07	03	-		
IV	5.8	5.3	5.5	5.5	-	05.2	75	53	68	65	29	086	022.8	16	-	08	01	-	-	-	07	10	12	11	04	09	04	-	
V	4.5-5.5	4.4	4.4	4.8	-	07.6	74	56	69	66	36	092	017.8	15	-	06	-	-	-	-	08	08	10	10	05	10	-	-	
VI	4.0	6.0	4.8	4.9	-	08.9	70	58	66	65	38	049	012.2	26	-	05	-	-	-	-	05	07	09	02	11	-	03	-	
VII	3.0	3.2	2.2	2.7	-	10.9	77	56	72	68	38	077	020.2	23	-	18	-	-	-	-	15	03	10	08	04	10	-	-	
VIII	3.0	4.0	2.1	3.0	-	11.0	85	55	84	76	41	123	046.2	22	-	13	02	-	-	-	14	03	08	07	04	08	-	-	
GOD.	4.5	5.2	4.5	4.8	-	07.0	80	63	77	73	29	1125	040.2	21	09	03	97	52	02	-	-	113	101	131	117	46	114	24	-
ČAPLJINA-KLEPCI																													
BR. St. 132																													
I	5.5	6.0	7.3	8.1	-	06.7	88	77	90	85	51	168	034.5	13	-	-	-	-	-	02	22	18	16	06	18	-	-		
II	7.5	7.6	7.1	7.4	-	07.7	85	74	85	83	44	080	014.5	12	-	-	-	-	-	01	-	-	-	-	-	04	01		
III	6.0	5.1	4.7	5.3	-	08.2	85	55	91	77	24	041	014.8	14	-	07	-	-	-	-	08	11	05	04	05	-	01	-	
IV	6.0	4.7	3.5	4.7	-	07.8	74	49	87	70	20	056	018.0	09	-	09	-	-	-	-	09	08	07	02	08	-	01	01	
V	5.0	5.7	4.4	5.0	-	11.4	78	54	86	73	19	039	017.3	10	-	-	21	04	-	-	10	08	07	04	02	07	-	03	
VI	3.2	5.4	2.9	3.8	-	12.9	79	47	91	69	30	010	010.3	03	-	-	25	13	-	-	09	04	02	01	01	02	-	-	
VII	2.3	3.6	2.1	2.7	-	14.2	69	37	85	64	21	049	030.7	23	-	-	31	26	02	-	17	01	04	02	04	-	02	-	
VIII	3.5	4.0	2.6	3.4	-	14.8	83	53	95	77	30	112	046.5	22	-	-	31	17	01	-	14	03	08	06	04	08	-	-	
GOD.	5.2	5.2	4.0	4.8	-	10.0	82	60	89	77	19	1194	062.0	40X	-	-	-	-	-	01	-	122	96	114	88	41	114	01	-
JABLANICA																													
BR. St. 133																													
I	9.0	8.3	6.2	8.5	-	05.8	85	82	88	88	45	206	044.2	16	-	07	-	-	-	05	01	24	17	12	05	17	-	02	
II	9.3	7.5	8.5	8.4	-	07.0	86	75	88	85	29	237	034.8	01	-	05	-	-	-	02	19	18	16	12	18	02	01		
III	5.8	4.7	4.5	5.1	-	-	-	-	-	-	-	259	084.0	13	-	01	03	-	-	08	10	08	06	06	01	-	01		
IV	6.5	5.6	6.4	6.2	-	-	-	-	-	-	-	090	024.6	15	-	04	-	03	-	04	10	12	09	02	12	-	01		
V	5.1	5.7	6.4	5.7	-	-	-	-	-	-	-	077	015.6	15	-	-	16	01	-	-	06	09	08	08	04	08	-	04	
VI	5.0	5.3	6.6	5.6	-	-	-	-	-	-	-	020	020.1	10	-	-	16	06	-	-	05	08	10	06	06	10	-	07	
VII	5.6	4.6	4.1	3.9	-	-	-	-	-	-	-	067	035.6	27	-	-	27	14	02	02	07	03	10	01	02	10	-	04	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	5.8	5.8	5.5	5.8	-	-	-	-	-	-	-	216	066.0	19	-	-	12	01	-	-	07	12	12	11	04	12	-	05	
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	8.6	7.3	5.1	7.1	-	07.1	97	75	93	88	47	244	047.5	26	-	-	-	-	-	01	13	14	16	09	17	02	-		
XII	5.6	4.8	4.4	4.9	-	-	-	-	-	-	-	192	033.4	02	01	-	22	-	-	-	12	11	13	10	07	11	04	-	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	08	07			
DCHMRCVICI																													
BR. St. 134																													
I	6.3	6.3	6.1	6.2	-	06.3	86	74	85	81	50	170	032.5	16	-	06	-	-	-	01	03	08	16	14	07	14	-	01	
II	6.5	6.5	5.4	5.6	-	06.7	82	63	80	75	55	104	014.5	12	-	02	-	-	-	01	03	13	12	05	13	-	01		
III	3.5	3.5	3.5	3.5	-	07.2	82	56	71	72	26	048	026.4	13	-	02	-	-	-	02	12	03	07	05	12	-	01		
IV	4.3	3.5	3.3	3.7	-	06.6	74	44	78	65	20	049	019.0	15	-	01	-	-	-	03	12	03	07	01	11	-	01		
V	3.6	3.4	3.4	3.7	-	10.0	73	46	74	65	29	052	031.0	28	-	-	13	01	-	-	05	01	05	05	02	05	-	01	
VI	1.0	3.7	1.8	2.4	-	11.6	65	56	63	54	24	010	010.0	03	-	-	22	05	-	-	05	08	10	01	01	01	-	01	
VII	1.9	2.7	1.5	2.0	-	13.0	68	39	69	59	17	064	040.0	23	-	-	30	15	02	-	16	03	03	02	03	-	01		
VIII	2.7	3.3	1.7	2.6	-	13.4	75	51	77	68	31	103	044.5	22	-	-	28	12	01	-	16	01	07	07	02	17	-	01	
IX	2.5	3.3	2.7	2.9	-	11.1	81	57	82	73	37	191	046.5	21	-	01	-	11	01	-	-	17	02	09	05	05	09	-	02
X	2.4	3.4	1.2	1.7	-	06.3	65	56	63	54	28	036	014.6	26	-	-	22	12	02	-	05	07	12	02	07	03	05	01	
XI	6.6	7.1	6.5	7.5	-	07.9	74	48	84	54	104	044.5	30	-</															

Mesec	Vazdušni Prstenski Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)																		
		Tm			Sred. (Dies.)	Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21								8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.					
$\varphi = 43^{\circ}46' N \lambda = 18^{\circ}02' E$ Gr. $\Delta G = +1h\ 12\ min.$																														
II	-	00.0	02.7	00.5	00.9	03.2	-01.9	08.3	27	-10.6	19	.	.	01	01.0	10	01.7	01	02.0	.	.	.	56	04.1	03	03.7	22			
II	-	01.5	04.5	02.0	02.5	05.5	-01.2	14.0	25	-06.0	28	.	.	01	02.0	14	01.6	02	03.0	.	.	01	01.0	51	04.6	04	04.5	11		
III	-	10.5	16.4	05.8	06.4	11.1	01.6	23.2	23	-05.3	01	.	.	01	01.0	16	02.3	01	04.0	.	.	01	01.0	31	02.3	01	02.3	23		
IV	-	04.4	10.2	05.5	06.6	11.3	01.9	22.8	30	-03.8	11	.	.	02	02.0	25	02.3	01	01.0	.	.	01	03.0	40	03.3	03	03.0	18		
V	-	10.5	16.4	10.6	12.0	17.6	07.2	24.8	19	00.6	29	01	C1.0	07	01.1	18	01.4	.	.	.	01	06.0	43	03.4	03	01.3	20			
VI	-	13.1	18.1	12.8	14.2	18.4	05.2	27.0	11	01.8	05	01	01.0	09	01.1	21	01.5	.	.	02	01.5	28	02.2	07	01.0	23				
VII	-	15.3	21.4	15.3	16.8	22.1	11.5	27.2	30	07.8	24	03	01.0	09	01.3	21	01.5	.	.	.	29	03.3	04	02.5	27					
VIII	-	13.8	20.3	13.9	16.5	21.2	10.8	28.0	30	04.8	26	02	02.0	07	01.1	11	01.5	.	.	.	24	02.8	10	01.9	39					
IX	-	08.1	13.9	09.4	10.2	15.1	06.5	22.8	13	-01.8	29	.	.	09	01.0	28	01.6	.	.	.	06	01.6	03	01.3	34					
X	-	06.3	13.9	08.3	09.2	14.4	04.9	15.6	09	-01.4	04	02	01.0	01	02.0	22	01.9	.	.	01	01.0	33	02.7	05	03.0	29				
XI	-	02.5	05.9	03.5	03.8	07.4	00.8	18.0	11	-01.8	21	.	.	03	01.0	14	01.6	.	.	.	32	04.2	06	04.2	35					
XII	-	-04.3	-02.3	-03.7	-03.5	-01.0	-06.4	06.5	28	-16.0	05	.	.	01	01.0	37	01.4	10	01.8	.	.	24	03.7	02	04.5	19				
GOD.	-	06.2	11.3	07.0	07.9	12.3	03.8	29.0	30	VM -16.0	05	xii	10	01.2	49	01.2	247	01.7	15	02.1	.	.	07	02.1	417	03.5	50	02.6	300	
$\varphi = 43^{\circ}06' N \lambda = 18^{\circ}11' E$ Gr. $\Delta G = +1h\ 13\ min.$																														
I	-	02.1	06.5	04.2	04.2	07.1	00.9	13.6	30	-05.0	10.0	01	14	02.6	13	01.9	33	01.7	.	.	14	01.6	05	L2.0	.	.	14			
II	-	04.8	08.9	01.1	06.5	09.9	03.1	17.0	24	-03.0	18.0	15	02.9	11	02.4	24	01.8	.	.	12	01.7	08	02.1	.	.	.	04			
III	-	05.9	14.2	08.6	09.3	14.8	03.7	24.8	24	-05.2	01	11	02.1	08	02.1	23	01.8	.	.	12	01.4	18	02.0	.	.	.	21			
IV	-	07.5	14.8	09.6	10.4	15.4	04.6	25.2	29	-02.4	18	24	02.7	06	01.5	18	01.9	.	.	06	01.3	11	02.2	.	.	.	23			
V	-	13.3	20.6	14.2	15.6	21.3	09.1	28.4	19	04.6	30	11	02.7	04	01.6	19	01.7	.	.	20	01.5	07	02.0	.	.	.	32			
VI	-	16.5	22.8	16.5	17.6	24.5	10.8	29.6	11	06.6	05	16	C2.2	04	01.8	09	01.0	.	.	20	01.5	08	01.9	.	.	.	35			
VII	-	19.0	27.5	19.1	21.1	28.3	14.0	33.8	30	03.6	28	15	02.1	03	01.3	11	01.4	.	.	22	01.4	15	02.1	.	.	.	27			
VIII	-	16.9	25.2	17.3	19.3	26.3	12.6	34.2	30	07.2	26	08	02.5	05	01.2	15	01.5	.	.	18	01.3	09	02.0	.	.	.	38			
IX	-	13.9	20.4	14.3	15.7	21.5	10.7	28.0	01	01.2	30	31	02.4	02	02.5	13	01.6	.	.	21	01.5	05	02.2	.	.	.	18			
X	-	05.6	18.6	10.3	12.0	18.2	05.5	22.2	08	04.6	05	13	C2.4	02	02.0	13	01.8	.	.	23	01.5	03	02.0	.	.	.	39			
XI	-	05.6	11.3	07.2	07.7	12.4	03.2	21.4	11	-05.4	21	17	01.8	07	02.0	12	01.8	.	.	21	01.8	09	02.1	.	.	.	24			
XII	-	00.7	06.3	02.5	03.0	07.2	-00.9	12.0	10	01.0	-06.0	23	42	02.5	03	02.0	15	02.0	.	.	18	01.5	03	02.0	.	.	.	12		
GOD.	-	09.6	16.4	10.8	11.9	17.3	06.4	24.2	30	VM -06.0	04	xvi	219	02.4	68	01.9	215	01.7	.	.	207	01.5	401	02.1	.	.	.	285		
$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = +1h\ 13\ min.$																														
I	-	585.9	-04.6	-04.1	-04.4	-04.4	-04.1	-05.8	00.3	05	-13.1	16	18	06.9	*	01	10.0	.	.	14	C5.1	49	07.3	04	05.8	04	02.5	03		
II	-	588.6	-03.3	-03.0	-03.3	-03.1	-04.9	-04.9	02.0	24	-17.2	26	20	04.5	01	03.0	01	05.0	.	.	07	10.1	51	06.6	03	06.7	01	04.0	.	
III	-	594.4	-01.2	00.0	-00.6	-00.6	01.1	-02.8	06.3	24	-18.4	01	32	07.4	02	03.0	01	04.0	.	.	20	08.6	28	07.2	01	03.0	07	06.0	02	
IV	-	596.0	-03.0	-01.7	-01.9	-01.9	-01.9	-04.3	13.1	12	39	07.9	01	06.0	.	.	12	07.4	34	06.5	01	03.0	01	03.0	02					
V	-	594.5	03.9	06.4	04.2	04.7	07.4	02.2	14.0	19	-05.0	29	22	05.1	01	03.0	02	03.0	.	.	27	07.0	29	05.2	02	03.0	03	02.3	07	
VI	-	594.9	06.3	09.2	06.6	07.2	09.9	04.6	16.0	11	-04.0	04.0	02	24	04.7	02	03.5	04	02.2	.	.	06	04.5	32	05.1	03	02.4	02	C1.0	11
VII	-	695.8	03.9	11.1	09.3	09.9	12.5	06.8	18.4	30	02.5	23	26	06.3	*	03	03.0	09	06.3	37	05.6	03	03.2	02	04.5	10				
VIII	-	596.0	09.2	11.2	09.1	09.7	12.5	07.1	20.2	30	00.9	25	21	04.4	06	03.0	02	02.5	02	03.0	01	04.0	09	06.0	02	01.5	09			
IX	-	597.0	03.6	05.4	04.2	04.4	04.3	06.4	02.2	13.3	02	-07.5	25	43	05.4	13	04.9	02	02.0	.	.	12	05.6	13	05.6	*	03	04.0	06	
X	-	597.9	03.7	05.7	04.0	04.4	06.4	02.7	09.7	03	-05.4	04	21	04.0	06	04.3	03.0	04.0	.	.	14	05.5	24	05.0	06	03.7	04	04.2	13	
XI	-	590.4	-01.1	00.2	-00.6	-00.5	01.8	-02.8	07.6	12	-11.5	28	17	05.0	01	02.0	03	06.0	02	02.5	15	08.3	21	07.0	01	06.0	06	04.0	04	
XII	-	591.8	-04.6	-05.7	-05.8	-05.8	-03.4	-07.7	04.5	24	-16.6	05	41	07.6	09	04.0	02.0	03.6	02	05.0	04	07.0	25	07.9	01	06.0	02	03.5	01	
GOD.	-	601.8	01.4	03.0	01.7	02.0	04.2	-00.2	20.2	20	xvi	328	06.1	42	04.1	27	04.4	09	03.3	154	07.2	399	06.6	32	03.9	38	03.9	66		
$\varphi = 43^{\circ}50' N \lambda = 18^{\circ}21' E$ Gr. $\Delta G = +1h\ 13\ min.$																														
I	-	717.6	00.1	05.1	01.4	02.0	0.5	05.5	-02.0	15.0	27	-12.2	19	.	.	02	01.0	01	04.0	12	04.2	01	07.0	02	01.5	09	01.7	10	02.0	56
II	-	715.8	03.2	08.9	04.6	05.4	10.4	01.0	20.7	24	-06.3	05	.	.																



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Mjesec	Vrstdišni Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																	
		Tm			Sred. (Diss.)	Max	Min	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21							8.	9.	10.	11.	12.	1.	2.	3.	4.	5.	6.	7.	8.						
γ = 43°31' N λ = 18°27' E Gr. ΔG = + 1h 14 min.																													
I	672.2	00.4	03.5	06.5	01.5	04.0	-01.5	10.2	29	-12.2	19.0	03	02.7	05	03.2	05	01.0	01	01.0	03	05.7	22	03.0	23	01.7	02	01.0	29	
II	665.6	02.6	05.3	02.8	03.4	06.4	00.6	14.8	24	-01.2	28	04	02.5	03	01.7	08	01.1	06	01.2	02	04.5	23	04.3	19	02.1	01	01.0	18	
III	673.9	03.5	10.7	05.5	06.3	11.6	01.5	20.7	24	-08.4	01	07	01.6	09	01.8	05	01.2	05	01.0	02	03.1	25	03.1	17	01.7	03	01.0	17	
IV	668.8	04.7	10.4	06.2	04.9	11.4	02.2	22.9	29	-05.5	16	10	02.3	07	02.0	09	02.3	04	01.0	02	01.0	26	03.0	15	01.5	08	01.0	05	
V	672.2	11.4	11.4	12.7	17.5	07.6	27.2	15	00.5	28	05	02.0	15	01.5	06	01.8	04	01.0	03	01.3	32	02.2	15	01.4	05	01.0	08		
VI	671.5	13.0	17.9	10.2	13.0	19.0	08.1	25.5	11	02.9	04	10	02.1	12	02.0	06	01.7	07	01.3	02	01.0	19	02.3	22	01.8	05	01.0	14	
VII	672.2	15.7	21.4	15.6	17.0	22.3	11.2	25.5	30	05.5	07	08	02.1	12	02.1	07	01.7	07	01.3	02	01.0	25	03.2	12	02.0	04	01.2	18	
VIII	672.8	14.1	20.4	14.1	15.0	23.4	09.8	29.9	25	04.4	26	05.8	04	01.8	04	02.0	08	01.8	07	01.0	02	01.0	24	02.6	04	02.0	01	01.0	36
IX	675.1	09.1	14.3	09.6	10.8	15.3	07.0	22.5	13	-00.1	30	08	02.1	17	01.9	24	01.6	07	01.0	02	01.3	32	02.2	15	01.4	05	01.0	16	
X	676.2	06.1	15.0	07.4	09.8	15.5	04.0	23.5	08	-04.2	18	01	02.0	12	01.6	16	01.8	04	01.2	02	01.0	11	02.5	07	01.3	07	01.0	46	
XI	666.7	03.5	07.2	04.4	04.7	08.3	01.2	17.6	11	-10.2	21	01	01.0	03	01.7	16	01.7	04	01.0	02	01.0	17	03.5	15	02.3	02	01.0	28	
XII	672.8	-02.2	01.0	-01.6	01.9	-04.1	05.0	01	-10.5	05	03	03.7	22	03.0	29	01.8	03	01.0	02	01.0	13	02.3	11	02.4	07	01.0	10		
GOD.	672.2	06.8	12.0	07.4	08.4	12.9	03.9	25.9	39.0	-12.2	40.9	65	02.2	121	02.1	141	01.7	52	01.1	27	01.8	244	02.6	164	01.8	36	01.0	243	
γ = 43°10' N λ = 18°33' E Gr. ΔG = + 1h 14 min.																													
I	-	41.7	02.3	-00.2	00.0	03.3	-03.7	08.5	25	-13.0	01	+	+	13	02.8	+	+	23	03.0	+	+	05	03.0	+	+	07	02.3	45	
II	-	03.6	05.9	02.4	03.2	07.1	06.6	14.0	24	-01.4	28	+	+	26	02.9	+	+	33	02.9	+	+	10	03.3	+	+	03	02.0	12	
III	-	02.2	11.9	05.7	04.6	12.7	08.5	22.5	24	-09.4	01	+	+	18	02.6	+	+	32	02.8	01	03.0	09	02.9	+	+	10	02.5	23	
IV	-	04.7	11.9	06.1	07.2	12.9	01.6	23.5	30	-29.2	18	+	+	32	03.3	+	+	23	02.5	+	+	07	03.6	+	+	11	03.0	17	
V	-	10.4	17.3	10.8	12.3	18.7	05.8	25.5	19	00.6	30	+	+	27	02.8	+	+	24	02.8	01	03.0	05	02.9	01	02.0	12	02.2	19	
VI	-	12.9	19.5	14.0	15.5	21.2	08.5	27.0	11	03.6	07	+	+	28	02.8	+	+	31	02.8	+	+	10	03.3	+	+	10	02.5	23	
VII	-	16.0	24.1	16.5	16.3	25.4	10.1	31.5	30	05.0	28	+	+	28	02.8	+	+	31	02.8	+	+	11	03.0	09	02.9	10	02.5	21	
VIII	-	13.5	22.2	15.6	16.5	24.0	09.0	31.3	30	02.5	26	+	+	26	02.2	+	+	18	02.6	02	02.0	05	02.8	01	02.0	17	02.6	21	
IX	-	10.1	17.2	11.3	12.5	18.6	07.1	26.6	13	-02.2	30	+	+	52	02.8	+	+	10	02.7	+	+	07	02.6	01	02.0	15	02.2	39	
X	-	03.8	16.4	07.4	08.9	17.2	02.1	21.6	24	-02.4	20	02	02.0	20	02.6	08	02.4	21	02.4	08	02.2	07	02.0	03	02.0	14			
XI	-	02.5	08.9	04.6	05.2	09.0	00.5	20.0	11	-06.4	21	02	02.0	24	02.8	08	02.0	20	02.8	07	02.0	06	02.8	07	02.0	14			
XII	-	-02.7	02.6	-01.2	-00.6	03.5	-04.5	10.0	01	-10.4	22	01	02.0	45	04.0	08	02.7	18	02.7	03	02.3	12	02.2	14	02.2	14			
GOD.	-	06.1	13.4	07.7	08.8	14.6	03.0	31.5	30.0	-13.0	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
γ = 43°14' N λ = 18°36' E Gr. ΔG = + 1h 14 min.																													
I	656.0	-01.3	00.7	-00.6	01.5	-03.1	06.7	06	-11.6	19	05	01.8	01	02.0	13	02.7	02	03.5	11	02.8	37	02.9	02	03.0	01	02.0	21		
II	648.8	00.4	02.3	03.4	01.0	03.6	-01.3	12.0	24	-10.7	28	08	01.6	02	02.0	08	03.6	01	04.0	07	03.4	40	04.0	05	02.4	02	03.0	11	
III	-	02.3	07.9	04.3	04.7	09.1	00.7	18.2	24	-23	11	01	02.1	03.1	02.0	04.1	05	02.2	34	03.1	10	02.5	01	02.0	09	02.0	09		
IV	646.4	02.6	07.4	04.4	04.6	08.7	06.7	17.6	29	-06.0	18	13	03.7	04	02.0	14	01.3	01	05	02.2	34	03.1	10	02.5	01	02.0	09		
V	-	06.7	13.3	04.5	09.9	14.7	05.6	23.0	19	-00.3	28	16	02.2	03	02.0	06	02.7	01	03.0	11	03.0	31	02.7	09	01.2	07	01.0	16	
VI	649.4	11.3	15.4	10.8	12.1	17.0	07.8	23.0	11	02.4	03	10	02.4	05	03.0	02	02.5	05	02.4	07	02.0	06	02.4	07	02.0	05	02.5	35	
VII	-	13.4	18.1	14.3	15.1	20.6	10.6	27.2	30	07.4	28	18	02.2	08	02.9	06	02.5	05	03.0	08	03.0	25	03.0	09	01.8	02	02.5	17	
VIII	653.5	12.9	18.1	13.7	14.6	20.2	10.2	29.2	30	05.4	26	10	01.8	08	02.0	05	02.6	01	02.0	05	03.0	27	03.0	12	01.9	04	02.0	21	
IX	-	07.9	12.8	09.0	9.7	14.3	06.3	21.2	13	-02.3	29	25	02.6	10	02.5	07	02.3	01	03.0	02	02.5	18	03.4	06	02.7	05	02.6	16	
X	655.9	05.5	12.5	07.3	08.2	13.5	04.3	17.5	09	-01.1	04	13	02.0	05	02.3	06	02.6	07	02.4	08	03.0	26	02.4	09	02.0	05	02.6	29	
XI	650.4	02.4	05.0	02.8	03.2	06.4	00.3	16.2	11	-05.0	21	22	02.0	08	01.9	06	02.0	01	02.0	03	03.7	27	03.6	08	02.9	07	01.0	11	
XII	652.1	-04.0	-02.0	-03.2	-03.2	-03.0	-05.6	07.6	01	-11.7	19	23	02.5	05	03.0	16	03.5	03	03.0	03	03.0	19	03.3	06	02.7	06	03.2	14	
GOD.	-	05.2	05.4	05.6	06.6	10.8	03.0	29.2	30.0	-11.7	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
γ = 43°40' N λ = 18°39' E Gr. ΔG = + 1h 16 min.																													
I	-	-03.3	02.4	-01.7	01.1	03.2</td																							



Mjesec:	Vrsta dana Prstenski Pm mm	Temperatura vazduha °C							Čestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																					
		Tm			Sred. (Dnes)	W	NW	C	N			NE			E			SE			S			SW			W			
		7	14	21					Min.	Max.	Dat.	Min.	Dat.	8.	J.	E.	J.	8.	J.	E.	J.	8.	J.	E.	J.	8.	J.	E.		
γ = 42°58' N λ = 18°06' E Gr. ΔG = + 1h 12 min.																														
I	-	04.1	08.2	06.7	06.4	08.7	00.4	12.6	29.5	-20.6	01	15	01.4	.	.	.	.	39	01.5	13	J1.6	11	J1.4	06	01.8	11	J1.2	05	01.6	
II	-	35.5	10.4	08.2	08.1	10.8	02.7	17.2	25	-03.6	05	23	01.6	v1	03.3	01	02.0	J1	01.0	26	01.2	12	J1.6	11	J1.4	06	01.0	05	01.6	
III	-	06.5	15.1	11.4	11.1	15.4	02.2	24.2	24	-03.8	01	35	01.2	.	.	.	.	29	01.6	11	X1.8	09	01.0	03	01.3	16	X1.2	05	01.3	16
IV	-	07.8	15.5	11.1	11.4	15.8	02.3	24.8	30	-04.0	18	42	01.3	.	.	.	.	12	01.5	12	U1.5	08	01.0	06	01.8	11	U1.2	05	01.8	11
V	-	12.7	21.2	15.8	16.4	21.6	08.2	28.4	19	03.2	12	25	01.2	.	.	.	.	31	01.5	14	01.6	32	01.5	08	01.4	13	01.2	05	01.6	
VI	-	16.1	24.1	18.8	19.4	24.3	12.4	29.0	13	07.4	01	49	01.3	01	01.3	.	.	06	01.2	06	01.3	01	01.0	06	01.5	21	01.2	05	01.5	
VII	-	18.4	27.4	20.7	21.8	27.6	12.3	33.0	30	08.4	28	46	01.2	.	.	.	.	09	02.3	06	01.5	02	01.5	07	01.3	23	01.2	05	01.3	
VIII	-	17.4	25.4	19.1	20.3	25.7	11.1	34.2	30	05.2	26	35	01.1	.	.	.	.	10	01.2	14	01.8	08	01.4	04	01.2	12	01.2	05	01.2	
IX	-	13.7	21.6	16.4	17.0	21.8	07.5	27.8	01	-01.6	30	33	01.2	.	.	.	.	20	01.3	11	01.4	02	01.0	04	01.2	20	01.2	05	01.2	
X	-	09.0	19.4	12.3	13.3	19.6	04.0	21.8	28	-01.4	19	41	01.1	.	.	.	.	15	01.5	08	X1.4	03	01.3	01	01.5	25	01.2	05	01.2	
XI	-	35.7	13.0	08.4	08.8	13.3	02.7	21.2	12	-06.4	21	21	01.1	.	.	.	.	24	01.4	20	01.2	09	01.0	08	01.0	29	01.2	05	01.0	
XII	-	01.1	07.9	03.6	04.0	08.5	-02.2	14.6	01	-11.0	22	36	01.3	.	.	.	.	19	01.4	10	01.4	07	01.1	10	01.9	11	01.2	05	01.9	
GOD.	-	09.8	17.4	12.7	13.2	17.8	05.4	34.2	30.W	-11.0	22.XM	307	01.2	v2	02.3	J1	01.0	0.3	231	01.4	137	01.5	66	01.2	67	01.5	193	01.2	67	01.5
γ = 42°53' N λ = 18°27' E Gr. ΔG = + 1h 14 min.																														
I	-	02.5	07.6	06.5	04.8	08.3	03.8	14.4	25	-05.6	10	22	01.5	06	01.0	22	01.5	07	03.0	17	02.0	07	01.0	06	01.2	06	01.3	02		
II	-	35.0	10.4	06.0	07.5	11.3	03.0	15.6	20	-02.8	28	16	02.1	13	01.3	13	01.3	12	02.3	21	01.9	02	01.0	02	01.0	05	01.6	26		
III	-	03.6	14.9	09.9	10.0	16.0	04.4	22.2	26	-06.0	01	16	01.9	10	01.9	10	01.9	09	02.4	23	02.0	02	01.0	01	01.0	03	02.3	01		
IV	-	07.8	15.5	10.2	10.9	16.4	05.0	24.8	30.W	-11.6	13	24	02.0	07	J1.3	19	01.8	22	02.1	01	01.0	02	02.0	06	03.2	01				
V	-	13.1	20.6	14.8	15.8	21.8	09.7	29.0	19	04.6	11	15	01.0	08	01.0	19	01.2	17	02.1	22	01.6	01	01.0	07	01.7	06	02.0	.		
VI	-	15.6	23.4	17.8	18.5	24.7	11.9	30.0	19.1	05.6	11	16	01.5	13	01.5	13	01.5	12	01.7	21	01.9	02	01.0	02	01.0	05	01.6	25		
VII	-	18.7	28.2	21.9	22.7	29.5	15.3	34.6	30	12.0	28	15	01.5	06	01.3	15	01.1	16	01.4	31	02.1	01	02.0	08	01.9	01	01.9	01		
VIII	-	15.7	25.7	19.7	20.2	27.5	14.1	35.8	29	08.6	26	18	01.3	09	12	01.9	12	01.0	20	01.6	04	01.8	01	01.0	07	01.1	01			
IX	-	12.3	21.6	15.7	16.3	22.5	10.8	28.4	01	01.6	30	17	02.2	11	01.0	23	01.0	09	01.0	17	01.8	02	01.0	04	01.5	06	01.5	01		
X	-	08.0	19.0	11.3	12.4	19.8	06.5	22.6	09	03.0	20.0	11	01.2	09	01.0	23	01.0	09	01.0	25	01.2	05	01.0	01	01.0	09	01.3	03		
XI	-	06.4	12.9	08.5	09.1	14.0	04.5	24.0	11	-03.6	28	12	01.2	06	01.0	30	01.1	10	01.8	21	02.3	05	01.0	03	01.0	09	01.3	03		
XII	-	01.6	07.8	03.0	03.9	09.0	-00.4	13.6	11.0	-05.2	03	23	02.4	09	01.1	23	01.1	14	01.6	14	01.1	06	01.0	03	03.0	04	02.5	.		
GOD.	-	09.4	17.3	11.9	12.6	18.4	07.1	35.6	29.W	-06.0	04.W	209	01.7	197	91.0	01.0	244	01.1	131	01.7	257	01.8	37	01.1	32	01.7	67	01.8	20	
γ = 42°43' N λ = 18°29' E Gr. ΔG = + 1h 14 min.																														
I	-	02.7	08.5	04.6	05.1	09.1	01.2	15.0	29	-05.0	01	.	.	.	10	01.5	02	01.5	30	01.3	01	01.0	01	02.0	.	.	25	02.3	24	
II	-	05.4	11.5	06.5	07.5	12.3	03.4	19.6	24	-02.4	09	.	.	.	12	02.2	01	01.0	25	01.4	01	02.0	09	01.0	01	03.0	25	02.2	18	
III	-	05.6	15.4	08.2	09.4	15.9	04.6	26.2	24	-04.0	01	.	.	.	10	01.5	04	01.0	24	01.6	01	02.5	01	01.0	03	02.6	26	01.6	26	
IV	-	07.6	16.4	09.1	10.6	17.0	04.7	24.2	30	-02.2	18	.	.	.	12	01.6	03	01.7	06	01.8	01	02.5	01	01.0	03	02.4	17	02.3	17	
V	-	13.3	21.9	15.5	16.6	22.7	08.6	30.8	19	04.6	11	.	.	.	03	01.7	.	15	01.3	.	.	01	01.0	07	01.7	06	02.4	37	02.4	37
VI	-	16.1	23.8	18.6	19.4	24.4	10.5	29.4	19.6	04.4	05	.	.	.	02	02.0	02	01.5	07	01.6	01	01.0	08	01.0	04	02.5	43	02.5	43	
VII	-	19.5	27.9	21.3	22.6	28.9	13.9	33.2	30	10.4	28	.	.	.	05	01.7	01	03.0	08	01.0	09	01.0	08	01.0	03	02.5	44	02.5	44	
VIII	-	16.4	25.8	20.1	20.6	27.1	12.5	31.0	30	05.0	29	.	.	.	02	02.0	02	01.5	07	01.6	01	01.0	08	01.0	04	02.0	50	02.0	50	
IX	-	12.7	21.9	16.4	16.5	22.8	10.2	29.7	20	07.4	01	02.0	08	01.8	01	01.0	02	02.5	03	01.3	01	01.0	08	01.0	04	02.0	49	02.0	49	
X	-	07.0	17.5	12.3	11.3	18.4	04.1	25.4	08.7	-00.2	02	19	14	01.6	09	01.8	12	01.3	15	02.3	09	01.8	10	02.4	02	01.0	12			
XI	-	04.4	08.7	05.3	06.0	09.8	03.1	26.9	12	-07.7	30	12	02.1	08	02.2	04	01.8	08	02.2	10	02.0	14	02.1	23	02.1	09	01.4	06		
XII	-	05.2	09.2	-00.2	-01.0	-01.7	00.7	-04.2	08.8	25	-14.2	06	12	02.2	08	01.9	14	02.0	12	02.0	09	02.0	09	01.8	14	02.4	10	01.7	05	
GOD.	753.0	08.5	14.9	10.1	10.9	16.2	06.3	33.6	4.VI	-14.2	06.W	144	02.1	119	01.8	111	01.8	121	02.3	99	02.0	139	02.2	148	02.3	126	02.0	88		
γ = 45°46' N λ = 19°09' E Gr. ΔG = + 1h 16 min.																														
I	-	175.4	-0.7	03.6	01.1	01.4	04.7	-02.3	14.0	30	-12.0	01	09	01.9	01	02.0	04	02.5	27	02.9	06	02.2	04	01.8	08	01.8	01	02.0	33	
II	750.0	03.3	08.2	05.5	09.5	02.1	16.2	25	-06.9	04	10	02.0	02	01.0	06	01.7	04	02.0	23	02.4	12	02.3	11	02.4	10	02.4	06	02.4	24	
III	755.5	05.1	13.7	08.6	08.8	15.0	03.6	27.5	24	-04.6	01	05	02.4	07	02.0	01	01.4	18	02.4	09	02.2	15	02.4	08	02.2	13	02.5	09		
IV	750.6																													

Mesec	Oblačnost Nm (0-10)			Insolacijas broj sati (Dnev.)	Vlažnost vazduha			Padavine R mm			Broj dana nesa:																		
								Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	*	•	*	•	*	•					
	7	14	21		mm	7	14	21	Min	Σ	Max	Dat.	W	<	W	W	W	<	W	W	W	W	R	T	≡				
<b>LJUBINJE</b>																													
BR <sub>a</sub> ST <sub>a</sub> 146																													
I 5.7 5.0 5.9 5.5	-	05.6 67 73 75 21 80 76 30	399 107.0	12	.	.	12	.	.	.	.	.	07	08	16	16	10	16	.	.	.	.	.	01	.				
II 5.0 4.8 4.4 6.7	-	36.5 81 75 80 78 49	202 032.6	11	.	.	07	.	.	.	.	.	07	05	16	16	09	16	.	.	.	.	.	01	.				
III 3.4 2.9 3.6 3.3	-	-	-	194 092.4	13	.	.	12	.	.	.	01	17	04	09	09	05	09	.	.	.	.	.	01	.				
IV 3.0 1.7 3.4 2.7	-	-	-	-	081 025.0	15	.	07	.	.	.	.	14	02	08	08	02	08	.	.	.	.	.	01	.				
V 3.7 2.9 3.8 3.5	-	-	-	-	082 025.0	15	.	.	09	.	.	.	10	03	08	08	03	08	.	.	.	.	.	01	02				
VI 2.0 2.7 2.0 2.2	-	11.0 66 52 75 64 39	036 014.0	03	.	.	15	.	.	.	.	.	18	04	04	02	04	.	.	.	.	.	01	01					
VII 1.6 1.7 1.9 1.7	-	12.6 73 45 75 65 35	020 020.0	23	.	.	28	03	.	.	.	.	21	02	01	01	02	.	.	.	.	.	01	.					
VIII 2.4 3.0 2.4 2.6	-	11.7 70 51 74 65 35	108 019.4	20	.	.	19	04	.	.	.	15	12	10	06	12	.	.	.	.	.	09	.						
IX 2.7 3.0 3.1 3.0	-	09.8 71 56 75 67 32	270 069.2	19	.	.	02	09	.	.	.	16	03	09	09	06	09	.	.	.	.	.	03	01					
X 1.8 1.4 1.9 1.7	-	-	-	091 039.0	11	.	.	03	.	.	.	14	03	05	03	03	05	.	.	.	.	.	01	15					
XI 3.8 4.5 5.3 4.5	-	-	-	436 106.0	23	.	.	08	.	.	.	13	05	13	13	05	13	.	.	.	.	.	03	07					
XII 3.9 3.4 3.8 3.7	-	04.5 69 67 72 69 30	190 041.2	10	02	.	21	.	.	.	.	13	04	10	10	09	10	01	.	.	.	.	.	01	.				
GOD.	3.2 3.1 3.5 3.3	-	-	-	2109 107.0	421	02	.	72	80	07	.	01	171	37	112	109	65	112	01	01	.	.	.	20	24			
<b>BILEČA</b>																													
BR <sub>a</sub> ST <sub>a</sub> 147																													
I 7.9 7.8 7.1 7.6	-	05.6 87 78 87 84 57	248 054.6	16	.	.	14	.	.	.	03	.	04	20	18	16	08	18	03	.	.	.	.	05	02				
II 7.4 8.0 7.1 7.5	-	06.6 89 77 86 84 57	218 028.6	12	.	.	06	.	.	.	04	.	15	19	18	18	19	.	.	.	.	.	02	01					
III 5.2 5.7 4.4 5.1	-	37.2 85 65 77 76 31	178 074.6	13	.	.	03	03	.	.	01	.	08	11	09	08	05	09	.	.	.	.	.	01	.				
IV 5.1 5.7 4.3 5.4	-	57.7 82 67 74 74 52	092 031.4	15	.	.	03	.	.	.	04	.	11	08	08	03	08	.	.	.	.	.	02	.					
V 5.8 7.2 5.6 6.2	-	10.7 86 69 76 77 58	086 023.8	09	.	.	12	.	.	.	01	.	05	13	09	07	04	09	.	.	.	.	.	04	01				
VI 4.0 7.1 3.7 4.9	-	12.5 85 68 75 76 60	038 014.6	03	.	.	17	02	.	.	04	.	04	06	04	06	01	08	.	.	.	.	.	03	.				
VII 2.6 5.0 3.5 3.7	-	15.1 81 63 71 72 51	012 009.0	23	.	.	30	16	.	.	01	.	11	03	05	02	05	.	.	.	.	.	03	.					
VIII 3.6 5.9 3.6 6.4	-	13.8 87 68 76 77 49	090 025.4	24	.	.	24	07	.	.	02	.	08	05	15	11	03	15	.	.	.	.	.	12	.				
IX 4.3 6.7 4.0 5.3	-	11.3 88 70 78 79 59	360 120.8	20	.	.	11	.	.	.	03	.	08	09	10	08	07	10	.	.	.	.	.	05	.				
X 3.6 3.3 1.8 2.9	-	09.3 91 72 84 82 61	112 043.2	03	.	.	06	.	.	.	04	.	15	03	05	05	03	05	.	.	.	.	.	04	.				
XI 6.5 7.1 6.7 6.7	-	07.9 92 82 87 87 64	274 052.4	17	.	.	06	.	.	.	02	.	12	18	16	17	18	.	.	.	.	.	06	02					
XII 4.3 4.7 4.3 4.6	-	05.1 82 76 78 79 63	219 047.8	10	.	.	21	.	.	.	02	.	12	09	12	10	05	11	04	.	.	.	.	.	02	01			
GOD.	5.1 6.2 4.7 5.3	-	-	-	09.4 86 71 79 78 31	1927 120.8	20.1K	.	.	53	97	25	.	23	.	86	115	136	115	54	135	07	.	.	.	.	49	07	05
<b>LASTVA</b>																													
BR <sub>a</sub> ST <sub>a</sub> 148																													
I 6.5 7.6 6.6 7.0	-	05.3 87 66 83 79 43	269 089.4	13	.	.	11	.	.	.	01	.	03	15	13	13	06	13	01	01	.	.	.	02	01	01			
II 6.9 7.2 7.0 7.0	-	36.2 91 61 83 78 33	203 034.6	12	.	.	04	.	.	.	01	.	02	11	17	16	07	17	.	.	.	.	.	02	02				
III 4.4 4.7 4.1 4.4	-	06.3 88 46 80 72 22	171 062.3	13	.	.	06	02	.	.	01	01	09	08	08	08	04	08	.	.	.	.	.	02	.				
IV 5.6 4.7 3.6 4.6	-	36.5 84 44 74 67 23	104 027.4	15	.	.	02	.	.	.	01	09	08	08	04	08	.	.	.	.	.	01	03	01					
V 4.8 5.0 4.0 4.8	-	09.6 81 49 75 68 32	065 022.5	10	.	.	12	01	.	.	09	08	11	07	01	11	.	.	.	.	.	02	01						
VI 2.8 4.0 2.5 3.1	-	11.3 79 49 76 68 30	038 017.4	03	.	.	15	.	.	.	02	01	12	02	05	05	02	05	.	.	.	.	.	01	.				
VII 1.9 3.3 3.3 3.2	-	12.7 71 42 74 62 24	038 019.4	07	.	.	31	09	.	.	01	11	07	04	02	07	.	.	.	.	.	02	.						
VIII 3.1 4.4 3.8 3.8	-	12.4 83 49 71 74 31	117 038.6	15	.	.	24	05	.	.	01	01	12	02	15	12	04	15	.	.	.	.	.	04	01				
IX 3.3 4.6 3.7 3.9	-	10.7 85 56 81 73 38	226 084.6	20	.	.	11	.	.	.	03	02	12	05	11	11	05	11	.	.	.	.	.	03	.				
X 3.1 2.1 2.1 2.4	-	08.3 94 58 84 79 34	128 073.6	12	.	.	06	03	.	.	01	03	10	05	05	05	03	05	.	.	.	.	.	02	12				
XI 6.0 5.3 5.3 5.3	-	07.4 94 68 88 83 47	350 078.2	17	.	.	03	03	.	.	01	01	06	09	17	15	08	17	.	.	.	.	.	04	05				
XII 4.2 4.3 3.5 4.0	-	04.3 81 56 79 72 37	229 076.2	30	.	.	19	.	.	.	03	08	08	07	08	06	02	02	.	.	.	.	.	01	03	01			
GOD.	4.4 4.8 4.2 4.5	-	-	-	08.4 84 53 79 72 20	1938 098.4	42.1K	.	.	45	95	15	.	13	36	117	79	126	111	54	126	03	03	.	.	01	26	28	02
<b>PALIC</b>																													
SR SRBIJA																													
BR <sub>a</sub> ST <sub>a</sub> 149																													
I 8.0 8.4 8.1 8.1	-	063.6 04.3 90 76 87 85 40	036 012.5	16	01	02	23	.	.	.	07	.	01	13	12	09	07	01	07	03	01	01	.	.	20	12			
II 7.9 7.5 6.8 7.4	-	100.7 05.6 89 69 86 49	068 022.5	15	.	.	07	.	.	.	12	04	.	12	16	11	12	05	02	01	.	.	01	.	10	03			
III 5.4 5.9 4.1 5.5	-	192.8 05.9 85 49 78 71 24	037 010.7	31	.	.	04	02	.	.	14	05	07	07	10	09	07	01	09	02	.	.	.	01	01				
IV 6.3 6.7 4.5 5.8	-	198.2 10.6 22 75 68 27	049 011.9	25	.</																								

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Mesec:	Vazdušni Prstenski Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Pm (0-12)																	
		Tm	7	14	21	Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.							
$\gamma = 45^{\circ}07' N \lambda = 19^{\circ}15' E$ Gr. $\Delta G = +1h\ 17\ min.$																													
I	-	00.6	04.5	02.0	02.3	05.4	-00.3	15.0	30.12	-07.0	01	03	02.0	03	02.0	06	01.7	49	03.8	.	.	05	33.2	04	02.8	11	02.5	12	
II	-	03.9	09.2	05.6	06.1	10.7	02.8	20.0	25	-08.0	04	03	02.7	16	03.0	02	02.3	.	.	05	02.2	.	.	17	03.1	07			
III	-	35.9	14.6	09.4	09.8	15.7	04.9	27.5	24	-04.0	01	05	02.2	19	31.8	07	02.4	37	03.1	.	.	01	03.3	01	03.0	18	02.0	05	
IV	-	37.2	15.2	06.9	10.4	16.2	05.1	27.1	29	-02.0	12	05	01.4	19	02.1	12	01.8	19	03.4	03	02.3	.	.	03	01.0	23	03.5	06	
V	-	14.8	21.6	15.7	17.0	22.8	11.8	30.5	20.0	04	05.5	29	12	02.3	10	01.9	17	01.4	31	02.7	01	02.3	.	.	04	32.0	11	01.7	07
VI	-	17.6	24.7	18.2	19.7	25.9	12.2	33.5	14	04.0	05.0	09	02.4	10	01.9	10	02.1	16	01.6	02	01.3	06	01.5	05	02.2	22	02.2	10	
VII	-	18.0	25.3	18.9	20.3	24.6	14.0	35.0	31	09.5	28	11	02.0	20	11.4	12	01.1	20	01.4	01	02.0	03	02.7	07	01.9	06	01.5	13	
VIII	-	17.4	25.4	18.0	20.1	26.1	14.6	31.0	09	09.0	26	06	02.5	14	01.4	13	01.7	32	01.8	.	.	03	32.0	02	01.5	21	02.5	02	
IX	-	11.6	19.6	13.4	14.5	20.6	09.4	29.5	05	02.5	30	06	02.3	21	01.7	10	01.7	16	02.6	01	03.0	01	02.5	17	02.7	16			
X	-	38.4	17.9	11.5	12.3	18.8	06.8	25.0	08.0	01	02.0	21,18	06	01.0	13	01.5	11	01.6	39	02.3	02	01.5	01	03.0	03	02.0	11	01.4	07
XI	-	36.8	09.1	06.4	06.7	10.6	03.4	21.8	12	-03.8	30	02	01.0	15	01.9	15	01.3	31	01.5	01	02.0	.	.	03	01.4	17	02.5	08	
XII	-	-32.8	00.3	-01.6	-01.4	01.2	-03.8	07.5	28	-14.0	06	05	04.8	13	01.7	11	01.8	33	03.2	.	.	01	32.0	03	02.7	18	01.0	09	
GOD.	-	09.0	15.6	10.7	11.5	16.7	06.7	33.5	44.VI	-14.0	06.XI	73	02.0	173	01.8	126	01.6	357	02.6	11	01.9	26	02.4	35	02.1	192	02.5	102	
$\gamma = 45^{\circ}22' N \lambda = 19^{\circ}34' E$ Gr. $\Delta G = +1h\ 17\ min.$																						BACKI PETROVAC		BR. ST. 152					
I	-	50.3	05.0	01.6	02.1	05.8	-01.0	15.0	12	-09.5	19	05	01.4	06	01.2	12	01.5	31	02.3	04	01.5	25	01.4	06	01.3	13	01.2	11	
II	-	34.9	09.8	06.1	06.7	10.9	03.2	19.5	25	-06.8	04	10	01.8	04	01.5	07	01.1	39	01.4	13	01.9	16	01.9	08	02.0	09	02.1	08	
III	-	25.8	14.9	08.6	09.5	15.9	04.3	28.7	24	-04.8	01	06	01.7	02	01.5	13	01.8	17	02.1	08	01.2	07	01.6	38	01.6	17	02.3	15	
IV	-	07.5	15.3	09.3	10.3	16.2	04.9	27.9	29	-01.1	12	01.6	08	01.6	09	01.6	12	02.6	04	01.5	05	01.4	11	02.1	19	03.1	19		
V	-	15.0	22.4	15.1	16.9	23.2	10.9	30.6	20	05.0	29	02	02.0	07	01.3	09	01.7	17	01.9	03	01.3	05	01.2	08	01.4	19	01.4	23	
VI	-	17.9	25.0	17.7	19.6	26.4	12.8	34.0	14	03.1	04	07	01.3	06	01.3	02	01.0	32	01.5	06	01.2	07	01.3	14	01.7	31			
VII	-	18.4	26.2	18.7	20.5	27.1	14.2	33.3	31	10.3	28	02	01.5	07	01.4	08	01.2	11	01.4	04	01.2	05	01.2	14	01.6	29			
VIII	-	17.4	25.6	18.6	20.0	26.6	14.5	31.0	10	11.0	26	06	01.7	11	01.5	16	01.6	05	02.0	05	01.7	14	01.7	25					
IX	-	11.2	20.1	12.6	14.1	20.9	08.6	30.1	05	-00.3	28	13	01.8	06	01.2	09	01.9	03	02.0	04	01.2	03	02.0	15	01.5	32			
X	-	07.2	18.1	11.1	11.5	16.8	05.9	26.1	06	00.4	18	04	01.0	04	01.2	14	01.4	19	01.8	02	02.0	06	01.7	07	01.3	05	01.2	32	
XI	-	36.6	09.8	05.7	04.4	10.9	02.8	23.7	12	-05.4	30	06	01.5	19	01.8	02	01.9	39	01.3	09	01.6	11	01.6	08	01.8	12	01.7	19	
XII	-	-02.6	00.6	-01.5	-01.3	01.3	-03.8	09.4	27	-15.7	06	08	01.1	07	01.1	09	02.2	21	02.0	08	01.4	37	01.1	13	01.5	10	01.7	10	
GOD.	-	09.0	16.1	10.2	11.4	17.0	06.4	34.0	44.VI	-15.7	06.XI	71	01.5	74	01.4	106	01.5	166	01.9	73	01.5	83	01.5	110	01.6	161	01.8	254	
$\gamma = 45^{\circ}49' N \lambda = 19^{\circ}39' E$ Gr. $\Delta G = +1h\ 18\ min.$																						BACKA TOPOLA		BR. ST. 153					
I	-	-00.2	04.0	01.5	01.7	04.6	-01.2	15.2	30	-09.5	19	•	•	07	01.0	•	•	52	02.1	•	•	16	01.1	01	01.0	00	01.3	08	
II	-	03.6	09.0	05.4	05.8	09.9	02.6	17.5	21.20	-06.2	04	•	•	06	01.7	07	01.4	•	•	25	01.5	01	03.0	19	01.6	08			
III	-	05.6	14.0	08.7	09.3	15.3	04.0	26.1	24	-05.0	01	06	01.5	05	02.1	04	02.1	35	01.9	02	01.0	14	01.2	05	02.3	10			
IV	-	07.0	14.3	09.1	09.9	15.3	04.2	27.0	29	-02.0	12	01	01.0	17	01.4	06	02.1	18	02.1	01	01.5	•	•	35	02.3	08			
V	-	14.4	21.9	15.8	17.0	23.1	10.8	31.0	20	04.4	28	01	04.0	13	02.2	07	01.4	27	01.9	01	01.0	14	01.2	05	02.0	16			
VI	-	17.6	25.0	18.7	20.6	26.5	13.0	33.6	14	03.0	04	07	01.4	08	01.1	08	01.4	39	01.2	02	01.0	31	01.7	01	01.0	25	01.5	14	
VII	-	17.6	25.0	19.4	20.5	27.1	14.3	32.2	31	10.5	28	01	01.0	06	01.0	08	01.4	16	01.2	01	01.0	03	01.5	01	01.7	13			
VIII	-	16.7	25.6	19.4	20.3	26.6	14.6	31.6	09.7	07.5	26	06	01.3	08	01.4	06	01.4	23	01.4	08	01.5	01	01.3	08	02.0	17			
IX	-	10.8	19.7	13.4	14.3	20.9	08.6	29.7	05	00.0	28	•	•	20	01.3	•	•	10	01.5	01	01.0	11	01.3	•	•	32	01.9	16	
X	-	17.1	17.9	11.2	11.9	18.7	06.1	25.5	18	00.0	28	•	•	08	01.0	•	•	34	01.5	•	•	08	01.4	•	•	21	01.2	13	
XI	-	04.3	08.8	05.8	06.2	09.8	03.1	21.4	12	-05.6	30	•	•	15	01.3	•	•	19	01.3	•	•	22	01.1	•	•	21	01.2	13	
XII	-	-03.0	06.1	-01.6	-01.6	00.7	-03.9	07.7	27	-13.1	06	•	•	12	01.1	•	•	30	01.8	•	•	16	01.3	•	•	24	01.2	11	
GOD.	-	08.5	15.5	10.6	11.3	16.5	06.4	33.6	34.VI	-16.0	06.XI	187	02.1	67	01.7	196	01.7	70	02.6	120	01.8	36	01.7	212	02.0	108	02.3	99	
$\gamma = 45^{\circ}34' N \lambda = 19^{\circ}39' E$ Gr. $\Delta G = +1h\ 18\ min.$																						NOVI SAD-RIMSKI SANČEVI		BR. ST. 155					
I	755.1	00.3	04.6	01.5	02.0	05.4	-00.9	15.4	12	-10.3	20	01	02.0	02	03.0	16	03.2	35	04.6	*	*	08	01.8						

Mesec	Oblačnost Nm (0-10)			Inicijacijski broj seta (tides)	Vlažnost vazduha			Padavine R mm			Broj dana na sa:																					
	7	14	21		7	14	21	Σ mm	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	■	□					
	mm	mm	mm		Σ mm	Max	Dat.	≤	<	<	≥	≥	≥	≥	≥	≥	<	>	≥	≥	≥	•	*	Δ	○	▲	■	□				
SID																																
BR. ST. 151																																
I 8.4 8.1 6.7 7.8	-	-	-	-	-	-	-	041	016.8	13	•	02	14	•	•	•	08	•	18	08	07	01	07	02	•	•	01	•	06			
II 9.0 8.1 5.8 7.6	-	06.0	89	74	88	84	40	092	025.2	15	•	02	05	•	•	•	03	•	15	16	15	15	15	03	•	•	01	03	06			
III 7.1 7.0 3.6 5.9	-	16.4	83	80	72	75	25	362	012.4	14	•	•	02	03	•	•	03	•	04	10	11	10	03	11	02	•	•	01	•	02		
IV 6.9 5.2 4.5 5.6	-	07.1	83	55	81	74	21	-	-	•	•	03	02	•	•	35	•	04	08	-	-	-	-	-	-	•	•	03	•	03		
V 4.5 5.8 5.5 5.2	-	10.8	84	56	81	74	30	056	021.8	07	•	•	10	02	01	02	•	06	09	10	07	02	10	•	•	•	•	05	01			
VI 3.5 4.6 3.1 3.7	-	12.0	78	50	77	69	26	060	035.0	17	•	•	18	07	•	01	01	11	04	07	05	01	07	•	•	01	04	•	•	01		
VII 5.5 5.5 5.2 5.4	-	13.5	87	56	84	76	31	089	020.0	23	•	•	23	05	•	02	01	04	06	15	14	04	15	•	•	06	•	06	•	06		
VIII 5.5 5.0 5.0 5.2	-	13.8	91	57	86	78	39	087	033.5	24	•	•	25	02	•	•	04	05	11	08	04	11	•	•	•	•	04	02	•	•	04	
IX 6.1 7.1 4.7 6.0	-	-	-	-	-	-	-	034	010.2	19	•	•	11	•	•	01	01	10	07	04	01	07	•	•	•	•	01	07	•	•	01	
X 6.6 4.5 2.4 4.5	-	08.4	91	61	83	78	33	024	017.5	03	•	•	02	•	•	01	01	05	03	03	01	03	•	•	01	02	•	•	12			
XI 8.1 7.7 6.3 7.4	-	-	-	-	-	-	-	109	023.5	27	•	•	07	•	•	01	01	02	15	15	13	04	15	03	03	•	•	08	•	08		
XII 8.6 7.5 5.4 7.0	-	-	-	-	-	-	-	077	014.8	02	04	15	25	•	•	•	•	05	17	13	11	04	09	11	•	•	05	•	14			
GOD. 6.6 6.3 4.8 5.9	-	-	-	-	-	-	-	04	19	56	94	16	01	-	-	50	122	-	-	-	-	-	-	01	01	21	-	-	-	-	-	
BACKI PETROVAC																																
BR. ST. 152																																
I 6.1 7.1 5.8 6.6	052.0	-	-	-	-	-	-	036	011.4	16	•	01	20	•	•	•	01	10	12	08	01	10	04	•	•	•	•	01	06			
II 7.0 6.0 6.4 6.4	087.5	06.2	87	73	85	82	42	086	027.9	15	•	01	05	•	•	02	•	02	10	19	12	02	16	03	•	•	01	01	04			
III 5.3 5.3 3.1 4.6	178.2	-	-	-	-	-	-	050	012.4	30	•	•	03	03	•	•	08	06	10	10	02	10	01	•	•	01	01	02				
IV 6.2 6.5 4.8 5.8	179.8	-	-	-	-	-	-	043	020.7	16	•	•	02	02	•	•	01	04	08	11	06	01	11	•	•	01	03	•	•	03		
V 4.6 5.9 4.5 5.0	217.6	-	-	-	-	-	-	079	012.6	09	•	•	10	02	•	•	06	04	13	10	05	13	•	•	07	•	•	07	•	07		
VI 3.4 5.1 3.6 4.1	259.7	-	-	-	-	-	-	058	018.4	28	•	•	21	07	•	02	08	02	10	08	03	10	•	•	01	09	01	•	01			
VII 4.7 4.9 3.5 4.4	252.5	-	-	-	-	-	-	038	015.0	16	•	•	22	08	•	05	05	13	10	01	13	•	•	08	•	•	08	•	04			
VIII 4.1 4.7 3.6 4.4	235.1	-	-	-	-	-	-	080	015.2	23	•	•	25	03	01	-	07	03	10	07	04	10	•	•	08	04	•	•	04			
IX 4.4 5.1 4.4 4.4	183.8	-	-	-	-	-	-	040	014.5	18	•	•	01	11	01	•	01	09	05	09	07	02	09	•	•	03	06	•	•	06		
X 4.7 4.1 2.8 3.9	156.0	-	-	-	-	-	-	020	019.1	03	•	•	03	03	•	•	12	04	05	01	05	01	05	01	•	•	16					
XI 7.1 6.2 6.4 6.6	063.0	-	-	-	-	-	-	087	016.5	17	•	•	08	•	•	01	02	10	18	12	04	17	04	01	•	01	12	01	01			
XII 7.7 7.2 6.8 7.2	054.9	-	-	-	-	-	-	062	014.2	02	03	12	24	•	•	-	03	18	13	08	02	08	07	•	•	09	11	•	•	11		
GOD. 5.4 5.7 4.6 5.3	1920.9	-	-	-	-	-	-	679	027.9	45	•	03	14	63	97	21	01	-	67	85	143	103	28	134	19	01	•	01	03	40	-	23
BAČKA TOPOLA																																
BR. ST. 153																																
I 7.8 7.4 6.7 7.5	-	04.5	90	77	87	84	44	033	007.5	16	•	02	20	•	•	•	01	13	13	07	•	08	06	01	•	•	05	05	05			
II 8.3 6.1 5.5 6.6	-	05.7	88	68	85	81	43	076	022.5	15	•	01	07	•	•	01	01	02	10	14	12	02	13	02	•	•	02	01	02			
III 5.5 5.5 5.0 2.7 4.4	-	05.9	89	49	74	68	21	046	011.8	31	•	•	02	03	•	•	01	01	09	09	06	02	09	•	•	01	01	01				
IV 6.2 6.2 4.2 5.0 5.2	-	06.1	78	49	74	67	27	038	007.0	25	•	•	05	02	•	•	02	01	04	10	10	09	10	•	•	01	01	01				
V 4.5 5.2 5.2 5.2 5.3	-	09.4	75	48	72	65	21	048	012.4	07	•	•	10	02	•	•	03	06	10	09	02	10	01	•	•	03	01	01				
VI 3.5 4.8 4.2 4.2 4.2	-	11.7	76	49	72	66	30	129	041.5	17	•	•	20	07	•	01	01	05	09	09	04	09	09	•	•	03	01	01				
VII 5.0 5.5 4.5 4.5 5.0	-	12.7	82	53	77	61	37	051	015.4	27	•	•	25	07	•	•	04	06	11	07	02	11	01	•	•	03	01	01				
VIII 4.0 5.5 3.5 4.3 4.3	-	12.9	86	52	73	39	050	018.6	14	•	•	22	04	01	•	03	05	11	09	02	11	01	•	•	03	01	01					
IX 3.4 5.5 4.3 4.4 4.4	-	08.7	83	51	78	70	31	041	015.9	19	•	•	11	•	•	01	01	09	05	06	05	02	06	•	•	01	01	01				
X 5.9 4.0 4.4 4.5 4.5	-	07.9	91	57	82	77	32	015	008.4	03	•	•	02	•	•	-	04	10	04	06	04	06	06	•	•	06	11	•	•	11		
XI 8.1 6.7 5.9 6.9 6.9	-	06.5	93	79	80	74	44	087	012.0	17	•	01	08	•	•	-	03	11	17	15	03	16	04	02	•	•	01	07	01			
XII 8.2 7.9 7.1 7.7 7.7	-	03.7	88	86	89	88	60	040	007.5	02	04	14	23	•	•	-	04	18	13	07	08	06	02	•	•	06	12	•	•	12		
GOD. - - - - -	-	2034.4	-																													

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Mesec	Vazdušni pritisak Fm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Fm (0-12)																		
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C		
		7	14	21	Sred. (dies)							8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.		
$\gamma = 45^{\circ}15' N \lambda = 19^{\circ}52' E$ Gr. $\Delta G = + 1h 18 min.$																														
I	750.1	01.4	04.8	02.4	02.8	05.9	-00.2	14.4	12	-09.5	19	16	01.5	03	02.3	21	03.0	43	03.9	07	03.7	13	02.5	08	02.5	09	01.8	03		
II	748.5	06.0	09.0	06.8	07.3	10.0	-00.1	19.8	25	-06.5	04	12	31.9	02	31.5	16	02.2	02	03.0	05	02.6	23	03.3	21	02.8	03	03.0	07	02.7	.
III	755.3	07.5	14.1	10.2	10.5	15.1	04.4	27.7	23	-04.0	01	08	02.4	01	31.1	18	02.7	19	03.2	04	02.8	21	02.0	15	02.5	07	02.7	.		
IV	748.3	38.1	14.4	10.2	10.7	15.4	06.3	25.9	29	00.3	12	12	02.1	07	01.6	09	02.0	14	03.1	05	02.4	14	02.1	11	02.8	18	02.8	.		
V	750.1	15.1	21.2	16.7	17.4	22.0	12.9	28.9	20	07.6	27	13	01.6	07	01.1	18	02.2	12	02.8	06	03.7	21	01.9	09	02.3	07	01.7	.		
VI	748.3	17.7	24.3	20.1	20.6	25.8	15.6	32.1	14	08.2	04	02	31.8	02	01.5	14	01.8	31	02.0	05	01.6	24	02.0	22	02.3	10	01.9	01		
VII	748.8	18.9	25.6	20.5	21.4	26.8	16.5	33.9	31	13.6	27	09	01.8	02	02.0	12	02.0	37	02.1	04	02.2	22	02.1	22	02.5	15	02.1	.		
VIII	748.4	18.1	25.1	20.4	21.0	26.0	15.9	30.9	09	12.4	25	12	01.5	07	01.4	18	02.2	16	02.1	06	01.3	19	02.2	18	02.6	08	02.2	01		
GOD.	750.8	09.9	15.5	11.8	12.2	16.6	08.2	33.9	34.VI	-09.5	42	08.X	113	01.8	59	01.5	173	02.4	150	02.9	61	02.3	225	02.1	210	02.5	96	02.2	08	
$\gamma = 45^{\circ}08' N \lambda = 20^{\circ}00' E$ Gr. $\Delta G = + 1h 20 min.$																														
I	-	-00.1	04.1	01.2	01.6	05.5	-01.7	14.8	30	-12.0	19	19	01.9	03	02.0	01	01.0	36	02.7	15	01.3	07	02.0	05	01.6	07	02.0	.		
II	-	03.5	09.1	05.0	05.6	10.8	02.3	19.6	23	-06.6	04	13	02.4	01	01.0	04	02.0	12	02.2	12	02.2	09	01.6	21	02.6	.				
III	-	05.7	14.2	08.3	09.1	15.3	04.7	28.0	23	-05.3	01	16	02.4	02	02.0	16	02.4	14	03.2	07	02.3	07	02.1	06	01.7	25	03.3	.		
IV	-	07.2	14.0	08.9	09.8	15.8	05.3	26.3	29	-01.3	12	11	02.7	05	03.2	08	01.6	10	03.2	09	02.1	09	02.2	09	03.5	.				
V	-	14.5	21.1	15.0	16.4	22.3	11.8	28.9	04	07.3	29	19	02.6	07	02.6	10	01.9	14	02.1	17	02.0	03	02.3	07	02.0	16	02.6	.		
VI	-	17.9	24.3	18.5	19.8	26.0	18.3	33.9	14	06.1	04	17	02.2	04	02.0	03	02.0	05	01.8	16	01.7	10	02.2	16	01.6	21	02.8	.		
VII	-	18.5	25.7	19.3	20.0	26.9	15.5	33.5	31	11.6	26	25	01.7	05	02.0	12	01.3	08	01.6	10	01.2	06	01.5	06	02.0	21	02.8	.		
VIII	-	17.2	25.3	18.7	20.0	26.6	15.1	32.0	10	11.1	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	09.0	15.3	10.2	11.2	-	07.0	-	-	-12.0	49.I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\gamma = 45^{\circ}38' N \lambda = 20^{\circ}02' E$ Gr. $\Delta G = + 1h 20 min.$																														
I	-	00.1	04.4	01.5	01.9	05.2	-00.9	13.8	30	-09.2	20	06	01.7	02	01.5	09	02.0	45	03.3	05	02.0	07	01.9	04	03.0	07	02.3	08		
II	-	33.8	09.1	05.2	05.8	10.2	02.7	18.1	23	-06.3	04	05	02.0	05	01.6	03	02.0	18	02.6	13	02.5	07	02.4	12	02.8	13	02.2	08		
III	-	05.6	14.4	08.8	09.4	15.4	04.6	28.8	24	-05.5	01	07	01.7	01	01.0	07	01.6	34	02.8	08	02.4	04	02.5	11	02.5	15	02.9	06		
IV	-	06.8	14.3	09.1	09.9	15.6	04.7	26.8	29	-01.6	12	16	02.0	06	01.7	05	02.0	19	02.9	07	01.9	04	02.4	20	03.0	05				
V	-	14.6	21.8	16.2	17.2	23.1	11.3	30.8	20	04.5	28.I	28	11	01.6	08	01.5	08	02.0	21	02.8	09	01.9	03	01.7	07	01.9	18	02.0	.	
VI	-	17.6	24.9	18.8	20.0	26.4	13.0	33.2	14	03.2	02	11	01.6	09	01.1	04	01.2	04	01.5	09	01.7	12	02.6	15	02.0	09	02.0	.		
VII	-	18.1	25.8	19.2	20.6	27.0	14.1	32.4	31	10.2	13	13	01.7	05	01.4	09	01.8	13	02.0	07	01.3	09	01.6	17	02.2	17	02.4	02		
VIII	-	17.0	25.0	19.4	20.2	26.2	14.8	31.4	10	08.0	26	18	01.0	10	01.2	06	01.9	24	02.0	08	02.1	08	02.2	11	01.6	02				
IX	-	11.1	19.7	13.4	14.4	21.0	09.2	30.3	05	00.8	28	21	01.5	04	01.5	13	01.9	11	01.8	04	01.5	07	01.3	11	01.7	13	01.8	06		
X	-	07.2	17.9	11.0	11.8	18.6	03.3	29.3	06	01.4	18	04	01.3	05	01.2	13	01.8	29	02.4	04	01.5	14	02.0	06	01.7	07	01.3	09		
XI	-	04.4	09.3	05.3	05.7	06.3	10.3	10.3	12	-05.4	30	11	01.6	06	02.2	08	01.8	16	02.3	15	02.1	09	01.7	13	02.2	09	02.1	03		
XII	-	-03.1	-00.2	-02.1	-01.9	00.6	-03.9	07.7	27	-14.9	05	07	01.6	05	01.2	13	01.8	22	02.6	06	01.5	07	01.4	14	01.9	15	01.9	04		
GOD.	-	08.6	15.5	10.5	11.3	16.6	06.6	33.2	44.VI	-14.9	49.VI	55	01.4	54	01.7	210	02.1	75	02.0	150	01.8	112	02.0	254	01.9	128				
$\gamma = 45^{\circ}56' N \lambda = 20^{\circ}05' E$ Gr. $\Delta G = + 1h 20 min.$																														
I	-	-0.4	04.5	01.7	01.9	05.0	-01.3	13.9	30	-10.4	01	05	01.4	03	01.0	09	01.9	41	02.4	10	02.3	09	02.0	09	02.1	07	02.0	.		
II	-	03.9	09.2	05.6	06.1	09.9	02.8	17.5	20	-05.6	04	05	02.0	05	01.6	03	02.0	18	02.6	13	02.5	07	02.4	12	02.8	13	02.2	01		
III	-	05.5	14.8	09.4	09.8	15.2	04.2	28.1	24	-05.0	01	05	02.4	07	01.7	10	01.8	20	02.2	11	01.5	11	02.3	13	02.0	05				
IV	-	07.5	14.0	09.7	10.4	15.6	04.8	26.9	29	-00.8	06	03	02.7	10	01.0	12	01.6	06	02.3	15	01.7	10	02.3	23	02.6	04				
V	-	15.2	22.2	16.5	17.6	23.3	11.3	31.7	20	05.6	29.7	10	01.9	01	01.0	03	01.3	15	02.3	04	01.5	15	01.9	06	01.8	19	01.9	20		
VI	-	18.4	25.7	18.2	20.4	27.2	13.5	34.8	14	03.0	04	02	05	01	01.0	04	01.2	06	02.5	04	01.5	09	02.0	08	01.7	11	01.6	22		
VII	-	18.6	26.7	19.7	21.2	28.0	14.4	34.0	31	10.8	28	*	06	01.3	04	01.5	05	02.0	13	02.3	04	01.8								

Meseč	Oblačnost Nm (0-10)			Insekcija Sred. (Dles)	Broj sati mm	Vlažnost vazduha		Padavine R mm	Broj dana na sat																				
	7	14	21			U m s			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	■	■			
	mm	7	14	21	Sred. (Dles)	Min	Σ	Dat.	30.00.0	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	0.0	9	Δ	*	Δ	▲	▲	■	■	
<b>NOVI SAD-PETROVARADIN</b>																													
BR. ST. 156																													
I 6.9 7.6 6.4 7.9	053.1	J4.3	78 70 78 75 40	029 006.9	13	.	02	16	.	.	.	.	.	18	07	03	14	10	08	.	09	05	02	.	01	.	06	06	
II 7.9 6.9 6.4 7.1	066.3	J5.4	76 65 74 72 28	094 027.2	15	.	01	05	.	.	.	.	.	14	03	03	12	12	09	14	02	17	03	01	.	.	02	04	
III 5.9 5.8 5.2 5.0	185.1	J0.8	71 52 66 62 23	062 015.1	30	.	.	02	02	.	.	.	.	15	01	09	08	12	09	02	12	02	02	01	.	01	.	01	01
IV 6.5 6.4 5.7 6.4	193.9	J0.9	71 50 64 62 24	037 034.0	16	.	.	01	.	.	.	.	.	13	01	10	11	07	01	11	.	.	.	.	.	.	01	02	.
V 5.5 6.8 5.5 5.9	233.4	J8.9	70 47 62 60 29	056 013.2	10	.	.	09	.	07	.	.	.	10	12	09	02	12	.	.	.	.	.	.	.	.	07	.	
VI 3.8 5.7 4.6 4.7	286.4	J10.6	71 45 62 58 28	032 010.0	17	.	.	19	06	03	08	01	08	05	09	06	01	09	.	.	.	.	.	.	.	07	01		
VII 4.9 4.9 3.3 4.2	275.1	J11.8	74 47 68 63 30	056 013.6	23	.	.	21	07	02	09	.	09	04	11	10	02	11	.	.	.	.	.	.	.	02	.		
VIII 4.7 5.1 4.3 4.7	255.6	J12.2	78 72 69 66 34	069 018.8	24	.	.	22	02	.	09	03	10	06	10	08	03	10	.	.	.	.	.	.	.	07	.		
IX 4.3 6.1 4.8 5.0	198.7	J06.4	77 51 67 65 30	036 016.6	18	.	.	10	.	04	01	08	08	07	05	01	07	.	.	.	.	.	.	.	02	01			
X 4.5 4.0 3.4 4.0	176.1	J07.6	81 55 71 69 29	018 013.2	03	.	.	05	.	08	01	16	08	07	04	01	06	.	.	.	.	.	.	.	01	.			
XI 7.2 7.3 6.3 6.9	071.5	J06.2	84 70 80 78 27	091 016.5	23	.	01	05	.	.	06	.	02	11	17	13	04	17	02	01	.	01	.	.	.	05	.		
XII 8.5 7.6 7.2 7.8	055.7	J03.6	85 80 81 82 43	078 014.8	02	.	17	22	.	.	11	02	04	19	15	11	03	09	09	.	01	.	.	.	05	16			
GOD. 5.8 6.2 5.1 5.7	2070.9	J07.6	76 57 70 67 23	678 037.2	45.8	.	21	50	84	15	05	122	20	79	115	139	104	22	130	21	06	.	03	01	27	28	26		
<b>GLAĐANOS</b>																													
BR. ST. 157																													
I 8.1 6.9 6.4 7.3	-	-	-	-	-	040	013.8	16	01	01	21	.	.	02	.	12	11	08	01	08	05	.	.	.	.	07	07		
II 8.2 6.7 6.8 7.3	-	06.1	91 79 89 86 56	114 042.1	15	.	01	05	.	.	04	.	05	10	17	15	02	15	03	01	.	.	01	06	03				
III 5.9 5.5 5.1 5.5	-	06.4	84 60 78 74 32	065 016.5	04	.	03	02	.	.	02	.	08	09	14	09	01	11	04	.	.	01	03	.	.	03	.		
IV 6.0 7.2 5.5 6.2	-	-	-	-	089 050.2	16	.	01	01	.	03	01	04	11	12	09	03	12	.	.	.	.	.	.	01	03	.		
V 5.5 6.3 6.4 6.0	-	10.4	80 63 76 72 43	053 013.5	16	.	.	10	.	01	10	11	08	01	11	.	.	.	.	.	.	.	.	02	.				
VI 4.2 6.2 6.9 5.7	-	-	-	-	021 005.0	26	.	.	19	06	01	.	.	03	06	11	09	01	11	04	.	.	.	.	04	.	.		
VII 4.3 4.7 5.0 4.7	-	12.8	79 54 77 70 34	060 011.0	16	.	.	23	08	.	01	.	07	05	16	16	02	16	.	.	.	.	.	.	03	.			
VIII 4.1 4.3 4.2 4.2	-	-	-	-	096 032.5	24	.	.	23	04	.	.	09	03	09	08	04	09	.	.	.	.	.	.	03	.			
IX 5.1 5.5 5.8 5.5	-	09.8	93 74 90 86	060 017.6	18	.	.	11	.	01	.	05	10	09	06	03	05	.	.	.	.	.	.	01	.				
X 4.9 4.2 3.3 4.1	-	-	-	-	026 016.0	03	.	02	.	.	08	04	06	02	01	06	.	.	.	.	.	.	.	11	.				
XI 7.6 7.5 7.2 7.4	-	-	-	-	085 015.0	17	.	01	08	.	02	.	01	17	17	15	04	17	02	02	.	.	.	04	.	.			
XII 8.3 7.9 8.0 8.1	-	-	-	-	074 018.0	01	03	28	.	.	04	.	04	23	14	12	03	10	09	03	.	.	.	.	17				
GOD. 6.0 6.1 5.9 6.0	-	-	-	-	783 050.2	46.8	04	67	-	01	-	-	53	120	147	117	25	135	23	06	.	.	01	-	-	27			
<b>BEČEJ</b>																													
BR. ST. 158																													
I 7.3 7.3 6.5 7.1	047.8	J04.2	85 67 91 78 21	022 080.3	16	.	01	14	.	.	.	.	14	04	-	-	12	08	.	08	05	.	.	01	.	07	04		
II 7.7 8.2 5.6 6.7	085.6	J05.5	87 64 78 36	048 024.9	15	.	01	06	.	.	08	02	02	10	16	12	02	15	02	.	.	.	.	01	.	01	02		
III 5.6 5.4 2.5 4.5	197.8	J05.4	82 63 68 47	040 010.8	31	.	.	03	03	.	.	15	09	07	07	12	02	11	02	01	.	.	.	01	.	.	01	.	
IV 5.5 6.7 3.9 5.4	202.6	J05.9	80 46 71 66 20	065 027.8	16	.	.	03	02	.	.	12	03	03	08	11	09	01	11	.	.	.	.	.	01	01	.		
V 4.5 6.5 3.7 4.9	250.7	J08.5	73 39 65 59 18	038 011.5	16	.	.	12	03	.	.	09	01	05	06	11	08	01	11	.	.	.	.	.	04	01	.		
VI 3.6 5.2 3.7 4.1	299.6	J10.3	73 39 68 61 22	034 006.7	15	.	.	21	07	.	.	10	01	09	07	10	06	01	10	.	.	.	.	.	07	01	.		
VII 4.6 5.2 2.8 4.0	288.9	J11.5	80 40 75 65 22	042 011.0	27	.	.	23	07	01	.	08	01	08	13	10	01	13	.	.	.	.	.	05	.	01			
VIII 4.1 4.0 3.0 4.0	252.9	J12.3	86 48 78 71 29	081 021.2	12	.	.	22	03	03	.	08	10	04	13	11	03	13	.	.	.	.	.	07	01	.			
IX 3.7 5.0 4.0 4.2	204.6	J08.1	84 42 75 67 23	033 015.6	18	.	.	11	01	.	05	.	11	05	06	04	02	06	.	.	.	.	02	.	02	.			
X 5.0 2.8 3.4 3.7	187.2	J07.1	90 45 78 21	017 009.4	03	.	01	02	.	.	03	.	04	15	06	06	06	06	.	.	.	.	.	10	.	10	.		
XI 7.4 7.2 5.9 6.8	061.8	J06.3	93 74 91 86 25	073 016.8	17	.	01	08	.	.	06	01	03	13	19	13	02	19	02	.	01	.	01	05	.				
XII 8.9 8.2 7.1 8.1	046.9	J03.6	91 83 88 87 43	041 008.7	03	03	16	23	.	.	07	01	20	13	10	09	06	.	.	.	.	.	06	11	.	11			
GOD. 5.6 5.9 4.3 5.3	2146.4	J07.4	83 52 76 71 17	564 027.8	46.8	03	19	59	96	21	01	103	13	-	-	142	104	14	132	17	01	.	01	02	28	33	17		
<b>SENTA</b>																													
BR. ST. 159																													
I 7.8 7.9 7.4 7.7	-	04.3	87 71 83 81 41	028 006.4	16	02	01	16	.	.	.	.	01	16															

Mesec	Vazdušni pritisak Pn mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nD, Fm (0-12)																						
		Tm				Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C					
		7	14	21	Sred. (Diss.)						8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.				
$\varphi = 45^{\circ}51' N \lambda = 20^{\circ}28' E$ Gr. AG = + 1h 21 min.											KIKINDA												BR. ST. 161									
I -	00.0	04.0	01.1	01.5	05.0	-01.8	14.3	30 -12.4	20.19	05	02.4	03	01.3	04	01.2	26	02.8	35	03.7	09	02.2	03	02.7	06	02.8	02	02.2	13	02.8	03		
II -	03.5	08.7	05.6	05.6	09.8	02.4	18.5	22 -05.7	04	12	02.6	07	02.1	03	02.3	23	02.8	05	02.5	15	03.1	10	02.2	13	02.8	03	02.2	13	02.8	03		
III 757.5	04.9	14.2	08.8	09.2	15.1	03.6	28.3	24 -05.5	01	08	02.6	06	02.8	02	01.5	10	02.4	33	03.2	14	02.4	02	02.9	18	03.1	02	02.2	13	03.1	02		
IV 752.6	06.8	14.1	09.0	09.7	15.2	04.3	25.7	29 -01.0	21	14	03.6	18	02.8	03	01.3	04	03.0	17	03.2	12	02.5	05	02.4	14	03.0	03	02.5	14	03.0	03		
V 754.1	14.3	21.7	15.8	16.9	22.7	10.7	30.4	21 04.6	27	19	02.0	10	02.5	02	02.0	07	02.9	24	03.3	04	01.2	11	01.9	04	02.2	12	01.9	12	02.2	12		
VI 751.9	17.7	25.0	18.7	20.0	26.2	13.1	33.0	14 04.0	02	16	02.6	13	02.3	04	01.0	32	02.5	09	01.8	08	02.1	14	02.4	10	02.2	14	02.4	10				
VII 752.0	17.9	25.7	19.7	20.7	27.1	14.3	32.6	31 11.2	28.24	16	02.5	05	01.6	04	02.5	03	01.7	12	02.2	04	02.8	13	02.1	21	02.0	15	02.1	21	02.0	15		
VIII 752.4	16.5	24.6	19.0	19.8	25.8	14.4	30.7	10 08.2	26	04.6	01.8	03.6	03	01.8	15	02.3	20	02.2	11	02.5	13	01.8	15	02.3	13	01.8	15	02.3	13			
IX 757.8	10.8	19.5	13.1	14.2	20.6	08.9	29.6	05 -00.9	28	11	02.7	17	01.6	02	01.5	07	02.0	11	02.3	02	01.5	14	01.6	07	01.9	19	01.6	07	01.9	19		
X 758.6	37.0	17.6	10.6	11.5	18.5	06.0	25.3	08 -00.5	18	05	01.8	02	01.5	07	01.8	07	02.1	09	01.5	04	01.8	08	02.0	09	01.5	30	01.5	30	01.5	30		
XI 752.9	04.1	09.6	05.7	06.1	09.9	03.0	21.0	12 -06.6	30	04	03.2	08	02.4	05	02.2	05	01.8	23	03.1	04	01.8	18	01.9	13	02.8	10	02.1	13	02.8	10		
XII 760.4	-03.2	-00.8	-02.4	-02.2	-01.9	-04.3	06.3	26 -14.0	06	24	02.4	05	02.4	02	01.0	12	02.4	22	02.9	06	01.7	10	02.1	02	04.0	14	02.1	02	04.0	14		
GOD. -	08.4	15.3	10.3	11.1	16.3	06.2	33.0	44.0 -14.0	06.0	138	02.5	103	02.2	34	01.7	91	02.4	257	02.9	92	02.3	119	02.1	125	02.8	139	02.1	125	02.8	139		
$\varphi = 45^{\circ}27' N \lambda = 20^{\circ}51' E$ Gr. AG = + 1h 22 min.											JASA TOMIC												BR. ST. 162									
I -	00.5	05.0	01.5	02.1	05.6	-01.5	15.0	30 -13.5	20	06	02.7	03	01.9	05	01.0	54	04.1	05	01.0	07	02.1	03	01.7	01	01.0	09	01.0	09	01.0	09	01.0	09
II -	04.3	09.5	05.6	06.2	10.2	02.9	18.0	23 -04.6	04	13	01.5	04	01.8	02	01.0	27	03.3	09	01.8	07	02.5	02	04.5	10	02.2	10	02.2	10	02.2	10	02.2	10
III 751.7	05.9	14.8	09.0	09.7	15.6	04.6	29.0	24 -06.0	01	05	01.8	02	01.5	07	01.1	42	02.7	07	01.1	03	01.3	08	01.9	13	03.2	13	03.2	13	03.2	13		
IV 752.1	07.1	15.0	10.6	11.3	16.1	04.9	26.0	29 -06.4	13.2	17	04.2	10	01.4	01	01.0	22	03.5	05	01.6	02	02.5	17	03.2	14	03.2	14	03.2	14				
V -	15.3	22.9	15.8	17.4	23.5	11.2	30.6	04 04.6	28	07	02.3	11	01.5	04	01.2	28	02.7	06	01.3	09	01.8	01	04.0	08	02.0	19	02.0	19				
VI -	18.8	26.8	18.4	20.6	27.6	13.8	34.2	14 03.6	34	04	11	02.5	03	01.3	07	01.2	18	01.2	04	01.2	18	01.8	04	02.0	19	02.6	22	02.6	22			
VII -	19.6	27.3	19.2	21.5	28.2	14.9	33.6	31 10.9	28	13	02.0	03	01.7	02	01.0	17	02.5	03	01.7	10	02.3	03	01.7	16	02.1	26	02.1	26				
VIII -	18.1	25.8	19.1	20.5	26.9	14.9	32.0	10 09.0	09.0	26	05	02.0	08	01.5	02	01.0	32	02.1	01	03.0	09	01.8	07	02.7	11	02.0	18	02.0	18			
IX -	11.7	20.6	13.6	14.8	21.2	09.6	31.0	05 00.2	30	19	01.9	14	01.6	02	01.5	15	01.6	01	01.0	12	01.6	03	01.3	04	02.0	20	01.6	04	02.0	20		
X -	07.9	17.9	11.6	11.8	18.5	06.8	26.2	08 01.3	18	04	01.2	07	01.4	02.5	01.5	34	02.6	08	01.0	11	01.5	04	01.8	04	01.2	19	01.2	19				
XI -	04.8	09.7	06.3	06.8	10.4	03.6	22.0	12 -05.3	30	07	01.3	11	01.8	07	01.4	16	01.9	08	01.1	19	01.6	02	03.5	18	01.6	09	01.6	09	01.6	09		
XII -	-03.0	-00.2	-02.2	-01.9	-00.3	-04.1	07.0	26 -14.5	05	16	01.6	13	01.4	07	01.4	31	02.4	05	01.4	06	01.5	05	03.0	05	01.4	12	01.4	12				
GOD. -	09.3	16.3	10.5	11.6	17.0	06.8	34.2	44.0 -14.5	05.0	123	02.2	89	01.5	20	01.1	336	02.8	62	01.3	113	01.7	44	02.4	117	02.3	191	02.3	191	02.3	191		
$\varphi = 45^{\circ}09' N \lambda = 21^{\circ}19' E$ Gr. AG = + 1h 25 min.											VR SAC												BR. ST. 163									
I 755.7	02.0	05.5	03.2	03.4	06.6	-00.4	16.2	30 -15.3	01	07	01.7	03	02.9	03	01.0	43	05.9	19	03.4	04	02.2	03	03.0	03	03.0	08	03.0	08	03.0	08	03.0	08
II 752.6	05.3	09.8	06.5	07.0	10.9	03.4	20.5	23 -06.4	05	02.0	07	02.3	02	01.5	17	05.2	21	03.4	02	02.0	09	02.6	11	02.4	10	02.4	10	02.4	10	02.4	10	
III 757.4	06.9	14.2	09.2	09.9	15.3	05.2	28.4	24 -07.9	01	08	01.9	09	01.6	07	02.9	05	05.5	21	02.8	07	01.9	08	02.4	07	02.7	04	02.7	04	02.7	04		
IV 752.1	08.1	14.2	09.9	10.5	15.3	05.4	24.4	30 -02.6	13	04	02.5	03	01.7	04	01.8	01	02.0	02	01.6	05	03.7	01	01.0	07	02.1	19	03.4	12				
V 753.9	15.6	21.4	16.0	17.2	22.4	11.6	29.4	21 02.9	25	11	02.4	06	02.3	06	02.3	24	04.5	21	02.8	05	01.6	09	02.3	03	02.3	08	02.3	08	02.3	08		
VI 758.0	17.8	24.8	18.1	19.7	26.2	12.3	32.4	14 00.8	04	01	02.2	10	01.9	05	02.2	04	02.5	19	02.8	09	01.5	13	02.3	10	02.4	10	02.4	10				
VII 751.9	19.0	25.3	19.3	20.7	26.7	14.0	32.3	31 09.1	13	01.1	10	02.1	05	01.5	11	04.5	14	02.9	09	01.5	12	02.1	09	02.1	14	02.1	14					
VIII 752.5	18.4	24.3	19.0	20.2	25.7	14.5	30.4	10 07.0	26	05	01.8	11	02.3	07	01.8	11	04.5	21	02.7	04	02.0	08	02.3	07	02.3	09	02.3	09				
IX 757.6	12.3	19.3	13.1	14.4	20.3	09.0	29.2	09 00.8	15	18	02.3	10	02.4	04	02.0</td																	

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha e <sub>m</sub> mm	Padavine R mm			Broj dana n s a:																												
								Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	R <sub>t</sub>	≡	•	△	*	Δ	▲	▲	T	≡				
	7	14	21	Sred. (Dnes)	7	14	21	Sred. (Dnes)	Min	Σ	Max	Dat.	10.00.0	0.0	25.0	0.020.0	6	8	2.0	8.0	0.1	1.00.0.0	•	△	*	Δ	▲	▲	T	≡						
KIKINDA																																				
BR. ST. 161																																				
I	7.2	7.4	6.8	7.1	072.6	04.6	87	74	86	82	39	038	010.2	16	03	02	20	•	•	•	08	•	02	14	12	09	01	09	04	•	•	•	01	06	09	
II	7.4	7.9	5.7	7.0	076.1	05.8	90	72	87	83	46	087	030.4	15	•	•	08	•	•	•	34	01	•	10	18	13	02	16	04	01	•	•	•	03	03	03
III	5.1	5.5	3.1	4.6	185.7	06.0	85	74	72	20	033	009.6	31	•	•	03	02	•	•	04	•	10	06	08	06	09	02	01	•	•	•	01	01	01		
IV	5.9	6.7	3.8	5.5	192.8	06.3	81	55	76	71	31	099	038.5	16	•	•	03	02	•	•	08	32	05	10	12	09	03	12	•	•	•	03	01	01		
V	5.1	6.0	4.5	5.2	232.9	09.2	74	46	70	63	27	030	009.1	16	•	•	11	02	•	•	04	•	04	05	10	06	08	10	•	•	•	06	•	•		
VI	3.2	5.0	4.4	4.2	300.6	11.0	74	44	68	62	28	060	013.2	27	•	•	22	05	•	•	01	•	04	02	10	09	02	10	•	•	•	09	•	•		
VII	4.6	5.0	3.9	4.5	286.0	12.0	70	49	71	62	33	054	019.0	27	•	•	23	07	•	•	03	08	13	09	02	13	•	•	•	09	•	•				
VIII	4.2	4.6	3.4	4.2	243.9	12.6	70	38	89	89	36	089	015.9	01	•	•	21	02	•	•	01	•	08	04	11	08	06	10	•	•	•	07	•	•		
IX	4.6	5.9	3.6	4.7	206.0	08.4	83	50	75	70	31	051	020.4	19	•	•	01	11	•	•	08	07	06	05	02	06	•	•	•	01	•	•				
X	4.7	5.1	2.5	3.4	189.8	07.6	91	55	62	62	32	013	005.4	03	•	•	01	02	•	•	13	04	05	05	03	05	•	•	•	01	10	•				
XI	6.9	7.5	5.6	6.7	351.8	06.6	94	80	92	89	46	095	021.5	17	•	•	01	08	•	•	01	•	03	11	17	13	03	15	02	•	•	01	10	•		
XII	6.9	7.4	6.8	7.7	036.5	03.6	91	86	89	89	62	037	006.9	03	03	17	25	•	•	02	•	03	18	12	09	07	01	•	•	01	01	08	20			
GOD.	5.6	6.1	4.5	5.4	2074.9	07.8	84	60	78	78	22	686	038.5	46.4	06	20	69	94	16	•	36	03	68	94	136	101	21	122	19	02	•	01	01	38	39	33
JASA TOMIC																																				
BR. ST. 162																																				
I	7.7	8.1	7.6	7.8	-	04.3	82	68	84	78	31	032	007.1	16	03	01	15	•	•	•	11	06	01	16	11	08	08	04	•	•	•	05	08	•		
II	6.0	8.4	7.3	8.2	-	06.1	89	72	87	83	48	088	022.7	15	•	01	05	•	•	03	01	•	15	17	14	03	16	03	•	•	01	01	04	03		
III	5.6	5.7	5.5	5.3	-	06.1	79	53	75	69	23	051	016.0	30	•	•	03	03	•	•	05	02	09	11	12	09	02	10	03	•	•	01	01	01	•	
IV	6.3	8.0	5.9	6.7	-	06.8	80	56	79	72	33	090	034.0	16	•	•	03	02	•	•	08	03	01	11	10	03	11	•	•	•	01	•	•			
V	5.8	8.1	6.6	6.8	-	10.8	79	56	78	71	34	042	028.2	08	•	•	14	01	•	•	03	01	02	16	09	06	01	09	•	•	•	04	02	•		
VI	4.6	7.3	5.0	5.6	-	11.6	73	42	74	63	29	016	006.3	23	•	•	23	11	•	•	04	06	05	03	05	05	•	•	•	08	•	•				
VII	4.5	6.5	4.4	5.1	-	13.1	76	49	78	68	32	050	013.4	01	•	•	26	08	•	•	03	06	12	07	02	12	•	•	•	07	01	•				
VIII	4.5	6.7	4.7	5.3	-	13.4	84	57	82	74	39	088	018.0	01	•	•	24	06	•	•	05	07	11	10	03	11	•	•	•	07	03	•				
IX	4.9	6.7	5.1	5.6	-	09.2	83	54	78	72	33	052	021.0	21	•	•	11	05	•	•	06	11	06	06	02	06	•	•	•	01	•	•				
X	5.6	4.8	4.8	5.1	-	07.9	87	58	85	76	33	025	011.0	03	•	•	03	03	•	•	03	01	09	11	06	06	01	06	•	•	•	07	•	•		
XI	6.7	7.9	7.6	7.6	-	06.7	92	79	80	82	05	085	020.0	17	•	•	06	•	•	•	05	01	02	17	13	04	15	01	01	06	•	•	06	•	•	
XII	9.2	7.9	7.3	8.1	-	03.6	87	86	89	87	64	066	017.8	03	03	15	23	•	•	01	•	01	21	14	10	02	10	05	•	•	•	07	18	•		
GOD.	6.0	7.2	6.0	6.4	-	08.3	82	60	81	74	23	685	034.0	46.4	06	17	55	106	31	•	-	-	43	148	129	102	23	119	16	01	•	•	01	28	34	30
VRSAC																																				
BR. ST. 163																																				
I	7.4	7.8	7.0	7.4	-	066.6	04.1	71	64	71	69	23	029	010.9	14	03	02	15	•	•	22	17	01	12	12	07	01	08	06	01	•	•	•	07	07	•
II	8.9	9.1	6.6	7.8	-	060.7	05.6	81	66	78	75	36	069	015.7	15	•	01	05	•	•	15	05	•	14	16	14	02	16	04	•	•	•	02	05	•	
III	5.5	5.9	3.6	5.0	-	185.7	06.2	84	99	76	70	23	057	020.1	30	•	•	06	02	•	•	20	15	10	13	05	02	11	03	•	•	01	05	02	•	
IV	6.2	6.7	5.4	6.5	-	154.8	06.4	75	56	72	68	32	108	031.1	16	•	•	02	•	•	•	16	08	02	14	11	04	11	•	•	•	01	01	01		
V	5.3	6.3	5.1	5.6	-	230.0	08.6	68	48	67	61	27	027	007.2	10	•	•	12	02	•	•	11	07	02	07	11	08	08	02	11	•	•	04	02	•	
VI	4.1	5.5	3.9	4.5	-	274.4	10.7	74	46	69	62	28	082	039.6	23	•	•	22	08	•	•	03	01	08	08	12	07	12	•	•	•	12	•	•		
VII	4.2	5.9	4.2	4.4	-	275.6	12.7	76	53	79	69	37	105	046.6	02	•	•	23	04	•	•	08	02	06	04	12	11	06	15	01	01	02	02	•	•	
VIII	4.6	5.5	4.1																																	

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Meseč	Vrednost pritisaka Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (O-12)															
		Tm			Sred. (Dnev)	MAX	MIN	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21							8.	J.	E.	J.	E.	J.	8.	J.	E.	J.	8.	J.	E.	J.			
$\varphi = 44^{\circ}58' N \lambda = 19^{\circ}38' E$ Gr. $\Delta G = +1h\ 18\ min.$																											
I	-	00.3	05.1	01.7	02.2	06.0	-01.2	15.8	30 -10.0	01	04	02.2	02	01.5	52	02.2	29	02.9	03	01.3	14	01.9	08	02.0	01		
II	-	03.8	10.1	05.7	06.4	11.7	02.0	21.2	23 -08.0	04	06	02.0	03	01.7	08	01.8	03	01.3	05	02.0	16	02.1	14	02.8	12		
III	-	05.4	15.4	08.7	09.5	16.4	03.8	28.9	24 -04.0	01	03	03.0	02	02.0	34	01.8	12	02.0	01	01.0	03	02.0	08	01.8	22	03.0	08
IV	-	07.4	15.2	09.3	10.3	16.6	04.6	27.3	29 -01.1	18	05	01.8	09	01.9	21	02.1	05	01.4	02	01.5	07	01.6	14	01.6	23	03.6	04
V	-	14.5	21.7	15.6	16.8	22.9	11.0	29.8	20 05.6	29	07	02.1	05	02.2	24	02.0	16	01.9	02	01.5	07	01.4	19	01.8	07	02.1	06
VI	-	17.2	24.7	17.7	19.3	26.0	12.5	32.8	14 03.0	04	05	01.4	09	01.8	09	01.4	03	02.0	03	01.3	16	01.6	27	01.0	16	02.4	05
VII	-	18.1	26.1	18.8	20.4	27.2	14.3	34.3	31 10.0	28	04	02.0	02	14	02.0	10	01.6	05	01.3	08	01.5	29	02.2	18	02.3	09	
VIII	-	17.0	25.5	18.5	19.6	26.7	14.3	31.2	10 08.0	26	05	01.6	03	01.0	27	01.9	12	01.8	04	01.0	05	01.2	21	02.1	07	02.7	09
IX	-	11.4	19.7	12.8	14.2	20.8	09.2	29.6	09 -09.7	30	05	02.0	06	01.5	19	02.0	07	02.4	01	02.0	09	01.6	19	01.9	09	02.8	15
X	-	07.3	18.2	10.2	11.5	19.1	06.0	25.8	01 00.7	18	01	03.0	05	01.6	33	01.9	04	01.8	03	01.3	07	01.1	17	01.5	05	01.8	18
XI	-	04.3	09.9	05.8	06.4	11.2	02.6	23.2	12 -04.8	30	03	01.3	08	02.0	27	01.6	06	01.5	06	01.2	03	01.3	19	02.5	07	01.9	11
XII	-	-02.5	00.5	-01.6	-01.3	01.3	-03.8	07.5	26 -13.4	06	02	02.0	10	01.4	33	02.6	05	01.0	01	01.4	02	01.0	19	01.7	16	01.9	05
GOD.	-	08.7	16.0	10.3	11.1	17.2	06.3	34.3	34.VI -13.4	06.XI	50	01.9	59	01.7	313	02.0	94	01.9	29	01.3	73	01.5	222	01.9	152	02.3	103
$\varphi = 44^{\circ}46' N \lambda = 19^{\circ}41' E$ Gr. $\Delta G = +1h\ 19\ min.$																											
I	-	00.9	05.9	02.5	03.0	06.5	-00.6	16.5	12 -08.5	20.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	04.8	10.0	05.9	06.9	11.8	02.0	21.8	23 -04.3	04	03	01.3	01	01.6	08	01.6	02	02.0	04	03.0	03	02.3	14	02.2	44		
III	-	02.3	15.6	09.3	09.9	16.4	04.1	20.4	24 -04.2	01	01	01.0	07	01.7	01.8	01.8	01.0	01.3	02	01.5	04	02.5	22	02.0	39		
IV	-	08.8	15.5	09.4	10.3	16.6	04.8	27.7	29 -01.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	14.3	22.6	15.9	17.2	23.5	11.4	31.2	20 06.0	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	16.8	25.3	18.2	19.6	26.3	13.1	33.2	14 04.5	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	17.6	26.0	19.4	20.6	27.0	14.8	34.2	31 11.2	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	16.4	26.1	18.8	20.0	26.9	14.6	31.4	28 08.5	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	10.6	20.0	13.1	14.2	20.8	09.1	30.5	09 -00.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	07.3	18.2	10.5	11.6	18.9	06.5	26.2	01 00.0	18	01	00.0	08	01.0	02.0	01.0	02.0	02	02.0	04	02.0	22	02.0	65			
XI	-	04.4	10.3	06.4	06.8	11.3	03.1	23.8	12 -04.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-02.2	01.2	-00.8	-00.6	01.9	-03.4	09.0	27 -16.0	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	08.6	16.4	10.7	11.6	17.3	06.7	34.2	34.VI -16.0	06.XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 44^{\circ}37' N \lambda = 19^{\circ}47' E$ Gr. $\Delta G = +1h\ 14\ min.$																											
I	-	00.9	05.9	02.6	03.0	06.8	-00.9	16.5	12 -10.0	20	02	01.0	03	02.0	20	02.8	14	02.3	02	02.5	01	01.4	37	01.8	64		
II	-	04.9	10.6	06.5	07.4	12.3	02.9	22.5	23 -06.0	04	03	01.3	01	01.6	08	01.6	02	02.0	04	03.0	03	02.3	14	02.2	44		
III	-	06.0	14.8	09.1	09.7	16.0	04.3	27.5	23 -04.5	01	01	01.0	07	01.7	01.8	01.8	01.0	01.3	02	01.5	04	02.5	22	02.0	39		
IV	-	07.4	14.9	09.0	10.4	16.1	04.5	27.5	29 -01.5	21	01	01.0	06	01.6	05	02.8	01.0	02.0	02	01.7	07	01.7	22	02.7	42		
V	-	15.1	21.8	15.6	17.0	22.7	10.9	29.5	04 05.5	29	04	01.5	02	01.5	04	01.8	39	02.0	01	01.8	01	01.8	64	01.8	64		
VI	-	17.5	24.8	19.0	19.6	26.1	12.5	32.0	14 03.5	04	04	01.0	02	01.0	02	01.5	01	02.0	02	02.0	04	02.1	65	02.0	65		
VII	-	16.9	26.2	19.3	21.1	27.2	14.4	34.0	31 10.5	28	02	01.5	01	01.0	03.0	01.0	02.0	01	01.0	03.0	01	03.0	09	02.4	73		
VIII	-	17.2	25.7	18.9	20.2	26.5	14.4	31.5	28 10.0	26	01	01.6	03	01.6	01.6	01.6	01.6	01.6	01	03.0	01	03.0	09	02.4	73		
IX	-	11.4	19.4	12.6	14.0	20.4	09.0	30.5	13.09 -01.0	30	06	01.2	02	01.5	04	01.8	39	02.0	01	01.8	01	01.8	60	01.8	60		
X	-	07.9	18.1	10.5	11.8	18.9	06.5	26.0	01 00.0	18	05	01.0	02	01.0	02	01.8	02	01.0	03	01.0	04	01.0	08	01.8	62		
XI	-	04.6	10.6	06.4	07.0	11.7	02.8	24.5	21 02.0	05	01	01.2	10	01.2	03	01.3	04	01.8	01	01.0	05	01.0	14	02.3	53		
XII	-	-02.2	01.0	-01.2	-00.9	02.0	-03.6	11.5	28 -15.0	06	01	01.0	13	01.5	04	01.5	04	01.0	01	03.0	07	01.7	23	02.2	41		
GOD.	-	09.2	16.2	10.6	11.1	17.6	05.5	35.2	34.VI -15.0	06.XI	34	01.9	42	02.0	60	01.8	12	02.8	20	02.5	13	02.8	101	01.9	39	02.6	774
$\varphi = 44^{\circ}17' N \lambda = 19^{\circ}55' E$ Gr. $\Delta G = +1h\ 18\ min.$																											
I	747.2	-00.6	06.3	02.1	02.4	07.8	-02.4	18.0	29 -14.6	19	01	02.0	*	06	01.3	04	02.8	02	03.0	*	04	01.2	03	01.0	73		
II	747.4	04.5	11.0	05.9	06.8	13.0	01.5	23.7	23 -04.6	05	*	05	*	04	02.0	02	01.0	*	07	03.0	07	02.7	13	02.2	02	02.5	49
III	749.5	04.6	15.3	07.9	09.0	16.9	02.2	28.8	23 -04.6	01	01	03.0	04	01.8	07	02.4	02	02.5	02	03.0	14	02.8	05	03.7	58		
IV	744.5	07.0	14.9	08.9	09.9	16.3	03.5	29.5	29 -00.8	21.18	01	03.0	06	02.0	05	02.2	03	03.0	01	04.0	01	03.0	17	02.1			

Mesec	Oblačnost Nm (0-10)	Sred. (Gles)	Broj sati Insolacija	Vlažnost vazduha				Padavine R mm		Broj dana na sat																							
								Tn	Tx	Tn	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	R <sub>t</sub>											
	7	14	21	mm	7	14	21	Sred. (Dob.)	Min	M	Max	Dat.	10.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.0	0.0	1.0										
SRMSKA MITROVIC																																	
BR <sub>s</sub> ST. 166																																	
I 7.4 8.2 6.1 7.2	-	04.6 87 73 86 82 33	041 012.2	13	01	02	20	.	.	.	04	01	14	09	06	02	08	03	.	01	01	01	08	04									
II 3.9 7.0 5.9 7.1	-	05.9 91 67 86 81 39	101 024.9	15	01	06	.	.	.	04	02	01	09	17	15	03	16	02	.	.	01	01	06	04									
III 5.2 5.2 5.4 4.7	-	06.3 88 48 78 72 23	052 012.1	04	.	05	03	.	.	05	01	07	08	02	08	03	11	02	01	.	01	02	01										
IV 6.7 7.1 5.7 6.5	-	06.6 84 51 77 70 27	054 025.2	16	.	02	03	.	.	07	03	02	11	11	07	02	11	.	.	.	.	03	01										
V 4.9 6.3 6.5 5.9	-	10.0 82 51 77 70 29	052 012.8	06	.	01	10	.	.	.	02	09	13	09	01	13	.	.	.	.	10	01											
VI 3.9 5.4 4.2 4.5	-	11.8 80 48 79 69 27	066 021.7	17	.	01	18	07	.	01	01	08	05	12	07	02	12	.	.	.	.	09	01										
VII 4.1 4.9 3.7 4.2	-	13.1 85 51 83 73 32	062 023.7	23	.	01	23	08	.	02	01	09	04	12	07	02	12	.	.	.	.	09	01										
VIII 4.2 4.8 3.8 4.3	-	13.5 90 55 88 78 40	099 039.4	12	.	01	24	04	.	05	02	10	05	12	09	04	12	.	.	.	.	08	.										
IX 4.9 5.5 4.4 5.0	-	09.4 90 55 86 77 33	054 017.6	18	.	01	11	.	.	01	01	07	09	11	08	01	11	.	.	.	.	04	01										
X 5.8 4.3 2.6 4.2	-	08.1 94 56 89 80 28	018 015.7	03	.	01	02	.	.	01	01	11	07	04	02	01	04	.	.	.	.	10	.										
XI 6.9 7.9 5.6 6.7	-	06.6 94 76 92 87 39	091 015.3	26	.	01	10	.	.	01	02	11	17	12	04	15	03	03	.	.	.	.	09	.									
XII 8.1 7.5 7.1 7.6	-	03.8 91 83 90 88 57	080 013.4	01	02	16	26	.	.	03	04	21	13	11	03	09	07	02	.	01	.	.	05	16									
GOD.	5.9 6.2 4.9 5.7	-	08.3 88 59 84 77 23	770 039.4	42.VW	03	19	70	94	19	.	34	12	63	113	143	101	28	134	17	06	01	02	01	46	24							
SABAC																																	
BR <sub>s</sub> ST. 167																																	
I 7.6 6.4 6.5 6.9	-	-	-	-	-	-	-	-	-	-	044 012.0	16	02	18	.	.	01	01	14	10	09	01	08	04	02	.	04	05					
II -	-	-	-	-	-	-	-	-	-	-	106 034.3	15	01	08	.	.	02	02	-	-	16	14	02	15	03	.	01	01	05				
III 4.1 3.8 2.5 3.5	-	-	-	-	-	-	-	-	-	-	048 011.3	04	01	05	03	.	.	16	06	10	07	02	10	01	.	.	02	.					
IV 5.8 5.0 4.6 5.2	-	-	-	-	-	-	-	-	-	-	077 036.8	16	01	04	03	.	.	09	08	13	08	02	13	.	.	02	01	.					
V 3.6 4.6 5.5 4.5	-	-	-	-	-	-	-	-	-	-	044 015.2	07	.	01	12	02	.	.	10	05	10	08	01	10	.	.	.	05	.				
VI 2.9 4.2 4.9 4.0	-	-	-	-	-	-	-	-	-	-	098 021.7	17	.	01	20	08	.	.	12	05	11	10	06	11	.	.	.	02	.				
VII 3.5 3.4 3.4 3.4	-	-	-	-	-	-	-	-	-	-	112 035.0	06	.	01	23	08	.	.	12	04	12	09	04	12	.	.	.	06	.				
VIII 2.7 3.6 3.6 3.3	-	-	-	-	-	-	-	-	-	-	073 037.0	01	.	01	25	05	.	.	16	05	10	09	02	10	.	.	.	04	01				
IX 4.8 3.8 4.2 4.3	-	-	-	-	-	-	-	-	-	-	081 023.2	21	.	01	11	01	.	.	13	07	10	09	04	10	.	.	.	01	.				
X 5.2 3.4 2.7 3.8	-	-	-	-	-	-	-	-	-	-	018 014.3	03	.	01	05	.	.	14	07	02	01	02	01	.	.	.	.	08	.				
XI 7.2 6.8 6.1 6.7	-	-	-	-	-	-	-	-	-	-	088 018.9	24	.	01	08	.	.	02	12	11	11	04	11	01	01	.	.	05	.				
XII 7.6 7.0 6.7 7.1	-	-	-	-	-	-	-	-	-	-	090 017.2	30	02	11	24	.	.	07	20	11	11	05	08	06	01	.	.	01	16				
GOD.	-	-	-	-	-	-	-	-	-	-	879 037.0	46.VW	02	13	68	102	24	.	03	02	-	-	126	106	34	120	15	04	.	.	.	20	24
VLADIMIRCI																																	
BR <sub>s</sub> ST. 168																																	
I 7.8 7.9 7.5 7.7	-	04.9 88 78 85 84 40	040 015.4	16	01	01	15	.	.	.	03	01	02	14	14	09	01	07	03	01	.	.	05	05									
II 7.7 7.2 6.2 7.1	-	06.4 88 74 85 82 36	127 028.0	15	01	07	.	.	.	01	13	12	12	05	11	03	.	.	.	.	01	02	06										
III 5.1 5.1 3.4 4.5	-	06.9 84 61 79 75 37	047 014.2	14	.	01	04	03	.	01	13	06	09	08	02	09	.	.	.	.	03	04	.										
IV 6.4 6.8 5.2 6.1	-	06.8 79 58 79 72 31	090 041.3	16	.	02	02	.	.	02	05	12	12	09	03	12	.	.	.	.	03	04	.										
V 5.4 6.0 5.5 5.6	-	10.8 82 59 79 73 40	039 009.5	07	.	01	12	.	.	06	08	10	10	09	10	08	01	10	.	.	.	02	.										
VI 3.5 5.5 4.9 4.7	-	-	-	-	-	-	-	-	-	-	047 012.4	23	.	01	19	08	.	07	06	11	07	02	11	.	.	.	03	.					
VII 4.4 4.5 4.9 4.5	-	-	-	-	-	-	-	-	-	-	115 037.3	23	.	01	24	09	.	08	07	13	10	04	13	.	.	.	05	02					
VIII 3.3 3.3 3.5 3.7	-	13.8 87 60 83 77 47	107 033.2	01	.	01	24	04	.	01	14	05	08	07	04	08	.	.	.	.	04	01	.										
IX 5.0 4.8 4.2 4.6	-	09.6 90 59 87 79 36	116 039.4	21	.	01	11	02	.	01	01	12	09	10	10	10	04	10	.	.	.	02	03										
X 5.6 3.9 4.0 4.5	-	08.4 93 61 88 81 34	026 019.8	03	.	01	04	.	.	01	12	08	04	02	01	04	.	.	.	.	11	.											
XI 6.4 6.6 5.9 6.4	-	08.6 80 53 89 85 35	093 028.1	17	02	08	.	.	.	04	09	12	08	04	12	02	01	01	01	.	.	07	01										
XII 8.1 7.2 7.1 7.5	-	-	-	-	-	-	-	-	-	-	084 022.0	30	01	11	23	.	.	05	20	12	11	04	07	07	01	.	.	12	16				
GOD.	5.7 5.8 5.2 5.6	-	-	-	-	-	-	-	-	-	931 041.3	46.W	02	12	60	99	23	.	-	-	87	118	121	100	34	114	15	03	.	.	20	47	
VALJEVO																																	
BR <sub>s</sub> ST. 169																																	
I 6.9 7.7 6.6 7.2	085.4	04.5 89 65 85 80 31	052 013.3	16	02	01	22	.	.	03	01	02	14	14	11	01	12	07	04	.	.	.	05	07									
II 7.9 7.5 6.7 7.0	097.6	05.4 85 88 81 75	120 030.8	15	01	05	.	.	.	03	01	01	11	15	11	03	14	04	.	.	.	02	04										
III 5.2 6.0 3.4 4.9	179.8	05.9 85 74 87 45	038 010.4	04	.	01	09	03	.	01	01	08	10	07	01	10	.	.	.	.	.	.	.										
IV 6.8 7.4 5.8 6.7	172.4	06.4 86 52 78 71	30 019.8	16	.	06	03	.	.	05	04	12	13	09	02	13	02	02	.	.	.	02	01										
V 6.0 7.6 6.2 6.6	201.8	10.1 86 54 72 39	084 018.9	07	.	01	10	01	.	02	01	11	13	12	02	13	.	.	.	.	09	.											
VI 4.1 5.9 5.3 5.1	248.5	11.8 80 50 65 32	066 019.9	23	.	01	17	05	.	02	01	07	08	03	12	08	03	17	.	.	.	10	.										
VII 4.7 5.3 4.4 4.8	262.0	13.3 84 55																															

Mesec	Vazdušni Prstenski Fm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																				
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C					
		7	14	21							8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.						
$\varphi = 44^{\circ}02' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = +1 h 22 min.$																																
GORNJI MILANOVAC																																
I	-	-02.2	04.8	00.2	00.7	05.9	-04.0	14.7	30	-16.5	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
II	-	03.0	09.7	04.5	05.4	11.3	00.3	22.4	23	-07.8	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
III	-	02.5	13.8	06.6	07.4	15.1	00.9	28.2	24	-05.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
IV	-	04.9	13.7	07.3	08.3	15.5	02.0	26.5	29	-04.5	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
V	-	11.7	20.4	13.4	14.7	21.7	08.9	28.4	04	01.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VI	-	14.7	23.5	15.0	17.1	25.2	10.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
$\varphi = 44^{\circ}08' N \lambda = 20^{\circ}31' E$ Gr. $\Delta G = +1 h 21 min.$																																
RUDNIK																																
I	-	02.0	03.9	02.7	02.8	05.3	-00.5	11.4	30	-09.3	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
II	-	03.9	06.5	04.6	04.8	08.5	01.3	18.6	23	-07.2	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
III	-	06.5	10.9	07.9	08.3	12.5	04.6	25.0	23	-08.6	01	-	-	-	-	-	-	-	-	-	-	-	-	-								
IV	-	05.9	10.2	07.5	07.8	12.7	03.6	24.5	30.29	-03.5	12	-	-	-	-	-	-	-	-	-	-	-	-	-								
V	-	12.3	18.0	13.2	14.2	19.2	10.1	27.3	20	03.6	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VI	-	15.0	20.5	17.2	16.5	22.3	12.8	30.0	14	05.5	02.01	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VII	-	15.9	20.8	17.6	17.8	22.7	14.0	30.6	31	10.2	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VIII	-	16.2	21.0	17.4	17.9	23.2	14.0	28.2	10	08.1	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
IX	-	10.0	15.0	11.3	11.9	16.3	08.5	26.3	09	01.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
X	-	09.9	13.6	11.4	15.2	19.4	11.7	21.0	01.3	01.3	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
XI	-	05.4	07.9	05.7	06.2	09.8	02.7	16.5	12	-0.5	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
XII	-	-03.6	-01.9	-02.6	-02.7	-00.7	-03.7	09.4	25	-11.9	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
GOD.	-	08.3	12.2	09.2	09.7	14.0	06.1	30.6	34.VI	-11.9	23.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
$\varphi = 44^{\circ}18' N \lambda = 20^{\circ}33' E$ Gr. $\Delta G = +1 h 22 min.$																																
BUKOVICKA BANJA																																
I	-	00.2	05.5	01.8	02.3	06.3	-01.6	15.3	30	-13.4	19	01	02.0	.	.	30	01.6	23	01.6	12	01.9	02	01.5	12	02.3	06						
II	-	04.7	10.1	06.1	06.7	11.5	02.4	22.0	23	-09.3	05	01	02.1	02	01.0	03	01.3	11	02.0	05	02.0	07	01.9	25	02.5	10						
III	-	05.1	13.8	07.5	08.5	15.0	03.4	27.7	24	-04.5	01	01	01.0	02	02.0	18	01.3	11	01.7	04	01.0	05	01.4	25	02.7	10						
IV	-	06.9	13.8	08.2	08.2	09.3	15.1	26.5	29	-00.5	21.12	01	01.0	02	01.3	03	01.3	13	01.1	05	01.2	06	01.7	17	02.5	20						
V	-	14.2	21.3	14.8	16.3	22.1	10.5	29.2	04	05.0	29	01	02	01.0	02	12	01.1	12	01.4	05	01.4	06	01.5	24	01.5	12	01.8					
VI	-	17.2	23.8	17.1	18.8	25.1	12.6	32.3	16	04.0	04	02	01.5	03	01.0	03	01.0	03	01.0	03	01.5	36	01.8	10	01.8	23						
VII	-	18.2	25.4	19.7	20.2	26.1	14.3	34.0	31	10.0	28	01	01.0	08	01.0	08	01.0	03	01.0	07	02.0	35	01.8	10	02.7	24						
VIII	-	16.8	25.0	18.0	19.4	26.2	14.1	31.2	16	08.5	26	02	01.5	04	01.0	14	01.2	06	01.0	04	01.5	18	02.2	10	02.0	31						
IX	-	11.0	18.7	12.0	13.4	19.8	08.9	30.8	09	-01.5	30.29	01	01.0	07	01.2	07	01.1	01	01.0	01	01.0	14	02.1	28	02.3	27						
X	-	07.5	17.0	09.2	10.7	17.8	05.8	24.6	08	-01.0	19	03	01.0	01	01.0	01	01.0	13	01.3	01	01.0	13	01.3	11	01.9	26						
XI	-	04.9	10.5	06.2	06.9	12.0	02.6	23.0	12	-04.0	30.20	04	01.0	02	02.5	05	01.2	11	01.5	03	02.0	30	02.4	20	01.6	09						
XII	-	-02.1	00.2	-02.0	-01.5	01.5	-04.3	11.3	28	-11.4	06	01	03	01.7	02	12	01.4	03	01.7	04	02.0	23	J3.0	15	03.2	21						
GOD.	-	08.7	15.4	09.8	10.9	16.5	06.1	34.0	34.VII	-13.4	49.1	13	01.2	22	01.4	141	01.3	126	01.4	72	01.5	54	01.8	262	02.1	151	02.3	254				
$\varphi = 44^{\circ}53' N \lambda = 20^{\circ}40' E$ Gr. $\Delta G = +1 h 22 min.$																																
PANCEVO																																
I	-	00.0	04.6	00.9	01.6	05.6	-01.1	16.2	30	-13.1	19	03	01.7	.	.	22	03.1	21	03.2	01	02.0	.	01	01.0	03	02.0	42					
II	-	04.2	10.1	05.9	06.5	11.4	02.2	22.4	23	-04.5	06.05	09	02.1	02	01.0	03	01.3	11	02.0	05	02.0	.	10	01.9	03	02.3	41					
III	-	05.3	14.1	08.8	09.3	15.3	03.8	28.1	24	-04.0	01	05	01.4	.	11	02.6	19	02.6	02	03.0	02	01.0	15	01.7	05	01.8	36					
IV	-	07.4	14.8	09.3	10.2	15.7	04.5	28.1	29	00.1	12	07	01.9	01	01.0	08	02.2	13	02.8	03	01.7	.	21									

Mesec	Oblačnost Nm (0-10) Sred. (Dies.)	Vlažnost vazduha mm	Padavine R mm	Broj dana na mesečnoj F(0-12) Nm(0-10) R mm																													
				Unite				Padavine				Broj dana na mesečnoj																					
				7	14	21	Sred. (Dies.)	7	14	21	Sred. (Dies.)	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	*	•	Δ	○	▲	■	□				
<b>BR. ST. 171 GORNJI MILANOVAC</b>												$H_s = 335 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																					
I	7.8 6.8 6.1 6.9	-	-	-	-	-	-	052	011.2	27	33	03	26	*	*	*	01	09	14	19	01	07	10	*	*	*	02	10					
II	6.9 6.4 6.4 7.0	-	-	-	-	-	-	076	018.9	15	*	01	12	*	*	*	01	12	12	13	03	10	34	02	*	*	*	01	03				
III	4.9 5.4 3.6 6.6	-	-	-	-	-	-	053	015.6	04	*	13	02	*	*	*	13	07	14	12	01	12	02	*	*	*	*	01	02				
IV	7.0 6.6 4.7 6.1	-	-	-	-	-	-	084	029.0	16	*	09	02	*	*	*	05	11	13	11	02	13	02	*	*	*	*	*	*				
V	6.9 6.1 5.5 6.7	-	-	-	-	-	-	086	020.8	08	*	*	09	*	*	*	*	04	10	14	13	03	14	*	*	*	*	01	03				
VI	4.3 5.8 4.8 5.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	*	*	*	*						
<b>BR. ST. 172 RUDNIK</b>												$H_s = 700 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																					
I	6.7 6.3 6.1 6.4	-	-	-	-	-	-	073	026.8	18	*	03	15	*	*	*	03	11	13	10	01	06	09	*	*	*	*	07	18				
II	6.9 6.2 4.9 6.0	-	-	-	-	-	-	101	024.1	15	*	04	13	*	*	*	02	09	14	11	04	12	06	03	01	*	*	*	*	09	12		
III	5.4 5.5 3.0 4.6	-	-	-	-	-	-	095	041.8	04	*	02	05	01	*	*	12	09	15	10	03	12	04	*	*	*	*	*	*	09	04		
IV	6.5 6.7 4.7 6.3	-	-	-	-	-	-	131	045.6	16	*	10	*	*	*	05	11	18	12	03	11	11	*	*	*	*	*	*	02	09	10		
V	5.7 5.8 5.2 5.6	-	-	-	-	-	-	082	015.8	08	*	*	04	*	*	*	05	06	16	12	02	16	*	*	*	*	*	*	01	03	*		
VI	3.9 4.9 4.0 4.6	-	-	-	-	-	-	085	024.1	25	*	*	10	01	*	*	06	05	14	09	03	14	03	*	*	*	*	*	*	06	02	*	
VII	4.5 5.5 3.1 4.4	-	-	-	-	-	-	122	022.3	11	*	*	10	01	01	*	08	03	15	14	05	15	*	*	*	*	*	*	05	07	*		
VIII	4.2 5.4 3.7 4.1	-	-	-	-	-	-	111	052.3	15	*	*	10	*	*	*	09	04	11	09	04	11	*	*	*	*	*	*	*	*	02	*	
IX	5.7 5.8 4.0 4.0	-	-	-	-	-	-	085	031.2	21	*	*	01	*	*	*	07	08	14	12	02	14	*	*	*	*	*	*	*	*	10	*	
X	3.9 4.3 2.4 3.6	-	-	-	-	-	-	024	014.1	03	*	*	02	*	*	*	14	04	05	03	01	05	*	*	*	*	*	*	*	*	*	08	*
XI	6.0 6.9 4.9 5.0	-	-	-	-	-	-	077	024.7	17	*	32	12	*	*	*	04	09	17	10	03	10	08	*	*	*	*	*	*	07	05	*	
XII	7.7 7.0 7.1 7.3	-	-	-	-	-	-	085	025.0	30	07	17	27	*	*	*	04	21	18	11	03	07	14	01	*	*	*	*	*	*	07	19	*
GOD.	5.5 5.9 4.4 5.3	-	-	-	-	-	-	1071	052.3	45.V	07	28	82	36	02	01	-	-	80	102	170	123	34	133	52	04	01	-	80	68			
<b>BR. ST. 173 BUKOVIČKA BANJA</b>												$H_s = 265 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$																					
I	5.8 5.0 6.1 5.6	-	04.5	84	67	82	78	35	028	J26.2	18	02	02	20	*	*	04	07	09	08	07	07	05	*	*	*	*	04	10				
II	6.3 5.9 5.7 5.9	-	05.3	81	63	78	74	28	110	J24.8	15	*	08	*	*	*	02	02	09	16	11	04	13	03	*	*	*	*	04	04			
III	4.0 4.2 3.8 4.3	-	06.0	84	55	78	72	22	057	J19.4	04	*	06	02	*	*	01	13	07	11	09	04	10	01	*	*	*	*	02	02	01		
IV	5.5 5.2 4.4 5.4	-	06.5	75	58	82	73	30	088	J37.4	16	*	03	01	*	*	07	07	14	09	02	14	03	03	*	*	*	*	01	03	01		
V	4.1 4.0 5.3 4.4	-	09.5	76	52	77	68	24	076	J23.6	10	*	*	10	*	*	*	08	04	12	10	03	12	*	*	*	*	*	*	*	*	*	
VI	2.8 4.2 5.9 4.3	-	11.1	45	78	67	39	059	J18.9	23	*	*	18	04	*	*	04	04	12	07	01	12	*	*	*	*	*	*	*	*	*		
VII	3.0 3.3 3.6 3.9	-	12.5	78	56	80	71	32	066	J18.0	23	*	*	21	07	*	*	04	04	12	07	01	12	*	*	*	*	*	*	*	*		
VIII	3.0 3.8 3.9 3.5	-	12.8	85	55	82	74	37	069	J25.5	15	*	*	23	04	*	*	09	02	11	09	01	11	*	*	*	*	*	*	*	01	*	
IX	5.4 5.3 4.4 5.0	-	08.7	86	55	84	75	33	070	J28.2	21	*	02	11	01	*	*	06	09	11	10	02	11	*	*	*	*	*	*	*	06	*	
X	4.3 3.4 3.4 3.7	-	07.6	88	58	88	78	32	015	J11.3	03	*	02	*	*	*	14	06	04	04	01	04	04	*	*	*	*	*	*	*	10	*	
XI	5.5 6.2 6.2 6.0	-	06.3	81	69	87	81	26	084	J22.8	17	*	10	*	*	*	03	07	14	09	01	13	05	04	*	*	*	*	01	10	01		
XII	7.9 6.4 6.4 6.7	-	03.7	85	82	89	85	51	089	J26.5	26	02	18	25	*	*	*	05	19	12	12	02	07	07	*	*	*	*	*	*	05	20	
GOD.	4.9 4.7 5.0 4.9	-	07.8	82	59	82	74	22	763	J37.4	46.V	04	20	76	86	16	*	-	87	85	143	110	19	132	24	07	*	*	*	18	44	37	
<b>BR. ST. 174 PANCEVO</b>												$H_s = 80 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																					
I	7.6 6.8 6.4 6.9	-	04.5	80	77	86	84	41	028	J07.2	16	03	02	19	*	*	08	01	02	12	08	07	07	02	01	*	*	*	*	03	*		
II	8.2 6.6 6.9 7.3	-	05.9	86	70	80	80	40	066	J16.0	15	*	07	*	*	*	04	02	12	11	04	11	02	01	*	*	*	*	02	03			
III	5.3 5.1 3.8 4.8	-	06.1	84	55	75	71	23	028	J13.0	04	*	06	02	*	*	01	02	09	10	01	10	01	*	*	*	*	*	*	02	*		
IV	6.0 6.6 4.8 5.9	-	07.3	84	65	81	71	31	090	J38.5	16	*	03	01	*	*	06	01	04	10	11	10	03	11	*	*	*	*	01	01			
V	5.0 5.3 5.3 5.5	-	10.2	81	52	76	70	32	039	J08.2	11	*	*	13	01	*	*	02	01	06	07	09	07	09	*	*	*	*	01	01			
VI	3.0 4.6 3.3 3.3	-	13.6	81	60	80	74	31	035	J12.5	23	*	*	22	09	*	*	01	13	03	36	04	01	06	*	*	*	*	03	*			
VII	4.6 4.5 4.0 4.4	-	15.8	85																													

Mesec	Vrstdišni Pristisk Pn mm	Temperatura vazduha °C						Čestina pravaca i srednja jačina veta nD, fm (0-12)																		
		Im		Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21	Sred. (dles)					8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
$\varphi = 44^{\circ}02' N \lambda = 20^{\circ}56' E$ Gr. $\Delta G = + 1h 24 min.$																										
I	-	00.8	05.5	02.2	02.6	06.6	-01.4	16.2	30 -10.2	19	01	01.0	04	08.0	41	04.7	09	03.6	03	03.0	01	07	02.6	08		
II	-	04.8	10.7	06.8	07.2	12.4	32.7	23.6	23 -06.2	05	06	02.5	02	02.0	-	-	04	02.5	13	02.4	17	02.5	01	02.0		
III	-	05.7	14.4	08.8	09.4	15.3	04.2	28.2	26 -04.0	01	07	02.3	-	-	01	01.0	09	02.6	11	02.9	08	02.5	-	15 02.7		
IV	-	07.3	14.7	09.1	10.0	15.9	04.3	25.6	29 -02.0	12	05	02.6	04	02.2	-	-	08	03.4	05	02.4	10	02.4	-	24 03.1		
V	-	14.0	24.3	15.3	16.5	22.5	13.7	29.2	29 02.3	02	32.0	04	02.5	17	03.6	12	03.0	11	02.4	-	-	02	03.5	43		
VI	-	16.9	24.7	17.4	19.1	26.2	12.9	33.6	14 03.6	05	34	02.8	-	-	01	02.0	05	02.6	15	02.4	21	02.2	-	12 02.4		
VII	-	18.1	25.6	19.3	20.6	27.0	14.5	35.4	31 09.4	28	08	02.1	07	01.7	01	01.0	01	02.0	09	01.9	08	01.8	-	19 02.5		
VIII	-	17.4	26.1	18.6	20.2	27.2	13.6	31.0	19.0 10.0	09.2	26	02.0	07	32.0	-	-	08	02.2	04	02.3	19	01.8	-	17 02.2		
IX	-	11.1	19.6	13.1	14.2	20.5	09.1	31.0	09 -02.2	30	10	02.5	08	02.2	02	02.0	07	02.1	02	02.0	08	02.2	-	15 02.6		
X	-	10.7	18.0	10.1	11.5	18.9	05.9	25.8	01 -31.2	18	05	02.2	06	02.0	-	-	05	02.2	09	02.3	11	02.0	-	07 02.4		
XI	-	06.1	11.9	07.9	07.7	13.1	04.0	25.2	12 -04.6	30	07	02.9	04	02.0	01	02.0	03	02.0	13	03.0	19	02.1	-	08 02.2		
XII	-	-32.2	00.7	-01.1	01.8	-03.8	09.2	28 -14.0	06	13	02.0	07	32.1	-	-	08	02.1	10	02.3	10	02.1	-	14 02.7			
GOD.	-	09.0	16.1	10.5	11.5	17.3	06.4	35.4	34 VI -15.4	49	75	02.4	49	02.0	38	02.1	77	02.7	104	02.5	153	02.2	01	02.0		
$\varphi = 44^{\circ}22' N \lambda = 20^{\circ}57' E$ Gr. $\Delta G = + 1h 22 min.$																										
I	752.8	00.3	05.3	01.8	02.3	06.1	-00.9	16.2	30 -13.4	19	03	02.3	-	-	24	02.2	43	02.6	01	03.0	J3	02.0	05	01.8	05	
II	749.5	04.6	10.4	06.6	07.0	11.9	03.6	23.4	22 -05.2	05	05	02.8	01	01.0	15	01.8	23	02.1	06	02.5	15	02.3	11	02.4		
III	754.4	05.0	14.2	08.6	09.1	15.1	03.6	26.3	24 -04.7	01	05	02.8	05	01.6	18	02.1	27	02.4	05	02.2	06	01.7	15	02.9		
IV	749.0	07.1	14.6	09.6	10.2	18.0	04.7	25.8	29 -01.4	12	02	02.5	03	01.7	21	02.2	01	03.0	07	02.0	22	03.0	16	03.6		
V	750.8	14.0	21.6	16.0	16.9	22.6	10.7	29.4	21 05.4	25	09	01.9	05	01.8	12	01.8	21	02.0	06	01.3	10	01.4	12	01.8		
VI	749.0	16.8	24.5	18.2	19.4	26.2	12.7	33.6	14 03.2	05	05	02.2	05	01.6	14	02.8	09	01.7	17	01.5	24	02.0	15	01.9		
VII	749.0	18.0	25.7	19.6	20.7	26.9	14.4	34.7	31 09.6	28	19	02.0	04	01.8	07	01.6	15	02.1	05	01.8	04	02.2	21	02.0		
VIII	749.4	16.6	25.4	19.0	20.0	26.7	13.6	30.5	28.13 06.4	27	04	02.2	04	01.8	20	02.0	03	01.7	18	01.6	04	01.5	13	01.4		
IX	754.3	14.0	19.6	12.8	14.0	20.5	08.6	30.9	09 -03.3	29	10	02.3	06	02.0	16	02.1	07	01.6	03	01.3	10	01.4	14	01.5		
X	755.7	17.3	19.3	13.1	13.3	18.3	05.5	25.8	01 -02.2	19	04	02.2	05	01.4	18	02.2	09	02.1	05	01.2	16	01.3	10	01.5		
XI	749.0	05.0	11.1	06.6	07.3	12.3	02.8	22.1	12 -05.2	30	05	02.2	01	01.0	14	01.9	19	02.1	03	01.7	07	02.3	18	02.4		
XII	757.0	-02.1	03.2	-01.6	-01.3	01.1	-03.8	08.2	30,29 -14.4	06	10	01.7	07	01.4	16	02.8	23	02.1	01	01.0	06	01.3	16	02.2		
GOD.	751.7	08.6	15.8	10.6	11.4	17.0	06.2	34.7	34 VI -14.4	06 XI	73	02.1	42	01.6	176	02.1	245	02.2	44	01.7	92	01.7	194	02.1	168	
$\varphi = 44^{\circ}05' N \lambda = 21^{\circ}05' E$ Gr. $\Delta G = + 1h 24 min.$																										
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	04.1	14.1	07.9	08.5	15.0	03.7	28.5	24 -14.0	01	03	02.0	01	02.0	-	-	26	05.7	15	02.3	04	02.2	16	02.2		
IV	-	06.4	14.6	08.7	09.6	15.7	01.4	24.0	29.26 -08.0	22	07	02.9	03	02.7	02	01.0	20	06.0	09	02.6	02	02.0	20	03.0		
V	-	14.3	21.6	14.7	16.3	22.8	08.6	29.5	21 04.0	25	07	02.3	01	02.0	01	02.0	32	04.2	04	02.5	03	01.7	03	02.3		
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	17.8	25.5	18.2	19.9	26.6	10.5	32.5	31,21 04.5	13	14	02.1	02	02.0	-	-	08	02.2	10	02.8	02	03.0	05	02.2		
VIII	-	16.6	24.8	17.5	19.1	25.7	10.5	31.0	10 02.5	27	04	01.8	-	-	02	02.0	12	04.1	11	02.5	01	03.0	06	03.3		
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 44^{\circ}56' N \lambda = 21^{\circ}08' E$ Gr. $\Delta G = + 1h 24 min.$																										
I	-	00.2	03.8	01.7	01.8	04.5	-01.2	14.8	30 -10.2	19	01	01.0	04	08.0	41	04.7	09	03.6	03	03.0	01	07	02.6	07	03.0	
II	-	03.7	09.0	02.5	05.8	10.2	02.0	20.7	23 -05.0	05	04	02.0	02	03.0	20	04.4	04	01.8	03	02.7	02	01.5	17	02.9	07	03.0
III	-	05.5	13.4	07.4	08.4	14.5	03.8	28.2	24 -07.2	01	01	02.0	03	02.0	38	03.9	03	02.3	03	02.0	17	03.1	01	02.0	27	
IV	-	07.1	13.9	08.5	09.5	15.0	03.9	23.2	30,29 -02.2	13	*	04	03.0	30	03.5	02	04.5	*	*	02	01.5	20	03.8	10	03.7	
V	-	14.4	21.5	14.7	16.4	22.7	11.1	30.0	21 04.0	26,25	*	03	02.3	28	03.1	06	04.7	*	*	*	*	09	02.2	08	02.2	
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	18.3	26.0	18.1	20.1	27.1	-	33.0	09,08,-0	-	02	02.0	08	02.2	05	02.0	05	03.6	03	02.3	06	02.0	14	02.6		
VIII	-	17.3	24.4	17.6	19.2	25.6	13.3	30,2	16	07.2	26	02.0	02.0	16	02.0	24	02.3	*	*	01	02.0	05	02.0	12	03.2	
IX	-	11.6	19.6	11.7	13.6	20.4	08.7	30.2	09 J1.0	30	*	07	02.3	22												

Mesec	Oblačnost Nm (0-10)	Iseljeno- broj sati hod (Dies)	Vlažnost vazduha L m %	Padavine R mm	Broj dana na sat																Nm (0-10)		R mm		•	*	*	Δ	○	▲	■	□		
					Tn				Tx				Tx				Tx				F(0-12)		Nm (0-10)		R mm		•	*	*	Δ	○	▲	■	□
					7	14	21	Sred. (Dies)	mm	7	14	21	Sred. (Dies)	Min	Σ	Max	Dat.	≤	<	≤	IN	IN	IN	IN	6	8	2.0	8.0	0.1	1.0	0.0	T		
KRAGUJEVAC																																		
BP. ST. 176																																		
I 6.5 6.5 5.4 6.6 3	088.8	94.4	84	66	79	76	35	043	015.8	18	02	02	17	.	.	.	31	.	03	09	11	10	01	08	07	03	.	.	.	.				
II 8.0 8.2 7.6 7.1	093.8	95.6	85	61	79	75	31	102	021.2	15	.	05	.	.	.	31	.	03	14	12	11	06	02	09	03	.	.	.	01					
III 5.5 5.2 3.8 4.8 3	169.4	96.2	85	53	77	72	26	147	016.8	04	.	04	02	.	.	11	10	10	08	02	09	02	.	.	.	.	01	01						
IV 6.7 7.4 4.2 6.1	181.8	96.6	82	55	78	72	32	361	018.2	16	.	03	01	.	.	04	09	13	08	01	13	01	01	.	.	.	02	.	.					
V 5.9 6.6 5.2 5.9 2	228.5	10.1	82	53	82	72	28	066	011.4	29	.	.	11	.	01	.	05	11	14	11	02	14	.	.	.	.	08	.	.					
VI 4.1 5.5 5.5 5.5 3	257.6	11.4	77	45	83	62	29	128	035.6	28	.	.	20	07	.	.	06	07	14	11	03	14	.	.	.	01	07	.	.					
VII 4.5 4.3 4.5 4.5 4	263.5	13.1	82	54	87	73	31	084	023.6	23	.	03	01	07	01	.	11	07	12	10	03	12	.	.	.	01	07	.	.					
VIII 3.8 4.8 5.0 4.6 6	258.0	12.9	84	49	86	73	37	040	013.8	23	.	03	05	07	01	08	06	12	07	02	12	.	.	.	.	05	.	.						
IX 5.5 5.5 5.5 5.6 2	228.5	10.1	82	53	82	72	28	066	011.4	21	.	03	11	01	.	01	04	08	12	09	01	12	.	.	.	03	.	.						
X 4.7 4.4 4.1 4.4 4	171.4	07.6	89	52	85	75	28	118	010.0	03	.	04	02	.	.	11	06	03	03	01	03	.	.	.	.	02	.	.						
XI 6.7 6.9 6.7 6.7 6.8	389.9	06.6	63	65	87	80	30	045	013.0	17	.	07	01	.	.	02	10	12	11	01	01	.	.	.	.	01	01							
XII 6.7 6.4 8.1 8.1 9	393.3	03.6	86	75	86	82	47	067	021.4	39	03	15	23	.	.	03	21	13	11	03	08	05	.	.	.	15	.	.						
GOD. 5.0 6.0 5.0 5.0 5.7 2	2121.9	08.1	84	56	82	74	26	764	035.6	28	v	05	17	63	96	22	01	03	06	71	118	138	110	26	125	19	04	.	.	01	35	05	28	
SMEĐEREVSKA PALANKA																																		
BP. ST. 177																																		
I 7.4 7.3 5.4 6.6 6	309.3	94.3	83	68	80	77	39	039	008.3	14	01	02	17	.	.	.	14	05	01	10	12	10	10	05	.	32	.	.	02	10				
II 8.3 8.3 6.0 7.5	052.4	05.6	85	62	88	75	23	092	020.1	12	.	05	.	.	.	14	04	01	14	18	14	03	17	03	.	.	.	02	03					
III 5.4 5.3 4.0 4.9 4	104.6	05.9	84	52	74	70	22	061	017.1	04	.	06	02	.	.	15	05	01	11	09	13	08	02	12	02	.	.	01	.	01				
IV 6.5 7.8 6.4 6.7 6.7	179.7	06.3	83	52	72	69	28	104	038.7	16	.	05	02	.	.	18	06	03	11	13	09	04	13	02	.	.	01	.	01					
V 5.9 6.3 5.6 5.6 5.9	245.3	09.4	80	49	71	67	23	088	034.6	09	.	.	12	.	.	12	02	05	09	12	10	02	12	.	.	.	07	03	.					
VI 3.7 6.2 5.2 5.0 5.0	276.9	11.0	79	45	72	65	29	078	040.3	25	.	04	09	.	.	06	07	17	04	11	02	11	.	.	.	10	01	.						
VII 4.3 4.3 3.8 4.3 4.3	280.7	12.8	62	52	78	70	32	033	007.4	23	.	03	05	07	.	08	02	10	04	15	12	01	.	.	.	05	02	.						
VIII 4.3 4.3 4.1 4.1 4.5	254.0	12.3	85	52	77	71	36	046	014.7	23	.	04	04	04	.	09	09	06	09	07	01	09	.	.	.	08	06	.						
IX 5.5 5.5 4.1 5.0 5.0	189.0	08.6	87	50	79	73	28	058	023.4	21	.	03	11	01	.	08	01	07	08	12	10	01	12	.	.	.	02	03	.					
X 5.5 5.3 4.6 4.6 4.6	190.9	07.4	89	55	82	75	27	015	009.1	03	.	02	01	.	.	05	11	10	05	03	03	05	.	.	.	06	.	.						
XI 6.2 7.5 6.4 6.7 6.7	392.1	06.4	89	69	86	81	40	055	027.2	17	.	07	.	.	.	35	03	12	13	08	01	13	01	.	02	.	.	01	06	.				
XII 8.5 7.8 7.3 7.9 7.9	354.2	03.6	87	80	84	85	47	077	019.8	30	03	18	22	.	.	08	03	04	21	19	13	03	14	09	01	.	02	.	.	18				
GOD. 6.0 6.3 5.1 5.1 5.8 5.8	2139.3	07.8	84	57	77	73	22	746	040.3	25	VI	04	20	67	95	21	.	122	28	72	129	153	111	19	144	22	04	.	06	01	.	35	31	32
FLAMUNDA																																		
BP. ST. 178																																		
I - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
II 8.4 7.1 6.2 7.2 7.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
III 4.5 5.2 4.2 4.6 4.6	-	36.3	83	57	85	75	23	065	021.2	30	01	13	02	.	.	-	11	11	10	10	02	09	02	.	.	.	01	01	01					
IV 5.6 7.4 5.8 5.8 5.8	-	36.7	82	57	85	74	31	098	035.2	16	.	03	04	.	.	-	11	11	10	10	02	09	02	.	.	.	01	01	01					
V 5.8 5.7 4.4 5.3 5.3	-	188.5	63	37	93	63	-	027	039.2	11	.	01	13	.	01	-	05	09	08	07	.	08	.	.	01	.	.							
VI - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VII - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VIII 4.4 4.2 3.7 4.1 4.1	-	230.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10	05	14	12	04	14	.	.	.	01	.	.						
IX - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10	07	08	06	02	08	.	.	.	.	.	.						
X - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13	12	01	13	01	01	.	.	.	.	.	.						
XI - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13	12	01	13	01	01	.	.	.	05	.	.						
XII - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10	07	08	06	02	08	.	.	.	.	.	.						
GOD. - - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
SUSAPĀ																																		





1977

Mesec m.	Vrednost Pratilask Pr. mm	Temperatura vazduha °C						Cestina pravaca i srednja jačina veta nD, Fm (0-12)																					
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21																									
$\varphi = 44^{\circ}14' N \lambda = 22^{\circ}33' E$ Gr. AG = + 1h 29 min.																													
I	762.3	-04.1	00.2	-03.1	-02.5	01.3	-06.4	09.6	28	-18.5	19	10	01.2	18	01.4	07	02.0	02	01.5	05	01.4	04	01.0	05	01.6	17	01.7	25	
II	757.3	-02.8	08.6	04.9	05.3	09.7	01.7	17.3	23	-02.1	04	14	01.7	11	01.5	23	01.4	06	01.0	01	01.0	03	03.0	19	02.9	07	01.7	11	
III	762.4	02.0	13.0	08.2	08.4	14.3	02.7	26.8	23	-03.0	01	04	02.0	03	01.0	16	01.9	15	01.7	02	01.5	13	03.2	12	02.7	28	01.8	13	
IV	755.8	08.1	15.3	09.9	10.8	16.6	05.5	24.4	30	-01.5	22	09	01.3	04	01.5	10	01.9	05	01.8	02	01.0	26	03.2	21	03.5	13			
V	758.0	14.4	22.5	15.7	17.1	23.5	10.8	31.0	21	06.2	25	12	01.6	07	01.6	20	01.9	06	01.8	01	01.0	06	01.3	13	02.6	13	02.1	15	
VI	755.5	18.0	24.9	18.9	20.2	26.3	14.0	33.2	14	07.2	05	04	02.2	06	01.2	05	01.0	03	01.0	04	02.0	21	02.3	23	02.2	19			
VII	755.4	19.7	26.6	20.7	21.9	27.8	16.0	33.9	09	11.4	14	09	02.1	08	01.6	05	10	11	03	01.0	03	02.3	19	03.1	25	02.6	12		
VIII	756.4	17.9	26.6	19.2	20.7	27.6	14.7	32.5	29	09.6	27	07	01.6	04	01.4	14	01.5	06	01.7	02	01.0	04	01.5	13	02.5	27	02.3	16	
IX	761.2	12.6	21.3	13.9	15.4	22.3	09.9	31.8	05	-03.6	30	11	01.9	07	01.3	19	01.6	08	01.8	01	03.0	02	02.0	12	02.4	17	02.4	13	
X	763.5	05.8	17.3	08.8	10.2	18.1	04.2	25.1	19	-02.2	18	06	01.5	10	01.4	30	01.3	14	01.1	01	01.0	06	02.3	08	02.5	18			
XI	764.4	-05.3	11.5	06.9	07.6	12.4	03.6	25.0	04	-04.2	30	13	01.7	13	01.5	05	01.0	02	01.0	05	01.2	19	02.7	15	02.6	13			
XII	764.4	-05.3	-06.6	-03.4	-00.6	-07.5	-06.3	-25	-22.0	13	13	16	20	01.3	06	02.0	-	01	01.0	03	01.3	19	02.9	15	03.3	16			
GOD.	759.1	08.3	15.6	10.0	11.0	16.7	05.8	33.9	09.VI	-22.0	43.XII	112	01.7	111	01.4	159	01.6	80	01.5	19	01.1	38	01.5	169	02.7	212	02.6	195	
$\varphi = 43^{\circ}55' N \lambda = 19^{\circ}26' E$ Gr. AG = + 1h 18 min.																				MITROVAC-TARA		BR. ST. 187							
I	-	-02.3	01.7	-01.6	-01.0	02.5	-04.0	10.0	29	-16.4	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	00.5	04.4	01.4	01.9	05.6	-01.3	13.4	25	-09.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	00.2	09.0	01.7	03.1	09.8	-01.4	20.4	24	-11.2	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	01.2	08.3	03.2	04.0	09.5	-06.4	23.6	29	-0.9	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	07.4	14.5	09.3	10.1	15.5	04.7	25.2	19	-01.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	10.1	16.6	11.1	12.2	17.6	06.4	26.0	14	-01.0	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	12.1	18.6	13.0	14.2	19.6	09.1	27.6	31	04.6	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	10.0	18.9	12.3	13.3	19.6	07.9	25.2	18	01.0	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IX	-	06.5	13.2	06.8	08.4	14.0	04.1	21.6	09	-05.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
X	-	02.5	12.7	04.7	06.1	13.5	01.6	19.0	08	-03.0	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-	01.3	05.3	02.1	02.7	06.9	-09.9	16.2	12	-11.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII	-	-06.4	-02.4	-05.5	-04.9	-00.7	-08.0	05.2	29	-16.2	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	03.6	10.1	04.9	05.8	11.1	01.5	27.6	34.VI	-16.4	49.I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}44' N \lambda = 19^{\circ}43' E$ Gr. AG = + 1h 17 min.																				ZLATIBOR		BR. ST. 188							
I	572.9	-00.9	02.4	00.1	00.4	03.8	-02.5	11.4	29	-10.6	19	13	01.7	*	01	03.0	13	02.9	51	03.3	08	02.6	*	*	04	01.5	03		
II	571.2	01.9	05.7	02.7	03.2	07.4	00.5	17.6	24	-09.0	22	12	01.7	*	01	01.0	05	03.4	50	03.8	11	02.4	*	*	05	01.8	04		
III	576.3	03.7	09.7	05.9	06.4	11.0	01.9	21.7	24	-23.10.9	01	15	02.1	03	01.7	04	01.8	10	02.6	36	03.2	09	02.8	03	02.0	09	01.7	04	
IV	571.6	04.0	09.2	05.9	06.4	11.2	02.1	22.5	29	-0.6	12	25	01.9	10	01.9	01	01.0	10	02.6	14	03.1	16	02.6	04	01.8	07	02.1	01	
V	-	07.4	16.0	11.1	17.7	25.2	07.8	25.2	20	01.7	28	13	01.4	20	01.8	05	02.0	06	02.2	13	03.1	25	02.6	03	02.0	01	01.0	07	
VI	573.9	12.7	17.4	13.1	14.1	19.0	09.3	26.6	14	03.4	04	12	01.6	13	01.5	04	02.0	08	01.6	03	01.7	32	02.3	35	01.8	04	08		
VII	574.3	14.0	19.6	15.5	16.3	21.0	11.9	27.7	31	08.3	07	16	01.8	15	01.7	08	01.5	05	01.6	29	02.5	04	02.0	05	01.8	06	02.6	06	
VIII	575.6	14.2	19.9	15.2	16.3	21.1	11.5	27.4	28	04.9	26	15	01.6	14	01.9	08	01.8	06	02.0	09	02.7	32	02.6	04	01.5	03	01.7	02	
IX	577.3	08.6	13.5	09.7	10.4	14.8	06.7	23.5	09	-02.0	29	22	01.8	27	01.9	06	01.8	04	01.5	02	03.2	17	02.1	01	02.0	03	01.3	06	
X	578.3	06.2	13.0	08.9	09.2	14.1	05.1	20.1	01	-00.5	04	13	01.4	18	01.6	04	02.0	04	01.5	08	02.1	34	02.6	06	01.5	02	01.0	06	
XI	571.7	02.6	06.5	04.0	04.2	08.2	00.9	18.6	12	-07.3	25	09	01.7	08	01.1	07	01.9	01	02.0	11	02.7	44	03.1	06	02.0	*	*	04	
XII	-05.4	-02.2	-04.3	-04.0	-00.4	-07.2	07.6	29	-13.3	18	17	01.5	11	01.6	02	01.0	01	03.1	32	02.9	08	02.5	02	01.0	13	01.0	03		
GOD.	-	07.2	15.2	09.7	10.4	16.4	05.6	33.9	34.VI	-12.6	30.I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\varphi = 43^{\circ}16' N \lambda = 20^{\circ}01' E$ Gr. AG = + 1h 20 min.																				SJENICA		BR. ST. 190							
I	574.1	-05.9	-00.1	-04.2	-03.6	01.0	-08.7	10.4	29	-27.4	20	10	01.8	02	01.0	11	01.7	13	02.1	09	01.8	09	03.1	02	02.0	05	01.4	32	
II	572.2	00.8	02.4	03.4	07.9	-00.8	17.5	24	-08.8	28	12	02.6	05	01.2	03	02.3	06	02.3	15	02.3	19	03.7	06	02.2	07	01.7	11		
III	577.1	-04.4	10.6	03.3	04.2	11.4	-02.2	21.9	23	-15.0	03	07	02.3	04	01.8	06	01.3	10	02.0	06	02.2	15	02.7	06	02.0	14	02.3	27	
IV	572.3	02.5	09.9	04.7	05.9	15.5	02.6	28.2	23	-04.3	01	04																	



Mjesec	Vrastudija prirodnih Pm mm	Temperatura vlastuda °C						Čestina pravaca i srednja jačina vjetra m/s, Pm (0-12)																			
		Tm			Max	Min	Det.	Max	Min	Det.	N		NE		E		SE		S		SW		W		NW		
		7	14	21							E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	
$\gamma = 43^{\circ}51' N \lambda = 20^{\circ}02' E$ Gr. $\Delta G = +1h\ 20\ min.$																											
I	735.7	-02.2	03.2	00.0	00.3	04.7	-03.8	17.7	29	-14.8	20	14	01.4	06	01.2	13	01.5	11	01.7	02	01.0	10	01.7	06	01.0	27	01.3 04
II	732.8	-02.2	10.3	05.3	05.6	12.1	00.7	21.6	23	-04.2	05	14	01.6	12	01.5	07	01.6	04	01.8	03	02.3	12	03.6	07	01.4	25	01.4 .
III	734.5	02.2	10.6	07.3	07.3	15.7	00.9	27.7	24	-04.4	01	14	01.7	10	01.5	06	01.6	13	01.6	04	01.0	06	02.7	08	01.9	24	01.5 06
IV	732.5	04.8	14.6	08.8	09.3	16.2	02.4	26.6	29	-03.4	18	11	01.7	09	02.0	10	01.2	05	01.8	05	03.4	16	02.4	05	01.8	24	02.1 05
V	734.6	10.8	20.4	14.1	14.9	21.8	09.0	29.6	20	04.5	30	08	01.4	11	01.6	07	02.6	08	02.5	03	01.7	09	01.8	13	01.4	28	01.3 06
VI	733.1	13.9	23.4	16.1	17.2	24.6	11.4	32.0	14	03.3	20	01.8	06	01.7	14	01.5	05	02.6	01	02.0	08	01.5	06	01.3	24	01.3 05	
VII	733.1	15.3	25.4	18.4	19.4	26.5	13.8	34.6	31	10.3	13	10	01.5	07	01.6	09	01.7	07	01.7	01	01.0	08	01.8	06	01.3	30	01.3 07
VIII	733.4	14.0	25.5	17.4	18.6	26.8	13.1	32.6	11	07.1	26	11	01.5	10	01.7	08	01.9	06	02.1	07	02.0	08	01.2	27	01.3 04		
IX	737.8	09.6	19.2	12.1	13.2	20.2	08.3	30.7	09	-01.8	30	16	01.6	10	01.6	12	01.5	03	02.0	03	01.7	04	01.2	06	01.2	30	01.3 06
X	739.1	05.7	16.8	08.2	09.1	18.0	04.4	25.8	20	01.6	19	10	01.3	09	01.4	04	01.5	05	01.4	04	01.0	07	01.1	10	01.2	27	01.1 17
XI	733.1	05.8	09.9	05.4	06.1	11.1	02.4	22.6	11	-03.6	25	14	01.1	05	01.0	03	01.7	05	01.0	05	01.4	12	01.5	15	01.2	29	01.3 02
XII	739.6	-03.4	-00.6	-02.9	-02.5	00.5	-05.3	06.0	27	-14.6	06	11	01.3	10	01.2	14	01.4	08	01.1	05	01.2	03	01.3	06	01.1	33	01.2 01
GOD.	735.2	06.3	15.2	09.2	10.0	16.5	04.8	34.6	34.7	-14.8	20.1	161	01.5	105	01.6	83	01.7	44	01.7	102	02.0	98	01.3	328	01.4 63		
$\gamma = 43^{\circ}35' N \lambda = 20^{\circ}14' E$ Gr. $\Delta G = +1h\ 21\ min.$																											IVANJICA BR. ST. 192
I	-	-01.7	04.5	00.5	00.9	06.1	-03.6	16.5	29	-18.7	20	07	01.6	05	02.0	21	02.0	06	01.8	03	01.7	.	.	12	02.2	17	02.5 22
II	-	03.8	10.1	05.8	06.2	12.1	01.9	21.3	24	-04.2	28	03	01.7	12	02.2	10	02.8	04	02.5	05	02.4	11	02.7	13	02.8	16	
III	-	03.1	13.8	06.4	07.4	15.1	01.9	26.0	24	-06.0	31	06	02.0	02	02.0	29	02.1	05	01.4	06	02.0	.	.	15	02.6	13	02.8 22
IV	-	03.6	13.5	07.6	08.6	15.3	03.0	27.1	29	-02.5	10.12	05	01.2	05	02.2	25	01.8	04	01.5	02	03.5	.	.	16	03.2	15	03.2 18
V	-	13.3	19.9	13.0	14.3	21.3	08.7	31.2	20	04.5	30	07	01.4	08	02.1	24	02.0	06	02.3	03	02.0	01	02.0	13	03.1	12	02.5 19
VI	-	14.4	22.4	14.3	16.3	23.9	11.0	32.0	14	03.6	06.05	08	02.0	07	02.0	26	02.1	10	02.5	02	01.5	01	03.0	05	02.4	10	02.3 21
VII	-	16.1	24.4	17.0	18.6	25.6	13.2	34.0	31	10.3	28	05	01.6	07	01.9	22	02.0	11	02.2	01	02.0	04	02.2	09	01.8	16	02.4 20
VIII	-	14.1	24.3	15.8	17.6	25.5	12.4	31.5	21	06.7	27	05	01.3	11	02.1	26	02.2	05	02.4	01	01.0	07	02.4	11	02.5	15	02.9 11
IX	-	09.6	18.0	10.8	12.3	19.2	08.2	28.8	29	-02.4	30	12	01.8	10	02.3	19	02.3	06	02.7	.	.	01	04.0	22	02.7	12	02.4 08
X	-	05.7	16.3	09.1	09.7	17.4	04.4	25.0	20	01.0	07	14	01.5	07	01.7	24	02.0	07	01.1	01	03	02.0	18	02.4	19	02.3 08	
XI	-	04.2	10.0	05.6	06.4	11.8	02.6	23.3	23	-05.2	25	05	01.4	04	02.0	08	02.1	07	02.0	01	05.0	01	02.0	18	02.3	24	02.1 22
XII	-	-04.0	-00.1	-02.7	-02.4	01.6	-05.7	10.6	29.28	-15.1	19	09	01.4	04	02.0	14	01.9	09	02.1	01	01.0	.	.	24	02.5	18	02.2 14
GOD.	-	06.9	14.8	08.5	09.7	16.2	04.8	34.0	34.7	-18.7	20.1	79	01.6	73	02.0	255	02.1	86	02.3	20	02.2	23	02.4	174	02.6	184	02.5 201
$\gamma = 43^{\circ}25' N \lambda = 20^{\circ}17' E$ Gr. $\Delta G = +1h\ 21\ min.$																											BELE VODE-GOLIJA BR. ST. 193
I	-	-02.1	01.4	-02.2	-01.3	03.0	-04.2	08.6	01	-13.2	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	00.1	03.2	00.4	00.9	05.2	-02.0	14.2	24	-14.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	01.2	07.4	02.0	03.1	08.9	-00.5	19.6	23	-13.8	01	04	03.0	16	02.3	18	01.8	23	02.2	02	01.5	13	02.1	04	02.8	10	02.7 03
IV	-	02.0	06.2	02.7	03.4	08.5	-00.3	20.4	29	-07.6	11	04	01.8	23	02.4	28	02.1	03	01.0	08	01.4	05	01.8	02	01.0	02	
V	-	08.5	12.8	08.3	09.5	14.6	05.2	23.5	20	19	-00.2	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	10.7	14.6	09.9	11.3	16.6	07.0	24.8	14	-01.4	05	01	02.0	09	02.2	46	02.0	21	02.4	07	02.0	02	03.0	04	02.5	.	
VII	-	10.7	14.6	15.9	16.3	20.8	09.7	26.4	31	05.4	07	12	02.6	37	01.7	17	02.2	08	01.5	07	02.1	04	02.5	01	02.0	.	
VIII	-	12.8	18.2	12.2	13.9	19.9	09.4	26.8	30	03.0	26	02	05	19	02.5	23	01.8	33	02.0	05	01.4	03	01.3	08	01.4	.	
IX	-	07.3	11.9	07.2	08.4	13.9	05.1	21.4	29	05	04.5	16	01.6	14	02.1	20	01.6	25	01.8	06	01.7	12	01.8	07	02.3	01	02.0
X	-	05.1	12.2	05.7	07.2	13.7	03.4	18.8	17	01	02.0	09	02.0	23	02.0	36	01.8	10	01.9	07	02.4	02	03.0	05	02.6	.	
XI	-	02.6	05.4	02.3	03.2	07.8	-00.2	17.2	24	-08.2	28	01	05.0	29	03.1	20	02.0	17	02.7	01	02.0	12	02.8	08	02.4	02	06.0
XII	-	-04.5	-01.1	-04.5	-03.6	01.3	-06.8	07.8	01	-12.8	12.05	01	02.0	12	02.6	29	02.0	19	02.5	05	02.4	20	02.3	05	02.2	02	01.5
GOD.	-	04.7	09.2	04.7	05.6	11.1	02.2	26.8	30.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\gamma = 43^{\circ}53' N \lambda = 20^{\circ}19' E$ Gr. $\Delta G = +1h\ 21\ min.$																											CACAK BR. ST. 194
I	-	-01.4	04.5																								



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Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Pm (0-12)																	
		Tm			Spred. (Dicas)	Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C	
		7	14	21								6.	1.	6.	3.	6.	1.	6.	3.	6.	3.	6.	3.	6.	3.	6.	3.		
$\gamma = 43^{\circ}44' N \lambda = 20^{\circ}41' E$ Gr. $\Delta G = + 1h 23 min.$																													
I	744.0	-0.6	05.2	02.0	02.2	06.2	-01.9	17.6	30	-14.4	20	.	.	.	.	40	03.3	02	02.5	.	03	03.3	05	02.4	11	01.5	02	01.5	51
II	741.0	04.6	11.0	07.1	07.5	12.0	02.7	25.5	23	-04.5	05	03	01.0	19	02.1	03	02.0	03	03.3	05	02.4	11	01.5	02	01.5	40			
III	745.7	05.2	14.7	09.5	09.8	15.8	03.8	27.6	24	-04.1	01	03	01.0	0.	32	02.9	03	01.3	01	01.0	02	01.0	12	02.0	03	01.3	37		
IV	740.7	06.9	15.4	10.1	10.6	16.8	04.6	26.1	29	-01.1	12	05	01.8	02	01.0	19	02.9	03	01.0	07.0	04	01.8	15	02.3	05	01.6	39		
V	742.4	13.4	21.2	15.9	16.6	22.7	19.6	29.8	20	05.0	29	05	01.6	01	02.0	29	02.6	01	05.0	03	02.5	05	02.5	08	01.6	05	02.5	49	
VI	740.7	16.3	25.0	17.8	19.2	26.0	12.9	32.7	14	05.0	05	08	02.0	0.	06	02.2	02	01.5	03	02.3	02	01.5	21	01.8	05	01.8	43		
VII	740.7	17.6	25.9	19.9	20.8	26.8	14.8	35.9	31	11.6	28	09	01.4	01	01.0	21	01.4	04	01.8	01	02.0	03	01.3	15	01.7	05	01.8	34	
VIII	741.1	16.3	26.3	19.1	20.2	27.2	13.7	32.3	29	07.9	27	07	02.0	01	03.0	14	03.1	04	02.2	0.	04	02.0	13	01.6	02	01.5	48		
GOD.	743.2	08.4	16.2	10.9	11.6	17.3	06.3	35.9	34.VI	-14.4	20.1	48	01.6	13	01.5	255	02.8	20	02.0	13	02.4	22	01.7	133	01.7	29	01.5	562	
$\gamma = 43^{\circ}37' N \lambda = 20^{\circ}54' E$ Gr. $\Delta G = + 1h 24 min.$																										VRNJAVAČKA BANJA		BR. ST. 197	
I	-	-01.6	05.1	00.5	01.1	06.0	-03.2	16.9	30	-17.0	20	05	01.4	.	.	17	02.9	03	03.0	29	01.3	03	01.3	01	01.0	09	01.8	16	
II	-	03.2	10.6	05.5	06.2	12.2	01.9	24.4	23	-06.3	05	10	01.5	02	02.5	03	02.0	02	02.0	26	01.7	07	02.1	02	01.0	12	01.8	18	
III	-	04.2	14.3	07.8	08.5	15.3	03.0	27.0	23	-9.0	01	04	01.8	02	02.5	09	02.7	05	02.0	30	01.4	02	02.0	02	02.0	22	02.3	17	
IV	-	06.1	14.6	08.6	09.6	16.1	03.6	25.7	08	-02.3	12	08	01.8	06	02.3	05	02.0	01	04.0	21	02.0	03	01.3	01	01.0	21	02.5	24	
V	-	12.8	20.8	14.2	15.5	22.0	10.0	29.4	20	05.4	30	06	01.6	07	02.3	06	01.7	04	02.8	17	01.6	03	02.0	02	02.0	10	01.6	36	
VI	-	16.1	24.0	16.2	18.1	24.9	12.3	31.4	14	03.8	05	07	02.0	0.	02.0	01	03.0	19	01.9	03	02.0	08	02.0	01	02.0	16	02.1	31	
VII	-	17.7	25.0	18.4	19.9	26.0	14.3	35.0	31	10.8	07	12	01.7	04	02.0	01	02.0	01	03.0	19	01.9	03	02.0	08	02.0	01	02.0	15	
VIII	-	15.8	25.2	17.6	19.0	26.3	13.5	31.6	19	08.2	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	10.5	19.1	12.1	13.4	19.8	09.0	28.8	30	-01.4	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	06.4	17.2	10.3	10.6	17.0	05.3	23.5	09	-00.4	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	04.7	11.2	06.0	07.0	12.3	03.2	21.0	16.1	-04.2	25	08	01.2	07	01.7	04	02.2	0.	01.9	26	01.4	08	01.4	04	01.8	13	01.5	20	
XII	-	-02.7	00.2	-02.4	-01.9	01.1	-04.6	08.4	29	-11.6	13	09	01.3	06	01.2	09	02.6	07	01.9	19	01.6	03	01.3	04	02.0	21	02.1	15	
GOD.	-	07.8	15.6	09.5	10.6	16.6	05.7	35.0	34.VI	-17.0	20.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\gamma = 43^{\circ}27' N \lambda = 21^{\circ}04' E$ Gr. $\Delta G = + 1h 24 min.$																										ALEKSANDROVAC		BR. ST. 198	
I	-	-03.5	02.8	-01.4	-00.8	04.9	-05.0	13.5	12	-13.5	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	02.7	09.3	04.4	05.2	11.5	00.7	22.5	23	-05.2	05	02	02.5	.	.	.	.	.	.	.	.	.	.	.	.	.	.		
III	-	02.4	11.7	05.8	06.3	14.6	01.0	26.0	24.3	-06.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	04.4	12.8	07.6	08.1	15.3	02.7	25.5	29	-02.5	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	09.7	17.7	12.6	13.2	20.5	08.8	30.0	20	04.0	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	14.1	21.6	14.5	16.2	23.6	12.1	31.0	19.14	04.0	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	15.3	22.9	17.8	18.4	24.9	13.9	31.4	09	10.8	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	14.9	24.4	17.6	18.7	26.2	13.9	31.2	28	08.6	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	09.5	17.6	11.3	12.4	18.7	08.1	28.5	09	-01.4	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	05.3	14.3	07.6	08.7	16.0	04.7	22.5	01	01.0	18.05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	03.9	09.3	04.8	05.7	10.9	02.7	21.0	12	-05.0	0	0	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-04.9	-01.6	-04.0	-03.6	00.0	-06.1	09.0	29	-15.0	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	06.2	13.6	08.2	09.0	15.6	04.8	31.4	09.VI	-15.0	06.XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\gamma = 43^{\circ}52' N \lambda = 21^{\circ}06' E$ Gr. $\Delta G = + 1h 24 min.$																										REKOVAC		BR. ST. 199	
I	-	-00.4	05.3	01.0	01.7	05.9	-02.9	15.5	30	-15.7	20	03	01.7	.	.	02	03.0	04	02.8	06	02.2	01	01.0	01	02.0	04	02.2	72	
II	-	03.7	10.9	05.4	06.3	12.0	01.2	24.0	23	-07.0	05	02	02.5	.	.	01	02.0	01	01.0	07	02.4	.	*	13	02.5	60			
III	-	04.5	14.6	07.5	08.6	15.4	02.6	28.6	24	-06.0	01	04	02.0	.	.	02	01.5	05	02.5	05	01.2	08	02.0	02	04.0	12	02.4	59	
IV	-	06.2	15.1	08.6	09.6	16.3	03.3	25.4	29	-02.6	12	04	02.5	.	.	03	01.3	02	01.0	04	01.8	01	03.0	07	03.1	12	03.3	57	
V	-	13.9	21.4	14.7	16.2	22.5	09.8	29.8	20	04.0	30	05	01.2	01	02.0	02	02.0	03	01.3	05	01.4	.	*	02	01.0	14	01.9	61	
VI	-	16.3	24.1	16.7	18.5	25.9	11.7	32.3	14	02.5	25	05	01.6	.	.	01	02.0	03	01.3	02	01.5	04	01.8	06	02.2	69			
VII	-	17.9	25.5	18.1	19.9	26.9	13.6	34.0	31	09.2	28</td																		

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha % e <sub>m</sub> mm	Padavine R mm mm	Broj dana na sat															
						Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	
	7	14	21	Sred. (Dnev.)	Min	Σ	Max	Dat.	≤	<	<	IV	IV	IV	<	>	IV	IV	IV	IV	
<b>KRALJEVO</b>																					
BR. ST. 196																					
I	6.5	7.7	7.2	7.2	0.677.1	0.4	3	85	68	79	78	32	0.50	0.13.9	18	02	02	19	*	*	
II	7.6	8.1	6.0	7.3	0.79.9	0.5	5.5	83	62	72	72	28	0.61	0.19.0	15	*	*	07	01	*	
III	5.9	6.2	4.3	5.5	1.72.5	0.5	7	82	49	66	66	19	0.56	0.18.0	14	*	*	07	02	*	
IV	6.9	7.6	4.6	6.3	1.72.0	0.6	4	83	53	69	68	26	0.71	0.18.4	16	*	*	03	04	*	
V	6.8	7.2	6.5	6.8	1.94.4	0.9	6	82	53	73	69	27	0.60	0.09.8	28	*	*	12	*	*	
VI	5.1	6.0	5.6	5.6	2.31.6	1.1	4	82	46	77	68	28	0.50	0.12.7	03	*	*	19	07	*	
VII	5.3	5.9	6.0	4.9	2.43.1	1.3	3	83	49	78	73	37	1.13	0.27.2	23	*	*	22	05	*	
VIII	4.2	4.6	3.8	4.2	2.34.8	1.2	6	81	51	78	72	34	0.50	0.18.8	15	*	*	24	03	*	
IX	6.3	6.5	5.3	6.5	1.75.4	0.8	9	88	72	76	72	32	0.67	0.24.5	21	*	*	02	11	01	
X	6.2	4.5	4.0	4.9	1.59.7	0.7	5	92	53	79	74	29	0.22	0.13.2	03	*	*	01	01	*	
XI	7.4	7.5	6.3	7.1	0.58.2	0.6	6	91	70	86	82	38	0.51	0.09.1	24	*	*	03	07	12	
XII	8.9	7.5	7.2	7.9	0.37.1	0.3	7	89	79	86	84	55	0.78	0.23.4	30	*	*	14	23	*	
GOD.	6.4	6.5	5.6	6.2	1.826.4	0.8	0	85	57	76	73	19	729	0.27.2	23.VII	05	16	68	95	16	
<b>VRNJACKA BANJA</b>																					
BR. ST. 197																					
I	6.5	7.2	5.8	6.5	0.92.6	0.4	2	90	68	85	81	29	0.64	0.19.7	18	02	02	22	*	*	
II	7.4	7.6	6.0	7.0	0.93.8	0.5	5	89	64	74	78	77	0.65	0.19.9	19	*	*	08	02	*	
III	5.2	5.9	3.5	4.9	1.57.3	0.5	6	86	49	72	69	17	0.65	0.19.5	04	*	*	08	02	*	
IV	6.7	6.6	3.6	5.6	1.76.5	0.6	2	84	52	75	70	23	0.68	0.13.1	16	*	*	05	02	*	
V	6.3	6.5	6.3	6.4	2.07.8	10	2	86	59	84	76	33	0.63	0.20.2	28	*	*	10	*	*	
VI	4.7	5.1	5.0	4.9	2.49.4	-	-	-	-	-	-	-	0.75	0.23.4	26	*	*	16	03	*	
VII	4.5	4.5	5.5	4.8	2.49.1	13	2	85	59	83	76	33	1.42	0.23.7	23	*	*	20	04	*	
VIII	3.9	4.6	2.6	3.7	2.54.2	-	-	-	-	-	-	-	0.46	0.14.4	12	*	*	23	02	*	
IX	5.1	5.4	4.4	5.3	1.79.3	-	-	-	-	-	-	-	0.55	0.14.3	19	*	*	02	10	*	
X	5.1	5.4	3.7	4.4	1.73.7	-	-	-	-	-	-	-	0.28	0.14.7	03	*	*	01	04	*	
XI	6.5	7.1	6.8	6.9	0.82.4	0.6	5	92	69	90	84	31	0.50	0.11.0	24	*	*	06	03	*	
XII	8.7	7.7	7.3	7.9	0.43.1	0.3	6	89	77	89	85	54	0.87	0.22.3	31	*	*	31	14	*	
GOD.	6.0	6.0	5.0	5.7	1.929.8	-	-	-	-	-	-	-	808	0.32.7	23.VII	08	16	78	83	09	
<b>ALEKSANDROVAC</b>																					
BR. ST. 198																					
I	4.9	5.7	5.1	4.5	-	-	-	-	-	-	-	-	0.56	0.14.0	18	05	03	25	*	*	
II	5.9	5.1	6.3	5.1	-	-	-	-	-	-	-	-	0.36	0.09.0	15	*	*	11	*	*	
III	4.6	5.6	4.6	4.0	-	-	-	-	-	-	-	-	0.38	0.12.0	04	*	*	12	02	*	
IV	5.1	5.1	4.3	3.7	-	-	-	-	-	-	-	-	0.49	0.18.5	16	*	*	05	01	*	
V	4.7	5.1	4.3	3.5	-	-	-	-	-	-	-	-	0.61	0.17.0	28	*	*	08	01	*	
VI	3.5	3.8	4.7	3.2	-	-	-	-	-	-	-	-	0.43	0.18.9	26	*	*	16	03	*	
VII	2.8	1.0	3.4	2.4	-	-	-	-	-	-	-	-	0.48	0.08.2	11	*	*	16	04	*	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	0.37	0.14.8	15	*	*	20	04	*	
IX	5.0	1.9	4.2	3.7	-	-	-	-	-	-	-	-	0.45	0.09.4	19	*	*	03	10	*	
X	-	-	-	-	-	-	-	-	-	-	-	-	0.26	0.14.2	03	*	*	02	02	*	
XI	4.6	3.9	5.3	4.6	-	-	-	-	-	-	-	-	0.53	0.08.2	24	*	*	01	10	*	
XII	7.2	5.8	7.0	6.7	-	-	-	-	-	-	-	-	0.65	0.14.8	31	*	*	17	28	*	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	557	0.18.9	26.VII	11	21	94	73	12	
<b>REKOVAC</b>																					
BR. ST. 199																					
I	6.6	6.3	6.2	6.3	-	-	-	-	-	-	-	-	0.44	0.89	70	83	81	37	0.65	0.22.8	
II	5.9	5.9	5.9	5.7	-	-	-	-	-	-	-	-	0.56	0.88	62	81	77	32	0.76	0.18.7	
III	4.5	4.6	4.2	4.5	-	-	-	-	-	-	-	-	0.59	0.85	50	78	71	21	0.53	0.18.3	
IV	5.1	6.0	4.4	5.2	-	-	-	-	-	-	-	-	0.65	0.81	54	79	72	29	0.79	0.22.8	
V	5.1	5.1	6.0	5.4	-	-	-	-	-	-	-	-	10.0	80	55	81	72	29	0.93	0.18.3	
VI	3.9	3.9	3.7	3.7	-	-	-	-	-	-	-	-	0.51	0.87	35	73	65	35	0.76	0.17.3	
VII	3.5	3.9	3.7	3.7	-	-	-	-	-	-	-	-	12.0	82	52	82	72	34	0.92	0.03.2	
VIII	3.3	4.1	4.1	3.9	-	-	-	-	-	-	-	-	12.7	86	53	86	75	37	0.94	0.17.7	
IX	5.1	4.9	4.9	4.9	-	-	-	-	-	-	-	-	0.90	89	57	85	77	32	0.43	0.14.0	
X	4.2	3.9	3.5	3.8	-	-	-	-	-	-	-	-	0.75	91	56	88	79	30	0.19	0.10.3	
XI	7.0	7.0	6.0	6.7	-	-	-	-	-	-	-	-	12.6	12.0	85	49	78	71	31	0.63	0.16.5
XII	8.3	7.4	7.4	7.7	-	-	-	-	-	-	-	-	12.6	97	70	89	84	41	0.038	0.08.6	
GOD.	5.2	5.3	5.2	5.2	-	-	-	-	-	-	-	-	24.0	86	52	82	74	70	36	0.043	0.15.6
<b>SVETOZAREVO</b>																					
BR. ST. 200																					
I	6.4	6.5	6.1	6.3	-	-	-	-	-	-	-	-	0.41	0.09.9	18	02	03	20	*	*	
II	7.0	7.5	7.0	7.2	-	-	-	-	-	-	-	-	0.59	0.08.2	15	*	*	05	07	*	
III	5.3	5.5	4.0	5.0	-	-	-	-	-	-	-	-	0.64	0.04.4	04	*	*	02	02	*	
IV	6.6	7.1	5.8	6.5	-	-	-	-	-	-	-	-	0.64	0.02.0	16	*	*	03	02	*	
V	6.4	5.1	6.1	5.9	-	-	-	-	-	-	-	-	0.59	0.07.2	29	*	*	14	01	*	
VI	6.4	4.5	6.0	5.6	-	-</															

Mesec	Vazdušni prstenski Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра nD, Pm (0-12)																	
		Tm			Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW					
		7	14	21						8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.				
$\gamma = 43^{\circ}08' N \lambda = 21^{\circ}16' E$ Gr. $\Delta G = + 1h 25 min.$																													
I	-	-01.9	05.5	00.6	01.2	06.3	-03.3	14.9	30 -15.5	20	07	01.9	08	01.5	01	01.0	03	02.0	16	02.3	33	01.3	01	02.0	13	01.0	11		
II	-	03.8	11.3	06.3	06.9	12.2	02.1	23.2	23 -05.4	05	12	01.8	09	01.1	03	02.7	19	04.6	26	01.8	02	01.0	05	01.2	09				
III	-	03.2	14.5	07.2	08.0	15.5	01.5	26.7	24 -36.5	03	10	01.5	11	01.9	03	01.7	02	02.0	12	03.2	34	01.3	01	01.0	07	02.0	13		
IV	-	05.4	15.3	08.3	09.4	16.7	02.6	26.6	30 -03.0	13.12	17	01.9	08	02.1	*	*	02	04.0	03	02.7	36	01.4	02	01.0	09	01.7	13		
V	-	12.4	21.0	13.5	15.1	22.5	08.4	31.0	20	03.2	30	07	01.9	09	01.8	01	02.0	07	01.6	06	01.5	28	01.3	01	01.0	08	01.8	26	
VI	-	15.4	23.3	15.6	17.5	24.8	10.7	31.9	19	02.0	05	07	01.6	14	01.6	*	*	05	01.4	07	01.6	28	01.2	*	*	07	01.7	22	
VII	-	17.1	25.7	18.0	19.7	27.0	13.3	34.1	31	08.7	01	11	01.6	12	01.5	*	*	05	01.6	07	02.1	27	01.3	01	01.0	10	01.3	20	
VIII	-	15.7	26.1	16.8	18.9	27.7	12.0	34.6	22	07.1	27	03	01.4	13	01.5	02	01.5	03	02.0	08	02.1	33	01.5	*	*	05	01.6	21	
IX	-	10.3	20.5	12.1	13.8	21.4	08.3	30.2	09	-03.9	30	13	01.8	16	01.2	01	01.0	02	01.0	*	*	23	01.2	01	01.0	07	01.4	27	
X	-	04.9	18.1	08.4	09.9	18.8	03.4	25.3	09	-02.0	18	08	01.5	12	01.3	*	*	03	01.7	06	02.0	37	01.4	*	*	04	01.0	23	
XI	-	05.2	12.2	06.6	07.7	13.7	03.0	24.0	12	-03.5	28	05	01.0	04.0	04.5	04	01.5	05	02.4	12	02.5	19	01.7	*	*	06	01.2	33	
XII	-	-02.9	00.8	-02.3	-01.7	01.7	-05.0	11.8	29	-13.2	14	21	01.2	23	01.4	02	02.0	03	03.0	17	01.2	*	*	07	01.3	15			
GOD.	-	07.4	16.2	09.2	10.5	17.4	04.8	34.6	22.VII	-15.5	20.I	126	01.6	140	01.5	14	01.6	43	02.0	101	01.2	28	342	01.4	09	01.1	88	01.4	233
$\gamma = 43^{\circ}34' N \lambda = 21^{\circ}21' E$ Gr. $\Delta G = + 1h 25 min.$																													
I	-	-01.5	05.4	00.7	01.3	06.5	-03.4	16.0	30 -18.4	20	02	02.5	04	02.8	11	03.6	05	03.8	05	04.0	01	05.0	02	03.5	*	*	63		
II	-	04.0	11.2	06.5	07.0	12.7	02.2	24.2	23 -05.6	05	09	03.8	04	04.0	04	02.8	04	03.8	11	04.4	02	04.5	02	06.0	03	04.3	45		
III	-	04.6	14.9	08.7	09.2	16.0	02.9	28.5	23 -03.7	01	03	02.7	03	03.0	11	03.5	05	03.2	10	04.7	01	03.0	10	03.7	01	04.0	49		
IV	-	06.2	15.5	09.0	10.3	16.8	03.7	26.4	29 -02.0	22	05	04.4	02	03.0	07	02.8	*	*	05	03.4	03	04.7	13	03.9	05	03.8	50		
V	-	13.3	22.0	15.8	16.7	23.1	10.1	30.2	20	05.3	30	25	06	02.8	02	02.5	08	02.4	02	03.0	07	02.3	*	*	08	02.8	05	03.2	55
VI	-	16.1	24.4	17.5	18.9	25.6	12.4	32.4	14	03.6	05	06	03.3	02	02.5	01	03.0	01	02.0	06	02.9	02	02.5	07	02.4	04	03.0	61	
VII	-	17.8	25.7	18.4	20.6	25.0	14.0	33.6	31	10.3	07	11	02.9	03	03.0	04	02.0	01	02.0	09	02.1	01	02.0	04	02.8	03	03.2	56	
VIII	-	16.1	26.4	19.1	20.2	27.7	13.4	33.8	22	07.6	27	06	03.2	02	02.5	03	04.0	01	03.0	05	02.8	01	02.0	06	03.2	03	03.0	66	
IX	-	10.4	20.2	13.3	14.3	21.2	08.6	30.6	09	-02.7	30	14	02.8	04	02.8	04	03.2	*	*	04	02.2	*	*	*	06	03.2	03	03.3	55
X	-	05.7	17.5	09.3	10.5	18.6	04.1	25.6	01	-01.6	18	02	02.0	04	03.0	08	02.9	02	03.0	*	*	*	04	03.0	*	*	73		
XI	-	05.2	12.0	06.2	07.4	13.2	03.2	21.7	12	-03.8	30	06	03.5	02	02.5	07	02.1	01	02.0	03	03.3	*	*	01	02.0	02	03.5	68	
XII	-	-02.5	00.2	-02.2	-01.7	01.1	-04.2	09.9	29	-14.6	06	03	02.3	09	02.3	11	02.5	03	02.0	05	02.7	01	02.0	06	02.7	03	02.0	58	
GOD.	-	08.0	16.3	10.4	11.2	17.5	05.6	35.6	34.VII	-18.4	20.I	73	03.1	41	02.8	79	02.9	23	03.2	67	03.1	11	04.0	69	03.3	33	03.3	699	
$\gamma = 43^{\circ}56' N \lambda = 21^{\circ}23' E$ Gr. $\Delta G = + 1h 25 min.$																													
I	-	752.9	-00.3	04.6	01.1	01.6	05.7	-02.1	17.0	30 -14.0	19	02	02.0	01	02.0	19	03.1	40	02.6	13	02.0	*	*	04	01.8	06	01.8	08	
II	749.5	03.8	10.8	06.6	12.0	12.9	01.9	23.8	23 -06.7	05	01	02.0	*	*	01	01.0	22	01.9	16	02.2	*	*	04	01.5	24	02.1	16		
III	754.3	05.3	14.3	08.3	09.0	15.4	03.2	28.6	24 -05.8	03	03	01.0	01	01.0	01	02.3	30	02.5	13	02.2	*	*	07	01.9	17	02.1	12		
IV	748.7	06.7	15.0	09.1	10.0	16.6	03.6	25.8	29 -03.7	13	03	01.8	01	01.0	05	02.6	15	02.6	13	02.1	*	*	12	02.1	20	02.4	21		
V	750.5	14.1	22.0	15.8	16.9	23.3	10.8	30.6	21	02.8	30	05	01.8	*	*	06	02.2	22	02.1	10	01.7	03	01.3	07	01.4	18	01.9	22	
VI	748.8	16.5	25.0	17.1	18.9	26.3	11.6	33.0	14	02.1	34	01	02.1	05	01.5	05	02.4	05	01.6	05	01.4	08	01.9	21	01.9	27			
VII	748.8	17.8	25.6	18.7	20.2	26.8	14.1	34.0	31	09.4	15	01.0	01.1	02.0	01	01.5	07	01.9	14	02.0	06	01.8	05	01.2	08	01.8	23		
VIII	749.2	16.7	26.6	19.8	27.7	13.1	31.7	10	05.9	26	04	01.8	01	03.0	05	02.0	15	02.2	09	01.7	01	02.0	06	01.8	16	02.2	26		
IX	753.9	10.7	20.5	12.4	14.0	21.2	08.3	31.2	09	-03.3	30	05	02.0	01	02.0	08	02.1	07	02.1	05	01.8	02	01.5	05	02.0	26	02.1	31	
X	755.5	07.1	17.9	05.8	10.6	18.6	04.6	25.8	08	-03.0	18	04	01.8	*	*	06	01.5	21	02.0	15	01.8	02	01.0	02	01.5	11	01.8	32	
XI	749.6	05.8	11.7	06.2	07.5	13.1	03.3	22.3	04	-05.1	30	04	01.8	*	*	04	01.2	23	01.8	14	02.0	*	*	02	01.5	21	02.0	22	
XII	750.6	-02.3	00.2	-01.9	-01.5	01.3	-03.8	08.5	29	-13.1	06	13	01.7	03	01.7	05	02.4	22	02.2	13	01.9	*	*	*	*	23	02.0	14	
GOD.	-	07.5	16.3	09.9	10.9	17.5	05.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\gamma = 43^{\circ}14' N \lambda = 21^{\circ}36' E$ Gr. $\Delta G = + 1h 26 min.$																													
I	-	-01.1	05.1	01.0	0																								

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha em mm	Padavine R mm mm 7 14 21 Sred. (Dnev) Inselektija Broj sati	Vlažnost vazduha U m s		Broj dana na sat																														
	Tn	Tx	Tn			7	14	21	Sred. (Dnev) Min	Σ	Max	Dat.	30.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.00.0.0	•	Δ	*	Δ	Δ	Δ	Δ										
	7	14	21			7	14	21	Sred. (Dnev) Min	Σ	Max	Dat.	30.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.00.0.0	•	Δ	*	Δ	Δ	Δ	Δ										
KURSUMLIJA																																						
BR. ST. 201																																						
I	6.4	6.7	5.5	6.2	053.7	04.2	90	65	87	81	43	038	008.7	25	04	01	22	•	•	01	04	09	12	09	•	09	04	•	•	•	01	11						
II	6.5	6.2	6.0	6.0	054.5	05.3	83	56	77	72	22	041	012.8	15	•	•	08	•	•	07	02	10	12	13	10	01	12	03	•	•	•	01	•					
III	5.2	5.2	2.9	6.4	159.4	05.4	86	48	73	69	19	031	008.9	14	•	•	12	02	•	02	10	07	11	08	•	08	04	01	•	•	02							
IV	6.2	6.5	3.7	5.5	156.3	06.0	81	47	74	68	28	048	021.0	16	•	•	10	03	•	02	03	09	04	02	09	•	•	•	01	01	01							
V	5.3	5.4	4.5	5.0	166.8	08.9	80	48	80	69	27	069	021.9	28	•	•	12	01	•	•	05	05	10	09	03	10	•	•	01	04	•							
VI	4.8	4.6	4.5	4.8	184.5	10.8	78	49	84	70	29	066	032.1	23	•	•	17	02	•	•	07	05	10	07	02	10	•	•	01	09	•							
VII	3.8	3.9	3.9	3.9	231.3	12.2	81	52	83	72	23	093	027.5	11	•	•	23	07	01	•	10	04	11	08	03	11	•	•	03	09	01							
VIII	2.4	3.4	2.3	2.7	231.3	11.4	81	47	84	70	23	024	009.2	15	•	•	26	06	•	01	•	16	•	08	04	•	08	•	•	06	•							
IX	5.8	4.3	4.2	4.8	164.0	08.5	87	47	80	71	14	019	007.2	19	•	•	02	12	01	•	•	08	07	09	05	•	09	•	•	01	•							
X	4.6	3.5	2.5	3.5	154.7	06.8	91	49	85	75	23	032	017.7	03	•	•	04	02	•	•	13	03	05	03	01	05	•	01	04	•								
XI	6.6	6.7	6.2	6.5	074.6	06.2	88	67	85	78	29	066	012.6	24	•	•	05	•	•	01	01	03	10	15	11	02	11	07	02	01	01	05						
XII	8.3	7.4	7.2	7.6	036.0	03.5	86	73	87	82	50	076	031.3	30	06	14	26	•	•	•	04	21	14	08	03	10	07	01	•	•	21							
GOD.	5.4	5.4	4.4	5.1	1608.9	07.4	84	54	82	73	14	603	032.1	25	VII	10	15	89	97	17	01	14	03	87	91	127	86	17	112	25	04	•	01	01	04	33	08	39
KRUSEVAC																																						
BR. ST. 202																																						
I	6.4	7.3	5.2	6.4	065.8	04.3	92	65	88	82	33	061	011.9	18	04	03	22	•	•	08	01	11	14	12	08	06	08	•	•	02	09							
II	7.1	8.1	5.9	7.0	074.6	05.6	90	59	82	77	21	056	013.7	15	•	•	07	•	•	11	03	02	13	13	08	01	12	03	•	01	•							
III	5.7	5.6	3.8	5.3	169.3	05.8	92	75	71	81	18	058	015.0	04	•	•	12	03	•	•	15	02	09	10	10	08	03	08	03	•	01							
IV	6.9	7.4	4.8	6.4	165.6	06.4	90	48	75	71	19	065	016.7	16	•	•	06	03	•	•	18	03	09	12	08	03	12	01	01	01								
V	5.9	6.7	5.8	6.1	206.3	09.6	87	45	78	70	17	118	036.8	06	•	•	13	01	•	07	•	04	10	17	13	05	17	•	•	01	01	07	01					
VI	5.3	5.2	5.1	5.2	231.0	11.4	86	41	85	71	24	068	020.4	28	•	•	18	05	•	08	•	06	05	14	10	02	14	•	•	11	•	•						
VII	4.2	4.8	4.4	4.5	257.0	13.4	88	50	88	76	29	120	025.4	02	•	•	22	09	•	09	•	05	06	12	11	04	12	•	•	09	01	•						
VIII	4.6	4.7	3.1	3.7	246.1	12.2	90	41	84	72	28	031	013.8	15	•	•	26	08	•	10	•	12	02	09	06	01	09	•	•	05	01	•						
IX	6.4	6.1	4.4	5.6	175.1	08.6	91	43	81	73	23	042	018.7	19	•	•	02	11	01	•	06	•	05	09	09	07	01	09	•	•	02	01						
X	4.6	4.1	3.1	3.6	163.0	07.0	96	46	90	78	19	027	015.4	03	•	•	05	03	•	•	10	04	04	03	01	04	•	•	01	05	•							
XI	7.3	7.4	6.0	6.0	071.5	06.5	91	61	93	83	29	051	010.2	24	•	•	05	•	•	02	13	15	11	01	13	03	01	•	•	07	02							
XII	9.0	7.7	7.6	8.1	030.8	03.6	86	76	89	85	44	082	023.7	30	04	16	24	•	•	02	22	14	09	03	09	07	•	•	•	01	19							
GOD.	6.0	6.0	5.0	5.7	1856.8	07.9	90	51	84	75	17	779	036.8	06	V	08	19	83	99	24	•	100	05	63	114	143	106	27	127	25	02	•	01	01	36	20	28	
CUPRIJA																																						
BR. ST. 203																																						
I	7.0	7.5	6.6	7.0	087.1	04.3	86	71	84	80	44	062	004.2	25	03	01	20	•	•	13	01	02	12	16	12	11	08	03	•	•	•	02	10					
II	6.6	8.0	5.6	6.0	076.5	05.8	89	53	76	72	26	061	017.6	15	•	•	08	•	•	09	03	11	14	10	04	13	03	01	•	•	01	01						
III	5.5	5.4	4.0	4.9	176.0	05.8	83	52	75	70	22	077	026.2	04	•	•	09	02	•	•	11	01	10	10	11	09	04	05	03	01	•							
IV	6.7	7.5	4.7	6.3	173.9	06.5	83	54	78	72	26	078	027.9	16	•	•	07	02	•	•	14	03	11	15	10	02	15	•	•	01	01							
V	5.9	6.4	5.7	6.0	236.1	09.5	77	49	74	67	28	038	004.4	29	•	•	14	02	•	07	•	04	06	05	07	07	01	•	•	07	01							
VI	4.9	5.2	5.0	5.0	268.0	11.5	82	47	82	70	25	096	028.0	26	•	•	22	08	•	03	•	07	07	14	12	03	14	•	•	10	•	02						
VII	5.3	6.4	4.4	4.6	257.5	13.6	87	57	85	76	30	095	024.6	02	•	•	22	08	•	08	01	08	09	14	10	03	14	•	•	08	02							
VIII	3.8	4.2	2.9	3.6	269.2	12.4	87	47	82	72	33	016	003.9	02	•	•	26	07	•	10	01	12	03	11	07	•	•	05	01	•								
IX	5.5	5.4	3.6	4.8	181.6	09.1	91	52	83	75	31	059	024.6	21	•	•	04	11	01	•	06	•	08	07	12	06	02	12	•	•	01	03						
X	4.3	4																																				

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Mesec	Vrednost pritisk Pn mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, Pm (0-12)																							
		Tm				Max		Min		Dat.		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnes)					Dat.			Dat.			E.	J.	E.	J.	E.	J.												
$\gamma = 43^{\circ}20' N \lambda = 21^{\circ}54' E$ Gr. $\Delta G = + 1h 26 min.$																																	
I	746.4	-00.3	05.2	01.9	02.2	06.2	-01.7	15.7	30	-13.2	20	02	03.0	02	03.5	24	01.8	10	01.5	02	02.0	03	02.7	05	01.2	10	01.3	35					
II	742.9	04.4	11.3	07.3	07.6	12.6	03.3	23.2	23	-04.8	05	01	01.0	01	01.2	01	01.2	07	01.6	13	02.3	06	02.0	05	01.2	18	02.4	29					
III	747.5	05.1	14.9	09.3	09.7	16.0	04.0	28.6	24	-04.4	01	02	03.0	02	03.0	24	01.7	07	01.4	07	02.0	07	01.0	05	01.0	13	02.0	28					
IV	742.0	07.0	15.6	10.1	10.7	16.9	04.7	26.1	24	-01.6	12	02	03.0	02	02.9	19	01.5	05	01.4	07	02.0	02	01.5	10	02.2	21	02.0	26					
V	743.8	14.2	22.9	16.3	17.4	23.7	11.4	31.0	20	05.5	12	07	01.6	01	02.0	18	01.8	36	01.3	06	01.5	02	01.5	04	01.0	18	01.7	31					
VI	742.1	16.5	24.4	18.2	19.1	25.6	19.3	31.8	14	04.9	05	06	01.2	01	01.0	11	01.0	01	01.0	04	01.2	02	01.5	07	01.9	45							
VII	742.1	18.2	26.4	20.0	21.1	27.4	15.4	35.9	31	11.9	13	09	01.9	01	03	01.3	05	01.4	06	01.2	04	01.2	07	02.0	32	01.8	32						
VIII	742.6	17.0	27.1	19.1	20.6	28.1	14.3	35.2	22	08.4	24	03	02.0	02	01.0	17	01.5	03	01.3	01	01.0	03	02.0	07	01.3	11	01.9	46					
IX	746.8	11.5	20.4	14.1	15.0	21.7	10.0	30.9	09	-02.0	30	02	02.0	07	02.4	19	01.6	01	01.0	01	02.0	07	02.1	35									
X	748.8	06.6	17.7	10.6	11.4	18.9	05.5	26.4	09	-00.5	18	02	02.0	03	01.7	17	02.1	01	01.0	04	01.2	07	01.7	56									
XI	742.9	06.3	12.5	07.0	07.8	13.5	04.3	23.8	08	-00.9	30.23	02	01.5	01	02.5	04	01.5	06	02.3	02	01.5	06	01.2	11	01.4	48							
XII	749.7	-02.2	00.0	-02.0	-01.5	01.0	-04.1	08.6	29	-11.0	06	06	01.3	01	03.0	12	02.8	05	01.8	01	03	01.0	03	23	02.4	43							
GOD.	744.8	08.7	16.5	11.0	11.8	17.6	06.7	35.9	34.VII	-13.2	20.1	42	01.7	20	02.3	180	01.8	54	01.5	44	01.9	37	01.5	56	01.4	208	02.0	454					
$\gamma = 43^{\circ}01' N \lambda = 21^{\circ}57' E$ Gr. $\Delta G = + 1h 26 min.$																																	
I	744.6	-01.3	04.8	00.8	01.3	05.7	-03.2	15.3	30	-16.9	20	08	02.9	01	03	01.3	11	01.5	04	01.7	02	01.5	06	01.3	02	02.0	07	01.0	47				
II	741.3	03.8	10.9	06.2	06.8	12.0	02.2	23.0	23	-08.0	05	13	02.7	01	01.0	01	01.0	12	01.9	11	01.5	11	01.9	03	02.3	01	01.0	31					
III	745.7	03.8	14.6	08.4	08.8	15.8	02.5	27.8	24	-04.2	01	10	02.8	01	01.0	03	01.3	16	01.8	04	01.2	10	02.1	06	01.8	06	02.7	37					
IV	740.4	05.8	15.7	10.1	10.4	17.3	03.3	28.5	30	-03.2	22	16	02.9	02	01.5	07	01.7	04	02.5	07	01.6	08	02.9	11	03.1	34							
V	742.2	13.2	22.4	15.3	16.6	23.4	09.8	30.6	21	03.0	12	06	01.7	01	01.0	02	01.0	09	01.9	06	01.7	20	01.8	05	01.8	14	02.4	30					
VI	740.5	15.7	23.8	17.6	18.7	25.5	11.9	31.6	14	03.4	05	07	02.3	03	01.7	01	01.0	07	01.6	07	02.0	09	02.2	17	01.9	38							
VII	740.4	17.6	26.8	20.1	21.1	27.9	14.2	35.5	31	09.6	07	19	02.6	01	03.0	01	02.0	01	01.7	09	02.0	07	02.0	15	02.1	31							
VIII	741.0	15.7	27.2	18.9	20.2	26.3	12.5	36.0	22	06.5	26	12	02.6	02	03.0	03	02.0	03	01.7	09	03.8	05	03.8	04	02.0	05	05						
IX	745.0	10.2	21.0	13.5	14.5	22.0	08.4	30.0	09	-03.8	30	18	02.8	02	03.0	03	01.7	04	01.8	03	01.0	04	01.5	06	02.3	07	02.4	43					
X	747.1	04.5	17.9	09.4	10.3	18.9	03.2	25.9	09	-02.1	18.01	10	01.8	08	01.8	05	01.8	08	02.0	08	01.6	05	01.6	05	01.2	07	02.1	53					
XI	741.3	05.0	12.5	07.1	07.9	13.6	03.3	22.9	12	-01.6	25	11	02.1	01	01.0	05	02.1	04	02.2	02	01.0	03	02.0	05	01.9	05	02.0	50					
XII	747.8	-02.8	00.2	-02.4	-02.0	00.7	-04.8	08.1	01	-13.7	06	14	02.3	04	02.7	02	03.0	07	01.9	03	01.7	02	01.5	04	01.8	09	01.9	48					
GOD.	743.1	07.6	16.4	10.4	11.2	17.6	05.3	36.0	21.VII	-16.9	20.1	144	02.5	17	02.1	26	01.7	90	01.8	68	01.7	92	01.9	65	02.1	96	02.3	497					
$\gamma = 43^{\circ}34' N \lambda = 22^{\circ}16' E$ Gr. $\Delta G = + 1h 29 min.$																																	
I	-	-03.9	02.4	-02.2	-01.5	03.6	-06.3	16.0	30	-21.5	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	03.1	10.9	05.0	06.1	12.2	01.8	22.0	23	-06.8	05	13	02.7	01	01.0	01	01.0	12	01.9	11	01.5	11	01.9	03	02.3	01	01.0	31					
III	-	02.5	13.7	06.8	07.4	14.9	01.0	29.5	24	-04.5	01	10	02.8	01	01.0	03	01.3	16	01.8	04	01.2	10	02.1	06	01.8	06	02.7	37					
IV	-	05.2	15.5	08.4	09.4	16.9	03.0	25.6	29	-03.6	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
V	-	12.6	22.7	14.5	16.1	23.8	08.7	31.6	21	02.5	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
VI	-	15.5	24.5	16.9	18.5	26.1	11.3	32.5	14	02.8	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
VII	-	17.9	26.7	18.7	20.3	28.1	13.2	35.5	31	09.5	14.13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
VIII	-	14.0	26.8	18.1	19.9	27.4	12.3	32.5	29	07.8	27	13	02.0	19	02.3	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
IX	-	10.8	20.5	14.0	14.3	21.7	08.6	31.0	09	-05.0	30	04	02.0	20	02.4	06	02.7	07	02.1	06	02.2	49	01.9	05	02.0	02	03.0						
X	-	04.9	17.6	08.5	09.9	18.5	02.9	25.7	01	-03.7	18	04	02.2	26	02.3	08	02.5	02	02.5	05	02.4	45	01.9	03	02.0	*	*						
XI	-	05.2	12.1	05.5	07.4	13.1	02.7	25.4	12	-05.2	30	05	02.6	17	02.5	03	02.0	02	01.5	11	02.8	47	02.4	02	03.0	02	01.5	01					
XII	-	-05.0	00.2	-04.3	-03.0	01.0	-08.2	09.3	14	-20.0	25	04	02.2	21	03.0	06	02.5	02	02.0	10	02.9	43	02.5	02	02.5	05	02.2	*					
GOD.	-	07.3	15.7	09.3	10.4	16.8	04.2	34.1	09.VII	-23.5	49.1	60	02.2	253	02.5	52	02.5	33	02.3	69	02.3	530	02.2	45	02.6	52	02.9	01					
$\gamma = 43^{\circ}04' N \lambda = 22^{\circ}26' E$ Gr. $\Delta G = + 1h 29 min.$																																	





Meseč	Oblačnost Nm (0-10)	Inovačija broj sati (tijek)	Vlažnost vazduha						Padavine R mm		Broj dana na sat																						
			Ljuna			Srednji (tijek) Min			Tn		Tx		Tx		Tn		F(0-12)		Nm(0-10)		R mm		•	*	*	Δ	Δ	Δ	Δ	R	T	≡	☒
			mm	7	14	21	Sred.	(tijek)	Min	Σ	Max	Dat:	≤	<	<	IV	IV	IV	IV	<	>	IV	IV	IV	IV	IV	IV	IV	IV	IV			
<b>PIROT</b>																																	
BR. ST. 211																											$H_s = 370 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$						
I 5.3 5.1 5.1 5.1	-	-	-	-	-	-	-	-	-	036 013.3	17	06	02	23	.	.	.	.	05	06	10	06	01	08	04	01	.	.	.	01	07		
II 6.1 6.5 6.2 6.3	-	-	-	-	-	-	-	-	-	065 021.2	03	.	01	09	.	.	.	.	01	09	14	11	02	12	04	.	.	.	01	03			
III 4.8 5.1 4.6 4.9	-	-	-	-	-	-	-	-	-	065 025.2	04	.	.	09	02	.	.	.	05	05	10	07	02	08	03	.	.	.	02	.			
IV 5.4 5.4 4.4 5.1	-	-	-	-	-	-	-	-	-	044 012.1	17	.	.	07	02	.	.	.	07	03	05	09	01	09	02	01	.	.	.	.	.		
V 5.0 5.1 2.6 4.3	-	-	-	-	-	-	-	-	-	094 031.3	28	.	.	13	02	.	.	.	07	04	09	09	03	09	.	.	.	.	02	01			
VI 3.9 5.1 3.4 4.1	-	-	-	-	-	-	-	-	-	108 027.0	03	.	.	15	02	.	.	.	07	03	10	09	05	10	.	.	.	01	07	01			
VII 5.3 4.0 4.5 4.6	-	-	-	-	-	-	-	-	-	050 020.0	11	.	.	22	06	.	.	.	11	04	09	09	02	07	.	.	.	07	.	.			
VIII 3.8 4.5 2.8 3.7	-	-	-	-	-	-	-	-	-	047 021.0	25	.	.	25	07	.	.	.	10	02	03	05	02	03	.	.	.	04	.	.			
IX 5.5 5.3 4.6 5.2	-	-	-	-	-	-	-	-	-	030 010.6	23	.	.	02	14	.	.	.	06	05	05	05	01	05	.	.	.	03	02	.			
X 5.4 3.0 3.8 4.1	-	-	-	-	-	-	-	-	-	006 005.5	04	.	.	07	01	.	.	.	08	04	01	01	01	01	.	.	.	04	.	.			
XI 7.7 6.5 7.2 7.1	-	-	-	-	-	-	-	-	-	066 018.2	27	.	.	06	.	.	.	.	02	13	11	11	02	10	05	02	.	.	01	01	01		
XII 8.0 7.5 7.6 8.0	-	-	-	-	-	-	-	-	-	067 023.0	31	04	11	24	.	.	.	.	02	22	11	09	02	08	05	.	.	.	01	06	.		
GOD. 5.6 5.3 4.7 5.2	-	-	-	-	-	-	-	-	-	678 031.3	28V	10	14	87	94	17	-	.	71	80	104	91	23	94	23	04	.	.	01	24	10	19	
<b>TOPLI DO</b>																											$H_s = 700 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$						
BR. ST. 212																											$H_s = 700 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$						
I 5.5 5.8 6.3 5.9	-	-	-	-	-	-	-	-	-	053 013.2	17	07	05	22	.	.	.	01	01	06	10	12	07	03	08	05	01	.	.	01	24		
II 7.3 7.8 6.9 7.3	-	-	-	-	-	-	-	-	-	101 018.4	07	.	01	08	.	.	.	01	01	17	14	04	13	08	02	.	.	08	.	.			
III 4.9 5.6 4.4 5.0	-	-	-	-	-	-	-	-	-	059 020.1	04	.	03	12	.	.	.	01	09	09	12	08	02	10	04	01	.	.	03	.			
IV 6.0 6.5 5.1 5.8	-	-	-	-	-	-	-	-	-	088 035.4	17	.	.	09	.	.	.	06	05	04	11	11	08	03	09	04	01	.	.	04	.		
V 5.3 6.5 4.4 5.4	-	-	-	-	-	-	-	-	-	087 025.7	28	.	.	03	.	.	.	04	08	15	10	03	15	.	.	.	01	04	.				
VI 5.5 6.8 4.3 5.5	-	-	-	-	-	-	-	-	-	101 023.6	03	.	.	06	.	.	.	02	05	12	12	04	12	.	.	.	06	.	.				
VII 4.9 4.9 4.1 4.6	-	-	-	-	-	-	-	-	-	150 054.9	05	.	.	14	01	.	.	08	05	11	11	05	11	.	.	.	10	01	.				
VIII 3.6 3.2 3.5 3.0	-	-	-	-	-	-	-	-	-	041 026.0	25	.	.	13	01	.	.	07	02	09	06	01	09	.	.	.	06	.	.				
IX 5.2 5.8 4.2 5.1	-	-	-	-	-	-	-	-	-	029 007.2	11	.	.	02	02	.	.	02	07	08	09	08	09	09	08	.	.	01	.	.			
X 3.8 3.0 2.5 3.1	-	-	-	-	-	-	-	-	-	007 003.2	04	.	.	02	.	.	.	15	04	05	02	05	03	05	04	.	.	01	.	.			
XI 7.1 6.8 5.9 6.6	-	-	-	-	-	-	-	-	-	082 025.0	27	0	01	12	.	.	.	04	14	13	13	03	10	08	05	.	.	01	04	.			
XII 6.4 6.6 6.1 6.4	-	-	-	-	-	-	-	-	-	107 033.0	30	10	15	29	.	.	.	07	16	12	08	03	08	08	04	.	.	03	19	.			
GOD. 5.5 6.0 4.7 5.4	-	-	-	-	-	-	-	-	-	906 054.9	05W	17	25	96	38	02	.	10	07	73	111	136	107	31	119	37	14	.	01	01	27	06	62
<b>DIMITROVGRAD</b>																											$H_s = 446 \text{ m } H_b = 446.8 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$						
BR. ST. 213																											$H_s = 446 \text{ m } H_b = 446.8 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$						
I 6.0 6.6 5.0 5.9	102.4	03.7	87	66	82	75	040	015.9	17	05	04	22	.	.	.	03	.	05	09	10	06	02	08	04	02	01	.	.	01	09			
II 7.1 7.9 6.3 7.1	092.3	05.2	88	59	79	76	28	040 009.7	07	01	01	08	.	.	.	06	.	02	11	16	07	01	14	04	.	.	01	04	.				
III 4.7 5.5 4.1 4.8	191.0	04.8	88	44	66	65	16	074 024.2	04	.	01	13	02	.	.	06	.	08	09	11	07	03	09	03	.	.	02	02	02				
IV 5.9 6.7 4.5 5.7	197.3	05.5	79	44	72	65	21	044 019.7	03	.	.	06	02	.	.	03	.	07	02	13	13	02	08	07	01	.	.	01	04	.			
V 5.3 6.6 3.2 4.6	242.9	08.4	79	46	76	66	21	085 033.7	28	.	.	11	.	.	.	08	.	04	08	11	06	02	11	.	.	07	.	.					
VI 4.3 5.6 3.2 4.0	259.6	10.6	85	55	82	74	34	119 030.5	03	.	.	14	.	.	.	01	.	07	02	14	12	04	14	.	.	01	14	02					
VII 4.9 3.8 3.2 4.0	206.4	12.2	85	50	82	72	33	095 031.8	11	01	.	21	05	.	.	04	.	08	11	09	02	11	.	.	06	.	.						
VIII 2.9 1.1 2.6 2.5	209.3	10.3	73	64	60	59	27	022 013.2	07	01	.	26	07	.	.	06	.	02	05	15	12	02	12	.	.	06	.	.					
IX 4.9 5.5 3.1 4.5	204.4	08.2	86	48	78	71	23	031 017.2	25	.	.	02	11	.	.	01	.	08	04	09	05	01	09	.	.	02	.	.					
X 4.7 2.8 3.0 3.5	201.7	06.2	89	44	79	71	21	007 004.6	04	.	.	06	.	.	.	04	.	14	05	04	01	04	04	.	.	05	.	.					
XI 7.6 7.1 5.8 6.2	092.9	05.9	89	64	65	79	24	078 030.5	27	.	.	07	.	.	.	02	.	01	03	14	12	09	02	06	02	.	.	04	05	.			
XII 8.1 7.5 7.2 7.6	055.3	03.4	87	77	87	84	35	061 022.6	31	05	13	25	.	.	.	01	.	03	20	17	08	01	10	12	01	02	.	.	05	11			
GOD. 5.5 5.7 4.2 5.1	2236.5	07.1	84	53	78	72	16	693 033.7	28V	11	19	89	85	11	.	36	04	87															



Mjesec	Oblačnost Nm (0-10)			Temperatura hvojsatne hrane	Vlažnost vazduha			Padavine R mm	Broj dana na sat																		
	7	14	21		e <sub>m</sub>	7	14		Tn	Tx	Tx	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	R	•	
	Sred. (Dnev.)				mm	Min.	Max.		10.00.0	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	10.0	•	Δ	*	Δ	Δ	T	•
ISTOK																											
BR. ST. 216																											
I 6.7 6.4 6.9 6.7	-	-	-	-	-	-	-	-	055	016.8	13	02	06	23	-	-	-	01	10	10	10	01	08	02	-	-	
II 6.1 6.0 5.9 6.0	-	-	-	-	-	-	-	-	074	021.0	13	-	-	08	-	-	-	04	06	11	10	03	11	-	-		
III 4.7 4.0 3.3 4.0	-	-	-	-	-	-	-	-	028	010.8	31	-	-	06	03	-	-	10	04	07	07	01	06	01	-		
IV -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	01		
V -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII -	-	-	-	-	-	-	-	-	046	015.2	15	-	-	-	-	-	-	-	07	07	02	07	-	-	-	-	
IX 5.6 5.8 4.9 5.6	-	-	-	-	-	-	-	-	046	010.8	19	-	-	01	10	-	-	03	04	08	08	01	08	-	-		
X 3.1 3.9 3.6 3.5	-	-	-	-	-	-	-	-	030	011.6	04	-	-	01	-	-	-	14	01	04	02	04	-	-	-	01	
XI 7.4 6.8 5.9 6.7	-	-	-	-	-	-	-	-	095	024.0	27	-	-	03	-	-	-	-	12	11	04	10	03	-	-	01	
XII -	-	-	-	-	-	-	-	-	034	-	01	05	24	-	-	-	-	-	-	-	-	-	-	-	03		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
KLINA																											
BR. ST. 217																											
I 8.9 7.9 7.4 8.1	-	-	-	-	-	-	-	-	060	014.5	13	01	05	22	-	-	-	02	21	13	11	02	09	07	-	-	
II 7.1 6.9 5.5 6.5	-	-	-	-	-	-	-	-	106	042.8	02	-	-	08	-	-	-	02	09	12	08	03	12	01	01	-	
III 5.1 5.2 3.7 4.6	-	-	-	-	-	-	-	-	029	014.5	31	-	-	12	04	-	-	-	-	05	03	02	05	01	01	-	
IV 5.9 6.0 4.0 5.3	-	-	-	-	-	-	-	-	088	058.6	16	-	-	05	04	-	-	05	05	09	07	02	08	01	-		
V 5.8 6.1 3.8 5.4	-	-	-	-	-	-	-	-	078	030.6	24	-	-	14	02	-	-	02	06	08	06	03	08	-	-		
VI 4.2 5.8 4.8 4.9	-	-	-	-	-	-	-	-	070	012.6	24	-	-	19	06	-	-	08	04	11	09	02	11	-	-		
VII 3.1 4.3 3.3 3.6	-	-	-	-	-	-	-	-	030	010.4	24	-	-	27	17	-	01	08	01	06	03	02	06	-	-		
VIII 3.1 4.0 2.7 3.3	-	-	-	-	-	-	-	-	064	029.2	25	-	-	29	15	-	01	12	01	05	03	02	05	-	02		
IX 4.9 5.5 5.6 5.3	-	-	-	-	-	-	-	-	030	015.6	19	-	-	02	16	01	-	05	05	07	05	01	07	-	-		
X 2.9 3.2 2.8 3.0	-	-	-	-	-	-	-	-	027	010.6	04	-	-	10	-	-	-	15	02	04	03	01	04	-	-		
XI 8.5 6.9 5.4 6.3	-	-	-	-	-	-	-	-	129	026.1	24	-	-	02	-	-	-	01	15	16	15	06	16	05	-		
XII 7.1 5.9 5.8 6.3	-	-	-	-	-	-	-	-	100	037.4	30	03	04	25	-	-	-	07	15	12	09	04	09	05	01		
GOD. 5.6 5.6 4.6 5.3	-	-	-	-	-	-	-	-	811	058.6	46.IV	04	09	86	113	41	-	-	-	108	84	30	100	20	08	-	05
DRAGAS																											
BR. ST. 218																											
I 6.5 6.3 6.5 6.4	-	-	-	-	-	-	-	-	073	029.6	28	-	04	-	-	-	03	04	12	12	02	07	07	01	-		
II 7.8 7.1 6.2 7.0	-	-	-	-	-	-	-	-	100	050.2	02	-	-	09	-	-	-	27	06	04	16	12	10	02	09		
III 5.1 5.6 4.7 5.1	-	-	-	-	-	-	-	-	04.1	63 47 62 52	16	034	019.3	14	01	02	08	-	04	08	09	06	05	01	04		
IV 5.4 6.7 4.8 5.6	-	-	-	-	-	-	-	-	04.6	67 48 62 59	25	055	016.2	16	-	01	10	-	03	03	06	09	13	10	01		
V 4.5 5.8 5.8 5.4	-	-	-	-	-	-	-	-	074	74 53 73 67	33	038	014.1	06	-	-	02	-	01	-	06	08	08	07	01		
VI 3.2 3.4 4.0 4.2	-	-	-	-	-	-	-	-	08.5	72 80 72 65	24	041	014.4	04	-	-	11	-	01	-	05	07	08	-	-		
VII 2.9 4.2 4.9 3.8	-	-	-	-	-	-	-	-	08.9	70 73 63 69	9	028	032.1	24	-	-	02	-	01	-	05	07	08	-	-		
VIII 2.7 3.1 2.9 2.9	-	-	-	-	-	-	-	-	08.8	69 45 70 61	13	058	017.4	07	-	-	11	-	01	16	03	09	06	03	04		
IX 5.4 5.4 4.4 5.9	-	-	-	-	-	-	-	-	074	85 56 74 72 30	056	015.0	19	-	-	-	-	08	07	11	08	02	11	-	-		
X 2.9 3.2 2.3 2.8	-	-	-	-	-	-	-	-	05.6	75 53 70 66	26	024	014.1	12	-	-	-	21	05	17	06	08	01	08	-		
XI 6.7 6.3 5.3 6.1	-	-	-	-	-	-	-	-	05.4	81 65 77 74	27	156	036.0	23	-	01	09	-	10	02	04	08	17	12	06		
XII 7.6 6.0 5.6 5.4	-	-	-	-	-	-	-	-	03.4	82 76 82 60	32	065	017.9	31	05	11	26	-	03	01	14	15	11	02	09		
GOD. 5.0 5.4 4.8 5.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33	16	-	126	96	24	105	40			
PRIZREN																											
BR. ST. 219																											
I 8.5 8.1 7.0 7.9	-	-	-	-	-	-	-	-	054	043.0	90	79	85	85	52	071	032.5	28	01	08	22	-	-	-	-		
II 6.9 7.2 5.7 6.6	-	-	-	-	-	-	-	-	05.6	05.4	78	56	69	68	21	093	052.4	02	-	-	03	-	-	-	-		
III 5.5 5.8 4.1 5.2	-	-	-	-	-	-	-	-	194.9	052.5	74	43	56	58	22	029	021.5	14	-	-	04	02	-	-	-		
IV 6.6 6.5 4.4 5.4	-	-	-	-	-	-	-	-	207.8	058.6	73	44	57	57	19	053	026.1	16	-	-	02	-	-	-	-		
V 5.2 5.5 4.8 5.2	-	-	-	-	-	-	-	-	08.7	82 48 68 62	52	052	021.8	28	-	-	14	04	08	01	03	-	-	-			
VI 3.2 3.4 4.3 4.0	-	-	-	-	-	-	-	-	273.7	097.9	68	42	59	56	25	065	027.8	28	-	-	22	10	01	10	-		
VII 2.4 3.5 2.6 3.7	-	-	-	-	-	-	-	-	320.3	11.1	69	40	55	51	21	049	029.5	24	-</td								

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Mesec	Vrastudni pričisk Pm mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina vетра nD, Pm (0-12)																			
		Tm			Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C			
		7	14	21						8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.		
$\gamma = 42^{\circ}39' N \lambda = 21^{\circ}09' E$ Gr. $\Delta G = + 1h 25 min.$																													
I	712.9	-02.0	02.9	-00.2	00.1	03.7	-03.3	11.7	30 -16.4	20	08	02.9	*	*	03	02.3	08	03.4	06	02.5	01	03.0	*	*	01	01.0	66		
II	710.2	03.2	10.1	05.1	06.1	11.2	02.2	20.2	25 -05.1	05	09	02.9	02	02.5	01	02.0	05	02.4	17	02.4	10	03.3	03	02.3	*	*	37		
III	714.7	03.1	13.5	07.8	08.0	14.6	01.8	26.0	24 -06.5	01	05	02.6	02	02.5	05	02.4	08	02.8	01	02.3	01	02.0	50	50					
IV	706.2	05.8	14.2	08.7	09.3	15.7	03.2	25.3	29 -03.4	13	17	02.5	02	03.0	*	*	06	02.8	06	02.0	02	04.0	06	03.3	06	02.7	45		
V	711.8	12.3	20.3	14.2	15.3	21.8	09.2	29.0	20 04.1	30	13	02.2	04	01.8	01	01.0	05	01.8	01	02.0	06	03.8	03	02.7	03	01.7	57		
VI	710.6	14.9	22.4	16.1	17.3	24.0	11.1	31.1	14 02.0	05	08	02.2	03	02.3	*	*	*	*	*	03	02.0	03	02.7	04	02.2	01	02.0	68	
VII	710.7	17.4	26.1	19.6	20.5	27.2	13.7	32.7	31 08.8	07	21	02.3	02	02.0	*	*	01	05.0	07	02.8	05	02.3	01	01.0	53				
VIII	711.2	15.5	25.4	18.6	20.6	26.8	12.5	33.9	29 06.5	26	07	02.1	05	01.4	*	*	02	01.5	07	02.6	06	03.2	04	02.8	01	02.0	61		
IX	714.3	10.7	20.2	13.6	14.5	21.2	09.2	27.8	09 -04.0	30	22	02.2	07	02.1	*	*	*	03	03.0	03	02.7	01	02.0	01	02.0	53			
X	716.1	04.7	17.4	09.2	10.1	18.4	03.3	23.2	09 -01.4	18	10	02.3	07	01.5	*	*	02	02.0	03	01.7	01	02.0	01	01.0	*				
XI	703.6	04.7	10.9	06.2	07.0	12.2	02.3	19.9	06 -07.8	23	11	02.3	02	02.0	01	02.0	06	03.0	14	02.4	03	04.0	02	02.0	*				
XII	715.1	-03.7	00.2	-02.6	01.4	-05.5	11.0	01 -14.2	04	19	02.8	05	02.8	01	01.8	*	*	*	01	03.0	01	02.0	56						
GOD.	711.4	07.2	15.3	09.7	10.5	16.5	05.0	33.9	29 VM -16.4	20	150	02.4	36	02.1	12	02.2	49	07	81	02.3	41	03.2	30	02.6	25	02.3	671		
$\gamma = 42^{\circ}23' N \lambda = 21^{\circ}10' E$ Gr. $\Delta G = + 1h 25 min.$																													
I	-	-02.9	02.4	-01.0	-00.6	03.2	-04.1	12.5	30 -17.1	20	24	01.2	01	02.0	*	*	24	02.5	02	01.0	07	01.6	07	01.4	27	01.7	01		
II	-	02.9	09.7	05.4	05.9	11.0	01.9	20.5	23 -04.7	03	06	02.2	02	02.0	*	*	24	02.9	01	01.0	19	03.5	02	01.5	42	01.6	*		
III	-	03.0	13.2	07.6	07.9	14.4	02.1	25.0	23 -07.2	03	14	01.4	06	02.2	02	01.5	27	03.0	02	02.5	05	02.4	01	01.0	36	01.9	*		
IV	-	05.8	14.6	09.1	09.7	16.1	03.2	24.4	23 -09.3	13	18	01.8	02	02.0	*	*	24	02.3	01	02.0	09	02.6	04	02.0	34	02.2	*		
V	-	12.5	21.0	14.0	15.8	22.3	09.1	30.0	22 03.4	30	09	01.3	04	02.2	*	*	19	02.4	02	02.0	24	01.8	06	02.3	29	01.9	*		
VI	-	14.6	23.3	16.4	17.7	24.6	10.5	30.4	14 03.1	05	15	01.2	03	01.7	*	*	22	01.5	02	02.0	09	02.1	*	*	59	01.8	*		
VII	-	16.8	26.6	19.1	20.4	27.7	13.0	33.1	31.09 08.0	08	14	01.3	02	02.0	*	*	11	01.8	06	02.0	17	02.7	07	02.1	34	02.1	02		
VIII	-	15.3	25.0	17.7	19.1	27.1	12.2	34.6	22 07.4	28	10	01.3	04	01.8	*	*	09	02.1	07	01.4	31	02.2	03	01.7	23	01.3	06		
IX	-	11.1	19.7	13.7	14.5	21.4	08.5	28.5	09 -02.2	30	20	01.0	/05	01.4	02	02.0	06	01.5	02	01.5	17	01.4	*	*	38	01.3	*		
X	-	04.6	17.0	09.9	18.2	20.8	22.2	02.01	-02.0	18	44	01.3	06	02.0	*	*	08	01.8	01	01.0	06	01.7	06	01.7	25	01.8	*		
XI	-	04.6	11.3	06.6	07.2	12.5	01.9	20.8	06 -08.0	24	18	01.4	04	02.0	*	*	09	03.2	*	*	08	02.9	03	03.7	48	01.7	*		
XII	-	-03.7	-00.3	-03.2	-02.6	01.0	-08.2	10.6	01 -14.4	06	11	01.2	03	02.0	*	*	13	02.3	01	01.0	03	02.0	03	01.3	58	01.0	01		
GOD.	-	07.0	15.4	09.6	10.4	16.6	04.6	34.6	22 VM -17.1	20	201	01.3	40	01.9	04	01.8	166	02.4	27	01.7	155	02.0	39	01.9	453	01.7	10		
$\gamma = 42^{\circ}47' N \lambda = 21^{\circ}36' E$ Gr. $\Delta G = + 1h 26 min.$																													
I	-	-00.5	05.0	00.8	01.5	05.8	-03.0	12.5	31 -15.5	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	03.7	10.3	05.1	06.1	11.4	01.6	22.3	23 -07.4	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	03.0	14.1	07.2	07.9	14.8	02.0	27.0	24 -05.6	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	04.3	14.9	08.5	09.0	16.1	02.4	25.9	29 -03.5	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	10.9	20.3	12.6	14.1	21.5	08.1	28.5	22 03.5	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	13.0	22.3	15.0	16.3	23.9	10.8	30.0	20 04.0	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	15.1	26.0	17.6	19.1	27.0	13.1	34.1	29 10.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	13.8	25.9	16.3	18.3	27.1	12.1	35.0	22 07.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	09.5	19.5	12.2	13.3	20.8	08.2	29.4	09 -03.4	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
X	-	04.9	17.4	07.7	09.4	18.3	03.8	23.5	07 -01.0	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	-	05.6	12.1	06.3	07.6	13.1	02.7	22.0	12 -03.5	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	-02.5	00.2	-02.3	-01.7	01.3	-04.9	11.0	01 -13.4	23.14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	-	06.7	15.7	09.0	10.1	16.8	04.8	35.0	22 VM -15.5	49.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\gamma = 42^{\circ}27' N \lambda = 21^{\circ}47' E$ Gr. $\Delta G = + 1h 26 min.$																													
I	-	-00.6	03.9	00.0	00.9	04.8	-02.8	12.6	31 -11.5	20	04	02.2	17	02.4	06	02.0	04	01.0	10	01.6	16	02.3	07	03.1	02	01.0	27		
II	-	03.1	09.4	05.1	05.7	11.1	01.6	20.2	23 -05.0	05	04	02.8	03	01.7	01	02.0	01	02.5	20	02.0	03	02.0	03	02.0	03	01.7	50		
III	-	03.2	13.2	07.1	07.6	14.5	01.5	25.8	24 -05.2	0																			

Mesec	Oblačnost Nm (0-10)			Inzlasti broj sati (dina)	Vlažnost vazduha e <sub>m</sub> mm			Padavine R mm			Broj dana na sata:																										
	7	14	21		7	14	21	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	▲	▲	□									
					mm	mm	mm	Min			-20.00.0	0.0	25.0	0.0	20.0	6	8	2.0	8.0	0.1	1.0	0.0	1.0	1.0	0.1	0.1											
<b>PRISTINA</b>																																					
BR. ST. 221																																					
I	8.1	7.6	6.3	7.3	064.0	04.1	90	78	88	86	61	040	009.6	28	02	09	21	*	*	08	02	15	19	10	*	10	10	01									
II	6.9	7.9	5.4	6.7	107.3	05.3	85	61	77	74	28	079	027.9	02	*	08	*	*	13	02	01	12	13	10	02	12	03	01									
III	5.4	5.6	3.1	4.7	192.8	05.2	83	48	67	66	23	028	013.0	14	*	01	10	01	*	08	09	08	12	08	01	09	04	*									
IV	6.8	6.5	3.4	5.6	197.5	05.6	76	48	65	63	24	034	014.2	16	*	07	02	*	13	01	03	08	11	07	01	11	01	*									
V	5.5	6.2	4.7	5.6	243.6	08.4	79	48	69	65	27	065	026.0	16	*	*	09	*	*	04	05	12	08	02	12	*	*	02	06								
VI	4.2	5.9	4.3	4.8	260.6	10.0	78	50	74	67	30	051	017.5	28	*	*	15	01	*	07	08	05	11	07	02	11	*	09	*								
VII	2.9	7.6	3.8	3.3	319.7	11.1	74	46	66	62	26	046	016.7	23	*	*	22	08	*	11	02	12	04	04	03	04	*	07	01								
VIII	2.6	6.2	2.6	3.1	312.6	10.7	80	45	68	64	29	060	021.3	25	*	*	23	05	*	08	12	03	07	07	02	07	*	02	08								
GOD.	5.6	5.9	4.2	5.2	2293.9	07.1	83	55	74	70	23	576	027.9	02.ii	07	26	85	84	14	*	92	06	76	97	136	90	18	114	34	04	02	01	05	*	32	35	21
<b>UROSEVAC</b>																											$H_s = 573 \text{ m } H_b = 576.1 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$										
BR. ST. 222																											$H_s = 580 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$										
I	9.3	7.3	5.4	7.3	062.5	04.1	92	81	91	88	53	055	022.1	28	06	08	24	*	*	01	*	15	10	05	02	05	03	*	*	08	12						
II	6.8	5.9	5.2	6.0	108.0	05.6	91	67	94	77	25	087	042.1	02	*	08	*	*	02	01	04	08	03	12	03	*	*	01	01	02							
III	5.6	5.2	3.7	4.7	188.5	05.4	90	50	69	70	23	021	009.4	14	*	01	09	01	*	02	01	07	07	11	06	*	38	03	*	02							
IV	5.4	5.5	2.1	4.3	203.5	05.8	81	49	64	65	24	039	014.2	16	*	06	*	*	03	04	11	05	02	11	01	*	*	01	01	01							
V	5.4	5.0	3.7	4.7	232.6	08.8	82	48	70	67	27	041	011.0	16	*	*	12	01	*	*	06	05	11	09	01	11	*	*	07	*							
VI	4.0	5.4	3.6	4.3	258.1	10.0	82	48	72	67	30	066	017.4	18	*	*	18	04	*	*	06	05	10	09	02	10	*	*	06	*	*						
VII	3.2	3.8	2.4	3.1	299.2	11.4	84	46	69	65	21	066	018.4	02	*	*	23	11	*	01	01	14	01	06	05	04	06	*	01	04	*						
VIII	2.9	3.4	2.1	2.8	297.3	11.0	85	43	78	68	16	058	041.2	07	*	*	27	04	*	02	12	01	07	05	01	07	*	*	08	*							
GOD.	5.7	5.3	3.5	4.8	2188.7	07.3	87	57	77	73	16	623	043.1	02.ii	14	23	90	92	20	*	13	04	78	77	122	82	21	103	23	*	*	01	30	24	47		
<b>SIJARINSKA BANJA</b>																											$H_s = 455 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$										
BR. ST. 223																											$H_s = 450 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$										
I	6.7	6.3	5.5	6.2	-	-	-	-	-	-	-	042	011.0	18	03	02	21	*	*	02	*	05	09	09	01	06	03	*	*	06	*						
II	7.0	6.8	5.8	6.5	-	-	-	-	-	-	-	059	017.5	03	*	01	10	*	*	02	07	07	07	03	07	01	01	*	02	03							
III	5.1	5.1	5.5	5.2	-	-	-	-	-	-	-	035	016.0	14	*	01	12	02	*	04	*	10	10	08	06	01	07	01	*	02	*						
IV	6.7	5.9	5.5	6.0	-	-	-	-	-	-	-	037	011.0	06	*	06	02	*	*	04	09	07	07	02	06	02	01	*	*	*							
V	6.1	6.3	6.2	6.2	-	-	-	-	-	-	-	076	023.0	09	*	*	10	*	*	01	10	11	10	03	11	*	*	02	*								
VI	5.5	5.8	6.6	6.0	-	-	-	-	-	-	-	053	015.5	03	*	*	15	01	*	01	09	11	10	02	11	*	*	05	*								
VII	6.5	6.9	4.9	7.4	-	-	-	-	-	-	-	043	016.5	23	*	*	22	09	*	01	06	06	06	01	06	*	*	01	*								
VIII	5.8	4.8	3.3	4.7	-	-	-	-	-	-	-	055	015.5	25	*	*	25	03	*	05	03	03	05	04	05	*	*	04	*								
IX	6.7	5.8	5.8	6.1	-	-	-	-	-	-	-	028	008.5	25	*	*	02	12	*	04	11	08	08	08	08	*	*	01	*								
X	4.0	5.3	5.0	5.0	-	-	-	-	-	-	-	035	017.0	04	*	01	*	*	09	10	06	04	02	06	*	*	*	*	01								
XI	8.2	7.7	7.2	7.7	-	-	-	-	-	-	-	071	025.0	24	*	*	05	01	*	02	15	11	09	02	06	07	*	*	02	*							
XII	8.6	7.7	8.4	8.2	-	-	-	-	-	-	-	043	009.7	30	06	14	25	*	*	02	03	23	10	09	06	08	03	*	03	17							
GOD.	6.5	6.0	5.0	5.6	-	-	-	-	-	-	-	575	025.0	24	XI	09	18	82	88	15	*	10	*	46	122	99	90	21	85	22	05	*	13	07			
<b>RUJANOVAC</b>																											$H_s = 400 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$										
I	7.8	7.5	5.0	6.8	-	-	-	-	-	-	-	029	023.5	28	02	03	21	*	*	06	*	05	16	13	07	01	09	06	*	*	04	03					
II	6.8	6.7	6.0	6.5	-	-	-	-	-	-	-	054	95	82	81	42	067	029.0	03	*	01	06	*	04	10	10	07	02	10	*	*	01					
III	5.1	4.8	2.6	4.2	-	-	-	-	-	-	-	058	92	54	78	75	30	01	02	6	*	14	02	10	02	07	04	*	*	01							
IV	4.8	5.5	1.7	4.0	-	-	-	-	-	-	-	064	89	55	73	72	31	035	012.2	03	*	06	01	*	11	04	04	04	02	04	*	*	02				
V	5.2	3.6	2.7	3.8	-	-	-	-	-	-	-	10.5	90	61	83	78	26	052	014.1	28	*	*	11	*	12	05	10	01	10	*	*	01					
VI	3.8	5.6	3.6	4.4	-	-	-	-	-	-	-	055	012.6	03	*	*	19	08	*	*	09	04	05	07													

Mesec	Vrednost prirodnih plinova mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova m/s, Fm (O-12)																
		Tm			Sred. (Dnev.)	Km	Km	Km	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21																								
$\varphi = 42^{\circ}45' N \lambda = 21^{\circ}59' E$ Gr. AG = + 1h 27 min.																												
I	-02.3	00.5	-01.6	-01.3	01.7	-03.8	06.5	12	-10.5	19.8	02	02.0	10	01.6	.	01	03.0	08	03.1	49	01.9	07	01.9	02	01.5	14		
II	-00.7	04.4	01.5	02.0	05.5	-00.7	15.0	23	-10.5	28	10	02.0	.	01	02.0	.	20	03.0	28	02.2	09	01.6	06	02.5	12			
III	-02.6	07.5	04.0	04.5	08.5	01.0	20.0	24	-12.5	01	06	02.3	08	02.0	01	01.0	.	06	02.0	36	02.1	08	01.5	09	01.9	19		
IV	-03.4	08.3	04.7	05.3	10.0	01.4	18.5	30.29	-06.0	10	12	02.3	10	02.2	02	01.0	.	02	01.5	33	02.5	06	03.5	08	02.6	19		
V	-10.0	14.7	10.2	11.3	15.6	07.5	23.0	21	03.0	28.11	.	18	01.9	05	01.6	01	02.0	03	02.0	27	02.1	05	02.0	04	02.5	30		
VI	-12.6	14.3	12.3	13.4	17.6	09.8	24.0	14	02.0	04	10	02.0	04	01.5	02	02.0	.	16	02.1	06	01.5	06	01.5	42				
VII	-14.6	20.4	14.7	16.1	21.1	12.0	27.5	31	08.5	16	13	02.2	07	01.4	.	12	02.2	16	02.1	*	*	11	02.2	34				
VIII	-14.3	19.9	14.5	15.8	21.0	11.9	28.0	22	06.0	25	10	02.1	12	01.5	05	01.8	.	22	02.5	01	03.0	04	02.2	39				
IX	-08.9	13.6	09.5	10.4	14.8	07.3	22.0	09	-03.0	29	26	02.0	16	01.8	05	02.0	.	*	13	02.1	02	02.5	08	02.6	20			
X	-07.1	12.4	08.2	09.0	13.3	05.8	19.0	09	-01.5	17	08	01.6	08	01.5	01	01.0	.	11	01.9	14	02.0	01	02.0	03	02.0	47		
XI	-03.5	06.7	03.7	04.6	07.7	01.6	16.5	12	-05.5	28.20	07	02.4	04	02.2	.	03	02.7	50	02.5	02	02.0	04	02.0	20				
XII	-04.1	-01.7	-03.9	-03.4	00.3	-06.1	06.5	24.23	-12.0	05.04	09	02.9	15	02.4	01	02.0	.	07	02.4	25	02.3	02	02.0	09	02.4	25		
GOD.	-	05.9	10.2	06.5	07.3	11.4	04.0	28.0	22.9	-12.5	04.8	111	02.1	114	01.8	23	01.7	02	02.5	72	02.5	329	02.2	49	02.0	74	02.2	321
$\varphi = 42^{\circ}58' N \lambda = 22^{\circ}08' E$ Gr. AG = + 1h 29 min.																												
I	-00.1	05.7	01.6	02.2	06.6	-02.1	15.0	30.12	-15.5	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-05.3	11.4	07.1	07.8	12.5	02.9	23.0	25	-11.0	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-06.0	15.1	09.2	09.9	16.1	03.8	28.0	24	-04.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-06.4	15.8	10.2	10.7	17.2	04.5	28.0	30	-02.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-14.3	22.9	15.5	17.1	24.0	11.3	31.0	22.1	06.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-25.0	17.2	19.0	19.8	26.3	13.2	32.5	14	06.0	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-19.2	27.0	19.4	21.0	28.1	15.2	36.5	31	12.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-17.4	27.9	18.9	20.8	29.1	14.1	37.0	22	10.0	27.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-11.7	21.1	14.0	15.2	22.0	09.9	29.5	09.02	-01.5	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-07.7	18.2	10.3	11.6	19.3	05.4	27.0	09	00.0	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-06.9	13.0	07.5	08.7	14.5	03.9	25.0	12	-00.5	28.25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-01.9	09.0	-01.8	-01.1	01.7	-03.9	11.0	29	-12.5	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	05.2	17.0	10.8	11.9	18.1	06.5	37.0	MW -15.5	30.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}50' N \lambda = 22^{\circ}08' E$ Gr. AG = + 1h 29 min.																												
I	-01.2	05.2	00.3	01.2	06.2	-03.1	14.5	31	-12.6	19	11	02.3	04	01.8	07	01.4	30	02.3	21	02.2	02	02.0	01	02.0	*			
II	-03.3	11.2	05.3	06.3	12.3	01.8	25.0	23	-08.5	05	04	02.3	03	01.7	09	01.9	22	01.9	12	01.9	05	02.4	*	02	01.5	17		
III	-03.5	14.2	07.7	08.3	15.2	02.2	29.1	24	-05.2	01	10	02.4	05	02.0	07	01.6	24	02.0	24	02.0	06	02.8	01	02.0	08	02.8	08	
IV	-06.0	15.1	08.9	09.7	16.9	03.0	28.0	30	-02.5	20	12	03.0	08	01.8	02	03.0	30	01.9	09	02.0	02	02.0	*	09	02.7	10		
V	-12.4	21.4	13.9	15.4	22.6	09.1	29.7	20	04.0	25.12	16	02.6	08	01.9	10	01.3	20	01.9	12	01.8	05	02.8	*	04	01.8	18		
VI	-15.2	23.2	16.4	17.7	24.6	11.6	32.0	14	03.5	05	14	02.1	08	02.0	07	01.6	15	01.8	11	01.8	01	02.0	01	02.3	22			
VII	-17.2	26.5	18.5	20.2	28.1	13.9	36.2	09	10.5	13.11	11	02.0	11	02.0	03	01.7	23	01.8	04	02.0	07	02.3	03	02.3	19			
VIII	-15.2	27.4	17.9	19.6	28.7	12.8	38.6	22	09.0	27	12	02.2	03	01.7	16	01.7	15	02.3	*	01	02.0	07	01.7	30				
IX	-10.3	20.1	12.5	13.9	21.6	06.5	28.8	09	-03.0	30	16	02.5	07	01.6	04	01.2	10	01.8	05	02.4	01	02.0	01	02.0	31			
X	-05.4	18.0	08.9	10.3	19.1	04.2	24.7	08	-06.9	19	10	02.3	02	02.0	06	01.3	17	01.8	06	01.8	07	02.0	01	01.0	11	02.4	33	
XI	-05.3	12.2	06.3	07.5	13.5	03.1	24.3	05	-02.7	23	17	01.8	08	01.4	08	01.4	23	02.0	09	02.3	05	02.2	05	02.4	19			
XII	-02.6	00.2	-02.4	-02.2	00.9	-05.0	09.2	01	-10.8	06	01	-11.5	14.0	36	02.2	05	01.6	09	02.4	05	02.8	02	02.0	07	02.4	15		
GOD.	-	07.5	16.2	09.5	10.7	17.5	05.2	38.6	22	MW -12.6	30.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 42^{\circ}41' N \lambda = 22^{\circ}11' E$ Gr. AG = + 1h 29 min.																												
I	-01.7	03.8	00.5	00.8	05.0	-02.9	13.4	30	-12.0	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-03.1	09.7	05.3	06.0	11.1	02.4	21.3	23	-08.6	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-05.9	13.2	07.6	08.1	14.5	02.9	26.3	24	-06.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-08.2	14.5	09.3	09.8	16.2	04.0	26.6	30	-02.3	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-13.2	21.4	14.6	16.0	22.3	10.5	28.8	22	04.8	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-15.6	22.6	16.5	17.8	24.5	12.5	31.0	19.15	05.7	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-17.5	26.7	19.3	20.7																								

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha % mm	Padavine R mm mm	Broj dana na sat																																
	7	14	21			U m s			Sred. (Dnev.) Min			Padavine R mm mm			Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	R	T	≡						
						7	14	21	Sred. (Dnev.) Min	Max	Dat.	M	Max	Dat.	10.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.0	10.0	•	Δ	Δ	Δ	Δ	R	T	≡						
<b>KUKAVICA</b>																																						
BR. ST. 226																																						
I	6.0	5.0	4.7	5.2	-	03.7	87	84	86	86	65	029	006.2	14	03	06	24	.	.	.	07	09	09	07	.	04	07	02	.	.	.	08	26					
II	6.8	6.0	5.1	6.0	-	04.2	84	70	81	78	45	071	027.4	03	01	02	15	.	.	.	02	.	05	10	08	08	02	03	08	02	.	.	06	-				
III	4.9	4.5	4.0	4.5	-	04.3	75	61	71	69	34	116	019.7	14	01	02	16	.	.	.	12	08	11	09	05	07	01	.	.	.	01	04	11					
IV	5.4	4.9	4.6	5.0	-	04.9	77	64	76	72	38	046	012.4	17	.	.	12	.	.	.	.	06	08	08	08	01	06	04	.	.	.	03	04	-				
V	4.7	4.5	3.6	4.3	-	07.5	80	64	77	74	45	067	021.6	28	.	.	.	.	.	.	.	10	05	09	07	02	09	.	.	.	.	01	05	.				
VI	3.8	5.3	3.7	4.3	-	08.7	77	67	77	74	41	063	018.6	23	.	.	.	.	.	.	.	10	04	10	08	03	10	.	.	.	.	01	04	04				
VII	3.7	3.3	3.1	3.4	-	10.1	78	63	72	72	42	059	019.4	11	.	.	02	.	.	.	.	15	04	07	03	07	.	.	.	.	.	03	06	.				
VIII	2.7	3.6	1.7	2.7	-	09.4	75	60	73	69	32	104	039.4	15	.	.	03	.	.	.	01	.	16	02	06	05	03	06	.	.	.	03	02	.				
IX	4.7	3.9	3.1	3.9	-	07.4	81	68	78	76	46	075	041.6	11	.	.	03	.	.	.	.	11	05	05	04	03	05	.	.	.	.	04	.					
X	2.6	2.3	2.0	2.3	-	05.7	71	57	70	66	37	035	012.6	04	.	.	02	.	.	.	.	21	02	04	04	02	04	01	.	.	.	.	.	.				
XI	7.5	6.2	5.6	6.4	-	05.4	84	76	85	82	43	062	021.6	27	.	02	12	.	.	.	06	13	12	10	03	07	08	03	.	.	.	11	.					
XII	6.2	6.1	5.3	5.9	-	03.2	88	83	87	85	44	072	017.2	31	07	11	29	.	.	.	11	15	09	09	04	04	08	.	.	.	03	11	28					
GOD.	4.9	4.6	3.6	3.9	4.5	-	06.2	79	68	78	75	32	839	041.6	44	W.M	12	23	113	05	.	.	03	.	130	85	98	87	31	72	45	13	.	.	01	14	64	-
<b>VLASOTINCE</b>																																						
BR. ST. 227																																						
I	5.2	5.5	5.0	5.3	-	-	-	-	-	-	-	036	013.0	18	03	01	18	.	.	.	06	08	09	06	02	06	04	01	.	.	.	07	.					
II	7.1	6.8	6.9	6.9	-	-	-	-	-	-	-	064	020.0	15	01	01	05	.	.	.	02	11	11	08	02	11	02	01	.	.	.	01	04	.				
III	4.8	5.2	4.1	4.7	-	-	-	-	-	-	-	067	019.4	04	.	.	03	03	.	.	.	10	05	11	10	03	09	03	.	.	.	01	.					
IV	5.5	6.3	4.9	5.6	-	-	-	-	-	-	-	053	008.5	03	.	.	04	05	.	.	.	04	10	08	06	08	08	08	.	.	.	.	.					
V	5.4	5.3	4.8	5.2	-	-	-	-	-	-	-	074	031.0	28	.	.	15	05	.	.	.	08	07	10	07	03	10	.	.	.	02	.						
VI	5.0	5.0	5.1	5.1	-	-	-	-	-	-	-	034	023.0	03	.	.	22	09	.	.	.	03	06	08	05	01	08	.	.	.	02	.						
VII	4.2	3.9	3.9	3.8	-	-	-	-	-	-	-	059	031.5	11	.	.	23	13	.	.	.	10	05	09	05	09	09	.	.	.	02	06						
VIII	3.0	4.0	3.0	3.3	-	-	-	-	-	-	-	050	024.5	25	.	.	20	16	.	.	.	08	01	07	07	01	07	.	.	.	01	.						
IX	5.0	5.8	2.8	3.8	-	-	-	-	-	-	-	070	021.5	25	.	.	02	12	.	.	.	11	04	10	10	04	10	.	.	.	02	.						
X	4.0	3.6	3.2	3.8	-	-	-	-	-	-	-	018	008.0	03	.	.	02	04	.	.	.	13	04	10	04	03	04	04	.	.	.	04	03	.				
XI	6.6	6.0	5.8	6.2	-	-	-	-	-	-	-	112	042.0	27	.	03	01	.	.	.	02	11	13	11	03	11	05	03	.	.	.	02	08	.				
XII	8.1	7.5	6.3	7.3	-	-	-	-	-	-	-	080	025.0	31	04	15	27	.	.	.	05	18	10	09	04	07	04	01	.	.	.	01	.	15				
GOD.	5.4	5.2	4.6	5.1	-	-	-	-	-	-	-	727	042.0	27	XI	08	17	62	111	43	.	.	.	82	90	110	91	28	100	18	07	01	01	02	13	03	29	
<b>PREDJANE</b>																																						
BR. ST. 228																																						
I	7.8	6.5	5.7	6.7	-	04.3	93	68	88	83	38	036	009.2	28	02	02	23	.	.	.	04	13	12	07	10	05	02	.	.	.	01	09	.					
II	8.2	7.2	6.0	7.1	-	05.8	92	68	80	83	33	084	020.0	15	01	01	07	01	.	.	.	02	10	10	08	02	09	02	.	.	.	02	04	.				
III	5.7	5.4	3.9	5.0	-	05.7	90	50	75	72	19	101	029.0	15	.	01	11	02	.	.	.	04	10	10	09	04	13	04	.	.	.	02	05	.				
IV	6.3	6.5	5.3	6.3	-	06.4	88	79	72	74	24	062	013.2	17	.	.	06	02	.	.	.	04	01	11	11	02	11	01	01	.	.	.	02	.				
V	5.7	5.3	4.2	5.0	-	09.8	89	51	85	75	28	063	020.5	28	.	.	12	.	.	.	.	07	06	12	08	03	12	.	.	.	05	04	.					
VI	4.4	3.5	4.6	4.8	-	11.5	88	52	87	76	32	046	023.3	03	.	.	18	02	.	.	.	06	04	13	08	01	13	.	.	.	04	03	.					
VII	5.6	4.2	4.1	4.6	-	13.0	88	51	84	74	30	059	020.8	11	.	.	23	12	.	.	.	01	08	05	09	07	02	09	.	.	.	03	04	.				
VIII	3.9	4.0	2.5	3.5	-	11.9	92	44	86	72	20	048	032.8	25	.	.	24	10	.	01	01	13	02	07	06	01	07	.	.	.	09	06	.					
IX	6.2	5.0	4.5	5.3	-	09.1	95	52	84	77	23	056	019.6	25	.	.	02	12	02	.	.	01	01	06	07	11	09	02	11	.	.	.	01	04	.			
X	6.0	3.9	3.4	4.4	-	07.3	96	52	89	79	22	024	013.3	04	.	.	02	04	.	.	.	02	10	06	05	03	05	05	.	.	.	01	09	.				
XI	8.4	6.8	6.1	7.1	-	06.5	93	66	89	83	33	092	029.3	27	.	.	07	.	.	.	.	02	03	16	12	12	03	10	06	04	.	.	01	05	.			
XII	8.8	7.8	7.6	8.1	-	03.																																

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Mjesec	Vrstdišni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vatra nD, Fm (0-12)														
		Fm			Sred. (Biša)				Max	Min	Dat.	Max	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C			
		7	14	21											8.	J.										
$\varphi = 42^{\circ}30' N \lambda = 22^{\circ}28' E$ Gr. $\Delta G = +1h\ 29\ min.$																										
I	-	-05.4	02.7	-03.0	-02.2	03.3	-06.7	09.0	30	-19.0	20	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-00.5	08.4	00.4	02.2	09.2	-02.0	19.5	23	-08.6	28	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	00.5	12.6	06.4	04.5	13.2	-00.2	23.0	23	-10.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	04.3	13.3	08.1	08.4	14.8	02.5	23.0	30	-03.0	22	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	11.0	19.9	13.0	14.2	20.7	08.0	29.5	21	02.5	30	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	13.1	21.7	15.4	16.4	23.0	09.6	29.5	14	02.5	06	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	15.4	24.8	17.5	18.9	25.9	13.0	32.7	31	07.5	14.13	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	14.3	25.3	17.2	18.5	26.6	11.2	34.5	29	07.0	26	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	08.8	18.8	12.0	12.9	19.9	07.0	27.5	09	-04.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	02.3	16.9	08.3	09.0	18.3	00.7	22.5	08	-04.0	19	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	02.0	11.1	04.8	05.7	12.2	00.4	22.0	05	04	-04.5	22	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-04.6	01.7	-02.3	-01.9	02.9	-06.5	07.5	01	-14.5	14	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	05.1	14.8	08.2	09.4	15.8	03.1	34.5	29	-0.0	-19.0	20	-	-	-	-	-	-	-	-	-	-	-	-		
SR CRNA GORA $\varphi = 43^{\circ}00' N \lambda = 18^{\circ}44' E$ Gr. $\Delta G = +1h\ 15\ min.$																										
I	-	-00.8	02.7	00.6	00.7	03.8	-02.5	00.0	29	-11.0	01	02	02.5	24	02.8	01	02.0	34	03.9	01	01.0	20	03.3	27		
II	-	01.9	05.5	02.9	03.3	06.4	00.3	12.0	25	-24	-06.6	28	01	01.0	16	02.6	01	02.0	34	03.9	01	01.0	09	03.9	16	
III	-	02.9	11.3	06.7	09.9	11.9	02.0	21.4	23	-08.0	01	01.0	16	02.4	01	02.0	32	03.0	01	01.0	19	03.0	22			
IV	-	04.6	10.9	06.4	07.1	12.0	02.3	22.4	29	-06.5	18.12	07	01.9	01	02.0	22	04.2	01	02.0	30	03.0	01	02.0	24		
V	-	10.3	16.3	11.6	12.5	17.7	07.5	25.4	19	02.0	10.09	01	-	10	03.6	01	02.0	32	03.0	01	02.0	10	03.1	24		
VI	-	12.9	18.8	13.9	14.9	20.2	09.7	25.2	13	11	06.0	06.04	04	-	10	03.4	01	02.0	26	02.5	01	02.0	15	03.5	27	
VII	-	16.2	23.1	17.1	18.4	24.6	12.7	30.5	30	10.0	07	-	13	03.6	01	02.0	26	03.0	01	02.0	10	03.0	25			
VIII	-	14.2	21.1	15.9	16.7	22.8	11.3	31.5	30	06.0	20	01	02.0	21	02.2	01	02.0	21	03.1	01	02.0	16	02.6	23		
IX	-	10.6	16.5	11.9	12.8	17.6	08.6	24.6	13	-01.0	30	-	15	03.1	-	-	18	02.8	01	02.0	06	02.7	01	02.0	33	
X	-	05.5	15.4	08.8	09.6	16.2	03.1	20.0	26	-0.3	30	-	15	03.1	-	-	18	02.8	01	02.0	06	02.7	01	02.0	35	
XI	-	-02.2	03.2	05.6	06.0	08.0	04.0	-04.5	09.5	01	-09.5	13.05	12	05.7	15	02.9	03	02.6	01	02.0	02	03.0	02	02.0	48	
GOD.	-	06.6	12.8	08.3	09.0	14.0	04.0	31.5	30	-0.0	-12.0	30	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 43^{\circ}09' N \lambda = 19^{\circ}08' E$ Gr. $\Delta G = +1h\ 17\ min.$																										
I	638.4	-03.3	00.6	-02.8	-02.0	02.1	-05.9	05.7	26	-16.2	19	05	02.4	02	02.0	02	02.5	04	03.2	01	01.0	20	03.5	48		
II	637.3	-01.4	02.5	-00.1	00.3	04.2	-03.0	13.1	24	-12.6	28	05	02.8	03	02.0	02	02.5	07	02.7	14	04.2	05	02.8	03	02.3	
III	642.2	-00.3	07.1	01.2	02.4	08.1	-02.0	17.0	23	-15.0	13	10	02.6	03	02.3	02	02.0	02	02.5	07	03.1	03	02.9	41		
IV	637.6	01.0	06.6	02.3	03.1	08.1	-01.2	19.6	29	-10.6	14	10	02.3	08	02.1	02	02.0	01	02.3	09	03.0	10	02.9	07	03.3	
V	641.0	08.4	12.5	07.4	08.9	14.0	03.7	21.9	19	-00.6	30	12	05	02.2	01	02.0	04	02.2	02	02.5	08	02.6	02	02.0	39	
VI	640.0	11.1	14.8	09.6	11.3	16.5	05.6	22.1	11	-00.6	05	10	02.1	08	02.0	05	01.6	01	02.5	04	02.0	02	02.0	37		
VII	641.4	12.5	18.7	12.8	14.4	20.2	09.0	26.0	30	06.0	07	11	02.5	08	01.8	03	02.0	03	02.0	14	02.1	11	03.2	07	03.4	
VIII	641.7	11.6	17.5	11.1	12.9	19.5	07.9	28.0	30	06.0	24	07	02.7	03	02.3	06	02.0	06	02.3	11	02.5	10	03.9	13	02.5	
IX	643.4	06.8	12.0	07.7	08.6	13.0	05.0	20.0	13	-05.4	30	10	02.5	04	02.2	15	01.9	05	01.8	14	02.6	04	01.5	34		
X	644.3	02.2	11.8	04.1	05.3	12.9	00.8	17.4	01	-03.5	17.05	04	02.0	02	01.7	11	01.9	06	02.2	08	03.0	02	03.5	05	02.6	
XI	643.8	01.2	05.0	01.6	02.3	06.4	-01.8	16.0	12	-11.5	21	02	03.0	03	02.0	05	02.0	09	02.6	14	03.3	12	03.8	04	02.8	
XII	640.7	-05.7	-00.9	-05.2	-04.3	01.2	-08.1	07.0	24	-16.5	05	11	03.4	05	02.6	08	02.4	17	03.0	01	06.0	04	04.5	01	03.0	
GOD.	640.6	03.9	09.0	04.2	05.3	10.5	00.8	28.0	30	-0.6	-16.5	93	02.6	54	02.0	63	02.0	51	02.4	178	02.7	86	03.6	72	02.7	49
$\varphi = 43^{\circ}21' N \lambda = 19^{\circ}21' E$ Gr. $\Delta G = +1h\ 17\ min.$																										
I	693.9	-01.1	04.4	00.9	01.3	05.5	-02.6	11.8	29	-16.0	19	02	02.0	02	02.0	04	02.0	05	02.4	06	02.8	01	05.0	02	02.5	70
II	691.9	02.6	08.3	04.3	04.9	09.8	01.0	18.0	24	-06.8	28	05	02.4	01	02.0	02	02.5	03	03.1	04	01.5	45				
III	696.6	01.2	12.6	06.1	05.3	13.6	00.2	23.6	24	-08.2	01	07	02.3	01	03.0	03	02.3	05	02.6	04	03.5	04	02.0	02	03.5	65
IV	691.8	03.2	12.6	07.4	07.7	14.1	01.7	26.6	29	-05.2	18	07	02.3	01	02.0	02	03.5	04	03.8	04	02.8	03	02.0	07	02.3	58
V	694.3	09.4	18.4	12.2	13.1	20.0	06.8	29.2	19	00.6	28	04	02.5	02	02.5	04	01.5	03	02.3	06	02.3	04	01.8	01	02.0	63
VI	693.6	10.8	20.4	14.2	14.9	22.1	08.4	29.0	14	02.0	05	05	02.0	01	01.0	02	02.0	01	01.5	06	01.8	08	01.6	01	02.0	67
VII	693.6	13.6	23.4	17.1	17.8	24.9	11.5	30.2	30	07.8	14	07	02.3	01	02.0	03	01.7	05	02.0	04	03.0	06	03.0	10	02.0	03
VIII	694.0	11.9	23.5	15.4	16.5	24.8	10.2	32.4	30																	

Meseč	Oblačnost Nm (0-10)	Inzolachija broj sati (Giese)	Vlažnost vazduha e <sub>m</sub> mm	Padavine R mm		B r o j d a n a n s a :																								
				U m s		Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx							
				7	14	21	Sred. (Giese)	7	14	21	Sred. (Dels.)	Min	M	Max	Dat.	0	+	*	Δ	▲	○	■	□							
<b>BOSILJGRAD</b>																														
BR. ST. 231																														
I	6.7	6.3	7.0	6.6	-	-	-	-	-	-	048	010.0	18	08	03	31	.	.	.	04	15	09	09	02	05	04				
II	7.8	7.4	7.6	7.6	-	-	-	-	-	-	058	017.0	03	.	22	.	.	.	02	17	06	06	03	06	.					
III	4.8	5.6	5.6	5.5	-	-	-	-	-	-	044	025.4	14	01	01	15	01	.	.	10	10	06	06	01	05	02				
IV	5.9	5.7	4.9	5.5	-	-	-	-	-	-	053	012.2	16	.	07	01	.	.	06	10	06	03	04	03	.					
V	4.0	6.7	5.5	5.4	-	-	-	-	-	-	045	022.5	28	.	.	08	.	.	05	08	05	05	02	05	.					
VI	3.4	6.6	5.7	5.2	-	-	-	-	-	-	049	011.0	21	.	.	14	.	.	01	04	08	11	11	01	11					
VII	4.7	5.7	4.8	5.1	-	-	-	-	-	-	034	010.5	24	.	.	17	04	.	.	04	04	05	05	01	05	.				
VIII	2.9	4.4	3.7	3.7	-	-	-	-	-	-	028	009.5	25	.	.	24	06	.	.	12	03	05	05	05	05	.				
IX	5.5	5.1	3.3	4.6	-	-	-	-	-	-	027	014.0	24	.	.	02	06	.	.	10	06	03	03	02	03	.				
X	3.6	2.5	2.3	2.8	-	-	-	-	-	-	010	007.0	12	.	.	17	.	.	.	19	05	02	02	02	02	.				
XI	7.5	6.6	7.6	7.2	-	-	-	-	-	-	071	017.5	27	.	.	15	.	.	.	05	16	09	09	03	07	04				
XII	6.8	5.5	5.6	6.0	-	-	-	-	-	-	052	012.2	31	09	02	29	.	.	.	08	13	10	09	01	05	06				
GOD.	5.3	5.7	5.3	5.4	-	-	-	-	-	-	539	025.4	44	18	06	138	71	10	.	01	.	89	115	77	76	19	63	19		
<b>KRSTAC</b>																														
BR. ST. 232																														
I	7.6	7.9	7.9	7.5	-	046	095	91	93	93	61	245	065.7	12	02	03	22	.	.	04	03	01	17	12	07	04	02			
II	7.9	7.4	7.0	7.4	-	052	028	90	82	88	28	246	036.4	12	.	12	.	.	.	06	03	01	15	17	17	10	14	06		
III	5.3	5.1	4.3	4.9	-	064	087	76	85	82	37	176	075.0	13	.	01	10	.	.	02	02	07	07	08	06	08	.			
IV	6.0	5.4	4.4	5.3	-	066	087	76	88	84	30	118	034.2	16	.	09	.	.	.	11	05	04	08	07	07	03	.			
V	5.5	6.8	5.2	5.8	-	098	85	84	89	86	63	099	027.2	10	.	.	01	.	.	05	01	01	08	09	09	05	09	.		
VI	6.0	6.4	4.7	5.0	-	114	85	83	88	84	40	046	014.5	03	.	.	03	.	.	02	02	01	04	07	06	02	07	.		
VII	3.5	3.1	3.9	4.1	-	135	3	74	87	81	48	033	024.4	23	.	.	18	01	.	04	01	04	02	02	01	02	.			
VIII	4.1	5.6	5.3	4.4	-	127	85	80	90	85	65	131	035.6	20	.	.	07	02	.	01	04	09	09	05	09	.				
GOD.	5.2	5.8	4.8	5.3	-	082	88	81	89	86	28	2038	080.3	30	05	04	107	29	03	.	52	24	66	98	107	106	71	103	24	05
<b>ZABLJAK</b>																														
BR. ST. 233																														
I	7.4	7.6	6.6	7.2	058.8	037.7	91	92	90	88	63	142	061.3	12	02	05	27	.	.	04	02	01	13	16	12	04	09	14	07	
II	7.6	6.3	6.2	7.2	090.2	04.0	87	76	86	83	39	149	036.5	12	02	02	20	.	.	03	01	01	12	19	16	07	09	13	01	
III	5.3	5.7	3.2	4.7	183.1	04.2	85	81	85	75	24	168	065.5	21	03	02	17	.	.	02	03	01	15	17	17	10	14	06	.	
IV	6.6	5.5	4.4	5.5	193.6	04.6	81	66	82	76	29	100	020.1	02	01	04	18	.	.	07	01	06	09	12	04	07	12	02	.	
V	5.3	6.5	4.4	5.4	207.7	06.4	78	62	81	74	28	071	028.6	28	.	.	04	.	.	05	02	03	06	09	09	07	09	.		
VI	3.6	6.4	3.7	4.6	221.7	08.0	81	65	84	77	45	065	016.0	28	.	.	01	.	.	02	02	01	04	07	05	04	05	.		
VII	3.8	6.4	2.9	3.8	291.3	09.0	77	59	81	73	48	044	023.2	23	.	.	01	.	.	03	06	16	11	03	16	.				
VIII	4.3	6.0	3.5	4.6	229.6	08.7	82	62	83	76	30	115	034.9	20	.	.	03	.	.	03	01	06	05	13	15	.				
IX	5.7	6.0	6.2	6.0	158.2	07.2	90	70	78	83	35	219	079.0	21	.	.	03	.	.	01	03	09	12	10	08	12	.			
X	3.4	3.8	2.4	3.2	206.6	05.6	91	63	89	81	28	132	042.4	12	.	.	13	.	.	18	07	07	06	03	06	02	.			
XI	7.0	7.1	6.1	6.7	086.2	04.9	88	80	88	86	20	220	056.0	17	02	05	16	.	.	02	02	11	18	15	06	15	09	03		
XII	5.9	5.8	4.5	5.4	094.5	03.0	88	77	86	84	37	104	031.1	30	15	09	27	.	.	03	02	09	12	13	11	02	07	10	04	
GOD.	5.5	6.0	4.5	5.4	2021.5	05.8	84	68	84	79	24	1549	079.0	24	04	04	04	04	.	27	07	73	103	170	132	48	129	71	20	05
<b>PLJEVLJA</b>																														
BR. ST. 234																														
I	7.9	7.5	6.0	7.1	045.9	04.3	90	71	84	82	53	076	030.0	13	02	06	19	.	.	06	01	01	13	14	11	03	09	07	07	
II	6.9	5.9	5.5	6.5	085.9	04.9	84	76	84	82	34	044	010.4	14	.	.	12	.	.	12	06	01	05	13	10	01	12	04	01	.
III	6.0	5.6	2.7	4.8	159.3	04.9	91	73	71	19	21	061	018.0	21	.	01	16	.	.	07	02	07	12	09	03	08	04	.		
IV	6.6	4.4	4.1	5.7	166.7	05.4	89	51	72	70	26	056	023.3	16	.	13	02	.	.	06	02	04	08	13	08	02	10	06	02	
V	6.5	6.9	3.5	5.6	189.3	07.8	77	71	79	23	046	023.9	28	.	.	07	.	.	05	01	02	06	11	02	11	01	02	01		
VI	6.3	6.6	3.9	5.6	197.1	09.6	92	54	88	77	32	092	035.4	17	.	.	11	.	.	05	01	02	06	12	11	02	12	.		
VII	6.3	6.3	3.9	5.2	250.3	11.1	91	83	71	27	23	076	019.7	23	.	.	20	01	.	08	03	05	12	07	06	04	12	.		
VIII	7.1	5.6	3.0	5.2	2																									

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Meseč	Vrednost pratnje m m	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра m/s, Fm (0-12)																			
		Tm			Max.			Min.			Dat.			N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)	Hm	Nm	Max.	Dat.	Min.	Dat.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.				
$\gamma = 42^{\circ}28' N \lambda = 18^{\circ}30' E$ Gr. $\Delta G = +1h\ 14\ min.$														HERCEGENVI-IGALC												BR. ST. 236					
I	758.6	07.6	11.1	08.0	08.7	12.2	05.8	17.0	25	01.0	19.0	05	02.8	*	*	07	03.7	15	03.3	04	01.5	02	03.0	04	03.2	05	01.8	51			
II	757.4	09.0	13.0	09.9	10.4	14.0	07.7	20.2	24	02.7	28	07	01.9	01	04.0	14	03.6	18	02.8	04	02.0	02	02.9	04	03.0	07	02.7	25			
III	761.6	09.4	15.9	11.5	12.1	16.8	08.2	26.7	26	-01.0	01	07	01.9	*	*	13	02.7	20	03.0	04	02.8	02	02.5	08	02.8	07	02.7	31			
IV	755.9	11.5	16.9	12.3	13.2	18.0	09.1	22.1	30	04.3	18	07	02.7	04	05.0	10	02.5	12	02.4	03	03.3	03	02.0	09	03.4	14	02.1	28			
V	757.6	16.9	21.8	16.7	18.0	23.2	14.0	31.4	19	09.2	11	02	02.0	02	01.5	13	02.5	13	02.2	05	02.2	03	02.7	08	01.8	07	01.7	40			
VI	756.1	19.7	24.3	19.4	20.7	25.5	16.0	29.9	18	12.4	06	02	01.5	*	*	09	02.3	10	02.0	02	01.5	02	03.0	13	02.5	11	01.8	41			
VII	755.6	22.7	27.9	22.9	24.1	29.1	19.0	31.7	20	16.7	06	02	02.5	02	02.5	11	02.5	12	02.5	06	02.2	04	02.5	06	02.8	15	02.2	35			
VIII	755.9	21.2	27.4	21.3	23.0	28.6	18.3	34.6	21	13.3	25	06	02.3	*	*	08	01.9	09	01.8	02	02.5	05	02.2	11	02.5	14	02.1	38			
GOD.	758.0	13.9	19.3	14.6	15.6	20.4	11.7	34.6	30	VM -01.0	04.0	56	02.3	16	03.4	121	02.8	156	02.7	43	02.2	40	02.5	106	02.5	138	02.1	419			
$\gamma = 42^{\circ}39' N \lambda = 18^{\circ}41' E$ Gr. $\Delta G = +1h\ 15\ min.$															GRADHOVC												BR. ST. 237				
I	-	-00.5	05.3	01.1	01.7	06.2	-02.9	11.5	25	-13.2	19	03	02.0	02	01.0	11	02.1	05	03.2	03	03.3	*	*	01	01.0	03	01.3	65			
II	-	03.2	08.2	03.8	04.6	06.1	01.1	16.2	24	-04.8	08	01	02.0	02	01.5	05	01.0	11	02.0	07	01.6	02	02.0	02	01.5	*	*	54			
III	-	02.9	12.7	04.1	06.0	13.7	00.6	23.0	23	-05.2	01	*	*	*	09	02.0	09	01.3	18	01.8	*	*	04	01.8	*	*	53				
IV	-	06.1	13.0	06.3	07.9	14.2	01.9	23.2	30	-03.6	16	07	01.9	08	02.4	05	01.8	11	02.3	03	02.3	01	02.0	02	01.5	02	02.5	51			
V	-	12.2	18.1	11.0	13.1	19.9	04.6	26.6	19	01.0	13.11	*	*	*	*	08	02.1	11	01.9	08	01.8	03	01.7	02	01.5	*	*	61			
VI	-	15.2	21.1	15.1	15.6	22.9	06.3	27.2	19.13	02.0	05	*	*	09	02.0	08	01.4	06	01.5	07	01.7	01	02.0	02	01.5	05	01.5	56			
VII	-	17.5	24.6	16.5	18.6	26.0	10.0	29.6	30	06.6	01	*	*	*	03	03.0	16	01.8	12	02.0	01	02.0	03	01.7	04	01.5	54				
VIII	-	15.3	22.9	15.7	17.4	24.6	09.2	32.5	29	03.4	26	*	*	03	02.3	02	01.0	08	01.6	12	01.4	02	01.0	02	02.5	*	*	64			
IX	-	11.5	19.4	11.2	13.3	20.4	06.8	26.0	30	03.3	03	03.0	04	01.5	08	01.6	11	01.5	02	01.0	02	01.0	02	02.5	55						
X	-	03.5	16.9	06.4	08.3	17.9	01.1	21.0	20	03.6	02.0	01	01.0	05	01.2	04	01.0	01	01.0	02	01.5	*	*	74							
XI	-	04.0	10.8	05.6	06.5	12.3	01.6	21.5	11	-01.2	21	01	01.0	*	06	03.5	09	01.8	06	02.3	03	02.0	02	01.0	01	03.0	62				
XII	-	-02.0	06.3	-00.6	08.6	07.2	-04.8	10.8	21	11	-12.4	23	10	02.2	07	02.7	01	02.0	05	02.2	03	01.0	01	02.0	02	01.5	63				
GOD.	-	07.4	14.9	07.8	09.5	16.2	03.0	32.5	29	VM -12.2	01.1	28	02.0	37	02.2	63	02.0	104	01.8	92	01.8	17	01.6	15	01.8	712					
$\gamma = 42^{\circ}26' N \lambda = 18^{\circ}42' E$ Gr. $\Delta G = +1h\ 15\ min.$															TIJAT												BR. ST. 238				
I	762.7	05.6	11.3	06.7	07.6	12.2	02.9	17.2	29	-03.6	01	06	03.5	05	02.4	05	01.0	17	02.2	07	02.4	03	01.7	04	02.0	04	01.5	42			
II	760.9	07.9	13.5	09.5	10.1	14.4	05.7	20.7	26	-01.0	05	05	02.4	05	01.8	12	01.4	15	02.4	14	02.9	05	02.6	05	01.6	01	02.0	18			
III	765.0	10.4	16.1	10.1	10.9	17.0	05.4	24.4	26	-00.5	04	03.5	04	02.5	14	01.2	19	02.2	14	03.0	13	02.5	03	02.3	03	02.3	19				
IV	759.4	11.0	17.1	12.0	12.9	17.9	07.9	24.0	30	01.6	18	09	04.0	11	03.0	11	02.2	05	02.0	04	02.0	12	02.8	05	03.4	09	02.7	24			
V	-	16.9	22.2	15.6	17.5	23.5	11.6	32.2	19	06.7	11	04	01.0	09	01.6	08	01.0	04	01.8	09	02.4	14	02.5	04	02.8	02	01.0	39			
VI	759.5	24.6	26.0	20.4	26.0	14.1	29.3	20	09.6	06.0	01	03	02.7	02	01.5	10	01.1	18	01.1	07	02.4	19	02.6	01	02.0	01	02.0	39			
VII	758.7	22.7	28.1	22.0	23.7	29.2	17.3	32.1	22	14.4	14	07	02.3	08	02.5	09	01.8	10	01.0	11	01.7	08	02.6	17	02.3	03	02.0	25			
VIII	759.3	20.7	27.6	20.5	22.3	28.9	16.2	34.6	30	11.2	26	04	01.8	05	02.2	18	01.1	11	01.5	09	02.6	19	02.4	04	02.0	01	01.0	22			
IX	762.6	17.1	21.7	17.9	25.6	14.3	31.6	06	04.0	04	09	03.3	07	02.3	14	01.3	06	01.5	10	02.6	12	02.2	08	01.9	05	01.8	19				
X	765.3	20.2	20.8	12.1	13.8	22.2	08.2	26.2	09	04.4	05	05	01.6	05	02.0	12	01.0	15	01.9	09	02.0	17	01.9	04	01.2	02	01.5	29			
XI	759.8	09.7	16.1	11.0	11.9	18.1	07.5	25.6	11	-01.2	28	02	01.5	05	01.4	19	01.4	10	02.0	11	03.2	07	01.7	07	02.4	07	01.4	22			
XII	764.1	05.0	12.6	12.6	06.2	07.5	14.4	24.2	11	-04.0	14	16	03.9	10	04.1	07	01.3	17	01.6	05	03.0	04	01.5	04	02.2	26					
GOD.	762.2	15.4	19.5	15.1	16.3	20.4	12.6	33.2	08	IK	00.5	18	04.0	27	03.0	13	03.6	19	02.2	37	03.1	354	02.2	40	02.0	23	02.2	23	02.2	559	
$\gamma = 42^{\circ}24' N \lambda = 18^{\circ}56' E$ Gr. $\Delta G = +1h\ 16\ min.$															CETINJE												BR. ST. 240				
I	-	-01.1	05.9	00.6	01.5	07.0	-03.0	12.8	25	-11.7	20	*	*	*	*	01	02.0	07	04.7	01	04.0	*	*	03	01.7	03	02.7	78			
II	-	03.0	08.5	04.1	04.9	09.3	01.3	12.6	24	-05.5	16	01	04.0	02	02.0	05	02.0	12	02.9	05	03.2	*	*	05	03.6	05	04.0	48			
III	-	02.7	12.5	05.9	08.0	13.7	01.1	23.2	24	-05.5	01	02</																			

Mesec	Oblačnost Nm (0-10)			Insolacije broj sati Sred. (Dnev)	Vlažnost vazduha e <sub>m</sub> mm			Padavine R mm			Broj dana na sat												•	*	*	Δ	Δ	▲	▲	R <sub>t</sub>	≡	█			
	7	14	21		7	14	21	Sred. Min	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R <sub>t</sub>	≡	█						
											0.0	0.0	0.2	0.0	0.0	0.0	6	8	2.0	8.0	0.1	1.0	10.0												
<b>BR. ST. 236 HERCEGNOVI-IGALO</b>																																			
I	7.0	8.1	6.3	7.1	075.1	07.2	83	77	88	82	36	273	095.3	16	.	.	.	.	.	04	01	01	15	15	15	14	07	15	.	.	.				
II	7.2	7.3	7.0	7.2	096.2	08.2	91	75	89	85	32	272	047.7	17	.	.	.	.	.	11	03	02	15	18	18	10	18	.	.	.					
III	4.8	5.0	4.3	4.7	196.2	08.4	83	64	78	73	33	251	036.4	13	.	.	01	01	.	11	04	07	07	06	03	07	.	.	.						
IV	6.0	5.4	3.8	5.1	236.5	08.0	76	57	72	69	30	078	027.4	15	.	.	.	.	.	10	04	07	07	08	04	08	.	.	.						
V	4.7	6.0	4.5	5.0	253.4	11.8	80	63	82	75	43	136	068.4	14	.	.	.	.	.	02	06	07	07	06	03	07	.	.	.						
VI	3.0	4.4	3.4	3.6	308.4	14.3	80	65	85	77	42	040	021.2	26	.	.	21	01	.	03	01	10	03	07	05	02	07	.	.	04					
VII	2.5	2.7	2.3	2.7	351.4	15.7	74	59	64	59	30	141	059.5	27	.	.	31	09	07	08	01	14	07	07	04	07	.	.	04						
VIII	3.7	4.0	2.3	3.3	289.4	15.3	78	60	78	72	40	176	086.2	23	.	.	30	06	06	07	03	16	02	10	08	05	10	.	.	01					
IX	3.4	4.3	3.1	3.6	235.6	12.7	79	59	80	73	33	210	093.5	21	.	.	15	03	.	11	03	12	04	13	10	03	13	.	.	04					
X	2.0	2.9	2.0	2.9	230.8	11.0	85	67	91	81	40	080	049.8	12	.	.	01	.	.	03	01	16	04	05	02	05	.	.	02						
XI	6.8	7.2	6.6	6.7	101.8	09.7	91	75	89	85	41	285	080.8	02	.	.	12	03	02	13	18	15	08	16	.	.	01	07	.						
XII	4.5	4.0	3.9	4.4	141.2	08.3	76	60	74	70	32	245	085.5	07	.	.	14	09	10	08	12	09	06	12	.	.	04	.	.	.					
GOD.	4.7	5.3	4.1	4.7	2515.9	10.7	81	65	82	76	30	2191	096.4	43.0	.	.	01	107	21	13	94	29	108	67	127	111	57	127	.	.	04				
<b>BR. ST. 237 GRAHOVO</b>																																			
I	7.0	6.9	5.8	6.6	-	04.8	89	84	92	88	60	584	210.4	12	02	.	22	.	01	.	03	17	12	11	07	12	03	02	.	.	02				
II	7.7	6.5	5.9	6.8	-	05.8	90	78	91	87	60	350	068.2	02	.	.	09	.	.	01	12	16	16	12	15	03	02	.	.	01					
III	4.4	4.5	3.4	4.1	-	06.1	89	66	93	83	33	528	174.6	21	.	.	14	.	.	14	06	08	08	08	08	08	08	.	.	01					
IV	4.9	5.1	4.0	4.7	-	06.0	78	84	73	82	23	149	034.2	02	.	.	07	.	.	08	07	10	09	05	10	02	02	.	.	01					
V	4.2	5.5	4.0	4.6	-	08.5	77	61	82	74	33	096	027.2	10	.	.	04	.	.	08	06	09	07	03	05	.	.	01	01	.					
VI	2.7	2.6	2.2	3.5	-	10.4	75	46	77	73	35	035	012.2	27	.	.	11	.	.	13	04	07	06	01	07	.	.	01	.	.					
VII	2.1	3.1	1.8	2.3	-	12.7	77	67	79	74	42	049	020.8	07	.	.	24	.	.	16	01	06	04	02	06	.	.	01	.	.					
VIII	3.4	4.5	2.4	3.6	-	12.2	81	70	84	78	46	268	082.4	23	.	.	16	02	.	12	11	10	04	11	.	.	03	.	.						
IX	3.0	3.7	2.9	3.2	-	09.6	85	65	86	78	33	313	129.2	21	.	.	01	08	.	16	04	09	06	04	05	.	.	01	.	.					
X	2.6	2.5	1.4	2.1	-	06.7	89	57	87	78	30	305	136.4	11	.	.	16	.	.	20	02	04	04	04	05	.	.	01	.	.					
XI	6.7	6.5	5.3	6.2	-	06.4	91	72	91	85	38	387	068.9	02	.	.	11	.	.	02	01	05	13	16	15	02	01	.	.	01					
XII	4.5	4.1	2.6	3.8	-	04.2	86	66	90	81	21	241	070.6	10	06	.	26	.	01	.	17	08	08	07	03	08	02	.	.	03					
GOD.	4.4	5.0	3.5	4.3	-	07.8	83	67	86	79	21	3310	210.4	42.1	08	.	106	63	02	.	05	01	133	80	116	105	67	114	12	08	.	02	07	18	08
<b>BR. ST. 238 TIVAT</b>																																			
I	7.0	7.5	6.2	7.0	-	06.5	86	69	87	81	35	185	066.0	13	.	.	06	.	.	01	02	13	15	14	07	15	.	.	.	01	04	01			
II	7.2	7.5	6.0	6.9	-	07.8	91	68	88	82	33	174	024.4	14	.	.	02	.	.	01	01	13	18	15	08	18	.	.	.	06	.	.			
III	4.7	4.7	3.7	4.4	-	07.7	85	60	85	77	27	110	044.4	13	.	.	01	.	.	02	02	08	06	03	08	.	.	01	.	.	01				
IV	5.9	5.2	3.0	4.7	-	07.5	73	52	74	66	25	082	020.4	15	.	.	.	.	.	06	04	09	09	03	10	.	.	01	04	01	.				
V	4.4	5.4	3.9	4.6	-	11.3	78	57	85	73	36	118	040.6	09	.	.	05	02	.	09	06	09	07	05	09	.	.	06	.	.	.				
VI	2.8	4.4	2.6	3.3	-	13.7	77	59	86	74	41	042	011.6	17	.	.	22	.	.	13	03	05	05	03	05	.	.	04	.	.	.				
VII	2.1	3.0	1.6	2.3	-	15.0	72	54	75	63	33	090	028.7	23	.	.	31	09	04	.	18	03	05	04	05	04	.	.	04	.	.	.			
VIII	2.1	3.1	1.6	2.7	-	14.9	88	56	82	73	38	134	046.3	23	.	.	31	08	01	.	17	02	12	07	04	12	.	.	06	.	.	.			
IX	3.6	3.8	2.9	3.5	-	11.9	76	54	78	70	33	136	046.1	24	.	.	17	02	.	01	01	14	03	10	09	03	10	.	.	06	.	.	.		
X	2.4	2.8	1.4	2.2	-	09.9	90	43	90	81	35	139	109.2	11	.	.	01	.	.	01	15	05	04	03	05	.	.	02	.	.	.				
XI	5.9	6.9	5.9	6.2	-	09.1	91	72	88	84	39	152	041.5	23	.	.	01	01	.	02	11	17	12	06	17	.	.	02	.	08	02				
XII	4.5	4.5	3.2	4.0	-	05.7	78	57	77	74	23	164	044.4	30	.	.	09	.	.	05	13	08	10	09	05	10	.	.	04	.	.	.			
GOD.	4.5	4.6	3.3	4.4	-	10.1	81	60	82	75	23	1489	066.0	43.0	.	.	19	113	21	05	07	01	127	75	126	105	54	126	.	.	02	02	59	10	
<b>BR. ST. 239 BUČVA</b>																																			
I	7.0	7.5	6.9	7.3	-	073.7	07.5	85	76	82	28	174	029.6	14	.	.	.	.	.	03	01	04	11	12	07	13	.	.	01	02	.	.			
II	7.9	7.0	6.0	7.0	-	092.5	08.1	86	74	87	83	154	022.8	12	.	.	10	.	.	01	11	18	14	09	18	.	.	.	05	.	.	.			
III	4.8	4.1	3.9	4.3	-	181.8	08.3	79	68</																										

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Mesec	Vazdušni Pratisk Fm mm	Temperatura vazduha °C						Cestina pravaca i srednja jačina veta nD, Fm (0-12)																				
		Tm			Sred. (Dnes)	Max	Min	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		7	14	21							8.	9.	10.	11.	12.	13.	14.	15.	16.	17.								
$\gamma = 42^{\circ}46' N \lambda = 18^{\circ}57' E$ Gr. $\Delta G = + 1h 16 min.$																												
I	706.2	00.9	05.7	02.6	03.0	06.5 -00.1	12.8	25 -06.6	01	22	02.1	20	02.2	02	01.5	06	03.0	25	03.7	03	02.7	05	01.2	03	01.7	07		
II	704.6	04.2	08.2	05.1	05.6	09.1	02.7	16.8	24 -03.6	08	20	02.6	13	02.3	07	01.6	07	32	03.6	03	05.7	02	02.0	04	01.8	03		
III	708.6	04.6	12.8	06.1	06.4	13.8	03.4	23.5	24 -08.0	01	18	01.9	18	02.0	06	02.5	07	01.9	34	03.8	05	02.4	02	02.5	02	02.0	01	
IV	703.7	06.8	13.2	08.0	09.4	14.3	04.5	23.8	30 -01.0	18	23	02.6	20	02.6	04	03.0	09	01.4	20	03.8	02	03.5	03	02.7	06	02.3	03	
V	706.2	12.3	18.4	13.4	14.4	20.0	08.6	27.0	19 04.0	11	25	01.5	14	01.6	07	01.1	06	02.2	25	03.4	03	02.0	03	01.7	04	01.0	06	
VI	705.2	15.1	21.5	14.1	17.2	23.5	10.8	26.8	09 04.2	08	23	01.7	13	02.4	04	03.0	04	01.2	20	03.4	06	03.2	06	01.5	06	02.2	05	
VII	705.2	18.1	26.2	20.0	21.1	27.4	14.1	31.4	30 10.4	28	26	02.1	13	02.1	02	02.5	10	02.5	22	03.8	06	03.7	05	01.8	06	01.8	03	
VIII	705.7	16.1	24.2	17.8	19.0	25.9	13.1	33.8	29 08.6	25.15	21	01.4	04	01.2	04	02.5	17	02.9	06	02.8	04	02.5	05	01.8	03			
IX	706.1	12.9	19.7	14.3	15.3	20.6	10.6	27.8	08 06.6	30	31	02.2	39	02.3	01	03.0	02	03.0	18	03.3	*	*	05	01.4	02	02.5	01	
X	710.0	04.8	17.2	9.7	10.9	18.5	05.5	22.6	09 01.0	05	26	01.7	31	01.7	02	02.0	03	04.0	25	03.0	02	02.5	01	*	01	01.0	03	
XI	704.4	05.2	10.8	06.9	07.5	11.6	03.8	22.2	11 -03.9	21	27	01.5	19	01.6	02	02.3	23	03.0	06	01.4	01	04.0	02	02.5	04			
XII	707.7	00.5	05.8	01.7	02.5	07.2	-01.2	12.3	21 -06.4	23	35	02.9	25	03.4	01	02.0	04	01.5	12	01.8	05	01.4	02	01.0	04	02.2	03	
GOD.	706.3	08.6	15.3	10.4	11.2	16.6	06.3	33.8	29.W -06.6	04.	301	02.0	241	02.1	35	02.2	66	02.1	213	03.4	47	02.8	38	01.8	45	01.9	47	
$\gamma = 42^{\circ}14' N \lambda = 19^{\circ}05' E$ Gr. $\Delta G = + 1h 16 min.$																				VIRPAZAR		BR. ST. 242						
I	-	02.7	08.2	04.3	04.9	-	01.2	-	-03.0	20.01	*	*	23	02.3	*	07	02.0	01	01.0	09	01.0	09	01.4	09				
II	-	07.2	13.8	08.4	09.4	14.1	05.2	20.2	25 02.0	28.08	*	*	*	*	01	02.0	20	02.7	04.5	48	02.5	05	01.2	*	*	07		
III	-	07.1	17.9	09.6	11.1	18.1	04.3	26.0	26 -01.0	03.02	*	*	*	*	37	02.4	05	01.4	37	02.2	07	01.1	*	*	07			
IV	-	08.4	17.4	10.3	11.6	17.6	05.8	24.8	30 01.5	18	05	01.0	35	02.5	01	02.0	11	02.1	01	01.0	26	01.9	05	01.0	02	02.0	04	
V	-	12.8	21.7	15.0	16.3	21.8	09.1	26.6	01	07.5	31.15	*	*	*	*	03	02.3	27	02.0	05	01.0	36	01.5	11	01.0	*	*	11
VI	-	17.8	27.3	18.6	20.6	27.5	11.4	32.0	19 07.0	01	*	*	*	*	02	01.0	16	21	02.1	03	01.7	52	02.3	04	01.1	*	*	09
VII	-	21.0	26.9	21.5	23.2	29.0	13.9	32.8	19 11.5	07.06	*	*	*	*	28	02.0	04	01.2	42	02.2	09	01.3	*	*	10			
VIII	-	22.7	31.4	23.3	25.2	32.0	17.2	37.6	30 14.0	01	*	*	*	*	01	02.0	21	02.0	03	01.3	42	02.4	15	01.1	*	*	11	
GOD.	-	16.9	20.0	12.3	13.9	-	07.2	-	-05.0	24.25	12	01.1	176	02.3	09	01.9	177	02.2	33	01.6	409	02.1	117	01.1	47	01.5	115	
$\gamma = 42^{\circ}06' N \lambda = 19^{\circ}06' E$ Gr. $\Delta G = + 1h 16 min.$																				BAR		BR. ST. 243						
I	762.5	07.7	11.2	08.1	08.8	12.6	04.5	18.1	29 -07.7	20	04	02.8	34	01.9	12	01.4	14	03.0	05	02.0	13	02.2	08	01.8	02	01.0	01	
II	760.9	09.7	15.1	10.3	10.8	14.3	07.7	21.1	24 01.7	05	03	01.7	22	02.3	11	01.7	20	02.4	10	02.8	06	01.8	08	01.9	01	02.0	03	
III	765.0	09.6	14.6	10.5	11.3	15.9	07.3	24.6	30 01.0	01	05	02.6	24	01.6	18	01.3	14	02.5	05	02.6	05	02.2	14	02.3	03	01.7	03	
IV	759.2	11.9	15.7	12.1	12.7	19.0	08.0	23.0	08 05.2	18	03	04.3	35	02.0	14	01.5	04	01.0	01	02.0	08	02.4	19	03.0	03	02.7	03	
V	760.8	17.7	21.0	16.1	17.7	22.4	13.4	32.0	19 08.4	11	02	02.0	29	01.7	20	01.4	01	01.0	04	01.8	11	01.5	18	02.2	03	01.7	05	
VI	759.4	20.1	23.0	18.4	20.0	24.1	15.4	27.1	30 10.5	01	05	01.2	27	01.5	18	01.1	01	01.0	04	02.5	07	02.0	26	02.6	01	01.0	05	
VII	758.7	23.5	26.2	20.0	23.4	27.7	18.6	33.0	22 16.0	22	06	01.7	24	01.5	16	01.6	03	03.0	04	02.5	09	02.2	15	02.8	06	02.2	10	
VIII	759.1	22.5	26.2	21.1	22.7	27.5	18.2	31.2	31 14.5	27	01.5	01.8	30	01.8	18	01.6	04	02.5	06	02.5	24	02.6	*	*	*	04		
IX	762.3	15.1	23.0	18.6	19.8	24.8	16.1	30.4	06 07.9	30	04	01.5	40	02.3	13	02.2	06	03.0	04	02.8	06	02.3	15	02.7	01	02.0	01	
X	765.1	13.6	19.6	15.3	21.0	24.0	11.4	26.2	09 07.8	05	01	02.0	32	02.0	24	01.8	05	02.6	14	02.1	20	02.2	02	02.0	02			
XI	755.8	12.0	15.9	12.8	13.4	17.9	09.8	23.0	11 01.7	27	01	02.0	29	01.9	19	01.6	08	03.5	10	03.3	09	02.6	09	02.2	04	02.8	01	
XII	763.9	07.6	11.7	07.5	08.6	13.4	04.7	18.4	01 -06.6	13	06	03.7	40	03.0	21	02.0	05	02.6	07	03.3	09	02.2	03	01.2	02	02.0	00	
GOD.	761.4	14.6	18.4	14.3	15.4	19.9	11.4	33.0	22.W -00.7	20.	42	02.3	366	02.1	202	01.7	85	02.6	57	02.7	96	02.1	182	02.4	28	02.1	37	
$\gamma = 42^{\circ}22' N \lambda = 19^{\circ}15' E$ Gr. $\Delta G = + 1h 17 min.$																				TITCGRAC-GCLUBCVCI		BR. ST. 244						
I	760.8	03.6	09.1	04.5	05.5	10.4	01.8	16.4	29 -04.4	20	06	03.2	55	03.6	02	01.5	02	02.0	08	02.8	03	01.7	04	01.8	*	*	63	
II	758.7	06.9	12.9	08.7	09.3	13.8	05.7	21.2	24 -04.4	08	11	01.9	07	03.1	01	02.0	11	02.1	15	02.3	03	02.0	02	02.0	*	*	34	
III	762.7	07.8	16.3	11.0	11.5	17.5	06.0	27.0	24 -00.8	03	15	02.3	11	03.2	03	01.3	04	02.8	19	02.3	06	02.0	01	02.0	*	*	34	
IV	756.9	11.2	17.7	12.4	13.4	18.6	08.0	27.6	30 02.4	17	15	03.4	16	03.3	03	02.0	08	02.5	16	02.3	03	02.0	02	02.0	01	02.0	26	
V	756.6	14.8	23.2	17.4	19.7	24.5	13.2	32.0	19 07.2	11	22	02.3	07	02.3	01	02.0	03	02.7	17	02.0	07	02.3	04	01.5	*	*	32	
VI	756.9	20.																										



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Meseč Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra nD, Fm (0-12)																		
	Tm			Sred. (dies)		Max		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C	
	7	14	21	Max	Min	Max	Dat.	Min	Dat.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.				
γ = 42°50' N λ = 19°32' E Gr. ΔG = + 1h 18 min.																								KLASIN	RR. ST. 246				
I	-02.3	03.4	-00.8	-00.1	04.6	-04.0	08.6	25	-14.6	20	14	03.4	.	.	.	.	.	21	02.6	07	02.0	01	01.0	.	.	50			
II	075.3	01.8	06.3	02.5	03.3	07.5	00.2	16.0	24	-07.4	28	15	02.6	.	.	.	.	30	02.7	06	02.0	02	02.0	02	02.0	59			
III	682.6	00.3	10.6	02.6	04.5	12.0	-01.0	22.4	24.2	-05.2	03	19	02.4	.	.	.	.	17	01.8	17	02.3	01	01.0	02	01.0	37			
IV	675.1	33.1	11.0	05.2	06.1	12.6	01.0	23.0	30	-04.8	18	25	02.6	.	.	.	.	08	01.9	18	02.3	06	01.0	05	01.6	26			
V	681.8	08.0	16.6	09.1	10.7	18.3	04.6	26.2	19	-00.4	30	09	02.9	.	.	.	.	12	02.1	23	02.0	03	01.7	05	01.4	41			
VI	681.1	09.8	18.3	11.2	12.6	20.6	06.7	25.6	13	-00.8	05	16	02.7	.	.	.	.	11	01.5	17	02.6	10	01.6	04	01.0	32			
VII	681.4	12.9	23.0	14.5	16.2	24.3	05.4	28.2	30.9	06.0	14	14	02.7	.	.	.	.	03	02.3	24	02.3	17	01.4	07	01.4	28			
VIII	681.8	10.7	22.0	13.3	14.8	23.7	09.0	31.8	30	04.0	26	10	02.0	.	.	.	.	09	02.4	14	02.1	04	01.8	05	01.8	51			
IX	684.0	08.0	16.3	09.5	10.8	17.3	06.7	24.8	01	-05.0	30	33	02.7	.	.	.	.	07	02.1	08	02.0	04	01.5	07	01.9	31			
X	685.5	01.7	15.8	05.3	07.0	16.7	00.8	20.6	09	-02.0	18	21	02.4	.	.	.	.	07	01.9	09	02.3	.	02	01.0	04	54			
XI	682.9	02.5	08.4	04.0	04.7	09.6	00.6	19.4	12	-02.2	28	16	01.6	.	.	.	.	23	02.3	11	01.6	01	01.0	03	01.0	36			
XII	682.9	-04.2	01.3	-02.9	-02.2	-06.0	09.2	01	-15.2	06	41	03.0	.	.	.	.	09	01.6	07	02.3	.	.	.	.	36				
GOD.	681.8	04.4	12.8	04.2	07.4	14.2	02.4	31.8	30W	-15.2	06X	233	02.6	.	.	.	.	157	02.2	161	02.2	49	01.5	42	01.5	453			
γ = 42°50' N λ = 19°52' E Gr. ΔG = + 1h 19 min.																								IVANGRAD	BR. ST. 247				
I	-02.3	04.2	00.1	00.5	05.5	-04.1	14.4	29	-17.9	19	10	01.7	06	02.0	.	02	01.0	12	02.4	11	02.4	01	01.0	05	01.6	46			
II	-03.4	09.1	05.5	05.9	10.6	01.9	20.3	24	-05.0	28	13	C2.1	04	01.8	01	01.0	05	01.5	15	03.5	24	03.7	.	07	01.7	15			
III	-01.4	12.9	06.6	06.9	14.0	00.5	24.9	23	-07.4	01	08	01.5	18	01.6	C3	01.0	02	01.0	13	02.5	12	02.7	04	01.2	09	01.1	24		
IV	-04.7	13.3	07.9	08.4	14.6	02.2	27.5	29	-04.9	18	17	01.9	12	01.8	C5	01.6	02	01.5	09	03.1	12	02.6	01	02.0	07	02.1	25		
V	-10.2	19.6	12.1	13.5	21.2	06.3	30.6	19	00.6	30	15	01.9	11	01.4	C2	01.5	03	01.3	C8	02.5	14	02.9	07	02.3	04	01.2	29		
VI	-12.3	21.4	14.6	15.7	23.0	08.4	26.7	14	00.6	05	14	01.9	13	01.8	C4	01.2	01	02.0	07	02.3	12	02.3	07	01.9	06	01.3	26		
VII	-15.1	25.2	17.9	19.1	26.7	11.0	31.0	30.1	21.7	14	08	C2.1	15	01.5	C3	01.3	02	01.0	05	03.2	17	03.5	05	01.2	11	01.8	27		
VIII	-13.3	24.3	15.9	17.4	25.8	10.2	33.0	30	04.6	27	14	01.6	16	01.7	C2	02.0	06	01.7	C6	02.2	12	03.8	04	01.8	06	01.3	27		
IX	-05.8	18.2	12.1	13.0	19.2	08.4	26.8	09	-04.2	30	16	02.2	17	01.9	C1	01.0	01	01.0	05	01.8	06	02.3	07	02.1	13	02.6	24		
X	-02.8	17.1	06.6	08.3	18.3	01.5	24.3	09	-03.4	18	07	01.6	12	01.4	C6	01.2	05	01.0	04	01.0	09	02.1	.	06	01.8	44			
XI	-03.6	10.5	05.9	06.5	11.9	02.4	20.5	04	-07.3	28	05	01.8	13	01.4	C3	01.3	05	01.2	11	02.4	16	02.4	04	01.0	05	02.0	29		
XII	-03.7	00.7	-02.8	-02.1	02.2	-03.7	13.4	29	-15.5	06	16	02.4	19	02.2	C1	02.0	04	01.0	05	02.6	04	01.8	03	01.0	08	01.5	33		
GOD.	-	05.9	14.7	08.5	09.4	16.1	03.6	33.0	30W	-17.9	49	143	01.9	156	01.7	20	C1.3	38	01.3	100	02.6	149	02.9	43	01.7	349			
γ = 41°55' N λ = 19°13' E Gr. ΔG = + 1h 17 min.																								ULCINJ	BR. ST. 248				
I	754.0	06.1	10.2	07.2	07.7	11.5	04.8	18.2	29	00.3	09	02	02.5	18	03.3	C1	03.0	03	02.0	11	04.3	01	02.0	06	02.7	01	02.0	.	
II	752.4	39.5	12.7	10.0	10.6	13.9	08.1	20.6	24	-02.4	28	05	03.2	16	02.4	18	02.7	12	02.7	15	03.3	03	04.0	09	02.9	06	03.0	.	
III	756.2	10.1	15.5	12.0	12.4	16.6	08.8	25.4	24	-00.1	01	07	02.6	19	02.8	22	02.5	06	02.5	05	02.4	11	03.4	10	03.2	11	03.4	02	
IV	750.7	11.4	16.2	12.1	12.9	17.4	05.4	23.8	08	05.0	18	12	03.7	14	02.1	29	02.5	07	02.7	05	02.8	01	03.0	09	02.3	22	03.2	.	
V	752.4	17.4	22.1	17.2	18.5	23.5	14.6	32.7	19	05.6	11	05	02.6	05	02.0	43	02.3	07	02.7	.	03	03.0	08	02.5	21	03.1	01		
VI	751.0	19.7	24.7	19.3	20.7	25.9	16.8	25.2	29	11.6	04	07	03.7	02	02.0	36	02.1	09	02.1	.	01	02.0	10	03.1	23	03.3	02		
VII	750.5	23.0	28.1	22.9	24.2	29.2	20.0	33.9	30	15.2	01	09	03.8	04	01.8	35	02.3	08	02.4	07	02.3	02	02.5	08	03.0	19	03.5	01	
VIII	750.9	22.2	28.2	23.5	23.8	29.2	19.5	36.4	30	14.7	24	09	02.9	22	02.5	04	02.4	15	02.4	02	02.0	02	05.0	09	03.1	25	03.2	.	
IX	753.5	17.9	24.0	15.0	20.0	24.8	16.5	31.0	08	08.6	30	29	03.0	06	02.0	36	02.6	10	03.2	08	03.1	02	02.5	04	03.0	12	03.2	03	
X	756.6	13.3	20.3	15.7	16.3	21.1	12.1	24.0	09	08.4	06	04	01.2	20	02.0	35	02.4	07	02.4	08	02.4	13	02.3	.	02	01.5	04	02.7	.
XI	751.4	11.4	15.2	12.7	13.0	16.7	09.9	22.6	11	03.0	28	02	02.4	37	02.4	07	04.6	05	03.4	09	03.8	10	02.7	.	02	04.5	05	02.6	.
XII	755.2	05.5	10.1	07.1	11.0	16.0	16.6	01.0	00.0	13	01	04.0	32	02.9	46	02.9	03	02.3	04	05.0	.	02	04.5	05	02.6	.			
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
γ = 42°01' N λ = 20°53' E Gr. ΔG = + 1h 24 min.																								TETCVO	BR. ST. 250				
I	-03.0	01.9	-00.8	-00.7	03.2	-04.5	15.0	31	-12.0	11.0	04	02	01.5	01	03.0	.	01	02.0	02	02.0	11	01.2	.	06	01.0	70			
II	-03.5	10.9	07.4	07.3	12.7	02.7	23.0	23	-03.5	05	07	01.3	01	02.0	.	03													

Mjesec	Oblačnost Nm (0-10)	Sred. (Dnev.)	Insolacije Broj sati	Vlažnost vazduha				Padavine R mm				Broj dana na sat																												
								Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	T	≡																
				mm	7	14	21	Sred. (Dnev.)	Min	Σ	Max	Dat.	30.00.0	0.0250.0	20.0	6	8	2.0	8.0	0.1	1.00.0.0	9	Δ	*	Δ	Δ	Δ	T	≡											
<b>KLASIN</b>																																								
<b>BP. ST. 246</b>																																								
I	8.3	6.1	6.9	7.8	070.7	04.2	95	76	52	88	45	320	096.4	13	05	04	24	.	.	03	02	02	15	18	16	07	13	06	01	.	.	.	04	05	27					
II	8.4	8.5	7.2	8.0	077.9	04.9	92	71	85	84	34	318	082.4	12	.	.	12	.	.	02	15	20	17	05	09	10	05	02	.	.	01	02	01	04						
III	5.9	6.1	4.2	5.4	166.2	04.8	92	55	83	77	23	254	069.2	31	.	02	21	.	.	02	07	10	14	11	06	14	05	01	.	.	04	01	03							
IV	6.8	6.2	5.1	6.0	184.5	05.3	87	55	80	74	29	315	100.6	01	.	.	12	.	.	01	03	09	16	11	08	11	09	04	.	.	03	01	04							
V	5.4	6.9	4.7	5.7	224.6	07.4	91	55	87	78	17	086	023.1	10	.	.	01	01	.	.	04	08	12	10	02	12	.	.	.	01	02	04	06							
VI	6.4	7.0	5.5	6.2	221.1	05.2	92	62	93	82	40	065	020.6	14	.	.	01	05	.	.	03	04	17	12	02	18	01	.	.	02	08	14								
VII	5.0	5.1	3.0	4.3	270.0	10.4	88	51	88	76	34	050	017.6	18	.	.	17	.	.	06	01	10	98	20	10	.	.	.	03	12	.									
VIII	6.4	6.4	2.6	5.2	218.7	04.2	81	61	81	59	34	288	095.9	22	.	.	11	02	.	.	03	05	12	12	08	12	.	.	.	12	18	.								
IX	6.8	6.4	5.4	6.2	165.1	08.3	53	63	91	82	23	184	045.2	18	.	.	02	05	.	.	06	11	15	10	05	15	.	.	.	05	06	.								
X	4.5	3.5	2.2	3.4	195.6	06.0	97	50	80	21	164	088.2	03	.	.	18	.	.	.	13	C3	07	05	03	07	.	.	.	01	10	.									
XI	8.7	7.8	7.6	8.0	083.5	05.8	95	76	91	87	37	372	060.0	10	.	.	14	.	.	01	01	19	18	17	09	15	07	02	.	.	05	06	07							
XII	6.2	6.2	4.5	5.6	097.2	03.6	90	75	89	85	44	242	050.1	30	10	07	25	.	.	10	13	14	13	08	10	08	03	.	.	01	02	22								
GOD.	6.6	6.4	4.8	5.9	1979.0	06.7	92	62	88	81	17	2658	100.8	04IV	15	13	130	34	02	.	10	03	58	113	173	142	67	152	47	13	.	.	01	05	52	84	67			
<b>IVANGRAD</b>																																								
<b>BP. ST. 247</b>																																								
I	9.5	6.2	7.2	8.3	-	04.1	54	71	85	83	28	104	044.9	13	03	04	25	.	.	10	.	21	14	11	02	11	04	.	.	.	02	12	13							
II	8.6	8.7	7.6	8.3	-	04.9	63	58	73	72	26	088	026.2	02	.	.	10	.	.	15	09	16	13	10	03	13	01	.	.	03	01	.								
III	6.6	6.5	5.0	6.2	-	05.0	91	48	72	70	21	077	028.4	31	.	.	14	.	.	11	02	03	10	12	06	02	10	03	.	.	03	03	.							
IV	6.8	7.3	6.0	6.7	-	05.2	82	47	65	65	25	122	043.7	16	.	.	11	02	.	12	04	03	10	15	10	05	12	05	01	.	01	01	.							
V	6.4	7.9	5.3	6.5	-	07.6	84	43	71	67	21	070	018.0	26	.	.	09	01	.	14	07	03	12	10	07	03	10	01	01	.	.	03	.							
VI	6.3	7.2	5.9	6.4	-	09.1	82	47	78	65	26	085	017.7	02	.	.	13	.	.	07	06	01	10	09	04	12	.	.	.	01	10	02								
VII	4.7	5.7	4.1	4.8	-	10.5	84	42	73	67	25	040	019.6	24	.	.	22	07	.	11	06	05	09	07	01	05	.	.	.	05	.	.								
VIII	5.6	5.8	3.3	4.9	-	10.5	88	47	82	72	31	086	024.7	07	.	.	20	04	.	08	07	04	15	10	09	13	00	.	.	05	03	.								
IX	7.8	6.7	6.1	6.9	-	08.7	93	54	84	77	27	116	026.3	18	.	.	02	05	.	06	02	02	10	14	11	04	14	.	.	.	04	05	.							
X	7.8	4.0	2.7	5.0	-	06.4	97	49	59	75	27	093	075.7	03	.	.	14	04	.	02	01	04	06	06	05	03	06	.	.	.	01	16	.							
XI	9.8	8.0	7.5	8.2	-	05.9	91	66	84	80	40	109	022.0	17	.	.	09	.	.	05	07	06	19	16	12	04	12	06	03	.	.	02	10	06						
XII	9.5	7.0	7.4	8.2	-	03.5	90	76	87	84	50	071	021.5	30	09	12	25	.	.	08	02	01	20	13	04	02	05	08	02	.	.	12	18	.						
GOD.	7.4	7.4	5.1	5.7	6.7	-	06.8	88	54	78	73	21	1020	044.9	45.1	.	.	12	18	110	72	12	.	112	47	26	147	144	106	36	125	28	07	.	.	01	01	40	59	.
<b>LLCINJ</b>																																								
<b>BR. ST. 248</b>																																								
I	6.8	7.2	5.7	6.6	092.7	05.5	76	65	74	72	24	176	067.9	13	.	.	.	.	.	22	06	03	11	13	05	05	13	.	.	.	01	04	.							
II	7.4	6.2	6.4	7.0	093.9	07.5	80	73	77	75	27	085	021.2	14	.	.	.	.	.	21	04	.	12	15	14	03	15	.	.	.	06	.	.							
III	4.6	4.4	4.0	4.3	207.5	07.3	70	66	69	65	29	092	055.9	14	.	.	01	.	.	20	04	13	07	08	07	02	08	.	.	.	02	02	01							
IV	5.4	4.0	3.8	4.1	276.0	10.6	72	55	69	67	22	021	011.2	10	.	.	11	02	01	17	02	12	05	06	04	01	06	.	.	05	.									
V	4.5	4.0	3.8	4.1	232.5	12.9	74	56	73	68	31	010	004.0	27	.	.	22	.	.	15	02	14	02	05	03	05	.	.	.	04	03	.								
VI	3.2	2.1	2.0	2.8	323.5	12.9	74	56	73	68	31	010	004.0	17	.	.	31	09	18	20	02	18	05	02	02	05	.	.	.	04	03	.								
VII	2.4	2.4	1.1	1.9	344.7	14.5	67	54	68	63	34	052	034.8	01	.	.	30	12	16	23	05	16	07	02	07	01	07	.	.	08	.									
VIII	3.1	2.5	1.8	2.5	319.8	14.1	67	55	67	63	37	058	036.5	24	.	.	30	12	16	23	05	16	07	02	07	01	08	.	.	08	.									
IX	3.8	2.8	3.2	3.3	253.2	10.8	66	51	63	60	18	100	027.2	19	.	.	14	03	06	19	02	13	02	11	11	09	04	11	.	.	07	.								
X	2.7	2.3	1.8	2.3	249.5	09.7	76	60	72	69	32	079	044.4	12	.	.	.	.	.	10	03	02	11	17	15	04	17	.	.	05	.									
XI	7.0	6.8	6.1	6.6	129.0	08.5	78	68	74	73</																														





Meseč	Vrednost Pratnje Po mm	Temperatura vazduha °C							Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																				
		Tm			Sred. (Dnev.)	Max	Min	Max	Dne.	Min	Dne.	N		NE		E		SE		S		SW		W		NW			
		7	14	21								E.	J.																
Υ = 41°32' N λ = 20°42' E Gr. ΔG = + 1h 23 min.																													
I	650.4	-0.2	7	01.9 -01.6 -01.1	03.2 -04.2	05.1	29 -13.1	19	22	02.1	24	02.2	04	03.2	05	06	03.5	12	02.6	15	02.1	03	02.7	07	01.0	0.5			
II	646.3	0.1	8	04.8 01.8 02.4	06.4 -00.5	16.4	24 -05.5	28	09	01.9	10	02.1	04	03.0	10	02.7	09	03.1	20	02.8	09	02.2	08	01.0	0.5	0.0			
III	653.4	0.1	8	08.8 03.5 04.2	10.0 -00.3	14.6	25 -23 -12.6	01	19	02.4	22	02.4	08	02.5	09	01.9	05	02.8	04	02.5	08	02.0	11	01.5	0.5	0.5			
IV	648.7	0.4	10	10.0 05.4 06.2	11.4 -00.8	20.9	29 -06.0	14	08	02.6	03	02.0	16	02.9	19	02.7	10	03.1	04	03.0	11	01.5	0.6	01.8	1.3				
V	752.2	09.6	15.5	10.3	11.5	16.8	06.1	23.6	20	-00.3	12	07	01.9	15	01.7	11	02.1	08	02.2	08	02.0	11	02.8	07	03.0	04	02.0	22	
VI	651.4	11.5	17.5	11.6	13.1	18.1	07.0	23.6	14	00.6	05	07	03.0	15	03.1	10	02.6	01	02.0	22	01.7	13	02.0	05	01.4	01	03.0	0.5	
VII	652.1	12.4	21.0	15.6	17.0	23.3	16.3	26.7	31	06.6	02	09	03.3	23	03.4	12	02.2	02	01.5	26	01.9	05	01.6	02	02.0	01	1.4	0.5	
VIII	652.5	13.6	21.0	14.6	16.0	22.6	16.1	32.1	29	03.9	12	03.2	04	03.4	23	01.7	07	01.7	07	05	02.0	05	01.8	07	02.9	1.0	0.5	0.5	
IX	653.9	08.5	15.3	09.4	10.7	16.4	04.6	22.8	01	-04.0	30	14	02.1	12	02.1	10	02.0	10	02.1	07	02.0	02	01.0	14	01.2	09	01.8	1.2	
X	753.5	04.7	13.3	06.4	07.7	14.3	03.0	15.0	08	-03.2	17	16	02.1	22	02.2	15	02.0	11	01.5	03	01.7	08	02.1	07	02.6	04	03.2	0.5	
XI	649.6	0.8	03.8	07.7	04.9	05.3	09.2	01.6	15.7	04	-07.3	21	14	02.1	14	02.4	15	01.9	04	01.5	03	02.7	13	04.1	01	05.0	0.2		
XII	651.5	-03.5	00.8	-02.9	-02.2	02.6	-05.7	06.7	30.0	-14.9	05	09	02.7	05	02.2	07	02.4	10	02.5	21	02.2	12	02.2	07	01.6	11	01.7	1.1	
GOD.	668.4	05.6	11.5	06.6	07.6	12.9	02.9	32.1	39W	-14.9	05.XX	146	02.4	179	02.5	116	02.4	91	02.2	149	02.1	56	02.4	103	02.3	81	02.3	134	
Υ = 41°42' N λ = 20°45' E Gr. ΔG = + 1h 23 min.																													
I	-	-02.3	02.4	-01.1	00.5	03.6	-00.6	10.5	29 -13.6	19	..	..	10	02.6	..	..	05	01.4	..	..	17	02.7	..	..	..	..	61		
II	-	0.0	0.6	-02.9	04.0	07.9	-00.2	16.5	24 -05.6	05	04	..	07	03.0	01	01.0	13	01.4	..	..	22	02.9	02	03.0	..	..	39		
III	-	0.3	9	10.6	05.7	06.3	11.9	-00.1	20.5	24 -14.5	01	..	..	01	04.0	02	01.0	08	01.4	..	..	09	02.6	..	..	..	..	73	
IV	-	0.7	1	12.1	07.7	08.7	13.3	01.7	20.8	24 -05.0	17	..	..	04	02.8	03	01.7	12	01.5	..	..	19	02.4	..	..	..	..	52	
V	-	11.0	15.9	11.1	12.3	17.3	05.3	26.0	20	02.5	30.10	..	..	..	01	01.0	03	01.3	03	01.0	..	..	16	01.8	..	..	..	..	70
VI	-	15.5	16.0	10.8	12.2	18.5	07.4	24.5	21	01.5	04	..	..	04	02.2	02	01.0	07	01.6	..	..	16	01.9	..	..	..	..	61	
VII	-	14.1	20.8	14.2	15.8	22.8	10.1	29.0	31	04.5	02	..	..	07	02.6	05	01.0	01	02.0	..	..	24	02.3	..	..	..	..	56	
VIII	-	15.3	21.1	15.7	16.9	22.8	04.9	25.0	30	03.0	24	..	..	04	02.5	01	01.0	04	01.5	..	..	14	03.8	..	..	..	..	60	
IX	-	09.3	14.1	09.4	10.5	15.6	05.5	22.0	01	-02.0	29.28	..	..	14	01.4	01	02.0	13	01.2	..	..	20	01.7	..	..	..	..	37	
X	-	06.1	11.3	06.2	07.5	13.0	02.4	17.2	01	-02.0	18	..	..	10	01.7	02	01.0	15	01.2	..	..	09	01.4	..	..	..	..	57	
XI	-	0.5	0.7	04.2	04.7	09.7	-00.1	19.0	04	-08.0	26	..	..	10	01.7	..	..	05	01.7	..	..	34	02.7	01	03.0	03	03.0	33	
XII	-	-03.1	-01.6	-03.0	-02.4	01.7	-06.4	08.5	02	-17.5	14	..	..	10	01.6	..	..	15	01.3	..	..	17	02.7	..	..	..	..	50	
GOD.	-	06.6	11.4	07.0	08.0	13.2	02.6	29.0	34W	-17.5	44.XX	..	..	82	02.1	20	01.2	107	01.4	..	..	217	02.4	03	03.0	10	02.3	656	
Υ = 41°07' N λ = 20°48' E Gr. ΔG = + 1h 23 min.																													
CMBRC																													
I	696.5	0.0	9	05.8	02.2	02.8	06.6	-00.6	13.7	29 -06.7	19	35	C1.9	05	01.0	04	02.0	01	04.0	17	02.6	15	02.1	01	01.0	10	01.3	05	
		695.0	0.4	2	0.9	05.8	06.5	11.1	02.8	20.4	23 -04.2	18	18	01.8	01	01.0	03	01.3	01	01.0	23	02.0	19	02.3	06	02.5	08	01.5	05
III	696.0	0.3	9	12.4	08.0	08.1	14.0	02.7	22.8	24 -06.8	03	23	B1.8	04	02.2	02	03.0	04	03.8	16	02.1	14	01.8	05	01.8	14	01.6	0.6	
IV	693.7	0.6	14.4	09.5	10.0	15.9	04.2	23.4	30	-01.8	18	20	02.0	03	02.0	03	02.0	02	01.5	27	02.0	15	02.3	08	02.5	07	01.6	05	
V	696.5	13.3	19.8	14.5	15.7	21.6	05.6	26.3	18	03.6	12	16	01.5	02	01.0	02	01.0	02	01.0	27	01.9	18	01.8	10	01.9	04	01.5	14	
VI	695.5	15.5	23.2	17.2	18.3	24.5	11.0	26.9	14	06.0	04	16	01.9	02	01.0	02	01.0	02	02.0	30	01.9	20	02.0	06	02.2	08	01.8	06	
VII	695.5	16.6	27.0	21.0	22.0	28.9	13.5	35.0	31	10.0	02	21	01.5	03	01.0	04	02.0	06	01.5	29	01.9	15	01.9	04	03.0	05	01.2	06	
VIII	696.0	16.8	26.2	19.8	20.7	27.7	14.3	32.5	30	08.2	26	20	01.8	03	01.0	04	02.0	06	01.3	30	01.3	15	02.3	08	02.2	06	01.3	11	
IX	698.3	12.4	15.8	14.0	15.1	21.1	10.3	24.6	02	01.0	30	37	02.0	07	02.1	03	02.7	01	02.0	14	01.9	05	02.2	08	01.6	04	01.5	04	
X	700.3	0.7	13.3	16.7	10.3	11.1	17.7	05.9	20.8	11	01.4	04	40	02.0	04	01.2	02	03.3	02.3	01.6	16	01.2	06	02.2	08	01.1	02.1	0.5	
XI	695.0	0.7	12.1	08.4	09.0	13.6	05.3	19.2	11	-00.3	20	23	01.9	03	01.7	01	01.0	04	01.7	15	02.7	19	02.5	12	02.6	10	01.5	07	
XII	697.0	0.2	0.5	04.1	01.9	06.3	-01.3	13.6	01.3	-07.1	05	37	02.4	11	03.0	04	03.0	03	01.7	06	01.8	11	01.8	06	02.2	09	01.9	06	
GOD.	-	07.9	15.9	11.0	11.4	17.6	04.8	35.0	09.W	-11.1	40.1	133	02.6	35	02.6	..	..	16	03.7	93	03.3	51	04.4	..	..	51	03.6	721	
Υ = 41°31' N λ = 20°58' E Gr. ΔG = + 1h 24 min.																													
KICFVC																													
I	-	-01.6	03.0	00.5	00.6	04.0	-02.8	13.0	29 -05.6	10	25	02.3	14	02.4	10	01.7	01	01.0	15	02.1	07	03.0	07	02.1	07	01.7			

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha			Padavine R mm	Broj dana na sat																												
	7	14	21	Sred. (Dnes)	Insolacija broj sati	U m s		Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	A	▲	□	T	≡	■									
	e <sub>m</sub>	mm	mm	7	14	21	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.										
	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm											
<b>BR. ŠT. 256 LAZARCPLE</b>																																				
I	6.5	7.3	5.6	6.5	112.9	32.2	86	61	78	73	29	679	016.0	30	01	05	24	.	.	02	.	03	12	16	10	05	08	12	04	.	.	.	03	21		
II	6.9	7.6	6.0	6.8	104.7	04.0	82	63	79	74	22	144	05.5	13	.	.	16	.	.	06	.	05	10	13	13	03	10	05	03	.	.	01	02	13		
III	4.3	4.8	3.5	4.3	221.5	04.3	79	51	71	66	26	208	013.1	14	03	03	15	.	.	05	10	16	15	13	04	01	05	05	.	.	01	04				
IV	4.6	6.4	4.6	5.2	213.9	05.0	76	58	76	70	32	041	016.4	03	.	.	14	.	.	07	.	05	10	08	01	05	06	.	.	.	.	02				
V	4.9	6.5	3.4	4.9	230.0	08.2	92	63	84	75	35	050	019.5	06	.	.	01	.	.	01	.	04	04	10	07	02	10	.	.	.	02	03				
VI	2.3	3.3	2.3	3.3	253.1	07.6	79	52	72	67	24	044	014.5	04	.	.	01	.	.	01	10	02	09	07	01	10	01	.	.	01	02	02				
VII	2.1	3.6	1.5	2.4	324.7	08.5	72	42	63	59	21	001	001.3	07	.	.	08	.	.	03	.	15	01	01	01	01	01	.	.	.	06	.				
VIII	2.6	4.3	2.4	3.1	297.5	08.7	80	45	73	66	17	043	020.1	31	.	.	08	02	.	05	.	11	10	05	01	10	.	.	.	.	06	.				
GOD.	4.5	5.7	3.8	4.7	-	36.0	82	56	77	72	17	857	055.5	13..	08	13	111	16	02	.	40	06	95	75	129	96	28	99	50	08	.	.	02	15	15	75
<b>BR. ST. 257 MAVCVI ANCVI</b>																																				
I	8.0	6.0	8.9	7.6	-	03.9	E5	22	88	85	37	053	008.2	30	03	03	27	.	.	01	.	.	14	12	12	04	05	.	.	.	.	31				
II	6.5	6.1	7.5	6.7	-	05.0	B2	74	82	79	47	083	022.5	15	.	.	14	.	.	01	.	.	10	10	02	06	06	.	.	.	02	17				
III	4.5	4.5	7.2	5.6	-	05.0	B6	57	72	68	20	025	009.4	01	02	01	11	.	.	05	06	05	03	03	.	.	04	.	.	02						
IV	4.6	4.6	7.0	5.5	-	05.5	T2	57	65	66	28	021	004.6	16	.	.	07	.	.	07	07	07	06	02	.	.	.	.	.	02						
V	4.5	4.6	6.3	5.1	-	05.6	59	51	60	57	24	042	010.2	29	.	.	04	.	.	02	06	05	09	01	05	01	.	.	.	02	.					
VI	3.9	4.9	6.9	5.2	239.9	06.1	59	48	64	57	33	010	003.5	26	.	.	12	.	.	01	07	01	04	04	04	01	01	.	01	03	01					
VII	2.2	3.8	5.1	3.7	310.0	04.6	51	37	39	49	26	018	009.0	01	.	.	12	.	.	01	07	02	05	04	04	04	.	.	01	01	.					
VIII	3.1	4.2	5.9	4.4	-	06.9	55	34	54	48	20	014	004.6	15	.	.	08	.	.	02	02	02	05	01	05	01	.	.	03	02	.					
IX	4.5	5.1	6.8	5.6	-	07.4	E6	59	79	75	30	019	010.0	03	.	.	05	.	.	01	06	02	02	01	02	01	.	.	07	.	.					
X	3.3	4.5	6.2	4.7	-	05.5	71	59	81	71	21	047	014.0	12	.	.	05	.	.	03	05	05	04	04	04	05	.	.	01	.	01					
XI	6.0	6.5	6.8	7.0	-	04.9	80	69	79	76	23	136	028.4	17	.	02	13	.	.	01	13	14	14	15	11	06	.	.	01	03	08					
XII	6.4	5.7	7.5	6.5	-	03.2	B0	81	82	81	47	084	020.0	08	15	23	29	.	.	01	04	11	17	14	02	06	14	.	.	06	31					
GOD.	4.8	5.1	7.0	5.6	-	05.5	T1	51	76	70	67	20	552	028.4	17..	20	29	111	24	.	06	18	86	95	89	15	65	41	01	.	.	07	26	94		
<b>BR. ST. 258 CHRIC</b>																																				
I	7.5	7.5	6.6	7.3	100.4	04.7	P6	72	84	80	49	038	010.7	13	.	.	16	.	.	04	01	02	16	10	06	01	09	05	02	.	.	01	03			
II	6.6	7.1	5.0	6.2	117.0	05.6	86	65	78	76	35	082	029.4	13	.	.	06	.	.	04	01	05	10	14	11	03	14	02	02	.	.	01	.			
III	4.3	4.8	2.8	4.0	200.4	05.3	78	51	67	65	27	031	016.8	14	.	.	06	.	.	06	11	07	05	03	02	05	01	01	.	.	01					
IV	4.4	5.7	4.0	4.7	234.8	06.1	71	52	68	65	31	032	016.9	16	.	.	04	.	.	02	09	06	08	05	01	08	02	02	.	.	.					
V	4.5	5.9	3.5	4.6	268.6	09.1	79	54	71	66	35	057	014.4	16	.	.	05	.	.	01	06	04	11	07	03	11	.	.	.	03	.					
VI	2.7	4.7	3.0	3.4	259.3	10.0	75	46	68	64	28	023	009.3	04	.	.	18	.	.	03	02	05	05	05	05	05	.	.	02	.						
VII	1.8	3.5	2.3	2.5	336.6	11.5	71	44	61	59	27	004	002.6	23	.	.	29	09	.	03	14	05	01	05	01	05	05	.	.	05	.					
VIII	2.3	2.9	1.6	2.2	309.6	10.9	76	43	66	62	31	034	017.1	07	.	.	26	08	01	03	19	06	04	01	08	.	.	06	.	.						
IX	4.6	5.3	3.5	4.5	196.7	09.3	82	57	78	74	33	105	025.6	03	.	.	06	.	.	05	08	07	12	11	05	12	.	.	.	05	.					
X	3.1	3.2	1.5	2.6	214.9	07.3	85	56	76	73	37	021	017.0	10	.	.	01	.	.	03	19	07	12	11	05	12	.	.	.	03	.					
XI	7.4	6.8	5.9	6.7	107.1	07.1	88	72	82	81	48	122	020.8	24	.	.	01	.	.	09	01	02	13	18	13	07	18	02	.	.	02	.				
XII	5.3	5.0	3.7	4.7	111.2	04.3	84	67	79	77	47	030	000.7	03	.	.	21	.	.	12	10	06	11	08	10	02	01	.	.	01	.					
GOD.	4.5	5.2	3.6	4.4	2456.7	07.6	80	56	72	70	27	583	024.4	13..	08	14	54	88	17	01	52	02	114	72	110	82	23	108	14	08	.	.	27	01	04	
<b>BR. ST. 259 GOSTIVAR</b>																																				
I	8.2	6.7	6.7	7.2	-	03.6	E0	82	77	75	15	023	005.7	09	08	06	27	.	.	02	04	15	08	08	03	07	02	.	.	08	.	27				
II	6.6	6.2	5.3	6.0	-	06.2	B3	76	73	79	20	034	040.0	02	.	.	11	.	.	06	04	10	08	08	03	06	.	.	02	.	.					
III	5.5	4.7	4.1	4.7	-	06.3	B3	62	73	73	28	037	002.5	31	.	.	16	02	.	03	01	08	08	04	04	03	01	01	.	.	01	.	01			
IV	4.5	5.5	3.7	4.6	-	06.1	E1	71	68	71	26	032	020.5	03	.	.	04	.	.	04	01	07	05	03	05	03	01	05	.	.	02					
V	4.6	5.9	5.1	5.2	-	10.5	T6	75	77	86	42	C58</td																								

Mesec	Vazdušni pritisak Fm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vетра nD, Fm (O-12)																		
		Tm				Sred. (Dies)				N		NE		E		SE		S		SW		W		NW		C		
		7	14	21		Max.	Min.	Max.		Dat.	Min.	Dat.		E.	J.	E.												
γ = 41°05' N λ = 21°01' E Gr. ΔG = + 1h 24 min.																												
I	-01.6	04.4	00.4	00.9	05.0	-04.4	12.7	29	-11.2	20	14	01.2	08	01.6	07	02.1	01	01.0	09	01.0	14	02.4	06	01.0	02	C1.0	32	
II	-02.3	05.5	04.7	05.3	10.8	00.5	20.0	24	-06.2	27	08	01.9	14	01.4	05	02.4	03	01.7	18	01.8	11	01.9	09	01.8	02	02.5	14	
III	-01.5	12.4	05.6	06.3	13.4	-00.6	22.8	24	-08.2	02	12	01.7	10	02.0	06	01.0	02	02.0	12	02.2	05	01.9	06	01.5	05	C2.0	1	
IV	-00.5	13.9	07.9	08.8	15.4	01.7	22.2	30	-06.0	17	14	01.2	10	02.3	12	01.7	04	01.8	08	01.5	07	02.9	06	01.7	05	C1.0	24	
V	-12.4	20.0	13.2	14.7	21.6	07.1	26.3	22	03.2	02	14	01.3	02	01.0	05	01.6	06	01.7	12	01.8	05	01.4	08	01.4	03	01.7	32	
VI	-12.8	22.4	14.5	16.6	23.0	07.6	28.8	22	03.2	07	11	02.1	07	01.3	08	01.5	06	01.0	06	01.0	05	02.0	08	01.9	08	01.6	36	
VII	-17.6	24.5	16.7	20.4	26.5	05.7	33.7	31	06.8	14	12	01.2	05	01.2	06	01.0	03	01.7	04	01.2	03	02.0	14	01.8	02	01.5	44	
VIII	-15.9	25.0	16.4	18.6	27.2	10.3	32.4	30	06.0	27	08	01.1	08	01.4	01	02.0	07	01.7	09	02.9	06	02.7	06	02.0	42			
IX	-10.5	18.4	11.5	13.0	19.3	06.1	24.0	09	-00.3	30	06	01.2	10	02.2	11	01.3	05	01.8	01	03.0	07	01.7	06	01.7	05	01.2	39	
X	-03.5	16.7	06.5	08.3	17.5	01.0	21.2	08	-05.2	20	06	01.0	04	01.5	06	01.3	03	02.0	07	01.1	08	01.6	02	01.5	57			
XI	-05.0	11.5	06.8	07.6	13.5	02.4	20.2	05	-02.1	22	05	01.2	02	01.5	04	02.2	02	02.0	08	02.0	17	02.5	09	01.4	08	01.3	56	
XII	-00.7	03.9	00.5	01.0	05.4	-03.6	12.7	02	-11.2	24	04	01.0	13	02.2	19	02.6	02	01.5	12	01.7	12	01.8	03	01.3	01	02.0	27	
GOD.	-	07.2	15.4	08.9	10.1	16.8	03.4	33.7	34.VII	-11.5	24.VII	114	01.3	93	01.8	90	01.8	39	01.8	104	01.6	107	02.2	81	01.7	47	01.6	420
γ = 41°31' N λ = 21°13' E Gr. ΔG = + 1h 25 min.																												
MAKEDONSKI BROD																												
BR. ST. 261																												
I	-01.7	0.1	00.2	01.2	04.5	-03.0	14.2	30	-10.0	21	03	03.3	*	*	*	*	03	04.0	11	03.3	01	02.0	*	*	*	*	*	75
II	-02.2	12.3	06.4	08.8	13.3	00.8	22.8	23	-06.5	05	01	02.0	01	02.0	*	*	02	02.0	05	03.2	*	*	*	*	*	02	02.0	73
III	-02.2	15.6	07.8	08.4	16.4	00.5	26.2	24	-05.0	09.01	03	02.0	01	06.0	*	*	02	05.0	03	02.0	01	04.0	*	*	*	*	*	
IV	-05.2	17.2	09.0	10.1	17.8	02.7	25.8	30	-04.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	*	
V	-11.3	22.4	14.1	15.5	23.2	06.7	25.6	21	03.6	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-13.8	25.2	16.4	18.0	25.8	06.3	31.4	23	05.0	07	04	02.0	*	*	*	*	11	02.5	09	02.4	*	*	*	*	*	66		
VII	-17.3	29.0	20.2	21.9	30.6	12.3	36.3	31	05.0	12	02	02.0	*	*	*	*	03	02.7	07	02.5	07	02.9	03	02.7	*	71		
VIII	-14.3	28.6	18.6	20.1	29.6	11.7	35.8	30	06.0	26	01	02.0	*	*	*	*	07	02.3	15	02.7	11	04.0	0	04.0	*	69		
IX	-10.6	22.4	12.6	14.5	23.2	06.5	25.2	09	-02.0	30	01	04.0	*	*	*	*	02	03.0	06	03.0	03	05.3	01	02.0	*	77		
X	-03.9	19.2	07.5	09.5	19.6	02.4	22.6	28	-07.0	02.6	01	*	*	*	*	05	02.0	04	02.0	01	04.0	*	*	*	83			
XI	-04.6	13.9	07.0	08.2	14.4	02.8	22.6	13	-01.2	12	05	02.8	*	*	*	*	02	02.0	05	02.0	*	*	*	*	*	77		
XII	-03.2	04.5	-01.4	-00.4	05.3	-04.5	16.2	30	-11.0	22	05	02.4	*	*	*	*	04	02.0	04	03.5	*	*	*	*	*	80		
GOD.	-	06.7	18.1	09.5	11.2	18.5	04.5	36.3	34.VII	-11.8	22.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
KRUŠEVAC																												
BR. ST. 263																												
I	-01.3	02.1	-00.5	-00.1	03.2	-02.5	08.8	26	-11.2	19	01	07.0	19	01.7	67	01.6	16	02.2	02	02.0	20	03.6	06	02.8	08	03.4	14	
II	-03.1	07.0	03.8	04.4	08.1	01.3	16.5	24	-09.2	28	02	03.0	13	02.3	09	01.9	11	02.2	02	04.0	17	03.3	20	03.4	06	02.8	20	
III	-03.9	05.4	05.6	06.1	10.4	01.5	15.8	24.3	-11.5	01	02.5	20	02.0	31	01.9	03	05.4	01	02.0	11	03.0	10	02.9	04	03.5	07		
IV	-06.0	11.0	06.6	07.6	12.3	02.8	19.5	30	-04.6	12	04	02.5	20	02.0	21	01.8	12	02.1	02	03.5	05	04.2	13	04.0	10	04.3	03	
V	-12.5	14.6	12.2	13.4	17.5	06.0	24.0	21	03.7	11	05	04.4	17	01.5	22	01.5	12	01.9	03	02.7	11	02.5	08	03.0	05	02.8	10	
VI	-15.4	15.0	14.5	15.8	20.4	11.2	26.8	14	03.8	04	03	02.0	30	02.0	28	01.8	06	02.3	02	03.0	11	02.0	12	03.2	08	03.5	03	
VII	-17.9	23.9	19.1	19.5	25.0	12.4	30.6	31	10.0	02	03	03.3	26	02.1	12	02.2	04	02.4	04	01.0	30	03.9	09	03.3	14	03.8	06	
VIII	-16.9	22.4	16.5	18.1	23.7	13.1	29.7	29	04.0	26	02	03.0	23	01.0	12	01.8	11	02.5	02	02.0	15	04.9	04	02.0	07	03.3	17	
IX	-10.9	15.4	11.4	12.4	17.1	06.6	23.0	21	01.6	30	08	03.6	34	02.0	14	01.6	7	02.9	02	02.0	06	03.0	04	04.0	03	03.3	12	
X	-07.6	13.6	08.0	09.7	14.3	05.6	17.7	17	01.0	03	28	01.9	11	01.1	07	02.3	03	02.3	03	04.0	01	05.0	02	05.5	06	05.5	36	
XI	-05.4	08.6	04.6	06.8	10.1	03.8	19.5	05	-04.7	21	03	01.7	13	01.5	07	01.7	12	02.2	03	04.3	22	03.5	11	04.4	07	02.7	22	
XII	-02.0	00.9	-01.6	-01.1	02.4	-03.4	08.8	01	-11.5	06.05	03	02.4	12	03.3	13	01.7	04	02.2	03	02.0	07	03.9	07	04.4	04	02.2	08	
GOD.	-	08.0	12.6	08.5	09.4	13.7	05.4	30.6	34.VII	-11.5	06.05	39	03.2	256	02.0	165	01.7	112	02.3	29	03.0	139	03.7	105	03.5	76	03.5	134
BITOLA																												
BR. ST. 264																												
I	712.0	-00.7	04.7	01.7	05.6	-01.8	13.6	30	-08.0	20.07	22	02.0	10	01.4	C2	01.0	C5	02.8	16	03.2	*	04	02.2	07	01.4	24		
II	709.3	03.2	12.0	07.3	13.5	02.0	22.6	23	-04.2	28	05	02.3	03	02.7	C2	01.5	C3	12	02.8	09	03.1	10	03.3	05	03.6			

Mesec	Oblačnost Nm (0-10)	Inzolacija broj sati	Vlažnost vazduha e <sub>m</sub> mm 7 14 21 Sred. (Dists) Min	Padavine R mm 7 14 21 Sred. (Dists) Min	Broj dana na sat																	
					Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○				
					10.00	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	10.0	•	□				
<b>RESEN</b>																						
<b>BR. ŠT. 261</b>																						
I	7.5 6.4 6.5 6.8	-	04.2 66 72 88 83 26	041 018.3	13	03	.	26	.	.	01	01	04	15	10	05	01	06	05			
II	7.5 6.7 5.5 6.3	-	05.0 69 73 79 75 27	074 020.5	15	.	.	11	.	.	01	02	10	11	08	03	11	.				
III	4.2 4.5 2.7 3.8	-	04.4 62 45 65 64 17	035 022.0	14	.	.	01	17	.	.	04	13	07	04	04	01	03	01			
IV	4.0 5.2 2.5 3.9	-	05.2 78 44 65 62 20	025 012.0	03	.	.	10	.	.	03	01	12	05	07	06	01	05	02			
V	4.6 6.5 3.3 4.6	-	07.5 73 44 72 63 19	048 018.2	06	.	.	10	.	.	01	.	07	04	08	07	02	05	.			
VI	2.9 4.6 2.1 3.2	-	08.4 69 73 71 60 24	028 014.1	04	.	.	13	.	.	01	.	10	03	06	05	01	06	.			
VII	1.4 5.2 1.3 1.9	-	10.4 67 42 65 56 20	001 000.8	01	.	.	27	11	.	01	.	15	*	01	.	02	.				
VIII	2.1 2.8 2.2 2.4	-	09.6 73 35 61 21 21	029 010.5	09	.	.	26	08	.	01	01	21	02	07	05	01	07	.			
IX	5.6 6.6 3.3 4.4	-	08.2 85 81 73 27	114 030.1	01	.	.	01	01	.	.	.	10	05	12	08	01	12	.			
X	3.2 2.4 1.8 2.5	-	05.8 89 43 63 72 20	012 005.1	11	.	.	14	.	.	03	01	17	03	04	04	04	01	.			
XI	6.7 6.4 5.3 6.1	-	05.9 84 64 80 76 32	103 020.0	29	.	.	08	.	.	03	01	05	13	13	12	04	11	02			
XII	5.6 6.4 4.8 5.0	-	03.9 77 70 79 75 28	032 006.8	03	03	02	25	.	.	01	.	10	09	07	05	04	05	01			
GOD.	4.5 4.8 3.4 4.3	-	06.6 79 51 74 68 17	542 030.1	04.IX	06	03	112	77	19	.	16	06	130	76	90	74	15	78	19		
<b>MAKEDONSKI BROD</b>																						
<b>BR. ST. 262</b>																						
I	8.5 7.5 7.5 7.8	-	04.3 91 62 92 82 36	031 006.6	30	01	.	19	.	.	02	.	01	18	10	08	09	02	04			
II	7.5 6.1 5.9 6.5	-	05.6 54 52 86 77 20	052 024.6	13	.	.	11	.	.	02	.	11	07	07	01	07	.				
III	5.1 5.4 4.4 5.0	-	35.7 94 40 81 72 22	022 011.4	14	.	.	13	02	.	03	.	06	05	06	05	01	05				
IV	5.0 5.0 3.4 4.5	-	06.4 93 43 75 70 24	034 011.6	03	.	.	08	01	.	09	07	07	06	01	07	03	02				
V	5.4 5.5 4.2 5.1	-	09.4 91 48 77 72 29	034 006.8	07	.	.	13	.	.	01	02	07	05	08	07	03	01				
VI	3.8 5.4 4.0 4.4	-	10.6 85 48 75 65 32	065 016.6	04	.	.	20	06	.	01	02	07	05	08	07	03	02				
VII	3.5 3.4 2.8 3.2	-	11.4 78 36 65 60 27	006 005.6	02	.	.	31	15	.	03	01	13	02	03	01	03	.				
VIII	3.4 3.4 2.2 3.3	-	10.9 84 32 71 64 24	020 014.2	07	.	.	28	15	.	02	.	13	01	04	04	01	03				
GOD.	6.1 5.3 4.3 5.2	-	07.6 90 48 81 73 20	508 024.8	27.IX	06	.	95	112	40	.	15	02	67	58	98	86	14	93			
<b>KRUŠEVAC</b>																						
<b>BR. ST. 263</b>																						
I	7.5 7.5 7.5 7.8	-	03.7 81 73 82 78 42	039 008.9	13	01	06	23	.	.	04	.	04	12	11	08	05	06	07			
II	6.4 7.0 3.9 5.7	-	04.4 74 66 70 70 31	070 036.7	12	.	.	07	.	.	07	.	05	04	11	05	03	07	06			
III	5.1 5.5 3.0 4.7	-	04.6 68 58 64 63 31	036 026.6	14	01	02	10	.	.	05	.	09	07	07	02	01	05	01			
IV	5.1 6.2 3.3 4.9	-	05.0 68 54 64 62 24	038 016.1	03	.	.	05	.	.	07	.	07	06	08	04	02	05	01			
V	5.1 6.6 4.2 5.3	-	09.2 78 72 80 76 36	056 020.4	29	.	.	01	.	.	03	.	02	07	13	12	*	04				
VI	3.4 5.6 3.0 4.0	-	08.8 67 59 69 65 25	060 021.6	12	.	.	13	.	.	04	.	06	05	05	05	01	05	02			
VII	2.7 3.3 2.1 3.1	-	09.5 65 48 56 51 31	010 005.9	23	.	.	18	01	01	05	01	12	*	04	02	04	03				
VIII	2.4 4.9 1.7 3.0	-	09.8 68 52 67 62 31	059 016.7	05	.	.	11	.	.	03	02	13	02	09	05	03	09	01			
IX	5.4 6.1 3.2 4.9	-	08.0 75 63 74 72 42	100 023.8	01	.	.	02	.	.	01	.	06	06	12	11	03	12	.			
X	3.8 3.2 1.4 2.8	-	06.5 77 63 71 71 43	016 005.4	13	.	.	08	.	.	02	.	16	03	04	03	04	02	.			
XI	7.8 7.7 6.1 7.2	-	06.0 84 77 80 80 20	093 020.9	24	.	.	07	.	.	03	02	14	16	12	02	05	07	.			
XII	5.8 6.8 5.3 5.6	-	03.4 78 74 77 76 36	042 011.5	11	03	08	24	.	.	03	01	09	13	14	11	01	06	10			
GOD.	5.1 5.6 3.4 4.8	-	06.6 73 63 71 69 20	619 030.7	45.II	05	16	82	33	01	01	45	06	93	77	115	81	19	65			
<b>BITOLA</b>																						
<b>BR. ST. 264</b>																						
I	6.7 6.5 5.4 6.4	095.3	04.3 89 71 83 81 37	022 006.7	13	.	01	20	.	.	06	02	05	10	10	07	* Cf 03	.				
II	5.6 6.7 4.8 5.7	142.4	05.2 86 53 69 65 18	040 013.2	13	.	.	10	.	.	15	02	03	06	09	06	02	09	.			
III	5.1 5.5 4.3 4.9	204.9	05.2 83 47 65 24	025 016.1	14	.	01	12	.	.	11	01	08	07	05	02	01	04	02			
IV	4.5 5.7 4.0 4.7	252.8	05.7 75 43 56 24	024 013.4	03	.	07	.	.	14	06	06	05	09	04	01	05	.				
V	5.1 6.6 4.2 5.3	268.7	08.5 74 43 60 23	048 009.4	08	.	.	12	01	.	11	.	05	03	12	05	*	07				
VI	3.5 5.7 3.3 4.1	308.7	09.1 70 35 55 21	026 011.6	04	.	.	21	09	.	16	.	05	03	06	05	01	06				
VII	2.4 4.4 2.4 2.9	355.9	10.4 67 35 50 18	012 009.0	02	.	.	24	15	.	16	.	15	*	04	03	04	05				
VIII	2.5 3.9 2.5 2.9	324.7	10.2 74 37 57 52	022 006.7	09	.	.	27	13	02	15	01	05	01	14	01	06	07				
IX	5.5 5.4 4.3 5.1	-	08.8 82 48 67 66 26	054 017.5	03	.	.	01	15	.	05	.	04	06	16	12	16	01				
X	3.4 7.1 1.9 2.7	223.2	06.3 61 47 65 23	003 003.5	12	.	.	08	.	.	06	.	04	07	09	06	02	05				
XI	7.3 7.0 6.2 6.9	115.8	06.5 87 63 77 76 24	052 016.5	27	.	.	22	14	.	07	01	10	04	10	07	10	02				
XII	6.1 5.9 4.8 5.6	-	03.9 85 66 55 79 39	024 006.0	04	.	01	25	.	.	06	01	09	11	12	06	06	05				
GOD.	4.8 5.5 4.0 4.8	-	07.0 80 48 66 65 18	365 017.5	03.IX	.	02	83	104	42	02	132	12	57	73	107	72	07	95			
<b>SKOPJE-PETROVAC</b>																						
<b>BR. ST. 265</b>																						
I	7.5 7.4 4.8 6.7	-	04.5 92 70 86 55	025 012.2	28	01	02	20	.	.	04	.	03	11	09	05	01	08	02			
II	7.0 6.4 5.5 6.3	-	06.1 92 63 76 44	042 014.5	03	.	.	10	.	.	05	.	04	07	09	06	02	09	.			
III	5.6 5.3 5.7 4.9	-	06.1 88 20 74 73	035 012.2	14	.	.	11	02	.	07	.	08	08	04	01	02	01	.			
IV	5.3 6.0 3.7 5.0	-	06.9 79 30 66 54	021 009.9																		

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Mesec	Vazdušni pritisak Fm mm	Temperatura vazduha °C						Čestina pravaca i srednja jačina vетра nD, Fm (0-12)																				
		Tn	7	14	21	Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NN	C								
		8.	14.	21.	8.	14.	21.	8.	14.	8.	14.	8.	14.	8.	14.	8.	14.	8.	14.									
$\gamma = 41^{\circ}59' N \lambda = 21^{\circ}31' E$ Gr. $\Delta G = +1h 26 min.$																												
I	-01.0	05.3	00.9	01.5	06.4	-02.7	15.0	31	-09.0	20	01	01.0	07	01.0	.	.	13	01.0	02	01.0	15	01.0	.	.	10	01.2	45	
II	-03.0	12.7	06.4	07.1	14.0	01.2	22.0	23	-04.0	05	.	04	01.0	15	01.0	04	01.0	25	01.0	.	.	07	01.0	29				
III	-04.0	16.2	08.7	09.4	17.4	02.1	27.3	24	-05.5	03	.	03	01.1	01	01.0	25	01.0	.	17	01.1	.	.	10	01.3	29			
IV	-06.6	18.5	10.7	11.5	19.5	03.7	25.0	30	-02.2	14	.	09	01.0	.	.	22	01.1	01	01.0	25	01.1	.	.	04	01.2	29		
V	-13.8	23.5	16.0	18.0	25.4	10.4	30.5	04	04.3	12	01	01.0	09	01.0	02	01.0	25	01.0	.	.	17	01.0	32					
VI	-16.3	27.3	15.0	20.4	26.3	12.0	30.0	15	06.0	06	02	01.0	06	01.0	.	.	23	01.0	01	01.0	17	01.0	.	.	05	01.0	36	
VII	-19.7	30.9	22.2	23.7	32.3	15.2	38.0	09	11.4	14	.	17	01.0	.	.	15	01.0	.	.	12	01.2	.	.	12	02.0	37		
VIII	-17.0	30.0	21.1	22.3	31.1	13.8	35.4	22	07.0	26	.	.	23	01.0	.	.	12	01.1	01	01.0	10	01.0	.	.	08	01.2	39	
IX	-12.3	23.2	16.1	16.9	24.9	10.0	31.0	02	-03.6	30	01	01.0	15	01.0	.	.	12	01.0	.	.	08	01.0	.	.	19	01.1	35	
X	-04.1	20.3	09.5	11.1	21.0	02.5	25.4	08	-02.3	05	02	01.0	13	01.0	01	01.0	16	01.0	.	.	11	01.0	.	.	07	01.0	43	
XI	-04.9	14.1	07.8	08.5	15.0	02.5	22.4	11	-01.8	28.22	.	17	01.0	.	.	13	01.1	.	.	20	01.1	.	.	13	01.0	27		
XII	-02.4	02.9	-01.3	03.0	03.6	-04.6	10.2	08	-16.4	16	.	15	01.0	.	.	11	01.0	.	.	15	01.0	01	01.0	12	01.0	39		
GOD.	-	08.2	18.8	11.5	12.5	19.9	05.6	35.4	22.VI	-10.4	16.XII	07	01.0	146	01.0	04	01.0	202	01.0	09	01.0	152	01.0	01	01.0	114	01.2	420
$\gamma = 41^{\circ}20' N \lambda = 21^{\circ}34' E$ Gr. $\Delta G = +1h 26 min.$																												
I	704.8	-00.4	04.8	01.5	01.9	06.0	-01.6	14.2	25	-08.0	20	06	03.8	04	03.2	.	.	01	03.0	10	04.5	07	01.9	05	02.0	01	02.0	59
II	702.3	03.9	11.2	06.9	07.2	12.6	02.7	21.7	23	-04.0	28	09	02.7	08	01.9	.	.	20	02.8	17	02.8	04	01.5	01	02.0	25		
III	706.7	03.7	13.4	08.0	08.6	14.8	02.8	24.8	24	-07.0	03	06	03.0	23	02.3	01	04.0	.	11	02.8	08	01.8	03	01.7	.	.	41	
IV	701.2	07.3	15.4	10.0	10.6	17.0	04.6	25.1	30	-01.1	18	11	03.4	24	02.7	02	02.0	02	04.0	10	03.6	09	02.8	04	01.0	03	01.7	25
V	703.8	13.7	21.3	15.5	16.5	22.8	10.2	30.4	21	04.4	12	14	02.1	16	02.5	01	02.0	.	08	03.1	15	02.7	03	01.3	01	02.0	35	
VI	702.4	16.2	24.1	17.6	18.9	25.6	12.2	31.4	14	07.0	06	10	02.2	19	02.4	.	01	02.0	04	02.5	12	02.1	13	01.9	01	02.0	30	
VII	702.3	19.4	28.7	22.0	23.0	30.3	15.7	37.1	31	12.2	25	07	02.7	32	02.3	02	02.5	.	04	02.4	15	03.0	05	04.2	.	.	28	
VIII	703.3	17.3	27.5	21.0	21.6	28.6	14.7	36.6	30	-08.4	24	08	02.6	21	02.3	01	02.0	.	06	04.3	14	03.0	09	02.1	02	02.5	32	
IX	706.0	12.6	20.6	15.0	15.8	21.5	10.7	26.0	30	17	02.7	22	02.5	02	02.0	.	.	04	02.0	06	03.2	02	01.5	03	01.0	32		
X	707.9	06.4	18.2	10.8	11.5	19.1	05.2	23.0	09	-00.4	01	05	02.8	16	02.0	01	02.0	.	05	02.4	11	02.1	03	01.7	01	01.0	32	
XI	702.3	06.5	12.8	08.6	09.1	14.1	05.3	21.9	13	-00.4	21	03	03.2	10	02.2	.	01	02.0	14	03.9	10	02.6	05	02.0	.	.	49	
GOD.	704.1	08.8	16.8	11.4	12.1	18.2	06.6	37.1	34.VII	-08.9	14.XII	107	02.8	213	02.5	10	02.3	05	03.0	59	02.6	59	02.0	14	01.7	455		
$\gamma = 41^{\circ}43' N \lambda = 21^{\circ}46' E$ Gr. $\Delta G = +1h 27 min.$																												
I	-00.2	06.6	02.0	02.7	07.4	-01.4	15.5	31	-16.0	20	.	01	01.0	06	01.3	.	.	07	04.1	.	.	06	02.3	.	.	17	03.0	57
II	-02.0	13.6	06.8	08.1	14.7	02.8	24.2	23	-02.5	08	01	01.0	02	01.0	.	.	12	02.6	.	.	08	03.9	.	.	22	02.3	39	
III	-04.9	16.4	09.6	10.1	17.1	03.5	25.4	24	-05.5	03	.	04	01.0	.	15	02.5	.	.	11	03.0	.	.	22	02.3	37			
IV	-08.7	18.2	12.4	12.9	19.3	05.1	28.2	30	-01.2	14	.	04	02.0	.	03	02.2	01	06.0	03	02.7	.	.	35	02.6	38			
V	-15.8	24.6	19.1	19.1	25.4	11.3	30.5	18	06.0	13.06	.	05	01.6	.	.	16	02.1	.	.	11	01.8	.	.	30	02.6	31		
VI	16.9	27.6	20.9	22.1	28.5	13.7	35.0	09	01.0	07	.	01	01.0	.	09	01.6	.	.	06	01.5	.	.	37	02.2	37			
VII	-21.7	30.8	24.5	25.6	32.1	17.1	36.0	09	13.0	08	.	03	03.1	.	11	02.1	.	.	03	02.7	.	.	45	02.3	31			
VIII	19.6	30.0	23.1	24.0	31.0	12.5	35.0	22	05.5	24	.	04	01.5	.	13	02.3	.	.	09	02.1	.	.	30	02.0	37			
IX	-15.4	24.0	18.0	18.5	25.2	12.9	31.0	06	00.0	30	.	03	01.3	.	05	02.4	.	.	08	02.0	.	.	34	02.6	40			
X	-07.3	20.6	11.9	12.9	21.5	05.5	27.0	02	-00.6	01	.	02	02.0	.	10	01.9	.	.	07	02.1	.	.	17	02.0	57			
XI	-07.3	14.7	09.5	10.2	15.7	05.7	23.0	06	-06.2	29	.	01	01.0	.	04	01.8	.	.	19	02.5	.	.	17	02.1	49			
XII	-00.8	03.9	00.5	01.0	04.0	-03.8	12.0	02.0	-05.8	29	.	01	02.0	.	02	03.0	.	.	06	02.7	.	.	32	03.8	52			
GOD.	-	10.3	19.2	13.2	14.0	20.3	07.4	39.0	22.VM	-10.0	20.I	01	01.0	36	01.4	.	.	113	02.3	01	06.0	97	02.4	.	.	342	02.5	505
$\gamma = 41^{\circ}50' N \lambda = 22^{\circ}02' E$ Gr. $\Delta G = +1h 28 min.$																												
I	-01.0	06.7	02.9	02.9	07.1	-02.3	15.8	31	-10.6	20	09	03.1	.	.	.	.	09	01.8	.	.	.	.	.	.	.	75		
II	-03.0	13.9	06.4	07.4	14.4	01.7	24.4	23	-04.4	05	10	02.7	.	.	.	.	02	02.5	.	.	.	.	.	.	.	72		
III	-03.6	16.0	08.3	09.1	16.5	01.8	25.2	23	-07.2	03	13	02.6	.	.	.	.	15	02.7	.	.	.	.	.	.	.	65		
IV	-07.4	17.6	10.5	11.5	18.3	03.4	27.0	30	-03.6	14	24	03.2	.	.	.	.	05	03.6	.	.	.	.	.	.	.	61		
V	-14.6	24.4	14.6	10.0	25.0	07.3	30.2	18	00.0	30	11	02.3	.	.	.	.	06	02.0	.	.	.	.	.	.	.	76		
VI	-17.5	27.7	19.2	21.1	28.2	13.4	34.0	20	06.0	03	10	02.6	.	.	.	.	05	02.3	.	.	.	.	.	.	.	79		
VII	-20.5	31.2	23.4	24.6	32.1	15.8	37.0	09	13.4	08	25	07	03.3	.	.	.	.	04	04.0	.	.	01	05.0	.	.	.	61	
VIII	-19.2	30.3	22.2	23.5	31.2	14.7	37.4	22	07.6	27	06	02.5	.	.	.	.	07	03.3	.	.	.	.						

Mesec	Oblačnost Nm (0-10)	Sred. (Dnev.)	Insolacije broj sati	Vlažnost vazduha						Padavine R mm		Broj dana n s a:												
				U m t				Tn Tx Tn Tx Tn F(0-12) Nm(0-10) R mm		● * * △ ○ ▲ □ R T					● * * △ ○ ▲ □ R T									
				7	14	21	Sred. (Glob.)	Min	Σ	Max	Dat.	≤	<	≥	IV	IV	IV	IV	IV	IV	IV			
TRIBAREVO																								
BR. ST. 266	I 8.1 6.5 5.3 6.8	-	04.5 87 78 88 64 44	022 011.0	28	.	.	22	.	.	.	.	.	02	11	06	05	01	05	01	.	04	01	
II 7.3 6.1 5.3 6.2	-	06.4 90 70 81 28 054	021.0	03	.	.	10	.	.	.	.	.	01	09	07	07	02	07	.	.	01	01		
III 5.4 5.3 3.4 4.7	-	07.0 88 61 81 77 44	016 010.1	14	.	.	12	02	.	.	.	.	09	06	02	02	01	01	01	.	01	01		
IV 5.6 5.8 4.0 5.1	-	07.4 79 53 77 70 35	021 008.3	03	.	.	05	06	.	.	.	.	02	06	04	04	..	04	.	.	02	01		
V 6.0 5.4 5.6 5.7	-	11.0 79 56 74 76 37	033 011.0	11	.	.	17	06	.	.	.	.	02	07	06	06	02	06	.	.	.	.		
VI 4.4 5.2 5.0 4.9	-	12.5 80 52 76 65 36	030 011.0	28	.	.	22	15	.	.	.	.	02	03	07	07	01	01	01	.	04	.		
VII 2.8 2.9 2.8 2.9	-	14.7 78 50 73 66 37	010 003.5	23	.	.	31	23	.	.	.	.	14	.	04	03	..	04	.	.	03	.		
VIII 3.2 3.8 3.0 3.3	-	14.2 82 52 76 70 30	040 024.0	07	.	.	29	21	.	.	.	.	09	02	04	04	01	04	.	.	02	.		
IX 5.8 5.7 4.9 5.5	-	10.7 84 56 76 73 35	023 006.5	07	.	.	02	17	04	.	.	.	04	08	05	05	05	05	.	.	02	.		
X 4.7 3.4 2.3 3.4	-	08.0 89 57 86 77 38	015 008.1	12	.	.	08	01	.	.	.	.	12	03	02	02	01	02	.	.	08	.		
XI 7.0 6.5 5.3 6.5	-	07.1 90 70 85 82 27	044 012.5	24	.	.	05	..	.	.	.	.	01	11	07	07	01	01	02	.	.	06	01	
XII 8.0 6.4 5.0 6.5	-	03.9 87 75 87 83 46	021 005.0	03	01	04	27	.	.	.	.	.	03	13	06	06	04	04	02	.	.	04	.	
GOD. 5.8 5.3 4.3 5.1	-	09.0 84 61 80 75 27	320 024.0	07.viii	01	04	91	126	71	.	.	.	61	79	60	58	09	06	.	.	15	20	04	
PRILEP																								
BR. ST. 267	I 6.5 6.9 5.0 6.2	089.6 04.7 94 76 98 87 44	016 005.4	17	.	02	19	.	.	.	.	05	.	04	09	11	05	05	07	.	.	05		
II 5.9 6.4 4.0 5.5	125.3 05.5 88 58 74 74 31	043 020.2	15	.	01	06	.	.	.	.	.	03	01	05	04	04	04	04	.	.	.	.		
III 5.4 5.3 3.9 4.7	211.5 05.4 84 67 67 77	025 021.1	14	.	01	08	.	.	.	.	.	04	08	06	06	02	01	05	05	.	.	.		
IV 4.4 5.4 3.2 4.3	251.2 05.5 75 45 42 61 24	025 011.9	03	.	02	01	.	.	.	.	05	02	08	05	07	04	01	01	01	.	02			
V 5.1 6.3 4.6 5.3	250.0 08.6 76 74 66 62 28	047 017.1	29	.	.	11	01	.	01	.	.	02	06	09	08	01	05	.	.	09	.			
VI 2.9 4.9 3.5 3.8	317.4 08.9 69 39 61 56 24	061 015.2	04	.	.	21	06	.	.	.	.	12	03	10	09	02	10	.	.	01	06	01		
VII 2.5 3.6 2.1 2.7	357.7 10.8 69 35 55 53 21	010 005.2	02	.	.	29	18	.	04	02	14	.	03	03	03	03	03	03	.	.	03			
VIII 2.1 3.2 2.7 2.7	329.5 10.3 74 36 58 56 18	030 021.5	07	.	.	26	11	01	06	02	16	02	05	04	01	05	.	.	01	08	.			
GOD. 4.7 5.2 3.8 4.5	2626.9 07.2 81 50 69 67 18	415 029.5	25.IX	.	05	61	102	36	01	31	36	08	107	71	96	63	12	82	19	01	.	02	32	08
TITOV VELES																								
BR. ST. 268	I 6.5 6.2 7.0 8.3	-	04.9 86 74 87 62 48	010 003.6	28	01	01	17	.	.	.	05	01	01	21	08	04	05	07	01	.	04	01	
II 7.9 7.2 6.5 7.9	-	06.3 87 60 77 75 42	036 020.3	15	.	01	09	.	.	.	04	.	13	07	05	02	07	02	.	.	03	.		
III 6.1 5.6 5.6 5.8	-	06.0 82 46 68 66 26	021 015.4	14	.	08	02	.	.	.	04	.	05	08	05	03	01	04	01	.	.	01		
IV 5.2 6.2 5.7 5.7	-	06.3 71 46 60 57 14	022 012.1	03	.	03	04	.	.	07	.	02	09	03	03	03	03	03	03	.	.	.		
V 5.5 5.5 5.1 5.5	-	09.4 70 43 64 59 23	024 008.5	29	.	.	17	05	.	04	.	02	09	07	05	07	01	.	.	01	.			
VI 4.9 6.0 6.3 5.7	-	10.9 68 38 62 56 21	044 018.2	17	.	.	23	16	.	01	.	04	07	11	08	01	11	11	.	.	01			
VII 4.2 4.3 4.9 5.5	-	12.3 65 37 55 52 22	019 007.4	02	.	.	31	24	01	02	.	06	04	05	05	05	05	05	.	.	02			
VIII 2.9 3.6 4.3 3.6	-	11.9 71 39 56 55 18	026 012.0	07	.	.	30	21	05	01	.	14	03	04	03	03	03	02	.	.	02			
IX 6.2 6.1 5.0 5.8	-	09.7 70 46 61 59 23	013 007.6	04	.	.	18	09	.	01	.	07	09	05	03	05	05	05	.	.	01			
X 6.5 7.2 6.4 4.9	-	07.2 81 44 69 65 23	014 011.2	12	.	01	01	.	.	.	.	02	04	02	02	01	02	01	.	.	01			
XI 9.4 6.6 6.5 7.6	-	06.9 82 62 74 73 21	038 015.9	27	.	01	01	.	.	.	.	01	14	08	06	02	08	08	.	.	03			
XII 8.8 7.1 6.7 7.5	-	03.9 65 74 76 73 33	021 008.2	11	.	01	25	.	.	06	.	15	05	05	03	02	02	02	.	.	.			
GOD. 6.4 5.5 5.5 6.1	-	08.0 75 50 67 64 16	287 020.3	45.II	01	02	164	126	75	06	35	01	44	116	70	52	09	66	04	.	.	05	11	02
ERDZELJJA																								
BR. ST. 269	I 6.1 5.1 4.5 5.2	-	04.8 84 79 81 81 53	023 006.4	28	01	01	21	.	.	.	08	08	06	06	06	06	06	06	06	.	04		
II 4.6 5.3 4.1 4.7	-	06.1 85 63 76 74 45	025 013.4	15	.	10	.	.	.	.	.	08	04	05	05	01	02	01	02	.	.	01		
III 2.7 3.2 2.1 2.7	-	05.9 83 50 73 69 16	019 017.0	14	.	11	01	.	.	.	.	20	05	03	02	02	01	02	01	.	.	01		
IV 4.3 4.7 2.4 3.8	-	06.6 77 51 62 64 23	036 015.2	03	.	04	03	.	.	02	.	12	05	05	05	02	02	02	.	.	01			
V 3.9 4.3 3.5 4.0	-	10.3 75 49 73 66 20	032 012.8	25	.	.	16	03	.	.	.	13	07	06	05	01	06	.	.	01	.			
VI 2.0 3.6 3.8 3.8	-	11.3 72 42 69 61 21	047 006.6	03	.	.	23	14	.	02	.	06	15	05	09	04	05	05	05	.	02			
VII 2.4 2.6 1.8 2.3	-	13.3 74 39 61 58 25	029 013.0	23	.	.	31	24	.	02	.	20	04	05	05	02	05	05	05	.	02			
VIII 2.6 2.3 1.3 2.0	-	12.6 72 41 65 59 35	024 015.2	07	.	.	30	21	02	01	.	21	02	03	03	01	02	01	.	.	01			
IX 4.2 3.7 3.2 3.7	-	10.6 81 53 72 69 32	021 007.2	28	.	02	18	05	.	01	.	15	07	06	04	06	06	06	06	.	.			
X 1.1 2.1 2.1 2.2	-	06.5 83 36 62 52 16	028 021.2	12	.	03	05	.	.	.	.	23	05	02	01	01	02	01	02	.	.	01		
XI 7.2 4.2 4.4 5.3	-	04.9 88 65 89 79 37	040 017.0	21	.	03	.	.	.	.	.	05	10	09	07	03	02	02	02	.	.	02		
XII 5.4 4.7 4.3 4.8	-	04.9 81 84 84 83 88	008 026.8	01	05	04	25	.	.	.	.	12	12	04	02	04	01	01	01	.	.	01		
GOD. 4.0 3.8 3.2 3.7	-	08.3 79 54 72 68 16	337 021.2	42.x	04	05	79	127	71	02	08	.	172	74	63	54	12	62	04	03	.	07	12	
KAVADARCI																								
BR. ST. 270	I 6.7 6.6 6.6 6.7	-	04.5 84 71 76 77 42	013 003.5	28	01	01	18	.	.	.	06	16	09	05	07	04	01	01	01	01	02		
II 5.7 5.9 6.4 6.6	-	05.9 80 55 68 65 28	014 006.6	15	.	04	.	.	.	.	04	10	08	05	06	02	02	02	02	02	02			
III 3.8 5.0 4.7 4.5																								

Mjesec	Vrstdunski Prstn. Fm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, Fm (0-12)																				
		Tm	7	14	21	Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.									
$\gamma = 41^{\circ}45' N \lambda = 22^{\circ}11' E$ Gr. $\Delta G = + 1h 29$ min.																														
I	733.5	-0.0	3	05.9	02.6	02.7	06.9	-0.1	1.3	16.4	30	-0.1	5	20	01	04.0	03	02.0	01	05.9	01	04.0	01	05.0	02	01.5	07	04.7	62	
II	732.0	0.4	0	11.9	08.3	08.1	13.6	03.2	22.1	23	-0.3	8	05	0	01	01.0	01	02.0	11	05.5	12	03.8	01	02.0	02	03.0	14	04.4	42	
III	730.6	0.4	3	14.4	09.5	09.4	15.5	03.6	24.1	23	-0.6	0	03	04	04.2	05	03.2	0	01	21	05.0	06	05.5	03	02.3	03	01.7	16	04.0	35
IV	730.7	0.7	2	16.3	11.7	11.7	18.0	05.4	26.6	30	-0.1	8	14	09	04.3	0	01	02.0	12	05.4	05	03.8	05	02.4	01	02.0	24	04.2	32	
V	732.8	14.4	23.0	17.6	18.2	24.3	12.2	30.1	21	06.8	30	06	02.8	0	01	18	04.1	07	04.4	04	02.2	03	02.3	20	03.0	35				
VI	731.0	17.1	26.2	19.5	20.7	27.2	14.1	33.0	15	09.4	0	01	09	02.1	01	01.0	0	06	03.3	04	03.5	06	02.8	03	03.0	17	03.8	44		
VII	730.8	20.1	25.7	23.4	24.3	30.9	17.5	34.7	10	13.8	13	10	03.6	01	02.0	02	03.0	18	04.7	07	02.6	06	01.8	02	01.0	16	03.7	31		
VIII	731.7	18.4	28.7	22.2	22.9	29.9	16.5	35.5	29	05.9	0	01	03	02.7	05	01.8	0	12	03.8	08	04.1	04	02.0	05	03.0	10	03.0	46		
IX	732.0	13.5	22.7	17.4	17.8	24.1	12.3	36.0	21	-00.4	30	08	03.5	03	02.3	01	01.0	12	03.2	03	06.0	04	03.0	0	01	02.0	12	03.8	46	
X	732.4	16.9	15.1	12.1	12.9	20.5	04.0	25.4	08	01.0	0	01	02	01.5	01	01.0	01	04.1	14	04.1	07	02.0	03	02.0	08	03.0	55			
XI	732.1	0.6	8	13.4	05.5	05.8	14.4	05.6	22.0	06	-01.9	0	29	+	01	02.0	18	05.7	06	03.5	03	02.7	+	01	01.0	15	03.1	47		
XII	732.7	-0.2	0	02.5	-0.0	02.2	03.8	-03.5	14.6	30	-06.4	25	01	02.0	08	02.5	03	01.0	09	02.9	01	02.0	0	01	01.0	21	05.0	49		
GOD.	733.6	0.9	2	17.8	12.9	13.2	19.1	07.6	35.5	29.8	-08.4	25.XI	53	03.2	28	02.2	10	01.8	16.8	04.6	62	03.9	44	02.2	26	02.2	180	03.9	524	
$\gamma = 41^{\circ}25' N \lambda = 22^{\circ}15' E$ Gr. $\Delta G = + 1h 29$ min.																						DEMIR KAPIJA		BR. ST. 272						
I	752.8	0.0	7	06.6	03.3	03.5	07.6	-0.5	19.0	30	-0.1	5	20	+	+	+	16	03.9	08	05.5	04	01.7	07	01.3	14	02.0	07	02.0	35	
II	750.0	0.9	13.2	10.3	03.4	14.4	04.7	20.5	02	-0.6	0	05	27	04.5	02.1	03.4	04	02.2	05	01.4	09	01.8	09	02.0	09	03.0	15			
III	754.6	0.5	1	15.6	10.3	10.3	16.2	04.4	20.1	24	-0.5	0	03	03	02.7	0	25	05.2	12	03.9	03	01.7	04	01.8	11	02.0	14	02.9	21	
IV	748.6	0.8	18.1	12.6	12.9	19.5	04.1	28.2	24	-06.9	0	14	01	02.0	0	21	04.0	06	03.5	01	02.0	05	01.8	06	02.2	22	02.9	20		
V	750.3	15.8	24.2	18.1	19.1	25.4	12.6	30.7	03	07.2	12	01	02.0	0	22	03.6	17	03.2	03	01.3	06	01.5	07	01.3	09	02.2	28			
VI	746.1	18.4	27.8	20.8	21.9	28.8	14.8	34.3	20.5	15.10	07.0	06	04	01.8	01	02.0	06	02.8	12	02.2	06	02.0	01	02.0	06	01.2	15	01.9	39	
VII	747.9	21.4	30.6	24.5	25.2	31.5	18.0	36.1	10	14.4	08	0	20	04.4	0	15	02.9	05	02.9	02.0	01.0	05	02.4	13	02.3	37				
VIII	748.6	19.5	29.7	23.4	23.9	30.6	17.0	35.4	30'	05.6	0	26	02	02.0	01	01.0	17	04.2	08	03.1	02	01.5	04	01.8	10	02.2	44			
IX	752.4	14.7	24.3	18.4	19.0	25.3	13.1	31.1	06.0	02	03.3	30	01	01.0	0	13	03.5	07	03.0	03	01.7	01	01.0	04	02.0	14	02.4	47		
X	755.4	0.6	9	20.0	13.5	20.9	06.0	27.0	02	00.0	0	01	01.0	02.0	01	03.0	13	03.5	11	03.0	07	01.6	04	01.2	05	01.8	47			
XI	756.1	0.7	9	14.7	10.7	11.0	15.7	05.9	22.4	06	-00.4	29.2	01	02.0	0	15	04.1	17	03.2	02	01.0	02	01.5	03	02.3	07	02.0	43		
XII	755.6	-0.8	0	04.3	01.4	05.2	-02.3	13.3	30	-08.6	25.2	01	02.0	0	10	03.5	13	03.2	03	01.7	0	14	02.4	15	02.1	37				
GOD.	751.3	10.3	19.0	13.8	14.3	20.1	08.3	36.1	40.VII	-09.1	20.I	15	02.0	03	02.0	205	04.2	141	03.3	42	01.7	40	01.5	88	01.5	140	02.4	421		
$\gamma = 41^{\circ}55' N \lambda = 22^{\circ}25' E$ Gr. $\Delta G = + 1h 30$ min.																						KOĆANI		BR. ST. 273						
I	-	0.1	0.6	02.6	02.9	07.0	-0.1	1.5	15.6	31	-06.2	20.5	11	02.5	0	01	0	06	02.3	0	01	0	01	0	01	0	01	76		
II	-	0.4	12.8	07.9	08.1	13.8	01.5	23.0	23	-03.6	05	26	02.2	0	01	07	02.3	0	02.0	0	01.8	09	02.0	09	03.0	51				
III	-	0.4	3	15.6	10.4	10.3	14.2	02.6	25.8	24	-06.4	0	03	24.2	02	02.5	0	08	02.6	01	02.0	0	01.5	05	01.8	56				
IV	-	0.7	3	17.7	12.6	12.5	18.4	05.0	26.5	30	-02.0	14	36	02.5	04	02.5	0	08	02.6	0	02.0	0	01.5	04	02.2	42				
V	-	15.1	23.9	18.5	19.0	24.7	12.0	30.0	21	07.0	30	05	02.0	02	02.0	0	08	02.1	0	02.0	24	02.0	0	01	0	01	54			
VI	-	21.4	26.3	19.3	20.7	26.9	13.6	32.0	15	09.5	06.0	05	26	02.6	0	01	14	02.2	01	02.0	0	01.8	09	02.0	09	03.0	49			
VII	-	20.0	30.4	23.6	24.4	31.0	14.9	32.8	29	12.2	13	13	02.3	0	01	14	02.2	0	02.0	0	01.8	09	02.0	09	03.0	63				
VIII	-	17.9	29.0	23.3	29.7	31.7	15.1	35.5	22	05.0	0	26	02.5	04	02.5	0	13	02.5	0	02.0	0	01.8	09	02.0	09	03.0	54			
IX	-	13.4	23.5	17.3	17.9	24.6	11.6	30.5	02	02.0	0	30	12	02.3	02	02.0	0	10	02.2	0	02.0	01	02.0	01	02.0	01	02.0	64		
X	-	17.2	19.9	13.4	13.5	20.8	05.1	25.5	09.8	00.6	0	01	11	02.2	0	01	07	02.1	0	02.0	0	01.8	09	02.0	09	03.0	75			
XI	-	0.6	3	14.4	10.0	10.2	15.3	04.6	22.5	06	-01.0	22	12	02.3	0	01	08	02.6	0	02.0	0	01.8	07	02.0	07	03.0	70			
XII	-	-0.2	9	03.3	00.0	00.1	03.9	-03.9	13.0	30	-05.2	21	14	02.4	0	01	08	02.8	0	02.0	0	01.8	07	02.0	07	03.0	71			
GOD.	-	0.9	2	18.6	13.3	13.6	15.4	06.9	36.8	09.VII	-09.2	24.XI	226	02.3	10	02.3	0	01	106	02.4	02	02.0	25	02.0	01	02.0	01	02.0	725	
$\gamma = 41^{\circ}38' N \lambda = 22^{\circ}27' E$ Gr. $\Delta G = + 1h 30$ min.																						RADOVIS		BR. ST. 274						
I	-	0.0	1	05.1	02																									

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm	Broj dana na sat																	
	7	14	21		L m s				Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	*	*				
					em	mm	7	14	21	Max	Dat.	II	<	<	IV	IV	V	V	V	V	V	V				
STIP																										
BR. ST. 271	$H_s = 326 \text{ m } H_b = 327.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$																									
I 6.6 6.5 5.5 6.2 -	04.5 90 67 80 79 44	017 004.1	17	• 02 19 • • • 09 02 05 10 08 04 • 07 02 • • • • • • • • • • • 06 03																						
II 6.5 7.6 5.5 6.3 122.3	05.7 86 57 71 71 33	019 012.8	15	• • 07 • • • 12 01 05 09 07 04 02 01 03 01 • • • • • • • • • • • 01 01																						
III 5.8 5.5 3.7 5.0 193.5	05.6 83 46 65 65 28	016 014.7	14	• • 07 02 • • 17 03 07 05 04 02 01 03 01 • • • • • • • • • • • 01 01																						
IV 4.9 5.5 3.7 4.7 232.1	06.2 78 45 61 26 16	019 012.4	03	• • 02 03 • • 14 03 07 06 04 03 01 04 • • • • • • • • • • • 01 01																						
V 5.2 5.5 4.2 4.9 233.3	09.2 78 45 61 27	046 022.0	25	• • • 14 01 01 04 01 08 10 10 07 01 10 • • • • • • • • • • • 05 • •																						
VI 4.8 5.4 4.3 4.2 304.7	10.5 75 74 62 59 27	053 013.0	17	• • • 23 16 • • 02 03 10 08 02 10 08 02 10 • • • • • • • • • • • 08 • •																						
VII 2.3 3.5 2.1 2.1 340.0	11.9 73 37 55 54 27	029 011.0	23	• • 30 20 04 10 03 17 01 06 04 02 06 • • • • • • • • • • • 01 06 01																						
VIII 2.5 2.7 1.5 2.0 317.7	11.4 73 39 59 57 21	040 027.7	07	• • • 26 19 04 09 01 18 01 06 05 01 04 • • • • • • • • • • • 04 • •																						
GOD. 4.8 5.2 4.0 4.6 -	07.6 80 45 65 15 18	300 027.7	07.VII	• • 07 62 119 51 10 10t 14 105 62 78 51 10 76 10 01 • • • 01 27 14 06																						
DEMIR KAPIJA																										
BR. ST. 272	$H_s = 125 \text{ m } H_b = 125.7 \text{ m } h_t = 2.1 \text{ m } h_r = 1.4 \text{ m}$																									
I 7.6 6.7 3.5 6.1 -	04.6 88 70 81 80 38	020 007.4	18	• 02 17 • • • 05 01 05 05 07 05 • 06 03 • • • • • • • • • • • 10 05																						
II 6.3 6.4 4.7 5.9 166.3	83 58 72 71 36	022 016.6	15	• • 06 • • • 10 • 05 07 04 04 01 04 • • • • • • • • • • • 02 • •																						
III 5.0 5.8 3.5 4.5 166.3	81 68 67 25	034 017.0	14	• • 06 02 • • 12 02 08 07 05 03 01 05 01 01 • • • • • • • • • • • 01 01																						
IV 4.5 5.4 2.6 4.2 166.6	76 43 60 60 27	017 010.4	03	• • 03 04 • • 05 02 08 05 04 03 01 04 • • • • • • • • • • • 02 • •																						
V 4.8 5.3 4.2 4.8 166.9	73 46 63 61 30	038 011.0	11	• • • 17 03 • • 02 • 07 08 09 06 01 09 • • • • • • • • • • • 02 05 • •																						
VI 2.7 4.5 3.7 3.7 115.5	74 41 64 60 28	058 015.0	04	• • 23 17 • • 10 04 12 10 02 12 • • • • • • • • • • • 05 • •																						
VII 1.9 3.2 1.5 2.3 122.9	69 40 56 55 21	072 035.1	07	• • 30 25 03 08 01 17 • 05 04 02 05 • • • • • • • • • • • 06 • •																						
VIII 2.2 2.2 2.1 2.1 121.1	73 39 57 56 23	045 033.5	07	• • 25 22 04 • • 15 02 05 04 03 01 05 • • • • • • • • • • • 03 • •																						
IX 4.9 4.9 2.9 4.2 166.5	75 43 55 59 20	019 015.6	25	• • • 18 08 01 • • 10 06 05 02 01 05 • • • • • • • • • • • 02 • •																						
X 3.0 2.5 1.1 2.2 167.1	86 43 62 64 20	007 003.6	04	• • 01 • • • 18 01 03 02 • 03 • • 01 05 04 02 05 • • • • • • • • • • • 03 • •																						
XI 7.0 6.1 4.5 5.9 167.2	81 60 74 72 33	018 009.3	21	• • 02 • • • 03 • 03 09 05 04 05 • 01 01 01 05 01 • • • • • • • • • • • 01 05																						
XII 6.6 6.2 4.1 5.6 166.6	81 66 76 75 47	039 002.6	11	• • 04 21 • • 02 • 06 08 08 05 • 03 04 • • 01 01 01 05 02 • • • • • • • • • • • 05 02																						
GOD. 4.7 5.0 3.3 4.3 -	08.2 78 50 66 65 20	359 035.1	07.VII	• • 06 55 124 75 08 49 06 116 66 70 52 10 66 09 02 • • • 01 02 26 27 08																						
KOCANI																										
BR. ST. 273	$H_s = 345 \text{ m } H_b = - \text{ m } h_t = 2.1 \text{ m } h_r = 1.2 \text{ m}$																									
I 7.1 6.2 5.8 6.4 -	05.3 91 64 51 80 50	036 011.0	28	• 02 21 • • • 05 10 07 07 01 06 01 • • • • • • • • • • • 01 • •																						
II 6.4 6.4 5.8 6.2 176.4	93 84 92 90 61	033 012.4	15	• • 12 • • • 04 07 06 06 01 06 01 • • • • • • • • • • • 02 • •																						
III 4.2 5.0 4.0 4.4 168.4	98 78 88 86 52	014 014.0	14	• • 08 02 • • 10 07 01 01 01 01 01 • • • • • • • • • • • 01 01																						
IV 4.5 4.9 5.3 4.9 169.2	89 70 87 82 39	022 014.7	03	• • 02 04 • • 10 08 04 04 01 04 • • • • • • • • • • • 01 • •																						
V 4.2 5.0 5.8 5.0 -	13.0 86 65 63 80 20	050 021.2	25	• • • 16 01 • • 04 05 04 04 02 04 • • • • • • • • • • • 02 • •																						
VI 2.7 4.7 4.5 4.1 142.4	86 60 84 78 32	116 082.0	17	• • 24 10 • • 02 04 07 04 07 02 02 07 • • • • • • • • • • • 01 03																						
VII 2.9 3.1 3.4 3.2 164.5	65 76 72 30	024 016.0	23	• • 30 22 • • 05 04 04 04 04 04 04 • • • • • • • • • • • 04 • •																						
VIII 3.4 3.2 3.8 3.2 152.8	88 55 75 73 27	022 007.6	25	• • 26 17 01 • • 11 02 04 04 04 04 04 • • • • • • • • • • • 03 • •																						
IX 4.0 4.9 4.4 4.8 12.5	90 66 73 63 80 35	020 015.0	25	• • • 19 03 • • 06 05 03 03 01 03 • • • • • • • • • • • 01 • •																						
X 2.7 2.7 2.2 2.5 169.3	85 67 82 78 17	014 009.5	12	• • 02 • • • 03 02 • • 03 02 03 03 • • • • • • • • • • • 03 • •																						
XI 6.8 6.3 7.2 6.8 167.8	84 73 85 81 47	066 017.0	27	• • 01 • • • 03 02 • • 02 • 07 12 04 04 01 01 01 01 • • • • • • • • • • • 01 01																						
XII 6.5 6.5 6.0 6.3 164.1	86 62 88 85 58	010 005.0	04	• • 06 24 • • 03 02 • • 03 02 03 02 03 02 • • • • • • • • • • • 01 01																						
GOD. 4.0 4.2 3.5 4.0 -	07.7 78 51 71 66 17	221 018.0	27.XI	• • 06 08 66 120 44 02 47 19 140 68 63 45 05 60 08 04 • • 01 • • 22 08 04																						
GEVGELIJA																										
BR. ST. 275	$H_s = 59 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.4 \text{ m}$																									
I 6.0 6.0 4.7 4.5 5.5 -	05.2 88 45 81 27	C54 016.6	17	• • 16 • • • 03 • 07 09 08 08 07 • 06 03 • • • • • • • • • • • 02 • •																						
II 6.4 5.8 3.9 5.4 -	66.7 86 63 81 76 43	035 016.4	15	• • 01 • • • 03 • 05 02 • • 03 02 • 07 05 03 02 01 03 • • • • • • • • • • • 04 • •																						
III 5.2 5.2 3.7 4.7 -	67.7 82 54 75 70 25	034 030.8	14	• • 03 02 • • 03 02 • 07 05 03 02 01 03 • • • • • • • • • • • 02 • •																						
IV 3.0 4.1 2.7 3.4 -	71.7 73 46 65 62 28	017 004.1	22	• • 01 05 • • 05 • 12 03 04 04 04 04 • • • • • • • • • • • 01 • •																						
V 3.7 4.8 3.8 4.1 -	10.8 75 51 73 66 32	098 028.3	05	• • • 16 03 • • 01 • 10 04 08 08 08 04 06 • • • • • • • • • • • 01 05 • •</td																						

1977

Mjesec	Vazdušni pritisak Pa mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina vatra nD, Fm (0-12)																			
		Tm				Min				Dat.				N		NE		E		SE		S		SW		W		NW	
		7	14	21	Sred. (dnev.)	Max	Min	Max	Dat.	Min	Max	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	
$\gamma = 41^{\circ}19' N \lambda = 22^{\circ}34' E$ Gr. $\Delta G = +1h\ 30\ min.$														VALANCOVC												BR. ST. 276			
I	-	01.9	08.4	04.6	04.9	09.1	00.8	17.8	31 -06.0	20.06	02	03.0	05	01.8	.	.	.	07	02.1	02	02.3	.	01	01.0	21	03.7	31		
II	-	06.4	13.4	10.1	10.0	13.5	05.2	22.0	23 -01.0	05	01	02.0	08	02.2	.	01	01.8	02	02.0	02	02.5	01	01.0	20	03.6	30			
III	-	06.0	15.7	11.9	11.6	16.4	05.5	21.7	24.23 -02.0	03	01	02.0	08	02.4	01	02.0	12	02.2	08	02.4	01	02.0	.	01	01.0	20	03.6	30	
IV	-	10.0	18.2	14.1	14.1	19.9	07.0	27.2	24 01.4	07	17	01	02.0	07	01.6	05	01.5	05	02.2	08	02.4	01	02.0	03	02.3	07	01.0	27	
V	-	15.0	25.1	19.5	19.6	25.4	12.6	31.0	03 06.8	13	.	.	.	12	01.5	02	02.5	06	01.3	08	02.4	05	01.8	.	01	01.0	26	03.2	34
VI	-	18.7	27.7	22.4	22.8	29.3	15.4	35.5	19.2	05.5	06	.	.	09	01.6	03	01.8	06	02.3	09	02.2	01	03.0	32	03.0	30			
VII	-	21.1	30.9	25.2	25.6	31.9	18.3	36.5	10 15.0	08	.	.	20	01.8	01	01.0	08	01.2	05	01.8	06	01.8	.	01	01.0	24	03.4	29	
VIII	-	20.1	29.9	24.7	24.8	31.1	17.4	34.6	01 11.5	27	.	.	09	01.8	.	.	06	01.8	09	02.2	07	01.4	01	04.0	26	03.0	35		
IX	-	16.2	24.6	19.9	20.2	25.9	13.4	31.6	02 03.2	30	01	03.0	14	01.9	.	.	06	02.2	.	.	05	02.2	.	.	01	01.0	31	03.0	33
X	-	08.8	21.0	14.5	14.7	21.7	07.1	25.6	02 02.0	18	.	.	13	01.5	.	.	09	01.6	11	01.7	04	01.5	.	01	01.0	13	03.6	43	
XI	-	09.1	15.4	11.8	12.0	16.4	07.7	23.1	04 06.5	22	01	05.0	10	01.9	.	.	08	01.9	05	01.8	03	01.0	.	01	01.0	27	02.6	36	
XII	-	06.6	05.7	03.0	03.1	06.7	00.6	13.0	01 07.5	06	03	02.3	08	01.8	.	.	01	01.0	05	01.4	03	02.7	.	01	01.0	37	03.7	36	
GOD.	-	11.2	19.6	15.1	15.3	20.7	05.2	36.5	40.VII -07.5	06.XII	10	03.1	125	01.7	06	01.8	76	01.8	86	02.1	51	01.9	03	02.7	328	03.3	410		
$\gamma = 41^{\circ}26' N \lambda = 22^{\circ}39' E$ Gr. $\Delta G = +1h\ 31\ min.$														STRUMICA												BR. ST. 277			
I	-	-00.7	06.4	01.5	02.4	07.2	-01.6	16.7	30 -06.0	20.06	20	05	02.8	07	01.1	12	01.1	06	01.3	08	02.4	.	.	.	01	01.0	16	02.0	39
II	-	03.8	12.3	07.5	07.8	13.8	02.7	20.2	12 -02.5	05	04	01.2	.	12	01.4	13	01.5	09	02.0	05	01.2	03	01.0	22	02.7	22			
III	-	04.1	15.4	09.5	09.6	16.6	02.8	27.7	24 -04.8	03	11	02.3	02	01.0	02	01.5	02	01.0	12	02.4	16	02.2	04	02.0	19	02.7	25		
IV	-	07.8	18.0	11.6	12.3	19.7	04.0	26.7	30.24 01.2	14	09	02.3	03	02.3	02	02.0	.	.	11	02.4	09	01.6	06	02.3	29	02.6	21		
V	-	15.0	24.1	17.6	18.6	25.1	10.8	30.6	23 04.5	30	02	02.0	01	01.0	02	01.5	01	02.0	09	02.4	15	01.9	10	01.6	19	02.1	34		
VI	-	17.9	27.2	20.8	21.2	26.2	12.3	33.8	20 04.4	01	05	02.0	01	01.0	02	02.3	03	01.7	07	01.7	03	01.8	07	01.1	26	02.6	36		
VII	-	20.4	30.2	22.1	22.2	31.0	12.8	35.2	10 11.3	13	09	01.4	03	01.3	03	01.3	04	01.2	10	02.2	08	01.6	09	01.9	20	02.2	27		
VIII	-	18.1	29.1	21.2	22.5	30.1	14.4	34.0	30.22 00.5	21	02	02.5	05	01.4	04	01.2	04	01.5	09	01.7	10	01.8	07	01.7	21	02.0	31		
IX	-	12.8	23.5	16.3	17.2	25.1	10.2	31.8	05 -00.3	30	09	01.8	07	01.4	04	01.5	06	02.0	06	02.3	02	02.0	07	01.1	13	02.1	36		
X	-	04.9	20.3	10.8	11.7	21.2	03.4	26.2	02 -01.3	01	06	01.3	.	07	01.4	03	01.7	07	01.7	06	01.3	07	01.4	06	01.5	51			
XI	-	06.0	14.0	08.6	09.4	16.0	04.0	22.3	11.05 -01.2	22	09	01.4	04	01.0	03	01.3	07	02.9	10	02.0	.	05	02.0	20	01.8	32			
XII	-	-02.9	03.9	-00.6	00.1	05.1	-03.8	12.4	02 -05.4	23	07	01.6	05	01.2	03	01.0	06	01.7	04	01.8	02	01.0	02	02.5	37				
GOD.	-	08.9	18.8	12.3	13.1	20.6	06.3	35.2	40.VII -09.4	45.XII	78	01.9	38	01.3	56	01.4	55	01.7	102	02.1	76	01.8	67	01.7	232	02.2	391		
$\gamma = 41^{\circ}13' N \lambda = 22^{\circ}43' E$ Gr. $\Delta G = +1h\ 31\ min.$														NCVI DOJRAN												BR. ST. 278			
I	-	02.7	07.0	03.2	04.3	07.8	01.1	15.5	31 -05.0	07	.	.	.	13	02.8	.	.	03	01.3	.	.	.	.	.	21	05.2	56		
II	-	06.6	11.5	07.8	08.4	12.8	04.9	18.5	13 -02.5	28	.	.	.	05	03.4	.	.	03	02.0	.	.	01	02.0	16	05.4	58			
III	-	06.8	14.0	08.6	09.7	15.0	05.3	26.5	24 -03.0	01	06	05.8	.	09	03.9	.	07	02.9	.	.	03	02.7	19	03.8	49				
IV	-	10.2	17.6	11.4	12.7	18.7	07.5	27.0	24 03.4	12	03	06.0	.	04	04.8	.	03	04.0	.	.	01	02.0	36	04.6	43				
V	-	16.2	23.7	16.7	16.4	24.5	12.8	29.7	23 06.4	28	01	04.0	.	10	03.3	.	02	01.0	.	.	.	.	19	04.2	61				
VI	-	20.2	27.3	20.7	22.2	28.2	15.9	33.6	12 10.6	06	01	02.7	.	03	02.7	.	03	02.7	.	.	30	03.6	57						
VII	-	21.9	30.1	23.0	24.5	31.1	16.7	37.3	10 12.3	08	.	.	.	04	02.5	.	03	02.3	.	.	32	04.3	54						
VIII	-	21.2	28.9	22.2	23.6	30.1	16.4	34.1	22 14.5	25	.	.	.	02	01.5	.	04	01.8	.	.	.	.	23	03.7	64				
IX	-	16.8	24.0	17.6	19.0	25.1	14.8	32.0	07.05 05.0	30	.	.	.	03	02.3	.	02	02.0	.	.	.	.	.	28	04.4	57			
X	-	18.9	23.2	13.7	19.6	25.3	10.3	32.2	20 05.6	01	.	.	.	07	02.0	.	01	02.0	.	.	.	.	09	03.4	77				
XI	-	09.8	14.1	10.4	11.2	15.0	08.4	22.0	11 03.0	20	.	.	.	20	03.3	.	01	06.0	.	.	.	.	21	04.6	46				
XII	-	01.6	05.6	02.5	03.0	06.4	00.1	11.6	30 -02.2	24	.	.	.	05	03.6	.	01	01.0	.	.	.	.	53	05.5	34				
GOD.	-	12.1	18.6	13.1	14.2	19.5	08.8	37.3	40.VII -05.2	24.XII	10	05.7	.	.	65	03.1	.	28	02.4	.	.	05	02.4	309	04.5	658			
$\gamma = 41^{\circ}58' N \lambda = 22^{\circ}46' E$ Gr. $\Delta G = +1h\ 31\ min.$														DELČEVAC												BR. ST. 279			
I	-	-02.5	05.7	-00.2	00.7	06.1	-04.1	13.5	31.36 -12.0	20.06	11	02.3	03	01.7	03	02.0	01	04.0	10	01.7	04	03.0	16	01.8	01	03.0	44		
II	-	01.9	11.3	05.6	0																								

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha e <sub>m</sub> mm	Padavine R mm	Broj dana na sat:																	
	7	14	21			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲		
	Sred. (Dnes)	Inspolacija broj sati	Min			Σ	Max	Dat.	H	<	<	IV	IV	<	>	IV	W	W	W	W	W		
VALANDOVAC																							
BR. ST. 276																							
I 5+7 5+4 4+7 5+3	-	05.0 80 65 79 75 32	038 011.2	17	.	.	13	.	.	.	01	.	08 10	07 07	01 07	.	.	.	.	.	.	.	
II 6+6 5+6 4+4 5+5	-	06.4 82 58 71 70 32	042 018.4	15	.	.	01	.	.	.	03	03 05	05 05	05 02	05	.	.	.	.	.	.	01	
III 5+3 5+1 4+1 5+0	-	06.5 78 48 63 63 19	031 030.0	14	.	.	03	02	.	.	.	11 08 02	01 01	01 01	01	.	.	.	.	.	.	.	
IV 4+1 4+1 3+4 3+9	-	06.8 71 44 56 57 24	021 007.0	16	.	.	05	.	.	.	01	11 04 05	05 05	05	.	.	.	.	.	.	.	.	
V 4+0 4+5 4+1 4+2	-	10.5 80 49 63 64 28	074 022.4	29	.	.	17	02	.	.	.	12 05	08 08	03 08	.	.	.	.	.	.	.	.	
VI 2+4 3+6 4+2 3+4	-	12.3 74 45 62 60 32	102 044.6	17	.	.	24	16 01	.	.	13 02	07 07	04 07	04	.	.	.	.	.	.	.		
VII 1+6 2+3 1+5 1+9	-	13.6 71 41 58 57 30	032 022.4	24	.	.	31	27 04	.	.	22 01	05 04	01 05	.	.	.	.	.	.	.	01		
VIII 2+1 2+0 2+0 2+2	-	12.8 72 42 55 56 25	056 040.2	07	.	.	30	24 03	.	.	19 01	04 04	01 04	.	.	.	.	.	.	.	.		
IX 3+7 4+6 4+4 4+3	-	09.9 68 45 55 56 27	011 005.0	24	.	.	19	09	.	.	01	10 06	04 04	04	04	.	.	.	.	.	.		
X 3+2 4+5 1+4 2+3	-	08.0 83 47 45 63 22	006 004.4	04	.	.	02	.	.	.	22 04	02 02	02 02	02	.	.	.	.	.	.	02		
XI 7+2 5+6 4+7 5+9	-	08.1 85 65 77 76 44	056 026.0	27	.	.	17	.	.	.	03 10	06 06	06 02	06	.	.	.	.	.	.	01 01		
XII 4+9 4+8 3+3 4+3	-	04.4 78 66 75 73 46	018 006.5	11	.	.	17	.	.	.	01	12 05	06 06	06	.	.	.	.	.	.	.		
GOD. 4+2 4+2 3+6 4+0	-	08.7 76 51 64 64 19	487 044.6	07.VII	.	.	34	130 78 08	07	.	146 61	61 59	15 60	01	.	.	.	.	02	01	03 01		
STRUMICA																							
BR. ST. 277																							
I 5+5 4+5 3+6 4+6	-	103.4 04.7 54 69	90 84 36	024 008.7	17	.	21	.	.	.	01	10 03	11 06	11 01	.	.	.	.	.	.	05		
II 5+7 5+2 4+0 5+0	-	139.9 06.4 93 63	62 20 43	035 014.5	15	.	05	.	.	.	04	06 06	07 05	05 01	07 01	.	.	.	.	.	.	08	
III 4+6 5+0 3+5 4+9	-	170.4 06.6 90 46	70 69 28	024 020.8	14	.	11	02	.	.	04	07 06	04 03	03 01	04 01	.	.	.	.	.	.	01	
IV 3+7 3+8 3+0 3+5	-	243.5 06.3 78 41	60 60 22	023 006.9	03	.	03	05	.	.	07	11 03	05 05	05	05	.	.	.	.	.	.	01	
V 3+6 3+2 3+2 3+8	-	260.5 09.7 75 44	66 62 26	056 022.2	29	.	18	03	.	.	.	09 05	10 05	02 10	.	.	.	.	.	.	05		
VI 2+2 4+1 3+2 3+2	-	300.4 11.6 76 43	70 63 29	059 013.9	04	.	24	12	.	.	12 02	10 09	03 03	02	.	.	.	.	.	.	07		
VII 1+1 2+2 1+9 1+7	-	358.1 13.1 73 42	61 56 24	031 021.4	24	.	31	23	.	.	04	22	06	02	01	06	.	.	.	.	.	06	
VIII 1+8 2+2 1+3 1+8	-	321.6 12.4 79 42	66 63 27	053 035.0	07	.	29	18	.	.	03	21	05	04	01	05	.	.	.	.	.	01 02	
IX 3+6 5+2 3+3 4+0	-	208.2 09.9 85 48	72 68 25	024 011.3	25	.	01	19	04	.	01	09 06	07 04	01 01	07	.	.	.	.	.	.	05	
X 2+5 2+5 1+5 2+2	-	220.2 07.2 53 46	75 71 27	001 000.8	04	.	06	02	.	.	21	03	02	02	02	.	.	.	.	.	.	06	
XI 6+9 5+2 4+2 5+4	-	116.0 07.1 91 61	85 79 35	041 014.4	21	.	04	.	.	.	03	07	11 06	02 11	01	.	.	.	.	.	.	09	
XII 4+8 4+8 3+0 4+1	-	107.0 04.0 90 71	91 84 48	015 004.6	10	.	26	.	.	.	12 06	10 05	08 03	.	.	.	.	.	.	.	05		
GOD. 3+8 4+1 3+0 3+6	-	2549.2 08.2 84 51	74 70 22	386 035.0	07.VIII	.	77	130 60	.	25	.	143 47	88 84	54 12	86	07	.	.	.	.	.	01 26 35	
NOVI DODRAZ																							
BR. ST. 278																							
I 6+2 5+4 5+4 5+6	-	05.5 87 80 88 85 53	053 015.0	12	.	.	10	.	.	.	06	02	08 12	07 07	03 03	07	.	.	.	.	.	01 01	
II 6+9 5+8 5+5 5+9	-	07.9 90 84 88 88 60	035 016.5	15	.	.	02	.	.	.	05	03	04 11	11 03	03 02	03	.	.	.	.	.	01 03	
III 5+6 5+2 5+0 5+3	-	07.6 87 72 84 81 41	046 043.0	14	.	.	03	01	.	.	04	02	08 09	04 04	01 01	03	.	.	.	.	.	04 01	
IV 5+1 4+3 2+7 4+0	-	08.6 78 74 70 74 40	024 010.0	22	.	.	03	.	.	.	09	02	12 07	04 03	01 01	04	.	.	.	.	.	01 01	
V 4+2 4+2 3+9 4+1	-	11.8 79 60 70 72 32	088 036.0	16	.	.	16	.	.	.	04	13 07	07 07	03 03	07	.	.	.	.	.	03 01		
VI 2+6 2+6 4+2 3+2	-	14.3 76 58 75 65 39	083 023.0	17	.	.	24	12	03	.	05	18 05	06 06	03 03	06	.	.	.	.	.	.	06	
VII 1+1 1+3 1+2 1+2	-	15.3 73 54 69 65 31	022 009.5	24	.	.	31	25 09	08	.	24	03	03	03	03	.	.	.	.	.	03	.	
VIII 2+4 2+4 2+3 2+3	-	14.7 79 55 70 66 21	026 061.0	07	.	.	29	18	07	04	18	02	05	01	05	.	.	.	.	.	03		
IX 4+1 5+1 3+8 4+3	-	10.6 71 51 70 64 31	013 006.0	26	.	.	19	07	.	03	02	13 08	03 03	03	03	.	.	.	.	.	.		
X 4+5 2+7 1+9 3+0	-	08.9 85 60 80 75 29	002 002.0	13	.	.	15	01	.	15	04	01	01	01	.	.	.	.	.	.	03		
XI 8+4 6+6 5+7 6+9	-	08.3 86 74 83 81 36	058 021.0	21	.	.	08	09	01	02	13 06	06 02	06	02	06	.	.	.	.	.	01 01		
XII 5+8 5+3 3+5 4+8	-	04.4 75 68 79 74 48	022 007.0	10	.	.	16	.	.	08	04	10 07	05 05	05	05	.	.	.	.	.	01 02		
GOD. 4+7 4+3 3+7 4+2	-	09.8 80 64 78 74 21	530 061.0	07.VIII	.	.	31	123 62 19	66	17 145 85 54	53 16 52	01	.	.	.	.	01	19 12 01	.	.	.		
DELCEVC																							
BR. ST. 279																							
I 6+5 5+5 4+6 5+5	-	04.1 77 72 84 78 41	040 011.5	28	03	01	24	.	.	.	01	08 08	07 05	01 06	02	.	.	.	.	.	04		
II 5+9 5+8 4+9 5+5	-	05.6 81 67 83 77 32	034 012.5	15	.	.	13	.	.	.	04	05 06	06 06	01 08	01	.	.	.	.	.	03		
III 4+1 4+2 5+3 3+9	-	05.5 82 57 77 72 16	029 022.2	14	01	01	12	01	.	.	05	16 06	07 04	01 03	02	.	.	.	.	.	01 03		
IV 4+5 5+0 3+8 4+5	-	06.3 79 55 66 67 21	025 014.5	16	.	.	07	01	.	.	06	12 06	05 04	01 05	.	.	.	.	.	.	01		
V 4+5 6+6 3+7 4+8	-	08.6 76 47 67 63 15	066 021.5	28	.	.	11	02	.	.	01	05 04	05 05	07 03	07	.	.	.	.	.	03 01		
VI 3+3 3+3 4+5 4+3	-	10.8 82 57 77 72 28	076 015.5	05	.	.	17	01	.	.	10	03	14	10 02	14	.	.	.	.	.	07		
VII 2+7 3+5 2+5 2+9	-	13.0 79 56 73 69 20	058 021.7	18	.	.	26	04	.	.	02	14	01	07	02	.	.	.	.	.	01 06		
VIII 2+7 3+7 1+7 2+7	-	12.1 80 57 70 69 19	025 009.7	25	.	.	25	06	.	04	01	16	01	04	04	.	.	.	.	.	04		
.IX 4+4 4+4 3+1 3+9	-	08.5 82 52 67 67 19	023 012.2	25	.	.	01	14	.	.	03	12 06	07 04	01 07	.	.	.	.	.	.	01		