

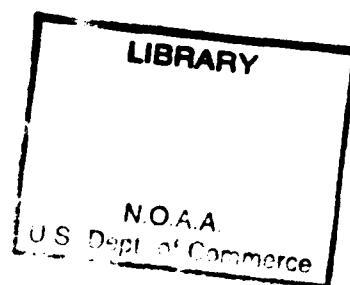
SOCIJALISTIČKA FEDERATIVNA REPUBLIKA JUGOSLAVIJA - RÉPUBLIQUE SOCIJALISTE FÉDÉRATIVE DE YUGOSLAVIE
HIDROMETEOROLOŠKA SLUŽBA - SERVICE HYDRO-MÉTÉOROLOGIQUE

METEOROLOŠKI GODIŠNjak I

ANNUAIRE METEOROLOGIQUE I

GODINA 1975 ANNÉE

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O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljaju se podaci 8 odabranih stanica, i to: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd i Skopje. U delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

φ = geografska širina, λ = geografska dužina od Griniča, ΔG vremenska razlika u odnosu na Grinič, H_g = nadmorska visina podnožja termometarskog zaklona, H_b = nadmorska visina rezervoara barometra, h_t = visina rezervoara termometra iznad tla, h_r = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebljene prema međunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

P = vazdušni pritisak u mm visine živinog stuba, reducirane na 0°C ; T = temperatura u $^{\circ}\text{C}$; e = pritisak vodene pare u mm visine živinog stuba; U = relativna vlažnost u procentima; D = pravac vetra po ruži vetra od 16 ili 8 pravaca; F = jačina vetra po Boforovoj skali (0-12); v = brzina vetra u m/sek; V = vidljivost u km; N = oblačnost (0-10); insola - cija = trajanje osundčavanja u satima; R = padavine u mm; R_s = padavine u mm; h_s = snežni pokrivač u cm; W = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan međunarodnim simbolima.

U rubrici "razvoj vremena" su potrebljene ove skraćenice:

n = u toku noći; a = pre podne; p = posle podne; i = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14, i 21 h po lokalnom vremenu računate su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente (P , e , U , N) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri suочitavani i uređivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h predhodnog dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebljene su oznake $M_{\overline{ax}}$ i $M_{\overline{In}}$; za rubrike broj dana sa \bullet ili \circ , \times ili Δ , i $\#$ prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Abrečnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SPRJ sa naznačenim klimatološkim stanicama u 1975 godini čiji brojevi odgovaraju brojevima stanica sa podacima u tablicama B.

NOTICE EXPLICATIVE

L'Annuaire météorologique I a deux parties: A) Observations journalières et: B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd et Skopje. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

φ = latitude, λ = longitude E de Greenwich, ΔG = différence entre l'heure locale et l'heure de Greenwich, H_s = altitude du pied de l'abri météorologique, H_b = altitude de la ouvette du baromètre, h_t = hauteur, au-dessus du sol, du réservoir du thermomètre, h_r = hauteur, au dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

La désignation des éléments météorologiques particuliers sont conformes aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

P = pression atmosphérique en mm (hauteur de la colonne de mercure réduite à 0°C); T = température en °C; e = tension de vapeur d'eau en mm de la hauteur de la colonne de mercure; U = humidité relative en %; D = direction du vent en rose des vents de 8 ou de 16 directions; F = force du vent d'après l'échelle Beaufort (0-12); v = vitesse du vent en m/s; V = visibilité en km; N = nébulosité (0-10); insolation = durée d'insolation en heures; R = = précipitations en mm; h_s = épaisseur de la couche de neige en cm; W = évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux.

Dans la colonne "Razvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

n = pendant la nuit; a = avant midi; p = après midi; i = avec interruption.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

et pour les autres éléments (P, e, U, N) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7h, 14 h et 21 h.

Les lectures des thermomètres à maxima et minima suivies de leur amorçage, ont été faits à 21 h et les valeurs inscrites le même jour.

Les valeurs journalières des précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau, de la force du vent $F \geq 6$ (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air les indications $M_{\overline{ax}}$ et $M_{\overline{in}}$ ont été utilisées; dans les colonnes "Broj dana sa" (Nombre de jours avec) e ou g, * ou Δ , et \otimes sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1975; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

AZBUČNI SPISAK STANICA

PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

I

S T A N I C A	Broj stan.	Redovna vidljiv. N. E.	Geografska latitudo N. S.	Geografska doljina V. U.	Red stavka	Jed strane	Vrednost pristisk mbar	Temperatura gradnja	Vlažnost gradnja	Vetar	Gledanj gradnja	Iskolicija gradnja	Prašine	Prečišćenje gradnja
S O C I J A L I S T I Č K A R E P U B L I K A S L O V E N I J A														
Ajdovščina	29	110	45°53'	13°54'	ob	I						x	x	x
Babno Polje	35	756	45 39	14 33	ob			x	x	x	x	x	x	x
Bovec	1	425	46 20	13 33	ob			x	x	x	x	x	x	x
Brnik-Letalisce	11	362	46 15	14 29	gl	I		x	x	x	x	x	x	x
Celje-Levec	18	294	46 15	15 14	ob			x	x	x	x	x	x	x
Črnomelj	38	156	45 34	15 12	ob			x	x	x	x	x	x	x
Dom na Komni	5	1520	46 17	13 46	ob			x	x	x	x	x	x	x
Golnik	10	500	46 20	14 20	ob			x	x	x	x	x	x	x
Gornji Lenart	39	150	45 56	15 34	ob			x	x	x	x	x	x	x
Ilirska Bistrica	31	414	45 34	14 15	ob			x	x	x	x	x	x	x
Javorje nad Poljanami	9	695	46 10	14 11	ob			x	x	x	x	x	x	x
Jeruzalem	23	345	46 28	16 12	ob			x	x	x	x	x	x	x
Jesenice	12	894	46 24	14 30	ob			x	x	x	x	x	x	x
Klenik pri Vrhah	14	550	46 07	14 51	ob			x	x	x	x	x	x	x
Kočevje	36	461	45 38	14 52	ob			x	x	x	x	x	x	x
Koper-Smedela	27	33	45 35	13 43	gl			x	x	x	x	x	x	x
Kredarica	6	2514	46 25	13 51	gl	I		x	x	x	x	x	x	x
Kubed	28	262	45 31	13 52	ob			x	x	x	x	x	x	x
Ljubljana-Beligrad	13	299	46 04	14 31	gl	I		x	x	x	x	x	x	x
Maribor	20	275	46 32	15 39	gl	I		x	x	x	x	x	x	x
Mačun	32	1017	45 38	14 22	ob			x	x	x	x	x	x	x
Muraka Bobota	22	184	46 38	16 11	gl	I		x	x	x	x	x	x	x
Nevelo pri Temnici	26	350	45 51	13 40	ob			x	x	x	x	x	x	x
Nova Gorica	25	113	45 57	13 39	gl	I		x	x	x	x	x	x	x
Nova Vas na Klekah	34	722	45 46	14 31	ob			x	x	x	x	x	x	x
Novo Mesto-Gotna Vas	37	220	45 48	15 11	gl	I		x	x	x	x	x	x	x
Postojna-Zaleg	30	533	45 46	14 12	gl			x	x	x	x	x	x	x
Pragerske	21	251	46 24	15 39	ob			x	x	x	x	x	x	x
Radeče	16	230	46 04	15 11	ob			x	x	x	x	x	x	x
Radlje ob Dravi	17	365	46 37	15 13	ob			x	x	x	x	x	x	x
Radovljica	8	495	46 21	14 11	ob			x	x	x	x	x	x	x
Rakitna	33	787	45 53	14 26	ob			x	x	x	x	x	x	x
Rateče-Planica	3	864	46 30	13 43	gl	I		x	x	x	x	x	x	x
Sela pri Planini nad Bevnico	19	550	46 06	15 24	ob			x	x	x	x	x	x	x
Šmartno pri Slovenskem Gradcu	15	452	46 29	15 07	gl			x	x	x	x	x	x	x
Tolmin	4	180	46 11	13 44	ob			x	x	x	x	x	x	x
Vedrije	2	258	46 01	13 33	ob			x	x	x	x	x	x	x
Veliki Dolenci	24	308	46 51	16 17	ob			x	x	x	x	x	x	x
Vojško	7	1070	46 01	13 55	ob			x	x	x	x	x	x	x
S O C I J A L I S T I Č K A R E P U B L I K A H R V A T S K A														
Bjelovar	63	141	45°54'	16°51'	ob	I		x	x	x	x	x	x	x
Boljajkovina	60	110	45 49	16 18	ob			x	x	x	x	x	x	x
Brestovača-Kovska	64	152	45 22	16 58	ob			x	x	x	x	x	x	x
Brestovac-Bolje	72	91	45 42	16 44	ob	I		x	x	x	x	x	x	x
Cres	76	5	44 57	14 25	ob			x	x	x	x	x	x	x
Crikvenica	49	2	45 10	14 42	ob			x	x	x	x	x	x	x
Čazma	62	144	45 45	16 38	ob			x	x	x	x	x	x	x
Daruvar	66	161	45 36	17 14	gl	I		x	x	x	x	x	x	x
Donji Meljani	68	120	45 44	17 38	ob			x	x	x	x	x	x	x
Donji Miholjac	70	97	45 46	18 10	ob			x	x	x	x	x	x	x
Dubrovački	99	49	42 39	18 06	ob			x	x	x	x	x	x	x
Djakovo	71	98	45 17	18 25	ob			x	x	x	x	x	x	x
Gospic	84	564	44 55	15 22	gl	I		x	x	x	x	x	x	x
Grades	85	560	44 18	15 51	ob	I		x	x	x	x	x	x	x
Evar	90	20	45 10	16 27	gl	I		x	x	x	x	x	x	x

AZBUČNI SPISAK STANICA

PO SOCIJALISTICKIM REPUBLIKAMA

II Znak x pokazuje da stanica raspolaze odgovarajućim podacima meteoroških elemenata navedenih u kolonama 7-14

SOCIJALISTIČKA REPUBLIKA BOŠNA I HERCEGOVINA

AZBUČNI SPISAK STANICA

PO SOCIJALISTICKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteorooloških elemenata navedenih u kolonama 7-14

III

SOCIJALISTIČKA REPUBLIKA SRBIJA

AZBUČNI SPISAK STANICA
PO SOCIJALISTIČKIM REPUBLIKAMA

IV Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14.

A Z B U Č N I S P I S A K S T A N I C A
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

A Z B U Č N I S P I S A K S T A N I C A PO SOSIJALISTIČKIM REPUBLIKAMA

VI

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

A) Dnevna osmatranja

$\varphi = 46^{\circ}04' \text{ N } \lambda = 14^{\circ}31' \text{ E } \Delta G = + 58 \text{ min.}$

BR. ST. 13

Dan	Vozdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih parov e mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	744.8	742.8	743.0	-01.6	05.4	00.1	00.9	05.3	-02.0	-07.5	03.7	03.9	04.0	92	59	86	79	E	1	NNE	1	NE	1
2	746.1	746.1	747.6	-03.4	06.0	00.9	01.1	06.1	-03.5	-08.3	03.3	04.7	04.3	96	68	88	84	NN	1	NE	1	NNW	1
3	747.6	746.4	746.6	00.7	04.8	00.6	01.7	05.2	00.6	-00.6	04.4	04.3	04.1	91	66	86	81	NE	1	NE	1	-	0
4	745.6	743.7	743.9	-02.5	-01.4	-03.4	-02.7	00.9	-03.7	-08.0	03.6	04.0	03.3	96	98	96	97	E	1	NE	1	NNE	1
5	745.5	743.8	743.3	-03.0	-00.6	-01.6	-01.7	-00.3	-04.6	-07.0	03.5	04.3	04.0	98	98	100	99	ESE	1	SSE	1	NN	1
6	741.1	738.8	738.2	-02.3	08.1	04.6	03.8	08.9	-02.4	-06.6	03.6	05.2	03.7	96	64	58	73	NN	1	NE	1	S	1
7	735.8	733.1	732.9	00.7	06.3	05.0	04.3	06.6	-01.6	-05.5	04.1	05.3	05.0	85	73	76	78	NNW	1	WSW	2	NN	2
8	728.4	728.8	735.0	02.8	07.8	05.2	05.3	08.3	02.6	01.2	04.5	05.4	02.1	80	68	31	60	NE	1	E	2	NW	2
9	741.1	743.9	745.1	-00.6	06.3	-01.8	00.5	06.4	-01.9	-04.0	02.8	02.8	03.4	64	40	87	64	SW	1	ESE	2	NE	1
10	743.8	743.4	744.3	-04.2	06.4	-01.0	00.1	08.3	-04.7	-09.7	02.9	03.8	03.1	91	53	72	72	WW	1	NE	1	N	1
11	743.1	742.0	742.1	-05.4	06.2	05.6	03.0	06.3	-05.4	-10.5	02.6	03.9	04.9	91	55	73	73	NNE	1	SW	2	M	2
12	741.6	741.5	742.7	-04.8	09.1	06.4	06.7	09.5	00.7	01.5	05.0	05.3	05.1	77	61	71	70	M	2	SW	3	SW	1
13	743.8	743.9	745.7	-01.2	09.0	00.3	02.1	09.8	-01.3	-05.0	04.0	05.3	04.4	96	62	93	84	NNE	1	ENE	1	NE	1
14	745.3	744.2	744.9	-03.7	08.1	06.1	04.2	09.0	-03.7	-08.7	03.3	05.1	05.1	98	63	72	78	NE	1	SM	3	SM	3
15	745.4	744.6	744.4	05.3	08.2	06.0	06.4	08.4	04.9	01.7	05.3	05.3	05.5	79	64	78	74	SW	2	SW	4	SW	3
16	742.6	741.3	741.0	06.2	08.7	08.2	07.8	09.4	05.3	03.6	05.8	06.3	06.1	81	74	75	77	SW	3	SW	2	WSW	1
17	739.1	737.5	736.5	08.3	10.1	09.6	09.4	10.4	07.3	05.9	06.1	06.7	07.1	74	72	79	75	WW	2	SW	2	WSW	3
18	734.2	734.5	734.3	08.6	09.0	07.9	08.4	10.0	07.9	07.0	07.8	07.3	07.1	93	84	89	89	SW	1	SM	2	NN	1
19	735.2	737.1	740.5	07.2	10.7	04.2	06.6	11.4	04.1	04.5	06.8	06.5	05.7	90	68	93	84	WSW	1	SW	2	N	1
20	744.4	744.2	743.1	05.6	07.9	05.7	06.2	08.0	03.6	04.5	06.3	06.2	06.1	93	77	89	86	N	1	NNW	1	NNW	1
21	741.9	741.2	742.5	03.4	06.7	03.0	04.0	08.2	02.6	01.4	05.8	05.3	05.3	98	72	94	88	NNE	1	ENE	1	NNW	1
22	743.4	742.5	740.9	03.2	06.3	04.8	04.8	06.7	01.9	-00.7	05.6	05.6	05.9	97	78	86	87	WW	1	NE	1	N	1
23	737.7	736.7	736.5	02.9	07.4	06.4	05.8	07.7	01.8	01.2	05.4	05.3	04.8	95	68	67	77	NNE	1	SW	2	SW	2
24	734.7	735.3	736.7	06.4	07.8	05.0	06.1	08.4	04.8	02.8	05.6	05.9	05.2	77	75	80	77	M	1	SW	2	M	1
25	738.1	737.9	737.6	04.1	09.7	07.7	07.3	10.2	02.7	-02.2	05.4	05.6	05.8	88	62	74	75	NE	1	ENE	1	W	2
26	737.7	739.3	741.2	05.4	10.6	08.0	08.0	11.1	05.2	03.3	05.6	06.1	05.8	83	63	73	73	NE	1	NE	2	ENE	1
27	740.6	736.0	730.5	05.4	06.0	06.8	06.3	08.5	05.0	04.6	05.4	05.0	05.7	80	72	77	76	ENE	1	SSW	1	SM	1
28	726.1	728.0	729.8	05.0	06.2	04.9	05.3	07.1	02.5	04.6	06.2	05.4	05.1	94	76	79	83	N	2	SSE	2	ENE	1
29	727.1	728.9	733.1	01.7	07.9	02.8	03.8	09.6	00.6	-03.4	05.0	05.5	05.2	97	69	92	86	SSW	1	ENE	1	W	1
30	734.6	736.2	740.5	00.4	06.4	05.5	04.5	07.2	-00.3	-04.4	04.6	04.7	05.3	98	65	78	80	SSE	1	NW	1	NNW	1
31	742.8	742.0	740.8	02.7	09.8	02.6	04.4	10.6	02.0	-02.7	04.9	05.0	05.0	87	54	90	77	ESE	1	ESE	1	W	1
MES.	VRED.	740.0	739.5	740.2	02.0	07.1	04.1	04.3	07.8	01.0	-01.5	04.8	05.2	04.9	89	68	80	79	1.2	1.6	1.3		

1	740.0	742.7	745.1	00.4	03.6	03.3	02.7	04.2	-00.6	-02.6	04.6	05.0	05.4	98	85	92	92	N	1	SE	1	NNE	1
2	745.9	743.8	741.6	02.0	10.0	04.8	05.4	11.1	01.6	-02.4	04.9	05.6	05.5	93	61	86	80	NNE	1	SM	1	NNE	1
3	741.2	742.4	744.8	03.2	05.9	02.6	03.6	06.4	02.2	-00.2	05.1	04.1	03.7	88	51	87	81	ESE	3	ENE	4	ENE	2
4	746.4	748.2	749.7	01.7	02.4	01.4	01.7	02.8	01.3	00.9	03.7	03.6	03.2	71	65	64	67	E	3	NE	2	E	2
5	750.8	749.0	748.9	-00.8	05.4	-01.4	00.5	05.6	-01.4	-05.2	03.4	03.8	03.5	80	56	85	74	NE	1	ESE	1	NNW	1
6	748.4	746.8	744.7	-04.0	02.1	-01.6	-01.3	06.6	-04.7	-09.0	03.3	04.5	03.8	100	84	92	92	NE	1	ENE	1	N	1
7	740.5	737.1	737.3	-05.4	10.3	01.1	01.8	12.4	-05.8	-08.8	02.8	04.1	04.0	98	44	80	74	-	0	NNE	1	NNW	1
8	741.2	742.4	744.0	-02.5	02.4	-00.4	-00.2	02.8	-02.6	-07.6	03.5	03.0	03.3	94	55	75	75	NN	1	SSE	2	N	1
9	743.3	741.6	740.3	-05.4	04.4	-02.4	-01.5	05.6	-05.9	-09.6	02.4	02.4	03.0	82	39	79	67	SW	1	SW	1	ESE	1
10	740.2	738.6	738.9	-06.3	07.7	03.4	02.1	08.1	-06.4	-10.0	02.6	04.0	04.2	95	51	71	72	ESE	1	SM	3	WSW	2
11	738.2	737.5	736.2	01.3	07.4	05.6	05.0	07.8	01.1	00.6	03.9	05.9	05.0	77	77	73	76	NNE	1	SW	2	WSW	2
12	733.8	733.3	732.3	06.6	08.4	07.4	07.5	08.7	05.3	03.3	04.1	06.0	05.5	83	73	71	76	W	1	W	3	NN	2
13	729.2	727.6	726.9	06.6	10.0	06.3	07.3	11.5	04.5	00.5	05.7	05.8	05.8	78	63	81	74	SW	1	NW	1	NNE	1
14	727.4	727.3	730.4	01.3	06.2	01.1	02.4	04.5	01.0	-02.6	05.0	05.9	04.7	98	83	95	92	ESE	1	NNE	1	NNE	1
15	734.1	735.0	736.9	01.4	07.0</td																		

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 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_x = 1.5 \text{ m}$

Dan	Vrijeme 0-9	Obločnost N (0-10)					Instalacija broj sati	Padavina R mm	Snožni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8 06	07 0	07	06.7	04.6	$\rightarrow 0-10^{\circ} 19^{\circ} 24; = 4^{\circ} 7^{\circ} 19^{\circ} 24; \rightarrow 6^{\circ} 7^{\circ} 19^{\circ} 0$	
2	6 01	04 0	09	04.7	03.4	$\rightarrow 0-11^{\circ} 18^{\circ} 24; = 0-14^{\circ} 17^{\circ} 24; \rightarrow 14^{\circ} 17^{\circ} 0$	
3	7 10	09	10	09.7	00.0	$= 0-0^{\circ} 19^{\circ} 24; \rightarrow 0-10^{\circ} 20^{\circ} 24; \rightarrow 0$	
4	1 00	10 0	10	06.7	00.0	$\rightarrow 0-12^{\circ} 19^{\circ} 24; = 0-6^{\circ} 19^{\circ} 24; \rightarrow 15^{\circ} 16^{\circ} 19^{\circ} 24; \rightarrow 0$	
5	4 10	07 0	10 0	09.0	00.0	$\rightarrow 0-10^{\circ} 24; = 0-24^{\circ} 13^{\circ} 14^{\circ} 0$	
6	5 01	00 0	00	00.3	06.2	$\rightarrow 0-10^{\circ} 20^{\circ} 24; \rightarrow 0-2^{\circ} 14^{\circ} 00^{\circ} 44^{\circ} 16^{\circ} 0$	
7	7 10	10	10	10.0	00.0	$= 0-8^{\circ} 10^{\circ} 16^{\circ} 24$	
8	7 10	02 0	00	04.0	04.5	$= 0-11^{\circ} 16^{\circ} 20^{\circ} 0$	
9	9 00	01 0	00	00.3	07.7	00.4	.	.	.	$\rightarrow 0-7^{\circ} 17^{\circ} 17^{\circ} 24; = 2^{\circ} 24^{\circ} 0$	
10	8 05	04 0	00	03.0	06.2	$\rightarrow 0-10^{\circ} 19^{\circ} 24; = 0-7^{\circ} 0$	
11	7 00	09	10	06.3	00.7	$\rightarrow 0-12^{\circ} 0$	
12	7 01	04 0	10	05.0	04.4	$= 9^{\circ} 10^{\circ} 20^{\circ} 24; \rightarrow 0$	
13	7 01	01 0	00	00.7	06.0	$\rightarrow 0-10^{\circ} 11^{\circ} 14^{\circ} 20^{\circ} 24; \rightarrow 6^{\circ} 10^{\circ} 18^{\circ} 24; \rightarrow 0$	
14	6 10	02 0	04	05.3	03.2	$\rightarrow 0-11^{\circ} 15^{\circ} 13^{\circ} 0$	
15	8 02	06 0	10	06.0	01.6	$\rightarrow 0-3^{\circ} 8^{\circ} 0$	
16	7 10	07 0	10	09.0	01.2	$\rightarrow 0-3^{\circ} 3^{\circ} 11^{\circ} 16^{\circ} 15^{\circ} 20^{\circ} 22^{\circ} 0$	
17	8 10	10	09 0	09.7	00.0	00.0	.	.	.	$\rightarrow 0-13^{\circ} 20^{\circ} 24; \rightarrow 0-24^{\circ} 14^{\circ} 9^{\circ} 15^{\circ} 19^{\circ} 20^{\circ} 0$	
18	6 10	10 0	10 0	10.0	00.0	08.9	.	.	.	$\rightarrow 0-14^{\circ} 18^{\circ} 20^{\circ} 24; = 18^{\circ} 24^{\circ} 0$	
19	7 10	09	00	06.3	00.2	03.7	.	.	.	$= 0-24^{\circ} 0$	
20	6 10	10	09	09.7	00.0	$= 0-24^{\circ} 0-5^{\circ} 6^{\circ} 43^{\circ} 0$	
21	5 10	01 0	09	06.7	02.7	$= 0-14^{\circ} 18^{\circ} 24; \rightarrow 0-14^{\circ} 7^{\circ} 22^{\circ} 0; \rightarrow 5^{\circ} 6^{\circ} 0$	
22	7 10	10 0	10	10.0	00.1	00.2	.	.	.	$= 0-11^{\circ} 0$	
23	7 09	09	10	09.3	00.0	00.0	.	.	.	$= 3^{\circ} 9^{\circ} 0$	
24	7 10	09	00	06.3	00.2	$\rightarrow 0$	
25	7 10	09 0	10	09.7	01.1	$\rightarrow 0$	
26	7 10	08 0	10	09.3	02.0	$\rightarrow 21^{\circ} 24^{\circ} 0$	
27	7 10	10	10	10.0	00.2	$\rightarrow 0-10^{\circ} 9^{\circ} 0$	
28	8 10	09	10	09.7	00.6	11.4	.	.	.	$\rightarrow 0-3^{\circ} 4^{\circ} 5^{\circ} 0-10^{\circ} 0$	
29	7 02	01 0	01	01.3	04.8	07.1	.	.	.	$\rightarrow 0-7^{\circ} 10^{\circ} 11^{\circ} 16^{\circ} 15^{\circ} 19^{\circ} 20^{\circ} 24^{\circ} 0$	
30	6 10	10	10 0	10.0	01.7	$\rightarrow 0-7^{\circ} 10^{\circ} 11^{\circ} 16^{\circ} 15^{\circ} 19^{\circ} 20^{\circ} 24^{\circ} 0$	
31	7 08	01 0	00	03.0	07.4	00.1	.	.	.	$\rightarrow 0-0^{\circ} 10^{\circ} 6^{\circ} 10^{\circ} 0$	
MES.	VРЕД.	07.0	06.4	06.7	06.7	70.7	31.0				

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1	6 10	09	10	09.7	00.0	$\rightarrow 0-0-9^{\circ} = 0-4^{\circ} 12^{\circ} 24; = 0-24^{\circ} 12^{\circ} 0; \rightarrow 9^{\circ} 13^{\circ} 0$	
2	7 10	01 0	07	06.0	07.3	00.9	.	.	.	$= 0-8^{\circ} 10^{\circ} 4^{\circ} 24; \rightarrow 0-23^{\circ} 24^{\circ} 0$	
3	7 10	05 0	09	08.0	05.8	01.5	.	.	.	$* 0-6^{\circ} 8^{\circ} 11^{\circ} 16^{\circ} 19^{\circ} 0$	
4	7 10	08 0	10	09.3	00.7	00.1	00	.	.	$= 7^{\circ} 16^{\circ} 00^{\circ} 10^{\circ} 19^{\circ} 24; \rightarrow 0-19^{\circ} 24^{\circ} 0$	
5	7 03	00 0	00	01.0	07.5	00.0	00	.	.	$\rightarrow 0-12^{\circ} 23^{\circ} 24; \rightarrow 0-23^{\circ} 24^{\circ} 0$	
6	4 10	00 0	00	03.3	03.8	$\rightarrow 0-10^{\circ} 12^{\circ} 24; = 2^{\circ} 4^{\circ} 13^{\circ} 24; = 0-4^{\circ} 13^{\circ} 00^{\circ} 15^{\circ} 17^{\circ} 0$	
7	8 10	00 0	00	03.3	05.7	$\rightarrow 0-12^{\circ} 19^{\circ} 24; = 0-0-19^{\circ} 24; = 0-0-12^{\circ} 19^{\circ} 24^{\circ} 0$	
8	7 00	10	10	06.7	00.0	$= 0-12^{\circ} 10^{\circ} 20^{\circ} 24; \rightarrow 0-23^{\circ} 24^{\circ} 0$	
9	8 00	00 0	00	00.0	09.0	$\rightarrow 0-10^{\circ} 10^{\circ} 20^{\circ} 24; \rightarrow 0-10^{\circ} 10^{\circ} 20^{\circ} 24; \rightarrow 0-10^{\circ} 10^{\circ} 20^{\circ} 24^{\circ} 0$	
10	7 00	00 0	07	02.3	06.8	$\rightarrow 0-10^{\circ} 12^{\circ} 00^{\circ} 12^{\circ} 13^{\circ} 0$	
11	7 09	10	06	08.3	00.0	$\rightarrow 1^{\circ} 2^{\circ} 2^{\circ} 0$	
12	8 10	10	00	06.7	00.0	00.0	.	.	.	$= 7^{\circ} 14^{\circ} 23^{\circ} 24^{\circ} 0$	
13	8 08	09	09	08.7	00.7	$= 0-2^{\circ} 1^{\circ} 2^{\circ} 2^{\circ} 0$	
14	6 10	10	10 *	10.0	00.0	$= 1^{\circ} 7^{\circ} 8^{\circ} 10^{\circ} 15^{\circ} 20^{\circ} 24^{\circ} 22^{\circ} 0$	
15	8 09	06 0	08	07.7	06.3	00.3	00	.	.	$= 0^{\circ} 8^{\circ} 0$	
16	7 10	06 0	00	05.3	02.7	$\rightarrow 0$	
17	8 01	01 0	00	00.7	09.0	$\rightarrow 0^{\circ} 10^{\circ} 12^{\circ} 24; = 7^{\circ} 10^{\circ} 00^{\circ} 10^{\circ} 4^{\circ} 0$	
18	8 00	01 0	00	00.3	08.9	$\rightarrow 0-11^{\circ} 12^{\circ} 11^{\circ} 21^{\circ} 15^{\circ} 18^{\circ} 21^{\circ} 0$	
19	6 02	04 0	09	05.0	05.2	$* 2-1-6^{\circ} = 1^{\circ} 10^{\circ} 0$	
20	8 09	09 0	00	04.0	00.2	02.6	03	.	.	$\rightarrow 0-12^{\circ} 23^{\circ} 24^{\circ} 0$	
21	8 07	04 0	10	07.0	03.1	00.0	00	.	.	$* 7-12^{\circ} 0$	
22	8 05	02 0	00	02.3	07.8	00.0	00	.	.	$\rightarrow 0$	
23	8 01	00 0	02	01.0	07.3	$\rightarrow 0-10^{\circ} 22^{\circ} 24; = 6^{\circ} 12^{\circ} 0$	
24	8 00	00 0	00	00.0	08.8	$\rightarrow 0-10^{\circ} 10^{\circ} = 4^{\circ} 10^{\circ} 00^{\circ} 10^{\circ} 21^{\circ} 0$	
25	6 00	01 0	07	02.7	08.9	$\rightarrow 0-4^{\circ} 9^{\circ} 0$	
26	8 07	01	00	02.7	09.0	$\rightarrow 7^{\circ} 14^{\circ} 00^{\circ} 11^{\circ} 13^{\circ} FENE 14^{\circ} 14^{\circ} 0$	
27	8 00	01	00	00.3	09.7	$\rightarrow 0-19^{\circ} 24^{\circ} 0$	
28	8 01	01	00	00.7	09.4	$\rightarrow 10-10^{\circ} = 6^{\circ} 9^{\circ} 00^{\circ} 11^{\circ} 12^{\circ} 0$	
MES.	VРЕД.	05.4	03.9	04.1	04.5	143.2	14.4				

$\varphi = 46^\circ 04' N \lambda = 14^\circ 31' E$ Gr. $\Delta G = + 58$ min.

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D S D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	739.4	737.6	737.3	-04.0	12.4	06.6	05.4	12.7	-04.7	-08.6	03.1	04.9	05.3	96	45	72	71	N	1	SM 3	SM 2	
2	737.7	737.6	738.4	00.0	11.9	09.2	07.6	12.6	-00.1	-03.0	04.3	05.6	05.8	93	54	67	71	-	0	WSW 3	SW 2	
3	736.4	735.0	734.3	09.2	11.9	08.6	09.6	13.2	07.9	07.5	06.1	06.6	05.8	70	63	70	68	WSW 2	W 3	M 1		
4	731.8	730.4	731.4	06.6	10.8	08.6	08.7	12.2	06.3	01.3	06.2	07.1	06.9	85	73	83	80	SSW 1	WNW 2	WSW 1		
5	731.6	732.6	734.6	06.8	08.4	07.8	07.7	08.9	06.5	05.4	06.9	07.9	07.0	93	95	89	92	N 1	NNE 1	W 1		
6	737.2	736.6	737.1	02.8	14.4	08.3	08.5	14.6	02.5	00.4	05.4	06.3	06.5	97	51	79	76	NNE 1	SSW 2	NNW 1		
7	737.4	735.2	735.0	02.7	15.1	11.1	10.0	16.6	02.6	-00.7	05.4	06.1	06.3	97	47	64	69	N	1	W 1	SW 2	
8	734.6	733.4	731.8	03.6	11.9	08.6	08.2	12.7	03.6	00.4	05.4	06.9	07.4	91	66	89	82	NNW 1	SSE 1	SSW 1		
9	728.6	725.4	723.2	04.4	16.2	11.6	11.0	17.2	04.0	01.0	06.3	07.3	06.1	100	53	60	71	SE 1	ENE 1	-	0	
10	723.5	724.8	727.7	06.4	10.2	08.6	08.5	12.6	04.2	04.4	07.0	08.2	07.8	97	88	93	93	-	0	NNW 1	WNW 1	
11	731.4	733.4	734.7	07.7	11.0	08.9	09.1	12.3	07.2	07.6	07.6	08.1	06.3	96	82	74	84	NNE 1	W 2	NW 2		
12	732.2	730.6	730.9	04.6	06.0	05.2	05.3	09.0	04.4	00.2	05.8	06.2	06.3	91	89	94	91	S 1	NNE 1	SSW 1		
13	731.1	731.8	732.3	03.9	06.3	06.4	05.8	08.1	03.5	02.0	05.8	06.8	06.9	96	95	96	96	NE 1	N 2	NW 1		
14	729.8	729.0	730.7	04.9	07.2	06.2	06.1	08.2	04.0	04.2	06.3	06.8	06.7	97	90	95	94	-	0	SE 1	NE 1	
15	732.9	733.3	734.0	04.8	09.4	05.0	06.1	11.9	04.7	04.2	06.3	06.3	06.2	97	72	94	88	SSE 1	ESE 1	-	0	
16	733.1	731.1	731.1	02.8	11.6	06.8	07.0	13.5	02.7	00.2	05.6	05.7	05.9	100	56	79	78	NNW 1	S 2	W 2		
17	729.6	729.6	730.1	04.2	03.6	01.0	02.5	07.3	00.7	03.5	05.8	05.2	04.8	94	88	97	93	N 1	-	0	SM 1	
18	728.5	729.1	730.6	00.6	01.6	01.2	01.2	03.0	00.3	01.4	04.7	04.9	04.8	98	95	97	97	ESE 1	SE 2	-	0	
19	726.0	726.0	728.9	02.2	03.6	04.4	03.7	05.4	01.0	01.5	05.3	05.8	06.1	98	98	98	98	W 1	N 1	SW 1		
20	731.1	731.6	732.4	01.4	11.3	07.1	06.7	11.7	01.4	-00.4	05.0	03.0	05.2	98	30	69	66	-	0	SW 2	W 1	
21	733.9	734.9	738.1	06.0	09.0	03.8	05.7	09.1	03.7	05.4	06.3	05.6	02.9	90	65	48	68	E 1	ESE 3	E 3		
22	738.9	734.8	733.2	-00.2	07.6	02.3	03.0	08.2	-00.7	-04.7	02.2	02.1	03.0	48	27	55	43	ESE 1	SE 3	ESE 2		
23	729.8	728.4	728.9	-02.2	03.3	00.2	00.4	04.0	-02.8	-06.1	03.2	03.1	03.5	82	53	76	70	-	0	SSW 1	E 1	
24	727.4	726.1	726.8	-03.4	07.4	02.2	02.1	08.7	-04.0	-04.5	03.2	02.9	03.4	92	37	64	64	W 1	ENE 1	NNE 1		
25	727.0	729.1	730.6	-02.8	08.9	03.4	03.2	09.7	-03.1	-05.8	03.3	02.0	02.6	92	23	45	53	NE 1	NW 7	W 1		
MES.	VRED.	731.1	730.6	731.2	02.8	08.8	05.6	05.9	10.3	02.1	00.7	05.2	05.6	05.5	91	68	79	79	0.8	1.8	1.2	

1	732.5	733.7	735.4	01.8	05.0	04.3	03.9	05.6	01.6	02.9	05.1	05.2	04.9	98	79	78	85	N 1	SE 1	SE 1	
2	733.2	731.1	729.8	03.3	05.0	03.9	04.0	05.7	02.7	02.6	05.5	05.3	05.2	94	82	85	87	NNW 1	NE 1	SE 1	
3	729.0	728.6	729.2	03.0	07.9	06.4	05.9	09.6	02.7	04.3	05.3	06.6	06.0	94	82	83	86	S 1	WW 2	S 1	
4	730.6	732.5	733.4	05.7	07.4	06.6	06.6	08.1	04.8	06.5	06.4	07.0	06.9	93	91	95	93	ENE 1	NNE 1	NW 1	
5	731.3	732.6	733.2	05.9	16.4	09.2	10.2	17.4	05.1	06.0	06.8	06.2	08.3	97	44	95	79	WWN 1	SSW 5	ENE 1	
6	733.4	732.2	732.3	08.3	12.8	10.4	10.5	13.1	07.9	07.7	07.8	08.2	08.8	95	74	93	87	E 1	WSW 2	NNM 1	
7	730.7	730.6	731.0	08.2	10.0	09.0	09.1	10.6	08.0	07.3	07.8	08.3	08.1	96	91	94	94	N 1	NNE 2	NM 1	
8	731.0	731.3	732.7	04.6	13.7	09.1	09.1	14.0	03.8	04.8	06.4	05.1	05.5	100	43	64	69	NNW 1	SW 3	WSW 1	
9	733.0	732.4	731.1	08.5	11.2	09.4	09.6	12.1	07.4	05.4	05.9	05.6	05.5	71	56	62	63	WSW 2	SE 1	NNE 1	
10	727.0	723.7	726.4	06.8	10.0	06.6	07.5	10.7	06.1	04.1	07.0	06.6	04.0	95	71	54	73	ESE 1	NW 2	NNM 2	
11	731.7	734.3	737.0	07.4	12.3	05.0	07.4	12.7	05.0	06.2	02.7	02.4	05.1	35	23	77	45	NNW 3	NM 2	SSW 2	
12	737.7	736.6	737.4	01.7	12.4	08.4	07.7	14.9	01.0	-00.6	04.8	04.4	04.9	93	41	59	64	WWN 1	SSW 1	SE 2	
13	737.6	735.8	736.8	02.4	15.8	10.7	09.9	16.3	02.2	00.8	04.9	05.9	06.4	90	44	67	67	NNE 1	SW 3	SM 3	
14	737.3	735.4	736.5	06.0	17.1	11.4	11.5	17.7	05.5	04.2	06.0	07.1	07.1	85	49	70	68	NNE 1	W 4	WSM 4	
15	732.4	730.7	729.2	08.7	13.0	11.3	11.1	15.0	07.4	02.4	06.5	07.2	06.7	77	64	66	69	NW 1	SW 3	WSW 2	
16	727.4	729.6	733.0	08.6	10.4	07.5	08.5	11.6	07.5	09.8	08.1	07.6	07.1	96	81	91	89	NNW 2	SE 1	WWN 1	
17	736.5	735.7	738.0	04.4	16.6	11.2	10.5	17.4	04.4	00.5	06.2	04.3	05.0	99	30	50	60	SSW 1	NNE 2	SE 2	
18	739.4	737.0	738.4	04.4	15.7	10.8	10.4	17.1	02.4	-00.6	05.1	04.8	05.5	81	36	56	58	NNE 1	ESE 1	ENE 1	
19	739.4	736.4	736.1	07.5	10.9	12.6	12.5	18.9	06.4	01.5	05.9	05.8	05.5	76	40	50	55	SSW 1	SM 3	ESE 2	
20	739.8	737.8	737.8	05.4	15.0	13.3	11.8	19.2	04.4	00.8	05.9	05.7	07.2	87	44	62	64	NNE 1	SE 1	NNW 1	
21	739.3	737.6	739.1	09.9	21.1	14.8	15.2	21.8	06.4	03.9	07.3	06.7	08.0	80	36	63	60	SSE 1	ENE 1	NE 3	
22	739.6	738.1	737.9	12.0	17.7	13.4	14.0	18.4	11.9	10.9	08.7	07.2	07.0								

BR. ST. 13

$$H_s = 299 \text{ m} \quad H_p = 297.6 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.5 \text{ m}$$

Dan	Vlhkosť 0-9	Oblačnosť N (0-10)					Inzidenčná početnosť broj sení	Padavina R mm	Snežné pekriviny h cm	Rozsah vremena w
		14	7	14	21	Sred Dnes				
1	7	01	000	00	00.3	09.1	.	.	.	$\rightarrow 0^{\circ} 12^{\circ} 9^{\circ} = 4^{\circ} 10^{\circ} \infty 10^{\circ} 2^{\circ}, 0$
2	8	07	050	10	07.3	03.9	.	.	.	$\rightarrow 4^{\circ} 8^{\circ} = 7^{\circ} 10^{\circ}, 0$
3	7	10	080	09	09.0	02.0	.	.	.	$\rightarrow 3^{\circ} 5^{\circ} 4^{\circ} 0$
4	8	09	100	100	09.7	01.5	00.4	.	.	$\rightarrow 0^{\circ} 2^{\circ} 1^{\circ} 1^{\circ} 24^{\circ} 0^{\circ} 12^{\circ} 12^{\circ}$
5	5	10	100	100	10.0	00.0	00.2	.	.	$\rightarrow 0^{\circ} 1^{\circ} 5^{\circ} 22^{\circ} 0^{\circ} 9^{\circ} 1^{\circ} 5^{\circ} 10^{\circ} = 6^{\circ} 24$
6	7	00	070	00	02.3	06.3	04.7	.	.	$= 0^{\circ} 4^{\circ} 0^{\circ} 6^{\circ} 2^{\circ} 0^{\circ} 8^{\circ} 14^{\circ} 0^{\circ}$
7	8	04	040	02	03.3	07.4	06.1	.	.	$\rightarrow 0^{\circ} 10^{\circ} 0^{\circ} 25^{\circ} 24^{\circ} 1^{\circ} 1^{\circ} 15^{\circ} 0^{\circ}$
8	7	09	10	06	06.3	01.7	.	.	.	$\rightarrow 0^{\circ} 2^{\circ} 2^{\circ} 24^{\circ} 1^{\circ} 3^{\circ} 9^{\circ} 22^{\circ} 24^{\circ} 0^{\circ}$
9	7	10	020	07	06.3	03.8	.	.	.	$\rightarrow 0^{\circ} 1^{\circ} 0^{\circ} 1^{\circ} 10^{\circ} 0^{\circ} 1^{\circ} 3^{\circ} 10^{\circ} \infty 14^{\circ} 22^{\circ}, 0$
10	6	07	100	100	09.0	00.0	00.7	.	.	$\rightarrow 0^{\circ} 4^{\circ} 2^{\circ} 24^{\circ} 1^{\circ} 9^{\circ} 5^{\circ} 1^{\circ} 3^{\circ} = 5^{\circ} 17^{\circ} 0^{\circ} 21^{\circ} 24^{\circ}, 0$
11	7	10	090	04	07.7	01.9	08.6	.	.	$\rightarrow 0^{\circ} 1^{\circ} 7^{\circ} 4^{\circ} 10^{\circ} 0^{\circ} 1^{\circ} 13^{\circ} 13^{\circ}, 0$
12	7	08	100	100	09.3	00.0	01.5	.	.	$\rightarrow 0^{\circ} 1^{\circ} 5^{\circ} 1^{\circ} 24^{\circ} 0^{\circ} 5^{\circ} 6^{\circ} 0^{\circ} 1^{\circ} 17^{\circ} 22^{\circ}, 0$
13	6	10	100	10	10.0	00.2	09.4	.	.	$\rightarrow 0^{\circ} 15^{\circ} 0^{\circ} 24^{\circ} 0^{\circ} 5^{\circ} 6^{\circ} 0^{\circ} 8^{\circ} 8^{\circ} 0^{\circ} 9^{\circ} 15^{\circ} 17^{\circ} 22^{\circ}, 0$
14	6	100	100	09	09.7	00.0	21.6	.	.	$\rightarrow 0^{\circ} 15^{\circ} 20^{\circ} 2^{\circ} 24^{\circ} 1^{\circ} 2^{\circ} 1^{\circ} 15^{\circ} 0^{\circ} 1^{\circ} 10^{\circ} 0^{\circ} 1^{\circ} 14^{\circ} 17^{\circ}, 0$
15	7	10	070	00	05.7	02.1	04.4	.	.	$\rightarrow 0^{\circ} 12^{\circ} 2^{\circ} 2^{\circ} 24^{\circ} 1^{\circ} 6^{\circ} 2^{\circ} 5^{\circ} 0^{\circ} 1^{\circ} 10^{\circ} 0^{\circ} 1^{\circ} 14^{\circ} 17^{\circ}, 0$
16	7	10	040	05	06.3	03.0	03.4	.	.	$= 0^{\circ} 2^{\circ} 11^{\circ} 13^{\circ}, 0^{\circ} 2^{\circ} 11^{\circ} 0^{\circ} 10^{\circ} 17^{\circ}, 0$
17	6	10	100	10*	10.0	00.0	04.6	.	.	$\rightarrow 1^{\circ} 24^{\circ} 0^{\circ} 1^{\circ} 5^{\circ} 0^{\circ} 2^{\circ} 3^{\circ} 0^{\circ} 1^{\circ} 14^{\circ} 12^{\circ} 0^{\circ} 1^{\circ} 21^{\circ}, 0$
18	5	10	10*	10*	10	00.0	21.3	03	.	$\rightarrow 0^{\circ} 24^{\circ} 0^{\circ} 1^{\circ} 18^{\circ} 2^{\circ} 24^{\circ} 1^{\circ} 2^{\circ} 1^{\circ} 15^{\circ} 0^{\circ} 1^{\circ} 11^{\circ} 12^{\circ} 18^{\circ} 19^{\circ} 2^{\circ} 1^{\circ} 13^{\circ}, 0$
19	4	100	100	100	10.0	00.0	15.1	03	.	$\rightarrow 0^{\circ} 14^{\circ} 0^{\circ} 1^{\circ} 24^{\circ} 1^{\circ} 2^{\circ} 1^{\circ} 15^{\circ} 0^{\circ} 1^{\circ} 20^{\circ} 1^{\circ} 11^{\circ} 10^{\circ} 1^{\circ} 14^{\circ} 17^{\circ} 19^{\circ} 2^{\circ} 1^{\circ} 13^{\circ}, 0$
20	8	10	040	10	06.0	06.3	75.4	.	.	$\rightarrow 0^{\circ} 6^{\circ} 4^{\circ} 10^{\circ}, 0^{\circ} 6^{\circ} 8^{\circ} 0^{\circ} 1^{\circ} 10^{\circ} 0^{\circ} 1^{\circ} 14^{\circ} 17^{\circ}, 0$
21	7	100	050	00	05.0	03.0	02.0	.	.	$\rightarrow 0^{\circ} 0^{\circ} 9^{\circ} 0^{\circ} 1^{\circ} 4^{\circ} 15^{\circ}, 0$
22	8	000	010	02	01.0	10.9	00.4	.	.	$\rightarrow 0^{\circ} 3^{\circ} 9^{\circ} 0^{\circ} 22^{\circ} 2^{\circ} 24^{\circ}, 0^{\circ} 8^{\circ} 1^{\circ} 4^{\circ} 15^{\circ}, 0$
23	7	09	090	00	06.0	00.8	.	.	.	$\rightarrow 0^{\circ} 0^{\circ} 8^{\circ} 0^{\circ} 21^{\circ} 2^{\circ} 24^{\circ}, 0^{\circ} 4^{\circ} 10^{\circ}, 0$
24	7	000	020	00	00.7	08.1	00.0	00	.	$\rightarrow 0^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 8^{\circ}, 0^{\circ} 8^{\circ} 0^{\circ} 1^{\circ} 10^{\circ} 0^{\circ} 1^{\circ} 14^{\circ}, 0$
25	9	010	020	03	02.0	09.8	.	.	.	$\rightarrow 0^{\circ} 0^{\circ} 9^{\circ} 0^{\circ} 1^{\circ} 4^{\circ} 15^{\circ}, 0$
26	8	060	040	00	03.3	06.7	.	.	.	$\rightarrow 0^{\circ} 1^{\circ} 4^{\circ} 8^{\circ} 0^{\circ} 1^{\circ} 14^{\circ} 2^{\circ} 0^{\circ} = 6^{\circ} 8^{\circ} 0^{\circ} 1^{\circ} 10^{\circ} 0^{\circ} 1^{\circ} 13^{\circ}, 0$
27	7	10	100	100	10.0	00.0	.	.	.	$\rightarrow 0^{\circ} 1^{\circ} 0^{\circ} 1^{\circ} 24^{\circ}, 0^{\circ} 3^{\circ} 1^{\circ} 17^{\circ} 0^{\circ} 1^{\circ} 20^{\circ} 0^{\circ} 23^{\circ}, 0$
28	7	100	10*	100	10.0	00.1	00.0	.	.	$\rightarrow 0^{\circ} 1^{\circ} 0^{\circ} 1^{\circ} 19^{\circ} 1^{\circ} 24^{\circ}, 0^{\circ} 3^{\circ} 1^{\circ} 13^{\circ} 0^{\circ} 1^{\circ} 15^{\circ} 0^{\circ} 1^{\circ} 20^{\circ}, 0$
29	5	10	10*	10*	10*	10.0	00.0	00.1	00	$\rightarrow 0^{\circ} 0^{\circ} 3^{\circ} 1^{\circ} 2^{\circ} 6^{\circ} 0^{\circ} 1^{\circ} 2^{\circ} 1^{\circ} 13^{\circ} 0^{\circ} 1^{\circ} 14^{\circ} 0^{\circ} 1^{\circ} 15^{\circ}, 0$
30	5	100	100	10	10.0	00.0	43.6	14	.	$\rightarrow 0^{\circ} 0^{\circ} 4^{\circ} 1^{\circ} 0^{\circ} 24^{\circ} 1^{\circ} 4^{\circ} 2^{\circ} 1^{\circ} 4^{\circ} 1^{\circ} 13^{\circ}, 0^{\circ} 0^{\circ} 7^{\circ} 6^{\circ} 0^{\circ} 1^{\circ} 13^{\circ} 0^{\circ} 1^{\circ} 14^{\circ}, 0$
31	6	100	10	09	09.7	01.7	13.8	08	.	$\rightarrow 0^{\circ} 1^{\circ} 6^{\circ} 1^{\circ} 19^{\circ} 2^{\circ} 4^{\circ}, 0^{\circ} 0^{\circ} 3^{\circ} 0^{\circ} 1^{\circ} 4^{\circ} 1^{\circ} 12^{\circ} 0^{\circ} 1^{\circ} 10^{\circ}, 0$

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1	7	10.0	10	10	10.0	00.0	05.7	04	= 0.3 ^o 10 ^o 13 ^o 9 ^o 2 ^o 3 ^o 9 ^o 14 ^o = -3 ^o 10 ^o 9 ^o 6 ^o 9 ^o , 田
2	7	10.0	10	10	10.0	00.0	00.1	.	= 5 ^o 14 ^o 14 ^o 5 ^o 6 ^o 13 ^o 15 ^o 16 ^o 15 ^o 8 ^o 00
3	7	10	09	09	04.3	01.8	00.0	.	= 5 ^o 10 ^o 13 ^o 15 ^o 22 ^o 15 ^o = 5 ^o 10 ^o 13 ^o 11 ^o 12 ^o 15 ^o , 0
4	6	10.0	10	10	10.0	00.0	04.6	.	= 5 ^o 10 ^o 4 ^o 5 ^o 9 ^o 6 ^o 24 ^o = 3 ^o 5 ^o 12 ^o 24 ^o
5	8	09	06	10	08.3	03.6	04.0	.	= 0-10 ^o 21-24 ^o ; = 0-2-2 ^o 1 ^o H ^o 4 ^o ; + 13 ^o 16 ^o 16 ^o 24 ^o , 0
6	7	08.0	10.0	10	09.3	00.0	32.3	.	• 1 ^o -2 ^o -5 ^o 7 ^o 24 ^o 0-6-5 ^o 31 ^o 13 ^o , 0
7	7	10 ^o	10	09	09.7	00.0	16.6	.	• 0-4 ^o 6 ^o 16 ^o 9 ^o 10 ^o 5 ^o 6 ^o 8 ^o 14 ^o 16 ^o 22 ^o ; = 0-6 ^o 8 ^o 22 ^o 24
8	8	10 ^o	04.0	06	04.7	00.1	03.7	.	= 5 ^o 10 ^o 9 ^o 10 ^o 22 ^o 11 ^o = 0-2 ^o 24 ^o , 0
9	8	09	09	09	09.0	01.7	00.0	.	• 6 ^o 9 ^o 16 ^o 15 ^o 10 ^o 11 ^o = 0-2 ^o 24 ^o , 0
10	7	09	10	10	09.7	00.3	02.0	.	= 0-2 ^o , 0-1-2 ^o 6 ^o 13 ^o 22 ^o ; = 4 ^o 9 ^o , 0
11	9	04.0	07.0	01	04.0	07.0	01.7	.	0
12	8	10	09.0	02	07.0	00.1	.	.	= 1 ^o 4 ^o 22 ^o 24 ^o ; - 4 ^o 7 ^o 00 8 ^o 9 ^o 13 ^o 14 ^o , 0
13	8	06.0	04.0	00	04.0	00.4	00.0	.	= 0-0-8 ^o , 0
14	8	09	03.0	00	04.7	00.0	.	.	= 0-1 ^o 4 ^o 10 ^o 2 ^o 5 ^o 00 8 ^o 10 ^o , 0
15	7	03.0	10	10	07.7	03.8	.	.	= 0-3 ^o , 0-19 ^o 19 ^o , 0
16	7	10.0	10	02	07.3	00.0	04.2	.	• 1 ^o -3 ^o 12 ^o 5 ^o 4 ^o 0
17	8	10 ^o	05.0	03	04.0	07.5	11.0	.	= 0 ^o 1 ^o 8 ^o 10 ^o = 1 ^o 8 ^o 0
18	7	01.0	04.0	01	02.0	12.0	.	.	= 20 ^o -5 ^o 10 ^o 5 ^o 4 ^o , 0
19	8	07	00.0	00	02.3	10.9	.	.	= 0-10 ^o 10 ^o 0
20	8	04.0	03.0	07	04.0	05.7	.	.	= 0-1 ^o 4 ^o 10 ^o 19 ^o 24 ^o , 0
21	7	09	07.0	06	07.3	03.6	.	.	• 0-9 ^o 6 ^o 10 ^o , 0
22	7	10	05.0	07	07.3	04.5	.	.	= 2 ^o 8 ^o 4 ^o 0
23	8	01.0	04.0	03	04.0	00.8	.	.	= 0-1 ^o 9 ^o 3 ^o 8 ^o , 0
24	7	02.0	04.0	03	03.0	10.2	.	.	= 0-2 ^o 9 ^o 20 ^o 24 ^o = 5 ^o 8 ^o 0
25	7	09	09	02	04.7	04.9	.	.	= 0-7 ^o 6 ^o 7 ^o 9 ^o 13 ^o 13 ^o , 0
26	8	08	09.0	02	06.3	05.7	00.0	.	• 2 ^o 8 ^o 3 ^o 14 ^o 4 ^o , 0
27	8	01.0	04.0	00	01.7	11.5	00.1	.	= 3 ^o 4 ^o 14 ^o 14 ^o 7 ^o , 0
28	8	00.0	02.0	00	00.7	12.0	.	.	= 0-1 ^o 4 ^o 20 ^o 24 ^o ; = 0-4 ^o 7 ^o , 0
29	7	00.0	00.0	00	00.0	12.0	.	.	= 0-0-9 ^o 27 ^o 24 ^o ; 0-5 ^o 4 ^o 0, 0
30	7	00.0	01.0	01	00.7	12.2	.	.	= 0-0-4 ^o , 0-4 ^o 6 ^o 0, 0

MES. **VR60.** **04.7** **04.4** **04.8** **04.6** **176.9** **86.6**

$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

Dn	Vzdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenih parov e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	740.1	741.6	742.7	10.2	17.0	14.2	13.9	19.4	09.0	03.2	06.3	07.0	07.5	89	48	62	66	SSE 1	ENE 1	SW 1	
2	742.7	739.6	739.6	06.4	21.1	12.3	13.0	22.3	03.1	-02.8	05.5	03.9	03.9	76	21	37	45	NNE 1	NNE 2	NE 1	
3	737.2	731.9	732.0	06.9	21.8	16.1	15.2	22.4	04.4	-01.8	05.4	05.7	06.3	73	29	46	49	NNE 1	SSE 2	ENE 2	
4	735.0	735.9	736.1	12.2	12.8	12.1	12.3	16.5	10.3	06.2	07.5	08.6	09.5	70	78	90	79	ENE 1	SE 2	S 1	
5	736.1	737.3	738.3	10.1	11.8	10.8	10.9	12.4	09.7	08.9	08.3	09.9	09.3	89	96	95	93	ENE 2	NE 1	NW 2	
6	737.6	737.1	736.1	10.4	14.0	12.8	12.5	19.3	09.8	08.3	09.0	08.7	09.5	95	73	86	85	ENE 1	NNE 1	NW 1	
7	735.3	734.5	733.0	11.3	17.6	16.6	15.5	20.1	11.2	10.4	09.7	11.8	12.1	97	76	86	87	NW 1	ENE 2	WWN 1	
8	730.0	730.3	730.5	12.8	16.4	13.0	13.8	18.2	11.4	11.8	09.8	08.5	07.4	88	61	66	72	SSW 2	SW 3	SW 2	
9	732.1	733.0	735.1	12.4	18.3	12.6	14.0	19.2	07.2	03.4	07.2	06.4	07.0	66	41	64	57	SM 2	SM 4	SW 2	
10	736.3	735.3	735.5	09.0	16.8	13.0	13.5	19.6	06.0	01.0	07.5	08.2	06.7	87	50	59	65	NE 1	SW 3	SW 1	
11	734.9	731.6	730.9	09.0	21.6	16.7	16.0	22.0	06.0	01.7	07.7	06.5	07.8	89	33	55	59	S 1	SW 2	SSW 2	
12	729.7	729.1	729.6	11.6	19.7	16.8	16.2	20.8	11.4	10.7	09.2	08.9	08.6	90	51	60	67	NW 1	ENE 2	NNW 2	
13	730.0	731.0	731.2	12.6	14.2	11.8	12.6	17.0	11.8	10.4	09.3	09.7	09.9	85	80	96	87	SSW 2	-	0	
14	730.3	728.4	730.0	10.6	24.4	14.8	16.2	24.6	10.2	10.6	09.4	09.6	11.2	98	42	89	76	S 1	NNE 3	ENE 1	
15	731.9	731.4	732.2	12.3	23.2	16.4	17.1	24.2	11.0	08.5	09.9	09.9	11.5	92	46	82	73	S 1	SSW 3	SSW 1	
16	733.9	732.3	733.3	12.0	24.8	18.6	18.5	26.1	11.1	10.2	10.2	09.1	08.4	97	39	52	63	ESE 1	NW 2	SSW 2	
17	735.4	735.3	737.0	13.4	25.1	19.0	19.1	27.1	09.7	05.0	09.0	06.8	08.9	78	29	54	54	ENE 1	S 2	SSW 2	
18	739.6	736.7	739.3	14.6	28.8	19.4	20.5	29.0	10.3	05.4	09.6	08.2	11.4	77	28	68	58	WWN 1	SE 2	NNE 1	
19	740.6	738.4	739.0	16.4	27.4	18.6	20.3	28.8	12.9	08.1	10.6	11.2	12.9	75	41	80	65	NNW 1	ESE 2	SM 1	
20	738.6	736.2	736.9	14.2	27.4	16.7	18.8	28.3	13.4	12.0	11.6	11.8	13.4	96	43	94	78	- 0	SE 2	SM 1	
21	737.8	736.1	736.6	14.3	25.4	16.2	18.0	26.0	13.6	08.7	11.6	11.7	11.2	95	48	81	75	SSW 1	E 3	WWN 3	
22	735.0	733.4	733.3	14.2	22.6	17.3	17.9	24.3	13.4	10.6	11.3	11.8	10.9	93	57	74	75	NNW 2	SW 2	S 1	
23	732.4	731.6	732.7	13.4	14.4	12.7	13.3	17.6	12.6	11.9	10.7	11.0	10.3	93	90	93	92	NW 1	NNE 2	NNE 1	
24	733.4	733.4	732.9	10.0	12.3	11.6	11.4	13.0	10.0	10.0	08.2	08.4	09.0	89	79	88	85	ESE 1	E 2	- 0	
25	732.4	732.4	733.0	12.2	20.7	15.0	15.7	21.2	10.5	10.5	09.5	09.0	10.6	89	49	83	74	NWW 1	SE 2	NNW 1	
26	734.7	734.7	735.3	14.4	17.6	14.8	15.4	18.6	13.8	09.6	10.7	10.2	11.2	87	68	89	81	ENE 1	ESE 2	S 1	
27	735.7	736.1	736.4	13.6	18.0	15.0	15.4	18.5	13.2	13.0	10.7	10.3	11.5	92	66	90	83	N 1	ESE 2	ENE 1	
28	736.4	736.0	736.6	14.7	22.5	15.4	17.0	22.7	13.2	11.0	11.0	10.9	12.2	88	53	93	78	ESE 1	E 3	SSE 1	
29	735.2	732.7	732.2	13.2	23.0	17.6	17.9	23.5	12.0	10.4	10.7	07.0	08.5	94	33	56	61	SSW 1	SW 3	MSW 3	
30	730.3	729.8	731.0	15.7	21.2	14.2	16.3	22.0	14.2	11.8	10.9	08.3	11.1	82	44	92	73	HWW 2	SW 3	MSW 3	
31	732.9	730.7	731.8	10.1	17.4	17.0	15.4	19.9	09.0	10.0	09.1	11.5	08.1	98	77	56	77	ENE 1	S 1	MSW 2	
MES.	VRED.	735.0	734.0	734.5	12.1	20.0	15.1	15.6	21.3	10.5	08.0	09.3	09.0	09.6	87	54	75	72	1.2	2.1	1.4

1	731.2	730.6	730.3	14.5	18.7	14.5	15.6	20.3	12.7	05.2	10.9	09.0	10.5	88	55	85	76	NE 1	SW 3	NW 2
2	731.2	731.5	732.0	08.1	09.6	09.5	09.2	14.7	08.0	06.2	07.5	08.4	08.4	92	94	94	93	ESE 2	NE 2	ENE 1
3	732.8	732.4	733.7	09.6	11.8	10.4	10.6	12.2	09.2	07.2	08.3	08.0	08.6	94	77	91	87	NNE 1	ESE 1	NNE 1
4	736.4	736.1	738.7	08.1	16.9	10.1	11.3	17.4	08.0	05.8	07.6	05.2	07.4	94	36	80	70	SW 2	ENE 2	N 1
5	740.9	739.8	741.2	07.2	17.7	10.9	11.7	18.7	04.8	-00.4	05.9	05.1	05.7	78	34	58	57	S 1	NE 2	N 1
6	742.0	740.4	740.7	09.1	19.0	13.2	13.6	20.2	04.6	-00.8	05.7	04.4	05.8	66	26	51	48	SSW 1	ENE 1	SE 1
7	739.9	737.7	737.6	07.4	19.2	15.3	14.3	19.6	04.6	-01.3	06.3	05.8	07.6	82	35	59	59	E 1	NE 1	ESE 1
8	735.3	734.1	734.6	10.2	14.4	12.0	12.2	16.0	06.0	02.9	08.1	09.7	09.8	87	79	93	86	ENE 1	NE 1	SW 1
9	733.0	731.2	732.5	11.2	20.3	14.2	15.0	21.2	09.8	07.2	08.6	08.4	08.9	86	47	73	69	SE 1	S 1	3 S 1
10	732.1	733.3	734.2	13.2	18.4	14.0	14.9	18.6	12.3	09.2	10.2	10.6	11.1	89	67	93	83	N 1	NE 1	- 0
11	736.8	736.6	737.6	12.4	21.4	15.7	16.3	21.5	11.3	09.5	10.1	11.0	11.9	93	58	89	80	NNE 1	ENE 2	NNE 1
12	738.1	737.5	737.4	12.7	20.1	17.2	16.8	21.9	11.8	07.8	10.8	12.7	13.1	98	72	89	86	E 1	NNW 2	S 1
13	736.9	734.5	734.5	16.0	25.4	19.4	20.1	26.7	14.7	12.3	11.8	11.0	13.2	86	45	78	70	ENE 1	S 2	NNW 1
14	734.9	733.2	733.6	15.6	28.9	20.4	21.3	30.3	14.1	09.7	12.6	10.7	11.6	95	34	65	65	NNE 1	S 1	SN 1
15	733.9	731.8	731.7	16.2	27.8	21.0	21.5	28.2	13.2	09.2	11.3	12.2	11.6	82	44	62	63	NNE 1	WSW 2	W 1
16	731.5	730.4	730.4	16.8	20.6	16.6	17.7	23.1	15.3	13.4	12.6	13.8	12.0	87	76	85	83	NE 1	ENE 2	E 1
17	731.7	732.3	733.1	15.7	16.8	15.3	15.8	19.0	15.2	13.2	12.2	13.3	12.3	91	92	94	92	- 0	E	

BR. ST. 13

$$H_g = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

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$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

D S	Vzdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	730.3	732.0	732.8	14.6	15.4	15.3	14.2	16.2	09.6	06.4	05.1	05.7	08.7	41	44	76	54	NNW 5	NNW 3	SSW 2
2	730.7	731.3	732.4	14.0	17.1	16.1	15.8	20.8	12.2	10.9	09.1	11.8	11.4	76	80	83	80	NNW 2	NNE 1	ENE 1
3	734.2	734.4	735.4	19.3	26.6	19.3	21.1	26.8	14.8	10.3	10.2	08.3	12.2	61	32	72	55	SW 1	S 2	NNW 1
4	733.9	731.7	732.0	16.1	26.6	17.2	19.3	27.0	13.0	08.6	12.3	11.0	12.7	89	42	86	72	NE 1	SM 3	SSM 2
5	730.6	730.5	732.3	15.6	23.6	16.4	19.1	24.6	14.6	11.9	11.7	11.3	12.1	88	52	75	72	NE 1	SE 1	NW 1
6	733.4	733.4	736.3	15.6	26.7	17.1	19.1	26.8	14.8	09.0	12.5	11.3	12.6	94	43	86	74	NE 1	ENE 2	NW 1
7	738.1	737.0	737.5	14.9	26.2	20.9	20.9	27.0	14.0	11.2	11.7	10.4	13.4	92	42	74	69	NW 1	SE 1	NW 1
8	738.0	736.7	737.1	16.6	26.0	22.7	22.5	28.7	14.0	10.3	12.3	13.4	12.6	87	48	61	65	NE 1	SM 2	SM 2
9	737.3	736.1	737.8	18.2	29.1	21.2	22.6	30.0	16.0	12.1	13.5	13.2	11.9	86	42	63	64	E 1	SW 2	NE 1
10	737.3	735.0	736.9	18.0	26.0	17.6	20.3	28.4	15.6	12.0	13.3	15.4	13.3	86	54	88	76	NNW 1	ENE 2	NNL 1
11	736.8	735.3	734.6	15.8	27.0	21.7	21.6	27.7	15.0	12.7	12.1	15.1	14.7	90	56	76	74	NW 1	ESE 2	NW 2
12	734.2	735.3	736.8	15.3	17.4	17.0	16.7	21.8	15.2	14.0	12.4	13.2	14.0	95	89	96	93	NNW 2	S 1	SE 1
13	738.6	736.5	739.3	14.8	26.6	20.5	20.6	27.1	14.2	10.4	12.2	11.6	14.4	97	44	80	74	SW 1	SE 1	NE 1
14	740.0	738.4	738.3	17.6	29.3	23.0	23.2	29.8	15.4	12.8	13.1	12.1	16.5	87	39	79	68	NE 1	SSW 1	ENE 1
15	738.1	736.4	736.3	17.7	31.4	25.0	24.8	32.0	17.3	13.9	14.2	16.8	15.8	93	49	67	70	ENE 1	WSW 2	SSW 2
16	735.9	734.0	735.3	21.1	23.2	18.8	20.5	27.3	18.2	16.4	14.1	16.3	15.5	75	76	95	82	NW 2	SW 2	NNE 1
17	735.2	734.1	734.8	19.2	26.4	19.8	21.3	27.4	17.6	15.2	14.9	14.9	15.2	89	58	88	78	NW 1	NE 1	W 3
18	734.6	732.6	731.3	18.4	29.6	22.9	23.5	31.1	16.3	13.5	13.2	11.7	15.5	83	57	74	71	E 1	ENE 2	SSW 1
19	730.4	733.1	734.7	20.8	24.6	20.7	21.7	26.1	18.8	16.3	15.3	10.7	12.9	83	46	70	66	NNE 1	E 1	ENE 1
20	736.2	735.2	734.9	16.5	25.8	19.2	20.2	26.3	13.9	10.3	10.8	08.5	14.0	76	34	84	63	NNE 1	E 2	NE 1
21	734.7	732.8	734.5	16.0	26.8	18.6	20.0	27.0	13.0	09.8	11.5	12.7	12.9	85	48	80	71	E 1	N 2	NW 2
22	735.2	734.4	734.9	16.1	24.6	17.4	18.9	25.4	15.2	10.0	12.5	12.6	13.5	91	54	91	79	NNW 1	E 2	SM 1
23	735.6	734.0	733.9	15.5	26.6	20.6	20.8	27.6	14.2	10.2	12.2	11.3	14.5	92	43	80	72	SE 1	ESE 2	SSM 1
24	733.7	732.2	732.2	16.2	27.7	20.8	21.4	27.8	15.8	12.3	13.4	12.4	13.4	97	45	73	72	NNE 1	NW 3	SW 2
25	733.6	734.3	738.2	15.0	17.0	13.0	14.5	21.0	12.9	14.8	12.1	10.9	10.4	95	75	92	87	ESE 1	ESE 2	NW 1
26	740.5	739.9	740.7	10.4	22.1	15.6	16.0	22.3	10.2	08.6	09.4	08.0	10.3	98	40	78	72	NE 1	SSE 2	ENE 1
27	741.3	739.2	738.8	11.8	22.3	16.9	17.0	23.5	09.8	05.9	09.0	08.2	10.3	87	41	71	66	E 1	ESE 3	NNE 1
28	739.4	737.7	738.4	11.6	24.8	18.4	18.3	25.8	10.1	06.1	09.8	08.9	11.9	95	38	75	69	NE 1	NNE 1	NNW 1
29	739.0	736.9	738.1	15.2	26.8	16.2	18.6	27.9	12.7	09.0	11.3	11.2	12.3	87	42	59	63	NE 1	SE 2	ENE 3
30	738.0	736.9	736.5	16.4	25.0	18.4	19.6	26.4	15.2	12.9	12.1	11.2	14.0	87	47	88	74	N 1	ENE 2	SW 1
31	738.6	737.8	739.6	14.8	26.4	19.3	20.0	27.9	13.4	09.9	11.6	11.4	13.3	92	44	79	72	SSE 1	NE 1	NNW 2
MES. MRED.	735.9	735.1	735.9	16.1	25.1	18.9	19.8	26.3	14.3	11.2	11.9	11.9	13.1	86	50	79	72	1.2	1.8	1.6

1	740.0	738.6	739.1	15.5	27.0	20.6	20.9	27.8	13.6	09.5	11.8	10.6	15.4	89	40	85	71	NE 1	SE 1	NE 1
2	740.2	740.8	740.8	16.8	27.8	20.6	21.5	27.8	15.6	11.2	13.0	12.2	12.5	90	43	69	67	SE 1	SSE 1	E 2
3	741.4	741.1	741.1	17.8	24.4	20.8	21.0	25.4	16.7	13.8	12.6	12.8	12.5	83	56	60	69	NE 1	SE 2	E 1
4	740.9	738.7	740.0	15.0	27.4	16.6	18.9	28.1	13.8	10.3	11.2	12.4	12.1	88	45	86	73	NE 1	SE 3	SSE 2
5	739.3	737.5	738.5	14.4	25.2	19.4	19.6	25.6	13.8	10.3	11.7	10.1	13.1	95	42	77	71	NNE 1	E 1	NNW 2
6	739.2	739.4	740.6	15.3	26.0	18.6	19.6	26.1	13.8	09.5	12.3	11.6	12.8	94	46	80	73	E 1	ESE 3	W 1
7	741.2	739.1	739.8	16.2	26.3	16.6	18.9	26.6	14.5	10.6	12.2	13.2	13.3	88	51	94	78	ENE 1	NNE 2	SE 1
8	738.8	738.7	738.1	15.3	20.2	17.5	17.6	22.6	14.9	10.8	11.7	14.6	12.9	90	82	86	86	W 1	NE 2	W 1
9	737.9	736.8	737.2	14.4	25.0	18.8	19.3	25.7	14.1	10.9	11.8	13.3	14.7	96	56	90	81	SM 1	SE 2	SH 1
10	738.0	737.4	737.9	15.7	27.2	20.1	20.8	27.3	15.0	11.2	13.1	13.2	15.3	98	49	87	78	S 1	E 2	N 1
11	738.2	736.5	735.9	16.5	27.6	20.8	21.4	27.8	13.5	11.5	13.9	13.8	14.1	99	50	77	75	NE 1	ESE 2	NNW 2
12	734.5	733.3	733.0	17.6	19.0	17.6	18.0	23.5	16.8	15.9	13.3	14.9	13.8	88	90	92	90	W 1	SSW 2	SM 1
13	732.6	734.0	735.6	15.9	21.7	19.0	18.9	23.3	15.7	11.8	12.7	12.5	14.7	94	64	89	82	SSM 1	SE 1	NNW 2
14	737.4	737.3	737.5	16.8	23.6	19.1	19.7	24.1	16.1	12.6	13.5	11.7	13.8	94	54	83	77	NE 1	ENE 1	NE 1
15	737.4	735.3	734.9	15.3	26.5	21.2	21.1	26.9	14.6	10.7	12.4	13.6	11.8	95	52	63	70	SE 1	SSM 3	SH 3
16	734.6	734.9	735.0	16.4	19.3	17.9	17.9	21.6	15.5	11.8	12.8	14.6	14.2	91	87	93	90	SSE 1	SE 2	NW 1
17	735.6	733.7	734.4	15.3	25.0	17.4	18.8	27.2	15.3	12.1	12.3	12.5	13.6	93	53	92	79			

OR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Výška 0-9	Obločnosť N (0-10)					Inzolačia boj	Padavina R mm	Snežný pokriva- k cm		Rezervy vremena w
		14	7	14	21	Sred Dies					
1	8	10 e	10	10	10.0	00.0	70.5	.	.	$\begin{array}{l} +0-2^{\circ} 6-7^{\circ} 23^{\circ} 24^{\circ} = 1^{\circ} 3^{\circ} 8^{\circ} 7^{\circ} 25^{\circ} 10^{\circ} / F 8^{\circ} 12^{\circ} \\ +0-4^{\circ} 6-7^{\circ} 20^{\circ} 24^{\circ}, 0 \end{array}$	
2	8	10 e	10	05	08.3	00.6	62.4	.	.	$\begin{array}{l} +0-9^{\circ} 6-20^{\circ} 24^{\circ} \\ +2^{\circ} 0-8^{\circ} 50^{\circ} = 4^{\circ} 6^{\circ} 19^{\circ} 19^{\circ} 19^{\circ} 19^{\circ} 20^{\circ} 20^{\circ} 17^{\circ} 19^{\circ} 20^{\circ} 20^{\circ} 20^{\circ} 22^{\circ} \\ = 4^{\circ} 7^{\circ} 5^{\circ} = 4^{\circ} 6^{\circ} 17^{\circ} \end{array}$	
3	8	01 0	02 0	02	01.7	13.9	00.9	.	.		
4	8	00 0	02 0	10 e	04.0	10.9	.	.	.		
5	7	07 0	06 0	09	07.3	04.9	02.6	.	.		
6	7	09	04 0	09	07.3	07.8	01.9	.	.	$\begin{array}{l} +0-0^{\circ} 10^{\circ} = 1^{\circ} 2^{\circ} 6^{\circ} 9^{\circ} 22^{\circ} 24^{\circ} = 2^{\circ} 6^{\circ} T^{\circ} 15^{\circ} 17^{\circ} 15^{\circ} 16^{\circ} 17^{\circ} 16^{\circ} \\ = 0-0^{\circ} 8^{\circ} 6^{\circ} 17^{\circ} 23^{\circ} 24^{\circ} = 1^{\circ} 2^{\circ} 8^{\circ} 8^{\circ} 20^{\circ} 24^{\circ} \\ = 2^{\circ} 0-10^{\circ} 22^{\circ} 24^{\circ} = 0-0^{\circ} 8^{\circ} 6^{\circ} 17^{\circ} 21^{\circ} 0 \end{array}$	
7	8	10 =	01 0	01	04.0	09.5	01.6	.	.		
8	7	00 0	02 0	00	00.7	12.6	.	.	.		
9	7	00 0	02 0	09	03.7	10.5	.	.	.		
10	7	02 0	05 0	10 e	05.7	09.0	.	.	.	$\begin{array}{l} +0-0^{\circ} 10^{\circ} = 3^{\circ} 9^{\circ} 10^{\circ} 9^{\circ} 17^{\circ} \\ = 0-0^{\circ} 10^{\circ} = 3^{\circ} 9^{\circ} 10^{\circ} 9^{\circ} 17^{\circ} \end{array}$	
11	7	10	01 0	10	07.0	07.4	04.0	.	.	$\begin{array}{l} +0-4^{\circ} 1^{\circ} 2^{\circ} 24^{\circ} = 0-4^{\circ} 5^{\circ} 5^{\circ} 6^{\circ} 22^{\circ} 24^{\circ} \\ = 0-0^{\circ} 5^{\circ} 0-13^{\circ} 6^{\circ} 7^{\circ} 0^{\circ} 5^{\circ} 6^{\circ} 5^{\circ} 7^{\circ} 2^{\circ} 0^{\circ} 2^{\circ} 20^{\circ} ; 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} \end{array}$	
12	7	10 e	10	10	10.0	00.0	17.4	.	.	$\begin{array}{l} = 0-4^{\circ} 6^{\circ} 6^{\circ} 7^{\circ} 4^{\circ} 6^{\circ} 6^{\circ} 0 \\ = 0-8^{\circ} 8^{\circ} 21^{\circ} 24^{\circ} - 4^{\circ} 10^{\circ} 23^{\circ} 24^{\circ} 00 10^{\circ} 14^{\circ} 0 \end{array}$	
13	8	06 0	03 0	00	03.0	11.6	07.5	.	.	$\begin{array}{l} +0-0^{\circ} 8^{\circ} 20^{\circ} 24^{\circ} - 0-3^{\circ} 8^{\circ} 10^{\circ} 4^{\circ} = 3^{\circ} 8^{\circ} 10^{\circ} 4^{\circ} 6^{\circ} 20^{\circ} 24^{\circ} \\ = 0-1^{\circ} 8^{\circ} T^{\circ} 12^{\circ} \end{array}$	
14	7	00 0	01 0	00	00.3	13.4	.	.	.	$\begin{array}{l} = 0-9^{\circ} 8^{\circ} 10^{\circ} 21^{\circ} 24^{\circ} \\ = 0-0^{\circ} 8^{\circ} 20^{\circ} 24^{\circ} - 0-3^{\circ} 8^{\circ} 10^{\circ} 4^{\circ} = 3^{\circ} 8^{\circ} 10^{\circ} 4^{\circ} 6^{\circ} 20^{\circ} 24^{\circ} \end{array}$	
15	7	10 =	01 0	03	04.7	10.5	.	.	.		
16	7	08 0	10 e	10	09.3	09.2	.	.	.	$\begin{array}{l} +0-1^{\circ} 0^{\circ} 8^{\circ} T^{\circ} 12^{\circ} \\ = 0-9^{\circ} 6^{\circ} 0^{\circ} \end{array}$	
17	8	07 0	08 0	05	06.7	08.4	34.1	.	.	$\begin{array}{l} = 5-7^{\circ} 6^{\circ} 0^{\circ} 1^{\circ} 2^{\circ} 24^{\circ} \\ = 0-7^{\circ} 7^{\circ} 2^{\circ} 21^{\circ} 24^{\circ} = 2^{\circ} 8^{\circ} 8^{\circ} T^{\circ} 6^{\circ} 7^{\circ} 17^{\circ} 0^{\circ} 0^{\circ} 1^{\circ} 7^{\circ} 8^{\circ} 8^{\circ} 6^{\circ} 22^{\circ} 20^{\circ} \end{array}$	
18	7	03 0	01 0	00	01.3	11.7	02.3	.	.	$\begin{array}{l} = 0-1^{\circ} 2^{\circ} 21^{\circ} 24^{\circ} = 2^{\circ} 8^{\circ} 8^{\circ} T^{\circ} 6^{\circ} 7^{\circ} 17^{\circ} 0^{\circ} 0^{\circ} 1^{\circ} 7^{\circ} 8^{\circ} 8^{\circ} 6^{\circ} 22^{\circ} 20^{\circ} \\ = 0-1^{\circ} 2^{\circ} 21^{\circ} 24^{\circ} = 2^{\circ} 8^{\circ} 8^{\circ} T^{\circ} 6^{\circ} 7^{\circ} 17^{\circ} 0^{\circ} 0^{\circ} 1^{\circ} 7^{\circ} 8^{\circ} 8^{\circ} 6^{\circ} 22^{\circ} 20^{\circ} \end{array}$	
19	8	10 e	02 0	04	05.3	09.4	.	.	.		
20	8	01 0	04 0	00	01.7	12.9	16.0	.	.		
21	8	01 0	09 e	10 e	06.7	09.3	.	.	.	$\begin{array}{l} +0-0^{\circ} 8^{\circ} 3^{\circ} 2^{\circ} 15^{\circ} 20^{\circ} 23^{\circ} T^{\circ} 13^{\circ} 15^{\circ} 15^{\circ} 15^{\circ} 20^{\circ} 23^{\circ} 1^{\circ} 1^{\circ} \\ +0-0^{\circ} 2^{\circ} 1^{\circ} 4^{\circ} 5^{\circ} 8^{\circ} T^{\circ} 6^{\circ} 7^{\circ} 17^{\circ} \end{array}$	
22	8	06 0	08 0	02	06.0	07.5	28.3	.	.	$\begin{array}{l} = 1^{\circ} 2^{\circ} 4^{\circ} 5^{\circ} 10^{\circ} = 0-1^{\circ} 2^{\circ} 4^{\circ} 5^{\circ} 3^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 2^{\circ} 4^{\circ} 0 \\ = 0-0^{\circ} 4^{\circ} 0^{\circ} 0^{\circ} 2^{\circ} 4^{\circ} 8^{\circ} - 10^{\circ} 8^{\circ} 10^{\circ} 2^{\circ} 0^{\circ} 10^{\circ} 24^{\circ} 15^{\circ} 23^{\circ} 24^{\circ} \end{array}$	
23	7	10	01 0	01	04.0	10.7	02.8	.	.		
24	7	10 =	03 0	06	06.3	09.4	.	.	.		
25	7	10 e	10	10	10.0	00.0	40.4	.	.		
26	8	10 e	03 0	00	04.3	10.4	09.1	.	.	$\begin{array}{l} +0-0^{\circ} 7^{\circ} 7^{\circ} 9^{\circ} 0^{\circ} \\ +0-0^{\circ} 10^{\circ} 20^{\circ} 24^{\circ} \end{array}$	
27	8	04 0	01 0	00	01.7	12.8	.	.	.	$\begin{array}{l} +0-1^{\circ} 2^{\circ} 0^{\circ} 9^{\circ} 0^{\circ} 20^{\circ} 24^{\circ} = 3^{\circ} 11^{\circ} = 0-1^{\circ} 2^{\circ} 0^{\circ} 9^{\circ} 0^{\circ} 20^{\circ} 24^{\circ} \\ +0-2^{\circ} 0^{\circ} 9^{\circ} 0^{\circ} 20^{\circ} 24^{\circ} = 3^{\circ} 11^{\circ} = 0-1^{\circ} 2^{\circ} 0^{\circ} 9^{\circ} 0^{\circ} 20^{\circ} 24^{\circ} \end{array}$	
28	7	00 0 =	01 0	00	00.3	12.3	.	.	.		
29	7	00 0	01 0	10 e	03.7	12.0	.	.	.		
30	7	03 0	06 0	03	04.0	08.9	06.0	.	.		
31	8	09 0	07	09	08.3	08.4	02.0	.	.	$\begin{array}{l} = 4^{\circ} 3^{\circ} 10^{\circ} 2^{\circ} 0^{\circ} \\ = 4^{\circ} 3^{\circ} 5^{\circ} 6^{\circ} 0^{\circ} \end{array}$	
MES.	VRED.	05.8	04.4	05.1	05.1	271.9	251.6				

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1	8	01○	03○	01	01.7	10.5	02.6	.	= ^{3°} _{0°} ^{9.5°} _{0°} ^{9.5°} ₁₃ , ^{-1°} _{0°} ^{20.5°} _{24,0}
2	7	03○	03○	02	02.7	C9.8	.	.	^{-1°} _{0°} ^{9.5°} _{0°} ^{9.5°} _{24,0}
3	7	00○	08○	02	03.3	10.1	.	.	^{0°} _{20.5°} ^{9.5°} _{24,0}
4	7	01○	05	06●	04.0	10.5	.	.	^{0°} _{20.5°} ^{9.5°} _{24,0}
5	7	10≡	06○	01	05.7	07.8	06.6	.	^{0°} _{20.5°} ^{9.5°} _{24,0}
6	7	03○	08○	00	03.7	10.7	C0.1	.	= ^{0°} _{0°} ^{8.5°} _{0°} ^{8.5°} _{12.0°} , ^{-1°} _{0°} ^{20.5°} _{24,0}
7	7	01○	08●R	03	04.0	08.6	01.5	.	^{0°} _{0°} ^{8.5°} _{0°} ^{8.5°} _{12.5°} , ^{-1°} _{0°} ^{20.5°} _{24,0}
8	7	09	09●R	09	09.0	C3.3	08.8	.	^{0°} _{0°} ^{8.5°} _{0°} ^{8.5°} _{12.5°} , ^{-1°} _{0°} ^{20.5°} _{24,0}
9	7	10≡	07○	03	06.7	05.8	02.0	.	= ^{0°} _{3.5°} ^{9.5°} _{0°} ^{9.5°} _{12-20.5°} , ^{14.5°} _{14.5°} , ^{14.5°} _{14.5°}
10	7	10≡	04○	04	06.0	09.1	00.6	.	= ^{0°} _{3.5°} ^{9.5°} _{0°} ^{9.5°} _{12-20.5°} , ^{14.5°} _{14.5°} , ^{14.5°} _{14.5°}
11	7	10≡	08○	00	06.0	06.5	.	.	^{4°} _{0°} ^{10.5°} _{0°} ^{10.5°} _{12.0°} , ^{-1°} _{0°} ^{20.5°} _{24,0}
12	7	05○	10●R	10	08.3	03.7	17.4	.	^{0°} _{0°} ^{10.5°} _{0°} ^{10.5°} _{12.5°} , ^{-1°} _{0°} ^{20.5°} _{24,0}
13	7	10○	04○	09	04.3	05.8	05.8	.	= ^{0°} _{3.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
14	7	09○	02○	07	06.0	07.9	03.5	.	= ^{0°} _{3.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
15	7	10≡	02○	00	04.0	08.4	.	.	= ^{0°} _{4.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
16	6	10●R	06○	03	07.3	01.6	00.6	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
17	8	09	02○	01	04.0	06.1	16.2	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
18	6	10≡	09	10	06.7	01.5	02.2	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
19	8	05○	05○	00	03.3	10.4	04.3	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
20	8	06○	01○	00	02.3	12.0	.	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
21	7	08○	02○	00	03.3	11.6	.	.	^{4°} _{2.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
22	7	04○	01○	06	03.7	09.8	.	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
23	7	04○	05○	05	04.7	09.2	.	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
24	6	09	10	10	06.7	00.0	.	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
25	7	09	07	10●	08.7	00.6	16.4	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
26	7	10○	08○	07	08.3	02.5	08.2	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
27	8	04○	07○	09	06.7	11.2	00.3	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
28	7	09	10	10	09.7	00.3	00.6	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
29	6	10○	08	10	06.3	00.1	02.4	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
30	7	10	09○	10●	06.7	05.2	04.8	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}
31	7	09○	05	00	04.7	07.3	C5.4	.	^{0°} _{1.5°} ^{12.5°} _{0°} ^{12.5°} _{24,0}

$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	737.5	737.5	737.9	14.2	25.4	18.0	18.9	26.1	14.2	12.2	11.4	11.4	14.0	94	47	91	77	S 1	SSE 1	NNE 1	
2	738.2	736.7	735.7	15.4	25.2	18.7	19.3	25.4	14.8	11.9	12.7	13.2	14.7	97	55	91	81	SSE 1	ESE 2	NE 1	
3	734.1	733.9	732.8	16.2	19.4	16.8	17.3	20.6	16.0	12.6	13.7	14.8	13.5	99	88	94	94	- 0	W 2	W 1	
4	733.7	733.6	734.0	13.8	25.3	17.7	18.6	25.8	13.3	11.5	11.5	12.4	14.2	97	51	93	80	NNE 1	SSE 2	N 1	
5	734.0	733.0	734.9	14.6	25.2	17.4	18.7	26.1	14.6	11.8	11.8	12.0	13.5	95	50	91	79	S 1	WSW 2	NW 2	
6	736.0	735.6	736.1	14.2	25.4	18.6	19.2	25.4	13.6	10.8	11.6	12.8	14.2	96	52	88	79	NE 1	SW 1	SW 1	
7	734.9	734.4	736.7	15.2	20.5	16.7	17.3	20.6	15.0	13.3	12.3	13.3	13.3	95	73	93	87	ESE 1	SE 1	ESE 1	
8	740.3	740.8	741.8	14.9	21.1	15.6	16.8	21.7	14.7	12.7	12.1	10.3	11.2	95	55	84	78	SW 1	SE 2	NNE 1	
9	741.4	739.3	739.1	12.4	21.7	15.8	16.4	22.7	11.6	09.1	10.3	09.9	12.0	96	51	89	79	E 1	ESE 1	NE 1	
10	738.8	737.3	737.0	12.2	23.1	16.2	16.9	24.2	11.8	07.9	10.4	11.7	12.6	98	55	91	81	NNE 1	ENE 1	NNE 1	
11	735.9	734.9	734.2	13.7	20.5	17.1	17.1	20.9	13.6	09.4	11.3	12.0	13.8	96	66	94	85	ENE 1	SSE 2	W 1	
12	732.2	731.6	730.8	16.0	23.4	14.4	17.1	23.5	14.4	14.4	13.1	10.5	10.7	96	48	87	77	ESE 1	SW 3	E 1	
13	733.4	737.4	730.4	11.8	12.0	11.5	11.7	14.7	11.0	10.4	07.3	08.6	08.7	72	81	85	79	NNW 3	NNW 2	NNW 1	
14	736.8	734.4	733.9	09.3	18.1	15.1	14.4	18.2	08.3	05.0	08.6	09.9	12.0	98	63	93	85	NNW 1	ESE 1	NNW 1	
15	734.7	734.9	737.8	13.0	22.9	16.4	17.2	23.4	12.9	08.8	10.9	12.5	13.2	97	60	94	84	W 1	NNE 1	NNE 1	
16	742.0	743.0	744.1	15.1	27.7	19.6	20.5	28.3	14.9	11.2	12.5	16.0	15.4	97	57	90	81	NNE 1	SE 2	NNE 2	
17	745.1	744.6	745.0	15.0	28.4	20.6	21.2	30.0	14.9	11.4	12.4	13.4	16.2	97	48	93	79	ENE 1	NE 1	NNE 1	
18	745.0	743.2	743.3	17.1	27.7	19.8	21.1	27.8	16.7	13.1	13.8	15.5	14.9	94	56	86	79	NNW 2	SE 2	E 1	
19	742.6	741.8	742.7	15.1	25.1	15.8	18.0	25.1	14.6	10.6	12.6	11.0	12.1	98	46	90	78	NNE 1	ESE 2	NNE 1	
20	742.3	740.9	741.9	12.3	24.2	14.7	16.5	24.6	11.6	06.7	10.5	10.7	11.0	98	47	88	78	ENE 1	ENE 2	NNW 1	
21	742.4	741.4	742.6	11.4	24.1	15.4	16.6	24.6	10.3	03.8	09.9	10.3	11.9	98	46	91	78	ENE 1	SE 2	ENE 1	
22	744.4	744.5	745.3	12.4	24.4	16.1	17.3	24.4	11.7	05.6	10.4	12.0	12.6	97	52	92	80	N 1	ESE 2	NNE 1	
23	745.0	743.2	742.6	12.8	23.0	16.2	17.1	23.1	12.5	07.7	10.4	11.0	13.0	93	52	94	80	NNE 1	ENE 2	SW 1	
24	741.7	739.6	739.4	13.8	21.7	17.0	17.4	23.8	13.6	09.1	11.6	13.2	11.4	98	68	79	82	NNW 1	NE 1	SSW 1	
25	737.8	736.0	735.4	12.4	22.8	17.5	17.6	23.6	12.3	08.4	10.6	10.7	12.4	98	52	82	77	NNE 1	SW 3	SW 2	
26	732.8	732.0	734.2	17.0	20.1	15.2	16.9	21.8	15.0	09.9	12.2	10.4	12.0	84	59	93	79	SW 3	SW 3	SSE 1	
27	738.5	740.2	740.7	14.9	19.0	15.3	16.1	20.6	14.6	13.5	11.8	11.2	12.4	93	68	95	85	NNE 1	ESE 1	SSE 1	
28	740.7	741.7	742.3	16.7	23.8	19.4	20.3	25.1	15.1	10.1	12.7	12.5	11.6	79	56	68	68	SW 3	SW 3	SW 2	
29	741.9	740.7	741.9	12.7	26.2	17.0	18.2	26.9	12.4	08.1	10.4	12.6	12.9	95	50	89	78	E 1	SSW 2	SSW 1	
30	740.5	737.8	737.7	14.2	23.7	18.2	18.6	24.6	13.9	07.9	11.9	14.0	14.8	98	64	94	85	NNE 1	NW 1	NNW 1	
MES.																					
VR.ED.	738.8	736.2	738.7	14.1	23.0	16.8	17.7	23.8	13.5	10.0	11.4	12.0	12.9	95	57	89	80	1.2	1.8	1.1	

1	738.1	738.1	738.9	16.6	22.9	18.0	18.9	24.0	16.0	15.7	12.9	12.2	14.3	91	58	93	81	SSW 1	SSW 1	ENE 1
2	739.5	740.7	742.1	15.3	23.6	15.6	17.5	23.9	15.2	11.5	12.9	11.9	12.2	99	54	92	82	NE 1	ENE 2	NNE 1
3	741.5	739.4	739.5	13.2	23.8	15.2	16.9	24.4	13.2	09.4	11.1	09.8	11.7	98	44	90	77	ENE 1	W 1	NNW 1
4	741.3	740.4	741.2	12.7	19.2	14.0	15.0	20.0	12.4	07.4	10.7	08.3	10.0	97	50	84	77	N 2	E 2	ESE 1
5	743.3	742.9	744.1	09.1	17.1	09.3	11.2	17.1	08.6	03.4	08.3	06.8	07.8	96	47	89	77	ENE 1	ESE 2	N 1
6	744.8	743.7	743.8	07.7	19.0	10.2	11.8	20.2	06.4	01.2	07.3	07.8	08.5	92	47	91	77	NME 1	SSE 2	NNE 1
7	741.6	738.7	738.6	07.1	20.4	12.4	13.1	21.0	07.1	04.2	07.4	08.2	08.4	97	46	77	73	ENE 1	SW 2	S 1
8	740.1	738.7	738.3	08.0	18.8	11.1	12.3	19.7	07.4	01.9	07.8	05.9	08.2	97	36	83	72	NNE 1	SE 1	NNE 1
9	737.5	736.3	736.6	09.6	13.0	06.3	08.8	13.6	06.0	07.0	06.3	05.4	06.6	71	48	92	70	ENE 1	SSE 2	NE 1
10	734.9	733.7	734.1	06.4	12.2	07.4	08.4	13.0	06.0	02.5	06.8	05.7	06.0	95	53	78	75	NME 1	SE 2	ENE 3
11	735.3	737.5	739.5	05.7	06.8	05.4	05.8	07.6	05.4	05.2	05.6	05.9	06.3	82	79	94	85	E 2	NE 2	NE 2
12	740.0	739.4	739.1	05.6	05.6	03.2	04.4	06.4	03.0	04.5	05.3	06.0	05.6	78	87	97	87	NE 2	ENE 3	SSW 1
13	735.9	732.0	731.3	04.2	07.6	07.2	06.6	08.1	03.0	03.0	06.0	06.7	07.1	97	86	93	92	NNW 1	SE 1	NW 1
14	730.6	733.0	734.5	07.1	09.0	07.4	07.7	10.0	06.8	05.0	07.3	07.9	07.2	96	91	93	93	NNE 1	W 1	SE 1
15	736.0	736.0	737.3	07.2	13.1	06.9	08.5	14.7	06.6	05.4	07.0	06.7	07.2	92	59	96	82	W 1	ENE 2	NNW 1
16	735.8	734.4	731.7	04.7	08.0	08.4	07.4	08.7	04.0	03.4	06.2	07.4	08.1	97	92	97	95	E 1	NNE 1	NW 1
17	726.1	724.6	726.8	06.7	10.6	09.2	09.4	11.1	08.2	08.0	08.1	08.5	08.1</td							

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Inzolacija broj seti	Padavine R mm	Snežni pokriva- h cm		Razvoj vremena		
		14	7	14	21	Sred Dies					7	7	w
1	7	10	—	06	00	05.3	08.6	.	.				
2	7	10	—	06	05	07.0	04.9	.	.				
3	6	10	—	10	09	09.7	01.1	00.0	.				
4	6	08	—	03	00	03.7	08.5	05.3	.				
5	7	10	—	04	09	07.7	03.3	.	.				
6	7	10	—	06	07	07.7	06.4	00.2	.				
7	7	07	—	09	10	08.7	00.8	16.6	.				
8	7	10	—	09	00	06.3	03.9	02.9	.				
9	7	10	—	01	00	03.7	08.6	.	.				
10	7	10	—	01	01	04.0	07.3	.	.				
11	7	10	—	10	10	10.0	01.6	.	.				
12	7	09	—	05	05	06.3	06.2	09.7	.				
13	8	09	—	10	09	09.3	00.1	04.9	.				
14	7	10	—	07	07	08.0	02.3	02.3	.				
15	7	10	—	08	05	07.7	02.0	00.1	.				
16	7	10	—	08	00	06.0	06.5	00.0	.				
17	7	10	—	00	00	03.3	08.5	.	.				
18	7	09	—	01	01	03.7	07.6	.	.				
19	7	10	—	01	01	04.0	07.8	.	.				
20	7	10	—	01	00	03.7	08.3	.	.				
21	7	10	—	01	00	03.7	07.8	.	.				
22	6	10	—	02	00	04.0	07.3	.	.				
23	6	10	—	00	00	03.3	04.0	.	.				
24	5	10	—	00	00	03.3	04.4	00.0	.				
25	6	10	—	03	00	04.3	07.1	00.0	.				
26	7	02	—	08	10	06.7	05.0	.	.				
27	7	06	—	07	03	05.3	02.5	02.8	.				
28	8	09	—	05	00	04.7	04.2	00.3	.				
29	7	01	—	00	00	00.3	09.1	.	.				
30	6	10	—	05	05	06.7	04.9	.	.				

L'USSI LANA-BEIGERAD

1978 SURVEY

1	7	10	09.0	10	06.7	02.4	.	.	$\Delta^0-9^{\text{h}} = -0-3, 20^{\text{m}} 24^{\text{s}}, 00^{\text{d}} 00^{\text{m}} 44^{\text{s}}, 3^{\text{f}} \rightarrow 15^{\text{h}} 45^{\text{m}} 0^{\text{s}}$
2	6	10 \equiv	05.0	00	05.0	04.2	00.2	.	$= -0-5^{\text{h}} 8^{\text{m}} 40^{\text{s}}, 18^{\text{h}} 24^{\text{s}}, 00^{\text{d}} 10^{\text{m}} 48^{\text{s}}, 0^{\text{f}} 17^{\text{h}} 24^{\text{s}}, 0$
3	7	10 \equiv	01.0	00	03.7	06.7	.	.	$\Delta^{+2} 0-10^{\text{h}} 19^{\text{m}} 24^{\text{s}} = 0-4^{\text{h}} 20^{\text{m}} 11^{\text{s}}, 00^{\text{d}} 10^{\text{m}} 48^{\text{s}}, 00^{\text{h}} 17^{\text{m}} 24^{\text{s}}, 0$
4	7	10 \equiv	03.0	06.	06.3	06.2	.	.	$\Delta^{+2} 0-9^{\text{h}} 0-1^{\text{m}} 5^{\text{s}}, 20^{\text{h}} 24^{\text{s}}, = 0-1^{\text{h}} 5^{\text{m}} 8^{\text{s}}, T^{\text{f}} 10^{\text{h}} 21^{\text{m}} 24^{\text{s}}, \oplus 19^{\text{h}} 20^{\text{m}} 13^{\text{h}} 20^{\text{s}}$
5	7	09 \odot	05.0	00	04.7	07.2	00.9	.	$= 0-9^{\text{h}} 20^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 0-0^{\text{h}} 1^{\text{m}} 24^{\text{s}}, \Delta^0-19^{\text{h}} 24^{\text{s}}, 0$ $L 20^{\text{m}} 21^{\text{s}}, 0$
6	8	07 \odot	02.0	00	03.0	06.7	.	.	$= 0-9^{\text{h}} 23^{\text{m}} 24^{\text{s}}, \Delta^{+2} 0-44^{\text{h}} 19^{\text{m}} 24^{\text{s}}, 00^{\text{d}} 9^{\text{m}} 12^{\text{s}}, 0$
7	7	10 \equiv	02.0	10	07.3	06.4	.	.	$\Delta^{+2} 0-10^{\text{h}} 24^{\text{m}} 24^{\text{s}} = 0-2^{\text{h}} 25^{\text{m}} 10^{\text{s}}, 00^{\text{d}} 12^{\text{h}} 21^{\text{m}} 0$
8	7	10 \equiv	03.0	10	07.7	05.9	.	.	$\Delta^{+2} 0-11^{\text{h}} 21^{\text{m}} 24^{\text{s}} = 0-5^{\text{h}} 20^{\text{m}} 41^{\text{s}}, 00^{\text{d}} 11^{\text{h}} 20^{\text{m}}, \oplus 44^{\text{h}} 17, 0$
9	7	10	09	04	07.7	00.9	.	.	$\Delta^{+2} 0-5^{\text{h}} 18^{\text{m}} 24^{\text{s}} = 0-4^{\text{h}} 15^{\text{m}} 19^{\text{s}}, 00^{\text{d}} 7^{\text{h}} 47^{\text{m}}, 0$
10	7	10	09.0	C9	09.3	01.4	01.1	.	$= 0-7^{\text{h}} 8^{\text{m}} 44^{\text{s}}, \Delta^{+2} 0-24^{\text{h}} 1^{\text{m}} 24^{\text{s}}, = 0-7^{\text{h}} 8^{\text{m}}, 0$
11	7	10	10	10.	10.0	00.0	00.9	.	$\Delta^{+2} 0-12^{\text{h}} 6^{\text{m}} 24^{\text{s}}, = 2^{\text{h}} 12^{\text{m}} 19^{\text{s}}, 0$
12	6	10 \bullet	10.	10	10.0	00.0	05.6	.	$= 0-24^{\text{h}} 0^{\text{m}} 20^{\text{s}}, 0$
13	7	10 \bullet	10	10.	10.0	00.0	14.0	.	$= 0-13^{\text{h}} 17^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 1-4^{\text{h}} 12^{\text{m}} 10^{\text{s}}, 21^{\text{m}}$
14	6	10	09.0	10	05.7	00.5	16.5	.	$= 0-4^{\text{h}} 15^{\text{m}} 12^{\text{s}}, 0^{\text{f}} 1^{\text{h}} 25^{\text{m}} 41^{\text{s}}, T^{\text{f}} 17^{\text{h}} 17^{\text{m}}, \Delta^{+2} 12^{\text{h}}, 0$
15	7	10	02.0	05	05.7	04.9	01.5	.	$= 0-14^{\text{h}} 19^{\text{m}} 22^{\text{s}}, 0^{\text{f}} 1-18^{\text{h}} 24^{\text{s}}, = 0-12^{\text{h}} 24^{\text{s}}, 0$
16	5	09	10.	10.	09.7	00.0	.	.	$\Delta^{+2} 0-9^{\text{h}} = 0-10^{\text{h}} 5^{\text{m}} 7^{\text{s}}, 00^{\text{d}} 10^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 19^{\text{h}} 24$
17	6	10 \bullet	10.	10.	10.0	00.0	20.1	.	$= 0-24^{\text{h}} 0^{\text{m}} 20^{\text{s}}, 0$
18	7	09	09	10	04.3	01.8	16.5	.	$= 0-11^{\text{h}} 20^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 1-18^{\text{h}} 24^{\text{s}}, 0$
19	6	10	06.0	09	08.3	01.2	.	.	$\Delta^{+2} 0-11^{\text{h}} 19^{\text{m}} 24^{\text{s}}, = 0-24^{\text{h}} 0^{\text{m}} 20^{\text{s}}, 0$
20	7	09	09.0	10	09.3	00.1	.	.	$\Delta^{+2} 0-7^{\text{h}} = 0-13, 21^{\text{h}} 24^{\text{s}}, 0^{\text{f}} 0-7^{\text{h}} 10^{\text{s}}, 18^{\text{h}} 19^{\text{m}}, 0$
21	7	10	06 \odot	00	05.3	01.8	01.0	.	$\Delta^{+2} 0-10^{\text{h}} 18^{\text{m}} 24^{\text{s}}, = 0-2^{\text{h}} 0^{\text{m}} 17^{\text{s}}, 00^{\text{d}} 10^{\text{m}} 24^{\text{s}}, 00^{\text{h}} 11^{\text{m}} 0^{\text{s}}$
22	6	10	10	10	10.0	00.6	.	.	$\Delta^{+2} 0-12^{\text{h}} 1^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 1-12^{\text{h}} 13^{\text{m}}, 0$
23	7	10 \equiv	00.0	09	06.3	05.5	00.0	.	$= 0-6^{\text{h}} 10^{\text{m}} 13^{\text{s}}, 0^{\text{f}} 1-18^{\text{h}} 24^{\text{s}}, = 0-2^{\text{h}} 25^{\text{m}} 4^{\text{s}}, 00^{\text{d}} 13^{\text{h}} 18^{\text{m}}, \Delta^{+2} 24, 0$
24	7	09	01.0	00	03.3	07.6	.	.	$\Delta^{+2} 0-9^{\text{h}} 19^{\text{m}} 24^{\text{s}} = 0-10^{\text{h}} 17^{\text{m}} 24^{\text{s}}, 00^{\text{d}} 10^{\text{m}} 17^{\text{m}}, 0$
25	7	10 \equiv	00.0	00	03.3	05.4	.	.	$\Delta^{+2} 0-10^{\text{h}} 18^{\text{m}} 24^{\text{s}} = 0-1^{\text{h}} 11^{\text{m}} 17^{\text{s}}, 00^{\text{d}} 13^{\text{h}} 19^{\text{m}}, 00^{\text{h}} 13^{\text{h}} 13^{\text{m}}, 0$
26	5	10 \equiv	01.0	10 \equiv	07.0	04.2	.	.	$\Delta^{+2} 0-11^{\text{h}} 20^{\text{m}} 24^{\text{s}}, \Delta^0-14^{\text{h}} 17^{\text{m}} 24^{\text{s}}, = 11^{\text{h}} 13^{\text{m}} 17^{\text{s}}, 00^{\text{d}} 13^{\text{h}} 17^{\text{m}}, 0$
27	5	10 \equiv	01.0	00 \equiv	03.7	04.2	.	.	$\Delta^{+2} 0-11^{\text{h}} 17^{\text{m}} 23^{\text{s}}, = 0-0-11^{\text{h}} 18^{\text{m}} 22^{\text{s}}, = 11^{\text{h}} 14^{\text{m}} 17^{\text{s}}, 00^{\text{d}} 13^{\text{h}} 24, 0$
28	5	10 \equiv	00.0	00	03.3	04.2	.	.	$\Delta^{+2} 0-12^{\text{h}} 0^{\text{m}} 24^{\text{s}}, = 0-0-12^{\text{h}} 10^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 0-12^{\text{h}} 10^{\text{m}}, 0$
29	6	10 \equiv	00.0	00	03.3	05.7	00.1	.	$\Delta^{+2} 0-13^{\text{h}} 17^{\text{m}} 24^{\text{s}}, = 0-2^{\text{h}} 10^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 1-13^{\text{h}} 18^{\text{m}}, 00^{\text{d}} 13^{\text{h}} 22^{\text{m}}, 0$
30	5	10 \equiv	01.0	00	03.7	05.6	00.0	.	$\Delta^{+2} 0-13^{\text{h}} 0^{\text{m}} 24^{\text{s}}, = 0-2^{\text{h}} 11^{\text{m}} 24^{\text{s}}, 0^{\text{f}} 1-13^{\text{h}} 20^{\text{m}}, 00^{\text{d}} 12^{\text{h}} 46^{\text{m}}, 0$
31	5	10 \equiv	C2.0	00	04.0	04.4	00.1	.	$\Delta^{+2} 0-14^{\text{h}} 18^{\text{m}} 24^{\text{s}}, = 0-0-11^{\text{h}} 22^{\text{m}} 24^{\text{s}}, = 11^{\text{h}} 13^{\text{m}}, 18^{\text{h}} 22^{\text{m}}, 00^{\text{d}} 13^{\text{h}} 18^{\text{m}}, 0$

$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

D d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pore • mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	738.2	737.8	738.2	03.3	06.6	08.0	06.5	08.0	02.9	-02.0	05.7	06.7	07.4	98	92	92	94	NE 1	SE 1	- 0
2	736.6	739.8	742.8	07.8	17.6	09.2	11.0	18.2	06.9	02.1	07.3	09.6	07.9	92	64	90	82	SW 1	ESE 1	S 1
3	743.9	743.3	743.9	08.6	11.0	09.8	09.8	11.7	08.3	06.2	08.0	08.3	08.3	95	84	92	90	E 1	SE 1	E 1
4	745.6	746.6	746.8	08.3	09.0	08.3	08.5	10.3	08.1	08.1	08.2	07.3	07.0	100	85	85	90	SSE 1	ESE 2	ENE 2
5	745.4	744.6	744.6	07.6	09.4	07.8	08.2	09.6	07.4	06.5	06.9	06.5	06.5	88	74	82	81	NNE 1	ENE 2	NE 1
6	743.2	742.2	742.4	06.8	08.2	06.9	07.2	08.5	06.7	05.3	06.3	06.3	06.0	85	78	80	81	WSW 1	ENE 1	NE 1
7	741.7	741.4	741.6	05.8	06.9	06.1	06.2	07.3	05.8	04.2	04.2	06.4	06.6	89	85	93	89	WW 1	ENE 1	NE 1
8	742.0	741.6	741.3	06.7	10.4	07.4	08.0	11.0	05.9	03.6	06.3	05.3	05.6	85	57	72	71	ENE 1	ENE 3	ENE 2
9	738.8	737.8	738.9	06.3	06.0	04.0	03.1	07.7	03.9	04.4	05.1	05.4	05.8	71	77	96	81	ENE 2	ENE 3	E 1
10	739.2	738.3	738.7	03.9	05.7	03.7	04.3	05.9	03.4	03.4	06.0	06.3	05.8	98	92	97	96	WW 2	E 1	S 1
11	740.3	741.2	741.5	03.8	06.2	05.7	05.4	06.4	03.4	02.5	05.7	05.9	06.4	95	82	93	90	WW 1	ENE 2	NNE 1
12	743.2	744.4	745.7	04.8	05.7	05.4	05.3	06.1	04.7	03.9	05.9	06.1	06.1	91	89	90	90	E 1	ENE 2	ENE 2
13	745.5	745.0	744.6	04.7	06.0	05.0	05.2	06.4	04.7	04.1	06.0	05.7	06.4	94	81	97	91	NE 1	SE 1	NNE 1
14	742.9	741.7	741.9	04.7	07.4	06.4	06.2	07.6	04.6	04.4	06.3	06.5	06.3	99	84	88	90	ENE 1	ENE 1	SSE 1
15	741.4	740.4	739.7	05.3	06.7	04.3	05.2	07.0	04.3	04.6	05.7	05.9	05.4	86	80	87	84	SE 1	ENE 2	NNE 1
16	734.3	729.1	726.9	02.6	02.6	02.0	02.3	04.8	01.9	00.9	05.1	04.8	05.0	92	87	95	91	NW 1	ESE 1	NE 1
17	722.9	722.3	723.2	01.9	01.8	02.0	01.9	02.7	00.4	00.5	05.0	05.0	05.1	95	97	97	96	ENE 1	ENE 1	NW 1
18	721.5	721.7	725.7	02.1	04.6	03.9	03.6	04.9	01.8	01.7	02.5	02.6	01.5	98	96	97	97	NNE 1	SSE 1	NNE 1
19	720.8	732.4	733.7	01.4	04.8	04.3	03.7	05.4	01.4	00.4	05.0	05.9	06.1	98	91	99	96	NNE 1	NE 1	ENE 1
20	730.5	727.7	726.4	04.4	05.9	06.4	05.8	06.7	04.3	03.9	05.5	06.2	06.1	88	89	84	87	W 1	ENE 1	NNE 1
21	732.0	735.6	737.2	02.8	07.4	00.5	02.8	08.9	00.5	-04.9	04.7	01.4	02.3	84	18	49	50	WW 2	WW 3	SSW 2
22	733.6	731.7	736.0	-06.0	02.4	-02.4	-02.1	03.9	-06.0	-11.7	02.6	03.4	02.0	93	-63	53	70	NW 1	ESE 1	NE 1
23	730.8	739.3	741.0	-04.6	03.6	-01.6	-01.1	03.6	-04.7	-13.2	02.0	01.8	01.8	66	30	44	47	S 1	ENE 3	ENE 2
24	741.6	740.1	741.6	-07.4	03.7	-03.9	-02.9	03.8	-08.6	-13.4	02.1	02.0	02.0	87	32	61	60	NW 1	SSE 1	WW 1
25	742.2	741.9	741.6	-09.2	01.8	-06.2	-05.0	02.7	-09.4	-15.1	02.0	01.8	02.3	94	33	83	70	WW 1	ENE 1	NNE 1
26	740.3	738.3	738.2	-09.2	02.4	00.2	-01.6	05.0	-09.3	-13.7	02.0	03.1	03.4	97	56	74	76	NNE 1	ESE 1	NNE 1
27	737.3	736.9	736.5	00.1	03.0	02.6	02.1	03.6	-00.3	-08.2	04.4	04.7	04.8	95	83	87	88	NE 1	- 0	WSW 1
28	734.3	732.9	733.4	02.5	05.4	04.8	04.4	05.8	02.3	01.2	05.2	06.2	06.2	95	92	96	94	WW 1	W 1	- 0
29	732.3	732.1	732.6	02.8	06.7	04.2	04.5	06.8	02.7	-00.8	05.4	06.6	05.8	97	89	94	93	NNE 1	SE 1	W 1
30	733.1	731.6	731.3	01.4	04.6	05.3	04.2	05.6	00.3	01.5	05.0	05.8	06.4	98	91	96	95	NNE 1	NM 1	W 1
MES. VRED.	737.8	737.3	737.9	02.5	06.1	04.0	04.2	06.9	01.6	-00.3	05.2	05.4	05.4	91	75	85	84	1.1	1.4	1.1

1	731.8	734.3	737.7	07.4	07.4	05.6	06.5	08.4	05.2	04.0	07.5	07.0	05.9	97	91	86	91	E 2	NW 2	ESE 2
2	736.6	735.2	734.7	04.7	06.2	05.6	05.5	06.6	04.6	03.8	05.6	05.8	06.2	90	81	90	87	SSE 1	ENE 1	NE 1
3	734.8	736.3	737.8	05.0	07.0	05.3	05.7	07.3	05.0	04.5	06.2	06.6	06.5	94	88	97	93	SSE 1	SSE 1	NNE 1
4	741.6	744.0	745.9	02.8	04.8	05.7	04.8	06.1	02.8	02.9	05.5	05.8	06.2	98	90	90	93	ENE 1	NMM 1	NMM 1
5	744.8	743.9	743.8	04.0	05.2	03.2	03.9	06.2	03.1	-01.2	05.9	05.2	05.0	97	79	86	87	ESE 1	ESE 1	E 1
6	741.6	737.4	736.7	01.4	05.4	03.2	03.3	09.8	00.6	01.4	04.7	05.1	05.0	93	76	86	85	NW 2	NW 2	NW 1
7	740.8	742.1	740.6	-01.2	04.2	-01.2	00.2	04.3	-01.6	-06.6	04.0	04.7	04.0	96	77	94	98	WW 2	ENE 3	ENE 1
8	736.0	735.8	736.5	-02.7	07.4	-00.3	01.3	08.2	-03.3	-07.5	03.6	04.7	04.3	98	61	91	83	NE 1	E 1	NNE 1
9	742.0	742.5	742.5	-01.6	-00.2	-01.2	-01.1	01.0	-03.2	-08.1	03.9	04.2	04.0	98	93	96	96	SW 2	SSW 1	NW 1
10	742.0	741.7	743.3	00.0	02.3	00.4	00.8	02.8	-01.6	-01.2	04.2	04.5	04.3	91	84	91	89	ENE 1	- 0	NW 1
11	744.8	744.6	744.1	-02.2	02.4	01.7	00.9	02.8	-02.6	-06.3	03.7	04.3	04.5	96	79	87	87	NNE 1	NNE 1	EME 1
12	741.2	738.8	737.2	01.2	02.2	01.1	01.4	02.9	00.9	-00.2	04.5	04.3	04.1	90	79	83	84	- 0	SSE 1	- 0
13	735.2	735.0	737.9	00.5	01.4	00.7	00.8	01.6	00.4	-01.1	04.0	04.2	04.2	84	83	88	85	SSE 1	W 1	NNE 1
14	740.8	742.2	744.5	00.9	01.0	-00.1	00.4	01.3	-00.4	00.4	04.3	04.3	04.3	88	88	95	90	ESE 1	SSE 1	- 0
15	744.6	743.2	743.8	-00.2	01.4	-00.5	00.1	01.6	-00.4	-01.0	04.1	04.2	04.1	91	83	86	87	ENE 1	NE 1	- 0
16	741.0	736.7	733.6	00.0	01.0	01.6	01.1	01.7	00.0	-00.3	04.3	04.6	04.7	95	93	92	93	ESE 1	NNE 1	NW 1
17	727.8	723.5	722.8	01.8	02.6	02.6	02.4	03.2	01.2	00.9	05.0	05.2	05.2	95	94	94	94	NM 1	NNE 1	W 1
18	727.6	733.3	737.0	03.2	01.4	00.8	01.6	03.4	00.4	01.6	05.3	04.6	03.9	92	92	81	88	ESE 2	ESE 1	ENE 1
19	739.3	740.1	741.5	-03.8	-02.4	-06.0</														

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$$H_s = 299 \text{ m} \quad H_b = 297.6 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_x = 1.5 \text{ m}$$

Dan	Výška 0-9 m	Občasnost N (0-10)					Intenzita bez. sítí	Podzemní R mm	Snežní pokrývka h cm	Rezervy vremena w
		14	7	14	21	Sred Dies				
1	5	10 ≡	10	10*	10.0	00.0	00.0	.	.	$\Delta^{+2} 0.12^{\circ} = \Delta^{-2} 0.12^{\circ} + -0.12^{\circ} 13^{\circ} 19^{\circ} 24^{\circ} ; 12^{\circ} 24$
2	6	09	09	04	07.3	03.2	00.1	.	.	$= 0.10^{\circ} 17^{\circ} 24^{\circ} ; 14^{\circ} 5^{\circ} 00^{\circ} 14^{\circ} 17^{\circ} ; -0.10^{\circ} 24^{\circ} ; 0$
3	5	10	09	10	09.7	00.0	00.1	.	.	$\Delta^{-0.4^{\circ}} 24^{\circ} = 0.23^{\circ} 0^{\circ} 4^{\circ} 6^{\circ} 14^{\circ} ; 23^{\circ} 24^{\circ} ; 0$
4	8	10 ≡	10	10*	10.0	00.0	00.6	.	.	$\Delta^{-0.0^{\circ}} = 0.19^{\circ} 9^{\circ} 12^{\circ} 15^{\circ} 23^{\circ} ; 7^{\circ} 24$
5	6	10	10	10	10.0	00.0	00.8	.	.	$= 0.10^{\circ} 13^{\circ} 24^{\circ} ; 9^{\circ} 3^{\circ} 4^{\circ} 00^{\circ} 10^{\circ} 48$
6	6	10	10	10	10.0	00.0	.	.	.	$= 0.24^{\circ} 7^{\circ} 2^{\circ} 7^{\circ} 10^{\circ} 24^{\circ} ; 0.20^{\circ} 24$
7	5	10	10*	10	10.0	00.0	00.0	.	.	$\Delta^{-0.9^{\circ}} = 0.24^{\circ} 0^{\circ} 9^{\circ} 19^{\circ} ; 9^{\circ} 10^{\circ} 14^{\circ} 15^{\circ} 16^{\circ}$
8	7	09	07*	09	08.3	02.0	00.7	.	.	$= 0.10^{\circ} 15^{\circ} 24^{\circ} ; 9^{\circ} 19^{\circ} 19^{\circ} 23^{\circ} 24^{\circ} ; 19^{\circ} 24$
9	7	10	10	10*	10.0	00.0	.	.	.	$\Delta^{+0.4^{\circ}} 23^{\circ} ; 9^{\circ} 19^{\circ} 19^{\circ} 23^{\circ} 24^{\circ} ; 0.24^{\circ} 24$
10	5	10*	10*	10*	10.0	00.0	03.0	.	.	$9^{\circ} 0^{\circ} 3^{\circ} 6^{\circ} 6^{\circ} ; 0.24^{\circ} 15^{\circ} 26^{\circ} 8^{\circ} 9^{\circ} 12^{\circ} 24$
11	6	10	10	10	10.0	00.0	18.2	.	.	$= 0.24^{\circ} 0^{\circ} 0^{\circ} 3^{\circ} 5$
12	6	10*	10	10*	10.0	00.0	08.5	.	.	$= 0.24^{\circ} 0^{\circ} 8^{\circ} 12^{\circ} 9^{\circ} 20^{\circ} 23^{\circ}$
13	6	10	10	10*	10.0	00.0	00.2	.	.	$\Delta^{-0.2^{\circ}} 24^{\circ}$
14	6	10*	10	10	10.0	00.0	21.1	.	.	$\bullet^{-0.0^{\circ}} = 0.24^{\circ} 17^{\circ} 24^{\circ} ; 0^{\circ} 9^{\circ} 10^{\circ} 13^{\circ} ; 17^{\circ} 24^{\circ} ; 0$
15	6	10	09	08	09.0	00.1	00.9	.	.	$= 0.24^{\circ} 17^{\circ} 24^{\circ} ; 0^{\circ} 9^{\circ} 10^{\circ} 13^{\circ} ; 17^{\circ} 24^{\circ} ; 0$
16	6	10	10*	10*	10.0	00.0	00.1	.	.	$\Delta^{-0.4^{\circ}} = 0.10^{\circ} 13^{\circ} 24^{\circ} ; 14^{\circ} 20^{\circ} 14^{\circ} 20^{\circ} ; 14^{\circ} 20^{\circ} 24$
17	4	10*	10*	10*	10.0	00.0	02.4	.	.	$= 0.24^{\circ} 0^{\circ} 2^{\circ} 7^{\circ} 19^{\circ} 24^{\circ} ; 15^{\circ} 18^{\circ} 19^{\circ} ; 0^{\circ} 10^{\circ} 19^{\circ} ; 0^{\circ} 19^{\circ} 19^{\circ}$
18	5	10*	10*	10	10.0	00.0	16.0	.	.	$\Delta^{+0.0^{\circ}} 24^{\circ} = 0.24^{\circ} 13^{\circ} 15^{\circ} 23^{\circ} 24^{\circ} ; 0.24^{\circ} 23^{\circ} ; 0$
19	4	10**	08	10 ≡	06.3	00.2	04.4	.	.	$= 0.24^{\circ} 0^{\circ} 6^{\circ} 28^{\circ}$
20	6	10*	10	10	10.0	00.0	00.3	.	.	$= 0.24^{\circ} 0^{\circ} 6^{\circ} 28^{\circ}$
21	9	02	02*	00	01.3	08.4	00.9	.	.	$= 0.6^{\circ} 1^{\circ} 2^{\circ} 12^{\circ} 13^{\circ} ; 1^{\circ} 19^{\circ} 20^{\circ} ; 0$
22	8	02	05*	01	02.7	04.0	.	.	.	$\Delta^{-0.1^{\circ}} 19^{\circ} 24^{\circ} ; 0$
23	8	01	02*	00	01.0	08.2	.	.	.	$\Delta^{-0.1^{\circ}} 19^{\circ} 24^{\circ} ; 0$
24	8	00	00	00	00.0	08.3	.	.	.	$\Delta^{-0.1^{\circ}} 19^{\circ} 24^{\circ} ; 0$
25	6	00	01*	00	00.3	05.7	.	.	.	$\Delta^{-0.1^{\circ}} 19^{\circ} 24^{\circ} ; 0$
26	5	00	00*	07	02.3	05.4	.	.	.	$\Delta^{-0.1^{\circ}} 21^{\circ} 24^{\circ} = 0.10^{\circ} 20^{\circ} 24^{\circ} 00^{\circ} 10^{\circ} 20^{\circ} ; 0^{\circ} 15^{\circ} 45^{\circ}$
27	4	10*	10*	10	10.0	00.0	00.1	.	.	$= 0.24^{\circ} 0^{\circ} 4^{\circ} 9^{\circ} 14^{\circ} 24^{\circ} ; 1^{\circ} 17^{\circ} 21^{\circ} ; 0$
28	4	10	10*	10	10.0	00.0	00.4	.	.	$= 0.7^{\circ} 12^{\circ} 24^{\circ} ; 0^{\circ} 2^{\circ} 4^{\circ} 12^{\circ} 14^{\circ} 17^{\circ} 18^{\circ}$
29	3	10**	08**	09 ≡	00.0	00.0	00.1	.	.	$\Delta^{-0.2^{\circ}} 18^{\circ} 24^{\circ} = 0.24^{\circ} 0^{\circ} 2^{\circ} 4^{\circ} 12^{\circ} ; 0$
30	4	10**	10*	10	10 ≡	10.0	00.0	.	.	$= 0.24^{\circ} 0^{\circ} 19^{\circ} 24^{\circ} ; 9^{\circ} 19^{\circ} 10^{\circ} 11^{\circ} 13^{\circ} 16^{\circ} ; 10^{\circ} 22^{\circ}$

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1	6	10 ≡ *	10 *	10 *	10.0	00.0	14.3	.	= 0-13 ³ * 0-21 ⁶ 8 ² 22 ⁶ 7 ⁶ 6 ³ 8 ² 6 ⁸ 8 ² 6 ⁸ 10 ⁶ = 13 ³ -15 ⁶ , 20 ³
2	6	15	10	10	10.0	00.0	14.3	.	= 5 ³ 2 ⁶ 7 ⁶ 2 ³ 24 ⁶ 6 ³ 17 ⁶ 17 ³
3	5	10 *	10	10 ≡	10.0	00.0	05.2	.	= 0-10 ³ 0-0-0 ² 3 ⁶ 10 ² 13 ⁶ 22 ⁶ 24, 0 ⁶ 0 ² 0 ³ = -0 ² 0 ² 2 ⁶ 19 ⁶ 24
4	4	10 ≡	10	10	10.0	00.0	00.8	.	= 0-8 ³ 0-10 ⁶ 0-0 ² 10 ⁶ 24
5	6	10 ≡	07	10	09.0	00.0	.	.	= 0-6 ³ 14 ⁶ 24, 0 ⁶ 6 ² 14 ⁶ 0
6	6	10	03 0	00	04.3	03.2	.	.	= 0-14 ³ ; = 0-7 ⁶ 8 ² 23 ⁶ 24, 0
7	7	10 ≡	02 0	00	04.0	03.0	.	.	= 0-2 ³ 0-9 ⁶ 19 ⁶ 24; = 1 ⁶ 1 ³ 7 ⁶ 13 ⁶ 19 ⁶ 22 ⁶ = 0-2 0 ² 7 ⁶ 22 ⁶ 24, 0
8	7	10 ≡	00 0	00	03.3	05.1	.	.	= 0-0-0 ² 0-10 ⁶ 0-0 ² 10 ⁶ 24; = 0-2 0 ² 7 ⁶ 22 ⁶ 24, 0
9	3	10 ≡	00 ≡	00 ≡	03.3	00.3	.	.	= 0-9 ³ 1 ⁶ 0-12 ⁶ 19 ⁶ 24; = 0-2 0 ² 7 ⁶ 22 ⁶ 24, 0
10	4	10 ≡	10	05	08.3	00.0	.	.	= 0-0-24, 0-0-7 ⁶ 20 ⁶ 24, 0 = 19 ⁶ 24, 0
11	5	10 ≡	10	10	10.0	00.0	.	.	= 0-2 ² 0-9 ⁶ 0-2 ⁶ 24; = 0-2 2 ⁶ 14 ⁶ 24, 0
12	5	09	10 *	10 *	09.7	00.8	00.1	.	= 0-9 ³ 15 ⁶ 24, 0 00 15 ⁶ 0 ² 12 ⁶ 15 ⁶ ; 19 ⁶ 24, 0 ⁶ 12 ⁶ 13 ⁶
13	5	10	10	10	10.0	00.0	00.0	.	= 0-24, 0 ² 0-10 ⁶ 0-0 ² 10 ⁶ 24
14	4	10 *	10 *	10 *	10.0	00.0	00.0	.	= 0-24, 0 ² 0-10 ⁶ 0-0 ² 10 ⁶ 24, 0
15	4	10 *	10	10	10.0	00.0	05.2	.	= 0-24, 0 ² 0-2 ⁶ 5 ⁶ 10 ⁶ ; 0 ⁶ 23 ⁶ 24, 0
16	5	10 0	10 0	10 0	10.0	00.6	02.2	.	= 0-24, 0 ² 0-24, 0
17	4	10 0	10 0	10	10.0	00.0	25.1	.	= 0-2 ³ 0-10 ⁶ 0-0 ² 10 ⁶ 24, 0
18	4	10 0	10 * 0	10	10.0	00.0	13.7	.	= 0-2 ³ 0-3 ⁶ 0-3 ⁶ 4 ⁶ ; = 5 ⁶ 24, 0 ⁶ 24, 0
19	0	07	10	00	05.7	00.0	16.2	.	= 0-1 ³ 7 ⁶ 19 ⁶
20	7	00	00 0	10	03.3	03.5	.	.	= 0 ⁶ 20, = 20-24, 0, 0
21	7	10	00 0	00	03.3	03.0	.	.	= 0-13 ⁶ 19 ⁶ 24, 0 00 13 ⁶ 19 ⁶ 22 ⁶ 24, 0, 0
22	5	02	01 0	00	01.0	03.0	.	.	= 0-10 ³ 17 ⁶ 23 ⁶ 0-0 ² 0-0 ² 00 10 ⁶ 17 ⁶ ; = 23 ⁶ 24, 0, 0
23	2	10 ≡	10 ≡	10 ≡	10.0	00.0	.	.	= 0-20-24, 0 ² 0-24, 0
24	2	10 ≡	10 ≡	10 ≡	10.0	00.0	.	.	V ⁰ 0-24, = 0-20-24, 0
25	4	10 ≡	10	10	10.0	00.0	.	.	= 0-7 ³ 0-24, 0-0 ² 24, 0
26	3	10 ≡	10 ≡	10 ≡	10.0	00.0	.	.	= 0-0 ³ = 0-0 ² 24 V ⁰ 0-24, 0 ² 9 ⁶ 13 ⁶ 0
27	3	07 ≡	01 ≡ 0	00 ≡	02.7	01.7	00.0	.	= 0-0 ³ 13 ⁶ 0-0-0 ² 10 ⁶ 24; = 3 ⁶ 3 ⁶ 14-17 ⁶ 0, 0
28	2	10 ≡	00 ≡ 0	10 ≡	06.7	00.0	.	.	= 0-20-24, 0, 0
29	2	10 ≡	00 ≡ 0	10 ≡	06.7	00.0	.	.	= 0-20-24, V ⁰ 0 ² 24, 0 ² 10 ⁶ 4 ⁶ 0
30	2	10 ≡	00 ≡ 0	10 ≡	06.7	00.0	00.2	.	V ⁰ 0-24, = 0-20-24, 0 ² 10 ⁶ 7 ⁶ 27 ⁶ * 0 ⁶ 8 ⁶ 10 ⁶ , 0, 0
31	1	10 ≡	10 ≡	10 ≡	10.0	00.0	00.1	.	V ⁰ 0-24, = 0-20-24, 0, 0

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h\ 04\ min.$

BR. ST. 57

D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, I (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	756.9	755.0	754.5	00.1	03.8	03.2	02.6	03.8	00.0	-	03.4	03.8	04.1	74	63	72	70	WWW 1	SW 2	WSW 1	
2	756.5	756.7	759.8	00.7	04.8	05.8	04.3	06.0	00.7	-	04.2	04.9	04.7	88	76	68	77	W 1	SSW 1	NE 2	
3	759.3	759.3	758.6	04.5	04.5	02.6	03.6	05.8	02.6	-	04.4	04.6	04.1	70	73	74	72	NE 1	SW 1	NNW 1	
4	757.8	756.2	756.8	-01.8	03.0	-01.9	-00.7	03.3	-01.9	-	04.1	04.8	03.7	78	85	93	85	W 1	S 1	ENE 2	
5	758.5	756.3	754.8	-02.0	-00.9	-00.4	-00.8	00.3	-02.3	-	03.9	04.2	04.2	98	96	96	97	ESE 1	WSW 2	SSE 1	
6	752.5	749.5	748.6	00.9	10.5	06.9	06.3	10.6	-00.4	-	03.8	04.9	04.9	90	52	66	69	SE 1	SSW 2	W 3	
7	746.1	743.2	743.5	04.8	10.7	08.1	07.9	10.8	04.2	-	04.8	05.8	05.6	74	60	69	68	NNW 4	NNW 4	NNW 3	
8	739.8	741.9	748.1	05.1	04.9	02.1	03.6	08.1	02.1	-	05.5	05.0	05.1	83	78	95	85	WSW 2	ESE 2	S 1	
9	753.9	757.1	757.9	01.3	02.7	-00.1	01.0	02.7	-00.2	-	03.6	04.1	03.5	70	73	80	74	NNE 1	SSW 2	NNW 1	
10	755.9	755.0	756.0	-02.8	04.7	01.9	01.4	04.7	-02.8	-	03.4	04.0	03.7	89	62	70	74	SSW 1	WSW 2	NE 1	
11	754.3	752.9	753.0	-01.8	07.0	04.7	03.7	07.3	-02.0	-	03.8	04.7	04.6	94	63	73	77	S 1	WSW 2	WSW 3	
12	753.2	753.0	754.4	05.0	10.2	06.6	07.1	10.2	04.2	-	04.7	05.4	05.2	72	58	70	67	WSW 1	WSW 2	W 1	
13	755.1	755.4	757.5	03.9	09.9	07.3	07.1	10.0	03.2	-	04.9	05.4	05.5	80	60	72	71	WSW 2	WSW 3	NNE 2	
14	757.2	755.8	755.8	00.8	07.1	05.8	04.9	07.7	00.7	-	04.5	05.2	05.5	93	69	80	81	ENE 1	WSW 2	WSW 2	
15	755.5	755.2	755.4	06.0	11.2	06.9	07.8	11.4	03.9	-	05.2	06.0	05.3	74	60	72	69	WSW 3	WSW 3	WSW 2	
16	753.7	752.4	752.3	03.6	10.5	07.1	07.6	10.6	04.8	-	03.1	06.0	05.3	78	63	70	70	WSW 2	SW 3	WSW 3	
17	750.9	749.2	748.8	05.5	11.8	09.2	08.9	12.0	05.5	-	05.2	06.4	06.1	76	62	70	69	NNW 2	WSH 4	WSW 2	
18	746.4	746.0	746.4	-08.7	12.4	09.7	10.1	12.6	08.1	-	06.3	06.8	06.7	74	63	74	70	NNW 2	WSW 4	WSW 1	
19	747.5	748.8	752.1	05.8	12.6	08.1	08.7	12.6	05.8	-	05.5	05.7	06.1	61	52	75	69	ESE 1	WSW 3	SE 1	
20	756.7	756.2	755.2	06.4	09.2	05.5	06.7	09.6	05.5	-	05.7	05.8	05.7	80	66	84	77	ENE 1	NNE 1	- 0	
21	754.1	753.5	754.5	04.6	08.0	05.0	05.7	08.0	03.6	-	05.7	05.8	05.2	88	72	80	80	ENE 1	ESE 2	ENE 2	
22	755.6	755.3	753.3	03.2	05.0	04.9	04.5	05.8	03.1	-	05.4	05.4	05.3	94	83	82	86	WSW 1	WSW 2	SSE 1	
23	750.2	748.2	747.9	02.8	08.7	08.1	06.9	08.9	02.8	-	05.3	05.8	05.2	94	68	64	75	SE 1	SSW 2	WSW 2	
24	746.2	746.5	748.0	05.5	09.9	07.4	07.6	09.9	05.5	-	05.2	05.9	05.7	76	65	74	72	WSW 2	NNW 2	NNW 2	
25	750.1	749.7	748.5	03.3	10.7	08.9	08.0	10.9	03.3	-	05.2	05.8	06.3	91	59	74	75	SSW 1	WSW 2	WSW 2	
26	748.8	751.6	754.5	09.6	11.2	06.7	08.6	11.2	06.7	-	06.1	06.6	06.2	68	66	64	73	NNW 3	E 2	ENE 1	
27	753.5	748.3	742.5	05.0	08.5	06.6	06.7	08.5	05.0	-	05.2	05.1	05.3	80	61	72	71	ENE 1	SSE 2	W 1	
28	737.9	740.7	742.7	06.0	06.2	06.0	06.1	06.7	04.7	-	06.0	05.6	05.2	86	79	74	80	NE 3	ENE 2	NNW 1	
29	739.3	740.5	745.3	04.0	10.4	07.6	07.4	10.4	02.8	-	05.1	04.9	04.9	84	52	62	66	WSW 1	NNE 1	NNE 2	
30	746.9	746.5	752.9	05.3	06.3	05.5	05.7	06.4	04.8	-	04.5	05.1	04.3	69	72	64	68	NNE 2	ENE 1	NNE 1	
31	755.3	754.5	753.5	04.3	07.4	04.6	05.2	07.7	03.8	-	05.1	04.9	04.4	81	63	69	71	W 1	SSW 2	NE 2	
MES. VRED.	751.9	751.4	752.0	03.6	07.8	05.5	05.6	08.2	02.8	-	04.8	05.3	05.1	82	67	75	74	1.5	2.1	1.6	

1975 FEBRUAR

ZAGREB-GRIC

1	752.4	755.7	758.6	01.5	04.2	04.3	03.6	04.9	01.5	-	04.5	05.3	05.0	87	87	80	85	SE 1	EWE 2	NE 1
2	756.2	756.2	753.8	04.6	05.9	05.6	05.4	06.2	04.0	-	05.8	06.1	06.4	90	88	93	90	NNW 1	W 2	WSW 1
3	753.4	755.2	757.5	04.7	03.9	02.7	03.5	05.6	02.7	-	04.9	04.5	04.7	76	75	84	78	NE 2	NNE 3	ENE 2
4	759.8	761.2	762.8	01.5	02.2	01.9	01.9	02.7	01.5	-	04.2	03.7	04.4	82	70	84	79	ENE 3	ENE 3	ENE 2
5	763.3	762.7	761.8	00.7	02.0	-00.5	00.4	02.0	-00.5	-	03.8	03.7	03.5	79	70	80	76	ENE 1	ESE 2	S 1
6	761.0	759.5	756.9	-02.9	03.6	01.8	01.1	03.7	-02.9	-	03.5	04.0	04.1	94	67	79	80	S 1	SSW 1	NNE 1
7	751.8	749.3	748.5	-02.6	05.2	04.8	03.1	06.7	-02.6	-	03.4	03.8	04.6	89	58	72	73	SE 1	SSE 1	E 2
8	755.9	755.2	756.5	00.0	03.5	00.5	01.1	04.8	00.0	-	03.3	02.7	02.5	72	47	53	57	NNE 1	SSW 3	WSW 1
9	755.5	754.2	753.0	-02.8	02.7	00.5	00.2	02.9	-02.8	-	02.5	02.7	03.2	68	51	68	62	N 1	SSW 2	SW 1
10	752.1	750.8	749.8	-03.6	06.0	05.6	03.4	06.1	-03.6	-	03.0	03.6	04.2	84	52	62	66	SW 1	SSW 2	NN 3
11	748.9	748.1	747.4	02.3	10.6	07.4	06.9	10.7	06.9	-	04.5	05.2	05.9	85	55	77	72	N 3	W 3	W 3
12	744.8	744.0	743.2	08.7	11.3	08.4	09.2	11.4	06.6	-	05.6	06.2	05.8	67	62	70	66	NNW 3	WSW 4	W 3
13	741.0	738.8	738.6	04.6	11.2	09.0	08.5	11.3	04.6	-	04.9	04.7	05.0	77	47	58	61	W 2	SSW 2	NE 2
14	739.2	738.9	742.3	04.2	08.5	03.3	04.8	09.0	02.7	-	05.0	06.3	05.0	85	63	86	78	W 1	NNW 2	NE 2
15	745.8	747.3	749.3	01.8	07.4	05.4	05.0	07.4	01.7	-	04.7	04.6	04.1	90	61	75	75	NNW 2	ESE 2	ME 2
16	752.4	757.2	761.4	02.6	C2.2	00.6	01.5	05.4	00.6	-	04.5	02.3	02.0	81	56	42	60	NE 3	ENE 3	NE 3
17	743.5	761.9	762.4	-03.3	01.2	-01.5	-01.3	01.4	-03.3	-	02.3	02.7	02.2	64	51	52	56	ENE 2	ENE 2	NNE 2
18	760.3	757.9	756.1	-04.2	01.8	00.0	-00.7	02.5	-04.5	-	02.6	02.5	03.1	78	48	68	65	ENE 1	SSE 2	E 1
19	752.7	748.0	74																	

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$

Dan	Vrijeme 0-9 0	Oblačnost N (0-10)					Intenzitet broj sni	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7 10	10	10	10	10.0	00.3	.	.	.	= n-j-n	
2	5 01	10	10	07.0	01.9	= n-n, w-n-8°	
3	5 10	10	07	09.0	00.0	= n-n	
4	5 00	01.0	10	03.7	03.0	= n-dp, v-n-dp, = n-10°, 16°, n; = 10°, 16°	
5	4 10	10	10	10.0	00.0	= n-10°, = n-10°, = 10°-n	
6	5 09	00.0	00	03.0	06.6	= n-10°, = 10°-n	
7	6 01	09	05	05.0	03.5	= n-n, Fww, 21°, 21°	
8	5 10	10	10	10.0	00.5	= n-20°, tr-17°, 9°, 17-20°, *-21°, 22°	
9	6 00	03.0	00	01.0	04.4	06.2	01	.	.	= pp-n, ■	
10	5 01	04.0	00	01.7	07.1	= H-n	
11	6 00	00.0	06	02.0	06.3	= n-14°	
12	7 10	01.0	01	04.0	05.8	= n-7°, 16°, n	
13	6 01	01.0	00	06.7	07.0	= n-n, = 8-8°	
14	6 00	00.0	00	00.0	06.8	= n-j-dp, = n-7°, 11°, n; = 7°, 11°	
15	7 04	09	04	05.7	04.0	= n-j-n	
16	6 06	09.0	02	05.7	00.6	= n-9°, Fsw, 15°, 15°	
17	7 02	09	01	04.0	04.3	Fw 15°, 15°	
18	8 08	10	06	08.0	01.2	= n-n, w-18°, 19°	
19	6 06	09	10	08.3	06.2	= n-12°, 17°, n, = 17°, 8°	
20	7 08	09	00	05.7	02.6	= n-8°, 18°, n, tr-8°, 8°, 14°, 20°	
21	5 10	03.0	10	07.7	03.0	= n-7°, 10°, n; = 7°, 10°	
22	3 10	10	10	10.0	00.0	= n-7°, 13°, n; = 7°, 13°	
23	4 10	09.0	10	09.7	01.6	= n-10°, = 10°, 11°, = 11°, 16°	
24	7 10	09	00	06.3	00.1	= n-12, 16, n	
25	7 03	03.0	10	05.3	06.7	= n-n, = n-11°, w-18°, 19°	
26	6 08	10	10	09.3	00.6	= n-8°, 18-n, tr-8°, 8°, 14°, 20°	
27	8 10	05.0	10	08.3	06.0	00.6	.	.	.	= n-10°, tr-10°, n-10°, 20°	
28	8 10	10	10	10.0	00.6	05.1	.	.	.	= n-9°, tr-10°, 20°	
29	7 10	01.0	03	04.7	04.7	06.0	.	.	.	= n-n, k-10°, 13°	
30	6 10	10	10	10.0	00.0	00.0	.	.	.	= n-k, = 10°, 13°	
31	6 10	02.0	01	04.3	03.0	00.2	.	.	.	= n-k	
MES. VРЕД.		06.4	06.3	05.7	06.1	101.2	18.3				

1	6 04	10.0	10	08.0	00.0	= n-n, = 10°, 18°	
2	5 10	10	10	10.0	00.0	01.9	.	.	.	= n-n, = 10°, 10°, 20°, 20°	
3	6 10	09	10	09.7	00.0	02.5	.	.	.	= n-7°, 10°, n, tr-10°, n-rj, H=13°, 16°, 20°, t=10°, 11°, 21°, 17°	
4	6 10	10*	10*	10.0	00.0	00.7	.	.	.	= n-n, *-n, k-10°	
5	6 10	10	00	06.7	00.0	00.0	.	.	.	= n-n	
6	6 00	00.0	00	00.0	00.1	= n-n, = n-10°, = 10°-n	
7	5 00	00.0	00	00.0	00.6	= n-n, = n-10°, = 10°-n	
8	6 02	05.0	01	02.7	02.3	= n-13°, = n-dp, *-n-11°, -11°	
9	8 00	00.0	00	00.0	00.8	00.0	.	.	.	= n-dp, = 7°, 9°, 9°	
10	6 00	00.0	00	00.0	07.6	= n-dp, = n-9°, = 9°	
11	6 00	09	05	04.7	05.8	= n-13°	
12	8 10	01	04	07.7	01.5	Fww 10°, 15°, tr-11°	
13	8 02	09.0	10	07.0	09.3	00.0	.	.	.	= n-8°, 15°, 13°, 10°, 10°, 10°, 10°	
14	5 10	10	10*	10.0	00.1	= n-n, = 8°, 10°, tr-10°, 9°, 17°, n	
15	8 04	08.0	10	07.3	06.2	04.4	.	.	.	= 7°, 12°	
16	6 10*	10	00	06.7	00.0	00.3	.	.	.	= n-n, rj-7°, *-7°, 8, *-7°, 8-10°	
17	6 00	00.0	00	00.0	05.9	00.0	.	.	.	= n-n, = 10°, 10°	
18	6 00	00.0	04	02.0	00.1	= n-j-dp, = 9°-n	
19	6 04	09.0	10	07.7	02.6	= n-j-dp, = n-j-2°, t=10°, 22°, ■	
20	5 10	10*	10	10.0	00.1	02.0	02	.	.	= n-10°, *-10°, 10°, 10°, 22°, ■	
21	6 10	08	10	09.3	00.4	00.6	.	.	.	= n-13°, *-7°, 8°	
22	7 07	02.0	00	03.0	00.6	00.0	.	.	.	= n-n	
23	6 01	00.0	00	00.3	00.9	= n-n, = n-dp	
24	6 00	00.0	00	00.0	00.3	= n-10°, = n-dp	
25	6 00	00.0	04	02.0	07.2	= n-n, = 7°-9°, = 9°-n	
26	8 00	01.0	00	00.3	09.2	= n-H°, Fwne 11°, 22°	
27	8 04	02.0	00	00.7	09.4	= n-8°, = 8°	
28	8 00	03.0	00	01.0	00.7	= n-9°	
MES. VРЕД.		04.1	03.1	04.4	04.5	130.6	12.4				

$\varphi = 45^{\circ}49' \text{ N } \lambda = 15^{\circ}59' \text{ E } \Delta G = + 1 \text{ h } 04 \text{ min.}$

BR. ST. 57

D o d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	750.8	749.0	748.5	-00.8	12.7	08.4	07.2	12.7	-00.8	-	03.3	03.3	04.9	78	30	59	56	SW	1	SSW	2	WSW	2
2	748.2	747.9	748.7	07.2	14.6	11.0	11.0	14.8	05.3	-	05.0	06.0	05.5	66	48	56	57	WSW	3	WSW	3	WSW	4
3	747.8	745.8	745.3	08.5	15.5	11.0	11.5	15.5	08.4	-	06.2	06.1	05.3	75	47	54	59	WSW	1	WSW	4	W	3
4	743.8	742.3	742.6	07.8	15.0	10.3	10.9	15.2	07.3	-	05.9	06.2	05.2	73	49	56	59	WNW	1	WSW	2	WSW	1
5	743.7	745.0	746.8	07.8	11.4	09.6	09.6	11.4	07.7	-	05.1	07.1	07.7	65	70	87	74	NE	2	SSE	1	SSE	1
6	749.1	748.5	748.8	05.8	14.0	11.5	10.9	14.2	04.8	-	06.6	06.3	05.6	87	53	54	65	WNW	2	WSW	2	NNE	2
7	749.0	748.0	747.3	08.4	13.7	10.7	10.9	13.7	08.1	-	06.4	07.3	08.0	78	62	82	74	N	1	SSE	2	SSW	1
8	746.2	744.0	743.3	08.3	17.2	12.0	12.4	17.3	08.3	-	07.6	07.4	07.2	92	49	68	70	-	0	WSW	3	N	1
9	739.8	736.8	735.4	07.9	14.8	12.2	11.8	15.5	07.9	-	06.6	07.6	05.8	82	60	54	65	-	0	WSW	1	WSW	1
10	735.4	736.5	738.9	08.9	13.6	11.6	11.4	14.0	08.9	-	07.1	06.3	06.8	83	54	66	68	ENE	1	ENE	1	WNW	2
11	743.1	745.1	746.6	09.3	14.3	10.4	11.1	14.3	09.3	-	07.7	07.5	06.2	88	62	66	72	WSW	2	WNW	2	W	2
12	744.4	742.5	742.7	07.2	08.5	07.7	07.8	11.0	07.0	-	05.2	06.6	07.0	68	79	91	79	NE	2	NE	2	SW	2
13	743.1	743.5	743.2	04.4	12.7	11.9	10.2	13.1	04.4	-	06.1	05.5	06.2	97	50	60	69	SE	1	SSW	1	WNW	1
14	741.2	740.4	743.1	08.2	07.9	07.5	07.8	12.0	07.5	-	07.1	07.6	07.0	86	95	90	90	NE	2	N	1	ESE	1
15	744.9	745.1	745.7	05.8	11.3	07.5	08.0	12.0	05.1	-	06.3	06.9	06.8	92	68	88	83	SSE	1	SSW	1	WNW	1
16	744.6	742.8	742.8	02.7	12.6	09.7	08.7	13.4	02.7	-	05.5	05.7	06.9	98	52	73	74	NW	1	WSW	2	-	0
17	741.8	740.6	742.0	06.1	10.9	05.1	06.8	11.0	05.1	-	06.6	05.8	05.2	93	59	80	77	ENE	2	WNW	3	NE	2
18	741.5	741.6	742.1	01.1	06.3	08.1	05.9	08.2	01.1	-	04.7	05.9	06.9	95	82	81	86	NE	2	NE	2	E	1
19	740.1	739.5	738.6	07.7	11.9	13.7	11.8	13.9	07.6	-	06.2	07.3	07.5	81	70	62	71	NE	3	ENE	2	ENE	2
20	741.7	743.0	743.6	07.4	11.8	10.2	09.9	13.7	07.4	-	06.0	07.2	07.3	78	69	78	75	WNW	2	SE	2	ENE	1
21	745.5	747.8	750.7	06.4	06.0	04.0	05.1	10.2	04.0	-	05.9	04.5	03.4	82	65	57	68	NE	4	NNE	2	NNE	4
22	751.4	747.8	745.4	01.0	05.6	02.7	03.0	05.8	01.0	-	02.6	03.0	03.3	52	44	60	52	NNE	3	NNE	2	NE	2
23	742.3	740.7	740.8	00.0	03.0	01.7	01.6	03.0	00.0	-	04.0	04.0	03.9	87	70	76	78	ENE	2	ENE	2	NE	2
24	739.0	738.4	738.9	00.9	07.0	03.7	03.8	07.1	00.1	-	04.0	03.3	03.5	83	44	61	63	ESE	1	NNE	1	NNE	1
25	738.9	740.4	743.1	-00.1	08.5	06.7	05.5	08.6	-00.1	-	03.6	02.0	02.3	80	24	32	45	WSW	1	NW	4	ENE	1
MES.	VRED.	743.1	742.4	742.8	05.5	10.9	08.6	08.4	12.0	05.1	-	05.6	05.8	05.7	81	59	69	70	1.6	2.3	1.6		

1975 APRIL

ZAGREB-GRČ

1	744.7	746.1	747.5	05.4	05.5	05.3	05.4	06.3	03.5	-	05.3	05.8	05.7	79	85	86	83	NE	3	ENE	2	-	0
2	745.3	742.8	741.9	05.5	06.0	05.5	05.6	06.2	05.0	-	05.2	05.8	05.5	76	83	81	80	ENE	2	ENE	2	NE	1
3	741.3	740.9	741.6	04.2	11.1	08.4	08.1	11.1	04.1	-	05.6	06.0	06.0	91	60	72	74	W	2	SSW	3	W	2
4	743.1	744.0	745.4	08.9	15.3	12.2	12.2	15.7	08.0	-	05.9	06.2	06.5	68	48	61	59	WNW	2	S	4	SSW	2
5	744.2	745.4	745.8	10.1	13.3	13.8	12.8	16.5	09.7	-	06.0	08.7	09.0	64	75	76	72	NE	2	SSW	4	W	2
6	745.4	743.6	741.8	13.1	19.9	19.6	18.1	20.7	11.2	-	08.4	09.4	06.7	75	54	39	56	WNW	2	WNW	1	NW	3
7	742.5	742.7	742.3	10.9	13.8	11.7	12.0	19.6	10.9	-	07.8	06.3	11.7	79	53	65	66	ESE	1	NE	1	NE	1
8	742.8	743.1	744.9	08.3	13.8	10.6	11.1	13.8	09.2	-	06.7	07.2	05.7	76	61	60	66	NNE	1	ESE	2	WSW	2
9	745.3	744.3	743.4	09.8	16.1	11.6	12.3	16.6	07.6	-	05.5	05.1	05.0	61	37	49	49	WSW	2	WSW	4	WNW	2
10	739.1	736.0	737.6	09.5	09.2	05.9	07.6	11.6	05.7	-	05.9	07.8	05.3	66	89	77	77	NE	2	NE	1	NE	1
11	744.1	746.7	748.8	05.6	12.4	08.1	08.6	12.4	04.0	-	04.7	03.9	04.8	68	36	59	54	WNW	3	SW	2	NNW	3
12	749.9	748.9	749.2	04.6	13.1	09.7	09.3	13.6	03.8	-	05.4	06.0	05.9	85	53	65	68	WSW	1	WSW	2	SSE	1
13	748.6	747.1	747.9	09.7	17.6	12.9	13.3	17.6	08.2	-	05.3	06.3	06.2	58	42	56	52	WNW	2	WNW	4	W	2
14	749.4	746.7	745.4	10.7	17.6	13.9	14.0	19.0	10.5	-	06.3	07.7	07.0	65	51	59	58	NE	2	WSW	2	WSW	3
15	743.7	740.9	740.1	10.7	18.7	13.5	14.1	18.6	10.4	-	06.4	06.8	07.1	66	42	61	56	WSW	2	SW	4	WSW	3
16	738.5	741.4	744.3	11.0	10.1	10.1	10.3	13.5	10.0	-	08.2	07.2	08.1	83	78	87	83	W	2	N	3	WNW	2
17	748.0	748.0	750.0	08.7	15.6	11.1	11.6	15.8	08.2	-	06.7	05.2	05.2	79	39	52	57	W	1	NNE	2	NNE	2
18	751.0	750.2	751.1	07.3	13.3	10.7	10.5	13.8	06.3	-	05.9	05.5	04.9	77	48	50	58	WNW	1	ENE	2	NNE	2
19	751.9	751.0	751.3	09.1	15.7	11.8	12.1	16.2	08.2	-	04.6	05.8	05.5	53	43	53	50	NE	1	SE	2	NNE	2
20	751.6	749.6	749.9	07.5	17.2	14.5	13.4	17.2	06.6	-	05.3	06.3	07.1	68	43	57	56	WNW	1	SSE	2	NNE	1
21	751.1	750.7	751.4	11.8	20.3	14.8	15.4	20.3	09.4	-	07.0	07.1	07.8	67	40	62	56	ENE	1	E			

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_x = 2.0 \text{ m}$

Dan:	Vidljivost 0-9	Oblačnost N (0-10)					Insekcija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8 00	00	00	00	00.0	08.5	.	.	.	= n-4 ^w	
2	6 08	08	06	07.3	07.3	= n-n, Fw 13 ^w 17	
3	8 09	08	05	07.3	07.2	= n-8 ^w	
4	8 05	09	09	07.7	04.3	= n-10 ^w	
5	6 09	10	10	09.7	00.3	= n-n, tr-18 ^w 8 ^w , 11 ^w 19 ^w	
6	8 10	06	10	08.7	06.3	02.2	.	.	.	= n-7 ^w 7 ^w 8 ^w 17 ^w n; tr 8 ^w 12 ^w	
7	7 08	09	10	09.0	02.5	= n-11 ^w 16 ^w n; n-16 ^w	
8	8 09	09	06	08.0	04.9	00.0	.	.	.	= n-10 ^w 15-17 ^w	
9	6 09	10	06	08.3	00.6	= n-n, d-19 ^w 13 ^w	
10	8 07	10	10	09.0	00.0	00.9	.	.	.	= n-12 ^w 16-n; o ^w n, 9 ^w 12 ^w 16 ^w	
11	8 03	09	10	07.3	03.7	00.0	.	.	.	= n-9 ^w 16-n; tr-0 13 ^w 14 ^w	
12	7 00	10	10	06.7	00.8	00.6	.	.	.	= n-12 ^w , tr-0 10 ^w 14 ^w ; 18 ^w n	
13	7 01	09	10	06.7	01.5	04.7	.	.	.	= n-n, r-9 ^w 9 ^w 15 ^w , 16 ^w	
14	6 10	10	07	09.0	00.6	00.5	.	.	.	= n-14 ^w 17 ^w	
15	6 10	08	01	06.3	03.1	02.1	.	.	.	= n-10 ^w 16-17 ^w , 18 ^w 16 ^w 17 ^w , 16 ^w 16 ^w	
16	7 10	04	08	07.3	05.6	09.5	.	.	.	= n-9 ^w 9 ^w 9 ^w 14 ^w tr 16 ^w 16 ^w	
17	7 10	10	10	10.0	02.2	02.1	.	.	.	= n-11 ^w 15 ^w 20 ^w 17 ^w 12 ^w 6 ^w 13 ^w 14 ^w , tr-0 15 ^w 18 ^w	
18	6 10	10	10	10.0	00.0	04.9	01	.	.	= n-n, r-7 ^w 12 ^w 13 ^w 14 ^w , 15 ^w 16 ^w 17 ^w , 18 ^w 19 ^w	
19	6 10	09	05	08.0	01.7	04.1	.	.	.	= n-13 ^w 14 ^w 15 ^w 16 ^w 17 ^w 18 ^w 19 ^w	
20	6 10	09	10	09.7	00.8	00.5	.	.	.	= n-0 7 ^w 11 ^w = n-7 ^w	
21	6 10	10	06	08.7	01.3	03.7	.	.	.	• n-11 ^w = n-14 ^w , F _{N-NNE} 7 ^w 8 ^w , 19 ^w 23 ^w	
22	8 00	02	00	00.7	09.9	00.7	.	.	.	= n-9 ^w	
23	6 05	10	09	08.0	00.1	= n-n, *tr-0 7 ^w 17 ^w	
24	6 09	04	00	04.3	03.7	00.1	.	.	.	= n-j-dp, F _{NW} 13-16	
25	8 06	08	10	08.0	07.3		
26	8 10	04	08	07.3	08.0	= rj-9 ^w F _{SW} 15-17	
27	7 10	10	10	10.0	00.4	= n-10 ^w 15 ^w	
28	8 10	09	10	09.7	01.4	00.0	.	.	.	= n-8 ^w 10 ^w 12 ^w 13 ^w 14 ^w , tr-0 14 ^w 14 ^w	
29	6 10	10	10	10.0	00.0	05.6	01	.	.	= n-n, o ^w 7 ^w 13 ^w 19 ^w n; * ^w 2 rj, 16 ^w 17 ^w , * ^w 9 ^w 9 ^w 17 ^w 19 ^w	
30	6 10	10	10	10.0	00.0	00.6	12.3	.	.	= n-15 ^w 19 ^w n; *tr-0 12 ^w	
31	5 10	10	01	07.0	01.9	00.4	.	.	.		
MES. VРЕД.	07.7	08.2	07.3	07.7	98.3	56.9					

1	5 10	10	10	10.0	00.0	03.4	.	.	.	= n-n, o ^w 7 ^w 18 ^w	
2	5 18	10	10	10.0	00.0	04.7	.	.	.	= n-n, o ^w 10 ^w 12 ^w 19 ^w	
3	6 18	09	05	08.0	02.2	02.0	.	.	.	= nj-13 ^w , nrj-7 ^w	
4	8 10	09	09	09.3	02.5	00.0	.	.	.	= tr-12 ^w 14 ^w i, o ^w 13 ^w 13 ^w , F _E 13 ^w 13 ^w , R' 13 ^w , o ^w 17 ^w n	
5	7 00	09	10	06.3	07.3		
6	7 02	10	10	07.3	01.8	03.3	.	.	.	= 12 ^w 13 ^w	
7	7 10	10	09	09.7	00.2	= n-8 ^w 16 ^w n	
8	6 10	08	01	06.3	03.4	00.0	.	.	.	= n-14 ^w , o ^w rj, 14 ^w 15 ^w ; 16 ^w HV	
9	7 04	08	00	04.0	08.2	00.2	.	.	.	= n-n, o ^w 16 ^w n	
10	5 10	10	10	10.0	00.0	00.0	.	.	.		
11	7 10	08	10	09.3	04.8	23.9	.	.	.	= tr-0 7 ^w i, 18 ^w 18 ^w	
12	8 10	02	04	07.0	04.6	00.5	.	.	.	= n-8 ^w 14 ^w n	
13	7 09	08	09	08.7	04.9	00.0	.	.	.	= n-7 ^w	
14	7 08	08	08	08.3	07.2	= n-8 ^w	
15	7 00	03	10	09.0	09.2	= n-8 ^w , F _W 17 ^w , o ^w 18 ^w 19 ^w , R 18 ^w	
16	6 10	10	10	10.0	00.0	00.3	.	.	.	= n-n, o ^w rj-19 ^w	
17	8 01	08	00	03.0	07.7	05.2	.	.	.	= n-9 ^w	
18	6 09	09	09	09.0	05.1	= n-12 ^w	
19	7 01	00	01	06.7	10.8	= n-8 ^w	
20	7 01	03	08	04.0	09.8	= nj-10 ^w , 18 ^w HV	
21	6 08	08	10	08.7	07.9	= n-n, o ^w 8 ^w	
22	5 10	07	09	08.7	05.2	00.0	.	.	.	= n-n	
23	6 09	09	06	08.0	06.6	= n-16 ^w o ^w 9 ^w 11 ^w , o ^w 20 ^w n	
24	6 08	09	03	06.7	09.0	= n-10 ^w	
25	6 10	10	07	09.0	03.5	00.0	.	.	.	= n-13 ^w , 16 ^w 17 ^w , o ^w 6 ^w 7 ^w R 17	
26	8 09	06	01	05.3	06.1	00.0	.	.	.	= tr-0 10 ^w pp, F _E 12-14 ^w lpp-n	
27	8 02	09	02	04.3	09.4	00.3	.	.	.	= 9-12 ^w o ^w 10 ^w 13 ^w l	
28	7 00	01	00	08.3	12.4	00.0	.	.	.	= n-14 ^w 19 ^w n	
29	7 00	00	00	06.0	12.5	= n-14 ^w	
30	7 00	01	01	06.7	12.7	= n-10 ^w	
MES. VРЕД.	06.4	07.1	06.2	06.6	175.5	43.8					

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h\ 04\ min.$

EKF. ST. 57

D&C	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %				Pravac i jačina vjetra D, f (0-12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	751.7	753.3	754.8	12.0	17.8	14.0	14.5	17.0	10.6	-	07.2	06.9	05.4	65	45	45	53	WSW	1	NW	3	NE	2
2	754.4	751.4	750.8	11.5	19.7	16.5	16.1	19.8	10.3	-	05.6	05.1	05.5	55	35	35	41	W	1	NNE	3	NNE	1
3	747.8	744.1	743.5	13.4	21.5	16.3	16.9	21.6	11.0	-	06.1	06.1	05.9	53	32	43	43	NW	2	NE	2	N	2
4	746.7	747.5	747.7	13.1	16.0	15.6	15.1	16.5	12.3	-	08.2	08.4	06.1	73	62	61	65	NE	2	ESE	3	NE	3
5	748.5	748.9	749.5	12.3	16.7	13.1	13.8	16.9	12.1	-	08.1	09.6	10.2	75	68	90	78	NE	3	ESE	2	NNW	1
6	749.7	748.1	747.0	13.0	18.8	18.4	17.2	19.0	12.6	-	09.7	10.2	09.6	86	63	54	70	SE	1	ENE	3	NNE	3
7	746.4	745.3	744.8	15.5	22.7	16.6	17.9	23.1	15.4	-	10.0	11.1	12.9	76	54	91	74	NNE	1	WSW	1	NNW	1
8	741.9	741.4	741.8	14.0	16.9	14.9	15.2	18.0	12.9	-	11.4	11.2	08.5	95	76	67	80	ENE	2	W	2	WSW	3
9	743.1	744.2	746.2	13.3	19.6	14.1	15.3	19.9	10.4	-	07.3	07.6	08.2	64	46	68	59	W	3	SW	3	WSW	2
10	748.0	747.3	746.7	11.8	17.8	15.5	15.2	20.5	9.8	-	07.6	08.1	07.9	74	53	60	67	WSW	2	WSW	3	NNW	1
11	746.1	743.8	742.4	11.2	21.6	17.8	17.1	22.1	09.7	-	08.2	07.6	08.0	82	39	52	58	WSW	1	SE	2	NNE	2
12	740.8	740.0	740.7	14.7	21.8	18.3	18.3	21.9	14.1	-	09.2	08.7	10.9	73	45	69	62	SW	2	ESE	2	E	2
13	741.4	741.9	741.0	14.3	14.1	15.1	14.7	18.3	12.9	-	07.1	09.9	10.4	56	82	81	74	NNE	4	WSW	1	WSW	1
14	740.3	739.5	741.3	15.1	23.2	19.8	19.5	23.2	12.6	-	09.9	10.0	09.9	77	47	57	60	ESE	1	NNE	3	NNW	2
15	742.9	743.2	743.5	15.5	22.6	17.9	18.5	23.1	14.4	-	11.6	12.4	12.4	68	61	61	77	NNE	1	ENE	2	N	1
16	744.4	744.2	744.5	15.9	25.8	20.8	20.8	25.8	13.9	-	11.0	12.5	13.3	82	50	73	68	ENE	1	SSE	2	N	1
17	746.5	746.9	747.9	18.9	24.7	20.3	21.1	24.7	14.7	-	09.5	12.0	11.9	58	51	67	59	NNW	2	NNW	1	N	1
18	750.1	749.9	750.7	18.9	26.6	22.4	22.6	26.6	16.1	-	12.2	11.8	12.0	74	45	59	59	E	1	ESE	2	N	2
19	751.5	750.2	750.0	18.5	27.2	24.4	23.6	27.4	17.8	-	11.6	11.6	11.8	73	43	52	56	ENE	1	NNE	2	N	2
20	749.6	748.4	748.7	19.3	24.9	23.2	22.7	25.3	17.3	-	12.4	14.9	13.6	74	63	64	67	W	1	ENE	1	NE	2
21	749.5	747.8	746.9	17.4	25.1	20.7	21.0	25.3	16.4	-	11.9	12.1	13.5	80	51	74	68	WSW	1	ESE	2	N	1
22	746.0	744.0	744.1	18.9	21.5	19.8	20.0	25.3	16.6	-	11.4	14.0	12.1	70	73	70	71	WSW	2	NNW	2	NNW	1
23	744.2	744.2	744.6	16.1	15.0	13.4	14.5	19.9	13.4	-	12.4	12.1	10.3	90	95	89	91	NE	1	E	2	ENE	2
24	745.2	744.6	744.3	11.7	12.5	12.8	12.5	13.9	11.6	-	07.8	10.1	10.5	76	93	95	88	NE	2	NNW	3	WSW	1
25	743.9	744.5	745.2	13.8	18.7	15.3	15.8	20.9	12.8	-	10.7	09.9	11.1	90	61	85	79	SW	1	W	1	NE	2
26	746.6	746.6	746.7	14.2	17.9	15.0	15.5	19.0	13.0	-	06.4	11.3	12.3	78	74	96	83	NE	2	ENE	2	NW	1
27	747.0	747.7	747.6	15.0	15.0	14.6	14.8	16.0	14.6	-	11.2	11.9	11.6	86	93	95	92	NNE	2	WSW	2	N	1
28	747.9	746.4	748.5	14.9	20.2	16.4	17.0	20.6	14.1	-	12.2	11.0	11.7	96	62	86	81	S	1	NE	1	NNW	1
29	746.9	743.7	743.1	15.2	24.4	19.0	19.4	24.6	13.6	-	11.1	11.0	08.9	86	46	54	63	SW	1	SD	3	WSW	3
30	742.1	740.8	741.9	16.5	23.4	18.8	19.4	23.5	16.1	-	09.8	10.5	10.0	70	49	61	60	WSW	3	SSW	5	SD	2
31	744.1	742.9	743.2	15.4	23.7	18.5	19.0	25.0	14.0	-	09.8	10.5	08.8	75	48	56	60	SE	1	SSW	2	SW	2
MES. VRED.	746.3	745.6	745.8	14.9	20.6	17.4	17.6	21.5	13.4	-	09.7	10.3	10.2	76	58	65	68	1.6	2.2	1.7			

1	743.0	742.3	742.7	17.2	21.7	16.3	17.9	23.0	15.4	-	10.4	09.8	12.3	71	51	88	70	E	1	SW	4	N	2
2	743.3	745.6	743.0	03.2	11.3	12.1	11.3	16.3	02.1	-	07.2	08.0	08.6	91	80	81	84	NE	1	ENE	3	NNW	1
3	744.5	744.1	744.5	11.5	13.3	13.2	12.8	13.5	11.5	-	07.7	08.7	09.4	76	76	84	79	NE	2	NE	2	Nb	1
4	747.2	747.7	749.8	11.1	17.3	13.0	13.6	17.3	11.1	-	06.7	06.5	06.8	68	44	61	58	NNW	3	ENE	2	NNW	2
5	752.2	751.5	752.8	13.5	17.1	13.7	14.5	17.1	11.6	-	05.2	05.7	05.6	45	39	48	44	N	2	NNE	3	N	3
6	753.4	752.6	752.5	12.5	17.1	14.2	14.5	17.1	12.0	-	05.1	05.7	05.8	47	39	48	45	NNE	2	ENE	3	NE	2
7	750.3	749.5	748.5	13.8	18.3	17.2	16.7	18.5	12.7	-	06.3	08.1	06.4	53	51	44	49	SSW	1	NE	2	NNW	2
8	746.3	745.8	746.0	14.0	22.7	19.3	13.3	17.2	12.7	-	06.5	09.3	10.2	55	85	69	76	W	2	WSW	2	WSW	2
9	744.4	743.0	743.3	13.6	19.5	13.6	15.1	20.0	11.9	-	09.8	08.9	10.7	85	52	90	76	SW	1	SSE	2	NNW	2
10	744.2	744.7	745.9	14.6	18.8	14.7	15.7	19.1	13.2	-	11.3	11.6	11.1	91	71	89	84	SE	1	WSW	2	ENE	1
11	747.9	748.6	749.1	15.3	19.3	19.3	16.3	20.3	14.3	-	11.3	10.5	12.1	87	63	72	74	-	0	NNE	1	N	2
12	749.5	748.6	748.3	18.0	24.2	20.1	20.6	24.6	16.8	-	12.2	11.5	13.0	79	51	79	70	ENE	1	NE	2	NW	2
13	747.9	746.4	745.5	18.1	25.9	20.1	21.1	26.3	16.7	-	12.9	12.4	12.7	83	50	72	68	NW	1	SE	2	N	1
14	745.3	745.1	744.7	19.9	28.1	24.3	24.2	26.3	17.2	-	12.7	13.6	14.1	73	48	62	61	SSW	1	SE	2	S	1
15	744.8	743.3	742.5	19.5	21.1	21.1	20.3	23.1	18.4	-	14.1	12.0	14.0	83	40	71	65	SE	1	S	3	WSW	2
16	742.9	742.4	741																				

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 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insekcija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena	
		14	7	14	21	Sred Dies				7	7
1	7	08	10	06	06.0	01.7	.	.	.	= nj-8 ⁴⁵	.
2	7	03 ⁰	03 ⁰	02	02.7	11.7	.	.	.	= n-11 ⁴⁵ tr-0 8-8 ³⁰ 20 ⁴⁵ n	.
3	8	00 ⁰	05 ⁰	00	01.7	11.1	.	.	.	= n-n, tr-0 nj-11 ³⁰ , 14 ⁴⁵ 19 ⁴⁵	.
4	7	10	10	10 [*]	10.0	00.6	.	.	.	= n-15 ⁴⁵ tr-0 nj-16 ⁴⁵ 19 ⁴⁵	.
5	6	10 [*]	10	10	10.0	00.0	01.9	.	.	= n-n, tr-0 nj-13 ³⁰ , 14 ⁴⁵ 19 ⁴⁵	.
6	5	10 [*]	10	10	10.0	03.0	00.5	.	.	= n-15 ⁴⁵ tr-0 nj-9 ⁴⁵	.
7	6	01 ⁰	07	09	05.7	04.2	00.2	.	.	= n-n, R 16 ⁴⁵ 19 ⁴⁵	.
8	9	10 [*]	07 ⁰	00	05.7	02.8	00.3	.	.	= nj-7 ⁴⁵ , = 7 ⁴⁵ 10 ³⁰ , 0 ⁰ -19 ⁴⁵ 12 ⁴⁵	.
9	8	00 ⁰	03	01	01.3	11.3	03.4	.	.	= tr-13 ⁴⁵ 13 ³⁰ , R 16 ⁴⁵ 16 ⁴⁰	.
10	8	00 ⁰	07	01	02.7	09.0	.	.	.	= tr-13 ⁴⁵ 13 ³⁰ , R 16 ⁴⁵ 16 ⁴⁰	.
11	8	02 ⁰	09 ⁰	08	06.3	10.8	00.0	.	.	= n-7 ⁴⁵	.
12	8	10	09 ⁰	10	09.7	03.7	.	.	.	= n-9 ⁴⁵ tr-0 22 ⁴⁵ n	.
13	6	10	10	10	10.0	00.4	00.8	.	.	= F-ENNE 12 ⁴⁵ 6 ⁴⁵ tr-0 7 ⁴⁵ 13 ³⁰	.
14	7	06 ⁰	07 ⁰	10	07.7	09.0	00.6	.	.	= n-14 ⁴⁵ F-ENNE 20 ⁴⁵ 20 ⁵⁴ , 0 21 ⁴⁵ n	.
15	6	09	05 ⁰	00	04.7	05.6	00.8	.	.	= n-14 ⁴⁵ , 0 n	.
16	6	01 ⁰	03 ⁰	00	01.3	10.8	.	.	.	= n-14 ⁴⁵	.
17	7	00 ⁰	06 ⁰	00	02.0	09.2	.	.	.	= n-13 ⁴⁵ 19 ³⁰ n	.
18	7	00 ⁰	05 ⁰	01	02.0	09.4	.	.	.	= n-10 ⁴⁵	.
19	6	00 ⁰	03 ⁰	01	01.3	11.9	.	.	.	= n-14 ⁴⁵ 18 ⁴⁵ n	.
20	6	00 ⁰	09 ^R ⁰	10	06.3	06.6	.	.	.	= n-n, tr-0 11-13 ¹⁵ , R 14 ⁴⁵ -14 ³⁰ , 0 14 ²⁸ 14 ⁴⁵	.
21	6	01 ⁰	01 ⁰	09	03.7	10.5	02.7	.	.	= n-n, 0 n	.
22	6	10	02 ⁰	01	04.3	09.4	.	.	.	= n-10 ⁴⁵ tr-2 12 ³⁵ 12 ³⁵ 0-2 12 ³⁵ 13 ⁰⁵ R 2 13 ²⁵ 13 ⁴⁰	.
23	6	10	10 ⁰	10	10.0	00.1	06.3	.	.	= n-n, 0 tr-0 12 ³⁵ 12 ³⁵ 0-2 12 ³⁵ 13 ⁰⁵ R 2 13 ²⁵ 13 ⁴⁰	.
24	6	10	10 ⁰	10 [*]	10.0	00.0	21.1	.	.	= n-n, 0 tr-0 12 ³⁵ 12 ³⁵ 0-2 12 ³⁵ 13 ⁰⁵ R 2 13 ²⁵ 13 ⁴⁰	.
25	6	10	07	02	06.3	02.7	08.3	.	.	= n-n	.
26	6	10	09	10	09.7	00.6	.	.	.	= nj-n, 0 16 ⁴⁵ -20 ⁴⁵ R 16 ⁴⁵ -18 ⁴⁵	.
27	5	10 [*]	10 [*]	10 [*]	10.0	00.0	06.6	.	.	= nj-n, 0 16 ⁴⁵ tr-0 16 ⁴⁵ 16 ⁴⁵	.
28	6	10 [*]	09 ⁰	10	09.7	01.9	15.3	.	.	= nj-9 ⁴⁵ , 0 R 14 ⁴⁵ , 0 16 ⁴⁵	.
29	7	00 ⁰	06 ⁰	10	05.3	12.1	01.2	.	.	= nj-9 ⁴⁵ , F 12 ³⁰ 17 ³⁰	.
30	7	10	01 ⁰	04	05.0	09.3	.	.	.	= nj-9 ⁴⁵ , 0 R 14 ⁴⁵	.
31	8	00 ⁰	05 ⁰	09	04.7	14.2	00.8	.	.	= n	.
MES. VRED.		05.5	06.7	05.9	04.1	193.6	71.0				

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1	7	04	10	10	09.7	02.3	.	.	.	= tr-0 18 ⁴⁵ 20 ⁴⁵	.
2	6	10 [*]	10	10	10.0	00.0	05.1	.	.	= n-9 ⁴⁵	.
3	5	10 [*]	10	10	10.0	00.0	04.3	.	.	= n-n, tr-0 6 ⁴⁵ 7 ⁴⁵	.
4	7	04	10	09	09.3	00.2	00.2	.	.	= n-n, tr-0 12 ⁴⁵ 15 ⁴⁵ 15 ⁴⁵	.
5	6	03 ⁰	07 ⁰	00	03.3	10.7	00.0	.	.	= n-14 ⁴⁵	.
6	8	02 ⁰	05 ⁰	00	02.3	13.0	00.0	.	.	F-ENNE 8-14 ³⁰	.
7	8	09	10	09	09.3	02.3	.	.	.	= n-8 ⁴⁵ tr-0 15 ⁴⁵ 15 ⁴⁵	.
8	6	10	10	10	10.0	00.0	00.0	.	.	= n-10 ⁴⁵ 12 ³⁰ , 11 ⁴⁵ n	.
9	8	09	09	10 [*]	09.3	06.0	00.9	.	.	= n-12 ⁴⁵ 14 ⁴⁵ , 14 ⁴⁵ 14 ⁴⁵ 18 ³⁰ n; R 18 ⁵² 19 ³⁰	.
10	6	09 ⁰	10 ⁰	10	09.7	02.6	07.4	.	.	= n-n, 0 tr-0 13 ³² 17 ⁵⁰	.
11	6	03 ⁰	09	06	06.0	05.2	01.2	.	.	= n-13 ⁴⁵ tr-0 10 ⁴⁵ 11 ³⁰	.
12	8	01 ⁰	07 ⁰	10	06.0	08.5	00.1	.	.	= n-10 ⁴⁵ △ n-dp	.
13	7	08	09	00	06.0	07.8	.	.	.	= n-10 ⁴⁵	.
14	7	05 ⁰	06 ⁰	04	05.0	11.5	.	.	.	= n-14 ⁴⁵	.
15	8	00 ⁰	00 ⁰	01	00.3	10.9	.	.	.	= n-10 ⁴⁵ , △ n-dp, R 0-15 ³⁰ 16 ³⁰ , tr-16 ⁴⁵ 16 ⁴⁵	.
16	6	10	10	02	07.3	00.8	01.7	.	.	= n-18 ⁴⁵ R 0-12 ⁴⁵ 12 ⁴⁵ 0-15 ⁴⁵ 18 ³⁰	.
17	7	10 [*]	10	06	08.7	00.8	22.0	.	.	= nj-10 ⁴⁵ tr-0 10 ⁴⁵ 15 ⁴⁵ 10 ⁴⁵ , R 0-15 ⁴⁵ 18 ³⁰	.
18	7	10	05	10	08.3	00.0	10.2	.	.	= n-10 ⁴⁵ , 0 nj	.
19	8	10	10	10	10.0	02.4	.	.	.	= tr-0 7 ⁴⁵ 9 ⁴⁵ , = 9 ⁴⁵ n	.
20	7	10	10	10	10.0	00.1	.	.	.	= n-n, 0 n	.
21	6	10 [*]	08 ⁰	10	09.3	02.3	02.2	.	.	= n-n, 0 8 ⁴⁵ tr-0 8 ⁴⁵	.
22	6	04	08 ⁰	05	07.3	05.5	00.9	.	.	= n-15 ⁴⁵ A dp n	.
23	6	03 ⁰	07	09 ^R	06.3	09.2	.	.	.	= n-14 ⁴⁵ △ n-dp, R 0-14 ⁴⁵ 14 ⁴⁵	.
24	5	10 [*] R	10 [*] R	10	10.0	00.5	05.4	.	.	= n-14 ⁴⁵ △ n-dp, R 0-14 ⁴⁵ 14 ⁴⁵	.
25	6	10 [*]	06 ⁰	10	08.7	07.1	44.5	.	.	= nj-7 ⁴⁵ , = 7 ⁴⁵ 13 ⁴⁵	.
26	8	01 ⁰	03 ⁰	00	01.3	14.6	.	.	.	= n-8 ⁴⁵	.
27	7	00 ⁰	01 ⁰	01	00.7	13.8	.	.	.	= n-8 ⁴⁵ tr-0 20 ⁴⁵ 20 ⁴⁵ n, R 20 ⁴⁵	.
28	7	01 ⁰	04 ⁰	10 [*] R	05.0	11.8	.	.	.	= n-8 ⁴⁵ △ 7 ⁴⁵ , 7 ⁴⁵ 8 ⁴⁵	.
29	7	10 [*]	04 ⁰	10	08.0	03.2	01.4	.	.	= n-12 ⁴⁵ , 0 nj-8 ⁴⁵ , 13 ⁴⁵ 16 ⁴⁵	.
30	8	10	10 ⁰	10 [*]	10.0	00.3	04.4	.	.	= nj-7 ⁴⁵ 14 ⁴⁵ 11 ⁴⁵ n, R 7 ⁴⁵ 8 ⁴⁵ 11 ⁴⁵ n, R 7 ⁴⁵ 7 ⁴⁵	.
MES. VRED.		07.1	07.6	07.1	07.2	160.8	116.9				

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 $\varphi = 45^{\circ}49' \text{ N } \lambda = 15^{\circ}59' \text{ E } \text{Gr. } \Delta G = + 1h \text{ 04 min.}$

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D d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	741.3	742.1	743.5	12.1	12.6	11.4	11.9	14.3	10.3	-	08.1	06.7	09.4	77	63	93	78	NW 2	N 1	WSW 2	
2	740.5	741.2	743.6	12.6	13.9	17.2	16.5	19.5	11.4	-	09.8	12.0	14.7	90	73	100	88	SSW 3	NNE 4	S 1	
3	743.5	745.9	746.6	20.5	25.4	21.9	22.4	25.4	17.2	-	10.2	11.2	12.6	56	47	64	56	N 3	NNE 2	N 2	
4	745.4	743.1	742.0	17.2	26.6	23.2	22.6	27.0	16.4	-	12.2	12.6	15.4	83	48	72	68	WSW 1	SSW 2	W 1	
5	741.5	742.5	743.7	17.1	21.7	19.1	19.3	23.2	16.9	-	12.4	13.2	15.4	87	68	93	83	WNW 2	WSW 1	NNE 1	
6	744.3	744.9	747.1	20.1	19.4	17.4	18.6	22.5	17.3	-	13.4	15.2	12.2	72	90	82	81	NNE 2	NNE 2	N 2	
7	748.8	748.8	748.9	18.3	26.3	22.5	22.4	26.5	16.8	-	13.4	10.6	13.3	85	42	65	64	WNW 1	NE 2	N 2	
8	749.3	748.6	748.7	18.9	28.0	23.7	23.6	28.3	18.3	-	13.0	13.6	15.6	79	48	71	66	ENE 1	S 2	NNE 2	
9	748.8	748.3	748.1	21.0	26.0	23.6	24.2	28.6	19.8	-	14.9	15.6	15.4	80	55	69	68	ENE 1	ESE 2	NNE 1	
10	748.2	746.7	746.5	20.6	28.1	24.1	24.2	28.8	18.8	-	15.1	12.5	15.1	83	44	67	65	- 0	ESE 2	NNE 2	
11	747.7	747.2	746.1	19.1	24.2	22.4	22.0	26.3	17.6	-	15.1	15.9	17.1	91	70	76	79	ENE 1	NNW 1	NNE 2	
12	745.3	745.8	747.9	17.9	18.9	18.2	18.3	22.4	17.6	-	12.8	14.6	13.2	83	89	84	85	W 1	NNE 1	W 2	
13	749.6	750.6	750.7	17.5	22.3	20.3	20.1	23.5	16.5	-	13.8	14.8	15.4	92	73	86	84	NNW 1	SSW 2	NW 1	
14	751.3	750.6	749.9	19.5	27.2	23.5	23.4	28.3	17.6	-	13.9	14.6	15.8	82	54	73	70	ENE 1	SSE 2	N 1	
15	749.4	748.7	747.7	20.8	29.9	25.7	25.5	30.6	19.2	-	15.7	17.1	16.5	85	54	66	68	ENE 1	SSE 2	N 2	
16	747.2	745.5	746.4	22.2	26.1	22.4	23.3	27.3	20.1	-	13.3	15.4	13.8	75	61	68	68	ENE 2	ENE 2	N 2	
17	746.7	745.6	746.3	20.3	28.0	24.3	24.2	28.4	18.4	-	14.5	14.2	15.7	81	50	69	67	WNW 1	ESE 2	N 2	
18	745.8	744.7	742.2	21.4	30.1	25.9	25.8	30.5	19.5	-	15.9	18.6	19.3	83	58	77	73	ENE 1	SSE 2	NNE 2	
19	741.7	745.2	746.4	21.7	22.8	19.2	20.7	25.9	16.8	-	14.4	15.0	12.9	74	72	77	74	NE 2	SSE 2	NNE 1	
20	747.7	746.8	746.6	18.3	24.5	20.2	20.8	25.7	16.0	-	12.4	11.5	11.9	79	51	67	66	ESE 1	ESE 1	N 1	
21	745.9	744.6	745.0	18.4	27.5	22.5	22.7	27.7	16.8	-	13.2	12.4	12.5	82	45	61	63	SSW 1	SSW 2	NNE 1	
22	746.6	746.2	746.3	19.2	23.7	21.1	21.3	25.0	17.4	-	13.5	13.5	13.7	81	61	73	72	WSW 1	SSW 2	NNE 2	
23	747.0	745.9	745.5	18.8	27.0	21.8	22.4	27.3	16.5	-	13.5	13.4	12.7	83	50	65	66	SSW 1	SSE 2	NNE 1	
24	745.0	743.5	743.2	19.4	29.0	24.5	24.4	29.3	18.0	-	14.4	14.4	15.5	85	48	67	67	SE 1	SSW 2	N 1	
25	744.9	746.3	749.7	17.0	17.1	17.4	17.2	24.5	16.0	-	13.0	13.0	08.1	85	89	54	77	NNW 1	NNW 1	NE 2	
26	751.9	751.9	752.7	14.4	22.0	17.7	18.0	22.4	13.3	-	09.5	08.5	09.0	77	43	59	60	ESE 1	ENE 2	NNE 2	
27	752.2	751.4	750.8	15.1	22.8	17.7	18.3	23.4	13.0	-	09.2	08.7	10.0	71	42	66	60	ESE 1	S 2	NNE 1	
28	750.5	749.3	750.1	15.6	23.9	20.1	19.9	24.9	13.5	-	10.6	09.7	11.5	80	44	65	63	ESE 1	SSW 2	NNE 1	
29	750.3	749.0	749.1	17.3	26.0	21.6	21.6	26.7	15.4	-	12.0	11.1	13.9	81	44	72	66	ESE 1	SSW 2	N 2	
30	748.7	748.1	748.3	20.9	25.8	22.7	23.0	26.7	17.9	-	14.3	11.7	11.6	77	47	56	60	ESE 1	ESE 1	NNW 2	
31	749.6	749.3	750.1	20.3	23.4	19.9	20.9	26.4	19.5	-	12.0	11.9	12.9	67	55	77	66	NNW 1	N 2	NW 2	
MES.	VRED.	747.1	746.7	747.1	18.5	24.4	21.1	21.3	25.7	16.8	-	12.9	13.0	13.6	80	57	72	70	1.3	1.8	1.6

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1	750.7	750.0	751.1	20.6	27.2	21.6	22.8	27.2	17.7	-	11.3	11.2	13.0	62	41	67	57	NW 2	NNE 2	NW 1
2	751.8	751.2	752.3	18.6	27.0	18.4	20.6	27.5	18.0	-	12.4	12.3	14.2	77	48	89	71	SSW 1	NNW 1	NNW 1
3	753.7	753.1	752.8	18.2	24.8	20.9	21.2	25.0	17.3	-	13.6	12.4	14.5	87	51	68	69	W 1	ENE 2	N 2
4	751.8	750.3	751.1	19.3	26.7	18.3	20.7	26.7	18.3	-	12.9	12.9	13.9	76	49	88	71	NNW 2	ENE 2	NNW 1
5	750.2	749.0	749.7	18.1	23.5	20.5	20.7	25.0	16.7	-	12.3	10.8	11.4	79	50	63	64	WSW 1	NNE 2	N 2
6	750.4	750.7	751.5	17.6	25.4	19.7	20.6	26.1	16.1	-	12.7	11.7	10.8	84	48	86	73	S 1	NE 2	W 1
7	751.9	750.4	749.8	18.6	24.3	18.8	20.1	25.3	15.6	-	13.8	14.1	14.7	86	62	90	79	ENE 1	WNW 1	WSW 1
8	749.8	749.0	748.9	17.7	23.6	18.9	19.8	24.0	16.5	-	13.6	13.7	15.9	89	62	95	82	NNW 1	NE 3	NNW 1
9	748.4	747.9	748.5	17.6	24.8	20.4	20.8	25.6	16.6	-	14.2	14.4	14.4	94	61	80	78	SE 1	NE 2	N 1
10	749.1	749.0	749.0	18.8	25.8	23.2	22.8	27.5	17.5	-	14.2	14.6	13.4	87	59	63	70	- 0	ESE 2	N 2
11	749.1	748.0	747.0	19.9	26.0	23.1	22.9	27.1	18.0	-	14.1	16.4	15.0	85	65	71	74	NW 1	NW 1	N 1
12	745.6	743.9	743.9	19.0	25.4	17.8	20.0	26.4	17.8	-	15.0	16.6	13.8	91	68	90	83	NE 1	S 2	WSW 1
13	743.9	745.1	747.3	17.1	21.3	20.9	20.1	23.1	16.1	-	13.6	14.8	12.8	93	78	69	80	NNE 1	SSW 1	NNE 2
14	749.6	749.7	749.3	16.1	22.9	19.2	19.4	23.1	15.9	-	10.2	12.2	13.0	74	58	78	70	ENE 2	SSE 2	NNE 1
15	748.9	747.3	746.0	16.3	25.0	22.2	21.4	25.7	15.2	-	12.2	14.3	15.3	88	60	76	75	ENE 1	SSE 2	NNE 2
16	745.3	745.6	746.6	18.8	25.0	18.9	20.4	25.2	17.8	-	13.6	13.6	15.1	85	57	92	78	WSW 1	NNW 1	ENE 1
17	746.7																			

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$$H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$$

Dan	Vrijest 0-9	Oblačnost N (0-10)					Iseljacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	10•	10	10•	10.0	00.0	12.6	.	.	$\bullet^{tr-1} n-13^{\circ}, 16-nl; \# 7^{\circ} 15^{\circ} 730 14^{\circ} 16^{\circ}$, $= 745 12^{\circ} 0$
2	8	15•	09	10•	09.7	02.1	11.7	.	.	$\bullet^{tr-0} n-12^{\circ}, 21^{\circ} n; \# n 10-nl; \# 12^{\circ} 18^{\circ} 21^{\circ} 5^{\circ}$
3	8	03•	03•	00	02.0	12.9	19.3	.	.	.
4	8	00•	01•	09	03.3	11.6
5	8	10•	01•	10 R	07.0	03.4	00.7	.	.	$\bullet^{tr-0} nj-8^{\circ}, R 9^{\circ} 2^{\circ} 930, 17^{\circ} 21^{\circ} 8^{\circ} 1^{\circ} 9^{\circ} 10^{\circ} 10^{\circ}, 17^{\circ} 20^{\circ} 20^{\circ}$
6	6	09	100 R	10•	09.7	02.5	03.0	.	.	$R^{\circ} 11^{\circ} 17^{\circ} 0, \bullet^{tr-1} 12^{\circ} 18^{\circ}, 20^{\circ} 22^{\circ}, \# 0^{\circ} 1^{\circ} 12^{\circ} 13^{\circ}$
7	7	00•	01•	00	00.3	12.7	04.7	.	.	$= nj-10^{\circ}$
8	6	01•	01•	00	00.7	11.7	.	.	.	$= nj-13^{\circ}$
9	6	08	03•	10 R	07.0	08.5	.	.	.	$= nj-n, R^{\circ} 1^{\circ} 19^{\circ} 30^{\circ} n, \# 20^{\circ} n, \# 20^{\circ} 21$
10	6	07	09•	09	06.3	09.9	00.3	.	.	$= nj-15^{\circ}, R 22-n, \# kv-n$
11	6	01•	09	00	03.3	05.4	07.4	.	.	$\# 10^{\circ} 0^{\circ} 1^{\circ} 2^{\circ} 10^{\circ} H^{\circ}, = nj-n$
12	7	10 R	10•	10	10.0	00.8	00.8	.	.	$R 6^{\circ} 4^{\circ} 4^{\circ} 4^{\circ}, \bullet^{tr-6^{\circ}} 8^{\circ} 12^{\circ} 17^{\circ} 22^{\circ}, 22-n; \# 0^{\circ} 1^{\circ} 10^{\circ} H^{\circ}$
13	7	10•	10	00	04.7	02.0	15.6	.	.	$= nj-n, \bullet^{tr-6^{\circ}} 10^{\circ}$
14	7	00•	02•	00	00.7	12.9	00.0	.	.	$= nj-10^{\circ}, \# nj-dp$
15	7	00•	00•	01	00.3	12.8	.	.	.	$= nj-10^{\circ}, \# nj-dp$
16	6	09•	09	08	08.7	05.4	.	.	.	$= nj-13^{\circ}, \# nj-dp, R 17^{\circ} 19^{\circ}, \# tr-17^{\circ}$
17	7	03•	01•	00	01.3	12.4	00.0	.	.	$= nj-8^{\circ}, \# nj-dp$
18	7	00•	01•	00	00.3	12.2	.	.	.	$= nj-11^{\circ}, \# nj-dp$
19	8	09	02•	00	03.7	06.4	00.7	.	.	$\# 1^{\circ} 2^{\circ} 2^{\circ} 4^{\circ} 4^{\circ} 4^{\circ}, 10^{\circ} 10^{\circ} 10^{\circ}, R^{\circ} nj, 10^{\circ} 10^{\circ}, \# 10^{\circ} 10^{\circ}$
20	8	02•	06•	00	02.7	10.0	13.6	.	.	$\# 1^{\circ} 2^{\circ} 3^{\circ} 3^{\circ} 3^{\circ} 3^{\circ}, 6^{\circ} 2^{\circ} 14^{\circ} 6^{\circ}, R^{\circ} 7^{\circ} 7^{\circ} 7^{\circ}$
21	8	00•	08•	08	05.3	09.9	.	.	.	$= n-8^{\circ}, \# n-0^{\circ}, \# tr-0^{\circ} 17^{\circ} 18^{\circ}$
22	8	09	08	01	06.0	06.4	00.0	.	.	$= n-7^{\circ}, \# n-1^{\circ}, \# n-1^{\circ}$
23	6	00•	04•	00	01.3	13.2	00.0	.	.	$= n-13^{\circ}, \# n-dp$
24	8	00•	01•	02	01.0	12.0	.	.	.	$= n-12^{\circ}, \# n-2^{\circ}, \# n-dp$
25	8	10•	10•	10	10.0	00.0	01.4	.	.	$= n-12^{\circ}, \# n-3^{\circ}, \# 3^{\circ} 3^{\circ} 3^{\circ}, 6^{\circ} 2^{\circ} 14^{\circ} 6^{\circ}, R^{\circ} 7^{\circ} 7^{\circ} 7^{\circ}$
26	9	01•	08•	01	03.3	12.0	11.9	.	.	$= nj-8^{\circ}, \# nj-dp, \# 10^{\circ} 17^{\circ}$
27	8	01•	05•	00	02.0	12.7	.	.	.	$= nj-8^{\circ}, \# nj-dp$
28	7	01•	02•	00	01.0	13.0	.	.	.	$= nj-11^{\circ}, \# nj-dp$
29	8	00•	03•	00	01.0	12.6	.	.	.	$= nj-11^{\circ}, \# nj-dp$
30	6	09	08•	03	06.7	08.2	.	.	.	$= nj-n, \# nj-dp, R^{\circ} 14^{\circ} 15^{\circ}, \# 15^{\circ} 15^{\circ}, \# 15^{\circ} 15^{\circ}$
31	8	00•	08•	00	02.7	10.6	00.0	.	.	$= nj-8^{\circ}, R^{\circ} 12^{\circ}, \# 13^{\circ}, \# 13^{\circ}, \# 14^{\circ}$

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1	8	00 0	07	10 0 R	05.7	10.2	00.0	.	$\equiv n-j-8^{30} \rightarrow 14^{30} 17^{45} - n; R^0-14^{30} - n$
2	7	00 0	06 0	09	05.0	09.1	.	.	$\equiv n-8^{30} 18^{30} n; \rightarrow 16^{30} 19^{30}; R^0-16^{30} 19^{30}$
3	8	09	06 0	00	05.0	10.6	03.6	.	$\equiv n-9^{30} 17^{30} n; \rightarrow 15-19^{30} R^0-18^{30} 19^{30}$
4	7	02 0	03 0	06	03.7	09.4	.	.	$\equiv n-j-11^{30} 17^{30} n; \rightarrow 15-19^{30} R^0-18^{30} 19^{30}$
5	7	00 0	07 0	08	05.0	04.9	00.3	.	$\equiv n-14^{30} n$
6	7	04 0	08 0	00	04.7	07.3	.	.	$\bullet^{+12^{30}} 16^{30} R^0 12^{30} 15^{30} 16^{30}, \nabla^{+15^{30}} 15^{30} \rightarrow 15^{30}$
7	7	01 0	10 0 R	03	04.7	07.2	11.6	.	$R^0-13^{30} 16^{30} n; \bullet^{+4-16^{30}} n, \nabla^{+2-15^{30}} 15^{30} F_{16} 15^{30}, \Delta^{+15^{30}} 16^{30}$
8	7	10	08 0	07	08.3	05.0	21.2	.	$\bullet^{+18-8^{30}} 14^{30} 18^{30} n; \nabla^{+17-15^{30}} 16^{30}, R^0-16^{30} 16^{30}$
9	6	09	09 0	10	04.3	04.6	04.6	.	$\equiv n-n, \Delta' n-dp$
10	6	03 0	09 0	01	04.3	09.3	.	.	$= n-13^{30}, 19^{30} n, \Delta' n-j-19^{30}$
11	6	00 0	03 0	03	02.0	09.6	.	.	$\Delta' n-j-8^{30} \nabla^{+0-1} n-j-8^{30}$
12	6	10	08	10	04.9	04.9	07.1	.	$R^0-17^{30}-6^{30} 15^{30} 16^{30}, \bullet^{+1-4^{30}} 6^{30} i, 15-16, \nabla^{+1-4^{30}} 5^{25} 5^{25} 16-17^{32} i$
13	6	10	09	07	06.7	02.3	04.4	.	$\equiv n-13^{30} \bullet^{+0-1} 10^{30} 12^{30} n$
14	6	00 0	01 0	01	00.7	10.9	01.7	.	$\equiv n-14^{30} 20-0$
15	6	00 0	05 0	06	04.3	10.6	.	.	$= n-13^{30}, 19^{30} n, \Delta' n-8^{30}$
16	7	07	09	01	05.7	03.1	.	.	$\Delta' n-8^{30} \bullet^{+0-1} 15^{30} 17^{30} i, \nabla^{+16^{30}} 16^{32}, R^0 16^{30} 16^{35} i$
17	6	10 30	03 0	02	05.0	06.7	04.3	.	$\equiv n-7^{30} n = 7^{30} n$
18	6	08	10	10 30	09.3	02.5	.	.	$\equiv n-14^{30} \Delta' n-dp, \bullet^{+0-11^{30}} 14^{34} 15^{30} 20^{30}, \nabla^{+0-14^{30}} 14^{34}$
19	8	10	08 0	01	04.3	03.2	03.0	.	$\bullet^{+0-10^{30}} n$
20	6	00 0	04 0	01	01.7	12.1	.	.	$= n-n, \Delta' n-dp$
21	7	00 0	02 0	00	00.7	12.4	.	.	$= n-14^{30} \Delta' n-dp$
22	7	00 0	01 0	00	00.3	12.3	.	.	$\equiv n-9^{30} \Delta' n-dp$
23	8	00 0	08 0	04	04.0	12.1	.	.	$= n-10^{30} 19^{30} n$
24	6	00	10	10	09.3	01.8	.	.	$\equiv n-n, R^0 14^{30} 15^{30}, \nabla^{+0-14^{30}} 15^{30} 17^{30} 19^{30}$
25	7	10	10	10	10.0	01.3	02.6	.	$\Delta' n-dp, = n-n, R^0 14^{30} 15^{30} \bullet^{+0-14^{30}} 20^{30}$
26	6	10	10	10	10.0	00.6	10.7	.	$\Delta' n-dp, \bullet^{+0-10^{30}} 15^{30} 15^{30} 16^{30} \rightarrow 10-17^{30}$
27	7	10	10	10	10.0	01.3	00.4	.	$F_{16} 10-17^{30} n, \bullet^{+0-10^{30}} 20^{30} 22^{30} n$
28	7	10	10 30	10	10.0	00.6	00.6	.	$F_{16} 10-12, \bullet^{+0-10^{30}} 12^{30} 18^{30} i, \nabla^{+5^{30}} 5^{30}$
29	5	10	10	07	09.0	00.3	03.6	.	$= n-n$
30	8	10 30	10	09	00.3	04.7	.	.	$\Delta' n-dp, \equiv n-\delta^{30} = 8^{30} 10^{30} 8^{30} 13^{30} 15^{30} i$
31	7	08	07 0	01	05.3	05.5	00.6	.	$\Delta' n-dp, = n-12^{30}, R^0 10^{30} 10^{30} n$

$\varphi = 45^{\circ}49' \text{ N } \lambda = 15^{\circ}59' \text{ E } \Delta G = + 1h \text{ 04 min.}$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, I (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	749.5	749.4	749.6	16.1	25.6	20.3	20.6	25.6	15.3	-	12.5	14.8	13.2	91	60	74	75	-	0	SSE 2	N 2
2	749.6	748.6	747.3	17.2	24.8	20.5	20.8	25.2	16.6	-	13.2	14.1	14.3	90	60	79	76	SSE 1	SSE 2	NNE 2	
3	745.6	744.9	744.0	18.3	23.6	19.4	20.2	23.9	17.3	-	14.4	16.3	14.2	90	75	84	83	ENE 1	SSE 2	NNE 1	
4	744.5	745.1	745.4	17.0	24.5	19.5	20.1	24.9	16.7	-	13.0	12.7	15.2	89	62	89	80	NNE 1	S 1	NNE 1	
5	745.6	744.8	746.4	16.4	24.0	18.5	19.4	25.0	16.2	-	13.2	14.1	11.5	94	63	72	76	SSE 1	SSW 2	ENE 1	
6	747.7	747.4	747.9	16.1	24.7	19.0	19.7	24.7	15.6	-	12.1	14.2	13.8	88	61	84	78	E 1	SSW 2	SSE 1	
7	746.3	747.0	748.3	16.8	15.8	16.1	16.2	19.0	15.8	-	13.8	12.9	12.6	96	96	92	95	WNW 2	WSM 3	WSW 2	
8	752.2	753.0	753.5	16.1	21.0	16.7	17.6	21.1	14.9	-	12.1	11.2	0.9	88	58	67	71	NNW 1	NE 2	NNE 2	
9	753.5	751.9	751.1	13.1	20.8	17.1	17.0	21.0	12.1	-	0.9	11.6	10.8	80	63	74	72	SW 1	SSE 2	NNE 2	
10	750.6	749.6	749.2	13.2	21.8	16.8	16.2	22.0	12.6	-	10.0	11.6	10.7	88	59	66	71	ENE 1	SSE 2	NNE 1	
11	748.1	747.0	745.8	16.1	21.7	19.3	19.1	22.1	15.7	-	0.9	7.1	11.5	12.1	71	59	72	67	ENE 2	SE 2	NNE 2
12	744.8	743.4	742.2	16.3	22.9	17.5	18.6	23.2	16.2	-	13.5	13.8	12.9	97	66	86	83	NW 1	SSE 2	NE 2	
13	745.4	749.3	750.2	14.3	13.9	12.3	13.3	17.5	12.3	-	0.9	0.9	0.9	73	83	85	80	NNE 2	SSE 2	N 2	
14	748.9	746.5	745.7	09.1	18.0	17.1	15.5	19.8	09.1	-	0.6	11.3	13.2	94	73	90	86	ESE 1	E 1	N 1	
15	746.1	746.8	748.5	14.3	24.1	21.0	20.1	24.3	13.9	-	11.9	14.6	12.5	97	65	67	76	NNE 1	ESE 2	NNE 2	
16	752.7	753.8	754.1	17.3	27.3	25.2	23.8	27.6	16.6	-	13.6	17.7	14.2	92	65	59	72	ENE 1	WSM 3	WNW 3	
17	755.9	756.3	756.7	18.4	27.2	23.7	23.4	28.3	18.1	-	12.1	16.1	18.2	86	57	83	75	NE 1	SSE 1	NNE 2	
18	756.1	755.1	755.1	20.1	26.6	22.0	22.7	26.7	19.8	-	16.2	12.3	15.3	92	47	77	72	-	0	ESE 3	NNE 2
19	754.6	753.9	753.7	16.9	23.8	20.1	20.2	23.9	16.6	-	11.2	11.5	11.1	78	52	63	64	NE 1	ENE 2	NNE 2	
20	753.4	752.9	753.0	15.0	24.0	20.4	20.0	24.0	14.7	-	10.8	11.4	11.2	85	51	62	66	-	0	ESE 2	N 2
21	753.3	753.3	754.2	15.3	23.7	20.5	20.0	24.2	15.0	-	11.4	11.8	12.1	88	54	67	70	NW 1	E 2	NNE 2	
22	755.7	756.3	756.9	15.1	23.3	19.9	19.6	23.6	14.4	-	11.7	12.7	11.5	91	59	66	72	-	0	NE 2	NNE 2
23	756.6	755.1	754.0	16.4	22.7	18.5	19.0	22.8	15.9	-	12.3	13.2	14.2	88	64	89	80	WSW 1	ESE 2	WNW 1	
24	753.1	751.8	750.9	14.6	22.0	17.5	17.9	22.3	14.5	-	12.2	13.5	12.6	98	68	84	83	NNW 1	SSW 2	NNE 1	
25	749.4	747.8	747.3	15.3	23.4	17.5	16.4	23.8	14.4	-	12.6	11.2	11.6	97	52	77	75	WNW 1	SSW 3	WSW 2	
26	744.6	743.2	746.2	15.9	23.7	17.9	18.9	24.3	14.5	-	0.9	7.7	9.9	72	45	88	68	WSW 2	SSW 5	WNW 1	
27	750.8	752.1	752.5	15.3	19.2	17.7	17.5	20.4	15.4	-	10.8	13.2	13.7	82	79	90	84	ESE 2	NNE 1	WNW 2	
28	752.4	752.7	753.8	16.3	26.0	19.9	20.5	26.0	16.0	-	12.0	12.6	14.4	86	50	83	73	W 2	WNW 3	WNW 2	
29	753.1	752.2	752.8	15.9	26.5	21.7	21.5	26.5	15.5	-	11.9	12.8	14.2	88	49	73	70	SSW 2	WNW 3	NNE 2	
30	751.7	749.8	749.2	16.5	23.8	20.4	20.3	24.0	16.2	-	12.7	14.4	14.4	90	65	80	78	W 1	ESE 2	N 2	
MES.	VRED. 750.4 750.0 750.2			15.9	23.0	19.2	19.3	23.6	15.3	-	11.9	13.0	12.9	88	62	77	76	1.1	2.2	1.7	

1	749.9	749.7	750.1	15.6	24.1	21.1	20.5	24.5	15.5	-	12.6	14.4	14.2	95	64	76	78	W 1	SSE 2	N 2
2	750.7	752.9	753.6	17.6	18.7	17.4	17.8	21.1	17.3	-	13.8	15.2	14.2	91	94	95	93	WSM 1	N 1	NW 2
3	752.8	751.7	751.1	13.7	21.5	17.1	17.4	21.5	13.3	-	11.2	14.6	12.6	95	76	86	86	ESE 1	SSE 2	NNE 1
4	753.4	752.6	753.7	16.1	17.9	15.7	16.4	18.3	14.4	-	11.6	0.9	2.0	84	60	68	71	E 2	NE 2	N 2
5	755.7	755.1	755.8	12.3	16.7	11.2	12.9	17.5	11.2	-	0.70	0.60	0.07.6	66	42	76	61	NE 1	NNE 2	NNW 1
6	756.4	756.3	755.8	10.0	16.8	11.6	12.5	17.3	09.2	-	0.61	07.7	08.0	88	54	78	73	S 1	SW 1	N 1
7	753.5	750.9	750.4	08.2	17.8	14.6	13.8	18.2	08.2	-	0.73	09.5	09.1	92	62	73	76	WSM 1	ESE 2	NNE 2
8	752.1	751.0	751.3	10.6	16.7	12.9	13.3	17.3	09.8	-	0.81	06.8	06.2	84	48	55	62	NNW 2	SSE 2	NE 2
9	750.6	749.1	749.0	10.4	11.9	08.4	09.8	12.9	08.4	-	0.57	05.8	06.4	60	55	78	64	NNE 1	N 1	NNE 1
10	747.1	746.0	746.1	07.6	12.4	08.6	09.3	12.6	07.2	-	0.66	06.2	07.0	84	57	82	74	ENE 1	ENE 2	N 3
11	747.7	749.5	751.3	07.0	09.9	08.0	08.2	09.9	07.0	-	0.66	05.9	05.8	88	65	72	75	NNE 3	NE 2	NNE 3
12	752.4	751.3	750.3	04.6	04.8	08.4	07.5	09.1	05.6	-	0.57	06.6	07.7	78	90	82	87	NE 3	NNE 3	NNW 3
13	748.0	744.6	743.9	08.1	08.0	08.0	08.0	08.5	07.5	-	0.78	07.6	07.6	95	94	94	94	NE 2	W 2	N 2
14	742.8	743.1	747.1	07.7	09.6	08.9	08.8	10.3	07.5	-	0.77	08.6	08.0	97	94	95	95	NE 1	WSW 2	W 1
15	746.3	746.5	749.0	07.5	08.6	08.0	08.0	10.3	07.0	-	0.75	07.0	07.6	96	82	95	91	S 1	WSM 1	NNE 1
16	747.8	745.9	743.7	04.9	11.5	11.3	10.3	11.6	06.2	-	0.72	07.4	09.2	97	72	92	87	NE 1	ENE 1	NE 3
17	738.3	736.3	736.5	10.9	11.5	10.6	10.9	11.6	10.5	-	0.92	09.4	09.4	95	93	96	95	NE 2	SSW 1	NNW 1
18	740.3	741.4	742.2	08.1	11.2	10.1	09.9	11.5	07.7	-	0.80	08.9	08.8	97	89	95	94	NNW 1	ESE 2	WNW 1
19	743.7	744.0	746.1	09.9	13.0	10.7	11.1	13.1	09.4	-	0.64	07.6	08.4	93						

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 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacija broj soči	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena	
		14	7	14	21	Sred Dies				7	7
1	6	000	060	00	C2.0	C5.2	.	.	.	$\Delta^2 n - dp = n - ni$	
2	6	050	070	06	04.3	C5.8	.	.	.	$= n - 15^{\circ}, 17^{\circ} n; \Delta^2 n - dp$	
3	5	C9	090	01	06.3	02.6	.	.	.	$= n - n, \Delta^2 n - dp, 0^{\circ} 8^{\circ} 25^{\circ}, 13^{\circ} 15^{\circ}, \Delta^2 n - 10^{\circ} 55^{\circ}$	
4	6	010	070	C1	03.0	06.2	0C.5	.	.	$= n - n, \Delta^2 n - dp, 13^{\circ} 15^{\circ}, \Delta^2 n - 17^{\circ} 10^{\circ}, \Delta^2 n - 17^{\circ} 24^{\circ}$	
5	6	00=	09	10	06.3	05.5	C2.0	.	.	$\Delta^2 n - dp, = n - 0^{\circ}, 9^{\circ} 16^{\circ}, = 0^{\circ} 6^{\circ} 19^{\circ} 15^{\circ}$	
6	8	010	050	02	02.7	C5.7	.	.	.	$\Delta^2 n - dp = n - 11^{\circ} 15^{\circ} 18^{\circ} 30^{\circ}$	
7	7	100	100	100	10.0	00.0	0C.4	.	.	$R^{\circ} - 6^{\circ} 6^{\circ} 6^{\circ}, H^{\circ} 15^{\circ}, \Delta^2 n - 16^{\circ} 16^{\circ} i, 20^{\circ} 55^{\circ} 21^{\circ} 0$	
8	6	10	09	00	06.3	05.6	02.4	.	.	$= n - n$	
9	7	000	040	00	01.3	08.1	.	.	.	$= n - n$	
10	7	000	000	01	00.3	10.4	.	.	.	$= n - 11^{\circ}$	
11	7	060	09	10	08.3	06.6	.	.	.	$= n - 12^{\circ} 0^{\circ}, 18^{\circ} 15^{\circ} n; \Delta^2 n - 15^{\circ} 15^{\circ} 15^{\circ}$	
12	8	100	070	05	C7.3	04.5	C5.5	.	.	$= n - 10^{\circ} 10^{\circ} 10^{\circ}, 17^{\circ} 20^{\circ} n; \Delta^2 n - 9^{\circ} 28^{\circ} 28^{\circ}, \Delta^2 n - 6^{\circ} 0^{\circ} 7^{\circ} 22^{\circ}$	
13	7	10	10	03	07.7	00.2	08.1	.	.	$= n - 9^{\circ} 0^{\circ}, = 9^{\circ} 0^{\circ} n$	
14	6	10=	09	00	06.3	06.6	0C.8	.	.	$\Delta^2 n - dp, = n - 7^{\circ} 3^{\circ}, = 7^{\circ} 3^{\circ} 14^{\circ} 45^{\circ}$	
15	6	09=	070	01	05.7	08.4	.	.	.		
16	5	07	050	06	06.0	07.3	.	.	.	$= n - 14^{\circ}, \Delta^2 n - dp$	
17	6	000	000	00	00.0	09.1	.	.	.	$\Delta^2 n - dp, = n - n$	
18	6	000	010	01	00.7	C5.4	.	.	.	$\Delta^2 n - dp, = n - n$	
19	6	000	010	00	00.3	10.4	.	.	.	$= n - n, \Delta^2 n - dp$	
20	6	000	010	00	00.3	10.0	.	.	.	$= n - n, \Delta^2 n - dp$	
21	6	000	020	00	00.7	06.1	.	.	.	$= n - n, \Delta^2 n - dp$	
22	6	00	030	00	01.0	04.4	.	.	.	$= n - n, \Delta^2 n - dp$	
23	6	08	06	08	07.3	04.6	.	.	.	$= n - n, \Delta^2 n - dp$	
24	5	10=	070	00	05.7	05.5	.	.	.	$\Delta^2 n - 8^{\circ} 30^{\circ}, = 2^{\circ} 4^{\circ} n = 9^{\circ} 0^{\circ} n$	
25	6	10=	000	00	03.3	06.2	.	.	.	$\Delta^2 n - dp, = n - 9^{\circ} 0^{\circ}, = 9^{\circ} 0^{\circ} n$	
26	8	000	09	100	06.3	06.2	.	.	.	$= n - 11^{\circ} 0^{\circ}, \Delta^2 n - dp, P 10^{\circ} 17^{\circ} 1^{\circ} 19^{\circ} 44^{\circ} 21^{\circ} 0$	
27	6	09	060	00	05.0	02.5	0C.6	.	.	$= n - n, 4^{\circ} 10^{\circ} 10^{\circ}, 11^{\circ} 5^{\circ}$	
28	7	080	070	00	05.0	07.8	0C.2	.	.	$= n - 12^{\circ} 30^{\circ}$	
29	7	010	010	00	00.7	09.4	.	.	.	$= n - 12^{\circ} 15^{\circ}, 18^{\circ} 30^{\circ} n$	
30	6	080	090	00	05.7	07.6	.	.	.	$= n - n, \Delta^2 n - dp$	
MES.		04.6	05.5	02.5	04.2	200.5	29.1				

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1	6	10=	010	00	03.7	06.5	.	.	.	$= n - 9^{\circ} 0^{\circ}, = 9^{\circ} 0^{\circ} 13^{\circ} 30^{\circ}$	
2	5	050	09	10	09.3	01.5	00.0	.	.	$= n - n, 6^{\circ} 3^{\circ} 13^{\circ} 15^{\circ}, R^{\circ} 0^{\circ} 17^{\circ} 15^{\circ} 10^{\circ}$	
3	6	020	040	00	02.0	05.5	10.2	.	.	$= n - n, 7^{\circ} 4^{\circ} 9^{\circ} 45^{\circ}$	
4	8	09	09	10	09.3	01.9	.	.	.	$= n - 8^{\circ} 4^{\circ} 17^{\circ} 15^{\circ} n$	
5	8	10	09	01	06.7	06.4	.	.	.	$= n - 9^{\circ} 0^{\circ}, 18^{\circ} n$	
6	8	09	09	00	06.0	00.7	.	.	.	$= n - 10^{\circ} 30^{\circ}$	
7	6	010	010	06	02.7	C6.9	.	.	.	$= n - 12^{\circ} 0^{\circ}, 18^{\circ} n; \Delta^2 n - 9$	
8	8	000	060	07	04.3	07.2	.	.	.	$\Delta^2 n - 11^{\circ} 30^{\circ}, \Delta^2 n - dp$	
9	7	10	09	00	06.3	00.8	.	.	.	$\Delta^2 n - 7^{\circ} 30^{\circ}, \Delta^2 n - 12^{\circ} 30^{\circ}$	
10	6	10	10	100	10.0	00.0	00.0	.	.	$= n - n, 6^{\circ} 0^{\circ} 19^{\circ} 30^{\circ} n$	
11	6	100	09	100	09.7	00.8	06.2	.	.	$= n - n, 0^{\circ} - 1^{\circ} n - 8^{\circ} 45^{\circ} i, 18^{\circ} 20^{\circ} K V$	
12	5	100	100	100	10.0	00.0	00.9	.	.	$= n - n, 0^{\circ} - 6^{\circ} 2^{\circ} 13^{\circ} 20^{\circ} i$	
13	5	100	100	100	10.0	00.0	20.2	.	.	$= n - n, 0^{\circ} - 1^{\circ} n - 17^{\circ} 20^{\circ}, 20^{\circ} n; R^{\circ} 0^{\circ} 19^{\circ} 9^{\circ} 45^{\circ}, 16^{\circ} 45^{\circ}$	
14	5	100	100	07	09.8	00.0	17.9	.	.	$= n - n, 0^{\circ} - 4^{\circ} 3^{\circ}, 9^{\circ} 45^{\circ} n, \Delta^2 K V - n$	
15	6	10=	06	01	05.7	02.6	02.0	.	.		
16	5	09=	09	100	04.3	00.5	.	.	.	$= n - n, 7^{\circ} 30^{\circ}, \Delta^2 n - 10^{\circ} - 11^{\circ} 44^{\circ} n$	
17	5	100	100	10	16.0	06.6	22.8	.	.	$= n - n, 0^{\circ} - 7^{\circ} 30^{\circ}, 19^{\circ} 30^{\circ} i$	
18	6	10	10	10	10.0	00.6	08.8	.	.	$= n - n, 10^{\circ} 30^{\circ}, \Delta^2 n - 17^{\circ} 30^{\circ}$	
19	7	10	09	10	09.7	01.0	00.3	.	.	$= n - n, 10^{\circ} 30^{\circ}, \Delta^2 n - 17^{\circ} 30^{\circ} i$	
20	6	10	10	100	10.0	00.6	00.6	.	.	$= n - n, 0^{\circ} - 10^{\circ} - 12^{\circ}, 14^{\circ} 20^{\circ} i$	
21	6	04	10	09	07.7	00.7	00.4	.	.	$= n - n$	
22	5	10	10	09	09.7	00.0	.	.	.	$= n - n$	
23	5	10	09	09	09.3	03.6	00.0	.	.	$\Delta^2 n - n - 13^{\circ} 17^{\circ} n$	
24	5	10	030	00	04.3	03.7	.	.	.	$= n - n, \Delta^2 n - dp$	
25	5	00	010	00	00.3	07.4	.	.	.	$= n - n, \Delta^2 n - dp$	
26	6	01	040	00	01.7	06.9	.	.	.	$= n - 14^{\circ}, \Delta^2 n - dp$	
27	5	00	020	00	00.7	07.7	.	.	.	$= n - n, \Delta^2 n - dp$	
28	6	000	000	00	0C.0	08.2	.	.	.	$= n - n, \Delta^2 n - dp$	
29	6	01	000	00	00.3	08.2	.	.	.	$= n - n, \Delta^2 n - dp$	
30	4	10=	010	00	03.7	09.7	.	.	.	$\Delta^2 n - dp, = n - 12^{\circ} 15^{\circ}, = 12^{\circ} 15^{\circ} n$	
31	3	10=	01=	01=	10=	07.0	03.8	.	.	$\Delta^2 n - dp, = n - 2^{\circ} n - 14^{\circ} 45^{\circ} n$	
MES.		07.3	06.5	05.5	06.4	99.4	52.7				

VIDLJIVOST OSMATRANA U 13 ČASOVA

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h\ 04\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	750.8	750.6	751.0	04.4	06.5	06.6	06.2	06.9	04.3	-	06.2	06.9	07.0	97	95	94	95	NNE 1	ESE 1	ENE 1	
2	751.6	752.5	755.5	06.6	10.7	08.6	08.7	10.7	06.5	-	07.2	08.2	08.0	97	85	94	94	ESE 1	E 2	ES E 1	
3	756.3	755.7	756.0	08.1	09.7	09.1	09.0	09.8	08.1	-	07.4	08.0	08.0	91	88	91	90	SSE 1	SSW 1	SW 1	
4	758.2	758.9	758.9	08.7	10.3	10.4	10.0	10.4	08.6	-	08.0	06.8	07.1	94	73	75	81	ENE 2	NE 2	NNE 2	
5	757.8	757.1	757.1	08.8	09.5	08.5	08.8	10.4	08.0	-	06.7	06.5	06.5	79	73	76	77	NNE 2	NNE 2	NNE 2	
6	755.8	754.5	754.6	07.7	08.6	08.0	08.1	09.0	07.6	-	06.1	06.4	06.6	77	75	82	78	NNE 2	SE 1	SE 1	
7	753.6	753.0	753.4	07.8	09.7	08.7	08.7	10.0	07.5	-	06.5	06.6	07.0	82	73	82	79	SE 1	SE 1	NE 2	
8	754.3	753.8	753.4	07.4	10.9	08.4	08.8	11.0	07.2	-	06.0	06.0	05.3	78	62	65	66	ENE 2	NE 2	NE 3	
9	751.0	750.4	750.9	06.7	05.4	06.1	06.1	08.4	05.4	-	05.0	05.6	06.6	67	65	93	84	ENE 2	NE 2	NNE 2	
10	751.4	750.4	749.9	05.7	06.5	06.1	06.1	06.8	05.5	-	06.6	06.5	06.6	96	90	93	93	ENE 1	ESE 2	NNE 1	
11	752.0	753.3	754.0	06.2	06.5	06.5	06.4	06.8	05.8	-	06.6	06.2	06.4	92	85	89	89	W 1	ENE 1	WSW 1	
12	756.1	756.8	758.2	05.6	07.7	05.0	05.8	07.8	04.9	-	06.2	05.7	05.7	91	72	67	83	ENE 2	ESE 2	ENE 2	
13	758.1	757.3	756.9	05.8	08.0	06.4	06.8	08.1	04.9	-	06.0	06.6	06.5	87	82	68	86	NE 1	ESE 1	ENE 1	
14	755.2	754.1	754.3	06.0	05.3	04.8	05.2	06.6	04.8	-	06.6	05.7	05.4	94	86	83	86	NE 1	E 2	ENE 2	
15	753.9	752.9	752.0	04.6	07.5	06.0	06.0	07.6	04.2	-	05.8	05.2	05.2	91	67	74	77	W 1	NE 1	NNE 1	
16	747.1	741.8	739.0	03.5	03.3	01.8	02.6	06.0	01.8	-	05.2	04.5	04.9	88	76	94	87	NE 1	NE 1	ENE 2	
17	734.8	734.5	734.8	02.1	03.3	04.3	03.5	04.3	01.5	-	05.2	05.1	05.6	95	88	90	91	NE 2	NE 2	NE 1	
18	733.3	733.2	737.1	05.5	07.2	05.9	06.1	08.8	04.3	-	06.5	07.0	06.5	96	91	94	94	E 1	WSW 1	WNW 1	
19	741.2	745.4	746.1	05.3	12.7	05.7	07.4	12.9	05.3	-	06.2	05.6	04.8	93	51	70	71	WNW 1	WNW 2	NNE 2	
20	742.3	739.0	738.6	04.7	06.9	08.9	07.4	09.3	04.7	-	05.2	06.4	06.0	80	87	71	79	SE 1	WSW 2	W 4	
21	744.0	747.1	749.7	05.3	08.0	01.8	04.2	09.6	00.1	-	05.8	02.6	02.7	87	32	51	57	E 2	N 3	ENE 1	
22	745.4	743.5	748.2	-01.8	03.2	02.2	01.5	04.3	-01.8	-	02.8	03.0	02.5	70	31	47	56	W 1	WSW 2	N 1	
23	751.0	751.7	753.5	00.5	01.3	-00.8	00.1	02.2	-00.8	-	02.4	02.6	02.5	49	52	57	53	NNE 4	NNE 4	NNE 3	
24	753.4	752.6	753.8	-01.8	01.4	-01.3	-00.8	01.5	-02.1	-	02.6	02.2	02.4	64	45	58	56	N 3	ENE 3	WNW 1	
25	755.0	754.6	753.9	-05.1	00.0	-02.6	-02.6	00.2	-05.1	-	02.4	02.8	02.8	77	55	72	69	N 1	SW 2	- 0	
26	752.4	750.7	750.6	-06.4	01.4	00.2	-01.2	01.5	-06.6	-	02.4	02.0	02.6	84	39	56	60	SW 1	SSW 2	SSW 1	
27	749.8	749.2	748.9	-01.1	03.3	03.5	02.3	04.3	-02.0	-	02.8	03.4	03.9	68	66	65	65	ENE 2	E 2	NE 1	
28	746.4	744.7	745.0	02.9	05.3	02.8	03.5	05.5	02.8	-	03.6	05.6	05.0	64	89	79	79	ENE 2	WSW 1	NW 1	
29	744.4	744.0	744.4	02.6	06.6	05.4	05.0	06.6	02.1	-	05.0	06.0	06.2	90	81	92	88	WSW 1	SE 1	SE 1	
30	745.3	744.0	743.8	03.9	08.0	06.7	06.3	08.0	03.6	-	05.8	07.0	06.6	97	87	89	91	SE 1	SSW 2	NE 2	
MES.	VRED.	750.1	749.5	750.1	04.0	06.5	05.1	05.2	07.2	03.4	-	05.4	05.4	05.4	84	72	79	78	1.5	1.6	1.4

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1	744.1	745.7	749.8	08.3	09.2	06.0	07.4	09.7	06.0	-	05.8	07.6	06.4	71	87	92	83	NE 2	SSE 1	WW 1
2	749.1	747.8	747.6	05.0	05.9	05.9	05.7	06.0	05.0	-	06.0	06.4	06.4	93	90	90	91	SW 1	SSW 2	SSE 1
3	747.8	746.6	749.9	05.3	06.0	06.8	06.2	06.8	05.3	-	06.2	06.4	07.0	93	90	94	92	S 2	SSE 1	WSW 2
4	750.0	750.6	758.3	04.0	05.9	06.0	05.5	06.8	04.0	-	06.0	06.6	06.6	99	96	95	97	NE 1	SSE 1	SSE 1
5	756.9	756.2	755.6	04.4	04.5	04.9	04.7	06.0	03.3	-	05.4	05.8	05.8	87	93	90	90	NNW 1	SSE 1	WSW 1
6	753.0	748.3	748.4	02.6	07.6	07.0	04.1	10.7	02.4	-	05.2	06.2	05.6	93	78	75	82	WSW 2	SW 3	NNE 2
7	753.5	754.2	752.9	03.8	06.2	02.7	03.9	07.1	02.4	-	04.1	04.1	04.2	69	57	74	67	E 2	SSW 2	WNW 1
8	747.6	747.8	750.6	00.3	06.1	04.4	03.8	06.3	00.0	-	03.2	04.4	04.4	70	62	72	68	WSM 2	SE 1	NNE 3
9	754.1	754.8	754.9	02.8	06.8	04.8	04.8	06.8	02.8	-	04.4	03.6	03.7	78	49	57	61	NNE 1	ESE 2	NE 1
10	754.0	754.0	756.1	03.0	05.3	03.0	03.6	05.6	02.9	-	03.9	04.0	03.8	69	59	65	64	ENE 1	ENE 1	NE 1
11	757.0	756.8	756.6	00.8	04.5	03.6	03.1	04.7	-00.1	-	04.3	04.5	04.6	83	72	80	78	ENE 1	SW 1	NE 2
12	754.1	751.4	750.0	00.6	01.5	-00.1	00.5	03.6	-00.1	-	04.4	04.4	04.0	91	85	89	88	ENE 2	E 1	ENE 2
13	747.8	747.7	750.5	00.6	02.0	01.1	01.2	02.0	-00.0	-	04.4	04.4	04.2	91	84	85	87	SE 1	SSE 1	NNW 2
14	753.6	754.9	757.4	01.1	01.2	01.2	01.2	01.5	00.7	-	04.6	04.4	04.2	93	87	83	88	NNE 2	NE 2	ENE 2
15	757.7	756.6	756.6	00.4	01.5	01.7	01.3	02.0	00.2	-	04.2	04.7	04.2	89	94	82	88	NE 2	ESE 2	ESE 2
16	753.8	749.4	745.6	00.9	02.1	02.0	01.8	02.1	00.5	-	04.4	04.8	04.8	91	90	89	90	NNE 1	ENE 1	WSM 1
17	739.7	735.3	732.2	02.4	04.2	04.5	03.9	05.1	02.0	-	05.0	05.9	06.0	92	95	95	94	ENE 1	E 1	SSW 2
18	741.2	745.8	749.9	02.3	02.7	00.8	01.7	04.5	-00.8	-	05.1	04.8	03.0	94	86	62	81	ENE 2	WNW 1	NE 2
19	752.5	753.0	754.0	-03.1	-01.3	-03.3	-02.8	00.8	-03.3	-	02.4	02.8	02.6	67	65	66	67	NE 2	NE 2	NE 1
20	755.9	757.3	760.5	-05.6	-00.2															

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 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_x = 2.0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insekcija broj sati	Padavina R mm	Snežni potkrivac h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	3	10≡	10≡	10	10.0	00.0	00.0	.	$\Delta^0 n - dp \equiv^0 n - 16^{45} = 16^{45} n, \bullet KV - n$		
2	5	10≡	00○	10	06.7	03.0	00.1	.	$\equiv^0 n - 14^{30} = 14^{30} - n$		
3	5	10	10	10	10.0	00.0	.	.	= n - n		
4	5	10	10	10	10.0	00.0	00.4	.	$\equiv n - n, \bullet n, \bullet^0 n - 6^{30}$		
5	5	10	10	10	10.0	00.0	.	.	= n - n		
6	5	10	10	10	10.0	00.0	.	.	= n - n		
7	5	10	10	10	10.0	00.0	.	.	= n - n		
8	6	10	09	10	09.7	00.0	.	.	$\equiv n - n, \bullet^0 n - 9^{30} 11^{30} 13^{45} ni$		
9	6	10	10○	10○	10.0	00.0	.	.	$\bullet^0 n - nj, 14^{45} n, \equiv^0 nj - \theta, = \theta - n$		
10	5	10≡	10	10○	10.0	00.0	01.6	.	$\equiv n - n, \bullet^0 n - nj$		
11	5	10	10	10	10.0	00.0	21.3	.	$\equiv n - n, \bullet^0 n - nj$		
12	6	10	09	10	09.7	00.5	00.1	.	$\equiv n - n, \bullet^0 n - nj$		
13	5	10	10	10	10.0	00.0	.	.	$\equiv n - n, \bullet^0 n - 8^{45} 10^{45} KV, \equiv^0 n - 9^{30}$		
14	6	10○	10	10○	10.0	00.0	01.8	.	$\bullet^0 n - 8^{45} 10^{45} KV, \equiv^0 n - 9^{30}, = 9^{30} n$		
15	5	10	09	10	09.7	00.1	00.5	.	$\equiv n - n, \bullet^0 n - 9^{30} n, = 9^{30} n$		
16	6	10	10	10○	10.0	00.0	.	.	$\equiv n - n, \bullet^0 n - 14^{45} n$		
17	5	10○	10	10	10.0	00.0	03.3	.	$\bullet^0 n - 13^{45} = n - n$		
18	5	10≡	10○	09	09.7	00.0	10.2	.	$\bullet^0 n - 8^{45} 15^{45} n, \equiv^0 n - 9^{30} = 9^{30} n, \bullet^0 n - 12^{45} 12^{45} KV - w 12^{45}$		
19	6	01	02○	03	02.0	04.3	10.4	.	$\equiv n - n, \bullet^0 n - 8^{45} 15^{45} n$		
20	5	10	10	09	09.7	00.0	.	.	$\equiv n - n, \bullet^0 n - 10^{45} 16^{45} n$		
21	9	10	03○	00	04.3	07.5	01.3	.	$\equiv n - 10^{45} \bullet^0 n - 11^{30} n$		
22	8	01	08	00	03.0	02.2	.	.	$\bullet^0 n - 10^{45} \bullet^0 n - 11^{30} n$		
23	7	06	03*	00	03.0	02.8	.	.	$\bullet^0 n - 12^{45} \bullet^0 n - 11^{30} n$		
24	7	03	00○	00	01.0	07.3	00.0	.	$\equiv n - n, \bullet^0 n - n$		
25	6	00	00○	00	00.0	07.2	.	.	$\equiv n - n, \bullet^0 n - n$		
26	6	00	00○	00	00.0	06.8	.	.	$\equiv n - n, \bullet^0 n - n$		
27	6	08	09	05	07.3	00.4	.	.	$\equiv n - n, \bullet^0 n - 15^{45} n$		
28	3	09	09	09	09.0	00.0	.	.	$\equiv n - n, \bullet^0 n - 15^{45} n$		
29	4	10	10	10	10.0	00.0	00.0	.	$\equiv n - n, \bullet^0 n - 15^{45} n$		
30	5	10≡	09	01	04.7	01.5	.	.	$\Delta^0 nj - M^0, \equiv^0 nj - M, = M^{45} n$		
MES.	VRED.	08.3	07.7	07.2	07.7	45.6	51.2				

1	5	05	10○	10○	08.3	00.0	.	.	$\equiv^0 n - \bullet^0 n - 19^{45} ni$		
2	6	10	10	10	10.0	00.0	07.6	.	$\equiv n - n$		
3	6	10	10	10	10.0	00.0	.	.	$\equiv n - n$		
4	5	10	10	10	10.0	00.0	00.0	.	$\bullet^0 n - nj - 14^{45} 17^{45}, \equiv^0 n - 15^{45}, = n^{30} n$		
5	2	07	10≡	10	09.0	06.6	00.6	.	$= nj - 8^{45} 15^{45} n, \equiv^0 nj - 9^{45}, \equiv^0 n - 15^{45}$		
6	5	10	05○	00	05.0	06.4	.	.	$\equiv n - 15^{45}$		
7	8	02	04○	00	02.0	07.3	.	.	$\equiv n - 11^{45} 15^{45} n$		
8	6	03	00○	00	01.0	06.2	.	.	$\equiv n - n, \bullet^0 n - n, \bullet^0 n - dp$		
9	6	10≡	00○	09	04.3	04.0	.	.	$\equiv n - n$		
10	5	10	08○	00	06.0	00.1	.	.	$\equiv n - n$		
11	3	10	10≡	10	10.0	00.0	.	.	$\equiv n - 8^{45} 16^{45} n, \equiv^0 n - 18^{45} 16^{45}$		
12	4	10	10	10	10.0	00.0	.	.	$\equiv n - 7^{45} 10^{45} n, \equiv^0 n - 7^{45} 10^{45}$		
13	5	10	10	10	10.0	00.0	.	.	$\equiv n - 7^{45} 10^{45} n, \equiv^0 n - 7^{45} 10^{45}$		
14	5	10	10	10	10.0	00.0	00.0	.	$\equiv n - n, \bullet^0 n - 10^{45} n$		
15	4	10	10	10	10.0	00.0	00.0	.	$= nj - 9^{45} 12^{45} n, \bullet^0 n - 7^{45} 10^{45}, \equiv^0 n - 7^{45} 10^{45}, \equiv^0 n - 12^{45} 13^{45}$		
16	5	10○	10	10	10.0	00.0	00.1	.	$\equiv^0 n - \bullet^0 n - 17^{45} 19^{45}, \bullet^0 n - 10^{45} n, \bullet^0 n - 17^{45} 19^{45}$		
17	2	10	10○	10○	10.0	00.0	00.6	.	$\equiv^0 n - 12^{45} 17^{45} n, \bullet^0 n - 10^{45} n, \bullet^0 n - 17^{45} 19^{45}$		
18	5	10○	10	10	10.0	00.0	00.3	.	$\equiv^0 n - 17^{45} \bullet^0 n - 17^{45}, \bullet^0 n - 17^{45} 19^{45}$		
19	5	10	10	10	06.7	00.0	00.3	.	$\equiv^0 n - n, \bullet^0 n - 7^{45} 12^{45}$		
20	6	10	01○	10	07.0	03.6	00.2	.	$= n - n$		
21	6	10	07○	03	06.7	03.6	.	.	$\equiv^0 n - n$		
22	5	06	03○	00	03.0	06.2	.	.	$\equiv^0 n - dj - M^{45} = M^{45} n$		
23	5	00	00○	00	00.0	06.3	.	.	$\equiv^0 n - dj - M^{45}, \bullet^0 n - dj - M^{45}, \bullet^0 n - M^{45} n = 8^{30} 11^{30}$		
24	2	06≡	10≡	10≡	06.7	00.0	.	.	$\equiv^0 n - n, \bullet^0 n - nj - n$		
25	4	10	10	08	09.3	00.0	.	.	$\equiv^0 n - n, \bullet^0 n - nj - n$		
26	4	10	06	06≡	06.7	00.4	.	.	$\equiv^0 n - n = nj - 15^{45}, \equiv^0 n - 15^{45} n$		
27	5	10	07○	09	06.7	00.7	.	.	$\equiv n - dj, = n - n$		
28	5	00	00○	00	00.0	04.4	.	.	$\equiv^0 n - dj, \bullet^0 n - dj, \bullet^0 n - M^{45} n = 8^{30} 11^{30}$		
29	3	00≡○	00≡○	00≡○	00.0	04.6	.	.	$\equiv^0 n - n, \bullet^0 n - n, \bullet^0 n - n$		
30	1	10≡	10≡	10≡	10.0	00.0	.	.	$\equiv^0 n - n, \bullet^0 n - n, \bullet^0 n - n = nj - n, nj - n$		
31	2	10≡	10≡	10≡	10.0	00.0	.	.	$\equiv^0 n - n, \bullet^0 n - n, \bullet^0 n - n = nj - n, nj - n$		
MES.	VRED.	07.8	07.2	06.7	07.2	56.6	50.5				

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 $\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

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č	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodené pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	753.4	754.6	755.5	04.7	08.8	09.4	08.1	10.3	03.6	-	01.7	01.0	04.5	27	12	51	30	NE	7	NE	6	NNW	2
2	756.8	756.9	756.1	08.6	10.2	07.4	08.4	10.8	08.3	-	03.5	03.3	03.3	42	35	43	40	NW	2	NE	4	NE	5
3	758.5	757.3	758.3	06.1	09.1	07.2	07.4	09.2	06.0	-	02.7	02.9	02.4	39	34	32	35	NNE	4	NNE	5	NE	2
4	758.3	758.0	758.1	06.2	09.7	08.0	08.0	10.0	05.6	-	02.6	04.9	05.5	36	54	69	53	NNE	1	SW	1	NE	2
5	758.0	757.9	758.5	06.6	11.0	09.8	09.3	12.1	06.1	-	02.7	04.6	04.0	37	47	44	43	NE	1	SW	1	SW	1
6	757.1	756.0	755.6	07.2	11.5	09.0	09.2	11.6	06.5	-	03.2	04.7	06.1	42	46	71	53	NE	1	-	0	-	0
7	753.0	750.2	746.9	07.2	10.4	09.3	09.0	10.5	07.2	-	05.2	06.6	07.1	68	70	81	73	ENE	2	NE	2	ENE	1
8	744.5	743.0	746.2	08.4	08.6	06.5	07.5	09.5	05.6	-	06.2	07.3	04.1	75	87	57	73	NE	1	NE	2	NNE	3
9	754.6	756.0	760.6	04.4	04.9	03.2	03.9	07.9	03.2	-	02.6	02.0	01.7	41	30	29	33	NE	3	NNE	5	NE	1
10	760.1	759.7	760.7	02.2	07.8	06.2	05.6	08.6	02.0	-	01.9	03.9	04.1	35	49	57	47	NE	1	SE	1	E	1
11	760.5	760.1	760.1	03.9	09.1	06.8	06.6	09.3	03.8	-	03.7	05.0	04.8	62	57	65	61	NE	1	SW	1	SE	1
12	758.6	758.1	759.0	06.6	10.4	08.0	08.2	10.6	05.6	-	04.2	05.9	05.4	58	63	67	63	ESE	2	ESE	3	SE	2
13	759.7	759.3	760.0	06.7	10.6	09.2	08.9	10.7	06.4	-	04.9	06.6	05.9	67	69	68	68	SE	1	SE	1	NW	1
14	761.0	761.7	762.5	06.2	11.0	08.2	08.4	11.0	06.0	-	05.8	06.2	05.8	82	63	71	72	ENE	2	SW	1	-	0
15	762.5	761.8	760.9	06.4	10.8	09.4	09.0	11.1	05.6	-	04.4	06.6	06.9	62	68	78	69	SE	1	-	0	-	0
16	759.7	758.4	758.1	05.5	10.4	08.9	08.4	10.8	05.5	-	04.6	05.6	05.4	68	59	63	63	NE	2	SSW	1	-	0
17	757.0	755.8	755.9	06.9	10.9	08.6	08.8	11.2	06.4	-	05.2	07.1	06.0	70	73	72	72	NNE	2	SE	1	SE	1
18	754.2	752.6	752.1	06.5	11.0	10.2	09.5	11.7	06.1	-	05.7	06.9	07.1	78	70	76	75	ENE	2	SE	3	ESE	5
19	751.9	752.5	755.3	09.2	12.8	10.8	10.9	13.2	09.2	-	06.0	07.1	06.6	69	64	68	67	ESE	2	ESE	6	ESE	2
20	756.8	756.7	756.4	07.9	12.4	09.8	10.0	13.0	07.6	-	05.8	06.3	07.3	72	58	80	70	ENE	1	-	0	NE	2
21	756.5	756.5	756.1	07.2	11.1	08.8	09.0	11.4	06.2	-	04.1	05.8	06.2	54	58	73	62	NE	3	-	0	NW	2
22	756.1	756.0	755.5	06.5	11.1	07.6	08.2	11.5	06.0	-	04.4	04.8	03.9	60	48	50	53	NE	2	SW	1	NE	2
23	754.8	754.2	753.9	05.1	07.2	07.2	06.7	08.2	05.0	-	03.9	05.4	05.6	60	71	74	68	NE	1	NE	1	NNE	1
24	752.5	752.6	753.3	08.1	09.5	08.9	08.8	09.8	06.6	-	06.5	06.9	06.3	80	77	73	77	ESE	3	E	1	ENE	2
25	754.5	754.8	754.6	08.4	12.2	09.8	10.0	12.5	08.2	-	06.5	07.7	08.2	79	72	90	80	SE	1	-	0	-	0
26	754.2	755.0	755.3	09.4	11.2	10.5	10.4	12.1	09.3	-	07.6	07.8	07.8	85	79	81	82	NE	3	SSW	1	W	1
27	754.7	752.5	748.9	08.0	11.8	09.5	09.7	12.8	07.8	-	05.7	06.9	06.8	71	66	76	71	N	2	SE	1	SE	1
28	739.9	739.2	742.1	10.3	08.8	08.5	09.0	10.5	07.8	-	08.4	08.0	04.6	89	94	55	79	SE	5	-	0	NE	3
29	742.7	744.1	747.3	07.6	09.8	09.2	09.0	10.6	07.6	-	04.6	05.3	04.3	59	58	49	55	MNE	2	MW	2	MNW	3
30	749.4	749.7	752.4	06.2	09.3	09.6	08.7	10.5	06.1	-	03.5	04.5	04.1	50	51	45	49	N	2	MNW	1	MNE	4
31	754.6	755.4	755.4	06.8	11.8	09.4	09.4	12.0	05.2	-	02.9	03.6	02.4	39	35	27	34	MNE	4	SW	2	ENE	3
MES.	VRED.	755.0	754.8	755.3	06.8	10.2	08.5	08.5	10.8	06.2	-	04.5	05.5	05.3	60	59	62	60	2.2	1.7	1.7	1.7	1.7

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1	753.4	753.2	754.8	07.0	11.2	11.1	10.1	11.6	06.4	-	02.0	03.6	03.7	27	36	37	33	NE	2	S	1	NE	3
2	755.9	755.6	754.9	08.9	11.9	09.3	09.8	12.0	08.8	-	03.4	03.4	03.8	39	32	44	38	NE	2	ENE	4	NNE	2
3	751.7	752.8	754.8	09.0	10.2	05.8	07.7	10.8	05.8	-	04.2	03.5	02.6	48	37	38	41	ENE	4	NE	5	NE	5
4	756.6	758.1	759.0	05.2	11.0	07.4	07.8	11.2	05.0	-	02.6	03.9	03.3	39	40	43	41	NE	6	ESE	3	NNE	4
5	760.3	759.7	760.2	06.4	12.2	10.0	09.6	12.7	05.5	-	03.3	05.0	03.1	45	47	34	42	MNE	4	SSW	2	NNE	1
6	759.4	759.5	758.4	08.7	13.3	09.3	10.2	13.6	07.8	-	02.5	03.2	05.9	29	28	67	41	MNE	2	SSW	1	ESE	1
7	755.8	753.7	751.9	06.1	11.5	09.4	09.1	11.8	05.8	-	03.3	05.3	05.4	47	52	61	53	MNE	3	S	2	SSW	1
8	751.2	752.9	754.9	06.7	06.0	03.1	04.7	10.5	02.7	-	03.7	02.5	01.6	51	36	27	38	MNW	2	NNE	6	NNE	6
9	756.5	756.6	756.3	00.2	06.0	03.7	03.4	06.3	-00.3	-	01.7	02.0	03.2	36	29	53	39	NE	3	SW	1	NW	2
10	754.1	756.0	755.4	03.1	08.0	07.8	06.7	09.5	02.4	-	02.2	04.3	05.3	39	53	67	53	NE	1	SW	1	W	2
11	755.4	755.2	754.3	06.8	08.4	07.5	07.6	08.4	06.1	-	05.2	06.2	06.1	70	75	78	74	NE	2	E	2	E	3
12	752.4	751.0	748.9	07.8	10.4	10.0	09.6	10.5	07.1	-	05.6	06.5	06.1	71	69	66	69	E	1	ESE	5	SE	5
13	744.7	742.3	740.9	09.4	13.0	08.9	10.0	13.4	07.4	-	06.1	06.8	07.3	69	61	85	72	ESE	4	ESE	4	NW	2
14	739.3	740.7	743.4	10.1	11.5	09.5	10.2	13.2	08.1	-	06.6	07.7	07.1	71	76	80	76	E	4	MW	3	MNW	2
15	744.7	748.7	749.4	07.7	11.6	09.6	09.6	13.1	07.4	-	06.6	06.8	05.6	83	66	63	71	ENE					

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_x = 1.0 \text{ m}$

Dan	Vrhovost 0-9	Oblakost N (0-10)					Insektacija % b	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8 04	10	08	07.3	00.5	$F_{NE} 0-9^{\circ}$
2	8 05	02 ⁰	01	02.7	07.8
3	8 09	01 ⁰	00	03.3	06.2
4	8 01	00 ⁰	00	00.3	08.4
5	8 03	05 ⁰	00	02.7	05.9
6	8 00	00 ⁰	00	00.0	08.1
7	8 04	10	09	07.7	01.5
8	6 10	10 ⁰	02	07.3	00.0	$0^{\circ}-1^{\circ} 14^{\circ} i$
9	8 05	02 ⁰	00	02.3	07.6	03.9
10	8 05	07	00	04.0	07.7
11	8 00	00 ⁰	00	00.0	07.8
12	8 10	07 ⁰	03	06.7	02.4
13	8 07	09	00	05.3	02.3
14	8 04	00 ⁰	00	01.3	07.8
15	6 02	06 ⁰	00	02.7	07.5	$\Delta^{\circ} n-rj, -10^{\circ}-12^{\circ}$
16	8 08	08 ⁰	00	05.3	04.8	$\Delta^{\circ} n-rj$
17	8 05	06 ⁰	02	04.3	04.8
18	7 04	10	07	07.0	03.8
19	8 09	09	02	06.7	04.5	$F_{NE} 11^{\circ}-15^{\circ}$
20	8 00	00 ⁰	00	00.0	08.1
21	7 00	00 ⁰	00	00.0	07.5
22	8 00	09 ⁰	03	04.0	06.7
23	7 04	09	07	06.7	00.0	$0^{\circ} 10^{\circ} 13^{\circ} i$
24	8 10	09	10	09.7	00.0	00.7	.	.	.	$0^{\circ} n-9^{\circ} i$
25	7 09	07 ⁰	09	08.3	03.7	05.0
26	8 10	10	10	10.0	00.0	$0^{\circ} 8^{\circ} 12^{\circ} i$
27	8 00	05 ⁰	09	04.7	07.5	00.4	.	.	.	$0^{\circ} 2^{\circ} 24^{\circ} i$
28	8 10 ⁰	10 ⁰	10	10.0	00.0	02.8	.	.	.	$0^{\circ} 0-14^{\circ} i$
29	8 10	10	00	06.7	01.7	14.5
30	8 07	10	07	08.0	00.0	00.0
31	8 03	00 ⁰	02	01.7	08.6
MES.	VRED.	05.1	05.8	03.2	04.7	143.6	27.3			

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1	8 04	08 ⁰	03	05.0	03.6	.	.	$F_{NE} 4^{\circ}-13$.	.
2	8 01	00 ⁰	00	00.3	08.4
3	8 09	03 ⁰	00	04.0	07.9	.	.	$F_{NE} 11^{\circ}-10^{\circ}$.	.
4	8 06	04 ⁰	00	03.3	06.7
5	8 00	00 ⁰	00	00.0	09.0
6	9 00	00 ⁰	00	00.0	09.5
7	7 00	00 ⁰	00	00.0	09.0
8	8 00	01 ⁰	00	00.3	09.0	.	.	$F_{NE} 9^{\circ}-18$.	.
9	8 00	00 ⁰	00	00.0	09.5
10	8 00	10	10	06.7	05.2
11	7 10	10	10	10.0	00.0	.	.	$0^{\circ} 7^{\circ} 10^{\circ} i$.	.
12	8 10	10	10	10.0	00.0	00.2
13	8 03	07 ⁰	10 ⁰	04.7	04.6	.	.	$0^{\circ} 16^{\circ} 17^{\circ} i$.	.
14	8 09	10	09	09.3	00.8	01.1	.	$0^{\circ} 18^{\circ}-19^{\circ} i$.	.
15	8 04	10	03	05.7	04.8	00.2
16	8 10 ⁰	09	06	08.3	01.7	00.0	.	$0^{\circ} n-9^{\circ}, F_{NE} 16-24$.	.
17	8 03	02 ⁰	06	01.7	09.3	00.2	.	$F_{NE} 11^{\circ}-12^{\circ} i$.	.
18	8 01	00 ⁰	00	00.3	09.4	.	.	$F_{NE} 6^{\circ}-8^{\circ} i$.	.
19	8 01	04 ⁰	03	02.7	09.1	.	.	$F_{NE} 7^{\circ}-24$.	.
20	8 10	10	07	09.0	00.7	.	.	$F_{NE} 0-24$.	.
21	8 08	05 ⁰	01	04.7	07.8	.	.	$F_{NE} 0-24$.	.
22	9 02 ⁰	00 ⁰	00	00.7	09.6	.	.	$F_{NE} 0-8^{\circ} i$.	.
23	8 01 ⁰	01 ⁰	00	00.7	09.8
24	8 01	02 ⁰	07	03.3	09.7
25	8 00 ⁰	00 ⁰	01	00.3	09.5
26	6 10	05	04	06.3	07.9	.	.	$F_{NE} 0-24$.	.
27	8 01 ⁰	04 ⁰	00	01.7	10.1	.	.	$F_{NE} 8-19^{\circ} i$.	.
28	8 00 ⁰	05 ⁰	00	01.7	10.2
MES.	VRED.	03.7	04.3	03.0	03.7	153.3	09.3			

$\varphi = 43^{\circ}31' \text{ N } \lambda = 16^{\circ}26' \text{ E}$ Gr. $\Delta G = + 1 \text{h } 06 \text{ min.}$

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DN	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pone e mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	754.2	754.8	755.1	09.5	12.2	08.8	08.8	12.6	05.1	-	04.2	04.9	04.8	61	46	57	55	ENE 2	SSE 1	SE 1	
2	755.2	755.4	755.4	07.1	12.9	10.1	10.0	13.3	06.6	-	04.5	06.8	07.0	59	61	75	65	NNE 2	ESE 4	ESE 4	
3	753.4	751.6	750.6	10.1	13.6	11.2	11.5	14.0	08.8	-	06.2	07.4	07.6	67	63	76	69	ESE 3	ESE 5	ESE 4	
4	748.8	747.6	747.7	10.8	13.4	11.3	11.7	13.7	10.6	-	07.6	06.8	07.8	78	59	78	72	ESE 5	ESE 5	ESE 5	
5	747.1	748.3	751.4	11.9	12.2	11.0	11.5	13.8	11.0	-	07.7	08.6	08.3	74	80	84	79	ESE 6	ESE 3	ESE 1	
6	752.8	751.6	750.6	09.9	16.2	13.3	13.2	16.4	09.4	-	06.7	05.0	06.1	73	36	54	54	NE 2	ESE 4	ENE 2	
7	750.8	751.3	751.2	12.5	15.6	13.4	13.7	15.7	12.0	-	09.1	08.6	07.7	84	65	67	72	ESE 5	ESE 4	SSE 3	
8	750.0	749.0	746.9	13.9	17.5	14.5	15.1	18.3	12.8	-	06.2	06.5	06.1	52	43	49	48	ESE 5	ESE 5	NNW 2	
9	742.9	740.8	740.1	11.9	16.2	11.4	12.7	16.8	10.8	-	04.5	07.2	08.6	43	52	85	60	ENE 1	ESE 4	SSE 5	
10	738.2	739.4	741.9	10.1	11.1	10.8	10.7	12.6	09.3	-	07.8	08.4	08.6	85	85	88	86	ESE 3	ESE 2	ESE 4	
11	747.7	751.0	750.7	09.5	12.5	10.9	11.0	13.0	08.6	-	08.1	09.1	07.8	91	84	79	85	SSE 1	ESE 2	ESE 5	
12	745.4	744.8	747.0	12.3	14.8	12.6	13.1	15.5	10.2	-	05.8	07.8	07.7	54	62	70	62	SE 7	SSW 6	ESE 5	
13	747.0	746.2	744.6	11.8	14.7	14.3	13.8	15.3	10.6	-	07.0	08.5	05.9	67	67	48	61	ESE 4	ESE 5	ESE 1	
14	742.0	743.5	746.7	10.5	14.9	11.3	12.0	15.7	10.0	-	05.9	08.0	08.1	62	63	81	69	ENE 2	SSW 2	SSE 2	
15	748.3	749.0	749.3	10.9	13.6	12.2	12.2	14.2	10.5	-	07.7	09.0	07.8	78	77	73	76	ESE 3	SSM 4	ESE 2	
16	746.0	747.7	747.3	09.3	10.0	09.4	09.5	12.3	07.9	-	07.2	07.5	06.5	82	81	74	79	E 2	E 2	NNE 1	
17	745.9	745.1	745.3	07.6	13.4	08.8	09.6	13.8	06.6	-	06.2	06.7	06.8	79	58	80	72	NNE 2	SW 2	ESE 2	
18	743.9	744.5	745.2	07.4	12.4	11.6	10.8	12.7	05.5	-	06.1	07.7	07.9	79	71	77	76	ENE 3	ESE 6	ESE 6	
19	743.9	744.0	745.0	11.6	13.9	14.2	13.5	14.6	10.7	-	08.7	08.6	07.1	85	72	59	72	ESE 7	ESE 4	ESE 4	
20	744.5	745.8	746.2	08.7	13.6	10.0	10.6	14.4	08.4	-	05.8	06.0	06.1	68	51	66	62	NNW 3	NNW 2	E 1	
21	744.8	744.0	745.1	09.2	11.6	08.3	09.4	12.4	08.2	-	06.4	05.8	03.0	74	57	37	56	NE 2	NE 4	NNE 6	
22	747.1	745.8	745.3	04.8	08.4	04.5	05.6	08.6	04.4	-	01.8	02.3	02.5	27	27	40	31	NNE 4	NNE 4	NE 4	
23	743.0	741.6	740.7	02.3	09.5	07.0	06.4	10.2	02.0	-	02.7	03.3	03.7	50	37	49	45	NE 3	SW 2	SE 4	
24	737.3	738.3	740.3	06.0	09.4	06.4	07.0	10.3	05.0	-	03.9	05.3	03.3	56	60	45	54	NNE 5	SSE 3	NNW 2	
25	741.8	742.5	745.5	04.8	12.9	07.2	08.0	13.0	04.0	-	02.8	04.2	02.9	43	37	38	39	NNE 1	NNW 2	E 1	
26	747.8	747.8	746.9	06.0	13.6	09.7	09.8	13.7	04.7	-	02.3	05.2	05.2	32	45	57	45	ENE 2	SSE 2	ESE 3	
27	745.9	745.1	744.3	10.3	11.8	11.6	11.3	12.4	09.4	-	06.5	07.3	08.5	69	70	83	74	ESE 5	ESE 5	ESE 5	
28	741.6	740.7	740.2	12.0	16.0	13.1	13.6	16.6	11.2	-	09.1	09.9	09.6	87	72	85	81	SSE 5	SSW 5	ESE 5	
29	741.9	743.6	743.9	12.9	13.7	13.2	13.2	14.5	12.1	-	08.9	08.8	10.5	80	75	92	82	ESE 3	ESE 4	ESE 6	
30	742.0	740.5	738.5	13.6	16.0	15.9	15.4	16.4	12.5	-	08.5	08.0	09.2	73	59	68	67	SE 2	SE 7	ESE 6	
31	724.2	740.9	745.2	15.5	15.3	14.4	14.9	17.0	13.6	-	09.3	09.7	08.4	70	74	68	71	SE 8	SSE 5	ENE 2	
MES.	VRED.	745.8	745.9	746.2	09.7	13.3	11.0	11.3	14.0	08.8	-	06.3	07.1	06.8	67	61	67	65	3.7	3.8	3.4

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1	744.5	746.4	747.6	10.2	14.6	10.9	11.6	14.8	09.2	-	07.6	08.5	08.1	81	68	83	77	NNW 1	SSW 2	NNW 2
2	744.9	744.3	744.4	10.6	15.4	08.0	10.5	15.7	07.5	-	08.2	07.6	06.7	86	58	83	76	WSW 1	SW 2	NN 3
3	745.3	747.4	747.6	08.0	12.8	11.1	10.8	14.2	07.3	-	06.0	07.3	07.1	75	62	72	71	ENE 1	SSE 2	ESE 5
4	748.8	749.4	750.4	11.7	14.7	13.0	13.1	14.9	10.8	-	07.3	08.6	08.0	70	68	72	70	SE 5	SSE 6	ESE 6
5	750.0	750.9	750.4	13.4	14.3	15.7	14.8	16.4	12.4	-	08.6	07.3	06.7	75	60	50	62	ESE 6	ESE 6	ESE 6
6	751.6	749.5	747.9	17.5	19.2	18.2	18.3	19.8	15.5	-	06.3	05.7	05.8	42	34	37	38	SE 6	ESE 7	ESE 1
7	748.5	746.0	745.9	17.1	18.4	16.4	17.1	18.6	16.4	-	05.1	06.3	07.3	35	39	52	42	SE 8	ESE 6	ESE 6
8	745.6	749.0	750.9	12.4	15.0	10.8	12.2	16.6	09.1	-	10.2	07.2	07.9	94	56	82	77	WSH 3	WSH 3	WS 1
9	750.8	750.2	748.5	11.2	15.7	12.7	13.1	15.8	09.4	-	07.3	07.7	04.8	73	58	61	64	ESE 4	ESE 5	ESE 4
10	742.0	739.5	740.8	12.0	11.8	08.7	10.3	13.2	08.7	-	07.9	09.2	07.4	75	89	88	84	SE 6	WSW 2	NNW 1
11	747.9	751.1	752.4	05.3	12.5	09.3	09.2	12.8	03.8	-	05.7	04.5	06.0	82	60	68	70	NNW 2	SW 2	N 1
12	752.8	753.3	754.3	07.5	13.6	09.0	09.8	14.6	05.8	-	05.6	06.4	05.9	72	55	69	65	NNE 1	WSW 4	ENE 2
13	755.2	755.1	754.1	09.0	14.0	11.9	12.2	16.2	07.6	-	05.7	07.8	08.8	66	57	84	69	ENE 1	SSE 1	NW 1
14	753.9	753.3	751.8	10.3	16.9	12.8	13.2	17.2	09.1	-	06.9	08.7	08.4	73	60	76	70	NNE 2	SSH 1	NNW 1
15	749.6	748.0	746.7	11.7	16.3	12.8	13.9	18.4	09.7	-	06.2	08.5	09.2	60	54	83	66	ENE 1	SSH 1	N 1
16	748.8	748.7	743.7	13.0	14.7	11.9	12.9	15.1	11.4	-	07.3	08.7	08.0	65	69	77	70	NE 1	ESE 2	NNE 3
17	745.3	747.2	749.1	14.4	17.3	13.9	14.8	17.6	11.5	-	05.8	05.7	05.1	47	38	43	43	NNE 6	NNE 5	NNE 5
18	750.2	750.3	751.1	12.1	17.7	13.3	14.1	17.8	11.4	-	04.3	04.5	04.2	40	29	36	35	MME 6</		

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_x = 1.0 \text{ m}$

Dan	Vrijeme 0-0 0-0	Oblačnost N (0-10)					Isotermalna broj števila	Padavina R mm	Snežni pokrov h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8 000	000	01	00.3	10.0
2	8 06	040	00	03.3	08.0
3	8 05	060	09	06.7	05.7
4	8 10	09	07	08.7	05.3
5	8 10	09	04	07.7	01.7
6	8 09	10	10	09.7	03.2	00.0
7	8 10	09	01	06.7	02.4	00.5
8	8 07	08	00	05.0	C6.5
9	8 050	060	100	07.0	06.7
10	8 10	100	100	10.0	00.0	09.5
11	8 100	10	06	08.7	00.8	17.1
12	8 10	070	04	07.0	C6.4	C0.1
13	8 09	09	10	05.3	00.9	04.1
14	8 07	050	04	05.3	06.6
15	8 07	10	09	08.7	02.1
16	8 08	10	02	07.0	03.0	02.4
17	8 10	070	03	06.7	08.0	10.8
18	8 10	09	10	09.7	C3.2	C1.2
19	8 100	10	07	09.0	00.0	01.4
20	8 08	080	07	07.7	C5.5	C5.2
21	8 10	10	10	10.0	00.2
22	8 040	010	00	01.7	16.5	00.1
23	8 030	050	07	05.0	10.1
24	8 10	09	03	07.3	02.3
25	8 080	040	01	04.3	09.8	00.0
MES. VRED.	07.8	07.5	06.0	07.1	140.0	52.4					

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1	8 100	07	03	06.7	04.1	01.2
2	8 10	090	100	05.7	04.0	00.5
3	8 08	09	05	07.3	05.5	12.9
4	8 09	080	09	08.7	02.5	00.6
5	8 09	10	10	09.7	00.0
6	8 10	10	10	10.0	00.1	00.0
7	8 10	050	09	08.0	02.8
8	8 100	040	00	04.7	C6.4	07.6
9	8 010	030	08	04.0	11.0	03.0
10	8 10	10	100	10.0	C0.0	03.3
11	8 07	08	10	08.3	05.8	27.3
12	8 000	060	00	02.0	10.0	01.6
13	8 020	030	02	02.3	10.9
14	8 000	020	01	01.0	11.5
15	8 000	010	09	03.3	11.5
16	7 10	100	10	10.0	C0.0
17	8 040	040	00	03.3	09.9	00.9
18	8 000	010	00	00.3	11.6
19	8 000	000	00	00.0	12.1
20	8 000	000	01	00.3	12.3
21	8 000	040	01	01.7	12.2
22	8 040	010	00	02.3	11.6
23	8 000	040	03	05.7	08.2
24	8 040	070	02	04.3	10.3
25	7 10	090	07	08.7	03.3
26	8 030	07	02	04.0	09.7	00.7
27	8 040	060	10	04.7	C6.9
28	8 000	020	00	03.3	09.3
29	8 000	000	00	00.0	12.4
30	8 000	000	00	00.0	12.6
MES. VRED.	05.2	05.1	04.4	04.9	231.9	56.8					

$\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

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D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	752.1	752.1	752.6	15.0	23.0	18.4	16.7	24.0	12.8	-	07.6	06.2	06.7	60	30	42	44	SE	1	WSW 2	NNE 6	
2	753.3	751.9	751.1	15.6	18.8	17.2	17.2	21.8	14.6	-	05.4	05.3	05.8	41	32	40	38	NE	6	NNE 5	NNE 5	
3	748.9	748.8	746.0	16.8	22.4	16.2	17.9	22.8	15.6	-	05.1	06.9	06.8	36	34	64	45	NE	3	SW 2	ESE 1	
4	747.2	748.4	749.3	16.6	19.6	16.6	17.4	20.6	14.6	-	06.9	07.6	07.2	49	44	50	48	E	3	SE 5	ESE 5	
5	750.3	750.7	751.3	14.5	17.9	17.0	16.6	18.9	14.1	-	10.2	09.0	06.7	83	59	46	63	ESE	5	SE 6	ESE 6	
6	750.1	749.8	750.3	17.2	20.6	17.1	18.0	21.3	14.0	-	06.4	06.4	13.0	43	46	89	59	ENE	3	SE 5	ESE 5	
7	750.0	749.5	748.2	16.6	21.3	17.0	18.0	22.3	15.9	-	11.9	12.0	11.8	84	63	81	76	SE	5	SSW 2	ESE 3	
8	746.1	746.6	747.3	16.0	15.0	14.7	15.1	17.6	14.0	-	12.4	12.0	10.1	91	94	81	89	SE	5	WSW 1	W 1	
9	749.1	750.1	751.2	14.6	18.4	14.9	15.7	19.6	12.4	-	10.2	08.7	06.7	82	55	69	69	SSE	1	WSW 3	NNE 1	
10	751.9	751.6	750.9	15.0	20.0	17.2	17.4	21.7	13.1	-	09.5	08.6	08.8	74	49	60	61	E	1	SW 4	SSE 1	
11	749.4	747.8	746.2	16.1	22.8	17.6	18.5	23.2	14.1	-	07.9	08.5	09.4	57	41	62	53	NE	2	SSW 1	WSW 2	
12	743.9	744.1	743.5	16.9	15.6	14.8	15.5	21.0	14.8	-	08.9	10.7	10.1	62	80	80	74	NE	2	NNE 1	ESE 2	
13	741.9	742.8	742.4	15.6	19.6	16.2	16.9	20.8	13.6	-	10.2	11.6	11.4	77	68	83	76	SE	1	S 2	E 1	
14	741.5	742.4	743.6	15.4	17.0	14.6	19.5	19.5	14.3	-	12.3	12.1	11.7	94	83	94	90	SSW	1	SSW 2	SSW 1	
15	749.3	746.0	746.8	15.7	19.5	16.6	17.1	20.0	14.2	-	14.6	13.3	12.9	94	78	91	88	SW	1	SW 3	ESE 1	
16	747.5	748.2	748.4	15.9	21.3	16.7	18.6	21.8	15.3	-	14.9	13.7	12.7	95	72	79	82	SE	1	SSW 1	ENE 1	
17	749.8	750.0	750.4	19.8	26.8	21.7	22.5	27.2	17.2	-	12.0	09.9	09.8	69	38	51	53	SSE	1	WSW 3	W 3	
18	752.0	752.0	752.3	21.7	27.2	24.2	24.3	27.4	19.2	-	09.6	11.9	11.2	49	44	50	48	NNE	1	SW 2	NE 1	
19	752.9	752.5	751.9	23.7	28.4	24.0	25.0	20.0	21.4	-	09.7	11.9	11.2	44	41	50	45	NNE	2	SSW 2	NNE 1	
20	751.8	750.7	751.1	22.4	26.0	20.0	22.1	27.3	19.0	-	12.4	14.5	11.1	61	58	63	61	E	1	SW 2	NE 3	
21	750.7	750.5	750.3	21.4	27.8	21.2	22.5	28.2	18.7	-	12.5	11.9	12.4	65	43	66	58	NNW	1	SSW 2	NNE 2	
22	750.4	749.4	749.3	21.8	26.5	20.8	22.5	27.1	18.9	-	12.4	14.0	14.5	63	54	79	65	SSW	1	SSW 2	ENE 1	
23	747.7	746.6	746.1	20.8	23.2	20.8	21.4	23.9	19.2	-	11.8	12.9	12.2	64	60	66	63	ESE	3	SE 5	SE 3	
24	744.9	745.1	745.3	18.9	20.5	18.8	19.2	21.8	16.2	-	11.6	11.9	11.8	71	66	73	70	NNE	2	ESE 3	NNE 1	
25	746.1	746.4	746.6	19.1	24.8	20.3	21.1	25.2	16.6	-	11.4	12.4	11.6	69	52	65	62	NNE	1	SW 3	NNE 1	
26	747.5	748.4	748.9	19.6	21.4	19.6	20.0	23.0	17.5	-	12.5	11.6	11.3	72	61	66	67	SSE	2	SSE 1	SSE 2	
27	749.4	750.4	750.3	18.1	18.8	17.8	18.1	22.0	16.4	-	11.5	14.4	12.2	74	76	80	77	NE	1	NW 2	NNW 2	
28	750.3	750.4	750.6	16.8	21.7	18.8	19.0	22.7	16.3	-	12.2	10.9	11.3	85	56	69	70	NNW	2	NNW 2	NNW 2	
29	750.7	750.1	749.2	19.4	24.7	26.0	21.0	25.1	16.1	-	11.0	11.5	11.4	65	49	65	66	SE	1	SSW 2	NNW 1	
30	748.3	747.6	746.6	16.9	21.1	19.9	19.4	21.4	16.7	-	11.8	11.2	10.5	82	60	60	67	ESE	2	ESE 4	ESE 4	
31	747.4	748.1	748.3	20.1	25.4	19.8	21.3	25.6	17.4	-	10.4	14.1	14.6	59	58	84	67	NE	2	SSE 2	S 1	
MES.	VRED.	748.6	748.6	748.6	17.9	21.8	18.5	19.2	23.0	16.0	-	10.4	10.9	10.7	68	56	68	64	2.1	2.6	2.2	2.2

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1	747.7	747.6	747.2	19.6	24.8	20.9	21.6	25.6	17.2	-	12.1	12.8	10.8	71	55	58	61	E	1	SSW 2	SSE 1
2	745.6	745.7	745.2	18.0	22.9	20.5	20.5	23.5	17.2	-	13.2	11.0	10.0	85	53	56	65	NNE	3	SSW 1	NW 1
3	744.6	744.5	745.7	19.8	25.0	18.9	20.6	26.4	16.9	-	10.4	12.7	05.8	60	54	35	50	N	1	WSW 2	NNW 2
4	747.1	747.8	749.2	17.4	20.2	16.8	17.8	21.3	15.5	-	08.8	07.9	06.5	59	44	45	49	NNW	3	NNW 1	NNE 5
5	750.9	751.2	751.5	15.2	19.2	15.5	16.4	19.3	14.9	-	04.9	05.3	04.7	36	32	36	35	NNE	7	NNE 5	NNE 5
6	751.6	751.0	751.5	13.5	18.5	16.5	16.2	18.6	13.2	-	05.0	05.3	05.7	43	33	41	39	NNE	5	NNE 5	NNE 5
7	751.2	749.9	750.5	16.0	22.4	17.3	18.2	23.3	14.1	-	05.1	07.4	07.2	37	36	48	40	NNE	4	SW 2	NNE 5
8	748.9	749.1	749.8	17.0	19.7	15.0	16.7	20.0	14.8	-	07.0	08.4	08.3	48	49	65	54	NNW	2	SSW 1	NE 4
9	748.7	748.5	748.2	12.9	15.2	16.1	15.0	16.4	12.2	-	10.2	12.2	12.1	93	94	88	92	NNE	2	SE 2	SSM 2
10	747.4	748.5	749.5	16.1	16.4	18.0	17.1	20.1	14.6	-	11.3	12.2	11.8	83	87	76	82	ENE	2	NNW 2	NNW 1
11	750.4	751.4	751.9	17.2	24.0	19.2	19.9	24.1	14.9	-	11.3	12.6	11.2	77	56	67	67	NE	1	SW 2	NW 2
12	751.0	751.1	750.2	19.7	22.0	18.0	19.4	22.5	16.2	-	11.7	12.6	12.0	68	64	77	70	NNE	2	SSW 1	NME 4
13	749.8	749.8	749.0	20.0	24.4	20.0	21.1	25.3	17.0	-	12.5	12.7	13.9	71	56	79	69	ENE	1	SW 2	SM 1
14	749.1	748.9	748.8	20.0	25.7	20.8	21.8	26.4	17.4	-	14.9	15.3	15.1	85	62	82	76	SW	1	SSW 2	SM 1
15	748.8	748.8	747.5	21.0	26.8	23.1	23.5	27.7	18.8	-	15.8	15.8	14.3	85	60	67	71	-	0	SW 2	NNE 2
16	747.0	746.5	746.2	22.7	24.0	18.4	20.9	25.2	18.1	-	12.7	11.6	14.7	61	52	93	69	SE	6	SE 4	SE 6
17	747.3	747.7	748.3	19.8	24.7	21.0	21.6	25.7	18.2	-	14.1	15.0	14.1	82	64	76	74	ESE	4	SSE 3	WSM 1
18	748.5	748.9	749.5	21.5</td																	

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Intenzitet bez osjeti	Padavina R mm	Snožni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 00	02	01	01.0	12.3	.	.	.	$\Delta rj-9^{\circ}, H_s 17^{\circ} ni$.
2	8 06	10	07	07.7	04.2	.	.	.	$F_{NE} n-8^{\circ}$.
3	8 09	06	04	06.3	08.9
4	8 05	08	10	07.7	07.9	.	.	.	$0^{\circ}-n-8^{\circ}, F_{NE} 9-16, 20-n$.
5	7 10	10	03	07.7	01.8	01.2	.	.	$0^{\circ}-n-8^{\circ}, F_{NE} 9-16, 20-n$.
6	8 03	01	09	04.3	07.6	00.6	.	.	$0^{\circ}-n-8^{\circ}, F_{NE} 11^{\circ} 13^{\circ}$.
7	8 10	08	01	06.3	03.3	.	.	.	$0^{\circ}-n-8^{\circ}, 13^{\circ} 23^{\circ} 24$.
8	6 10	10	02	07.3	02.5	00.0	.	.	$0^{\circ}-n-8^{\circ}, 13^{\circ} 23^{\circ} 24$.
9	8 03	02	00	01.7	13.1	09.6	.	.	$0^{\circ}-n-8^{\circ}, 13^{\circ} 23^{\circ} 24$.
10	8 07	02	00	03.0	11.9
11	8 07	08	10	08.3	10.7	.	.	.	$0^{\circ}-10^{\circ} 12^{\circ} 14^{\circ}, 10^{\circ} n$.
12	7 09	10	10	09.7	01.0	00.2	.	.	$0^{\circ}-13^{\circ} 24^{\circ} 25^{\circ} i$.
13	8 09	10	10	09.7	01.8	03.3	.	.	$0^{\circ}-n-8^{\circ}, 13^{\circ} 23^{\circ} 24$.
14	7 10	10	10	10.0	00.2	01.3	.	.	$0^{\circ}-10^{\circ} 12^{\circ} 14^{\circ}, 13^{\circ} 23^{\circ} 24$.
15	8 09	05	05	06.3	09.6	13.8	.	.	$0^{\circ}-n-8^{\circ}, 13^{\circ} 23^{\circ} 24$.
16	3 10	05	00	05.0	07.9	.	.	.	$= 10^{\circ} 14^{\circ} 15^{\circ}$.
17	8 00	01	00	00.3	13.7	.	.	.	$\Delta rj-9^{\circ}, = rj-8^{\circ}$.
18	8 00	02	00	00.7	13.3	.	.	.	$T^{\circ} 13^{\circ} 13^{\circ}$.
19	7 00	09	00	03.0	12.2	.	.	.	$0^{\circ}-15^{\circ} 16^{\circ}, T 14^{\circ} 16^{\circ} i, T 15^{\circ} 16^{\circ} i$.
20	7 00	04	04	02.7	08.2	.	.	.	$T 14^{\circ} 16^{\circ} i, T 15^{\circ} 16^{\circ} i$.
21	8 04	04	00	02.7	12.2	00.7
22	8 01	02	02	01.7	12.6	.	.	.	$F_{NE} 11^{\circ} 13^{\circ}$.
23	8 08	07	08	07.7	08.8	.	.	.	$0^{\circ}-14^{\circ} 45^{\circ} i, M 45^{\circ} 15^{\circ} i$.
24	8 09	10	09	09.3	00.9	02.4
25	8 00	04	01	01.7	13.3	00.6
26	8 09	07	07	08.3	04.1	.	.	.	$0^{\circ}-17^{\circ} 19^{\circ} 20^{\circ} i, T 9^{\circ} 9^{\circ} 12^{\circ} i$.
27	7 10	10	03	07.7	02.1	00.6	.	.	$0^{\circ}-10^{\circ} 12^{\circ} 14^{\circ} i, T 10^{\circ} 10^{\circ} 10^{\circ} i$.
28	8 10	09	01	06.7	04.8	14.4	.	.	$0^{\circ}-4^{\circ} 7^{\circ} 24^{\circ} i$.
29	8 08	03	07	06.0	12.3	00.0	.	.	$0^{\circ}-n-8^{\circ}, 11^{\circ} 13^{\circ} 15^{\circ} i, T 19^{\circ} 19^{\circ} 19^{\circ} i$.
30	8 10	10	08	09.3	01.0	01.7
31	8 00	05	03	02.7	10.5	00.7
MES. VRSD.	04.0	06.3	04.4	05.6	234.4	51.6				

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1	8 00	08	07	08.0	07.4	.	.	$0^{\circ} 17^{\circ} 17^{\circ} \sim 17^{\circ} 17^{\circ} 17^{\circ}$.	.
2	8 10	07	01	06.0	02.7	00.7	.	$0^{\circ} 3^{\circ} 44^{\circ} i$.	.
3	8 01	02	01	01.3	13.6	00.5	.	.	$F_{NE} 18-24i$.
4	8 03	09	09	07.0	06.6	.	.	$F_{NE} 0-24i$.	.
5	8 02	03	02	02.3	12.3	.	.	$F_{NE} 0-24i$.	.
6	8 06	07	02	05.0	02.9	.	.	$F_{NE} 0-24i$.	.
7	8 04	04	09	05.7	10.7	.	.	$F_{NE} 0-4i$.	.
8	8 09	09	10	09.3	00.1	.	.	$0^{\circ} 19^{\circ} 24^{\circ} i$.	.
9	7 10	10	09	09.7	00.0	04.8	.	$0^{\circ}-10^{\circ} 12^{\circ} 14^{\circ} 22^{\circ} 23^{\circ} i$.	.
10	7 10	10	10	10.0	01.4	13.2	.	$0^{\circ} 2^{\circ} 5^{\circ} 14^{\circ} 14^{\circ} 24^{\circ} i$.	.
11	8 09	09	10	09.3	03.3	02.7	.	$= 7^{\circ} 9^{\circ} 20^{\circ}$.	.
12	8 05	10	10	08.3	01.7	.	.	$0^{\circ}-17^{\circ} 20^{\circ} i$.	.
13	8 07	04	01	04.0	12.0	05.8	.	$F_{NE} 0-4i$.	.
14	7 02	03	00	01.7	11.8	.	.	$\Delta rj-10^{\circ} i$.	.
15	7 07	01	02	03.3	11.6	.	.	$\Delta rj-9^{\circ}, \Delta rj-9^{\circ} i$.	.
16	7 04	08	10	07.3	02.7	.	.	$F_{NE} 6-12^{\circ} 16^{\circ} 24^{\circ} i, 0^{\circ}-10^{\circ} 10^{\circ} 10^{\circ} i, 17^{\circ} 17^{\circ} 22^{\circ} i, \Delta 17^{\circ} 17^{\circ} 17^{\circ} i, R^{\circ} 17^{\circ} 17^{\circ} 17^{\circ} i$.	.
17	7 09	05	05	04.3	07.8	06.8	.	$F_{NE} 0-14^{\circ} i$.	.
18	8 06	05	01	04.0	12.1	.	.	$= rj-9^{\circ} i$.	.
19	8 02	04	04	03.3	12.1	.	.	$TNE 15^{\circ} 15^{\circ} 2^{\circ}$.	.
20	8 10	07	08	08.3	03.4	00.1	.	$0^{\circ}-3^{\circ} 10^{\circ} i$.	.
21	8 08	05	05	06.0	11.2	05.1	.	$TNE 15^{\circ} 16^{\circ} i$.	.
22	8 00	05	09	04.7	10.5	.	.	$T 17^{\circ} 19^{\circ} i$.	.
23	8 01	02	04	02.3	12.8	.	.	$= rj-7^{\circ} 13^{\circ} i$.	.
24	8 03	07	04	04.7	07.3	.	.	$T 13^{\circ} 13^{\circ} i$.	.
25	8 01	08	01	03.3	08.0	.	.	$T 13^{\circ} 13^{\circ} i$.	.
26	8 01	03	02	02.0	12.9
27	7 01	02	00	01.0	13.3
28	8 05	01	01	02.3	12.0
29	8 00	01	02	01.0	12.9
30	8 00	07	09	09.3	11.8
MES. VRSD.	04.0	05.5	04.9	05.1	248.9	47.7				

$\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

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D	Vršutni pritisak P mm			Temperatura vazduha T °C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dieis	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dieis	7	14	21	
1	741.9	742.6	744.7	15.7	16.8	16.6	16.9	23.1	14.0	-	11.1	07.5	06.7	82	46	47	59	NNW 2	NNW 3	NNW 2	NNW 4
2	742.8	743.4	743.0	14.4	19.3	18.8	17.8	20.6	13.2	-	08.4	10.2	12.0	68	61	74	68	NNW 3	NNW 3	NNW 2	NNW 2
3	745.7	747.4	749.2	19.6	26.2	23.9	23.4	27.4	17.5	-	13.0	09.9	10.7	76	39	48	54	SE 1	NNE 3	NNE 3	NNE 1
4	749.0	748.3	746.4	22.8	27.8	24.4	24.8	29.0	21.0	-	11.5	12.9	10.8	55	46	47	49	ESE 1	SSW 3	ESE 2	
5	744.0	744.9	745.5	22.2	19.1	19.2	19.9	24.5	16.4	-	11.7	12.5	14.4	58	75	87	73	ESE 5	N 1	WSW 1	
6	745.6	747.2	748.9	19.2	20.0	20.3	20.0	24.4	17.1	-	14.9	14.5	14.6	89	83	83	85	E 1	NW 1	SSE 1	
7	750.2	750.3	751.1	21.4	28.1	24.4	24.6	28.6	18.8	-	15.4	12.1	13.3	81	42	58	60	SSE 1	WSW 4	WSW 1	
8	751.7	751.8	751.7	24.0	29.0	25.0	25.8	29.3	21.6	-	12.8	14.3	12.9	57	48	54	53	NNE 1	SW 2	ENE 1	
9	751.5	751.1	750.6	24.0	30.6	26.0	26.6	31.1	21.6	-	14.8	14.2	14.1	66	43	48	52	NNE 1	SW 2	ESE 1	
10	749.9	749.1	748.4	25.1	30.8	25.6	26.8	31.6	23.1	-	16.4	15.8	13.6	69	47	55	57	NE 1	SW 2	SW 1	
11	748.6	748.7	748.7	25.4	30.6	25.0	26.5	31.4	23.0	-	17.5	15.7	18.3	72	48	77	66	ENE 1	SW 3	SW 1	
12	749.3	748.9	748.7	24.8	28.3	23.6	25.1	29.7	22.5	-	18.4	17.7	13.1	78	61	60	66	SE 1	WSW 3	WWN 2	
13	750.4	750.4	751.0	22.0	29.7	29.6	25.7	30.5	20.6	-	11.2	12.4	11.7	56	40	47	48	NNW 2	SW 1	NNE 4	
14	752.3	752.2	752.1	25.1	31.2	25.7	26.9	31.8	22.9	-	12.1	14.1	17.0	51	41	68	53	NNE 3	WSW 3	ESE 1	
15	752.3	752.1	750.9	25.8	32.1	25.6	27.3	32.2	23.4	-	14.5	16.9	17.2	58	47	70	58	ENE 1	SW 2	SW 1	
16	749.9	748.7	746.0	25.5	33.1	28.4	28.8	33.3	23.4	-	18.3	13.9	14.5	75	37	50	54	NNW 1	SW 2	NNW 1	
17	747.8	747.4	747.9	26.7	33.1	28.7	29.3	33.9	24.8	-	13.2	14.6	12.4	50	39	42	44	WSW 2	NNW 2	NNW 1	
18	748.4	748.1	746.9	26.9	34.7	30.1	30.4	35.2	24.4	-	15.9	14.9	13.3	60	36	42	46	ENE 1	SW 2	ENE 1	
19	745.7	746.1	746.5	29.6	32.8	26.6	28.9	33.6	26.6	-	12.4	12.6	11.2	40	34	43	39	ESE 4	NNW 2	NNW 2	
20	746.7	746.7	747.0	24.8	29.7	25.4	26.3	31.1	23.0	-	09.8	09.5	09.6	42	30	40	37	NNE 4	NNE 4	NNE 5	
21	747.4	746.1	746.2	24.8	31.5	27.5	27.8	32.6	22.6	-	08.4	09.6	10.4	36	28	38	34	NNE 1	WSW 3	NE 1	
22	746.5	746.9	747.2	25.8	27.0	26.2	26.3	32.6	23.1	-	09.7	10.5	10.7	39	39	42	40	NE 3	NNE 4	NNE 2	
23	748.5	748.1	748.3	25.2	30.5	24.4	26.1	31.3	22.7	-	11.3	12.9	14.6	47	39	63	50	ESE 2	WSW 3	ENE 2	
24	748.2	747.8	747.6	24.6	30.3	21.9	24.7	31.0	21.9	-	13.4	10.2	18.2	58	32	94	61	NNE 1	WSW 3	SSW 1	
25	747.2	747.0	747.8	24.6	29.8	26.0	26.6	31.0	22.2	-	12.6	15.3	17.2	54	48	71	58	SSE 1	WSW 2	WSW 1	
26	749.6	751.1	752.2	20.6	26.2	21.2	22.3	26.7	19.9	-	10.3	08.3	08.0	56	32	42	43	NNE 6	NNE 3	NNE 5	
27	752.1	751.8	751.1	20.7	26.9	23.1	23.4	27.5	18.6	-	06.5	08.3	08.7	36	31	41	36	NNE 3	WSW 4	NNE 2	
28	751.0	751.2	751.0	21.6	27.8	23.6	24.2	29.0	20.1	-	06.3	09.1	13.0	33	33	59	42	NNE 6	WSW 2	ENE 2	
29	751.7	750.9	750.6	24.0	29.3	25.2	25.9	30.2	21.7	-	10.9	13.5	11.6	49	44	48	47	NNE 2	WSW 3	WSW 1	
30	749.9	749.3	749.4	24.8	29.1	25.0	26.0	31.5	21.6	-	11.4	13.5	10.1	48	45	43	45	NE 3	SM 3	NNE 2	
31	750.5	750.0	751.1	25.4	29.9	25.4	26.5	30.2	23.4	-	10.5	08.9	09.2	43	28	38	36	N 2	NNE 4	NNE 5	
MES.	748.6	748.6	748.7	23.4	28.5	24.5	25.2	29.9	21.2	-	12.4	12.5	12.6	58	43	55	52	2.2	2.6	1.9	
VRSD.	748.6	748.6	748.7	23.4	28.5	24.5	25.2	29.9	21.2	-											

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1	752.0	751.2	751.6	24.6	30.3	26.2	26.8	31.0	22.6	-	10.3	08.7	09.9	44	27	39	37	NNE 3	NNW 3	NNE 3	
2	752.8	752.3	753.1	24.7	30.8	25.9	26.8	31.6	22.9	-	10.1	08.9	10.4	43	27	41	37	NNE 2	NNE 2	NE 2	
3	751.8	752.9	753.2	24.2	30.8	24.1	25.8	31.2	23.2	-	09.8	10.9	08.9	43	33	40	39	NNE 4	SW 2	NE 5	
4	753.2	751.8	751.2	23.8	28.8	24.8	25.6	30.5	22.0	-	10.4	11.3	09.9	47	38	42	42	NNE 3	WSW 3	NNE 3	
5	750.2	750.1	750.2	23.3	27.5	24.0	24.7	28.8	21.3	-	11.2	10.1	08.3	52	37	37	42	NNE 3	WSW 2	ENE 3	
6	750.9	751.5	752.4	22.1	28.0	24.8	24.9	29.1	21.1	-	08.7	08.8	08.2	44	31	35	37	NNE 4	WSW 2	NE 2	
7	752.8	751.4	751.1	23.7	30.2	24.3	25.6	32.0	21.9	-	09.8	12.4	09.2	45	39	40	41	NNE 2	WSW 2	ENE 2	
8	749.9	749.0	748.8	24.0	28.8	25.7	26.0	31.0	22.3	-	09.8	10.7	09.6	44	36	39	40	NNE 3	SW 3	NNE 3	
9	748.6	748.6	749.7	25.0	30.5	26.4	27.1	31.9	23.5	-	10.7	12.8	11.1	45	39	43	42	SSW 1	ESE 3	ENE 2	
10	750.1	750.8	751.0	25.4	31.0	26.0	27.1	31.4	23.3	-	12.2	15.2	13.0	50	45	51	49	SSW 1	WSW 2	ENE 1	
11	751.4	750.9	750.6	23.8	30.0	25.0	26.0	30.6	22.0	-	13.2	14.8	11.8	60	47	50	52	NE 1	SW 2	NNW 1	
12	749.1	747.3	746.5	23.2	30.4	25.4	26.1	30.5	22.1	-	14.2	11.7	13.1	67	36	54	52	NE 1	SSW 1	ESE 3	
13	745.3	745.6	747.6	22.6	27.0	23.3	24.0	29.0	21.5	-	15.0	12.3	12.4	73	46	58	59	SE 1	NNW 2	NNE 2	
14	749.5	750.2	750.7	23.0	30.2	25.0	25.8	30.4	21.6	-	10.0	10.7	10.0	47	33	42	41	NNE 5	WSW 2	ENE 2	
15	751.8	751.4	750.5	22.0	29.4	23.4	24.6	29.6	20.0	-	09.3	11.7	12.5	47	38	58	48	NNE 2	WSW 2	WSW 2	
16	750.4	749.7	749.2	22.4	26.5	24.3	24.4	28.5	21.6	-	13.4	11.1	12.0	66	43	53	54	ENE 1	WSW 1</		

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijeme 00-09 09-18 18-27	Oblačnost N (0-10)					Insolacije broj sati	Padavina R mm	Snežni pekrivac h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8 09	08	08	08	08.3	05.6	06.3	.	T' 6° 7° 10° 12° 16° 26° 9° 0° n-6° 12° 12°	.	.
2	8 10	10	10	10	10.0	00.5	00.6
3	8 08	06	03	03	05.7	08.9	00.0
4	7 00	01	01	01	00.7	13.2	.	.	Fase 9° 10° 15° 10° 12° 12°, 0°-2 10° 14°, 0° 11° 11°	.	.
5	8 10	10	10	10	10.0	03.7
6	7 10	10	05	05	08.3	05.2	21.0	.	0° 12° 14° 16° 18° 19°, T 12° 13°	.	.
7	8 00	03	02	02	01.7	12.7	02.6	.	= 9-H	.	.
8	7 00	00	01	01	00.3	13.6	.	.	= rj-9	.	.
9	7 01	00	00	00	00.3	13.2	.	.	= rj-11	.	.
10	7 01	01	01	00	00.7	12.8	.	.	= rj-11	.	.
11	7 02	03	00	00	01.7	13.0	.	.	= rj-10°, T 11° 12°	.	.
12	6 00	01	03	01	01.3	12.8	.	.	= rj-15	.	.
13	8 09	06	00	00	05.0	10.4	.	.	= rj-7	.	.
14	8 00	03	00	00	01.0	13.4	00.0	.	= rj-14°	.	.
15	6 00	00	00	00	00.0	13.7	.	.	= rj-7	.	.
16	8 00	01	00	00	00.3	13.6	.	.	= rj-7	.	.
17	7 00	01	00	00	00.3	13.3	.	.	= rj-9	.	.
18	8 00	00	01	01	00.3	12.5
19	8 01	00	01	01	00.7	12.8	00.0	.	= n	.	.
20	8 00	02	00	00	00.7	13.6
21	8 00	01	01	01	00.7	13.8
22	8 02	04	01	02	02.0	12.3
23	8 00	03	00	00	01.0	13.6
24	8 00	02	01	01	01.0	13.3
25	8 00	00	04	04	04.7	09.1	.	.	0° 11° N 0°	.	.
26	8 00	01	00	00	03.3	11.3	00.7	.	0° rj, FNN 0°-10°	.	.
27	8 00	00	00	00	00.0	13.8	.	.	FNN 6°-7°	.	.
28	8 00	00	00	00	00.0	13.7
29	8 00	01	01	00	00.7	13.4	.	.	T 15° 15°, 0° 15° 15°	.	.
30	8 00	05	00	00	01.7	09.6
31	8 01	04	01	01	02.0	12.4	00.9
MES. VRED.	02.6	03.1	01.7	02.5	354.6	32.3					

1	8 00	05	00	01	01.7	12.1
2	8 00	03	01	02	02.0	12.6
3	8 06	03	00	00	03.0	11.8
4	8 03	07	00	00	04.3	09.2	.	.	0°-14°-15°	.	.
5	8 04	09	03	00	04.0	10.1	03.0
6	8 04	07	02	02	05.0	11.3
7	8 05	06	05	05	04.0	07.5
8	8 07	06	07	07	07.3	09.3
9	8 01	06	09	04	04.0	09.6
10	8 03	01	00	01	01.3	12.6
11	8 01	01	02	02	01.3	12.0	.	.	-rj-9	.	.
12	7 00	04	10	10	08.3	04.5	.	.	T 16° 20° 20°, 0° 20° 21	.	.
13	8 02	09	01	01	04.0	09.7	00.0	.	T 10° 17°, 0° 17° 16°	.	.
14	7 00	04	00	01	01.3	12.1	00.3
15	7 00	00	01	01	00.3	12.3
16	8 00	10	09	09	04.0	04.4	00.0	.	0°-0 6°-6° 10°-14°-10°, 20°-21	.	.
17	8 02	06	05	04	04.3	10.9	00.2
18	7 01	04	03	02	02.7	11.5	.	.	0°-rj-10°-12°-23°-24	.	.
19	9 01	07	01	01	03.0	10.2	24.0	.	0°-23°-1-0°-11-3°, FNN 10-24	.	.
20	8 00	04	00	01	01.3	12.3	.	.	FNN 0-14	.	.
21	8 00	02	00	00	00.7	12.2
22	8 00	01	00	00	00.3	12.5
23	8 01	01	00	00	00.7	10.3
24	6 10	10	10	10	10.0	02.3	.	.	T 6°-14°, 0°-27°-13°-12°-13°-19°-21, F-see 4°-14°-10°, 0°-19°-20°	.	.
25	7 10	09	09	09	00.3	03.0	13.6	.	0°-15°-7°-10°-10°-10°-10°, 10°-23°-23°-23°, R-7-7	.	.
26	8 10	10	04	04	00.0	00.2	12.8	.	0°-4°-4°-4°, 17°-17°-17°, T 7°-10°	.	.
27	8 05	07	10	07	07.3	04.5	11.8	.	0°n	.	.
28	8 00	10	07	07	00.7	03.0	03.0	.	0°-7-2°	.	.
29	8 00	03	00	00	04.0	07.2	.	.	0°-7-6-9-6-6	.	.
30	9 10	04	02	02	03.3	00.6	01.2	.	0°-6-6-8-T 6°-8°	.	.
31	7 02	04	00	00	00.0	11.6	15.0
MES. VRED.	04.1	05.6	03.5	04.4	203.4	203.7					

$\varphi = 43^{\circ}31' \text{ N } \lambda = 16^{\circ}26' \text{ E}$ Gr. $\Delta G = + 1 \text{h } 06 \text{ min.}$

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D O	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	750.6	751.1	751.1	20.3	27.1	23.0	23.4	27.3	19.4	-	13.9	14.6	17.0	76	54	81	71	NNE	2	SW	2	SE	1
2	751.2	751.0	750.1	21.6	27.1	23.0	23.7	27.3	20.7	-	13.2	16.4	16.4	68	61	78	69	NE	2	SW	2	NNW	1
3	748.1	747.2	747.1	21.6	24.6	18.2	20.6	25.0	17.8	-	14.3	13.4	13.8	74	58	86	73	ESE	3	ESE	4	NNE	1
4	746.0	747.5	748.2	19.7	25.0	22.1	22.2	25.4	17.6	-	12.1	15.0	14.5	70	63	73	69	NNE	1	SW	2	WSW	2
5	748.8	749.4	749.7	20.6	25.6	21.2	22.2	26.0	19.8	-	14.6	16.7	16.9	80	68	90	79	NE	1	WSW	2	SW	1
6	751.0	751.6	751.9	20.0	26.3	22.4	22.8	26.6	19.1	-	14.0	17.5	14.8	80	68	73	74	NNE	1	SSW	2	NNW	1
7	751.2	750.1	750.9	20.7	24.0	22.1	22.2	24.1	19.4	-	15.6	14.0	15.1	85	62	76	74	ESE	2	ESE	3	ESE	2
8	752.5	753.2	753.5	19.2	23.8	21.6	21.6	25.0	17.4	-	14.2	12.0	10.8	85	54	56	65	NNW	1	NNW	1	NNE	3
9	753.9	753.3	752.5	19.8	25.5	22.2	22.4	25.6	19.4	-	10.3	13.2	12.4	59	54	62	58	NNE	3	WSW	2	NW	2
10	752.0	751.7	751.3	19.4	25.2	22.4	22.4	25.7	18.6	-	10.3	13.7	10.7	61	57	53	57	NE	1	SM	2	WSM	1
11	750.3	750.4	749.7	19.6	22.9	22.0	21.6	24.5	19.0	-	10.6	13.2	14.2	62	63	72	66	NE	2	ESE	3	ESE	3
12	748.3	748.4	746.3	21.2	23.3	21.3	21.8	23.6	18.6	-	16.0	16.5	17.0	85	77	90	84	ESE	4	ESE	2	ESE	4
13	717.9	749.6	751.5	18.2	22.2	20.5	20.4	22.7	16.4	-	12.8	14.1	11.9	82	70	66	73	ENE	1	SE	1	NNW	2
14	751.5	750.3	749.6	18.3	24.4	21.7	21.5	24.8	17.3	-	11.0	12.4	13.6	70	54	70	65	NNE	2	ESE	4	SE	3
15	749.3	750.8	752.9	22.3	24.3	23.5	23.4	24.6	21.1	-	14.8	16.4	13.6	73	72	63	69	ESE	5	ESE	5	ESE	5
16	755.8	757.2	757.6	23.2	29.7	26.5	26.7	29.8	22.5	-	11.4	11.6	11.6	54	37	44	45	NNE	1	SW	1	WSW	1
17	757.6	756.5	756.6	24.9	31.6	30.8	29.5	32.2	24.1	-	11.6	17.3	09.8	49	50	29	43	NE	1	WSW	1	N	2
18	756.5	755.4	755.4	25.0	29.4	24.4	25.8	30.8	24.4	-	13.0	13.2	13.2	55	43	57	52	ESE	3	SW	2	WSW	1
19	755.4	755.1	754.5	22.4	26.6	22.1	23.3	26.9	21.3	-	12.1	16.2	17.3	60	62	87	70	ESE	1	SW	1	NNW	1
20	754.2	753.9	753.5	20.6	26.6	22.2	22.9	27.0	20.1	-	11.9	13.8	16.8	63	53	83	66	NNE	2	SSW	1	SW	1
21	754.1	754.3	754.7	20.8	26.7	23.5	23.6	27.0	20.1	-	10.4	11.7	13.3	57	45	61	54	NE	3	SSW	1	SE	1
22	755.8	756.5	757.0	22.1	27.9	23.6	24.3	28.1	20.3	-	10.3	12.5	11.0	52	44	50	49	NNE	3	WSW	1	NNE	4
23	757.4	757.1	756.2	21.0	26.8	23.2	23.6	27.0	20.6	-	10.3	12.4	11.7	55	47	55	52	NNE	3	SSW	2	NW	1
24	755.7	755.3	754.4	20.0	25.8	22.3	22.6	26.0	19.3	-	10.8	15.3	12.0	62	61	60	61	NNE	3	SW	1	NNE	1
25	753.3	752.5	751.9	19.2	25.7	21.5	22.0	25.7	18.6	-	09.9	11.8	14.0	59	48	73	60	NE	2	SSW	1	SSW	1
26	750.3	750.2	751.4	21.0	23.8	21.6	22.0	24.8	19.6	-	11.8	15.8	16.6	63	71	86	73	SE	3	ESE	3	ESE	3
27	753.8	755.4	756.4	20.2	26.1	22.1	22.6	26.4	20.0	-	13.7	16.1	17.1	77	63	86	75	NE	2	SSW	2	WSW	1
28	757.3	757.6	757.1	19.8	26.1	23.1	23.0	26.3	19.5	-	14.7	17.1	16.0	85	67	75	76	NNE	2	SW	2	NW	1
29	756.7	755.9	755.4	20.2	26.4	22.5	22.9	26.8	19.7	-	12.5	17.1	16.4	70	66	80	72	NE	3	SW	1	ESE	1
30	753.6	752.7	752.3	20.2	26.2	22.6	22.9	26.7	20.2	-	13.7	17.7	15.5	77	69	75	74	NNE	2	SSW	1	NNW	1
MES.	VRED.	751.7	752.7	752.7	20.8	25.9	22.6	23.0	26.3	19.7	-	12.5	14.6	14.2	68	59	70	66	2.2	1.6	1.6	1.6	

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1	753.1	753.5	753.6	21.4	26.1	22.4	23.1	26.5	20.4	-	11.6	16.8	13.9	61	66	68	65	ENE	2	SSW	2	ESE	1
2	753.7	753.6	753.8	19.8	26.0	23.0	23.0	26.4	19.7	-	12.0	14.1	14.2	69	56	67	64	NNE	1	SW	1	NNE	3
3	754.1	753.9	753.6	20.8	26.1	21.8	22.6	26.6	20.4	-	11.9	14.8	14.5	65	58	74	62	NNE	2	SW	2	WSW	1
4	753.4	752.7	752.4	19.3	25.2	21.2	21.7	25.5	18.8	-	13.5	15.7	10.8	81	65	57	68	ENE	1	SW	2	NNE	2
5	752.7	753.8	753.4	17.3	20.3	15.5	17.2	21.3	15.5	-	06.7	06.6	05.4	45	37	41	41	NNE	6	NNE	5	NE	6
6	756.7	756.5	756.9	15.6	21.1	16.8	17.6	21.6	14.6	-	05.3	06.8	06.7	40	36	47	41	NNE	6	SSE	2	NNE	5
7	756.1	754.6	753.8	15.4	22.2	17.7	18.2	22.2	14.8	-	07.4	11.1	11.8	57	55	78	63	N	1	SSW	2	NNW	1
8	752.7	752.8	752.6	16.8	22.1	17.3	18.4	22.6	15.1	-	10.1	06.1	09.0	70	40	60	57	NE	1	SSE	3	ENE	2
9	751.2	749.8	749.0	15.1	12.8	14.0	14.0	17.5	11.4	-	06.6	08.7	07.9	51	79	66	65	NNE	3	NNW	4	NNE	2
10	746.8	745.4	743.6	13.4	16.2	12.8	13.8	17.6	12.5	-	06.4	08.2	08.6	56	59	78	64	NE	3	ESE	3	NNE	2
11	745.2	747.2	747.8	13.1	18.7	16.6	16.2	19.0	11.9	-	06.6	08.8	08.0	58	54	56	56	NE	2	ESE	2	ESE	2
12	747.7	747.7	748.9	15.1	19.7	20.4	18.9	20.5	13.0	-	08.7	12.8	16.1	68	74	89	77	NE	3	ESE	5	ESE	6
13	746.4	744.6	746.0	19.8	15.9	17.4	17.6	21.7	15.8	-	15.5	12.6	13.9	89	93	93	92	ESE	7	NNW	3	WSW	1
14	742.9	749.2	751.1	11.6	13.3	11.4	11.9	17.8	10.6	-	09.3	08.9	08.3	91	78	82	84	NW	3	NNW	2	ENE	2
15	751.0	752.0	752.7	11.2	17.6	15.3	14.8	18.1	10.3	-	07.9	10.2	10.5	80	67	80	76</td						

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vreme 0-9 0-9	Obložnost N (0-10)					Intenziteta broj sati	Padovina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8	000	030	00	01.0	10.0	.	.	.	$\Delta^{+} rj-8 = rj-9$.
2	7	000	010	00	00.3	11.3	.	.	.	$\Delta^{+} rj-8 = rj-9$.
3	8	01	040	10+	00.3	04.1	00.0	.	.	$\Delta^{+} rj-8 = rj-9$.
4	8	040	030	00	03.3	08.1	00.1	.	.	$\Delta^{+} rj-8 = rj-9$.
5	7	000	020	00	00.7	10.7	00.0	.	.	$\Delta^{+} rj-8 = rj-9$.
6	7	030	030	01	02.3	09.4	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
7	8	10	040	07	07.0	01.9	00.4	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
8	8	030	01	00	04.7	03.9	12.7	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
9	7	060	010	00	02.3	10.1	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
10	8	000	010	00	00.3	10.0	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
11	8	01	10	00	00.0	03.3	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
12	8	01	040	10	01.7	03.9	00.4	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
13	8	01	030	00	03.7	03.4	10.4	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
14	8	030	030	00	01.0	10.0	01.0	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
15	8	02	010	01	01.3	10.2	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
16	8	000	000	00	00.0	01.4
17	8	000	000	00	00.0	00.3
18	8	000	000	00	00.0	10.0
19	7	000	000	00	00.0	00.1	.	.	.	$\Delta^{+} 10^{\circ} n = 10^{\circ} n$.
20	7	000	000	00	00.0	10.0	.	.	.	$\Delta^{+} 10^{\circ} n = 10^{\circ} n$.
21	8	000	020	01	01.0	10.0
22	7	04	04	00	03.3	08.7	.	.	.	$\Delta^{+} rj-14^{\circ}$.
23	7	030	030	00	02.0	03.3	.	.	.	$\Delta^{+} rj-15^{\circ} n = n$.
24	6	000	010	00	00.3	09.0	.	.	.	$\Delta^{+} rj-14^{\circ}$.
25	7	000	010	00	04.3	09.2	.	.	.	$\Delta^{+} rj-14^{\circ}$.
26	7	000	01	02	03.7	09.7	.	.	.	$\Delta^{+} rj-14^{\circ}$.
27	7	01	040	00	04.3	06.6	.	.	.	$\Delta^{+} rj-10^{\circ}$.
28	7	030	070	00	01.3	06.4	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
29	8	000	000	00	00.0	10.2	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
30	8	010	010	00	00.0	07.1	.	.	.	$\Delta^{+} rj-9^{\circ} = rj-10^{\circ}$.
MES.		02.3	03.2	01.4	02.6	292.1	63.1				

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1	8	070	030	00	04.0	01.4	.	.	.	$\Delta^{+} rj-9$.
2	8	00	030	00	03.1	01.1	.	.	.	$\Delta^{+} rj-8$.
3	7	000	000	00	00.0	00.0	.	.	.	$\Delta^{+} rj-7^{\circ}$.
4	7	000	030	00	03.7	00.4	.	.	.	$\Delta^{+} rj-8 = rj-9$.
5	8	020	030	00	01.7	00.3	.	.	.	$\Delta^{+} rj-8 = rj-9$.
6	8	010	010	00	00.7	10.2	.	.	.	$\Delta^{+} rj-7^{\circ}$.
7	8	000	000	00	00.0	10.1	.	.	.	$\Delta^{+} rj-7^{\circ}$.
8	8	00	030	00	03.0	00.3	.	.	.	$\Delta^{+} rj-7^{\circ}$.
9	7	09	100R	09	09.3	00.0	.	.	.	$\Delta^{+} rj-7^{\circ} = 17^{\circ} i$.
10	8	000	10	100R	00.0	02.0	00.4	.	.	$\Delta^{+} rj-7^{\circ} = 17^{\circ} i$.
11	8	010	040	10	07.7	04.2	00.4	.	.	$\Delta^{+} rj-7^{\circ} = 17^{\circ} i$.
12	8	10	01	09	09.3	02.1	04.4	.	.	$\Delta^{+} rj-7^{\circ} = 17^{\circ} i$.
13	8	10	100R	07	09.0	00.0	00.0	.	.	$\Delta^{+} rj-7^{\circ} = 17^{\circ} i$.
14	8	10	040	09	07.7	03.0	23.1	.	.	$\Delta^{+} rj-7^{\circ} = 17^{\circ} i$.
15	8	09	040	03	09.3	00.3	13.0	.	.	$\Delta^{+} rj-7^{\circ} = 17^{\circ} i$.
16	7	100	10	10	10.0	04.1	00.4	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i = 19^{\circ} 23^{\circ} - 24^{\circ} R' 6^{\circ} 6^{\circ} F_{\text{ee}} 14^{\circ} 24^{\circ}$.
17	8	01	09	06	00.0	02.4	21.1	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i = 19^{\circ} 23^{\circ} - 24^{\circ} R' 6^{\circ} 6^{\circ} F_{\text{ee}} 14^{\circ} 24^{\circ}$.
18	8	00	000	07	07.7	01.4	07.4	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i = 19^{\circ} 23^{\circ} - 24^{\circ} R' 6^{\circ} 6^{\circ} F_{\text{ee}} 14^{\circ} 24^{\circ}$.
19	8	030	09	100	00.0	02.0	00.7	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i = 19^{\circ} 23^{\circ} - 24^{\circ} R' 6^{\circ} 6^{\circ} F_{\text{ee}} 14^{\circ} 24^{\circ}$.
20	9	10	01	05	00.0	00.0	04.1	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i = 19^{\circ} 23^{\circ} - 24^{\circ} R' 6^{\circ} 6^{\circ} F_{\text{ee}} 14^{\circ} 24^{\circ}$.
21	8	030	050	01	03.0	00.2	00.1	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
22	8	010	040	01	02.0	00.2	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
23	8	020	00	06	05.3	00.3	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
24	8	01	010	00	03.0	07.3	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
25	8	030	000	00	01.0	00.3	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
26	9	040	010	00	01.7	00.0	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
27	8	030	040	00	02.3	01.0	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
28	9	020	010	00	01.0	10.0	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
29	8	010	000	00	00.0	00.0	00.0	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
30	8	000	000	00	00.0	00.0	00.0	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
31	7	000	020	00	00.7	00.0	.	.	.	$\Delta^{+} rj-16^{\circ} i = 19^{\circ} i$.
MES.		05.0	04.6	03.9	04.4	203.7	144.0				

$\varphi = 43^{\circ}31' \text{ N } \lambda = 16^{\circ}26' \text{ E}$ Gr. $\Delta G = + 1 \text{h } 06 \text{ min.}$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0—12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min S cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	753.7	754.0	754.4	12.3	17.2	15.0	14.9	18.0	11.7	-	07.8	09.8	09.1	73	66	71	70	NE	2	SW	1	NE	1
2	754.8	755.1	756.3	13.6	18.3	16.5	16.2	18.6	13.2	-	08.5	11.1	11.1	73	71	79	74	NE	1	ESE	3	ESE	3
3	757.1	757.3	757.8	15.1	19.4	16.4	16.8	19.7	14.8	-	09.8	11.5	11.8	76	66	85	76	E	3	ESE	3	ESE	1
4	757.5	757.2	757.2	13.6	18.2	15.2	15.6	18.5	13.4	-	09.5	11.7	09.4	81	75	73	76	ENE	2	S	1	E	1
5	756.7	756.0	756.1	12.2	17.8	14.3	14.6	18.1	11.8	-	05.9	09.0	08.1	56	59	66	60	NE	3	SW	2	NE	3
6	755.6	754.8	754.8	11.3	15.2	14.2	13.7	15.7	11.0	-	06.5	08.3	09.4	65	64	78	69	NE	3	NNE	1	NE	1
7	753.9	753.4	752.7	12.2	14.0	13.8	13.4	14.5	10.9	-	06.8	08.2	07.6	64	69	65	66	NE	1	ENE	1	NE	2
8	752.3	751.2	750.1	11.6	15.0	12.5	12.9	15.0	10.9	-	05.3	05.8	05.0	52	46	46	48	NNE	3	NE	2	NNE	4
9	747.7	749.0	751.9	12.0	14.4	12.5	12.8	14.6	09.5	-	07.1	10.3	09.9	68	84	91	81	NE	3	ESE	6	N	2
10	752.2	750.8	750.4	12.2	14.2	11.7	12.4	15.0	11.5	-	09.0	10.4	06.6	85	86	64	78	NE	2	ESE	4	NW	2
11	753.3	753.9	755.0	11.0	13.0	10.2	11.1	13.6	10.0	-	07.8	08.8	06.1	80	79	66	75	NW	2	SSW	1	NE	3
12	755.9	756.6	758.6	10.0	14.3	12.3	12.2	14.7	09.4	-	06.8	08.5	08.6	74	70	80	75	NNE	2	SE	2	ENE	1
13	759.2	758.9	758.3	09.7	15.2	12.8	12.6	15.5	09.7	-	06.3	08.6	08.0	69	66	72	69	NE	2	ESE	1	E	2
14	754.5	753.0	752.4	10.8	10.8	12.1	11.4	13.3	10.2	-	08.5	08.7	07.1	87	90	67	81	E	2	ENE	2	NNE	2
15	751.6	751.2	751.4	11.4	13.8	08.4	10.5	13.8	08.2	-	05.5	04.2	04.2	55	36	51	47	NE	4	NE	6	NNE	6
16	748.6	744.0	740.2	05.4	05.0	10.4	07.8	10.5	04.1	-	05.8	06.1	06.2	86	93	87	89	NE	1	NNE	3	E	4
17	735.4	736.5	736.0	14.2	16.2	16.9	16.0	16.9	08.7	-	11.3	10.9	14.0	93	79	83	85	ESE	6	SSE	1	SE	6
18	735.6	738.8	742.1	17.0	15.3	14.3	15.2	17.6	10.6	-	11.8	09.2	08.4	81	71	69	74	SE	7	SSW	6	SSW	6
19	744.8	745.7	746.6	11.8	13.1	11.0	12.1	15.0	10.6	-	08.5	07.8	07.2	82	69	69	73	SSW	6	SSW	1	NE	3
20	746.4	744.9	744.9	10.4	11.6	10.5	10.0	13.6	09.9	-	06.8	06.4	08.6	72	82	91	82	NE	1	ESE	1	NNE	1
21	743.7	745.8	748.3	09.8	07.5	04.4	06.5	10.8	04.4	-	08.0	03.7	02.3	88	48	37	50	NNE	3	NNE	6	NE	6
22	746.9	744.3	745.8	04.4	06.4	05.9	06.2	08.6	03.6	-	01.6	01.2	02.4	25	15	34	25	NE	4	NNE	3	NNW	5
23	746.4	747.2	749.9	02.5	04.3	02.8	03.1	05.9	02.4	-	02.4	02.6	02.5	44	42	45	44	NNE	1	NNE	6	NNE	6
24	749.4	750.1	753.3	02.5	03.6	02.0	02.5	04.8	01.8	-	02.4	02.0	02.0	44	34	37	38	NNE	3	NNE	6	NE	5
25	754.6	755.3	755.8	01.0	05.4	03.0	03.1	05.6	00.0	-	01.8	01.9	01.5	37	28	27	31	NNE	3	NNE	3	NNE	1
26	755.5	755.1	755.0	01.3	08.4	05.9	05.4	08.7	00.5	-	01.5	04.9	04.5	30	60	65	52	NNE	2	WSW	1	NNE	3
27	754.1	753.2	753.2	04.7	09.1	09.6	08.2	09.9	04.1	-	03.4	05.4	06.6	53	62	74	63	NE	4	ESE	5	ENE	3
28	748.6	747.2	746.3	11.6	11.9	11.8	11.8	12.4	09.1	-	09.3	09.1	07.9	91	87	76	85	SE	7	SE	2	NE	2
29	746.6	747.3	748.3	11.4	13.5	11.7	12.1	14.4	09.9	-	07.8	08.5	07.9	78	73	77	76	NE	2	E	2	NE	3
30	749.3	748.8	748.9	12.0	13.6	13.7	13.2	14.2	11.0	-	09.2	09.2	09.6	88	79	81	83	SSW	2	SE	4	SE	5
MES.	VRED.	750.7	750.6	751.1	10.0	12.6	11.1	11.2	13.6	08.6	-	06.8	07.5	07.1	68	65	67	67	3.1	3.2	3.1		

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1	748.2	748.8	750.4	14.4	14.2	11.1	12.7	15.1	10.9	-	09.6	10.9	09.5	78	90	95	88	SE	1	SSE	6	NNE	2
2	748.7	748.5	748.7	12.1	15.1	13.9	13.8	15.3	10.7	-	09.8	09.2	06.8	92	72	57	74	ESE	4	ESE	2	NE	2
3	750.1	751.6	753.0	10.6	14.0	12.5	12.4	14.3	10.1	-	07.2	07.9	07.8	75	66	72	71	ENE	2	NW	1	NW	1
4	756.5	756.6	758.5	09.8	13.4	11.8	11.7	13.6	09.5	-	06.6	08.6	08.3	73	75	80	76	NE	2	SW	1	NWW	1
5	757.7	757.1	757.0	09.8	12.9	10.6	11.0	13.3	09.0	-	06.4	06.4	06.1	71	58	64	64	NE	1	SSW	1	NWW	1
6	756.5	754.8	752.5	07.3	11.6	09.0	09.2	12.0	07.1	-	05.2	07.5	06.9	68	73	80	74	N	2	SW	1	NWW	2
7	751.8	754.5	755.4	08.8	08.7	06.0	07.4	09.8	05.8	-	04.7	01.9	02.2	56	23	31	37	NNE	1	NE	5	NE	3
8	753.1	752.4	752.4	03.9	08.0	08.4	07.2	08.6	03.6	-	02.7	05.0	05.9	45	63	72	60	NE	2	WSW	1	NW	1
9	754.5	756.1	756.6	06.6	10.9	09.0	08.9	11.0	06.4	-	04.9	05.4	04.7	67	55	55	59	NNE	2	SSE	1	NE	2
10	757.5	757.4	757.2	07.6	9.0	08.0	08.2	10.5	06.8	-	04.3	05.5	06.0	55	64	75	65	NE	1	NE	2	NE	2
11	755.9	755.7	755.3	09.2	11.6	08.6	09.6	11.7	07.7	-	04.8	04.7	04.5	55	46	52	51	NE	6	NE	2	NE	3
12	753.0	751.6	750.3	08.0	09.8	06.4	07.6	10.0	06.3	-	04.2	04.7	06.7	52	52	63	66	NE	3	ENE	2	NE	2
13	748.6	749.1	751.2	06.8	09.7	10.0	09.1	10.6	05.9	-	06.0	07.2	06.5	81	80	71	77	NE	3	NW	1	E	1
14	752.1	752.9	755.0	08.7	12.4	10.3	10.4	12.4	08.4	-	05.1	06.6	04.6	60	61	49	57	NE	2	S	1	NE	2
15	756.6	756.4	756.6	08.1	12.5	11.5	10.9	12.8	07.8	-	04.3	07.4	06.6	53	68	65	62	NE	2	SE	2</		

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 $H_s = 122 \text{ m } H_h = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9 0-9	Oblačnost N (0-10)					Intenziteta broj seti	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	6 020	09	06	05-7	05-3	.	.	.	$\Delta^2 rj-12^{\circ} = kv-n$	
2	6 03	010	00	01-3	07-4	.	.	.	$= T-14^{\circ}$	
3	8 05	040	00	03-0	06-9	.	.	.	$= n-14^{\circ}, \Delta rj-10$.
4	6 03	03	00	02-0	08-0
5	8 010	040	00	01-7	07-8
6	8 10	09	10	09-7	01-7	.	.	.	$\Delta^2 15^{\circ}-16^{\circ}$	
7	7 10	10	10	10-0	00-0	00-0	.	.	$\Delta^2 17^{\circ}-13^{\circ}$	
8	8 05	09	05	06-3	04-4	01-8	.	.	$\Delta^2 12^{\circ}, 15^{\circ}-17^{\circ}, 20^{\circ}-20^{\circ}, F_{NNNE} 9^{\circ}-15^{\circ}$	
9	8 10	09	10	09-7	00-0	01-5	.	.	$\Delta^2 12^{\circ}, 15^{\circ}-17^{\circ}, 20^{\circ}-20^{\circ}, F_{NNNE} 9^{\circ}-15^{\circ}$	
10	8 09	10-0	03	07-3	00-4	07-3	.	.	$\Delta^2 12^{\circ}, 15^{\circ}-17^{\circ}, 20^{\circ}-20^{\circ}, F_{NNNE} 9^{\circ}-15^{\circ}$	
11	8 09	09	01	06-3	01-6	06-3	.	.	$\Delta^2 12^{\circ}, 16^{\circ}-16^{\circ}$	
12	8 10	050	08	07-7	04-6	00-3	.	.	$\Delta^2 rj, 16^{\circ}-16^{\circ}$	
13	8 020	070	08	05-7	07-9	00-0	.	.	$\Delta^2 12^{\circ}, 8^{\circ}-10^{\circ}, 11^{\circ}-18^{\circ}, T-10^{\circ}-15^{\circ}$.
14	6 100	100	10	10-0	00-0	02-8	.	.	$F_{NNNE} 9^{\circ}-14^{\circ}, 16-n$.
15	8 05	020	06	04-3	08-3	13-0	.	.		.
16	6 100	100	100	10-0	00-0	01-8	.	.	$\Delta^2 14^{\circ}-24^{\circ}$	
17	8 100	10	100	10-0	00-0	13-5	.	.	$\Delta^2 10-11^{\circ}, 14^{\circ}-14^{\circ}, HV-i, F_{NNNE} 12^{\circ}-12^{\circ}, HV-HV, R-7^{\circ}, 8^{\circ}-8^{\circ}, \Delta 8^{\circ}-8^{\circ}$	
18	8 10	080	08	08-7	02-2	05-7	.	.	$F_{NNNE} 12^{\circ}-21^{\circ}, \Delta 15^{\circ}-15^{\circ}$	
19	8 10	10	07	09-0	02-8	24-1	.	.		.
20	8 09	09	100	09-3	03-2	04-4	.	.	$\Delta^2 12^{\circ}-21^{\circ}, \Delta 15^{\circ}-15^{\circ}$	
21	8 090	10	02	07-0	00-0	06-2	.	.	$\Delta^2 15^{\circ}-11^{\circ}, F_{NNNE} 9^{\circ}-n$	
22	9 02	020	00	01-3	08-6	09-4	.	.	$F_{NNNE} rj-n$.
23	8 03	070	07	05-7	04-0	.	.	.	$F_{NNNE} 7^{\circ}-n$.
24	8 04	080	00	04-0	01-8
25	8 00	000	00	00-0	08-7
26	8 03	010	03	02-3	08-1
27	8 07	10	10	09-0	00-3
28	6 100	100	100	10-0	00-0	00-2	.	.	$F_{NNNE} rj-16^{\circ}, \Delta^2 15^{\circ}-n$.
29	8 08	080	04	07-3	03-5	05-0	.	.	$\Delta^2 12^{\circ}-4^{\circ}$.
30	8 10	08	09	09-0	02-0	00-3	.	.	$\Delta^2 12^{\circ}-4^{\circ}$.
MES. VRED.		06.6	07.1	05.6	06.4	111.5	103.6			

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1	7 09	09	10-0	04-3	00-3	.	.	$F_{NNNE} rj-14^{\circ}, \Delta^2 9^{\circ}-9^{\circ}, 12^{\circ}-n; T-12^{\circ}-n$	
2	8 100	050	02	05-7	05-2	45-8	.		
3	7 04	050	00	03-0	04-7	01-2	.		
4	8 06	09	00	05-0	02-2	.	.		
5	8 03	060	00	01-0	07-6	.	.		
6	8 02	09	00	03-7	05-2	.	.		
7	8 02	000	00	06-7	07-6	.	.	$F_{NNNE} 7^{\circ}-15^{\circ}$.
8	8 00	10	09	04-3	02-3	.	.		.
9	8 00	000	00	00-0	07-8	.	.	$\Delta^2 12^{\circ}-17^{\circ}$.
10	7 09	100	10	09-7	00-0	.	.		.
11	8 03	020	06	04-3	04-9	00-7	.	$\Delta^2 rj-9^{\circ}, F_{NNNE} 6^{\circ}-9^{\circ}$	
12	7 10	100	100	10-0	00-0	.	.	$\Delta^2 13^{\circ}-24^{\circ}$	
13	8 09	060	09	06-0	03-2	07-3	.	$\Delta^2 0-4^{\circ}$	
14	8 08	020	02	04-6	05-0	.	.		.
15	8 08	05	09	07-3	05-6	.	.		.
16	8 10	10	100	10-0	00-0	.	.	$\Delta^2 9^{\circ}-n, F_{SE} 12^{\circ}-n$	
17	7 100	100	100	10-0	00-0	07-8	.	$F-F_{SE} n-16^{\circ}, \Delta^2 14^{\circ}-n$.
18	8 06	08	100	04-0	03-6	13-0	.	$\Delta^2 17^{\circ}-24^{\circ}$.
19	8 04	09	04	05-7	02-3	01-1	.	$F_{NN} n-n$.
20	8 08	010	00	00-3	04-6	.	.		.
21	8 02	030	00	01-7	07-4	.	.	$F_{NN} rj-9^{\circ}$.
22	8 03	020	00	01-7	08-0	.	.		.
23	8 03	000	00	01-0	07-9	.	.		.
24	8 00	010	09	03-3	07-5	.	.		.
25	7 100	10	10	10-0	00-0	00-0	.	$\Delta^2 n-7^{\circ}, F_{NNNE} 18^{\circ}-n$.
26	8 02	020	00	01-3	07-4	00-0	.	$F_{NNNE} 12^{\circ}-20^{\circ}$.
27	8 04	080	04	06-0	02-9	.	.		.
28	8 01	080	00	00-3	07-7	.	.	$\Delta^2 20^{\circ}-n$.
29	8 00	000	00	00-8	07-7	.	.		.
30	7 00	04	00	01-3	07-0	.	.	$\Delta^2 rj-9^{\circ}$.
31	7 04	09	00	04-3	09-8	.	.		.
MES. VRED.		04.6	05.1	04.1	04.6	140.2	76.9		

$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h\ 13\ min.$

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D	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, I (0-12)						
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21				
1	590.0	591.0	590.4	-17.0	-14.0	-07.6	-11.6	-07.6	-17.0	-	Cl.0	01.3	02.4	85	81	93	86	N	8	N	5	N	8	
2	590.0	592.2	594.2	-09.0	-09.8	-10.4	-09.9	-07.0	-10.4	-	0.1	02.0	01.9	94	91	90	91	N	11	N	8	N	6	
3	594.8	594.4	595.2	-11.0	-11.0	-11.6	-11.3	-10.4	-11.6	-	01.8	01.8	01.7	90	90	89	90	N	7	N	6	N	6	
4	596.0	595.9	596.1	-10.4	-07.4	-07.0	-08.0	-06.7	-11.6	-	01.9	02.4	02.5	90	93	93	92	NNE	3	N	3	N	5	
5	594.8	594.0	596.2	-09.0	-07.0	-02.4	-05.2	-02.4	-09.4	-	02.1	02.3	02.6	92	85	98	92	N	11	N	9	N	9	
6	597.1	596.3	595.4	00.0	-01.2	-02.2	-01.4	01.4	-02.4	-	02.7	03.6	02.4	58	86	86	77	NNW	5	WSW	6	WSW	6	
7	592.3	588.2	587.2	-03.0	-02.8	-04.0	-03.4	-02.0	-04.0	-	02.9	03.2	03.3	80	87	96	88	SSW	7	SW	10	SW	8	
8	584.3	582.4	584.1	-04.2	-04.6	-11.0	-07.7	-03.0	-11.0	-	03.2	03.1	01.8	96	96	90	94	SW	7	SW	8	N	9	
9	585.3	589.2	592.0	-12.6	-13.2	-15.4	-14.2	-11.0	-15.4	-	01.5	01.5	01.2	88	88	86	87	NW	9	NW	8	NW	7	
10	595.3	597.2	597.2	-12.6	-07.6	-07.0	-08.6	-07.0	-16.0	-	01.5	02.4	02.5	88	93	93	91	NW	5	NW	4	NW	1	
11	598.0	597.1	596.2	-05.8	-04.8	-04.4	-04.6	-04.0	-07.0	-	02.8	03.1	03.2	94	95	96	95	-	0	SW	3	SW	4	
12	595.9	597.4	596.5	-05.0	-04.0	-04.2	-04.4	-03.6	-05.2	-	03.0	03.2	03.1	95	93	92	93	SW	4	W	2	W	2	
13	597.0	597.4	596.1	-04.8	-04.0	-05.4	-04.9	-04.0	-05.4	-	02.9	03.0	02.8	92	89	91	91	SW	2	SW	3	NW	2	
14	599.2	600.2	601.2	-04.0	-02.8	-02.6	-03.0	-02.0	-05.6	-	02.7	03.2	03.3	78	85	87	83	-	0	-	0	WSW	5	
15	601.3	601.2	601.1	-01.0	02.0	01.0	00.0	04.6	-03.4	-	02.3	01.3	02.8	53	24	65	47	W	5	NW	3	SW	5	
16	598.7	597.5	597.1	-00.4	00.6	00.2	00.2	01.0	-01.2	-	02.1	01.8	01.5	46	37	32	38	SW	11	SW	10	SW	12	
17	595.6	594.8	594.8	00.0	00.6	-01.0	0.0	01.2	-01.0	-	01.3	01.4	01.4	29	28	32	30	SW	12	SW	10	SW	9	
18	593.4	592.3	592.4	-01.4	01.0	-00.6	-00.4	01.2	-01.6	-	01.5	01.7	01.3	36	35	29	33	SW	8	SW	8	SW	8	
19	591.3	593.4	596.0	-00.6	00.8	-00.4	-00.2	01.0	-01.6	-	01.2	01.6	01.8	26	34	39	33	SW	11	SW	8	SW	4	
20	597.1	597.4	596.9	-02.0	-00.6	-00.4	-00.8	01.0	-02.0	-	01.2	01.2	01.7	30	26	38	31	NNE	3	E	2	SE	2	
21	596.4	596.2	596.0	-00.6	C1.0	-01.2	-00.5	01.4	-01.2	-	01.5	01.3	01.2	33	27	30	30	-	0	W	2	SW	2	
22	595.1	594.2	592.9	-02.0	-02.4	-06.0	-04.1	-01.2	-09.0	-	01.4	01.7	01.6	35	43	56	45	SW	2	SW	2	N	3	
23	592.2	592.0	591.3	-04.8	-04.0	-04.7	-04.6	-03.2	-06.0	-	02.5	03.0	03.1	77	89	95	87	NNW	7	SW	4	SW	7	
24	590.9	591.1	591.8	-04.2	-04.2	-04.0	-04.1	-04.0	-05.2	-	03.2	03.2	03.3	96	96	96	96	SW	7	SW	6	SW	4	
25	593.0	594.0	593.8	-05.0	-03.4	-03.1	-03.6	-02.8	-05.4	-	03.0	03.5	02.9	95	97	76	90	-	0	-	0	SW	5	
26	593.5	594.4	594.5	-03.2	-01.6	-03.1	-02.8	-01.4	-04.2	-	03.5	04.0	03.5	97	96	97	97	NW	4	N	4	N	2	
27	593.3	592.4	587.3	-06.4	-05.4	-04.3	-05.1	-02.8	-06.6	-	02.7	02.3	03.2	94	76	96	89	N	2	NW	3	SSM	10	
28	583.0	581.5	583.5	-03.6	-03.8	-03.8	-03.8	-02.2	-04.8	-	03.4	03.3	03.3	97	96	96	96	SSM	13	SW	5	S	3	
29	582.5	583.8	585.7	-05.6	-06.0	-06.0	-06.9	-03.2	-06.0	-	02.9	02.8	02.3	95	94	92	94	SW	7	NNE	8	N	10	
30	587.7	588.4	587.5	-09.4	-07.6	-10.2	-09.4	-07.0	-10.2	-	02.1	02.4	01.9	91	93	90	91	N	7	N	7	N	10	
31	591.0	593.8	594.6	-11.0	-08.0	-08.2	-08.8	-07.5	-11.4	-	01.8	02.3	02.3	90	92	92	91	N	12	NNE	7	NNE	5	
MES.	VRED.	593.1	593.3	593.4	-05.5	-04.3	-05.0	-05.0	-03.0	-06.9	-	02.2	02.4	02.4	75	75	78	76	6.1	5.3	5.8	5.8	5.8	5.8

1975 FEBRUAR

BJELAŠNICA

1	793.1	594.2	595.3	-03.8	-06.0	-08.8	-06.8	-03.0	-08.8	-	03.3	02.0	01.9	94	69	81	81	N	7	N	5	N	7
2	595.4	594.4	592.0	-10.6	-08.0	-07.0	-08.2	-06.8	-10.6	-	01.8	02.3	02.5	90	92	93	92	N	5	N	6	N	8
3	589.7	590.8	592.6	-07.8	-09.0	-11.6	-10.0	-07.0	-11.6	-	02.4	02.1	01.7	93	92	89	91	N	7	N	7	N	6
4	594.4	596.4	597.9	-11.0	-06.4	-07.0	-07.8	-06.2	-12.6	-	01.8	02.7	02.5	90	94	93	92	NE	3	E	2	E	3
5	599.2	599.2	598.8	-06.4	-07.0	-08.0	-07.4	-05.0	-09.4	-	01.8	02.2	01.9	63	81	77	74	NE	3	NE	2	N	6
6	598.8	599.1	598.9	-06.4	-02.4	-02.4	-03.4	-02.2	-08.2	-	00.8	02.2	01.5	29	58	40	42	N	6	ESE	2	-	0
7	595.2	592.9	589.6	-03.0	-02.2	-05.0	-03.8	-01.2	-06.2	-	01.7	02.4	01.7	47	62	55	55	SW	7	SW	3	N	9
8	586.3	584.0	588.0	-12.0	-14.6	-17.0	-15.2	-05.0	-17.0	-	01.6	01.3	01.0	89	67	85	87	N	13	N	13	N	9
9	589.0	590.9	591.5	-18.0	-14.7	-11.0	-13.7	-11.0	-18.0	-	00.9	01.3	01.7	84	87	85	85	N	4	N	5	N	3
10	592.9	593.1	592.2	-06.0	-05.2	-04.2	-04.9	-03.6	-11.0	-	02.2	01.6	01.1	75	53	34	54	N	2	W	4	W	5
11	592.2	592.0	591.5	-07.8	-05.8	-06.4	-06.6	-04.0	-07.8	-	02.4	02.8	02.7	93	94	94	94	W	5	W	8	W	9
12	590.7	590.0	588.0	-06.4	-05.4	-06.2	-06.0	-05.2	-06.8	-	02.7	02.9	02.7	94	95	94	94	SW	6	SW	7	SW	8
13	584.8	585.0	583.8	-04.6	-03.2	-03.0	-03.4	-02.7	-06.6	-	03.1	03.5	03.6	96	97	97	97	SW	11	SW	5	SSM	5
14	583.0	583.5	584.4	-03.4	00.4	-02.2	-02.0	00.4	-03.6	-	03.5	04.4	03.8	97	100	98	96	-	2	SE	2	SSW	2
15	587.0	588.8	590.0	-05.0	-02.0	-03.2	-03.4	-01.4	-05.4	-	03.0	03.9	03.5	95	98	97	97	NW	2				

OJELAŠNICA

1975 JANUAR

DR. ST. 139

$$H_{\text{g}} = 2067 \text{ m} \quad H_{\text{b}} = 2070,4 \text{ m} \quad h_t = 3,0 \text{ m} \quad h_r = 1,5 \text{ m}$$

REFLEXIONE

1973 EDITION

1	8	66	10	10	06.7	05.0	.	50	$V^{\circ} 20-10^{\circ} 23^{\circ} 24^{\circ}$, $F-F_{Nw}-0-24, = 0-24^{\circ} 24^{\circ}$, $= 0-24^{\circ} 24^{\circ}$, \boxed{B}
2	8	10	10	10	10.0	00.0	.	49	$F-F_{Nw}-0-24, = 0-24^{\circ} 24^{\circ}$, $V^{\circ} 0-9^{\circ} 13^{\circ} 24^{\circ}$, \boxed{B}
3	8	10	10	10	10.0	00.0	.	49	$V^{\circ} 0-24^{\circ}$, $F-F_{Nw}-0-24, = 0-24^{\circ} 24^{\circ}$, \boxed{B}
4	8	10	10	10	10.0	00.0	00.6	52	$\frac{1}{2} 0-15^{\circ} V^{\circ} 0-24^{\circ}, F_w 0-0^{\circ} 0^{\circ} 45^{\circ} 24^{\circ}$, \boxed{B}
5	8	66	66	66	00.0	00.0	09.8	52	$V^{\circ} 0-24^{\circ}, \frac{1}{2} 0-15^{\circ} F-F_{Nw}-0-24, = 15^{\circ} 24^{\circ}$, \boxed{B}
6	8	66	66	66	00.0	00.0	C9.9	51	$V^{\circ} 0-45^{\circ} F-F_{Nw}-0-9^{\circ}$, \boxed{B}
7	8	66	66	66	00.0	00.0	09.9	49	$\frac{1}{2} 0-44^{\circ} F-F_{Nw}-0-24^{\circ} 24^{\circ}, 44^{\circ} 24^{\circ}$, \boxed{B}
8	8	10	10	10	10.0	00.0	.	48	$F-F_{Nw}-0-24^{\circ} F-F_{Nw}-0-24^{\circ} 24^{\circ} V^{\circ} 45^{\circ} 24^{\circ}$, \boxed{B}
9	9	10	10	10	00.0	03.3	08.7	47	$F-F_{Nw}-0-10^{\circ}$, $\frac{1}{2} 0-8^{\circ} V^{\circ} 0-24^{\circ}, 8^{\circ} 10^{\circ}$, \boxed{B}
10	9	66	66	66	00.0	00.0	10.3	47	$V^{\circ} 0-40^{\circ}, F_w 16^{\circ} 24^{\circ}$, \boxed{B}
11	8	10	10	10	10.0	00.0	.	46	$F-F_{Nw}-w-0-24, V^{\circ} 4^{\circ} 24^{\circ} = 5^{\circ} 22^{\circ}$, \boxed{B}
12	8	10	10	10	10.0	00.0	.	46	$V^{\circ} 0-24^{\circ}, F-F_{Nw}-0-24, = 0-24^{\circ} 24^{\circ}$, \boxed{B}
13	8	10	03	10	07.7	03.0	.	46	$V^{\circ} 0-24^{\circ}, F-F_{Nw}-0-24^{\circ} = 0-40^{\circ} = 44^{\circ} 24^{\circ} * 15^{\circ} 24^{\circ}$, \boxed{B}
14	8	10	10	10	10.0	00.0	04.6	53	$V^{\circ} 0-15^{\circ} 24^{\circ}, \frac{1}{2} 0-24^{\circ} F-F_{Nw}-0-4^{\circ} 32^{\circ} 24^{\circ} * 0-0^{\circ} 10^{\circ} 24^{\circ}$, \boxed{B}
15	8	10	10	10	10.0	03.4	08.4	63	$* 0-5^{\circ} 17^{\circ} 19^{\circ} 20^{\circ} = 20-7^{\circ} V^{\circ} 0-24^{\circ}, 7^{\circ} 24^{\circ} 24^{\circ} = 0-24^{\circ} 24^{\circ} F_{Nw}-0$
16	8	67	10	10	09.0	01.6	01.0	64	$V^{\circ} 20-24^{\circ} 0-0^{\circ} 6^{\circ} 24^{\circ} 7^{\circ} 24^{\circ} = 20^{\circ} 24^{\circ} F-F_{Nw}-0^{\circ} 24^{\circ} 12^{\circ} 24^{\circ}$, \boxed{B}
17	9	66	66	10	09.3	08.1	02.8	68	$V^{\circ} 0-24^{\circ}, = 0-5^{\circ} 15^{\circ} 24^{\circ}, 15^{\circ} 24^{\circ} 0-20^{\circ} * 0-0^{\circ} 14^{\circ} 6^{\circ} 24^{\circ} 24^{\circ}$, \boxed{B}
18	8	10	06	06	03.3	05.4	.	66	$V^{\circ} 0-24^{\circ}, 20-10^{\circ} F-F_{Nw}-0-0^{\circ} 5^{\circ} 24^{\circ} 14^{\circ} 24^{\circ} 10^{\circ} 24^{\circ} = 15^{\circ} 17^{\circ}$, \boxed{B}
19	8	66	62	65	02.3	07.8	.	66	$V^{\circ} 0-24^{\circ}, F_{Nw}-0-5^{\circ} 4^{\circ} 12^{\circ} 24^{\circ} 12^{\circ} 24^{\circ}$, \boxed{B}
20	8	10	10	10	10.0	00.0	.	65	$V^{\circ} 0-24^{\circ}, F-F_{Nw}-3^{\circ} 24^{\circ}, = 6^{\circ} 24^{\circ}$, \boxed{B}
21	8	10	10	10	10.0	00.0	.	64	$V^{\circ} 0-24^{\circ}, = 0-24^{\circ} F-F_{Nw}-0-24^{\circ}$, \boxed{B}
22	8	22	010	10	04.3	00.7	.	63	$V^{\circ} 0-24^{\circ}, = 0-6^{\circ} 15^{\circ} 24^{\circ} F-F_{Nw}-0-24^{\circ}, = 6^{\circ} 10^{\circ}$, \boxed{B}
23	8	10	030	10	07.7	06.6	.	62	$V^{\circ} 0-24^{\circ}, F-F_{Nw}-0-22^{\circ}, = 0-10^{\circ} 18^{\circ} 21^{\circ} 12^{\circ} 24^{\circ} 14^{\circ} 24^{\circ} = 16^{\circ} 18^{\circ}$, \boxed{B}
24	8	62	06	10	06.0	07.6	.	62	$V^{\circ} 0-24^{\circ} 5^{\circ} 14^{\circ} 24^{\circ} = 14^{\circ} 24^{\circ}$, \boxed{B}
25	8	66	10	10	06.7	C1.4	.	62	$V^{\circ} 0-24^{\circ}, = 0-20-24^{\circ}, F-F_{Nw}-0-24^{\circ}$, \boxed{B}
26	8	10	10	10	10.0	00.0	.	62	$V^{\circ} 20-24^{\circ}, = 0-24^{\circ} F-F_{Nw}-0-24^{\circ} * 16^{\circ} 20^{\circ} + 16^{\circ} 24^{\circ}$, \boxed{B}
27	8	10	02	00	04.0	07.4	01.2	64	$V^{\circ} 0-24^{\circ}, = 0-8^{\circ} F-F_{Nw}-0-24^{\circ} + 0-4^{\circ} 24^{\circ} + 0-8^{\circ} 13^{\circ}$, \boxed{B}
28	9	66	02	00	06.7	10.5	.	64	$V^{\circ} 0-24^{\circ}, F-F_{Nw}-0-24^{\circ} + 0-4^{\circ} 13^{\circ} 24^{\circ} 19^{\circ}$, \boxed{B}

$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h\ 13\ min.$

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d d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina vетра D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	592.0	594.3	594.3	-06.4	-03.4	-02.6	-03.8	-02.2	-08.2	-	61.0	01.4	01.2	35	38	32	35	N	8	SW	3	SW	4	
2	593.2	595.0	595.0	-03.2	-01.2	01.0	-00.6	01.0	-05.0	-	01.9	02.6	02.4	53	61	49	54	SW	9	SW	5	WSW	5	
3	591.3	592.9	591.7	-00.2	-00.2	-02.6	-01.5	01.0	-03.0	-	01.3	01.7	03.6	28	38	96	54	SW	7	SSW	5	SSW	6	
4	588.6	587.0	586.0	-04.4	-03.0	-04.0	-03.8	-02.7	-04.4	-	03.2	03.6	03.3	96	97	96	96	SW	9	SW	1C	SW	11	
5	587.4	588.5	589.4	-03.6	-02.4	-03.2	-03.1	-02.2	-04.6	-	03.4	03.8	03.5	97	98	97	97	SW	8	SSW	8	SSW	9	
6	591.5	593.7	592.6	-03.0	-01.0	-01.8	-01.9	-00.8	-03.4	-	03.6	04.2	03.9	97	99	98	98	SW	9	S	6	SSW	9	
7	591.5	593.0	591.0	-01.6	00.6	-01.0	-00.8	00.8	-02.0	-	04.0	04.8	03.5	98	100	83	94	S	10	SSW	8	SSW	12	
8	590.6	593.1	591.9	-00.5	01.4	00.4	00.4	01.4	-01.4	-	02.4	02.7	01.8	54	54	38	49	SSW	11	SSW	5	SSW	4	
9	587.2	588.6	583.0	-00.1	00.4	-02.4	-01.1	01.4	-02.4	-	02.1	03.1	03.8	46	65	98	70	SSW	4	SW	3	SSW	7	
10	581.8	583.4	584.7	-02.4	00.4	-01.6	-01.3	02.0	-02.6	-	03.8	04.6	04.0	98	97	98	98	SSW	8	S	6	S'	6	
11	587.0	591.1	591.0	-02.8	-02.0	-03.8	-03.1	-01.4	-03.8	-	03.6	03.9	03.3	97	98	96	97	SSW	8	SW	6	SSW	7	
12	588.2	587.9	587.2	-04.0	-03.2	-03.6	-03.6	-01.8	-06.6	-	02.6	03.5	03.4	77	97	97	90	SW	12	S	10	SW	10	
13	587.2	588.4	588.4	-04.6	-01.6	-02.4	-02.8	-01.4	-04.6	-	03.1	03.9	03.8	96	95	98	96	SW	12	SSW	11	E	5	
14	584.4	586.5	586.4	-01.8	-00.2	-02.8	-01.9	00.2	-02.8	-	03.9	04.5	03.6	98	100	97	98	S	11	SW	5	SW	7	
15	587.8	589.6	590.0	-03.8	-02.8	-03.6	-03.4	-02.6	-04.4	-	03.3	03.6	03.4	96	97	97	97	SW	9	SW	7	SW	7	
16	588.7	588.4	587.2	-04.0	-00.8	-04.6	-03.2	-00.4	-04.6	-	03.3	04.3	03.3	96	99	96	97	SW	6	SW	4	SW	5	
17	586.1	586.1	586.0	-05.6	-01.4	-03.0	-03.2	-00.8	-05.8	-	02.9	04.1	03.3	95	99	90	95	SW	5	SW	3	SW	3	
18	584.9	585.1	586.0	-06.0	-04.4	-04.2	-04.7	-03.0	-06.2	-	02.8	03.2	03.2	94	96	96	95	SW	7	SW	8	SW	8	
19	585.1	587.8	587.0	-03.0	00.0	-00.4	-01.0	00.4	-04.6	-	03.6	04.2	03.7	97	91	84	91	SSW	9	SSW	5	SSW	8	
20	586.2	588.1	588.8	-01.4	00.0	-00.1	-00.4	00.8	-01.8	-	04.1	04.6	04.5	99	100	98	99	SSW	7	SW	3	SW	2	
21	587.5	586.3	584.7	-02.0	-05.0	-09.8	-04.6	00.0	-06.8	-	03.9	03.0	02.0	98	95	91	95	-	0	N	5	N	8	
22	584.4	585.9	582.4	-14.0	-12.8	-13.2	-13.3	-09.8	-14.8	-	01.4	01.5	01.5	87	88	88	88	N	7	N	9	N	8	
23	580.6	580.1	581.5	-12.0	-05.2	-05.0	-06.8	-04.8	-13.4	-	01.6	03.0	03.0	89	95	95	93	-	0	SSW	5	SE	4	
24	578.4	579.3	580.1	-09.0	-07.2	-10.0	-09.0	-04.6	-10.0	-	02.1	02.5	01.9	92	93	91	92	NE	3	NE	2	NNE	3	
25	580.4	581.9	582.2	-11.4	-09.0	-11.2	-10.7	-08.4	-11.6	-	01.7	02.1	01.8	89	92	90	90	NNE	5	N	6	N	10	
26	586.0	587.0	585.4	-12.0	-05.8	-05.2	-07.0	-04.0	-12.4	-	01.5	02.6	02.4	84	87	78	83	N	6	SW	6	SW	10	
27	586.3	584.5	583.0	-05.4	-03.6	-03.0	-03.8	-03.0	-06.2	-	02.9	03.4	03.6	95	97	97	96	SW	8	SW	12	SW	12	
28	582.0	580.8	580.0	-01.8	-01.0	-00.2	-00.8	-00.2	-03.0	-	03.9	04.2	04.5	98	99	100	99	SW	13	SW	13	SW	14	
29	583.6	584.7	585.4	-00.8	00.8	-01.6	-00.9	00.0	-01.0	-	04.3	04.3	04.2	99	99	99	99	SW	12	SW	14	SW	10	
30	584.6	584.5	585.0	-01.4	00.0	00.0	-00.4	00.4	-02.0	-	04.1	04.6	04.2	99	100	92	97	SSW	12	SW	11	SSW	12	
31	585.8	584.8	588.0	00.4	01.3	00.6	00.7	01.8	-00.2	-	04.5	05.0	04.8	95	100	100	98	SW	7	SSW	5	SW	7	
MES.	VRED.	586.8	587.2	586.9	-04.2	-02.4	-03.4	-03.3	-01.4	-05.4	-	03.0	03.5	03.2	86	89	89	88	7.9	7.0	7.0	7.5		

1	585.4	587.6	589.3	01.1	00.0	-00.4	00.1	01.6	-00.4	-	65.0	04.6	04.5	100	100	100	100	SW	10	SW	6	SW	5
2	587.4	586.0	584.8	-01.0	-00.6	-02.4	-01.6	00.0	-02.4	-	04.2	04.4	03.8	99	100	98	99	SW	4	SW	6	SSW	7
3	584.4	584.6	586.0	-04.6	-03.8	-04.0	-04.1	-02.4	-05.2	-	03.1	03.3	03.3	96	96	96	96	SSW	6	SW	7	SW	8
4	588.3	590.2	591.0	-04.2	-03.0	-03.0	-03.3	-01.8	-04.4	-	03.2	03.6	03.6	96	97	97	97	SW	10	SSW	8	SSW	8
5	586.8	593.4	590.5	-03.0	00.0	00.0	00.8	00.0	-03.9	-	03.6	04.6	04.6	97	100	100	99	SSW	11	SSW	14		
6	595.0	595.6	598.0	02.0	04.0	03.4	03.2	04.2	00.0	-	03.3	03.0	02.3	62	50	39	50	SSW	10	SSW	1C	SSW	11
7	591.0	591.2	589.6	03.0	04.4	02.6	03.2	05.4	02.0	-	02.0	02.2	01.9	35	34	34	34	SSW	12	SW	12		
8	588.1	588.7	590.0	00.6	-02.0	-02.8	-01.8	03.0	-02.8	-	04.8	03.9	03.6	100	98	97	98	SW	11	SW	7	SW	5
9	590.4	591.4	589.2	-03.4	00.4	-02.0	-01.8	00.6	-04.4	-	03.4	04.0	02.7	97	85	69	84	SW	8	SW	7	SW	11
10	587.0	582.3	580.2	-01.8	-00.8	-02.6	-02.0	-00.1	-03.2	-	03.9	04.3	03.7	98	99	97	98	SW	10	SW	8	SSW	11
11	586.1	589.8	591.0	-04.6	-07.2	-03.6	-05.2	-02.6	-08.0	-	02.6	02.5	03.4	94	93	97	95	SW	5	N	5	SW	4
12	590.6	591.6	592.5	-03.4	-04.6	-05.8	-05.9	-03.0	-04.8	-	02.9	02.6	02.8	95	94	94	94	MSW	2	N	4	N	3
13	593.6	593.7	593.3	-03.4	-01.2	-01.6	-02.0	-01.0	-07.4	-	03.5	04.2	04.0	97	99	98	98	W	2	SW	7	MSW	6
14	593.5	594.2	593.8	-03.0	00.4	00.0	-00.6	00.8	-04.0	-	03.4	04.1	04.2	94	88	91	91	N	4	SW	2	SW	5
15	591.1	589.1	586.4	-00.4	01.2	-00.4	-00.1	01.2	-01.4	-	02.5	04.0	03.6	56	81	82							

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 $H_a = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vrhovost 0-9	Oblaknost N (0-10)					Isotrofija broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	9 00	00 0	00 0	00	00.0	10.9	.	61	F-Fsw 0-24, $\frac{1}{2} 5^{\circ} 12^{\circ}, Fsw 24^{\circ} 23^{\circ}, \boxed{\star}$	
2	9 06	02 0	00	02.7	05.2	.	56	F-Fsw 0-24, $\frac{1}{2} 24^{\circ}, \boxed{\star}$		
3	9 05	01 0	05	03.7	09.9	.	50	F-Fsw 0-24, $\frac{1}{2} 10^{\circ} 20^{\circ} 24^{\circ}, V^{\circ} 22^{\circ} 24^{\circ}, \boxed{\star}$		
4	0 10	10 \equiv	07	09.0	00.0	.	48	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$		
5	0 10	10 \equiv	10 \equiv	10.0	00.0	.	48	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$		
6	8 10	06	03	06.3	03.5	02.0	52	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$		
7	8 05	09	04	06.0	03.5	.	50	F-Fsw 0-24, $\frac{1}{2} 0-16^{\circ}, \boxed{\star}$		
8	8 09	10	00	06.3	00.0	.	46	F-Fsw 0-24, $\frac{1}{2} 0-20^{\circ}, \boxed{\star}$		
9	8 06	05	10 \equiv	07.7	06.5	.	43	$\frac{1}{2} 10^{\circ} 24^{\circ}, \frac{1}{2} 24^{\circ}, F-Fsw 17^{\circ} 24^{\circ}, V^{\circ} 22^{\circ} 24^{\circ}, \boxed{\star}$		
10	0 10	10 \equiv	10 \equiv	10.0	00.0	01.2	43	$\frac{1}{2} 0-78^{\circ}, \frac{1}{2} 24^{\circ}, F-Fsw 0-24, V^{\circ} 0-24, \boxed{\star}$		
11	0 10	10 \equiv	10 \equiv	10.0	00.0	01.5	44	F-Fsw 0-24, $\frac{1}{2} 0-23^{\circ}, V^{\circ} 0-24, \frac{1}{2} 17^{\circ} 14^{\circ}, \boxed{\star}$		
12	0 00	10 \equiv	03	04.3	00.6	01.4	46	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 10^{\circ} 16^{\circ}, \frac{1}{2} 20^{\circ} 24^{\circ}, V^{\circ} 22^{\circ} 23^{\circ}, \boxed{\star}$		
13	8 09	10	10 \equiv	09.7	01.1	03.2	53	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-8^{\circ} 4^{\circ}, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 16^{\circ}, \frac{1}{2} 20^{\circ} 24^{\circ}, V^{\circ} 22^{\circ} 23^{\circ}, \boxed{\star}$		
14	0 10	10 \equiv	10 \equiv	10.0	00.0	11.2	68	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 16^{\circ}, \frac{1}{2} 20^{\circ} 24^{\circ}, V^{\circ} 22^{\circ} 23^{\circ}, \boxed{\star}$		
15	0 10	10 \equiv	10 \equiv	10.0	00.0	00.0	78	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 16^{\circ}, \frac{1}{2} 20^{\circ} 24^{\circ}, V^{\circ} 22^{\circ} 23^{\circ}, \boxed{\star}$		
16	0 10	10 \equiv	10 \equiv	10 \equiv	10.0	01.1	81	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \frac{1}{2} 16^{\circ} 24^{\circ}, \boxed{\star}$		
17	8 10	10	04	08.0	00.0	01.2	83	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 16^{\circ}, \boxed{\star}$		
18	0 10	10 \equiv	10 \equiv	10.0	00.0	.	80	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 16^{\circ}, \boxed{\star}$		
19	8 10	09	07	08.7	03.2	.	79	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 16^{\circ}, \frac{1}{2} 20^{\circ} 24^{\circ}, \boxed{\star}$		
20	0 10	10 \equiv	10 \equiv	10.0	00.0	.	77	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 16^{\circ}, \frac{1}{2} 20^{\circ} 24^{\circ}, \boxed{\star}$		
21	0 10 \equiv	10 \equiv	10 \equiv	10.0	00.0	06.4	84	V^{\circ} 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \frac{1}{2} 16^{\circ} 24^{\circ}, \boxed{\star}$		
22	0 10	10 \equiv	10 \equiv	10.0	00.0	10.4	102	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
23	8 10	09	10 \equiv	09.7	00.0	.	100	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
24	0 10 \equiv	10 \equiv	10 \equiv	10.0	00.0	01.4	100	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
25	8 04	09	10 \equiv	07.7	08.9	08.1	109	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
26	9 05	04	01	03.3	10.8	02.0	112	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
27	0 10	10 \equiv	10 \equiv	10.0	00.0	01.2	110	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
28	0 10	10 \equiv	10 \equiv	10.0	00.0	03.0	113	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
29	0 10	10 \equiv	10 \equiv	10	10.0	00.0	110	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
30	9 10	05	02	05.7	06.7	.	104	F-Fsw 0-24, V^{\circ} 0-15^{\circ}, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
31	0 10	10	10	10 \equiv	10.0	00.0	06.5	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$		
MES. VRED.	08.4	08.4	07.3	08.0	76.6	76.3				

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1	0 10	10 \equiv	10 \equiv	10 \equiv	10.0	00.0	07.4	67	F-Fsw 0-15 $\frac{1}{2} 20^{\circ} 23^{\circ}, \frac{1}{2} 12^{\circ} 18^{\circ}, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$
2	0 10 \equiv	10 \equiv	10 \equiv	10.0	00.0	20.1	68	$\frac{1}{2} 0-24, \frac{1}{2} 24^{\circ}, F-Fsw 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
3	0 10	10 \equiv	10 \equiv	10.0	00.0	07.4	78	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
4	0 10	10 \equiv	10 \equiv	04	08.0	00.0	76	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
5	8 06	10	04	06.7	06.7	02.4	73	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
6	8 08	09	04	07.0	04.1	.	64	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
7	8 09	08	00	05.7	03.5	.	58	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
8	0 10	10 \equiv	10 \equiv	00	06.7	00.0	52	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 14^{\circ}, \frac{1}{2} 10^{\circ} 14^{\circ}, \frac{1}{2} 10^{\circ} 14^{\circ}, \frac{1}{2} 10^{\circ} 14^{\circ}, \boxed{\star}$	
9	9 10	01	01	01	04.0	10.3	52	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
10	0 10	10 \equiv	10 \equiv	10.0	00.5	00.3	50	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 10^{\circ} 14^{\circ}, \frac{1}{2} 10^{\circ} 14^{\circ}, \frac{1}{2} 10^{\circ} 14^{\circ}, \boxed{\star}$	
11	1 10	10 \equiv	00	06.7	00.5	08.0	56	V^{\circ} 0-24, F-Fsw 0-14 $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \frac{1}{2} 12^{\circ} 18^{\circ}, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
12	0 10 \equiv	10 \equiv	00	06.7	02.9	15.8	68	V^{\circ} 0-24, F-Fsw 0-14 $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
13	8 00	04	00	01.3	09.3	05.4	74	V^{\circ} 0-24, F-Fsw 0-14 $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
14	9 01	03	02	02.0	12.8	.	65	V^{\circ} 0-24, F-Fsw 0-14 $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
15	9 00	02	01	01.0	12.5	.	60	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
16	0 10	10 \equiv	10 \equiv	10.0	00.0	.	57	F-Fsw 0-15, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
17	0 10	10 \equiv	10 \equiv	10.0	00.0	01.0	57	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
18	0 10	10 \equiv	10 \equiv	10.0	00.0	.	57	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
19	8 10	06	10 \equiv	06.7	05.7	.	57	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
20	8 00	00	00	00.0	12.8	.	56	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
21	8 00	02	04	02.0	12.8	.	54	V^{\circ} 0-24, F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
22	7 08	08	10	08.7	06.0	.	49	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
23	8 10	08	10 \equiv	09.3	03.8	.	47	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
24	0 10	10 \equiv	10 \equiv	10.0	00.0	.	44	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
25	0 10	10 \equiv	10 \equiv	10.0	00.0	00.5	41	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
26	0 10	10 \equiv	10 \equiv	10.0	00.0	10.4	51	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
27	0 10	10 \equiv	10 \equiv	10.0	00.0	04.8	57	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
28	0 10	10 \equiv	10 \equiv	10.0	00.0	04.8	61	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \frac{1}{2} 12^{\circ} 18^{\circ}, \boxed{\star}$	
29	8 04	03	00	02.3	13.1	.	60	F-Fsw 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
30	8 00	03	02	02.0	13.2	.	57	V^{\circ} 0-24, $\frac{1}{2} 0-24, V^{\circ} 0-24, \boxed{\star}$	
MES. VRED.	07.5	07.6	05.8	07.0	126.2	87.6			

$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h\ 13\ min.$

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D G	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	594.3	595.4	594.8	-00.4	01.2	01.0	00.7	02.4	-01.2	-	04.2	03.4	04.9	94	68	100	87	N	7	N	8	N	10
2	592.2	591.3	590.3	-02.4	-02.4	-01.4	-02.0	01.0	-02.7	-	03.8	03.7	04.1	98	97	100	98	N	12	N	12	N	12
3	589.7	590.8	590.8	-01.2	-00.6	00.0	-00.4	00.1	-01.4	-	04.2	04.4	04.6	100	100	100	100	N	9	N	5	N	2
4	590.9	590.0	593.3	00.0	00.4	01.0	00.6	01.0	-00.1	-	04.6	04.7	04.9	100	100	100	100	-	0	-	0	SW	4
5	593.5	595.5	595.8	-00.2	03.2	02.6	02.0	03.6	-00.3	-	04.5	05.0	04.6	100	86	83	90	SW	8	SW	6	SSM	5
6	595.5	595.3	595.2	02.4	06.0	03.8	04.0	06.0	01.6	-	02.7	04.5	05.0	49	64	83	65	SSE	6	S	7	SW	8
7	595.1	594.6	594.1	05.0	06.8	05.8	05.8	08.0	03.0	-	06.5	06.9	06.9	100	93	100	98	SM	7	-	0	-	0
8	591.0	589.5	590.8	04.8	05.0	02.0	03.4	06.7	01.9	-	06.5	06.5	05.3	100	100	100	100	SW	8	SW	8	SW	4
9	591.0	592.5	593.6	00.6	04.0	01.0	01.6	04.8	00.3	-	04.8	03.8	04.8	100	63	97	87	SM	4	SM	5	SM	3
10	593.9	595.0	594.7	02.2	06.4	03.6	04.0	06.4	-00.2	-	04.3	05.0	05.3	80	69	89	79	-	0	-	0	-	0
11	594.0	593.4	591.9	04.8	06.2	05.6	04.0	06.6	02.6	-	06.2	05.3	06.1	96	90	84	-	0	-	0	SM	5	
12	590.0	589.7	588.7	04.6	07.0	03.0	04.4	07.6	03.0	-	04.4	05.2	05.6	70	69	99	79	SW	4	S	6	N	3
13	587.8	586.2	587.6	03.4	05.6	03.4	04.0	06.1	02.8	-	05.8	06.6	05.8	100	100	100	100	NE	4	E	5	NE	5
14	588.8	587.3	587.7	03.0	02.3	02.0	02.3	04.1	02.0	-	05.7	05.4	05.3	100	100	100	100	N	7	N	6	-	0
15	589.0	591.5	592.4	02.0	05.2	05.0	04.3	05.2	02.0	-	05.3	06.6	06.5	100	99	100	100	N	2	N	3	N	2
16	592.6	594.4	595.2	06.0	07.0	07.4	07.0	10.7	04.2	-	05.3	06.1	07.7	76	81	100	86	N	2	-	0	W	3
17	595.2	596.2	597.3	07.0	10.2	08.0	08.3	10.6	06.7	-	04.1	05.9	07.1	95	63	88	69	NW	5	-	0	NNW	2
18	597.4	598.7	598.7	06.3	09.0	06.2	06.9	09.6	06.0	-	07.2	04.9	06.8	100	57	95	84	N	4	NW	6	N	7
19	598.5	599.4	599.9	06.0	09.6	08.0	07.9	10.6	05.0	-	07.0	07.0	08.0	100	78	100	93	N	7	NE	3	N	3
20	598.4	598.0	597.2	08.4	10.4	06.8	08.1	11.5	06.8	-	06.2	06.1	05.7	75	64	76	72	N	3	SSM	3	N	4
21	596.8	597.5	597.4	05.6	10.0	08.2	08.0	10.4	05.0	-	06.8	05.1	06.3	100	55	77	77	N	6	NE	2	SW	2
22	596.4	599.6	599.0	09.2	13.4	07.2	09.3	13.8	C7.0	-	06.5	07.5	07.3	74	64	95	78	SW	3	SSW	5	SW	7
23	594.1	592.8	593.0	07.4	12.0	07.2	08.4	12.0	05.9	-	07.5	06.9	05.9	98	65	77	80	SM	5	SM	7	SM	4
24	592.0	590.9	591.3	06.8	07.3	04.1	06.6	07.6	05.2	-	07.0	07.7	06.7	94	100	95	96	SW	4	SW	7	-	0
25	591.4	593.2	593.1	05.4	11.6	06.3	07.4	11.6	04.8	-	06.7	05.9	07.2	100	58	100	86	SW	5	-	0	W	1
26	593.4	593.6	594.0	06.6	07.9	05.2	06.2	10.3	05.1	-	06.7	06.8	06.6	92	85	100	92	S	5	W	5	SSM	5
27	593.2	594.0	593.8	04.5	06.0	04.2	04.7	07.9	04.2	-	05.9	07.0	06.2	93	100	100	98	SM	5	SM	3	SM	2
28	593.2	593.9	594.9	03.5	04.0	04.0	03.9	04.4	03.2	-	05.9	06.1	06.1	100	100	100	100	SW	1	NW	5	NW	4
29	595.0	595.4	594.6	06.0	09.2	06.3	07.8	09.4	03.4	-	07.0	06.9	06.0	100	79	83	87	SW	2	SSM	6	SSM	8
30	592.4	593.3	592.7	05.3	05.0	05.5	05.3	08.0	04.9	-	06.7	06.5	05.7	100	100	84	95	SSM	8	SSM	7	SSM	8
31	593.0	594.2	592.6	06.7	09.8	05.8	07.0	10.1	03.1	-	04.4	06.9	06.9	60	76	100	79	SSM	5	SSM	8	SSM	12
MES. VR ED.	593.1	593.7	593.6	04.2	06.5	04.5	04.9	07.4	03.0	-	05.6	05.8	06.0	90	80	94	88	4.8	4.4	4.4			

1	593.1	593.6	593.2	06.8	10.2	07.0	07.8	10.5	05.0	-	04.4	06.7	05.9	59	72	79	70	SSM	9	SSM	8	SSM	11
2	591.3	591.6	591.3	08.0	08.0	06.7	07.4	10.0	06.0	-	05.3	08.0	06.2	66	100	85	84	SSM	10	SSM	9	SM	8
3	590.6	590.1	590.1	07.0	10.0	05.0	06.8	10.2	05.0	-	05.8	06.7	06.5	77	73	100	83	S	3	-	0	-	0
4	590.0	591.8	592.0	01.0	00.0	-00.4	00.0	05.0	-00.4	-	04.9	04.6	04.5	100	100	100	100	N	5	N	7	N	7
5	590.0	591.0	591.1	-02.6	-02.4	-02.2	-02.4	-00.2	-02.6	-	03.7	03.8	03.8	97	98	98	98	N	9	N	8	N	10
6	589.2	592.2	593.0	-01.4	-02.4	-01.4	-02.2	-01.5	-03.4	-	03.2	03.8	04.0	97	98	98	98	N	13	N	8	N	8
7	591.4	592.0	592.2	-02.6	-01.0	-00.6	-01.0	-00.4	-02.2	-	03.9	04.3	04.4	98	100	100	99	N	8	N	7	N	6
8	592.0	592.0	592.2	00.0	01.2	00.4	00.5	01.4	-00.8	-	04.6	05.0	04.7	100	100	100	100	NW	3	SW	5	SM	6
9	591.6	591.7	591.4	00.6	02.6	02.0	01.8	03.0	00.0	-	04.2	05.5	05.3	100	100	100	100	SM	8	SM	10	SM	10
10	591.8	593.1	593.0	02.8	05.6	04.0	04.1	06.0	01.8	-	05.6	06.5	06.1	100	95	100	98	SW	7	SW	4	SM	5
11	594.7	596.6	597.4	05.2	04.2	04.4	04.0	07.8	03.0	-	06.3	07.1	07.2	95	100	100	98	SW	3	-	0	-	0
12	597.2	597.5	597.4	08.8	09.4	08.2	08.6	10.2	03.4	-	07.0	07.5	08.2	82	85	100	89	-	0	SE	2	-	0
13	596.8	596.2	595.6	07.4	12.0	08.0	08.8	12.0	06.4	-	07.7	05.9	06.8	100	56	84	80	S	5	SM	2	-	0
14	595.5	596.0	596.5	08.6	11.0	08.8	09.3	11.4	06.6	-	07.8	04.3	08.5	93	64	100	86	-	0	N	3	N	4
15	596.5	596.7	595.4	11.7	10.4	12.0	12.0	08.2	-	06.8	07.1	09.5	66	54	100	73	-	0	M	3	N	10	
16	594.8	594																					

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 $H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_x = 1,5 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Intenzitet broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes					
1	8	000	08	10	06.6	11.5	.	54	V ⁰⁻⁴ 0-12, F ⁻ N-NW 0-24, = ² 16 ⁵⁰ 17 ⁵⁰ , T ¹ 17-17 ⁵⁰ , ■		
2	0	16	10	10	10.0	00.0	00.8	52	F ⁻ N 0-24, = ² 0-24, V ⁰⁻⁴ 0-24, ■		
3	0	10	10	10	10.0	00.0	.	52	= ² 0-24, V ⁰⁻⁴ 0-24, F ⁻ N 0-15 ⁵⁰ , = ² 0-4 ⁵⁰ 15 ⁵⁰ , ■		
4	8	000	10	10	06.7	03.9	00.0	51	= ² 0-4 ⁵⁰ 7 ⁵⁰ 24, V ⁰⁻⁴ 0-24, = ² 4 ⁵⁰ 8 ⁵⁰ , = ² 0-16 ⁵⁰ 18 ⁵⁰ , ■		
5	8	16	10	06	08.7	00.9	00.3	49	V ⁰⁻⁴ 0-8 ⁵⁰ , = ² 0-8 ⁵⁰ , F ⁻ SW 0-24, ■		
6	8	040	050	10	06.3	05.1	.	42	F ⁻ P ⁻ SW 0-24, = ² 0-4 ⁵⁰ 15 ⁵⁰ , 23 ⁵⁰ 24, = ² 2 ⁵⁰ 24, ■		
7	8	10	06	04	06.7	04.4	01.1	32	F ⁻ SW 0-8 ⁵⁰ , = ² 0-8 ⁵⁰ , 18 ⁵⁰ , 19 ⁵⁰ , = ² 0-2 ⁵⁰ 14 ⁵⁰ , 15 ⁵⁰ , 16 ⁵⁰ , T ¹ 14 ⁵⁰ 12 ⁵⁰ , ■		
8	0	10	10	10	10.0	00.0	05.8	23	= ² 2 ⁵⁰ 24, F ⁻ SW 5 ⁵⁰ 19 ⁵⁰ , = ² 0-2 ⁵⁰ 14 ⁵⁰ , 13 ⁵⁰ , 14 ⁵⁰ 17 ⁵⁰ , ■		
9	8	040	040	03	03.7	11.5	09.0	20	= ² 0-3 ⁵⁰ , = ² 0-3 ⁵⁰ , 19 ⁵⁰ , = ² 0-4 ⁵⁰ 3 ⁵⁰ , F ⁻ SW 10 ⁵⁰ 19 ⁵⁰ , ■		
10	8	030	050	02	03.3	11.2	.	18	■		
11	8	050	09	05	06.3	10.0	.	15	F ⁻ SW 20 ⁵⁰ 24, ■		
12	8	10	10	10	10.0	01.1	.	12	F ⁻ SW 0-5 ⁵⁰ , 13 ⁵⁰ , 17 ⁵⁰ , 12 ⁵⁰ , 18 ⁵⁰ , 23, = ² 18 ⁵⁰ 9 ⁵⁰ , ■		
13	7	08	09	10	09.0	01.3	01.1	10	= ² 0-24, F ⁻ N 0-17, = ² 0-2 ⁵⁰ 14 ⁵⁰ , 23-24, = ² 14 ⁵⁰ 17 ⁵⁰ , = ² 10 ⁵⁰ 19 ⁵⁰ , ■		
14	0	10	10	10	06.0	00.0	15.9	06	= ² 0-17 ⁵⁰ , F ⁻ N 0-17, = ² 0-17 ⁵⁰ , = ² 17 ⁵⁰ 20, ■		
15	8	10	09	10	09.7	03.9	14.7	06	= ² 0 ⁵⁰ 24, = ² 2 ⁵⁰ 22, ■		
16	8	020	08	10	06.7	07.7	.	05	= ² 2-0-3 ⁵⁰ 9 ⁵⁰ 10 ⁵⁰ 20 ⁵⁰ 24, = ² 2-1 ⁵⁰ 14 ⁵⁰ , = ² 12 ⁵⁰ 14 ⁵⁰ , = ² 17 ⁵⁰ 17 ⁵⁰ , = ² 20 ⁵⁰ 20 ⁵⁰ , ■		
17	8	000	06	08	04.7	09.8	09.3	03	= ² 0-1, F ⁻ NW 2-10 ⁵⁰ , = ² 18 ⁵⁰ , ■		
18	8	10	09	06	08.3	06.2	.	.	= ² 0-7 ⁵⁰ , F ⁻ N-NW 6-3 ⁵⁰ , 12 ⁵⁰ , = ² 0-2 ⁵⁰ 14 ⁵⁰ , ■		
19	8	10	06	08	08.0	07.9	.	.	= ² 0-19 ⁵⁰ , = ² 1-2 ⁵⁰ , = ² 0-2 ⁵⁰ 14 ⁵⁰ , = ² 20 ⁵⁰ 24, ■		
20	8	020	16	05	05.7	07.4	.	.	= ² 0-2 ⁵⁰ , = ² 0-8 ⁵⁰ , T ⁰ 4 ⁵⁰ 10 ⁵⁰ , = ² 13 ⁵⁰ , = ² 15 ⁵⁰ , = ² 14 ⁵⁰ 16 ⁵⁰ , F ⁻ N 21 ⁵⁰ 24, ■		
21	8	10	06	03	06.3	04.9	09.0	.	F ⁻ N 0-8 ⁵⁰ , = ² 2-0-3 ⁵⁰ 6 ⁵⁰ 10 ⁵⁰ 25 ⁵⁰ 6 ⁵⁰ , T ⁰ 10 ⁵⁰ 17 ⁵⁰ , T ¹ 17 ⁵⁰ 18 ⁵⁰ [22 ⁵⁰ 24]		
22	8	040	08	04	05.3	13.4	.	.	F ⁻ SW 0-10 ⁵⁰ 24, = ² 23 ⁵⁰ 24		
23	8	03	09	09	07.7	06.2	.	.	F ⁻ SW 0-20 ⁵⁰ , = ² 0-5 ⁵⁰		
24	0	10	10	10	10.0	00.0	00.4	.	F ⁻ SW 0-4 ⁵⁰ 17 ⁵⁰ , = ² 2 ⁵⁰ 6 ⁵⁰ , = ² 6 ⁵⁰ 12 ⁵⁰ , = ² 19 ⁵⁰ 20 ⁵⁰ , = ² 10 ⁵⁰ 10 ⁵⁰ , = ² 10 ⁵⁰ 24, = ² 12 ⁵⁰ 10 ⁵⁰		
25	8	10	08	10	09.3	07.2	07.9	.	= ² 0-8 ⁵⁰ , 18 ⁵⁰ , = ² 0-2 ⁵⁰ 13 ⁵⁰ , = ² 12 ⁵⁰ , F ⁻ SW 2 ⁵⁰ 8 ⁵⁰		
26	7	06	10	10	08.7	03.2	.	.	= ² 0 ⁵⁰ 8 ⁵⁰ , = ² 1 ⁵⁰ 4 ⁵⁰ , = ² 15 ⁵⁰ 24, F ⁻ SW 6 ⁵⁰ 24, = ² 14 ⁵⁰ 18 ⁵⁰ , T ¹ 13 ⁵⁰ 15		
27	6	09	10	10	09.7	00.4	09.4	.	= ² 0-2 ⁵⁰ 8-24, = ² 0-19 ⁵⁰ , = ² 0-2 ⁵⁰ 10 ⁵⁰ 9 ⁵⁰ 24, = ² 2 ⁵⁰ 8		
28	0	10	10	10	10.0	00.0	01.3	.	= ² 0-24, = ² 0-2 ⁵⁰ 11, = ² 20 ⁵⁰ , F ⁻ SW 0-24, = ² 2 ⁵⁰ 2 ⁵⁰ , = ² 12-19		
29	8	020	06	00	02.7	13.2	09.1	.	= ² 0 ⁵⁰ H, F ⁻ SW 9-24		
30	0	10	10	05	08.3	01.0	.	.	F ⁻ SW 0-24, = ² 6-15, = ² 9-12, = ² 12-13, = ² 21-23		
31	8	050	080	02	05.0	08.5	06.0	.	F ⁻ SW 0-24, = ² 4-5, = ² 20 ⁵⁰ 21		
MES. VRED.		06.7	08.4	07.2	07.4	165.6	97.1				

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1	8	060	060	02	04.7	08.3	.	.	F ⁻ P ⁻ SW 0-24	
2	1	060	10	04	04.7	03.4	.	.	F ⁻ SW 0-24, = ² 0-17 ⁵⁰ , 18 ⁵⁰ , = ² 20-24	
3	8	09	08	10	05.0	02.1	02.4	.	= ² 0-24, F ⁻ N 3-24, = ² 2-7 ⁵⁰ 8, = ² 8-9 ⁵⁰ , = ² 19 ⁵⁰ 21 ⁵⁰ V ⁰ 20 ⁵⁰ 24, ■	
4	0	10	10	10	10.0	00.0	01.4	.	= ² 0-24, F ⁻ N 0-24, V ⁰ 0-24, = ² 10 ⁵⁰ 24, = ² 10 ⁵⁰ 24, ■	
5	8	10	10	10	10.0	00.0	04.2	01	= ² 0-24, F ⁻ N 0-24, V ⁰ 0-24, = ² 10 ⁵⁰ 17 ⁵⁰ , ■	
6	8	10	10	10	10.0	00.0	03.8	10	= ² 0-24, F ⁻ N 0-24, V ⁰ 0-24, = ² 0-24, = ² 0-3 ⁵⁰ 14 ⁵⁰ , ■	
7	8	10	10	10	10.0	00.0	00.0	10	= ² 0-24, F ⁻ N 0-24, V ⁰ 0-24, = ² 0-10 ⁵⁰ , ■	
8	0	10	10	10	10.0	00.0	.	08	= ² 0-24, F ⁻ SW-NW 0-3-9 ⁵⁰ , = ² 1-2 ⁵⁰ 8, = ² 1-2 ⁵⁰ 19 ⁵⁰ , ■	
9	0	10	10	10	10.0	00.0	02.3	04	= ² 0-24, F ⁻ SW 0-24, = ² 0-24, = ² 0-24, = ² 0-13 ⁵⁰ , F ⁻ SW 0-10 ⁵⁰ , ■	
10	7	10	10	10	10.0	01.0	03.4	.	= ² 0-10 ⁵⁰ , F ⁻ SW 0-5 ⁵⁰ , = ² 3 ⁵⁰ 12 ⁵⁰ , = ² 17 ⁵⁰ 18 ⁵⁰ , ■	
11	7	10	10	10	10.0	02.6	01.2	.	= ² 0-10 ⁵⁰ , F ⁻ SW 0-5 ⁵⁰ , = ² 3 ⁵⁰ 12 ⁵⁰ , = ² 17 ⁵⁰ 18 ⁵⁰ , ■	
12	7	03	10	10	07.7	04.4	02.4	.	= ² 0-3 ⁵⁰ 8-14, = ² 2 ⁵⁰ 24, = ² 1-3 ⁵⁰ 8, = ² 1-3 ⁵⁰ 16, = ² 1-3 ⁵⁰ 16, ■	
13	8	10	060	04	06.7	05.5	02.4	.	= ² 0-3 ⁵⁰ 8-14, = ² 2 ⁵⁰ 24, = ² 1-3 ⁵⁰ 8, = ² 1-3 ⁵⁰ 16, ■	
14	7	05	07	10	07.3	08.8	.	.	= ² 0-7 ⁵⁰ , = ² 0-8 ⁵⁰ , = ² 0-8 ⁵⁰ 14 ⁵⁰ , ■	
15	8	000	050	00	01.7	14.2	.	.	= ² 4 ⁵⁰ , F ⁻ SW 10 ⁵⁰ , ■	
16	8	06	09	10	08.3	06.4	.	.	F ⁻ SW 0-24, = ² 1-15 ⁵⁰ , = ² 17 ⁵⁰ 24, ■	
17	7	10	09	10	09.7	02.5	22.9	.	= ² 0-9 ⁵⁰ , = ² 5-8, = ² 20-24	
18	8	050	060	10	07.7	07.6	00.3	.	= ² 0-24, F ⁻ N 0-24, = ² 0-24, = ² 0-15 ⁵⁰ , ■	
19	0	10	10	10	10.0	00.0	00.0	.	= ² 0-24, F ⁻ N 0-24, = ² 0-24, = ² 0-17-24	
20	0	10	10	10	10.0	00.0	14.2	.	= ² 0-24, = ² 0-15, F ⁻ N 0-22, = ² 0-15-20	
21	0	10	10	10	10.0	06.7	07.7	.	= ² 0-24, = ² 1-15 ⁵⁰ , = ² 15 ⁵⁰ , F ⁻ N 10-20	
22	0	000	09	10	04.0	04.3	02.0	.	= ² 0-24, = ² 20 ⁵⁰ 24	
23	7	10	10	10	10.0	01.5	.	.	= ² 0-24, F ⁻ N 3-24, T ¹ 14 ⁵⁰ 14 ⁵⁰	
24	8	000	09	07	04.0	07.5	.	.	= ² 3 ⁵⁰ 0-5 ⁵⁰ , = ² 12 ⁵⁰ , = ² 17 ⁵⁰ , = ² 19 ⁵⁰ 23, ■	
25	1	10	10	10	10.0	03.1	01.2	.	= ² 6 ⁵⁰ 24, = ² 14 ⁵⁰ 13 ⁵⁰ , = ² 14 ⁵⁰ 16 ⁵⁰	
26	0	10	10	10	10.0	00.0	01.8	.	F ⁻ N-NW 0-2, = ² 12-14 ⁵⁰ , = ² 0-24, = ² 6-14	
27	8	10	07	10	09.0	03.0	03.0	.	= ² 0	

$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

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D	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21				
1	597.5	597.2	597.2	05.6	01.6	00.8	02.2	10.6	00.8	-	05.2	05.1	04.9	76	100	100	92	SM	2	N	7	N	8	
2	596.6	597.9	597.5	00.4	02.6	04.4	03.0	04.4	-00.3	-	04.7	05.5	06.3	100	100	100	100	N	6	N	1	N	6	
3	598.3	592.3	593.9	04.0	05.7	07.4	04.1	07.4	03.9	-	06.1	06.9	07.7	100	100	100	100	N	8	N	9	N	10	
4	595.6	595.8	594.2	07.4	11.2	09.0	09.2	12.3	06.5	-	07.7	07.0	05.2	100	70	61	77	N	2	W	3	SSW	8	
5	591.9	592.1	592.7	08.2	09.7	07.8	08.4	10.2	07.3	-	07.3	08.0	07.9	90	88	100	93	SSM	9	S	7	-	0	
6	591.7	593.6	594.8	05.5	06.9	07.4	06.8	07.8	05.4	-	06.8	07.5	07.7	100	100	100	100	N	4	N	3	N	5	
7	595.8	597.4	598.4	06.6	08.7	09.0	08.3	09.5	06.6	-	07.3	08.4	08.6	100	100	100	100	N	7	N	6	N	6	
8	598.3	599.1	599.3	08.3	11.2	10.8	10.3	12.5	05.7	-	06.2	06.1	07.8	75	61	80	72	N	6	N	4	NW	1	
9	598.9	599.9	599.7	10.0	13.6	12.3	12.0	14.0	09.3	-	06.7	06.6	08.0	95	56	74	75	N	5	N	2	SW	2	
10	598.7	598.4	597.7	13.4	16.5	13.8	14.4	16.8	11.8	-	07.8	09.6	11.1	67	68	94	76	-	0	S	2	SW	3	
11	597.3	597.9	597.5	13.8	12.1	11.6	12.3	13.8	11.3	-	10.0	10.6	09.2	85	100	90	92	-	0	S	2	SSW	4	
12	596.8	596.3	596.5	12.0	14.0	09.3	11.2	14.3	09.3	-	08.9	07.8	08.8	85	65	100	83	SM	6	SM	7	SM	4	
13	596.7	598.0	598.9	07.2	08.8	08.6	08.3	09.6	07.2	-	07.6	08.5	08.4	100	100	100	100	N	3	N	4	N	7	
14	599.6	600.4	600.8	07.6	10.8	10.6	09.9	11.7	07.2	-	07.8	09.7	09.6	100	100	100	100	E	5	NE	2	N	2	
15	600.1	600.8	600.5	12.9	15.0	14.2	14.1	15.6	09.8	-	08.2	11.5	07.3	73	90	60	74	-	0	N	2	W	1	
16	598.9	598.7	595.8	13.6	18.8	14.0	15.6	19.0	13.9	-	04.5	10.8	10.0	34	66	83	61	-	0	SW	3	SW	4	
17	596.8	597.6	598.0	11.6	14.6	14.0	13.6	15.0	10.4	-	09.0	09.5	10.6	88	76	88	84	N	3	NE	2	-	0	
18	598.3	599.2	598.6	15.2	19.0	16.2	16.6	19.2	12.6	-	08.2	07.5	08.4	63	46	61	57	SM	2	-	0	SW	5	
19	596.1	595.8	596.1	15.0	17.8	11.0	13.7	18.0	11.0	-	06.5	07.0	09.8	51	46	100	66	SM	8	-	0	SW	0	
20	595.3	595.3	595.2	05.4	07.4	06.8	06.6	11.0	05.0	-	06.7	07.7	07.4	100	100	100	100	N	8	N	3	N	6	
21	594.8	595.4	595.3	06.0	10.1	08.0	08.0	10.5	05.0	-	07.0	06.9	07.9	100	74	98	91	E	6	NE	2	N	2	
22	594.7	595.3	595.9	07.4	09.8	08.0	08.3	10.0	06.2	-	07.7	08.7	08.0	100	96	100	99	N	4	N	2	-	0	
23	596.0	596.4	596.8	08.0	11.2	10.4	10.0	11.4	07.0	-	08.0	07.9	08.6	100	80	91	90	-	0	NE	1	-	0	
24	596.2	596.3	596.0	11.6	12.4	11.0	11.5	13.4	09.4	-	08.4	09.3	08.4	82	86	86	85	M	2	-	0	SW	3	
25	595.3	595.6	596.5	12.0	12.2	10.2	11.2	13.6	09.8	-	06.7	09.2	08.5	63	86	91	80	SM	6	SM	5	-	0	
26	597.0	597.3	597.3	01.4	02.3	03.0	02.4	10.4	00.6	-	05.1	05.4	05.7	100	100	100	100	N	6	N	6	N	9	
27	597.3	597.8	597.8	01.6	04.2	04.0	07.0	01.0	-	05.1	05.7	06.2	100	80	100	93	N	7	N	5	N	3		
28	596.7	597.8	598.2	02.6	07.6	05.6	05.4	08.8	02.2	-	05.2	05.7	06.8	94	72	100	89	N	5	NNE	4	N	3	
29	597.7	598.5	598.2	05.6	07.4	08.2	07.4	09.5	04.4	-	06.8	07.7	08.2	100	100	100	100	N	6	N	5	N	3	
30	597.0	597.0	596.9	07.6	10.4	07.2	08.1	10.5	06.6	-	07.8	08.1	07.6	100	85	100	95	N	5	N	5	N	5	
31	596.4	597.0	596.9	06.8	08.6	07.6	07.6	09.0	06.0	-	07.4	07.4	07.8	100	89	100	96	N	10	N	8	N	10	
MES.	VRED.	595.8	596.4	596.4	08.3	10.4	09.1	09.2	11.8	06.9	-	07.1	07.8	08.0	88	83	92	88	4.4	3.9	4.0	-	-	-

1	597.4	598.0	598.0	06.6	08.0	07.0	07.2	08.2	05.6	-	07.3	08.0	07.5	100	100	100	100	N	8	N	5	N	7
2	598.4	599.2	599.0	07.0	07.6	07.2	07.2	07.8	06.8	-	07.5	07.8	07.6	100	100	100	100	N	8	N	5	M	7
3	598.2	599.0	599.1	05.4	06.4	06.2	06.0	07.3	05.4	-	06.7	07.2	07.1	100	100	100	100	N	8	N	7	N	6
4	598.0	598.1	597.2	06.0	07.2	06.2	06.4	07.6	05.0	-	07.0	07.6	07.1	100	100	100	100	N	8	N	6	N	8
5	596.2	596.8	596.5	06.0	06.8	05.0	05.7	07.0	05.0	-	07.0	07.4	06.5	100	100	100	100	N	6	N	4	N	3
6	596.0	596.9	597.7	04.4	05.4	05.4	05.2	05.8	04.2	-	06.3	06.7	06.7	100	100	100	100	N	5	N	3	N	5
7	597.7	597.5	597.3	06.2	06.6	06.0	06.2	07.2	05.4	-	07.1	07.3	07.0	100	100	100	100	N	6	N	5	N	6
8	596.6	596.8	597.0	05.0	07.0	06.4	06.2	07.2	04.8	-	06.5	07.5	07.2	100	100	100	100	N	5	NE	4	NNE	3
9	596.9	596.8	597.1	06.0	08.0	07.4	07.2	08.6	05.7	-	07.0	08.0	07.7	100	100	100	100	N	7	N	5	N	4
10	597.3	598.0	598.3	07.2	10.6	10.0	09.4	11.3	06.8	-	07.6	07.4	08.2	100	77	89	89	ENE	3	E	1	NE	2
11	599.2	599.0	598.5	10.0	12.7	11.0	11.2	13.2	08.6	-	06.9	07.7	06.8	75	70	70	72	N	1	SW	1	SW	3
12	597.0	596.7	594.5	10.0	14.0	10.2	11.1	14.6	09.8	-	04.9	06.6	07.0	53	55	75	61	SM	4	SM	5	SM	6
13	592.5	592.5	593.4	08.6	10.0	06.8	08.0	10.6	06.6	-	08.4	09.0	07.4	100	98	100	99	SM	2	SSW	4	N	4
14	595.0	596.8	597.4	05.6	07.2	07.0	06.7	07.6	05.6	-	06.8	07.6	07.5	100	100	100	100	N	5	N	4	N	6
15	597.4	598.8	598.3	10.4	12.4	11.3	11.4	13.1	03.0	-	02.2	05.9	06.7	24	55	67	49	-	0	-	0	-	0
16	597.8	597.4	597.8	11.6</td																			

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$$H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_r = 1,5 \text{ m}$$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacija broj sata	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	0	08	1C≡	10≡	09.3	C2.2	CC.C	.	.	F-Fsw 0-5, =^2-0-3^o 8-24; *3^o 7^o 10^o 4^o 13^o 11^o 12^o 13^o 8^o 11^o 12^o *17^o =8^o *
2	0	10≡	1C≡	1C≡	1C≡	00.0	13.1	.	.	=^2-0-24, =^2-0-24, F-n 0-13, 18-24; *17-20^o
3	0	10≡≡	1C≡	1C≡	1C.C	00.0	C8.C	.	.	=^2-0-24, F-pn 0-24, =^2-0-24
4	7	10≡	08	00	06.0	09.1	00.3	.	.	=^2-0-8^o F-n -35w 0-5^o 5^o 20-24;
5	7	10 R	10	1C≡	1C.C	00.6	.	.	.	F-Fsw 0-17, *06^o 7^o 12^o 12^o 15^o 16^o 16^o 20^o 24; F-n 6^o 7^o 12^o 14, =^2-16-24
6	0	10≡	10≡	1C≡	10.0	00.8	16.4	.	.	*^2-0-3, 8^o 14, 20-21^o, =^2-0-24
7	1	10≡	10≡	1C≡	1C.C	C2.4	C6.C	.	.	F-n 0-24, =^2-0-24, =^2-0-24, *13^o 13^o, =^2-21^o 24
8	0	01○	05 ○	00	02.0	14.0	00.0	.	.	=^2-0-24, F-n 5-14, =^2-5-8
9	0	01○	03 ○	CC	01.3	12.5	.	.	F-nw 0-8	
10	8	00○	07 ○	08	05.0	08.6	.	.	T 16^o 17^o, *0-17-17^o, =^2-20^o 24	
11	0	04○	10 R ≡ 01	05.C	C1.7	CO.C	.	.	*'0-2, △'0^o 6, =^2-7-14, *10-10^o 14^o 17, 13^o 13^o 17, 8^o 13^o 13^o, △'14^o 14^o 14^o F-p	
12	8	01○	09	04	04.7	08.9	05.8	.	.	F-Fsw 0-23, 13^o 15-17^o, =^2-16^o 17^o, =^2-17^o 17^o
13	0	10≡	10≡	1C≡	10.0	01.2	C1.4	.	.	=^2-0-24, =^2-0-24, 10^o 10^o 19^o 19^o, F-n 15-24
14	7	10≡	08○	10≡	09.3	C6.1	C2.C	.	.	=^2-0-11, 18-23, F-n 6-0-8
15	8	00○	05○	00	01.7	14.0	.	.	.	
16	9	00○	03○	01	01.3	14.4	.	.	F-nw 3-5	
17	8	03○	04○	00	02.3	12.3	.	.	=^2-0-8^o 6, =^2-20^o 24, =^2-3^o 6^o, F-p 5^o 10^o	
18	9	00○	02○	00	0C.7	13.5	.	.	F-p 6-0-6, F-n 17-24	
19	9	00○	02○	10≡	04.0	12.7	.	.	F-p 0-20, =^2-19^o 24, =^2-22^o 24	
20	0	10≡	10≡	1C≡	1C.C	00.0	.	.	F-p 0-10^o, 15^o 24, =^2-0-24, =^2-0-24	
21	8	10≡	05○	00≡	05.0	11.8	.	.	=^2-0-7^o F-p 0-10^o, =^2-20^o 24	
22	7	10≡	07 R	10≡	09.C	02.4	.	.	=^2-0-8^o, =^2-0-3^o 24, T 13^o 16^o	
23	8	10≡	07	02	06.3	04.8	.	.	=^2-0-10^o, =^2-9^o 9^o, =^2-15^o 16^o, =^2-19-24	
24	8	00○	09○	04	04.3	05.4	01.8	.	=^2-0-6^o, =^2-10^o, 15^o 14^o 14^o 14^o, F-p 23-24	
25	9	00○	09○	07	05.3	08.0	20.0	.	F-p 0-21^o, =^2-15^o 14^o, =^2-24^o, =^2-24^o, =^2-24^o	
26	0	10 ≡	10≡	10≡	1C.C	00.6	C3.5	.	.	=^2-0-24, =^2-0-24, 21^o 23^o, F-p 0-24, =^2-0-3^o 8^o
27	8	02○	05○	00≡	02.3	14.1	00.1	.	.	F-p 0-19^o, =^2-0-20^o, =^2-0-5^o, =^2-20^o 24
28	9	07○	01○	00	02.7	12.5	.	.	=^2-0-5^o, =^2-0-7^o, =^2-24, F-nw 0-2^o 13^o 16^o 18^o 24, =^2-22^o 24	
29	8	10≡	07	00	05.7	04.1	.	.	=^2-0-20-24, =^2-24, F-p 2^o 14^o 18^o 24, =^2-24, =^2-10^o 18-24	
30	8	10≡	06	10≡	08.7	C3.6	.	.	=^2-0-8^o F-p 0-24, =^2-0-10^o, =^2-6^o 15^o 24, =^2-16^o 17^o T 16^o 17^o	
31	8	10≡	07○	10≡	09.0	06.1	03.C	.	.	=^2-0-2-0-14, F-p 0-24, =^2-0-5^o, =^2-16^o 19-22, =^2-16^o 24

SJEĆAŠNICA

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$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	597.5	598.6	598.8	07.4	10.4	08.8	08.8	10.8	06.8	-	07.7	09.5	08.5	100	100	100	100	NE	2	NE	3	NE	2
2	598.4	598.7	598.0	09.6	11.6	10.0	10.3	12.6	06.2	-	05.0	05.2	05.0	100	90	98	96	SW	2	S	3	S	2
3	596.5	595.9	594.5	09.8	11.8	10.6	10.4	12.0	08.8	-	06.8	08.5	09.0	74	82	98	85	SW	4	S	4	SE	4
4	593.3	594.8	595.2	08.2	09.6	08.2	08.6	10.4	06.2	-	07.4	09.0	08.2	91	100	100	97	S	5	NE	2	N	3
5	595.5	596.2	595.9	09.2	13.0	08.8	10.0	13.2	07.8	-	07.4	08.8	06.8	85	78	80	81	-	0	S	3	-	0
6	595.9	598.0	599.0	07.6	11.6	09.0	09.3	12.3	07.2	-	07.3	07.6	08.6	93	74	100	89	-	0	SW	2	SW	3
7	598.0	596.0	596.8	09.0	07.8	08.0	08.2	09.4	07.7	-	07.4	07.9	08.0	86	100	100	95	SW	5	SW	9	SW	7
8	598.0	598.8	599.3	07.0	06.4	06.0	06.4	08.2	05.8	-	07.5	07.2	07.0	100	100	100	100	N	1	N	4	N	3
9	599.3	599.2	598.2	05.0	06.4	04.6	05.2	06.8	04.5	-	06.5	07.2	06.4	100	100	100	100	N	2	N	2	N	3
10	596.9	598.0	597.9	05.0	08.0	07.2	06.8	08.2	03.8	-	03.6	05.2	03.8	54	64	50	56	N	5	N	3	N	1
11	596.3	596.6	596.2	07.6	11.4	07.4	08.4	11.6	07.0	-	03.9	04.9	06.8	50	49	88	62	SW	4	SSW	3	SSW	5
12	595.2	595.2	594.4	07.4	08.4	07.2	07.6	08.6	07.0	-	07.7	08.3	07.6	100	100	100	100	SW	7	SW	3	SW	5
13	592.2	594.8	595.8	06.0	07.8	06.4	06.6	08.4	04.9	-	05.6	06.5	07.2	79	82	100	87	SW	8	SW	5	SW	5
14	596.6	597.3	595.0	07.0	10.0	07.4	08.0	10.2	05.6	-	04.2	06.7	06.5	56	73	84	71	SW	2	SSW	5	SW	7
15	595.7	598.4	601.0	08.0	11.8	12.0	11.0	12.2	07.4	-	04.5	06.2	04.8	56	60	46	54	SW	7	S	7	SSW	7
16	604.3	606.3	606.2	15.8	18.2	12.2	14.6	18.2	12.0	-	03.6	06.2	06.3	27	40	59	42	SW	6	S	2	NNW	7
17	604.9	605.1	604.3	13.4	15.1	10.8	12.5	18.3	10.7	-	05.0	07.3	09.7	43	56	100	66	N	7	N	7	N	7
18	603.3	603.1	602.8	07.4	10.3	07.2	08.1	11.1	05.8	-	07.4	08.0	06.6	96	85	86	85	N	5	N	5	NE	2
19	601.7	601.7	601.6	09.4	11.8	08.5	09.6	12.1	07.3	-	02.6	05.6	04.6	29	54	55	46	SE	2	-	0	E	3
20	600.4	600.8	600.6	10.6	09.1	07.2	08.5	10.9	07.2	-	02.6	06.0	06.5	26	70	86	61	E	4	E	2	NE	3
21	600.3	601.1	601.7	07.6	09.7	07.8	08.2	10.4	06.8	-	06.4	05.5	07.9	81	61	100	81	E	5	E	4	NE	3
22	601.5	603.0	603.3	06.2	08.5	07.4	07.4	08.6	06.2	-	07.1	07.5	07.7	100	90	100	97	NE	5	NE	4	NNE	4
23	602.9	603.0	602.6	06.0	11.2	08.8	08.7	11.5	05.6	-	07.0	05.6	07.0	100	56	82	79	E	5	S	4	-	0
24	601.1	601.1	600.0	07.8	11.4	07.6	08.8	11.6	06.8	-	05.3	05.3	04.5	67	52	57	59	S	6	S	5	S	7
25	598.5	598.4	597.7	07.4	11.0	07.3	08.2	11.4	06.6	-	04.0	04.8	04.9	52	49	63	55	SW	5	S	6	SSW	7
26	595.6	594.9	595.1	06.8	09.2	06.3	07.2	09.6	05.9	-	04.8	05.9	06.6	64	67	93	75	SSW	9	SSW	10	SW	10
27	598.9	601.3	602.4	07.1	11.6	09.2	09.3	11.7	06.2	-	07.0	06.5	06.8	93	64	78	78	SW	6	S	2	W	1
28	602.5	603.6	604.0	10.4	12.9	12.2	11.9	13.4	08.5	-	05.7	06.6	04.2	60	59	39	53	SW	6	W	4	N	2
29	603.1	603.7	603.4	14.2	13.6	13.0	13.4	15.0	12.2	-	02.9	06.0	04.2	24	51	38	38	NW	5	N	2	N	1
30	601.8	601.1	600.5	14.0	16.0	12.0	13.5	16.5	12.0	-	04.7	06.4	05.2	39	47	49	45	-	0	S	3	SW	4
MES.	VRED.	598.9	599.5	599.4	08.6	10.8	08.6	09.2	11.5	07.3	-	05.8	06.9	06.7	71	72	61	74	4.3	3.9	3.9	3.9	

1	599.9	601.4	601.0	10.4	14.4	11.0	11.7	14.6	10.0	-	06.2	07.1	07.6	65	58	77	67	SW	5	S	3		
2	600.2	600.3	601.0	10.0	11.4	06.4	08.6	13.0	06.4	-	06.0	08.2	07.2	66	82	100	83	SSW	2	NNW	1	NE	2
3	600.8	600.5	600.3	07.4	12.4	08.4	09.2	12.6	06.4	-	05.2	08.3	07.7	68	76	93	79	-	0	NNE	2	NW	2
4	599.3	598.8	598.5	05.4	07.0	05.0	05.6	08.4	05.0	-	06.7	07.5	06.5	100	100	100	100	N	4	NE	1	N	3
5	596.5	596.3	596.8	-01.4	-00.5	-02.0	-01.5	05.2	-02.0	-	04.1	04.4	03.9	99	100	98	99	N	6	N	7	N	8
6	596.0	598.6	598.8	-01.8	00.0	-00.6	-00.8	00.2	-02.1	-	03.9	04.6	04.4	98	100	100	99	N	8	N	7	N	5
7	598.1	597.1	597.1	00.2	04.4	03.9	03.1	05.3	-01.3	-	04.7	05.3	06.1	100	84	100	95	N	4	-	0	SW	5
8	595.7	595.7	595.5	-01.8	-01.2	-01.4	-01.4	04.0	-03.8	-	04.0	02.8	03.3	100	66	79	82	N	5	N	6	N	5
9	594.5	593.9	592.5	01.2	03.4	00.2	01.2	04.3	-01.4	-	03.7	03.4	04.1	74	58	89	74	W	4	SW	4	W	2
10	590.3	589.8	588.7	-01.9	02.9	-02.1	-01.1	02.9	-02.7	-	03.5	04.6	03.8	88	81	100	90	NNE	3	S	1	E	5
11	589.0	591.3	592.7	-02.6	01.4	01.1	00.2	01.4	-04.4	-	03.8	05.1	05.0	100	100	100	100	-	0	SSW	5	S	5
12	593.0	594.2	594.9	01.6	04.7	05.7	04.4	05.7	-00.8	-	05.1	06.4	06.9	100	100	100	100	S	5	S	5	S	10
13	594.4	590.6	590.8	05.2	05.8	05.0	05.2	06.0	04.9	-	06.6	04.9	06.5	100	71	100	90	S	9	S	11	SSW	7
14	587.0	587.4	591.9	-00.6	00.0	-01.8	-01.0	05.0	-02.0	-	04.4	04.6	03.9	100	100	98	99	SW	6	SW	7	SW	5
15	592.4	593.6	594.8	-01.0	-00.1	00.1	-00.2	00.6	-01.8	-	04.2	04.5	04.6	99	100	100	100	SW	6	SW	3	SW	6
16	593.4	592.9	590.3	00.6	03.0	03.2	02.5	04.0	00.0	-	04.3	05.7	05.8	89	100	100	96</td						

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$$H_s = 2067 \text{ m} \quad H_p = 2070,4 \text{ m} \quad h_t = 3,0 \text{ m} \quad h_f = 1,5 \text{ m}$$

Dan	Vlakrost 0-9	Oblačnost N (0-10)					Insekcija broj seti	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	3	00=○	06=○	03	03.0	06.0	01.2	.	.	# 0-5 ⁴⁰ , = 0-2 ^{5⁴⁰} 24i
2	6	03○	08	01	04.0	07.2	.	.	.	= 0-0 ³⁰ , = 0-3 ²⁰ 12 ¹⁵ 13, 15 ²⁵ 16 ³⁵ 18 ⁰⁻¹ 12 ²⁰ 13 ³⁰ , T ⁰⁻⁴ 15 ³⁵ K ⁰⁵ , F _{sw} 23 ⁰⁻²
3	8	01○	08	09	06.0	07.0	00.8	.	.	F _{sw} 0-16 ²⁴ , = 0-4 ²⁰ H ⁰⁵ 18 ²² 24, = 0-4 ²³ 24 ⁰⁻¹
4	8	08	08○	10=	06.7	05.9	04.2	.	.	= 0-0 ⁴⁰ , = 0-1 ⁰⁻¹ K ⁰⁵ 18 ⁰⁻¹ , = 0-0 ²⁰ , = 0-2 ⁰⁻¹ 12 ⁴⁵ , = 0-1 ¹⁶ 22 ³⁰
5	6	00○	06	04	03.3	07.3	01.6	.	.	# 2 ⁴⁰ 9, T ¹ 15 ³⁵ 16 ³⁵ 18 ²⁰⁻²⁴
6	8	04○	09○	10=	07.7	08.3	.	.	.	≤ 0-2 ³⁰ , = 0-4 ²⁰ 9, = 0-2 ¹⁸ 24 ⁰⁻¹
7	0	10	10=	10=	10.0	00.0	.	.	.	F _{sw} 0 ²⁴ , = 0-2 ²⁴ , = 0-7 ²⁰ 24i, = 0-7 ⁴⁰ 7 ⁰⁵
8	0	10=	10=	10=	10.0	00.0	01.1	.	.	F _{sw} -ev 0-4 ²⁰ 9-14 ³⁰ , = 0-24, = 0-6 ²⁵ 7 ⁰⁵ , H ⁰⁵ 15i
9	0	04○	10=	10=	08.0	05.1	03.0	.	.	= 0-2 ¹⁰ , = 0-6 ²⁰ 9 ⁰⁵
10	8	00○	02○	00	00.7	11.9	.	.	.	F _n 0 ²⁰ , = 0-4 ²⁰ 10 ²⁰
11	8	05○	04○	10	06.3	08.0	.	.	.	# 4 ⁴⁰ 8 ⁰ , = 2 ⁴⁰ 23, F _{sw} 21 ⁴⁵ 24
12	0	10=	10=	10=	10.0	00.0	.	.	.	F _{sw} 0-24, = 2 ²⁰ 24i, = 0-8-9 ⁰⁵ , = 2 ¹⁰ 24, R ¹⁹ 24 ⁰⁻¹
13	6	04○	10	10=	08.0	04.1	33.2	.	.	F _{sw} 0-23, = 0-3 ³⁰ , = 0-3 ³⁰ , = 2 ²⁰ 24, = 0-2 ²⁰ 18 ⁰⁻¹ , = 2 ²⁰ 24
14	8	02○	09	03	04.7	C9.2	.	.	.	# 0-10 ⁴⁰ , = 2 ²⁰ 24
15	8	00○	03○	02	01.7	10.1	.	.	.	= 0-6 ⁴⁵ , F _{sw} 0-24
16	9	05○	00○	00	01.7	10.3	.	.	.	F-F _n -s-sw-nww 0-9, 18-24i
17	8	00○	00○	10=	03.3	10.4	.	.	.	F-F _n 0-24, = 5-8 ³⁰ , = 0-18 ²⁰ 19 ²⁰ , = 2 ¹⁹ 24
18	8	00○	04○	00	01.3	09.4	.	.	.	= 0-0 ⁴⁰ , = 2 ²⁰ 17 ⁰⁵ , F _n 0-19, = 0-13 ³⁰ , = 17 ²⁰ 20
19	9	00○	02○	00	00.7	11.9	.	.	.	# 0 ²⁰ H ¹⁸ 24, = 18 ⁴⁵ 19 ⁴⁵
20	8	00○	02○	00	00.7	11.7	.	.	.	# 0-18, 18-20, = 20-24
21	8	00○	04○	10=	04.7	11.1	.	.	.	= 10-12, = 6-8, = 2 ¹⁸ 24
22	7	10=	08○	10=	06.3	04.6	.	.	.	= 0-24, F _{sw} 4-49 ⁰⁵ , = 0-12-15
23	7	00=○	06○	02	02.7	08.5	.	.	.	= 0-2-12, = 0-6-12, = 12-23, = 19 ³⁰ 24
24	8	02○	06○	00	02.7	10.7	.	.	.	# 0-8, 21 ²⁰ 24, = 0-6 ⁰⁵ , F _n 1-24
25	8	00○	06○	00	02.0	10.9	.	.	.	# 0-0 ²⁰ , F _{sw} 0-24
26	8	00○	04○	10=	04.7	08.7	.	.	.	F-F _n -s-w 0-24, # 0-11 ⁴⁰ , = 2 ²⁰ 24
27	8	09	08	00	05.7	04.1	.	.	.	F _w 0-8, = 0-5 ²⁰ , = 18 ²⁰ 24
28	8	03○	09○	02	04.7	C6.5	.	.	.	= 0-6 ⁴⁰ , F _{sw} 3 ²⁰ 9, = 23-24
29	9	02○	00○	00	00.7	11.0	.	.	.	# 0-44
30	9	00○	06○	00	02.0	08.3

DJEJLAŠNICA

1876 SKETCHES

MES.
WRED.

$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

BR. ST. 139

D an	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenih parova e mm			Relativna vlažnost u%				Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	595.5	596.1	597.0	02.7	04.4	05.0	04.3	05.0	02.1	-	05.3	06.3	06.5	96	100	100	95	SW	6	SW	5	SW	6
2	597.0	598.9	600.4	02.8	06.3	05.0	04.8	06.4	02.8	-	05.6	07.2	04.6	100	100	70	90	W	4	-	0	S	2
3	600.8	601.0	601.3	07.4	07.6	06.4	07.0	08.0	05.0	-	04.1	04.5	04.5	53	57	62	57	-	0	-	0	NE	4
4	600.6	601.0	600.3	04.4	04.4	03.4	03.9	06.6	03.4	-	04.3	03.6	03.5	69	57	60	62	NE	7	NE	4	E	7
5	599.2	598.6	598.3	03.4	05.6	03.2	03.8	06.8	02.5	-	03.4	03.1	03.6	58	45	62	55	SE	5	SE	3	-	0
6	597.0	596.6	596.5	01.0	03.6	-00.2	01.0	03.6	-00.2	-	02.8	04.2	03.5	56	71	78	68	-	0	-	0	N	1
7	595.1	594.7	594.5	-03.2	-03.0	-04.4	-03.8	00.6	-04.5	-	03.5	03.6	03.2	97	97	96	97	N	2	N	3	N	3
8	593.8	593.6	593.3	-04.4	-04.2	-05.0	-04.6	-03.0	-05.1	-	03.2	03.2	03.0	96	96	95	96	N	5	NNE	5	NE	3
9	591.7	592.3	593.5	00.6	00.3	-00.2	00.1	01.0	-05.0	-	04.8	04.7	04.5	100	100	100	100	SE	7	S	7	S	8
10	594.3	593.8	592.0	00.1	00.2	-00.4	-00.1	00.6	-00.4	-	04.6	04.7	04.5	100	100	100	100	SW	7	SW	7	SSW	7
11	592.2	593.5	594.8	-00.2	-03.6	-01.6	-01.8	00.4	-02.8	-	04.5	03.4	02.9	100	97	95	97	W	5	NW	3	SW	2
12	595.4	597.1	598.3	-01.0	00.6	-02.0	-01.1	00.8	-02.3	-	04.2	04.8	03.9	99	100	98	99	SSW	4	S	1	-	0
13	598.6	599.2	599.1	-03.0	00.0	01.0	-00.2	01.6	-03.2	-	03.6	04.3	03.7	97	94	76	89	-	0	W	2	SW	2
14	596.8	595.0	594.4	00.0	-01.0	-02.0	-01.2	01.2	-02.2	-	04.6	04.3	03.9	100	100	98	99	SSW	7	S	5	N	2
15	592.6	592.4	591.3	-05.0	-05.8	-07.6	-06.2	-01.8	-07.0	-	03.0	02.8	02.5	95	94	93	94	N	6	N	5	N	5
16	587.4	584.2	581.2	-03.0	-01.0	-01.6	-01.9	-00.8	-07.2	-	03.6	04.2	03.9	57	99	98	98	SW	5	SW	7	SSW	8
17	580.7	581.3	582.5	00.0	01.7	03.3	02.1	03.4	-02.4	-	04.6	05.2	05.8	100	100	100	100	SSW	7	SSW	0	SSW	1
18	581.8	581.5	583.6	02.8	00.6	-01.4	00.2	03.8	-01.6	-	05.6	04.8	04.1	100	100	99	100	S	1	SSW	1	SSW	0
19	586.6	588.8	588.9	-01.8	-01.6	-02.2	-02.0	-01.4	-02.4	-	03.9	04.0	03.8	98	98	98	98	SSW	7	SSW	4	N	2
20	587.1	585.7	584.9	-03.8	-01.7	-02.8	-02.8	-01.6	-03.8	-	03.3	04.0	03.6	96	98	96	97	W	5	SW	7	SSW	1
21	586.2	586.2	586.3	-00.3	-10.0	-11.8	-08.5	-00.2	-11.8	-	04.5	01.9	01.7	100	91	89	93	SW	2	N	8	N	8
22	584.7	583.1	583.0	-15.9	-14.3	-12.9	-14.0	-11.8	-16.2	-	01.1	01.3	01.5	86	87	88	87	N	8	N	6	NN	8
23	582.8	583.2	582.8	-14.8	-14.1	-14.2	-14.3	-12.8	-14.9	-	01.3	01.3	01.3	86	87	87	87	NW	8	N	8	N	9
24	582.4	582.4	585.0	-15.9	-16.2	-16.3	-16.2	-14.2	-16.8	-	01.1	01.1	01.1	86	85	85	85	N	0	N	0	N	2
25	586.9	589.5	591.6	-16.4	-17.0	-13.0	-14.8	-13.0	-17.2	-	01.1	00.8	00.9	85	63	55	68	N	0	N	8	N	9
26	591.4	592.5	593.6	-06.4	-03.4	-01.4	-03.2	-01.2	-13.0	-	00.5	03.5	00.7	18	97	18	44	N	2	N	7	-	0
27	593.0	591.4	590.8	-04.8	-05.2	-04.4	-04.7	-01.4	-05.6	-	01.8	02.8	03.2	56	91	96	81	SSW	7	SW	8	SW	0
28	589.8	589.4	589.8	-01.0	-00.2	-01.0	-00.8	-00.1	-04.4	-	04.2	04.5	04.2	99	100	99	99	SW	1	SSW	0	SE	6
29	589.2	589.5	590.7	-01.2	-01.2	-01.4	-01.3	-00.8	-02.6	-	04.2	04.2	04.1	99	99	99	99	SSW	6	SW	5	SW	4
30	591.2	589.8	589.5	-00.4	-01.0	-01.6	-01.2	00.0	-02.0	-	04.4	04.2	04.0	100	99	98	99	SW	5	SW	9	SW	1
MES.	VRED.	591.4	591.4	591.6	-02.6	-02.3	-02.7	-02.6	-00.5	-04.7	-	03.6	03.8	03.4	87	90	86	88	4.5	4.5	3.8		

1	590.2	590.0	591.8	-01.0	-00.4	-00.4	-00.6	-00.2	-02.2	-	04.2	04.4	04.4	99	100	100	100	SW	10	SW	13	SW	8
2	592.5	591.4	591.3	-00.6	00.2	-00.3	-00.2	00.6	-01.0	-	04.4	04.7	04.5	99	100	100	100	S	5	SSE	2	N	1
3	592.0	593.6	595.3	-02.0	-01.2	-00.1	-00.8	-00.1	-02.2	-	03.8	04.2	04.6	95	100	100	98	W	1	W	3	MSW	3
4	597.0	597.9	598.4	-00.5	00.2	-02.0	-01.1	00.6	-02.0	-	04.3	04.5	04.0	96	97	100	98	MSW	3	-	0	N	3
5	597.4	596.7	596.4	-04.1	-04.6	-05.8	-05.1	-02.0	-05.8	-	03.4	03.3	01.6	100	100	55	85	N	1	N	2	N	4
6	595.5	593.4	592.0	-02.6	-02.0	-01.1	-01.7	-00.9	-04.2	-	02.6	03.6	02.1	68	91	49	69	NW	3	SW	6	NN	1
7	590.4	588.0	590.4	-09.6	-11.8	-12.4	-11.6	-01.1	-12.4	-	02.2	01.8	01.7	98	97	97	97	N	7	N	7	N	7
8	590.5	590.6	591.7	-05.6	-04.6	-06.6	-05.8	-04.1	-12.5	-	00.8	02.1	02.7	27	65	96	63	N	5	N	5	N	4
9	592.7	594.1	595.4	-08.6	-06.0	-03.4	-05.4	-03.4	-08.6	-	02.4	02.8	02.1	99	94	58	84	N	6	SW	3	N	2
10	595.4	595.7	595.7	-04.0	-04.0	-04.2	-04.1	-01.8	-04.2	-	02.7	03.3	03.2	78	96	96	90	SW	4	W	3	NN	3
11	595.4	595.4	595.3	-06.4	-06.0	-03.4	-04.8	-03.4	-07.4	-	02.7	02.5	03.9	94	86	97	92	N	1	NE	3	NE	3
12	592.8	591.8	590.0	-03.0	-02.0	-03.0	-02.8	-01.8	-04.2	-	02.5	03.0	03.6	68	75	97	80	S	6	SSW	5	SSW	5
13	586.5	589.4	591.5	-03.4	-02.4	-04.0	-03.4	-02.0	-04.1	-	03.5	03.8	03.0	97	98	99	95	SSW	5	-	0	-	0
14	592.6	593.7	594.7	-05.2	-05.0	-06.0	-05.6	-03.8	-06.0	-	03.0	03.0	02.8	95	95	94	95	N	2	E	2	NE	2
15	595.3	596.0	597.0	-04.8	-02.6	-02.7	-03.2	-01.8	-04.6	-	02.7	01.8	02.7	84	49	72	68	W	2	N	5	-	0
16	595.2	592.6	589.4	-02.2	-02.6	-00.1	-01.2	-00.1	-03.8	-	03.6	03.7	04.5	93	97	100	97	SSW	7	SSW	9	S	11
17	587.6	583.7	581																				

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$$H_s = 2067 \text{ m } H_d = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_x = 1,5 \text{ m}$$

Dan	Vjetrost 0-9	Oblačnost N (0-10)					Insoleća srednja vrijednost R mm	Padavina R mm	Snožni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	08	020	04	04.7	07.7	.	07	F _{new} 3-4, F _{new} 24, □	
2	9	01	000	00	00.3	09.0	.	04	F _{new} 0-6, F _{new} 5-14, □	
3	9	09	010	00	03.3	08.6	.	02	F _{new} 5-9, F _{new} 20-22, □	
4	8	03	050	00	02.7	09.1	.	02	F _{new} 0-24, F _{new} 24, □	
5	8	03	060	00	03.0	08.6	.	01	F _{new} 0-10, F _{new} 0-24, □	
6	8	02	050	00	02.3	09.7	.	01	F _{new} 0-4, F _{new} 20-24, □	
7	0	04	10=	10=	08.0	02.5	.	01	F _{new} 0-5, F _{new} 5-13, □	
8	0	10	10=	10=	10.0	00.0	.	01	F _{new} 0-24, F _{new} 24, □	
9	0	10	10*	10*	10.0	00.0	00.4	02	F _{new} 0-24, F _{new} 24, F _{new} 24, □	
10	0	10	10*	10*	10.0	00.0	04.0	03	F _{new} 0-24, F _{new} 24, F _{new} 24, □	
11	0	10	10=	10=	00	06.7	00.0	08.0	F _{new} 0-12, F _{new} 23, F _{new} 24, □	
12	0	10	10=	10=	00	06.7	00.0	10	F _{new} 0-24, F _{new} 0-18, F _{new} 3-5, □	
13	0	00	030	03	02.0	08.9	02.6	13	F _{new} 0-24, F _{new} 24, □	
14	0	10	10=	10=	10.0	00.0	.	11	F _{new} 0-24, F _{new} b-24, F _{new} 24, F _{new} 24, □	
15	0	10	10=	10=	10.0	00.0	02.4	14	F _{new} 0-24, F _{new} 0-23, F _{new} 24, □	
16	0	10	10*	10*	10.0	00.0	01.6	17	F _{new} 0-24, F _{new} 24, F _{new} 24, □	
17	0	10	10=	10=	10.0	00.0	02.4	20	F _{new} 0-12, F _{new} 0-24, F _{new} 24, □	
18	1	10	10=	10=	10.0	00.0	23.6	10	F _{new} 0-24, F _{new} b-24, F _{new} 24, F _{new} 24, □	
19	0	10	10=	10=	10.0	00.0	19.0	09	F _{new} 0-24, F _{new} 0-24, F _{new} 0-24, □	
20	0	03	10=	10=	07.7	00.0	20.0	11	F _{new} 0-6, F _{new} 24, F _{new} 24, F _{new} 24, □	
21	0	10*	10=	10=	10.0	00.0	00.4	10	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
22	0	06	02	10=	06.0	00.0	00.3	13	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
23	0	10	10=	10=	10.0	00.0	00.3	13	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
24	0	10	10*	10*	10.0	00.0	00.3	10	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
25	0	04	020	00	02.0	08.6	01.1	26	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
26	0	04	00	00	01.3	07.7	.	25	F _{new} 0-4, F _{new} 0-16, F _{new} 24, □	
27	0	00	020	10=	04.0	07.1	.	22	F _{new} 0-4, F _{new} 0-24, F _{new} 24, □	
28	0	10	10=	10=	10.0	00.0	01.1	24	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
29	0	10	10=	10=	10.0	00.0	02.0	26	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
30	0	10	10=	10=	10.0	00.0	.	26	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □	
MES. VRSTO.		07.2	07.3	06.6	07.0	87.5	89.5			

BJELAŠNICA

1975 DECEMBER

1	0	10=	10=	10*=	10.0	00.0	.	25	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □
2	0	04	06	00	03.3	04.9	00.9	26	F _{new} 0-17, F _{new} 0-5, F _{new} 24, □
3	0	00	08	00	02.7	09.0	.	25	F _{new} 0-12, F _{new} 23, □
4	0	05	10	10=	08.3	04.7	.	23	F _{new} 0-5, F _{new} 17, F _{new} 24, □
5	0	09	000	00	03.0	05.6	.	22	F _{new} 0-4, F _{new} 0-17, F _{new} 24, □
6	0	01	000	00	00.3	08.7	.	21	F _{new} 0-24, F _{new} 24, □
7	0	10*	10=	00	06.7	00.0	01.0	23	F _{new} 0-24, F _{new} 24, F _{new} 24, □
8	0	00	000	10=	03.3	08.5	00.0	23	F _{new} 0-45, F _{new} 18, F _{new} 24, □
9	0	10=	000	00	03.3	08.5	.	23	F _{new} 0-8, F _{new} 13, F _{new} 24, □
10	0	00	040	10=	04.7	06.5	.	21	F _{new} 0-8, F _{new} 24, □
11	0	10=	020	03	05.0	05.1	.	20	V _{new} 0-24, V _{new} 0-23, V _{new} 24, □
12	0	04	020	10=	04.0	06.4	.	17	V _{new} 0-4, V _{new} 0-24, V _{new} 24, □
13	0	10*	10=	00	06.7	00.0	03.2	20	V _{new} 0-24, F _{new} 0-24, F _{new} 24, □
14	0	10=	010	00	03.7	05.6	02.4	24	V _{new} 0-24, F _{new} 0-24, F _{new} 24, □
15	0	04	010	04	03.0	06.3	.	23	V _{new} 0-24, F _{new} 0-24, □
16	0	00	10=	10=	09.3	00.0	.	22	V _{new} 0-24, F _{new} 3-24, F _{new} 24, □
17	0	10	10=	10=	10.0	00.0	05.9	20	V _{new} 0-4, F _{new} 0-24, F _{new} 24, □
18	0	04	00	10=	07.3	03.8	26.4	19	V _{new} 0-24, F _{new} 3-24, F _{new} 24, □
19	0	10=	09=	01	06.7	00.6	.	19	V _{new} 0-24, F _{new} 3-24, F _{new} 24, □
20	0	10=	10=	10=	10.0	00.0	06.0	19	V _{new} 0-24, F _{new} 3-24, F _{new} 24, □
21	0	00	020	10=	04.0	06.2	.	19	V _{new} 0-24, F _{new} 24, □
22	0	10=	010	00	03.7	07.5	.	19	V _{new} 0-3, F _{new} 22, □
23	0	09	010	00	03.3	07.4	.	16	V _{new} 0-3, F _{new} 22, □
24	0	00	000	00	00.0	09.1	.	16	V _{new} 0-24, F _{new} 24, □
25	0	10=	10*	10=	10.0	00.0	.	15	F _{new} 0-24, F _{new} 12, F _{new} 24, □
26	0	02	10=	10=	07.3	00.0	01.5	16	F _{new} 0-2, F _{new} 24, F _{new} 0-24, □
27	0	10=	10*	10=	10.0	00.0	00.6	16	V _{new} 0-24, F _{new} 0-24, F _{new} 24, □
28	0	10=	00	00	05.3	06.9	00.0	16	F _{new} 0-24, F _{new} 0-24, F _{new} 24, □
29	0	00	000	00	00.0	09.2	.	16	V _{new} 0-2, F _{new} 0-2, F _{new} 24, □
30	0	00	010	03	01.3	08.8	.	15	#0-24, □
31	0	00	000	01	03.0	06.1	.	14	#0-24, □
MES. VRSTO.		05.8	05.2	04.6	05.2	141.4	41.3		

$\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$

BR. ST. 141

dan	Vazdušni pritisak P mm				Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina vjetra D, f (0-12)				
	7	14	.21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	7	14	21	
1	714.1	710.4	712.8	-09.1	-02.4	-02.6	-04.2	-01.6	-05.4	-	01.8	02.4	02.7	76	62	71	70	E	2	H	2	-	0	
2	713.4	710.4	715.2	-03.4	01.1	00.7	-00.2	01.4	-04.4	-	03.3	04.1	04.4	93	82	92	89	-	0	-	0	N	2	
3	715.6	715.0	716.3	-00.8	02.0	-00.6	-00.2	02.5	-00.9	-	03.6	03.5	02.8	84	66	66	72	-	0	ENE	3	NW	2	
4	715.5	713.6	714.7	-07.3	00.4	-05.0	-04.2	01.2	-07.6	-	04.2	03.1	02.7	61	66	67	78	ESE	3	-	0	ESE	1	
5	717.0	714.3	714.7	-08.5	00.0	-02.0	-03.1	01.5	-08.6	-	01.2	03.2	03.2	92	71	80	81	-	0	-	0	-	0	
6	713.0	710.6	709.9	-04.4	04.2	00.2	00.0	05.0	-04.5	-	03.0	03.9	04.0	92	62	86	80	-	0	-	0	ESE	3	
7	707.2	704.1	705.1	-02.3	08.6	05.0	04.1	09.4	-04.5	-	03.0	04.7	04.9	78	56	75	70	SE	2	NW	2	-	0	
8	698.3	697.3	703.6	02.8	02.7	-01.0	00.9	05.4	-01.2	-	04.9	05.0	04.0	88	85	93	90	-	0	WSW	2	NW	1	
9	708.0	712.2	715.2	-01.0	-01.6	-06.4	-03.8	-00.5	-06.4	-	04.0	03.5	02.3	93	87	81	87	N	3	H	4	-	0	
10	716.3	715.4	715.8	-11.8	-02.8	-07.0	-07.2	-01.6	-13.2	-	01.5	02.4	02.4	83	64	89	79	ESE	2	-	0	-	0	
11	715.8	712.7	713.0	-10.4	00.6	-02.4	-03.6	01.0	-12.5	-	01.9	03.1	03.3	90	65	86	80	-	0	-	0	SE	2	
12	719.2	713.1	714.2	-03.0	05.7	01.4	01.4	06.6	-03.6	-	03.1	05.3	03.9	86	77	80	82	SE	2	-	0	E	2	
13	715.6	714.2	716.1	-01.6	05.5	-01.1	00.4	05.5	-02.5	-	03.7	03.5	04.1	91	51	96	79	-	0	-	0	ESE	3	
14	716.2	716.0	717.0	-04.4	03.6	00.2	-00.1	04.4	-05.0	-	03.0	04.9	03.5	92	82	74	83	SE	1	-	0	ESE	4	
15	716.7	715.4	715.8	-02.3	07.2	01.4	01.9	07.8	-04.4	-	02.8	05.0	03.9	72	65	77	71	ESE	4	-	0	E	4	
16	714.7	712.9	712.5	-03.2	05.8	02.4	01.8	07.0	-03.5	-	03.1	04.2	03.8	85	61	69	72	SE	3	-	0	ESE	3	
17	712.0	710.5	709.7	-01.0	09.4	02.3	03.2	09.4	-01.2	-	03.0	04.3	03.7	71	49	68	63	ESE	5	-	0	ESE	2	
18	709.0	706.8	707.2	-00.6	09.4	02.2	03.3	10.2	-01.1	-	03.0	04.7	03.4	68	53	63	61	ESE	4	-	0	ESE	3	
19	707.3	706.2	711.1	-01.8	10.2	00.6	02.4	10.4	-02.6	-	02.3	04.9	03.8	56	52	80	63	ESE	4	-	0	ESE	2	
20	714.4	713.7	713.6	-04.4	05.6	-00.3	00.2	06.5	-04.5	-	03.0	03.8	03.9	92	55	86	78	ESE	2	-	0	ESE	2	
21	712.0	711.6	712.0	-04.6	03.8	-01.4	-00.9	05.1	-05.7	-	03.0	03.5	03.7	94	59	89	81	SE	2	-	0	-	0	
22	713.0	712.2	711.7	-04.0	01.0	00.5	-00.5	01.2	-05.0	-	03.1	04.1	04.0	92	83	85	87	-	0	-	0	-	0	
23	709.9	708.9	708.4	-04.4	00.2	00.6	-00.8	01.4	-04.4	-	03.0	03.9	04.3	90	83	90	88	SE	2	-	0	-	0	
24	708.0	707.0	707.5	00.0	05.4	03.6	03.2	04.5	-00.2	-	04.2	05.2	05.4	91	77	91	86	SE	2	-	0	-	0	
25	708.5	708.8	709.3	03.0	10.0	02.7	04.6	10.6	-02.3	-	05.3	04.9	04.6	94	54	83	77	ESE	2	H	2	-	0	
26	708.8	709.8	711.6	04.2	06.4	03.6	04.4	08.1	01.0	-	04.8	06.4	05.7	77	88	96	87	-	0	-	0	ESE	2	
27	712.8	708.5	703.9	01.2	08.2	01.4	03.0	08.6	-00.2	-	04.5	05.0	04.8	90	62	95	82	-	0	SE	2	ESE	4	
28	697.1	695.4	698.8	05.7	07.0	00.8	03.6	07.2	-00.8	-	05.1	05.4	04.5	74	71	93	79	SSE	2	ESE	3	-	0	
29	698.8	700.2	703.7	-00.4	02.4	01.1	01.0	03.2	-01.0	-	04.3	05.1	04.8	96	94	97	96	E	2	NNW	1	-	0	
30	706.2	706.0	709.8	-01.2	01.2	00.0	00.0	02.0	-01.4	-	04.0	04.3	04.4	96	85	97	93	-	0	SW	2	-	0	
31	714.1	712.5	712.6	-01.6	05.0	-01.6	00.0	05.0	-02.4	-	03.5	04.2	03.4	85	65	83	78	NNW	1	H	2	-	ESE	2
MES.	VRED.	711.0	709.9	711.0	-02.6	04.0	00.0	00.3	04.8	-03.6	-	03.3	04.2	03.9	85	69	84	79	1.6	0.8	1.4			

1	710.9	711.6	713.8	-04.9	02.4	01.4	00.1	03.0	-05.2	-05.7	02.7	03.5	03.9	85	63	77	75	-	0	NNW	1	-	0
2	715.2	715.0	711.5	00.4	01.6	00.4	01.0	01.6	-00.2	-01.8	03.6	04.2	04.3	76	81	88	82	-	0	-	0	-	0
3	708.6	710.7	715.0	00.2	01.4	-00.6	00.0	01.6	-01.2	-02.0	04.5	04.0	03.1	97	79	72	83	-	0	-	0	ENE	2
4	715.7	715.9	717.1	-01.2	02.0	00.3	00.4	02.6	-01.8	-01.8	03.2	03.8	04.0	76	72	86	78	ESE	3	SE	2	-	0
5	718.1	716.1	716.4	-02.0	03.3	-02.2	-00.8	03.4	-02.2	-03.6	03.3	03.5	03.5	83	60	90	78	E	3	H	2	-	0
6	718.5	718.3	715.0	-05.4	02.2	-01.7	-01.6	03.0	-05.9	-05.0	02.8	03.7	03.4	91	69	85	82	-	0	SH	1	ESE	2
7	711.1	707.0	706.8	-05.3	05.8	01.2	00.7	06.6	-05.6	-06.4	02.9	04.0	04.0	95	58	80	78	-	0	-	0	-	0
8	709.8	710.3	711.8	-00.8	-00.4	-04.3	-02.4	01.4	-04.6	-04.4	03.2	03.1	01.9	73	69	56	66	N	2	H	4	ENE	2
9	712.2	711.1	711.5	-09.5	00.1	00.1	-05.0	01.2	-09.5	-09.5	01.7	01.8	02.2	78	40	68	62	ESE	3	H	2	ESE	2
10	710.8	711.1	709.2	-08.6	05.0	-00.5	-01.2	07.0	-08.6	-09.6	01.9	03.5	02.7	77	53	61	64	ESE	2	SH	1	-	0
11	709.4	708.7	709.2	-04.4	08.2	02.2	02.0	08.5	-05.4	-06.4	02.6	04.5	03.9	78	55	72	68	ESE	2	WSW	5	-	0
12	708.0	706.2	704.3	04.2	08.2	03.3	05.8	09.8	00.9	01.6	04.4	05.0	03.9	72	62	59	64	WSW	2	S	4	S	2
13	700.9	698.3	698.2	-00.1	12.8	03.2	03.8	12.8	-00.4	-02.6	03.5	04.5	06.3	76	40	94	70	ESE	2	WSM	2	-	0
14	697.3	699.0	699.2	03.0	04.8	04.3	04.1	05.4	02.8	01.4	05.4	06.3	06.1	95	97	97	96	-	0	-	0	-	0
15	704.0	704.5	706.3	00.8	07.1	03.2	03.6	08.7	00.8	00.2	04.5	04.2</td											

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 $H_s = 630 \text{ m } H_d = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijeme 0 9	Oblačnost N (0-10)					Insekticij broj seti	Padavina R mm	Snežni pokrival h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7 00	10	10	06.7	04.7	00.1	04	= 0-17 ³⁰ 24; * 0-22 ³⁰ 24; □		
2	6 10*	10	10	10.0	00.0	04.1	09	= 0-10-23 ¹⁰ ; * 0-14 ¹⁰ ; 15 ⁴⁰ 20 ¹⁰ ; □		
3	7 10	09	08	09.0	01.4	01.1	13			
4	7 00	00.0	00	00.0	07.1	*	08	= 0-17 ³⁰ 24; □		
5	6 06	05.0	00	03.7	02.0	*	07	= 0-20-24; □		
6	4 00	00.0	00	00.0	C9.7	*	07	= 0-12-0-24; □		
7	6 01	01.0	10	04.0	07.4	*	07	= 0-7 ³⁰ 24; □		
8	5 10	10*	10	10.0	00.0	*	06	= 0-7 ³⁰ 24; □		
9	6 10*	10*	00	06.7	00.1	05.3	06	= 0-14 ¹⁰ ; * 2 ²⁰ 16; □		
10	7 00	00.0	00	00.0	C7.1	02.0	10	= 15 ¹⁰ 24; V 22-24; □		
11	5 00	00.0	00	00.0	02.6	*	08	= 0-10; V 0-10 ³⁰ ; □		
12	6 07	10	00	05.7	04.1	*	08	= 0-8; 10 ³⁰ 24; □		
13	5 10	06.0	00	05.3	03.8	*	04	= 0-12-0-24; □		
14	6 00	00.0	00	00.0	05.3	*	04	= 0-24; V 0-10 ³⁰ ; □		
15	5 00	00.0	00	00.0	07.0	*	04	= 0-20-24; □		
16	5 00	09	05	04.7	05.6	*	04	= 0-10-24; □		
17	7 05	05.0	06	05.3	05.7	*	04	V 20 ³⁰ 24; □		
18	8 04	01.0	00	01.7	06.2	*	03	= 15 ¹⁰ 19 ³⁰ ; □		
19	6 00	00.0	00	00.0	07.9	*	01	= 0-24; □		
20	6 00	00.0	00	00.0	07.2	*	01	= 0-16 ¹⁰ 24-24; V 23 ³⁰ 24		
21	4 00	00.0	00	00.0	06.7	*	*	= 0-9 ¹⁰ 13 ³⁰ 24; V 0-10 ³⁰ ; = 9 ¹⁰ 13 ³⁰		
22	6 09	08	10	09.0	00.0	*	*	= 0-24		
23	5 00	10	08	04.0	02.4	*	*	= 0-20-24; V 0-9		
24	7 00	10	10*	06.7	00.8	*	*	= 0-6 ¹⁰ 02 ¹⁰ 13 ³⁰ 24; = 15 ¹⁰ 24		
25	6 10	00.0	00	03.3	04.1	00.0	*	= 7 ³⁰ 18 ³⁰ ; = 9 ¹⁰ 24		
26	6 10	10	10	10.0	00.2	*	*	= 0-1-0-7 ³⁰ 8 ³⁰ 12 ³⁰ 23 ³⁰ ; = 13 ¹⁰ 23 ³⁰		
27	8 05	00.0	06	03.7	08.6	01.1	*	= 0-19 ³⁰ 23 ³⁰		
28	7 10	10	10*	10.0	00.0	00.1	*	= 0-15 ¹⁰ 12 ³⁰ 15 ¹⁰ 18 ³⁰ ; * 0-18 ³⁰ 23 ³⁰ ; = 10 ¹⁰ 24		
29	7 04	10	00	04.7	00.1	01.1	*	= 0-16 ¹⁰ 12 ³⁰ 13 ³⁰ 24; = 15 ¹⁰ 24		
30	2 10*	10*	10	10.0	00.4	01.0	*	= 0-6 ¹⁰ 02 ¹⁰ 22 ³⁰ 24; = 16 ¹⁰ 24; = 2 ²⁰ 21 ³⁰ 22 ³⁰ ; * 0-6 ¹⁰ 12 ³⁰ 17 ³⁰		
31	6 04	04.0	00	02.7	04.4	01.4	02	= 0-5 ¹⁰ 7 ³⁰ 20 ³⁰ ; = 20 ³⁰ 24; □		
MES. VRED.	04.4	09.1	04.0	04.5	120.6	25.1				

1	6 00	08	10	06.0	04.7	*	*	= 0-10 ³⁰ ; = 15 ¹⁰ 24		
2	6 10	10	10	10.0	00.0	*	*	= 0-24; * 14 ¹⁰ 16 ¹⁰ 22 ³⁰ 24; □		
3	6 10*	09	10	09.7	00.0	00.4	02	= 0-24; * 0-11; □		
4	6 10	10	10	10.0	00.1	00.0	*	= 0-24		
5	6 07	01.0	00	02.7	04.7	*	*	= 0-15 ¹⁰ 20 ³⁰ 24		
6	6 10	00.0	00	03.3	07.0	*	*	= 0-24; = 0-10 ³⁰ 18 ³⁰ 24		
7	3 00	00.0	00	00.0	05.7	*	*	= 0-7 ³⁰ 15 ¹⁰ 24; = 0-10 ³⁰ 23 ³⁰ 24; V 0-3 ³⁰ 10 ³⁰ ; = 7 ³⁰ 15 ¹⁰		
8	7 08	05.0	04	05.7	01.6	*	*	= 0-6 ¹⁰ 14 ¹⁰ 17 ³⁰		
9	7 01	00=	00	00.3	08.9	00.0	*	= 0-4 ¹⁰ 9 ¹⁰ 17 ³⁰		
10	6 00	00.0	00	00.0	08.5	*	*	= 19 ³⁰ 14 ³⁰ ; = 29 ³⁰ 24		
11	7 00	06.0	10	05.3	06.7	*	*	= 0-9 ⁴⁰ ; = 9 ⁴⁰ 14 ³⁰ ; P 13 ³⁰ 14 ³⁰		
12	8 10	09	01	04.7	04.0	*	*	= 4 ²⁰ 8 ³⁰ ; = 8 ³⁰ 13 ³⁰ ; = 16 ³⁰ 20 ³⁰		
13	7 03	05.0	10	06.0	06.5	*	*	= 5 ²⁰ 24; = 8 ³⁰ 14 ³⁰ ; = 17 ³⁰ 24		
14	5 10	10	10*	10.0	00.0	01.4	*	= 0-5 ¹⁰ ; = 14 ¹⁰ 17 ³⁰ ; = 0-14 ¹⁰ 4 ³⁰		
15	7 10	07.0	07	08.0	05.8	07.2	*	* 0-5 ¹⁰ ; = 14 ¹⁰ 17 ³⁰ ; = 0-14 ¹⁰ 4 ³⁰		
16	6 10	10	10*	10.0	00.0	00.0	*	= 0-9 ¹⁰ 19 ³⁰ ; * 0-15 ¹⁰ 22 ³⁰		
17	8 08	01.0	10	06.3	08.7	00.0	*	= 12 ³⁰		
18	7 10	00.0	00	03.3	04.5	*	*	= 20 ³⁰ 24		
19	5 00	01.0	07	02.7	04.2	*	*	= 0-10 ³⁰ ; = 2-5 ³⁰ 9 ³⁰ 14 ³⁰ 18 ³⁰ ; = 19 ³⁰ 44 ³⁰		
20	6 08	10*	10*	09.3	00.0	*	*	= 6 ³⁰ 9 ³⁰ 12 ³⁰ 24; * 0-12 ³⁰ 24		
21	7 10*	09*	10*	09.7	00.0	00.1	01	* 0-24; = 0-10 ³⁰ ; □		
22	8 01	00.0	00	00.3	04.3	00.0	*	* 0-4 ³⁰ ; = 22 ³⁰ 24; P 13 ³⁰ 14 ³⁰ 10 ³⁰ 16 ³⁰		
23	5 06	01.0	00	02.3	08.3	*	*	= 0-9 ³⁰ 22 ³⁰ 24; = 2-6 ³⁰ 12 ³⁰		
24	7 03	07	04	04.7	04.7	*	*	= 15 ³⁰ 8 ³⁰ ; = 17 ³⁰ 12 ³⁰		
25	6 08	07	07	07.3	02.2	*	*	= 15 ³⁰ 8 ³⁰ ; = 17 ³⁰ 12 ³⁰		
26	6 10*	07*	10*	08.0	01.2	00.0	*	* 4 ³⁰ 23 ³⁰ ; = 7 ³⁰ 24; □		
27	7 01	01.0	00	00.7	C9.8	03.0	03	= 7 ³⁰ 44 ³⁰ ; □		
28	6 00	00.0	00	00.0	09.4	*	*	= 0-8 ³⁰ ; = 9 ³⁰ 14 ³⁰		
MES. VRED.	05.8	04.8	05.4	05.3	134.5	12.9				

1975 MART

SARAJEVC

 $\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$

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D S	Vozdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	709.9	709.2	709.6	-04.2	11.7	02.2	03.0	12.4	-05.3	-16.0	02.2	02.5	03.6	67	28	66	54	ESE 3	WSW 1	ESE 2	
2	709.5	709.2	709.4	-00.8	15.0	05.5	06.3	15.0	-01.8	-01.8	03.0	05.4	04.0	69	42	55	57	ESE 1	W 4	- 0	
3	708.3	706.1	707.0	00.3	15.3	07.2	07.5	16.0	-01.0	-03.4	03.6	03.5	05.0	76	27	65	56	ESE 3	NNW 2	ESE 2	
4	706.4	704.2	703.7	05.0	12.0	08.6	08.6	13.3	04.2	01.8	04.7	06.2	04.5	73	59	53	62	WSW 1	SW 3	S 4	
5	704.0	705.0	707.6	06.5	09.2	08.4	08.1	12.0	06.1	01.6	04.6	06.3	05.9	63	72	71	69	NNW 2	SW 2	SSW 2	
6	709.2	709.0	707.7	02.0	14.6	07.8	08.0	14.8	01.3	01.8	04.6	04.8	05.1	87	39	65	64	SSE 1	W 2	ESE 1	
7	707.3	707.1	708.2	10.7	16.7	13.0	13.4	17.6	04.3	00.1	04.4	04.0	04.3	46	28	36	37	N 2	S 4	SSE 3	
8	708.2	705.9	704.0	12.4	17.8	07.8	11.4	18.3	07.4	06.6	03.8	04.5	04.0	35	29	51	38	SW 2	W 2	ESE 3	
9	700.4	696.6	697.2	02.6	16.7	11.0	10.3	18.0	02.0	00.9	04.0	03.6	05.5	72	26	56	52	- 0	SW 2	SSE 2	
10	695.2	694.8	697.9	07.0	13.8	09.2	09.8	14.7	06.0	05.0	05.3	05.4	05.4	70	45	61	59	ESE 3	SE 3	ENE 1	
11	703.1	706.3	708.2	07.6	11.4	08.0	08.8	13.4	06.7	04.9	05.3	05.4	05.1	68	54	64	62	NW 1	S 2	S 1	
12	706.4	702.7	704.3	05.4	12.6	06.8	07.9	14.5	03.2	01.6	03.9	05.9	05.1	57	54	69	60	ESE 5	W 2	NW 3	
13	703.3	702.7	702.6	09.0	14.0	09.6	10.2	14.4	05.3	04.2	03.6	03.6	05.4	41	30	63	45	S 3	S 3	E 3	
14	699.6	701.5	702.5	04.2	11.2	08.0	07.8	11.4	02.6	03.8	05.8	06.6	05.0	94	66	62	74	WSW 1	ESE 4	S 2	
15	704.5	704.8	706.0	04.9	11.8	07.4	07.9	12.1	04.2	03.0	05.1	04.3	04.9	75	41	62	61	E 4	SE 2	ENE 2	
16	705.2	702.8	702.6	03.6	11.0	06.4	06.8	12.0	02.4	01.6	05.0	04.7	05.4	84	47	75	69	ESE 3	SSW 2	- 0	
17	701.2	699.8	700.3	01.0	09.6	05.4	05.4	11.0	00.6	-00.6	04.3	04.5	04.6	87	50	68	68	ESE 2	W 2	NW 2	
18	699.8	701.2	702.6	01.0	10.4	07.1	06.4	11.2	00.4	-00.8	04.3	04.2	04.6	87	45	60	64	ESE 3	S 2	ESE 3	
19	701.9	701.0	701.6	08.2	17.1	10.4	11.5	17.4	05.6	-01.0	C5.0	04.5	05.0	61	31	53	48	ESE 2	S 3	ENE 2	
20	700.0	701.8	701.9	09.2	11.0	09.6	09.8	14.2	08.0	07.0	05.5	06.7	07.1	64	68	79	70	ESE 2	- 0	ESE 2	
21	701.1	702.1	706.0	06.4	02.5	06.0	02.2	10.0	-00.2	06.1	06.6	05.0	04.3	92	91	93	92	ESE 3	W 1	- 0	
22	707.4	705.4	701.8	-03.0	00.2	-01.4	-01.4	02.0	-03.4	-03.6	02.7	02.5	03.1	73	55	74	67	NW 2	W 2	ESE 1	
23	699.1	696.7	697.7	-02.3	05.1	02.2	01.8	05.4	-02.8	-03.0	02.7	03.6	03.6	71	55	67	64	E 3	ESE 4	ESE 3	
24	697.0	695.2	696.9	-00.4	01.0	00.1	00.2	02.3	-00.6	00.0	03.8	04.6	04.1	86	93	90	- 0	W 3	W 3	W 2	
25	697.6	698.2	701.6	-01.0	05.6	00.2	01.2	06.4	-01.8	-00.5	03.8	03.5	04.0	89	51	86	75	NNW 2	- 0	NE 1	
MES.	VRED.	702.7	702.1	702.8	04.8	11.4	07.3	07.7	12.8	02.9	01.6	04.4	04.8	04.8	69	50	63	61	2.4	2.6	2.1

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1	701.2	702.9	704.6	07.6	06.8	05.2	06.2	13.0	04.9	06.0	07.0	06.9	06.3	90	93	94	92	N 1	NNW 2	NW 1
2	702.5	699.9	701.0	03.2	07.4	07.2	06.2	09.4	02.7	03.4	05.6	06.9	06.3	97	90	82	90	SW 2	SE 1	SW 2
3	700.4	702.0	703.6	04.2	10.2	07.2	07.2	10.7	03.1	03.3	05.7	04.8	04.2	91	51	56	66	ESE 2	SSW 4	S 3
4	705.0	706.0	707.6	08.4	14.2	09.6	10.4	14.5	04.5	04.2	04.2	05.3	04.7	51	44	52	49	SSW 4	SSW 4	ESE 2
5	707.0	707.7	708.4	11.4	19.0	16.4	15.8	19.2	06.4	04.6	04.5	05.2	05.1	44	32	37	38	ESE 3	WSW 5	SSW 5
6	708.6	707.0	705.6	16.5	23.6	20.2	20.1	23.8	14.8	12.6	05.1	04.2	04.0	36	19	22	26	WSW 1	SSW 4	S 6
7	704.0	704.5	702.6	18.4	22.8	17.6	19.1	23.9	13.3	14.4	03.5	04.9	01.9	22	23	13	19	S 7	S 5	S 3
8	701.4	703.1	706.6	14.9	09.2	07.2	09.6	17.6	06.8	11.0	04.3	06.7	05.0	50	77	65	64	SH 4	NNW 2	NNW 1
9	707.2	702.3	704.7	04.6	17.6	11.0	11.0	18.0	01.6	00.6	04.2	04.6	03.0	65	30	30	42	ESE 3	SSW 4	SSW 4
10	699.5	695.7	695.5	08.8	11.3	09.6	09.8	15.6	08.2	00.5	06.1	06.5	06.3	72	65	70	69	NM 1	NNW 2	W 2
11	703.1	707.2	707.8	01.6	06.0	02.0	02.9	05.6	00.0	00.4	04.6	04.8	04.1	90	68	78	79	W 1	SW 2	ESE 1
12	707.8	707.8	709.7	01.6	05.4	03.2	03.4	08.2	00.3	-00.9	04.8	05.1	04.8	94	76	84	85	- 0	M 5	- 0
13	709.7	709.2	708.0	01.8	14.0	09.2	08.6	14.5	-00.2	-01.1	03.8	06.5	04.8	73	54	56	61	E 2	M 5	NNW 1
14	708.7	706.7	706.2	04.2	19.0	11.4	11.5	19.0	02.5	02.6	04.8	05.9	05.8	77	36	58	57	- 0	WSW 2	- 0
15	705.0	703.2	702.4	06.3	18.8	12.2	12.4	19.2	04.7	01.4	05.4	05.1	04.6	75	31	43	50	E 1	WSW 4	SSW 3
16	701.4	700.0	701.5	10.2	10.8	09.4	10.0	12.2	09.4	07.4	05.6	07.8	07.8	60	80	88	76	W 1	- 0	- 0
17	704.8	706.0	706.9	08.4	08.7	07.3	07.9	09.4	07.0	08.1	05.9	05.9	06.7	71	70	87	76	NNW 2	W 1	- 0
18	707.7	707.7	708.6	06.0	09.2	06.3	10.2	10.2	04.6	05.0	05.2	04.7	04.2	74	53	65	64	NNW 2	NNW 1	ESE 2
19	709.2	708.8	709.2	05.4	14.4	07.4	08.6	14.6	04.4	02.5	04.7	04.8	04.5	70	39	58	56	- 0	M 2	- 0
20	710.3	708.2	709.3	02.0	15.8	07.9	08.4	17.0	00.4	-00.9	04.5	04.0	03.8	84	30	48	54	- 0	W 3	SE 1
21	710.6	709.1	710.8	03.0	09.0	11.4	08.7	19.9	00.6	00.6	04.2	08.2	05.3	73	95	52	73	ESE 1	M 2	M 3
22	710.2	707.4	708.0	07.2	17.4	12.0	12.2	18.0	05.0	04.4	05.6	07.8	07.2	74	52	68	65	ESE 1	NNW 1	ESE 3
23	707.1	706.2	708.3	07.6	17.4	10.8	11.6	17.5	06.0	05.0	06.6	06.1	06.5	85	41	67	64	E 1	ENE 2	E 2
24																				

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vidljivost 0- km	Oblačnost N (0-10)					Instalacija bez gazu	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8 00	000	00	00.0	10.3	$\sqcup^{\circ} 2^{\circ}-8^{\circ} = 8^{\circ} 12^{\circ}$	
2	8 05	040	00	03.0	09.1	$\sqcup^{\circ} 23^{\circ} 24$	
3	7 08	080	00	05.3	10.2	$\sqcup^{\circ} 0-8^{\circ} = 0-2^{\circ} 12^{\circ}$	
4	8 08	05	04	07.0	03.4	$F_{sw} 10^{\circ}$	
5	8 07	100	100	05.0	01.5	$F_{e} 3^{\circ} = 0^{\circ} 74^{\circ} 9^{\circ}, 0^{\circ} 12-15^{\circ}, 20^{\circ} 22^{\circ}$	
6	8 01	09	04	04.7	04.1	00.0	.	.	.	$\sqcup^{\circ} 0-7^{\circ} = 0^{\circ} 9^{\circ} 11^{\circ}, 0^{\circ} 16^{\circ} 16^{\circ}$	
7	8 08	09	03	06.7	03.5	00.0	.	.	.	$F_{sw} 3^{\circ} 3^{\circ} 9^{\circ} 9^{\circ} 10^{\circ}, 0^{\circ} 13^{\circ} 14^{\circ}$	
8	8 09	09	00	06.0	00.7	
9	8 08	08	10	08.7	06.8	
10	8 06	10	10	08.7	03.3	
11	8 09	09	08	08.7	02.3	00.4	.	.	.	$0^{\circ} 12^{\circ} 5^{\circ}$	
12	7 07	08	08	07.7	04.7	$F_{sw} 6^{\circ} 44^{\circ} 24^{\circ}, 0^{\circ} M^{\circ} 13^{\circ} 23^{\circ} 24$	
13	8 10	10	100	10.0	00.3	01.4	.	.	.	$0^{\circ} 3^{\circ} 20^{\circ} 24^{\circ}, 0^{\circ} 5^{\circ} 2^{\circ} 5^{\circ} 10^{\circ}$	
14	7 10	080	04	07.3	02.0	06.6	.	.	.	$0^{\circ} 3^{\circ} 14^{\circ}, 0^{\circ} 3^{\circ} 12^{\circ}, F_{e} 8^{\circ} 2^{\circ} 8^{\circ}$	
15	8 08	09	08	08.3	03.3	17.8	.	.	.	$F_{sw} 14^{\circ}$	
16	7 100	080	09	09.0	02.8	00.2	.	.	.	$0^{\circ} 4^{\circ} 8^{\circ} 30^{\circ} 44^{\circ} 12^{\circ}, 16^{\circ} 19^{\circ} L, 0^{\circ} 6^{\circ} 8^{\circ} 20^{\circ}$	
17	8 03	09	090	07.0	04.9	00.8	.	.	.	$\sqcup^{\circ} 4^{\circ} 7^{\circ}, 0^{\circ} 7^{\circ} 10^{\circ}, 0^{\circ} 20^{\circ} 24^{\circ}$	
18	7 050	09	06	06.7	03.1	00.3	
19	8 10	10	05	08.3	01.6	$F_{e} M^{\circ} 14^{\circ}$	
20	7 10	09	09	09.3	00.5	$0^{\circ} 8^{\circ} 2^{\circ} 4^{\circ}$	
21	5 100	10*	10	10.0	00.0	07.9	.	.	.	$0^{\circ} 1^{\circ} 3^{\circ} 5^{\circ} 13^{\circ} 45^{\circ}, 0^{\circ} 9^{\circ} 24^{\circ}, 0^{\circ} 13^{\circ} 20^{\circ}, \boxed{0}$	
22	7 10	10*	10	10.0	00.0	20.3	04	.	.	$0^{\circ} 0^{\circ} 9^{\circ} 0^{\circ} 6^{\circ} 13^{\circ} 22^{\circ} 15^{\circ}, \boxed{0}$	
23	7 10*	07	090	08.7	04.2	00.0	.	.	.	$*^{\circ} 6^{\circ} 9^{\circ}, *^{\circ} 5^{\circ} 24^{\circ}, *^{\circ} 1^{\circ} 5^{\circ} 24^{\circ}, \boxed{0}$	
24	5 10*	10*	10*	10.0	00.0	00.4	.	.	.	$*^{\circ} 0^{\circ} 6^{\circ} 13^{\circ} 20^{\circ}, \boxed{0}$	
25	7 09	10*	09	09.3	03.6	03.8	01	.	.	$*^{\circ} 0^{\circ} 6^{\circ} 13^{\circ} 20^{\circ}, \boxed{0}$	
MES. VRED.		07.7	08.3	06.0	07.3	110.6	73.1				

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1	6 100	100	10	10.0	00.0	05.8	.	.	.	$0^{\circ} 12^{\circ} 16^{\circ} 23^{\circ} 24^{\circ}, 13^{\circ} 3^{\circ} 8^{\circ} 25^{\circ} 8^{\circ} = 0^{\circ} 8^{\circ} 24$	
2	6 100	080	100	09.3	00.3	44.3	.	.	.	$0^{\circ} 2^{\circ} 0.24^{\circ} = 0^{\circ} 17^{\circ}$	
3	8 060	080	04	06.0	07.2	08.5	.	.	.	$0^{\circ} 2^{\circ} 1^{\circ} 0^{\circ} 22^{\circ} 24^{\circ}, F_{e} 12^{\circ} 22^{\circ} 15^{\circ}$	
4	8 08	070	04	06.3	06.1	00.2	.	.	.	$0^{\circ} 3^{\circ} F_{sw} 22^{\circ}$	
5	8 080	060	07	07.0	08.2	$F_{sw} 13^{\circ} 20^{\circ} 24^{\circ}$	
6	8 070	10	04	07.0	05.7	$F_{e} 6^{\circ} 9^{\circ} 24^{\circ}$	
7	8 07	070	00	04.7	06.0	$F_{sw} b^{\circ} 20^{\circ}$	
8	7 060	09	00	05.7	02.1	$F_{sw} 12^{\circ} 0^{\circ} 2^{\circ} 8^{\circ} 16^{\circ}$	
9	8 000	010	00	00.3	12.3	05.5	.	.	.	$F_{sw} 20^{\circ} 24^{\circ}$	
10	8 090	100	100	09.7	03.0	00.0	.	.	.	$0^{\circ} 6^{\circ} 7^{\circ}, M^{\circ} 24^{\circ}, F_{e} 9^{\circ} 3^{\circ} 23^{\circ} 23^{\circ}$	
11	7 100	09	09	09.3	02.6	05.8	.	.	.	$0^{\circ} 0^{\circ} 3^{\circ} 6^{\circ} 7^{\circ} 4^{\circ} 11^{\circ}, 0^{\circ} 1^{\circ} 9^{\circ} 2^{\circ} 3^{\circ} 14^{\circ}, 0^{\circ} 3^{\circ} 6^{\circ} 14^{\circ} 12^{\circ}, F_{sw} 11^{\circ}$	
12	7 10*	100	04	08.0	02.7	02.5	.	.	.	$*^{\circ} 4^{\circ} 2^{\circ} 1^{\circ} 0^{\circ} 2^{\circ} 6^{\circ} 10^{\circ}, 0^{\circ} 1^{\circ} 0^{\circ} 13^{\circ} 14^{\circ}, 0^{\circ} 2^{\circ} 20^{\circ} 24^{\circ}$	
13	8 000	030	00	01.0	11.5	02.6	.	.	.	$\sqcup^{\circ} 4^{\circ} 2^{\circ} 8^{\circ}, 0^{\circ} 2^{\circ} 2^{\circ} 8^{\circ} 3^{\circ}, 0^{\circ} 2^{\circ} 20^{\circ} 24^{\circ}$	
14	8 000	020	00	00.7	11.3	$\Delta^{\circ} 0^{\circ} 8^{\circ} 20^{\circ} 24^{\circ}$	
15	8 000	010	02	01.0	12.3	$\Delta^{\circ} 0^{\circ} 8^{\circ} 0^{\circ} 0^{\circ} 2^{\circ} 24^{\circ}$	
16	8 10	100	10	10.0	00.0	$0^{\circ} 4^{\circ} 5^{\circ} 17^{\circ}$	
17	7 10	10	10	10.0	00.0	01.2	.	.	.	$0^{\circ} 7^{\circ} 2^{\circ} 19^{\circ}$	
18	7 09	09	07	08.3	01.1	00.3	
19	7 090	040	00	04.3	09.3	$\Delta^{\circ} 0^{\circ} 8^{\circ} 20^{\circ} 24^{\circ}$	
20	8 000	000	00	00.0	12.5	$0^{\circ} 0^{\circ} 8^{\circ} 20^{\circ} 24^{\circ}$	
21	8 060	030	03	02.0	12.5	$\Delta^{\circ} 0^{\circ} 4^{\circ} 6^{\circ} 1^{\circ} 4^{\circ} 6^{\circ}$	
22	8 04	09	10	08.3	03.0	$\Delta^{\circ} 0^{\circ} 8^{\circ} = 0^{\circ} 7^{\circ} 13^{\circ}, 0^{\circ} 9^{\circ} 2^{\circ} 9^{\circ}$	
23	7 080	090	09	08.7	02.6	$\Delta^{\circ} 6^{\circ} 7^{\circ} 0^{\circ} 0^{\circ} 2^{\circ} 24^{\circ}$	
24	7 100	10	10	10.0	00.0	00.0	.	.	.	$\Delta^{\circ} 0^{\circ} 6^{\circ} = 0^{\circ} 5^{\circ} 8^{\circ}, 0^{\circ} 6^{\circ} 7^{\circ} 9^{\circ} 6^{\circ}$	
25	7 100	100	00	06.7	00.6	00.0	.	.	.	$\Delta^{\circ} 0^{\circ} 6^{\circ} = 0^{\circ} 5^{\circ} 8^{\circ}, 0^{\circ} 6^{\circ} 7^{\circ} 9^{\circ} 6^{\circ}$	
26	7 100	100	100	10.0	00.2	04.0	.	.	.	$\Delta^{\circ} 0^{\circ} 8^{\circ}, 0^{\circ} 1^{\circ} 8^{\circ} 8^{\circ} 11^{\circ} 19^{\circ}, \Delta^{\circ} 0^{\circ} 2^{\circ} 19^{\circ} 24^{\circ}$	
27	7 100	100	100	10.0	00.0	04.6	.	.	.	$\Delta^{\circ} 0^{\circ} 7^{\circ} 0^{\circ} 0^{\circ} 2^{\circ} 23^{\circ}, 0^{\circ} 7^{\circ} 2^{\circ} 23^{\circ}$	
28	8 10	08	09	08.0	02.4	01.3	
29	7 040	050	00	03.0	12.5	$\Delta^{\circ} 0^{\circ} 8^{\circ} = 5^{\circ} 8^{\circ}$	
30	8 000	010	00	00.3	12.5	$\Delta^{\circ} 0^{\circ} 3^{\circ}$	
MES. VRED.		06.6	07.0	05.1	04.2	160.9	90.6				

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 $\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h + 14 min.$

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d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina vjetra D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	710.0	709.3	711.3	05.6	19.2	05.8	11.1	20.0	04.0	03.0	05.2	05.1	07.0	76	31	77	61	-	0	N	3	-	0
2	710.8	710.0	709.0	08.0	08.6	07.5	07.9	10.7	07.1	07.6	05.7	05.8	07.1	71	65	91	77	W	3	W	2	-	0
3	706.1	704.3	703.9	07.6	11.0	09.6	09.4	11.5	06.4	07.5	07.4	06.8	07.5	95	69	84	83	-	0	-	0	-	0
4	705.0	705.7	707.3	08.2	17.4	12.6	12.7	18.0	05.4	05.2	06.5	06.7	08.1	79	45	74	66	-	0	S	2	WSM	1
5	707.9	707.8	708.7	09.0	19.4	12.2	13.2	19.7	07.4	06.7	06.8	07.3	06.4	79	43	60	61	ESE	3	ESE	3	SE	1
6	709.0	706.2	707.4	10.0	22.3	15.9	16.0	23.0	06.0	08.0	07.5	07.1	07.1	82	35	52	56	-	0	ESE	3	-	0
7	706.8	704.8	705.2	13.5	23.2	14.7	16.5	23.5	11.0	09.5	08.6	09.2	10.3	74	43	82	66	ESE	2	WSM	3	-	0
8	703.0	702.0	702.8	13.7	17.2	14.2	14.6	20.6	10.7	09.6	09.8	11.5	08.3	84	78	69	77	ESE	2	NW	1	-	0
9	704.8	704.3	706.8	08.6	20.3	13.4	13.9	20.4	07.5	07.3	07.6	05.8	05.8	90	33	50	58	-	0	W	2	-	0
10	707.9	707.4	706.8	08.0	20.8	13.2	13.8	20.8	05.2	04.5	06.1	05.7	07.4	75	31	65	57	-	0	W	2	E	2
11	706.8	703.6	704.0	09.8	22.6	17.4	16.8	23.0	07.2	06.5	07.2	09.2	07.8	79	45	52	55	-	0	-	0	NNW	2
12	702.7	700.0	699.6	11.8	20.0	15.4	15.6	20.3	09.0	08.0	06.9	07.5	10.6	66	43	81	63	ESE	2	-	0	NN	1
13	699.5	698.7	699.1	12.0	14.2	12.2	12.6	21.5	11.1	09.9	08.9	09.9	09.3	85	81	87	84	-	0	E	3	NN	1
14	698.8	699.6	700.2	11.4	12.8	10.8	11.4	12.8	10.2	10.4	09.2	10.2	09.3	91	92	95	93	-	0	WNW	1	-	0
15	702.3	702.7	704.0	10.7	18.8	14.8	14.8	20.0	09.1	07.9	09.0	09.2	09.2	92	57	73	74	-	0	ESE	1	-	0
16	704.6	704.0	705.5	11.6	23.8	17.8	17.8	24.0	05.8	08.4	08.8	08.3	10.5	86	37	66	64	-	0	W	2	E	1
17	706.9	706.4	708.2	12.4	25.5	18.9	18.9	25.6	10.1	09.8	09.2	08.1	09.9	85	33	61	60	-	0	W	1	ESE	1
18	710.2	710.0	710.9	12.4	25.0	16.4	17.6	25.4	10.8	09.3	09.3	09.4	09.2	86	40	65	64	-	0	NNW	2	ENE	1
19	711.4	709.4	711.2	13.4	25.0	17.6	18.4	25.3	10.4	09.9	08.9	10.8	10.2	78	45	67	63	-	0	NNW	2	-	0
20	711.2	708.0	709.1	14.0	23.8	15.4	17.2	25.6	11.2	10.6	09.1	10.0	09.9	76	45	75	65	-	0	NE	4	-	0
21	709.9	707.4	707.7	13.6	24.0	16.0	17.4	24.5	11.6	11.6	10.0	11.8	10.1	86	53	74	71	-	0	W	2	E	2
22	707.3	706.4	706.2	13.8	24.8	19.8	17.6	24.2	10.2	10.0	09.7	10.0	10.2	82	43	75	67	ESE	2	W	3	ESE	1
23	705.0	702.2	703.1	14.5	25.0	16.8	18.3	25.6	11.0	10.5	09.3	09.5	09.4	75	40	66	60	ESE	2	SSW	3	-	0
24	703.2	702.2	703.1	13.0	17.3	14.0	14.6	18.5	11.8	11.5	09.7	12.5	10.8	86	84	90	87	-	0	W	1	ESE	1
25	703.5	702.8	704.5	13.2	23.4	16.8	17.6	23.9	12.0	12.2	10.2	08.7	10.9	90	40	76	66	-	0	N	1	ESE	1
26	705.2	704.2	706.4	13.8	22.6	13.2	15.7	22.6	10.8	10.7	09.7	09.5	10.9	82	46	96	75	ESE	2	ENE	2	-	0
27	706.4	706.0	706.5	11.7	16.4	12.3	13.2	17.0	10.3	10.1	10.1	10.1	10.1	98	72	95	88	-	0	SSW	1	-	0
28	706.3	706.6	708.2	12.4	15.4	13.2	13.6	16.0	11.6	10.2	10.3	10.1	09.5	96	77	83	85	WSM	1	WSM	1	-	0
29	707.5	705.6	705.4	12.8	23.2	18.0	18.0	23.6	11.5	12.0	09.5	10.7	04.8	85	50	31	55	-	0	WSM	2	NW	1
30	704.3	705.1	704.0	16.2	17.0	16.0	16.3	19.0	11.8	10.8	08.1	09.2	09.1	59	64	67	63	SW	1	S	2	-	0
31	705.8	703.8	704.5	13.6	24.4	17.6	18.3	24.6	11.0	10.5	09.2	09.7	08.8	79	42	58	60	-	0	NNW	2	-	0
MES.	VRED.	706.1	705.0	705.8	11.6	20.1	14.5	15.2	21.0	09.6	09.1	08.5	08.9	08.9	82	52	72	65	0.6	1.0	0.6	0.6	

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1	704.9	703.7	703.6	15.3	24.4	18.8	19.3	25.0	10.1	09.5	09.6	08.1	07.8	73	35	48	52	ESE	2	SSE	3	-	0
2	702.2	702.9	702.3	17.6	16.7	16.0	16.6	22.4	13.8	11.5	09.1	11.6	10.8	60	81	79	73	SM	1	ESE	2	-	0
3	702.4	700.2	702.9	13.1	22.2	11.4	14.5	22.2	11.2	11.1	10.5	08.8	09.4	93	44	93	77	-	0	NW	1	-	0
4	704.6	705.9	707.3	09.8	10.6	09.5	09.8	12.3	09.3	09.9	08.7	07.2	07.8	95	75	87	86	WSM	1	SSM	1	WSM	2
5	708.9	708.9	709.3	07.5	09.8	06.6	07.6	10.5	06.2	07.1	06.1	06.4	06.6	79	70	91	80	WSM	1	NNW	1	-	0
6	708.9	709.2	709.7	04.0	07.8	08.0	07.4	08.8	05.3	06.4	06.6	06.0	07.4	95	75	92	87	-	0	-	0	-	0
7	708.2	707.9	707.7	07.8	10.0	09.4	09.2	10.6	07.2	07.8	06.6	04.5	06.4	83	71	72	75	-	0	C	-	0	0
8	706.3	705.4	706.2	08.6	09.8	08.7	09.0	10.0	07.8	08.4	07.6	08.2	08.0	90	91	95	92	-	0	-	0	-	0
9	705.5	704.8	704.9	08.7	10.4	11.6	10.6	13.4	07.6	08.0	08.1	08.6	09.1	96	91	89	92	-	0	C	-	0	0
10	704.3	704.2	705.8	11.4	17.6	13.4	14.0	19.0	09.1	08.5	08.6	11.1	09.9	85	73	86	81	ESE	2	E	1	-	0
11	707.0	708.5	709.0	12.0	21.9	16.4	16.7	22.0	10.2	09.8	08.9	10.2	10.2	85	52	73	70	-	0	NW	2	ESE	1
12	708.2	707.5	708.4	15.1	23.9	16.0	17.8	25.0	12.3	12.0	10.6	09.8	12.3	82	44	90	72	-	0	SE	1	-	0
13	707.7	705.9	707.4	15.2	24.6	16.6	18.2	25.4	14.5	15.2	11.7	10.4	11.3	90	45	80	72	-	0	NNW	2	-	0
14	706.9	705.5	706.8</																				

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_x = 1.0 \text{ m}$

Dan	Vrijest O-9	Obločnost N (0-10)					Imogljici sati broj	Padavina R mm	Snežni pokrivač h cm	Rozvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8	00	0	07	0	08	05.0	C9.0	.	$\Delta^2 3-8^{\circ} P_{ANE} 16^{\circ}-17^{\circ}$	
2	7	10	10	10	0	10	10.0	00.0	00.0	$\bullet^0 3^{\circ}-5^{\circ} 16^{\circ}-24^{\circ}$	
3	6	10	0	10	0	08	09.3	C0.0	03.7	$\bullet^0 10-14^{\circ}, -5^{\circ} 8^{\circ}$	
4	8	05	0	09	10	08	08.0	06.6	00.4		
5	8	10	10	06	08	07	00.8	.	.		
6	8	10	08	08	08	08	08.7	04.4	00.0	$\bullet^0 5^{\circ} 6^{\circ}$	
7	8	08	05	04	04	05	05.7	C5.6	.	$\Delta^0 0^{\circ} 7^{\circ} 12^{\circ} 16^{\circ}, 0^{\circ} 15^{\circ}-16^{\circ}$	
8	8	07	0	07	0	00	04.7	03.1	03.8	$\bullet^0 14^{\circ} 12^{\circ}$	
9	8	03	0	04	03	03	03.3	11.6	C1.8	$\bullet^0 2^{\circ} 3^{\circ}$	
10	8	01	0	03	03	00	01.3	12.2	.	$\Delta^0 0-8^{\circ}, 24^{\circ} 24^{\circ}$	
11	8	00	0	08	03	03	03.7	11.1	.	$\Delta^0 0-7^{\circ}$	
12	8	07	09	10	0	08	08.7	02.6	.	$\bullet^0 0^{\circ} 19^{\circ} 20^{\circ}$	
13	8	08	10	10	0	08	05.3	02.9	00.0	$\bullet^0 10^{\circ} 10^{\circ} 12^{\circ} 19^{\circ} 22^{\circ} 24^{\circ}, 12^{\circ} 14^{\circ} 13^{\circ}, P_{E} 13^{\circ}$	
14	6	10	0	10	0	08	09.3	00.0	18.4	$\bullet^0 0-18^{\circ}=0-24^{\circ}$	
15	8	10	08	05	05	07	07.7	04.0	20.6	$=^0 0-3^{\circ}, \Delta 22^{\circ} 24^{\circ}$	
16	7	04	0	02	01	01	02.3	11.7	.	$\Delta^0 0-8^{\circ}=0^{\circ} 6^{\circ} 13^{\circ}$	
17	7	00	0	04	00	01	01.3	11.9	.	$\Delta^0 0-8^{\circ} 12^{\circ} 12^{\circ} 12^{\circ}$	
18	8	00	0	04	00	01	01.3	11.6	.	$\Delta^0 0-7^{\circ}$	
19	8	03	0	06	00	03	03.0	10.6	.	$\Delta^0 0-7^{\circ}$	
20	7	00	0	10	03	08	06.0	07.2	.	$\Delta^0 0-7^{\circ}, 13^{\circ} 13^{\circ} 13^{\circ}, 0^{\circ}-15^{\circ} 17^{\circ}$	
21	7	05	0	09	03	03	05.7	06.1	00.1	$\Delta^0 0^{\circ} 8^{\circ} 14^{\circ} 16^{\circ} 15^{\circ} 15^{\circ} 15^{\circ}$	
22	8	05	0	07	04	04	05.3	C9.7	03.2	$\Delta^0 0-7^{\circ} 24^{\circ} 24^{\circ} 13^{\circ} 14^{\circ} 17^{\circ} 18^{\circ}, 0^{\circ}-14^{\circ} 14^{\circ} 16^{\circ} 17^{\circ}, P_{E} 20^{\circ} 21^{\circ}$	
23	8	01	0	06	09	09	05.3	08.8	00.2	$\Delta^0 1^{\circ} 2^{\circ} 2^{\circ}, 5-42^{\circ} 18^{\circ} 23^{\circ}$	
24	7	10	0	09	10	08	09.7	00.8	00.5		
25	8	10	05	07	07	03	08.8	14.2	.		
26	8	01	0	09	10	10	06.7	C5.4	.	$\Delta^0 0-7^{\circ} 14^{\circ} 11^{\circ} 13^{\circ} 15^{\circ} 15^{\circ} 15^{\circ}, 0^{\circ}-2 14^{\circ} 21^{\circ} 14^{\circ} 14^{\circ} 14^{\circ}$	
27	7	10	10	07	09	09	00.0	21.3	.	$\Delta^0 0-8^{\circ} 5-5^{\circ} 12^{\circ} 12^{\circ} 14^{\circ} 15^{\circ} 15^{\circ}, 0^{\circ}-2 24^{\circ}$	
28	7	10	09	10	09	05	05.7	00.1	09.1	$\bullet^0 0-11^{\circ} 12^{\circ} 9^{\circ}$	
29	8	08	07	00	05	05	11.3	01.7	.	$\Delta^0 0-7^{\circ}, 13^{\circ} 13^{\circ}$	
30	8	10	10	10	10	10	10.0	00.5	.	$\Delta^0 1^{\circ} 2^{\circ}, 5-42^{\circ} 18^{\circ} 23^{\circ}$	
31	8	04	05	02	03	07	09.7	10.7	04.0	$\bullet^0 0-1$	
MES. VREDO		05.8	07.4	05.6	04.3	190.1	105.8				

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1	8	07	08	00	05	05.0	07.5	.	$\Delta^0 0^{\circ} 8^{\circ}$		
2	7	04	10	05	06	04.2	.	.	$\bullet^0 1^{\circ} 2^{\circ} 12^{\circ} 12^{\circ}, 1^{\circ} 2^{\circ} 12^{\circ} 15^{\circ} 15^{\circ} 15^{\circ} 15^{\circ}, 0^{\circ}-15^{\circ} 15^{\circ}, \Delta 15^{\circ} 15^{\circ}$		
3	7	09	09	07	06	02.1	01.8	.	$\bullet^0 1^{\circ} 2^{\circ} 12^{\circ} 12^{\circ}, 1^{\circ} 2^{\circ} 12^{\circ} 15^{\circ} 15^{\circ} 15^{\circ}, 0^{\circ}-15^{\circ} 15^{\circ}, \Delta 15^{\circ} 15^{\circ}$		
4	7	10	10	10	10	10.0	00.0	42.6	.		
5	7	10	10	10	10	10.0	00.0	03.3	.	$\bullet^0 0-1^{\circ} 1^{\circ} 24^{\circ}$	
6	7	10	10	10	10	10	10.0	00.0	04.5	$\bullet^0 0-10^{\circ}$	
7	7	10	10	10	10	10	10.0	00.0	00.2	$\bullet^0 0-10^{\circ}$	
8	6	10	10	10	10	10	10.0	00.0	01.3	$\bullet^0 0-19^{\circ}=14^{\circ} 24^{\circ}$	
9	6	10	10	10	10	10	10.0	00.0	00.8	$\Delta^0 0-2^{\circ} 6-17^{\circ} 1^{\circ} 0^{\circ} 14^{\circ} 14^{\circ}$	
10	7	04	07	04	05	05.7	00.7	02.6	.	$\bullet^0 13^{\circ} 15^{\circ}$	
11	7	03	06	10	04	04.3	02.7	00.8	.	$\Delta^0 0^{\circ} 8^{\circ} 17^{\circ} 17^{\circ} 19^{\circ} 23^{\circ} 18^{\circ}$	
12	7	01	09	10	04	04.7	04.8	.	$\Delta^0 2^{\circ} 12^{\circ} 0^{\circ} 6^{\circ} 7^{\circ} 15^{\circ} 17^{\circ}, 1^{\circ} 15^{\circ} 17^{\circ}$		
13	7	00	09	09	09	04.7	01.2	02.6	.	$\Delta^0 20^{\circ}-24^{\circ}$	
14	7	10	07	00	05	05.7	00.3	00.4	.	$\Delta^0 0-8^{\circ}$	
15	7	00	03	01	01	01.3	12.6	.			
16	8	07	08	10	04	04.3	04.7	.	$\Delta^0 0^{\circ} 7^{\circ} 0^{\circ} 14^{\circ} 23^{\circ}$		
17	8	03	09	06	06	04.7	04.4	07.2	.	$\bullet^0 12^{\circ} 15^{\circ}$	
18	8	04	04	10	04	04.0	03.8	02.5	.	$\bullet^0 7^{\circ} 8^{\circ}$	
19	7	10	10	10	10	10.0	00.0	05.6	.	$\bullet^0 4^{\circ} 12^{\circ}=15^{\circ}$	
20	7	10	10	10	10	10.0	00.0	04.7	.	$\bullet^0 4^{\circ} 12^{\circ}=15^{\circ}$	
21	7	10	09	08	09	09.0	01.1	04.8	.	$\Delta^0 0-3^{\circ} 14^{\circ} 15^{\circ} 14^{\circ} 14^{\circ} 14^{\circ}, 0^{\circ} 14^{\circ} 15^{\circ} 15^{\circ} 15^{\circ}, 0^{\circ} 14^{\circ} 15^{\circ} 15^{\circ} 15^{\circ}$	
22	7	10	09	08	08	04.3	00.6	04.4	.	$\bullet^0 14^{\circ} 14^{\circ} 15^{\circ} 15^{\circ}$	
23	7	10	10	08	08	09.3	00.3	01.5	.	$\Delta^0 6^{\circ} 9^{\circ} 15^{\circ} 15^{\circ} 15^{\circ} 15^{\circ}$	
24	7	04	06	06	06	04.0	03.4	01.2	.	$\bullet^0 4^{\circ} 5^{\circ} 8^{\circ} 10^{\circ} 13^{\circ} 12^{\circ} 12^{\circ} 13^{\circ}, 1^{\circ} 12^{\circ} 12^{\circ} 12^{\circ} 12^{\circ}$	
25	7	10	08	08	08	06.7	00.8	25.3	.	$\Delta^0 2^{\circ} 9^{\circ} 5^{\circ} 13^{\circ} 12^{\circ} 17^{\circ}, 0^{\circ} 12^{\circ} 16^{\circ}$	
26	7	10	09	02	07	07.0	00.6	07.2	.	$\bullet^0 2^{\circ} 4^{\circ} 2^{\circ} 5^{\circ} 8^{\circ}, =^0 3^{\circ} 10^{\circ}, \Delta 20^{\circ} 24^{\circ}$	
27	8	01	06	06	05	05.8	00.8	00.2	.	$\Delta^0 0-9^{\circ}$	
28	8	00	01	03	01.3	10.0	.	.	$\Delta^0 0-7^{\circ}$		
29	8	00	03	00	04	09.3	.	.	$\Delta^0 0-8^{\circ}$		
30	8	01	04	02	02	02.3	00.1	.	$\Delta^0 0-8^{\circ}, \Delta 20^{\circ} 23^{\circ}, 0^{\circ} 22^{\circ} 23^{\circ}$		
MES. VREDO		07.0	07.0	06.6	07.1	92.7	134.9				

$\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h + 14 min.$

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d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, I (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	699.6	699.7	701.7	14.2	11.6	10.0	11.4	20.6	06.6	13.4	16.0	05.1	06.2	62	85	86	86	NNW	1	SE	1	WSW	2	
2	699.7	700.4	700.4	09.4	12.4	11.6	11.2	12.6	08.6	09.5	07.6	09.2	09.8	66	85	96	85	-	0	-	0	-	0	
3	702.8	704.9	706.5	12.0	17.6	16.6	15.8	19.0	11.4	09.6	10.1	10.6	11.4	96	72	80	83	-	0	W	2	-	0	
4	707.2	704.5	703.5	14.4	26.2	19.6	20.0	26.4	12.4	11.2	10.8	10.2	09.7	88	40	57	62	-	0	NW	1	N	1	
5	702.3	701.7	703.3	15.8	21.2	15.4	17.0	23.6	14.4	12.2	08.1	10.1	09.4	60	53	72	62	ESE	2	W	1	E	2	
6	702.9	704.4	706.4	14.6	19.2	15.6	16.2	19.2	14.0	14.4	16.0	12.9	12.5	80	78	94	84	-	0	SW	2	ESE	2	
7	708.3	708.4	709.3	15.6	22.4	17.5	18.2	23.4	14.0	14.2	12.5	12.6	11.6	94	62	77	78	-	0	SW	2	ENE	2	
8	710.4	709.0	709.1	14.7	25.5	18.8	19.4	26.0	12.1	11.1	10.7	12.2	10.6	85	50	65	67	ESE	2	SW	2	ESE	2	
9	709.6	708.9	708.9	16.0	27.8	20.4	21.2	28.2	13.4	12.4	10.6	13.3	09.2	77	47	51	58	ESE	1	NW	1	ESE	1	
10	708.4	708.4	706.6	17.2	29.2	21.7	22.4	29.5	14.4	13.6	11.8	12.0	15.2	80	39	76	66	SE	2	SW	2	-	0	
11	706.8	706.6	707.3	18.2	24.6	16.3	18.8	26.5	15.9	13.7	14.3	13.9	13.0	91	60	93	81	-	0	NE	3	E	1	
12	706.8	704.8	706.1	16.0	28.4	15.6	18.9	28.6	13.2	13.0	12.1	14.2	11.6	88	49	87	75	SSE	1	W	4	ESE	3	
13	707.9	708.8	710.8	15.6	22.2	19.0	19.0	23.2	13.6	12.9	11.6	12.7	12.5	87	63	76	75	-	0	NW	1	SE	2	
14	711.2	710.2	711.0	15.6	25.6	20.4	20.5	26.0	13.4	12.4	11.7	13.1	12.9	88	53	74	71	E	1	W	2	NNE	1	
15	711.0	709.4	709.0	15.8	28.8	21.3	21.8	29.0	13.8	12.3	11.9	14.0	15.4	88	47	81	72	ESE	1	W	2	SE	2	
16	706.1	706.0	705.3	17.7	31.0	22.8	23.6	31.2	15.3	14.0	12.8	14.4	14.1	85	37	66	63	ESE	1	WNW	2	SSE	1	
17	706.4	705.7	706.5	18.6	28.3	22.2	22.8	29.0	17.0	15.1	12.8	14.9	14.1	80	52	70	67	ESE	1	W	2	SE	2	
18	707.4	706.2	705.8	18.6	31.8	23.3	24.2	32.3	16.6	15.4	13.8	10.2	12.7	86	25	55	52	SW	1	WNW	1	-	0	
19	704.2	703.8	705.6	24.4	32.8	21.4	25.0	32.0	17.7	16.0	10.5	11.5	12.7	46	31	67	48	NW	2	WSW	3	S	2	
20	707.4	706.3	706.6	17.8	23.0	17.2	18.8	23.7	16.5	16.2	10.0	10.1	10.4	65	46	70	61	ESE	3	S	1	ESE	2	
21	706.3	704.7	705.1	13.4	24.5	18.4	18.7	26.0	11.2	10.8	08.9	09.9	10.2	78	43	64	62	-	0	NNW	2	ESE	3	
22	706.0	705.4	706.3	14.2	24.4	17.8	18.6	24.6	11.0	11.7	10.0	11.9	10.7	82	52	70	68	-	0	SE	2	ENE	2	
23	707.2	705.7	706.5	15.4	26.3	19.3	20.1	26.8	13.2	12.8	10.1	12.5	12.1	77	49	72	66	E	1	W	1	ESE	2	
24	706.2	704.9	704.9	16.0	28.0	20.6	21.3	28.2	14.2	14.0	11.3	11.7	12.6	83	41	69	64	-	0	W	2	ESE	1	
25	704.3	704.1	706.9	16.8	25.4	18.4	19.8	27.2	13.9	13.5	10.7	12.4	13.1	74	51	82	69	E	1	NNW	1	NW	4	
26	710.7	711.2	711.8	11.6	15.7	11.1	12.4	19.4	10.8	12.5	08.9	07.9	08.5	87	59	86	77	ESE	2	W	1	ESE	1	
27	712.0	709.3	710.2	10.0	22.2	14.4	15.2	22.4	07.4	07.4	08.2	08.4	08.4	90	42	68	67	SSW	1	SSE	1	E	2	
28	710.4	708.8	709.9	10.2	23.4	16.1	16.4	23.6	08.3	08.0	07.8	09.6	08.5	84	45	62	64	-	0	NW	3	E	2	
29	710.2	709.2	709.1	12.6	23.3	17.2	17.6	23.6	10.5	10.2	08.2	10.7	11.0	75	50	75	67	-	0	S	1	SE	2	
30	709.0	707.0	708.5	12.8	24.6	15.7	17.2	25.2	11.4	11.2	09.7	11.5	11.8	87	50	88	75	ESE	1	NNW	2	-	0	
31	709.2	707.5	709.7	14.8	25.0	16.0	18.0	25.0	13.8	13.7	11.6	10.0	11.6	92	42	85	73	W	1	N	3	-	0	
MES.	WRED.	707.1	706.2	707.0	15.2	24.3	17.6	16.8	25.3	13.0	12.5	10.6	11.5	11.5	82	52	75	70	0.8	1.7	1.5			

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1	709.9	709.3	710.8	14.0	23.2	17.0	17.8	23.7	12.6	12.0	11.0	09.7	10.1	92	46	65	69	-	0	N	2	S	1
2	711.6	710.4	711.4	14.0	23.6	16.0	17.4	24.3	12.8	12.5	10.8	10.6	11.1	90	49	81	73	NNW	3	W	5	-	0
3	712.0	711.6	712.1	15.4	19.1	16.4	16.8	20.4	14.6	12.4	11.7	10.6	10.2	89	64	73	75	-	0	NN	2	-	0
4	711.1	709.7	709.7	14.4	20.0	14.2	15.7	21.6	19.0	12.3	10.5	10.6	10.2	85	60	84	76	SE	1	NNW	2	-	0
5	709.4	707.7	709.3	13.8	19.2	13.6	15.0	20.9	13.0	12.6	10.4	10.8	10.5	88	65	90	81	-	0	WSN	1	SSE	1
6	709.7	710.8	711.3	12.3	16.0	12.1	13.1	19.0	10.4	10.4	09.6	11.6	09.8	89	85	92	89	ESE	1	SE	1	SE	1
7	711.0	710.0	709.9	13.0	19.0	14.0	15.0	19.1	10.8	10.8	10.1	12.0	11.2	89	73	94	85	SE	2	WSN	2	NNW	1
8	709.2	707.9	708.4	12.8	20.2	17.0	16.8	22.0	10.9	10.5	09.9	12.2	10.6	89	69	73	77	ESE	2	SE	1	SE	1
9	708.0	707.3	708.6	13.6	21.6	17.2	17.4	22.3	12.2	11.5	10.0	13.6	12.8	86	70	87	81	-	0	WSN	2	SSE	2
10	709.0	708.9	709.8	13.4	25.4	17.6	18.6	25.9	12.1	11.5	10.3	12.9	13.1	90	53	85	76	ESE	1	SW	2	E	1
11	709.7	708.7	708.5	14.4	27.4	19.0	20.0	27.4	12.8	12.3	10.8	12.5	13.6	86	46	82	72	SE	2	SSW	2	E	1
12	707.0	704.3	704.5	15.0	26.4	20.4	20.6	26.5	13.3	12.9	11.5	12.1	11.6	90	47	64	67	WSW	1	W	2	-	0
13	703.8	703.4	704.1	15.8	19.1	15.2	16.3	20.4	14.6	14.0	11.6	13.7	12.2	86	83	94	88	-	0	NW	1	-	0
14	708.3	708.7	709.8	14.4	21.4	15.6	16.8	22.0	13.7	14.4	11.6	11.9	10.5	94	62	79	78	WNW	1	WNW	2	-	0

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Den	Vidljivost 0-9	Oblačnost N (0-10)					Insektacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	6	09	10	10	09.7	C2.1	C0.6	.	• 17 ²⁵ 9 ²⁰ 12 ²⁰ 24 ¹ ; ▲ 17 ²⁵ 7 ²⁵ 12 ²⁵ 8 ²⁵ 12 ²⁵ 13 ²⁵ = 12-24; Pw 12 ²⁵	
2	7	10	10	10	10.0	00.0	12 ²	.	• 10 ²⁵ 7 ²⁵ 16 ²⁵ 24 ¹ ; ▲ 0-4-12-24	
3	7	10	05	09	09.3	C2.2	C0.9	.	• 0-3-8-9-10-11	
4	8	00	03	00	01.0	13.0	C1.2	.	• 0-3 ² 8-12 ²⁵ 9-20 ²⁵ 24	
5	8	09	10	10	09.7	C1.7	.	.	• 0-8-11 ² 17 ²⁵ 17 ²⁵ 17 ²⁵ 17	
6	7	10	09	10	09.7	00.1	00.5	.	• 5 ²⁵ 12 ²⁵ 10 ²⁵ 24 ¹	
7	7	09	09	00	06.0	06.2	07.2	.	• 0-1 ² 14-9 ²⁵ 19 ²⁵ 24	
8	8	00	05	00	01.7	12.5	.	.	• 12-0-9-20 ²⁵ 24; = 5 ²⁵ 9	
9	8	00	03	00	01.0	13.3	.	.	• 0-8 ² 12 ²⁵ 20 ²⁵	
10	7	00	01	07	C2.7	10.6	.	.	• 0-8 ² 12 ²⁵ 20 ²⁵	
11	7	10	09	00	06.3	C3.3	.	.	• 0-8 ² 15 ²⁵ 13 ²⁵ 13 ²⁵ 16 ²⁵ ; = 15 ²⁵ 16 ²⁵	
12	8	02	06	00	02.7	C9.1	02.9	.	• 6 ²⁵ 10 ²⁵ 15-17 ²⁵ 17 ²⁵ 17 ²⁵ 17 ²⁵	
13	8	09	09	09	09.0	02.9	04.0	.	• 9 ²⁵ 8 ²⁵ 10-12 ²⁵ 14 ²⁵	
14	7	05	05	04	04.7	10.0	06.8	.	• 0-8 ² 22 ²⁵ 24	
15	8	00	03	00	01.0	13.4	.	.	• 0-8 ² 22 ²⁵ 24	
16	8	00	02	00	00.7	13.4	.	.	• 0-8 ² 20 ²⁵ 24; = 5 ²⁵ 9	
17	7	00	01	00	00.3	13.2	.	.	• 0-8 ² 8 ²⁵	
18	7	00	01	00	00.3	12.8	.	.	• 22 ²⁵ 24	
19	8	01	01	10	04.0	12.5	.	.	• 0-8 ² 22 ²⁵ 24	
20	8	07	09	03	04.3	02.4	.	.	• 0-8 ² 22 ²⁵ 24	
21	7	00	06	01	02.3	09.7	.	.	• 0-8 ²	
22	7	10	06	07	07.7	C7.0	.	.	• 0-8 ²	
23	8	02	03	00	01.7	11.0	.	.	• 0-8 ² 22 ²⁵ 24; = 5 ²⁵ 9	
24	8	00	05	03	02.7	10.8	.	.	• 0-8 ² 22 ²⁵ 24	
25	7	00	09	07	05.3	04.6	.	.	• 0-8 ² 22 ²⁵ 24; = 5 ²⁵ 9	
26	8	10	10	01	07.0	00.0	04.6	.	• 0-8 ² 22 ²⁵ 24	
27	8	05	05	05	05.0	08.2	00.0	.	• 0-8 ² 20 ²⁵ 24	
28	8	00	03	00	01.0	13.1	.	.	• 0-8 ² 20 ²⁵ 24	
29	7	10	07	00	05.7	C3.6	.	.	• 0-8 ² 20 ²⁵ 24	
30	7	07	06	04	05.7	05.3	.	.	• 2-7 ²⁵ 7 ²⁵ 15 ²⁵ 16 ²⁵ ; = 5 ²⁵ 9	
31	8	10	07	07	00.0	C5.7	01.6	.	• 0-2 ²⁵ 18 ²⁵ 19 ²⁵ ; = 2-11 ²⁵	
MES. VREO		04.7	05.9	03.8	04.8	235.9	48.5			

1	7	08	07	01	05.3	04.9	.	• 15-14 ²⁵ 21 ²⁵ 23		
2	7	05	07	05	05.7	07.1	04.6	• 0-10 ²⁵ 19-13 ²⁵ 12 ²⁵ < 20 ²⁵ 22 ²⁵		
3	7	10	10	08	09.3	00.9	00.4	• 0-4 ²⁵ 2-14 ²⁵ 13 ²⁵		
4	7	10	09	08	09.0	02.6	00.1	• 0-6 ²⁵ = 4 ²⁵ 12 ²⁵ 0-6 ²⁵ 8, 16 ²⁵ 21; Pw 10 ²⁵		
5	7	10	09	05	08.0	04.0	03.8	• 0-9 ²⁵ 0-2-3-4 ²⁵ 13 ²⁵ 16 ²⁵ ; = 15 ²⁵ 16		
6	7	07	09	03	06.3	01.9	01.2	• 0-5 ²⁵ 13 ²⁵ 0-9 ²⁵ 16 ²⁵ ; = 15 ²⁵ 16 ²⁵		
7	7	06	09	01	05.3	01.0	02.9	• 0-4 ²⁵ 18-15 ²⁵ 14 ²⁵ 15 ²⁵		
8	7	09	09	09	09.0	03.4	01.5	• 0-6 ²⁵ 10 ²⁵		
9	6	10	10	09	06.7	00.0	00.4	• 0-5 ²⁵ 7 ²⁵ 17 ²⁵ 20 ²⁵ 4= 6-15 ²⁵		
10	7	01	05	00	02.0	08.6	00.7	• 0-3 ²⁵ 10 ²⁵ ; = 16 ²⁵ 8-15 ²⁵ 16 ²⁵		
11	8	00	05	00	01.7	09.0	04.0	• 15 ²⁵ 16 ²⁵ 0-8 ²⁵ 19 ²⁵ 6		
12	8	08	06	01	05.0	09.0	00.1	• 0-2 ²⁵ 5 ²⁵ 14 ²⁵ 17 ²⁵ 22 ²⁵ ; = 16 ²⁵ 16 ²⁵ 8-15 ²⁵ 16 ²⁵		
13	6	10	10	10	10.0	00.5	04.0	• 0-2 ²⁵ 5 ²⁵ 12 ²⁵ 14 ²⁵ 17 ²⁵		
14	7	09	09	05	07.7	02.1	12.7	• 0-9 ²⁵ 20-24		
15	8	10	00	00	03.3	10.2	.	• 0-9 ²⁵ 15 ²⁵ 16 ²⁵ 17 ²⁵ 18 ²⁵		
16	8	02	08	04	04.7	07.8	.	• 0-8 ²⁵		
17	8	09	07	01	05.7	07.2	00.3	• 0-5 ²⁵ 0-5-6 ²⁵		
18	7	01	02	03	02.0	09.4	.	• 0-9 ²⁵ 15 ²⁵ 18 ²⁵ 18 ²⁵ 18 ²⁵		
19	7	09	10	10	05.7	00.6	05.8	• 15 ²⁵ 16 ²⁵ 17 ²⁵ 18 ²⁵ 19 ²⁵		
20	7	08	08	09	08.3	02.2	05.2	• 5-11		
21	8	08	05	00	04.3	09.6	00.0	• 0-0 ²⁵ 0-1-24 ²⁵		
22	8	00	01	00	00.3	12.6	.	• 0-9 ²⁵ 15 ²⁵ 19 ²⁵ 24		
23	8	00	02	00	00.7	12.7	.	• 0-9 ²⁵ 15 ²⁵ 19 ²⁵ 24		
24	8	07	10	09	08.7	03.3	.	• 0-9 ²⁵ 14-16 ²⁵ 19 ²⁵ 20 ²⁵ 23 ²⁵ 24		
25	7	08	10	02	04.7	01.6	14.6	• 0-4 ²⁵ 0-6 ²⁵ 12 ²⁵ 17 ²⁵ 15 ²⁵ 18 ²⁵		
26	6	10	10	04	08.0	00.1	11.0	• 2 ²⁵ 10 ²⁵ 13 ²⁵ 16 ²⁵ 18 ²⁵ 14 ²⁵		
27	7	08	09	10	09.0	01.1	03.0	• 3 ²⁵ 6 ²⁵ 0-13 ²⁵ 15 ²⁵ 23 ²⁵ 24		
28	7	10	10	09	09.7	00.4	06.2	• 0-6 ²⁵ 12 ²⁵ 20-20 ²⁵ 23 ²⁵ 24; = 5 ²⁵ 12		
29	7	10	07	00	05.7	03.0	03.2	• 0-0 ²⁵ 14 ²⁵ 0-6 ²⁵ 14 ²⁵ , = 14 ²⁵		
30	8	09	10	04	07.7	04.0	01.4	• 13 ²⁵ 13 ²⁵ 0-3 ²⁵ 14 ²⁵		
31	8	08	04	04	05.3	08.6	01.4	• 0-9 ²⁵ 20-24; = 5 ²⁵ 5 ²⁵		
MES. VREO		07.1	07.3	04.3	04.2	151.6	95.5			

$\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h + 14 min.$

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60	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	709.4	708.5	709.1	13.4	25.0	17.0	18.1	25.2	12.2	12.0	10.8	11.6	12.2	94	49	84	76	ESE 2	SSE 1	E 2	
2	709.0	708.3	708.2	13.2	24.2	18.2	16.4	25.0	12.2	11.6	10.7	14.2	13.4	94	63	86	81	ESE 2	WSW 2	SE 2	
3	706.6	705.3	703.6	13.8	22.6	16.6	17.4	24.0	12.2	11.7	11.1	13.3	11.5	94	65	81	80	-	0	M 1	
4	704.2	704.4	705.9	13.4	21.7	16.4	17.0	21.7	12.8	11.5	11.0	11.5	12.1	96	59	87	81	-	0	SW 2	
5	706.6	705.5	706.4	13.5	25.6	16.2	17.9	25.6	12.5	12.0	10.4	11.9	12.5	90	48	90	76	ESE 3	NW 2	-	
6	707.6	708.1	708.7	12.8	25.2	17.0	18.0	25.2	11.2	10.9	10.3	09.9	11.1	93	41	76	70	SSE 2	M 2	SW 1	
7	708.3	707.4	707.7	14.0	17.4	16.0	15.8	20.7	12.8	12.0	10.8	13.5	11.8	90	91	87	89	SE 2	-	0	
8	710.2	711.6	712.5	14.0	17.1	14.8	15.2	18.9	13.0	12.1	11.5	11.8	11.4	96	81	90	89	-	0	M 2	
9	712.1	710.8	710.9	14.1	23.0	13.6	16.1	23.0	12.3	14.0	11.4	09.3	08.3	95	44	71	70	-	0	NNW 2	
10	710.3	709.2	709.8	08.4	22.4	13.6	14.4	22.5	08.2	08.2	07.2	10.4	09.8	89	51	84	75	SE 1	NNW 1	ESE 3	
11	708.6	706.6	707.0	09.8	24.1	17.8	17.4	25.0	08.6	08.0	08.2	09.0	10.2	91	40	67	66	SE 1	NW 2	ESE 2	
12	706.0	705.8	705.0	15.8	18.2	15.6	16.3	21.7	13.7	08.0	10.6	14.2	12.8	79	93	96	89	-	0	WSW 2	
13	704.4	706.4	709.5	11.6	20.0	12.0	13.9	20.7	10.8	10.6	10.0	10.4	08.9	98	60	85	81	E 3	M 2	NW 2	
14	709.2	707.8	707.0	11.8	23.6	15.4	16.6	24.4	11.3	11.0	09.5	10.1	09.8	91	46	74	70	-	0	NW 2	ESE 1
15	707.7	708.1	710.7	14.6	27.4	17.4	19.2	27.4	12.0	11.4	10.7	10.2	11.2	86	37	75	66	E 3	NW 3	ESE 3	
16	714.5	714.0	716.1	14.2	29.6	19.3	20.6	29.8	12.4	11.4	09.7	11.8	13.7	80	38	82	67	ESE 4	-	0	
17	714.3	715.7	716.3	14.6	28.4	19.4	20.4	28.4	13.4	13.0	11.3	14.2	14.5	91	49	86	75	ESE 2	NW 2	ENE 2	
18	715.5	713.9	715.0	15.2	25.4	15.4	17.8	25.8	14.1	13.0	12.3	12.0	09.4	95	49	72	72	E 2	E 4	ESE 3	
19	714.2	712.4	713.2	11.6	24.6	15.2	16.6	25.1	10.4	09.2	08.9	11.0	10.0	87	47	77	70	-	0	M 3	E 2
20	713.0	711.8	712.3	09.4	24.6	14.4	15.7	24.7	08.2	08.0	08.3	08.0	09.2	94	35	74	68	E 1	ESE 2	E 3	
21	713.0	711.8	713.3	10.3	24.6	16.2	16.8	25.3	09.4	09.5	08.3	12.1	11.5	88	52	83	74	SE 1	WSW 1	E 2	
22	714.3	714.6	716.0	11.2	22.8	15.6	16.3	23.0	10.6	10.0	09.6	10.7	11.2	97	51	85	78	E 1	M 2	E 1	
23	716.2	714.0	714.0	10.6	24.1	15.0	16.2	24.3	10.0	09.4	08.9	11.6	11.0	93	52	86	77	-	0	-	ESE 2
24	713.7	711.6	711.2	10.0	23.8	13.8	15.4	24.4	09.2	08.7	08.6	08.9	09.2	95	40	78	71	ESE 1	SE 1	ESE 4	
25	710.8	709.9	709.3	09.4	24.6	13.9	15.4	25.1	08.0	07.8	08.0	07.0	08.3	90	30	69	63	SE 2	WSW 1	SE 1	
26	707.7	706.2	706.4	10.4	24.8	17.4	17.5	25.3	08.6	07.7	07.5	10.0	08.5	80	43	57	60	ESE 3	SW 4	-	
27	710.3	712.0	713.3	13.4	26.2	16.8	18.3	26.2	12.0	10.6	09.9	10.2	11.2	86	40	78	68	ESE 2	E 2	SE 3	
28	714.4	714.3	714.9	12.2	25.2	16.2	17.4	25.6	11.6	10.6	09.6	11.0	12.0	90	46	87	74	ESE 3	M 2	ESE 1	
29	714.3	719.3	719.3	11.0	25.9	16.2	17.3	26.5	09.2	09.0	09.2	11.2	10.2	93	45	74	71	SSE 1	M 2	ESE 2	
30	712.6	709.7	710.2	10.4	25.8	17.4	17.8	25.8	10.0	09.0	08.8	10.4	11.7	93	42	78	71	-	0	WSW 1	ESE 2
MES.	710.7			12.3	23.9	16.0	17.0	24.5	11.1	10.3	09.8	11.0	11.0	91	51	80	74	1.4	1.8	1.7	
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1	711.1	710.2	711.3	12.2	27.2	17.4	18.6	27.9	11.0	10.0	09.5	13.5	11.4	89	50	76	72	ESE 2	SW 1	ESE 1	
2	711.5	710.3	713.2	12.0	25.4	17.8	18.2	26.4	11.1	10.0	09.9	11.4	11.5	95	47	75	72	ESE 2	SW 2	SE 2	
3	712.2	711.6	711.4	13.2	21.7	13.8	15.6	21.7	12.2	11.8	10.2	10.7	10.5	90	55	89	78	ESE 1	M 1	E 1	
4	712.5	711.2	711.2	10.6	20.4	14.6	15.0	21.2	09.5	09.1	09.1	10.0	09.1	95	56	73	75	-	0	-	ESE 1
5	712.9	712.2	714.0	10.2	14.8	10.1	11.3	17.0	09.7	09.5	06.7	05.5	05.8	72	43	62	59	SSW 1	M 2	NE 1	
6	714.4	714.2	714.4	07.1	15.5	08.2	09.8	15.5	06.6	05.5	06.5	06.2	06.6	86	47	80	71	-	0	ENE 3	E 2
7	713.2	710.8	709.9	03.8	18.1	10.8	10.9	18.6	03.4	02.9	05.7	07.5	07.8	94	48	80	74	ESE 3	SW 1	-	
8	711.9	710.0	710.3	07.4	15.4	05.6	08.3	15.6	04.0	02.8	06.5	05.2	05.2	85	40	76	67	E 2	M 4	E 3	
9	705.1	707.1	707.2	02.7	10.4	07.8	07.2	12.0	08.9	00.5	04.6	09.9	07.1	83	73	90	82	ESE 1	NW 2	-	
10	705.3	703.4	703.5	07.0	13.2	06.6	08.4	14.5	06.5	07.0	04.7	05.0	06.5	90	44	89	74	ESE 1	SE 4	ESE 3	
11	704.7	706.9	706.3	03.4	05.8	06.1	05.4	06.6	02.3	02.0	05.6	06.4	06.1	95	92	87	91	-	0	-	SE 2
12	708.2	707.8	708.3	04.2	13.8	10.8	10.4	13.9	05.4	03.0	04.7	07.4	08.9	95	63	92	83	-	0	SE 3	ESE 4
13	707.4	704.4	702.7	12.7	19.4	14.0	15.0	21.2	10.3	10.4	10.2	07.3	08.4	93	43	70	69	ESE 5	SE 3	-	
14	700.4	703.6	706.7	04.6	09.6	07.4	08.2	14.7	07.4	08.0	08.0	08.0	07.1	95	89	92	92	E 3	NNW 2	-	
15	707.5	707.6	709.2	04.8	13.6	06.3	08.6	15.0	05.8	05.6	06.8	07.3	06.4	92	62	86	80	ESE 2	-	0	
16	706.0	706.4	703.8	05.6	14.8	11.5	10.8	15.8	03.8	03.6	05.9	07.0	07.6	86	55	75	72	ESE 3	WSW 2	ESE 3	
17	698.2	699.0	700.2	09.3	16.0	08.9	10.8	16.4	06.6	09.3	08.4	06.5	07.9	95	47	90	77	-	0	SW 4	ESE 3
18	699.3	699.3	700.7	06.4	09.4	07.8	08.4	10.8	07.6	07.0	04.										

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$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vlaknost 0-9	Obločnost N (0-10)					Imelotija broj seti	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	07	050	00	04.0	C7.7	•	Δ ² 0-9, 20 ³⁰ 24, 0°15 ⁵⁰ 16 ³⁰		
2	8	020	070	00	03.0	09.4	00.2	Δ ² 0-10, 15 ¹⁷ 20 ³⁰		
3	7	00	00	09	07	05.3	06.7	Δ ¹ 0-10, = 16-8, = 18-11, 0°-19-19 ⁵⁰ 23 ³⁰ 24, 0°19 ⁵⁰ 20, 15 ²³ -24		
4	8	09	080	01	06.0	05.2	04.7	• 0°-13 ⁵⁰ 10-14 ⁵⁰ , Δ ² 20-24		
5	8	060	040	00	03.3	08.0	•	Δ ² 0-9, 19 ³⁰ 24, = 15 ³⁰ 17 ³⁰ , 15 ¹⁵⁻¹⁶ 05, 0°15 ³⁰ 16 ⁰⁵		
6	8	030	030	00	02.0	10.6	00.6	Δ ² 0-9 ⁴⁵		
7	8	10	10	C5	08.3	02.1	•	Δ ¹ 0-7 ⁴⁵ , 0°-17 ⁰⁵ 74 ⁰ 12 ³⁰ -13 ³⁰		
8	7	10	10	10	10.0	C0.0	02.6	• 0°40 ¹⁰ , 10 ³⁰ 14 ³⁰ , = 4 ³⁰ 9 ³⁰		
9	7	10	060	00	05.3	G7.0	00.2	= 13 ³⁰ 11, Δ ² 20 ³⁰ 24		
10	7	030	020	00	01.7	10.7	•	Δ ² 0-9 ⁴⁵ , 21-24		
11	7	050	040	09	06.0	08.9	•	Δ ¹ 0-10 ⁴⁵		
12	7	08	100	10*	05.3	00.2	•	• 0°-8 ³⁰ 24		
13	8	07	09	10	08.7	05.9	26.7	• 0°-3, 15 ² 0 ³⁰ 2 ³⁰		
14	8	10	030	00	04.3	08.5	•	Δ ¹ 19-24		
15	8	000	060	00	02.0	10.6	•	Δ ² 0-9 ⁴⁵		
16	8	030	000	00	01.0	10.0	•	Δ ¹ 2-9 ³⁰ 19 ³⁰ 24		
17	8	000	000	00	00.0	10.1	•	Δ ¹ 0-8 ¹ 19 ³⁰ 24		
18	7	000	030	00	01.0	10.1	•	Δ ¹ 2-0-6 20-24		
19	7	000	000	00	00.0	10.6	•	Δ ¹ 2-0-10 ⁴⁵ 21-24		
20	8	000	000	00	00.0	10.3	•	Δ ¹ 2-0-9 ⁴⁵ , 19-24		
21	8	000	040	00	01.3	09.6	•	Δ ² 0-9, 19 ³⁰ 24, 16-12		
22	7	030	070	00	03.3	C6.6	•	Δ ¹ 0-9 ⁰⁵ , = 16 ³⁰ , 16 ⁴⁰ , = 06 ⁴⁰ 9 ⁵⁰		
23	6	00	00	050	05	03.3	08.3	• 0°-9 ³⁰ , = 16 ³⁰ , 9 ⁵⁰ , = 19-15 ³⁰		
24	8	04	030	00	02.3	08.9	•	• 0°-9 ³⁰ , 16-10 ³⁰		
25	8	000	020	00	00.7	10.1	•	Δ ² 0-9, 19 ³⁰ 24		
26	8	000	040	00	01.3	09.2	•	Δ ¹ 0-9 ³⁰		
27	8	09	030	00	C4.0	07.5	•	Δ ¹ 0-8 ³⁰		
28	8	000	080	05	04.3	08.0	•	Δ ¹ 0-9		
29	8	000	000	00	00.0	10.2	•	Δ ¹ 0-10 ³⁰ , 17 ³⁰ 11		
30	8	000	050	00	01.7	07.7	•	Δ ¹ 0-10, 19 ³⁰ 24		

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 $\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h + 14 min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog parne e mm			Relativna vlažnost u %				Pravac i jačina vetro D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	709.5	708.9	710.2	03.0	17.4	08.4	09.3	17.7	02.2	-01.0	04.4	05.7	06.3	77	38	76	64	WSW 2	W 1	E 1	
2	711.6	711.4	713.4	04.4	17.4	08.7	09.8	17.7	03.9	03.0	05.6	06.8	06.7	89	46	80	72	ESE 3	WSW 1	ESE 3	
3	714.3	713.5	714.9	03.7	16.8	09.4	09.8	17.2	03.2	02.0	05.7	07.3	07.0	96	51	79	75	- 0	WSW 1	ESE 4	
4	714.9	714.6	716.3	03.0	13.8	05.4	06.9	14.7	02.8	01.9	05.2	07.0	05.9	91	59	88	79	SE 2	NW 3	- 0	
5	715.3	713.8	714.2	04.4	10.2	04.9	06.1	10.6	02.8	01.8	05.7	05.0	05.5	91	54	85	77	ESE 3	WNW 2	- 0	
6	713.1	711.4	712.4	05.4	11.6	02.8	05.6	11.8	02.6	05.2	05.6	04.7	04.9	84	46	88	73	- 0	WNW 1	SE 1	
7	711.5	710.4	710.3	03.6	09.2	05.4	05.9	10.5	01.0	00.0	05.2	04.6	04.9	88	52	73	71	- 0	NW 1	E 2	
8	710.8	710.0	709.8	04.0	08.6	06.0	06.2	09.1	03.7	02.2	05.4	04.3	04.3	88	51	61	67	- 0	ESE 4	ESE 4	
9	707.8	707.5	708.4	04.0	07.2	05.7	05.6	07.2	03.8	02.2	05.1	05.6	05.9	84	74	86	81	WSW 1	WSW 2	WNW 1	
10	709.4	708.4	706.9	04.5	07.6	07.2	06.6	08.0	03.9	02.6	06.1	07.4	07.2	97	95	95	96	ESE 1	- 0	E 5	
11	707.8	710.3	711.9	04.2	05.4	04.4	04.6	07.2	03.4	02.0	05.9	05.8	04.7	96	86	75	86	- 0	WSW 1	- 0	
12	712.4	713.6	715.4	02.0	04.6	04.7	04.0	05.1	01.4	00.0	04.7	05.8	06.0	89	91	93	91	- 0	- 0	- 0	
13	715.7	714.7	714.6	04.4	12.2	05.8	06.0	12.2	03.2	00.0	05.7	05.5	05.2	91	51	87	76	- 0	SE 2	ESE 3	
14	712.8	711.5	710.4	01.5	03.8	03.4	03.0	04.2	-00.2	-00.1	04.6	05.5	05.5	90	91	94	92	SE 4	W 1	- 0	
15	709.8	709.5	708.7	03.0	02.0	02.2	02.4	04.0	01.2	03.5	05.3	05.0	04.9	94	94	91	93	WNW 2	- 0	SSW 2	
16	704.2	700.4	697.4	01.6	04.0	04.4	03.6	04.6	01.2	01.2	04.8	05.2	05.0	94	86	80	87	SSE 2	- 0	E 2	
17	693.6	693.6	694.5	07.0	14.3	13.5	12.1	14.6	04.0	04.0	05.4	06.8	08.3	72	56	71	66	ESE 3	S 3	WSW 1	
18	695.7	695.8	699.5	14.8	11.3	08.2	10.6	15.8	07.8	10.0	06.0	08.0	06.0	48	79	74	67	S 1	S 4	SE 2	
19	701.0	702.4	702.9	04.5	11.6	07.3	08.9	12.4	07.0	05.5	05.2	05.1	07.2	59	49	94	67	SSE 3	SSW 3	- 0	
20	702.4	701.2	699.7	04.6	10.3	07.7	07.6	10.7	04.2	04.6	05.6	04.6	05.9	89	49	74	71	- 0	W 3	W 3	
21	699.7	704.7	707.0	05.8	01.2	00.4	02.0	08.0	-00.4	04.9	06.5	04.5	03.1	93	90	66	83	ESE 2	- 0	N 1	
22	704.5	701.2	702.3	-05.9	01.8	-01.2	-01.6	01.8	-07.7	-06.5	02.2	02.7	03.0	75	53	71	66	ESE 1	WSW 2	- 0	
23	704.3	704.5	706.7	-03.4	-02.2	-03.8	-03.3	-01.0	-04.4	-01.8	02.9	03.1	03.1	81	80	90	84	W 2	W 3	NW 2	
24	706.1	706.7	708.9	-05.3	-04.6	-05.0	-05.0	-03.0	-05.6	-04.6	02.7	02.7	02.8	89	83	87	86	WNW 1	W 2	- 0	
25	710.3	711.0	711.6	-09.8	-02.8	-09.2	-07.8	-02.0	-10.4	-10.6	01.9	01.9	01.7	86	50	76	71	- 0	WNW 1	ESE 1	
26	711.8	710.0	710.2	-14.4	-02.6	-07.2	-07.8	-02.2	-14.6	-14.0	01.1	01.9	02.4	73	51	89	71	ESE 3	SW 1	- 0	
27	710.1	709.5	709.6	-10.3	01.8	-01.0	-02.6	01.8	-10.9	-09.9	01.8	02.5	03.2	88	48	75	70	- 0	- 0	- 0	
28	706.1	703.9	703.7	00.6	06.4	03.6	03.6	07.8	-01.6	-01.5	04.3	04.8	05.4	90	66	91	82	E 1	ESE 4	S 1	
29	703.6	703.5	704.9	01.6	08.3	04.8	04.9	08.8	01.0	00.4	04.8	05.6	05.7	94	68	89	84	- 0	SE 1	- 0	
30	705.9	704.4	704.6	00.3	09.6	09.2	07.1	11.0	00.2	-00.2	04.4	05.7	05.1	93	64	59	72	ENE 1	- 0	SSW 2	
MES.	VRED.	707.9	707.3	708.1	01.7	07.2	03.8	04.1	08.2	00.3	00.2	04.7	05.0	05.1	86	65	81	77	1.5	1.5	1.4

1975 DECEMBAR

SARAJEVO

1	705.3	706.2	707.3	07.2	11.8	08.0	08.8	12.6	05.9	03.8	05.6	04.3	05.9	74	41	73	63	E 1	W 2	ESE 3
2	706.7	705.1	705.8	05.4	10.4	03.4	05.6	11.2	03.2	03.2	04.9	06.5	04.7	73	69	81	74	E 3	- 0	ESE 3
3	707.1	708.4	710.8	-00.2	02.2	01.6	01.3	04.1	-00.6	-01.5	04.4	05.0	04.8	96	94	94	95	- 0	- 0	- 0
4	712.7	713.9	715.4	-00.2	01.1	01.4	00.9	02.0	-00.5	-00.5	04.4	04.8	04.9	96	97	97	97	- 0	- 0	- 0
5	719.1	719.6	719.7	01.6	05.0	03.1	03.2	05.2	01.0	01.8	05.0	05.1	04.8	97	78	83	86	- 0	- 0	SE 1
6	712.2	708.3	706.9	-00.4	06.2	01.1	02.0	06.7	-01.4	-00.8	04.1	04.0	03.7	91	56	75	74	ESE 2	- 0	ESE 2
7	710.5	710.7	711.5	00.3	01.0	-03.2	-01.3	02.3	-03.5	-02.0	04.1	02.9	02.9	88	58	80	75	- 0	NW 1	- 0
8	708.3	707.4	709.2	-04.4	03.0	-01.6	-01.6	03.0	-07.2	-07.0	02.4	03.6	03.2	83	63	79	75	ESE 2	- 0	- 0
9	711.9	712.2	713.2	-03.0	05.3	-01.3	-00.1	05.5	-03.2	-06.8	03.3	03.3	03.2	89	50	76	72	- 0	- 0	ESE 2
10	713.5	712.1	713.1	-05.2	04.4	01.4	00.5	04.6	-05.6	-06.0	02.7	03.7	04.0	87	58	79	75	ESE 1	- 0	- 0
11	713.5	713.1	713.2	00.0	03.2	02.3	02.0	03.4	-01.3	-03.1	04.4	04.1	04.0	97	72	74	81	- 0	- 0	E 3
12	710.3	708.3	706.6	01.2	02.8	01.5	01.8	02.9	00.9	00.8	03.6	04.1	03.7	72	73	73	73	ESE 3	- 0	- 0
13	705.2	705.7	706.3	-00.2	02.8	00.4	00.6	02.2	-00.3	00.0	04.4	04.7	04.5	96	90	95	94	- 0	- 0	- 0
14	709.9	710.8	713.6	-02.0	-00.6	-00.8	-01.0	00.6	-02.8	-03.1	03.7	04.1	04.0	93	92	92	92	- 0	- 0	WNW 2
15	715.0	713.7	714.0	-01.0	00.6	-00.1	-00.2	00.9	-01.4	-00.8	03.9	04.1	04.2	92	85	91	89	- 0	W 1	W 1
16	712.3	708.7	705.6	-01.6	03.2	10.2	05.5	10.2	-01.8	-02.5	03.6	05.1	06.3	88	88	68	81	ESE 3	- 0	S 3
17	701.2	697.4	699.1	11.0	14.2	09.4	11.0	15.4	06.0	03.5	07.0	06.6	06.8	71	55	77	68	ESE 1	S 4	S 4
18	698.2	699.7	705.2	04.8	05.0	01.4	04.2	12.8	01.4	02.4	05.8	06.0	04.5	90	70	87	82	- 0	NW 3	SH 1
19	706.9	707.2	708.4	-00.4	00.4	-01.3	-00.6	01.6	-01.6	-00.3	04.0	03								

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vremenska časost 0-9 0-9	Oblačnost N (0-10)					Intenzija sunca sat	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7 03	00○	00	01.0	08.1	•	•	•	•	•
2	6 00	00○	00	00.0	07.8	•	•	•	•	•
3	5 07	01○	00	02.7	06.1	•	•	•	•	•
4	6 00	03○	05	02.7	07.3	•	•	•	•	•
5	7 10	05○	10	08.3	03.1	•	•	•	•	•
6	7 10	00○	00	03.3	04.0	•	•	•	•	•
7	6 10	10	05	08.3	01.5	•	•	•	•	•
8	6 06	10	08	08.0	01.2	•	•	•	•	•
9	6 10*	09	10	09.7	00.0	01.0	•	•	•	•
10	3 10	10○	10*	10.0	00.0	00.0	•	•	•	•
11	7 07	10	10	09.0	00.0	17.1	•	•	•	•
12	6 09	10	10	08.7	00.0	01.4	•	•	•	•
13	7 10	03○	00	04.3	07.3	01.1	•	•	•	•
14	6 08	10*	10*	09.3	00.0	•	•	•	•	•
15	4 10*	10*	10	10.0	00.0	06.4	•	•	•	•
16	6 07	10*	10	09.0	00.0	05.4	•	•	•	•
17	7 08	10*	10*	09.3	00.3	00.6	•	•	•	•
18	6 10*	10*	10*	10.0	00.0	03.7	•	•	•	•
19	5 10	10	10*	10.0	00.0	14.8	•	•	•	•
20	8 10	10	10*	10.0	00.0	04.2	•	•	•	•
21	6 10*	10*	09	09.7	00.0	00.6	•	•	•	•
22	8 04	00○	05	03.0	04.7	07.5	•	•	•	•
23	6 10*	10*	10*	10.0	00.0	00.6	01	•	•	•
24	6 10*	10*	10*	10.0	00.0	03.9	08	•	•	•
25	7 07	00○	00	02.3	05.5	02.4	10	•	•	•
26	6 00	00○	00	00.0	06.5	•	04	•	•	•
27	6 00	00○	09	03.0	03.3	•	04	•	•	•
28	7 10	10	10*	10.0	00.1	•	03	•	•	•
29	6 05	00	01	04.7	00.5	02.3	•	•	•	•
30	7 08	00	00	05.3	05.4	•	•	•	•	•
MES.	VRED.	07.3	06.6	06.4	06.8	78.9	79.1			

SARAJEVO

1975 DECEMBAR

1	8 07	09	03	06.3	00.6	•	•	•	•	•
2	8 03	03	00	02.7	04.5	•	•	•	•	•
3	2 00	10	10	06.7	00.0	•	•	•	•	•
4	2 10	10	10	10.0	00.0	00.0	•	•	•	•
5	4 10	08	08	04.7	00.1	•	•	•	•	•
6	6 09	00○	00	03.0	06.0	•	•	•	•	•
7	7 10*	09	00	06.3	02.7	00.8	•	•	•	•
8	6 00	00○	04	01.3	06.4	00.2	•	•	•	•
9	6 05	02○	00	02.3	04.9	•	•	•	•	•
10	3 00	00	00	00.0	06.2	•	•	•	•	•
11	5 10	09	10	09.7	00.0	•	•	•	•	•
12	7 10	09	10*	09.7	00.0	•	•	•	•	•
13	5 10*	10	10	10.0	00.0	05.4	07	•	•	•
14	4 10	10	10	10.0	00.0	04.2	05	•	•	•
15	5 10	10	10	10.0	00.0	00.0	04	•	•	•
16	7 04	09	08	07.6	00.4	00.6	03	•	•	•
17	8 08	09	10	09.0	01.3	00.2	•	•	•	•
18	7 05	07○	10	07.3	05.0	12.3	•	•	•	•
19	7 10	10	10	10.0	00.0	00.0	00	•	•	•
20	7 10*	10	04	00.0	02.2	00.0	•	•	•	•
21	7 07	09	07	07.1	03.5	•	•	•	•	•
22	5 10	04○	00	04.7	02.7	•	•	•	•	•
23	6 08	00○	00	05.7	04.2	•	•	•	•	•
24	5 00	00○	00	00.0	02.0	•	•	•	•	•
25	4 10	10	00	04.7	00.0	•	•	•	•	•
26	6 01	06	10	09.7	03.1	00.0	•	•	•	•
27	5 10*	10*	10*	10.0	00.0	01.8	03	•	•	•
28	6 10	08○	00	04.6	01.8	05.4	04	•	•	•
29	3 00	10	10	04.7	00.0	•	•	•	•	•
30	3 00	09	10	09.7	00.0	00.0	•	•	•	•
31	3 10	10	10	10.0	10.0	00.0	•	•	•	•
MES.	VRED.	07.0	07.2	05.2	04.7	57.6	30.5			

1975 JANUAR

BEOGRAD

 $\varphi = 46^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = + 1h 22 min.$

BR. ST. 171

5 d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, I (0-12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	760.1	758.2	757.0	-05.0	-00.6	-01.2	-02.0	00.0	-05.1	-08.0	02.5	02.8	03.5	78	63	82	74	M	1	WSW	2	SW	2	
2	758.7	760.1	761.5	-01.2	00.2	00.3	-00.1	00.5	-02.3	-04.0	03.8	03.9	04.3	91	84	91	89	NNE	2	NW	2	NNW	2	
3	761.8	762.3	762.4	-01.7	-01.6	-02.4	-02.0	00.3	-02.4	-01.8	03.8	03.7	03.6	93	91	94	93	N	1	NNW	2	SSW	1	
4	761.4	759.7	759.3	-02.5	01.9	-01.4	-00.8	03.0	-03.1	-03.1	03.6	03.9	03.8	96	74	91	87	SSW	1	NNW	1	SE	1	
5	759.5	758.9	757.2	-01.4	05.0	04.6	03.2	05.4	-02.5	-04.6	03.8	04.4	04.3	91	67	68	75	WSW	3	WSW	2	SSE	2	
6	754.8	753.0	751.6	07.0	14.2	08.8	09.7	14.7	04.0	02.3	04.5	04.8	05.1	60	40	60	53	WSW	2	WSW	3	SE	2	
7	749.9	746.1	746.2	02.4	11.3	08.2	07.6	12.8	02.2	-02.4	04.7	05.5	04.6	87	54	57	66	SE	1	N	2	WSW	2	
8	743.5	743.1	747.8	05.6	02.4	01.0	02.5	08.2	01.0	03.8	06.2	05.3	04.7	91	97	95	94	SE	2	N	2	NNW	2	
9	753.5	756.9	760.4	00.2	02.2	00.3	00.8	02.7	00.0	-01.2	03.8	04.1	03.9	82	76	84	81	NW	3	NW	3	WSW	2	
10	760.9	759.5	759.6	-03.0	05.1	-00.8	00.1	05.4	-03.4	-07.6	03.0	02.7	03.4	82	41	78	67	-	0	S	2	SE	2	
11	758.8	757.2	757.3	-01.1	10.1	02.1	03.3	10.2	-01.1	-05.5	03.0	04.1	04.4	72	44	82	66	ESE	1	ESE	2	SE	2	
12	756.7	757.1	758.2	01.7	08.0	04.4	04.6	08.2	01.1	-03.6	04.1	04.0	04.6	79	50	74	68	SW	1	WSW	2	ESE	1	
13	759.3	759.2	760.4	02.7	10.6	04.0	05.3	12.0	02.2	-02.3	04.6	05.0	05.0	83	52	82	72	ESE	2	ESE	3	SE	1	
14	761.6	760.6	760.4	00.5	10.6	05.0	05.3	10.8	-00.3	-04.2	04.3	04.9	04.6	91	51	70	71	E	1	ESE	3	SE	3	
15	760.1	759.6	759.2	02.8	11.1	06.3	06.7	12.4	02.0	-03.6	04.4	05.3	04.4	78	53	60	64	ESE	2	ESE	2	ESE	2	
16	757.8	756.8	756.0	03.0	12.7	06.6	07.2	12.7	02.7	-01.9	03.9	04.4	04.0	69	40	54	54	SE	2	SE	3	ESE	3	
17	755.3	753.6	753.4	00.4	09.8	03.8	04.5	10.2	00.4	-05.0	03.9	04.5	04.7	82	50	71	70	ESE	1	NNE	2	ESE	1	
18	751.9	750.5	751.1	01.4	13.3	07.0	07.2	14.6	00.0	-04.5	04.0	04.3	03.7	80	37	49	55	ESE	1	ESE	1	ESE	3	
19	750.4	752.5	753.3	04.4	10.8	03.2	05.4	11.9	03.2	-00.4	03.3	04.2	03.6	53	43	63	53	SE	3	NNW	2	ESE	3	
20	758.8	758.9	758.7	-01.2	05.2	01.0	01.5	06.3	-01.2	-04.4	03.4	04.8	04.7	81	72	95	83	SE	2	NW	1	SE	1	
21	758.0	757.3	758.1	-01.2	04.8	-00.4	00.7	05.0	-01.5	-05.0	03.8	04.2	03.6	91	64	80	78	SE	2	ESE	3	ESE	3	
22	758.9	758.3	757.3	-00.6	02.1	01.1	00.9	02.1	-01.0	-04.2	03.6	04.0	04.2	82	76	85	81	ESE	1	ESE	1	ESE	1	
23	754.6	752.9	752.1	01.6	05.6	05.0	04.3	07.8	01.0	00.3	04.5	04.7	04.5	88	70	69	76	ESE	1	W	1	ESE	1	
24	751.2	750.4	751.5	03.8	12.3	09.2	08.6	13.4	01.4	-03.0	04.4	04.5	05.4	73	42	62	59	SE	1	S	2	-	0	
25	753.4	753.2	753.0	04.2	12.5	06.0	07.2	13.0	04.1	-00.6	05.3	06.5	06.0	85	60	86	77	SSE	1	W	4	SE	2	
26	752.3	753.3	756.6	07.8	10.6	07.6	08.4	11.0	05.7	00.0	06.0	07.3	05.2	76	76	67	73	SW	2	W	2	NNW	2	
27	756.9	753.8	748.7	01.7	08.2	03.1	04.0	09.4	01.6	-01.4	04.8	02.7	04.1	92	33	72	66	WSW	1	SW	1	SE	3	
28	742.6	741.2	743.6	03.2	02.4	01.4	02.1	03.4	01.4	-00.1	03.8	04.8	04.8	66	89	95	83	ESE	3	ESE	4	ESE	3	
29	743.3	743.5	747.6	02.0	06.3	03.6	03.9	06.3	01.0	-00.3	05.0	05.2	05.6	95	73	94	87	S	1	WSW	1	W	2	
30	749.4	749.9	753.0	00.8	06.4	04.4	04.0	07.0	00.6	-02.6	04.0	04.2	04.9	83	58	78	73	NNW	2	NW	3	NNW	3	
31	757.1	757.6	757.7	-00.9	06.0	01.2	01.9	06.5	-01.0	-03.0	03.9	04.3	04.4	91	61	88	80	W	3	WSW	3	SSE	1	
MES.	VRED.	755.2	754.7	755.2	01.2	07.1	03.3	03.7	08.0	C	06.3	-02.6	04.1	04.5	04.4	82	61	77	73	1.6	2.2	1.9		

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1	756.1	757.4	760.2	-00.7	04.2	01.4	01.6	05.8	-01.6	-05.7	04.0	04.0	04.4	93	65	86	81	ESE	2	NNE	3	NNW	1
2	760.8	758.8	756.5	-00.6	00.8	00.6	00.4	02.2	-02.4	-02.4	04.2	04.5	04.7	96	93	98	96	NE	1	-	0	W	1
3	754.3	756.8	759.7	-00.6	-00.1	-00.2	-00.3	00.6	-00.8	-01.0	04.1	04.4	04.4	93	96	96	95	NE	2	N	1	W	1
4	762.7	764.6	765.5	-00.8	01.8	-01.0	-00.2	02.2	-01.1	-01.8	03.5	03.7	03.4	81	70	79	77	ESE	3	E	2	ESE	3
5	766.0	765.5	765.0	-00.1	01.2	-00.4	00.1	01.3	-01.6	-05.0	03.3	03.3	03.6	73	66	80	73	ESE	1	WSW	3	WSW	3
6	764.3	762.7	760.7	-01.2	03.1	-00.4	00.3	04.2	-01.2	-01.3	03.6	03.5	03.9	85	62	87	78	WSW	2	W	2	ESE	2
7	755.1	750.6	749.1	-02.7	04.4	04.3	03.1	07.0	-02.7	-04.7	03.1	03.9	04.6	82	54	74	70	ESE	1	WSM	3	W	3
8	752.0	755.6	758.2	00.1	00.9	-01.3	-00.6	04.3	-02.0	-00.6	03.7	02.3	02.3	80	46	58	61	NM	3	N	3	N	2
9	758.2	757.8	756.7	-00.4	01.2	-02.2	-02.4	02.0	-00.6	-03.5	02.3	02.4	02.7	80	49	70	66	SW	1	W	2	SSE	2
10	755.8	754.9	753.6	-04.0	06.3	00.8	01.0	07.2	-04.9	-08.7	02.5	03.1	03.4	74	44	69	62	SE	2	ESE	2	ESE	2
11	753.2	752.2	751.6	-00.7	11.5	06.7	06.0	12.3	-02.4	-07.0	03.2	04.1	04.7	73	40	63	59	SE	2	SW	3	SSW	2
12	749.8	746.9	747.7	05.8	11.0	08.9	08.6	11.5	04.0	-02.1	04.5	05.0	04.7	65	51	55	57	SE	2	SE	2	S	3
13	745.3	742.2	741.8	04.2	14.6	08.8	09.1	15.1	04.2	-02.0	04.4	05.1	04.8	71	41	57	56	SE	2	S	2	SE	3
14	740.7	741.1	742.8	07.0	07.8	06.9	07.2	08.8	06.1	-04.7	05.5	06.2	05.8	74	78	77	7						

Den	Vidljivost 0-9	Obločnost N (0-10)					(metri) sači- šljivo	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	7 00	09.0	10*	06.3	01.8	.	.	.	V ⁻¹ 10 ⁴⁵ * 10 ⁴⁵ 24, ■		
2	6 10	10	10	10.0	00.0	02.5	02	.	X ⁻¹ 0-1 ⁴⁵ 10 ⁴⁵ 24, ■		
3	5 10	10	10	10.0	00.0	.	02	.	= 20-24, ■		
4	6 10	08.0	00	06.0	00.7	.	01	.	= 20-1 ⁴⁵ 15 ⁴⁵ 24; = 1 ⁴⁵ 5 ⁴⁵ ; = 20 ⁴⁵ 24, ■		
5	7 06	06	10	07.3	02.5	.	.	.	= 20-4 ⁴⁵ , = 10-9 ⁴⁵		
6	7 07	00.0	00	02.3	05.4	.	.	.	= 23 ⁴⁵ 24		
7	7 00	02.0	09	03.7	07.7	.	.	.	= 0-9 ⁴⁵ 23 ⁴⁵ 24		
8	7 10*	10*	10	10.0	00.0	02.7	.	.	* 0-42, F _N 12 ⁴⁵ X ⁻¹ 12 ⁴⁵ 14 ⁴⁵ X ⁻¹ 14 ⁴⁵ 14 ⁴⁵ , = 14 ⁴⁵ 24		
9	6 00	07	00	02.3	03.9	11.5	.	.	= 0-14 ⁴⁵ , = 12 ⁴⁵ 8 ⁴⁵ 20 ⁴⁵ 24		
10	8 00	04.0	00	01.3	07.4	.	.	.	= 20-10 ⁴⁵ , = 10 ⁴⁵ 24		
11	8 00	00.0	00	00.0	07.9	.	.	.	= 0-10 ⁴⁵ 19 ⁴⁵ 24		
12	7 04	10	06	06.7	00.6	.	.	.	= 0-0-9 ⁴⁵		
13	7 06	05.0	00	04.3	04.7	.	.	.	= 0-8 ⁴⁵ 20 ⁴⁵ 24		
14	7 00	00.0	00	00.0	07.4	.	.	.	= 0-10 ⁴⁵ 24 ⁴⁵ 24		
15	7 00	00.0	00	00.0	08.0	.	.	.	= 0-0-9 ⁴⁵ 24 ⁴⁵ 24		
16	8 00	00.0	00	00.0	07.6	.	.	.	F _{SE} 0 ⁴⁵ 5 ⁴⁵ 9 ⁴⁵		
17	7 00	03.0	00	01.0	07.3	.	.	.	= 0-2 ⁴⁵ , = 0-1 ⁴⁵ 10 ⁴⁵ 24		
18	6 02	02.0	00	01.3	07.5	.	.	.	F _{SE} 0 ⁴⁵ , = 20 ⁴⁵ 24		
19	8 00	00.0	00	00.0	07.9	.	.	.	= 0-10 ⁴⁵ , = 21 ⁴⁵ 24		
20	6 03	04.0	00	02.3	06.3	.	.	.	= 0-0-10 ⁴⁵ , = 21 ⁴⁵ 24; = 0-2 ⁴⁵ 24		
21	6 04	00.0	03	02.3	07.0	.	.	.	= 0-4-10, = 10 ⁴⁵ 24, = 0-0-24, F _{SE} 10 ⁴⁵		
22	6 10	07	10	09.0	00.0	.	.	.	= 0-9 ⁴⁵ , = 0-5, = 14 ⁴⁵ 24		
23	6 10	10.0	07	09.0	02.8	.	.	.	= 0-2 ⁴⁵ , = 20 ⁴⁵		
24	7 09	09.0	10	09.3	05.7	.	.	.			
25	7 00	02.0	00	00.7	06.2	.	.	.			
26	7 10*	08	10	09.3	01.2	00.3	.	.	= 0-45, = 0-9 ⁴⁵ 10 ⁴⁵		
27	8 00	02.0	00	00.7	07.8	00.4	.	.	= 2-6 ⁴⁵		
28	8 10*	10.0	10.0	10.0	00.0	00.0	.	.	F _{SE} 0 ⁴⁵ , = 16 ⁴⁵ , = 0-6 ⁴⁵ 7 ⁴⁵ 9 ⁴⁵ 21 ⁴⁵ ; = 21 ⁴⁵ 24		
29	7 10	10.0	10.0	10.0	02.5	04.9	.	.	= 0-0-45, = 0-2-10 ⁴⁵ , = 0-13 ⁴⁵ 21 ⁴⁵		
30	7 01	05.0	10	05.3	07.8	03.3	.	.	= 0-3 ⁴⁵ , F _{NW} 11 ⁴⁵ , = 21 ⁴⁵ 24		
31	7 00	00.0	00	00.0	07.1	.	.	.	= 0-0-45, = 0-14 ⁴⁵ 9 ⁴⁵ , = 24 ⁴⁵ 24		
MES. VR _{ED}		04.3	04.9	04.4	04.5	144.7	25.6				

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1	7 00	06.0	10	05.3	04.9	.	.	.	= 0-10 ⁴⁵		
2	4 15	10	10*	10.0	00.0	.	.	.	= 0-0-24, = 0-24, ■		
3	6 10*	10*	10*	10.0	00.0	02.0	J1	.	* 0-10-24, = 0-24, ■		
4	7 10	00.0	00	03.3	07.0	03.6	04	.	* 0-3 ⁴⁵ , = 4 ⁴⁵ , F _{SE} 6 ⁴⁵ , = 10 ⁴⁵ , ■		
5	7 10	09	09	09.3	00.0	.	02	.	■		
6	7 10	00.0	00	03.3	05.6	.	01	.	= 2-20 ⁴⁵ 24, ■		
7	7 00	00.0	05	01.7	06.6	.	.	.	= 0-9 ⁴⁵ , = 24 ⁴⁵ 22 ⁴⁵		
8	7 10*	04.0	00	05.3	03.3	00.0	.	.	F _N -NW 4 ⁴⁵ , = 7 ⁴⁵ , = 16 ⁴⁵ ; * 0-16 ⁴⁵ 9 ⁴⁵ , ■		
9	8 00	00.0	00	00.0	06.6	01.4	.	.	= 0-3 ⁴⁵ , = 5 ⁴⁵ , = 10 ⁴⁵ 10 ⁴⁵		
10	8 00	00.0	00	00.0	08.8	.	.	.	= 0-0-6 ⁴⁵		
11	8 00	00.0	02	00.7	06.8	.	.	.	= 0-9 ⁴⁵ 23 ⁴⁵ 24, = 20 ⁴⁵ 23 ⁴⁵		
12	8 10	09	09	09.3	00.3	.	.	.	= 0-10 ⁴⁵		
13	8 02	03.0	06	04.3	08.6	.	.	.	= 0-3 ⁴⁵ , = 6 ⁴⁵		
14	7 09	10	09	09.3	00.0	00.1	.	.	* 0-3 ⁴⁵ , = 5 ⁴⁵ , = 10 ⁴⁵ 10 ⁴⁵		
15	8 09	06	00	05.0	02.4	01.6	.	.	*		
16	7 09	10.0	10	09.7	00.0	.	.	.	F _N -ESE 6 ⁴⁵ , = 9 ⁴⁵ , = 14 ⁴⁵ , = 0-13 ⁴⁵ 15 ⁴⁵ , = 0-15 ⁴⁵ 15 ⁴⁵ , ■		
17	8 04	04.0	00	02.7	05.1	00.0	.	.	= 0-4 ⁴⁵ , = 8 ⁴⁵		
18	8 00	00.0	00	00.0	09.3	.	.	.	F _{SE} 0 ⁴⁵ , = 10 ⁴⁵ , = 20 ⁴⁵ 24		
19	8 00	00.0	10	03.3	08.4	.	.	.	= 0-0-45, F _{SE} 2 ⁴⁵ , = 21 ⁴⁵		
20	7 10	10	10*	10.0	00.0	.	.	.	F _{SE} 0 ⁴⁵ , = 3 ⁴⁵ , = 20 ⁴⁵ , = 22 ⁴⁵		
21	7 10*	07.0	09	08.7	02.6	00.0	.	.	* 0-2 ⁴⁵ , = 3 ⁴⁵ , = 18 ⁴⁵ ; = 0-4 ⁴⁵ , = 4 ⁴⁵ , = 5 ⁴⁵ , = 7 ⁴⁵ , = 22 ⁴⁵ , = 7 ⁴⁵ , = 8 ⁴⁵ , F _E 12 ⁴⁵ , = 14 ⁴⁵		
22	7 02	02.0	00	01.3	09.0	00.2	.	.	= 0-3 ⁴⁵ , = 9 ⁴⁵		
23	7 00	00.0	00	00.0	08.9	.	.	.	= 0-0-2 ⁴⁵		
24	7 02	06.0	05	04.3	05.5	.	.	.	= 0-4 ⁴⁵ , = 9 ⁴⁵		
25	7 10	05.0	10	08.3	02.3	.	.	.			
26	7 04	09	02	05.0	06.3	.	.	.	F _N -NW 5 ⁴⁵ , = 21 ⁴⁵ ; * 0-11 ⁴⁵ , = 12 ⁴⁵ , = 16 ⁴⁵ , = 17 ⁴⁵ ; F _N 14 ⁴⁵ , = 18 ⁴⁵		
27	8 05	04.0	00	03.6	09.0	00.0	.	.			
28	8 00	06.0	00	02.0	07.8	.	.	.			
MES. VR _{ED}		05.2	04.7	04.6	04.8	141.8	08.9				

$\varphi = 44^\circ 48' N \lambda = 20^\circ 28' E$ Gr. $\Delta G = + 1h 22 min.$

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5 0	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D. f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	754.1	753.6	752.4	-00.5	12.3	05.8	05.8	13.6	-01.7	-07.0	02.7	02.2	02.9	60	21	42	41	SSW 2	WSW 2	ESE 2	
2	752.2	751.8	751.2	02.2	16.5	10.3	09.8	17.0	01.2	-04.2	02.7	03.8	04.1	51	27	43	40	SSE 1	SW 2	SE 2	
3	751.2	749.7	748.3	05.4	16.8	11.0	11.0	18.0	05.2	-01.2	04.7	05.1	04.4	69	36	45	50	SE 1	NNE 2	NE 2	
4	748.2	747.0	746.9	05.6	16.4	09.9	10.4	17.5	04.3	-01.5	04.9	04.7	04.7	72	34	51	52	WSW 2	SW 2	SE 2	
5	747.9	747.9	749.9	09.6	18.5	14.4	14.2	19.6	08.5	02.4	04.4	04.7	06.6	49	30	53	44	ESE 2	S 2	NNW 1	
6	753.0	752.2	751.7	10.0	17.5	14.2	14.0	18.2	09.1	02.1	05.4	05.1	04.8	59	34	40	44	SSW 2	NE 2	ESE 3	
7	751.3	750.4	750.4	12.2	18.7	13.3	14.4	19.2	11.0	06.7	05.6	06.2	06.1	53	38	54	48	S 2	E 2	ESE 2	
8	749.7	748.5	746.9	12.4	23.0	14.6	16.2	24.1	12.1	07.9	05.2	03.5	04.4	48	17	36	34	ESE 2	NM 2	E 2	
9	743.3	740.7	739.5	13.1	21.6	14.8	16.1	22.1	12.5	06.7	05.2	03.9	05.3	46	20	42	36	SE 3	SE 3	SSE 4	
10	739.1	738.9	740.7	10.4	19.8	13.3	14.2	20.0	10.4	08.0	06.6	05.6	05.6	70	32	49	50	ESE 4	ESE 4	ESE 3	
11	745.6	747.5	749.8	11.2	19.5	13.6	14.5	20.0	10.6	08.0	06.3	06.2	06.2	64	36	53	51	SE 1	SSW 2	SSW 2	
12	749.0	744.8	747.0	09.2	21.5	13.2	14.3	21.9	08.5	01.8	05.6	04.7	04.5	64	24	40	43	ESE 3	ESE 3	MSW 2	
13	746.7	746.9	746.7	11.2	17.2	13.6	13.9	17.5	09.6	02.7	05.2	04.0	04.2	52	27	36	38	SSE 2	SW 2	ESE 3	
14	744.2	744.0	746.8	10.5	11.5	07.7	09.4	14.1	07.3	06.0	06.0	05.9	07.3	63	58	92	71	ESE 5	E 6	ESE 5	
15	749.1	749.1	748.9	06.6	13.8	08.2	09.2	14.7	06.5	05.0	05.6	07.3	06.0	77	62	74	71	ESE 2	E 4	ESE 4	
16	748.2	746.4	745.4	07.0	15.7	11.1	11.2	16.0	06.9	04.3	05.7	05.6	06.1	76	42	61	60	ESE 3	NW 1	SE 2	
17	744.9	743.3	744.0	07.2	14.7	08.2	09.6	16.2	06.3	02.4	06.7	04.3	06.8	88	34	84	69	SSW 2	WSW 3	NNE 2	
18	745.0	745.0	746.5	05.8	15.6	11.0	10.8	16.2	05.6	01.5	06.6	05.3	06.2	96	40	63	66	SE 2	ESE 3	ESE 3	
19	747.1	745.9	745.2	09.2	16.5	12.8	12.8	16.7	08.8	06.3	05.5	05.2	06.1	63	37	55	52	ESE 4	ESE 4	ESE 4	
20	744.0	744.2	745.4	09.7	18.1	11.6	12.8	18.7	09.5	08.0	06.0	07.0	08.0	66	45	78	63	ESE 4	ESE 2	MSW 2	
21	745.2	747.3	750.4	07.0	06.0	04.6	05.6	11.6	04.5	06.2	05.7	04.8	02.6	76	69	41	62	N 3	NNW 3	N 3	
22	751.8	750.0	748.6	-01.0	01.5	01.4	00.8	04.6	-01.0	-01.0	03.1	03.8	04.0	72	75	78	75	WSW 2	WSW 1	E 2	
23	745.2	743.8	743.6	00.4	03.9	02.7	02.4	04.2	00.2	00.0	04.4	04.3	04.4	93	72	79	81	E 3	SE 3	E 2	
24	741.0	740.5	740.7	02.4	03.5	03.2	03.1	04.0	01.6	-00.5	04.6	05.2	05.4	84	88	94	89	SE 2	E 2	W 3	
25	741.8	742.4	744.4	02.3	08.4	03.4	04.4	08.8	01.9	01.7	05.1	04.0	05.1	95	48	88	77	W 3	W 2	W 3	
26	747.0	746.6	744.0	00.6	09.6	07.0	06.0	10.8	00.0	-01.1	04.1	02.6	03.0	86	30	40	52	W 2	NNW 2	SSE 3	
27	744.2	744.0	742.9	07.8	14.9	11.5	11.4	15.6	06.0	01.7	03.4	05.3	05.0	42	42	49	44	SSE 2	ESE 3	S 3	
28	741.0	741.2	740.1	09.4	09.5	11.4	10.4	12.5	09.0	06.6	05.2	07.7	07.0	59	87	69	72	SE 3	SE 3	SE 3	
29	739.8	743.8	745.0	12.0	09.6	07.6	09.2	18.1	07.6	08.3	06.4	06.9	06.6	61	77	85	74	SSE 4	NM 3	ENE 1	
30	743.5	741.3	739.8	13.6	15.8	17.0	15.8	18.0	06.5	01.7	06.7	07.4	07.0	58	55	48	54	SE 3	ESE 3	SE 4	
31	739.0	737.9	743.8	15.9	26.5	17.0	19.1	26.7	15.0	12.5	07.5	06.6	07.1	55	26	49	43	SE 4	S 4	NW 2	
MES.	VREO.	746.2	745.7	746.0	07.7	14.6	10.3	10.7	16.0	06.6	03.3	05.2	05.1	05.4	67	44	58	56	2.6	2.6	2.6

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1	746.4	746.9	750.2	08.4	07.9	05.7	06.9	17.0	05.7	05.8	07.6	06.9	06.0	92	86	87	88	NNE 3	NW 3	NM 3
2	747.5	745.3	744.6	05.3	06.3	07.1	06.4	07.4	05.0	04.7	06.5	06.7	06.8	97	93	89	93	N 2	NW 2	SSW 2
3	743.6	744.3	746.9	07.4	13.2	09.3	09.8	15.0	06.8	06.0	07.1	06.6	06.2	92	58	70	73	SE 1	WSW 2	ESE 2
4	748.7	749.3	750.2	10.5	18.4	14.0	14.2	20.2	08.8	03.0	05.7	05.7	06.1	59	36	51	49	SSE 3	SSE 3	ESE 1
5	750.5	750.4	751.2	12.0	22.0	20.0	18.5	22.4	10.2	02.8	05.0	05.9	05.8	48	30	33	37	ESE 3	SE 4	SE 2
6	751.6	749.5	748.2	17.7	26.4	22.7	22.9	28.6	16.5	11.5	05.9	05.4	05.8	39	12	28	29	SE 3	S 3	SE 3
7	746.2	744.5	743.6	20.8	22.8	22.6	22.2	25.7	20.0	15.5	05.9	06.3	06.1	32	30	29	30	SE 4	SE 3	S 3
8	744.0	745.5	747.9	11.7	09.8	08.0	09.4	23.2	08.0	05.5	07.8	08.2	07.5	76	90	94	87	W 2	NW 3	SE 1
9	749.7	748.8	747.4	08.4	16.2	12.4	12.8	19.0	06.0	00.2	06.1	04.9	06.0	74	31	56	54	SE 2	WSW 2	E 2
10	744.4	738.2	737.9	10.2	18.0	13.0	13.6	20.6	09.6	02.4	08.4	07.9	09.0	90	51	80	74	SE 3	E 4	SSE 3
11	743.9	749.0	751.4	05.0	04.0	03.5	03.0	13.1	03.1	04.6	05.0	05.6	04.2	76	92	63	77	WSW 5	W 4	NNW 2
12	752.6	752.2	751.7	04.8	10.2	07.4	07.4	11.4	03.6	-01.2	04.6	03.8	04.9	71	40	63	58	W 2	WSW 3	SSE 2
13	751.2	750.2	749.8	08.4	16.4	11.6	12.0	17.0	06.5	04.3	04.8	04.8	07.6	59	34	75	56	W 2	W 3	NW 2
14	753.0	751.9	749.6	08.8	11.4	06.6	08.8	13.1	06.4	05.9	04.8	06.4	06.9	65	64	82	70	N 3	NE 2	ESE 2
15	747.4	744.7	742.3	12.5	21.2	14.7	15.8	22.2	06.8	02.5	07.3	06.0	07.3	67	32	58	52	WSW 2	NNW 2	ESE 2
16	742.4	741.8	744.3	13.1	18.2	12.9	14.3	19.5	11.1	05.6	07.4	06.7	08.8	66	43	79	63	ESE 1	NW 2	NW 2
17	747.4	746.0	749.4	10.9	13.6	12.0	12.1	14.8	10.6	09.0	07.4	07.7	06.9	76	66	66	69	NW		

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 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Dan	Vrijeme 0-9 0	Oblačnost N (0-10)					Temperatura zraka °C	Padavina R mm	Snožni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 00	00 0	00	00	00.0	09.5	•	•	•	•
2	8 00	06 0	00	02.0	09.2	•	•	•	•	•
3	7 06	07 0	00	04.3	07.4	•	•	•	•	•
4	7 05	06 0	00	03.7	06.7	•	•	•	•	•
5	8 04 0	02 0	07	04.3	08.8	•	•	•	•	•
6	8 02 0	06 0	06	04.7	07.2	•	•	•	•	•
7	8 10	10	10	10.0	01.6	•	•	•	•	•
8	8 09	05 0	00	04.7	05.5	•	•	•	•	•
9	8 09	04 0	02	05.0	08.2	•	•	•	•	•
10	8 05	02 0	00	02.3	09.3	•	•	•	•	•
11	8 09	05 0	05	06.3	05.2	•	•	•	•	•
12	8 03 0	07 0	00	03.3	05.2	•	•	•	•	•
13	8 05	10	10	08.3	01.6	00.2	•	•	•	•
14	8 09	09	10 0	09.3	03.1	00.0	•	•	•	•
15	8 05	05 0	00	03.3	06.8	10.7	•	•	•	•
16	8 00 0	06 0	00	02.0	07.0	•	•	•	•	•
17	8 07 0	06 0	10	07.7	07.3	00.0	•	•	•	•
18	8 00 0	04 0	00	02.0	08.1	11.2	•	•	•	•
19	8 07	09	09	06.3	01.6	•	•	•	•	•
20	8 04 0	05 0	05	04.7	07.2	•	•	•	•	•
21	7 08	10 0	10	09.7	00.0	•	•	•	•	•
22	7 10	10 0	09	09.7	00.0	01.1	•	•	•	•
23	7 10 0	10 0	09	09.7	00.0	03.6	03	•	•	•
24	7 10	10	10 0	10.0	00.0	00.4	•	•	•	•
25	7 10	08	03	07.0	04.3	01.4	•	•	•	•
26	8 04 0	04 0	00	02.7	08.2	00.2	•	•	•	•
27	8 10	09	09	08.0	00.5	•	•	•	•	•
28	7 09	10 0	10	09.7	00.0	00.0	•	•	•	•
29	7 06	10	05	07.0	01.7	09.8	•	•	•	•
30	8 10	10	10	10.0	00.0	•	•	•	•	•
31	8 03 0	09	03	09.0	07.4	•	•	•	•	•
MES. VRED.	04.1	07.0	04.8	06.0	149.4	38.6				

1	7 10 0	10 0	10	10.0	00.0	00.0	•	•	•	•
2	6 10 0	10	10	10.0	00.0	02.3	•	•	•	•
3	7 10	06 0	03	06.3	06.0	04.3	•	•	•	•
4	8 04 0	07 0	00	04.3	06.1	03.7	•	•	•	•
5	8 09	04 0	10	07.7	06.3	•	•	•	•	•
6	8 10	06 0	10	06.7	05.3	•	•	•	•	•
7	8 10	10	06	08.7	00.6	•	•	•	•	•
8	7 05 0	10 0	00	05.0	04.6	•	•	•	•	•
9	8 00 0	00 0	00	00.0	11.5	05.6	•	•	•	•
10	7 10 0	09 0	10 0	09.7	02.1	03.4	•	•	•	•
11	6 10 0	10 0	06	06.7	00.0	06.5	•	•	•	•
12	8 00	09	04	07.3	05.8	04.0	•	•	•	•
13	8 00	06 0	10 0	08.3	05.1	•	•	•	•	•
14	8 10	04 0	01	05.0	05.3	02.5	•	•	•	•
15	8 00 0	00 0	00	00.0	11.8	•	•	•	•	•
16	8 07	10	09	06.7	02.5	•	•	•	•	•
17	8 10	10	10	10.0	00.0	•	•	•	•	•
18	8 07	10	08	06.3	01.7	00.0	•	•	•	•
19	8 03 0	06 0	09	06.0	09.8	•	•	•	•	•
20	7 08 0	02 0	00	00.7	11.1	•	•	•	•	•
21	8 00 0	00 0	00	00.0	11.9	•	•	•	•	•
22	8 00	04 0	10 0	06.3	04.2	•	•	•	•	•
23	8 06	09	10	08.3	04.0	00.0	•	•	•	•
24	7 10 0	10	10	10.0	00.0	00.0	•	•	•	•
25	7 09	10	09	09.3	03.3	00.0	•	•	•	•
26	7 10	07 0	07	06.0	03.5	00.2	•	•	•	•
27	7 06 0	10	10	06.7	00.8	00.7	•	•	•	•
28	8 04 0	10	00	04.7	09.6	00.0	•	•	•	•
29	8 00 0	00 0	00	00.0	12.0	•	•	•	•	•
30	8 00 0	00 0	00	00.0	12.3	•	•	•	•	•
MES. VRED.	04.6	04.7	03.7	04.4	148.0	42.4				

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 $\varphi = 44^\circ 48' N \lambda = 20^\circ 28' E$ Gr. $\Delta G = + 1h 22 min.$

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GD	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	751.7	751.7	752.6	10.8	23.0	15.2	16.0	23.0	07.2	02.0	05.6	06.8	09.2	58	33	71	54	WSW 2	NM 3	NM 1	
2	752.6	751.4	749.8	10.3	10.3	12.6	11.4	15.2	10.2	09.4	08.5	08.4	10.0	91	89	91	90	WNW 3	W 3	NNW 2	
3	748.2	747.6	747.3	11.4	12.6	10.8	11.4	14.3	10.8	10.2	09.0	09.4	08.9	89	86	92	89	NM 2	W 3	SSW 1	
4	748.6	749.7	750.3	11.6	15.1	11.6	12.5	19.0	07.6	03.2	09.0	10.0	09.3	88	78	91	86	WSM 1	NM 2	SE 1	
5	751.5	751.5	752.4	12.4	21.6	14.6	15.8	22.3	09.0	05.2	09.3	09.0	09.2	86	46	74	69	S 1	WSW 2	NE 1	
6	752.4	750.7	750.1	15.6	23.2	19.3	19.4	24.1	10.5	05.8	09.8	09.0	09.1	74	42	54	57	ESE 1	ESE 2	N 1	
7	749.6	747.9	747.3	17.9	26.2	20.4	21.2	26.4	14.5	10.1	10.9	11.5	12.4	71	45	69	62	SE 2	ESE 3	ESE 3	
8	746.0	744.2	745.4	17.7	24.5	15.2	18.2	25.0	15.2	14.0	11.6	11.8	11.6	76	51	90	72	SE 2	SE 5	ESE 2	
9	746.6	748.0	748.8	15.2	17.5	14.7	15.3	19.4	13.4	10.5	12.2	09.1	10.5	94	61	84	80	SM 2	W 1	SE 2	
10	750.7	751.3	749.3	13.2	21.1	14.4	15.8	22.0	09.5	06.1	08.7	08.6	09.3	77	46	76	66	WSW 2	ESE 2		
11	749.8	747.1	746.0	16.2	22.8	15.2	17.4	23.4	10.0	06.5	09.3	07.7	09.6	67	37	74	59	S 1	NE 2	ESE 1	
12	743.7	742.7	742.3	17.6	26.0	19.4	20.6	26.1	12.6	08.2	08.7	08.8	10.1	58	35	60	51	ESE 3	ESE 3	E 3	
13	742.9	741.7	741.6	18.6	25.2	19.0	20.4	25.4	17.0	15.2	12.1	10.4	09.9	75	43	60	59	ESE 2	ESE 3	ESE 3	
14	741.3	741.7	742.5	15.3	17.8	15.3	15.9	19.0	15.0	11.3	12.4	11.0	11.6	95	72	89	85	WSW 2	ESE 3	ESE 3	
15	744.9	745.1	745.4	13.2	21.7	18.9	18.2	22.2	12.2	08.9	10.6	12.5	12.0	93	64	74	77	W 2	W 3	W 3	
16	745.8	745.8	746.9	16.5	21.9	20.2	19.7	26.0	15.8	14.8	11.9	17.4	12.2	85	88	69	81	WSM 3	S 2	SE 1	
17	746.5	749.0	750.4	18.2	22.5	17.7	19.0	26.0	16.0	12.0	12.5	13.2	11.4	80	65	75	73	WSM 2	S 2	W 1	
18	752.1	752.3	753.0	16.7	25.6	17.6	19.4	26.5	13.0	10.0	11.2	12.7	13.8	78	52	91	74	SSW 2	W 2	SE 1	
19	752.2	753.2	752.4	18.4	27.2	19.8	21.3	27.8	14.1	10.4	13.0	11.3	12.0	82	42	69	64	NNW 1	SE 2	SE 2	
20	752.0	749.9	750.8	20.9	27.5	16.8	20.5	28.0	14.9	11.1	13.0	11.8	11.9	70	43	63	65	W 1	WSW 2	S 2	
21	751.0	750.2	749.8	16.3	26.0	19.2	20.2	26.0	13.6	11.0	11.6	10.0	12.0	84	40	72	65	WSW 3	NW 2	ESE 2	
22	749.5	747.6	748.4	19.4	27.8	17.5	20.6	28.2	14.2	10.0	11.1	10.6	13.0	66	38	87	64	SE 2	SE 2	WNW 2	
23	747.0	745.4	747.1	19.2	26.0	16.2	19.4	27.6	14.6	11.5	11.5	11.6	13.0	69	46	94	70	SSE 2	ESE 2	WSM 3	
24	747.1	746.2	745.1	14.7	18.8	17.8	17.3	19.7	14.7	14.5	10.9	12.1	14.4	87	74	94	85	N 1	ENE 2	S 2	
25	746.6	747.0	747.0	15.8	21.8	18.8	18.8	23.1	15.4	15.0	12.5	12.1	13.1	93	62	80	78	WSW 2	NNE 2	N 2	
26	748.8	748.4	749.2	16.6	23.0	14.9	17.4	23.3	14.9	14.5	12.4	12.7	12.2	87	60	96	81	N 2	NNE 3	WSM 2	
27	746.8	746.3	748.3	15.3	21.0	16.0	17.1	21.2	14.4	10.4	12.6	12.0	12.3	97	64	90	84	S 1	WSW 2	WSW 2	
28	748.1	748.4	749.7	14.7	19.3	14.8	15.9	20.8	14.1	13.9	11.8	12.4	12.2	94	74	97	88	WSM 1	W 2	WSW 2	
29	749.9	748.7	748.4	15.5	23.2	20.3	19.8	24.6	14.4	13.0	12.0	12.1	13.4	91	57	75	74	WSM 2	SSW 2	ESE 3	
30	745.6	745.6	745.1	20.6	23.0	20.6	21.2	25.2	16.6	13.0	11.9	11.5	13.2	65	55	72	64	SE 2	S 3	SSE 2	
31	746.8	746.7	745.3	18.3	25.0	19.7	20.7	26.0	15.0	13.0	11.5	12.1	14.5	73	51	84	69	S 1	NNE 2	E 3	
MES.	VRED.	748.5	747.9	747.9	15.9	22.2	16.9	18.0	23.4	13.2	10.5	10.9	11.0	11.5	80	56	80	72	1.8	2.4	2.0

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1	747.3	746.2	745.1	18.4	25.2	21.0	21.4	25.8	15.4	12.8	11.9	10.8	11.8	75	45	63	61	S 1	ESE 3	ESE 2
2	744.6	744.9	745.5	21.2	20.9	17.0	19.0	24.8	16.6	13.1	13.9	11.5	12.4	73	62	86	74	MNE 1	NE 3	N 1
3	746.3	745.6	744.8	13.2	16.4	15.6	15.2	17.0	13.0	10.5	11.0	12.4	12.5	97	88	94	93	MNE 2	N 2	MSW 2
4	747.0	747.9	748.9	11.7	15.7	14.0	13.8	16.1	11.4	11.1	10.0	08.8	10.2	96	66	85	82	WNW 3	W 3	NNW 3
5	750.6	750.7	751.1	10.6	15.0	12.0	12.4	15.7	10.6	10.2	07.7	07.8	07.6	80	61	73	71	WNW 3	NW 3	N 2
6	751.1	751.4	752.3	11.4	16.4	12.6	13.2	17.4	09.5	08.8	06.8	07.0	07.1	67	50	65	61	NNW 2	N 3	N 2
7	750.7	749.9	748.6	11.5	12.5	12.9	12.4	12.9	10.5	09.2	07.1	08.2	08.9	70	75	80	75	NNW 3	WSM 3	
8	744.3	747.0	748.7	10.6	11.6	11.0	11.0	12.9	10.5	10.3	09.1	09.5	09.6	95	93	98	95	W 3	SSW 3	SSW 2
9	748.6	748.4	747.9	13.0	18.5	14.8	15.3	19.5	10.7	10.0	09.9	09.1	11.0	88	57	87	77	SE 2	SSW 2	ESE 2
10	747.4	746.9	747.7	15.3	23.3	18.3	18.8	24.4	11.2	07.2	10.3	08.1	12.8	79	38	81	66	MNE 1	SSW 1	ESE 2
11	749.6	750.8	751.4	15.3	22.5	17.0	18.0	23.2	14.6	13.5	11.7	12.8	13.4	90	63	92	82	WSM 2	HSM 2	ESE 1
12	752.4	751.4	750.6	18.3	25.7	19.6	20.8	26.2	13.4	11.1	12.0	12.8	15.0	75	52	88	72	- 0	M 2	ESE 1
13	750.7	749.0	748.4	19.7	25.7	17.5	20.1	26.0	16.8	14.6	13.0	15.5	14.4	76	63	96	78	ESE 3	ESE 3	ENE 1
14	747.9	746.6	747.9	19.0	26.1	22.1	22.3	26.6	16.3	15.7	14.4	14.5	15.1	87	57	76	73	SW 2	SW 2	SW 2
15	748.4	748.0	746.6	20.8	27.7	23.3	23.8	28.8	17.0	14.3	14.5	14.0	12.8	79	50	60	63	S 1	ENE 2	ESE 2
16	746.8	745.7	744.2	24.0	30.1	25.2	26.1	30.7	20.5	16.8	13.7	12.5	10.7	61	39	45	48	ESE 2	S 3	S 3
17	746.3	746.1	747.8	21.6	27.3	21.2	22.8	27.9	18.8	17.2	13.4	12.8	13.0	69	47	62	62	NE 1	WSM 2	WSM 3
18	747.9	747.3	749.0	19.4	26.5	19.5	21.2	27												

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$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_x = 1.2 \text{ m}$$

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1	8	07 0	09 0	05	07.0	06.5	04.7	.	$\Delta^0 22^{\circ} 24$
2	8	04 0	05 0	08	05.7	07.1	.	$\Delta^0 0^{\circ} 8^{\circ} 18^{\circ} 15^{\circ} 16^{\circ} 8^{\circ} 2^{\circ} 15^{\circ} 16^{\circ}$	
3	6	10 0	10 0	09	09.7	00.0	15.5	.	$\Delta^0 1^{\circ} 1^{\circ} 4^{\circ} 4^{\circ} 1^{\circ} 12^{\circ} 18^{\circ} 18^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 2^{\circ} 2^{\circ} 2^{\circ} 2^{\circ} 2^{\circ} 2^{\circ}$
4	7	10 0	09	10 0	09.7	01.4	05.3	.	$\Delta^0 1^{\circ} 8^{\circ} 8^{\circ} 0^{\circ} 1^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}, \Delta^0 4^{\circ} 2^{\circ} 5^{\circ} 1^{\circ} 1^{\circ} 13^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
5	7	10 0	10 0	10 0	10.0	06.6	04.0	.	$\Delta^0 1^{\circ} 3^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 17^{\circ} 1^{\circ} 17^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
6	7	09	09	00	06.0	04.9	12.9	.	$\Delta^0 0^{\circ} 3^{\circ} 2^{\circ} \Delta^0 0^{\circ} 3^{\circ} 2^{\circ} 1^{\circ}, \Delta^0 8^{\circ} 2^{\circ} 9^{\circ} 5^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
7	8	10	10	10	10.0	00.0	.	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
8	6	10 0	10	10 0	10.0	00.0	07.8	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
9	7	10	10	10	10.0	01.5	06.0	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
10	8	08 0	04 0	09	07.0	10.4	00.2	.	$\Delta^0 0^{\circ} 1^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
11	7	09	07 0	00	05.3	04.4	00.3	.	$\Delta^0 0^{\circ} 0^{\circ} 3^{\circ} 1^{\circ}, \Delta^0 7^{\circ} 2^{\circ} 11^{\circ} 3^{\circ}, \Delta^0 0^{\circ} 1^{\circ} 8^{\circ} 2^{\circ} 8^{\circ} 5^{\circ}$
12	8	00 0	04 0	02	02.0	10.7	06.6	.	$\Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
13	8	07	05 0	10 0	07.3	04.9	.	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
14	7	07 0	02 0	04	05.0	11.3	21.0	.	$\Delta^0 0^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
15	8	00 0	02 0	00	00.7	12.1	.	.	$\Delta^0 0^{\circ} 2^{\circ} 0^{\circ} 0^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
16	8	00 0	01 0	07	02.7	10.9	.	.	$\Delta^0 0^{\circ} 2^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ} 0^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
17	8	08	06 0	10 0	06.0	07.6	00.0	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
18	8	04 0	06 0	10 0	06.7	07.7	03.2	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
19	7	10	10 0	10	10.0	00.0	07.0	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
20	7	10	07 0	10	09.0	00.9	03.6	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
21	7	10 0	10 0	09	09.7	05.2	05.0	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
22	8	06 0	06 0	04	05.3	07.2	00.0	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
23	8	04 0	04 0	04	04.0	11.1	.	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
24	8	02 0	02 0	06	04.0	13.0	.	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
25	8	05 0	06 0	09	06.7	10.8	.	.	$\Delta^0 0^{\circ} 2^{\circ} 3^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}$
26	8	10 0	07	00	05.7	07.4	01.7	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
27	8	00 0	03 0	00	01.0	12.7	00.0	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
28	8	00 0	05 0	00	01.7	12.7	.	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
29	8	10	05 0	00	05.0	09.5	00.4	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$
30	8	05 0	04 0	02	03.7	08.6	00.0	.	$\Delta^0 0^{\circ} 0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, \Delta^0 2^{\circ} 2^{\circ} 2^{\circ} 1^{\circ}$

1975 JUL

BEOGRAD

 $\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = +1h\ 22\ min.$

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d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	741.3	742.5	742.4	15.8	13.0	14.5	14.4	16.6	12.7	12.5	12.9	10.6	11.1	96	94	90	93	N	2	SSW 4	WSW 3	
2	741.6	741.9	742.9	12.4	14.1	14.0	13.6	14.8	12.2	11.8	09.7	11.6	11.1	90	96	93	93	WSW 3	SSW 3	NW 1		
3	744.9	746.2	747.5	14.2	22.9	18.0	16.3	23.8	12.7	10.1	11.4	13.0	14.6	94	62	94	83	MSW 2	MNW 2	SM 1		
4	747.6	746.8	745.6	19.0	27.0	20.0	21.5	27.6	16.0	12.2	13.5	12.0	14.9	82	45	85	71	MSW 2	MNW 2	ESE 1		
5	744.5	744.1	745.0	20.0	26.3	21.2	22.2	27.1	16.5	15.5	14.9	17.3	15.1	85	68	80	78	S 2	NNE 1	WSW 3		
6	746.4	747.0	748.1	18.0	22.8	19.6	20.0	24.1	16.4	16.0	14.2	14.4	15.0	92	69	88	83	-	0	MNW 1	WNW 1	
7	750.2	750.5	750.8	17.2	23.6	18.8	19.6	25.0	17.1	16.1	14.0	15.3	14.9	95	70	92	86	MSW 2	MSW 2	ESE 2		
8	751.7	751.6	751.6	18.5	26.1	20.2	21.2	27.0	16.2	13.5	14.5	12.8	13.6	91	50	77	73	MNW 2	NW 2	ENE 1		
9	752.0	751.9	751.5	21.0	27.3	20.2	22.2	28.4	15.8	12.6	14.0	12.0	12.8	75	44	72	64	-	0	N 2	E 2	
10	751.1	750.1	748.7	21.8	29.3	23.8	24.7	29.6	15.8	12.8	13.6	13.2	15.0	69	43	68	60	NE 1	ESE 2	ESE 3		
11	749.0	749.2	748.7	22.8	29.8	23.6	25.0	30.3	19.0	16.0	14.3	15.8	14.0	68	50	64	61	ESE 3	SSE 2	E 3		
12	748.1	746.5	749.2	22.2	29.8	17.4	21.7	30.0	17.4	18.1	15.6	16.6	13.6	78	53	91	74	ESE 2	SSE 2	ESE 3		
13	751.7	752.1	752.6	18.4	24.3	20.3	21.0	25.2	15.8	14.0	13.3	14.1	15.7	84	62	86	77	ESE 2	MNW 2	WSW 1		
14	753.9	753.0	752.6	20.6	27.6	22.0	23.0	27.6	17.2	14.9	15.4	14.9	17.2	84	54	87	75	SSE 1	MNW 1	WSW 1		
15	752.8	752.2	751.0	22.2	29.6	23.1	24.5	30.3	18.4	15.9	15.6	15.8	16.1	78	51	76	68	SW 1	ESE 2	ESE 2		
16	749.6	747.9	747.1	24.2	31.0	24.8	26.2	31.6	19.3	16.2	17.7	16.5	17.4	78	49	74	67	E 1	ESE 2	ESE 2		
17	748.8	748.6	748.8	19.9	27.3	22.2	22.9	28.1	18.4	15.8	15.9	15.7	15.6	91	58	78	76	MSW 2	NW 2	ESE 1		
18	749.2	748.7	746.9	22.6	30.4	25.2	25.8	30.7	17.4	14.9	14.4	13.5	14.3	70	41	59	57	ESE 1	ESE 3	ESE 3		
19	745.1	743.6	748.1	24.0	32.0	22.3	25.2	31.4	22.3	15.0	14.0	14.8	12.9	62	53	64	60	SE 3	ESE 3	MNW 2		
20	749.7	748.8	748.4	19.2	25.1	21.2	21.7	25.4	17.4	15.0	12.2	11.6	13.7	73	49	73	65	MNW 2	MNW 2	WNW 2		
21	748.8	747.6	747.1	18.7	26.1	20.7	21.6	26.6	15.5	12.8	12.6	11.4	14.3	78	45	78	67	MSW 2	MNW 1	SE 1		
22	748.1	747.9	748.5	20.6	24.7	19.7	21.2	25.3	16.9	13.7	11.6	12.6	13.9	64	54	81	66	MNW 1	N 2	W 1		
23	749.4	748.7	748.6	19.6	27.2	20.6	22.0	27.5	17.1	14.4	14.1	14.6	14.0	82	54	77	71	MSW 1	NW 2	E 1		
24	748.2	747.0	746.1	22.0	29.3	23.0	24.3	30.2	17.2	14.3	14.8	11.8	15.7	75	39	75	63	ESE 2	SSE 2	ESE 2		
25	745.6	745.6	750.1	22.6	28.0	17.7	21.5	28.4	17.7	16.3	15.1	14.7	12.4	74	52	81	69	W 2	MNW 2	WNW 2		
26	753.9	753.9	754.3	15.7	20.5	18.7	18.4	21.7	15.5	13.4	09.3	09.8	09.4	68	54	58	60	W 2	S 3	NNW 2		
27	752.6	753.9	753.2	15.2	21.0	15.7	16.9	22.4	11.7	08.5	09.8	07.7	10.1	75	41	76	64	MSW 2	MNW 2	SSW 1		
28	752.8	751.6	752.0	15.6	22.1	20.7	19.8	24.0	11.3	08.0	09.6	08.7	10.9	72	44	59	58	MSW 2	MNW 3	W 2		
29	751.8	751.1	750.9	18.6	25.7	20.1	21.1	26.2	16.3	13.4	11.9	12.2	15.2	74	49	86	70	MNW 1	MNW 2	W 1		
30	750.1	749.0	749.2	19.3	25.7	19.6	21.0	27.1	16.4	13.6	13.0	12.5	12.1	82	51	71	68	MSW 2	MNW 2	ESE 1		
31	750.0	749.7	750.7	18.5	25.0	20.5	21.1	26.6	16.6	13.4	13.2	13.2	13.2	83	55	73	70	MSW 3	N 3	W 2		
MES.	VRED.	749.1	748.7	749.0	19.4	25.6	20.3	21.4	26.6	16.4	13.9	13.4	13.4	13.9	79	55	78	71	1.7	2.1	1.7	

1975 AVGUST

BEOGRAD

1	751.3	750.9	751.6	17.5	26.7	21.3	21.7	27.6	15.7	13.6	13.4	12.0	13.2	90	46	70	69	MSW 2	NW 3	W 2	
2	752.4	752.2	753.0	18.1	24.7	18.0	19.7	25.9	16.8	13.9	13.4	12.7	14.6	86	55	94	78	MSW 2	MNW 2	ESE 2	
3	753.8	753.3	753.9	17.6	23.7	21.0	20.8	24.0	15.8	13.4	13.0	13.4	13.1	86	61	70	72	MNW 2	NNW 2	W 2	
4	753.1	751.8	751.5	17.6	19.8	19.0	18.8	24.7	16.0	12.5	12.6	14.1	14.8	83	82	90	85	MSW 1	SW 2	MSW 2	
5	751.5	750.3	751.5	16.6	24.3	15.9	18.2	24.7	14.7	12.0	12.5	10.8	12.5	88	47	92	76	MSW 2	NNE 2	SSW 1	
6	752.1	752.3	754.9	17.4	24.1	18.3	19.3	24.6	14.4	12.0	12.7	10.4	14.4	85	46	92	74	SSW 1	MNW 2	- 0	
7	753.0	751.8	752.1	17.8	21.7	16.8	18.3	25.0	16.7	15.5	13.3	17.2	13.5	87	88	94	90	SSW 1	N 2	SM 2	
8	751.7	751.5	751.0	15.8	21.1	19.0	18.7	22.7	15.8	13.5	12.6	14.2	15.3	94	76	93	88	MSW 1	W 1	S 1	
9	747.4	750.5	750.0	17.6	25.4	21.7	21.6	26.3	15.9	13.6	13.9	14.0	17.2	92	58	88	79	SE 1	MNW 2	WSW 2	
10	752.1	751.1	751.3	20.4	27.8	21.6	22.8	28.7	16.5	14.4	14.9	12.7	15.5	83	45	80	69	SW 1	MNW 1	WSW 1	
11	752.2	751.4	749.8	21.2	29.2	21.4	23.3	29.4	16.0	14.8	15.1	13.2	14.5	80	44	86	70	MSW 1	NW 1	SE 1	
12	748.5	746.5	746.0	22.2	30.1	21.4	23.8	30.6	17.6	14.8	14.0	13.0	15.1	70	42	79	63	SE 1	MSW 1	ESE 1	
13	749.9	749.5	748.2	18.6	24.1	18.1	19.7	24.3	17.4	17.0	15.2	15.0	15.0	94	67	96	86	S 1	MNW 1	W 1	
14	751.8	752.7	752.6	13.2	21.1	15.2	16.2	22.4	13.0	11.2	08.4	08.8	11.0	74	47	85	69	WW 1	MNW 2	ESE 1	
15	752.5	751.2	750.0	16.0	24.7	19.5	19.9	25.6	12.0	09.0	11.8	10.4	11.7	86	45	69	67	ESE 2	SE 3	SE 3	
16	748.5	747.8	750.1	18.5	30.1	20.9	22.6	30.3	15.7	12.5	12.1	13.6	13.6	76							

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 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_x = 1.2 \text{ m}$

Dan	Vrijeme 0-6 0	Oblačnost N (0-10)					Intenzitet količina sunčevog svetlosti	Padavine R mm	Snežni Pokrivalo h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	6	100	100	10	10.0	00.0	32.7	.	.	$T^0 0^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0 23^0$	
2	7	100	100	04	08.0	00.0	22.5	.	.	$0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0 23^0$	
3	7	10	10	01	07.0	03.2	05.3	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
4	7	020	040	00	02.7	11.9	00.3	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
5	7	040	050	10	06.3	04.4	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
6	7	10	060	06	07.3	04.1	47.3	.	.	$R^0 0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
7	7	10	09	06	06.3	06.2	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
8	7	10	030	01	04.7	11.2	03.3	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
9	8	000	040	00	01.3	13.4	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
10	8	030	000	00	01.0	13.5	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
11	8	000	020	04	02.0	12.1	.	.	.	$\Delta^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
12	8	000	000	10	03.3	10.2	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
13	8	060	030	00	03.0	10.0	04.4	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
14	8	040	040	00	02.7	10.2	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
15	8	000	030	00	01.0	12.0	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
16	8	000	000	00	00.0	12.7	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
17	8	07	040	00	03.7	10.8	14.7	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
18	8	000	000	00	00.0	12.9	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
19	8	010	000	07	02.7	07.6	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
20	8	020	040	06	04.0	11.0	06.0	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
21	8	000	040	03	02.3	10.8	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
22	8	050	09	04	04.0	10.2	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
23	8	000	060	00	02.0	11.5	00.0	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
24	8	000	020	02	01.3	12.1	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
25	8	000	040	07	03.7	09.4	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
26	8	050	050	03	04.3	05.5	00.0	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
27	8	000	050	00	01.7	10.2	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
28	8	000	00	09	05.7	06.0	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
29	8	030	050	00	02.7	06.2	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
30	7	050	07	00	04.0	06.9	.	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
31	8	000	050	02	02.3	10.9	01.0	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
MES. VRED.		03.4	04.6	03.1	03.7	279.1	131.5				

1	8	040	050	00	03.0	10.8	.	.	$\Delta^0 0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
2	8	04	050	04	05.7	04.6	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
3	8	040	060	09	06.3	04.9	11.2	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
4	7	050	070	10	07.3	05.3	00.0	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
5	8	020	050	09	05.3	08.5	01.4	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
6	8	030	050	00	02.7	09.3	01.7	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
7	7	060	10	07	07.7	02.6	00.3	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
8	7	08	06	06	07.3	06.7	05.4	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
9	7	050	060	09	06.7	05.4	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
10	8	020	030	06	01.7	10.6	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
11	8	000	080	00	02.7	10.3	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
12	8	010	020	04	02.3	10.6	00.0	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
13	7	060	070	10	06.3	02.2	01.8	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
14	7	08	020	00	03.3	04.9	11.5	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
15	8	000	000	06	00.0	12.1	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
16	8	000	040	10	04.7	06.6	.	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
17	8	050	04	03.0	03.0	08.5	01.0	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0 9^0 10^0 11^0 12^0 13^0 14^0 15^0 16^0 17^0 18^0 19^0 20^0 21^0 22^0$	
18	8	040	040	100	06.0	07.3	02.5	.	$=0^0 1^0 2^0 3^0 4^0 5^0 6^0 7^0 8^0$	

$\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = + 1h 22min.$

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D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	751.6	751.9	752.1	17.4	20.7	18.1	16.6	24.7	16.1	14.0	14.3	15.2	13.7	96	63	88	89	WSW 2	SW 1	- 0	
2	752.3	751.4	750.4	17.4	25.3	20.2	20.8	26.4	15.5	12.7	14.3	16.2	16.3	96	67	92	85	NNE 1	NNE 2	E 2	
3	748.6	747.2	746.4	19.9	26.8	20.0	22.2	29.0	17.9	14.1	14.1	14.6	13.0	81	49	74	68	ESE 3	SE 3	SM 3	
4	746.8	746.8	747.3	18.2	26.4	20.0	21.2	27.4	16.4	14.4	13.6	15.0	15.7	87	58	89	76	SE 1	N 1	SE 1	
5	748.3	747.8	747.7	18.0	26.9	21.0	21.7	27.2	17.0	14.3	14.9	14.9	15.3	96	56	82	78	S 1	NNW 2	ESE 2	
6	749.8	750.4	751.1	17.3	24.2	17.8	19.3	24.8	17.0	15.4	14.1	13.6	14.4	95	60	94	83	W 2	W 3	- 0	
7	750.1	749.4	749.9	18.8	22.0	19.2	19.8	22.9	15.5	13.0	12.6	15.3	15.2	78	77	91	82	SE 2	SSW 2	WSW 2	
8	752.3	753.8	755.3	16.8	21.6	17.0	18.1	22.2	16.7	12.0	13.5	12.5	11.5	94	65	79	79	WSW 2	NNW 2	N 3	
9	755.7	755.2	754.2	12.0	19.0	12.6	14.0	20.9	11.4	0.9	08.1	08.2	09.6	77	50	88	72	NNE 2	N 2	ENE 1	
10	753.9	753.3	753.0	10.9	20.7	13.0	14.4	21.3	0.8	0.8	07.2	07.1	09.7	74	39	86	66	- 0	W 3	- 0	
11	752.0	750.5	750.1	13.1	23.7	16.8	17.6	24.0	10.1	07.0	07.9	09.6	10.6	70	44	74	63	ESE 2	SE 3	ESE 3	
12	748.4	748.1	747.0	16.8	22.6	18.4	19.0	23.6	15.5	12.2	09.7	14.5	14.7	68	71	93	77	SE 3	SSE 3	SE 3	
13	747.8	750.8	753.2	15.5	14.9	13.3	14.2	18.4	13.3	14.5	12.5	10.5	10.2	93	83	89	89	W 1	NNW 2	WSW 1	
14	752.8	751.3	749.9	11.8	23.0	18.2	17.8	24.1	09.5	06.8	09.9	11.5	13.1	95	55	82	78	ESE 2	SE 2	ESE 2	
15	750.2	750.8	752.6	16.8	27.6	20.6	21.4	28.0	14.7	11.1	11.9	13.7	14.9	83	50	82	72	ESE 3	SE 3	ESE 3	
16	756.2	756.3	756.9	19.0	29.8	21.7	23.0	30.9	17.4	14.6	13.8	17.0	17.3	84	54	89	76	SE 1	SW 1	ESE 1	
17	758.0	758.0	758.3	19.6	29.2	21.2	22.8	29.4	18.2	14.4	16.8	16.9	14.9	98	56	79	78	SM 2	NW 2	NNE 2	
18	759.3	758.8	758.6	18.5	25.0	17.8	19.8	25.2	17.8	15.0	10.0	11.0	11.8	63	46	77	62	SSE 3	E 3	ESE 2	
19	757.7	757.1	756.7	16.7	26.1	17.5	19.4	26.1	14.8	10.7	10.1	09.8	11.5	71	39	77	62	ESE 3	E 3	ESE 2	
20	756.0	755.3	755.0	15.1	26.9	17.7	19.4	27.2	13.4	0.9	11.0	10.2	12.9	86	38	85	70	- 0	ESE 2	NNE 1	
21	755.5	755.0	755.6	14.4	26.5	20.2	20.3	26.6	13.0	09.8	11.9	11.7	10.8	97	45	61	68	W 1	N 2	NNE 2	
22	757.0	757.9	758.4	15.4	25.1	17.9	19.1	25.7	13.7	10.2	11.9	12.1	13.8	91	50	90	77	SSW 2	NNW 2	- 0	
23	758.9	757.9	756.6	15.7	24.6	18.2	19.2	25.2	14.9	11.5	13.0	14.6	14.4	97	63	92	84	W 1	NNE 2	E 1	
24	755.6	754.4	753.6	16.2	25.0	18.2	19.4	25.2	15.3	11.2	12.8	15.0	14.9	93	63	95	84	W 1	W 2	SSE 2	
25	752.6	751.4	751.2	16.9	25.8	17.7	19.5	26.6	15.5	11.7	14.2	10.6	12.4	98	42	81	74	SSW 1	WSW 1	ESE 1	
26	749.8	748.1	749.0	17.6	27.8	19.6	21.2	28.0	15.4	09.5	10.2	09.1	12.0	67	33	70	57	SE 2	S 3	SSE 2	
27	754.3	755.5	756.1	16.0	21.0	16.4	17.4	22.4	16.0	11.6	10.7	11.3	13.0	79	60	93	77	NNE 2	W 2	ESE 2	
28	756.4	756.4	757.0	16.6	28.0	18.6	20.4	28.2	14.6	10.8	12.2	12.6	15.0	87	44	94	75	ESE 1	WSW 1	SE 1	
29	756.3	755.8	755.5	16.4	28.6	20.1	21.3	29.2	14.8	11.5	13.2	12.9	15.0	94	44	85	74	ESE 1	SSW 1	ESE 2	
30	754.7	753.1	752.7	18.8	27.6	20.6	21.9	27.6	17.6	13.1	12.8	13.6	12.4	79	49	68	65	ESE 2	SE 3	SE 3	
MES.	VRED.	753.3	753.0	753.0	16.4	24.8	18.3	19.5	23.6	14.9	11.7	12.1	12.7	13.3	86	54	84	75	1.7	2.1	1.7

1	752.8	753.8	753.7	19.6	24.6	20.6	21.8	24.4	19.0	16.0	11.4	10.2	08.7	67	40	48	52	SE 4	ESE 3	ESE 4
2	753.8	754.5	755.4	17.1	22.6	17.7	18.8	23.7	16.7	14.0	09.7	11.7	09.2	66	57	61	61	ESE 4	E 3	SE 3
3	755.5	754.7	753.9	15.8	21.1	15.8	17.1	21.9	14.6	10.9	09.6	12.8	12.4	71	68	92	77	SE 1	WSW 2	SSW 2
4	755.0	755.0	755.2	15.3	20.9	16.1	17.1	21.2	14.6	09.9	12.0	07.9	09.3	92	43	68	68	WSW 1	NW 2	NNW 2
5	755.8	755.3	756.6	09.6	17.5	13.0	13.3	17.7	0.9	0.2	07.2	06.8	06.6	81	43	59	62	W 2	NH 2	NNW 2
6	750.1	750.1	750.0	08.2	16.5	12.8	12.6	17.3	07.3	03.5	07.4	08.4	08.7	91	60	79	77	WSW 2	NW 2	NNW 2
7	756.6	754.2	752.9	11.3	17.2	13.8	14.0	18.3	09.0	05.4	08.8	08.9	10.2	87	60	86	78	SM 1	WSM 2	SSE 1
8	754.2	753.4	753.6	09.2	16.3	10.4	11.6	16.7	08.9	08.1	07.9	05.2	05.3	90	37	56	61	NNW 2	NM 3	NNW 2
9	753.2	751.0	751.5	06.6	14.5	11.5	11.5	15.6	07.4	03.7	06.1	05.4	06.7	73	44	66	61	SSW 2	NNW 2	NNW 2
10	750.3	749.0	748.4	06.6	13.8	11.0	10.6	14.3	04.8	01.2	06.9	05.8	06.5	95	49	66	70	SSE 1	NE 2	NE 2
11	748.4	751.2	753.6	08.4	08.9	08.6	08.6	11.0	08.2	08.2	08.0	08.2	07.7	96	96	92	95	NNE 2	N 3	NNE 1
12	754.3	755.3	754.8	08.3	09.7	08.1	08.6	11.6	06.0	07.0	07.6	06.8	07.0	92	75	86	84	E 3	ESE 4	ESE 4
13	753.5	750.3	748.5	09.4	12.9	10.2	10.7	14.0	06.0	07.6	08.3	07.9	08.8	93	71	94	86	SE 5	ESE 5	S 5
14	748.6	744.8	750.2	12.0	14.9	08.2	10.8	16.7	08.2	10.3	08.5	09.7	07.3	81	76	90	82	ESE 4	SE 4	N 3
15	751.6	752.0	753.1	06.4	13.3	07.2	08.5	14.4	04.4	02.5	06.8	08.4	07.5	94	73	99	89	ESE 2	SSE 1	ESE 1
16	752.6	751.6	749.6	08.6	16.4	13.4	13.8	18.2	06.0	02.4	07.3	09.0	08.2	86	65	71	74	ESE 3	ESE 3	ESE 4
17	742.6	742.1	743.1	11.1	15.5	14.3	13.8	18.6	11.2	10.7	08.3	09.1	08.9	83	69	73	75	ESE 4	E 4	SE 3
18	743.5	743.1	743.8	11.1	12.8	10.6	11.3	15.6	07.9	05.8	07.6	10.7	09.5	76	77	99	91			

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$$H_a = 132 \text{ m} \quad H_b = 132.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Instalacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10	10	00	06.7	04.2	.	.	.	$\Delta^{+20-94} = 5^{\circ} 9^{\circ} ; 0^{\circ} 12^{\circ} 12^{\circ} 15^{\circ} ; 13^{\circ} 12^{\circ} 15^{\circ}$
2	7	000	050	00	01.7	09.2	01.7	.	.	$\Delta^{-2-1-9-5} 18^{\circ} 24$
3	8	000	000	10	03.3	10.2	.	.	.	$\Delta^{-20-8^{\circ}} \Delta^{-8-4^{\circ}} 10^{\circ} 13^{\circ} 20^{\circ} ; 0^{\circ} 24^{\circ} 22^{\circ} 13^{\circ} 23^{\circ} 24, 0^{\circ} 23^{\circ} 23^{\circ}$
4	8	020	030	00	01.7	09.0	00.7	.	.	$\Delta^{-1-3-8} 20^{\circ} 24$
5	8	10	040	05	06.3	09.1	.	.	.	$\Delta^{-0-0-8-5} 8^{\circ} 20^{\circ} 22^{\circ} T^{\circ} 22^{\circ} 22^{\circ} 13^{\circ} 22^{\circ} 24, 0^{\circ} 22^{\circ} 23^{\circ} 0^{\circ} 23^{\circ} 24$
6	8	10	090	00	06.3	07.2	06.9	.	.	$18^{\circ} 0-2^{\circ} 0^{\circ} 1^{\circ} 0^{\circ} 2^{\circ} 0^{\circ} ; 0^{\circ} 1^{\circ} 2^{\circ} 4^{\circ} ; 0^{\circ} 18^{\circ} 24$
7	7	07	100	100	09.0	01.5	.	.	.	$\Delta^{-0-10-0-9} 0^{\circ} 1^{\circ} 10^{\circ} 44^{\circ} ; 17^{\circ} 21^{\circ} 24$
8	7	10	10	10	10.0	03.8	03.3	.	.	$0^{\circ} 3^{\circ} 9^{\circ} ; 18^{\circ} 16^{\circ} 17$
9	8	000	030	00	01.0	10.5	02.5	.	.	$\Delta^{-0-4-5} 8^{\circ} 18^{\circ} 24$
10	8	000	000	00	00.0	10.9	.	.	.	$\Delta^{-0-0-10-0} 20^{\circ} 24$
11	8	040	030	00	02.3	11.1	.	.	.	$\Delta^{-0-10-9-5} 18^{\circ} 24$
12	8	05	10	08	07.7	02.4	.	.	.	$\Delta^{-0-10-6-4} F_{\infty} S_{\infty} -8^{\circ} 0^{\circ} 2^{\circ} 8^{\circ} 9^{\circ} ; 0^{\circ} 11^{\circ} 14^{\circ} 24$
13	7	10	10	02	07.3	01.1	06.6	.	.	$18^{\circ} 0-3^{\circ} 4^{\circ} 4^{\circ} F_{\infty} S_{\infty} 3^{\circ} 4^{\circ} 4^{\circ} ; 0^{\circ} 6^{\circ} 0^{\circ} 4^{\circ} ; 0^{\circ} 9^{\circ} 4^{\circ} 5^{\circ} 10^{\circ} 10^{\circ} ; \Delta^{\circ} 20^{\circ} 24$
14	8	000	020	00	00.7	11.0	00.1	.	.	$\Delta^{-0-0-9-3} 20^{\circ} 24$
15	8	000	000	02	00.7	10.8	.	.	.	$\Delta^{-0-0-7-3} F_{\infty} S_{\infty} 8^{\circ} 24$
16	8	030	000	00	01.0	08.4	.	.	.	$\Delta^{-0-0-8-5} 18^{\circ} 24$
17	7	10	010	00	03.7	09.5	.	.	.	$\Delta^{-0-0-9-0} = 5^{\circ} 5^{\circ} 14^{\circ} 24$
18	8	000	000	00	00.0	09.9	.	.	.	$F_{\infty} S_{\infty} 14^{\circ} 14^{\circ} 24 ; \Delta^{\circ} 21^{\circ} 24$
19	8	000	000	00	00.0	09.9	.	.	.	$\Delta^{-0-0-8-0} 14^{\circ} 24$
20	8	000	000	00	00.0	09.6	.	.	.	$\Delta^{-0-0-9-4} 18^{\circ} 24$
21	7	000	000	00	00.0	09.2	.	.	.	$\Delta^{-0-20-9-0} 20^{\circ} 24$
22	7	030	000	00	01.0	06.9	.	.	.	$\Delta^{-0-0-8-4} 20^{\circ} 24$
23	7	000	000	00	00.0	06.8	.	.	.	$\Delta^{-0-0-9-1} 18^{\circ} 24 ; 0^{\circ} 13^{\circ} 10^{\circ} 24$
24	7	000	000	00	00.0	08.4	.	.	.	$\Delta^{-20-9-0} 18^{\circ} 24 ; 0^{\circ} 4^{\circ} 8^{\circ} 24$
25	7	100	020	00	04.0	05.2	.	.	.	$\Delta^{-0-0-6-2} 20^{\circ} 24 ; = 0^{\circ} 24^{\circ} 6^{\circ} 0^{\circ} 9^{\circ} 12^{\circ} ; = 0^{\circ} 16^{\circ} 6^{\circ} 15^{\circ} ; = 0^{\circ} 6^{\circ} 15^{\circ} 9^{\circ}$
26	7	000	000	06	02.0	09.3	.	.	.	$\Delta^{-0-0-8-0} 20^{\circ} 24$
27	7	100	040	00	04.7	02.8	C0.0	.	.	$\Delta^{-0-10-4-3} 17^{\circ} 24 ; 0^{\circ} 4^{\circ} 8^{\circ} 24$
28	7	030	020	00	01.7	08.9	00.4	.	.	$\Delta^{-0-0-9-0} 18^{\circ} 24$
29	8	020	050	00	02.3	09.6	.	.	.	$\Delta^{-0-10-4-0} 18^{\circ} 24$
30	8	000	040	03	02.3	08.3	.	.	.	$\Delta^{-0-0-8-0} F_{\infty} S_{\infty} 19^{\circ} 23^{\circ}$

REFUGIADO

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1	8	030	020	00	01.7	07.1	.	.	F _{SE} 2 ⁰⁵ 24 ⁱ
2	8	050	040	05	05.3	01.7	.	.	F _{SE} 0-9 ⁰⁰ 18 ^m , F _{SE} 3 ³⁷ , 15 ⁰ 8 ²⁰ , = 0 ⁸ 9 ²⁰ i
3	8	10	030	00	04.3	04.4	00.0	.	= 0-10 ⁰⁰ 7 ^m , K _{SE} 24
4	8	07	030	06	05.3	06.0	.	.	= 0-20 ⁰⁰ F _{SW} 12 ⁰⁰ 15 ^m , = 0 ¹⁹ 20 ⁰⁰ i
5	8	000	050	06	03.7	04.6	00.0	.	F _{NW} 13 ⁴⁷ , = 0 ²² 24 ⁱ
6	8	000	060	07	04.3	06.5	.	.	= 0-10-0 ⁵⁰ 21 ⁰⁰ 24
7	8	050	070	10	07.3	02.1	.	.	= 0-10-0 ⁵⁰
8	8	10	040	02	05.3	09.0	02.0	.	F _{NW} 0 ⁰⁸ 2 ⁴⁶ 9 ⁴ 16 ²⁴ i, = 0 ⁰² 5 ²⁰ i, = 0 ²² 24
9	8	08	10	10	09.3	02.9	.	.	= 0-0-7 ⁰⁰ 0 ¹⁷ 21 ⁴⁵ i
10	8	020	09	10	07.0	04.7	00.0	.	= 0 ²³ 24
11	6	100	100	10	10.0	00.0	03.8	.	= 0-0-15 ⁰⁰ 16 ^m 19 ²⁰ i, = 0 ¹⁵ 19 ¹⁰
12	7	100	100	100	10.0	00.0	02.9	.	= 0-14 ⁴⁵ 9 ⁰⁰ 13 ⁴⁵ 24 i, F _{SE} 6 ³⁷ 18 ^m , F _{SE} 48 ⁴⁵ 24
13	7	100	09	100	09.7	01.1	04.2	.	= 0-0 ⁵⁰ 10 ⁰⁰ 16 ^m 16 ²⁰ 18 ^m 23, F _{SE} 0-23 ⁰⁰ F _{SE} 23 ⁰⁰ 24
14	7	10	100	10	10.0	01.4	03.2	.	= 0 ⁰⁰ 17 ⁰⁰ 10 ^m 19 ³⁰ i, F _{SE} 3 ⁴⁵ 6 ³⁰ i, = 0 ⁷ 9 ⁰⁰ 9 ³⁰ i, 13 ³⁰ 17 ⁰⁰ i, = 0 ¹ 2 ⁴⁴ 44 ⁴⁰ 14 ⁴⁰ 14 ⁴⁰ [K _{SE}]
15	7	050	060	00	03.7	03.4	12.6	.	= 0 ¹⁰ 30 12 ⁴⁵ 13 ⁴⁵ i, = 0 ¹⁹ 23 ⁰⁰
16	7	030	10	03	06.0	04.2	00.1	.	= 0-13-10 ³⁰ F _{SE} 10 ⁴⁵ 12 ⁰⁰ i, = 0 ¹⁴ 2 ⁴⁵ 20 ⁰⁰ i
17	7	100	09	09	09.3	01.7	00.2	.	F _{SE} 0-19 ⁰⁰ i, F _{SE} 0 ⁰² 4 ^m 7 ⁰⁰ i, = 0 ⁵ 9 ⁰⁰ i, 18 ²⁰ 19 ²⁰ i
18	8	05	10	10	08.3	00.3	01.8	.	F _{SE} 12 ⁴⁵ 12 ⁰⁰ i, 12 ⁴⁵ 12 ⁰⁰ 15 ^m 24 i, 22 ⁴⁵ 24
19	8	04	10	05	07.0	02.1	03.8	.	= 0-0-2 ²⁰ = 0 ² 16 ²⁰ 24
20	6	100	100	100	10.0	00.0	01.5	.	= 0-0-0 ²⁰ = 0 ² 16 ²⁰ 24, = 0 ⁵ 22 ²⁰ i
21	7	10	10	100	10.0	00.0	05.2	.	= 0 ¹⁰ 8 ⁴⁵ = 0 ² 13 ⁵⁰ 24
22	7	10	10	100	10.0	00.1	05.8	.	= 0-0-2 ²⁰ 14 ²⁰ 24 ⁰⁰ i
23	6	100	100	100	10.0	00.0	00.4	.	= 0-5 ⁴⁵ 13 ⁰⁰ i, = 0 ¹⁵ 20 ²⁰ 23 ²⁰
24	7	06	060	07	04.3	04.8	05.2	.	= 0 ¹⁷ 45 ²⁴ i, = 0 ¹ 24 ²⁴ 24, = 0 ⁶ 13 ²⁰
25	7	09	030	00	04.0	04.9	.	.	= 0-0-9 ⁴⁵ 16 ⁴⁵ 24, = 0 ⁶ 13 ²⁰
26	7	7 ⁴⁵	000	00	03.3	04.1	.	.	= 0-2-0-5 ^m 16 ²⁰ 24 = 0 ³⁰ 5 ⁴⁵ 7 ⁴⁵ 11 ⁴⁵ , = 0 ⁵ 7 ⁴⁵
27	6	04	000	00	01.3	07.2	.	.	= 0-10-0 ²⁰ 17 ²⁰ 24 i, = 0 ⁴ 24 ²⁴
28	6	00	000	00	00.0	09.0	.	.	= 0-0-2 ²⁰ 0-5 ¹ 17 ²⁰ 24, = 0 ⁵ 7 ²⁰
29	6	00	000	00	00.0	08.4	.	.	= 0-0-19 ⁴⁵ 18 ⁴⁵ 0-9 ¹ 18 ⁴⁵ 24
30	6	00	000	00 ⁴⁵	00.0	00.1	.	.	= 0-0-9 ²⁰ 18 ⁴⁵ 20 ⁰⁰ , = 0-2-5 ⁴⁵ 20 ⁴⁵ = 0 ²⁰ 15 21 ³⁰ , = 0 ²¹ 30 ²⁴
31	5	10 ⁴⁵	10	10	10.0	02.2	.	.	= 0-0-8 ⁴⁵ 18 ⁴⁵ 24 i, = 0 ⁸ 45 9 ³⁰ , = 0 ¹² 9 ³⁰ 18 ⁴⁵

$\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = + 1h 22 min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	753.3	754.2	755.0	05.4	10.0	08.0	07.8	10.3	05.0	04.8	06.6	07.4	06.6	99	80	82	87	ESE 1	NNW 1	SE 3	
2	755.8	756.2	757.9	08.6	15.3	08.6	10.3	15.6	07.9	07.2	07.3	07.8	07.6	87	60	91	79	SE 3	ESE 3	ESE 3	
3	759.0	758.9	759.0	06.9	15.5	07.8	09.3	15.5	06.9	06.1	07.3	08.9	07.2	97	67	91	85	ESE 2	ESE 2	SE 3	
4	759.7	761.3	761.7	03.2	07.2	07.3	06.2	07.8	03.0	02.5	05.7	07.4	07.6	98	97	99	98	WSM 2	WSM 2	NNW 1	
5	760.9	759.9	760.0	07.0	10.7	06.6	07.7	10.7	06.6	06.4	06.2	06.4	05.7	83	66	79	76	ESE 2	ESE 3	ESE 2	
6	758.7	757.5	757.1	04.8	13.9	09.3	09.3	14.3	03.6	01.5	05.9	06.7	06.5	91	56	74	74	SE 2	ESE 4	ESE 3	
7	756.0	756.2	756.1	08.7	09.5	08.8	09.0	09.6	08.6	06.7	06.2	05.7	06.1	73	64	72	70	ESE 4	ESE 4	ESE 4	
8	757.3	756.7	755.8	06.2	09.4	06.2	07.0	09.6	06.1	07.6	05.2	05.0	05.3	73	57	74	68	ESE 3	E 3	E 3	
9	753.7	754.0	754.7	06.4	07.2	06.2	06.5	08.0	06.0	06.0	05.8	05.2	05.6	81	69	78	76	ESE 4	E 4	ESE 4	
10	754.3	753.6	752.1	05.4	10.0	06.0	06.8	10.5	05.4	05.4	05.6	05.3	05.7	83	58	81	74	ESE 4	ESE 3	ESE 3	
11	752.4	754.8	757.3	05.0	05.8	05.2	05.3	06.5	04.8	04.2	04.4	06.2	06.3	98	90	96	95	ESE 2	WSM 3	WSM 1	
12	759.0	759.8	761.6	05.7	07.6	05.6	06.1	07.7	05.2	04.5	06.5	05.8	06.0	94	74	87	85	ESE 3	E 3	E 3	
13	762.3	761.6	761.2	04.8	09.6	03.4	05.3	09.6	03.4	03.9	05.1	05.2	04.2	80	58	71	70	ESE 4	ESE 3	ESE 5	
14	758.8	756.7	756.2	02.3	07.7	02.5	03.8	08.7	02.1	-00.4	04.4	04.7	04.7	81	60	86	76	ESE 4	ESE 4	ESE 4	
15	755.9	755.2	755.2	02.5	05.2	00.8	02.3	05.4	00.8	-00.6	04.1	04.1	03.7	75	62	76	71	ESE 3	E 3	ESE 4	
16	751.6	746.8	743.0	00.0	04.1	02.0	02.0	04.7	-00.2	-02.0	04.3	04.2	04.8	95	69	92	85	ESE 3	ESE 3	ESE 4	
17	739.7	739.1	739.8	03.5	08.4	08.6	07.3	08.7	02.0	01.4	04.8	06.8	07.2	82	82	86	83	ESE 4	ESE 5	ESE 5	
18	740.3	738.6	742.8	10.4	12.6	12.6	12.8	15.6	08.4	06.4	07.7	07.8	09.2	81	58	87	75	ESE 4	ESE 4	SW 3	
19	744.7	745.6	747.2	11.8	12.2	08.0	10.0	12.6	08.0	08.6	07.6	07.3	06.0	74	69	75	73	SSE 3	S 3	NNE 3	
20	746.8	742.8	742.4	05.2	10.7	08.7	08.3	11.0	05.2	04.1	05.7	05.3	07.5	86	54	89	76	WSM 2	S 3	WSM 3	
21	746.1	748.3	751.5	02.8	05.1	01.1	02.5	08.7	01.1	02.0	05.2	04.9	03.9	92	74	78	81	N 3	NNW 3	W 3	
22	749.5	746.4	748.4	-02.2	03.2	00.6	00.6	04.0	-02.6	-07.1	03.2	03.2	03.5	83	55	74	71	SSE 1	NE 1		
23	749.9	750.1	751.3	-00.8	-00.2	-00.2	-00.4	00.4	-00.8	-04.3	04.2	03.9	04.4	96	37	98	94	NN 2	NNN 2	NW 2	
24	750.5	750.7	752.5	-00.7	-01.8	-02.2	-01.7	-00.2	-02.2	-01.6	03.6	03.9	03.5	82	96	90	89	NN 2	NN 3	NN 3	
25	755.2	756.6	757.0	-05.1	-02.0	-05.3	-04.4	-01.7	-05.4	-05.9	02.6	02.7	02.6	82	68	84	78	N 3	NNW 3	WSM 3	
26	756.2	755.5	755.4	-07.8	00.9	-05.9	-04.5	01.5	-08.0	-16.5	02.2	01.9	02.3	85	39	77	67	SSM 1	W 1	ESE 2	
27	755.2	754.1	754.0	-06.2	03.3	-01.9	-01.7	03.6	-07.3	-15.0	01.8	02.4	02.4	63	42	60	55	ESE 2	SE 3	ESE 3	
28	751.8	749.3	748.2	-00.3	06.8	04.7	04.0	07.2	-02.1	-05.7	03.2	04.2	04.1	72	57	64	64	SE 4	ESE 3	ESE 4	
29	747.1	747.4	748.2	04.6	07.0	04.3	06.0	08.1	03.7	02.2	05.7	05.6	06.4	90	75	89	85	SE 3	NNW 1	NNW 2	
30	749.0	748.6	749.1	03.2	12.3	05.2	06.5	12.7	02.6	-01.6	05.2	06.2	05.3	91	57	80	76	ESE 2	SE 3	SE 3	
MES.	VРЕД.	753.0	752.6	753.0	03.4	07.7	04.5	05.0	08.2	02.6	01.0	05.2	05.4	05.4	85	67	82	78	2.7	2.9	3.0

1975 DECEMBAR

BEOGRAD

1	750.3	751.4	752.6	03.8	10.7	05.4	06.3	10.7	03.8	01.6	04.8	06.3	05.0	80	65	75	73	ESE 4	ESE 4	ESE 4
2	752.0	751.5	751.5	03.4	07.7	03.2	04.4	09.0	03.0	02.0	04.7	05.1	04.6	80	65	80	75	SE 5	ESE 4	ESE 4
3	752.2	752.6	754.2	02.6	08.4	03.6	04.6	08.6	02.6	00.6	04.3	04.9	04.3	78	60	73	70	SE 3	SE 4	SE 4
4	755.5	757.0	760.6	02.3	07.0	04.4	04.5	08.0	02.1	-00.5	04.4	05.2	05.6	81	70	90	80	SE 3	NW 3	W 3
5	760.5	758.8	758.3	03.6	07.4	02.8	04.2	08.5	02.8	00.8	05.6	03.8	04.5	94	50	81	75	NNW 2	SSE 1	WSM 2
6	756.2	751.3	750.1	02.1	12.4	06.4	06.8	12.9	01.8	-01.8	04.7	03.7	05.3	89	34	73	65	SSM 2	SW 2	WSM 3
7	752.8	755.0	755.4	03.9	05.3	01.6	03.1	06.4	01.6	01.9	04.4	03.6	03.8	73	34	74	67	NW 3	NNW 3	SW 1
8	752.0	750.8	752.5	-00.8	05.7	04.3	03.4	05.7	-01.1	-06.6	03.8	03.4	04.1	89	50	66	68	SE 2	W 2	W 2
9	756.3	757.4	758.5	02.2	06.9	03.0	03.8	07.1	02.0	-02.5	03.9	03.8	03.8	73	51	68	64	W 2	NNW 3	SSM 2
10	758.0	757.0	756.9	-00.5	06.3	05.2	04.0	07.6	-01.0	-06.6	03.7	04.3	04.3	83	60	65	69	SE 1	NNW 2	NNW 2
11	759.1	760.2	759.8	00.6	03.5	01.4	01.7	05.2	-00.2	-03.3	04.0	04.3	04.6	84	73	90	82	SW 2	W 1	ESE 2
12	757.8	754.4	753.0	00.3	04.6	00.9	01.7	05.4	00.2	-04.7	04.1	04.1	03.7	88	64	76	76	ESE 2	E 3	ESE 3
13	750.9	750.8	752.8	01.2	04.4	02.5	02.6	06.7	00.9	-01.6	04.2	05.2	05.2	85	84	95	88	SE 3	WSM 2	WSW 2
14	755.6	757.1	760.1	01.4	01.6	00.8	01.2	02.5	00.8	01.2	04.7	04.9	04.5	93	95	93	94	NW 2	NNW 2	NW 2
15	761.0	760.3	760.6	00.8	02.3	01.8	01.7	02.5	00.6	00.4	04.4	04.3	04.3	90	79	82	84	W 1	ESE 1	ESE 2
16	757.3	752.4	750.1	00.7	06.8	04.7	04.2	07.0	00.7	-04.2	04.0	04.5	04.6	83	61	73	72	ESE 3	SE 5	ESE 4
17	745.3	741.1	738.3	07.0	11.4	10.9	10.0	12.6	04.7	03.8	04.4	05.1	06.5	85	65	66	72	SE 4	SE 4	SE 3
18	742.3	746.8	750.7	06.4	03.5	02.2	03.6	10.9	02.2	-05.9	04.1	04.3	04.2	85	73	77	78			

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 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Dan	Vremenski interval 0-9	Oblačnost N (0-10)					Insekcija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w		
		14	7	14	21	Sred Dnes				7	7	
1	6 10	040	00	04.7	03.2	$\equiv^{\circ} 0-6^{\circ} 20^{\circ} 18^{\circ}$	$\equiv^{\circ} 6^{\circ} 15^{\circ} 6^{\circ} 20^{\circ} 18^{\circ}$	
2	8 05	000	00	01.7	07.0	$F_{ESE-SE} 7^{\circ} 7^{\circ} 10^{\circ} 12^{\circ} 19^{\circ} 24^{\circ}$	$\Delta^{\circ} 20^{\circ} 24^{\circ}$	
3	7 00	000	00	00.0	07.0	$\Delta^{\circ} 0-10^{\circ} 18^{\circ} 24^{\circ}$		
4	6 00	10	10	06.7	00.0	$\Delta^{\circ} 0-6^{\circ} 20^{\circ} 24^{\circ} \equiv^{\circ} 16^{\circ} 24^{\circ} \equiv^{\circ} 6^{\circ} 8^{\circ} 40^{\circ}$		
5	7 10	070	00	05.7	00.2	$\equiv^{\circ} 0-11^{\circ} \Delta^{\circ} 0-8^{\circ} 20^{\circ} 24^{\circ}$		
6	7 03	050	00	02.7	06.3	$\Delta^{\circ} 0-9^{\circ} 20^{\circ} 24^{\circ} \equiv^{\circ} 4^{\circ} 10^{\circ} F_{ESE} 12^{\circ} 12^{\circ} 32^{\circ}$		
7	7 09	09	10	09.3	00.0	$\Delta^{\circ} 0-2^{\circ} F_{ESE} 0^{\circ} 10^{\circ} 24^{\circ} F_{ESE} 8^{\circ} 10^{\circ} 6^{\circ}$		
8	8 10	09	10	09.7	00.0	$F_{ESE} 0-3^{\circ} 6^{\circ} 10^{\circ} 13^{\circ} 19^{\circ} 24^{\circ}$		
9	8 10	10	02	07.3	00.0	$F_{ESE} 0^{\circ} 24^{\circ} F_{ESE} 4^{\circ} 4^{\circ} 24^{\circ}$		
10	8 07	060	10	07.7	02.8	$F_{ESE} 0-24^{\circ} 10^{\circ} 20^{\circ} 24^{\circ}$		
11	7 10	10	10	10.0	00.0	08.3	.	.	.	$F_{ESE} 0-4^{\circ} \equiv^{\circ} 0-3^{\circ} 5^{\circ} 9^{\circ} 22^{\circ}$		
12	7 10	10	10	10.0	00.0	00.6	.	.	.	$F_{ESE} 13^{\circ} 21^{\circ} 24^{\circ}$		
13	7 09	020	00	03.7	04.5	$F_{ESE} 14^{\circ} 24^{\circ} F_{ESE} 20^{\circ} 23^{\circ} 5^{\circ}$		
14	8 02	020	00	01.3	07.5	$F_{ESE} 0-23^{\circ} 24^{\circ} F_{ESE} 2^{\circ} 3^{\circ} 5^{\circ}$		
15	7 10	10	09	09.7	00.0	$\Delta^{\circ} 0^{\circ} 7^{\circ} 17^{\circ} F_{ESE} 17^{\circ} 24^{\circ} 7^{\circ} 17^{\circ} 24^{\circ}$		
16	7 10	050	100	08.3	03.0	$\Delta^{\circ} 0^{\circ} 2^{\circ} 7^{\circ} F_{ESE} 0-24^{\circ} 24^{\circ} 17^{\circ} 24^{\circ} 24^{\circ}$		
17	7 10	09	10	05.7	00.0	05.9	.	.	.	$\Delta^{\circ} 0-4^{\circ} 6^{\circ} 12^{\circ} F_{ESE} 0-24^{\circ} F_{ESE} 9^{\circ} 14^{\circ} 24^{\circ} 19^{\circ} 20^{\circ}$		
18	8 09	10	10	09.7	00.0	00.4	.	.	.	$F_{ESE} 0-14^{\circ} F_{ESE} 5^{\circ} 4^{\circ} 5^{\circ} 9^{\circ} 24^{\circ} 14^{\circ} 24^{\circ}$		
19	8 10	10	08	09.3	00.0	04.4	.	.	.	$\Delta^{\circ} 0-1^{\circ} 7^{\circ} 14^{\circ} 24^{\circ} F_{ESE} 11^{\circ} 12^{\circ} 24^{\circ}$		
20	7 10	060	100	08.7	02.8	00.1	.	.	.	$\Delta^{\circ} 0-2^{\circ} 9^{\circ} 16^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$		
21	7 10*	100	00	06.7	00.0	11.1	.	.	.	$\Delta^{\circ} 0-13^{\circ} 9^{\circ} 13^{\circ} 15^{\circ} F_{ESE} 4^{\circ} 6^{\circ} 13^{\circ} 19^{\circ} 24^{\circ} 6^{\circ} 15^{\circ} 15^{\circ} 14^{\circ} 15^{\circ}$		
22	7 04	040	06	04.7	07.0	03.4	.	.	.	$\Delta^{\circ} 0-0^{\circ} 9^{\circ} 20^{\circ} 24^{\circ}$	$\Delta^{\circ} 23^{\circ} 24^{\circ}$	
23	7 10*	10*	10*	10.0	00.0	00.3	01	.	.	$\Delta^{\circ} 0-5^{\circ} \times 0-4^{\circ} 24^{\circ} 24^{\circ} \square$		
24	6 10	10*	10*	10.0	00.0	05.2	05	.	.	$\Delta^{\circ} 0-2^{\circ} 6^{\circ} 4^{\circ} 24^{\circ} 24^{\circ} \square$		
25	7 10	020	00	04.0	03.6	08.7	20	.	.	$\times^{\circ} 0-0^{\circ} 4^{\circ} F_{ESE} 3^{\circ} 11^{\circ} \square$		
26	8 06	020	00	00.7	05.5	.	14	.	.	\square		
27	8 06	010	00	00.3	00.2	.	07	.	.	$F_{ESE} 10^{\circ} 11^{\circ} 20^{\circ} 21^{\circ} \square$		
28	8 04	040	06	06.0	02.8	.	05	.	.	$F_{ESE} 1^{\circ} 4^{\circ} 10^{\circ} 24^{\circ} \square$		
29	8 10*	09	10	05.7	00.0	00.0	02	.	.	$F_{ESE} 0-3^{\circ} 0^{\circ} 3^{\circ} 8^{\circ} \square$		
30	8 00	040	00	01.3	07.5	00.0	.	.	.	$\Delta^{\circ} 0-1^{\circ} 2^{\circ} 9^{\circ} F_{ESE} 20^{\circ} 24^{\circ}$		
MES. vred.		67.1	66.4	65.4	64.3	79.3	48.6					

1	8 03	030	00	02.0	05.2	$F_{ESE} 0-24^{\circ} F_{ESE} 23^{\circ} 3^{\circ}$		
2	8 00	020	00	00.7	07.5	$F_{ESE} 0-24^{\circ} F_{ESE} 6^{\circ} 7^{\circ} 9^{\circ} 23^{\circ} 24^{\circ}$		
3	8 00	040	00	01.3	07.3	$F_{ESE} 0-0^{\circ} 4^{\circ} F_{ESE} 3^{\circ} 2^{\circ}$		
4	7 00	09	10	06.3	02.5	$F_{ESE} 0-9^{\circ} 17^{\circ} 24^{\circ} \Delta^{\circ} 19^{\circ} 24^{\circ}$		
5	7 09	040	00	04.3	05.1	$\Delta^{\circ} 0-5^{\circ} 17^{\circ} 24^{\circ} 22^{\circ} 24^{\circ}$		
6	8 07	020	08	05.7	06.1	$\Delta^{\circ} 0-0^{\circ} 5^{\circ} 7^{\circ} 23^{\circ} 24^{\circ}$		
7	8 10	030	02	05.0	04.6	00.0	.	.	.	$F_{ESE} 2^{\circ} 1^{\circ} 1^{\circ} 2^{\circ} 24^{\circ} \square$		
8	8 00	07	09	05.3	02.2	$\Delta^{\circ} 0-0^{\circ} 9^{\circ} 24^{\circ} 24^{\circ} \square$		
9	8 02	040	06	04.0	05.8	$\Delta^{\circ} 20^{\circ} 24^{\circ} \square$		
10	7 00	09	10	06.3	04.3	$\Delta^{\circ} 10^{\circ} 11^{\circ} \square$		
11	6 08	09	04	07.6	00.0	$\Delta^{\circ} 3^{\circ} 6^{\circ} 24^{\circ} 24^{\circ} \equiv^{\circ} 14^{\circ} 17^{\circ}$		
12	7 06	050	00	03.7	05.5	$\Delta^{\circ} 0-8^{\circ} 10^{\circ} 24^{\circ} \square$		
13	7 10	10	10	10.0	06.8	00.0	.	.	.	$F_{ESE} 0-5^{\circ} 6^{\circ} 8^{\circ} 24^{\circ} \equiv^{\circ} 15^{\circ} 18^{\circ} 24^{\circ}$		
14	5 10	10	10	10.0	00.0	00.9	.	.	.	$\Delta^{\circ} 0-24^{\circ} 0^{\circ} 4^{\circ} 21^{\circ} \square$		
15	5 10	10	10	10.0	00.0	00.4	.	.	.	$\equiv^{\circ} 10^{\circ} 24^{\circ} \square$		
16	5 02	040	10	05.3	06.2	$\Delta^{\circ} 0-20^{\circ} 0^{\circ} 4^{\circ} 9^{\circ} 24^{\circ} F_{ESE} 8^{\circ} 24^{\circ} \square$		
17	7 10*	10	10	10.0	00.0	01.2	.	.	.	$F_{ESE} 0-24^{\circ} 0^{\circ} 2^{\circ} 24^{\circ} 22^{\circ} 24^{\circ} F_{ESE} 18^{\circ} 20^{\circ} 22^{\circ} 24^{\circ}$		
18	7 10	10	10	10.0	00.0	00.5	.	.	.	$\Delta^{\circ} 0-0^{\circ} 5^{\circ} 6^{\circ} 22^{\circ} 22^{\circ} 24^{\circ} F_{ESE-NW} 0-1^{\circ}, 10^{\circ} 10^{\circ} 21^{\circ} 24^{\circ}$		
19	7 10*	04	10	05.7	00.0	00.0	.	.	.	$\Delta^{\circ} 5^{\circ} 7^{\circ} 24^{\circ} \square$		
20	7 02	030	00	01.7	03.3	00.0	.	.	.	$\Delta^{\circ} 3^{\circ} 8^{\circ} F_{ESE-NW} 8^{\circ} 10^{\circ} \square$		
21	7 05	05	10	04.7	02.4	$\Delta^{\circ} 1^{\circ} 4^{\circ} 13^{\circ} \square$		
22	7 10	060	10	04.7	02.8	$\Delta^{\circ} 24^{\circ} 24^{\circ} \square$		
23	7 10	000	00	03.3	04.7	$\Delta^{\circ} 0-9^{\circ} 10^{\circ} 23^{\circ} 24^{\circ} \equiv^{\circ} 2^{\circ} 23^{\circ} 24^{\circ} 23^{\circ} 24^{\circ}$		
24	5 02	000	00	00.7	03.3	$\Delta^{\circ} 0-9^{\circ} 18^{\circ} 24^{\circ} \equiv^{\circ} 0-0^{\circ} 5^{\circ} 12^{\circ} \square$		
25	6 10**	10	00	06.7	00.0	$\equiv^{\circ} 0-0^{\circ} 5^{\circ} 12^{\circ} 24^{\circ} \equiv^{\circ} 0-0^{\circ} 5^{\circ} 12^{\circ} \square$		
26	6 00	10*	04	05.3	00.7	.	02	.	.	$\Delta^{\circ} 0-9^{\circ} * 12^{\circ} 14^{\circ} \square$		
27	7 10*	10	10	10.0	00.0	03.7	01.0	.	.	$\times^{\circ} 3^{\circ} 8^{\circ} 0^{\circ} 13^{\circ} K^{\circ} \square$		
28	7 10	020	00	04.0	03.7	01.0	.	.	.	$\Delta^{\circ} 1^{\circ} 9^{\circ} 24^{\circ} \square$		
29	6 00	000	10**	03.3	07.4	$\Delta^{\circ} 0-10^{\circ} 4^{\circ} 8^{\circ} 24^{\circ} \equiv^{\circ} 6^{\circ} 19^{\circ} \equiv^{\circ} 19^{\circ} 20^{\circ} \equiv^{\circ} 20^{\circ} 24^{\circ}$		
30	2 10**	10**	10**	10.0	00.0	00.1	.	.	.	$\Delta^{\circ} 0-10^{\circ} 5^{\circ} 12^{\circ} 24^{\circ} \equiv^{\circ} 0-12^{\circ} 14^{\circ} \square$		
31	2 10	100	100	10.0	00.0	00.0	.	.	.	$\Delta^{\circ} 0-19^{\circ} L^{\circ}, 9^{\circ} 0^{\circ} 2^{\circ} L^{\circ}, 12^{\circ} 22^{\circ} \equiv^{\circ} 6^{\circ} 8^{\circ} 19^{\circ} 24^{\circ} \equiv^{\circ} 19^{\circ} 22^{\circ}$		
MES. vred.		94.0	94.0	94.0	94.0	94.0	94.0	.	.			

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 $\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$ Gr. $\Delta G = +1h\ 17\ min.$

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D O	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm				Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	7	14	21	
1	760.5	760.1	760.7	02.4	09.2	08.4	07.1	10.0	02.3	01.0	02.1	02.2	01.4	38	26	17	27	N	10	N	7	N	5	
2	760.6	761.7	764.3	09.0	09.5	07.0	08.1	12.3	06.8	04.4	03.6	03.4	02.8	42	39	37	39	N	4	N	6	N	5	
3	765.5	764.5	764.9	05.6	09.0	05.7	06.5	09.2	05.3	03.0	02.7	03.2	02.6	40	38	38	39	N	6	N	7	N	6	
4	765.6	764.8	765.7	-00.8	09.2	00.8	02.5	09.6	-01.5	-05.5	02.9	03.7	03.7	67	42	70	62	-	0	S	2	-	0	
5	765.0	764.3	765.3	-02.4	12.4	03.4	04.2	12.6	-03.0	-06.0	03.4	03.8	03.6	88	35	61	-	0	0	N	6	-	0	
6	764.6	763.4	763.5	-00.8	12.6	02.4	04.2	12.8	-01.0	-03.6	03.8	04.7	04.6	89	43	84	72	NE	1	SSE	1	-	0	
7	761.2	758.4	757.0	-00.4	08.6	05.6	04.8	09.5	-00.6	-04.6	04.0	04.7	05.9	89	57	86	77	-	0	-	0	-	0	
8	752.6	749.2	750.2	04.6	07.0	08.4	07.1	08.6	04.6	04.2	05.6	06.5	03.7	88	87	45	73	-	0	SE	1	N	5	
9	756.6	760.6	765.9	05.4	07.0	03.7	05.0	10.6	03.3	02.0	02.6	02.6	02.3	38	35	39	37	N	6	N	6	N	5	
10	767.6	767.3	768.0	00.4	07.6	-00.8	01.6	08.6	-00.8	-03.5	01.8	02.1	03.3	39	27	76	47	NNW	2	S	2	-	0	
11	767.8	767.3	767.9	-03.6	08.8	00.2	01.4	09.8	-03.8	-07.5	02.8	02.8	03.7	79	33	79	64	-	0	-	0	-	0	
12	767.3	766.1	766.3	-01.8	10.4	03.2	03.8	10.8	-01.8	-05.0	03.4	03.5	04.7	84	37	81	67	-	0	SSE	1	-	0	
13	766.2	765.7	766.9	00.6	10.4	01.8	03.6	10.4	00.3	-03.0	03.7	04.2	04.8	77	45	92	71	-	0	-	0	-	0	
14	766.5	767.7	769.7	-01.0	13.6	02.4	04.4	14.1	-01.2	-04.2	03.9	04.6	04.9	92	40	90	74	-	0	SSE	1	-	0	
15	769.8	767.8	769.0	00.8	13.6	02.4	04.8	13.8	00.0	-03.8	03.9	04.6	04.9	81	40	90	70	-	0	SE	2	-	0	
16	767.1	765.6	765.7	-01.8	14.2	01.8	04.0	14.4	-01.8	-05.6	03.7	04.5	04.7	92	37	90	73	-	0	-	0	-	0	
17	764.4	762.7	763.3	-01.6	13.0	01.2	03.4	13.2	-02.0	-06.0	03.8	04.5	04.3	92	40	86	73	-	0	SSE	1	-	0	
18	762.4	760.4	761.3	-01.8	11.6	02.3	03.6	11.6	-01.9	-06.0	03.5	04.0	04.3	68	39	79	69	-	0	SSE	2	-	0	
19	761.0	760.6	762.6	-00.2	12.6	01.6	03.9	13.2	-01.0	-04.8	03.2	04.7	04.8	71	43	93	69	-	0	-	0	-	0	
20	763.8	763.1	763.5	-01.8	12.6	01.8	03.6	13.6	-01.8	-05.8	03.7	04.1	04.7	92	38	90	73	-	0	SE	1	-	0	
21	764.3	763.7	763.4	-02.4	12.2	02.2	03.6	12.4	-02.4	-06.2	03.4	04.5	04.5	88	42	84	71	-	0	SE	2	-	0	
22	763.5	762.3	762.7	-02.1	11.0	01.8	03.1	11.7	-02.1	-06.1	03.5	03.9	04.4	88	40	83	70	-	0	SSE	1	-	0	
23	762.5	761.1	761.4	-02.0	09.6	03.0	03.4	10.4	-02.2	-05.5	03.6	04.4	04.8	90	49	84	74	-	0	SSE	2	-	0	
24	760.9	760.3	760.9	03.4	09.4	03.6	05.0	11.1	02.2	01.1	05.1	05.3	05.4	88	60	91	80	-	0	SM	1	-	0	
25	761.5	760.9	761.9	03.4	13.4	04.4	06.4	14.4	02.4	-00.5	05.2	05.6	05.6	89	48	90	76	-	0	SE	2	-	0	
26	762.1	761.9	762.2	03.6	10.4	05.6	06.0	10.8	01.5	-02.1	05.4	05.6	05.8	91	59	88	79	-	0	-	0	-	0	
27	761.9	759.5	757.2	08.4	13.6	05.2	06.1	15.0	05.0	02.8	05.8	05.6	05.5	70	48	83	67	N	2	SSE	3	-	0	
28	751.6	747.8	749.4	05.6	08.2	06.0	06.4	08.6	04.9	00.8	06.2	07.5	06.4	92	92	92	92	-	0	-	0	NNE	1	
29	749.4	749.2	751.8	03.8	11.2	10.6	09.0	11.3	03.0	00.0	05.4	06.3	04.0	89	64	42	65	-	0	-	0	N	6	
30	755.7	755.4	757.8	07.8	13.2	07.6	09.0	13.2	06.5	02.4	03.1	03.8	03.4	39	33	43	38	NNW	4	NNE	4	N	4	
31	760.4	761.1	762.6	07.6	12.4	08.4	09.2	12.5	05.7	02.2	03.2	03.8	03.5	41	35	43	40	N	6	N	6	N	4	
MES.	WRED. 762.3			761.4	762.4	01.5	10.9	03.9	05.0	11.7	00.8	-02.3	03.8	04.3	04.3	75	45	73	64	1.3	2.2	1.3		

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1	761.1	760.3	761.8	00.0	12.8	11.3	08.8	13.0	-00.4	-03.8	03.9	04.4	03.6	86	40	36	54	-	0	SE	2	N	5
2	763.6	762.3	762.1	07.4	12.4	07.6	08.8	13.0	07.0	05.0	03.5	04.2	03.6	45	39	46	43	N	6	N	6	N	6
3	759.4	759.3	761.6	04.0	10.8	09.0	08.2	11.3	03.6	02.0	04.6	04.6	04.2	76	48	48	57	-	0	SSE	2	N	4
4	765.2	765.3	767.2	04.6	12.6	08.0	08.8	13.6	06.5	04.8	03.6	04.7	03.7	49	43	46	46	N	5	SW	2	N	4
5	767.8	766.4	766.5	01.2	12.8	09.0	08.0	13.0	00.7	-02.6	04.2	04.5	02.7	83	41	31	52	-	0	SSE	2	NM	3
6	767.1	765.7	765.4	01.2	13.0	03.4	05.2	13.7	00.5	-03.3	04.3	03.7	04.2	86	33	71	63	SE	1	SE	2	-	0
7	763.3	760.3	758.7	-01.8	12.6	04.8	05.1	13.5	-02.1	-05.6	03.5	03.7	05.0	88	34	77	66	-	0	SE	2	-	0
8	756.6	756.0	762.8	04.8	07.4	01.2	03.6	10.7	01.2	-02.0	04.0	02.5	01.6	62	32	32	42	NW	2	NNE	6	NMM	5
9	764.6	763.0	763.3	-01.2	11.0	02.2	02.0	06.6	-02.2	-04.3	01.6	02.2	02.2	38	32	56	42	N	5	S	4	-	0
10	764.0	763.1	764.1	-02.2	09.2	-00.2	00.9	09.7	-02.4	-08.8	02.2	03.0	03.1	71	34	68	58	-	0	SE	3	-	0
11	764.2	763.3	763.2	01.6	08.4	05.0	05.0	08.9	-01.6	-05.8	03.4	03.8	05.4	66	46	83	65	-	0	S	1	-	0
12	761.4	760.4	758.9	04.8	07.0	05.6	05.6	07.4	04.4	03.5	05.9	06.8	06.3	91	91	93	92	-	0	NM	2	NM	2
13	753.9	751.4	748.3	04.4	07.3	04.2	06.0	08.2	04.0	02.0	05.6	07.0	06.4	90	91	90	90	-	0	NM	3	-	0
14	748.9	750.2	752.2	04.4	06.4	04.6	05.5	07.8	04.3	03.5	06.4	06.5	05.6	89	90	88	89	WNN	1	-	0	NM	2

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 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_x = 1.2 \text{ m}$

Dan	Vrijeme O	Oblačnost N (0-10)					Insekticij broj sati	Padavina R mm	Snežni pokrival h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	9 04	03 0	10	05.7	05.7	.	.	$F_N 0^{\circ} 22^{\circ} 15^{\circ}, F_N 0^{\circ} 23^{\circ} 50^{\circ}$		
2	9 09	03 0	02	04.7	05.4	.	.	$F_N 0^{\circ} 24^{\circ} 17^{\circ}, F_N 0^{\circ} 25^{\circ} 17^{\circ}$		
3	9 01	00 0	00	00.3	06.6	.	.	$F_N 0^{\circ} 23^{\circ} 14^{\circ}, F_N 2^{\circ} 19^{\circ} 55^{\circ}$		
4	8 02	06 0	00	03.3	07.6	.	.	$F_N 0^{\circ} 23^{\circ} 14^{\circ}, F_N 0^{\circ} 23^{\circ} 14^{\circ}$		
5	9 02	04 0	00	02.0	06.2	.	.	$\Delta^{\circ} n - 7^{\circ}, F_N 0^{\circ} 23^{\circ} 14^{\circ}, F_N 11^{\circ} 43^{\circ}$		
6	9 00	00 0	00	00.0	06.6	.	.	$\Delta^{\circ} n - 8^{\circ}$		
7	8 02	08	10	06.7	02.9	.	.	$\Delta^{\circ} 2^{\circ} 9^{\circ}, 1^{\circ} 10^{\circ} 10^{\circ}, 14^{\circ} 18^{\circ}, F_N 18^{\circ} 20^{\circ}, =^{\circ} n - 19^{\circ}, F_N 19^{\circ} 24^{\circ}, F_N 20^{\circ} 23^{\circ} 55^{\circ}$		
8	5 10*	10	02	07.3	00.0	00.7	.	$F_N 0^{\circ} 23^{\circ} 14^{\circ}, F_N 0^{\circ} 23^{\circ} 14^{\circ}$		
9	9 04	02	00	02.0	06.6	09.0	.	$F_N 0^{\circ} 24^{\circ} 17^{\circ}, F_N 0^{\circ} 24^{\circ} 17^{\circ}$		
10	8 00	06 0	00	02.0	06.5	.	.	$\Delta^{\circ} 20^{\circ} 24^{\circ}, F_N 0^{\circ} 23^{\circ}$		
11	9 00	00 0	00	00.0	06.7	.	.	$\Delta^{\circ} 0^{\circ} 8^{\circ} 20^{\circ} 24^{\circ}$		
12	8 04	07 0	03	04.7	06.2	.	.	$\Delta^{\circ} 0^{\circ} 8^{\circ}$		
13	9 08	07 0	03	06.0	00.0	.	.	$\Delta^{\circ} n - 10^{\circ}, =^{\circ} 19^{\circ} n$		
14	8 00	00 0	00	00.0	06.8	.	.	$\Delta^{\circ} n - 8^{\circ}, =^{\circ} 19^{\circ} n$		
15	9 00	00 0	00	00.0	06.8	.	.	$\Delta^{\circ} n - 9^{\circ}$		
16	8 00	00 0	00	00.0	06.7	.	.	$\Delta^{\circ} n - 9^{\circ}, =^{\circ} 19^{\circ} n$		
17	9 03	02 0	00	01.7	06.2	.	.	$\Delta^{\circ} n - 8^{\circ}$		
18	8 03	02 0	00	01.7	06.8	.	.	$\Delta^{\circ} n - 9^{\circ}$		
19	9 02	03 0	00	01.7	06.8	.	.	$\Delta^{\circ} n - 8^{\circ}, =^{\circ} 19^{\circ} n$		
20	8 00	00 0	00	00.0	06.9	.	.	$\Delta^{\circ} n - 9^{\circ}$		
21	8 00	00 0	00	00.0	09.0	.	.	$\Delta^{\circ} n - 9^{\circ}, =^{\circ} 19^{\circ} n$		
22	8 00	00 0	00	00.0	06.8	.	.	$\Delta^{\circ} n - 8^{\circ}, =^{\circ} 17^{\circ} 9^{\circ}$		
23	8 00	02 0	08	03.3	08.1	.	.	$\Delta^{\circ} n - 8^{\circ}, =^{\circ} 17^{\circ} 9^{\circ}$		
24	6 08	07	06	07.0	01.4	.	.	$\Delta^{\circ} 0^{\circ} 8^{\circ}, =^{\circ} 14^{\circ} n$		
25	8 10	03 0	01	04.7	07.1	.	.	$\Delta^{\circ} 0^{\circ} 8^{\circ}, =^{\circ} 17^{\circ} 9^{\circ}$		
26	6 10	09	08	09.0	00.7	.	.	$\Delta^{\circ} n - 8^{\circ}, =^{\circ} 10^{\circ} 16^{\circ}, \Delta^{\circ} 10^{\circ} n, =^{\circ} 19^{\circ} n$		
27	9 10	02 0	03	05.0	07.8	.	.	$\Delta^{\circ} 0^{\circ} 8^{\circ}, =^{\circ} 10^{\circ} 16^{\circ}, R 12^{\circ} 16^{\circ}, =^{\circ} n - 17^{\circ}$		
28	6 10*	10 0	05	08.3	00.0	03.4	.	$F_N 20^{\circ} 24^{\circ}, F_N 23^{\circ} 23^{\circ}$		
29	8 02	07	05	04.7	02.1	20.0	.	$F_N 0^{\circ} 24^{\circ}, F_N 0^{\circ} 24^{\circ}$		
30	8 00	05 0	00	01.7	04.8	.	.	$F_N 0^{\circ} 23^{\circ} 20^{\circ} 20^{\circ}, F_N 2^{\circ} 14^{\circ} 05^{\circ}$		
31	9 02	00 0	00	00.7	09.3	.	.			
MES.	VRED.	03.4	03.5	02.1	03.0	199.1	41.3			

1	8 00	03 0	00	01.0	09.2	.	.	$\Delta^{\circ} n - 8^{\circ}, F_N 18^{\circ} 23^{\circ}$		
2	8 00	00 0	00	00.0	09.2	.	.	$F_N 0^{\circ} 22^{\circ} 17^{\circ}, F_N 1^{\circ} 3^{\circ} 5^{\circ}$		
3	8 09	06 0	08	07.7	01.8	.	.	$F_N 17^{\circ} 23^{\circ}$		
4	8 07	02 0	00	03.0	07.2	.	.	$F_N 0^{\circ} 21^{\circ} 45^{\circ}$		
5	8 00	00 0	00	00.0	09.5	.	.	$\Delta^{\circ} n - 8^{\circ}$		
6	8 00	00 0	00	00.0	09.5	.	.	$\Delta^{\circ} n - 7^{\circ} 40^{\circ}$		
7	8 00	00 0	00	00.0	09.5	.	.	$\Delta^{\circ} n - 8^{\circ}, =^{\circ} 20^{\circ} n$		
8	8 01	01 0	00	00.7	09.4	.	.	$\Delta^{\circ} 0^{\circ} 1^{\circ} n - 8^{\circ}, F_N 9^{\circ} 24^{\circ}, F_N 11^{\circ} 21^{\circ}$		
9	8 00	00 0	00	00.0	09.7	.	.	$F_N 0^{\circ} 14^{\circ} 21^{\circ}$		
10	9 00	00 0	00	00.0	09.7	.	.	$\Delta^{\circ} n - 9^{\circ}$		
11	8 10	10	10	10.0	00.7	.	.	$\Delta^{\circ} 19^{\circ} 21^{\circ}$		
12	8 10	10	10	10.0	00.0	00.0	.	$\Delta^{\circ} 15^{\circ} 17^{\circ}$		
13	8 10*	10	10	10.0	00.0	02.0	.	$\Delta^{\circ} 1^{\circ} 15^{\circ} 30^{\circ}, =^{\circ} 1^{\circ} 2^{\circ} 19^{\circ} n$		
14	5 10*	10	10	10.0	00.0	06.4	.	$\Delta^{\circ} 5^{\circ} 10^{\circ}, =^{\circ} 1^{\circ} 2^{\circ} 19^{\circ} n, =^{\circ} n - n i$		
15	8 10	09	03	07.3	02.7	19.4	.			
16	8 10	10	10	10.0	00.0	05.2	.	$\Delta^{\circ} 13^{\circ} 9^{\circ}, F_N 6^{\circ} 22^{\circ} 7^{\circ}, F_N 17^{\circ} 25^{\circ} 24^{\circ}, F_N 18^{\circ} 24^{\circ}$		
17	7 10*	09	00	04.3	00.8	00.6	.	$\Delta^{\circ} 5^{\circ} 9^{\circ}, =^{\circ} n - 10^{\circ}, F_N 0^{\circ} 24^{\circ}, F_N 0^{\circ} 19^{\circ} 30^{\circ}$		
18	9 00	00 0	00	00.0	10.0	00.1	.	$F_N 0^{\circ} 3^{\circ} 41^{\circ}$		
19	9 00	00 0	00	02.7	10.0	.	.	$\Delta^{\circ} n - 8^{\circ}, =^{\circ} 18^{\circ} n$		
20	6 10	10	10	10.0	00.0	.	.	$\Delta^{\circ} 9^{\circ} 14^{\circ}, =^{\circ} 10^{\circ} 16^{\circ}, 19^{\circ} n, F_N 13^{\circ} 24^{\circ}, F_N 14^{\circ} 24^{\circ}$		
21	9 10	09	04	07.7	02.1	00.0	.	$F_N 0^{\circ} 24^{\circ}, F_N 0^{\circ} 24^{\circ}$		
22	9 02	00 0	00	00.7	10.0	.	.	$F_N 0^{\circ} 24^{\circ}, F_N 0^{\circ} 7^{\circ} 10^{\circ} 24^{\circ}$		
23	9 00	00 0	04	01.3	10.1	.	.	$F_N 0^{\circ} 24^{\circ}, F_N 0^{\circ} 6^{\circ} 10^{\circ} 24^{\circ}$		
24	9 00	04 0	00	01.3	09.9	.	.	$F_N 0^{\circ} 13^{\circ} 10^{\circ} 24^{\circ}$		
25	9 00	00 0	00	00.0	10.2	.	.	$F_N 0^{\circ} 0^{\circ} 7^{\circ} 10^{\circ} 24^{\circ}, F_N 17^{\circ} 25^{\circ} 17^{\circ} 22^{\circ} 23^{\circ}$		
26	9 02	03 0	00	01.7	00.3	.	.	$F_N 0^{\circ} 5^{\circ} 10^{\circ} 24^{\circ}, F_N 0^{\circ} 2^{\circ} 0^{\circ} 15^{\circ} 16^{\circ} 20^{\circ} 24^{\circ}$		
27	9 01	00 0	00	00.3	10.2	.	.	$F_N 0^{\circ} 2^{\circ} 10^{\circ}, F_N 0^{\circ} 13^{\circ} 10^{\circ}, F_N 17^{\circ} 15^{\circ} 17^{\circ} 50^{\circ}$		
28	9 00	00 0	00	00.0	10.4	.	.	$F_N 0^{\circ} 5^{\circ} 20^{\circ}$		
MES.	VRED.	04.0	03.8	03.1	03.6	188.1	33.7			

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 $\varphi = 42^\circ 26' \text{ N } \lambda = 19^\circ 17' \text{ E}$ Gr. $\Delta G = + 1 \text{h} 17 \text{ min.}$

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EG	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, I (0-12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	762.1	761.3	762.5	-01.4	14.2	04.6	05.5	14.6	-01.6	-05.6	03.1	04.0	03.5	77	33	55	55	-	0	S 2	- 0	
2	764.1	763.3	763.3	01.0	14.8	05.6	06.8	15.0	00.5	-04.0	03.1	04.3	04.4	63	34	64	54	-	0	S 3	- 0	
3	762.2	759.1	758.8	03.7	16.4	08.4	09.2	17.2	02.4	-02.1	03.9	05.7	05.8	66	41	70	59	-	0	ESE 3	- 0	
4	757.5	756.1	756.7	06.5	15.6	10.3	10.7	17.3	06.0	01.8	05.3	05.7	07.3	73	43	70	65	-	0	SSE 3	ENE 1	
5	757.3	758.3	760.0	08.0	10.0	08.8	08.9	11.2	07.7	05.2	07.3	08.1	07.6	91	88	90	90	-	0	N 1	- 0	
6	760.6	759.3	758.8	06.6	17.6	12.0	12.0	18.3	05.2	01.5	05.7	06.4	06.4	79	43	78	67	NW 2	- 0	- 0	- 0	
7	759.5	759.3	759.1	10.0	21.6	12.6	14.2	23.0	09.8	07.0	36.6	06.7	06.3	72	35	57	55	NNE 1	ESE 2	- 0	- 0	
8	758.2	755.1	752.9	09.8	21.2	11.0	13.2	23.3	09.2	04.5	05.6	06.6	07.6	55	35	77	56	N 1	- 0	- 0	- 0	
9	750.5	748.7	747.4	08.6	16.0	11.2	11.8	18.2	07.4	04.4	06.7	06.9	07.9	80	50	80	70	- 0	SE 4	- 0	- 0	
10	745.5	746.3	750.6	08.8	16.3	10.2	11.4	16.8	08.2	05.6	07.4	06.7	08.2	88	48	88	75	- 0	- 0	ESE 1	- 0	
11	756.1	759.6	759.9	09.4	12.7	08.8	09.9	13.0	08.3	07.5	07.1	07.9	06.1	81	71	72	75	- 0	- 0	C	- 0	
12	757.0	756.0	756.3	08.5	14.8	13.8	12.7	15.7	06.5	02.5	25.1	08.3	09.4	61	66	79	69	NNE 3	SSE 5	ESE 4	- 0	
13	756.1	753.9	752.2	11.0	16.8	14.0	14.0	18.5	10.9	08.0	08.7	08.1	05.7	88	57	47	64	- 0	N 2	NNW 3	- 0	
14	749.2	751.5	755.5	11.2	12.2	08.6	10.2	15.0	08.5	09.6	07.8	07.7	06.7	79	72	80	77	- 0	SSE 4	- 0	- 0	
15	757.7	757.8	757.5	09.0	14.0	09.7	10.6	15.8	08.0	04.1	06.8	06.5	07.4	79	55	82	72	WNW 2	ESE 5	- 0	- 0	
16	756.2	755.5	755.1	08.4	11.3	07.8	08.8	13.8	07.1	03.4	06.8	06.4	06.9	82	64	87	78	- 0	- 0	- 0	- 0	
17	753.5	752.5	753.2	07.6	10.0	07.0	07.9	12.0	06.3	02.6	06.8	08.1	06.8	87	88	91	89	- 0	SSE 2	- 0	- 0	
18	754.2	754.6	755.4	06.8	11.0	08.2	08.6	13.0	06.0	02.8	06.7	06.5	07.3	91	66	90	82	- 0	WSM 2	- 0	- 0	
19	755.1	753.2	751.2	07.8	17.6	13.6	13.2	18.6	07.6	04.3	06.9	06.5	07.6	87	43	65	65	- 0	- 0	- 0	- 0	
20	751.1	751.6	753.2	10.8	16.8	13.2	14.0	19.5	10.8	06.5	09.9	07.6	08.3	71	47	73	64	- 0	C	N 4	- 0	
21	751.7	749.0	751.5	09.6	16.4	08.4	10.7	18.0	08.3	06.0	07.9	07.0	05.1	88	50	62	67	- 0	WSW 2	NNE 6	- 0	
22	752.5	751.2	751.1	06.2	07.0	04.0	05.3	13.2	04.0	03.9	02.5	02.8	03.1	35	37	51	41	N 2	NNE 8	NNW 7	- 0	
23	750.0	748.6	746.1	04.8	11.2	06.4	07.2	11.6	04.0	03.2	03.5	05.0	04.7	54	50	65	56	NE 2	SW 2	- 0	- 0	
24	745.2	745.2	745.2	05.4	04.2	05.7	05.2	07.6	04.0	00.6	06.0	05.6	06.2	89	91	90	90	NW 2	NW 3	NNW 1	- 0	
25	747.6	747.8	752.0	05.1	10.4	04.5	06.1	12.5	04.5	02.8	05.4	04.0	05.0	79	43	80	67	N 2	S 2	- 0	- 0	
26	755.8	754.8	755.7	05.6	13.4	06.6	08.0	13.8	04.0	-01.2	02.3	03.3	04.2	34	25	58	40	NNE 3	S 4	SE 2	- 0	
27	755.8	756.2	756.8	06.4	07.0	06.6	06.6	10.2	02.6	-01.5	04.9	05.9	06.5	68	79	89	79	- 0	NNW 2	- 0	- 0	
28	751.9	751.5	750.4	07.8	10.3	10.4	09.7	12.1	06.0	05.8	07.9	08.6	08.3	100	92	86	93	- 0	NW 4	NNE 2	- 0	
29	750.4	753.0	753.9	13.0	17.6	14.0	14.6	18.5	10.1	09.5	16.0	08.8	10.2	89	58	85	77	ESE 4	SE 4	- 0	- 0	
30	752.7	749.0	748.7	10.6	22.0	14.4	15.4	22.7	09.0	05.3	08.5	07.6	07.9	86	38	64	63	- 0	- 0	- 0	- 0	
31	748.4	750.2	753.7	13.7	18.0	16.0	15.9	20.7	11.2	06.9	07.9	10.9	10.7	67	70	79	72	N 1	SW 5	SE 3	- 0	
MES.	VRED.	754.4	753.8	754.3	07.8	14.2	09.6	10.3	15.8	06.5	03.6	06.1	06.6	06.8	76	55	75	68	1.0	2.4	1.1	- 0

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1	752.3	753.7	754.9	14.0	15.7	13.3	14.1	18.0	12.6	10.0	10.6	10.9	11.3	88	81	99	89	-	C	ESE 4	- 0	
2	751.6	752.1	752.8	12.4	14.0	11.4	12.3	16.0	11.4	11.2	10.0	09.5	09.1	92	79	90	87	W 3	SSW 3	SE 5	- 0	
3	754.2	756.9	757.9	07.6	10.0	08.6	08.7	12.4	07.4	07.3	06.8	07.7	07.2	87	83	86	85	-	0	- 0	- 0	
4	758.9	760.0	760.8	10.6	16.0	10.4	11.8	16.5	03.2	06.3	07.8	07.5	08.3	81	55	88	75	SE 5	S 4	- 0	- 0	
5	761.1	760.7	761.7	09.4	21.3	14.0	14.7	22.1	07.8	03.9	07.8	06.6	08.1	88	35	68	64	-	0	SE 4	- 0	- 0
6	762.1	759.6	759.3	12.2	25.7	14.5	16.7	26.0	09.2	05.0	07.4	09.1	08.1	70	37	65	57	-	0	- 0	- 0	- 0
7	757.7	756.1	755.1	12.7	24.0	15.0	16.7	25.2	10.5	06.2	07.9	06.5	07.5	71	29	59	53	-	0	SSE 3	- 0	- 0
8	754.6	756.7	757.9	17.0	13.0	09.8	12.4	18.7	08.5	08.0	09.0	07.9	07.5	62	71	82	72	SE 5	ESE 4	- 0	- 0	
9	759.2	757.8	757.3	09.5	17.5	12.7	13.1	18.6	05.9	01.4	06.5	06.8	07.2	73	46	65	61	-	0	WSM 5	- 0	- 0
10	751.8	749.4	749.2	12.0	11.0	12.2	11.8	14.0	11.0	07.0	06.5	08.7	08.1	61	88	76	75	-	0	NNW 2	WSM 2	- 0
11	755.4	757.5	759.6	09.0	13.4	10.6	10.6	17.8	07.6	04.4	05.3	05.3	06.6	64	46	72	60	-	0	WSW 2	NW 2	- 0
12	760.0	760.2	762.1	08.0	10.8	06.0	07.7	11.4	05.0	01.0	06.0	05.8	06.0	75	60	86	74	-	0	NNW 3	- 0	- 0
13	763.4	761.9	761.2	05.0	14.2	09.4	09.5	15.7	02.3	-01.2	05.6	06.0	07.3	86	49	83	73	-	0	NNW 3	- 0	- 0
14	761.3	759.3	758.5	08.3	17.4	11.2	12.1	19.4	05.0	00.9	07.0	07.8	07.4	64	52	74	70	-	0	NW 3	- 0	- 0
15	757.3	754.4	753.4	10.2	20.4	12.6	14.0	21.1	06.4	02.6	06.9	07.5	07.7	74	42	70	62	-	0	NNW 4	- 0	- 0
16	751.4	748.8	749.1	10.6	19.2	13.8	14.4	20.5	06.8	03.6	06.7	06.2	07.8	70	37	66	58	-				

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_k = 1.2 \text{ m}$$

Dan	Vrijednost 0.9	Oblačnost N (0-10)					Insekcija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	9	00	000	00	00.0	10.5	.	.	✓ ⁿ⁻⁹ , ^{20°n}	
2	9	02	020	00	01.3	10.2	.	.	✓ ^{n-7.50}	
3	9	04	060	10	06.7	10.1	.	.		
4	8	08	080	08	08.0	04.3	.	.	△ ⁰ ²⁻⁸ , ^{20°n}	
5	8	10	100	07	09.0	00.0	02.1	.	● ⁰ ^{32-7.5} , ^{14.50-19.50}	
6	9	04	080	10	07.3	05.8	08.6	.	△ ⁰⁻¹⁻² , ^{12°n}	
7	9	09	060	05	06.7	04.6	.	.	△ ⁰⁻⁸ , ^{12°n}	
8	9	05	06	03	04.7	03.0	.	.		
9	9	06	10	10	08.7	05.2	.	.	✓ ^{14.50-14.55} , ^{0-1-17.50-24 = 16.50} n	
10	7	09	09	100	09.3	00.4	.	.		
11	8	10	10	04	08.0	00.0	14.5	.	● ⁰⁻¹ ⁰⁻² , ^{7.50-10.45}	
12	8	10	10	08	09.3	01.2	02.4	.	● ⁰ ^{12-12.5} , ^{FSE-S 13.51-16.35-22.00-22.40} ; E-S-E-S 13.20-14.30;	
13	6	08	10	10	09.3	02.3	00.4	.	= ^{07-16.0-2-3.5} , ^{FUN-E 16.34-16.35}	
14	7	10	100	05	08.3	00.1	.	.	= ^{0-18.50-17.50} , ^{FSE-S-E-UNW 2.50-3.25} ; 8.45-9.25-12.55-13.55-17.25-17.40; 8.30-8	
15	8	07	08	00	05.0	05.3	29.1	.	● ^{0-10.50-5.40} , ^{FSE-S-E 13.30-14.1} , ^{△-9.95-n}	
16	8	09	080	02	06.3	03.4	.	.	● ^{19.45-12} , ^{△-n-9}	
17	9	08	100	07	04.3	01.5	03.0	.	● ⁰ ^{10.05-17.15} , ^{FNNW 15.40-15.40}	
18	8	10	100	10	10.0	01.6	04.0	.	● ^{0-19.5-10.25} , ^{FSE-S-E 14.19-n}	
19	9	07	09	06	07.3	03.8	00.4	.		
20	9	05	090	07	07.0	00.9	.	.	△ ² ^{n-7.50} , ^{FSE-S-E 14.19-n}	
21	9	08	08	100	08.7	03.1	.	.	△ ⁿ⁻⁸ , ^{0-18.5-22.0} , ^{FN 20.50-n} , ^{F ~ 20.50-n}	
22	8	08	10	10	09.3	02.0	07.7	.	FNN-E 14.20-Fn-20i	
23	9	10	070	06	07.7	05.6	.	.	FNN-E 2.40-3.50	
24	6	10	100	100	10.0	00.2	01.0	.	● ^{0-2-4.50-8.00-22.30} , ¹⁰⁻ⁿ	
25	8	06	08	03	05.7	05.5	13.3	.	● ^{0-16-6.85-14.40} , ¹⁰⁻¹⁹⁻ⁿ	
26	9	00	040	00	01.3	10.8	.	.	△ ^{20°n}	
27	7	10	100	10	10.0	08.3	.	.	● ^{0-1-2-13.50-14.10-19.50} , ⁿ	
28	7	100	100	100	10.6	08.0	14.9	.	● ^{1-2-17-14.10-19.50} , ⁿ	
29	8	100	09	06	08.2	01.8	30.3	.	● ^{0-10-9.5} , ^{FSE 14.45-14.50}	
30	9	07	070	06	06.7	08.3	01.4	.	△ ² ⁸	
31	7	10	100	10	10.0	00.0	.	.	● ^{13.50-14.17.5-18.45} , ^{= n-11.20, T-17.40-17.50, 6-18-n, 2-n-8.50}	

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1	7	10	100	100	10.0	00.0	00.0	.	
2	7	100	10	100	10.0	01.9	00.3	.	
3	7	100	10	100	01.3	15.6	.		
4	8	100	070	00	05.7	03.0	18.9	.	
5	8	090	080	06	07.7	07.6	01.4	.	
6	8	030	070	03	04.3	08.8	.		$\Delta^{0-1} n-8^{\circ} 19^{\circ} 0^{\circ} n$
7	8	060	040	05	04.3	04.8	.		$\Delta^{0-1} n-8^{\circ} 19^{\circ} 0^{\circ} n$
8	8	08	040	00	04.7	05.3	.		$F_{\text{NE}} 3^{\circ} 4^{\circ} 4^{\circ} 12^{\circ} ; F_{\text{SE}} 9^{\circ} 20^{\circ} 12^{\circ} ; \Delta^{0-1} 10^{\circ} 13^{\circ} , \Delta 19^{\circ} n$
9	8	010	000	05	02.0	12.4	02.0	.	$\Delta^{0-1} n-9^{\circ} 19^{\circ} 0^{\circ} n$
10	7	10	100	06	08.7	00.0	.	.	$\bullet^{0-1} 17^{\circ} 19^{\circ} 0^{\circ} ; F_{\text{SW-W}} 17^{\circ} 18^{\circ} 21^{\circ} 21^{\circ} 0^{\circ}$
11	8	050	070	04	05.3	05.2	37.4	.	$=^{n-10^{\circ}} \Delta^{+2} 8^{\circ} 10^{\circ} 0^{\circ}$
12	7	07	10	00	05.7	00.4	01.1	.	$\Delta^{0-1} n-8^{\circ} 10^{\circ} 41^{\circ} 14^{\circ} -17^{\circ} 20^{\circ} ; F_{\text{ENE}} 10^{\circ} 5^{\circ} 10^{\circ} 0^{\circ} \Delta 19-24$
13	8	000	08	00	02.7	10.4	03.2	.	$\Delta^{0-10^{\circ}} 8^{\circ} 19^{\circ} 0^{\circ} n$
14	8	000	000	00	00.0	12.2	.	.	$\Delta^{2-12^{\circ}} 9^{\circ} 19^{\circ} 0^{\circ} n$
15	8	02	000	00	00.7	12.3	.	.	$\Delta^{2-12^{\circ}} n-8^{\circ} 20-0^{\circ} n$
16	8	060	070	07	04.7	03.0	.	.	$\Delta^{1} n-8^{\circ} 0^{\circ}$
17	8	07	040	03	04.7	10.2	.	.	$F_{\text{NNE}} 5^{\circ} 23^{\circ} ; F_{\text{NNE}} 9^{\circ} 20^{\circ} -17^{\circ} 0^{\circ}$
18	8	010	010	01	01.0	12.0	.	.	$F_{\text{N-NNE}} 1^{\circ} 20^{\circ} 17^{\circ} 0^{\circ} ; 20^{\circ} 22^{\circ} ; F_{\text{NNE}} 8^{\circ} 30^{\circ} 8^{\circ} 35^{\circ}$
19	8	000	000	00	00.0	12.4	.	.	$F_{\text{N}} 3-3^{\circ} 4$
20	8	000	000	00	00.0	12.4	.	.	$F_{\text{NNE}} 1^{\circ} 4$
21	8	000	020	03	01.7	12.8	.	.	$\Delta^{19^{\circ} 20^{\circ} 0^{\circ}}$
22	8	000	050	08	04.3	12.4	.	.	$F_{\text{NNE}} 23^{\circ} 23^{\circ} 0^{\circ}$
23	8	070	070	10	06.0	07.1	.	.	$F_{\text{NNE}} 3^{\circ} 12^{\circ} 0^{\circ} 16^{\circ} 22^{\circ} ; F_{\text{NNE}} 8^{\circ} -8^{\circ} 20^{\circ}$
24	7	08	10	09	04.0	00.8	.	.	$F_{\text{NNE}} 8^{\circ} 2^{\circ} 9^{\circ} 20^{\circ} ; F_{\text{NNE}} 2^{\circ} 16^{\circ} -23^{\circ} ; \Delta 16^{\circ} 20^{\circ} -16^{\circ} 35^{\circ} ; T 16^{\circ} 20^{\circ} 17^{\circ}$
25	8	090	070	100	08.7	04.7	.	.	
26	8	06	07	07	04.7	10.1	05.3	.	$F_{\text{NNE}} 7^{\circ} 50^{\circ} 18^{\circ} ; F_{\text{NNE}} 10^{\circ} -16^{\circ} 20^{\circ}$
27	7	10	10	07	09.0	04.0	.	.	$F_{\text{NNE}} 0^{\circ} 4^{\circ} 17^{\circ} 0^{\circ}$
28	8	060	050	00	03.7	12.4	.	.	$F_{\text{NNE}} 4^{\circ} 45^{\circ} 19^{\circ} 0^{\circ} ; F_{\text{NNE}} 11^{\circ} 4^{\circ} 12^{\circ} 0^{\circ}$
29	8	000	000	00	00.0	13.0	.	.	
30	8	000	030	06	01.0	12.2	.	.	

$\varphi = 42^\circ 26' \text{ N } \lambda = 19^\circ 17' \text{ E}$ Gr. $\Delta G = + 1 \text{h} 17 \text{ min.}$

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d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm				Relativna vlažnost u %				Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	7	14	21	
1	758.6	756.8	758.4	13.6	24.4	21.0	20.0	25.0	09.5	05.8	09.1	09.4	06.5	78	41	35	51	-	0	SE	2	NNE	5	
2	757.8	756.9	756.1	17.0	19.2	16.5	17.3	21.9	16.5	12.7	06.8	06.6	07.1	47	39	50	45	WSW	3	NNE	6	-	0	
3	754.1	752.1	752.8	17.8	21.6	17.6	18.6	23.0	15.3	12.6	07.1	07.6	08.3	47	39	55	47	NNW	4	NNW	3	-	0	
4	755.1	755.7	758.1	15.4	22.4	16.3	17.6	22.6	14.4	12.1	09.3	07.4	07.1	71	36	51	53	NNE	2	SSE	5	-	0	
5	759.1	758.7	759.4	15.4	22.7	16.3	17.7	23.5	11.6	07.2	07.1	07.8	07.3	54	38	53	48	N	2	SSE	3	-	0	
6	758.5	758.0	758.2	17.3	23.3	19.8	20.0	25.5	13.5	09.0	09.0	07.1	10.7	60	33	62	52	-	0	SW	4	E	3	
7	758.6	756.1	755.3	15.2	21.2	17.2	17.7	23.5	15.0	12.9	11.9	13.0	12.9	92	69	88	83	-	0	SSE	3	-	0	
8	754.6	754.1	754.5	17.4	18.5	16.4	17.2	20.2	15.8	13.6	12.9	13.1	12.1	87	82	86	85	-	0	SE	3	-	0	
9	755.0	755.5	757.8	15.1	21.8	15.0	16.7	22.3	13.9	10.4	11.2	09.3	10.0	87	47	78	71	-	0	SE	5	SE	2	
10	758.3	756.9	756.7	14.4	22.8	17.4	18.0	23.5	10.0	06.5	09.3	07.8	10.3	76	38	69	61	-	0	SE	4	-	0	
11	756.7	753.3	752.9	15.8	25.0	18.8	19.6	26.4	11.2	07.5	09.1	08.3	11.4	68	35	70	58	-	0	SSE	3	-	0	
12	751.2	750.8	749.8	16.5	20.6	15.6	17.1	23.1	13.4	09.5	09.5	11.3	11.2	67	62	84	71	-	0	SE	2	N	1	
13	749.1	748.4	749.3	14.4	17.0	14.0	14.8	19.4	14.0	12.9	10.3	12.5	10.2	84	86	85	85	NNW	3	-	0	-	0	
14	748.7	749.5	750.6	13.6	14.4	13.5	13.8	16.5	13.0	13.1	10.9	10.5	10.7	94	86	92	91	-	0	-	0	-	0	
15	751.4	751.4	752.9	14.7	21.4	16.9	17.5	23.0	11.1	08.3	10.1	10.5	12.1	81	55	84	73	-	0	SSE	4	-	0	
16	754.4	753.8	755.2	15.8	23.6	18.2	19.0	25.0	12.4	10.0	12.1	12.7	13.1	90	58	84	77	-	0	SE	4	-	0	
17	756.4	755.3	757.0	19.0	26.0	19.2	20.8	27.0	15.7	13.3	13.0	13.6	14.0	79	54	84	72	-	0	SSE	3	-	0	
18	758.5	757.0	756.8	19.0	29.0	21.6	22.8	29.5	15.5	13.0	14.5	12.1	11.7	88	40	60	63	-	0	SE	4	MNW	1	
19	759.3	757.8	759.7	22.6	29.6	22.5	24.5	30.0	18.0	12.9	09.9	09.1	10.6	48	29	51	43	-	0	SSE	3	SE	5	
20	758.7	757.0	756.9	20.8	29.0	22.2	23.6	30.0	15.6	13.0	12.1	11.8	12.8	65	39	64	56	-	0	SE	1	-	0	
21	757.7	756.1	757.5	21.2	28.5	17.6	21.2	29.6	16.1	14.4	10.4	10.1	14.0	55	35	92	61	NW	2	SW	2	WNN	2	
22	757.9	756.1	756.4	19.3	26.1	21.2	22.0	27.0	15.6	12.9	11.3	12.9	11.6	67	51	61	60	N	1	S	3	S	3	
23	756.0	754.0	753.8	20.2	27.0	20.1	21.8	27.4	16.0	13.5	11.5	11.0	10.2	65	41	58	55	-	0	SE	4	-	0	
24	752.6	750.0	751.2	19.0	27.0	21.2	22.1	28.4	17.2	14.3	13.1	11.6	11.0	80	43	58	60	-	0	WSW	1	-	0	
25	752.4	750.9	752.2	20.2	28.8	21.9	23.2	29.4	16.0	12.6	17.1	12.0	13.5	96	41	69	69	NW	3	SE	2	-	0	
26	755.0	754.2	755.8	20.8	27.6	21.0	22.6	27.6	15.5	12.0	10.0	11.0	13.0	54	40	69	54	-	0	SW	4	SSE	3	
27	756.2	756.6	757.0	19.2	21.4	17.0	18.6	23.4	16.6	14.2	12.6	10.9	12.6	75	57	87	73	-	0	NW	3	-	0	
28	757.0	756.6	757.6	17.4	20.0	16.5	17.6	22.5	14.2	12.0	12.4	13.0	12.0	83	74	86	81	-	0	SE	2	-	0	
29	757.5	756.2	756.5	16.6	25.4	19.3	20.2	26.5	13.0	10.9	11.3	11.1	12.5	80	45	75	67	-	0	SSE	4	S	2	
30	756.2	755.5	753.8	16.8	25.6	21.3	21.2	26.5	15.3	12.2	11.9	11.7	12.4	83	47	65	65	NW	1	SE	3	-	0	
31	755.2	755.4	755.1	21.0	26.1	20.4	22.0	27.0	15.7	11.5	11.7	11.7	12.3	63	46	68	59	-	0	SSE	5	-	0	
MES.	VRED.	755.7	755.4	755.4	17.5	23.6	18.5	19.6	25.0	14.4	11.5	10.9	10.6	11.1	73	49	70	64	0.7	3.1	0.9			

1	755.1	754.0	754.1	22.7	28.7	21.9	23.8	29.7	16.8	13.1	11.5	11.6	10.3	56	39	52	49	-	0	SSW	4	-	0
2	752.8	750.9	750.9	22.0	30.4	23.2	24.7	31.4	17.5	13.0	12.0	14.0	12.2	61	43	57	54	NE	3	SE	2	-	0
3	751.0	750.5	751.3	20.6	24.0	20.1	21.2	25.5	16.6	12.6	12.7	13.2	12.3	70	59	70	66	-	0	NE	1	ESE	1
4	752.4	753.4	754.5	19.6	17.0	17.2	17.8	25.7	15.0	11.4	10.8	10.6	10.3	63	73	70	69	-	0	NE	6	N	6
5	756.2	756.0	756.6	16.0	20.1	15.7	16.9	21.2	15.6	14.0	07.9	08.4	06.7	58	48	50	52	NNE	5	NNE	5	NNE	5
6	755.4	755.7	756.5	15.2	18.4	17.0	16.9	21.7	13.9	11.7	05.9	06.1	05.9	46	39	41	42	NNE	6	N	8	NNE	6
7	755.6	755.3	756.5	17.6	19.9	17.0	17.9	22.0	15.6	12.1	06.0	06.6	06.8	40	38	47	42	NNE	6	NNE	7	NNE	6
8	755.3	756.0	757.2	16.6	19.4	15.0	16.5	22.1	15.0	13.4	07.6	10.2	11.9	54	60	93	69	NE	1	SSW	4	SE	4
9	757.2	757.0	755.5	15.2	18.4	15.6	16.0	21.8	14.2	12.7	10.9	12.2	12.0	90	77	90	86	SE	3	NW	3	-	0
10	754.8	753.9	755.5	17.2	24.0	18.4	19.5	26.1	13.4	10.2	09.3	08.6	09.4	63	38	59	53	N	2	S	4	-	0
11	757.5	757.2	758.6	17.2	25.4	20.6	21.0	26.8	13.8	10.4	11.2	11.5	13.9	76	47	76	66	-	0	SE	3	-	0
12	758.3	756.8	756.6	21.2	28.0	23.2	23.9	28.5	16.6	13.4	13.0	09.9	12.7	69	35	60	55	NW	2	SSM	3	NNE	3
13	757.1	755.4	755.3	22.2	29.2	20.6	23.2	29.7	18.2	15.2	13.4	12.9	10.0	67	43	55	55	-	0	SW	3	-	0
14	755.7	754.3	755.0	21.1	26.6	22.6	23.7	30.4	16.4	12.1	08.7	09.3	12.9	46	32	63	47	N	2	WNN	2	-	0
15	755.9	754.4	754.6	21.6	32.1																		

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Iseljacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	9	00 0	03 0	04	02.3	10.6	.	.	.	F NNE 20° 22
2	8	10	10	06	08.7	03.0	.	.	.	F NNE 10° 16°, 20° 20°; F NNE 10° 12°
3	9	07 0	06 0	07	06.7	02.6	.	.	.	9 11 12 13
4	9	09	04 0	00	04.3	07.9	00.0	.	.	5 5 5 5
5	9	09 0	06 0	05	06.7	04.9	00.0	.	.	.
6	8	00 0	10	09	06.3	05.5	.	.	.	0-1 4 3 9 30 20-n
7	9	10 0	06 0	05	07.0	04.1	03.2	.	.	0-4 13 19 35 21 30
8	7	10	10	10 0	10.0	00.0	02.5	.	.	0-2 20 20 10 30 19 35 10, 18 9 4 10, F 336 14 05 17 50, 19 40 n
9	9	03 0	03 0	01	02.3	09.2	02.7	.	.	0-1 7 16 40 20 0 8
10	9	06 0	03 0	00	03.0	12.9	00.4	.	.	0-1 n-8
11	9	02 0	04 0	06	04.0	11.7	.	.	.	0-1 17 19 30 22 23
12	8	08	10	10	09.3	01.5	.	.	.	0-2 2 30 4 30 8 50 10 40 13 20 17 24
13	7	10	10	10 0	10.0	00.7	06.1	.	.	0-1 9 16 40 20
14	7	10 0	10 0	06	08.7	00.0	17.4	.	.	0-2 20 0 7
15	9	01 0	08	02	03.7	08.7	02.4	.	.	0-1 n-8
16	9	08	03 0	00	03.7	10.2	.	.	.	0-1 n-7 30 19 35 n, 1 n - 8 30
17	9	02 0	04 0	04	03.3	11.3	.	.	.	0-1 n-8 14 14 15
18	9	06 0	06 0	03	05.0	10.5	.	.	.	18 1-2 19 10 20 3 20 45 20 45 18 1-2 19 10 20 45
19	9	00 0	04 0	08 0	04.0	12.5	.	.	.	0-1 n-8
20	9	00 0	06 0	00	02.0	12.3	00.7	.	.	0-1 n-8
21	9	02 0	04 0	03	03.0	10.7	.	.	.	T 12 45 18 55 18 2 16 25 17 15, 8 16 30 16 55 18 15, 1 17 45 17 40 17 45 17 45 18 35 F NNE
22	9	00 0	03 0	10	04.3	12.7	20.6	.	.	0-1 8 20 0 20 45 n
23	9	03 0	04 0	04	03.7	10.6	.	.	.	0-1 n-8 1
24	9	10	04 0	07	07.0	05.6	00.0	.	.	0-6 10 6 25
25	9	00 0	02 0	00	00.7	13.4
26	9	05 0	04 0	04	04.3	11.4	.	.	.	0-1 7 30 15 15 15 15 16 30 16 30 F 555 17 50 18 10
27	9	06	07 0	04	05.7	04.1	00.1	.	.	0-1 7 40 15 8 30 9 05, 8 14 8 35 9 05 1 1 10 19 05 9 30, F 555 17 50 18 10
28	7	07 0	10 0	04	07.0	02.4	01.5	.	.	0-1 13 25 17
29	9	01 0	05 0	02	02.7	12.5	03.5	.	.	0-1 15 25 13 28
30	7	10	08	09	09.0	03.8	.	.	.	0-1 15 25 13 28
31	9	02 0	05 0	02	03.0	13.4	00.0	.	.	0-1 7 30 12 13 i
MES. VRED.		05.1	05.9	04.7	05.2	241.1	61.1			

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1	8	020	050	00	02.3	12.8	.	.	$\Delta n - 17^{\circ} 30'$
2	8	000	070	00	02.3	13.4	.	.	$R_9 - 12^{\circ} 0^{\circ} 10^{\circ} 30' 12^{\circ}$
3	8	08	08	03	06.3	04.0	.	.	$R_12^{\circ} 55' 13^{\circ} 45' 13^{\circ} 05' 13^{\circ} 00' E_N - NW 13^{\circ} 20' 13^{\circ} 55' 19^{\circ} 24' 24^{\circ}$
4	8	040	090	R	03	05.3	09.4	01.5	$F_{NW} 13^{\circ} 30' 13^{\circ} 00' \Delta^{\circ} 2^{\circ} 13^{\circ} 30' 14^{\circ} 45' T 13^{\circ} 30'$
5	8	10	070	08	08.3	05.5	01.6	.	$F_{NNE} 4^{\circ} 10' 17^{\circ} 30' 12^{\circ} 45' 13^{\circ} 05' [14^{\circ} 30']$
6	8	070	070	10	08.0	04.5	.	.	$F_4^{\circ} 20' 19^{\circ} 02' 1^{\circ} 17^{\circ} 30' 19^{\circ} 04' 1^{\circ}$
7	8	070	060	10	07.7	10.4	.	.	$P_0 - P_0^{\circ} F_{10^{\circ} 35'} 19^{\circ} 1^{\circ}$
8	8	060	100	100	06.7	00.7	.	.	$\Delta^{\circ} 13^{\circ} 45' 24^{\circ} 1^{\circ}$
9	8	100	080	04	07.3	04.9	05.5	.	$\Delta^{\circ} 0^{\circ} 1^{\circ} 6^{\circ} 20' 12^{\circ} 30'$
10	8	02	040	02	02.7	12.9	03.0	.	$\Delta^{\circ} n - 8^{\circ} 20^{\circ} n = n - 11^{\circ} 30'$
11	8	09	070	10	08.7	08.0	.	.	.
12	8	030	080	05	05.3	06.2	.	.	$\Delta^{\circ} 16^{\circ} 20' 16^{\circ} 30' = 0^{\circ} 1^{\circ} n - 16^{\circ} 1^{\circ}$
13	8	040	060	00	03.3	10.6	00.0	.	.
14	8	000	050	04	03.0	12.0	.	.	.
15	8	000	020	00	00.7	14.0	.	.	.
16	8	000	08	100	R	06.0	07.0	.	$=^{\circ} n - 17^{\circ} 20' \Delta^{\circ} 1^{\circ} 2^{\circ} 14^{\circ} 35' 14^{\circ} 40' 16^{\circ} 50' 22^{\circ} 20' F_{new} 17^{\circ} 45' 20^{\circ} 45' \Delta^{\circ} 20^{\circ} 50' 21^{\circ} R^{\circ} 20^{\circ} 55' 21^{\circ} 1^{\circ}$
17	8	070	070	00	04.7	05.8	08.7	.	.
18	8	000	040	00	01.3	12.2	.	.	$R_{14^{\circ} 20'} 15^{\circ} 20' \Delta^{\circ} 1^{\circ} 2^{\circ} 15^{\circ} 15^{\circ} 20' R^{\circ} 20' 20^{\circ} 20'$
19	8	000	070	10	05.7	09.8	.	.	$F_{0^{\circ} 2^{\circ} 0^{\circ}} 10^{\circ} 35' 19^{\circ} 10' \Delta^{\circ} 1^{\circ} 10^{\circ} 40' 20^{\circ} R^{\circ} 18^{\circ} 45' 19^{\circ} 10' \Delta^{\circ} 6^{\circ} 19^{\circ} 20' 19^{\circ} 40'$
20	8	07	10	04	07.0	04.7	01.5	.	.
21	8	10	070	06	07.7	09.0	03.0	.	$F_{12^{\circ} 4^{\circ} 12^{\circ} 20'} \Delta^{\circ} 1^{\circ} 17^{\circ} 45' 18^{\circ} 20'$
22	8	07	09	05	07.0	07.9	00.8	.	.
23	8	02	07	00	03.0	06.4	.	.	$F_{17^{\circ} 57'} 18^{\circ} 23' F_{17^{\circ} 57'} 18^{\circ} 23' \Delta^{\circ} 1^{\circ} 2^{\circ} 18^{\circ} 20' 21' \Delta^{\circ} 18^{\circ} 45' 18^{\circ} 50'$
24	8	03	05	10	R	06.0	10.4	.	$F_{18^{\circ} 2^{\circ} 21^{\circ} 45'} \Delta^{\circ} 1^{\circ} 18^{\circ} 45' 19' R^{\circ} 18^{\circ} 45' 19'$
25	8	10	060	10	08.7	07.8	<u>18.0</u>	.	.
26	8	000	08	R	00	02.7	12.0	00.0	$F_{8^{\circ} 45'} 20^{\circ} 45' R^{\circ} 13^{\circ} 20' 14$
27	8	000	10	03	04.3	09.1	.	.	.
28	8	000	020	00	00.7	13.4	.	.	.
29	8	000	030	00	01.0	13.7	.	.	$F_{H^{\circ} 18^{\circ} 20'}$
30	8	000	020	00	00.7	13.3	.	.	.

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 $\varphi = 42^{\circ}26'$ N $\lambda = 19^{\circ}17'$ E Gr. $\Delta G = + 1h\ 17min.$

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d	Vozdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost v%			Pravac i jačina vetro D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	747.6	748.0	748.4	24.0	22.8	16.4	19.9	27.0	16.1	21.7	16.7	13.1	12.9	74	63	92	76	N	1	NNE	6	SE	3
2	748.5	749.1	750.5	17.6	19.7	15.0	16.8	21.8	12.5	13.5	12.7	11.2	11.5	84	65	90	80	SE	3	S	2	-	0
3	752.0	752.7	754.8	17.4	23.8	21.2	20.9	24.7	14.3	13.3	11.6	11.9	13.3	78	54	70	67	NNE	2	SE	4	-	0
4	755.8	753.5	753.4	19.7	29.4	23.5	24.0	29.9	15.9	14.0	15.2	16.1	15.3	88	52	71	70	-	0	SE	3	SE	2
5	752.4	751.9	751.9	21.5	22.6	19.5	20.8	28.2	16.0	16.2	14.0	16.2	15.6	73	79	92	81	-	0	SE	4	-	0
6	752.5	752.7	754.5	17.4	24.6	20.5	20.8	26.9	17.0	16.5	14.1	14.8	12.8	94	64	71	76	-	0	SSE	3	N	3
7	756.5	755.9	756.6	20.4	29.1	23.2	24.0	30.0	16.8	14.8	12.6	15.6	16.6	70	52	78	67	-	0	ESE	3	-	0
8	757.8	756.5	757.0	23.4	31.2	25.0	26.2	32.0	21.0	18.4	16.2	13.1	16.7	75	38	70	61	NW	1	SE	4	NE	2
9	757.9	756.7	756.6	23.5	31.9	26.0	26.8	32.6	21.1	17.6	12.4	13.9	15.3	57	39	61	52	-	0	SSE	3	-	0
10	756.7	754.9	754.1	24.2	33.4	26.5	27.6	33.5	22.0	19.0	13.3	14.8	19.3	59	38	74	57	N	2	S	3	-	0
11	754.7	754.3	755.5	25.5	33.3	26.2	27.8	33.9	22.4	20.0	13.7	13.8	14.4	56	36	57	50	-	0	SSE	4	-	0
12	755.8	754.3	754.5	24.5	32.2	26.4	27.4	33.0	22.4	20.2	14.0	13.1	13.9	61	36	54	50	NNE	2	S	3	-	0
13	756.9	755.9	757.2	20.8	30.2	23.6	24.6	31.4	19.1	18.3	14.8	14.7	13.9	80	46	64	63	NNW	3	NNW	3	-	0
14	758.2	757.3	757.9	25.2	31.7	26.8	27.6	32.8	22.4	18.7	13.1	13.3	17.4	54	38	66	53	-	0	SE	3	NE	2
15	758.7	757.0	756.6	25.8	33.5	28.0	28.8	34.3	23.6	21.9	13.5	13.6	16.2	54	35	57	49	-	0	S	2	NNNE	2
16	755.9	753.4	753.0	26.4	34.8	29.0	29.8	35.6	23.3	20.5	15.3	18.9	12.1	59	45	40	48	NE	1	SE	3	N	3
17	753.8	752.5	753.5	25.7	34.6	29.0	29.6	35.8	22.1	21.6	13.6	13.9	17.5	55	34	58	49	NNW	2	SSE	2	-	0
18	754.3	753.1	753.1	26.8	36.2	29.9	30.6	37.2	25.2	22.3	14.8	17.8	17.7	56	39	56	50	NW	3	SE	4	-	0
19	754.0	752.0	751.7	28.2	34.8	27.4	30.0	37.1	26.2	24.2	14.4	16.0	15.7	50	34	57	47	NNE	2	SSE	5	-	0
20	751.8	750.2	751.2	27.0	34.6	25.4	28.1	34.6	24.6	21.2	15.7	14.2	11.8	59	34	46	47	NW	3	NE	4	NE	6
21	752.9	751.2	751.5	25.0	32.4	27.5	28.1	33.7	23.8	21.7	10.7	10.2	10.7	45	28	39	37	NNE	6	-	0	NE	3
22	752.1	751.0	752.8	25.7	32.8	24.6	26.9	33.8	23.6	20.4	10.2	12.6	14.0	41	34	60	45	N	4	ESE	2	NW	2
23	754.5	753.4	754.3	24.4	31.3	26.2	27.0	32.9	22.7	20.9	12.0	11.3	12.4	52	33	49	45	NNW	3	S	2	N	1
24	754.5	753.0	753.3	23.7	31.8	25.5	26.6	32.6	21.5	19.2	13.5	13.3	12.6	62	38	52	51	-	0	SE	4	-	0
25	754.1	753.2	753.9	24.2	32.6	26.4	27.4	33.5	20.0	20.0	13.6	09.7	09.6	60	26	37	41	-	0	ESE	3	-	0
26	755.6	756.7	757.8	24.0	24.2	21.0	22.6	27.2	20.8	19.9	10.5	09.1	07.2	47	40	39	42	N	5	N	6	N	1
27	758.4	756.4	756.2	22.0	30.4	24.7	25.4	31.0	19.5	18.2	10.0	08.4	09.3	50	26	40	39	N	4	NE	3	NNE	4
28	757.3	755.9	756.8	22.0	30.7	24.0	25.2	31.3	20.5	17.8	08.6	09.4	10.8	44	28	48	40	NNW	1	SSE	2	-	0
29	757.9	755.9	756.3	24.4	31.5	27.1	27.5	32.4	21.9	19.0	09.2	07.7	10.3	40	22	38	33	N	3	SSE	4	ESE	4
30	756.2	754.0	755.3	25.0	31.6	25.2	26.8	32.0	22.0	18.6	12.0	11.1	12.8	50	32	53	45	NNW	1	SSE	3	NW	4
31	755.1	754.0	755.3	25.5	31.3	26.0	27.2	32.3	22.9	20.9	11.1	09.3	09.3	46	27	37	37	NNW	3	NNE	5	NNW	4
MES.	VRED.	754.8	753.7	754.4	23.6	30.5	24.7	25.9	31.8	20.9	19.0	13.0	13.0	13.5	60	40	59	53	1.8	3.3	1.7		

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1	756.8	755.7	757.4	24.8	31.0	25.3	26.6	32.3	22.9	20.7	10.1	09.0	10.0	43	27	41	37	N	4	NNE	3	N	3
2	758.1	756.9	758.3	23.7	31.5	24.5	26.0	31.9	22.4	18.9	10.6	09.0	09.5	48	26	41	38	-	0	NNE	4	NNM	2
3	754.9	757.5	758.5	24.3	29.8	24.5	25.8	30.3	22.2	19.0	09.5	10.0	09.4	42	32	41	38	N	2	NNE	5	NNE	4
4	758.2	755.9	756.4	23.7	31.6	25.6	26.6	31.9	22.3	20.5	10.6	09.7	10.2	48	28	42	39	NNE	4	NE	4	NNE	3
5	756.5	754.9	756.2	23.8	29.4	24.6	25.6	31.4	21.0	17.2	09.7	08.9	08.9	44	29	38	37	NE	3	NNE	4	NNE	4
6	757.3	757.2	758.1	22.3	29.0	22.3	24.0	29.4	19.0	18.4	09.4	08.5	10.8	47	28	53	43	-	0	N	3	NNE	4
7	758.1	756.4	756.6	23.1	29.7	24.5	25.4	30.6	20.7	17.0	09.4	09.8	09.7	44	31	42	39	N	3	NNE	5	NNE	3
8	755.2	754.2	754.0	23.4	28.7	25.0	25.5	30.0	21.9	19.7	09.4	10.4	09.7	44	35	41	40	NNE	4	N	5	NNE	6
9	754.0	754.2	755.0	23.5	26.2	24.2	24.5	28.4	22.4	20.8	12.0	10.8	11.8	55	42	52	50	N	1	NNE	3	-	0
10	756.0	755.9	756.7	25.3	31.4	26.8	27.6	32.9	23.4	19.5	12.3	10.7	08.9	51	31	34	39	N	4	SSE	3	N	1
11	757.9	756.7	756.2	24.3	31.4	26.4	27.1	33.4	22.7	19.6	10.9	13.0	11.3	48	38	44	43	N	2	SM	2	N	3
12	756.2	753.8	753.1	22.8	32.7	27.0	27.4	33.8	20.6	17.8	11.2	10.7	08.6	54	29	32	38	N	2	NNE	3	-	0
13	752.5	750.9	753.3	23.3	29.0	22.8	24.5	30.3	21.4	18.5	11.8	15.0	12.5	55	50	60	55	-	0	SSE	5	NNE	2
14	755.0	754.8	756.7	23.2	31.0	25.8	26.4	31.6	19.2	18.6	12.3	10.5	11.9	58	31	48	46	NE	4	NE	4	E	3
15	758.0	756.7	757.0</td																				

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vremenska čas	Oblačnost N (0-10)					Insekcija broj sati	Padavine R mm	Snežni pokrivalo h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8 05	08	08	07.0	06.8	F _{SSW} 10 ⁴⁰ -14 ⁴⁵ , 17 ⁴⁵ -20 ⁴⁵ ; R ₁₄ ⁴⁵ -17 ⁴⁵ , 0 ⁴⁵ 14 ⁴⁵ -17 ⁴⁵ ; 21 ⁴⁵ -23, 0 ⁴⁵ -22-24
2	8 08	08	10	06.7	03.6	07.0	.	.	.	F _{NE} 0-4, 14 ⁴⁵ -20 ⁴⁵ ; F _{NE} 17 ⁴⁵ -12 ⁴⁵
3	8 05	06	08	06.3	07.0	01.3
4	8 00	02	00	06.7	13.5	F _{SSW} 11 ⁴⁵ -13 ⁴⁵ , 0 ⁴⁵ -12 ⁴⁵ -13 ⁴⁵ ; R ₁₆ ⁴⁵ -17 ⁴⁵ -22 ⁴⁵ -23 ⁴⁵ ; R ₁₂ ⁴⁵ -13 ⁴⁵
5	8 07	10	10	09.0	05.2	0 ⁴⁵ -0 ⁵⁰ -1 ⁰⁵ , 3 ⁴⁵ -6 ⁴⁵ ; 0 ⁴⁵ -2 ⁴⁵ -3 ⁴⁵ ; F _{NNE} 17 ⁴⁵ -17 ⁵²
6	8 07	05	05	05.7	07.5	11.3
7	8 03	05	00	02.7	11.9
8	8 00	00	00	00.0	13.3
9	8 02	02	00	01.3	13.5
10	8 00	01	03	01.3	13.1
11	8 00	03	00	01.0	13.1
12	8 01	02	00	01.0	13.1
13	8 09	04	00	04.3	08.2	03.3	.	.	.	0 ⁴⁵ -2 ⁴⁵ -3 ⁴⁵ ; F _{SSW} 2 ⁴⁵ -2 ⁴⁵
14	8 00	02	00	00.7	13.5
15	8 00	01	00	00.3	13.5
16	8 00	01	00	00.3	13.6
17	8 00	03	00	01.0	13.5
18	8 00	01	00	00.3	13.3
19	8 00	00	00	00.0	12.9	F _{SSW} 12 ⁴⁵ -13 ⁴⁵
20	8 00	04	03	02.3	13.2	F _{NNE} 7 ⁴⁵ -24i, F _{NNE} 17 ⁴⁵ -24i
21	8 01	04	03	02.7	12.9	F _{NNE} 0-7 ⁴⁵ ; F _{NNE} 0-7 ⁴⁵
22	8 03	04	00	02.3	11.5	F ₃ 14 ⁴⁵ -14 ⁴⁵ ; R ₁₇ ⁴⁵ -17 ⁴⁵ ; 0 ⁴⁵ -17 ⁴⁵ -17 ⁴⁵
23	8 00	07	00	02.3	10.8	00.8	.	.	.	R ₁₄ ⁴⁵ -15 ⁴⁵ ; 0 ⁴⁵ -15 ⁴⁵
24	8 00	03	00	01.0	13.6	0.1
25	8 00	01	00	00.3	13.3
26	8 07	05	00	04.0	10.2	F- _F NNE 4 ⁴⁵ -24i
27	8 00	00	00	06.0	13.6	F _{NNE} 0-24i, F _{NNE} 0-3 ⁴⁵ i, F _{NNE} 3 ⁴⁵ -24i
28	8 00	02	00	00.7	13.5	F _{NNE} 0-8 ⁴⁵ i
29	8 00	03	06	03.0	12.6	F _{NNE} 16 ⁴⁵ -21 ⁴⁵ i; R ₁₈ ⁴⁵ -21 ⁴⁵ i, 0 ⁴⁵ -19 ⁴⁵ -19 ⁴⁵
30	8 00	07	08	05.0	10.3	F _{NNE} 5 ⁴⁵ -24i
31	8 06	07	00	04.3	12.7	00.0
MES.	VRED.	02.1	03.6	02.1	02.6	358.7	23.8			

1	8 04	04	00	02.7	11.1	.	.	F _{N-NNE} 7 ⁴⁵ -16 ⁴⁵ ; R ₁₄ ⁴⁵ -14 ⁴⁵	
2	8 04	06	00	03.3	10.5	.	.	F _{NNE} 12 ⁴⁵ -24 ⁴⁵ ; F _{NNE} 17 ⁴⁵ -18 ⁴⁵	
3	8 07	03	00	03.3	09.6	.	.	F _{NNE} 8 ⁴⁵ -22 ⁴⁵ ; F _{NNE} 12 ⁴⁵ -12 ⁴⁵	
4	8 04	08	04	05.3	09.6	.	.	F _N 2 ⁴⁵ -8 ⁴⁵ ; 0 ⁴⁵ -24 ⁴⁵	
5	8 06	06	10	07.3	07.9	.	.	0 ⁴⁵ -4 ⁴⁵ ; 24-22 ⁴⁵ ; F ₄ 16 ⁴⁵ -22 ⁴⁵	
6	8 07	08	00	05.0	05.3	00.0	.	R ₁₂ -15 ⁴⁵ ; F _{NNE-NE} 12 ⁴⁵ -12 ⁴⁵ ; 19 ⁴⁵ -24i	
7	8 06	06	00	04.0	06.7	04.8	.	F _{NNE} 2 ⁴⁵ -12 ⁴⁵	
8	8 02	04	00	02.0	12.7	.	.	F _{NNE} 3 ⁴⁵ -24i	
9	8 10	10	03	07.7	00.0	.	.	F _{NNE} 8-18 ⁴⁵	
10	8 03	07	00	03.3	11.5	.	.	F _{NNE} 12 ⁴⁵ -8 ⁴⁵	
11	8 00	08	00	02.7	11.3	.	.	F _N 14 ⁴⁵ -14 ⁴⁵	
12	8 00	05	00	01.7	11.7	.	.	0 ⁴⁵ -13 ⁴⁵ -15 ⁴⁵	
13	8 10	07	04	07.0	06.6	.	.	0 ⁴⁵ -7 ⁴⁵ -7 ⁴⁵ -14 ⁴⁵ -15 ⁴⁵ ; R ₁₉ ⁴⁵ -19 ⁴⁵	
14	8 02	02	00	01.3	12.7	00.1	.	F- _F NNE 7 ⁴⁵ -17 ⁴⁵ ; 7 ⁴⁵ -17 ⁴⁵	
15	8 00	00	00	00.0	12.7	.	.	.	
16	8 00	07	04	03.7	11.4	.	.	0 ⁴⁵ -22 ⁴⁵ -22 ⁴⁵	
17	8 07	05	C5	05.7	11.3	00.0	.	F _{SE} 14 ⁴⁵ -16 ⁴⁵	
18	8 06	05	00	03.7	10.1	.	.	F _{SE} 12 ⁴⁵ -12 ⁴⁵	
19	8 10	06	01	05.7	08.4	01.0	.	0 ⁴⁵ -2 ⁴⁵ -8 ⁴⁵ ; F- _F NNE 7-7 ⁴⁵ ; F _{NNW} 16 ⁴⁵ -24i	
20	8 05	02	02	03.0	10.1	33.6	.	F- _F N 0-22 ⁴⁵	
21	8 03	04	00	02.3	12.3	.	.	F- _F N 0 ⁴⁵ -23 ⁴⁵	
22	8 00	01	00	00.3	12.6	.	.	F _N 3 ⁴⁵ -3 ⁴⁵	
23	8 00	00	00	00.0	12.7	.	.	F _N 7 ⁴⁵ -7 ⁴⁵	
24	8 08	10	08	08.7	03.6	.	.	F _{NNW} 12 ⁴⁵ -13 ⁴⁵	
25	8 10	07	07	06.0	03.7	01.3	.	F _{NNW} 3 ⁴⁵ -3 ⁴⁵ ; F- _F N ₃ 13 ⁴⁵ -14 ⁴⁵ ; 0 ⁴⁵ -2 ⁴⁵ -6 ⁴⁵ ; 18 ⁴⁵ -22 ⁴⁵	
26	8 08	10	04	07.3	03.9	06.0	.	0 ⁴⁵ -13 ⁴⁵ -13 ⁴⁵ ; 18 ⁴⁵ -18 ⁴⁵	
27	8 09	05	10	08.0	07.5	00.4	.	0 ⁴⁵ -5 ⁴⁵ -6 ⁴⁵	
28	8 08	10	07	08.3	06.5	.	.	0 ⁴⁵ -2 ⁴⁵ -2 ⁴⁵ ; 0 ⁴⁵ -2 ⁴⁵ -3 ⁴⁵	
29	8 08	05	00	04.3	09.0	07.3	.	.	
30	8 05	07	05	05.7	09.2	.	.	.	
31	8 02	C3	00	01.7	12.6	.	.	.	
MES.	VRED.	05.0	05.5	02.4	04.3	183.8	54.5		

$\varphi = 42^{\circ}26' \quad \text{N}, \lambda = 19^{\circ}17' \quad \text{E}$ Gr. $\Delta G = + 1\text{h } 17\text{ min.}$

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S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	756.9	756.0	756.6	20.0	30.6	24.0	24.6	32.4	19.0	16.7	15.7	16.6	17.8	89	50	80	73	NW	2	SE	2	-	0	
2	757.5	756.0	756.1	23.4	31.6	24.2	25.8	32.7	20.2	16.8	15.7	18.6	18.6	73	53	82	69	NNW	4	SW	1	-	0	
3	756.0	754.3	752.7	22.2	30.5	25.0	25.7	31.2	20.2	17.0	16.0	19.9	16.7	80	61	70	70	-	0	SE	4	-	0	
4	754.1	754.0	754.2	19.4	24.2	19.0	19.6	26.0	16.0	16.0	13.2	14.5	14.7	94	64	89	82	NNW	5	SE	1	-	0	
5	755.2	754.8	756.0	19.2	28.0	21.8	22.7	29.2	16.5	14.7	13.6	16.8	17.3	81	59	88	76	NNW	2	SE	1	-	0	
6	757.7	756.8	758.4	21.0	28.4	22.4	23.6	28.7	18.7	17.2	15.5	20.6	16.2	83	71	80	78	-	0	SE	3	-	0	
7	759.5	756.4	757.8	19.4	23.0	20.0	20.6	26.0	17.8	16.0	13.9	18.3	16.8	82	87	96	88	NW	2	-	0	-	0	
8	758.8	758.2	759.8	20.1	27.0	22.3	22.9	29.0	17.6	15.5	15.8	19.1	14.8	89	71	73	78	-	0	SSW	3	-	0	
9	760.0	758.4	758.5	21.3	28.3	22.6	23.7	29.0	19.4	16.8	12.1	15.0	17.7	64	52	86	67	N	2	SE	3	NW	2	
10	759.0	757.0	757.7	20.0	28.0	21.6	22.8	28.7	17.5	14.4	14.0	12.6	13.7	80	44	71	65	NN	3	SE	4	NNW	3	
11	757.6	756.9	758.0	18.8	27.6	20.0	21.6	28.1	17.2	14.5	10.1	13.6	15.8	62	49	90	67	NE	2	SE	3	-	0	
12	756.8	756.8	755.6	20.4	20.8	19.6	20.1	22.8	19.0	16.2	14.1	17.0	15.9	79	92	93	88	-	0	NM	2	-	0	
13	755.1	755.9	758.0	17.0	22.4	18.5	19.1	25.0	16.2	15.5	14.3	17.3	13.8	98	85	86	90	-	0	-	0	-	0	
14	758.5	757.5	757.2	18.0	27.6	20.0	21.4	28.2	16.0	13.5	12.9	12.6	14.3	83	46	82	70	NNW	2	SE	1	-	0	
15	758.3	759.3	760.8	19.0	29.0	20.5	22.2	29.0	16.6	13.5	14.8	20.8	16.0	90	69	89	83	NNW	3	SE	2	-	0	
16	763.3	762.9	763.2	20.2	32.4	23.0	24.6	32.5	17.5	13.5	14.7	16.6	19.2	83	45	91	73	-	0	-	0	-	0	
17	762.8	761.4	762.4	22.0	36.2	28.6	28.8	36.5	19.0	15.2	16.4	19.9	18.1	83	44	62	63	NW	1	NNE	3	NNE	4	
18	763.0	761.4	762.0	23.2	31.0	24.0	26.0	32.2	23.4	18.8	19.3	20.8	17.5	80	62	78	73	-	0	SE	4	NNE	4	
19	762.7	761.0	760.5	20.0	28.6	22.6	23.4	29.3	19.4	16.6	12.8	18.3	16.1	73	62	78	71	NNW	4	-	0	N	1	
20	760.9	759.5	759.8	21.2	28.8	20.2	22.6	29.2	20.0	16.5	15.1	20.0	15.6	80	67	88	78	NNW	5	S	1	NE	1	
21	760.7	760.1	760.6	20.4	30.2	22.0	23.6	30.5	19.2	15.5	14.9	21.2	18.0	83	66	91	80	NE	2	-	0	NW	2	
22	762.2	762.1	762.9	21.7	30.2	24.4	25.2	30.4	21.1	18.0	16.5	21.2	18.0	85	66	78	76	N	2	SW	2	NW	2	
23	764.7	762.8	762.5	22.2	29.4	21.0	23.4	30.4	20.9	17.8	16.4	22.7	16.1	82	74	86	81	NW	4	NW	1	-	0	
24	762.8	760.8	760.0	19.6	30.4	21.7	23.4	31.0	18.2	14.6	14.7	19.0	16.4	86	58	84	76	NW	2	SE	1	-	0	
25	759.8	758.6	758.9	18.6	28.8	19.8	21.8	29.5	17.4	13.5	13.5	20.0	15.5	84	67	89	80	-	0	SE	2	-	0	
26	758.5	757.9	758.7	18.3	27.2	19.6	21.2	28.0	17.0	12.8	13.7	19.0	15.6	87	70	91	83	-	0	SE	3	-	0	
27	761.0	761.3	763.3	19.4	26.0	19.2	21.0	26.2	18.4	15.5	14.8	19.6	15.6	87	78	94	86	-	0	S	2	-	0	
28	764.2	763.2	763.7	18.8	29.6	21.2	22.7	30.2	16.5	14.0	14.2	23.4	16.9	87	75	90	84	-	0	SE	2	-	0	
29	763.3	761.3	761.7	18.2	31.6	21.6	23.2	32.0	16.5	18.5	14.2	22.2	17.7	91	64	91	82	-	0	-	0	-	0	
30	760.4	758.6	759.2	19.8	32.0	21.2	23.6	32.5	16.2	12.7	14.1	22.6	17.3	82	63	91	79	-	0	-	0	-	0	
MES.	VRED.	759.7	758.8	759.2	20.1	28.6	21.7	23.0	29.5	18.3	15.6	14.6	18.7	16.4	83	64	84	77	1.6	1.7	0.6			

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TITOGRAD

1	760.4	760.0	760.2	21.1	30.5	21.2	23.5	30.6	16.0	14.2	15.6	13.4	14.9	83	41	79	68	N	1	S	2	-	0
2	760.4	759.1	759.3	19.6	29.8	24.0	24.4	30.0	17.6	15.0	15.0	17.0	16.2	88	54	72	71	-	0	SE	2	NNW	2
3	760.4	759.4	759.8	22.0	29.5	20.2	23.0	30.0	16.6	15.0	14.2	12.5	12.9	72	40	73	62	NNW	3	SSE	2	-	0
4	760.3	758.7	758.8	18.8	28.0	22.0	22.7	28.5	16.9	14.0	13.5	22.3	16.5	83	78	83	81	-	0	SE	3	N	1
5	759.5	758.9	760.6	18.6	22.2	17.2	18.8	22.8	15.5	14.5	09.1	07.3	07.3	56	36	50	47	NNW	6	NNW	7	NNW	7
6	762.4	761.5	762.8	15.6	22.2	17.4	18.2	22.7	15.0	13.2	08.7	10.5	10.3	66	52	69	62	NNW	6	NNW	6	MNE	6
7	763.1	760.8	760.7	13.6	22.2	13.8	15.8	23.0	12.5	12.2	06.7	07.4	08.2	58	37	69	55	NNW	3	SSW	4	-	0
8	759.9	759.0	759.8	13.0	21.6	16.0	16.6	22.2	09.7	07.0	09.8	12.2	09.2	87	63	68	73	-	0	MNE	4	NNW	3
9	759.4	757.0	756.0	11.2	21.0	13.7	14.6	22.0	09.5	06.5	08.4	11.1	10.9	84	60	93	79	-	0	-	0	-	0
10	754.1	752.5	751.9	12.6	19.4	13.4	14.4	19.5	11.5	11.0	09.6	12.4	11.3	88	78	98	88	-	0	-	0	-	0
11	752.2	754.3	755.3	12.8	21.9	18.0	17.7	22.8	11.6	11.0	10.6	15.6	12.6	96	79	82	86	-	0	SSE	4	NNE	3
12	757.1	758.5	759.1	13.8	16.4	15.4	15.2	18.5	12.3	12.5	10.8	13.7	13.1	92	98	100	97	NNW	4	N	1	-	0
13	758.8	756.7	755.9	16.2	20.1	15.8	17.0	21.8	14.8	14.6	12.9	14.7	12.4	93	83	92	89	NN	1	-	0	N	2
14	753.5	756.5	756.8	15.4	13.4	11.6	13.0	18.4	11.0	13.0	11.3	10.5	10.0	86	91	98	92	SW	1	E	2	-	0
15	759.5	759.9	760.8	10.0	15.6	11.2	12.0	17.6	08.2	07.0	08.5	09.0	09.2	93	67	92	84	-	0	-	0	-	0
16	759.5</																						

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$$H_s = 49 \text{ m} \quad H_d = 50.6 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

Dan	Vremenska doba 0-0-0	Oblačnost N (0-10)					Insoljeno svjetlo hranljivo h cm	Padavina R mm	Snežni pokrivali h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 00	03	00	01.0	12.4
2	8 00	03	00	01.0	12.2
3	8 00	04	07	03.7	10.1
4	8 10	04	00	04.7	06.5	37.5
5	8 00	06	00	02.0	11.8	05.4
6	8 06	06	00	04.0	11.3
7	8 10	10	00	06.7	05.8
8	8 03	08	03	04.7	07.8	00.0
9	8 07	03	00	03.3	07.1	06.2
10	8 00	00	00	00.0	11.8
11	8 06	06	04	05.3	09.5
12	8 10	10	06	08.7	00.0
13	8 08	10	00	06.0	07.4	08.5
14	8 00	02	00	00.7	11.6	00.1
15	8 00	00	03	01.0	11.0
16	8 00	00	00	00.0	10.8
17	8 00	00	00	00.0	10.8
18	8 00	01	00	00.2	11.6
19	8 00	00	00	00.0	11.4
20	8 00	00	00	00.0	11.2
21	8 00	00	03	01.0	10.5
22	8 00	03	00	01.0	09.9
23	8 00	02	02	01.3	10.4
24	8 00	02	00	00.7	11.4
25	8 00	02	00	00.7	11.1
26	8 00	02	00	00.7	10.1
27	8 10	03	00	04.3	05.5
28	8 00	03	00	01.0	10.4
29	8 00	00	00	00.0	10.9
30	8 00	02	00	00.7	09.5
MES.	VRED.	02.3	03.2	00.9	02.2	291.2	117.7			

1	8 01	00	00	00.3	09.5
2	8 02	03	00	01.7	10.4
3	8 01	01	00	00.7	10.1
4	8 00	03	00	01.0	09.1
5	8 10	03	00	04.3	06.7	01.7
6	8 00	00	00	00.0	10.6
7	8 00	00	00	00.0	10.4
8	8 00	03	00	01.0	10.0
9	8 07	08	10	08.3	06.3
10	8 08	10	10	05.3	04.0	00.6
11	8 04	07	10	07.0	07.6	07.1
12	7 10	10	10	10.0	00.1	26.7
13	8 10	09	10	09.7	01.3	11.5
14	8 08	10	10	09.3	00.7	18.0
15	8 10	08	06	08.0	34.0	04.8
16	8 10	10	10	10.0	00.4	01.5
17	7 10	10	07	09.0	00.0	29.0
18	8 10	10	10	10.0	01.1	79.3
19	8 07	10	10	09.0	30.6	20.5
20	8 10	10	10	10.0	00.3	15.2
21	8 10	08	08	08.7	02.5	15.7
22	8 09	07	07	07.7	06.5	01.6
23	8 10	04	03	05.7	06.8
24	8 08	09	03	06.7	05.4
25	8 01	02	00	01.0	09.6
26	8 00	01	00	00.3	05.1
27	8 04	02	00	02.0	08.5
28	8 00	00	00	00.0	09.5
29	8 00	00	00	00.0	09.0	29.7
30	8 00	00	00	00.0	09.7	09.7
31	8 00	00	00	00.0	09.7	09.7
MES.	VRED.	05.2	05.1	04.3	04.9	192.0	244.0			

$\varphi = 42^{\circ}26' \text{ N } \lambda = 19^{\circ}17' \text{ E}$ Gr. $\Delta G = + 1 \text{ h } 17 \text{ min.}$

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č	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, I (0-12)						
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	-21				
1	761.1	759.8	762.0	09.4	19.2	12.0	13.2	20.0	06.6	06.0	07.2	13.4	10.0	82	80	95	86	N	1	SE	1	-	0	
2	762.7	762.3	764.1	10.9	20.6	11.9	13.8	21.0	09.0	06.0	08.9	12.7	09.6	91	70	92	84	-	0	-	0	-	0	
3	764.7	763.8	764.6	08.6	20.9	11.0	12.8	21.0	07.5	05.7	08.0	13.9	09.0	95	76	92	88	-	0	-	0	-	0	
4	764.3	763.5	764.4	07.0	19.6	10.1	11.7	20.0	06.2	04.0	07.0	11.8	08.8	93	69	95	86	-	0	SE	2	-	0	
5	764.1	763.3	763.7	05.4	17.8	08.4	10.0	18.2	04.8	02.7	06.5	10.5	07.8	97	69	95	87	-	0	-	0	-	0	
6	763.3	761.6	761.8	07.2	17.4	09.6	11.0	18.1	06.0	03.5	06.2	11.1	07.9	82	74	88	81	NW	2	-	0	-	0	
7	761.1	759.4	760.0	10.4	18.4	10.1	12.2	19.0	06.4	03.7	08.1	10.4	08.1	86	66	87	80	-	0	S	2	-	0	
8	759.3	757.2	757.8	10.6	18.0	13.8	14.0	18.2	06.5	05.7	08.7	11.8	05.8	91	76	49	72	N	2	SE	2	NWW	4	
9	757.5	758.4	760.5	09.5	13.2	11.0	11.2	14.8	09.0	09.0	08.5	09.9	09.8	95	87	100	94	-	0	-	0	-	0	
10	761.5	760.8	759.2	10.4	12.8	10.6	11.1	14.0	10.1	09.7	09.0	10.4	09.6	95	93	100	96	-	0	-	0	N	1	
11	760.3	760.3	762.2	09.5	16.2	11.0	11.9	18.0	09.2	07.3	08.4	11.0	09.3	94	80	94	89	NWW	2	SSE	3	-	0	
12	763.7	764.3	765.7	10.6	11.4	08.2	09.6	13.4	08.0	09.4	08.9	09.6	07.9	93	95	97	95	-	0	NWW	3	-	0	
13	767.2	766.3	766.7	04.6	16.0	07.6	09.0	16.9	04.3	02.0	05.9	08.4	07.6	93	62	97	84	-	0	-	0	-	0	
14	765.0	761.8	759.5	07.1	10.4	09.0	08.9	12.0	04.4	02.8	07.1	07.7	08.3	93	81	96	90	-	0	-	0	-	0	
15	758.3	758.0	758.0	09.2	08.4	07.8	08.3	12.5	07.4	07.5	07.4	07.6	07.7	85	92	97	91	WNN	1	NW	3	-	0	
16	756.2	753.2	751.1	02.6	06.2	05.6	05.0	08.7	02.2	00.2	05.5	06.9	06.6	100	97	97	98	-	0	NW	3	NW	1	
17	747.7	749.0	747.9	07.4	15.1	16.4	13.8	17.2	05.0	05.5	07.3	11.2	12.5	95	87	89	90	NW	1	SSE	5	SSE	6	
18	747.6	748.1	750.1	15.4	20.6	18.0	18.0	21.8	15.4	13.0	12.1	15.4	14.0	92	84	91	89	SSE	2	SSE	1	SSE	5	
19	753.6	754.2	753.8	11.8	11.8	10.1	11.0	18.0	09.7	11.5	09.4	09.4	08.9	91	91	96	93	WNN	4	NW	1	-	0	
20	753.5	752.2	753.0	09.2	10.8	09.4	09.7	11.5	08.5	07.0	06.3	09.0	08.5	95	93	96	95	-	0	-	0	-	0	
21	751.2	752.1	754.6	08.6	08.8	06.3	07.5	11.4	05.5	06.8	08.4	06.8	06.9	100	80	96	92	-	0	NWW	5	NWW	7	
22	751.9	749.3	750.9	06.0	07.4	05.3	06.0	08.0	05.0	04.4	05.5	05.8	04.7	78	75	71	75	NNE	6	NE	4	NNE	5	
23	751.8	751.1	752.8	03.8	06.4	04.3	04.7	06.8	03.5	02.6	04.7	05.6	04.9	79	77	78	78	NWW	2	NNE	7	NNE	5	
24	754.0	755.2	758.5	04.2	05.0	01.8	03.2	05.5	01.6	02.0	02.5	04.7	03.7	40	72	71	61	NNE	6	NWW	6	NWW	5	
25	761.3	761.6	762.9	01.8	07.6	02.4	03.6	08.2	01.5	-00.4	03.3	02.6	02.9	63	33	53	50	NWW	3	NW	2	-	0	
26	763.5	762.3	762.7	-01.0	08.7	-00.8	01.5	09.0	-01.2	-05.3	02.7	03.9	03.7	63	47	85	65	NW	2	NNE	1	-	0	
27	763.4	762.7	762.2	00.6	10.0	06.6	06.0	10.6	-01.7	-05.5	04.1	04.7	04.6	86	51	63	67	NWW	3	NE	1	NW	2	
28	759.4	755.5	755.2	06.2	10.5	07.2	07.8	12.0	05.5	04.0	06.0	06.9	07.6	85	72	100	86	-	0	-	0	-	0	
29	755.0	754.8	756.0	07.0	11.6	08.6	09.0	11.9	06.0	04.0	07.3	08.6	08.3	97	84	97	93	-	0	-	0	-	0	
30	757.9	757.7	758.9	03.4	09.1	05.0	05.6	10.6	03.0	01.0	05.5	08.2	06.3	94	95	96	95	-	0	-	0	-	0	
MES.	VRED.	758.7	758.0	758.7	07.2	13.0	08.6	09.4	14.2	05.9	04.5	C6.9	09.0	07.7	87	77	88	84	1.4	2.0	1.6	-	-	-

1	759.1	758.6	758.8	05.7	09.0	08.3	07.8	09.2	C1.6	01.1	06.9	08.2	07.9	100	95	96	97	-	0	-	0	-	0
2	757.9	756.0	756.1	03.3	14.4	05.8	07.3	14.6	02.5	01.0	05.5	08.1	06.2	95	66	90	84	-	0	-	0	-	0
3	757.8	757.5	760.6	02.5	14.0	05.0	06.6	14.4	02.2	-00.4	05.5	09.9	06.5	100	82	100	94	-	0	-	0	-	0
4	764.0	763.6	765.9	02.8	14.3	06.2	07.4	14.8	02.0	-00.3	05.3	07.3	05.9	95	60	84	80	-	0	-	0	-	0
5	764.6	762.9	763.5	04.0	14.4	05.0	07.1	14.7	03.1	-00.3	05.9	10.0	06.5	97	82	100	93	-	0	-	0	-	0
6	764.1	761.5	759.7	00.9	12.3	04.0	05.3	13.2	C0.1	-02.0	04.6	07.0	05.7	95	65	94	85	-	0	SE	2	-	0
7	757.0	757.9	761.5	07.2	09.8	04.6	06.6	11.3	02.5	-00.4	07.0	04.9	05.1	92	54	80	75	NW	2	NWW	6	NWW	4
8	760.8	758.7	759.9	-00.4	10.0	01.0	02.9	10.2	-01.2	-04.6	04.0	03.7	04.1	89	40	83	71	NE	1	NW	2	-	0
9	762.3	762.5	763.8	-01.2	11.6	02.2	03.7	12.5	-02.4	-04.4	04.1	04.7	04.6	100	45	85	77	-	0	SE	2	-	0
10	765.8	764.4	764.5	04.0	11.0	05.5	06.5	11.5	-00.3	-03.5	05.0	05.2	05.4	82	53	79	71	NWW	2	-	0	-	0
11	763.6	761.6	762.5	01.4	12.1	C3.0	04.9	13.5	-00.4	-02.4	04.7	08.6	05.5	93	81	97	90	-	0	SE	2	-	0
12	761.6	759.1	758.3	-00.8	07.6	05.1	04.2	07.8	-01.5	-04.0	04.2	05.0	06.2	96	63	94	84	-	0	-	0	-	0
13	756.2	756.5	758.0	04.8	08.0	07.2	06.8	09.5	03.9	04.2	06.3	07.8	07.4	97	97	97	97	-	0	-	0	-	0
14	759.5	758.9	762.2	04.8	13.3	05.7	07.4	14.0	04.0	02.0	06.3	08.4	06.6	97	73	96	89	-	0	SE	1	-	0
15	764.2	763.4	765.2	02.8	12.0	04.0	05.7	12.4	02.3	00.0	05.1	06.7	05.7	90	64	94	83	-	0	-	0	-	0
16	765.2	762.7	761.2	02.0	07.8	05.6	05.4	08.0	00.5	-01.4	05.0												

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 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Dan	Vjetarost 0-9	Oblačnost N (0-10)					Insolacije broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	08	040	00	04.0	08.8	.	.	$\Delta^0-0-8, 19^{45} 24$	
2	8	07	000	00	02.3	07.2	.	.	$\Delta^0-0-7^{30}, 18^{45} 24$	
3	8	06	040	00	03.3	08.5	.	.	$\Delta^0-0-8, 18^{45} 24$	
4	8	04	040	00	02.7	08.7	.	.	$\Delta^0-0-8, 18^{45} 24$	
5	8	08	070	00	05.0	05.1	.	.	$\Delta^0-0-8, 19^{45} 24$	
6	8	05	060	00	03.7	08.2	.	.	$\Delta^0-0-8, 19^{45} 24$	
7	8	08	070	00	05.0	07.5	.	.	Δ^0-0-6	
8	8	03	060	08	05.7	08.2	.	.		
9	8	10	10	10*	10.0	00.0	01.2	.	$\bullet^0-10^{45}, 5^{20} 7^{30}, 7^{45}, 17-17^{45}, 19^{35}, 21^{30}$	
10	7	09	10*	10*	09.7	00.1	09.8	.	$\bullet^0-10^{45}, 10^{20}, 13^{30}, 22^{20}, 18^{45}, 23$	
11	8	08	060	07	07.0	05.8	34.1	.	$\bullet^0-6^{40}, \Delta^0-19^{30} 24$	
12	7	10	10*	04	08.0	00.3	.	.	$\Delta^0-0-6^{45}, 19^{30} 24, \bullet^0-12^{20}, 14$	
13	8	02	030	07	04.0	09.1	00.7	.	$\Delta^0-0-9^{40}, 19^{30} 24, 22^{10}$	
14	7	07	10	10	09.0	00.6	.	.	$\Delta^0-0-8^{40}, 19^{30} 22^{10}$	
15	7	10	10*	10*	10.0	00.0	02.0	.	$\bullet^0-10-2, 10^{30}, 21^{30}$	
16	7	03	10*	10*	07.7	01.3	06.2	.	$\Delta^0-7-9, \bullet^0-24, 18^{45}, 20$	
17	7	10*	10*	10	10.0	00.0	54.1	.	$\bullet^0-0-15^{45}, 22^{35}, 24$	
18	7	10	10*	10*	10.0	00.0	15.9	.	$\bullet^0-15^{20}, 10^{15}, 10^{25}, 15^{50}, 22^{20}, 18^{45}, 23^{50}, 19^{30}, 23^{50}, 19^{30}, 20^{20}$	
19	7	10*	10*	10	10.0	00.0	05.6	.	$\bullet^0-12^{20}, 24$	
20	8	10	09	10	09.7	00.0	17.1	.	$\bullet^0-15-13^{40}, 18-21, 18-70^{45}, 9$	
21	7	10	10*	10*	10.0	00.5	13.2	.	$\bullet^0-7^{40}, 24, \bullet^0-11^{45}, 24$	
22	8	10	09	00	06.3	00.0	01.0	.	$\bullet^0-8^{40}, 22^{30}$	
23	8	07	060	00	04.3	06.7	.	.	$F^0-5^{30}, 22^{30}$	
24	8	09	09	00	06.0	00.0	.	.	$F^0-2^{30}, 23^{40}$	
25	8	03	000	00	01.0	08.6	.	.	.	
26	8	03	000	00	01.0	08.6	.	.		
27	8	02	000	10	04.0	08.6	.	.	$\Delta^0-10^{45}, 22^{30}$	
28	8	10	10	10*	10.0	02.3	.	.		
29	8	10	10	10	10.0	00.0	08.2	.	$\equiv 5^{50}, 7^{45}, \equiv 7^{45}, 11^{40}, 16-7, \equiv 11^{40}, 16$	
30	6	01	10	10	07.0	00.9	.	.		
MES.	VRED.	07.1	07.0	05.5	06.5	116.1	165.1			

TITOGRAĐ

1975 DECEMBAR

1	8	10	100	10	10.0	00.0	00.5	.	$\bullet^0-14^{20}, 4^{40}, 19^{45}, 20^{30}$	
2	8	03	040	00	02.3	07.4	00.2	.	$\equiv, rj-7^{45}, \Delta^0-19^{30} 24$	
3	8	00	000	00	00.0	07.8	.	.	$\Delta^0-8^{30}, 19^{30} 24$	
4	8	00	08	00	02.7	06.2	.	.	$\Delta^0-8^{20}, 19^{30} 24$	
5	8	05	030	03	03.7	06.7	.	.	$\Delta^0-8^{20}, 19^{30} 24$	
6	8	00	020	00	00.7	08.1	.	.	$\Delta^0-7^{45}, 7^{45}$	
7	8	07	030	00	03.3	08.1	.	.	$\Delta^0-0-7^{30}, F^0-13^{30}, 15^{40}$	
8	8	00	000	00	00.0	08.6	.	.	$\Delta^0-7^{40}, 7^{40}$	
9	8	03	000	00	01.0	08.5	.	.		
10	8	08	000	10	06.0	06.2	.	.		
11	8	02	030	00	01.7	07.7	.	.	$\Delta^0-14^{30}, 24$	
12	8	05	10	10*	08.3	00.5	.	.	$\Delta^0-0-8^{20}, \bullet^0-17^{30}, 18, \bullet^0-14^{30}, 24$	
13	7	10	10	10	10.0	00.5	14.0	.	$\bullet^0-0-6^{20}, 10^{10}, 16^{20}$	
14	8	10	020	08	06.7	05.0	01.8	.	$\equiv 5^{40}, 9^{20}, \Delta^0-18^{45}, 24$	
15	8	04	000	03	02.3	08.1	.	.	$\Delta^0-0-9^{30}, 17^{30}, 24$	
16	7	10	10	10*	10.0	00.0	.	.	$\Delta^0-8^{45}, \bullet^0-15^{40}, 24$	
17	7	10*	10*	10*	10.0	00.0	12.4	.	$\bullet^0-0-24, F^0-14^{30}, 24^{30}, \Delta^0-20^{20}, 20^{25}, 18^{30}, 21^{40}$	
18	8	10	030	05	06.0	05.5	38.3	.	$\bullet^0-0-30, \Delta^0-19^{30}, 24$	
19	8	00	10	04	04.7	04.2	.	.	$F-E^0-7-24$	
20	8	10	000	00	03.3	07.7	.	.	$F-E^0-0-24$	
21	8	00	050	00	01.7	06.8	.	.	$F-E^0-0-24$	
22	8	02	000	00	00.7	08.6	.	.	$F-E^0-0-8$	
23	8	03	020	00	01.7	05.4	.	.	$\Delta^0-7^{40}, 8^{30}$	
24	8	00	000	00	00.0	08.5	.	.	$\Delta^0-7^{40}, 8^{30}, F^0-20^{30}, 21^{30}$	
25	7	10	10	10	10.0	00.0	.	.		
26	8	03	020	01	02.0	06.8	00.7	.	$F^0-50, 23$	
27	8	07	09	08	08.0	01.6	.	.		
28	8	02	000	00	00.7	08.5	.	.		
29	8	00	000	00	00.0	08.5	.	.		
30	8	02	080	00	03.3	06.2	.	.		
31	8	00	000	00	00.0	08.5	.	.		
MES.	VRED.	04.4	04.0	03.3	03.9	176.3	67.9			

1975 JANUAR

SKOPJE - PETROVAC

 $\varphi = 41^{\circ}57'$ $N\lambda = 21^{\circ}38'$ E Gr. $\Delta G = +1h 27min.$

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d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u%			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	747.3	747.5	748.0	-01.2	00.8	-05.4	-02.8	01.2	-05.4	-01.6	03.8	03.6	02.8	91	74	93	86	W	2	NW	3	E	1	
2	746.2	746.6	749.0	-02.7	00.8	00.4	-00.3	01.3	-06.2	-08.2	03.6	03.8	03.3	95	77	70	61	NNW	1	N	4	N	1	
3	750.6	750.1	751.2	-01.8	03.9	00.2	00.6	04.6	-02.0	-04.2	03.2	04.2	03.3	80	69	72	74	N	2	NNE	2	NNE	2	
4	751.6	750.4	749.9	-07.2	02.4	-05.4	-03.9	03.3	-07.6	-10.0	02.4	03.4	02.8	91	62	90	81	NNE	1	NE	1	-	0	
5	750.0	749.9	750.3	<u>-08.6</u>	01.8	-00.6	-02.0	03.4	<u>-09.7</u>	-11.1	<u>02.1</u>	03.8	03.9	89	72	89	83	NE	1	N	1	-	0	
6	749.3	747.3	746.3	-03.0	04.8	-01.6	-00.4	06.0	-05.0	-05.6	03.3	04.2	03.7	89	66	91	82	-	0	SM	1	-	0	
7	744.0	740.3	739.3	-05.2	03.7	-02.0	-01.4	04.2	-05.9	-07.6	03.0	04.3	03.7	95	71	94	87	-	0	-	0	S	1	
8	736.8	732.9	734.0	-02.2	00.7	01.0	00.1	01.0	-05.0	-06.0	03.7	04.2	04.8	94	88	97	93	-	0	S	1	NNW	3	
9	740.8	744.3	749.2	02.2	03.1	01.7	02.2	03.7	00.8	00.3	03.0	03.1	02.9	56	54	56	55	NNW	5	NNW	5	NNW	2	
10	751.8	751.0	751.5	-05.0	03.2	-03.6	-02.2	04.4	-05.0	-07.4	02.5	02.8	02.9	78	49	82	70	E	1	WSW	2	-	0	
11	751.9	750.7	750.7	-08.0	02.9	-04.0	-03.3	03.7	-08.6	-10.6	02.2	03.1	03.1	87	56	90	78	-	0	SSW	1	SSW	1	
12	750.4	749.3	750.3	-07.4	03.6	-01.8	-01.8	04.6	-07.9	<u>-11.2</u>	02.4	03.6	03.5	93	61	87	80	-	0	SM	1	-	0	
13	751.9	750.5	751.9	-04.0	01.8	-01.9	-01.5	03.9	-04.8	-07.0	03.1	03.6	03.8	92	70	96	86	-	0	S	1	-	0	
14	752.7	752.5	754.2	-05.8	05.8	-01.0	-00.5	06.0	-06.0	-07.4	02.8	04.4	03.9	94	63	92	83	S	1	ESE	1	SSE	1	
15	754.3	753.2	753.9	-05.4	-00.4	-02.8	-02.8	02.7	-06.4	-09.0	02.9	04.3	03.3	95	96	89	93	SSE	1	-	0	SSE	1	
16	753.3	751.6	751.3	-04.0	-02.1	-03.4	-03.2	-01.5	-06.0	-08.2	03.3	03.8	03.4	96	96	95	96	-	0	-	0	SE	1	
17	750.4	748.2	748.4	-04.8	-03.1	-04.0	-04.0	-03.0	-04.9	-05.6	03.1	03.5	03.3	95	97	96	96	-	0	-	0	-	0	
18	747.3	745.3	746.1	-04.9	-03.8	-04.6	-04.5	-03.0	-05.0	-05.2	03.0	03.3	03.1	95	96	96	96	-	0	-	0	-	0	
19	746.5	746.5	748.2	-05.6	-04.4	-04.6	-04.8	-04.0	-06.2	-05.4	02.9	03.1	03.1	95	94	96	95	SE	1	SSE	1	-	0	
20	750.1	749.4	749.8	-05.2	-02.8	-03.8	-03.9	-02.8	-05.4	-05.0	03.0	03.6	03.3	95	97	96	96	-	0	-	0	-	0	
21	750.1	749.1	749.5	-05.4	-03.9	-04.6	-04.6	-03.6	-05.4	-05.1	03.1	03.4	03.3	100	100	100	100	SSE	1	-	0	-	0	
22	749.5	748.7	748.6	-04.3	-02.6	-02.4	-03.0	-02.2	-05.4	-05.0	03.2	03.7	03.7	100	98	96	98	-	0	SSE	2	-	0	
23	747.3	746.3	746.0	-02.6	00.2	-03.6	-02.4	00.7	-03.6	-03.0	03.5	04.5	03.5	94	96	100	97	-	0	NNW	1	SE	2	
24	745.3	744.9	745.1	-04.7	-00.6	-02.6	-02.7	01.0	-06.3	-09.0	03.1	04.0	03.6	95	92	97	95	SE	1	-	0	-	0	
25	745.7	745.2	746.1	-02.2	04.6	-01.5	-00.2	06.4	-04.0	-06.6	03.7	04.7	04.0	94	74	97	88	-	0	-	0	-	0	
26	745.5	745.4	746.6	-04.7	02.2	00.2	-00.5	03.0	-05.0	-07.0	03.0	04.2	04.5	93	77	96	89	-	0	SW	1	SSW	1	
27	746.6	744.8	742.4	03.2	06.6	-01.2	01.8	07.0	-01.2	-02.2	04.5	04.6	03.8	78	63	90	77	NNW	2	MSW	2	NE	1	
28	738.2	735.4	735.1	-02.0	02.0	01.0	00.5	02.4	-04.0	-06.4	03.7	04.2	04.6	92	79	93	88	-	0	NE	1	NE	1	
29	734.4	733.8	735.6	00.8	<u>09.0</u>	02.2	03.6	10.2	00.6	00.4	04.7	<u>02.5</u>	04.7	97	64	87	83	NE	1	-	0	-	0	
30	739.3	739.0	740.5	03.6	07.6	01.8	03.7	09.0	06.9	-00.9	03.6	03.0	03.4	61	32	64	55	NNW	2	N	3	NNE	2	
31	744.3	745.8	747.8	04.2	05.1	01.2	02.9	06.5	01.1	-02.0	03.8	04.5	04.2	62	68	85	72	N	4	NNE	5	NNE	3	
MES.	VRED.	747.2	746.3	747.0	-03.4	01.7	-01.8	-01.3	02.6	-04.7	-05.9	03.2	03.9	03.6	89	76	89	85	0.9	1.3	0.8			

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1	746.5	745.4	747.6	-03.4	09.1	03.2	03.0	05.8	-04.0	-07.0	03.3	04.3	04.0	93	50	69	71	NE	1	SSW	2	NNE	4
2	750.0	748.3	747.1	00.4	06.0	00.4	01.8	06.6	-01.2	-03.6	03.4	03.3	03.6	72	47	77	65	N	3	N	4	NNE	2
3	744.5	744.8	747.7	-02.4	06.1	03.1	02.5	07.2	-02.4	-04.6	03.6	03.8	04.4	94	53	77	75	ENE	1	-	0	NE	1
4	750.7	752.6	753.7	01.8	04.0	00.4	01.6	04.6	-01.0	-01.5	04.7	04.6	04.0	90	76	84	83	NE	2	-	0	NE	2
5	754.8	753.3	753.0	-00.4	04.6	-01.8	00.2	05.0	-01.9	-04.5	03.3	03.5	03.1	75	55	76	69	NNE	4	NE	4	NE	5
6	753.5	751.8	750.7	-05.8	05.7	-00.4	-00.2	06.6	-06.0	-09.0	02.7	03.5	03.2	90	51	71	71	-	0	NNE	2	NNW	2
7	747.6	742.5	739.1	-07.3	07.4	-02.0	-01.0	09.0	-08.0	-11.0	04.5	03.3	03.2	93	43	60	72	NNE	2	MSW	2	-	0
8	738.0	742.3	746.0	03.2	04.4	-02.3	-00.2	05.8	-05.0	-09.4	03.3	03.1	02.7	58	65	70	64	NNE	7	N	5	NNE	1
9	747.8	747.3	747.4	-08.6	02.4	-04.9	-04.0	02.4	-10.0	-13.5	02.1	02.1	02.0	87	39	64	63	NE	3	NW	3	NNE	2
10	747.6	746.2	746.0	<u>-10.4</u>	04.9	-05.6	-04.2	06.7	<u>-11.5</u>	<u>-14.6</u>	01.8	02.5	02.0	85	38	66	63	-	0	WSW	1	-	0
11	746.4	745.2	744.8	-10.0	08.2	-03.6	-02.2	09.6	-10.1	-12.9	01.8	02.5	02.4	85	31	69	62	-	0	SW	1	-	0
12	744.9	742.3	741.5	-08.8	10.6	01.2	01.0	12.9	-09.0	-11.5	02.2	03.4	03.7	92	35	75	67	-	0	W	1	SE	1
13	739.6	737.6	735.9	-04.6	05.4	02.1	01.2	06.8	-05.4	-08.4	02.8	04.7	04.7	87	69	89	82	SE	1	SE	1	SSE	1
14	733.6	734.3	734.0	-00.3	13.6	06.2	06.4	14.8	-00.4	-02.2	04.2	05.2	05.6	94	45	78	72	SE	1	-			

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 $H_a = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_x = 1.3 \text{ m}$

Dan	Vrijeme s p. o.	Oblačnost N (0-10)					Inzolacija kraj seči	Padavina R mm	Snežni pokrivali h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7 10*	10	01	07.0	00.2	09.0	02	$\mu_0 0-2^{25} * 0-0-0-9^{30} \square$		
2	7 10*	05	10	08.3	00.1	01.7	03	$* 0-14^{21} 12^{21} 15^{20} \square$		
3	7 06	08	02	05.3	05.3	00.5	03	$\square 19^{22} 24^{20} \square$		
4	7 01	01*	00	06.7	06.7	*	*	$\square 0-1-0-10^{20} 10^{20} 24-23^{20} 24$		
5	6 03	09	00	04.0	01.0	*	*	$\square 0-1-0-11^{21} 24-24; = 0-15^{25} 22^{25} 24$		
6	6 08	00	00	02.7	04.1	*	*	$\square 0-1-20-0-9^{30} 19^{20} 24; = 0-7^{25}$		
7	5 00	00	00	00.0	04.5	*	*	$\square 0-10^{20} 17^{20} 24; = 6^{20} 24$		
8	3 10	10	10*	10.0	00.0	*	*	$\square 0-12^{24} = 0-7^{25} 20^{20}; = 0-7^{25} 20^{20}; = 0-14^{25} 19^{20} 20^{20}; = 0-20^{25} 24^{25} \square$		
9	7 08	07	04	06.3	01.9	06.0	*	$\mu_0 0-20^{24} = 0-1-0-7^{25} 20^{20}; = 0-7^{25} 20^{20}; = 0-14^{25} 19^{20} 20^{20}; = 0-20^{25} 24^{25} \square$		
10	7 00	01	00	00.3	07.9	*	*	$\square 0-19-24$		
11	7 00	00	00	00.0	05.7	*	*	$\square 0-1-20-0-11^{25} 24$		
12	6 07	05	00	04.0	04.0	*	*	$\square 0-1-20-0-19^{20} 24; = 0-16^{25} 17^{30}$		
13	5 09	09	04	07.3	00.3	*	*	$\square 0-10-12^{25} 24; = 0-16^{25} 24$		
14	5 00	00*	00	00.0	06.1	*	*	$\square 0-20-11^{25} 24; = 0-1-0-0-24$		
15	2 00	10*	00	03.3	01.6	*	*	$= 0-20-8^{25} 24; = 0-1-0-13, 17-24; = 0-8^{25} 9^{30}, V^0 8^{25} 13^{30}, = 0-9^{25} 14^{30}$		
16	2 10**	10**	10**	10.0	00.0	*	*	$\square 0-24, = 0-3^{20} V^0 3-24 = 3^{20} 24$		
17	2 10**	10**	10**	10.0	00.0	*	*	$\square 0-24, = 0-20-24, V^0 0-24$		
18	2 10**	10**	10**	10.0	00.0	*	*	$\square 0-24, = 0-20-24, V^0 0-24$		
19	4 10**	10	10	10**	00.0	*	*	$\square 0-24, = 0-20-0-11^{25} 16^{25} 24; = 0-11^{25} 15^{25} 16^{25}; = 13^{25} 15^{25}$		
20	3 10**	10**	10**	10**	00.0	*	*	$\square 0-24, = 0-20-0-24$		
21	2 10**	10**	10**	10.0	00.0	*	*	$\square 0-24, V^0 0-24 = 0-24$		
22	4 10**	10	10	10.0	00.0	*	*	$\square 0-24, V^0 0-24, = 0-20-24, = 12^{25} 24$		
23	5 10	10	00	04.7	00.0	*	*	$\square 0-24, = 0-12^{25} 17^{25} 24; = 0-10-12^{25} 17^{25} 24; = 0-24, = 0-4^{25} 5^{30}$		
24	5 10	09	06	08.3	00.6	*	*	$= 0-24, = 0-10-12^{25} 17^{25} 24; = 0-24, = 0-4^{25} 5^{30}$		
25	3 10	01	00	03.7	03.3	*	*	$= 0-24, = 0-10-9^{25} 24, = 0-8^{25} 9^{30}$		
26	7 10	10	09	09.7	00.0	00.0	*	$\square 0-10^{20} = 0-6^{25} 12^{20} 24; = 6^{25} 12^{20} 16^{20} 17^{30}; = 0-17^{25} 18^{30}$		
27	8 05	04	00	03.0	01.0	00.0	*	$= 0-20-5^{25} \square 17^{25} 24$		
28	4 10	09	10	09.7	00.0	*	*	$\square 0-10-12^{25} 17^{25} 24; = 0-24, = 0-8^{25} 24, = 0-11^{25} 13^{30}$		
29	6 10	01	09	06.7	04.9	00.2	*	$\square 0-14^{25} 10^{25} 14^{25} 23^{25} \square$		
30	8 05	04	01	03.3	05.6	*	*	$\mu_0 0-5^{25} 10^{25} 14^{25} 17^{25} 18^{25}$		
31	8 10	09	02	07.0	01.1	*	*	$\mu_0 11^{25} \square$		
MES. VRED.	07.2	06.5	04.4	06.0	67.9	17.4				

1	7 00	01*	00	00.3	08.0	*	*	$\square 0-11^{25} 9^{30} 23^{25} 24; = 7^{25} 9^{30}$		
2	7 01	04	09	04.7	06.8	*	*	$\square 0-8, \mu_0 10^{25} 16^{25} \square$		
3	7 10	07	10	09.0	01.3	*	*	$\square 0-20-9^{25} 16^{25} 17^{30}$		
4	7 10	10	00	06.7	00.0	00.0	*	$\square 0-3^{25} 4^{25} 8^{25} 9^{25} = 9^{25} 11^{40}$		
5	7 09	01	00	03.3	06.2	*	*	$= 0-11^{25} \mu_0 15^{25} 23$		
6	7 00	00	00	00.0	08.3	*	*	$\square 0-12^{25} 9^{25} 22^{25} 24$		
7	6 00	00	00	00.0	06.7	*	*	$\square 0-20-9^{25} 20^{25} 24; = 6^{25} 13^{25}$		
8	7 02	06	08	07.3	02.6	*	*	$\square 0-6, \mu_0 15^{25} 16^{25} + 12^{25} 13^{25}$		
9	8 00	01*	00	00.3	08.9	00.0	*	$\square 0-3^{25} 8^{25} 10^{25} 11^{25}$		
10	8 00	00*	00	00.0	08.9	*	*	$\square 0-10, 20^{25} 24$		
11	7 00	00	00	00.0	08.8	*	*	$\square 0-9^{25} 22^{25} 24$		
12	7 01	01	05	02.3	08.5	*	*	$\square 0-9^{25}$		
13	7 06	10	10	08.7	00.4	*	*	$\square 0-2-8$		
14	7 10	06	07	07.7	05.2	*	*	$= 0-16, 12^{25} 15^{25} 18^{25}$		
15	8 08	01	02	03.7	06.9	*	*	$\square 0-12, 9^{25} 16^{25} 12^{25} 17^{25}$		
16	6 10	10	10*	10.0	00.0	*	*	$\square 0-14, 7, 0-7-9^{25} 17^{25} 24, 8^{25} 14^{25} \mu_0 18^{25}-22^{25}$		
17	5 00*	00*	00	00.0	00.0	05.6	01	$\square 0-10, 8, 0-12, 7, 0-20-24, \square$		
18	7 10*	08	10	09.3	03.2	01.4	*	$= 0-14, 8, 0-12, 7, 0-20-24, \square$		
19	6 00	01	00	00.3	08.5	00.0	*	$\square 0-25, 9^{25} 6^{25} 17^{25} 24$		
20	4 10	10*	10	10.0	00.0	*	*	$\square 0-9, = 0-20-15^{25} 16^{25}, 0-10^{25} 16^{25}, * 16^{25} 18^{25}$		
21	6 10*	09	10	05.7	00.3	02.2	*	$* 0-10^{25} H^{25}, = 10^{25} 15^{25} \mu_0 18-22, \square$		
22	7 04	06	00	03.3	08.1	*	*	$\square 10-40$		
23	8 00	01*	02	01.0	09.6	*	*	$\square 0-9^{25} = 0-7^{25} H^{25}$		
24	7 10	07	00	05.7	05.6	*	*	$\square 0-10, = 0-5^{25} 10^{25}, \mu_0 21-24$		
25	7 03	03*	04	03.3	06.1	*	*	$\mu_0 12^{25} 18, = 0-7^{25} 12^{25}$		
26	7 04	10	10	08.0	00.3	*	01	$\square 0-10^{25} 3^{25}, \mu_0 9^{25} 18^{25}, \square$		
27	8 10	03*	01	04.7	08.9	00.1	*	$\square 0-10^{25} 3^{25}, \mu_0 9^{25} 18^{25}, \square$		
28	8 00	04*	06	03.3	08.9	*	*			
MES. VRED.	04.6	04.3	04.1	04.4	147.0	09.3				

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 $\varphi = 41^{\circ}57'$ $N\lambda = 21^{\circ}38'$ E Gr. $\Delta G = + 1h 27 min.$

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d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina vetrova D, I (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	744.7	744.7	745.6	-06.4	12.4	-01.2	00.9	13.6	-07.2	-10.0	02.4	02.1	02.8	85	19	66	57	NE	1	W	3 ESE 2	
2	746.4	744.5	744.4	-07.0	15.2	00.6	02.4	16.4	-07.4	-11.6	02.4	02.8	03.5	89	22	72	61	-	0	W	1 - 0	
3	744.8	741.5	741.0	-04.2	16.2	04.0	05.0	18.6	-05.6	-07.9	02.7	03.1	03.3	79	23	53	52	-	0	N	1 ENE 2	
4	741.7	739.6	739.6	-02.8	14.9	08.2	07.1	16.2	-03.5	-05.5	03.4	04.6	04.4	92	36	54	61	-	0	S	1 ENE 1	
5	741.8	740.6	742.6	-01.8	17.6	08.2	08.0	18.3	-02.1	-05.5	03.7	04.7	05.0	93	31	62	62	ENE 1	SSE 2	-	0	
6	745.9	744.2	744.7	-00.2	17.2	11.0	09.8	18.5	-01.1	-03.6	04.2	05.4	05.6	93	37	57	62	-	0	SSE 3	ESE 2	
7	746.2	744.9	745.0	03.0	14.4	07.0	07.8	16.6	02.0	00.2	05.0	06.6	06.1	87	53	81	74	ENE 1	NN 1	E	2	
8	744.9	741.4	739.5	01.2	17.4	13.4	11.4	18.8	00.2	-01.6	04.8	06.9	06.4	97	46	56	66	-	0	WSN 1	ESE 1	
9	737.0	735.1	734.5	05.0	11.8	09.8	09.1	15.8	04.1	02.1	05.8	07.6	07.4	88	74	81	81	-	0	SSE 5	SSE 3	
10	732.0	730.8	733.4	08.2	15.7	10.0	11.0	16.3	07.5	07.0	07.3	06.4	06.6	90	48	72	70	SE 2	SSE 4	SSE 1		
11	738.8	741.0	743.2	06.8	15.8	07.2	09.2	17.4	04.6	02.1	07.0	06.1	06.2	95	45	82	74	S	2	NNM 1	- 0	
12	744.1	740.1	739.9	00.4	18.4	12.0	10.7	18.6	-00.7	-03.1	04.4	05.0	04.6	93	32	44	56	-	0	SSE 5	SSE 3	
13	740.6	738.0	738.4	02.6	20.2	12.2	11.6	21.0	00.9	-01.2	04.6	05.7	06.6	84	32	59	59	NNE 2	S	2 SE 3		
14	738.2	736.7	739.6	10.4	18.8	09.4	12.0	19.7	09.4	08.0	07.3	06.9	08.4	77	42	95	71	SSE 3	SSE 1	NN 4		
15	741.9	741.1	740.2	05.0	15.3	08.6	09.4	18.1	04.6	02.4	06.0	07.0	06.7	91	54	80	75	E	1	W	1 SSE 1	
16	740.2	737.1	737.0	04.2	15.4	07.4	08.6	17.1	04.1	01.3	06.0	06.1	06.7	97	46	87	77	ENE 1	W	1 NE	1	
17	736.9	734.4	735.0	04.8	15.6	00.0	09.1	16.4	03.4	00.8	06.0	05.5	06.0	93	42	75	70	E	1	NNM 2	- 0	
18	737.3	737.3	739.0	02.4	15.2	06.2	07.5	16.6	02.0	-00.3	05.0	04.9	05.4	92	38	76	69	-	0	E	2 - 0	
19	741.4	740.2	739.2	05.4	16.2	12.2	11.5	17.3	03.2	02.0	05.6	07.0	06.8	83	51	64	66	MNE 2	NN 2	SSE 3		
20	737.5	736.5	736.6	10.3	13.0	06.6	09.1	15.4	06.6	06.5	06.9	07.5	06.7	73	67	92	77	SE 2	ESE 2	E	1	
21	735.7	733.6	735.1	07.4	16.2	09.4	10.6	16.6	05.5	04.0	07.3	07.6	08.0	95	55	90	80	-	0	- 0	NE 1	
22	738.6	737.5	736.9	02.6	03.7	00.4	01.8	09.4	00.3	01.1	04.3	03.9	04.6	78	66	96	80	W	2	NNM 2	- 0	
23	734.8	733.6	734.0	-00.3	05.2	04.2	03.3	06.0	-00.4	-00.7	04.2	04.6	05.1	94	69	82	82	-	0	E	2 - 0	
24	731.3	730.4	729.8	04.6	04.7	04.6	04.6	06.4	03.5	03.0	05.1	05.7	06.1	80	88	96	88	ESE 2	W	1 E	1	
25	731.2	731.5	734.4	03.8	08.6	03.0	04.6	09.5	02.7	00.6	05.5	04.9	04.4	91	59	78	76	NN 2	N	5	ENE 3	
26	737.6	737.9	738.3	02.4	10.4	02.8	04.6	10.9	-01.4	-03.9	03.4	03.5	03.7	62	37	66	55	NNM 2	NNM 5	S	1	
27	739.7	737.8	737.8	-01.1	14.2	08.8	07.7	15.6	-04.1	-06.6	03.4	03.5	04.8	81	29	57	56	-	0	S	2 S	3
28	737.7	736.3	735.5	05.0	13.6	10.8	10.0	14.8	03.2	01.8	05.4	06.1	06.0	83	52	62	66	-	0	SE	5 SE 6	
29	737.3	736.8	738.2	10.0	17.0	11.2	12.4	17.7	08.6	07.6	07.3	08.3	07.7	79	57	77	71	S	3	SSE 4	E	2
30	739.3	736.2	736.2	05.4	19.9	14.4	13.5	20.8	04.3	02.6	06.3	07.3	08.1	94	42	66	67	-	0	SE	4 ENE 5	
31	736.6	735.0	737.7	13.6	22.2	17.2	17.6	22.4	10.9	08.5	09.0	10.5	09.6	77	52	65	65	ENE 1	SSE 5	NNM 2		
MES.	VRED.	739.4	737.9	738.5	03.2	14.6	08.0	08.4	16.0	01.9	00.1	05.2	05.7	05.9	87	46	72	68	1.0	2.6	1.7	

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1	738.9	738.4	739.9	13.8	19.1	13.0	14.7	20.7	12.2	10.5	10.3	08.2	10.5	87	49	93	76	SE	3	SSE 6	E 2	
2	737.4	735.6	734.6	09.5	19.4	15.4	14.9	20.2	08.9	08.1	08.6	09.5	07.9	96	56	60	71	-	0	ESE 4	SSM 3	
3	735.2	737.7	740.6	10.0	15.8	07.2	10.0	17.0	05.6	02.6	07.0	04.1	05.1	77	31	66	58	WWN 4	WSM 4	SM 2		
4	743.2	742.0	743.2	04.0	19.2	13.4	12.5	20.2	02.2	00.0	05.7	04.4	04.9	94	26	43	54	SE 1	S	2		
5	745.8	744.5	745.6	06.8	21.2	12.4	13.2	23.1	02.8	00.0	06.2	06.6	06.5	84	35	60	-	0	-	0	SE 2	
6	747.5	744.0	743.2	07.4	25.4	20.0	18.2	26.9	05.6	02.8	07.1	07.3	06.3	92	30	36	53	-	0	SE 1	S 4	
7	743.7	740.4	739.4	10.8	26.0	17.0	17.7	26.2	05.8	05.1	07.5	06.2	04.6	77	25	32	45	N	1	SE 3	SE 2	
8	738.4	732.9	739.1	10.2	20.8	11.6	15.6	29.4	05.8	03.4	07.2	04.2	04.8	77	14	47	46	N	2	SW 5	NE 2	
9	742.4	739.9	739.7	05.8	19.4	09.8	11.2	21.3	00.4	-02.5	06.0	03.8	05.3	86	23	58	56	SE 1	NNE 2	E 1		
10	738.2	735.7	733.1	08.0	14.4	14.3	12.8	15.9	05.0	02.4	06.2	08.5	07.1	77	69	58	68	NNW 2	SE 5	SE 2		
11	735.1	738.1	741.6	12.2	14.8	07.4	10.4	16.9	07.4	05.1	04.5	03.8	04.8	42	30	62	45	WWN 5	WWN 5	ENE 3		
12	743.7	741.5	744.3	01.8	14.4	06.6	07.4	16.2	-01.6	-04.1	05.2	03.8	05.4	100	31	73	68	-	0	N	3 NE 4	
13	745.9	742.6	741.8	02.0	17.2	07.6	08.6	18.7	-01.3	-04.2	05.1	03.7	04.9	97	25	62	61	-	0	NE 3	S 2	
14	743.8	741.3	740.3	03.5	20.6	12.0	12.0	21.4	00.0	-03.0	05.4	05.3	05.2	92	29	50	57	-	0	SE 2	NE 2	
15	740.6	736.4	735.2	07.1	23.6	16.8	16.1	24.4	02.6	-00.9	07.1	04.7	06.0	93	22	42	52	E	1	SE 3	SE 2	
16	735.1	731.2	732.1	06.4	22.9	14.8	14.7	23.6	01.6	-01.0	06.8	06.0	08.2	94	29	65	63	-	0	SSE 4	S 3	
17</																						

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 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$

Dan	Visinovost O-9	Oblačnost N (0-10)					Inseleacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8 000	000	00	00	00.0	-	.	.	✓ 0-8 ³⁰	
2	8 000	040	00	01.3		-	.	.	✓ 0-9 ³⁰	
3	8 020	050	C0	02.3		-	.	.	✓ 0-8 ³⁰	
4	7 09	07	06	07.3		-	.	.		
5	8 01	020	00	01.0		-	.	.	✓ 0-14 ³⁰ 7 ⁴⁵ , ✓ 0-23 ⁴⁵ 23 ⁴⁵	
6	8 020	08	02	04.0		-	00.0	.		
7	7 08	09	00	05.7		-	.	.	= 0-9 ³⁵ 12 ³⁰	
8	7 07	09	10	08.7		-	.	.	= 0-16-13 ³⁰ ; = 6 ³⁵ 7 ³⁰	
9	8 10	09	10	09.7		-	.	.	F ₃₅₅ 10 ³⁵ 13 ³⁰ , F ₄₅₅ 14 ³⁵ 15 ³⁰	
10	8 09	C6	10	C8.3		-	00.2	.	✓ 0-17 ³⁰ H ₁ , F ₃₅₅ 10 ³⁵ 4 ³⁰	
11	8 10	040	02	05.3		-	01.6	.	✓ 0-3 ³⁵ 6 ⁴⁵	
12	7 000	10	00	03.3		-	.	.	✓ 0-10-4 ³⁰ , ✓ 0-4 ³⁰ 8 ³⁰ , F ₃₅₅ 13-19	
13	7 000	03	00	01.0		-	.	.	F ₃₅₅ 7 ³⁵ 20 ⁴⁵ , ✓ 0-19 ⁴⁵ 23 ³⁰	
14	7 02	04	10	05.3		-	.	.	✓ 0-1-1, 22 ³⁰ 24 ³⁰ ; F ₃₅₅ 20 ³⁵ 23 ³⁰ , ✓ 0-1-23 ³⁰ 23 ³⁰ , F ₃₅₅ 24, ▲ 23 ³⁰ 23 ³⁰	
15	8 02	040	04	03.3		-	17.2	.		
16	8 020	030	00	01.7		-	09.4	.	F ₃₅₅ 10 ³⁵ 10 ³⁰ T ₁₅ ³⁵ 14 ³⁵ , ✓ 0-120-24	
17	7 07	06	02	05.0		-	.	.	✓ 0-0-9 ³⁰ 12 ³⁰ , ✓ 0-16 ³⁵ 16 ³⁰	
18	7 01	04	00	01.7		-	00.2	.	✓ 0-0-10-20-24	
19	8 09	09	09	09.0		-	.	.	✓ 0-8 ³⁰ 15 ³⁰ , □ 20 ³⁰ 24 ³⁰ , ✓ 0-120 ³⁰ 24	
20	8 10	08	04	07.3		-	.	.		
21	7 10	07	10	09.0		-	01.0	.	✓ 0-1-0-4 ³⁰ 12 ³⁰ 6 ³⁰ 16 ³⁰ 23 ³⁰ ; = 6 ³⁵ H ₁ , T ₁₅ ³⁵ 17 ³⁵ , F ₃₅₅ 16 ³⁵ 16 ³⁰ 24-8 ³⁰ 13 ³⁰ 15 ³⁰	
22	7 10	10	10*	10.0		-	09.6	.	✓ 0-2 ³⁰ 4 ³⁰ 18 ³⁰ 24 ³⁰	
23	7 10*	10	09	09.7		-	05.9	03	* 0-10-9 ³⁰ = 0-8 ³⁰ 13 ³⁰	
24	7 10	10	10	10.0		-	00.4	.	✓ 0-1-20-24	
25	8 10	08	05	07.7		-	05.4	.	✓ 0-1-0 ³⁰ 0 ³⁰ 5 ³⁰ 7 ³⁰ , 15 ³⁰ 16 ³⁰ ; = 4 ³⁰ G ³⁰ , F ₃₅₅ 10 ³⁵ 19 ³⁰	
26	8 03	04	00	02.3		-	00.0	.	✓ 0-1-4-5 ³⁰ 20 ³⁰ 24, ✓ 0-5 ³⁰ 7 ³⁰ , F ₃₅₅ 0 ³⁰ 15 ³⁰	
27	8 000	040	02	02.0		-	.	.	✓ 0-1-0-9	
28	7 10	10	09	09.7		-	.	.	F ₃₅₅ 13 ³⁰ 24	
29	7 10	10	03	07.7		-	.	.	F ₃₅₅ 0-1 ³⁰	
30	7 07	09	00	05.3		-	.	.	✓ 0-0-9 ³⁰ = 0-15 ³⁰ 9 ³⁰ , F ₃₅₅ 14 ³⁰ 24	
31	7 06	01	00	02.3		-	.	.	F ₃₅₅ 0-0 ³⁰ 8 ³⁰ 16 ³⁰ , □ 0-3 ³⁰ , ▲ 0-17 ³⁰ 17 ³⁰	
MES. VRED.	05.7	06.4	04.1	05.4	-	51.1				

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1	7 10	10	10*	10.0	02.3	01.0	.	T 1 ³⁵ 2 ³⁰ ; ✓ 0-1-1 ³⁰ 2 ³⁰ , 15 ³⁵ 16 ³⁵ , 19-23 ³⁰ ; F ₃₅₅ 9 ³⁰ 15 ³⁰	
2	7 07	09*	02	06.0	04.1	C5.7	.	✓ 0-1-8 ³⁰ 10 ³⁰ ; F ₃₅₅ 18 ³⁰ 19 ³⁰	
3	8 09	05	00	04.7	08.2	00.4	.	✓ 1 ³⁰ 6 ³⁰ 0-6 ³⁰ 7 ³⁰ ; F _{NN} 9 ³⁰ 16 ³⁰	
4	8 090	060	00	05.0	10.2	00.2	.	✓ 0-9 ³⁰	
5	8 08	08	00	05.3	07.5	.	.	✓ 0-1-7 ³⁰ 21 ³⁰ 24	
6	8 09	07	00	05.3	C7.6	.	.	✓ 0-10-9	
7	8 10	06	00	05.3	07.2	.	.	F ₃₅₅ 16 ³⁰ 20	
8	8 020	010	00	01.0	07.0	.	.	✓ 0-1-8 ³⁰ , F ₃₅₅ 10-20 19 ³⁰	
9	8 000	020	00	0C.7	11.8	.	.	✓ 1 ³⁰ 9 ³⁰	
10	7 10	09*	02	07.0	04.0	00.0	.	✓ 0-0-4 ³⁰ , □ 4 ³⁰ 5 ³⁰ 10 ³⁰ ; 13 ³⁰ 14 ³⁰ ; F ₃₅₅ 8 ³⁰ 20	
11	8 030	06	00	03.0	09.1	00.0	.	✓ 0-10-6 ³⁰ F ₃₅₅ 18 ³⁰ 20 ³⁰ , T ₂₂ ⁴⁵ 23 ³⁰ ; ✓ 0-12-23 ³⁰	
12	8 030	09	10	07.3	07.0	.	.	✓ 0-3 ³⁰ 7 ³⁰ ; F ₃₅₅ 16-20 ³⁰ , □ 0-19-19 ³⁰	
13	8 000	010	00	00.3	11.0	00.0	.	✓ 2 ³⁰ 8 ³⁰	
14	8 000	010	00	00.3	11.7	.	.	✓ 0-4 ³⁰ 7 ³⁰	
15	8 040	010	00	01.7	11.2	.	.	✓ 0-3-7 ³⁰	
16	8 010	060	C2	03.0	11.5	.	.	✓ 0-1-0-6 ³⁰ F ₃₅₅ 18 ³⁰ 20 ³⁰ , T ₂₂ ⁴⁵ 23 ³⁰ ; ✓ 0-12-23 ³⁰	
17	7 100	10	10	10.0	00.3	01.7	.	✓ 0-5 ³⁰ 7, F ₃₅₅ 18 ³⁰ 18 ³⁰	
18	7 10	10	06	08.7	02.4	.	.	F _{NN} 4 ³⁰ 18 ³⁰	
19	7 08	060	00	04.7	C2.8	.	.	F ₃₅₅ 8 ³⁰ 17 ³⁰	
20	7 06	020	00	02.7	08.7	.	.	F ₃₅₅ 8 ³⁰ 9 ³⁰ , 13 ³⁰ 18 ³⁰	
21	7 000	000	00	00.0	12.0	.	.	✓ 0-3-4 ³⁰ , □ 0-4 ³⁰ 7 ³⁰	
22	7 010	050	01	02.3	08.9	.	.	F ₃₅₅ 16 ³⁰ 17	
23	7 10	10	10	10.0	CC.C	00.0	.	✓ 0-6 ³⁰ 7 ³⁰ , 14 ³⁰ 24 ³⁰ ; = 0-7 ³⁰ 12 ³⁰	
24	6 100	10*	10*	10.0	00.0	05.5	.	✓ 0-10-14, 16 ³⁰ 17 ³⁰ 24 ³⁰ ; = 0-14 ³⁰ 17 ³⁰ 21 ³⁰ 24	
25	7 09	08	10	09.0	03.6	01.8	.	= 0-3 ³⁰ 5 ³⁰ 11 ³⁰ ; □ 11 ³⁰ 12 ³⁰ 16 ³⁰ 24	
26	7 100	08	100	09.3	01.4	00.4	.	✓ 0-4-6 ³⁰ , 9 ³⁰ 14 ³⁰ 20 ³⁰ 22 ³⁰ ; F _{NN} 10 ³⁰ 14, 17 ³⁰ 20 ³⁰	
27	7 10	10	10	10.0	00.0	02.2	.	✓ 0-4-10 ³⁰ 17 ³⁰ 24 ³⁰ 24; □ 12-16 ³⁰	
28	7 10	09	10	09.7	00.2	03.2	.	✓ 0-0-3 ³⁰ 9 ³⁰ 14 ³⁰ 15 ³⁰	
29	7 01	04	00	01.7	11.6	00.0	.	✓ 1 ³⁰ 9 ³⁰	
30	7 00	01	00	0C.3	12.1	.	.	✓ 0-10-7 ³⁰ 20 ³⁰ 24; = 0-8-10 ³⁰	
MES. VRED.	06.0	06.0	03.4	05.1	195.7	22.5			

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 $\varphi = 41^{\circ}57' \text{ N } \lambda = 21^{\circ}38' \text{ E}$ Gr. $\Delta G = + 1 \text{h} 27 \text{ min.}$

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d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetroa D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	742.0	740.1	741.4	09.8	22.4	15.2	15.4	22.9	04.4	01.5	06.8	05.9	06.8	80	29	53	54	-	0	WNW 4	NNE 3
2	741.1	740.2	740.4	11.6	13.2	16.6	11.5	16.2	10.6	10.6	08.9	07.6	07.8	86	67	81	78	-	0	WNW 5	NNE 2
3	738.8	737.5	738.1	11.8	16.0	11.6	12.8	18.4	09.0	08.6	08.8	08.8	08.2	84	64	80	76	WNW 2	NNE 4	S 2	
4	739.8	739.6	741.5	10.4	20.4	12.0	13.7	21.4	07.6	05.2	08.6	07.0	06.7	91	39	82	71	-	0	NW 2	S 1
5	743.9	742.2	743.2	11.6	22.2	16.6	16.4	23.0	06.9	05.0	08.9	08.9	09.0	86	44	66	65	-	0	SE 2	SW 1
6	744.2	741.7	741.1	13.6	25.2	18.4	18.9	25.8	10.4	09.0	09.5	11.9	10.8	81	49	68	66	NE 1	SSE 4	SSE 2	
7	742.3	740.0	739.7	14.2	22.2	17.6	17.9	22.4	11.4	10.0	10.1	10.8	11.8	84	54	78	72	SSE 1	N 3	S 2	
8	739.2	737.5	737.5	14.8	21.8	16.6	17.4	23.8	12.4	10.5	11.3	11.3	11.7	90	58	83	77	-	0	SSE 5	SE 3
9	738.2	738.7	740.1	14.2	20.2	12.0	14.6	21.5	10.0	09.4	11.1	09.4	08.4	92	53	80	75	SW 2	SSE 3	SSE 1	
10	741.8	740.3	740.2	11.4	21.0	15.2	15.7	22.8	05.7	03.6	08.5	07.2	07.5	84	39	58	60	-	0	NNE 2	NNE 2
11	741.2	738.0	737.3	11.6	24.0	14.0	15.9	25.1	06.1	04.1	08.6	07.5	07.4	84	34	62	60	E 1	WSW 2	ESE 1	
12	736.4	733.7	733.6	13.2	24.2	15.3	17.0	25.6	08.9	06.0	08.1	08.5	10.3	71	37	79	62	-	0	SE 3	SSE 2
13	734.1	732.4	733.3	14.6	21.0	12.8	15.3	21.8	12.4	11.6	11.4	09.8	09.9	92	52	89	78	-	0	SSE 3	SE 2
14	732.2	732.6	733.6	12.4	16.6	12.4	13.4	18.0	10.5	10.5	10.3	09.7	09.8	96	68	91	85	-	0	ESE 1	N 1
15	734.0	734.7	735.6	13.4	18.4	12.7	16.6	20.4	10.7	09.7	10.1	11.6	12.2	87	73	83	81	WN 1	N 2	ESE 1	
16	736.7	736.6	738.7	16.8	23.4	18.9	19.5	24.6	14.4	13.4	11.6	11.3	11.6	81	52	71	68	W 1	WNW 2	NNE 3	
17	740.0	739.6	741.1	15.4	24.4	18.4	19.2	26.4	11.9	06.6	11.2	11.4	12.7	85	50	80	72	WNW 1	N 3	NE 2	
18	743.4	743.2	743.5	15.0	22.4	19.2	19.0	23.8	13.5	12.0	11.5	12.1	11.5	90	60	69	73	-	0	WNW 2	N 2
19	744.6	742.6	743.3	15.8	26.8	16.0	18.6	27.6	12.6	10.0	12.3	09.6	12.3	91	36	90	72	NE 1	S 1	E 1	
20	743.3	741.3	741.0	15.2	27.3	17.2	19.2	28.3	10.2	10.2	10.9	08.0	10.9	84	29	74	62	-	0	S 2	-
21	742.3	740.8	741.2	16.8	25.8	19.0	20.2	27.2	13.9	12.0	11.6	11.0	11.6	81	44	70	65	NE 1	WSW 2	NE 1	
22	742.1	739.8	739.6	16.0	26.2	18.2	19.6	27.7	11.2	08.9	11.5	09.7	11.5	84	38	73	65	-	0	E 2	S 2
23	740.4	737.5	736.7	16.2	28.4	20.6	21.4	28.6	11.4	08.9	11.1	09.7	12.3	81	33	68	61	-	0	SSE 3	E 1
24	738.4	735.5	737.0	16.5	26.6	14.4	18.0	27.0	14.4	13.3	12.8	13.6	11.5	91	52	94	79	SSW 1	SSE 3	-	
25	737.9	736.0	738.2	14.4	26.6	16.2	18.4	27.0	11.1	09.4	11.8	11.5	12.2	96	44	68	76	-	0	S 4	S 2
26	739.9	737.7	740.7	15.0	26.6	15.4	18.1	26.6	10.8	08.2	11.7	10.3	12.1	92	39	92	74	S 1	SSE 2	-	
27	740.7	738.6	739.7	14.2	25.4	13.2	16.5	25.4	10.4	08.8	10.9	12.4	10.2	90	51	89	77	-	0	S 2	NW 1
28	740.6	738.6	740.2	13.0	24.4	16.4	17.6	25.2	08.4	08.5	10.0	08.6	11.3	89	38	81	69	-	0	NW 1	NNE 2
29	741.2	740.7	739.5	15.9	23.8	17.8	18.8	25.3	13.0	10.8	12.1	12.0	11.9	89	54	78	74	-	0	NNW 2	-
30	740.4	738.9	738.7	17.1	26.6	21.7	21.8	28.0	11.4	10.0	12.3	12.7	14.5	84	49	75	69	SE 1	SSE 2	S 2	
31	739.1	737.3	737.4	18.6	29.3	21.4	22.7	30.2	14.3	12.6	12.9	09.5	12.3	80	31	65	59	-	0	SSE 2	ESE 2
MES.	VRED.	740.0	738.5	739.1	14.2	23.3	16.2	17.4	24.5	10.6	09.0	10.6	10.0	10.7	86	47	77	70	0.5	2.6	1.9

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1	739.2	737.0	737.2	17.8	29.2	21.2	22.4	31.0	12.4	11.1	11.5	12.0	13.0	75	39	69	61	-	0	NN 2	N 2
2	736.2	734.9	734.3	18.8	31.8	23.0	24.2	32.7	13.4	11.0	11.2	10.7	13.0	69	30	62	54	-	0	SSE 4	SSE 1
3	735.7	732.3	735.7	19.2	30.2	19.3	22.0	31.4	14.8	11.4	13.2	10.3	12.0	79	32	71	61	NN 2	NNE 2	NNE 6	
4	735.4	735.3	736.6	17.8	19.8	15.8	17.3	22.6	12.4	10.4	11.1	06.9	07.4	73	40	55	56	N 2	N 2	N 4	
5	739.4	739.7	740.7	13.6	12.8	11.0	12.1	13.6	11.0	07.4	07.8	07.4	07.4	63	70	75	69	NNW 3	NNW 3	NNW 2	
6	739.1	739.8	739.6	10.0	11.0	12.4	11.4	12.8	10.0	09.1	07.7	08.3	08.5	83	84	78	82	WNW 2	WSW 2	N 3	
7	740.0	739.6	740.7	12.8	15.0	12.2	13.0	15.8	11.8	10.8	07.1	06.9	07.4	64	54	70	63	N 4	NE 3	N 3	
8	739.5	738.4	739.8	11.0	19.1	16.2	15.6	21.8	06.4	05.4	08.0	10.2	08.9	82	62	64	69	-	0	NN 2	-
9	740.4	739.1	738.8	13.6	23.2	16.0	17.2	24.0	10.7	10.0	10.0	08.4	10.5	85	40	77	67	-	0	NW 1	E 1
10	739.2	738.2	738.9	13.8	23.6	16.0	17.4	24.4	12.3	10.2	10.3	09.0	11.0	87	41	81	70	-	0	SE 2	S 2
11	740.2	740.4	742.1	15.0	27.0	19.4	20.2	27.2	09.2	06.9	10.0	10.1	10.3	78	38	61	59	-	0	SW 2	NE 2
12	743.7	741.7	741.5	17.6	26.6	22.0	22.0	28.0	14.0	13.0	11.5	08.9	12.3	76	34	62	57	-	0	SSW 2	SSE 1
13	742.4	739.2	741.2	20.9	29.6	16.4	20.8	29.6	16.4	14.9	12.7	11.5	12.6	69	37	90	65	-	0	SE 4	NNE 3
14	740.4	738.5	739.0	15.7	25.2	19.0	19.7	26.0	12.9	11.5	12.4	14.6	12.4	93	61	75	76	S 1	NNW 2	-	
15	740.8	739.4	739.4	17.8	29.4	20.8	22.2	30.2	13.3	11.8	13.4	10.4	12.4	88	34	67	63	ESE 1	ESE 2	-	
16	741.6	738.7	738.1	19.2	30.9	25.0	25.0	32.0	14.4	12.4	12.6	10.7	09.7	75	32	41	49	NW 1	SE 5	S 2	
17	739.3	737.3	737.6	20.6	29.6	22.0	23.6	30.6	16.8	16.3	13.3	12.1	13.2	73	39	66	59	NE 2	SSW 2	-	
18	739.2																				

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$$H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_x = 1.3 \text{ m}$$

Dan	Vlajkost 0-9	Oblačnost N (0-10)					Isolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	01	01	09	08	06.0	08.2	.	.	$\Delta^{+0-9} F_{NNW-NNW} 14-17^{\circ}, 21^{\circ}, 22^{\circ}, 21^{\circ}, 22^{\circ}$
2	8	10	10	10	10	00.0	01.6	.	.	$\Delta^{+0-2} 24^{\circ}$
3	8	08	07	02	05.7	07.1	02.1	.	.	$\Delta^{+0-2} 2^{\circ}$
4	8	10	06	03	06.3	06.8	.	.	.	$\Delta^{+2-10}, \Delta^{+10-17^{\circ}}$
5	8	06	09	01	05.3	06.1	00.3	.	.	$\Delta^{+0-9}, 22^{\circ}, 24$
6	8	08	06	00	04.7	06.3	.	.	.	Δ^{+0-9}
7	7	10	10	10	10.0	00.0	.	.	.	
8	7	00	09	01	03.3	02.3	00.0	.	.	$\Delta^{+2-5^{\circ}}, 4^{\circ}, 10^{\circ}, 0^{\circ}, 15^{\circ}, 7, 13^{\circ}, 13^{\circ}, 16^{\circ}, 17^{\circ}, T 12^{\circ}, 13^{\circ}, 15^{\circ}, 19^{\circ}, 20^{\circ}$
9	8	10	03	00	04.3	08.7	03.6	.	.	$\Delta^{+0-14^{\circ}}, 6^{\circ}, 4^{\circ}, 8^{\circ}, 6^{\circ}, T 6^{\circ}, 7^{\circ}, 15^{\circ}, 16^{\circ}, F_{NNW} 8^{\circ}, 9^{\circ}, 15^{\circ}, 16^{\circ}, \Delta^{+2-24}$
10	8	00	06	00	02.0	10.4	01.6	.	.	$\Delta^{+0-6^{\circ}}$
11	8	01	04	00	01.7	12.2	.	.	.	Δ^{+0-8}
12	8	04	09	10	07.7	07.0	.	.	.	$\Delta^{+0-7^{\circ}}, \Delta^{+18^{\circ}, 19^{\circ}, 21^{\circ}, 24}$
13	7	10	10	10	10.0	00.9	00.3	.	.	$\Delta^{+1-3^{\circ}}, 3^{\circ}, 15^{\circ}, 24^{\circ}, \Delta^{+4-7^{\circ}}$
14	8	10	08	03	07.0	01.0	11.8	.	.	$\Delta^{+0-10^{\circ}}, 6^{\circ}, 10^{\circ}, \Delta^{+4-12^{\circ}, 20^{\circ}}$
15	7	10	06	10	05.7	00.6	01.8	.	.	$\Delta^{+0-4^{\circ}}, 12^{\circ}, 20^{\circ}, 20^{\circ}$
16	7	09	09	09	09.0	05.6	02.9	.	.	$T 12^{\circ}, 14^{\circ}, 20^{\circ}, 21^{\circ}, \Delta^{+20^{\circ}, 21^{\circ}}$
17	7	01	09	06	05.3	09.5	00.3	.	.	$T 13^{\circ}, 14^{\circ}, \Delta^{+10^{\circ}, 11^{\circ}}$
18	7	10	08	09	09.0	04.9	03.6	.	.	$\Delta^{+1-3^{\circ}}, 4^{\circ}, 6^{\circ}, T 4^{\circ}, 6^{\circ}, 10^{\circ}, 19^{\circ}, \Delta^{+4-14^{\circ}, 10^{\circ}, 20^{\circ}, 20^{\circ}, 20^{\circ}}, \Delta^{+10-12^{\circ}}$
19	7	02	03	01	02.0	10.7	00.2	.	.	$\Delta^{+0-1-3^{\circ}}, 0^{\circ}, 9^{\circ}, T 16^{\circ}, 17^{\circ}, 18^{\circ}, 17^{\circ}, \Delta^{+4-14^{\circ}, 18^{\circ}}, \Delta^{+4-14^{\circ}, 18^{\circ}}$
20	7	00	03	00	01.0	11.5	00.5	.	.	$\Delta^{+0-1-3^{\circ}}, 21-24, \Delta^{+22-24}$
21	8	09	04	05	06.0	06.5	.	.	.	$\Delta^{+0-8^{\circ}}, T 15^{\circ}, 16^{\circ}, 18^{\circ}, 19^{\circ}, F_{NNW} 18^{\circ}, 19^{\circ}, \Delta^{+18^{\circ}, 19^{\circ}}$
22	7	00	04	09	04.3	09.6	00.0	.	.	$\Delta^{+0-7^{\circ}}, \Delta^{+14^{\circ}, 11^{\circ}}$
23	7	04	03	02	03.0	12.0	.	.	.	$\Delta^{+0-10^{\circ}}, \Delta^{+13^{\circ}, 14^{\circ}}$
24	7	10	06	08	08.0	05.2	00.7	.	.	$\Delta^{+0-1-3^{\circ}}, \Delta^{+4-17^{\circ}, 20^{\circ}}, \Delta^{+6-17^{\circ}, 17^{\circ}}, \Delta^{+8-17^{\circ}, 17^{\circ}}, F_{-F_{NNW}}-WW 14^{\circ}, 16^{\circ}$
25	7	06	04	08	06.0	04.8	04.0	.	.	$= 3^{\circ}, 11^{\circ}, F_{SE} 14^{\circ}, 15^{\circ}, T 25^{\circ}, 17^{\circ}, \Delta^{+0-16^{\circ}}, \Delta^{+20^{\circ}}, \Delta^{+20^{\circ}}, \Delta^{+20^{\circ}}, [T K 17^{\circ}, \Delta^{+16^{\circ}, 16^{\circ}, 16^{\circ}, 16^{\circ}}]$
26	7	00	04	04	02.7	08.8	01.0	.	.	$= 3^{\circ}, 9^{\circ}, T 12^{\circ}, 15^{\circ}, F_{W} 14^{\circ}, 16^{\circ}, T 8, 15^{\circ}, 18^{\circ}, \Delta^{+0-15^{\circ}, 16^{\circ}, \Delta^{+1-15^{\circ}, 15^{\circ}, 15^{\circ}, 15^{\circ}, 0-16^{\circ}, 16^{\circ}, 16^{\circ}, 16^{\circ}}}$
27	7	04	04	03	03.7	C7.5	26.2	.	.	$= 4^{\circ}, 5^{\circ}, 5^{\circ}, \Delta^{+0-17^{\circ}, 10^{\circ}}, \Delta^{+14-17^{\circ}, 17^{\circ}}, T 24^{\circ}, 18^{\circ}, T 8, 16^{\circ}, 17^{\circ}, \Delta^{+4-17^{\circ}, 17^{\circ}, 24^{\circ}}$
28	7	08	05	10	07.7	08.7	10.2	.	.	$= 5^{\circ}, 6^{\circ}, 6^{\circ}, \Delta^{+17^{\circ}, 20^{\circ}}$
29	8	09	04	00	04.3	09.1	00.2	.	.	$\Delta^{+0-2-3^{\circ}}, 0^{\circ}, 20-24$
30	8	00	06	08	04.7	08.9	.	.	.	$\Delta^{+0-9^{\circ}}, \Delta^{+13-19^{\circ}}$
31	7	00	02	00	00.7	12.4	.	.	.	$\Delta^{+0-3-9^{\circ}}$

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 $\varphi = 41^{\circ}57' \text{ N } \lambda = 21^{\circ}38' \text{ E}$ Gr. $\Delta G = + 1 \text{ h } 27 \text{ min.}$

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d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	732.0	730.0	731.8	21.4	28.2	20.6	22.7	29.6	15.3	13.3	12.3	06.7	05.5	65	23	30	39	-	0	WSW 4	NNE 4	
2	732.4	732.9	733.6	16.4	17.6	16.2	16.6	21.4	13.5	10.5	09.0	08.9	09.5	65	59	72	65	-	0	NNW 2	- 0	
3	735.6	735.9	736.0	16.6	23.6	19.4	19.8	24.4	12.9	11.9	09.9	08.6	10.1	70	39	60	56	2	2	N 3	NNE 2	
4	739.4	738.4	738.1	20.4	27.4	20.0	22.0	28.6	16.4	13.6	11.6	10.6	12.2	64	39	70	58	2	2	SSE 1		
5	737.6	735.0	736.4	17.0	28.6	17.8	20.3	29.2	12.6	10.3	14.5	11.1	15.3	100	38	100	79	SW 1	S 2	NNW 1		
6	736.8	735.5	738.1	17.6	25.8	17.4	19.6	26.8	14.0	12.0	13.6	11.9	11.7	89	48	79	72	-	0	W 2	SE 3	
7	740.4	740.2	741.4	17.4	26.1	19.8	20.8	27.3	15.6	15.1	13.8	12.3	12.6	92	49	73	71	-	0	NNW 3	E 1	
8	743.0	741.6	742.3	18.4	26.8	21.4	22.0	28.3	14.4	13.1	14.1	12.9	12.6	89	49	66	68	1	1	N 3	N 2	
9	743.5	742.4	742.7	18.2	29.0	21.6	22.7	29.0	13.5	11.9	12.8	10.1	10.7	82	34	55	57	-	0	N 4	- 0	
10	743.5	741.1	739.9	18.2	29.2	21.7	22.7	30.6	13.0	10.8	12.5	09.0	10.8	80	30	55	55	-	0	W 1	SSE 1	
11	741.3	739.9	740.5	20.9	30.2	23.3	24.4	31.0	16.9	14.5	13.2	12.1	14.5	71	38	67	59	1	1	SSW 2	SE 1	
12	741.0	738.6	739.2	20.4	30.4	23.2	24.3	31.0	17.0	15.0	14.6	14.6	12.9	81	45	60	62	-	0	S 3	E 3	
13	741.3	740.7	743.0	20.0	26.9	19.8	21.6	28.4	16.0	13.5	13.0	13.5	13.1	74	51	76	67	1	1	NNW 3	ENE 2	
14	744.0	742.7	743.2	18.8	29.1	23.4	23.7	29.6	14.8	13.3	13.5	11.4	13.4	83	38	62	61	-	0	NNW 3	NE 2	
15	744.2	742.3	741.9	20.9	30.8	24.2	25.0	31.6	15.6	13.6	14.0	11.8	13.3	76	35	59	57	-	0	NN 2	NNE 2	
16	742.3	739.1	738.1	20.6	32.2	24.0	25.2	33.6	16.0	13.4	13.8	09.3	12.8	75	26	57	53	-	0	WSW 2	- 0	
17	739.0	737.4	739.0	20.6	32.2	26.2	26.3	33.5	15.6	13.6	13.0	15.4	14.9	72	43	58	58	-	0	N 2	NNE 4	
18	740.9	739.5	736.8	21.8	32.2	24.6	25.8	34.4	19.5	16.3	15.2	15.7	11.3	78	38	49	55	1	1	WW 2	ESE 1	
19	740.8	737.3	736.2	19.8	34.5	26.6	27.9	35.7	15.4	12.9	12.6	11.3	13.6	73	27	46	49	-	0	SE 3	E 1	
20	738.0	736.6	738.7	24.1	28.6	22.6	24.5	29.2	20.5	18.8	14.1	13.6	12.0	63	46	58	56	3	3	NNE 3	N 4	
21	739.4	737.5	737.6	21.2	27.4	23.3	23.8	28.2	18.4	16.0	12.4	12.0	10.5	66	44	49	53	-	0	NNW 4	NNE 3	
22	738.1	736.1	738.9	19.4	24.4	22.1	22.0	27.4	17.4	15.3	11.4	12.4	10.9	67	54	54	58	1	1	NE 3	NW 2	
23	740.2	739.0	739.4	18.0	28.4	23.9	23.6	29.0	13.4	11.0	12.1	12.1	11.7	78	42	52	57	1	1	NNW 3	NNE 3	
24	740.4	737.6	738.4	19.2	31.2	21.2	23.2	31.9	15.4	12.8	12.6	11.6	14.5	75	34	77	62	-	0	WSW 2	- 0	
25	738.8	737.2	737.2	18.7	30.9	24.4	24.6	32.7	15.6	13.3	13.4	10.8	14.4	83	32	63	59	-	0	NNE 2	SSE 1	
26	741.7	741.2	744.4	21.0	27.4	18.4	20.0	24.4	18.4	17.5	12.3	11.0	08.8	66	54	55	58	1	1	WW 2	NNW 3	
27	742.0	742.9	742.7	17.6	25.1	21.4	21.4	25.6	14.8	11.5	09.4	08.8	07.8	62	37	41	47	1	1	NNW 2	NNE 3	
28	743.2	741.8	742.4	17.6	25.6	20.8	21.2	26.4	16.3	14.4	10.3	09.1	07.8	68	37	42	49	2	2	NNE 4	NNE 4	
29	744.2	741.8	741.8	15.5	26.6	21.0	21.0	27.6	11.4	08.6	09.2	09.9	11.1	69	38	60	56	-	0	ENE 3	NNE 3	
30	742.0	739.1	739.6	17.6	28.2	22.2	22.6	29.4	13.0	10.8	12.3	11.9	11.7	81	41	58	60	-	0	NN 2	N 2	
31	740.5	738.7	740.5	21.0	28.1	23.2	23.9	29.0	17.0	14.8	12.3	09.6	10.3	66	34	48	49	2	2	N 4	NNE 4	
MES.	VRED.	740.3	738.8	739.5	19.2	28.0	21.9	22.7	29.2	15.5	13.3	12.5	11.2	11.7	75	40	60	58	0.8	2.9	2.0	

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1	741.5	740.3	742.1	20.8	26.0	20.2	21.8	26.7	16.0	14.1	11.8	10.2	10.2	64	40	57	54	-	0	NNW 4	NNE 2
2	743.1	741.6	743.4	20.4	28.8	22.6	23.6	29.0	15.2	13.0	11.4	10.4	10.3	64	35	50	50	2	2	NNE 4	N 4
3	743.9	743.0	743.8	19.6	24.4	21.8	21.9	26.0	16.3	14.4	11.0	10.8	11.0	64	47	56	56	2	2	NN 4	NNW 4
4	743.5	741.1	741.6	19.8	26.4	21.6	22.4	27.2	16.8	15.4	11.7	10.1	11.1	68	39	57	55	2	2	NNE 3	
5	741.7	740.9	741.8	17.2	18.4	16.6	17.2	21.7	15.8	12.8	11.7	12.3	10.7	79	77	75	77	1	1	ENE 1	
6	743.0	741.7	742.7	14.8	23.4	18.4	18.8	25.1	11.4	09.8	11.1	10.4	11.2	68	48	71	69	-	0	WW 4	W 2
7	743.6	741.1	742.0	17.4	26.2	16.9	19.4	27.0	12.6	11.0	12.3	11.1	12.1	82	43	84	70	1	1	ESE 1	N 3
8	741.1	739.6	739.7	18.2	25.0	20.4	21.0	25.4	14.3	13.0	12.3	11.1	11.7	78	47	65	63	1	1	NNE 1	NNE 4
9	739.5	740.5	741.4	18.4	20.9	19.7	20.7	23.0	17.1	15.8	13.8	13.4	13.2	87	73	77	79	1	1	W 3	NNE 1
10	741.7	741.4	742.0	17.4	28.4	19.4	21.2	28.6	15.4	13.4	12.9	11.5	12.8	87	40	76	68	-	0	NN 3	S 1
11	743.4	741.7	741.4	17.2	29.8	22.0	22.8	31.0	13.4	11.6	13.0	11.7	12.3	89	37	62	63	-	0	W 2	SE 2
12	741.4	736.3	736.9	17.0	31.0	23.0	23.5	32.4	14.0	11.8	11.9	11.7	11.8	82	35	56	58	1	1	SSW 1	WSW 2
13	737.8	735.2	736.1	18.4	30.0	23.0	23.6	30.6	14.3	12.2	11.9	10.7	10.7	75	34	51	53	-	0	NN 2	N 2
14	739.9	741.1	743.0	20.2	25.0	19.6	21.1	25.5	17.4	15.1	11.8	11.1	09.1	67	47	53	56	2	2	NNE 3	
15	744.7	742.3	741.8	13.2	27.2	20.0	20.1	28.9	1G.3	07.6	09.4	08.6	09.0	83	32	51	55	-	0	ENE 1	- 0
16	742.5	740.2	739.8	15.8	30.6	24.4	23.8	32.0	11.0	09.6	11.1	11.3	13.5	82	34	59	58	-	0	W 1	SSE 2
17	742.2	739.1	739.4	18.6	31.6	23.2	24.2	32.6	15.6	14.1											

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 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_x = 1.3 \text{ m}$

D	Vrijeme 0-9 14	Oblačnost N (0-10)					Intenziteta broj soji	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7 01	01	04	05	03.3	12.5	.	.	$\Delta^{0-1} 0-7^{\text{so}} F_{\text{WW}} 13^{\text{so}} 19^{\text{so}}$	
2	8 08	08	07	04	06.3	06.7	.	.	$\bullet^{0-1} 0-12^{\text{so}} T 12^{\text{so}} 13^{\text{so}} \Delta^{0-1} 20^{\text{so}} 24$	
3	8 04	04	06	04	04.7	09.3	CO.2	.	$\Delta^{0-1} 0-6, F_N 16^{\text{so}} 18^{\text{so}}$	
4	8 07	07	04	00	03.7	09.3	.	.	$\Delta^{0-1} 0-7^{\text{so}} T 12^{\text{so}} 20^{\text{so}} \Delta^{0-1} 13^{\text{so}} 15^{\text{so}}, 18^{\text{so}} 19^{\text{so}}$	
5	7 07	09	R	10	08.7	06.6	.	.	$\Delta^{0-1} 0-7^{\text{so}} T 12^{\text{so}} 20^{\text{so}} \Delta^{0-1} 13^{\text{so}} 15^{\text{so}}, 18^{\text{so}} 19^{\text{so}}$	
6	7 09	09	07	R	10	08.7	05.9	02.2	$\Delta^{0-1} 0-10^{\text{so}} T 12^{\text{so}} 15^{\text{so}} 18^{\text{so}} 24$; $F_{\text{EE-W}} 15^{\text{so}} 16, 19^{\text{so}} 20^{\text{so}} \Delta^{0-1} 16^{\text{so}} 17, 20-24, R 20^{\text{so}} 20$	
7	7 06	06	04	02	04.0	05.7	05.8	.	$\bullet^{0-1} 0-0^{\text{so}} T 0^{\text{so}} 1^{\text{so}} 8^{\text{so}}$	
8	7 02	05	01	01	02.7	11.3	.	.	$\Delta^{0-1} 0-7^{\text{so}} = 4^{\text{so}} 9^{\text{so}}$	
9	7 00	00	03	01	01.3	12.2	.	.	$\Delta^{0-1} 0-7^{\text{so}} = 5^{\text{so}} 8^{\text{so}}$	
10	8 00	00	01	01	00.7	13.0	.	.	$\Delta^{0-1} 0^{\text{so}} 7^{\text{so}}$	
11	7 09	09	03	04	05.3	10.2	.	.	$\Delta^{0-1} 0-4^{\text{so}} T 3 4^{\text{so}} 5^{\text{so}} 18^{\text{so}} 19^{\text{so}}$	
12	7 00	00	04	R	02	02.0	10.3	.	$\Delta^{0-1} 0-7^{\text{so}} T 13^{\text{so}} 15^{\text{so}} 20^{\text{so}} 24, F_{\text{NN-E}} 22^{\text{so}} 23^{\text{so}}$	
13	7 09	09	10	R	10	09.7	05.1	.	$\Delta^{0-1} 0-2^{\text{so}} T 13^{\text{so}} 19^{\text{so}} \Delta^{0-1} 14^{\text{so}} 15^{\text{so}}, F_{\text{NW}} 14^{\text{so}} 16^{\text{so}}$	
14	7 05	05	03	01	03.0	10.8	00.0	.	$\Delta^{0-1} 0-4^{\text{so}} = 5^{\text{so}} 8^{\text{so}}$	
15	7 00	00	01	00	00.3	12.9	.	.	$F_{\text{SW}} 12^{\text{so}} = 12^{\text{so}}$	
16	7 00	00	01	00	00.3	13.2	.	.	$\Delta^{0-1} 0-7^{\text{so}}$	
17	7 00	00	03	01	01.3	11.8	.	.	$\Delta^{0-1} 0-7, F_{\text{NN-E}} 16^{\text{so}} 24$	
18	7 00	00	01	00	00.3	13.3	.	.	.	
19	8 00	00	00	00	00.0	12.4	.	.	$\Delta^{0-1} 8^{\text{so}}; F_{\text{NN-E}} 10^{\text{so}} 21^{\text{so}}, T 16^{\text{so}} 17^{\text{so}}, 0^{\text{so}} 17-17^{\text{so}}$	
20	7 00	00	02	04	02.0	08.1	.	.	$\Delta^{0-1} 0-7^{\text{so}}; F_{\text{NN-E}} 10^{\text{so}} 21^{\text{so}}, T 16^{\text{so}} 17^{\text{so}}, 0^{\text{so}} 17-17^{\text{so}}$	
21	7 03	05	04	04	04.0	09.3	00.0	.	.	
22	7 09	06	00	05	05.0	03.0	00.0	.	$\bullet^{0-1} 6^{\text{so}} 7, F_{\text{NN-E}} 9^{\text{so}} 12^{\text{so}}$	
23	7 01	04	01	02	02.0	10.6	.	.	$\Delta^{0-1} 0-7^{\text{so}} T 15^{\text{so}} 16, 22^{\text{so}} 23^{\text{so}}, 0^{\text{so}} 16-17^{\text{so}}, 20^{\text{so}} 21^{\text{so}}, R 16-17^{\text{so}}$	
24	7 00	02	10	R	04	04.0	08.9	.	$\Delta^{0-1} 0-7^{\text{so}} = 5^{\text{so}} 10^{\text{so}}$	
25	7 00	01	01	01	00.7	12.6	00.1	.	$F_{\text{NN-E}} 10^{\text{so}} = 10^{\text{so}}$	
26	7 07	08	10	08	08.3	03.6	.	.	$F_{\text{NN-E}} 10^{\text{so}} = 20^{\text{so}}$	
27	7 09	09	04	06	06.3	09.4	.	.	$F_{\text{NN-E}} 8^{\text{so}} = 9^{\text{so}}$	
28	7 06	03	00	03	03.0	08.9	.	.	$F_{\text{NN-E}} 16^{\text{so}} = 18^{\text{so}}$	
29	7 00	01	01	00	00.3	11.7	.	.	$F_{\text{NN-E}} 12^{\text{so}} = 13^{\text{so}}$	
30	7 05	03	00	02	02.7	10.6	.	.	$\Delta^{0-1} 5^{\text{so}} 10^{\text{so}} T 15^{\text{so}} 16^{\text{so}}, F_N 15^{\text{so}} 15^{\text{so}}$	
31	7 03	05	06	04	04.7	09.2	.	.	$F_N 12^{\text{so}} = 13^{\text{so}}$	
MES. VRED.		03.5	03.9	03.2	03.5	298.9	08.3			

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1	7 05	05	01	01	03.7	09.0	.	.	$\Delta^{0-1} 0-7^{\text{so}}$	
2	7 03	05	02	03.3	07.7	.	.	.	$\Delta^{0-1} 0-10^{\text{so}} T 12^{\text{so}} 15^{\text{so}} 18^{\text{so}} 20^{\text{so}}$	
3	7 07	08	06	07.0	07.1	.	.	.	$\Delta^{0-1} 0-10^{\text{so}} T 14^{\text{so}} 14^{\text{so}}$	
4	7 07	04	04	05.0	06.8	.	.	.	$F_N 8^{\text{so}} 14^{\text{so}} 20^{\text{so}}$	
5	7 10	09	00	06.3	04.8	00.0	.	.	$\bullet^{0-1} 5^{\text{so}} 9^{\text{so}} 13^{\text{so}}$	
6	7 02	09	R	01	04.0	07.0	05.0	.	$\Delta^{0-1} 0-8^{\text{so}} T 12^{\text{so}} 15^{\text{so}} 18^{\text{so}} 24$	
7	7 08	06	09	07.7	05.4	.	.	.	$\Delta^{0-1} 0-7 T 14^{\text{so}} 18^{\text{so}}, R 14^{\text{so}} = 15^{\text{so}}, 0^{\text{so}} 14^{\text{so}} = 15^{\text{so}}$	
8	7 08	07	06	07.0	04.9	04.8	.	.	$F_N 8^{\text{so}} = 17^{\text{so}}$	
9	7 10	10	10	10.0	00.9	00.0	.	.	$\bullet^{0-1} 5^{\text{so}} 14^{\text{so}}$	
10	7 09	06	R	00	05.0	05.8	00.4	.	$T 13^{\text{so}} 15, 0^{\text{so}} 14^{\text{so}} 15^{\text{so}}$	
11	7 00	02	00	00	00.7	11.4	00.4	.	$\Delta^{0-1} 0-7^{\text{so}} = 5^{\text{so}} 11^{\text{so}}$	
12	7 00	02	00	00	00.7	11.4	.	.	$\Delta^{0-1} 0-7, 13^{\text{so}} 15^{\text{so}}, T 14^{\text{so}} 15^{\text{so}}, F_{\text{NN-E}} 22^{\text{so}} 23^{\text{so}}$	
13	7 02	06	03	03	03.7	09.6	.	.	$\Delta^{0-1} 0-9^{\text{so}} 24^{\text{so}}$	
14	7 05	05	00	00	03.3	06.6	05.6	.	$\Delta^{0-1} 0-9^{\text{so}} = 24^{\text{so}}$	
15	7 00	00	00	00	00.0	12.0	.	.	$\Delta^{0-1} 0-9$	
16	7 00	01	06	R	02.3	11.8	.	.	$\Delta^{0-1} 0-7 T 19^{\text{so}} 21^{\text{so}}, 0^{\text{so}} 20^{\text{so}} 20^{\text{so}}$	
17	7 04	02	05	R	03.7	10.8	04.7	.	$T 18^{\text{so}} = 22^{\text{so}}, 0^{\text{so}} 21^{\text{so}} 21^{\text{so}}, R 21^{\text{so}} = 21^{\text{so}}$	
18	7 03	02	03	02	02.7	11.6	04.4	.	$\Delta^{0-1} 0-7 T 15^{\text{so}} 21^{\text{so}}, 0^{\text{so}} 16^{\text{so}} 16^{\text{so}}, 19^{\text{so}} 20^{\text{so}}, F_N 17^{\text{so}} 19^{\text{so}}, R 19^{\text{so}} = 20$	
19	7 01	06	05	04	04.0	09.8	.	.	$\Delta^{0-1} 0-7^{\text{so}} T 15^{\text{so}} 21^{\text{so}}, 0^{\text{so}} 16^{\text{so}} 16^{\text{so}}, 19^{\text{so}} 20^{\text{so}}, F_N 17^{\text{so}} 19^{\text{so}}, R 19^{\text{so}} = 20$	
20	7 08	05	02	02	05.0	03.5	04.2	.	$\Delta^{0-1} 0-7^{\text{so}} = 10^{\text{so}} 9^{\text{so}}, 0^{\text{so}} 8^{\text{so}} 14^{\text{so}}$	
21	7 09	08	04	07	01.4	.	.	.	$\Delta^{0-1} 0-7$	
22	7 04	02	C1	C2.3	10.5	.	.	.	$\Delta^{0-1} 0-7^{\text{so}}$	
23	8 02	01	04	02.1	11.8	.	.	.	$\Delta^{0-1} 0-7^{\text{so}}$	
24	8 08	06	C6.0	07.7	07.6	.	.	.	$\Delta^{0-1} 0-7^{\text{so}}$	
25	7 04	04	C2	03.3	05.5	.	.	.	$T 0-1^{\text{so}} 7^{\text{so}} 9^{\text{so}}, 0^{\text{so}} 8^{\text{so}} 14^{\text{so}}$	
26	7 09	06	06	07.0	05.2	04.1	.	.	$\Delta^{0-1} 0-7^{\text{so}}$	
27	7 09	01	03	06.0	07.4	.	.	.	$\Delta^{0-1} 0-7^{\text{so}} F_N 14^{\text{so}} 21^{\text{so}}$	
28	7 09	04	02	C5.0	09.4	.	.	.	$\Delta^{0-1} 0-7^{\text{so}} 24^{\text{so}}$	
29	7 06	04	C3	C4.3	09.3	.	.	.	$T 17^{\text{so}} 20^{\text{so}}, 0^{\text{so}} 18^{\text{so}} 19^{\text{so}}, 0^{\text{so}} 20^{\text{so}} 22^{\text{so}}$	
30	7 00	03	C1	C1.7	C5.7	02.5	.	.	$\Delta^{0-1} 0-7^{\text{so}} T 19^{\text{so}} 21^{\text{so}}, 0^{\text{so}} 19^{\text{so}} 21^{\text{so}}$	
31	8 01	03	01	C1.7	11.7	.	.	.	$\Delta^{0-1} 0-6^{\text{so}} F_{\text{NN-E}} 15^{\text{so}} 18^{\text{so}}$	
MES. VRED.		04.9	04.6	03.4	04.3	251.1	22.1			

$\varphi = 41^{\circ}57'$ N $\lambda = 21^{\circ}38'$ E Gr. $\Delta G = + 1h\ 27\ min.$

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D č	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodené pare • mm			Relativna vlažnost v %			Pravac i jačina vetro D, I (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	742.3	741.0	741.9	18.2	29.2	23.0	23.4	29.8	14.8	-	11.7	10.5	11.8	75	34	56	55	-	0	NNW 3	N 4
2	743.1	741.0	740.9	17.2	30.4	24.8	24.3	31.4	14.6	-	13.0	11.1	13.0	89	34	55	59	-	0	WSW 2	ESE 2
3	741.2	738.3	739.3	18.8	31.6	23.0	24.1	32.6	16.8	-	12.5	10.8	10.1	77	31	48	52	-	0	S 3	E 4
4	738.7	738.0	739.1	16.1	22.0	18.6	18.8	26.6	13.8	-	11.2	13.2	12.9	82	66	80	76	-	0	W 5	S 1
5	740.4	739.1	739.3	15.3	27.6	21.2	21.3	29.0	13.7	-	11.6	10.7	12.0	89	39	64	64	-	0	-	0
6	741.3	740.3	741.4	15.3	29.9	22.6	22.6	30.7	13.3	-	10.8	10.7	11.7	83	34	57	58	SH 1	WNW 2	NNE 4	
7	743.2	740.9	741.5	15.8	27.6	19.2	20.4	28.2	14.0	-	11.1	12.2	13.2	82	44	79	68	ENE 1	NW 2	-	
8	742.4	741.9	745.3	14.8	26.6	19.6	20.2	26.6	12.2	-	11.1	11.2	12.7	88	43	74	68	-	0	NNE 5	NNW 2
9	745.3	743.6	743.5	16.4	24.6	19.4	20.4	26.4	15.9	-	11.6	11.0	09.8	73	47	58	59	NNE 2	N 3	N 4	
10	744.0	742.7	743.4	16.4	24.8	17.8	19.2	25.5	15.0	-	08.8	08.4	07.6	63	36	50	50	NNE 2	NNE 3	N 2	
11	744.1	741.7	741.9	10.3	26.0	20.8	19.5	27.0	07.5	-	06.9	07.8	11.5	73	31	62	55	ENE 1	S 2	ESE 2	
12	742.8	740.4	740.3	14.0	26.8	19.8	20.1	27.6	11.8	-	10.0	12.0	12.0	83	45	69	66	-	0	SSE 3	SE 1
13	740.3	739.9	742.0	16.0	24.6	18.8	19.6	25.5	16.0	-	12.3	13.1	12.2	90	56	75	74	W 2	ENE 1	SE 1	
14	744.0	742.0	741.8	14.0	26.9	18.8	19.6	28.2	12.0	-	11.2	12.2	12.8	94	46	79	73	ENE 1	NNE 1	-	
15	743.7	742.7	744.9	15.4	28.2	21.8	21.8	30.3	12.9	-	11.8	12.2	13.0	90	42	66	66	-	0	SE 2	ESE 1
16	748.7	747.7	748.3	16.6	21.0	22.4	23.1	32.8	14.0	-	13.1	13.0	11.6	92	39	57	63	ESE 1	WNW 2	E 1	
17	748.6	746.7	747.6	16.8	21.8	23.0	23.6	32.2	15.2	-	12.2	13.3	14.5	95	38	69	64	-	0	N 4	NNW 2
18	748.7	747.2	746.6	21.0	27.7	20.0	22.2	28.6	20.0	-	10.1	07.2	08.6	54	26	49	43	NNE 2	NE 3	NNE 3	
19	748.7	746.0	746.4	12.2	27.6	20.1	20.0	28.6	09.8	-	08.3	09.1	10.0	78	33	57	56	-	0	N 3	NE 1
20	746.5	744.5	745.2	14.0	28.0	19.6	19.8	28.5	10.0	-	08.4	09.0	09.2	80	32	54	55	-	0	NNW 2	NNW 2
21	745.8	744.3	745.5	13.0	28.2	23.2	21.9	29.2	11.4	-	09.8	11.1	11.3	87	39	53	60	-	0	NW 3	NNW 3
22	747.6	746.7	748.0	15.0	27.2	22.8	22.0	28.0	13.5	-	10.7	10.0	11.6	84	37	56	59	SSE 1	N 3	NNW 2	
23	750.1	747.5	748.2	15.0	28.2	18.0	19.8	28.9	13.2	-	11.0	10.2	11.8	86	36	76	66	-	0	WSW 2	-
24	748.2	745.5	746.1	12.4	27.4	19.0	19.4	28.5	10.8	-	09.6	09.6	09.0	89	35	54	59	-	0	ENE 1	E 2
25	745.6	743.1	743.5	11.4	29.0	16.0	18.1	29.4	09.7	-	09.0	09.1	07.8	89	30	57	59	ESE 1	N 1	ESE 1	
26	743.8	741.3	742.0	10.4	27.8	17.0	18.0	28.2	08.4	-	09.2	09.1	08.0	98	33	55	62	-	0	NNW 2	-
27	745.5	745.4	746.9	09.2	27.5	18.2	18.3	28.6	08.8	-	07.9	10.6	10.4	90	38	66	65	-	0	NNE 1	S 1
28	749.2	747.7	748.0	12.4	28.9	19.6	20.1	29.8	11.1	-	09.8	10.6	10.5	91	36	61	63	-	0	NNE 2	-
29	748.7	746.2	746.6	14.2	30.2	19.2	20.7	30.8	12.0	-	09.7	10.3	10.4	80	32	62	58	ESE 1	N 1	S 1	
30	746.9	744.3	744.7	14.0	29.4	22.4	22.0	29.6	11.9	-	09.8	11.3	11.0	81	37	54	57	-	0	ENE 2	-

MES.
VRED. 745.0 743.2 744.1 14.7 27.9 20.3 20.8 29.0 12.8 - 10.5 10.7 11.1 83 38 62 61 0.5 2.4 1.6

1	746.9	745.5	746.1	13.6	26.6	20.8	21.0	29.3	12.2	10.2	10.4	09.0	08.3	89	31	45	55	-	0	SSE 2	- 0
2	747.1	744.5	745.3	11.4	25.4	20.6	19.5	27.3	09.7	06.5	07.8	10.2	11.9	78	42	65	62	-	0	WSW 2	SE 2
3	746.4	745.4	745.0	15.3	23.9	16.0	17.8	24.9	13.0	11.5	10.8	11.1	10.0	83	50	73	69	-	0	NNW 2	- 0
4	745.5	744.2	744.3	12.8	24.6	18.6	18.6	25.8	11.0	08.7	10.0	10.2	08.7	90	44	54	63	-	0	N 2	N 3
5	745.9	744.7	746.4	13.0	15.6	12.0	13.2	18.6	11.0	12.0	10.0	08.5	07.5	89	64	72	75	NNW 2	NNW 3	NNW 3	
6	747.4	747.2	748.1	12.0	18.4	12.4	13.8	19.4	11.0	09.6	06.3	07.1	06.7	59	45	62	55	WNW 2	WNW 4	N 3	
7	748.2	745.2	744.6	04.6	19.4	09.8	10.9	20.3	03.4	01.2	05.4	06.3	07.4	93	38	81	71	-	0	NNW 2	S 1
8	745.3	745.3	745.2	08.0	13.6	07.0	08.9	15.9	05.9	03.9	07.2	07.0	05.9	90	60	79	76	SSE 1	WSW 2	S 2	
9	745.7	742.7	741.1	00.6	17.6	11.6	10.4	18.6	-0.4	-0.3	04.5	04.3	06.2	95	29	61	62	-	0	NE 1	- 0
10	740.3	739.5	738.4	09.6	12.6	11.2	11.2	13.0	09.0	09.0	08.3	07.9	08.8	93	72	89	85	-	0	E 2	-
11	737.9	739.6	742.3	10.6	15.1	13.4	13.1	16.9	10.2	09.9	09.1	10.6	09.3	92	82	81	86	-	0	NNE 2	NE 3
12	742.7	744.9	747.2	11.2	14.8	12.4	12.7	15.3	10.9	10.3	09.1	10.6	10.6	91	84	98	91	NE 3	NNE 1	- 0	
13	747.2	745.2	743.6	13.2	18.2	15.7	15.7	18.8	12.2	12.0	10.9	11.7	11.1	96	75	83	85	-	0	SE 5	SSE 4
14	737.9	738.0	741.2	14.6	19.8	11.0	14.1	20.7	11.0	13.2	10.2	06.1	06.8	82	35	69	62	SE 5	W 1	WSW 1	
15	744.0	742.6	744.7	04.6	18.2	09.0	10.2	18.7	03.8	01.5	06.0	05.6	07.4	94	35	86	72	WSW 1	SSE 2	- 0	
16	746.0	743.8	742.4	04.6	17.4	14.8	12.9	20.0	03.7	01.6	06.2	09.0	09.1	97	61	72	77	-	0	NW 2	SE 1
17	737.6	736.7	737.7	13.3	15.4	09.2	11.0	17.2	09.2	11.5	09.9	11.8	08.1	86	90	93	90	SE 3	WNW 2	WSW 2	
18	736.7	735.6	735.3	06.6	12.3	11.0	10.2	13.7	06.6	05.0	07.1	09.9	09.2	97	92	93	94	NE 1	S 2	WSW 1	
19	737.4	737.6	737.9	06.4	16.6	11.6	11.6	16.7	05.8	04.0	0										

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 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$

Dan	Vrijeme 0-9 0-9	Oblačnost N (0-10)					Insektacija bez R	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8 010	010	01	01.0	11.0
2	8 010	030	04	02.7	11.3
3	7 010	050	10	05.3	07.5
4	7 020	09R	07	06.0	02.6
5	7 010	020	00	01.0	10.4
6	7 000	020	00	00.7	10.8
7	7 000	09	02	03.7	05.2
8	7 05	09	09	07.7	05.6	00.2
9	7 030	07	00	03.3	06.9	00.1
10	7 030	010	00	01.3	10.4
11	8 040	050	04	04.3	09.4
12	7 060	09	02	05.7	04.5
13	8 100R	030	04	05.7	05.8	05.1
14	8 000	010	00	00.3	09.5	03.8
15	7 09	010	00	03.3	08.7
16	7 000	000	00	00.0	C9.7
17	7 000	010	02	01.0	10.1
18	8 000	010	00	00.3	10.1
19	8 000	020	00	00.7	09.5
20	7 010	010	00	00.7	C9.4
21	7 000	030	05	02.7	08.8
22	7 000	05	09	04.7	C9.7
23	6 000	000	07	02.3	07.7
24	7 010	010	01	01.0	08.6	08.8
25	7 010	050	02	02.7	C8.3
26	8 000	030	00	01.0	C8.6
27	8 050	010	00	02.0	C9.1
28	7 000	030	02	01.7	09.7
29	7 010	000	00	00.3	C9.5
30	8 000	000	00	00.0	09.6
MES. VRED.	01.8	03.1	02.4	02.4	256.2	16.0				

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1	8 050	050	00	02.3	08.3	.	.	Δ^0-0-7	.	.
2	8 010	060	02	03.0	C7.2	.	.	Δ^0-0-11^{40}	.	.
3	7 10	030	00	04.2	C4.4	.	.	Δ^0-2-6^{25}	$= 4^0-13^{20}, 0-16^{25} 7, 23^{45} 24$.
4	7 060	05	03	04.7	06.2	00.4	.	$\Delta^0-2-8^{00} 0$.	.
5	7 100	00	00	03.3	00.0	02.2	.	$\Delta^0-2-8^{00} 0$.	.
6	7 050	060	00	03.7	C7.6	C1.6	.	$\Delta^0-0-8^{00} 0$.	.
7	7 000	020	00	00.7	C9.1	.	.	Δ^0-0-9	.	.
8	8 03	06	00	03.0	03.4	.	.	$\Delta^0-1-8^{00} 0$	Δ^0-8-11^{20}	.
9	8 050	060	10	07.0	06.2	.	.	$\Delta^0-0-8^{00} 0$	$\Delta^0-2-23^{00} 24$.
10	7 100	09	10	05.7	00.1	03.3	.	$\Delta^0-0-3^{00} 0$	$\Delta^0-5^{00} 8^{00} 0, 17^{00} 24$.
11	7 10	08	10	05.3	C1.2	16.2	.	$\Delta^0-0-5^{00} 24^{00} 24$	$= 5^{00} 12^{00}$.
12	6 10	10	09	09.7	00.0	11.4	.	$\Delta^0-0-5^{00} 10^{00} 11^{00} 16^{00} 17^{00} 3^{00} 4^{00}$	$= 12^{00} 17^{00} 20^{00} 24$.
13	8 10	09	10	05.7	C1.7	C0.5	.	$\Delta^0-0-9^{00} 0$	$\Delta^0-10^{00} 10^{00} 24, 0-16^{00} 24$.
14	8 080	020	C3	04.3	06.5	C3.1	.	$\Delta^0-0-3^{00} 5^{00} 10^{00} 0-17^{00} 17^{00} 6^{00}$.	.
15	8 010	07	00	02.7	C6.2	03.5	.	$\Delta^0-12-10, 20-24$.	.
16	7 08	05	09	07.3	05.5	.	.	$\Delta^0-0-8^{00} 0$	$= 9^{00} 14^{00} \Delta^0-23^{00} 24$.
17	6 070	100	03	04.7	00.6	02.4	.	$\Delta^0-0-12^{00} 0-2-6^{00} 0-9^{00} 17^{00} T 14^{00} 16^{00} 17^{00} 14^{00} 15^{00}$	$= 16^{00} 16^{00} 16^{00} 18^{00} 24^{00}$.
18	6 020	09R	10	07.0	00.3	14.6	.	$\Delta^0-3^{00} 5^{00} 7^{00} 9^{00} 0-15^{00} 14^{00} 0-15^{00} 14^{00} 17^{00} 18^{00}$.	.
19	7 10	09	10	05.7	C1.5	01.5	.	$\Delta^0-0-7^{00} 12^{00} 4^{00} 12^{00} = 3^{00} 14^{00} 17^{00} 17^{00} 22^{00}$.	.
20	6 07	06	08	07.0	02.6	04.7	.	$\Delta^0-0-5^{00} 24^{00} 23^{00} 24, F_n 22^{00} 23$.	.
21	7 020	020	03	02.3	C7.4	CC.2	.	$\Delta^0-0-0^{25} = 3^{00} 7^{00} 0, = 6^{00} 6^{00} 14^{00} 15^{00}$.	.
22	7 10	09	10	05.7	00.2	.	.	$\Delta^0-4^{00} 24$.	.
23	7 10	09	10	05.7	00.5	C6.7	.	$\Delta^0-0-6^{00} 14^{00} 19^{00} 23^{00} 24, F_n 22^{00} 23$.	.
24	7 09	10	10	05.7	00.0	00.8	.	$\Delta^0-0-6^{00} 14^{00} 12, F_n 4^{00} 4^{00} 22^{00}$.	.
25	7 05	06	01	04.0	00.9	00.0	.	$\Delta^0-12-9^{00} = 5^{00} 12$.	.
26	7 010	010	00	00.7	07.8	.	.	$\Delta^0-0-9^{00} = 5^{00} 9^{00}$.	.
27	8 060	010	00	02.3	C8.3	.	.	$\Delta^0-0-9^{00} = 7^{00} 40^{00}$.	.
28	7 000	000	00	00.0	08.3	.	.	$\Delta^0-0-5^{00} 24^{00} 24 = 2^{00} 7^{00} 0-15^{00} 7^{00}$.	.
29	8 000	000	00	00.0	09.2	.	.	$\Delta^0-0-5^{00} 20^{00} 24 = 0-15^{00} 14^{00} 0-15^{00} 8^{00}$.	.
30	6 000	000	00	00.0	C8.0	08.6	.	$\Delta^0-0-3^{00} 20^{00} 24 = 3^{00} 8^{00} 0-15^{00} 8^{00}$.	.
31	7 000	010	00	00.3	08.9	.	.	$\Delta^0-0-3^{00} 20^{00} 24 = 3^{00} 8^{00} 0-15^{00} 8^{00}$.	.
MES. VRED.	05.5	05.2	04.2	05.0	140.1	78.6				

$\varphi = 41^{\circ}57'$ N $\lambda = 21^{\circ}38'$ E Gr. $\Delta G = +1h\ 27\ min.$

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D	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21				
1	745.5	744.1	745.7	00.3	17.6	27.2	08.1	17.7	-06.2	-03.1	04.4	07.5	07.0	95	50	92	79	-	0	S	3	-	0	
2	748.2	747.2	749.2	06.2	17.0	07.4	09.5	17.6	03.8	01.3	06.7	09.0	07.5	94	62	97	84	2	S	2	SSW	1	-	0
3	750.4	749.5	750.3	08.8	16.0	06.8	09.6	16.3	03.6	03.2	07.6	09.0	07.1	90	66	96	84	-	0	SE	1	-	0	
4	750.2	749.9	750.8	08.4	15.0	06.2	09.0	15.9	05.8	03.3	07.8	08.3	06.5	95	65	92	84	-	0	-	0	S	2	
5	750.9	750.0	749.9	09.2	14.0	06.8	09.2	14.0	06.0	03.6	06.2	07.2	06.4	71	60	87	73	ENE	2	SE	3	-	0	
6	749.2	747.4	747.3	05.4	14.4	11.4	10.6	15.2	03.0	00.0	06.5	05.7	06.1	97	46	61	68	-	0	SSE	4	-	0	
7	746.7	746.0	746.4	09.8	12.0	10.2	10.6	12.3	09.1	08.1	06.1	05.6	05.7	67	54	61	61	SSE	1	S	3	SE	7	
8	746.6	746.4	745.8	08.8	10.8	05.8	05.8	10.8	08.4	06.9	06.2	05.2	05.5	73	54	61	63	SSE	1	SE	3	SE	2	
9	745.0	745.7	746.9	08.2	11.4	09.0	09.4	11.6	08.2	07.3	06.1	06.6	06.9	75	65	80	73	-	0	SSE	3	-	0	
10	746.8	745.1	745.0	06.3	14.6	10.6	10.5	15.2	06.2	03.2	06.5	06.7	07.0	90	54	73	72	SSE	1	SSW	2	-	0	
11	743.7	743.7	746.1	09.4	14.6	09.6	10.6	15.4	08.4	07.4	08.2	08.7	07.4	93	70	82	82	WSW	1	-	0	NNE	3	
12	748.8	748.8	750.3	07.0	10.6	08.8	08.8	10.6	06.1	04.2	06.7	06.5	06.6	89	68	78	78	-	0	NE	1	NNE	3	
13	752.1	752.0	752.2	07.8	10.5	08.8	09.0	10.8	07.8	07.3	06.7	06.5	06.8	85	68	80	78	-	0	SE	1	SE	1	
14	751.6	747.8	746.4	06.2	10.8	06.4	07.4	11.5	05.3	04.0	06.5	06.6	05.8	92	68	81	80	ESE	1	S	3	ESE	2	
15	744.6	743.7	743.4	06.0	08.2	06.4	06.8	08.6	06.0	03.6	05.7	05.5	05.7	81	68	80	76	NNNE	2	NE	2	-	0	
16	741.1	738.7	737.5	04.9	07.2	06.2	06.1	07.3	04.9	04.6	05.5	06.2	05.6	84	82	78	81	SE	3	-	0	SSE	1	
17	734.8	735.9	737.0	07.6	11.6	11.2	10.4	12.0	05.6	04.8	06.2	07.7	07.7	79	76	77	77	SSE	3	SSE	5	SSE	5	
18	736.8	735.9	736.8	13.4	18.6	16.6	16.3	18.6	11.0	05.6	08.9	09.2	10.4	77	57	74	69	SE	6	SE	1	SE	5	
19	737.1	738.2	737.1	15.2	14.2	12.0	13.4	15.4	11.9	14.0	10.1	10.2	10.0	78	90	95	88	SSW	3	S	2	ESE	1	
20	736.3	734.6	735.1	06.2	15.6	08.8	09.8	16.6	06.0	03.8	07.1	08.0	06.6	100	60	78	79	E	1	-	0	SSE	1	
21	735.1	737.0	739.9	05.8	C6.0	05.2	05.6	09.2	05.0	03.4	06.1	05.3	04.0	89	75	61	75	-	0	N	5	N	4	
22	736.5	736.2	736.4	00.6	-00.2	-01.4	-00.6	05.2	-01.8	-01.6	02.8	04.2	03.9	59	93	95	82	NNNE	4	NNNE	3	NNNE	1	
23	737.1	736.8	737.7	-01.6	01.6	00.6	00.3	02.4	-01.7	-01.0	03.9	04.0	04.0	95	77	83	85	-	0	NNW	2	N	4	
24	737.8	738.1	741.6	-00.8	01.8	-01.6	-00.6	02.5	-01.6	-01.3	04.1	03.5	03.1	96	67	76	80	NNW	2	N	4	WSW	2	
25	743.6	745.8	746.6	-01.4	02.0	-03.6	-01.6	02.2	-03.9	-03.9	02.9	03.8	02.4	70	71	69	70	-	0	SE	1	NNNE	4	
26	746.8	746.1	746.8	-C7.4	02.0	-05.6	-03.8	02.9	-07.4	-10.4	02.3	03.4	02.6	88	65	82	78	-	0	-	0	-	0	
27	748.5	747.5	748.2	-08.0	02.6	-02.6	-C2.6	03.3	-08.6	-11.0	02.3	03.3	03.4	92	59	90	80	S	1	NW	1	SSE	1	
28	747.1	744.6	743.5	-03.4	01.5	00.6	-00.2	01.8	-05.2	-06.2	03.2	04.0	04.6	89	78	96	88	-	0	NNW	1	-	0	
29	741.7	741.0	741.4	01.0	0	06.8	03.0	03.4	08.2	06.4	04.8	06.2	05.5	97	84	97	93	-	0	0	E	1		
30	743.1	743.2	744.6	03.0	04.4	03.6	C3.6	04.6	03.0	03.0	05.1	05.4	05.6	91	85	94	90	-	0	-	0	ESE	1	
MES.	VRED.	744.2	743.6	744.2	04.8	09.8	06.0	06.6	10.5	03.5	02.2	05.8	06.3	05.9	86	68	82	78	1.1	2.0	1.7			

1	745.8	745.9	746.8	03.2	C8.8	04.9	C5.4	C9.4	C3.2	03.2	05.4	06.2	05.8	94	73	90	86	-	0	-	0	NNW	1
2	744.9	743.1	743.2	04.4	10.2	06.2	06.8	11.0	04.2	04.0	05.7	07.2	05.8	91	77	81	83	-	0	SSE	3	SSE	3
3	744.3	743.9	746.3	-00.1	11.6	02.0	C3.9	12.0	-06.1	-02.0	04.5	06.6	04.9	98	64	93	85	-	0	NE	1	ESE	1
4	748.5	746.7	749.8	-02.2	C3.4	01.8	01.7	06.0	-02.7	-03.5	03.9	05.8	04.9	100	86	93	93	ESE	1	-	0	E	2
5	750.0	748.5	748.7	01.8	08.3	03.1	04.1	08.6	02.2	-01.5	05.0	05.7	04.4	97	69	77	81	ENE	2	NNW	2	NNNE	2
6	748.3	744.8	742.1	-02.6	08.1	00.2	01.5	08.4	-02.8	-05.9	03.6	05.2	04.2	96	64	89	83	S	1	-	0	-	0
7	741.8	742.3	745.9	-00.4	05.4	02.6	02.6	06.1	-03.0	-06.0	04.1	03.8	03.3	93	56	59	69	-	0	NNW	5	NNW	2
8	744.7	743.2	744.0	-04.7	05.2	-02.2	-01.0	05.6	-05.1	-08.1	03.0	03.3	03.4	93	50	86	76	-	0	N	1	SE	1
9	746.6	747.4	749.5	-00.7	09.2	00.8	C2.5	09.6	-03.7	-06.1	03.9	03.7	03.5	89	42	73	68	-	0	N	2	NNE	2
10	750.3	748.8	748.9	-05.0	05.8	-02.0	-01.3	06.2	-06.0	-09.6	02.9	03.9	03.3	91	57	89	79	-	0	WSW	1	S	1
11	748.8	748.2	750.1	-03.2	07.6	-01.0	00.6	08.1	-05.9	-08.3	C3.5	03.9	03.6	96	50	85	77	S	1	NNE	3	SSW	1
12	749.5	747.1	746.1	-05.6	03.2	02.8	00.8	03.0	-02.6	-08.9	02.9	04.5	04.9	95	78	87	87	-	0	S	1	SW	1
13	744.8	743.8	744.2	02.8	04.7	C3.1	03.4	05.0	02.2	01.3	04.9	05.5	05.5	87	85	95	89	SSE	2	NW	1	-	0
14	744.5	745.0	747.0	02.0	06.6	04.6	04.4	07.0	01.9	01.6	05.1	05.7	05.1	97	75	80	85	-	0	-	0	NNE	3
15	750.0	750.6	751.4	03.2	04.4	03.2	03.5	05.0	02.9	02.4	04.3	04.4	04.7	75	69	81	75	N	3	NNE	3	-	0
16	750.1	747.3	746.4	02.2	05.4	05.2	04.5	05.7	02.2	01.8	C4.9	05.0	05.7	92	75	86	84	NE	1	-	0	E	1
17</																							

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 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_x = 1.3 \text{ m}$

Dan	Veličina O. °	Oblačnost N (0-10)					Inseleacija broj satih	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	03	04	01	02	0.7	08.4	.	.	$\Delta^{\circ} 0-2^{\circ} 19^{\circ} 24^{\circ} = 0-14^{\circ} 2^{\circ} 7^{\circ}$
2	7	09	01	CC	C3.3	C5.5	.	.	.	$\Delta^{\circ} 20-8^{\circ} 18^{\circ} 24^{\circ} = 0-10-12^{\circ}$
3	6	10	03	00	04	0.3	02.5	.	.	$\Delta^{\circ} 0-11^{\circ} 19^{\circ} 24^{\circ} = 0-24$
4	6	09	08	00	05	0.7	00.6	.	.	$\Delta^{\circ} 0-10-20-24^{\circ} = 0-24$
5	6	10	04	00	04	0.7	C1.0	.	.	$\Delta^{\circ} 0-9-20^{\circ} 24^{\circ} = 0-14^{\circ}$
6	7	10	05	10	05	7	C3.?	.	.	$\Delta^{\circ} 0-8^{\circ} = 5^{\circ} 12^{\circ}$
7	7	10	10	10	10	0.0	CC.C	.	.	.
8	7	10	10	10	10	0.0	00.0	.	.	$0^{\circ} 0^{\circ} 1^{\circ}$
9	7	10	10	10	10	0.0	00.C	CC.C	.	$0^{\circ} 17^{\circ} 24$
10	7	08	08	09	08	3	03.7	.	.	.
11	7	10	04	09	C7.3	C4.0	01.6	.	.	$0^{\circ} 18^{\circ} 7^{\circ} = 0-17-10^{\circ}$
12	7	09	10	10	05.7	00.C	CC.C	.	.	$0^{\circ} 18^{\circ} 19^{\circ}$
13	7	10	10	10	10	0.0	CC.C	CC.C	.	.
14	7	08	06	06	06.7	02.9
15	7	10	10	10	10	0.0	00.C	00.C	.	$0^{\circ} 19^{\circ} 24$
16	7	10	10	05	09	7	00.C	00.0	.	$0^{\circ} 0-14^{\circ}$
17	8	10	09	05	08	0	00.C	CC.C	.	$F_{\text{SE}} 0-24, 0^{\circ} 19^{\circ} 20^{\circ} 24$
18	7	10	10	10	10	0.0	00.C	00.C	.	$F_{\text{SE}} 0-6-0^{\circ} 15^{\circ} 18^{\circ} 24$
19	6	10	10	10	10	0.0	10.C	00.C	.	$F_{\text{SE}} 0-4-0^{\circ} 9^{\circ} 10^{\circ} 24 = 5^{\circ} 6^{\circ}$
20	7	01	08	09	06	0	03.8	12.1	.	.
21	7	08	10	10	05	3	00.C	00.C	.	$0^{\circ} 10^{\circ} 16^{\circ} 12^{\circ} 24$
22	5	10	10*	10*	10*	0.0	00.C	01.2	.	$0^{\circ} 5^{\circ} 7^{\circ} * 0^{\circ} 17^{\circ} 24$
23	7	10*	05	10	05.7	00.4	10.C	12	.	$* 0^{\circ} 0-7^{\circ} F_{\text{WW}} 20^{\circ} 24^{\circ}$
24	8	10*	06	06	07	3	03.1	00.2	24	$F_{\text{WWNNW}} 2^{\circ} 5, 10^{\circ} 14^{\circ}, * 0^{\circ} 4^{\circ} 9^{\circ},$
25	8	10*	02	CC	04.C	00.C	00.0	02	.	$* 0^{\circ} 6^{\circ},$
26	7	00	01	00	00.3	07.3	.	.	.	$0^{\circ} 1^{\circ} 4^{\circ} 17^{\circ} 24$
27	7	00	00	03	C1.0	07.2	.	.	.	$0^{\circ} 0-10^{\circ} 17^{\circ} 24 = 0^{\circ} 6^{\circ} 12^{\circ} 17^{\circ} 24$
28	5	10	10	10	10	0.0	00.0	.	.	$0^{\circ} 0-10^{\circ} 0-24, 0^{\circ} 17^{\circ} 24$
29	6	10	03	10	07	7	C2.5	03.1	.	$= 0^{\circ} 17^{\circ} 24 = 17^{\circ} 21^{\circ} 10^{\circ} 20^{\circ}$
30	6	10	10	10	10	0.0	00.C	.	.	$= 0^{\circ} 0-10^{\circ} 13^{\circ} 24, 0^{\circ} 8^{\circ} 12^{\circ} = 10^{\circ} 13^{\circ} 20^{\circ}$
MES.	VRED.	08.5	C7.2	06.9	07.5	60.6	28.4			

SKOPJE - PETROVAC

1975 DECEMBAR

1	7	10	05	05	10	08.3	03.5	CC.2	.	$0^{\circ} 12^{\circ} 24 = 0-12^{\circ}, 17^{\circ} 24$
2	7	10	05	01	05.3	01.2	00.C	.	.	$= 0-12^{\circ}$
3	7	01	00	00	00.3	06.5	.	.	.	$\Delta^{\circ} 10-9^{\circ} 18-24 = 0^{\circ}-9^{\circ}$
4	4	10	10	00	00	03.3	00.6	.	.	$\Delta^{\circ} 0-9^{\circ} 18-24 = 6^{\circ} 6^{\circ} 13^{\circ} 19^{\circ} = 6^{\circ} 7^{\circ} 10^{\circ} 11^{\circ} = 7^{\circ} 13^{\circ}, 0^{\circ} 18^{\circ} 24$
5	5	10	06	C1	05.7	CC.C	.	.	.	$\Delta^{\circ} 0-8^{\circ} 18-20-24 = 7^{\circ} 7^{\circ} 20^{\circ}$
6	6	01	00	00	00.3	06.5	.	.	.	$0^{\circ} 1^{\circ} 9^{\circ} 24^{\circ} 24^{\circ} 24 = 0^{\circ} 24$
7	8	10	06	09	08.3	C1.3	00.2	.	.	$\Delta^{\circ} 0-5^{\circ} 18-24 = 0-9^{\circ} 15^{\circ} 14^{\circ}, F_{\text{WW}} 8^{\circ} 28^{\circ} 13^{\circ} 18$
8	7	00	04	01	01.7	08.2	00.7	.	.	$0^{\circ} 13-10^{\circ} 18-24 = 0^{\circ} 24$
9	7	09	00	00	03.0	C7.6	.	.	.	$0^{\circ} 9^{\circ} 24^{\circ} 24$
10	7	00	00	00	00.0	00.C	06.0	.	.	$0^{\circ} 0-10^{\circ} 18-24$
11	7	10	00	00	00	03.3	C4.4	.	.	$\Delta^{\circ} 0-10^{\circ} 24-24 = 5^{\circ} 12^{\circ} F_{\text{WW}} 12^{\circ} 17^{\circ}$
12	5	08	10	10	09	05.3	00.6	.	.	$\Delta^{\circ} 0-9^{\circ} 18-24 = 3^{\circ} 24^{\circ} 0^{\circ} 19^{\circ} 21^{\circ} 22^{\circ}$
13	7	16	09	10	05.7	CC.C	00.6	.	.	$= 0^{\circ} 7^{\circ} 17^{\circ} 24 = 0^{\circ} 24^{\circ} 20^{\circ} 6^{\circ} 9^{\circ}$
14	4	10	10	09	09.7	00.C	01.1	.	.	$= 0^{\circ} 0-18^{\circ}$
15	7	10	10	10	10.0	00.0
16	6	10	10	10	10.0	00.C	.	.	.	$= 0^{\circ} 6^{\circ} 17^{\circ} 23^{\circ} 24$
17	6	10	10	09	09.7	00.0	.	.	.	$= 0^{\circ} 17^{\circ} 24 = 24^{\circ} 22^{\circ}$
18	7	10	10	10	10.0	00.C	00.4	.	.	$F_{\text{WW}} 0-8^{\circ} = 10^{\circ} 17^{\circ} 0^{\circ} 12^{\circ} 13^{\circ} = 5^{\circ} 10^{\circ} 15^{\circ} 16^{\circ}$
19	6	10	10	10	10.0	00.C	01.8	.	.	$X^{\circ} 5^{\circ} 9^{\circ} 17^{\circ} 22^{\circ}$
20	7	10*	06	02	06.0	CC.8	00.0	.	.	.
21	7	10	C6	00	05.3	01.8	00.C	.	.	$= 0^{\circ} 13^{\circ} 22^{\circ} 24$
22	7	06	02	01	03.C	05.9	.	.	.	$\Delta^{\circ} 0-10^{\circ} 18-24 = 0^{\circ} 3^{\circ} 13^{\circ}$
23	7	C1	00	00	00.3	C6.5	.	.	.	$\Delta^{\circ} 0-10^{\circ} 20^{\circ} 24 = 3^{\circ} 10^{\circ}$
24	6	00	00	00	00.0	00.C	C5.2	.	.	$\Delta^{\circ} 0-10^{\circ} 20^{\circ} 24 = 3^{\circ} 10^{\circ}$
25	5	10	02	03	05.0	02.5	.	.	.	$\Delta^{\circ} 0-10^{\circ} 18^{\circ} F_{\text{WW}} 6^{\circ} 24^{\circ}$
26	7	C4	08	04	C5.3	C5.8	.	.	.	$\Delta^{\circ} 5^{\circ} 8^{\circ} F_{\text{WW}} 9^{\circ} 15^{\circ}$
27	7	C4	10	09	07.7	00.C	.	.	.	$\Delta^{\circ} 5^{\circ} 9$
28	7	10	10	C9	09.7	CC.C
29	6	C2	00	00	00.7	06.6	.	.	.	$\Delta^{\circ} 2^{\circ} 20^{\circ} 24 = 6^{\circ} 13^{\circ}$
30	2	10	10	10	10	10.C	00.C	.	.	$\Delta^{\circ} 0-6^{\circ} 20^{\circ} 24 = 6^{\circ} 26^{\circ} 15^{\circ} = 6^{\circ} 12^{\circ} 15^{\circ} 24$
31	1	10	10	10	10	10.C	00.C	.	.	$\Delta^{\circ} 0-6^{\circ} 14^{\circ} 24 = 6^{\circ} 24^{\circ} 24 = 6^{\circ} 24$
MES.	VRED.	07.3	05.4	04.8	C5.8	81.3	11.1			

**B) Mesečni i godišnji
pregled**

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																			
		Tm				Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW						
		7	14	21	Sred. (Dnes)						8.	15.	22.	29.	1.	8.	15.	22.	29.	1.	8.	15.	22.	29.	1.	8.	15.	22.	29.		
SR SLOVENIJA																															
$\varphi = 46^{\circ}20' N \lambda = 13^{\circ}33' E$ Gr. $\Delta G = + 54$ min.																															
I	-	00.0	06.0	01.4	02.2	06.5	-06.5	10.8	31 -06.7	11 09	01.1	.	.	08	01.6	.	.	12	01.5	64				
II	-	-01.0	06.5	01.6	02.7	05.0	-02.2	14.6	19 -07.8	18 02	06.9	08	02.9	24	05.3	.	.	17	02.4	03	01.0	03	00.5	.	.	.	26				
III	-	01.9	07.1	04.2	04.3	08.4	00.4	15.7	07 -06.7	26 05	00.7	03	01.2	04	C1.0	.	.	25	03.9	07	01.8	01	00.2	.	.	.	48				
IV	-	05.7	13.7	07.5	08.6	14.7	02.8	21.7	20 -01.6	03.02	20 04.1	08	02.4	02	00.5	01	00.3	18 03.3	07	02.1	06	02.3	.	.	.	28					
V	-	11.6	18.5	12.6	13.8	16.8	08.3	27.8	19 02.8	03	07	01.3	03	01.2	09	01.4	.	.	29	04.8	11	03.1	02	00.3	.	.	.	32			
VI	-	13.1	20.1	14.2	15.4	21.4	09.5	27.8	27 03.2	05	16	C2.7	09	03.0	02	00.3	.	.	30	04.4	05	01.3	01	00.2	.	.	.	27			
VII	-	16.0	24.5	17.3	18.8	25.4	12.4	26.9	19 06.4	26	10	01.5	04	01.4	03	00.5	.	.	26	03.1	20	05.0	04	00.7	.	.	.	26			
VIII	-	15.8	23.9	17.3	18.6	24.6	13.1	27.9	07 07.2	20	11	01.4	01	00.3	14	04.4	.	.	17	03.0	06	01.5	06	01.1	.	.	.	38			
IX	-	12.6	22.1	15.1	16.3	22.9	11.5	29.0	17 05.8	14	02	00.3	.	.	01	00.2	.	.	27	03.8	12	03.4	04	00.7	.	.	.	44			
X	-	05.5	15.5	07.6	09.1	16.2	04.5	24.6	03 00.3	26	16	02.6	03	00.8	05	01.2	.	.	21	02.5	14	02.8	07	01.4	.	.	.	27			
XI	-	01.8	07.2	03.3	03.9	07.9	00.6	15.5	03 -05.7	25	11	01.8	06	02.4	04	01.3	.	.	20	02.4	06	01.3	03	00.4	.	.	.	40			
XII	-	-01.8	04.2	-00.5	00.3	04.9	-02.8	08.7	29 -09.0	21.20	08	01.0	01	00.3	08	01.7	.	.	18	01.8	03	00.5	05	.	.	.	55				
GOD.	-	06.8	14.3	08.5	06.5	15.1	04.8	29.0	7. IX -09.7	25 XI	118	02.1	46	02.2	84	02.9	01	00.3	260	03.3	94	02.9	37	01.1	.	.	.	455			
VEDRIJAN																										BR. ST. 2					
$\varphi = 46^{\circ}01' N \lambda = 13^{\circ}33' E$ Gr. $\Delta G = + 54$ min.																										BR. ST. 2					
I	-	04.9	08.4	05.7	06.2	09.2	04.0	14.0	30 00.5	11	.	.	42	12.2	.	.	16	03.6	.	.	22	05.2	.	.	01	00.2	12				
II	-	03.9	C9.5	09.6	05.8	10.4	02.6	16.5	19.08 -01.0	17	.	.	40	26.3	.	.	10	02.9	.	.	12	02.6	.	.	01	00.3	01				
III	-	06.1	09.6	07.4	11.3	04.9	16.5	09	00.5	24	01	00.2	47	16.5	.	.	22	06.0	.	.	20	04.7	.	.	03	00.7	.				
IV	-	09.5	15.4	11.0	11.7	16.4	08.1	23.6	21 03.5	12	.	.	38	13.4	.	.	24	06.1	.	.	22	04.7	.	.	06	01.2	.				
V	-	14.7	21.0	15.5	16.9	22.1	13.0	25.6	20 05.8	09	.	.	50	18.2	.	.	11	03.1	.	.	31	08.7	.	.	01	00.3	.				
VI	-	16.1	22.0	17.2	18.2	23.4	14.2	26.5	27.23 08.8	05	.	.	53	17.2	.	.	13	02.9	.	.	20	05.1	01	00.3	03	00.8	.				
VII	-	18.8	26.3	20.9	21.8	27.1	16.9	30.2	18 11.0	01	.	.	54	19.4	.	.	11	02.4	.	.	28	07.3				
VIII	-	18.6	24.9	20.1	21.0	26.0	17.1	29.9	10 14.6	20	.	.	55	19.4	.	.	11	02.7	.	.	25	06.1	.	.	02	00.4	.				
IX	-	17.2	24.4	19.0	19.9	25.4	16.6	31.0	18 11.0	13	.	.	57	20.6	.	.	10	03.9	.	.	15	03.7				
X	-	10.9	17.5	12.4	13.3	18.6	09.9	26.5	03 05.5	12	.	.	68	27.7	.	.	03	01.2	.	.	20	04.9	.	.	02	00.6	.				
XI	-	06.4	09.4	07.1	07.5	10.8	05.5	18.0	03 -02.8	25	.	.	70	29.0	.	.	14	03.8	.	.	05	01.2	.	.	01	00.2	.				
XII	-	04.4	08.2	05.0	05.7	09.5	03.3	14.6	28 -01.2	21	01	00.4	62	22.3	.	.	16	03.9	.	.	13	03.1	.	.	01	00.2	.				
GOD.	-	10.9	16.4	12.2	13.0	17.9	09.7	31.0	MAX -02.8	25 XI	02	00.3	656	21.0	.	.	169	04.3	.	.	233	05.6	01	00.3	21	00.7	13				
RATEČE-PLANICA																										BR. ST. 3					
$\varphi = 46^{\circ}30' N \lambda = 13^{\circ}43' E$ Gr. $\Delta G = + 54$ min.																										BR. ST. 3					
I	650.4	-02.9	04.5	-01.4	-00.3	05.1	-03.7	06.8	06 -10.2	05	.	.	01	00.2	05	01.2	05	00.7	01	00.2	02	00.4	10	01.9	.	.	69				
II	692.1	-05.2	04.6	-02.4	-01.4	05.2	-06.2	13.2	28 -12.2	10	01	00.1	03	00.8	14	03.0	04	00.5	.	03	00.5	08	01.4	.	.	51					
III	681.9	-01.5	04.9	00.3	01.0	06.0	-02.4	12.1	07 -11.2	24	.	.	01	00.1	15	03.0	08	01.6	.	04	01.0	07	01.0	.	.	38					
IV	686.2	01.4	10.0	03.5	04.7	11.1	00.4	20.0	30 -05.0	11	01	00.3	04	00.4	10	01.6	04	00.5	01	00.2	05	00.9	09	01.5	.	.	56				
V	686.5	08.1	15.8	09.4	10.7	16.7	04.9	25.4	20 -03.0	02	01	00.2	04	00.6	04	00.6	08	01.3	01	00.1	04	00.8	09	01.4	.	.	62				
VI	686.0	10.0	16.7	11.6	12.5	18.3	06.7	26.5	27 -01.6	05	01	00.1	02	00.4	08	01.3	07	00.8	.	02	00.2	03	00.4	.	.	67					
VII	688.8	12.4	21.6	14.8	15.9	22.7	05.0	26.0	15 02.2	26	.	.	04	00.6	05	00.7	04	00.7	01	00.1	02	00.3	11	01.2	01	00.2	65				
VIII	685.8	11.9	20.0	14.0	15.0	21.0	09.7	25.8	04 04.3	20	.	.	03	00.4	06	00.7	04	00.7	.	02	00.3	08	00.9	.	.	70					
IX	691.0	10.3	19.5	12.5	13.7	20.6	08.3	26.8	17 06.5	14	.	.	01	00.2	08	02.2	09	02.3	.	69	01.9	05	01.0	01	00.2	57					
X	650.7	02.1	12.2	03.6	05.4	12.8	01.1	21.8	03 -02.8	26	.	.	04	00.6	02	00.4	08	01.6	02	00.4											

Mesec	Vrednost pristisak mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, Fm (O-12)																							
		Tm				Sred. (Dnes)	Hm	Hc	Hs	Dat.	Min	Max	Dat.	N		NE		E		SE		S		SW		W		NW							
		7	14	21	E.									J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.									
$\varphi = 46^{\circ}23' N \lambda = 13^{\circ}51' E$ Gr. $\Delta G = +55$ min.																																			
KREDARICA																																			
I	560.9	-04.9	-04.1	-04.7	-04.6	-01.7	-07.3	05.6	15	-15.0	09	17	C8.9	.	.	C2	C1.2	15	06.8	.	.	01	00.4	01	00.4	33	18.9	24							
II	561.0	-08.9	-07.1	-08.6	-08.3	-05.0	-11.3	01.6	06	-16.4	17	20	11.6	.	.	C5	C2.0	14	05.1	.	.	03	01.3	32	14.1	10									
III	553.4	-07.5	-06.1	-07.3	-07.1	-04.7	-09.2	03.2	01	-16.7	22	14	09.0	01	00.3	04	01.3	42	21.6	03	01.1	.	.	01	00.5	14	07.3	14							
IV	558.2	-04.9	-03.1	-05.1	-04.6	-01.9	-07.2	04.6	30	-13.3	11	25	13.6	01	00.3	04	01.5	19	11.0	31	14.2	10							
V	561.6	00.6	01.5	00.5	00.8	02.9	-01.2	05.8	20	-07.4	02	09	C3.0	.	.	C4	C1.2	31	13.3	03	01.3	.	.	01	00.3	22	08.9	23							
VI	563.0	01.5	03.0	01.7	02.0	04.5	-00.3	13.7	27	-08.0	06	16	C7.4	01	00.4	01	00.2	24	07.4	02	00.9	.	.	01	00.4	22	09.1	23							
VII	565.4	04.9	07.6	05.2	05.8	09.2	02.9	15.0	15	-04.3	01	21	C8.5	18	05.4	.	.	02	00.7	31	10.6	21									
VIII	565.9	04.4	08.8	04.8	05.2	07.5	03.1	14.0	04	-06.2	26	14	05.2	.	.	19	04.7	01	00.4	24	10.4	33									
IX	567.1	05.5	07.0	05.7	06.0	08.7	03.6	16.4	17	-03.2	13	03	01.3	.	.	02	00.5	26	10.3	01	00.3	.	.	08	04.2	24	09.0	26							
X	563.7	-01.1	00.5	-01.1	-00.7	01.6	-02.7	12.2	29	-08.7	11	09	C4.5	01	00.3	02	00.6	22	08.9	02	00.6	.	.	03	00.8	36	12.2	18							
XI	568.9	-05.8	-04.6	-05.6	-05.4	-02.5	-08.0	04.6	04	-20.6	23	19	10.2	03	01.1	01	00.3	27	12.1	04	01.8	.	.	03	01.2	21	11.4	12							
XII	561.2	-04.4	-03.1	-04.4	-04.1	-01.6	-06.9	06.8	23	-16.6	19	12	06.4	01	00.3	.	.	24	09.7	02	00.6	.	.	03	00.9	35	15.3	16							
GOD.	561.7	-01.7	-00.1	-01.6	-01.2	01.4	-03.7	18.4	47 IX	-26.6	24 XI	179	08.7	08	00.6	25	01.2	281	11.0	17	01.1	01	00.4	27	01.8	327	12.4	230							
$\varphi = 46^{\circ}01' N \lambda = 13^{\circ}55' E$ Gr. $\Delta G = +56$ min.																																			
VOJSKCI																																			
BR. ST. 7								
I	-	00.4	02.6	00.9	01.2	03.6	-01.7	07.7	04	-07.0	01	01	00.1	03	00.3	C6	00.6	12	01.3	02	00.2	12	01.6	37							
II	-	-02.7	01.0	-01.6	-01.2	C2.9	-04.7	10.3	19	-10.5	17	.	.	22	04.0	14	01.9	07	00.7	02	00.3	01	00.1	38							
III	-	00.6	02.9	01.2	01.5	04.2	-01.5	10.3	09.0	-07.9	24	.	.	C2	00.3	05	00.5	12	01.5	.	.	01	00.1	73							
IV	-	04.3	07.7	05.2	05.6	08.9	01.9	14.9	21	-02.1	03	.	.	01	00.1	14	01.4	01	00.2	02	00.2	20	02.1	52							
V	-	10.3	13.6	10.5	11.3	15.6	07.5	22.5	20	03.7	24	02	11	01.1	07	01.0	05	00.5	04	00.4	66						
VI	-	11.8	14.7	11.4	12.4	16.1	08.5	22.1	14	03.0	04.0	02	01	00.1	08	00.9	14	01.6	01	00.1	.	.	07	00.7	.	01	00.1	58							
VII	-	15.4	19.2	14.7	16.1	20.4	11.6	25.1	15	05.5	26	01	04	00.6	.	.	11	01.1	03	00.3	02	00.2	.	.	73						
VIII	-	14.0	17.6	13.6	14.9	18.9	11.3	22.0	01	06.7	20	.	.	05	00.6	20	02.1	01	00.2	67							
IX	-	13.2	16.8	13.3	14.2	17.7	10.7	27.0	17	05.0	13	18	01.9	12	01.4	.	.	02	00.2	58							
X	-	05.8	10.1	06.5	07.2	11.0	04.4	19.7	03	-01.3	12	.	.	08	01.1	22	02.3	03	00.3	60							
XI	-	00.5	01.8	01.0	01.1	03.3	-01.2	11.3	03	-11.0	24	08	01.2	02	00.6	22	02.5	03	00.4	01	00.1	03	00.3	51							
XII	-	-00.2	01.3	-00.1	00.2	03.0	-02.9	11.0	28	-11.9	20	11	.	.	.	18	02.0	03	00.3	02	.	03	00.3	72							
GOD.	-	06.1	06.1	06.4	07.0	10.4	03.7	27.0	47 IX	-11.5	20 XII	14	00.9	51	02.2	175	01.8	02	00.2	02	00.2	87	01.3	12	00.3	27	00.9	725							
$\varphi = 46^{\circ}21' N \lambda = 14^{\circ}11' E$ Gr. $\Delta G = +57$ min.																																			
RADOVLJICA																																			
BR. ST. 8								
I	-	-00.9	04.7	01.4	02.2	07.4	-01.8	11.6	04	-07.6	11	18	C2.5	C8	01.1	.	.	04	C1.2	08	01.3	01	00.1	.	.	15	02.4	37							
II	-	-03.1	05.9	00.5	01.0	06.8	-04.0	12.1	28	-10.5	18	16	C2.4	13	02.4	.	.	09	C2.0	09	01.2	10	01.8	.	.	02	00.3	25							
III	-	01.1	07.4	04.1	04.2	08.3	00.2	15.1	09	-06.5	24	14	C2.2	08	01.5	.	.	11	C2.0	14	02.3	.	.	04	00.9	40									
IV	-	05.1	12.6	08.9	08.6	13.5	03.1	22.4	30	-02.6	02	12	C2.2	09	01.7	.	.	13	C2.7	14	02.2	02	00.3	.	.	06	01.6	34							
V	-	11.5	18.5	13.8	14.4	19.5	06.2	27.4	18	03.2	09	16	C2.8	09	02.0	.	.	05	00.9	04	00.6	05	00.9	.	.	09	01.5	45							
VI	-	13.3	18.9	14.8	15.5	20.3	10.5	27.9	14	04.8	05	14	C2.6	06	01.6	.	.	10	C2.7	09	01.5	06	01.4	.	.	10	03.1	33							
VII	-	15.6	23.5	17.7	18.6	24.2	12.4	28.9	15	08.0	27	14	C3.7	12	02.8	.	.	10	C1.9	03	00.6	03	01.0	.	.	13	03.6	38							
VIII	-	14.9	22.3	17.2	17.6	23.1	12.8	26.4	07	04.6	20	10	C1.5	08	01.8	.	.	09	C2.0	08	01.3	04	01.1	.	.	06	01.1	48							
IX	-	12.8	21.3	15.7																															

Mjesec	Vazdušni pritisak Pa (mm)	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра m/s, Fm (0-12)															
		Tm					N	NE	E	SE	S	SW	W	NW	C												
		7	14	21	Sred. (Dnev.)	N	NE	E	SE	S	SW	W	NW	C													
$\varphi = 46^{\circ}13' N \lambda = 14^{\circ}29' E$ Gr. $\Delta G = + 58$ min.																											
I	733.5	-01.7	06.9	00.2	01.4	07.7	-03.6	11.0	31 -05.8	11 01	CC.1	G6	00.7	G5	00.9	G2	00.3	12	G2.4	10	01.5	23	03.7	01 00.1	33		
II	735.9	-05.1	06.0	-02.0	-00.8	07.1	-06.6	13.1	28 -13.2	18 04	CC.6	G9	01.7	G3	03.6	C2	00.3	04	01.0	06	00.6	21	02.6	02 00.3	23		
III	725.1	00.6	08.1	02.9	03.7	05.5	-01.1	16.9	09 -05.2	24 04	00.6	G4	00.7	G4	02.8	G1	00.1	08	01.2	13	G2.3	22	03.6	03 00.4	24		
IV	726.9	04.9	13.4	06.7	07.9	14.8	01.5	22.9	30 -04.4	28 04	CC.6	G9	01.6	G7	03.1	C4	00.7	08	01.6	08	01.5	12	02.0	04 01.4	22		
V	728.8	11.5	19.0	13.3	14.3	20.4	07.1	27.7	18 -01.8	02 07	C1.1	G1	02.1	G2	02.1	C2	00.3	05	00.8	12	G2.3	11	01.9	03 00.8	30		
VI	729.6	12.9	19.1	13.8	14.9	21.0	08.8	27.6	27.15 -00.4	07 08	C1.4	G4	02.1	G1	02.6	C2	00.2	08	01.0	07	01.2	12	G2.3	07 00.3	23		
VII	730.1	15.2	23.8	16.6	18.1	25.2	11.0	30.6	15 05.0	28 09	01.3	G7	01.1	G1	01.9	C6	01.1	05	01.0	05	00.8	13	G2.8	03 01.1	34		
VIII	731.1	14.5	22.8	15.4	17.3	24.1	11.2	27.2	11 06.0	20 05	CC.6	G7	00.9	G5	02.4	G5	00.8	11	01.5	05	00.5	08	01.5	03 00.4	34		
IX	732.1	12.0	21.9	14.1	15.5	23.1	09.4	28.5	17 04.8	21 01	CC.1	G8	01.3	G2	02.0	C4	00.5	07	01.1	04	00.5	13	G2.2	01 00.1	40		
X	733.5	04.2	13.6	C5.7	07.3	14.6	02.4	23.7	02 -03.5	27 03	CC.4	G9	01.4	G7	01.5	C2	00.3	05	00.5	04	00.4	15	01.9	02 00.2	46		
XI	731.7	01.2	05.7	02.6	03.0	06.4	-03.3	17.4	02 -14.4	23 05	00.5	G6	01.1	G10	01.8	C2	00.2	07	00.9	07	00.7	18	03.3	01 00.1	34		
XII	734.8	-03.9	00.8	-03.2	-02.4	01.6	-05.5	08.4	01 -17.2	20 03	CC.3	G8	00.9	G6	00.9	G1	00.1	02	00.2	03	00.4	12	01.6	01 00.2	57		
God.	731.4	05.5	13.4	07.2	08.4	14.6	02.9	30.6	15.VII -17.2	20.XV	54	CC.8	G9	01.4	138	02.4	33	00.6	82	01.3	84	01.3	180	02.6	26 00.7	400	
$\varphi = 46^{\circ}24' N \lambda = 14^{\circ}30' E$ Gr. $\Delta G = + 58$ min.																											
JEZERSK																								BR. ST.11			
I	-	-01.5	C3.2	-00.8	00.0	04.4	-03.5	07.9	26 -1C.4	11	.	.	13	02.9	.	.	17	03.8	63	
II	-	-04.3	C4.1	-02.7	-01.4	C4.5	-05.8	12.6	07 -13.7	18	.	.	28	08.0	02	00.7	C4	01.2	.	.	08	02.1	04	01.0	01 00.2	37	
III	-	-00.2	04.9	01.3	01.9	05.8	-01.2	13.5	09 -10.8	24	.	.	24	04.8	03	00.4	14	04.6	13	04.2	04 02.0	33	
IV	-	02.7	10.0	04.8	05.6	11.1	00.9	20.0	30 -02.0	12	.	.	C9	02.2	G7	02.1	02	01.1	.	.	11	04.3	09	03.6	14 04.4	37	
V	-	08.7	15.7	10.2	11.2	16.8	08.3	25.4	15 -0C.4	02	.	.	05	06.8	02	00.4	02	00.6	.	.	07	02.0	11	02.8	05 01.3	61	
VI	-	10.5	15.5	11.6	12.3	17.6	07.7	25.0	14 02.2	05	.	.	13	03.1	G9	01.9	03	00.7	.	.	13	03.3	06	01.3	.	46	
VII	-	11.9	20.7	14.1	15.2	21.8	05.4	28.3	15 04.6	27	.	.	15	03.5	01	00.3	10	02.3	.	.	10	02.9	03	00.8	02 00.8	52	
VIII	-	11.9	19.6	13.4	14.9	20.5	09.9	24.3	15 06.0	20	.	.	C9	01.5	G6	01.0	06	01.2	.	.	09	02.0	05	01.1	01 00.3	57	
IX	-	04.7	15.9	12.4	13.5	20.4	08.7	27.9	17 03.4	14	.	.	02	00.3	G1	00.2	05	01.5	.	.	10	02.4	11	02.3	10 02.4	51	
X	-	03.0	12.4	04.1	05.9	13.0	02.0	22.3	03 -01.2	16	.	.	13	02.4	G8	01.8	05	01.0	.	.	03	00.9	.	.	03 00.6	61	
XI	-	-00.9	03.2	00.5	00.8	04.4	-02.0	15.8	03 -11.9	25	.	.	07	01.2	.	.	07	01.6	.	.	06	00.9	01	00.2	15 03.5	54	
XII	-	-03.4	01.8	-03.3	-02.1	03.3	-05.2	10.6	27 -12.4	21	.	.	08	01.4	G4	00.7	06	01.2	.	.	04	01.0	02	00.6	05 00.8	64	
God.	-	04.0	10.9	05.5	06.4	12.0	02.3	28.3	15.VII -13.7	18.II	.	.	146	03.8	43	01.4	68	02.5	.	.	95	02.8	65	02.5	62 02.7	616	
$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.																											
LJUBLJANA-BEŽIGRAD													BR. ST.13														
I	736.9	02.0	07.1	04.1	04.3	07.9	01.0	11.6	19 -05.4	11 09	01.0	23	02.4	08	01.0	03	00.3	03	00.4	24	04.8	10	01.4	12 01.5	01		
II	742.0	-01.4	06.3	01.6	02.0	07.3	-02.0	12.4	28.07 -05.5	18 13	01.3	23	03.9	18	03.6	04	00.6	.	.	08	01.4	04	00.8	08 00.9	06		
III	731.0	02.8	08.8	05.9	05.9	10.3	02.1	17.2	09 -04.7	01 12	01.3	08	00.8	09	01.3	10	01.5	05	00.8	12	02.2	16	02.5	07 01.4	14		
IV	724.7	06.1	14.1	10.0	10.0	15.2	04.9	24.0	30 01.0	28.12	11	01.3	15	01.9	10	01.5	16	02.3	06	03.1	14	03.1	06	01.2	12 01.7	.	
V	-	12.0	18.3	14.4	14.8	19.3	05.6	26.0	20.19 -02.5	11 09	01.8	09	01.7	05	00.9	12	02.5	13	02.5	18	04.6	22	06.2	04 01.1	01		
VI	-	13.5	20.4	15.9	16.5	21.6	12.0	30.3	14 04.6	07.06	11	C1.4	22	02.8	14	01.6	07	00.9	15	02.3	20	05.8	03 00.6	07 01.1	06		
VII	-	13.5	16.1	25.1	18.5	19.8	26.3	14.3	32.0	15 07.6	01	07	01.2	24	02.7	14	02.1	20	05.4	06	01.6	17	02.6	.	17	02.6	.
VIII	-	13.6	23.6	18.1	18.7	24.0	13.4	30.0	15 07.6	01	07	01.2	24	02.7	14	02.1	20	05.4	06	01.6	17	03.0	08	01.0	08 00.6	01	
IX	-	13.8	21.4	16.8	17.2	22.0	12.3	26.5	17 08.0	14	02	00.5	24	03.9	05	00.8	14	03.6	14	02.2	13	03.7	10	02.8	05 01.2	03	
X	-	06.7	13.9	06.5	09.9	14.4	05.6	23.6	C1 00.2	26	07	01.1	21	03.1	G5	01.0	04	03.4	20	04.0	13	03.0	07	01.8	.	04	
XI	-	02.5	05.8	03.9	04.0	06.4	01.4	18.2	02 -08.2	25	04	00.6	08	01.5	03	01.0	12	02.3	27	04.4	13	02.3	13	02.6	07 01.2	03	
XII	-	-01.5	02.6	00.0	00.3	03.6	-02.8	10.0	06 -10.2	20	03	0C.4	13	02.5	G7	01.3	14	02.8	06	01.2	30	05.2	12	01.9	05 01.0	03	
God.	-	07.4	13.1	09.6	09.9	14.1	05.8	30.0	16.VII -1C.2	20.XV	78	CC.5	18.9	04.0	57	01.2	122	02.7	158	03.2	202	04.0	175				

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha e _m mm	Padavine R mm			Broj dana nasa:																														
	7	14	21		7	14	21	Sred. Min.	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	*	•	Δ	▲	▲	R _t	•									
	Sped. (Dnes)	Inzakcija broj sati									=	<	<	=	=	=	=	=	=	>	N	N	N	N	9	Δ	▲	▲	T	=								
BR. ST.11																																						
BRATK-LETALISTE																																						
I	5.8	6.0	6.0	5.9	097.0	04.3	94	66	90	83	33	013	006.3	28	.	.	26	.	.	.	02	.	06	11	08	04	.	08	.	00								
II	4.7	3.5	3.8	4.1	159.4	03.2	90	53	80	74	21	014	008.4	15	06	.	27	.	.	.	03	.	12	66	05	02	.	04	03	.	03							
III	7.7	7.9	7.0	7.6	058.8	05.2	54	71	91	86	30	250	C78.8	20	.	.	17	.	.	.	C2	.	02	17	18	16	10	18	03	03	03							
IV	6.8	7.1	5.5	6.5	164.6	05.5	89	55	81	75	26	106	C31.2	06	.	.	10	.	.	.	05	.	02	10	11	09	03	11	.	.	01							
V	6.4	7.0	7.0	6.8	168.8	09.3	90	58	82	77	21	121	C16.7	06	.	.	J2	06	.	.	03	.	03	12	20	18	04	20	.	.	01							
VI	6.8	7.1	6.3	6.7	139.2	10.8	92	66	90	83	30	178	031.6	02	.	.	02	04	.	.	01	.	11	22	16	06	21	.	.	.	13							
VII	4.7	4.9	5.5	5.0	257.8	12.3	90	56	89	78	36	183	049.4	01	.	.	22	01	.	.	C8	03	C2	05	17	11	06	17	.	01								
VIII	5.2	6.6	5.7	5.9	191.3	12.1	95	60	91	82	38	087	023.8	25	.	.	13	.	.	.	03	.	07	17	12	03	17	.	.	01								
IX	5.9	5.2	3.9	5.0	155.6	11.4	98	62	96	86	46	045	009.0	13	.	.	07	.	.	.	06	06	12	07	11	09								
X	5.5	5.8	4.8	5.5	119.9	06.5	98	66	96	86	38	075	020.0	17	.	.	09	.	.	.	07	09	17	07	04	13	.	.	.	02								
XI	8.1	7.6	7.6	7.8	048.4	05.0	90	74	88	84	25	084	030.5	18	05	.	12	.	.	C3	01	05	21	16	08	03	14	02	02	01								
XII	7.1	6.2	6.8	6.7	065.3	03.8	94	88	94	92	61	132	042.8	02	07	09	27	.	.	.	05	16	11	08	05	10	04	01	01	01								
GOD.	6.3	6.3	5.8	6.1	1666.1	07.5	92	64	89	82	21	1288	078.8	20	III	16	09	132	56	01	.	30	04	50	131	174	118	44	166	14	04	03	01	02	03	73	128	24
BR. ST.12																																						
JEZERSKE																																						
I	5.5	4.8	4.3	4.9	-	03.9	90	71	88	83	42	028	009.1	28	01	01	27	.	.	.	09	09	10	06	.	04	05	.	.	02								
II	4.9	3.6	3.6	4.0	-	02.9	84	53	79	72	20	024	014.1	15	02	03	27	.	.	.	12	06	08	03	01	03	07	.	.	01								
III	6.2	7.7	6.5	7.5	-	04.3	90	69	86	82	28	367	059.6	20	01	01	17	.	.	.	01	17	19	17	11	16	13	07	.	01								
IV	6.2	7.3	5.4	6.3	-	05.0	86	55	81	74	19	336	101.0	07	.	.	15	.	.	.	03	12	11	10	05	11	03	01	.	01								
V	6.1	7.2	5.8	6.4	-	07.9	91	60	87	79	26	172	025.6	06	.	.	01	01	.	.	04	11	19	14	07	15	.	.	.	02								
VII	6.7	8.0	7.1	7.3	-	09.0	88	70	87	81	30	279	049.1	02	.	.	01	.	.	.	01	14	22	20	10	22	.	.	07	01								
VIII	5.7	6.2	5.6	5.8	-	10.5	92	59	90	89	37	304	084.5	01	.	.	06	.	.	.	05	06	19	14	10	19	.	.	.	11								
GOD.	5.5	5.9	5.1	5.5	-	10.2	94	63	90	82	40	136	044.1	25	01	09	18	17	04	18	.	.	.	07								
BR. ST.13																																						
LJUBLJANA-BEŽIGRAD																																						
I	7.0	6.4	6.7	6.7	070.7	05.0	89	68	80	79	31	032	011.4	28	.	01	12	.	.	.	04	14	07	04	01	07	.	.	.	07								
II	5.3	3.5	4.1	4.5	143.2	03.8	84	54	68	69	22	014	009.3	15	.	.	17	.	.	.	01	08	05	03	04	03	01	.	.	03								
III	7.8	7.2	6.3	7.1	092.3	05.5	91	68	79	79	23	248	075.4	20	.	.	07	.	.	.	04	14	21	16	06	21	04	04	.	01								
IV	6.7	6.6	4.8	6.0	176.9	06.0	85	52	66	68	23	089	033.3	06	02	04	09	12	01	01	.	.	.	01								
V	7.4	6.4	6.5	6.8	185.7	09.3	87	54	75	72	21	192	079.2	31	.	.	06	.	.	.	04	13	20	18	04	20	.	.	.	02								
VI	6.0	7.2	6.1	7.1	150.2	10.6	88	55	79	76	26	180	030.0	30	.	.	04	01	.	.	01	12	20	14	07	20	.	.	.	02								
VII	5.8	4.4	5.1	5.1	271.9	12.3	86	50	80	72	32	252	070.5	01	.	.	24	03	.	.	01	07	06	18	06	18	.	.	.	01								
VIII	7.0	6.0	4.8	6.0	208.7	12.5	92	57	84	77	37	110	017.4	12	.	.	19	.	.	.	01	10	20	16	03	20	.	.	.	01								
IX	9.0	4.6	3.2	5.6	180.6	12.1	95	57	89	80	46	044	016.0	07	.	.	11	01	.	.	01	04	10	07	01	10	.	.	.	09								
X	9.7	5.0	5.5	6.0	111.9	07.4	94	61	90	82	36	075	020.7	17	.	.	04	.	.	.	01	12	13	08	04	11	.	.	.	01								
XI	8.1	8.0	7.9	8.0	045.5	04.5	91	75	85	84	18	080	021.1	14	.	.	06	.	.	.	01	23	20	07	03	20	01	.	.	01								
XII	9.2	6.6	7.6	7.8	022.8	04.1	93	84	92	80	59	119	036.3	02	10	20	01	19	12	08	05	08	04	01	.	01								
GOD.	7.6	6.0	5.7	6.5	1640.4	07.8	89	61	80	77	18	1435	079.2	34	V	11	62	65	05	05	14	.	37	143	178	128	43	171	15	08	.							

Mjesec	Vardunski Dijeljak Dan	Temperatura vazduha °C										Čestina pravaca i srednja jačina vatra nD, Pm (0-12)																	
		Tm					Det.					N			NE		E		SE		S		SW		W		NW		
		7	14	21	Sred. (Dnev.)	N	H	K	M	D	M	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.				
$\varphi = 46^{\circ}04' N \lambda = 15^{\circ}11' E$ Gr. $\Delta G = +1h\ 01\ min.$															RADECE												BR. ST. 16		
I	-	02.5	08.8	04.2	04.9	05.6	06.8	15.5	06	-05.5	10	18	03.1	.	.	C5	00.9	.	.	08	01.2	01	00.3	17	04.4	09	02.7	35	
II	-	-01.1	06.8	01.5	02.2	08.0	-02.4	14.6	28	-06.6	18	16	C3.8	.	.	08	02.1	01	00.2	24	06.5	.	.	06	01.1	08	03.3	21	
III	-	03.5	09.9	06.2	06.4	11.6	02.0	17.3	09	-04.3	01	23	05.2	.	.	08	02.4	.	.	10	02.2	.	.	14	03.5	06	02.2	32	
IV	-	06.7	14.7	09.2	10.0	15.6	04.0	23.8	30	00.6	12	36	C8.1	01	00.3	01	00.2	.	.	05	01.3	.	.	07	01.5	11	03.9	29	
V	-	13.3	20.3	15.0	15.9	21.7	10.2	26.4	20	04.7	11	29	07.4	01	00.2	04	00.8	.	.	08	01.6	.	.	03	00.9	10	03.2	38	
VI	-	14.8	20.7	15.6	16.7	22.0	11.4	29.3	15	03.7	05	35	C7.9	03	01.1	03	00.6	02	00.4	47		
VII	-	16.9	25.0	16.8	26.4	14.0	31.6	15	08.3	27	25	05.1	.	.	04	01.2	.	.	10	02.1	.	.	04	00.9	01	00.3	49		
VIII	-	16.3	24.0	17.4	18.8	24.7	14.0	28.9	15	10.7	22	34	07.8	01	00.2	C1	00.3	.	.	06	01.2	.	.	.	04	01.5	47		
IX	-	14.2	23.3	16.0	17.4	24.3	12.7	30.5	17	07.8	14	19	02.9	01	00.3	C1	00.2	.	.	12	02.4	.	.	04	00.6	01	00.2	52	
X	-	07.3	19.3	08.7	10.0	16.5	06.0	26.8	01	06.7	28	18	03.9	.	.	02	00.3	.	.	07	01.4	.	.	.	07	02.3	57		
XI	-	03.1	06.9	04.3	04.7	07.8	01.5	16.5	02	-10.1	26	24	07.0	.	.	01	00.2	.	.	01	00.1	.	.	04	01.1	61			
XII	-	-06.9	03.9	00.3	00.9	04.7	-02.0	13.2	06	-08.2	20	17	04.2	.	.	01	00.1	.	.	04	00.8	.	.	.	04	00.9	67		
600.	-	08.0	15.0	09.8	10.6	16.1	06.0	31.6	15.VN	-10.1	26.XI	294	06.0	07	00.6	38	01.4	C1	00.2	95	02.9	01	00.3	55	02.7	67	02.5	537	
$\varphi = 46^{\circ}37' N \lambda = 15^{\circ}13' E$ Gr. $\Delta G = +1h\ 01\ min.$															RADLJE OB DRAVI												BR. ST. 17		
I	-	-00.1	07.5	02.2	02.9	08.2	-01.2	13.8	19	-07.4	11	03	C0.4	01	00.2	01	00.2	04	00.7	01	00.3	13	02.5	05	00.6	09	01.7	56	
II	-	-03.0	06.4	-00.3	00.7	07.6	-04.3	14.2	28	-09.8	18	17	03	00.3	03	00.4	02	00.2	05	00.5	01	00.2	05	00.7	02	00.3	05	00.6	38
III	-	02.1	09.6	03.1	05.5	11.1	00.8	18.8	09	-06.2	01	02	00.3	03	00.3	01	00.2	04	00.6	.	.	04	00.9	06	00.6	05	00.5	48	
IV	-	04.7	14.0	08.6	09.0	15.6	02.6	24.5	30	-01.6	28	01	00.1	02	00.4	04	00.6	05	00.6	01	00.3	12	02.7	04	00.6	07	01.1	54	
V	-	11.2	19.4	14.1	14.7	21.2	09.2	27.9	19	01.3	03	02	00.2	04	01.1	03	00.6	03	00.6	07	00.6	10	01.9	64
VI	-	12.9	19.6	15.0	15.6	20.8	10.8	25.8	15	01.8	06	02	00.5	01	00.1	02	00.2	04	00.8	.	.	02	00.4	03	00.6	01	00.1	73	
VII	-	14.6	24.7	17.5	18.6	26.3	13.2	31.4	15	08.8	27	02	00.2	01	00.1	05	00.7	.	.	04	00.7	03	00.3	07	01.0	69			
VIII	-	14.7	23.3	17.1	18.1	24.1	13.9	28.4	15	09.0	20	02	00.3	09	00.5	02	00.2	05	00.5	01	00.1	04	00.4	.	.	03	00.7	69	
IX	-	13.9	23.7	15.9	17.4	24.6	12.5	30.7	17	04.7	14	01	00.2	01	00.1	.	.	03	00.4	02	00.2	03	00.5	02	00.3	11	01.5	67	
X	-	06.9	15.3	07.8	09.4	15.9	05.2	26.9	01	-01.4	27	01	00.2	.	.	01	00.1	03	00.3	.	.	02	00.3	05	00.3	03	00.3	78	
XI	-	01.2	06.2	02.4	03.0	07.2	00.0	19.3	03	-11.6	25	03	00.4	02	00.2	.	.	04	00.5	.	.	04	00.5	05	01.0	06	00.9	66	
XII	-	-02.2	03.3	-01.4	-00.4	04.3	-03.4	05.6	29	-11.2	20	01	00.1	.	.	01	00.1	03	00.4	.	.	04	00.5	05	00.9	04	00.4	75	
600.	-	06.4	14.4	08.7	09.5	15.6	04.9	31.4	15.VN	-11.6	25.XI	21	00.3	20	00.3	15	00.3	51	00.6	09	00.3	62	01.4	47	00.6	73	01.1	797	
$\varphi = 46^{\circ}15' N \lambda = 15^{\circ}14' E$ Gr. $\Delta G = +1h\ 01\ min.$															CELJE-LEVEC												BR. ST. 18		
I	-	00.8	07.7	02.9	03.6	08.2	-01.2	13.7	06	-08.9	11	.	09	00.5	.	.	C3	00.3	.	.	35	06.0	.	.	08	01.1	42		
II	-	-03.6	06.1	-00.6	00.3	07.0	-05.4	14.0	28	-11.7	18	.	14	01.7	01	00.1	10	01.5	.	.	13	02.3	.	.	02	00.2	44		
III	-	02.1	09.3	04.9	05.3	10.5	00.0	16.6	09	-07.7	01	.	06	00.6	.	.	21	03.9	02	00.4	05	00.4	03	00.9	43				
IV	-	05.0	13.9	08.3	08.9	15.0	02.0	23.0	30	-02.4	18	.	20	02.5	01	00.1	23	02.4	.	.	19	02.9	.	.	06	01.0	21		
V	-	12.4	19.7	14.7	15.4	21.0	08.6	28.2	18	02.2	03	01	00.1	18	02.0	.	.	18	02.6	.	.	33	05.1	01	00.1	08	01.1	14	
VI	-	14.2	19.7	15.1	16.0	21.1	10.8	29.4	14	01.8	05	02	00.2	12	01.5	02	00.2	23	02.9	.	.	36	04.8	.	.	07	00.8	68	
VII	-	16.1	24.7	19.0	19.7	26.2	13.1	32.3	15	06.4	27	01	00.1	17	02.0	06	00.9	08	01.0	.	.	14	02.0	06	00.6	12	01.8	29	
VIII	-	15.1	23.1	16.2	17.7	24.2	13.0	28.0	11	09.4	21	01	00.1	20	02.2	02	00.3	23	02.4	.	.	14	01.8	02	00.2	06	00.7	25	
IX	-	13.4	23.1	15.1	16.7	23.7	11.4	28.6	17	05.4	14	.	13	01.6	.	.	14	01.7	.	.	13	02.2	.	.	07	00.7	43		
X	-	06.0	14.7	08.6	08.6	15.3	03.9	25.7	01	-01.8	27	.	14	01.5	.	.	15	01.7	.	.	10	01.0	.	.	05	00.5	49		
XI	-	01.9	05.6	02.1	02.9	06.4	-00.3	11.6	03	-12.7	25	.	16	01.7	.	.	15	01.8	.	.	07	01.1	.	.	07	01.1	45		
XII	-	-02.6	02.4	-01.5	-00.6	03.2	-04.5	09.8	06	-11.7	20	.	10	01.0	.	.	09	00.9	.	.	12	01.2	.	.	09	00.9	53		
600.	-	07.7	14.2	08.6	09.5	15.2	04.3	32.3	15.VII	-12.7	26.XI	165	01.8	12	00.6	177	02.1	.	.	227	03.7	11	00.						

Mjesec	Vazdušni pritisak Pm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)																					
		Tm				Srednje (Dnev.)						N						NE		E		SE		S		SW		W		NW		C	
		7	14	21	Srednje (Dnev.)	M	H	K	M	D	M	E	J	S	J	S	J	E	J	S	J	E	J	S	J	E	J	C					
$\varphi = 46^{\circ}24' N \lambda = 15^{\circ}39' E$ Gr. $\Delta G = + 1h 03 min.$																									PHAGERSKO		BR. ST. 21						
I	-	08.4	07.9	03.0	03.6	08.4	-06.6	15.3	06	-06.0	10	.	.	03	00.4	40	09.1	04	00.7	01	00.1	45					
II	-	-02.6	06.4	00.3	01.1	06.8	-03.6	12.0	28.13	-1c.2	18	.	.	23	06.0	c2	00.4	18	03.5	02	00.4	04	00.4	34					
III	-	03.2	10.0	05.3	06.0	11.1	01.7	16.7	09	-03.7	01	.	.	21	03.9	.	.	03	00.6	.	.	28	08.4	41					
IV	-	06.3	14.2	08.3	09.3	15.0	02.6	22.4	30	-01.5	26	.	.	20	03.8	c1	00.2	c6	00.9	.	.	23	05.5	01	00.1	02	00.3	37					
V	-	12.2	20.6	14.3	15.4	21.3	09.3	26.0	19.18	03.0	03	.	.	09	01.5	c4	00.6	12	02.2	01	00.2	16	04.3	.	.	04	00.9	47					
VI	-	14.5	20.2	15.0	16.2	21.4	11.0	29.6	15	03.0	05	.	.	05	01.0	c3	00.3	c7	01.0	.	.	11	02.0	02	00.3	13	02.6	49					
VII	-	15.9	24.7	17.7	19.0	25.2	13.2	30.8	15	07.3	26	.	.	12	03.0	.	.	c5	01.8	.	.	08	01.1	.	.	10	01.6	56					
VIII	-	15.3	23.2	16.6	18.0	24.2	13.1	27.5	11.10	05.8	21	.	.	12	02.1	c1	00.2	c7	01.0	.	.	09	01.3	.	.	08	01.5	56					
IX	-	13.4	22.9	15.5	16.8	23.5	11.5	25.0	17.16	04.4	14	.	.	11	01.9	25	04.6	54					
X	-	08.1	14.6	08.1	09.3	14.9	04.7	26.0	01	-01.2	26	.	.	18	02.7	c2	00.3	c1	00.1	.	.	10	01.5	.	.	03	00.4	59					
XI	-	02.1	05.9	03.1	03.6	06.5	00.8	11.5	03	-10.5	26.25	.	.	25	03.9	.	.	08	01.1	.	.	03	00.6	04	00.9	07	01.1	43					
XII	-	-02.3	03.0	-00.4	00.0	03.5	-03.2	10.4	03	-10.8	20	.	.	10	01.6	.	.	01	00.2	.	.	09	01.2	07	01.0	06	00.7	60					
600.	-	07.0	14.5	08.4	09.9	15.2	05.1	30.8	15.VII	-10.8	20.XII	.	.	158	03.4	14	00.4	65	01.4	01	00.2	200	05.2	20	00.7	58	01.4	578					
$\varphi = 46^{\circ}38' N \lambda = 16^{\circ}11' E$ Gr. $\Delta G = - 1h 05 min.$																									MURSKA SOBOTA		BR. ST. 22						
I	748.4	00.2	06.7	01.9	02.7	07.5	-01.6	15.3	06	-08.7	11	10	01.6	04	00.8	05	00.6	03	00.5	22	08.6	02	00.3	06	01.0	04	00.8	37					
II	751.7	-02.9	05.6	00.1	00.7	06.5	-04.4	13.6	13	-10.9	18.17	10	03.7	11	02.8	c2	00.3	c7	01.3	06	01.4	.	08	02.3	03	00.3	37						
III	740.0	02.3	10.2	05.7	06.0	11.3	00.8	16.0	28.08	-06.6	01	06	02.0	12	02.3	01	00.2	05	00.9	13	04.3	09	03.5	05	00.9	13	02.9	29					
IV	744.0	06.3	14.0	08.1	09.1	14.8	02.6	22.1	30	-03.6	12	11	02.6	15	02.9	c3	00.6	05	00.7	15	03.4	05	01.4	03	00.7	14	03.0	19					
V	743.5	19.2	20.3	14.4	15.6	21.0	09.3	27.2	19	03.2	10	08	01.6	17	03.7	03	00.7	08	01.5	11	03.2	04	01.6	05	00.6	12	02.4	25					
VI	744.4	15.0	20.5	15.4	16.6	21.6	11.4	29.3	19	04.9	05	16	04.8	09	01.7	10	01.5	c2	00.3	14	03.4	.	04	00.9	10	02.0	25						
VII	744.5	17.1	24.5	17.7	19.3	25.2	13.1	29.8	19	07.3	26	12	02.0	11	01.8	06	00.8	15	02.2	04	00.7	06	00.8	10	01.5	24	04.7	05					
VIII	745.7	16.2	23.7	17.2	18.6	24.3	12.4	27.9	11	07.3	22	17	03.3	19	03.4	c3	00.8	05	00.9	06	01.1	05	00.9	03	00.4	09	01.7	30					
IX	747.6	13.6	22.8	15.4	16.8	23.1	10.4	28.5	17	04.4	14	01	00.2	06	01.5	03	00.5	09	01.7	21	05.0	04	00.6	02	00.3	02	00.3	42					
X	748.8	08.0	14.2	07.3	08.7	14.7	03.3	25.3	01	-02.8	29.28	13	02.0	17	03.4	11	02.2	03	00.8	09	01.4	02	00.5	02	00.3	02	00.4	34					
XI	747.5	01.9	05.7	03.0	03.4	06.2	00.7	10.3	19	-11.2	23	05	01.6	13	02.7	14	02.5	14	02.9	08	01.6	01	00.2	07	01.1	09	02.3	19					
XII	-02.0	02.4	-00.8	-00.3	03.0	-03.8	09.5	03	-11.1	20	05	01.1	05	00.9	06	01.2	16	03.0	05	00.7	04	00.5	06	01.1	04	00.1	40						
600.	-	08.3	13.5	09.9	10.4	14.4	06.8	28.5	15.VII	-08.0	20.XII	.	.	427	09.5	04	00.3	138	03.2	.	.	464	09.2	05	00.3	51	02.1	06					
$\varphi = 46^{\circ}28' N \lambda = 16^{\circ}12' E$ Gr. $\Delta G = + 1h 05 min.$																									JERUZALEM		BR. ST. 23						
I	-	02.6	07.4	04.2	04.6	08.3	01.8	16.5	06	-03.0	05	.	.	16	03.4	c1	00.2	07	01.2	.	.	69	15.8	.	.	01	00.1	01					
II	-	-01.2	04.9	01.6	01.7	09.8	-01.8	12.9	28.12	-08.0	17	.	.	45	11.5	.	.	c6	01.0	.	.	29	04.1	02	00.5	01	00.1	01					
III	-	03.9	09.5	06.1	06.4	10.3	03.1	16.0	06	-02.5	24.22	.	.	31	08.0	.	.	09	01.0	.	.	53	13.4	.	.	02	00.4	01					
IV	-	07.3	13.4	09.3	09.8	14.2	05.4	22.0	30	01.3	12	.	.	42	10.6	.	.	03	00.7	.	.	43	10.3	.	.	02	00.4	01					
V	-	13.7	19.2	15.1	15.8	20.5	10.7	24.5	18	02.0	02	.	.	46	11.7	.	.	03	00.6	.	.	36	07.4	.	.	05	01.3	.					
VI	-	15.1	19.2	15.6	16.4	20.6	12.3	26.5	15	06.3	06.02	.	.	34	09.2	01	00.3	12	02.8	04	00.2	01	00.8	01	00.8	01	00.8	01					
VII	-	17.7	23.3	19.0	19.7	24.2	15.0	26.5	19	08.5	01	.	.	19	05.1	.	.	17	03.8	.	.	40	07.2	.	.	15	04.1	02					
VIII	-	16.5	22.5	17.9	18.7	23.3	13.9	27.5	11	12.0	14	.	.	33	08.6	.	.	14	03.2	.	.	36	07.3	.	.	09	02.1	01					
IX	-	15.2	22.2	17.6	18.2	22.4	13.4	27.5	16	08.0	14	.	.	26	06.1	.	.	27	05.9	.	.	33	06.9	.	.	04	01.0	.					
X	-	07.9	13.4	09.5	10.1	14.0	07.3	25.5	01	02.0	21.12	.	.	39	10.2	.	.	15	03.6	.	.	27	06.0	01	00.2	01	01.7	01					
XI	-	01.8	04.7	03.0	03.1	05.3	01.2	08.5	15	-07.8	25	.	.	52	11.7	02	00.4	07	01.4	.	.	25	05.4	01	00.2	03	00.8	01					
XII	-	-01.0	02.0	00.1	00.3	02.8	-01.6	08.5	08.06	-06.0	20	.</																					

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana n s a:																																		
	7	14	21		Sred. mm	7	14	21	Sred. Min	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■													
													≤	<	<	≤	≤	≤	≤	≤	≤	≤	<	>	≤	≤	≤	6	8	2.0	8.0	0.1	1.0	2.0	0.0	0.25	0.30	0.20	0.6						
PRAGERSK																																													
BR. ST. 21																																													
I 5.2	5.4	5.0	5.2	-	04.7	85	66	82	78	47	020	COS.2	05	.	.	18	08	C8	04	03	.	04	01	01	03	03										
II 3.6	3.6	3.6	3.6	-	03.7	81	59	74	71	28	023	C10.4	15	01	.	23	14	C8	04	03	01	02	03	01	05											
III 6.2	6.4	5.3	6.0	-	05.7	87	69	84	80	34	100	C19.8	21	.	.	08	C2	.	07	13	13	12	04	10	05	01	03									
IV 5.6	6.5	6.3	6.1	-	06.6	85	60	77	74	44	039	C10.0	11	.	.	05	05	12	09	08	01	09									
V 5.7	5.6	5.8	5.7	-	10.6	90	65	84	80	31	062	C12.1	27	.	.	08	07	12	13	12	01	13	01	.											
VI 6.0	7.1	5.9	6.3	-	11.7	89	70	89	83	38	099	C27.3	25	.	.	06	06	13	11	10	03	11	03	.											
VII 4.4	3.5	4.4	4.2	-	13.7	93	63	90	82	53	216	C31.8	01	.	.	22	01	.	.	.	12	08	18	18	08	18	07	.											
VIII 5.1	5.4	6.1	5.5	-	13.5	56	69	93	86	47	191	C45.5	25	.	.	16	05	09	14	14	06	14	02	05											
IX 6.2	3.2	3.2	4.2	-	12.7	97	68	95	87	57	075	C47.8	08	.	.	08	09	C4	06	04	01	06	01	07											
X 7.5	5.1	4.9	5.8	-	07.8	96	68	95	86	38	119	C24.6	17	.	.	06	01	.	.	.	04	12	12	12	05	12	08	.											
XI 7.8	7.8	7.7	7.7	-	05.3	90	78	89	86	41	050	C12.2	14	02	.	09	04	21	07	07	01	07	03	.											
XII 6.5	6.0	5.2	5.9	-	03.9	86	75	87	83	45	044	C021.5	18	01	04	24	08	14	03	03	02	03	08	.											
GOD.	5.8	5.5	5.3	5.5	-	08.3	89	67	86	81	28	1038	C049.5	25W	04	04	97	61	01	.	02	.	89	134	114	108	33	109	09	01	.	.	.	02	17	33	11								
PURSKA SOBOTA																																													
BR. ST. 22																																													
I 7.9	6.4	4.2	6.2	-	090.8	04.8	53	72	89	25	43	011	C05.7	28	.	01	25	.	.	.	03	.	03	07	05	03	.	05	02	02	.	.	.	09	01										
II 5.4	5.1	3.8	4.8	-	144.3	03.8	82	59	85	79	34	015	C08.6	15	02	.	24	.	.	.	02	.	09	07	04	03	.	04	04	02	.	.	.	03	01										
III 7.9	7.7	6.1	7.2	-	107.1	05.5	53	63	83	79	27	064	C10.9	15	.	.	10	.	.	.	04	02	15	14	10	01	13	03	02	.	.	.	01	03											
IV 6.0	6.5	4.3	5.6	-	176.8	06.6	87	57	82	75	32	054	C23.4	17	.	.	05	.	.	.	03	07	10	05	02	10	03	.											
V 5.5	6.7	5.0	5.7	-	159.4	10.1	87	58	83	76	26	060	C10.4	13	.	.	04	.	.	.	02	.	07	08	14	11	02	14	06	03										
VI 6.4	7.7	5.5	6.3	-	161.0	11.4	84	65	86	78	42	133	C037.2	25	.	.	05	.	.	.	01	.	05	09	19	12	03	13	.	.	.	01	05	01											
VII 5.1	4.9	4.4	4.8	-	246.9	13.7	89	62	90	84	44	208	C033.2	01	.	.	22	.	.	.	06	04	14	13	07	14	.	.	.	01	07	04													
VIII 5.4	6.0	4.5	5.3	-	204.3	13.2	92	62	91	82	47	066	C022.1	25	.	.	12	.	.	.	01	03	04	16	12	02	16	10	02										
IX 6.3	4.7	2.3	4.4	-	177.0	12.5	97	65	94	86	44	032	C013.5	13	.	.	06	.	.	.	01	.	05	02	06	04	01	06	.	.	.	04	17	.											
X 7.8	5.7	4.9	6.2	-	116.9	07.6	96	70	89	87	45	091	C026.8	18	.	.	04	01	.	.	.	04	08	09	04	09	04	15	.										
XI 6.2	8.1	7.8	8.0	-	050.1	05.4	92	81	91	84	44	033	C010.4	18	02	.	09	.	.	.	02	03	20	12	06	01	12	02	02	.	.	.	04	.											
XII 6.2	6.7	6.0	7.0	-	049.7	04.2	95	82	94	90	48	038	C028.5	18	01	04	24	03	14	05	03	01	04	03	12	.										
GOD.	6.7	6.4	4.9	6.0	-	1724.3	08.2	91	66	88	82	26	805	C057.2	25.VI	05	05	103	54	.	.	19	.	53	107	130	91	24	124	16	08	.	.	01	01	33	78	03							
JERUZALEM																																													
BR. ST. 23																																													
I 6.3	5.9	5.0	5.7	-	102.5	04.8	80	69	76	75	43	014	C005.2	09	.	.	07	.	.	.	C2	.	07	11	04	03	03	04	04	01										
II 3.5	3.9	2.3	3.3	-	154.3	03.8	80	67	74	73	40	021	C011.0	15	.	.	21	.	.	.	04	.	18	05	08	03	01	03	04	.	.	.	03	05											
III 7.2	7.6	5.8	6.9	-	109.9	05.5	83	67	78	76	31	071	C017.5	21	.	.	06	.	.	.	07	.	01	19	14	11	02	14	05	01	.	.	.	01	03										
IV 5.8	6.1	4.5	5.5	-	185.2	06.1																																							

Meseč Vremenski priobrask PM MM	Temperatura vazduha °C	Čestina pravaca i srednja jačina veta nD, fm (0-12)																		
		Tm	7	14	21	Sred. (Dnev.)	W	NW	NE	E	SE	S	SW	W	NW	C				
$\varphi = 45^{\circ}51' N \lambda = 13^{\circ}40' E$ Gr. $\Delta G = +55$ min.																				
I	-04.4	07.3	05.2	05.6	08.0	03.0	12.0	05 -01.0	11 .	. .	13 04.4	. .	03 00.8	. .	04 01.2	. .	73			
II	-03.1	08.1	04.2	04.9	09.0	01.1	14.7	06 -03.4	17 02	00.5 .	40 19.0	. .	C2 00.7	. .	01 00.3	. .	39			
III	-06.2	09.3	04.7	07.3	10.3	04.3	16.4	09 -01.3	24 01	00.4 .	25 09.4	02 00.6	11 04.0	. .	01 00.2	. .	53			
IV	-09.6	13.6	09.9	10.8	14.6	07.3	16.9	24 03.6	03 01	00.4 02	20 06.5	08 02.8	15 05.8	01 00.4	04 01.4	. .	39			
V	-15.0	19.3	15.1	16.1	19.5	12.4	28.0	20 07.8	02 .	. .	01 00.4	28 09.8	11 03.8	13 04.8	04 01.6	06 02.5	. .	30		
VI	-16.7	20.6	16.8	17.8	21.6	13.8	26.5	27 06.0	05 01	00.3 01	03 02.2	22 06.6	03 01.1	06 02.2	04 01.8	09 03.1	01 00.4	43		
VII	-19.6	25.2	20.1	21.3	25.8	17.0	29.0	18.17	10.1	01 03	00.9 .	. .	23 08.1	05 01.7	09 02.9	. .	06 01.8	. .	45	
VIII	-18.0	23.4	19.0	20.1	24.3	16.5	28.0	11 12.2	26 05	C1.8 03	01.0 29	09.0	04 01.8	03 00.9	01 00.4	03 01.0	. .	43		
IX	-17.8	22.8	18.3	19.3	23.5	15.6	29.0	18 11.6	20.14	01 00.4	29 10.4	06 03.0	04 02.1	04 01.1	03 01.1	. .	38	
X	-11.0	16.2	12.0	12.8	16.5	09.5	25.0	03.01	04.2	12.11 .	. .	02 00.9	48 18.9	11 03.5	03 01.0	. .	01 00.3	. .	28	
XI	-05.9	08.7	06.6	07.0	09.6	03.9	16.5	03.02	-04.0	24 03	00.9 .	. .	41 16.5	09 03.7	04 01.4	. .	02 00.6	. .	31	
XII	-04.3	07.8	04.8	05.5	08.4	02.1	12.6	29 -03.5	21.19	01 00.2	01 00.4	31 13.0	06 01.9	04 00.9	01 00.2	49		
GOD.	-	11.0	15.2	11.6	12.4	16.0	08.4	29.0	46.1X	-04.0	24.XI	17 01.0	11 00.7	351 12.4	70 02.8	79 03.3	15 01.3	40 01.8	01 00.4	511
$\varphi = 45^{\circ}33' N \lambda = 13^{\circ}43' E$ Gr. $\Delta G = +55$ min.																				
KOPER-SENEDELA														BR. ST. 27						
I	-06.3	09.1	06.9	07.3	09.7	04.9	15.3	20 01.0	02 .	. .	04 01.1	09 02.4	15 03.1	05 01.0	03 00.5	05 01.1	12 02.9	40		
II	-04.6	09.6	06.0	06.5	10.5	03.6	14.2	02 -00.6	18 .	. .	19 07.3	21 08.1	08 01.3	02 00.4	01 00.1	06 01.3	08 02.2	19		
III	-08.3	11.2	09.0	09.4	12.7	06.4	16.9	30.19	01.5	23 .	. .	04 01.4	15 04.2	22 04.6	03 00.6	10 02.0	03 00.7	02 01.1	28	
IV	-11.3	15.9	11.9	12.7	16.7	09.0	23.2	22 05.4	12 .	. .	04 01.2	12 03.2	21 05.0	04 01.2	07 01.9	05 01.7	11 03.1	26		
V	-16.7	20.8	16.9	17.8	21.9	14.5	28.0	20 10.5	11 .	. .	05 01.5	C6 01.7	09 01.6	04 01.0	13 03.4	08 02.2	10 02.7	38		
VI	-19.1	22.4	18.6	19.7	24.1	15.5	30.0	26 10.5	04 .	. .	03 00.8	10 02.6	07 01.4	06 01.1	05 01.2	18 04.5	35			
VII	-21.4	26.3	21.0	22.9	27.3	18.4	31.7	22 13.2	01	03 01.3	05 00.7	01 00.1	. .	08 01.9	20 04.9	56		
VIII	-20.7	25.0	21.1	22.0	26.6	16.4	32.5	03 15.6	26 .	. .	06 01.5	10 02.3	10 01.5	04 01.4	20 05.0	41		
IX	-19.3	29.2	19.9	21.1	25.4	17.6	26.8	18 14.2	14 .	. .	01 00.2	08 01.3	15 02.2	02 00.9	08 01.9	08 02.1	11 02.1	37		
X	-12.5	17.8	13.4	14.3	18.7	11.2	27.5	01 07.9	11 .	. .	12 04.2	17 05.3	12 01.7	02 00.2	03 00.8	05 01.1	09 02.8	33		
XI	-08.3	12.1	08.6	09.4	13.2	06.6	20.0	02 -00.8	22 .	. .	20 07.3	17 05.5	11 01.9	. .	03 00.7	. .	09 02.0	30		
XII	-06.0	09.3	06.5	07.1	10.3	04.5	19.1	17 06.1	24 .	. .	09 03.1	14 04.4	04 00.5	. .	02 00.4	02 00.5	10 02.1	52		
GOD.	-	12.9	17.0	13.4	14.2	18.1	10.9	32.5	03.VII	-00.8	22.XI	. .	87 04.6	142 04.3	139 02.7	29 00.8	55 01.9	62 01.5	435	
$\varphi = 45^{\circ}31' N \lambda = 13^{\circ}52' E$ Gr. $\Delta G = +55$ min.																				
KUREK														BR. ST. 28						
I	-03.0	08.4	03.7	04.7	09.3	01.1	13.0	20 -03.5	10 08	C1.7 02	00.4 12	02.9	08 01.2	34 04.1	14 02.1	13 02.2	02 00.3	. .		
II	-01.6	08.8	03.0	04.1	09.1	00.9	-03.3	15 04.0	10 06	01.2 04	00.8 43	14.6	05 00.9	09 01.6	08 01.6	08 01.4	01 00.2	. .		
III	-05.4	10.3	06.2	07.1	11.9	03.7	18.0	09 -03.5	01 04	00.7 02	00.6 10	02.4	07 01.8	53 10.3	10 02.3	05 00.8	02 00.4	. .		
IV	-09.0	14.6	08.8	10.3	15.1	03.8	22.0	22.21	01.5	12 07	01.7 03	00.8 11	03.2	08 01.6	39 07.9	04 01.1	16 02.1	02 00.6	. .	
V	-14.9	20.6	14.3	16.1	21.4	11.4	29.5	21 05.6	01 04	01.0 02	00.7 06	01.9	07 01.4	39 04.2	18 03.3	15 03.0	02 00.5	. .		
VI	-17.0	21.2	16.1	17.6	23.4	13.0	29.5	26 05.5	05 04	01.0 .	. .	15 03.5	05 01.2	40 07.0	14 02.6	10 01.9	06 00.4	. .		
VII	-19.0	26.0	18.0	20.3	27.1	14.9	31.5	18 16.0	01 05	01.2 02	00.6 12	03.2	14 02.3	18 02.6	05 00.5	27 04.2	10 02.2	. .		
VIII	-18.4	24.4	18.3	19.9	25.9	13.1	30.0	15.03	12.0	20 06	01.7 04	01.1 17	05.2	10 02.5	39 05.3	04 00.7	12 02.5	01 00.2	. .	
IX	-15.6	24.2	16.6	18.3	25.6	14.2	31.5	18 10.0	29 06	01.4 02	00.5 04	C4 01.2	05 00.9	50 08.1	07 01.4	15 02.2	01 00.1	. .		
X	-08.9	17.7	11.0	12.2	18.9	08.1	26.0	03.01	02.0	31 06	01.3 01	00.2 31	10.0	08 01.7	16 03.0	17 02.4	10 01.8	04 00.8	. .	
XI	-05.5	10.7	06.4	07.3	11.1	02.9	19.0	03.02	-04.0	25 05	01.0 08	01.9 15	04.6	04 01.4	48 09.9	06 01.3	01 00.1	01 00.2	. .	
XII	-01.9	08.5	03.5	04.4	09.6	00.5	13.2	29 -06.1	23 08	02.0 02	00.4 15	04.2 04	04 00.8	31 05.7	11 01.6	18 02.0	04 00.7	01 00.1	. .	
GOD.	-	10.0	16.3	10.9	17.4	07.5	31.3	46.1X	-06.0	25.XI	69 01.4	32 01.0	151 07.1	87 C1.6	416 07.1	118 02.1	150 02.6	32 01.0	. .	
$\varphi = 45^{\circ}53' N \lambda = 13^{\circ}54' E$ Gr. $\Delta G = +54$ min.															AJDCVSCINA					
KOPER-SENEDELA														BR. ST. 29						
I	756.5	02.6	08.9	04.2	05.0	05.6	01.1	13.5	31 -06.6	14 01	00.1 08	02.9	05 01.4	02 00.6	* * .	03 00.4	08 01.3	04 00.6	42	
II	757.2	02.8	09.1	04.4	05.2	09.7	00.9	17.4	19 -07.0	20 02	00.5 21	10.0	09 04.1	16 06.7	07 02.0	01 00.2	04 01.0	. .	24	
III	747.0	06.3	10.8	06.8	07.7	12.0	04.1	18.6	09 -06.0	01 01	00.1 20	06.0	07 02.0	08 02.0	03 00.9	04 00.8	06 00.6	05 00.8	41	
IV	750.7	10.4	15.4	09.6	11.4	16.7	04.7	23.0	03 00.4	03 05	00.9 18	07.0	03 01.2	09 02.3	02 00.6	06 01.8	04 00.6	35		
V	749.9	16.3	21.2	15.2	17.0	22.2	11.8	30.4	19 04.9	01 06	01.0 14	05.6	C8 02.3	02 00.6	03 00.4	04 00.7	14 03.1	07 01.2	35	
VI	750.4	17.5	22.0	17.2	18.5	23.3	13.3	28.8	27 04.8	05 03	00.7 16	06.6	11 02.3	03 00.6	02 00.4	02 00.3	06 01.1	04 00.7	43	
VII	750.7	20.5	26.8	20.1	21.9	27.6														

Mesec	Vrednost pritisak Pa	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, fm (0-12)																			
		Tm				Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW					
		7	14	21	Sred. (Dnev.)							E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.						
$\varphi = 45^{\circ}34' N \lambda = 14^{\circ}15' E$ Gr. $\Delta G = +57$ min.																															
ILIRSKA BISTRICA BR. ST. 31																															
I	-	01.1	08.3	03.2	03.9	08.7	06.1	12.2	31	-06.8	10	17	04.2	0	0	09	01.9	05	02.1	28	07.2	02	00.4	02	00.3	.	.	30			
II	-	-01.0	07.4	01.8	02.5	03.3	-02.3	14.7	19	-09.6	18	34	14.7	01	00.2	01	01.9	04	01.3	10	02.8	28			
III	-	03.7	08.7	05.2	05.7	05.7	02.1	16.9	09	-06.0	01	16	04.9	01	00.2	10	02.2	06	04.2	19	06.9	02	00.7	04	00.7	01	00.1	31			
IV	-	05.8	13.3	08.5	09.0	14.5	04.2	21.3	21	-00.7	12,02	27	07.1	01	00.1	08	03.4	04	01.6	26	09.6	02	01.2	22			
V	-	11.0	18.8	13.5	14.2	20.2	05.2	27.4	18	03.1	03	13	04.1	01	00.1	02	00.4	01	00.2	22	04.4	02	00.7	03	00.8	02	00.6	47			
VI	-	13.6	16.8	15.3	16.0	21.5	11.4	28.2	27	04.9	07	27	07.6	.	.	03	01.0	06	02.1	12	03.3	03	00.9	02	00.2	05	01.5	32			
VII	-	14.4	24.8	17.8	18.8	25.5	12.9	29.5	15	04.6	27	34	10.7	03	00.4	03	00.8	.	06	01.9	02	00.4	02	00.6	02	00.3	41				
VIII	-	14.4	22.5	17.0	17.7	23.9	13.1	27.7	02	07.6	20	25	07.6	03	01.4	05	01.2	03	00.8	07	02.3	01	00.4	02	00.6	03	00.8	44			
IX	-	12.2	22.8	15.2	16.4	23.6	11.7	31.7	17	04.5	21	07	01.4	01	00.1	05	01.4	01	00.3	19	04.4	05	01.0	02	00.5	.	.	50			
X	-	04.8	16.5	08.1	09.4	17.3	04.2	25.9	03	-02.7	30	23	07.1	06	01.7	04	01.1	04	00.9	08	01.9	02	00.6	01	00.1	01	00.4	44			
XI	-	02.2	08.4	03.6	04.5	05.3	00.4	16.9	04	-11.0	25	26	07.5	03	01.0	06	00.9	03	01.0	12	04.0	01	00.2	02	00.4	04	01.0	33			
XII	-	-00.8	07.1	01.4	02.3	08.1	-01.7	13.4	20	-07.5	22	15	04.0	01	00.2	.	.	04	01.1	11	02.1	02	00.3	02	00.5	03	00.7	55			
GOD.	-	06.8	14.9	09.2	10.0	19.6	05.4	31.7	17.IX	-11.0	25.XI	264	07.9	21	00.9	62	01.8	44	02.0	180	05.5	24	00.7	22	00.5	21	00.9	487			
$\varphi = 45^{\circ}38' N \lambda = 14^{\circ}22' E$ Gr. $\Delta G = +57$ min.																															
MASUN BR. ST. 32																															
I	-	-00.4	03.5	00.0	00.8	04.1	-02.2	05.8	04	-04.4	09	.	.	13	01.7	11	01.9	C1	00.2	01	00.1	41	08.9	02	00.2	23	03.0	01			
II	-	-04.4	01.2	-03.1	-02.4	01.8	-05.5	09.8	19	-11.6	18	.	.	22	04.0	27	06.5	12	02.8	.	.	09	01.6	06	01.1	08	01.2	.			
III	-	00.3	03.5	00.8	01.4	04.7	-01.4	12.3	09	-06.3	01	.	.	11	02.4	14	02.2	03	00.4	36	06.0	08	01.2	08	01.2	13					
IV	-	03.3	08.1	03.4	04.5	09.3	00.6	16.7	21	-04.1	12	02	00.4	13	01.6	18	02.8	06	01.0	.	16	03.6	12	03.1	13	02.1	08				
V	-	09.3	13.9	09.1	10.3	14.7	05.8	22.1	20	-06.7	03	.	.	04	00.5	30	04.1	04	00.4	03	00.3	21	03.0	19	02.1	11	01.6	10			
VI	-	11.2	14.8	10.9	11.8	16.4	07.4	23.5	27	-01.4	05	.	.	06	00.9	18	03.4	23	02.7	01	00.1	11	02.0	18	02.9	05	00.8	08			
VII	-	13.0	19.5	13.0	14.7	20.4	05.2	25.8	15	04.5	01	03	00.3	14	02.4	22	03.3	08	01.0	.	08	01.4	11	01.4	19	02.5	08				
VIII	-	12.1	17.5	12.7	13.7	16.4	05.1	22.9	10	04.1	20	06	00.6	20	02.7	17	03.5	20	03.5	01	00.2	04	00.4	13	01.6	10	01.0	02			
IX	-	11.4	17.4	11.7	13.1	16.6	04.5	28.9	17	04.5	14	.	.	06	00.6	19	02.9	13	02.1	01	00.3	22	04.9	21	03.1	06	00.7	02			
X	-	03.0	10.5	04.2	05.5	11.1	01.7	20.4	03	-02.9	31	02	00.2	20	03.0	21	03.5	23	04.3	.	06	01.3	03	00.4	18	02.5	.				
XI	-	00.2	02.7	00.9	01.0	03.4	-01.8	13.5	03	-10.6	25	03	00.4	18	04.1	16	03.4	21	02.7	01	00.3	25	05.0	01	00.1	05	00.3	.			
XII	-	-02.2	03.4	-01.4	-00.4	04.7	-04.3	11.8	29	-11.0	20	.	.	10	01.8	32	05.9	13	01.4	03	00.6	09	01.4	04	00.6	22	02.8	.			
GOD.	-	04.7	09.7	05.1	06.2	10.7	02.3	28.9	17.IX	-11.4	18.II	14	00.4	146	02.4	242	03.9	160	02.6	14	00.4	208	03.0	109	02.1	148	02.1	52			
$\varphi = 45^{\circ}53' N \lambda = 14^{\circ}26' E$ Gr. $\Delta G = +58$ min.																															
RAKITNA BR. ST. 33																															
I	-	00.9	04.5	01.7	02.2	05.5	-01.2	10.6	06	-10.6	09	13	03.4	07	01.6	04	01.0	06	01.4	16	03.7	02	00.5	12	02.9	32	10.3	01			
II	-	-03.6	02.3	-02.6	-01.6	03.4	-05.6	10.9	07	-18.4	18	05	00.9	12	03.0	24	07.2	13	04.2	07	01.3	06	01.1	05	00.8	02	03.1	.			
III	-	01.3	04.8	02.1	02.6	06.0	-00.5	12.8	09	-05.5	01	.	01	00.1	07	01.1	08	02.5	15	03.6	18	03.1	06	01.5	10	01.0	23	06.3	01		
IV	-	04.8	09.8	05.4	06.3	11.3	01.9	16.0	30	-03.9	26	10	01.9	15	04.0	06	02.5	22	04.8	14	03.7	02	00.7	11	02.6	01					
V	-	10.7	15.5	11.0	12.1	16.6	04.6	24.4	19	-03.1	02	07	01.5	15	03.0	04	00.6	07	01.6	21	04.0	07	01.6	15	02.7	17	03.9	.			
VI	-	12.5	16.5	13.6	13.1	17.3	08.1	24.6	14	-01.0	05	14	02.0	13	02.6	14	03.1	09	01.9	14	02.3	08	01.5	12	01.7	04	01.1	.			
VII	-	14.0	20.7	14.5	16.2	22.0	05.5	27.4	15	03.6	27	17	02.9	12	02.8	12	02.1	07	01.6	10	01.										

Mjesec	Vazdušni pritisak Pa	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, Fm (0-12)																	
		Tm	7	14	21	Sred. (Dnev.)	Min	Max	Prec.	Min	Prec.	N	NE	E	SE	S	SW	W	NW	C									
												E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.					
$\varphi = 45^{\circ}38' N \lambda = 14^{\circ}52' E$ Gr. $\Delta G = + 59$ min.																													
I	-	00.1	07.0	01.4	02.6	07.9	-01.2	10.9	31 -07.5	11	04	00.8	25	04.6	27	07.2	02	00.5	28	06.0	07			
II	-	-03.5	05.0	-00.7	00.0	05.6	-04.5	13.1	28 -13.3	18	04	01.1	16	02.9	44	09.6	14	03.4	06			
III	-	02.4	08.0	04.5	04.9	04.9	01.1	16.5	09 -04.5	01	08	02.3	12	02.2	17	04.3	04	01.4	.	.	02	00.9	.	.	36	06.7	14		
IV	-	05.4	13.0	07.9	08.5	13.9	02.6	23.0	30 -01.9	27	.	.	28	06.2	12	04.6	06	02.7	.	.	04	01.4	.	.	30	07.3	10		
V	-	11.0	18.6	13.5	14.2	13.9	08.7	20.0	20,18	06.1	03	02	00.7	24	05.1	06	02.0	02	00.8	.	.	01	00.2	.	.	45	09.6	13	
VI	-	12.6	18.8	14.1	14.9	20.1	10.1	28.2	14	00.4	05	02	00.6	27	04.9	11	02.7	03	00.7	36	08.4	11		
VII	-	14.7	23.6	16.8	18.0	24.6	12.2	32.5	15	06.0	27	05	01.2	29	06.2	17	04.5	01	00.3	26	05.4	15		
VIII	-	13.7	22.1	16.1	17.0	23.0	12.2	27.6	02	07.4	22,21	.	.	19	03.1	04	00.9	04	01.0	44	09.5	20		
IX	-	12.7	22.1	14.5	15.9	22.7	11.3	28.8	17	08.0	16	.	.	13	02.9	16	04.1	07	02.1	.	.	01	00.2	02	00.5	31	07.0	20	
X	-	04.9	13.7	06.6	07.9	14.3	04.6	24.8	01 -02.9	27	06	01.7	38	08.3	11	03.4	.	.	02	00.5	04	00.9	.	.	16	03.0	16		
XI	-	01.5	05.8	02.7	03.2	06.5	00.4	18.0	02 -13.3	25	20	05.5	29	04.9	22	05.5	02	00.6	.	.	01	00.2	.	.	06	01.4	10		
XII	-	-02.5	03.0	-01.1	-00.4	04.2	-03.3	10.1	06 -12.1	20	14	02.8	16	02.6	34	08.0	09	01.0	13	02.8	11			
600.	-	06.1	13.4	08.0	08.9	14.3	04.5	32.5	45.VII -13.3	25.XI	65	03.0	276	05.0	221	06.2	36	01.4	02	00.5	13	00.8	02	00.5	327	07.0	133		
$\varphi = 45^{\circ}48' N \lambda = 15^{\circ}11' E$ Gr. $\Delta G = 1$ h 01 min.																													
NOVO MESTO-GOTVANA VAS																													
BR. ST.36																													
I	747.5	01.0	08.2	03.1	03.9	08.9	00.0	13.4	19 -05.6	04	.	.	06	00.8	04	01.0	07	00.9	20	02.7	23	04.2	21	03.6	05	01.1	07		
II	758.0	-02.5	05.5	06.8	01.1	01.5	03.0	13.6	28 -09.6	18	03	00.9	15	04.5	13	03.2	07	01.2	13	01.4	15	02.4	09	01.6	03	00.9	06		
III	758.5	02.8	09.5	05.9	06.0	11.0	01.9	15.4	09 -04.7	23	02	00.3	07	01.4	10	02.6	03	00.5	11	01.7	24	04.7	17	03.3	09	01.9	10		
IV	742.3	05.9	14.2	09.4	09.8	15.4	03.7	23.1	30 -01.1	27	02	00.4	13	03.8	10	02.2	02	00.2	15	03.2	22	03.5	17	03.3	04	01.0	05		
V	741.9	12.5	19.6	14.8	15.5	20.8	10.2	27.6	18	02.4	03	01	00.1	17	03.3	13	02.7	07	01.5	09	01.4	20	03.3	12	02.2	10	01.8	04	
VI	742.7	13.8	19.8	15.7	16.3	21.3	11.5	29.2	19	03.1	05	02	00.6	10	02.1	12	02.9	06	01.2	17	02.3	14	02.0	18	02.4	05	00.8	04	
VII	743.0	16.1	23.8	18.6	19.3	23.5	13.8	31.2	19	09.2	27	02	00.4	08	01.7	10	02.9	09	01.4	18	02.8	12	01.6	16	02.1	06	01.0	07	
VIII	744.0	15.2	22.0	17.3	17.9	23.6	13.9	27.7	19	10.1	22	05	00.8	10	01.5	14	02.5	03	00.5	23	02.7	12	01.4	19	02.7	04	01.1	03	
IX	746.0	13.6	22.2	16.2	17.1	23.2	12.7	28.4	17	08.8	14	07	01.1	10	01.9	12	02.1	03	00.3	17	02.4	11	01.4	27	03.7	02	00.4	01	
X	746.9	04.5	14.0	06.2	09.2	14.8	05.8	26.0	01 00.1	31.30	05	00.6	11	01.8	23	04.2	03	00.3	18	02.5	09	01.2	19	02.5	04	00.4	01		
XI	745.5	02.1	05.9	03.1	03.6	06.4	01.4	11.8	19 -18.8	25	08	01.3	15	02.9	28	05.1	01	00.1	18	02.7	07	01.1	07	01.6	06	00.6	01		
XII	-	01.2	03.7	00.6	06.9	04.4	-02.2	11.2	08 -10.4	20	02	00.2	11	01.3	40	06.4	08	01.1	16	02.8	05	00.6	06	00.9	03	00.5	02		
600.	-	07.5	14.7	10.2	10.6	15.8	06.1	31.0	45.VII -11.3	26.25	XI	108	02.2	121	02.0	95	01.7	45	01.1	50	01.0	143	04.7	58	01.1	14	00.4	441	
$\varphi = 45^{\circ}34' N \lambda = 15^{\circ}12' E$ Gr. $\Delta G = 1$ h 01 min.																													
GORNJI LENART																													
BR. ST.38																													
I	-	02.1	08.5	04.8	05.1	09.3	01.1	15.8	06 -07.5	10	07	01.1	11	01.7	05	00.9	.	.	06	01.0	29	07.3	05	01.2	01	00.2	29		
II	-	-02.2	06.6	01.4	01.7	07.0	-02.9	15.0	28 -09.5	18	18	05.0	12	02.2	05	01.0	03	00.5	02	00.3	22	04.1	04	00.4	.	.	18		
III	-	03.9	10.3	06.8	06.9	11.8	02.6	16.5	06 -04.6	01	08	01.9	06	01.2	01	00.1	05	00.8	04	00.6	23	04.6	10	01.9	.	.	36		
IV	-	08.1	14.8	09.9	10.2	15.8	04.5	24.0	30 -00.8	26	06	01.2	10	02.3	06	01.2	07	01.8	21	04.6	02	00.5	02	00.5	35				
V	-	12.6	20.6	15.7	16.1	21.9	10.8	28.5	20	03.4	03	03	00.5	06	01.2	12	02.3	03	00.6	08	01.5	07	02.5	03	00.5	02	00.3	49	
VI	-	14.3	20.3	16.4	16.9	22.2	11.5	30.0	15	04.1	07	06	02	00.2	19	03.2	.	.	08	01.2	01	00.1	23	02.9	08	01.1	10	01.3	51
VII	-	16.1	24.7	19.0	19.7	25.6	14.1	31.0	15	08.6	26	07	01	03	08	01.5	10	02.1	12	02.0	06	00.7	07	01.3	03	00.6	38		
VIII	-	15.2	23.3	17.8	18.6	24.5	14.0	28.0	10	08.8	22	06	01.2	05	01.0	09	01.7	03	00.6	03	00.6	09	01.6	03	00.6	32			
IX	-	13.3	22.9	17.1	17.6	23.9																							

Mesec	Oblačnost Nm (0-10)				Insektacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sata:																								
	7	14	21	Sred. (bles.)		mm	7	14	21	Sred.	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	~	Δ	▲	□	T	≡	■				
						mm	mm	mm	mm	mm	mm	30.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.020.0	9	Δ	~	Δ	▲	□	T	≡	■							
KCCCEVJE																																				
BR. ST. 36																																				
I	6.4	5.3	4.4	5.4	-	04.7	52	68	90	83	48	039	011.2	28	.	20	.	.	.	05	07	06	05	01	06	02	.	.	.	06	01					
II	4.4	5.1	4.3	4.6	-	03.9	91	66	92	83	30	028	006.2	20	03	.	23	.	.	.	12	08	10	08	.	05	10	02	.	.	02	04	12			
III	7.7	7.6	7.1	7.6	-	05.5	94	71	90	85	27	224	043.9	30	.	09	.	.	.	02	04	19	22	15	05	21	05	01	.	.	02	04	04			
IV	5.6	6.8	4.5	5.8	-	05.8	83	55	74	71	32	092	019.0	17	.	07	.	.	.	05	07	04	14	12	03	16	01	03	.			
V	6.4	7.1	5.7	6.4	-	09.1	87	60	77	75	25	128	020.1	13	.	.	04	.	.	02	03	13	18	13	06	18	.	.	.	01	07	03	.			
VI	7.1	7.1	6.0	6.8	-	10.5	91	68	86	82	37	142	035.4	02	.	.	05	.	.	02	01	12	17	14	05	17	.	.	.	02	05	03	.			
VII	5.5	5.2	4.0	4.9	-	12.4	93	60	87	80	42	211	054.2	01	.	.	21	02	.	.	07	04	14	13	07	16	.	.	.	01	11	07	.			
VIII	7.8	6.1	5.5	6.5	-	11.7	96	62	87	81	36	130	042.9	25	.	.	11	.	.	.	02	11	18	14	04	18	.	.	.	04	07	.				
IX	8.6	5.2	3.2	5.7	-	11.2	95	61	89	82	28	066	015.9	04	.	.	04	.	.	02	04	13	07	02	13	.	.	.	03	18	.					
X	8.2	5.6	4.0	5.9	-	06.9	94	65	92	84	33	136	054.6	17	.	.	06	.	.	03	12	13	09	04	13	01	.	.	.	01	13	01				
XI	8.3	7.4	6.9	7.5	-	05.2	92	76	91	87	41	085	023.3	18	02	.	05	.	.	03	19	15	12	03	15	02	02	.	.	01	.	09	.			
XII	7.3	5.4	5.3	6.0	-	04.0	91	79	92	87	49	064	031.8	02	01	03	25	.	.	07	14	09	09	02	08	03	.	.	.	01	10	02				
GOD.	6.9	6.2	5.1	6.1	-	07.6	91	65	87	81	25	1345	054.6	72x	06	03	99	48	02	.	11	.	56	134	173	135	42	166	23	05	.	02	01	34	85	26
NOVO MESTO-GOTNA VAS																																				
BR. ST. 37																																				
I	6.4	6.0	5.3	5.9	119.5	04.9	94	62	88	81	36	018	008.0	29	.	01	15	.	.	01	03	00	04	03	04	07	.					
II	4.8	5.1	3.9	4.6	146.8	03.7	92	57	78	75	20	014	003.5	03	.	.	22	.	.	03	01	11	07	06	04	06	03	.	.	02	03					
III	8.1	7.6	5.4	7.0	109.0	05.6	93	64	81	80	23	094	027.7	30	.	.	10	.	.	03	01	02	11	18	13	03	17	05	04	.	03	08	03			
IV	6.0	7.1	4.7	5.9	188.6	06.1	89	49	72	70	31	094	017.8	11	.	.	02	.	.	03	01	04	08	11	07	02	11	.	.	.	01	03	.			
V	6.4	6.7	5.9	6.4	202.3	10.0	88	60	81	77	30	118	018.2	24	.	.	04	.	.	03	10	15	14	06	15	.	.	.	01	09	05					
VI	7.6	7.5	6.7	7.3	145.3	11.1	91	62	86	80	34	095	024.1	02	.	.	07	.	.	01	02	17	19	15	02	19	.	.	.	10	05	.				
VII	5.2	4.7	5.5	5.1	270.6	13.2	90	60	88	79	42	264	047.6	10	.	.	22	02	.	01	07	07	15	14	09	15	.	.	02	11	03	.				
VIII	7.0	6.3	6.5	6.6	186.0	13.2	97	69	92	86	44	127	030.1	25	.	.	11	.	.	03	02	11	17	12	04	17	.	.	.	10	10	.				
IX	8.4	5.2	3.2	5.6	172.9	12.7	98	67	95	86	50	035	020.3	12	.	.	07	.	.	01	02	04	07	06	01	06	.	.	.	03	19	.				
X	8.0	6.0	5.1	6.3	126.9	07.9	98	70	97	88	39	106	038.8	13	.	.	01	.	.	04	13	11	07	04	10	.	.	.	01	18	.					
XI	8.2	7.9	7.7	8.0	050.1	05.5	95	86	92	90	29	054	018.6	11	02	.	09	.	.	01	02	20	16	10	01	14	.	.	.	01	08	.				
XII	8.7	6.4	6.4	7.2	082.2	04.3	95	80	95	90	48	048	023.2	02	01	05	23	.	.	03	14	12	06	02	11	02	.	.	.	07	02	.				
GOD.	7.1	6.4	5.5	6.3	1800.2	08.2	93	65	87	81	20	1027	047.6	40W	03	06	81	52	02	.	17	04	45	133	152	113	34	145	13	07	.	01	03	49	95	08
CRNCMELJ																																				
BR. ST. 38																																				
I	6.3	6.3	5.9	6.2	-	05.3	89	68	83	80	46	024	017.1	29	.	01	13	.	.	01	05	11	07	04	01	07	01	01	.	.	.	09	.			
II	6.0	5.1	4.2	5.1	-	04.0	89	63	81	78	25	043	016.1	19	.	.	20	.	.	01	08	07	11	09	01	08	08	01	02	.	04	03	.			
III	8.0	8.2	6.8	7.7	-	05.8	89	67	79	78	34	112	030.7	30	.	.	06	.	.	01	02	16	18	14	03	17	04	02	01	.	01	07	01			
IV	5.8	6.4	5.7	6.0	-	36.3	85	53	72	70	28	070	023.2	11	.	.	01	.	.	04	10	16	10	02	16	.	.	.	01	07	.					
V	5.6	6.3	6.4	6.1	-	10.2	88	56	78	75	30	152	037.6	24	.	.	07	.	.	06	11	14	11	06	16	.	.	.	04	03	.					
VI	7.0	7.2	6.5	6.9	-	11.7	90	68	84	81	36	138	021.4	02	.	.	07	.	.	01	04	15	17	14	07	17	.	.	.	01	08	01				
VII	3.7	5.0	4.4	4.4	-	13.7	91	62	85																											

Meseč Broj	Vrednost Pritisak Pa MM	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pa (0-12)																		
		Tm				Srednji (Dnevni)						N				NE		E		SE		S		SW		W		NW		C
		7	14	21		Mj	Mj	Mj	Mj	Mj	Mj	D	D	D	D	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	
$\varphi = 46^{\circ}18' N$ $\lambda = 16^{\circ}23' E$ Gr. $\Delta G = + 1h 05 min.$																														
VARAŽDIN																														
I	751.4	01.8	08.2	03.6	04.3	08.8	00.5	14.4	19.0	-04.2	04	06	01.5	05	02.6	05	01.6	04	01.5	18	02.5	27	02.9	22	02.2	05	01.6	01		
II	754.5	-01.9	05.5	00.8	01.3	06.4	-02.9	13.0	12	-08.8	18	18	02.8	12	03.3	04	02.0	02	01.5	10	02.1	12	02.2	20	01.8	03	01.7	01		
III	743.1	03.1	10.7	04.2	06.6	12.0	02.0	17.3	09.0	-04.0	01	17	02.2	07	02.1	07	02.1	.	.	12	02.2	19	03.0	19	02.7	03	01.8	01		
IV	746.8	07.3	14.4	09.4	10.1	15.4	04.3	22.3	30	-00.4	20	20	02.2	08	02.6	10	01.9	03	01.0	04	03.0	20	02.6	11	02.0	12	01.8	01		
V	746.3	13.7	20.5	15.0	16.1	21.7	09.8	28.4	18	05.9	03	18	02.4	14	02.4	09	01.7	02	01.5	06	02.2	08	02.0	21	02.0	10	02.6	01		
VI	747.1	15.9	20.3	16.1	17.0	21.9	12.2	29.7	23.15	06.0	05	20	02.2	09	01.4	02	01.5	09	01.9	09	02.2	15	01.9	11	01.9	06	.	.		
VII	747.3	17.5	24.6	18.8	19.9	25.6	14.1	30.3	15	07.9	27	11	02.6	05	02.2	07	02.0	02	01.0	10	01.8	12	01.6	17	01.6	17	01.8	12	.	
VIII	748.4	16.7	23.4	17.4	18.7	24.3	14.0	28.4	11	09.8	21	19	01.8	12	02.1	08	01.9	06	01.9	03	02.0	22	01.6	13	01.5	06	.	.		
IX	750.4	14.2	23.1	17.6	17.3	23.8	12.1	28.4	17	06.4	14	04	01.5	08	01.8	12	01.6	03	01.0	14	02.3	06	02.8	15	01.5	04	01.6	02	.	
X	751.5	06.7	14.3	08.6	09.6	14.8	05.4	25.4	01	-00.6	29	11	01.9	12	02.4	09	01.7	04	01.7	05	02.6	13	01.5	16	01.5	07	01.3	14	.	
XI	750.2	02.5	06.2	03.8	04.1	06.9	01.7	12.3	02	-04.6	26.25	20	02.4	10	02.2	17	02.1	.	.	21	02.1	06	02.3	06	01.2	03	01.7	07	01	
XII	753.3	-01.3	02.9	-00.1	00.3	03.5	-02.3	09.0	08	-09.6	20	12	01.6	04	02.8	15	01.7	04	01.5	16	02.0	11	02.1	14	01.7	07	01.7	10	.	
GOD.	749.2	08.0	14.5	09.6	10.4	15.4	05.9	30.3	15.74	-09.6	20XII	176	02.2	106	02.4	112	01.8	30	01.4	133	02.2	146	02.4	198	01.9	99	01.7	97	.	
$\varphi = 46^{\circ}02' N$ $\lambda = 16^{\circ}33' E$ Gr. $\Delta G = + 1h 07 min.$																														
KRIEVCI																														
I	753.1	01.2	07.1	03.0	03.6	07.8	-00.4	13.0	18.17	-05.8	11	08	02.2	12	02.8	04	02.0	03	02.3	16	02.2	32	02.9	08	02.8	10	01.9	.		
II	755.8	-01.4	05.2	01.2	01.6	06.0	-02.3	12.5	13.12	-09.3	18	15	03.2	30	03.0	02	02.5	02	02.5	06	02.3	16	02.8	05	02.4	08	01.9	.		
III	744.3	03.5	10.9	07.2	07.2	12.4	02.2	18.0	09	-04.5	01	13	02.9	22	02.9	07	02.4	08	02.0	07	02.4	24	03.2	03	02.7	09	02.3	.		
IV	748.0	07.4	14.4	09.6	10.2	15.4	05.0	22.2	30	01.0	29.12	24	03.3	18	03.1	04	02.8	03	02.0	06	02.5	21	03.2	02	03.5	12	02.2	.		
V	747.3	13.7	20.6	15.3	16.3	21.7	10.4	27.5	19.18	04.2	10	22	03.0	31	03.1	02	02.5	06	02.0	04	02.0	16	03.2	01	02.8	11	02.5	.		
VI	748.1	15.5	20.2	16.2	17.0	22.0	12.5	29.2	23	07.5	02	26	03.7	20	03.0	02	01.5	07	02.1	07	02.3	08	02.6	03	02.7	17	02.6	.		
VII	748.3	17.6	24.4	18.8	19.9	25.4	14.1	29.5	18.15	06.0	27	20	03.1	17	02.8	05	02.6	06	02.3	16	02.4	03	02.7	21	02.5	.	.			
VIII	749.4	16.9	23.7	17.4	18.9	24.5	14.1	29.0	11	10.0	21	20	02.8	32	03.1	02	02.0	03	03.0	03	02.3	10	02.3	03	02.0	20	02.2	.		
IX	751.6	14.2	23.2	16.6	17.6	23.9	12.3	28.5	17	06.3	14	10	02.6	22	02.4	08	02.6	04	02.2	11	02.3	17	02.7	02	03.5	16	01.9	.		
X	752.8	07.3	13.3	08.4	09.4	14.2	05.6	24.8	01	-00.5	26	13	02.8	29	02.9	08	02.4	09	02.0	12	02.0	10	02.1	01	02.0	12	02.0	.		
XI	751.5	02.2	06.0	03.5	03.8	06.7	01.3	12.5	02	-10.0	26	18	03.2	31	02.6	09	02.0	06	01.8	09	02.7	01	02.0	07	02.0	.	.			
XII	754.7	-01.0	02.4	-00.1	00.3	03.1	-02.2	07.2	04	-09.5	20	13	02.4	26	02.3	02	03.0	07	02.1	14	02.2	03	02.3	08	02.1	.	.			
GOD.	750.4	08.1	14.3	09.8	10.5	15.3	06.0	25.5	16.45	YH -10.0	26.XI	202	03.0	290	02.8	59	02.3	65	02.2	100	02.2	167	02.8	35	02.6	151	02.2	.		
$\varphi = 46^{\circ}11' N$ $\lambda = 16^{\circ}49' E$ Gr. $\Delta G = + 1h 07 min.$																														
Koprivnica																														
I	-	02.4	17.7	03.9	04.3	08.2	01.3	12.6	18	-03.8	05	05	01.0	10	01.6	.	.	05	01.6	13	01.8	33	02.8	03	01.0	04	01.2	.		
II	-	-01.4	05.7	01.1	01.7	06.3	-01.7	13.2	12	-08.0	18	08	02.6	21	01.7	02	01.8	04	01.8	15	01.7	20	01.8	04	01.3	10	01.5	.		
III	-	04.1	11.4	07.1	07.4	12.7	03.2	16.0	09	-03.3	01	23	01.3	16	02.0	03	01.7	07	01.3	13	02.2	03	01.7	21	01.3	.	.			
IV	-	07.5	15.2	09.3	10.3	16.1	05.4	23.4	30	01.5	20	15	02.2	16	01.7	03	01.3	07	01.3	17	02.0	22	01.8	09	01.2	11	01.2	.		
V	-	13.9	21.6	19.4	16.6	22.6	11.3	25.4	18	07.0	01	12	02.2	23	01.9	03	01.7	08	01.2	02	02.0	25	02.0	05	01.2	19	01.3	.		
VI	-	15.6</																												

Mesec	Oblačnost Nm (0-10)				Indikacijski broj	Vlažnost vazduha				Padavine R mm		Broj dana na sat																							
	7	14	21	Sred. (Dnev.)		U	m	%	Padavine R mm		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡						
						mm	7	14	21	Sred.	Min	Max	Dat.	=	>	≤	<	≥	≤	<	>	≥	≤	≥	≤	≥	≤								
VARAŽDIN																																			
BR. ST. 41																																			
I	6.3	5.6	4.5	5.5	115.1	05.0	87	67	82	79	45	014	005.2	09	.	.	14	.	.	08	.	04	07	05	04	.	04	02	01	.	01	.	07	01	
II	4.2	4.8	4.0	4.3	162.5	03.8	86	60	79	75	33	015	008.5	15	.	.	23	.	.	08	01	11	07	08	04	.	04	06	02	.	.	04	03		
III	7.7	8.0	6.1	7.3	116.9	05.5	88	61	79	76	27	051	011.9	29	.	.	08	.	.	09	01	01	13	13	10	01	12	03	01	.	.	01	07	02	
IV	6.0	5.9	5.3	5.7	194.3	04.3	80	52	72	68	29	040	017.2	11	.	.	01	.	.	12	01	04	10	11	05	02	11	
V	5.2	6.5	5.9	5.9	211.1	09.9	80	56	78	72	28	091	031.8	28	.	.	08	.	.	05	01	05	13	14	10	03	14	07	01	
VI	6.9	7.3	6.1	6.8	183.5	11.4	82	64	82	76	40	103	032.9	25	.	.	09	.	.	07	01	04	14	17	12	02	17	.	.	.	09	02	.		
VII	4.5	4.7	4.2	4.5	270.0	13.7	87	59	87	77	41	150	043.6	02	.	.	24	01	.	04	.	07	05	17	12	05	17	14	02	
VIII	4.8	6.4	5.1	5.4	217.6	13.2	89	62	90	80	40	106	028.1	13	.	.	14	.	.	01	.	06	07	16	11	05	16	10	01	
IX	4.5	4.3	2.5	3.8	206.0	12.5	95	64	92	83	49	053	014.3	13	.	.	09	.	.	01	01	10	03	08	07	02	08	05	16	
X	7.0	6.2	4.7	6.0	127.5	07.8	95	68	82	85	38	092	026.1	14	.	.	02	01	.	01	07	12	13	08	04	12	04	14		
XI	7.7	7.6	7.6	7.7	053.7	05.4	90	77	85	84	35	034	010.9	19	.	.	08	.	.	05	01	03	19	12	05	02	12	01	01	.	.	.	04	.	
XII	7.8	7.3	6.7	7.3	061.0	04.2	93	80	90	88	52	036	028.0	18	.	03	26	.	.	01	.	02	17	07	03	01	04	01	.	.	01	.	.	11	.
GOD. 6.0 6.2 5.2 5.8 1919.2 08.2 88 64 84 78 27 785 043.6																													50 69 06						
KRIZEVCI																																			
BR. ST. 42																																			
I	2.5	3.1	1.2	2.3	096.9	04.9	89	70	85	82	34	018	007.4	29	.	01	17	.	.	03	.	13	.	09	03	.	05	01	01	.	.	.	06	.	
II	4.6	5.5	4.7	5.0	147.1	03.9	86	61	77	75	31	010	004.9	15	.	.	20	.	.	05	.	07	06	05	04	.	04	01	.	.	.	03	.		
III	7.3	6.9	7.0	7.1	112.3	05.7	89	62	75	75	34	052	022.3	21	.	.	04	.	.	07	.	02	11	11	08	02	11	01	01	.	.	.	04	.	
IV	6.4	5.5	5.0	5.6	191.5	06.2	78	52	71	67	24	051	024.3	11	12	.	04	08	09	08	01	09	01	.		
V	5.4	6.1	6.1	5.9	207.8	10.0	82	57	78	72	31	086	028.1	28	.	.	08	.	.	04	.	05	11	11	07	03	11	07	01		
VI	6.7	6.5	6.3	6.5	171.6	11.5	83	64	83	77	40	124	058.0	25	.	.	10	.	.	11	01	04	13	16	13	02	16	.	.	.	01	07	01		
VII	4.3	4.2	4.6	4.4	272.6	13.5	86	57	88	77	40	105	024.4	01	.	.	22	.	.	02	.	09	06	11	09	06	11	.	.	.	10	04	.		
VIII	5.7	6.1	4.6	5.5	212.2	13.3	89	61	91	80	44	071	016.9	08	.	.	19	.	.	01	.	04	07	10	12	01	10	.	.	.	13	04	.		
IX	4.7	4.3	2.9	4.0	215.2	12.7	94	63	93	83	45	041	014.1	04	.	.	13	.	.	02	.	07	02	12	08	01	11	.	.	.	06	10	.		
X	8.4	6.3	7.3	7.3	088.6	07.9	94	73	93	87	44	097	034.2	14	.	01	01	.	.	01	15	18	09	03	18	.	.	.	02	16	.				
XI	8.2	7.8	7.0	7.7	050.1	05.4	91	77	88	85	38	040	011.9	19	01	.	10	.	.	03	20	11	04	01	11	01	01	.	.	08	.				
XII	8.2	7.9	6.8	7.6	045.2	04.2	92	78	91	87	22	043	038.8	18	.	06	23	.	.	01	.	05	19	09	03	01	05	.	.	.	14	.			
GOD. 6.0 6.2 5.3 5.7 1811.1 08.3 87 64 84 78 22 738 058.0																																			
POREC																																			
BR. ST. 44																																			
I	6.6	4.5	6.0	6.4	-	06.2	85	77	85	82	30	021	089.6	28	.	.	06	.	.	04	.	13	04	03	.	04	05	12			
II	4.6	4.2	4.0	4.3	-	04.4	71	57	67	65	35	012	008.3	14	.	.	18	.	.	05	.	11	06	05	02	.	05	.	.	.	02	.			
III	7.2	6.1	6.1	6.4	-	07.0	84	71	81	79	29	082	020.2	13	.	.	03	.	.	03	.	11	13	11	03	13	.	.	.	01	.				
IV	4.3	4.4	4.1	4.3	-	07.8	82	68	80	76	40	072	020.8	11	18	07	10	09	02	10	.	.	.	01	.					
V	5.5	4.0	5.5	5.0	-	11.5	82	65	85	78	46	101	031.0	27	.	.	03	.	.	07	09	12	09	03	12	.	.	.	04	.					
VI	3.8	4.6	5.5	4.6	-	13.1	80	67	83	77	44	072	035.4	25	06	06	09	04	02	05	.	.	.	03</						

Mjesec	Vazdušni pritisak Pa mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vatra nD, Pa (0-12)																		
		TM			Sred. (Dnev.)	Min.	Max.	Dat.	Min.	Dat.	N		NE		E		SE		S		SW		W		NW					
		7	14	21							E	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.				
$\varphi = 45^{\circ}14' N \lambda = 13^{\circ}56' E$ Gr. $\Delta G = + 56$ min.															PAZIN															
I	740.2	02.0	09.8	03.8	04.9	10.4	00.4	15.5	20	-07.1	10	05	C2.0	01	01.0	06	01.7	04	02.0	06	02.5	06	01.3	08	01.2	03	01.3	04		
II	740.5	-00.9	09.4	02.2	03.3	10.4	-02.2	16.7	15	-09.0	18	02	01.5	16	02.5	14	02.0	07	02.1	03	02.0	01	01.0	02	01.5	01	02.0	03		
III	730.7	04.9	10.9	06.7	07.3	12.0	02.9	17.5	07	-06.7	01	02	02.5	03	02.3	05	02.2	16	02.7	23	02.5	08	01.9	03	01.7	03	02.0	03		
IV	734.7	06.2	15.0	08.9	09.8	16.2	02.9	22.6	20	-01.5	12	01	01.0	03	03.0	09	02.0	14	02.4	13	02.7	07	02.6	05	02.4	.	.	38		
V	734.4	12.2	21.4	14.7	15.7	22.7	10.0	24.7	20	03.2	03	02	01.5	03	02.3	11	01.8	09	02.2	10	02.2	08	02.4	05	02.8	02	02.5	43		
VI	735.0	14.8	22.4	17.1	17.8	24.2	11.8	32.0	27	04.5	05	05	01.8	04	01.2	10	02.0	05	02.4	10	02.6	07	02.7	06	02.8	02	02.0	41		
VII	735.4	14.3	27.3	19.4	20.6	28.7	13.6	33.7	15	08.5	27	05	01.6	03	02.7	03	02.7	02	03.0	04	02.5	03	02.3	07	02.6	05	02.0	37		
VIII	734.3	19.7	25.2	18.3	19.4	27.1	13.7	31.5	02	09.8	21	03	02.3	04	01.2	15	01.6	08	01.8	03	01.3	02	03.0	05	01.8	04	01.8	47		
IX	736.5	13.6	25.3	16.8	18.1	26.2	12.2	32.5	18.17	07.5	21	.	.	07	01.6	08	01.6	06	02.7	04	02.8	11	02.1	04	01.2	.	.	50		
X	736.1	06.6	19.0	09.3	11.0	19.7	05.1	28.4	C3	-01.2	31	02	01.0	08	02.0	14	02.1	09	01.9	03	01.7	04	01.8	04	02.0	03	01.0	44		
XI	736.4	03.4	11.4	09.4	06.4	12.4	01.1	20.3	04	-10.5	25	04	01.8	09	02.2	04	01.5	13	02.7	04	01.8	05	01.8	02	01.0	03	01.3	44		
XII	736.6	00.9	09.7	02.0	04.0	10.7	-00.8	15.8	29	-07.9	21	02	01.0	03	01.3	08	01.6	05	02.4	07	01.6	04	01.2	02	01.0	01	01.6	61		
600.	736.6	08.0	17.2	10.4	11.5	18.4	04.0	33.7	15.VN	-10.5	25.XI	33	01.7	64	02.1	167	01.9	98	02.4	92	02.3	66	02.1	53	01.9	33	01.7	949		
$\varphi = 45^{\circ}20' N \lambda = 14^{\circ}27' E$ Gr. $\Delta G = + 58$ min.															RIJEKA												BR. ST.47			
I	757.0	06.7	10.7	07.7	08.2	11.3	03.5	14.4	31	01.6	09	05	02.0	32	02.2	.	.	04	02.8	09	02.0	06	01.2	01	01.0	01	01.0	35		
II	757.6	04.3	05.5	05.7	06.3	10.6	03.2	16.3	06	-02.0	18	03	04.3	41	03.3	06	05.0	02	02.5	04	01.5	06	01.3	.	.	.	22			
III	747.6	08.1	11.6	09.1	09.4	12.7	06.5	17.3	07	00.2	23	03	02.0	22	02.5	05	02.0	18	02.3	12	02.2	02	01.0	03	01.7	.	28			
IV	751.4	10.7	19.0	11.8	12.3	16.4	08.9	22.0	24.21	04.9	12	02	02.5	27	02.6	03	04.0	05	02.4	08	02.2	10	01.4	06	01.7	03	01.3	26		
V	750.6	16.2	20.8	17.0	17.7	22.0	14.1	29.0	18	04.7	11	03	01.7	18	02.2	05	02.6	.	06	01.8	14	01.8	02	01.5	04	02.0	04	02.0	41	
VI	751.1	18.5	22.5	18.7	19.6	24.2	15.9	30.4	25	11.2	05	04	03.0	21	02.3	03	02.7	03	02.0	08	01.8	11	01.4	01	01.0	03	02.2	02	02.5	32
VII	751.3	21.0	27.2	21.9	23.0	28.2	18.4	32.4	18	13.4	01	03	03.0	20	02.0	03	01.0	.	04	01.2	15	01.5	.	07	02.3	01	01.0	03	01.3	41
VIII	752.3	20.1	25.0	21.2	21.9	26.6	18.2	31.6	11	19.2	20	.	.	27	02.2	04	02.2	02	01.5	02	01.7	01	02.0	02	01.0	02	01.3	04	01.0	44
IX	754.6	16.8	24.6	19.7	20.6	25.8	17.0	30.8	18	12.6	14	01	01.0	23	01.8	04	01.8	01	02.0	03	01.7	10	01.9	01	03.0	02	02.0	43		
X	754.7	11.9	18.2	13.3	14.1	19.0	10.8	26.8	02	-07.0	22	03	02.0	43	02.6	08	02.9	01	01.0	.	10	01.2	01	01.0	04	02.0	02	01.3	23	
XI	753.3	08.0	11.4	08.8	09.3	12.8	06.3	20.0	03	-02.6	25	07	02.3	47	02.7	02	03.5	05	03.6	05	01.8	.	02	01.3	03	01.3	19			
XII	756.4	05.8	10.4	06.7	07.4	11.3	04.3	14.4	01	-01.6	21	05	02.0	31	02.1	04	02.8	05	02.8	02	01.0	01	01.0	02	01.0	01	02.0	42		
600.	753.2	12.5	17.2	13.5	14.2	18.4	10.8	32.4	16.VN	-02.6	25.XI	39	02.4	352	02.5	47	02.8	48	02.4	63	01.9	94	01.5	20	01.6	32	01.9	400		
$\varphi = 45^{\circ}36' N \lambda = 14^{\circ}38' E$ Gr. $\Delta G = + 59$ min.															PAG												BR. ST.48			
I	690.7	01.3	04.5	02.5	02.8	03.8	-00.2	11.6	06	-05.8	09	01	03.0	05	01.6	C1	02.0	24	01.2	30	01.7	24	02.8	01	01.0	03	02.0	04		
II	692.2	-02.2	01.8	-01.4	-00.8	03.2	-04.3	09.5	07	-11.3	18	05	01.0	12	02.7	03	02.3	34	01.6	10	01.9	12	01.8	02	01.5	04	02.5	02		
III	682.5	01.4	04.5	02.4	02.7	08.1	-00.2	14.3	09	-04.9	23	05	01.4	01	02.0	01	02.0	38	01.4	17	01.8	26	02.0	.	05	01.0	.	01		
IV	687.0	04.7	08.9	05.4	06.1	10.7	02.1	18.4	21	-01.6	11	09	01.3	05	01.4	03	01.3	31	01.8	17	02.2	20	02.6	.	04	01.0	.	01		
V	687.2	10.0	16.3	10.8	11.3	17.3	07.3	24.2	19	03.1	02	03	01.7	15	01.6	01	01.0	31	01.4	19	01.7	14	02.2	.	05	01.0	.	01		
VI	688.5	12.4	15.8	12.3	13.2	17.6	09.0	24.4	27.23	03.9	04	04	02.2	11	02.0	04	01.5	45	01.3	11	01.8	13	02.1	.	02	02.5	02	02.5	02	
VII	689.2	14.8	20.1	15.8	16.6	22.1	11.2	28.5	15	08.2	01	01	03.0	08	01.8	.	47	01.2	16	01.5	06	01.7	.	13	02.8	02	02.0	02		
VIII	691.0	13.8	18.6	14.3	15.3	20.4	11.4	24.3	02	09.2	22	02	01.5	06	01.8	01	01.0	36	01.2	19	01.5	05	01.6	01	01.0	02	01.5	0		

Mesec	Vrednost pritisaka Pn mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																
		Tm			Sred. (Dnes)	N	NE	E	SE	S	SW	W	NW	C	E.	J.	E.	J.	E.	J.	E.	J.						
		7	14	21																								
$\varphi = 45^{\circ}25' N \lambda = 14^{\circ}35' E$ Gr. $\Delta G = + 1h 00 min.$																												
I	-	02.7	05.0	08.4	03.7	06.1	-00.6	10.3	06 -06.5	10.0	09	02.6	09	02.0	02	02.0	18	01.7	01	02.0	15	03.1	11	03.2	24	03.1		
II	-	-01.4	02.1	-00.5	00.0	03.2	-05.0	11.0	07 -12.8	18	02	03.5	22	02.5	15	03.1	19	03.2	01	01.0	14	02.9	05	01.8	04	02.2		
III	-	02.8	06.2	04.1	04.3	07.9	-06.5	15.2	09 -06.5	01	05	02.6	12	02.3	11	02.6	03	02.3	07	02.4	24	02.6	15	02.9	16	02.6		
IV	-	06.1	10.5	07.1	07.7	12.0	01.9	20.3	30 -02.4	12	01	02.0	14	02.1	21	01.7	09	02.1	02	03.5	13	02.7	24	03.0	06	02.5		
V	-	11.3	16.6	12.9	13.4	17.9	07.2	25.3	18	03.5	02	01.5	20	01.6	15	01.9	11	01.5	07	01.1	14	01.9	22	02.0	02	01.0		
VI	-	13.2	17.0	13.8	14.4	16.8	08.7	26.6	14	02.2	05	03	01.7	22	01.8	22	01.6	09	01.9	07	01.3	13	01.8	08	01.9	04	01.0	
VII	-	15.1	21.0	17.0	17.5	23.1	10.8	30.3	15	05.7	01	01	02.0	19	01.8	17	01.9	14	01.4	05	01.2	10	01.2	13	01.3	17	01.3	
VIII	-	14.4	19.5	15.8	16.4	21.0	10.8	24.7	21.0	01	07.5	22.20	03	01.3	18	01.6	30	01.5	07	01.4	07	01.0	08	01.0	13	01.8	07	01.0
IX	-	13.7	19.8	15.3	16.0	21.0	10.2	27.3	17	06.0	14	03	01.0	12	01.5	13	01.3	03	01.0	21	01.9	17	01.8	08	01.4	04	01.0	
X	-	05.9	11.2	07.3	07.9	12.3	02.8	22.5	01	-02.2	12	01	01.0	26	01.8	26	02.1	07	01.3	02	01.0	14	01.6	12	01.4	05	01.0	
XI	-	01.9	04.4	03.1	03.1	05.7	-01.5	16.1	02	-11.7	23	01	01.0	30	02.1	22	01.6	02	02.5	03	02.3	17	02.5	08	02.3	07	01.3	
XII	-	-00.1	02.6	00.3	00.8	04.1	-03.9	12.5	24	-12.5	20	02	01.5	25	01.8	28	02.0	07	01.7	04	01.3	13	01.8	10	01.3	04	01.5	
600.	-	07.1	11.3	08.3	08.6	12.8	03.4	20.3	65.0	-12.8	45.11	37	02.1	22.5	01.9	11.9	01.9	49	01.5	17.6	02.2	13.6	02.1	10.7	02.0	02.0	02.0	
$\varphi = 45^{\circ}16' N \lambda = 15^{\circ}14' E$ Gr. $\Delta G = + 1h 01 min.$																												
OGULIN																												
BR. ST.51																												
I	737.2	03.9	06.1	04.8	05.3	09.5	01.6	15.3	06 -05.2	10	06	02.2	05	02.0	05	01.2	09	01.8	08	03.1	07	03.3	27	03.1	14	02.3		
II	736.3	-02.5	04.6	00.2	00.6	05.9	-03.4	15.2	07 -13.9	18	07	02.6	17	02.6	04	02.2	05	01.6	14	01.8	06	04.5	13	02.0	11	01.9	05	
III	728.2	03.9	09.4	06.3	06.5	10.8	03.1	16.5	08 -03.2	24	03	02.0	15	02.1	07	01.6	03	01.7	10	03.2	20	03.6	17	02.4	06	02.8	12	
IV	732.2	04.8	13.0	09.1	09.5	14.2	05.1	22.3	30 -00.4	24	08	02.1	10	02.4	07	02.0	09	02.1	06	02.8	09	04.6	14	02.6	13	02.1	14	
V	732.0	12.7	18.6	14.6	15.2	20.1	10.2	27.1	18	03.3	02	07	01.7	10	02.0	07	02.0	04	01.5	04	02.0	11	03.9	23	01.8	10	01.9	17
VI	732.6	10.4	14.4	19.2	19.4	21.0	11.9	28.0	28	04.9	05	08	02.0	17	02.0	08	01.8	05	01.8	07	01.7	08	02.9	27	01.9	06	02.0	02
VII	732.2	16.3	23.4	18.0	18.9	25.0	13.6	31.4	18	07.9	27	06	02.3	12	01.9	06	01.8	05	01.6	02	01.5	09	03.1	21	01.9	18	02.4	06
VIII	734.2	15.2	21.7	16.7	17.6	23.2	13.6	28.2	15	08.7	22	04	02.2	19	01.8	06	02.0	07	01.7	01	03.0	09	02.2	29	02.0	24	02.0	02
IX	736.2	13.9	21.9	16.3	17.1	23.0	12.5	29.0	16	08.7	10	04	01.8	09	02.0	09	02.0	01	02.0	08	01.6	08	02.6	16	01.9	30	01.9	05
X	736.0	06.4	13.3	07.6	08.7	14.1	05.2	29.7	01	00.0	31.27	08	01.9	23	01.9	08	01.9	07	01.7	01	01.0	01	02.0	17	01.8	04	01.7	04
XI	735.1	02.6	06.4	04.0	04.3	07.5	01.5	20.9	02	-10.7	25	10	02.0	23	01.9	10	01.7	04	01.8	11	01.6	01	04.0	12	01.8	08	01.6	11
XII	730.1	-01.0	03.6	00.6	00.9	05.3	-01.9	14.2	29	-09.9	20	04	01.2	22	01.8	17	01.5	15	01.6	07	01.6	03	03.0	16	01.9	07	01.9	02
600.	734.6	07.3	13.2	09.8	10.0	15.0	06.1	31.4	65.0	-13.9	45.11	75	02.0	17.6	02.0	98	01.8	74	01.7	79	02.1	88	03.5	240	02.1	173	02.0	92
$\varphi = 45^{\circ}30' N \lambda = 15^{\circ}33' E$ Gr. $\Delta G = + 1h 02 min.$																												
KARLOVAC																												
BR. ST.53																												
I	736.0	01.3	08.6	04.1	04.5	09.6	00.6	14.4	19 -05.5	10	01	01.0	20	01.4	02	01.5	.	.	03	02.0	21	01.8	01	01.0	04	01.2	41	
II	736.5	-01.2	06.0	02.2	07.1	-01.7	13.2	12	-11.0	18	08	01.8	19	01.8	14	01.4	14	01.5	03	01.3	10	01.3	03	02.0	04	01.2	40	
III	747.0	04.5	11.3	07.5	07.7	12.8	03.4	16.8	08 -03.0	01	02	01.0	18	01.8	.	04	01.2	.	.	20	02.0	.	.	04	01.5	45		
IV	750.0	04.6	15.5	11.0	16.7	20.2	04.0	24.0	30 -00.9	24	01	01.0	21	01.8	02	01.0	05	02.0	21	02.2	.	.	02	02.0	42			
V	750.0	12.9	21.2	16.8	16.9	22.6	11.5	29.0	20.0	19.0	05.0	03	03	01.0	18	01.7	02	01.0	02	02.0	.	.	17	02.0	.	01	03.0	50
VI	750.6	14.7	21.7	17.8	18.0	23.2	13.0	31.2	15	04.0	07	04	01.5	22	01.5	01	01.0	01	01.0	13	01.0	02	01.0	01	01.0	47		
VII	751.0	16.8	25.3	20.8	20.9	27.0	15.4	32.1	15	10.4	01	05	01.6	20	01.2	05	01.4	01										

Mjesec	Vazdušni pritisak Pa	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, fm (0-12)																			
		TM				Hm				M:		Min.		Dat.	N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dnev.)	Hm	Hm	Hm	Hm	M:	M:	Min.	Dat.	S.	J.	S.	J.	S.	J.	S.	J.	S.	J.	S.	J.	S.	J.				
$\varphi = 45^{\circ}56' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = +1h\ 04\ min.$															STUBIČKA GORA														BR. ST. 56		
I	-	02.7	05.3	03.2	03.6	06.5	01.2	13.6	06	-04.6	10	08	01.6	09	02.0	06	01.3	12	03.3	01	01.0	37	04.4	11	03.1	05	02.8	04			
II	-	-01.0	02.4	-00.1	00.3	05.9	-02.7	16.2	20.7	-06.4	17	07	01.4	38	02.0	02	01.5	11	02.3	-	00	04.0	04	03.0	07	02.0	05				
III	-	04.2	07.5	04.8	05.3	05.8	02.3	12.8	09.0	-05.2	22	-	-	23	02.7	06	01.8	17	02.7	02	02.0	21	03.9	03	02.6	14	03.1	05			
IV	-	06.6	11.1	07.6	06.2	12.5	04.7	19.4	22	00.0	03.0	05	02.6	26	02.7	07	01.6	17	03.4	03	01.7	07	04.7	11	02.7	10	03.2	04			
V	-	12.7	17.3	13.7	14.3	18.2	10.5	24.2	20.19	06.8	24.02	07	02.1	20	02.8	06	01.2	17	02.8	03	01.7	10	03.4	07	02.1	16	02.5	07			
VI	-	14.2	16.9	14.0	14.8	18.4	11.5	26.1	15	04.8	02	05	01.2	26	02.6	03	02.3	12	02.2	02	02.5	07	03.1	13	01.2	15	02.5	07			
VII	-	17.0	20.9	17.5	18.2	22.1	14.7	27.6	15	06.8	01	04	02.0	17	02.3	11	01.5	25	02.3	03	01.3	08	02.8	04	01.5	09	02.9	02			
VIII	-	16.6	19.9	16.1	17.2	20.8	14.0	24.6	10	10.8	26	09	01.4	34	02.4	07	01.4	13	02.4	07	02.0	02	01.5	06	01.3	10	02.4	05			
IX	-	16.0	19.9	16.9	17.2	20.8	14.0	26.0	17	07.8	14	03	01.7	09	02.7	12	01.2	25	02.5	11	01.7	09	02.3	07	01.6	10	02.2	04			
X	-	08.2	11.6	08.6	09.3	12.4	06.4	23.4	01	01.2	12	03	01.0	27	02.3	05	01.2	19	02.6	02	01.0	09	01.2	12	01.9	11	02.1	05			
XI	-	02.5	04.1	03.0	03.1	05.4	01.0	15.2	02	-07.6	23	07	02.9	31	02.1	13	01.6	13	03.3	03	02.0	03	02.3	03	01.0	09	02.2	05			
XII	-	06.3	02.8	06.6	01.0	04.6	-01.7	15.6	29	-06.4	19	01	01.0	28	01.6	11	01.4	09	02.6	02	02.8	14	01.6	12	01.7	10	02.4	05			
OO.	-	08.3	11.6	08.8	09.4	12.3	06.4	27.6	45.VII	-08.4	47.II	61	01.8	288	02.4	09	01.5	190	02.7	39	01.8	123	03.6	98	01.9	135	02.4	72			
$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = +1h\ 04\ min.$																ZAGREB-GRAČ														BR. ST. 57	
I	791.0	03.6	07.9	05.3	05.6	06.2	02.0	12.6	19.10	-02.8	10	04	01.2	14	01.5	07	01.6	06	01.2	08	01.4	21	02.1	27	01.9	05	02.6	01			
II	784.3	05.3	05.3	03.3	03.2	05.9	00.1	11.4	12	-04.5	10	09	02.4	26	02.2	11	01.8	06	01.7	08	01.6	08	01.9	13	02.2	02	05.8	01			
III	742.8	05.3	10.7	06.6	06.4	12.0	05.1	17.3	08	-06.6	01	07	01.7	23	02.0	08	01.4	07	01.3	04	01.2	15	02.2	19	02.2	07	01.9	09			
IV	744.6	09.2	14.9	11.7	11.9	15.7	00.1	21.3	30	03.5	01	13	02.0	28	01.8	09	01.7	04	02.0	04	02.3	08	03.0	17	01.9	06	02.6	01			
V	745.0	14.0	20.6	17.4	17.6	21.3	13.4	27.4	19	06.2	10	15	01.7	22	02.0	08	02.0	07	01.6	02	02.0	16	02.0	17	01.6	04	01.5	-			
VI	746.7	16.3	20.8	18.2	18.4	21.9	15.1	29.3	15	06.1	02	19	01.8	23	01.6	08	01.8	07	01.6	06	01.5	11	01.6	07	01.7	04	01.9	01			
VII	747.0	16.5	24.4	21.1	21.3	25.7	16.0	30.8	15	10.3	01	27	01.7	15	01.7	10	01.2	09	01.6	12	01.7	05	02.0	05	01.4	06	01.3	01			
VIII	748.0	16.7	23.7	19.3	20.0	24.4	16.4	27.7	11	08.6	20	23	01.8	23	01.9	08	01.4	06	01.3	09	01.6	04	01.6	09	01.6	10	01.2	01			
IX	750.2	15.9	23.0	19.2	19.3	23.6	15.3	28.3	17	06.7	14	15	01.7	20	01.6	08	01.6	09	01.7	10	01.7	06	02.5	11	01.6	07	01.7	04			
X	751.2	06.7	15.9	15.0	16.0	14.8	00.1	24.5	01	03.3	27	16	01.7	31	01.7	08	01.6	07	01.3	04	01.2	10	01.2	05	01.2	05	01.2	05			
XI	749.9	04.8	06.3	05.1	05.2	07.2	03.4	12.9	19	-06.6	24	10	02.2	31	01.8	13	01.6	13	01.1	01	02.0	08	01.4	11	01.3	02	01.0	01			
XII	750.1	06.8	03.3	02.1	02.1	03.9	00.2	16.7	04	-06.2	20	07	01.4	29	01.4	10	01.5	07	01.1	12	01.7	11	01.5	03	01.3	03	01.3	01			
OO.	749.0	09.6	14.6	11.9	12.0	15.3	08.7	26.8	45.VII	-06.6	46.XI	185	01.8	285	01.8	108	01.6	88	01.5	83	01.6	119	02.0	160	01.7	67	01.6	20			
$\varphi = 45^{\circ}18' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = +1h\ 04\ min.$																TOPUSKO														BR. ST. 58	
I	-	01.2	09.4	02.7	04.0	10.2	-01.7	16.6	06	-07.4	10	07	01.4	05	01.8	-	09	01.8	02	02.0	27	02.1	12	01.5	19	01.7	12				
II	-	-01.0	00.1	01.1	01.1	06.7	-04.3	15.2	28	-11.8	10	05	01.2	04	02.2	04	01.2	16	02.2	-	13	02.4	09	01.3	19	01.4	14				
III	-	02.6	12.3	06.6	07.0	13.2	00.5	20.6	06	-04.3	01	06	01.8	12	02.1	-	07	01.4	06	01.2	22	02.3	07	01.4	16	02.1	17				
IV	-	07.4	19.4	09.2	10.3	16.7	03.6	23.4	06	-01.5	28	08	01.2	09	02.1	04	01.8	16	02.9	03	02.3	17	02.4	09	01.3	18					
V	-	14.1	21.1	14.4	16.0	22.1	09.6	26.0	22.21	02.8	03.01	09	01.7	03	02.3	15	01.7	06	02.0	12	01.5	16	01.8	15	01.7	09	01.8	09			
VI	-	15.1	21.7	17.0	17.1	22.6	10.9	26.6	15	01.8	06	06	01.8	03	02.0	06	02.0	19	02.1	09	01.6	15	01.9	11	01.7	13	01.7	18			
VII	-	17.3	25.1	17.6	19.3	26.1	15.2	31.3	10.15	07.2	28	07	02.4	13	02.3	05	01.8	08	02.1	07	01.4	14	01.6	01	01.0	17	01.9	20			
VIII	-	19.8	23.9	17.0	18.4	22.2	11.0	26.1	10	05.0	11	16	01.6	08	01.6	06	01.6	10	01.7	02	02.0	14	01.2	03	02.4	17					
IX	-	14.4	24.5	16.0	17.7	24.9	12.1	26.2	16	06.5	14	05	01.2	15	02.0	04	02.2	05	01.6	06	01.0	16	01.7	02	01.0	27	01.3	27			
X	-	07.0	14.6	07.																											

Mjesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm			Prvi dan u rascjedima																										
	7	14	21		e _m	U _m	%	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	*	•	▲	▲	■													
	Sred. (Dles.)				mm	7	14	21	Stred.	Min	Σ	Max	Dat.	=	<	≤	≥	≥	≤	≤	≤	≤	≤	≤													
STUBIČKA GORA																																					
BR. ST. 56																																					
I	5.2	5.3	3.9	4.8	-	04.7	82	74	82	79	41	026	013.4	28	.	05	.	.	08	01	06	06	05	04	01	04	02	01	.	.	.	05	04				
II	4.2	5.1	4.3	4.5	-	03.6	78	72	76	75	38	022	006.3	15	.	05	23	.	.	04	.	10	06	08	07	01	07	.	.	.	05	05					
III	7.5	7.5	5.7	6.9	-	05.4	75	73	81	78	37	092	C16.5	16	.	01	09	.	.	06	.	03	15	17	12	03	12	05	02	01	.	01	04	06			
IV	6.5	6.7	5.3	6.2	-	06.0	77	67	75	73	43	047	022.7	11	06	.	04	11	07	05	02	04	05	.	.	.	05	.				
V	5.6	7.1	5.6	6.1	-	09.5	82	71	77	77	43	083	021.6	24	01	.	05	11	14	10	03	14	02	04				
VI	6.6	8.1	6.2	7.0	-	10.5	83	77	82	81	48	118	021.6	17	.	.	.	01	.	02	.	04	13	18	15	05	18	.	.	.	05	05					
VII	4.2	5.6	4.3	4.7	-	11.9	70	70	75	75	52	128	037.8	02	.	.	.	03	.	09	07	14	09	05	14	.	.	.	08	05							
VIII	5.6	7.7	5.5	6.3	-	11.8	82	73	82	79	49	128	031.8	26	03	10	17	14	03	17	.	.	.	08	07							
IX	3.8	5.4	1.3	3.5	-	11.9	83	74	80	79	52	043	012.5	12	.	.	.	02	.	.	10	03	09	07	02	05	.	.	.	01	02						
X	5.6	6.2	5.4	5.7	-	07.5	85	80	83	83	45	141	035.8	17	01	.	09	11	10	06	11	.	.	.	02	09							
XI	7.7	7.5	6.4	7.2	-	05.0	84	81	85	83	28	056	020.8	11	.	03	08	.	.	02	02	17	08	06	02	01	.	.	.	16	01						
XII	6.8	5.9	5.6	5.9	-	04.0	81	77	77	79	29	043	041.0	18	.	07	21	.	.	01	.	08	12	04	02	01	03	01	.	.	.	12	03				
GDH.	5.8	6.5	4.9	5.7	-	07.6	81	74	79	78	28	927	C41.0	48x	.	16	70	06	.	.	31	01	73	122	132	102	33	115	25	03	01	.	.	31	03	29	
ZAGREB-GRČIĆ																																					
BR. ST. 57																																					
I	6.4	6.3	5.7	6.1	101.2	05.1	82	67	75	74	52	018	006.2	09	.	06	.	.	03	.	04	11	05	03	05	01	09	01					
II	4.1	5.1	4.4	4.5	130.6	03.8	78	57	64	66	23	012	004.4	15	.	13	.	.	03	.	10	06	07	04	03	03	.	.	.	07	01						
III	7.7	8.2	7.3	7.7	098.3	05.7	81	59	69	70	24	057	012.3	30	.	02	.	.	04	.	02	14	17	10	01	14	05	02	.	.	01	03	02				
IV	6.4	7.1	6.2	6.6	175.5	06.2	70	50	59	59	30	044	C23.9	11	04	01	13	10	06	01	10	.	.	.	01	01	.						
V	5.5	6.7	5.9	6.1	193.6	10.1	76	58	69	68	30	071	021.1	24	.	.	.	07	.	03	01	04	10	16	09	02	16	06	01				
VI	7.1	7.6	7.1	7.2	160.8	11.5	60	61	74	72	39	117	044.5	25	.	.	07	.	01	02	01	03	16	16	12	C3	16	.	.	01	01	08	02				
VII	4.3	5.3	3.6	4.4	266.2	13.2	80	57	72	70	42	104	019.3	03	.	.	.	21	02	01	03	10	07	14	10	06	14	.	.	.	11	.					
VIII	5.9	7.1	5.3	6.0	201.6	13.0	85	61	78	74	41	099	027.2	08	.	.	16	.	02	01	04	12	15	13	03	15	.	.	.	01	11	02					
IX	4.6	5.5	2.5	4.2	200.5	12.6	88	62	77	76	45	029	008.4	07	.	.	08	.	01	09	02	09	05	06	05	01	.	.	.	03	05						
X	7.3	6.5	5.5	6.4	099.4	08.0	88	63	80	82	40	093	025.8	17	.	.	.	05	.	14	10	07	04	10	.	.	.	02	04								
XI	6.3	7.7	7.2	7.7	045.6	05.4	84	73	79	78	32	051	021.3	11	.	06	.	.	02	.	03	20	11	07	03	11	.	.	.	07	.						
XII	7.8	7.2	6.7	7.2	034.0	04.4	84	79	82	82	49	050	040.3	18	.	02	17	.	.	04	18	07	02	01	06	03	.	.	.	02	14						
GDH.	6.2	6.7	5.6	6.2	1729.3	08.2	82	63	73	72	23	745	044.5	25M	.	02	44	59	02	02	27	04	62	143	137	88	24	133	12	02	02	.	01	03	49	56	04
TOPUSKO																																					
BR. ST. 58																																					
I	7.4	6.7	7.6	7.2	-	06.2	97	89	95	94	71	031	016.8	29	.	01	21	09	05	04	01	05	01	18	01				
II	5.4	5.5	6.2	5.7	-	05.0	95	92	94	93	68	039	009.6	21	01	.	23	.	.	07	11	09	09	05	05	.	.	.	04	10							
III	8.2	8.2	7.0	7.8	-	07.7	97	94	95	95	69	063	C27.5	18	.	09	.	.	01	16	15	13	02	14	02	.	.	01	01	02	03	01					
IV	6.2	6.8	6.2	6.4	-	09.4	95	94	95	95	69	073	034.0	11	.	06	.	.	04	11	11	09	02	11	.	.	.	01	02	.							
V	5.9	6.4	5.8	6.0	-	14.0	96	94	96	95	80	115	028.7	08	.	.	09	.	.	08	10	13	13	04	13	.	.	.	04	02	.						
VI	7.3	7.5	7.5	7.4	-	15.1	98	95	97	97	73	098	015.8	18	.	.	11	02	.	01	15	17	13	04	17	.	.	.	01	08	04						
VII	4.9	5.1	5.9	5.3	-	17.2	98	92	96	95	73	192	039.0	01	.	.	23	04	.	05	07	15	13	09	15	.	.	.	01	11	10						
VIII	5.8	7.3	7.5	6.9	-	16.0	98	92	96	96	80	104	024.0	28	.	.	18	.	.	13	19	15	04	19	.	.	.	12	18	.							
IX	7.7	5.7	5.4	6.3	-	15.6	98	91	97	96	82	040	023.7	08	.	.	16	02	.	03	08	07	06	01	07	.	.	.	04	21	.						
X	6.7	6.6	7.5	7.6	-	09.2	97	94	97	96	78	108	032.0	17	.	03	01	.	.	02	16	10															

Meseč	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																				
												Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R _T	III	II		
	7	14	21	Sred. (Dles)		mm	7	14	21	Sred.	Min	Σ	Max	Dat.	30.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.020.0	•	Δ	Δ	▲	▲	R _T	III	II	
SISAK																											$H_a = 98 \text{ m } H_b = 106.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$					
BR. ST. 61																											$H_a = 98 \text{ m } H_b = 106.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$					
I 6.2 6.5 4.0 5.6	105.9	05.2	89	68	83	80	54	021	013.8	29	.	02	17	.	.	.	01	.	03	07	08	04	01	04	02	.	.	01	.	.	06	.
II 4.5 5.0 4.2 4.5	140.5	04.1	90	63	78	77	28	021	005.5	03	.	.	21	.	.	.	01	.	11	07	12	03	.	04	07	.	.	01	.	.	02	02
III 8.3 8.0 6.0 7.4	116.3	04.0	87	60	76	74	27	033	009.4	18	.	.	07	.	.	.	01	.	01	15	19	10	.	18	02	02	.	.	08	04	.	
IV 5.9 4.0 4.1 5.3	201.8	04.7	83	54	70	69	32	005	038.6	11	03	01	04	07	15	09	02	15	03	.	
V 5.4 5.7 4.6 5.3	221.4	10.9	85	61	80	75	35	003	019.5	24	.	.	.	10	.	.	03	05	07	15	18	04	14	04	04	.	
VI 6.8 6.6 7.3 6.9	184.3	12.3	85	65	84	78	40	093	026.8	17	.	.	.	12	02	.	03	01	02	12	18	14	04	18	.	.	.	01	08	04	.	
VII 4.1 3.5 3.7 3.7	289.1	14.6	89	61	82	78	43	142	034.2	13	.	.	.	22	03	.	.	13	04	14	10	09	14	11	04	.		
VIII 6.2 6.3 3.6 5.4	197.9	13.9	92	62	89	81	48	072	027.8	24	.	.	.	20	.	.	.	04	06	14	07	02	13	10	10	.	
IX 5.3 4.4 2.4 4.0	263.9	13.3	96	63	91	83	47	034	026.5	06	.	.	.	15	.	.	.	06	02	09	03	01	05	01	20	.		
X 8.8 7.0 5.4 7.1	078.4	08.5	96	75	89	84	36	102	035.0	14	.	.	02	01	.	.	.	01	15	16	10	03	13	02	15	.		
XI 6.5 6.0 7.3 8.0	046.2	06.1	92	83	91	89	39	048	020.6	11	01	.	09	.	.	01	01	02	20	13	05	01	12	02	01	.	01	.	07	.		
XII 6.9 6.9 7.3 7.7	049.7	04.3	92	80	89	87	46	027	021.6	10	.	04	19	.	.	.	02	20	05	02	01	03	01	.	02	.	10	.				
GOŠ. 6.6 6.2 5.0 5.9																											$H_a = 1835.6 \text{ m } H_b = 1846.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$					
BR. ST. 62																											$H_a = 144 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$					
I 7.0 6.3 4.5 5.6	-	06.2	90	89	91	90	74	020	005.5	28	.	.	12	02	11	05	04	.	05	01	.	.	.	04	.			
II 4.7 5.5 3.1 5.1	-	05.3	88	92	91	90	75	016	004.5	15	.	.	22	09	09	07	04	.	03	04	.	.	.	04	.			
III 7.0 7.4 7.1 7.4	-	07.8	91	91	92	91	73	026	009.7	21	.	.	05	01	15	14	03	.	11	04	.	.	.	03	01			
IV 6.3 6.0 4.4 6.2	-	06.8	92	91	91	91	82	072	026.0	11	04	10	14	09	01	14	01	.				
V 5.6 6.6 4.4 5.3	-	15.6	93	89	92	91	73	092	039.6	27	.	.	.	06	.	.	.	04	11	10	08	03	10	02	.			
VI 5.9 6.9 7.2 6.7	-	15.3	93	92	93	93	80	032	056.6	25	.	.	.	12	01	.	.	02	13	16	14	03	16	.	.	.	01	03	01			
VII 4.0 4.5 4.7 4.4	-	16.3	94	89	93	92	76	077	019.6	02	.	.	.	24	03	.	.	09	07	12	11	02	12	.	.	.	01	01	.			
VIII 5.2 6.9 6.5 6.2	-	17.4	94	93	93	93	61	078	026.7	24	.	.	.	22	01	.	.	04	11	13	10	02	13	.	.	.	01	02	.			
IX 5.2 4.5 4.5 4.9	-	16.8	94	93	93	94	85	019	011.2	08	.	.	.	19	01	.	.	05	04	05	04	01	05	.	.	.	01	05	.			
X 6.4 6.7 7.1 7.0	-	09.3	94	94	94	94	87	102	043.2	14	.	.	02	01	.	.	.	19	13	10	03	02	12	.	.	.	02	15	.			
XI 6.4 7.6 8.2 8.1	-	04.2	94	94	94	94	82	042	015.6	11	.	04	02	21	19	08	01	06	03	01	.	.	.	03	.			
XII 6.3 7.6 8.0 8.0	-	05.0	92	94	93	93	78	038	032.6	10	01	03	21	.	.	.	04	22	03	02	01	03	03	.	.	.	10	.				
GOŠ. 6.5 6.4 6.5 6.5																											$H_a = 11.1 \text{ m } H_b = 144 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$					
SJELOVAR																											$H_a = 141 \text{ m } H_b = 142.4 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$					
I 5.7 5.5 4.5 5.2	-	05.8	91	69	86	82	48	020	007.8	28	.	01	16	.	.	.	01	.	06	08	05	.	08	01	01	.	.	05	.			
II 4.6 4.3 3.5 3.9	-	04.6	89	63	83	78	32	016	004.4	15	.	.	22	13	07	07	04	.	04	04	01	.	.	03	01			
III 4.6 4.7 4.5 5.9	-	05.9	90	60	78	76	35	047	019.0	21	.	.	06	.	.	.	01	06	14	09	01	13	03	02	.	.	02	04	.			
IV 5.8 5.1 4.4 5.1	-	04.5	83	52	72	69	28	039	028.4	11	.	.	02	.	.	.	01	04	07	11	00	01	11	.	.	.	01	01	.			
V 5.6 5.6 4.4 5.5	-	10.5	84	96	78	73	32	008	026.2	28	.	.	.	11	.	.	.	05	09	15	10	04	15	.	.	.	04	02	.			
VI 4.7 6.7 5.4 6.2	-	11.9	85	67	82	80	35	122	036.4	20	.	.	.	11	.	.	.	10	06	12	11	05	12	.	.	.	02	02	.			
VII 6.1 5.3 5.6 5.8	-	12.6	86	69	84	80	42	041	016.4	25	.	.	.	13	01	.	.	01	07	11	12	10	01	12	.	.	.	03	01	.		
VIII 5.1 3.9 2.6 3.9	-	14.2	90	61	79	75	42	128	046.2	02	.	.	.	24	04	.	.	12	05	11	09	05	08	05	.	.	01	03	01			
VIII 5.8 5.7 4.2 5.2	-	13.8	94	68	86	82	43	096	028.4	28	.	.	.	17	.	.	01	09	07	13	13	03	13	.	.	.	03	04	.			
IX 4.5 2.3 3.0 3.3	-	13.3	94	62	88	82	45	049	023.8	05	.	.	.	20	01	.	.	12	02	06	04	01	06	.	.</							

Mesec	Vazdušni pritisak Pa MM	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра m/s, fm (0-12)																							
		Am					Mm					E						SE						S			SW			W			NW		
		7	14	21	Sred. (Dnev.)	N	M	N	M	D	M	E	J	S	J	E	J	S	J	E	J	S	J	E	J	S	J	E	C						
$\varphi = 45^{\circ}36' N$ $\lambda = 17^{\circ}14' E$ Gr. $\Delta G = + 1h\ 09\ min.$																									CARUVAR		BR. ST.66								
I	752.4	02.3	08.6	04.0	04.7	09.2	00.8	15.2	06 -05.0	04	05	02.0	04	01.5	07	01.0	13	01.1	20	01.4	12	01.5	07	01.3	06	01.2	19								
II	754.7	-01.7	09.3	00.8	01.3	06.0	-02.3	13.6	13 -07.6	18	15	01.8	14	01.7	04	01.2	08	01.0	04	01.5	04	01.8	06	01.3	07	01.0	22								
III	749.3	05.1	12.5	07.6	08.2	14.1	03.9	19.8	09 -02.4	22	13	01.5	16	01.4	08	01.2	09	01.1	12	01.4	11	01.8	04	01.3	06	01.3	14								
IV	747.6	08.0	19.3	09.8	10.7	16.7	09.5	24.6	06 00.4	28.20	21	01.5	10	01.1	02	01.0	08	01.4	11	01.6	04	01.2	06	01.7	07	01.6	21								
V	746.3	14.5	21.4	15.6	16.8	22.8	11.3	28.8	18 04.6	02	20	01.6	07	01.1	06	01.0	05	01.0	10	01.0	08	01.1	07	01.1	13	01.2	11								
VI	746.9	16.0	21.9	16.6	17.0	23.4	13.0	30.3	15 05.4	07	27	01.7	04	01.2	05	01.0	09	01.1	06	01.3	07	01.0	10	01.2	20										
VII	747.2	16.2	25.7	19.2	20.6	26.9	15.5	32.9	27 08.1	19	01.2	07	01.3	04	01.0	05	01.0	01	01.0	04	01.0	15	01.1	33											
VIII	746.3	16.7	24.5	17.6	19.1	25.4	14.1	30.2	11 10.2	22.21	19	01.2	12	01.1	04	01.2	03	01.0	03	01.0	06	01.0	01	01.0	08	01.0	37								
IX	750.6	14.4	25.2	17.0	18.4	25.8	12.4	30.0	17 06.7	14	09	01.1	03	01.0	03	01.0	14	01.0	06	01.0	09	01.0	04	01.0	01	01.0	41								
X	751.6	07.3	14.5	09.3	10.1	15.3	06.3	30.0	01 00.2	31	22	01.0	14	01.1	06	01.0	01	01.0	04	01.0	03	01.0	09	01.0	29										
XI	750.6	02.3	07.3	04.2	04.5	07.9	01.5	16.4	02 -10.5	26	14	02.0	19	01.4	04	01.5	05	01.2	07	01.7	02	01.5	02	01.0	07	01.4	30								
XII	750.6	-00.2	03.9	00.3	01.1	04.4	-01.6	18.2	01 -09.2	20	18	02.0	04	01.9	04	01.2	08	01.0	09	02.0	05	01.8	09	01.1	05	01.0	27								
600.	749.4	08.6	19.3	10.2	11.1	16.3	06.6	32.9	46.W -10.3	26.XI	202	01.5	118	01.3	57	01.1	88	01.2	97	01.4	45	01.4	56	01.2	94	01.2	318								
$\varphi = 45^{\circ}20' N$ $\lambda = 17^{\circ}41' E$ Gr. $\Delta G = + 1h\ 11\ min.$																									SLAVONSKA POŽEGA		BR. ST.67								
I	-	-01.1	07.3	03.9	03.3	06.3	-02.0	16.2	06 -07.2	10	23	01.3	07	01.0	03	01.0	06	01.2	14	01.0	14	01.3	13	01.3	13	01.0	-								
II	-	-02.2	05.9	02.2	01.0	04.8	-03.1	14.1	28 -06.2	18	25	01.2	11	01.7	02	02.0	08	01.2	06	01.2	22	01.1	09	01.0	-										
III	-	03.7	13.4	07.8	06.2	14.1	02.0	19.8	09 -04.8	01	12	01.3	17	01.7	06	01.2	04	01.0	10	01.3	12	01.2	23	01.4	09	01.1	-								
IV	-	07.9	19.8	10.2	11.0	16.9	04.8	25.7	04 01.0	09	25	01.6	06	01.5	03	01.3	03	01.3	12	01.9	14	01.3	10	01.2	15	01.3	-								
V	-	14.3	21.7	16.7	17.4	22.8	10.7	28.4	18 04.5	01	17	01.6	05	02.0	11	01.5	07	01.3	09	01.0	09	01.1	14	01.1	21	01.3	-								
VI	-	16.4	23.2	19.0	19.4	24.1	12.9	30.3	15 04.9	07	24	01.5	05	01.4	07	01.3	07	01.2	13	01.2	13	01.1	16	01.3	-										
VII	-	18.4	25.6	21.1	21.6	26.7	16.2	30.8	18 08.2	27	16	01.4	05	01.8	08	01.3	01	02.0	16	01.1	26	01.1	12	01.1	14	01.0	-								
VIII	-	17.2	24.3	17.9	19.4	25.4	13.9	30.2	18 08.8	19	12	01.2	08	01.1	04	01.6	03	01.3	03	01.0	21	01.1	24	01.0	18	01.1	-								
IX	-	13.5	25.1	18.3	18.8	25.4	11.3	31.6	16 05.6	14	10	01.4	11	01.4	08	01.9	02	01.0	25	01.1	15	01.0	15	01.3	-										
X	-	07.1	15.2	11.3	11.2	16.1	05.9	27.9	01 -06.5	27	19	01.2	16	01.2	09	01.2	04	01.0	05	01.2	07	01.1	17	01.0	16	01.0	-								
XI	-	02.3	07.2	04.9	04.8	06.0	01.2	17.6	02 -11.1	26	21	01.2	20	01.2	11	01.2	02	01.0	05	01.2	18	01.0	13	01.2	-										
XII	-	-01.0	04.4	01.3	01.6	09.1	-02.0	13.0	01 -07.7	20	11	01.1	14	01.5	14	01.6	06	01.0	03	01.0	11	01.1	18	01.0	16	01.1	-								
600.	-	08.0	19.8	11.2	11.6	16.7	09.8	31.6	46.W -11.1	26.XI	215	01.3	125	01.4	88	01.3	45	01.2	91	01.1	145	01.2	199	01.1	175	01.2	-								
$\varphi = 45^{\circ}44' N$ $\lambda = 17^{\circ}38' E$ Gr. $\Delta G = + 1h\ 11\ min.$																									DONJI MELJANI		BR. ST.68								
I	-	01.8	08.7	04.3	04.8	10.0	-06.4	17.8	18 -04.0	05.04	10	01.7	02	01.0	08	01.2	07	01.3	05	01.8	33	01.3	14	01.3	14	01.2	-								
II	-	-00.1	05.2	02.1	02.4	07.1	-02.7	16.2	13 -08.2	18	10	01.6	13	01.4	02	01.5	05	01.0	02	01.5	27	01.1	14	01.6	09	01.4	-								
III	-	05.3	12.6	08.3	08.6	14.0	03.2	19.5	11 -03.0	01	02	01.5	08	01.8	15	01.7	19	01.3	06	01.2	21	01.5	14	01.5	13	01.6	-								
IV	-	08.3	14.9	10.3	11.0	17.4	04.7	26.8	04 01.0	02	16	02.0	05	01.8	02	01.5	08	01.0	24	01.5	14	01.2	18	01.6	-										
V	-	15.3	21.3	16.1	17.3	23.6	03.3	29.2	22 04.4	01	12	01.7	05	01.6	05	01.6	12	01.3	02	01.5	24	01.4	12	01.7	21	01.8	-								
VI	-	16.2	22.0	18.4	19.4	24.1	11.3	32.0	15 05.8	07	19	01.9	07	01.1	02	01.5	05	01.8	01	01.0	16	01.1	19	01.4	29	01.5	-								
VII	-	18.0	25.6	19.4	20.8	27.8	13.0	32.7	15 07.0	03	12	01.8	07	01.4	05	01.0	07	01.1	03	01.3	22	01.1	12	01.5	25	01.7	-								
VIII	-	17.3	24.3	18.1	19.4	25.4	13.8	30.2	11 09.4	15	19	01.6	03	01.3	08	01.4	08	01.2	01	01.0	09	01.2	26	01.4	-										
IX	-	15.5	24.8	18.7	19.4	26.0	11.2	30.2	17 07.2	16.09	13	01.2	04	01.5	09	01.6	20	01.4	03	01.0	25	01.1	10	01.3	06	01.3	-								
X	-	09.0	14.7	10.6	10.9	16.6	04.8	27.8	01 03.0	31.30	08	01.5	05	01.4	08	01.8	10	01.4	03	01.0	25	01.2	14	01.1	.20	01.4	-								
XI	-	02.6	06.4	04.0	04.2	08.1	01.5	14.3	19 -08.7	26	09																								

Mjesec	Oblačnost Nm (0-10)			Sred. (Dnev.) Indeks broj sati	Vlažnost vazduha						Padavine R mm		Broj dana n s a:												R									
					U m t						R mm		Tn	Tx	Tn	Tx	Tx	Tn	F(O-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ	R	T	≡	■	
	7	14	21		mm	7	14	21	Sred.	Min	Σ	Mx	Dat.	=	<	<	=	=	=	=	<	>	Σ	Σ	Σ	Σ	Σ	Σ	Σ	Σ				
DARUVAR																																		
BR. ST. 66																																		
I	5.8	5.0	3.9	4.9	124.7	04.6	03	57	77	73	24	022	010.5	20	.	.	12	06	08	06	04	01	04	01	01	01	04			
II	4.8	4.9	3.4	4.4	145.5	03.8	08	50	78	75	26	023	007.8	21	.	.	19	12	07	08	05	04	05	01	.	.	02	03		
III	7.0	7.6	5.3	6.7	113.7	05.6	04	51	75	70	21	049	022.4	21	.	.	04	01	10	14	11	01	13	01	.	.	01	.		
IV	5.7	5.9	4.7	5.4	182.7	06.2	79	47	70	66	22	074	043.2	11	05	08	13	08	01	13		
V	5.2	6.6	4.8	5.5	200.0	10.3	03	34	80	72	32	128	038.2	28	.	.	.	18	06	08	14	11	05	14	.	.	.	05	.	
VI	6.5	6.6	6.3	6.3	150.4	11.5	03	57	83	74	29	131	046.7	14	.	.	19	02	.	.	.	02	14	20	13	03	26	.	.	.	01	08		
VII	4.4	4.9	3.4	4.2	276.4	13.0	03	50	83	72	31	116	041.0	02	.	.	25	04	.	.	.	08	05	09	07	04	09	.	.	.	04	.		
VIII	5.9	6.4	3.9	5.4	202.0	13.7	95	60	95	83	40	098	022.0	20	.	.	20	01	.	.	.	06	05	18	13	04	18	.	.	.	12	03		
IX	3.1	4.3	1.9	3.1	219.3	12.8	96	54	92	81	37	041	019.9	08	.	.	24	01	.	.	.	11	01	07	05	01	07	.	.	.	04	02		
X	7.0	6.7	5.1	6.3	104.7	08.1	96	70	94	87	34	104	051.7	14	.	.	01	01	.	.	.	06	14	12	10	03	12	.	.	.	01	03		
XI	8.0	7.5	7.3	7.6	056.0	05.8	97	77	91	88	30	054	014.1	19	02	01	09	.	.	.	02	18	12	06	02	11	01	.	.	04	04			
XII	7.6	6.9	6.4	7.0	055.3	04.5	93	78	95	89	41	011	004.8	18	.	07	23	.	.	.	04	13	06	03	03	02	.	.	.	01	01			
GOD. 5.9 6.1 4.7 5.6 1830.7 08.3 88 59 84 77 21 853 051.7																																		
SLAVONSKA POŽEGA																																		
BR. ST. 67																																		
I	5.0	5.2	3.6	4.6	-	04.8	90	71	86	82	35	034	015.1	20	.	.	24	.	.	.	01	.	07	03	03	02	01	01	.	.	07	.		
II	4.6	5.2	3.1	4.1	-	04.3	89	71	86	82	37	010	004.2	21	.	.	24	12	03	04	03	02	02	02	.	.	01	02		
III	6.1	6.4	4.6	5.7	-	06.4	91	60	84	78	35	039	008.4	15	.	.	10	02	04	12	10	01	11	01	.	.	01	02		
IV	5.2	6.3	4.0	5.2	-	07.5	87	59	84	76	36	074	027.9	11	.	.	02	05	05	12	11	02	12	.	.	.	02	.		
V	5.3	6.3	4.5	5.5	-	11.8	87	64	86	79	39	164	045.4	20	.	.	10	.	.	.	01	.	04	07	15	14	04	15	.	.	10	01		
VI	6.1	6.8	4.7	5.9	-	13.1	86	64	82	77	39	057	013.4	29	.	.	14	01	.	.	01	.	02	04	15	12	02	19	.	.	07	01		
VII	4.0	5.4	3.4	4.2	-	14.8	85	61	84	77	45	100	029.4	17	.	.	23	04	.	.	.	04	04	10	09	03	10	.	.	.	08	.		
VIII	4.7	6.5	3.4	4.9	-	13.9	89	64	91	81	46	048	008.7	14	.	.	20	01	.	.	.	04	03	10	12	04	18	.	.	.	03	03		
IX	3.0	3.6	1.6	2.7	-	12.9	90	61	85	79	26	040	024.4	08	.	.	21	02	.	.	.	12	01	04	03	02	04	.	.	.	02	02		
X	6.6	6.8	4.5	5.5	-	08.6	85	73	74	87	55	104	041.2	14	.	.	02	01	.	.	.	05	10	11	09	03	11	.	.	.	02	09		
XI	7.2	7.5	6.9	7.2	-	05.8	91	80	90	87	59	043	021.2	19	01	.	08	02	14	13	09	02	12	04	03	.	.	04		
XII	6.5	6.5	6.1	6.4	-	04.5	92	80	89	87	52	014	004.2	27	.	02	23	05	14	08	05	04	02	.	.	.	11	01		
GOD. 5.3 6.0 4.2 5.2																																		
DONJI MELJANI																																		
BR. ST. 68																																		
I	5.1	4.3	3.4	4.3	-	05.8	89	83	86	86	58	023	014.5	20	.	.	14	09	05	04	03	01	04	.	.	.	02	.		
II	4.5	4.6	4.1	4.4	-	04.6	83	82	86	84	60	029	007.0	21	.	.	20	14	08	06	04	03	04	.	.	.	01	05		
III	6.8	6.2	5.2	6.1	-	06.6	87	71	76	78	26	073	029.5	21	.	.	03	04	08	12	12	02	11	01	.	.	03			
IV	5.3	5.9	4.4	5.1	-	07.0	00	65	67	71	34	088	033.0	11	.	.	02	05	06	13	11	03	13	.	.	.	01	.		
V	5.2	6.5	4.3	5.3	-	10.7	82	64	63	70	14	164	068.8	27	.	.	13	03	07	11	09	05	11		
VI	5.9	6.3	5.6	5.9	-	12.1	83	67	71	74	45	088	018.2	29	.	.	19	04	.	.	.	05	11	15	15	02	19		
VII	4.0	4.8	2.6	3.8	-	13.4	76	12	69	70	22	090	022.2	13	.	.	27	06	.	.	.	12	04	09	08	04	09	.	.	.	02	.		
VIII	5.0	6.2	4.9	5.4	-	13.1	85	68	68	75	24	163	035.7	28	.	.	21	01	.	.	.	08	09	15	15	06	15	.	.	.	04	03		
IX	3.9	3.3	1.9	3.0	-	12.3	83	67	63																									

Meseč NR.	Vrednost pritisaka Pm hPa	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)															
		Tm		Sred. (Dnev.)	N	NE	E	SE	S	SW	W	NW	C	E.	J.												
		7	14	21																							
$\varphi = 45^{\circ} 17' N$ $\lambda = 18^{\circ} 25' E$ Gr. $\Delta G = + 1h 14 min.$																											
I	-	-00.4	06.6	02.2	02.7	07.3	-01.5	13.6	06	-05.5	11	03	01.7	06	01.3	.	14	01.2	12	01.7	28	01.2	06	01.7	24	01.5	
II	-	-01.5	05.1	01.4	01.6	06.2	-02.3	14.2	12	-05.5	10.9	20	02.0	06	02.5	07	01.6	09	01.3	04	01.0	09	01.7	06	02.2	23	01.7
III	-	04.1	13.6	07.8	08.3	14.6	21.2	21.6	09	-04.0	01	06	02.7	07	02.7	06	02.3	16	01.5	09	01.7	17	01.9	04	03.0	28	01.7
IV	-	08.8	19.0	09.9	10.9	16.3	05.9	27.2	07	01.4	01	09	03.4	06	02.2	01	03.0	12	01.8	03	02.3	19	02.6	06	03.7	34	03.0
V	-	15.1	21.2	15.6	16.9	22.4	11.5	27.6	22	04.5	01	14	02.8	09	02.4	01	03.0	06	02.5	07	02.9	09	02.4	13	02.8	34	02.3
VI	-	14.9	22.5	17.4	18.9	23.8	11.7	30.8	24	08.8	11	08	02.9	04	03.0	04	02.5	08	02.6	04	02.0	12	02.2	11	03.0	39	02.5
VII	-	19.1	25.1	19.4	20.7	26.4	19.1	31.0	18	09.4	27	06	02.3	01	02.0	06	02.2	01	03.0	03	02.3	16	02.2	17	02.4	43	02.4
VIII	-	17.6	24.1	18.1	19.5	29.1	14.4	28.6	11	10.0	15	11	02.9	06	02.8	03	02.7	10	02.5	06	01.7	15	01.9	07	02.7	35	02.6
IX	-	18.0	24.6	17.4	18.6	25.5	12.6	31.6	16	07.0	14	08	02.6	09	02.7	11	02.7	15	02.6	05	02.2	21	02.0	05	02.8	16	02.1
X	-	08.0	14.4	09.9	10.4	19.4	05.9	24.2	01	00.6	10	12	02.6	04	02.8	08	03.0	09	02.9	06	02.0	24	02.4	12	02.8	18	03.0
XI	-	02.4	07.0	04.2	04.9	07.6	01.6	19.0	02	-09.0	26	07	02.6	14	02.5	15	02.5	08	02.9	06	02.5	14	02.0	03	02.3	23	02.7
XII	-	-00.6	03.8	00.8	01.2	04.6	-02.0	12.5	01	-07.5	21	12	02.4	10	02.4	03	02.3	10	02.0	07	02.1	22	02.3	03	03.0	26	02.5
600.	-	08.7	15.3	10.3	11.2	16.3	06.5	31.6	6. IX	-09.0	26. XI	116	02.6	82	02.5	65	02.9	118	02.1	72	02.0	206	02.0	93	02.7	343	02.4
$\varphi = 45^{\circ} 42' N$ $\lambda = 18^{\circ} 44' E$ Gr. $\Delta G = + 1h 15 min.$																									BRESTOVAC-BELJE		
BR. ST. 71																									BR. ST. 72		
I	750.8 -00.2	06.7	01.8	02.9	07.1	-01.2	13.1	18	-05.2	01	09	02.1	05	01.8	04	01.3	03	02.0	26	01.7	19	01.6	16	01.8	09	01.9	.
II	760.8 -02.5	05.7	00.8	01.2	06.3	-04.1	13.8	13	-08.2	09	08	01.9	23	02.3	07	01.9	03	02.0	10	01.6	07	01.7	14	01.7	10	02.1	.
III	750.8 03.6	14.1	07.7	08.3	14.9	02.2	22.9	09	-06.5	01	04	02.8	24	02.2	11	02.1	13	02.4	07	02.0	15	01.7	09	02.2	11	02.3	.
IV	755.5 08.4	15.2	10.2	11.0	16.3	05.6	26.9	06	01.2	11	17	02.9	13	02.1	08	01.6	04	01.5	11	02.3	01	03.0	14	02.0	22	02.2	.
V	752.7 19.5	22.4	16.4	17.6	23.0	12.1	28.8	17	06.3	01	19	02.8	12	01.8	12	02.0	10	01.6	08	01.8	06	01.7	19	01.9	07	01.8	.
VI	753.2 17.8	23.0	17.8	18.9	23.8	13.9	30.6	24	10.1	07	24	02.5	04	01.7	06	02.0	02	02.0	11	01.6	04	01.8	18	01.9	.	751.6	.
VII	753.6 19.1	25.1	19.4	20.7	26.2	19.3	30.9	16	09.7	27	13	02.2	04	01.8	09	01.4	05	01.2	13	01.5	13	01.5	19	01.8	.	751.6	.
VIII	754.7 17.8	24.5	18.5	19.7	25.3	14.7	30.5	11	07.5	19	17	01.9	13	01.6	11	01.8	04	01.5	07	01.6	10	01.5	12	01.6	17	01.8	.
IX	751.2 14.8	24.9	17.3	18.6	25.4	12.8	31.4	16	08.0	14	11	01.8	08	01.4	19	01.5	17	02.1	07	01.9	07	01.7	12	01.8	09	01.9	.
X	750.2 07.9	14.6	09.9	10.6	15.3	06.4	27.5	01	01.1	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.
XI	751.2 02.3	06.9	03.9	04.1	07.7	00.4	14.1	02	-09.3	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.	
XII	750.7 -01.1	04.0	00.8	01.1	05.0	-01.9	11.4	17	-07.3	21	12	02.2	15	01.1	09	01.0	08	01.1	10	01.1	02	01.0	27	01.1	10	01.6	.
600.	755.8 08.9	15.6	10.3	11.2	16.4	06.3	31.4	6. IX	-09.3	26. XI	170	01.7	155	01.5	70	01.6	143	01.6	127	01.5	109	01.5	194	01.8	.		
$\varphi = 45^{\circ} 32' N$ $\lambda = 18^{\circ} 44' E$ Gr. $\Delta G = + 1h 15 min.$																									CSIJERK		
BR. ST. 73																									BR. ST. 74		
I	750.9 -00.4	06.9	01.6	02.4	07.3	-01.3	13.4	06	-05.3	10	03	02.3	03	01.3	C4	01.5	26	01.3	25	01.2	11	01.4	09	01.1	12	01.9	.
II	761.0 -02.6	06.0	00.8	01.2	04.8	-03.2	14.7	13	-07.4	10	13	02.0	19	01.6	C3	01.3	12	01.5	10	01.1	07	01.4	08	01.4	12	01.8	.
III	749.7 03.4	14.5	07.7	06.3	15.6	02.4	23.8	09	-04.6	01	11	02.0	13	01.6	C7	01.7	20	02.1	11	01.7	16	01.6	09	02.1	04	02.0	.
IV	753.1 07.9	19.8	10.3	11.1	17.4	05.9	28.2	07	01.4	11.09	18	02.1	10	01.5	04	01.8	05	02.2	11	01.8	07	01.6	10	02.8	23	02.0	.
V	752.2 15.0	23.0	16.5	17.8	24.0	12.1	28.6	22	04.1	01	18	01.4	15	01.3	C6	01.5	03	01.7	11	01.4	11	01.5	11	01.6	18	01.7	.
VI	752.7 16.7	23.6	18.0	19.1	24.8	14.1	31.4	24.16	10.1	06	20	02.0	11	01.6	C2	02.0	10	01.5	10	01.5	04	01.3	07	01.7	24	01.7	.
VII	753.0 16.8	25.6	19.8	21.0	27.1	19.4	31.6	15	09.0	27	13	01.5	14	01.4	C5	01.0	08	01.4	06	01.2	21	01.5	21	01.6	23	01.7	.
VIII	754.2 16.8	24.8	18.8	19.8	26.1	15.1	31.2	11	09.9	19	23	01.3	14	01.1	C5	01.2	07</										

Mesec	Oblačnost Nm (0-10)				Inzolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																											
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. Min.			≤	<	<	≥	IV	TX	Tn	P(O-12)	Nm(0-10)	R mm	•	*	*	Δ	~	▲	▲	R	T	≡	■							
		mm	mm	mm		Σ	Max	Dat.	-30.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.00.0	9	Δ	~	▲	▲	R	T	≡	■													
CJAKOVAC																																							
BR. ST. 71																																							
I	5.7	5.6	5.1	5.5	-	04.7	86	78	85	83	54	033	016.5	09	.	.	22	01	04	04	05	01	01	01	.	.	.	08							
II	5.2	5.2	5.2	5.2	-	04.3	84	72	87	81	29	014	004.6	15	.	.	22	01	08	06	03	02	04	.	.	.	02	01							
III	6.7	6.2	4.8	5.9	-	04.3	84	59	83	75	30	029	007.2	18	.	.	08	03	11	07	10	01	01	.	.	.	01	02							
IV	6.9	5.9	5.3	6.1	-	07.4	78	61	84	74	33	056	019.6	11	.	.	02	.	.	.	03	02	04	12	07	02	12	01	.	.	.	01	.						
V	5.5	6.1	5.9	6.0	-	11.2	85	62	81	76	40	245	078.5	27	.	.	05	.	.	02	01	.	08	15	14	04	15	.	.	.	01	09							
VI	6.6	6.2	6.8	6.5	-	12.6	84	63	82	77	45	083	028.4	11	.	.	16	01	.	02	.	09	16	11	02	16	.	.	.	04	01								
VII	4.7	4.9	4.2	4.9	-	14.1	82	60	85	75	41	100	024.4	02	.	.	22	03	.	01	.	01	03	11	00	04	11	.	.	.	05	01							
VIII	5.5	5.8	6.0	5.7	-	13.6	89	61	90	80	44	084	018.0	14	.	.	19	.	.	02	.	05	17	13	04	17	.	.	.	07	05								
IX	3.8	4.1	3.1	3.7	-	12.7	92	58	86	79	36	026	016.8	08	.	.	21	01	.	.	.	02	01	03	01	06	.	.	.	07	.								
X	7.0	7.0	6.0	6.7	-	08.2	91	71	89	84	43	051	016.8	14	.	.	01	14	12	08	02	12	.	.	.	04	.								
XI	8.1	7.8	6.9	7.6	-	05.6	90	79	87	85	53	057	021.6	11	.	01	10	16	12	11	01	11	01	.	.	.	01	05							
XII	6.1	7.1	7.6	7.6	-	04.3	87	78	87	84	55	008	002.2	13	.	02	26	13	07	04	04	04	.	.	.	01	13								
GOD.				6.2	6.0	5.7	6.0	-	08.8	86	66	85	79	29	786	078.5	27.V	.	03	88	96	07	.	10	01	07	94	131	96	21	122	12	02	.	.	02	28	66	04
BRESTOVAC-BELJE																																							
BR. ST. 72																																							
I	6.1	5.9	4.0	5.3	092.4	04.6	90	70	87	83	48	018	004.5	09	.	01	19	07	07	10	04	09	01	.	.	.	15	.							
II	4.4	5.2	4.0	4.5	111.2	03.7	87	59	78	74	22	004	001.3	21	.	.	24	11	09	04	02	01	03	.	.	.	06	01							
III	7.4	7.3	5.8	6.8	124.0	05.6	86	50	74	70	20	024	006.0	29	.	.	07	03	11	13	06	12	02	01	.	.	01	04							
IV	6.1	6.4	5.5	6.0	158.0	04.6	88	54	72	68	28	048	020.0	11	.	.	02	05	09	12	08	01	12	02	.	.	01	.							
V	5.6	6.6	6.0	6.1	202.3	11.3	82	57	82	73	37	141	027.3	28	.	.	12	02	08	14	10	07	14	.	.	.	01	11							
VI	7.1	6.6	7.3	7.0	174.5	12.7	84	60	83	76	40	067	016.8	21	.	.	14	02	.	01	.	01	12	14	10	02	16	.	.	.	09	03							
VII	9.6	6.1	4.6	4.8	238.0	14.3	85	59	87	77	44	147	039.5	07	.	.	22	03	.	.	.	02	05	09	09	05	09	.	.	.	07	03							
VIII	5.7	6.5	6.3	6.2	186.2	13.7	90	60	88	79	43	075	020.0	27	.	.	18	01	.	.	.	05	10	17	12	02	17	.	.	.	14	04							
IX	4.2	3.7	2.5	3.5	188.3	12.5	93	54	86	78	37	014	004.4	27	.	.	19	01	.	.	.	09	03	04	04	04	04	.	.	.	02	15							
X	-	-	-	-	-	087.5	-	-	-	-	-	077	022.0	14	.	.	01	-	12	06	03	12	05	.							
XI	8.9	8.6	7.6	8.4	045.6	05.3	92	76	88	83	46	039	014.6	11	.	01	10	21	12	07	01	10	03	.	.	.	05	01							
XII	8.5	7.6	7.8	8.0	052.5	04.4	92	77	89	86	50	007	001.7	18	.	01	28	.	.	01	.	17	03	05	02	03	.	.	.	08	02								
GOD.				-	-	-	-	-	-	-	-	1660.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
OSIJEK																																							
BR. ST. 73																																							
I	4.6	5.5	4.5	4.9	106.1	03.1	97	91	94	91	64	014	007.3	09	.	.	24	07	07	07	03	06	02	01	01	.	.	04							
II	3.9	4.3	4.0	4.0	131.4	04.2	96	68	83	83	32	005	002.3	21	.	.	23	15	09	05	02	02	03	.	.	.	01	01							
III	7.4	7.7	7.2	6.8	137.3	04.5	94	59	83	79	32	032	015.2	21	.	.	10	02	11	15	06	01	13	02	.	.	01	01							
IV	6.3	5.7	5.1	5.7	170.5	07.6	92	79	77	77	40	043	016.3	11	.	.	02	05	09	12	07	02	12	.	.	.	01	.							
V	5.1	6.0	4.6	5.2	205.5	12.6	92	64	89	82	43	102	028.8	28	.	.	15	04	07	14	12	02	14	.	.	.	10	01							
VI	7.0	5.6	6.1	6.3	192.0	14.1	93	66	83	87	47	049	013.8	20	.	.	16	05	.	.	.	05	10	17	11	01	17	.	.	.	09	01							
VII	2.7	3.1	3.1	3.6	262.3	15.5	92	65	89	87	47	049	020.5	01	.	.	25	05	.	.	.	11	04	09	03	09	04	.	.	.	06	01							
VIII	5.0	5.5	5.6	5.4	201.2	15.2	90	62	91	87	51	113	025.4	31	.	.	21	03	.	.	.	04	07	18	15	03	18	.	.	.	13	01							
IX	3.1	2.8	1.6	2.5	220.0	13.6	97	58	93	82	41	009	003.3	13																									

Mesec	Vazdušni pritisak Pa	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, fm (0-12)																
		Z				NE				E				SE				S				SW		W		NW		
		7	14	21	Sred. (Dnev.)	M	M	M	M	D	D	M	M	D	D	M	M	E	J.	E.	J.	E.	J.	E.	J.	E.	J.	
$\varphi = 44^{\circ}57' N$ $\lambda = 14^{\circ}23' E$ Gr. $\Delta G = + 58$ min.																												
I	-	04.5	10.8	04.6	06.1	11.8	03.4	14.5	22	06.0	07	0	02.7	22	01.5	C3	01.0	.	.	25	02.3	26	01.3	17	01.2	-		
II	-	03.9	09.8	04.3	05.6	10.5	02.5	15.0	18	-02.3	27	03	02.7	54	02.9	06	03.5	06	03.3	.	03	02.3	03	01.0	07	01.9	-	
III	-	08.4	12.4	08.5	09.5	12.9	05.7	17.5	07	-01.8	01	0	.	16	03.2	C3	01.0	22	04.0	10	03.3	10	01.9	12	01.3	20	01.6	-
IV	-	09.8	16.4	06.7	11.3	17.2	07.2	22.0	22	04.0	18	07	01.4	19	02.1	04	02.0	20	03.7	07	01.7	03	01.0	01	01.0	29	01.5	-
V	-	-	-	-	-	-	-	-	-	-	-	04	01.0	13	01.5	C4	01.5	19	01.5	06	02.2	06	01.5	19	01.3	22	01.2	-
VI	-	18.6	23.3	17.4	19.2	24.3	13.5	31.0	27	07.8	06	02	01.0	03	02.0	.	.	06	02.2	02	01.5	24	02.0	15	01.5	35	01.5	03
VII	-	23.2	27.9	20.9	23.0	29.2	16.5	-	-	-	-	05	02.4	01	03.0	41	01.3	46	01.7	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	15.8	25.8	26.2	21.5	26.4	17.3	31.1	18	12.4	01	14	01.2	17	01.8	C5	01.0	19	01.2	13	01.8	.	04	01.2	04	01.5	16	
X	-	13.3	18.8	13.9	15.0	19.6	11.6	26.7	03	07.6	21	22	01.7	25	02.3	10	01.4	06	02.0	08	01.8	03	01.0	05	01.4	04	01.5	10
XI	-	09.1	12.7	09.8	10.3	13.6	07.0	20.3	03	-00.9	26	17	01.9	24	02.2	07	01.6	11	01.9	15	02.1	02	01.0	.	06	01.5	08	-
XII	-	06.6	10.6	06.8	07.7	11.4	04.6	19.9	03	00.7	23	12	02.1	22	02.3	08	01.5	11	02.1	10	02.3	03	01.0	01	01.0	09	01.0	17
600.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 44^{\circ}32' N$ $\lambda = 14^{\circ}28' E$ Gr. $\Delta G = + 58$ min.																												
I	742.1	08.5	10.7	04.1	09.4	11.5	07.6	13.6	31	09.0	01	06	03.2	11	04.3	.	.	18	02.9	10	02.3	11	02.1	13	01.9	15	01.7	09
II	761.9	04.9	09.9	07.4	08.0	10.7	06.0	14.3	02	01.8	27	14	03.6	28	04.6	07	04.1	06	03.0	09	03.0	03	02.3	12	02.0	05	02.4	04
III	792.3	09.3	12.7	10.2	10.6	18.5	08.3	17.2	04	03.3	23	03	04.4	12	02.8	04	02.2	31	03.6	21	03.4	07	02.6	06	02.8	01	03.0	08
IV	756.1	11.8	15.6	12.3	13.0	16.5	10.4	21.6	22	03.6	11	11	02.5	20	03.6	.	.	13	03.5	21	03.1	10	02.2	07	02.9	03	02.3	05
V	752.3	16.6	20.5	17.1	17.8	21.6	14.6	27.6	19	11.0	02	06	02.0	22	02.5	C6	02.2	C5	02.8	13	02.3	18	02.4	14	02.4	04	01.5	01
VI	759.6	19.1	22.7	19.3	20.1	24.0	17.1	29.6	29	13.6	09.04	11	03.0	22	03.7	03	02.3	06	02.7	16	02.6	06	02.7	19	02.6	07	02.0	-
VII	759.7	22.2	26.8	22.8	23.7	28.1	20.3	32.0	01	13.2	21	20	02.8	29	03.2	04	01.8	01	03.0	07	02.6	06	01.8	17	02.5	07	02.4	02
VIII	759.4	21.3	25.6	21.6	22.6	26.7	19.6	30.6	11	16.9	25	13	03.8	42	03.5	04	02.0	05	03.0	14	03.1	03	03.3	06	02.5	03	01.7	03
600.	757.6	14.3	17.7	14.8	15.4	18.6	13.0	32.0	17.VII	01.7	24.XI	148	03.1	278	03.5	54	02.8	133	03.3	126	02.9	93	02.4	134	02.4	72	02.1	57
$\varphi = 44^{\circ}45' N$ $\lambda = 14^{\circ}46' E$ Gr. $\Delta G = + 59$ min.																												
I	764.7	08.1	11.4	08.5	09.2	11.6	06.5	15.6	20	02.1	16	09	03.1	12	02.2	C7	01.1	32	03.7	11	01.9	04	01.5	.	.	07	02.1	11
II	764.5	06.1	11.1	07.2	07.9	11.8	04.6	16.7	02	00.8	18	13	02.8	19	03.1	19	04.2	10	03.9	05	01.2	06	01.5	.	.	03	02.3	09
III	764.0	07.3	12.8	10.2	10.6	13.7	07.6	17.2	30	02.1	24	10	03.6	13	02.0	C7	02.3	44	04.6	07	02.4	04	01.5	01	01.0	04	01.8	03
IV	758.8	11.6	15.9	12.5	13.1	17.2	09.6	23.0	22	04.8	11	18	02.5	07	02.6	C6	03.0	28	04.7	06	02.5	07	02.1	.	.	03	01.8	13
V	757.9	16.9	20.8	17.4	18.1	22.3	14.5	29.0	19	10.3	01	17	02.1	10	03.1	C5	02.0	16	02.6	09	02.3	07	01.7	04	01.8	01	01.3	18
VI	758.4	19.0	23.2	19.3	20.2	24.4	16.9	30.6	25	13.2	06	13	03.9	22	03.2	04	04.5	22	03.2	04	02.0	12	02.1	02	02.6	04	02.1	22
VII	758.4	21.7	26.9	22.5	23.4	28.2	19.1	32.0	30	11.6	01	23	03.0	09	03.4	C1	02.0	10	02.2	09	01.7	11	01.3	03	02.9	19	02.3	19
VIII	759.2	21.2	26.2	21.9	22.8	27.3	18.9	31.7	09	15.8	28.29	34	02.9	15	03.4	C1	01.0	13	02.2	01	05.0	08	01.6	02	01.0	04	02.3	19
IX	761.8	19.8	25.6	20.7	21.7	26.2	18.3	30.0	18	15.2	14	10	01.3	09	01.1	C2	01.0	26	02.8	09	03.3	17	01.8	02	02.0	04	01.0	17
X	761.6	14.1	19.6	15.1	15.9	20.5	12.6	27.4	04	05.4	31	10	01.5	36	02.0	11	02.5	07	03.1	07	01.9	02	01.0	02	02.0	04	01.8	07
XI	762.4	10.0	13.3	10.5	11.1	14.4	08.1	20.3	03	06.4	24	15	02.3	11	02.5	C7	01.7	29	04.0	03	02.3	02	01.5	.	.	08	01.4	05
XII	763.7	08.0	11.9	07.6	08.0	11.4	05.5	16.6	17	-02.2	20	04	02.0	17	04.4	36	04.5	13	02.2	03	04.0	.	.	.	05	02.4	13	
600.	759.4	13.7	17.4	14.5	15.0	18.7	11.1	33.0	48.VII	-02.3	17.II	67	02.3	211	05.4	368	04.1	157	02.3	82	02.5	57	02.4	34	02.0	69	02.0	50
$\varphi = 44^{\circ}59' N$ $\lambda = 14^{\circ}59' E$ Gr. $\Delta G = + 1h 00$ min.																												
I	633.3	-02.3	-01.0	-02.0	-01.8	00.3	-03.6	04.0	05	-05.6	09	01	C3.0	.	.	.	31	04.1	.	.	.	05	05.6	39	04.2	10	03.3	07
II	625.2	-04.3	-03.6	-05.0	-05.0	-01.4	-03																					

Meseč	Oblačnost Rm (0-10)				Indolacija broj sati (Dnes)	Vlažnost vazduha				Padavine R mm				Broj dana na sat																											
														Tn		Tx		Tx		Tx		Tn		F(0-12)		Rm(0-10)		R mm		•	*	*	Δ	Δ	▲	▲	R	T	≡	■	
	7	14	21	Sred. (Dnes)		mm	7	14	21	Sred.	Min	Σ	Max	Dat.	<	<	<	<	<	<	<	<	<	<	>	>	>	>	•	Δ	Δ	▲	▲	R	T	≡	■				
CRES																																									
BR. ST. 76																																									
I	4.7	5.2	5.4	5.1	-	05.4	73	68	75	72	38	021	020.6	29	04	11	01	01	01							
II	3.5	2.9	3.4	3.3	-	04.6	69	61	64	65	41	010	010.0	16	.	.	04	13	05	01	01	01						
III	7.7	7.7	7.5	7.6	-	06.6	74	66	74	72	35	109	030.3	20	.	.	02	03	17	11	10	04	11	01	.	.							
IV	4.9	4.5	4.4	4.4	-	07.0	69	61	70	67	30	078	020.7	11	11	08	04	04	04	06							
V	4.5	5.3	5.8	5.2	-	-	-	-	-	-	-	088	024.2	24	-	-	-	-	-	-	.	07	10	07	07	05	07	01	.	.							
VI	4.4	4.7	5.9	5.0	-	11.7	68	62	70	67	46	079	019.0	17	.	.	.	13	04	.	.	06	07	08	08	04	08	02	.	.							
VII	2.8	2.3	2.1	2.1	-	13.6	63	52	70	62	-	055	030.5	01	-	-	-	-	-	-	.	26	03	05	05	01	05	01	.	.							
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
IX	3.7	3.4	1.7	2.9	-	14.0	08	59	78	72	30	041	022.3	13	.	.	.	25	01	03	.	.	14	02	07	05	04	07	04	.	.						
X	4.1	3.8	3.1	3.7	-	08.9	79	58	70	68	25	116	030.2	17	.	.	.	04	14	04	10	09	04	10	03	02	.						
XI	6.0	5.6	4.9	5.3	-	07.1	79	64	73	72	29	103	023.5	18	.	.	.	04	09	11	11	09	05	11	02	02	.						
XII	5.6	5.0	4.8	5.0	-	06.3	82	70	80	77	45	052	012.5	18	01	.	09	10	09	07	03	09	.	.	01	01	.							
600.																																									
PALI LEBINJ																																									
BR. ST. 77																																									
I	5.9	6.5	4.0	5.3	092.1	06.6	79	67	77	74	45	034	018.5	29	01	04	08	02	01	02							
II	3.8	4.3	3.0	3.7	161.7	04.9	64	52	63	51	26	016	009.4	16	10	02	13	04	04	02	.	04	.	.	.	02	01	.							
III	6.5	6.9	4.8	6.1	150.2	07.3	61	66	77	75	39	073	025.8	13	08	03	04	14	09	02	14	01	01	.	02	01	.								
IV	4.5	4.5	3.8	4.3	233.9	07.5	73	55	72	67	30	040	012.5	17	06	10	07	09	08	02	09	.	.	.	01	.	.								
V	6.0	5.2	3.4	4.8	261.6	11.3	79	62	79	73	37	063	015.1	08	.	.	.	04	.	.	08	06	13	08	03	13	.	.	.	02	01	.									
VI	4.8	4.1	4.1	4.3	249.0	12.3	73	60	73	65	36	087	042.3	11	.	.	.	12	03	04	11	06	09	04	01	09	.	.	.	03	.	.									
VII	2.4	2.2	1.6	2.1	367.7	13.6	70	49	67	62	25	021	009.4	01	.	.	.	28	12	22	02	01	23	03	03	03	03	03	.	02	.	02	01	.							
VIII	4.4	4.2	4.3	4.4	289.6	14.1	75	57	74	69	33	074	035.8	19	.	.	.	23	01	15	06	10	08	10	03	10	.	.	.	08	01	.									
IX	3.7	2.7	2.1	2.9	267.3	14.7	82	58	80	73	39	045	019.4	12	.	.	.	26	01	10	01	15	03	05	04	02	09	.	.	.	03	.	.								
X	4.3	3.9	2.1	3.4	210.2	09.9	72	62	76	64	44	144	046.7	13	.	.	.	03	02	05	15	04	11	09	04	11	.	.	.	03	.	.									
XI	6.5	6.1	4.1	5.6	109.5	07.7	74	66	71	50	128	034.2	11	.	.	.	07	05	05	10	11	11	03	11	.	.	.	01	03	.	.	01	.	.							
XII	5.1	6.5	4.8	5.3	097.4	06.9	78	70	78	76	37	070	041.2	10	.	.	.	03	02	07	07	06	02	07	02	.	.	.	03	.	.	03	.	.							
600.																																									
SEŠNIJ																																									
BR. ST. 79																																									
I	6.9	6.5	5.2	6.2	097.6	05.8	67	61	68	66	33	022	010.1	29	10	02	05	12	07	04	01	07							
II	5.9	5.2	4.8	4.4	153.6	03.9	57	45	55	53	13	021	008.4	21	.	.	03	.	.	.	21	14	12	04	08	05	07	04	02								
III	7.5	6.2	6.0	7.2	117.6	06.2	57	59	66	64	33	103	025.5	20	08	02	03	14	17	13	03	17	.	.	05	.	.								
IV	6.1	6.2	4.5	5.6	213.3	08.4	62	51	57	56	26	078	019.7	11	11	06	08	12	08	04	12	.	.	03	01	01	.								
V	6.5	6.5	5.5	6.2	222.2	10.3	70	56	68	65	24	133	029.1	25	.	.	.	07	03	07	07	13	15	10	05	15	.	.	.	07	.	.									
VI	5.9	6.2	5.3	5.8	226.3	11.3	67	57	62	58	28	197	013.8	25	.	.	.	13	02	05	16	01	04	07	12	11	03	.	.	08	.	.									
VII	2.8	3.3	2.8	2.9	309.7	12.4	62	45	59	55	30	094	037.4	01	.	.	.	28	13	19	06	17	05	19	06	03	16</														

Mesec	Vrednost pritisaka hPa	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (0-12)																	
		TM		7	14	21	28. (ned.)	1M M	15 M	2 M	3 M	Dat.	N	NE	E	SE	S	SW	W	NW	C								
													8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
		$\varphi = 44^{\circ}27' N$	$\lambda = 15^{\circ}04' E$ Gr.	$\Delta G = + 1h\ 00\ min.$																									
I	-	06.7	11.0	17.9	08.4	12.5	04.7	14.2	20	-01.2	10	12	02.6	06	03.2	10	01.1	24	01.6	16	01.7	01	01.0	04	01.0	20	01.4	...	
II	-	05.9	11.0	07.4	07.9	11.9	03.8	15.7	19	-02.4	28	27	03.7	21	04.1	04	01.0	12	01.6	05	02.0	01	01.0	14	01.0	14	01.0	...	
III	-	05.9	14.1	10.6	11.2	14.4	07.3	18.3	03	-00.2	01	08	03.4	04	04.8	03	01.7	29	02.6	27	02.7	03	01.7	03	02.0	16	01.5	...	
IV	-	12.4	17.8	13.9	12.4	18.6	09.9	24.1	22	03.6	12	17	02.8	10	03.4	05	01.4	19	02.5	15	02.7	06	01.7	04	02.3	16	01.8	...	
V	-	18.8	22.6	18.5	19.6	23.4	14.6	29.3	21	08.1	02	17	02.2	05	03.0	05	01.6	13	01.8	10	02.1	07	01.6	11	01.6	25	01.7	...	
VI	-	20.3	24.8	20.9	21.5	25.3	17.6	31.0	28	13.0	09	20	02.8	12	03.4	06	01.3	15	01.9	10	02.2	02	02.0	08	01.7	19	02.4	...	
VII	-	24.0	26.7	23.8	25.0	29.4	20.0	35.0	18	14.8	02	28	02.5	11	02.5	04	01.2	06	01.7	09	01.3	03	01.7	03	02.3	29	01.8	...	
VIII	-	22.8	27.3	23.0	24.0	26.5	19.9	32.5	05.0	04	18.4	25	29	02.4	14	02.9	05	01.2	14	01.4	05	02.0	06	01.8	09	01.4	11	01.6	...
IX	-	21.0	27.7	21.6	23.0	26.5	18.8	33.0	18	15.1	25	10	01.9	07	02.0	08	01.1	18	01.8	14	02.1	07	01.9	11	01.7	15	01.5	...	
X	-	14.4	20.2	18.4	16.4	21.6	12.2	30.1	04.01	06.5	31	24	02.5	19	02.7	13	01.3	11	01.6	04	02.0	03	02.0	05	01.4	14	01.4	...	
XI	-	09.9	13.5	10.9	11.3	14.4	07.4	21.4	03	-03.5	25	20	02.8	14	03.4	05	01.2	19	02.3	14	02.5	03	01.3	07	01.1	08	01.5	...	
XII	-	07.4	11.6	08.3	06.9	12.7	05.1	16.0	28	00.0	24	17	02.6	12	03.1	04	01.0	15	01.8	13	02.1	03	01.0	09	01.2	20	01.3	...	
600.	-	14.4	19.2	18.1	16.0	20.1	11.8	35.0	10.24	-03.5	25.0	22.0	02.7	13.5	03.2	7.0	01.3	18.1	02.0	14.2	02.2	4.4	01.7	7.7	01.6	20.7	01.6	...	
		$\varphi = 44^{\circ}08' N$	$\lambda = 15^{\circ}13' E$ Gr.	$\Delta G = + 1h\ 01\ min.$																									
I	746.0	04.8	11.1	08.2	08.6	11.8	03.4	14.9	26	00.5	10	04	02.5	06	01.3	13	01.4	21	01.8	30	01.7	01	01.0	02	01.5	16	02.2	27	
II	745.9	04.9	10.5	07.0	07.3	11.3	03.8	15.3	02	-01.1	09	14	02.4	13	03.4	11	02.0	07	02.4	02	02.0	01	02.0	04	02.2	16	02.1	28	
III	745.6	04.8	13.0	10.5	10.7	14.0	07.8	17.1	38	00.6	23	07	01.7	03	02.7	06	02.2	29	03.1	10	02.7	01	02.0	09	03.8	18	...		
IV	746.1	11.3	16.1	13.2	16.4	09.1	22.6	23	04.6	12	08	02.5	06	01.8	05	01.8	17	03.3	13	03.2	08	02.7	16	02.6	22	...			
V	759.2	16.9	20.4	17.5	18.1	21.6	14.2	25.3	20	08.3	01	04	01.8	04	01.8	02	02.0	14	02.1	10	02.4	08	02.2	20	02.4	33			
VI	759.0	19.2	22.6	18.6	20.3	24.1	16.4	28.5	25	11.5	05	03	03.0	08	01.8	03	01.3	08	01.6	15	02.2	08	02.1	28	02.8	33			
VII	759.5	21.8	26.4	23.2	23.1	27.5	18.6	31.9	31	15.2	01	09	03.0	05	02.6	06	01.4	04	02.0	05	02.0	08	02.8	32	02.8	35			
VIII	760.3	21.0	26.0	22.0	22.7	27.3	18.3	32.0	09	18.3	24	06	02.3	07	02.4	08	02.1	11	02.0	05	02.0	08	02.1	21	02.7	33			
IX	763.0	19.1	23.3	20.7	21.4	26.0	17.6	28.4	22.18	18.8	24	07	02	02.5	04	02.0	13	02.4	05	02.0	01	02.0	01	02.0	17	02.2	47		
X	762.7	13.5	19.3	14.9	15.1	20.2	11.8	27.0	01	07.1	22	03	05	02.2	19	02.2	08	02.0	02	02.0	01	02.0	01	02.0	19	02.3	46		
XI	761.6	09.2	13.6	10.8	10.7	14.7	07.6	26.1	02	-03.4	25	05	02.2	09	02.8	15	01.9	33	02.4	07	02.9	01	01.6	04	01.8	05	02.6	11	
XII	764.9	07.1	11.8	08.4	08.9	12.7	04.8	19.8	09.01	08.9	21.20	03	01.6	06	02.0	16	01.9	24	02.3	04	02.2	08	01.7	09	02.4	26			
600.	761.6	13.3	16.0	14.5	15.1	19.8	11.4	32.0	02.8	-03.4	25.0	66	02.3	74	02.4	102	01.9	199	02.4	106	02.3	95	01.6	31	02.3	204	02.4	331	
		$\varphi = 44^{\circ}45' N$	$\lambda = 15^{\circ}19' E$ Gr.	$\Delta G = + 1h\ 01\ min.$																									
I	-	06.1	06.6	02.1	02.7	07.2	-01.8	12.6	19	-08.3	10	10	01.9	03	02.0	05	01.8	17	02.4	10	01.2	04	01.8	15	01.1	29			
II	-	-02.8	04.4	08.1	08.5	09.2	-03.7	11.3	28	-16.2	18	14	02.4	08	02.1	02	01.0	02	01.0	04	02.6	06	01.0	26	01.9	18			
III	-	04.3	10.4	06.1	06.6	11.3	02.1	17.2	30	-07.1	01	08	02.0	06	01.2	01	01.0	06	02.0	22	03.3	15	03.5	04	01.2	19	01.2	28	
IV	-	13.3	19.2	07.6	09.1	09.1	14.3	03.3	21.7	21	-02.1	29	15	01.9	04	01.0	05	01.4	13	03.7	10	04.0	02	02.5	25	01.6	13		
V	-	12.0	19.4	12.1	13.0	20.6	01.7	27.0	20.18	01.8	01.8	12	01.7	10	01.5	03	01.0	10	01.8	08	02.0	02	01.6	02	01.4	27			
VI	-	14.0	20.4	16.0	15.0	21.9	10.6	28.6	14	03.1	05	16	01.4	10	01.6	03	01.0	09	02.3	07	02.1	02	01.5	13	01.3	25			
VII	-	14.9	24.3	15.4	17.3	23.6	11.1	31.6	18	04.5	27	15	01.4	03	01.7	02	01.5	05	01.4	05	01.6	06	01.5	06	01.4	36			
VIII	-	14.2	22.4	15.3	16.8	23.9	10.6	28.6	10	06.0	21	21	01.5	09	01.6	03	01.0	05	01.0	02	02.0	04	01.0	16	01.5	35			
IX	-	13.3	22.0	14.5	16.3	24.2	10.8	26.2	17	06.3	25	09	01.4	06	01.0	05	01.2	13	02.2	05	01.4	03	01.0	04	01.5	25			
X	-	09.4	13.7	06.7	07.0	14.5	02.7	25.6	01	-04.6	30	20	02.0	08	02.5	06	01.2	03	02.3	07	02.0	02	01.3	02	01.3	30			
XI	-	01.0	05.4	02.6	02.9	06.6	-00.6	18.1	02	-16.3	26	18	02.3	03	02.0	04	01.3	09	03.1	01	01.0	03	02.5	03	02.2	46			
XII	-	01.6	-01.6	04.3	06.1	06.7	03.0	-03.0	12.0	17	-16.0	23	17	02.3	01	02.0	02	02.0	07	02.3	02	02.0	08	01.2	05	01.2	55		
600.	713.5	04.8	13.2	08.2	08.9	14.4	03.8	31.1	15.4	-18.3	26.0	177	02.4	80	02.6	11	01.8	99	02.3	57	02.0	70	02.2	48	02.1	54	01.7	509	
		$\varphi = 44^{\circ}33' N$	$\lambda = 15^{\circ}22' E$ Gr.	$\Delta G = + 1h\ 02\ min.$																									
I	716.2	-06.6	05.5	01.7	02.0	06.7	-01.4	11.0	16	-10.1	10	07	02.1	05	03.4	01	02.0	08	01.8	03	02.7	02	02.0	06	02.0	26	02.0	30	
II	717.0	-03.9	03.4	-06.6	-06.3	04.5	-04.4	11.0	07	-11.7	10	29	03.0	09	03.1	01	02.0	03	02.0	01	02.0	02	02.0	08	02.0	22	02.0	33	
III	707.3	03.5	09.1	05.8	06.1	10.3	01.8	15.7	09	-07.8	01	09	02.1	03	04.0	02	02.0	24	02.6	14	02.4	09	02.4	22	03.5	27	03.0	27	
IV	711.3	05.8	12.4	07.9	08.5	13.3	03.2	20.9	21	-02.1	12	10	02.6	15	02.5	00	01.4	11	02.8	10	02.9	04	02.8	04	02.2	26	01.6	13	
V	711.3	10.9	16.1	12.9	13.7	19.4	07.3	26.0	20	01.3	11.01	13	02.6	05	02.0	01	02.0	08	02.4	07	01.6	04	01.8	04	01.8	44			
VI</																													

Mesec	Oblačnost Nm (0-10)		Inhalacija broj sati: 7 14 21 Sred. (Distr.)	Vlažnost vazduha				Padavine R mm				Broj dana na sat:																
	•m	m		m	s			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ				
	mm	7		14	21	Sred.	Min	Σ	Max	Dat.	≥	<	<	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV				
PAC																												
BR. ST. 81																$H_s = 3 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$												
I	6.8	6.1	4.4	5.8	885.0	06.1	79	65	75	73	39	015	065.0	28	.	.	01	.	.	.	05	10	06	04	06			
II	4.8	3.9	3.9	4.3	101.7	04.4	60	45	58	55	20	004	002.0	14	.	.	03	.	.	.	04	02	10	08	04			
III	7.7	6.6	6.4	6.9	127.8	06.9	73	58	72	68	24	087	022.0	11	.	.	01	.	.	.	04	14	14	11	04			
IV	5.2	4.9	4.3	4.8	211.3	07.1	67	50	60	59	27	096	038.8	03	01	10	07	10	07			
V	5.4	5.5	3.4	4.7	241.1	11.1	68	54	71	64	30	106	C30.9	08	.	.	.	08	.	.	01	11	05	11	07			
VI	6.7	4.4	5.1	4.7	264.1	11.9	63	62	66	60	34	080	024.7	11	.	.	16	03	04	.	08	06	08	07	02			
VII	2.6	2.6	2.4	2.5	349.1	13.3	58	47	59	55	24	034	023.0	05	.	.	28	19	15	.	20	04	05	03	01			
VIII	4.1	4.7	3.9	4.2	256.7	12.6	60	48	61	56	30	064	C28.0	19	.	.	26	11	15	.	12	07	10	08	01			
IX	4.0	3.1	1.2	2.5	250.0	14.2	74	54	73	67	30	014	010.1	04	.	.	29	07	07	.	17	02	05	04	05			
X	5.4	4.5	3.0	4.3	189.7	08.2	74	53	67	55	32	149	045.5	13	.	.	07	02	.	.	10	06	11	04	09			
XI	5.6	5.4	4.4	5.5	102.5	04.9	72	60	64	66	25	110	055.4	11	.	.	03	.	.	.	02	07	10	09	11			
XII	5.8	5.3	3.6	4.9	093.8	05.8	73	60	72	68	29	068	037.0	18	.	.	.	03	.	.	09	09	08	07	03			
GOD. 3.2 4.7 3.8 4.6 2264.8 09.1 68 53 66 63 20												819	055.4	Hxi	.	.	08	114	42	44	14	02	123	90	103	76	23	101
ZAGAR																												
BR. ST. 82																$H_s = 3 \text{ m } H_b = 7.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$												
I	5.6	5.9	3.8	5.1	116.1	04.6	95	69	82	77	40	035	024.9	23	.	.	01	.	.	.	06	09	07	04	01	07		
II	5.9	4.6	2.1	3.3	180.0	04.7	64	54	63	62	27	019	011.7	14	.	.	01	.	.	.	02	13	02	04	03	01	04	
III	6.4	6.7	5.0	6.0	149.4	07.3	81	67	77	75	37	087	015.2	16	.	.	.	03	.	.	05	08	15	11	03	13		
IV	4.5	4.8	3.4	4.2	241.7	08.1	76	62	75	71	32	066	028.9	11	.	.	04	.	.	.	08	04	11	06	03	11		
V	5.4	5.3	3.2	4.6	263.9	12.1	82	70	79	77	34	068	047.0	08	.	.	01	.	.	.	10	04	15	07	03	15		
VI	4.3	4.5	4.0	4.5	234.1	13.4	77	64	76	73	35	087	026.6	11	.	.	12	02	.	.	10	06	09	08	03	09		
VII	2.3	3.9	1.7	2.0	353.7	13.8	73	60	77	70	28	038	021.0	01	.	.	27	04	06	02	22	03	08	06	01	08		
VIII	5.8	4.5	2.5	3.7	270.4	14.9	74	61	73	69	30	064	021.3	19	.	.	26	02	04	.	10	02	11	04	02	11		
IX	3.2	4.4	1.3	2.3	257.3	18.1	84	65	84	78	25	079	038.6	08	.	.	28	01	.	.	17	01	04	02	04	06		
X	4.2	4.6	2.4	3.4	190.7	09.7	78	59	77	71	35	204	051.3	13	.	.	04	.	.	.	14	06	11	09	06	11		
XI	6.0	6.2	3.5	5.2	115.7	07.4	78	64	73	72	19	112	023.6	11	.	.	02	.	.	.	04	08	13	09	04	13		
XII	5.4	6.2	4.6	5.4	104.7	06.8	81	67	80	76	26	085	041.3	18	.	.	.	03	.	.	09	11	06	06	03	08		
GOD. 4.6 4.7 3.2 4.1 2478.7 10.1 77 63 76 72 19												966	051.3	Hxi	.	.	03	95	86	15	15	.	132	68	118	82	34	118
BREGA LEPICE																												
BR. ST. 83																$H_s = 443 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 2.0 \text{ m}$												
I	6.3	5.5	4.2	5.4	-	04.8	87	75	85	82	62	623	008.6	28	.	.	23	.	.	.	05	09	06	05	03	02		
II	5.0	5.6	5.0	5.2	-	03.8	83	68	84	78	35	019	003.2	14	01	01	24	.	.	.	03	08	10	07	04	05		
III	7.4	6.4	5.9	6.7	-	03.7	84	62	79	76	40	098	026.7	30	.	.	07	.	.	.	04	02	01	21	14	04		
IV	4.9	6.0	4.2	5.0	-	06.2	77	57	81	71	34	102	028.4	11	.	.	07	.	.	.	05	01	07	14	04	01		
V	6.4	5.5	4.1	5.3	-	09.4	86	59	86	77	37	081	017.5	13	.	.	04	.	.	.	07	07	18	14	03	18		
VI	7.7	6.7	4.9	6.4	-	10.2	81	59	82	74	28	051	009.0	09	.	.	09	.	.	.	01	07	13	10	03	13		
VII	6.0	3.9	2.5	4.1	-	11.7	88	54	87	77	36	114	049.4	01	.	.	26	02	.	.	04	04	11	07	04	11		
VIII	7.5	6.2	4.7	6.1	-	11.3	90	59	87	79	38	134	037.5	19	.	.	13	.	.	.	01	09	16	11	04	16		
IX	8.8	3.9	2.1	4.9	-	11.7	93	63	90	82	44	054	036.8	08	.	.	08	.	.	.	01	02	06	03	02	06		
X	8.8	0.0	4.8	6.5	-	07.0	92	66	86	81	40	126	058.4	17	.	.	07	01	.	.	01	13	13	08	04	13		
XI	8.1	7.8	6.3	7.4	-	05.3	87	77	85	83	53	136	036.5	11	03	03	09	.	.	.	03	14	15	12	04	08		
XII	6.4	5.7	5.6	6.6	-	04.3	88	77	86	84	53	076	038.1	18	01	03	23	.	.	.	01	14	09	06	02	08		
GOD. 7.1 5.8 4.5 5.8												07.6	86	64	84	78	28	1014	058.4	Hxi		
GOSPIĆ																												
I	6.5	7.1	4.8	6.1	085.7	04.4	89	68	87	81	37	020	064.5	29	01	.	23	.	.	.	04	10	05	05	02	01		
II	5.6	5.9	4.5	5.3	122.4	03.4	88	58	79	75	33	019	005.3	15	03	03	25	.	.	.	02	09	08	06	04	05		
III	6.5	6.1	6.2	7.6	099.6	05.2	84	58	77	74	27	108	022.1	13	.	.	08	.	.	.	01	16	16	13	04	16		
IV	5.5	6.9	4.7	5.7	194.1	05.4	81	52	69	67	23	108	032.7	11	.	.	06	.	.	.	03	08	13	11	04	12		
V	6.3	7.0	4.1	5.8	215.8	08.5	87	54	79	73	27	120	019.5	27	.	.	03	.	.	.	05	07	16	13	05	16		
VI	7.5	6.6	5.4	6.5	188.3	10.0	84	57	84	75	38	076	041.2	13	.	.	06	.	.	.	01	07	13	10	03	13		
VII	3.5	4.7	2.9	3.7	296.7	11.6	91	53	87	77	35	056	024.6	05	.	.	19	02	.	.	12	05	09	06	02	05		
VIII	4.9	6.5	4.1	5.2	217.4	11.4	95	59	91	82	37	095	029.6	24	.	.	16	.	.	.	04	07	14	11	03	14		
IX																												

Mjesec	Oblačnost Nm (0-10)				Temperatura sati broj	Vlažnost vazduha			Padavine R mm			Broj dana na sat:																									
						U m t			R mm			Tr	Tx	Tn	Tx	Tx	Tx	Tr	F(0-12)	Nm(0-10)	R mm	●	★	▲	▲	▲	■	■	T	≡							
	7	14	21	Sred. (Dnev.)		mm	7	14	21	Sred.	Min	Max	Dat.	≤	<	<	≥	≥	≥	≥	≥	6	8	2.0	8.0	0.1	1.0	0.0	9	△	★	▲	▲	■	■	T	≡
BR. ST. 86																																					
KRUM																																					
I	5.8	6.5	4.2	5.5	136.6	04.4	78	51	73	67	22	035	010.5	25	.	.	17	04	08	04	04	01	06	84	.	
II	4.1	4.6	2.6	3.8	195.9	03.4	62	35	56	52	67	012	009.0	14	.	.	10	.	.	.	04	.	12	04	03	03	84	.	
III	7.6	7.9	6.4	7.3	129.4	05.8	76	50	67	65	12	059	010.8	11	.	.	02	02	16	12	09	03	12	83	.	
IV	5.8	6.7	3.2	5.3	214.8	05.8	68	44	60	58	07	089	057.0	11	05	04	10	07	01	10	83	.	
V	6.7	7.6	4.2	6.2	239.1	10.0	79	49	74	67	21	189	092.2	27	.	.	.	16	02	.	.	.	03	08	13	18	05	15	82	.
VI	5.5	7.4	5.0	5.9	249.4	11.4	78	54	73	68	33	098	025.3	18	.	.	.	14	04	.	.	.	04	09	13	11	01	13	82	.
VII	3.0	4.1	1.9	3.0	357.5	11.7	67	38	42	56	21	012	005.2	01	.	.	27	18	04	.	.	15	03	04	02	04	04	81	.	
VIII	5.1	6.3	3.1	4.8	245.5	11.3	71	47	65	61	29	111	039.2	30	.	.	.	25	07	01	.	.	06	04	11	09	04	11	81	.
IX	2.8	5.2	1.9	3.3	266.6	12.0	86	45	77	69	28	066	044.6	13	.	.	.	23	08	01	.	.	13	04	06	05	02	06	81	.
X	5.5	5.2	3.5	4.7	212.4	07.4	81	45	74	68	23	270	136.7	14	.	.	01	04	01	.	.	10	08	11	07	04	11	81	.	
XI	6.4	6.5	6.4	6.5	104.8	05.8	78	59	73	70	29	098	036.2	11	.	.	06	.	.	03	.	05	12	12	10	04	12	01	82	.
XII	5.0	5.1	4.1	4.7	135.4	05.1	81	56	78	72	20	083	028.8	02	.	.	13	.	.	02	.	06	07	07	03	03	07	81	.	
600. 5.3 6.1 3.9 9.1 2507.4 07.4 75 48 69 64 07 1122 136.7												Mx	.	.	49	107	37	06	09	.	85	90	110	84	28	110	01	82	58	29	.		
BR. ST. 87																																					
SIBENIK																																					
I	4.8	6.3	4.1	5.1	142.5	05.3	69	55	69	64	16	014	063.4	25	.	.	01	.	.	.	05	01	05	08	05	04	.	03	.	.	.	01	.	02	.		
II	3.8	4.2	2.6	3.5	181.5	03.7	52	38	50	47	16	019	012.6	14	.	.	04	.	.	14	09	12	02	03	02	.	03	.	.	.	01	.	03	.			
III	7.5	7.4	5.9	6.9	156.9	06.4	69	52	64	62	14	070	021.9	11	11	07	03	13	11	09	.	11	.	.	.	01	.	03	.		
IV	5.0	5.3	5.0	5.1	252.3	06.4	61	46	60	56	22	056	032.1	11	12	02	07	09	03	01	.	03	.	.	.	01	.	02	.		
V	6.2	5.9	4.5	5.5	255.0	16.3	71	53	68	64	27	062	023.5	27	.	.	07	.	.	04	01	05	10	13	08	02	13	03	.	02	.		
VI	4.6	5.8	3.7	4.7	275.6	11.3	66	51	64	60	26	041	010.5	11	.	.	17	01	02	04	01	10	07	08	04	01	06	04	.	04	.		
VII	2.3	2.2	1.6	2.1	359.8	12.1	59	57	53	57	19	025	011.1	06	.	.	28	16	08	.	.	22	04	04	03	01	09	03	.	03	.		
VIII	3.9	5.2	3.0	4.0	285.6	11.7	60	45	59	55	23	104	040.6	25	.	.	23	07	14	04	01	09	04	08	07	03	00	04	.	04	.		
IX	3.4	3.2	1.5	2.7	275.9	13.0	72	51	70	64	37	044	020.3	13	.	.	38	03	03	01	.	15	62	04	02	04	01	.	01	.			
X	5.0	4.6	4.1	4.1	203.9	08.0	49	32	47	43	29	220	076.7	14	.	.	04	.	.	06	.	12	04	11	09	07	11	01	.	02	.		
XI	6.5	6.7	5.9	6.4	116.2	06.0	71	58	65	63	24	128	037.6	11	.	.	03	.	.	10	32	04	13	17	12	04	17	01	.	01	.		
XII	5.2	5.5	4.7	5.2	134.8	05.8	61	55	70	65	23	056	017.4	19	09	05	10	08	06	06	01	.	01	.				
600. 4.9 5.3 3.8 4.6 2650.6 08.4 65 56 43 59 14 838 076.7												Mx	.	.	02	108	20	24	28	06	184	35	04	64	05	01	42	00	.				
BR. ST. 89																																					
SPLIT-HARJAN																																					
I	5.1	5.8	3.3	4.7	142.6	05.1	60	51	62	60	12	027	014.5	29	02	15	02	04	01	06		
II	3.7	4.3	3.8	3.7	193.3	03.6	44	41	46	43	17	089	008.7	14	.	.	02	.	.	11	13	C5	04	01	04	
III	7.8	7.5	6.0	7.1	140.0	06.7	67	61	67	65	27	053	017.1	11	10	03	02	14	13	08	02	13	01	02	.				
IV	5.2	5.1	4.4	4.9	231.9	06.7	50	56	56	52	25	060	027.3	11	12	02	07	08	11	07	02	11	01	03	.				
V	6.0	6.3	4.4	5.6	234.4	10.7	60	56	68	64	30	052	014.4	28	.	.	09	01	01	05	.	06	07	14	08	02	14	04	01	.			
VI																																					

Mesec	Vadudini pritisak mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																	
		Tr			Sred. (Dnev.)	M	M	N	S	Ist.	Min.	Dat.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.					
		7	14	21																									
$\varphi = 43^{\circ}43' N$ $\lambda = 16^{\circ}40' E$ Gr. $\Delta G = + 1h 07 min.$																													
I	-	-06.8	06.0	02.8	03.2	09.2	-02.5	13.6	06	-07.8	16	14	02.4	10	02.6	C2	01.0	C4	01.5	11	01.4	03	01.0	02	01.0	02	03.0	45	
II	-	01.1	09.4	03.6	04.4	10.2	-01.1	14.7	15	-08.9	10	26	03.2	26	03.3	.	06	01.2	C8	01.8	01	01.0	.	03	01.3	14	.	.	.
III	-	05.8	12.3	08.2	08.6	13.3	03.5	18.6	30.0	-06.0	01	08	02.5	06	03.3	.	18	02.9	27	02.5	09	01.7	.	.	03	01.7	22		
IV	-	09.1	16.1	10.8	11.7	16.7	04.2	23.6	21	-00.6	13	10	02.9	15	03.1	.	10	03.1	11	03.1	12	02.8	03	02.3	07	01.9	22		
V	-	14.8	21.3	15.3	16.7	22.4	10.9	25.6	18	03.4	01	10	02.1	04	02.0	C3	01.3	05	01.8	08	01.5	18	02.2	.	.	62	01.9	43	
VI	-	17.1	23.2	17.5	17.5	24.1	12.4	30.6	23	07.2	04	13	02.8	14	02.5	C2	02.0	10	01.2	12	02.1	02	01.5	05	01.6	28			
VII	-	19.3	27.2	20.7	22.0	28.6	15.7	34.3	18	11.4	02	22	02.4	19	02.6	C1	01.0	03	01.0	15	02.0	03	02.3	01	02.0	29			
VIII	-	18.5	26.1	20.0	21.1	27.0	15.7	31.4	11.10	10.9	22	26	02.1	17	02.8	C1	01.0	06	01.5	07	01.4	10	01.7	.	.	07	01.4	18	
IX	-	14.6	26.1	18.1	19.3	26.9	12.7	34.1	17	09.2	25	03	01.7	C1	01.0	C3	01.0	07	01.9	03	02.0	14	01.5	04	02.0	01	02.0	36	
X	-	09.2	18.3	11.8	12.8	19.4	07.2	27.7	03	-00.5	31	28	01.8	15	02.3	C1	01.0	04	02.0	13	01.6	06	01.5	28	
XI	-	04.6	11.3	07.1	07.6	12.3	02.8	20.3	04	-09.3	26	15	02.6	12	02.9	C2	01.9	12	02.5	11	02.5	04	01.5	34	
XII	-	01.5	10.0	04.0	04.9	10.7	00.2	14.7	02	-04.8	31	15	02.2	13	02.5	.	07	02.1	11	01.8	02	01.5	45		
600.	-	09.6	17.4	11.7	12.6	18.4	07.0	34.3	46.W	-09.3	26.XI	190	02.4	152	02.8	15	01.3	89	02.2	113	02.0	184	01.9	14	01.9	37	01.7	261	
$\varphi = 43^{\circ}01' N$ $\lambda = 17^{\circ}34' E$ Gr. $\Delta G = + 1h 10 min.$																													
I	-	08.2	10.4	07.0	06.9	11.8	01.5	15.7	27	-01.4	19.11	15	C3.9	C8	03.2	10	02.9	56	02.8	02	01.5	02	02.5	.	.	.	03	02.7	
II	-	08.1	10.9	06.4	06.7	13.0	00.9	15.4	22	-02.5	10	18	03.4	21	03.1	11	02.7	31	02.7	03	02.7	
III	-	09.6	15.3	11.8	12.1	16.4	07.8	22.0	12.08	01.5	22	03	04.0	C2	03.0	C8	03.0	49	03.1	01	05.0	09	03.0	01	03.0	.	03	02.6	
IV	-	12.9	20.3	15.5	16.1	21.5	11.2	26.6	30	04.2	09	01	05.0	05	03.2	.	49	03.3	02	04.5	18	03.2	14	03.1	05	03.6	.		
V	-	14.9	24.2	17.9	18.7	25.3	12.1	30.0	19	07.9	08	03	03.3	51	02.7	03	04.3	17	02.4	17	02.6	02	02.5	.	
VI	-	16.8	25.8	21.5	21.9	27.3	15.8	32.4	27	12.8	07	07	03.7	05	02.6	05	01.8	31	02.5	.	.	12	02.7	27	02.2	03	02.7	.	
VII	-	21.4	29.5	24.3	24.9	30.3	16.5	35.3	18	12.5	02	03	02.7	06	03.0	10	02.3	18	02.3	.	.	13	02.3	36	02.5	07	02.9	.	
VIII	-	19.6	27.2	23.0	23.2	26.8	17.6	32.0	11	08.7	25	01	04.0	06	03.2	02	03.0	36	02.6	03	02.3	13	02.5	23	02.6	04	02.7	.	
IX	-	16.3	27.0	21.8	22.2	28.4	14.4	32.8	16	12.8	26	01	02.0	04	02.8	C5	02.6	39	02.8	05	02.8	15	02.4	20	02.6	01	02.0	.	
X	-	13.1	19.7	16.2	16.3	21.6	10.9	26.2	03	-04.7	31	08	03.0	13	02.5	10	03.0	32	02.8	04	03.0	12	02.2	13	02.9	01	03.0	.	
XI	-	07.4	13.4	10.3	10.4	14.3	05.8	22.2	03	-03.7	26	06	03.5	14	02.9	06	02.8	51	02.4	07	03.6	05	02.4	01	02.0	.	.	.	
XII	-	03.7	11.2	06.0	06.8	12.7	02.4	18.2	04	-01.3	10	.	.	13	02.8	34	02.6	41	02.5	01	02.0
600.	-	12.2	19.6	15.1	15.5	21.0	10.1	35.9	46.W	-03.7	26.XI	63	03.5	57	02.9	104	02.1	503	02.8	27	03.3	120	02.6	153	02.6	28	02.9	.	
$\varphi = 42^{\circ}24' N$ $\lambda = 16^{\circ}16' E$ Gr. $\Delta G = + 1h 05 min.$																													
I	751.3	09.4	11.3	10.0	10.2	12.1	08.9	14.0	27.06	06.4	09	14	C5.0	C5	02.2	C1	03.0	06	03.3	14	03.6	10	01.8	05	03.0	28	03.1	10	
II	750.3	08.3	10.5	08.8	09.2	11.4	04.2	14.3	02	02.6	09	16	C4.1	15	04.9	C7	04.6	07	04.7	08	03.6	01	02.0	06	04.8	19	03.9	05	
III	747.9	10.6	13.0	11.7	11.7	13.8	05.7	17.6	31	06.0	24	06	03.8	06	03.8	04	02.8	22	05.4	35	04.5	08	03.2	03	02.7	08	04.8	01	
IV	751.6	12.6	15.6	12.7	13.4	16.6	10.9	20.4	23.22	07.8	11	22	04.3	03	05.0	C1	03.0	05	04.2	21	04.4	07	04.1	07	02.3	16	04.1	04	
V	750.9	16.3	19.6	17.2	17.7	20.5	14.9	24.5	23	12.0	13.04	C8	02.9	02	02.5	C7	03.0	17	03.9	18	03.8	04	03.0	07	03.1	23	03.8	07	
VI	751.2	19.0	22.7	19.9	20.6	24.0	17.2	31.9	30	14.5	12.06	17	03.6	04	02.2	C1	01.0	06	03.7	16	03.2	07	03.9	37	04.6	02			
VII	751.2	22.4	25.6	22.4	23.2	26.8	20.6	32.0	18	15.6	02	14	04.6	04	01.5	C1	03.0	04	04.2	08	02.8	01	04.0	10	03.9	41	04.4	10	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
600.	-	13.9	16.8	14.3	15.4	20.0	11.0	35.5	46.W	-03.5	28.II	98	02.3	54	01.9	277	01.1	338	02.6	30	01.8	06	02.7	136	02.7	136	02.6	20	
$\varphi = 42^{\circ}58' N$ $\lambda = 16^{\circ}43' E$ Gr. $\Delta G = + 1h 07 min.$																													
I	-	04.7	11.9	06.5	07.4	12.8	02.8	16.3	06	-02.9	10	12	02.8	08	01.4	36	03.0	19	02.0	03	01.0	.	.	03	02.0	12	02.3	.	
II	-	04.3	11.4	06.4	07.1	12.3	02.7	13.5	02	-03.5	28	09	02.9	15	02.5	30	01.4	12	02.0	03	01.0	.	.	04	02.5	11	02.5	.	
III	-	10.2	14.1	11.2	11.7	15.1	06.6	18.4	31	-01.5	23	06	02.2	G2	02.5	16	01.4	58	03.3	03	02.0	.	.	01	03.0	07	03.0	.	
IV	-	12.7	17.0	12.4	13.6	18.0	01	23.8	23.22	04.5	13	12	02.8	02	03.0	17	01.0	24	04.1	09	01.4	03	02.7	07	03.4	17	02.6	01	
V	-	17.9	21.0	17.2	18.3	22.1	10.1	29.0	19	08.4	01	03	02.0	01	01.5	18	01.1	34	02.8	03	01.7	.	.	.	16	02.8	14	02.6	03
VI	-	20.8	24.2	20.0	21.3	23.9	17.2	31.7	29	11.3	07	11	02.7	03	01.0	08</td													

Mesec	Vremenski pristisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																	
		Tm			Sred. (°C)	Max	Min	Max	Dat.	M/S	Dat.	N		NE		E		SE		S		SW		W		NW			
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.				
$\varphi = 42^{\circ}58' N \lambda = 17^{\circ}09' E$ Gr. $\Delta G = +1h\ 12\ min.$																													
I	-	07.6	11.3	08.4	09.0	12.0	05.1	14.0	06	-01.4	10	02	02.5	04	02.8	18	02.1	17	01.6	09	01.0	17	01.1	24	01.3	02	03.0		
II	-	07.2	11.0	08.5	08.8	11.2	04.4	15.8	08	-01.2	13	08	02.5	09	04.3	36	03.2	03	02.0	04	01.2	08	01.0	15	01.3	01	02.0		
III	-	11.0	13.7	11.6	12.0	14.3	08.1	17.4	08	01.0	23	01	02.0	06	04.2	41	02.7	31	02.1	03	01.0	05	01.2	04	01.5	02	03.0		
IV	-	13.9	16.4	13.2	14.3	17.2	11.0	22.4	23	07.4	03	03	02.3	07	03.1	25	02.4	17	01.8	02	01.5	03	01.0	27	01.3	04	01.8		
V	-	18.2	20.3	17.5	18.4	22.6	15.8	24.5	19	11.8	01	.	.	03	01.7	37	02.0	22	01.7	01	01.0	06	01.2	23	01.7	01	03.0		
VI	-	21.4	24.0	20.1	21.4	25.2	18.4	31.5	26	15.0	06	02	02.5	04	02.8	20	02.2	16	01.5	.	03	01.3	35	01.4	16	02.1	.		
VII	-	24.3	27.4	23.2	24.5	28.7	20.7	33.7	17	14.5	02	02	03.5	04	02.0	19	02.1	09	01.0	01	03.0	18	01.6	38	02.0	10	01.6		
VIII	-	23.0	26.0	22.4	23.4	27.3	19.3	31.0	01	12.4	24	01	02.0	02	02.5	24	02.0	16	01.5	04	01.2	10	01.5	29	01.9	07	01.9		
IX	-	22.2	25.7	21.6	22.8	26.6	19.4	31.0	18	16.7	13	01	01.0	01	01.0	26	02.5	16	01.8	01	01.0	09	01.1	34	01.7	04	01.8		
X	-	16.0	19.6	14.5	17.1	20.5	13.4	27.5	03	05.6	19	01	01.0	04	03.8	26	03.1	14	02.3	07	01.3	12	01.1	26	01.4	03	02.3		
XI	-	11.6	14.1	12.0	12.5	15.3	09.7	20.1	04	06.3	25	02	02.0	07	04.4	38	02.3	17	02.0	10	01.0	10	01.1	05	01.4	01	02.0		
XII	-	08.2	12.3	09.9	10.3	13.7	07.7	17.5	18	03.1	22	.	02	04.5	15	01.9	23	01.6	11	01.3	16	01.0	20	01.0	06	01.5	.		
GOD.	-	18.5	18.9	19.4	18.2	19.6	12.6	33.7	77.W	-01.4	10.1	23	02.3	53	03.4	319	02.4	165	01.8	53	01.2	111	01.2	282	01.5	37	01.9	02	
$\varphi = 42^{\circ}58' N \lambda = 17^{\circ}10' E$ Gr. $\Delta G = +1h\ 09\ min.$																									DREBICE		BR. ST. 97		
I	-	06.0	12.1	06.6	07.8	12.6	04.1	14.8	06	-02.1	10	33	01.4	17	02.4	C1	02.0	16	02.4	03	01.3	06	02.5	06	02.7	07	01.4	04	
II	-	06.2	11.4	07.5	08.2	12.3	04.7	15.0	06	-01.0	20.10	14	01.6	49	03.5	04	02.5	09	02.4	01	02.0	02	03.0	04	02.0	05	02.0	.	
III	-	10.4	13.9	11.3	11.8	14.4	08.9	19.4	08	08.9	01	15	01.2	18	02.3	04	02.5	41	03.0	05	03.2	03	03.3	02	02.9	05	01.4	.	
IV	-	13.6	17.1	12.0	13.7	17.9	09.6	22.7	23	04.6	13	15	01.5	21	03.0	C5	02.0	25	02.4	02	02.0	06	02.7	10	02.7	02	02.0	04	
V	-	17.8	20.9	17.0	18.2	21.8	14.1	27.2	19	08.0	01	15	01.3	10	02.4	10	02.2	25	02.2	02	02.0	09	02.1	16	02.8	06	02.0	06	
VI	-	20.8	24.0	19.9	21.4	25.7	17.0	32.1	26	13.7	09	13	01.9	15	02.5	C5	02.2	16	02.2	03	01.3	12	02.9	14	03.0	07	02.3	03	
VII	-	24.0	28.1	22.4	24.2	29.0	19.3	32.1	03	16.0	23	11	01.3	20	02.5	01	01.0	22	02.0	03	01.5	10	03.3	13	02.7	06	01.7	05	
VIII	-	22.9	27.0	22.8	23.7	27.9	20.0	31.5	09	18.4	23	15	01.9	23	02.9	03	02.7	18	02.1	.	08	03.1	15	02.4	03	01.3	08		
IX	-	20.9	26.0	20.1	21.9	27.0	17.0	31.4	18	15.0	25	20	01.2	15	02.5	C5	02.0	23	02.1	01	02.0	06	02.7	09	02.9	02	01.8	09	
X	-	15.1	20.1	19.1	16.4	21.1	12.7	27.6	03	08.0	27	16	01.6	32	02.4	C4	03.0	11	02.7	04	02.5	06	02.8	07	02.1	07	01.7	06	
XI	-	11.1	14.7	11.4	12.2	15.4	09.1	21.2	03	-01.2	24	14	01.2	30	02.9	C3	03.3	25	02.8	01	02.0	04	02.5	02	02.0	03	01.7	06	
XII	-	08.2	13.0	08.8	09.7	13.9	06.3	17.4	03	00.6	08	24	01.2	29	02.7	C1	03.0	13	03.2	01	03.0	04	02.5	07	02.1	09	01.4	03	
GOD.	-	14.0	19.1	14.4	15.6	20.0	12.0	32.1	22.W	-02.1	10.1	205	01.4	275	07.8	46	02.4	244	02.5	25	02.2	80	02.8	104	02.6	62	01.7	54	
$\varphi = 42^{\circ}50' N \lambda = 17^{\circ}42' E$ Gr. $\Delta G = +1h\ 11\ min.$																									STON		BR. ST. 98		
I	-	08.7	11.3	04.3	05.9	12.0	06.5	14.7	20	-04.2	11	27	C2.3	09	01.9	C1	C1.0	C8	02.4	C1	01.0	03	01.7	05	01.2	09	01.4	30	
II	-	09.1	10.8	06.4	07.2	12.0	02.3	15.3	05	-04.3	10	38	C2.9	04	02.2	C2	C1.5	03	02.7	03	01.0	04	01.8	02	01.0	07	02.7	21	
III	-	05.9	13.8	11.3	11.7	14.9	07.3	19.4	30	-03.4	01	10	02.4	04	02.5	07	02.4	42	03.8	02	02.5	02	01.0	03	02.3	21	.		
IV	-	12.9	17.1	12.4	18.7	20.8	08.7	23.3	24	01.0	13	19	C2.7	05	01.6	C3	C2.7	24	03.8	01	02.0	05	02.2	01	04.0	11	02.4	21	
V	-	17.2	21.0	16.8	17.9	22.2	12.9	26.5	19	08.4	11	17	01.7	04	01.5	C5	02.4	25	02.8	C3	02.3	01	01.0	05	01.6	05	04.2	28	
VI	-	20.6	24.2	19.8	21.1	25.5	16.1	32.5	26	12.2	09	28	02.7	02	02.0	C5	02.4	16	02.9	02	01.0	04	01.8	07	01.7	04	02.0	22	
VII	-	23.8	28.0	22.5	24.2	29.3	18.4	35.0	17	18.0	25.01	32	02.1	04	01.2	C5	02.2	10	02.5	05	02.2	04	02.2	01	01.0	13	02.0	19	
VIII	-	23.0	27.1	23.4	28.4	28.4	18.6	33.0	01	12.6	23	36	01.9	04	02.5	.	15	02.5	04	03.0	03	02.7	03	02.3	06	02.5	22		
IX	-	18.0	26.0	20.3	21.4	27.2	16.4	32.0	17	11.0	26	21	01.7	02	02.5	C4	02.2	16	02.2	C4	01.8	05	C1.8	04	01.0	03	02.0	29	
X	-	14.3	19.9	14.2	15.7	21.2	11.2	29.0	03	02.02	05.3	31	36	C2.2	04	02.2	C1	C5.0	17	03.5	05	01.6	04	02.8	04	01.0	02	02.5	20
XI	-	09.9	13.8	10.5																									

Meseč	Oblačnost Nm (0-10)				Inzolacija broj sati	Vlažnost vazduha				Padavine R mm				Broj dana na sat																	
	7	14	21	Sred. (Dnev.)		7	14	21	Sred.	Σ	R _{av}	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(O-12)	Nm(0-10)	R mm	•	+	*	Δ	▲	▲	R	T	≡	■
						mm	mm	mm	mm	mm	mm	mm	0.00.0	0.025.0	0.020.0	0.06	0.8	2.0	6.0	0.1	1.0	0.0	•	Δ	*	Δ	▲	▲	R	T	≡
KROŠČULA																															
BR. ST. 96																															
I 4.2 4.7 3.5 4.1	-	06.1	73 55 74 65 10	014 008.4	09	.	.	.	01	12	07	03	03	03
II 3.0 3.5 2.5 3.0	-	04.8	59 48 58 55 20	029 015.4	14	.	.	.	01	08	.	16	05	07	04	01	07	01	.	.
III 7.5 7.3 6.5 7.1	-	07.9	77 66 77 74 34	172 027.6	10	02	.	04	16	17	12	07	17	02	.	03	.	
IV 4.8 4.6 2.9 4.1	-	07.7	64 57 67 62 30	038 009.4	01	02	.	08	05	07	07	07	07	02	.	02	.	
V 5.3 5.1 3.4 4.8	-	11.5	76 65 77 74 38	038 009.4	14	.	.	.	03	09	08	08	09	09	02	01	.	.
VI 3.8 3.7 3.3 3.6	-	13.5	68 62 74 68 30	004 003.0	17	.	.	.	18	01	07	03	.	11	03	03	01	03	03	.	.	.		
VII 2.2 1.5 1.2 1.6	-	14.6	65 56 66 62 34	010 004.8	06	.	.	.	27	12	23	.	.	24	03	04	03	04	01	01	.	.		
VIII 3.3 4.1 2.8 3.4	-	13.8	65 59 67 64 32	274 071.3	26	.	.	.	24	05	14	01	.	12	02	08	07	06	08	04	.	.	.		
IX 2.5 2.4 1.7 2.2	-	14.8	74 61 76 70 37	042 018.5	13	.	.	.	24	02	12	01	.	21	02	03	02	03	02	.	.	.		
X 4.5 5.0 3.4 4.3	-	10.3	72 61 73 69 30	249 046.3	17	.	.	.	04	.	01	04	.	12	07	13	12	08	13	01	00	.	.		
XI 5.9 6.7 5.9 6.2	-	08.3	75 67 78 73 29	158 032.0	29	03	.	05	10	13	13	06	13	01	03	.	.		
XII 4.5 4.5 4.1 4.4	-	06.1	76 63 74 71 31	066 020.1	17	03	.	15	03	07	05	03	07	02	.	.	.		
GDH. 4.3 4.4 3.4 4.1	-	10.8	70 60 71 67 10	1096 071.3	SLW	.	.	.	02	102	20	27	27	.	.	.	96	81	33	96	04	.	34	01	.		
CNEBIC																															
BR. ST. 97																															
I 3.9 4.5 3.6 4.0	-	03.4	19 56 76 69 14	022 009.9	09	.	.	.	01	01	.	14	06	05	04	05	01	.	.	
II 3.4 3.6 3.2 3.4	-	04.2	56 44 51 50 20	033 026.3	14	.	.	.	03	01	.	15	03	04	01	04	01	05	.	.	
III 7.9 7.1 6.9 7.3	-	07.7	77 66 73 72 30	154 024.7	13	02	15	16	12	07	16	01	05	.	.		
IV 5.0 3.9 4.1 4.3	-	07.5	64 54 70 63 31	030 011.0	11	04	03	08	07	01	08	01	.	.	.			
V 5.2 5.5 4.7 5.1	-	11.6	77 65 76 73 33	034 008.9	15	.	.	.	01	01	.	10	10	10	07	10	02	.	.		
VI 3.8 4.1 4.0 4.0	-	12.8	68 58 68 65 31	005 004.7	17	.	.	.	16	02	02	.	.	09	01	01	01	01	01	01	.	.		
VII 2.2 1.7 1.5 1.8	-	13.7	61 53 63 59 30	008 003.7	01	.	.	.	28	12	15	.	.	23	02	03	03	03	01	.	.	.		
VIII 3.3 3.3 2.8 3.1	-	13.7	64 58 65 63 29	316 118.7	27	.	.	.	27	06	13	.	.	12	02	08	08	07	08	03	.	.	.		
IX 2.8 2.2 1.9 2.3	-	14.5	76 61 78 72 38	098 040.3	12	.	.	.	30	01	04	.	.	19	02	04	04	04	04	02	.	.	.		
X 4.0 4.9 3.8 4.2	-	11.1	77 73 79 76 33	269 056.4	17	.	.	.	04	13	08	12	12	05	12	04	.	.	.		
XI 6.5 7.0 6.5 6.7	-	08.3	77 67 75 73 30	202 043.4	29	.	.	.	01	03	12	16	15	06	14	01	.	.	.		
XII 4.3 4.4 3.3 4.0	-	04.6	74 62 73 70 26	672 023.1	18	740	14	07	07	05	03	07	01	.	.	.		
GDH. 4.4 4.4 3.9 4.2	-	09.8	78 99 70 67 14	1293 115.7	27V	.	.	.	05	107	21	34	61	740	143	75	100	84	38	100	02	21	.	.	
STON																															
BR. ST. 98																															
I 3.5 4.0 2.7 3.4	-	03.2	83 28 78 73 35	024 014.8	29	.	.	.	12	02	.	15	03	04	04	01	04	02	.	01	.	
II 3.2 3.1 2.2 2.8	-	04.6	67 52 60 60 25	030 006.4	12	.	.	.	07	03	02	18	04	07	07	07	07	01	.	.	.	
III 7.0 6.4 5.9 6.4	-	07.6	78 65 72 72 24	169 076.6	14	.	.	.	03	07	03	11	15	15	05	15	02	.	02	.		
IV 4.8 3.9 3.3 3.9	-	07.1	67 52 65 61 30	036 041.8	02	02	.	10	07	08	08	03	08	02	.	02	.		
V 5.8 4.2 3.8 4.6	-	11.6	80 65 76 74 31	053 014.8	14	.	.	.	04	.	02	.	.	04	03	09	09	07	02	06	02	.	.	.		
VI 3.5 3.3 3.7 3.5	-	12.6	69 57 71 65 33	033 026.5	21	.	.	.	19	02	04	01	.	10	01	04	04	01	04	01	02	.	02	.		
VII 1.9 1.4 1.4 1.6	-	13.8	63 49 68 60 26	024 020.3	06	.	.	.	28	15	08	.	.	23	02	03	02	01	03	07	01	01	.	.		
VIII 3.3 3.2 2.8 3.0	-	13.4	69 53 63 66 33	197 101.4	24	.	.	.	28	10	01	.	.	12	01	07	07	03	07	07	03	.	03	.		
IX 2.6 2.1 1.4 2.0	-	14.6	85 62 82 82 36	090 033.5	12	.	.	.	25	03	03	.	.	19	01	04	03	05	05	05	01	01	.	.		
X 4.2 4.2 3.0 3.8	-	10.0	76 62 80 72 32	280 087.6	21	.	.	.	03	.	02	.	.	01	13	03	12	12	07	12	01	01	.	.		
XI 5.6 5.5 5.3 5.4	-	08.3	83 68 83 78 24																												

Mjesec	Vrstdunini pričesak mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nD, fm (0-12)																				
		fm				N	NE	N	NE	N	NE	E	SE	S	SW	W	NW	C												
		7	14	21	Sred. (Dnes)	N	NE	N	NE	N	NE	E	SE	S	SW	W	NW	C												
$\varphi = 45^{\circ}13' N$ $\lambda = 16^{\circ}54' E$ Gr. $\Delta G = + 1h\ 08\ min.$																														
I	-	-00.9	07.4	01.4	02.3	08.0	-02.3	15.0	18	-07.8	10	02	02.0	01	02.0	17	02.2	03	02.0	11	02.4	08	02.1	03	02.0	31				
II	-	-02.2	06.0	00.5	01.2	06.3	-03.5	14.5	12	-08.4	11	08	02.9	09	02.9	19	02.0	05	02.2	04	02.2	16	02.3	07	02.3	22				
III	-	03.5	13.0	07.6	07.9	14.0	01.9	19.0	19	-06.4	01	10	02.8	02	03.0	13	02.5	05	02.6	05	02.2	08	02.2	11	02.5	06	02.3	33		
IV	-	07.8	15.5	09.8	10.7	16.4	05.0	25.0	06	00.8	19	14	03.1	05	03.0	06	02.2	04	02.2	08	02.6	16	02.2	07	02.3	04	02.8	26		
V	-	14.3	21.1	15.4	16.5	21.8	10.3	27.5	18	02.0	02.01	06	02.7	05	03.2	10	02.4	08	02.4	05	02.4	10	02.3	08	02.2	19	02.4	22		
VI	-	16.1	21.5	16.9	17.9	22.9	12.7	30.0	28	05.2	07	17	02.8	01	02.0	15	01.8	06	02.0	04	02.5	12	02.2	16	02.6	25				
VII	-	17.5	24.6	18.9	20.0	25.3	14.2	30.0	18.15	06.2	27	05	03.2	01	02.0	11	01.7	03	02.3	04	02.0	11	02.0	18	02.1	09	02.0	31		
VIII	-	16.5	23.3	17.2	18.6	23.4	13.2	28.0	18.10	07.2	28	15	02.1	04	02.2	07	02.0	03	02.7	04	01.8	12	01.9	06	01.7	03	02.0	39		
IX	-	14.0	24.3	18.1	17.8	24.6	12.1	29.0	17	08.0	14	04	01.8	02	02.0	12	02.2	05	02.0	03	02.0	13	02.3	07	01.9	02	02.0	42		
X	-	07.5	14.0	08.5	09.6	14.5	05.9	27.0	01	-08.4	28.27	14	02.0	-	-	11	01.6	03	01.7	01	01.0	09	01.9	03	01.7	07	01.9	45		
XI	-	02.6	06.9	04.1	04.4	07.6	01.1	15.5	02	-11.0	26	11	02.3	04	02.2	17	01.8	10	01.7	02	01.5	04	02.0	02	01.5	06	02.0	34		
XII	-	-00.8	03.8	00.4	00.9	04.2	-02.1	14.5	01	-06.4	23	11	02.0	04	01.8	12	01.7	08	01.9	05	02.0	05	02.0	07	02.0	36				
600.	-	08.0	19.1	09.8	10.6	19.8	09.7	30.0	16.15	07.11.0	26.XI	117	02.5	38	02.6	130	02.0	63	02.1	56	02.1	125	02.2	91	02.1	09	02.2	386		
$\varphi = 45^{\circ}00' N$ $\lambda = 17^{\circ}55' E$ Gr. $\Delta G = + 1h\ 12\ min.$																						CERVENTA		BR. ST.102						
I	-	-01.1	07.3	00.7	01.9	07.8	-02.4	14.8	18	-07.6	10	01	01.0	03	01.3	01	01.0	52	
II	-	-02.3	05.9	00.2	01.0	06.4	-03.4	15.0	12	-09.0	10	01	01.0	03	01.3	01	01.0	66	
III	-	03.8	14.1	07.3	08.1	15.3	01.9	19.4	09.03	-04.5	01	01	01.0	03	01.7	07	01.3	01	01.0	.	.	.	05	01.2	.	.	.	76		
IV	-	08.1	16.4	09.9	11.1	17.2	05.0	28.2	06	01.0	20	01	01.0	07	01.1	.	.	.	02	01.5	02	01.5	07	01.3	04	01.2	45			
V	-	14.3	21.7	15.3	16.7	22.4	10.9	27.4	22.18	04.0	01	.	.	.	05	01.2	03	01.3	01	02.0	07	01.0	01	01.0	76	
VI	-	16.4	22.0	17.6	18.6	23.7	13.8	30.0	15	07.5	07	.	.	.	07	01.1	04	01.0	06	01.0	08	01.0	91	
VII	-	18.1	25.4	19.3	20.5	26.0	15.0	31.0	18	05.0	28	.	.	.	06	01.0	03	01.8	02	01.8	02	01.8	82
VIII	-	17.1	24.0	18.1	19.3	24.7	14.7	29.0	18.11	10.5	19	.	.	.	04	01.2	02	01.0	01	01.0	05	01.0	06	01.0	78	
IX	-	14.4	29.2	16.8	18.3	25.4	12.3	30.4	14	07.5	10	.	.	.	02	01.0	06	01.0	02	01.0	.	.	.	82	
X	-	08.3	14.8	09.6	10.6	15.4	04.5	27.4	01	00.9	31.28	.	.	.	03	01.3	07	01.1	02	01.0	.	.	.	81		
XI	-	02.3	07.3	03.7	04.3	07.6	01.1	14.4	02	-11.5	26	.	.	.	01	02.0	04	01.0	01	01.0	.	.	.	85	
XII	-	-00.4	03.9	00.3	01.0	04.6	-02.2	10.6	28	-08.8	21	.	.	.	01	01.0	07	02.1	04	01.0	01	01.0	.	.	.	92
600.	-	08.2	19.7	09.9	11.0	18.4	06.1	31.0	18.15	07.11.5	26.XI	02	01.0	52	01.3	31	01.1	02	01.0	02	01.5	04	01.3	29	01.1	27	01.2	946		
$\varphi = 44^{\circ}49' N$ $\lambda = 15^{\circ}53' E$ Gr. $\Delta G = + 1h\ 04\ min.$																						BIMAC		BR. ST.103						
I	744.3	03.2	09.7	05.0	05.5	09.8	C1-C	16.1	06	-04.6	10	02	03.5	01	01.0	02	03.0	17	03.2	15	01.9	20	02.4	07	02.1	12	01.2	17		
II	744.3	-01.9	04.7	01.0	01.2	05.7	-03.1	15.2	07	-13.2	10	03	01.0	07	02.1	05	01.8	05	03.4	11	01.6	12	01.2	11	01.5	09	01.7	21		
III	735.1	05.2	11.3	07.9	08.1	12.7	03.7	15.0	08	-03.2	25	01	05.0	03	01.3	06	03.2	22	03.4	09	03.0	21	01.9	17	01.5	06	02.7	08		
IV	735.0	08.0	14.6	10.4	10.8	16.1	05.3	25.4	06	00.4	26	04	01.5	02	02.0	06	02.0	22	02.3	11	02.8	16	02.4	08	01.1	10	01.4	11		
V	738.6	13.1	19.6	15.2	15.8	21.7	10.4	27.4	22.18	04.0	01	03	01.0	04	01.5	12	01.7	12	01.2	10	02.4	10	01.6	18	01.1	10	01.4	22		
VI	738.4	19.1	20.3	16.2	17.0	22.3	12.6	30.4	28	04.0	06	03	01.7	07	01.4	18	02.0	10	01.5	16	01.6	15	01.2	09	01.0	10	01.2	12		
VII	739.4	16.2	24.3	18.5	19.4	24.1	13.5	33.6	18	07.4	27	05	01.2	04	01.2	05	01.2	11	01.8	09	01.1	15	01.1	09	01.2	24				
VIII	740.0	15.2	22.8	17.3	18.2	24.4	13.4	30.6	15	06.2	21	04	01.2	04	01.2	07	01.4	14	01.5	02	01.0	16	01.0	10	01.0	10	01.0	27		
IX	742.9	14.7	23.6	17.1	18.2	25.1	12.9	30.4	29	07.8	14	03	01.3	03	01.7	06	01.2	14	01.3	14	01.5	13	01.3	11	01.6	01	01.0	25		
X	743.3	07.3	14.4	08.8	09.8	15.1	06.0	29.0	01	-01.2	27	06	01.5	02	01.0	07	01.3	02	01.5	09	01.1	14	01.1	10	01.1	09	01.2	34		
XI	742.2	02.9	07.0	04.6	04.8	09.3	01.4	22.2	02	-13.6	25	06	01.5	03	02.0	01	01.0	09	02.6	08	02.0	21	01.0	18	01.1	01	02.0	23		
XII	745.1	00.2	04.3	01.2	01.7	05.7	-01.7	15.6	17	-07.2	20	04	01.0	03	01.7	01	01.0	07	02.1	04	01.5	15	01.1	17	01.1	01	01.1	24		
600.	-																													

Mesec	Oblačnost Nm (0-10)				Inkolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																					
	7	14	21	Sred. (Dies)		mm	7	14	21	Sred.	Min	Σ	Max	Dat.	-30.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.00.0.0	,	Δ	Δ	Δ	Δ	R	T	≡		
						mm	7	14	21	Sred.	Min	Σ	Max	Dat.	-30.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.00.0.0	,	Δ	Δ	Δ	Δ	Δ	Δ	Δ		
BOSANSKA DUBICA																																	
BR. ST. 101																																	
I	9.3	6.2	4.6	6.7	-	-	-	-	-	-	020	009.5	29	.	.	27	.	.	.	01	12	04	04	-	04	05			
II	6.7	5.3	4.1	6.0	-	-	-	-	-	-	018	006.7	21	.	.	22	.	.	.	01	04	09	06	04	03	02	04	01	
III	6.6	8.0	5.1	7.2	-	06.5	94	64	83	80	33	033	012.0	08	.	.	10	.	.	.	01	12	10	09	01	10	
IV	6.5	6.6	3.9	5.7	-	07.4	90	60	83	78	26	072	034.0	11	.	.	01	.	.	.	05	09	10	09	01	10	
V	6.0	7.2	4.6	5.9	-	11.5	88	66	87	81	40	118	022.5	24	.	.	10	.	.	.	01	03	09	13	13	05	13	01	01
VI	6.4	6.9	5.8	6.4	-	12.7	89	64	88	81	39	032	013.0	25	.	.	12	01	.	.	02	02	10	07	06	01	07
VII	4.8	4.4	3.4	4.2	-	14.7	93	65	91	83	46	126	034.5	22	.	.	21	02	.	.	07	07	10	10	05	10	05	.	
VIII	6.9	6.2	5.1	6.1	-	14.3	94	72	95	87	50	092	018.0	24	.	.	15	.	.	.	05	08	11	11	03	11	04	
IX	8.0	3.8	1.6	4.5	-	13.6	97	68	96	87	49	039	014.4	08	.	.	14	.	.	.	04	01	04	06	01	04	34	
X	9.5	7.4	6.8	7.9	-	08.3	86	75	95	89	39	105	041.4	14	.	.	02	01	.	.	01	18	11	09	02	11	20	
XI	9.5	9.1	7.0	8.5	-	06.0	95	87	96	93	56	063	020.3	11	01	01	11	.	.	.	02	22	09	08	02	08	01	14	
XII	9.7	7.3	5.2	7.4	-	04.6	94	85	96	92	46	020	008.2	18	.	09	20	.	.	.	01	14	04	04	04	04	10	
BR. ST. 102																																	
DERVENTA																																	
I	9.2	5.2	5.0	5.1	-	04.6	93	72	93	86	41	036	018.3	29	.	.	27	.	.	.	09	09	06	04	01	01	01	01	
II	9.4	4.7	4.0	4.7	-	04.8	90	62	90	81	28	014	007.5	21	.	.	21	.	.	.	10	09	03	04	03	03	01	01	02
III	9.9	6.6	6.0	6.1	-	05.8	88	48	83	73	22	038	015.0	14	.	.	04	.	.	.	04	11	12	06	01	12	03	03	
IV	6.8	6.2	6.0	6.3	-	07.0	82	54	82	73	21	084	022.5	11	.	.	02	.	.	.	06	13	14	11	02	14	
V	5.5	5.4	5.3	5.4	-	11.6	90	41	89	80	40	128	038.4	28	.	.	12	.	.	.	08	09	15	11	04	15	01	04	
VI	6.8	6.6	6.3	6.8	-	13.4	89	45	91	82	48	075	020.7	04	.	.	17	01	.	.	05	16	12	04	15	03	03		
VII	4.0	3.2	3.4	3.6	-	14.6	90	40	91	80	46	111	027.0	02	.	.	22	03	.	.	01	01	13	04	08	04	09	03	02
VIII	6.2	6.1	5.6	6.0	-	14.3	92	67	93	84	48	156	024.8	26	.	.	14	.	.	.	04	09	18	16	07	18	05	05	
IX	5.9	2.5	2.2	3.5	-	13.3	96	59	95	84	39	050	027.7	08	.	.	20	02	.	.	11	02	07	02	02	07	17		
X	6.1	6.4	6.6	7.1	-	08.7	96	74	95	88	41	075	023.5	14	.	.	01	.	.	.	04	16	13	13	02	13	16		
XI	7.8	7.7	6.7	7.4	-	05.9	94	82	94	90	37	066	019.5	11	01	01	10	.	.	.	04	20	14	11	02	14	02	.	.	.	J1	04	03
XII	7.3	7.3	6.1	6.9	-	04.6	94	82	93	90	54	015	006.0	13	.	02	27	.	.	.	05	17	10	03	08	04	01	08	02
BR. ST. 103																																	
SINAC																																	
BR. ST. 103																																	
I	9.5	6.6	3.6	5.3	-	102.6	04.5	77	57	71	68	24	036	027.6	29	.	.	13	.	.	.	17	01	04	06	02	01	03	03	.	.	04	02
II	9.8	6.1	5.1	5.7	-	109.3	03.6	64	61	79	75	33	041	016.1	21	01	.	21	.	.	.	06	02	07	14	10	09	02	04	.	.	04	13
III	6.4	6.2	6.1	7.6	-	096.7	05.3	79	54	65	68	22	050	016.8	08	.	04	.	.	.	17	04	11	14	20	13	01	19	01	.	01	02	
IV	6.2	7.2	4.8	6.0	-	169.2	05.7	77	47	62	20	119	044.1	11	.	.	01	.	.	.	12	04	04	11	14	09	03	14	.	.	01	01	
V	6.3	7.7	5.5	6.5	-	175.4	09.7	83	59	73	31	153	052.6	06	.	.	05	.	.	.	06	03	10	13	12	06	13	.	.	09	03		
VI	7.1	6.0	7.0	7.4	-	156.3	11.2	64	83	77	39	094	015.0	19	.	.	11	02	.	.	04	01	13	14	04	19	01	.	.	06	04		
VII	6.6	5.1	3.2	4.3	-	251.5	12.8	90	54	81	76	32	114	046.0	02	.	.	22	03	.	.	09	07	11	07	04	11	01	.	.	04	02	
VIII	7.5	7.3	4.7	6.5	-	178.0	12.3	92	60	80	80	38	189	066.4	27	.	.	15	01	.	.	02	10	19	13	05	19	01	.	.	11	07	
IX	6.1	5.4	2.8	4.6	-	170.3	11.8	90	56	83	76	30	053	029.4	08	.	.	15	02	.	.	04	06	02	05	03	02	05	.	.	02	14	
X	7.4	6.5	5.8	6.4	-	095.1	07.4	92	65	80	81	22																					

Mesec	Vasdušni pritisak Pn mbar	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta mD, Pm (0-12)																
		tm					Sred. (Dnev.)	N	NE	E	SE	S	SW	W	NW	C												
		7	14	21	Mj.	Nis.		M.	Av.	Sr.	Sep.	Okt.	Nov.	Dec.		E.	J.	E.	J.	E.	J.	E.	J.					
$\varphi = 44^{\circ}31' N$ $\lambda = 16^{\circ}28' E$ Gr. $\Delta G = + 1h\ 06\ min.$																												
I	-	00.4	05.9	01.5	02.3	07.7	-02.3	13.5	04	-08.5	10	10	02.6	24	02.3	59			
II	-	-02.9	02.4	-02.2	-01.2	03.6	-05.6	11.5	07	-14.5	10	10	02.2	09	02.0	42			
III	-	04.3	08.5	05.3	05.8	10.5	01.7	17.5	30.0	-08.0	29	12	01.5	41	02.1	40			
IV	-	05.9	10.5	06.9	07.6	12.2	02.8	20.0	04	-01.5	19	12	01.8	05	02.4	01	02.0	.	29	02.4	.	.	02	01.0	41			
V	-	10.9	17.3	11.5	12.6	16.2	06.7	23.5	21.17	02.0	85.0	04	04	01.8	11	01.5	.	.	93	02.3	75		
VI	-	13.2	18.3	13.2	14.5	19.2	07.7	26.0	20.15	03.5	07	13	02.5	10	02.1	01	04.0	02	02.5	64			
VII	-	15.2	22.0	19.6	17.1	22.5	-	30.0	18	-	-	20	02.0	03	01.3	11	02.3	.	.	94	03.0	53		
VIII	-	13.6	19.8	14.8	15.8	20.5	-	24.0	15	-	-	08	02.1	08	01.8	77			
IX	-	13.1	21.0	14.0	15.7	22.0	-	29.0	16	-	-	04	01.2	10	01.9	76			
X	-	06.5	13.1	06.8	08.3	13.5	-	25.0	01	-	-	09	01.3	12	01.8	04	01.2	.	02	01.0	65			
XI	-	00.8	09.5	02.3	02.7	04.1	-01.3	18.0	02	-18.5	25	14	C1.7	07	02.0	49			
XII	-	-06.3	05.0	00.7	01.5	04.3	-02.5	13.0	20.17	-11.5	21	23	01.5	03	01.7	.	.	.	16	01.4	02	03.0	.	.	40			
600.	-	06.7	12.5	07.5	08.6	13.3	-	30.0	MW	-	162	01.9	24	01.8	09	01.4	.	.	178	02.1	03	03.3	13	02.5	.	.	710	
$\varphi = 44^{\circ}46' N$ $\lambda = 16^{\circ}42' E$ Gr. $\Delta G = + 1h\ 07\ min.$																												
I	-	-01.3	07.4	01.2	02.2	08.7	-02.4	17.2	10	-07.2	10	03	02.3	.	01	03	02.0	01	03.0	04	01.2	05	02.0	10	01.3	06	02.3	61
II	-	-02.7	05.4	00.4	00.9	06.7	-03.7	14.0	12	-09.4	23	13	02.7	06	01.8	02	02.0	02	01.7	04	02.8	02	01.5	05	02.2	43		
III	-	03.2	13.3	02.2	07.7	14.3	02.1	20.0	06	-05.5	25.0	01	04	02.8	07	01.9	01	01.0	07	03.1	10	02.5	06	02.8	13	02.2	40	
IV	-	07.0	15.2	09.2	10.2	16.3	04.0	23.6	04	-06.8	20	13	02.8	03	02.0	.	.	09	03.8	06	02.6	02	01.5	10	02.0	40		
V	-	12.0	20.7	14.4	15.6	21.9	09.0	28.0	22	01.6	01	13	02.4	04	02.2	02	01.9	.	03	02.8	04	02.6	07	01.7	14	01.4	44	
VI	-	14.9	21.7	16.3	17.3	23.0	12.0	30.4	24	02.8	07	10	02.7	02	03.0	01	01.0	01	02.0	03	03.0	01	01.6	04	01.5	28	02.4	48
VII	-	16.2	25.4	16.1	19.5	26.4	15.8	32.2	18	02.3	20	08	02.0	04	02.2	.	.	.	02	01.0	03	02.0	03	01.3	21	02.1	52	
VIII	-	15.2	23.3	17.0	18.1	24.3	13.1	29.1	14	07.6	15	08	02.5	04	02.0	01	03.0	.	03	01.7	02	01.6	04	01.5	12	02.1	59	
IX	-	13.6	24.9	16.2	17.6	25.3	12.1	30.2	17	07.0	25	09	02.3	03	02.7	.	.	01	03.0	01	04.0	01	03.0	04	01.8	61		
X	-	07.6	14.8	09.9	10.0	15.4	04.3	26.3	01	-01.1	28	09	02.1	03	02.3	.	.	01	04.0	01	01.0	02	01.5	17	01.8	60		
XI	-	02.0	07.4	03.9	04.3	06.2	00.7	20.7	02	-14.1	24	05	02.8	04	02.0	01	02.0	.	04	01.5	03	01.7	07	02.1	11	01.5	53	
XII	-	-00.4	04.7	04.8	01.9	05.9	-02.0	17.4	17	-08.5	21	10	02.1	.	.	04	01.0	06	02.2	03	01.0	02	01.6	04	01.4	16	01.5	49
600.	-	08.2	15.3	09.5	10.4	16.4	05.4	32.2	MW	-14.1	36 XI	105	02.5	42	02.1	11	01.8	20	03.0	48	02.6	40	01.7	157	02.0	612		
$\varphi = 44^{\circ}59' N$ $\lambda = 16^{\circ}45' E$ Gr. $\Delta G = + 1h\ 07\ min.$																												
I	-	-01.2	04.2	01.2	01.8	07.0	-01.3	14.4	14	-06.0	11	04	C1.8	C5	01.2	09	01.8	.	.	66	02.2	01	01.0	46
II	-	-01.3	05.9	01.2	01.7	06.6	-02.0	16.0	12	-07.3	10	09	C1.7	04	04.0	03	02.3	06	01.5	10	01.7	07	02.4	03	01.3	42		
III	-	03.9	12.7	07.0	07.7	13.6	02.8	19.6	19	-04.7	01	10	02.9	06	02.2	04	01.8	05	02.2	10	03.0	03	03.3	06	01.8	32		
IV	-	08.2	15.3	10.0	10.9	16.3	05.7	24.3	06	01.2	13	12	02.6	01	03.0	.	.	02	03.0	12	04.1	04	03.5	10	01.8	37		
V	-	14.2	20.8	14.8	16.2	22.1	11.1	27.3	18	04.2	01	14	02.7	01	03.0	05	01.6	04	02.0	02	02.8	02	01.5	12	01.3	08	02.0	45
VI	-	18.8	21.2	16.5	17.7	22.7	13.0	30.4	15	06.6	07	25	C1.0	01	02.0	01	01.0	.	04	02.2	03	01.7	11	01.9	06	01.5	37	
VII	-	17.0	24.1	17.4	19.1	29.1	13.9	31.3	18	08.7	20	12	02.8	.	.	02	01.0	10	01.6	01	01.0	14	01.6	07	02.0	47		
VIII	-	16.5	23.1	16.0	18.9	24.4	15.0	29.0	18.11	11.0	22	20	02.3	01	01.0	03	02.7	03	01.7	05	01.6	04	01.0	07	01.3	46		
IX	-	14.5	24.0	17.1	18.2	25.0	13.3	30.0	16	08.6	14	08	01.9	01	01.0	.	.	02	01.0	07	01.7	02	02.5	08	02.0	06		
X	-	09.0	15.1	10.1	11.1	15.8	06.1	29.2	01	01.6	20	13	01.8	05	01.8	02	02.0	03	02.0	01	02.0	.	.	14	01.4	07	01.7	48
XI	-	02.5	06.4	04.0	04.3	06.1	01.6	18.6	02	-16.7	26	14	02.8	01	01.0	C1	01.0	04	01.8	01	01.0	07	01.4	03	01.8	58		
XII	-	-00.3	03.4	00.3	01.0	04.0	-01.4	13.6	01	-07.6	21	10	02.1	.	.	04	01.0	06	02.2	03	01.0	.	.	04	01.8	03	01.7	43
600.	-	08.2	14.9	09.8	10.7	15.8	06.4	31.3	MW	-18.7	36 XI	159	02.5	21	02.2	25	01.8	42	01.8	74	02.3	22	02.5	109	01.7	66	01.7	583
$\varphi = 44^{\circ}16' N$ $\lambda = 16^{\circ}52' E$ Gr. $\Delta G = + 1h\ 07\ min.$																												
I	-	-01.0	02.8	00.4	00.6	03.2	-03.0	08.2	15	-07.6	09	09	03.1	13	02.6	.	.	

Mjesec	Oblačnost Nm (0-10)					Inzolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																				
	%		mm		mm		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	*	*	Δ	Δ	▲	▲	R	T	≡								
	7	14	21	Sred. (Dnev.)			7	14	21	Sred.	Min	Max	Dat.	=	<	<	=	=	=	=	=	=	?	Δ	*	Δ	▲	▲	R	T	≡		
DRINIĆ																																	
BR. ST. 106																																	
I 4.6 5.8 3.8 4.7	-	04.8	81	86	84	84	48	018	009.2	29	.	01	24	08	08	04	04	.	03	02	04			
II 5.0 5.4 5.4 5.3	-	03.7	76	84	80	80	61	038	008.0	21	05	06	26	09	10	07	07	.	01	01	16			
III 7.0 7.2 6.3 6.8	-	05.7	82	79	80	80	30	081	014.4	14	.	01	06	03	13	15	14	03	15	01	01	01	02		
IV 6.3 6.5 5.6 6.1	-	05.4	74	64	71	70	20	127	046.0	11	.	01	03	04	12	12	11	05	11	04	02	01	01	01
V 6.1 6.6 4.3 5.7	-	09.6	85	79	83	82	50	110	036.0	14	.	01	01	05	09	15	15	09	15	05	02	.		
VI 6.7 7.6 6.3 6.9	-	11.2	84	85	86	85	57	064	027.4	13	.	01	01	03	12	15	12	02	15	02	.	.		
VII 5.1 5.8 3.9 5.0	-	13.0	84	82	84	84	48	128	039.5	02	.	01	01	05	04	11	07	04	11	04	.	.		
VIII 7.1 7.9 5.1 6.6	-	12.2	91	84	89	88	72	146	028.6	23	.	01	04	04	12	15	14	04	15	01	.	.		
IX 3.6 5.3 2.9 3.9	-	12.9	90	88	90	89	70	044	023.3	13	.	01	01	10	05	05	04	02	05	02	01	.		
X 7.3 6.3 5.4 6.3	-	07.4	88	78	89	85	42	178	080.9	14	.	01	01	08	17	12	11	04	12	02	01	.		
XI 7.5 7.9 7.3 7.6	-	05.1	86	83	84	85	56	141	045.2	19	04	05	08	02	10	14	11	04	11	18	06	.		
XII 5.6 5.6 5.0 5.4	-	04.5	83	79	86	82	55	095	028.7	18	01	04	25	09	12	07	06	02	03	04	04	07	.	
GOD. 6.0 6.5 5.1 5.9	-	08.0	84	81	84	83	20	1222	080.9	Mx	-	15	-	20	01	-	.	70	134	135	114	39	117	24	03	17	19	34	
SANSKI MOST																																	
BR. ST. 107																																	
I 4.6 5.9 4.0 5.5	104.3	04.8	95	67	90	84	39	044	025.0	29	.	01	28	03	08	05	04	02	05	02	02	11			
II 5.4 5.3 4.6 5.1	130.3	03.9	90	60	84	79	26	038	010.4	21	.	01	20	.	.	.	03	07	08	09	07	01	06	04	01	05			
III 4.1 7.9 5.9 7.3	104.0	05.8	92	52	90	74	25	048	017.4	17	.	01	09	.	.	.	04	01	19	17	11	01	15	02	01	01	.		
IV 6.2 6.9 5.3 5.6	150.4	06.4	88	51	76	71	21	076	031.4	11	.	01	04	01	.	.	03	02	05	08	12	11	02	12	01	.	.		
V 5.9 6.9 3.8 5.5	183.9	10.7	90	61	90	80	34	174	033.3	14	.	01	10	.	.	.	06	09	17	13	07	17	07	03	.				
VI 7.1 7.6 6.2 7.0	162.0	12.3	90	65	89	82	46	095	043.0	13	.	01	14	01	.	.	03	01	03	10	16	08	03	14	09	02	.		
VII 6.2 4.9 3.5 4.9	243.9	13.9	93	58	92	81	38	116	043.3	01	.	01	22	07	.	.	01	01	05	07	12	09	03	11	09	10	.		
VIII 6.0 6.9 4.1 6.3	169.5	13.3	96	66	93	85	43	171	048.7	26	.	01	15	.	.	01	01	02	08	18	13	07	17	08	12	.			
IX 8.0 4.6 1.9 5.1	179.1	12.7	98	59	94	84	37	039	018.0	13	.	01	17	02	.	.	02	02	02	03	02	05	03	05	03	28	.		
X 9.6 6.6 3.8 7.3	091.4	08.2	87	70	94	87	35	105	052.5	14	.	01	02	01	.	.	01	01	02	03	16	22	10	02	13	02	19	.	
XI 8.7 8.1 6.7 7.6	037.2	05.7	92	76	90	87	31	061	017.0	11	01	08	01	19	21	12	02	16	03	01	07	06			
XII 8.2 6.9 7.4 7.5	059.2	04.6	93	76	91	87	42	026	010.2	18	01	03	21	.	.	.	01	20	11	04	01	04	05	01	06	02			
GOD. 7.4 6.5 4.8 6.2	1642.8	08.5	92	63	88	81	21	993	052.5	Mx	02	03	93	80	18	.	19	05	36	130	179	105	35	139	16	02	.	.	.	38	91	17	
PRIJEĐOR																																	
BR. ST. 108																																	
I 7.4 5.6 6.3 6.4	-	04.3	91	65	87	81	42	027	012.6	29	.	01	25	.	.	.	04	01	01	10	04	04	01	04	13				
II 7.1 4.9 5.6 5.6	-	03.9	90	54	82	79	21	021	004.4	17	.	01	19	.	.	.	08	01	04	09	07	04	01	04	04	.	03		
III 7.5 6.6 6.3 6.8	-	05.3	92	49	77	72	14	037	010.9	07	.	01	08	.	.	.	04	01	11	10	10	01	16	04	.	.			
IV 6.2 5.3 5.0 5.5	-	06.2	84	48	63	65	24	073	030.2	11	.	01	01	.	.	.	14	05	03	07	11	11	01	11	01	.	.		
V 5.9 5.8 5.3 5.7	-	10.3	86	54	84	75	28	133	025.2	13	.	01	11	.	.	.	13	02	06	05	17	14	05	17	02	01	04		
VI 6.5 5.6 5.6 5.9	-	11.4	85	57	83	75	32	032	011.5	18	.	01	11	01	.	.	11	01	01	07	09	07	01	09	01	02	02		
VII 4.6 3.4 4.3 4.1	-	12.4	86	50	90	75	31	164	055.0	02	.	01	20	02	.	.	03	02	07	02	10	10	04	10	03	04	.		
VIII 7.8 5.9 6.6 6.8	-	13.0	92	58	91	80	23	093	024.1	19	.	01	14	.	.	.	08	17	14	02	17	11	.	.					
IX 9.6 4.2 4.6 6.1	-	12.2	95	51	92	79	30	066	026.7	08	.	01	14	01	.	.	04	01	01	06	05	03	03	05	23				
X 9.7 6.7 7.4 7.9	-	08.2	92	62	82	73	23	098	046.4	14																							

Mjesec	Vrstdujni pritisak Pa	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Fm (0-12)																							
		Tm			Srednji (dnev.)				Min.			Max.			Dat.			N		NE		E		SE		S		SW		W		NW		C	
		7	14	21		Hx	Hs	Hm		Mx	Ms	Mm		Dat.			č.	j.	č.	j.	č.	j.													
$\varphi = 44^{\circ}47' N$ $\lambda = 17^{\circ}13' E$ Gr. $\Delta G = + 1h\ 09\ min.$																SANJA LUKA												BR. ST. 111							
I	752.0	-00.6	08.5	01.5	02.7	05.6	-02.3	17.7	18	-07.2	10	19	01.7	11	01.2	C4	01.5	04	01.2	G6	01.0	G7	02.7	05	01.4	06	01.5	31							
II	755.0	-02.1	05.5	00.6	01.2	06.4	-03.5	16.2	12	-05.4	23	17	C1.9	21	02.1	C9	02.0	.	.	G1	G3.0	05	G3.2	07	01.7	06	01.7	18							
III	749.7	04.1	13.4	08.1	08.4	14.7	02.4	20.2	19	-05.1	01	15	C1.9	15	02.3	C6	01.8	05	01.8	G8	01.9	13	G3.1	06	02.2	11	02.0	14							
IV	747.6	08.1	15.7	10.3	11.1	16.6	05.0	27.6	06	00.1	20	20	C1.9	07	02.1	C4	01.5	11	C1.3	G2.9	09	G3.1	11	03.1	05	01.8	15								
V	746.9	14.0	20.9	15.2	16.3	22.3	10.6	27.7	18	03.0	01	09	02.1	19	01.8	11	01.4	11	C1.3	04	01.2	C3	02.3	10	02.7	16	02.2	10							
VI	747.5	16.3	22.1	17.1	18.1	23.3	13.2	36.0	15	05.0	07	18	C1.9	10	01.8	10	01.5	C9	01.1	04	01.7	06	01.2	11	01.8	06	01.0	12							
VII	747.8	17.8	25.1	18.7	20.1	26.4	14.1	32.1	19	18	07.4	28	16	C1.7	20	01.7	13	C1.7	C8	01.4	01	01.0	.	16	02.9	08	02.2	17							
VIII	748.9	16.6	23.2	17.8	18.8	24.7	14.0	29.8	16	09.2	15	17	C1.9	16	02.1	C5	01.0	14	C1.1	02	01.0	04	01.8	06	01.2	22									
IX	751.1	14.2	24.8	17.1	18.2	25.5	12.5	30.0	17	07.8	14	19	C1.3	17	02.2	C4	01.5	05	01.0	C1	01.0	06	C2.2	.	.	05	01.6	33							
X	751.8	07.7	14.7	09.3	10.2	15.2	04.2	28.1	01	-04.4	31	23	C1.7	21	01.6	C6	01.8	.	.	05	01.4	.	01	03.0	09	01.2	28								
XI	750.6	02.4	07.4	04.0	04.4	08.2	01.1	17.0	02	-12.6	26	22	C1.3	25	01.2	C7	01	01.0	01	01.0	07	01.7	01	03.0	05	02.8	08	01.4	14						
XII	754.0	-00.3	04.8	01.2	01.7	05.5	-01.5	18.6	01	-06.0	21	19	C1.2	32	01.2	10	C1.4	03	01.3	04	01.8	03	01.3	.	.	13	01.2	09							
600. 749.8 08.2 15.5 10.1 10.9 16.3 06.6 32.1 19.6 VII -12.6 26 XI 214 01.7 214 01.7 89 01.5 71 01.2 53 01.7 57 02.9 71 02.2 103 08.7 323																																			
$\varphi = 44^{\circ}21' N$ $\lambda = 17^{\circ}16' E$ Gr. $\Delta G = + 1h\ 09\ min.$																										JAJCE									
I	-	-01.8	04.9	00.2	00.9	05.7	-03.4	11.4	18	-08.8	10	01	01.0	04	02.0	G3	03.3	G1	G3.0	G1	04.0	G4	01.5	G3	G1.3	.	16								
II	-	-02.8	05.2	00.3	00.8	05.8	-04.2	14.0	13	-10.0	24	06	03.7	.	.	06	03.5	04	03.2	04	02.8	05	04.0	05	01.8	01	01.0	51							
III	-	04.5	12.9	07.7	08.2	13.9	02.0	21.6	30	-06.6	01	06	C2.3	08	03.8	G1	02.0	.	.	04	02.2	04	03.2	07	02.4	08	03.1	55							
IV	-	07.3	14.5	09.4	10.1	15.7	03.6	23.4	07.64	-00.2	19.13	.	.	08	03.6	C3	01.3	02	03.0	01	02.0	09	03.2	04	04.2	04	05.1	54							
V	-	11.8	20.4	18.9	15.0	22.1	08.2	26.4	20	00.4	11	.	.	01	03.0	C3	02.0	02	02.5	02	02.5	06	02.7	04	02.8	02	02.5	73							
VI	-	14.7	21.2	18.5	17.2	22.4	13.2	31.0	15	05.4	03	03	01.7	02	01.5	.	.	01	03.0	04	02.5	03	03.0	.	.	04	02.5	77							
VII	-	15.0	25.2	18.1	19.3	26.0	13.9	33.0	19.18	07.0	28	02	02.0	05	02.4	G1	01.0	.	.	04	02.5	06	02.8	01	03.0	74									
VIII	-	14.7	21.9	16.6	17.5	23.4	13.2	26.8	14	08.6	22	03	02.0	03	02.3	02	02.5	01	01.0	.	.	04	02.2	05	02.4	01	02.0	74							
IX	-	18.7	24.1	16.0	17.5	24.8	12.4	28.0	17	08.4	24	02	02.5	.	.	04	01.5	01	02.0	01	03.0	03	03.0	04	02.8	07	02.5	75							
X	-	07.5	14.6	08.9	10.2	15.2	06.1	24.6	01	-00.2	31	02	02.5	02	04.0	G3	03.7	01	02.0	08	01.8	03	03.0	08	02.5	01	04.0	65							
XI	-	01.8	07.5	04.2	04.4	08.2	00.4	19.0	02	-14.8	24	02	02.5	06	02.0	01	01.0	.	.	01	05.0	01	04.0	07	03.6	01	02.0	71							
XII	-	00.3	04.2	01.2	01.8	05.4	-01.7	16.6	17	-06.4	08	.	.	03	02.3	02	02.0	.	.	01	04.0	04	02.2	11	02.7	.	.	72							
600. - 07.3 14.7 09.4 10.2 15.7 05.3 06.2 11.5 01.1 29.2 16 VII -14.8 26 XI 399 C2.6 16 02.9 C3 02.0 . . 213 03.1 . . 08 03.0 . . 466																										KOTOR VAROS									
$\varphi = 44^{\circ}38' N$ $\lambda = 17^{\circ}23' E$ Gr. $\Delta G = + 1h\ 10\ min.$																										BR. ST. 114									
I	-	-01.8	08.0	00.5	01.8	08.8	-03.7	17.2	18	-08.5	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
II	-	-03.3	C4.8	00.2	00.5	C5.7	-04.8	14.6	13	-11.9	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
III	-	04.6	13.9	07.5	08.4	14.7	02.3	20.3	31.08	-05.3	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25									
IV	-	04.9	15.3	09.0	10.1	16.6	03.7	26.2	07	00.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16									
V	-	13.0	20.9	14.2	19.6	22.1	05.3	28.0	20	04.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41									
VI	-	15.4	21.5	16.2	17.3	22.7	12.1	30.4	15	04.2	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	42									
VII	-	16.5	25.6	17.7	19.4	26.5	12.5	33.2	18	06.0	28.27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	42									
VIII	-	15.5	23.2	16.7	18.0	24.2	12.3	29.3	11	08.0	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34									
IX	-	15.4	25.4	16.3	18.3	25.5	10.5	30.3	17	05.1	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
X	-	06.7	14.8	08.0	09.5	05.0	02.6	26.4	01	-01.8	31	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
XI	-	01.4	07.4	03.0	03.7	05.0	-06.8	22.0	02	-16.0	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
XII	-	-00.6	04.9	00.6	01.4	04.9	-02.7	16.3	01	-04.5	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
600. - 07.3 15.5 09.2 10.4 16.5 04.7 33.2 16 VII -18.0 25 XI -																										BUGJIMC									
$\varphi = 44^{\circ}04' N$ $\lambda = 17^{\circ}28' E$ Gr. $\Delta G = + 1h\ 10\ min.$																										BR. ST. 115									
I	716.0	-02.8	04.0	-00.8	-00.4	03.4	-05.1	13.4	16	-11.5	10	18	C1.6	C1	03.0	.	.	C3	01.7	09	C2.1	.	.	07	C1.7	35									
II	717.1	-03.3	03.8	-00.4	-00.1	03.0	-04.1	12.0	13	-11.2	24	25	C2.4	05	03.6	C1	C2.0	C3	C2.0	03	C2.7	02	C2.5	01	01.6	12	C2.6	32							
III	718.1	02.9	11.0	03.6	03.7	12.3	01.8	18.7	30	-08.1	01	13	C1.8	01	02.0	C2	02.4	27	C2.8	10	03.0	01	03.0	10	C1.5	65									
IV	718.6	05.8</td																																	

Mesec	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																									
	7	14	21	Sred. (Dnev.)		U m t	Sred.	Min	Max			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	≤	<	≤	IV	IV	IV	IV	IV	IV	9	*	*	Δ	○	▲	□	T
		mm	mm			Σ				20.00.0	0.0250	0.0200	0.6	8	2.0	8.0	0.1	1.000.0																			
BR. ST. 111																																					
EARJA LUKA																																					
I	6.0	5.6	4.3	5.4	117.6	04.5	92	61	85	81	37	051	022.6	28	.	.	23	.	.	02	.	05	08	07	06	03	07	62	05	01			
II	4.9	5.6	4.5	5.0	124.4	03.5	88	62	82	77	35	036	012.6	21	.	.	22	.	.	03	.	08	09	07	01	05	03	04	.				
III	7.5	8.5	5.4	7.1	104.3	05.8	88	53	75	72	24	031	005.8	22	.	.	07	.	.	05	02	01	14	18	09	16	02	01	.				
IV	6.5	7.1	4.9	6.2	141.9	04.5	81	52	71	68	19	077	032.6	11	.	.	02	.	.	10	03	05	12	13	12	02	13	01	.				
V	6.0	7.0	5.2	6.1	175.3	11.0	87	62	86	78	39	152	026.0	14	.	.	11	.	.	07	.	05	11	16	12	07	16	2	11	02			
VI	7.5	7.2	6.4	7.0	145.9	12.5	85	63	86	78	44	096	030.1	19	.	.	14	01	.	03	02	03	13	18	19	02	18	09	03	.			
VII	3.8	4.9	3.8	4.2	262.1	13.9	87	59	88	78	39	141	037.2	01	.	.	23	08	.	02	01	11	07	12	11	05	12	07	.				
VIII	6.4	7.1	4.2	5.9	157.0	13.4	94	65	91	83	44	118	037.3	19	.	.	14	.	.	01	01	04	09	17	11	03	17	08	03	.			
IX	9.3	4.5	2.2	4.0	190.1	12.6	96	58	92	82	31	041	016.2	08	.	.	18	01	.	01	.	09	03	07	05	02	07	05	10	.			
X	6.5	6.4	5.4	6.1	106.7	08.3	95	71	92	86	36	105	051.0	14	.	.	01	01	.	01	.	08	14	12	03	14	01	19	.				
XI	7.9	8.0	6.4	7.4	093.8	05.7	92	76	91	86	29	068	017.1	11	02	01	08	.	.	02	.	03	17	17	12	02	14	04	01	.	01	09	05				
XII	6.0	7.6	6.5	7.4	052.0	04.6	94	76	92	87	42	021	006.4	13	.	01	21	.	.	.	04	18	12	06	07	03	04	01	.				
GOD.	6.4	6.6	4.9	6.0	1621.1	08.6	89	63	86	78	19	937	091.4	14.X	02	02	02	84	07	.	34	09	64	135	160	116	30	144	18	01	.	.	02	48	33	13	
JAJCE																																					
BR. ST. 112	$H_a = 430 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																				
I	9.3	5.1	5.5	6.6	073.8	04.2	93	70	92	85	45	038	010.5	09	.	.	30	.	.	01	10	07	06	01	05	04	01	21	.				
II	6.9	5.2	5.9	6.7	113.6	03.7	88	58	79	75	22	010	004.3	14	01	.	25	.	.	02	.	01	12	04	04	03	01	09	01				
III	6.2	6.9	5.7	6.9	115.9	05.6	83	65	63	64	17	032	010.6	14	.	.	10	.	.	04	02	11	12	07	01	12	07	.					
IV	7.1	6.3	5.6	6.3	144.1	05.7	82	62	49	64	16	046	009.8	11	.	.	02	.	.	02	03	11	11	10	01	04	.						
V	8.3	7.0	7.0	7.4	161.6	09.9	93	56	87	79	26	003	022.7	14	.	.	09	.	.	01	14	17	14	02	17	02	12						
VI	7.4	7.5	7.9	7.6	134.5	12.5	93	68	91	84	35	080	018.7	13	.	.	14	01	.	01	14	20	14	03	20	01	06						
VII	6.6	5.3	6.5	6.5	232.8	12.9	93	82	88	78	29	003	028.6	03	.	.	21	07	.	01	02	10	11	09	02	11	01	16					
VIII	9.1	7.0	8.1	8.1	139.5	12.8	98	65	95	86	36	111	017.9	19	.	.	11	.	.	03	17	16	05	17	04	11							
IX	9.4	8.7	7.5	7.2	170.1	12.3	99	54	97	83	34	021	007.3	04	.	.	19	.	.	07	07	05	03	07	19	.							
X	6.5	6.0	7.8	7.7	100.9	07.9	97	64	95	85	26	117	046.8	14	03	01	01	.	01	.	19	14	13	03	14	01	19						
XI	9.6	6.8	7.5	8.0	056.8	05.5	94	71	87	84	40	069	028.3	10	03	03	08	.	01	.	17	17	13	03	14	04	08	06					
XII	9.5	6.0	8.4	8.0	088.0	04.5	90	73	89	84	26	030	008.3	10	03	03	25	.	.	01	16	08	07	03	03	08	02						
GOD.	6.3	6.2	7.0	7.2	1545.6	08.1	92	60	86	79	16	740	046.8	14.X	04	06	101	71	08	.	07	.	11	150	149	110	20	136	14	01	.	.	09	137	09		
MUPRES																																					
BR. ST. 113	$H_a = 1190 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																				
I	4.4	4.7	4.6	4.6	-	03.1	70	74	77	74	37	013	004.2	27	07	06	31	.	.	04	04	05	05	09	02	04	31	.					
II	5.1	4.7	4.3	4.7	-	02.9	73	76	78	75	45	014	003.8	21	04	01	24	.	.	05	01	07	04	06	01	07	28	.					
III	7.5	7.0	6.9	7.2	-	04.8	85	88	84	84	43	126	032.2	22	02	01	15	.	.	04	01	17	18	10	03	14	07	13	.				
IV	6.1	6.5	5.9	6.2	-	05.0	81	89	84	77	30	110	017.6	17	.	.	16	.	.	05	01	02	10	19	13	05	13	05	.	.	04	.					
V	6.0	6.7	6.3	6.3	-	07.5	83	81	83	76	29	003	019.2	15	.	.	01	01	.	05	.	09	20	13	03	20	01	.					
VI	6.5	7.0	7.1	6.9	-	08.9	86	89	81	84	48	081	019.6	13	.	.	14	01	.	01	12	19	12	02	15	01	.						
VII	5.6	5.4	4.9	5.3	-	10.1	86	88	86																												

Mesec	Vrstdinski pritisak Pa MM	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Fm (0-12)																		
		Tm				N						NE						E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dnev.)	Hx	Hm	Max	Min.	Hx	Min.	Max	Min.	Hx	Min.	Max	Min.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	
$\varphi = 44^{\circ}14' N$ $\lambda = 17^{\circ}40' E$ Gr. $\Delta G = + 1h 11 min.$																									TRAVNIK		BR. ST. 116			
I	-	-04.0	02.1	-01.6	-01.3	-	-05.7	-	-	-11.0	11.10	-	-	01	01.0	-	-	25	01.8	25	C1.5	-	-	01	02.0	02	01.0	39		
II	-	-03.1	03.4	-00.8	-00.3	-	-	-	-	-	-	02	02.5	02	02.0	01	02.0	19	02.2	C1.6	C1.8	04	03.2	02	02.5	02	02.5	44		
III	-	03.0	11.5	06.4	06.8	13.5	01.3	22.0	30	-07.0	25	01	03.0	04	02.0	05	02.0	19	01.7	C1.5	C1.8	04	02.0	05	02.4	05	02.0	45		
IV	-	05.9	13.2	07.8	08.7	15.2	03.1	23.5	04	00.0	30.02	-	-	07	02.1	02	02.0	19	01.4	-	-	02	02.0	08	02.1	-	-	52		
V	-	10.6	19.6	12.8	13.9	21.1	08.1	25.0	22.16	02.5	04	-	-	06	02.0	-	-	12	01.8	C1.5	C1.0	03	02.3	03	01.7	63				
VI	-	13.1	19.6	14.1	15.2	21.5	10.4	28.8	28	05.4	06	-	-	08	02.4	C1	02.0	12	01.6	C1.3	C1.0	01	02.0	-	-	64				
VII	-	14.0	24.4	16.1	17.7	25.6	11.5	30.6	18	05.5	27	01	03.0	06	02.0	05	01.5	C1.5	C1.5	03	02.3	-	-	70						
VIII	-	13.2	21.7	14.4	16.2	23.0	11.0	27.0	18	06.5	22	01	02.0	-	-	07	01.1	C1.0	-	-	-	-	-	-	-	81				
IX	-	11.4	21.9	14.0	15.3	23.4	06.4	28.4	17	05.0	14	02	02.5	02	02.0	-	-	04	01.4	C1.3	C1.0	02	01.0	-	-	77				
X	-	05.6	13.5	07.6	08.6	14.5	04.0	25.5	C1	-02.2	27	03	02.0	06	02.0	01	04.0	13	02.1	C1.3	C1.0	05	01.6	01	02.0	66				
XI	-	00.7	04.0	03.0	03.2	07.6	-00.8	17.0	17	-15.2	26	02	02.5	02	02.5	02	01.5	65	01.4	-	-	11	02.1	-	-	02	02.5	86		
XII	-	-01.3	03.9	-00.2	00.4	04.6	-03.0	16.0	18	-08.5	21	-	-	01	02.0	-	-	02	02.0	-	-	03	02.0	-	-	01	01.0	85		
600.	-	05.8	13.4	07.8	08.7	-	-	-	-	-	12	02.4	48	02.1	13	02.1	146	C1.8	51	01.8	40	02.1	26	02.2	17	01.8	748			
$\varphi = 44^{\circ}52' N$ $\lambda = 17^{\circ}42' E$ Gr. $\Delta G = + 1h 11 min.$																									PRKJAVCI		BR. ST. 117			
I	-	-01.9	07.3	01.1	01.9	07.9	-03.2	17.0	18	-10.4	05	04	01.0	10	01.1	21	01.0	C6	C1.1	13	01.1	20	01.2	09	01.4	02	01.0	09		
II	-	-02.3	05.2	00.2	00.8	05.6	-03.3	15.0	12	-08.0	18	07	01.4	13	01.6	16	01.2	10	01.1	13	01.0	20	01.4	02	01.0	09	-	03		
III	-	02.3	13.3	07.6	07.7	14.0	01.4	19.5	19	-04.6	-	08	01.8	12	01.4	20	01.5	C7	C1.4	13	01.5	24	01.5	09	02.0	01	02.0	03		
IV	-	07.7	15.6	04.5	10.6	16.3	05.2	26.5	07	01.0	13	04	01.2	13	01.4	14	01.4	C6	C1.4	07	01.3	32	01.6	04	02.0	04	01.0	03		
V	-	13.3	26.9	14.5	16.0	22.1	10.1	28.0	22.16	02.6	01	05	01.4	11	01.3	11	01.4	C6	01.5	12	01.3	25	01.7	09	02.1	-	-	14		
VI	-	16.1	22.4	16.7	18.0	23.3	13.1	30.5	28	07.8	07	03	01.0	12	01.1	C6	01.4	04	01.0	16	01.1	27	01.6	01	02.0	-	-	19		
VII	-	18.1	25.1	18.4	20.0	26.2	15.0	32.0	18	10.4	28	03	01.0	04	01.5	11	01.2	C4	01.0	11	01.3	28	01.6	09	01.4	04	01.2	23		
VIII	-	16.0	23.7	17.1	18.5	24.9	14.1	29.3	18.11	09.0	15	04	01.8	10	01.1	18	01.2	C1	01.0	22	01.1	19	01.5	09	01.6	02	02.0	12		
IX	-	13.8	25.0	16.2	17.8	25.4	11.4	30.0	17.16	07.6	10	06	01.5	12	01.2	25	01.1	04	01.0	13	01.2	16	01.1	01	01.0	02	01.5	17		
X	-	07.9	14.9	05.0	10.2	15.4	06.6	-	-	-	-	10	01.7	18	01.3	16	01.1	04	01.2	12	01.2	21	01.2	02	01.3	02	01.3	07		
XI	-	01.2	07.3	03.2	03.7	07.6	00.2	16.5	02	-14.0	26	13	01.3	17	01.5	10	01.3	08	01.5	11	01.2	28	01.6	02	01.0	-	-	01		
XII	-	-01.0	04.3	00.5	01.0	04.9	-02.5	10.6	28	-07.2	21	09	01.1	17	01.2	14	01.5	06	01.2	16	01.3	25	01.6	04	01.0	01	01.0	01		
600.	-	07.6	15.4	09.5	10.5	16.1	09.8	-	-	-	76	01.4	149	01.3	184	01.3	72	01.2	199	01.2	279	01.5	49	01.6	19	01.3	112			
$\varphi = 44^{\circ}36' N$ $\lambda = 17^{\circ}54' E$ Gr. $\Delta G = + 1h 11 min.$																									TESLICE		BR. ST. 118			
I	-	-02.7	07.3	00.0	01.1	07.5	-02.6	14.6	06	-10.6	10	24	C1.2	-	-	01	02.0	01	04.0	02	C2.0	02	02.0	-	-	-	-	-	68	
II	-	-02.7	05.1	00.0	00.6	05.5	-03.1	14.6	13	-09.4	24	27	C1.7	01	02.0	01	01.0	02	02.0	01	01.7	06	02.3	-	-	-	-	-	48	
III	-	01.9	13.6	05.6	06.7	14.3	00.7	20.2	19	-06.2	01	15	01.3	01	02.0	-	-	03	03.3	04	02.1	01	02.0	-	-	-	-	-	68	
IV	-	05.2	14.6	08.6	09.4	15.2	03.2	26.4	07	00.0	21.20	20	01.3	-	-	03	03.3	04	02.0	01	01.0	-	-	-	-	-	57			
V	-	11.5	20.6	14.6	15.3	21.6	06.6	27.0	19	04.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	13.9	21.2	16.0	16.8	22.5	12.4	30.2	28	05.4	08	03	C1.3	-	-	01	-	-	-	-	-	-	-	-	-	-	-	-	64	
VII	-	15.3	25.0	17.6	18.9	25.7	13.9	32.2	19	07.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	66		
VIII	-	14.3	22.5	16.3	17.4	23.0	13.3	26.0	11	08.6	22.15	04	01.0	02	01.0	-	-	01	-	-	-	-	-	-	-	-	-	66		
IX	-	13.1	24.3	15.6	17.2	25.0	11.8	30.0	29	06.4	15	09	C1.0	-	-	01	-	-	01	04.0	-	-	02	01.8	-	-	-	78		
X	-	07.0	14.7	09.5	10.2	15.4	05.4	25.4	C1	-03.2	31	20	01.2	-	-	01	-	-	01	-	-	01	-	-	-	-	-	65		
XI	-	01.5	06.2	03.4	03.6	07.0	00.5	14.2	30	-15.0	26	25	C1.2	-	-	01	02.0	-	01	03.0	-	-	01	02.0	-	-	-	69		
XII	-	-01.4	03.9	00.0	00.6	04.5	-02.5	14.6	01	-06.0	20	22	01.2	02	02.0	-	-	02	02.0	-	-	01	-	-	-	-	-	-		
600.	-	06.4	14.9	09.0	09.8	19.7	05.1	32.2	19.76	-15.0	26.XI	60	C2.5	20	02.3	11														

Mjesec	Vrednost pritiska Pa	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра nD, fm (0-12)																
		7	14	21	Sred. (Dnev.)	NW	NE	W	E	SW	S	N	NE	E	SE	S	SW	W	NW	C								
$\varphi = 44^{\circ}59' N$ $\lambda = 18^{\circ}18' E$ Gr. $\Delta G = + 1h 13 min.$																												
I	-	-06.2	06.7	01.6	02.4	07.4	-01.4	14.8	19	-07.0	10	09	01.2	06	01.3	.	.	04	01.8	.	.	06	01.0	14	01.1	24	01.5	30
II	-	-01.1	09.2	01.2	01.6	06.0	-02.3	13.0	12	-06.8	10	24	02.1	09	01.9	05	01.4	02	01.5	.	04	01.8	08	01.8	20	01.6	12	
III	-	04.4	13.6	07.1	08.1	14.4	01.8	21.2	16	-02.8	03.01	14	02.0	05	01.8	13	01.9	04	01.2	06	01.5	07	01.7	11	01.4	16	01.4	17
IV	-	09.1	15.2	10.4	11.3	14.6	04.8	27.3	06	01.3	01	13	02.0	05	01.6	05	01.8	02	01.5	.	.	12	02.0	11	01.5	26	01.8	16
V	-	15.4	21.3	16.5	17.4	21.8	10.7	20.1	22	03.5	02	07	02.6	12	01.5	11	01.7	07	01.3	.	.	15	01.4	14	01.4	19	01.6	06
VI	-	16.6	22.4	18.5	19.2	23.1	13.5	24.0	24	04.4	06.6	11	02.3	03	01.7	01	01.0	04	01.7	.	.	07	01.4	09	01.3	32	01.6	21
VII	-	19.3	25.0	20.9	21.5	25.8	14.4	30.6	19	09.2	29	06	02.0	08	01.8	02	02.6	04	01.0	.	.	04	01.5	13	01.4	44	01.6	10
VIII	-	17.9	23.7	19.1	19.9	24.2	13.3	29.5	18	09.4	21.20	09	01.3	15	01.4	01	02.6	05	01.4	.	.	08	01.1	06	01.5	31	01.6	16
IX	-	15.5	24.6	18.9	19.5	25.2	11.2	29.6	16	07.8	10	02	02.9	05	01.8	11	01.9	06	02.0	.	.	05	01.0	04	01.0	20	01.4	37
X	-	09.1	14.9	11.5	11.8	15.6	05.2	26.2	01	06.9	30.10	12	01.7	17	01.5	04	01.8	03	01.8	.	.	07	01.1	03	01.7	19	01.3	27
XI	-	02.5	06.9	04.1	04.3	07.5	00.3	13.9	02	-10.7	26	01	02.0	23	01.6	11	01.4	18	01.6	.	.	01	03.0	08	01.3	19	01.7	22
XII	-	-06.2	03.9	00.7	01.3	04.5	-02.6	11.9	17	-06.7	26	07	01.6	10	01.3	03	01.7	04	01.3	.	.	01	01.0	03	01.4	34	01.6	27
600.	-	09.1	15.3	10.9	11.5	16.0	05.7	30.8	MVN	-16.7	26.XI	117	01.9	118	01.6	67	01.7	66	01.5	84	77	01.4	191	01.4	204	01.6	245	
$\varphi = 44^{\circ}11' N$ $\lambda = 18^{\circ}22' E$ Gr. $\Delta G = + 1h 14 min.$																									PONIKVE			
BR. ST. 121																									BR. ST. 122			
I	-	-07.3	01.8	-04.8	-03.8	02.3	-	04.6	19	-	-	17	01.3	04	01.2	.	.	02	02.0	.	.	04	01.2	07	01.6	39		
II	-	-08.7	01.8	-06.3	-05.3	02.5	-	11.2	12	-	-	26	01.7	02	01.5	.	.	03	01.0	.	.	05	01.6	08	02.2	41		
III	-	02.0	09.3	01.9	03.8	11.1	-	21.9	30	-	-	06	01.5	01	02.0	04	01.4	.	.	03	01.4	01	01.0	09	01.3	05	01.6	38
IV	-	04.3	13.4	04.6	04.8	14.6	-	23.6	06	-	-	01	01.0	03	01.7	12	01.4	.	.	02	01.4	06	01.6	44				
V	-	16.2	17.0	08.6	11.1	18.3	-	23.4	17	-	-	08	01.4	.	.	01	01.0	01	01.0	24	01.3	02	01.0	57				
VI	-	18.2	19.3	11.6	18.7	20.7	-	31.5	30	-	-	09	01.1	.	.	01	01.0	04	01.6	12	01.6	57	01.1	57				
VII	-	15.0	22.0	18.7	16.1	23.0	-	32.0	18	-	-	16	01.6	01	02.0	.	.	17	02.3	02	01.0	18	02.3	02	01.0	56		
VIII	-	18.4	21.7	16.9	14.0	23.2	04.4	27.0	15	07.3	07	01	02.0	.	.	08	01.7	01	01.0	34	02.3	03	03.0	29				
IX	-	12.3	20.9	12.2	14.5	22.1	10.8	27.4	17	07.4	10	03	01.0	01	02.1	19	02.1	.	.	08	02.1	05	02.6	56				
X	-	02.9	11.9	05.6	06.2	13.2	02.0	25.6	01	-04.0	30	14	02.2	.	.	04	02.5	.	.	16	02.3	03	02.3	56				
XI	-	-03.0	03.2	-06.6	-06.3	04.4	-04.6	12.0	08	-22.4	26	21	02.5	.	.	04	02.8	.	.	01	02.0	.	.	12	03.2	.	52	
XII	-	-06.2	01.8	-03.6	-02.9	02.7	-07.2	10.0	17	-14.6	23	19	02.1	01	02.0	.	.	01	04.0	.	.	08	02.4	01	04.0	67		
600.	-	03.6	12.6	04.4	06.2	15.3	-	32.6	-	-	121	01.8	12	01.7	97	01.8	03	02.0	20	01.8	07	01.3	172	02.6	51	01.9	612	
$\varphi = 44^{\circ}19' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$																									RACCA			
BR. ST. 123																									BR. ST. 124			
I	-	-01.0	04.1	00.1	00.8	05.5	-02.4	11.0	07	-06.4	10	01	01.0	22	01.6	14	01.9	03	01.3	02	02.0	48	
II	-	-02.4	04.2	-00.8	00.6	05.0	-03.8	14.0	13	-06.4	27.22	.	02	01.0	12	01.6	04	04.5	31	01.5	04	01.8	35	
III	-	05.2	12.7	04.4	07.7	14.5	02.0	23.5	30	-05.2	01	02	01.0	14	01.6	38	02.0	02	05.0	.	.	.	12	01.1	23			
IV	-	07.6	14.2	08.1	09.5	15.7	04.2	26.5	07	06.4	20	-	02	01.5	13	01.5	09	02.0	04	04.2	.	.	01	02.0	21	01.2	40	
V	-	13.5	19.9	13.2	14.9	21.6	10.0	26.5	23.22	09.4	01	01	01.0	.	17	01.4	08	01.8	.	.	.	04	01.0	18	01.4	43		
VI	-	15.4	21.0	15.3	16.8	22.2	12.6	31.0	30	07.4	06.05	03	01.3	.	18	01.7	04	02.3	.	.	04	01.5	22	01.5	39			
VII	-	17.1	24.0	16.8	17.5	25.5	13.5	34.0	19	07.6	28	03	01.0	20	01.4	20	01.4	02	01.0	01	01.0	11	01.5	16	01.7	38		
VIII	-	15.9	21.0	16.1	17.5	23.4	13.5	29.5	18	09.6	22	02	01.0	01	02.0	12	01.5	.	.	01	02.0	16	01.6	61				
IX	-	14.4	23.5	19.0	17.0	24.9	12.1	31.0	16	07.8	10	03	01.0	24	01.5	05	02.0	.	.	01	01.0	03	01.0	14	01.3	40		
X	-	07.8	14.8	09.8	09.8	15.7	06.4	26.0	01	00.4	27	01	01.0	02	01.0	15	01.4	01	05.0	.	.	01	01.0	05	01.0	56		
XI	-	02.2	07.1	04.1	04.5	08.1	01.1	20.6	18	-16.0	24	04	01.5	13	01.4	01	01.0	05	01.0	.	.	03	01.2	02	01.2	41		
XII	-	00.0	04.6	01.0	01.4	05.6	-02.3	18.6	17	-08.0	20	03	02.0	15	01.3	05	01.4	02	02.0	.	.	08	01.5	03	01.0	57		
600.	-	03.6	10.6	09.5	10.4	16.3	09.8	32.0	MVN	-16.0	26.XI	16	01.6	144	01.4	22	01.5	57	01.3	12	02.6	06	01.8	06	01.5	664		
$\varphi = 44^{\circ}33' N$ $\lambda = 18^{\circ}42' E$ Gr. $\Delta G = + 1h 15 min.$																												

Mesec	Oblačnost Nm (0-10)			Inkolacija broj sati • ■	Vlažnost vazduha m s			Padavine R mm		Broj dana n sa:																										
	7	14	21		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	A	A	R	•		Δ	Δ	A	A	R	•							
	Sred. (dies)				mm	7	14	21	SR.	Min	Σ	Mx	Dat.	≤	<	<	IV	IV	IV	IV	8	2.0	8.0	0.1	1.0	0.0	•	Δ	Δ	A	A	R	•			
MEĐICA																																				
BR. ST. 121																																				
I	5.5	5.2	4.7	5.2	-	04.8	92	74	92	86	42	630	017.2	29	.	.	25	.	.	.	08	11	04	04	01	04	01	.	.	.	04	.				
II	5.5	5.1	4.4	5.1	-	04.2	92	66	89	83	31	615	005.6	21	.	.	21	.	.	.	01	10	09	05	.	02	03	.	.	.	01	02				
III	6.3	5.9	5.7	6.0	-	06.0	91	53	81	75	30	029	008.1	14	.	.	12	.	.	.	06	08	12	08	.	12	01	01	.	.	01	02				
IV	6.5	6.4	5.5	5.6	-	07.1	79	57	78	71	21	056	022.5	02	.	.	02	.	.	.	06	08	12	10	02	12	01	.	.	.	02	.				
V	5.0	5.7	6.1	5.6	-	11.3	85	63	76	75	37	156	029.4	28	.	.	07	.	.	.	02	06	12	10	04	12	12	.	.	.	01	08				
VI	6.6	6.0	7.5	6.7	-	13.0	83	64	82	76	46	073	026.3	23	.	.	14	01	.	.	02	02	12	17	11	02	17	.	.	.	10	.				
VII	3.1	4.5	3.8	3.8	-	14.7	85	63	81	76	47	162	042.0	01	.	.	21	03	.	.	02	01	10	03	11	09	05	11	.	.	.	08	01			
VIII	5.6	5.5	5.3	5.5	-	14.2	88	67	87	81	50	103	014.4	05	.	.	13	.	.	.	04	08	17	15	03	17	.	.	.	03	02					
IX	5.3	2.6	2.2	3.3	-	13.4	94	60	84	79	35	048	020.4	68	.	.	21	.	.	.	10	02	04	04	02	04	02	04				
X	6.7	6.3	6.0	6.3	-	09.4	94	81	93	79	33	035	014.4	14	.	.	01	.	.	.	06	14	13	08	02	13	.	.	.	01	04					
XI	6.2	7.6	7.1	7.6	-	09.9	94	85	94	91	44	060	020.2	11	01	01	09	.	.	.	02	04	19	14	11	01	12	04	02	.	.	01	01			
XII	7.8	6.9	8.0	7.6	-	04.7	95	84	93	91	53	013	003.2	17	.	.	03	29	.	.	.	01	17	07	03	03	04	03	.	.	04	01				
GOD.	5.0	5.5	5.5	5.7	-	09.0	89	68	86	-	21	800	042.0	04VII	01	04	94	75	04	.	C6	02	71	119	128	100	24	120	13	03	.	.	01	36	25	09
POBINE																																				
BR. ST. 122																																				
I	4.8	5.5	5.9	5.4	-	-	-	-	-	-	-	041	010.5	02	.	08	-	.	.	.	02	C8	C8	08	01	02	C8	01	.	.	08	31				
II	5.5	5.6	5.1	5.0	-	-	-	-	-	-	-	030	004.1	03	.	09	-	.	.	.	01	09	09	09	.	02	09	01	.	.	01	28				
III	4.1	5.0	5.9	5.0	-	-	-	-	-	-	-	035	010.9	21	.	01	-	.	.	.	05	04	11	11	01	04	03	.	.	.	10	.				
IV	5.9	6.2	6.5	6.2	-	05.4	86	48	90	75	20	120	028.5	02	.	.	02	.	.	.	01	08	14	13	04	16	01	.	.	.	08	04				
V	5.6	5.8	6.4	5.9	-	06.7	75	42	88	68	-	172	054.5	21	.	.	-	-	.	.	.	C8	12	12	04	12	.	.	.	02	05	04				
VI	6.3	6.2	7.4	6.6	-	08.4	80	48	86	71	22	097	015.0	04	.	.	07	01	.	.	.	02	16	19	18	02	14	.	.	.	04	15				
VII	3.8	4.6	4.0	4.8	-	10.5	81	55	88	75	33	077	015.0	03	.	.	11	01	.	.	.	05	04	12	12	02	12	02	.	.	03	16				
VIII	5.3	6.2	6.7	6.0	-	09.7	88	54	92	78	35	144	032.0	19	.	.	08	.	.	.	01	06	20	20	01	20	.	.	.	01	23					
IX	3.1	4.2	5.0	4.1	-	-	-	-	-	-	-	060	028.0	13	.	.	04	.	.	.	07	C6	C7	07	03	07	.	.	.	18	.					
X	5.7	5.8	7.2	6.2	-	-	-	-	-	-	-	109	018.3	13	.	.	06	01	.	.	.	07	11	14	14	05	14	.	.	.	01	23				
XI	6.0	6.5	7.0	6.5	-	-	-	-	-	-	-	146	040.2	19	04	07	21	.	.	.	01	07	16	12	03	09	09	.	.	01	21	13				
XII	6.3	5.5	6.1	5.9	-	-	-	-	-	-	-	049	020.3	18	10	09	30	.	.	.	01	05	09	09	01	02	08	.	.	14	23					
GOD.	5.2	5.6	6.4	5.7	-	-	-	-	-	-	-	1086	054.5	24V	-	-	-	-	-	03	.	43	97	147	145	29	111	47	02	.	.	02	14	193	109	
RAČA																																				
BR. ST. 123																																				
I	3.7	4.5	4.3	4.2	-	03.8	83	76	84	79	41	640	019.6	02	.	.	24	12	08	08	06	03	06	02	.	.	.	12				
II	5.3	4.6	5.2	5.1	-	03.5	80	61	82	74	36	035	010.9	21	.	.	23	01	09	11	10	08	01	05	09	04	.	01	14			
III	5.6	6.3	6.1	5.4	-	05.2	72	51	76	66	25	044	013.4	21	.	.	07	04	07	08	06	01	00	03	03	.	.	01	01			
IV	6.4	5.9	5.1	5.0	-	06.1	74	54	83	70	19	109	032.0	02	.	.	02	03	.	.	.	01	08	13	14	12	02	14	04	04	.	04	04			
V	5.7	6.4	5.1	5.8	-	10.3	84	62	92	80	39	160	024.2	08	.	.	10	06	09	18	14	06	18	.	.	.	06	03				
VI	6.2	6.3	6.8	6.5	-	12.0	85	67	93	82	34	129	024.5	18	.	.	11	01	.	.	.	04	11	20	18	04	20	.	.	.	03	04				
VII	4.2	4.7	3.8	4.3	-	13.3	85	62	93	80	35	091	027.4	19	.	.	18	04	.	.	.	12	08	15	15	03	15	.	.	.	04	04				
VIII	6.5	6.8	5.7	6.3	-	13.1	92	76	95	86	44	116	011.5	14	.	.	11	06	13	19	17	06	16	16	.	.	10	16				
IX	2.8	3.8	1.7	2.8	-	12.1	88	62	94	82	38	031	013.2	13	.	.	14	01	.	.	.	16	02	08	06	01	01	08	.	.	03	04				
X	5.9	5.4	5.9	5.9	-	08.0	92	68	95	85	38	116	020.8	24	.	.	01	09	12	16	15	03	14	.	.	.	01	06				
XI	6.3	6.2	6.2	6.2	-	05.6	88	78	90	85	46	075	018.2	24	02	03	07	.	.	.	01	01	05	14	13	02	11	05	.	.	02	07				
XII	5.3	6.2	4.7	5.4	-	04.4	84	77	89	83	60	044	017.9	28	.	.	29	02	05	07	06	04	02	05	.	.	04	10				
GOD.	5.4	5.6	4.8	5.3	-	08.1	84	65	89	79	15	1084	032.6	02IV	02	05	86	67	05	.	.	09	01	96	119	156	136	34	142	32	16	.	.	26	46	48
TUZLA																																				
BR. ST. 124																																				
I	4.1	4.9	4.1																																	

Mjesec	Vrstdišni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, Pm (0-12)																	
		Tm				M	M	M	M	M	M	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21	Sred. (D18)								č.	j.															
$\varphi = 44^{\circ}12' N$ $\lambda = 18^{\circ}57' E$ Gr. $\Delta G = + 1h\ 16\ min.$																													
I	-	02.0	05.9	03.6	03.8	07.1	-00.4	12.0	04	-06.2	16	08	C1.2	04	C1.0	C8	01.4	12	01.0	18	01.0	09	01.1	25	01.2	02	C1.0	07	
II	-	-02.3	C2.9	-00.7	-00.2	C5.2	-04.6	11.8	07	-11.0	09	13	C1.1	09	C1.3	12	C1.1	16	C1.1	07	C1.1	05	C1.4	14	C1.6	C8	C1.2	-	
III	-	05.7	10.8	07.1	07.7	12.8	02.2	26.8	31	-05.4	01	17	C1.6	14	C1.9	11	C1.5	C8	C1.9	11	C1.9	06	C1.7	13	C1.9	06	C1.3	07	
IV	-	08.2	12.1	08.5	09.3	14.4	04.1	23.4	07	00.0	12	11	C2.2	03	C3.0	20	02.0	22	C1.7	15	C1.9	06	C1.7	04	C1.8	03	C2.3	06	
V	-	13.7	16.7	12.9	14.0	18.4	05.2	24.8	19	05.2	02	18	C1.2	04	C1.5	14	C1.7	16	C1.4	11	C1.3	11	C1.6	13	C1.5	04	C2.2	02	
VI	-	15.2	18.2	15.5	16.1	20.1	11.2	26.8	30	04.4	08	23	C1.2	03	C1.0	13	C1.4	16	C1.6	10	C1.4	10	C2.0	06	C1.8	01	C1.0	08	
VII	-	18.1	22.6	17.4	18.9	24.0	12.8	32.8	19	07.8	02.01	20	C1.0	04	C1.2	12	C1.5	20	C1.7	11	C1.4	07	C1.9	09	C2.2	06	C1.3	04	
VIII	-	17.0	20.5	16.6	17.7	22.1	12.5	26.2	12	10.2	30.15	27	21	C1.5	08	C1.8	11	C2.1	13	C1.0	08	C2.0	14	C1.5	01	C1.0	09		
IX	-	16.0	21.8	16.6	17.7	22.5	12.5	29.8	16	07.8	10	39	C2.0	05	C2.0	04	C1.2	05	C1.4	01	C1.0	09	C1.8	07	C1.4	07	C2.1	13	
X	-	08.9	13.3	09.4	10.3	16.1	05.9	26.4	01	02.4	26	35	C2.1	04	C1.0	07	C1.1	02	C2.0	04	C1.0	08	C1.2	12	C1.2	06	C1.0	15	
XI	-	02.5	05.9	03.4	03.8	08.2	-00.1	17.6	02	-12.6	25	25	C2.0	02	C2.5	14	C1.1	06	C1.5	02	C1.0	04	C1.2	17	C1.4	10	C1.3	10	
XII	-	-00.5	03.7	01.4	01.5	06.3	-03.1	14.2	17	-11.8	20	38	C2.0	03	C1.7	14	C1.9	13	C1.3	06	C1.3	11	C1.5	05	C2.2	-			
God.	-	08.7	12.8	09.3	10.0	14.9	05.2	32.8	49.VII	-12.6	25.XI	274	C1.6	57	C1.6	137	C1.5	147	C1.5	106	C1.3	89	C1.6	145	C1.5	59	C1.5	81	
$\varphi = 44^{\circ}47' N$ $\lambda = 19^{\circ}16' E$ Gr. $\Delta G = + 1h\ 17\ min.$																													
I	-	-00.3	C6.0	01.2	02.2	07.6	-01.6	18.0	06	-06.0	01	.	.	01	01.0	21	C1.1	13	C1.2	03	C1.0	17	C1.3	38	
II	-	-01.6	C6.0	00.5	01.4	06.4	-02.8	14.5	13	-07.7	09	08	C1.0	02	C1.5	03	C1.0	.	22	C1.3	07	C1.3	03	C1.3	16	C1.8	21		
III	-	04.1	14.7	07.4	08.4	16.2	02.5	25.6	31	-05.4	01	06	C1.5	06	C1.3	07	C1.0	22	C1.4	10	C1.9	06	C1.0	09	C1.4	27			
IV	-	08.5	15.8	09.6	10.9	17.2	06.1	27.6	07.06	01.2	12	03	C1.7	.	.	01	C1.0	.	.	18	C1.6	04	C1.5	11	C1.2	33	C1.7	20	
V	-	14.8	22.2	19.4	17.0	23.3	11.7	28.2	20	05.1	01	03	C1.0	.	.	06	C1.3	03	C1.3	22	C1.3	04	C1.5	10	C1.4	17	C1.9	28	
VI	-	18.8	23.1	17.4	18.7	24.3	14.5	31.4	24	09.5	06	02	C1.0	.	.	02	C1.0	03	C1.3	19	C1.3	03	C1.7	14	C1.4	16			
VII	-	18.6	25.8	19.2	20.7	26.9	19.5	32.5	29	05.6	27	04	C1.0	.	.	C2	C1.0	01	C1.0	06	C1.5	07	C1.6	09	C1.5	25			
VIII	-	17.1	24.4	17.6	19.2	25.3	19.4	30.3	11	11.7	19	03	C1.0	01	C1.0	02	C1.5	19	C1.1	03	C1.3	12	C1.1	31	C1.3	24			
IX	-	19.0	25.3	17.0	18.6	29.1	13.3	31.1	16	08.2	14	03	C1.0	01	C2.0	04	C1.0	02	C1.0	26	C1.1	11	C1.0	14	C1.0	19	C1.3	10	
X	-	08.2	19.2	09.5	10.6	18.2	07.1	27.7	01	00.0	30	02	C1.0	.	.	04	C1.9	06	C1.7	08	C1.2	11	C1.2	13	C1.0	33	C1.1	16	
XI	-	02.5	07.6	04.1	04.6	08.6	01.9	19.8	18	-10.7	26	01	C1.0	02	C1.5	20	C1.3	11	C1.7	12	C1.7	09	C1.4	05	C1.2	21	C1.5	09	
XII	-	-00.3	04.1	00.9	01.4	05.3	-01.5	12.4	17	-04.5	21	06	C1.0	01	C1.0	15	C1.3	C2	C1.5	04	C1.2	05	C1.4	15	C1.3	26	C1.3	19	
God.	-	08.6	15.9	10.0	11.1	17.0	06.8	32.5	49.VII	-10.7	26.XI	41	C1.3	08	C1.4	67	C1.2	37	C1.4	195	C1.3	87	C1.4	115	C1.2	288	C1.4	257	
$\varphi = 44^{\circ}07' N$ $\lambda = 19^{\circ}19' E$ Gr. $\Delta G = + 1h\ 17\ min.$																													
I	-	-02.4	04.7	00.5	00.8	-	-	-	-	-	-	05	C1.0	26	C1.0	62	
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	05.3	10.8	07.1	07.6	11.9	03.8	19.0	30	-08.2	22	08	C1.2	.	.	22	C1.9	.	.	07	C1.3	56		
IV	-	08.8	13.1	09.7	10.3	14.4	06.1	21.7	21	02.1	27	11	C1.4	.	.	.	35	C1.5	44			
V	-	14.7	20.7	14.2	16.2	21.6	12.3	26.0	12	08.1	24	-	-			
VI	-	15.4	21.5	14.6	16.5	22.4	12.5	28.1	24	05.0	09	-	-			
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	14.9	22.1	15.4	17.0	23.1	12.5	27.3	23	10.1	26.14	01	C1.0	.	.	.	C7	C1.0	85			
IX	-	14.6	20.9	15.4	16.6	21.9	13.1	26.6	16	11.2	06	19	C1.0	.	.	.	C5	C1.0	66			
X	-	08.9	13.8	09.9	10.9	14.7	08.4	22.8	01	05.2	27	08	C1.0	.	.	.	C3	C1.0	72			
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
God.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 43^{\circ}50' N$ $\lambda = 17^{\circ}01' E$ Gr. $\Delta G = + 1h\ 08\ min.$																													
I	-	701.8	-02.7	05.3	-00.2	00.5	04.5	-03.8	10.4	06	-05.8	11	02	C2.5	02	C1.5	10	C1.9	C2	C1.9	02	C1.0	C4	C1.8	05	C2.4	08	C2.8	52
II	-	701.3	-03.3	05.1	-00.3	00.2	04.4	-04.5	14.0	19	-10.3	09	14	C4.7	03	C2.3	06	C1.3	02	C2.5	05	C2.0	06	C2.3	16	C3.1	26		
III	-	693.8	03.3	04.1	05.3	05.7	10.1	01.4	16.2	08	-07.4	23.01	.	.	10	C2.6	33	C3.2	20	C2.8	05	C1.8	01	C2.0	04	C3.5	01	C3.0	17
IV	-	697.2	06.1	12.1	07.7	08.4	13.3	03.2	20.4	21	-0																		

Meseč Broj	Vrednost pritisak mm Hg	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, fm (0-12)																
		Tm					H	H15	H30	H45	H60	H75	H90	P	N	NE	E	SE	S	SW	W	NW	C					
		7	14	21	Srednji (Dnev.)																							
$\varphi = 43^{\circ}23' N$ $\lambda = 17^{\circ}36' E$ Gr. $\Delta G = + 1h\ 10\ min.$																												
I	-	00.1	09.8	02.8	03.6	10.6	-01.6	14.8	20.0	-08.2	10	12	C3.3	01	08.0	.	.	81		
II	-	-00.1	09.7	03.5	04.1	10.2	-01.6	17.0	06	-08.0	10	27	C4.5	02	02.3	.	.	56		
III	-	06.3	12.4	08.6	09.0	-	03.9	-	-	-03.4	01	07	C5.1	06	02.3	.	.	80	.	.	.		
IV	-	10.2	16.5	11.2	12.3	-	06.2	-	-	00.2	13	28	C2.5	02	01.5	.	.	01	02.0	.	.	59	
V	-	14.9	21.4	15.6	17.0	22.6	10.5	30.4	18	04.6	01	06	C2.7	03	02.0	84	
VI	-	17.6	24.1	17.9	19.4	25.5	13.0	31.6	23	08.0	07	13	C4.1	01	01.0	76	
VII	-	20.2	28.9	20.7	22.7	29.8	15.0	36.2	18	04.6	02	14	C2.1	02	02.0	.	.	01	02.0	.	.	76	
VIII	-	19.1	26.8	19.7	21.3	28.7	14.6	33.2	10	10.6	23	34	C2.7	58	
IX	-	14.8	26.8	17.9	19.4	27.7	12.5	35.0	17	09.4	25	07	C2.4	01	04.0	82	
X	-	09.4	18.8	11.3	12.7	20.0	07.1	29.0	03.01	01.0	31.2	13	C2.5	01	02.0	79	
XI	-	04.6	11.0	06.6	07.2	12.5	02.3	21.0	02	-01.8	24	13	C4.5	02	03.0	75	
XII	-	01.8	10.8	03.8	09.1	11.4	-00.3	16.0	28	-04.0	21	08	C4.0	85	
600.	-	09.9	18.1	11.6	12.8	-	06.0	-	-	-09.8	06.XI	182	C3.3	17	02.1	.	.	04	04.0	.	.	892	
$\varphi = 43^{\circ}50' N$ $\lambda = 17^{\circ}38' E$ Gr. $\Delta G = + 1h\ 10\ min.$																												
I	-	-04.0	05.5	-01.0	-00.1	07.2	-06.6	12.4	17	-15.2	10	08	C1.9	.	.	C1	C2.0	C5	C2	C1.5	.	.	01	C3.0	.	.	72	
II	-	-03.6	04.3	-00.9	-00.3	05.6	-05.8	11.8	13.0	-07.11.6	18	07	C1.7	02	02.5	.	.	07	02.6	03	02.0	02	02.5	02	02.5	62		
III	-	01.5	09.9	03.6	04.7	11.5	-00.5	16.8	08	-05.4	01	13	C1.8	.	.	04	02.2	06	02.5	01	02.0	03	02.0	02	02.5	62		
IV	-	05.7	12.4	07.0	08.1	14.3	02.2	21.4	06	-00.1	13	06	C2.0	03	03.0	01	02.0	01	02.0	02	01.5	01	02.0	12	02.1	67	02.9	57
V	-	11.6	18.5	11.9	13.5	20.4	06.8	27.4	17	01.2	02	03	C2.3	01	03.0	C2	C2.0	C2	C2.5	.	.	08	C1.9	02	C2.5	75		
VI	-	19.4	25.7	12.9	14.7	21.4	07.8	29.4	29	02.0	06	07	C2.1	.	.	01	03.0	05	01.6	.	.	06	C1.8	03	C2.7	68		
VII	-	19.4	23.8	15.8	17.7	25.8	10.6	33.6	18	03.2	01	01	C3.0	.	.	04	02.0	03	01.7	.	.	18	C1.6	08	C2.2	59		
VIII	-	14.0	21.9	14.6	16.3	24.1	09.9	28.8	18	06.6	22	01	C2.0	.	.	03	01.3	04	01.8	02	02.0	11	01.6	02	02.0	70		
IX	-	12.2	22.8	13.1	15.3	24.7	08.8	31.6	17	06.4	24	01	C1.0	.	.	01	01.0	05	01.4	.	.	11	C1.7	03	C2.0	69		
X	-	05.7	14.6	07.6	08.8	16.2	02.9	27.4	01	-02.6	27	10	C1.9	03	02.3	01	01.0	02	02.5	02	01.0	07	02.0	07	02.0	63		
XI	-	01.0	07.0	02.7	03.4	08.6	-01.8	19.2	02	-16.4	26	13	C2.2	.	.	02	02.5	01	04.0	04	02.0	07	01.6	04	02.2	71		
XII	-	-01.7	05.9	00.0	01.1	07.9	-04.5	15.4	02	-11.6	08	07	C2.0	.	.	01	03.0	01	01.0	.	.	09	01.6	04	02.2	71		
600.	-	08.9	13.9	07.3	08.6	15.6	02.4	33.6	08.VII	-16.6	06.XI	77	02.0	09	02.7	05	01.8	37	02.4	35	01.8	05	02.4	88	01.8	42	02.3	797
$\varphi = 43^{\circ}05' N$ $\lambda = 17^{\circ}43' E$ Gr. $\Delta G = + 1h\ 11\ min.$																												
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	14.4	23.3	16.3	18.1	25.0	12.1	31.0	19.18	06.0	10	24	C1.6	02	02.5	.	.	03	01.3	.	.	31	C3.3	.	.	16	C1.5	17
VI	-	20.3	27.0	19.1	21.4	26.3	14.6	32.5	29	11.3	11	32	C2.6	.	.	03	04.2	.	.	20	C4.2	.	.	33	C1.6	09		
VII	-	22.4	30.0	21.4	24.0	32.1	16.1	37.5	18	11.0	02	40	C1.9	.	.	03	03.3	23	C2.8	.	.	16	C1.9	11				
VIII	-	20.0	28.0	20.7	22.6	30.1	-	34.0	18.10	-	37	01.6	03	03.0	.	.	01	02.0	27	C2.4	.	.	14	C1.1	11			
IX	-	14.3	26.3	18.1	20.2	29.7	13.6	34.0	17	18.2	25	23	C1.4	.	.	01	03.0	23	C1.9	03	01.0	13	C1.2	27				
X	-	10.3	20.7	12.9	15.9	22.6	02.2	-	-	-	-	34	C1.6	.	.	01	02.9	14	C1.9	.	.	10	C1.1	25				
XI	-	08.8	13.3	08.2	08.9	15.1	04.4	24.5	18	-06.0	26	45	C1.6	.	.	04	01.0	06	04.0	.	.	10	C1.3	25				
XII	-	02.9	11.8	04.8	06.1	13.8	01.7	17.2	03	-04.0	27	44	C1.7	.	.	04	01.2	02	02.0	02	05.0	.	.	03	01.0	36		
600.	-	08.8	16.8	11.8	12.3	-	07.0	-	-	-08.4	07.XI	161	C2.7	01	03.0	52	03.2	.	.	81	C3.3	.	.	67	03.1	.	.	693
$\varphi = 43^{\circ}40' N$ $\lambda = 17^{\circ}46' E$ Gr. $\Delta G = + 1h\ 11\ min.$																												
JASLANICA																												
BR. ST. 134																												
I	-	-01.8	06.3	00.1	01.2	07.4	-02.7	11.2	27	-06.0	11	18	C3.1	.	.	C4	C5.0	.	.	13	C3.0	.	.	62	C2.0	.	.	56
II	-	-00.4	07.4	01.0	02.8	08.7	-01.4	14.4	19	-07.2	20	21	C3.7	.	.	02	03.5	.	.	02	03.0	.</td						

Mesec	Oblačnost Nm (0-10)				Inzolacijska broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																					
	7	14	21	Stot. (dies)			m	t		R	mm	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	Δ	Δ	▲	▲	R	T	≡	■	
						%	7	14	21	Σ	mm	7	14	21	Σ	mm	6	8	2.0	8.0	0.1	1.0	0.0	P	Δ	Δ	Δ	Δ	▲	▲	R	T	≡
LISTICA																																	
BR. ST.131																																	
I 4.1 4.4 2.7 3.7	-	04.5 75 61 77 71 38	032 015.8	29	-	-	21	-	-	03	-	12	65	04	03	02	04	-	-	-	-	-	-	-	-	-	-	-	-	01			
II 3.4 3.5 2.2 3.0	-	04.6 73 62 81 72 45	010 006.0	14	-	-	18	-	-	12	03	16	64	04	03	02	04	-	-	-	-	-	-	-	-	-	-	-	-	01			
III 7.7 7.7 6.2 7.2	-	07.0 81 71 83 79 45	213 043.2	29	-	-	05	-	-	02	02	02	17	16	14	06	16	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV 5.2 5.0 3.2 4.5	-	07.8 70 66 77 71 39	124 031.0	02	-	-	-	-	-	01	01	10	09	10	04	04	04	-	-	-	-	-	-	-	-	-	-	-	-	-			
V 4.2 4.1 4.8 5.0	-	11.4 71 70 81 77 37	133 031.2	21	-	-	-	05	01	01	11	10	12	12	01	12	-	-	-	-	-	-	-	-	-	-	-	-	02				
VI 4.3 5.0 4.3 4.8	-	12.3 74 62 76 71 26	061 014.5	17	-	-	-	20	04	02	02	07	03	10	10	02	10	-	-	-	-	-	-	-	-	-	-	02					
VII 2.0 2.3 1.4 2.2	-	13.9 71 54 74 66 33	022 009.0	06	-	-	-	27	21	-	19	01	04	04	04	04	-	-	-	-	-	-	-	-	-	-	03						
VIII 4.1 5.0 2.7 3.9	-	13.9 73 56 77 69 35	115 041.0	27	-	-	28	14	02	01	08	08	08	08	08	08	-	-	-	-	-	-	-	-	-	-	02						
IX 1.7 3.6 1.1 2.1	-	12.8 82 58 82 74 38	076 042.0	13	-	-	-	27	03	01	18	02	04	04	01	04	-	-	-	-	-	-	-	-	-	-	04						
X 4.3 4.8 3.9 4.3	-	08.0 81 68 79 76 47	364 176.4	13	-	-	-	06	-	-	15	09	13	13	04	13	-	-	-	-	-	-	-	-	-	03							
XI 5.2 4.3 5.1 5.5	-	06.7 84 70 84 82 61	193 046.6	11	-	-	06	-	-	04	01	08	11	15	13	04	15	-	-	-	-	-	-	-	-	-	-	-					
XII 3.6 3.6 2.7 3.3	-	05.9 82 70 81 78 23	142 042.2	18	-	-	19	-	-	02	01	18	06	07	07	03	07	-	-	-	-	-	-	-	-	-	-	-	-				
600. 4.2 4.9 3.4 4.1	-	09.0 77 65 79 79 23	1487 176.4	65X	-	-	69	-	-	30	11	144	81	107	103	38	107	-	-	-	-	-	-	-	-	-	-	14	02				
PROZOR																																	
BR. ST.132																																	
I 4.8 4.8 4.5 4.7	-	03.0 71 77 81 76 25	022 005.0	09	03	-	29	-	-	12	08	09	07	07	03	01	-	-	-	-	-	-	-	-	-	02	06						
II 3.5 4.1 4.4 4.0	-	03.0 66 77 84 80 53	017 005.0	14	01	-	26	-	-	16	09	07	04	04	03	-	-	-	-	-	-	-	-	-	-	03							
III 6.9 6.8 6.8 6.7	-	05.4 83 73 83 79 53	108 022.0	14	-	-	11	-	-	05	14	19	17	03	16	05	-	-	-	-	-	-	-	-	-	04							
IV 5.7 6.0 4.7 5.5	-	05.9 73 65 70 69 52	076 017.0	01	-	-	01	-	-	10	11	11	10	04	10	02	-	-	-	-	-	-	-	-	-	01							
V 5.0 6.7 6.7 5.5	-	07.0 67 59 65 64 45	065 019.2	15	-	-	02	-	-	05	09	16	14	01	14	-	-	-	-	-	-	-	-	-	02								
VI 5.0 7.2 7.0 6.4	-	09.5 73 68 67 70 32	071 015.6	10	-	-	08	-	-	03	13	12	11	03	12	-	-	-	-	-	-	-	-	-	02								
VII 3.7 3.9 3.9 3.7	-	11.6 80 62 78 73 39	035 008.6	02	-	-	21	07	-	13	05	10	08	08	10	-	-	-	-	-	-	-	-	-	01								
VIII 5.7 6.2 4.9 5.6	-	10.9 81 64 80 76 47	122 029.4	25	-	-	14	-	-	07	09	15	14	03	15	-	-	-	-	-	-	-	-	-	02								
IX 3.4 4.3 3.8 3.9	-	10.3 82 61 81 75 48	030 016.0	13	-	-	14	01	-	18	04	04	04	01	04	-	-	-	-	-	-	-	-	-	02								
X 5.9 5.9 5.9 5.9	-	06.6 82 64 76 74 36	144 035.4	14	-	-	06	03	-	09	12	12	11	03	12	-	-	-	-	-	-	-	-	02									
XI 6.2 6.8 7.0 7.1	-	04.0 77 71 80 76 21	087 023.4	19	03	03	10	-	-	04	19	12	10	03	10	03	-	-	-	-	-	-	-	-	11	04							
XII 5.6 5.4 4.1 5.0	-	04.0 74 70 78 74 46	044 025.6	18	03	02	26	-	-	07	10	09	03	01	04	-	-	-	-	-	-	-	-	-	07								
600. 5.1 5.7 5.1 5.3	-	07.0 77 68 77 74 21	823 035.4	64X	10	09	109	63	08	-	101	123	136	115	26	121	20	01	-	-	-	-	-	-	-	07	23						
ČAPLIJINA-KLEPČI																																	
BR. ST.133																																	
I - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV 4.6 4.2 3.5 4.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	02				
V 5.0 5.5 4.2 5.2	-	10.9 70 53 75 69 19	051 005.1	20	-	-	-	15	03	-	02	04	06	11	05	11	-	-	-	-	-	-	-	-	-	01							
VI 4.1 5.3 3.2 4.2	-	12.2 64 49 69 61 27	014 004.4	17	-	-	-	25	11	-	03	06	02	05	05	05	05	-	-	-	-	-	-	-	-	01							
VII 2.0 2.7 1.9 2.1	-	13.3 65 41 70 59 20	027 014.0	31	-	-	-	20	25	-	-	21	02	05	05	01	05	-	-	-	-	-	-	-	-	03							
VIII 3.5 4.0 2.1 3.2	-	12.6 74 42 73 63 24	199 062.7	25	-	-	-	20	20	-	-	11	10	10	14	14	10	04	14	-	-	-	-	-	-	04							
IX 2.1 2.4 1.6 2.0	-	14.0 90 54 90 78 38	090 072.3	13	-	-	-	30	14	-	-	19	01	05	04	01	05	-	-	-	-	-	-	-	-	03							
X 4.8 5.0 3.4 4.4	-	09.2 84 56 84 79 27	216 036.7	14	-	-	-	-	-	-	-	13	07	12	11	08	12	-	-	-	-	-	-	-	-	04							
XI 6.2 6.8 4.8 5.0	-	07.1 82 69 84 78 25	141 040.7	11	-	-	03	-	-	01	05	10	17	13	05	17	-	-	-	-	-	-	-	-	03								
XII 4.2 4.5 3.2 4.0	-	05.6 77 65 81 74 36	088 034.0	18	-	-	09	-	-	11	09	04	04	04	04	04	-	-	-	-	-	-	-	-	02								
600. - - - -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
JABLJANICA																																	
BR. ST.134																																	
I 6.9 4.6 5.0 5.5	-	04.2 86 68 90 81 45	024 012.2	08	-	-	24	-	-	02	04	07	05	04	01	05	-	-	-	-	-	-	-	-	-	01							
II 4.6 4.1 5.2 4.7	-	04.6 89 69 85 81 43	004 003.0	14	-	-	16	-	-	02	01	08	08	02	01	02	-	-	-	-	-	-	-	-	-	01							
III 6.9 7.0 8.0 8.0	-	06.9 84 64 82 78 34	264 084.0	29	-	-	05	-	-	03	01	21	19	18	07	19	-	-	-	-													

M esec	Vaspodolni pritisak P ₀	Temperatura vazduha °C										Cestina pravaca i srednja jačina vatra nD, fm (0-12)																													
		Zm					Jn					Cestina pravaca i srednja jačina vatra nD, fm (0-12)																													
		7	14	21	28 (D18)	1M	15	2M	3M	4M	5M	Dati.	N	NE	E	SE	S	SW	W	NW	C	8.	9.	8.	9.	8.	9.	8.	9.												
$\varphi = 43^{\circ}21' N$ $\lambda = 17^{\circ}48' E$ Gr. $\Delta G = + 1h 11 min.$																									MCSTAR		BR. ST. 136														
I	751.4	02.0	09.4	04.5	09.1	10.0	01.1	13.8	27	-03.0	11	31	02.2	16	03.6	1	5	1	2	01.5	1	1	1	1	1	1	1	1	1	03	01.3	43									
II	756.5	03.8	10.3	05.8	06.4	11.1	02.7	16.2	19	-03.0	10	26	03.9	30	04.3	02	01.5	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1								
III	746.9	07.2	14.2	10.3	10.5	15.2	06.4	22.2	08	-03.2	01	18	02.3	16	02.4	1	1	1	1	14	02.8	05	02.0	10	01.7	07	01.4	23													
IV	751.4	10.6	17.7	13.0	13.6	18.9	08.7	24.6	06	02.0	13	26	02.8	13	03.7	01	02.0	01	02.0	09	03.3	04	01.5	10	02.0	05	02.0	21													
V	750.5	15.6	23.1	17.2	18.3	24.3	13.1	30.3	18	07.0	01	19	02.4	11	02.5	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1								
VI	750.5	18.6	25.7	20.0	21.1	26.9	19.9	33.0	29	12.0	09	29	02.7	14	02.9	02	02.0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1							
VII	750.3	21.7	30.3	23.6	24.8	31.1	19.0	37.4	18	13.6	03	31	02.7	23	02.9	04	02.5	05	01.6	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1					
VIII	751.4	20.2	27.9	22.1	23.1	29.1	18.0	34.2	11.10	14.5	23	35	02.8	22	03.1	02	02.5	02	02.0	05	02.0	02	03.0	04	01.8	03	02.7	14													
IX	754.7	17.8	26.2	20.4	21.7	28.7	14.6	34.2	17	12.4	26	36	01.7	11	02.1	04	01.5	02	01.5	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1					
X	754.2	12.2	19.7	14.3	15.1	20.8	11.3	30.4	01	06.0	31	39	03.1	20	03.2	01	02.0	02	04.5	02	02.0	04	02.2	01	02.0	08	02.6	16													
XI	753.6	06.7	11.6	08.1	08.6	12.8	05.5	21.8	02	-03.8	27	35	03.0	09	03.3	01	01.0	02	02.5	02	03.5	01	02.0	01	02.0	16	01.9	23													
XII	750.4	04.6	10.7	05.8	06.8	11.3	03.4	16.8	02	-01.0	08	35	02.5	04	04.0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1								
ODD.	753.0	11.8	19.1	13.8	14.6	20.0	10.1	37.4	45.WN	-03.8	27.XI	360	02.7	197	03.2	17	01.9	18	02.2	49	02.7	36	02.2	64	01.9	92	02.3	262													
$\varphi = 43^{\circ}46' N$ $\lambda = 18^{\circ}02' E$ Gr. $\Delta G = + 1h 12 min.$																									IVAN SEDLO		BR. ST. 137														
I	-	-02.7	01.9	-01.2	-00.8	02.6	-04.2	07.3	25	-12.6	10	03	01.0	10	01.6	14	01.4	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1						
II	-	-04.4	00.0	-02.6	-02.4	01.0	-05.7	06.6	13	-10.4	27	.	.	28	02.6	29	03.2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1						
III	-	02.9	07.0	04.1	04.3	08.2	01.3	14.6	26	-04.8	26.22	01	01.0	08	02.5	05	03.4	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1						
IV	-	04.6	09.4	04.5	06.8	10.9	02.5	18.8	06	-01.0	26	01	01.0	15	02.2	22	02.7	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1						
V	-	10.6	16.7	11.5	12.6	17.6	08.2	22.1	22	03.4	04	02	01.0	10	01.6	10	02.2	01	01.0	03	01.0	19	02.1	28	03.1	1	1	1	1	1	1	1	1	1	1						
VI	-	12.4	17.2	12.5	13.6	18.2	10.0	25.6	28	02.8	06	03	01.3	04	01.5	21	02.0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1						
VII	-	14.0	20.4	15.0	16.1	21.5	11.7	29.0	18	06.1	28	03	01.0	19	01.7	17	01.9	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1						
VIII	-	12.7	18.6	13.8	14.7	19.3	11.4	24.4	17.12	07.3	22	01	01.0	15	01.8	20	01.6	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1						
IX	-	12.2	19.8	13.8	14.9	20.2	10.7	25.3	16	06.6	26	01	02.0	07	01.4	09	01.8	01	03.0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1				
X	-	05.2	10.9	04.9	07.5	11.7	04.4	24.0	26	01	01.0	10	01.3	34	02.0	1	1	01	00.0	1	1	21	02.7	02	02.0	24															
XI	-	06.9	04.2	01.7	02.1	05.6	-00.6	16.3	03	-14.0	26	.	.	08	01.4	22	02.5	1	1	01	00.0	02	02.0	30	03.1	01	01.0	24													
XII	-	-01.6	01.9	-00.4	-00.2	02.6	-03.0	10.0	17	-08.7	21	.	.	10	01.3	31	02.4	1	1	02	05.5	05	01.6	16	03.4	.	29														
ODD.	-	05.6	10.6	06.8	07.4	11.6	03.9	29.0	45.WN	-14.0	26.XI	16	01.1	144	01.9	234	02.3	02	02.0	07	04.6	95	03.2	300	03.4	16	01.9	281													
$\varphi = 43^{\circ}06' N$ $\lambda = 18^{\circ}11' E$ Gr. $\Delta G = + 1h 13 min.$																									BERKOVICI		BR. ST. 138														
I	-	-00.6	07.5	01.6	02.9	07.9	-02.1	12.2	20	-04.6	10	28	02.9	06	01.7	02	01.5	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1			
II	-	00.2	07.4	02.4	03.1	07.8	-01.2	13.2	19.0	-08.4	10	53	03.3	09	01.4	01	02.0	1	1	08	01.4	05	01.8	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
III	-	05.9	10.9	06.9	07.5	11.7	03.2	18.2	31.0	-05.2	01	10	03.7	27	02.1	31	02.2	1	1	16	01.6	03	02.0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
IV	-	09.6	15.0	10.1	11.2	15.7	06.0	23.6	06	-01.0	13	22	03.0	14	01.9	24	02.2	1	1	09	01.8	11	02.4	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
V	-	14.2	20.1	14.2	15.7	21.3	09.7	27.2	19	04.4	10.01	01	03.0	10	02.2	24	01.8	1	1	22	01.6	08	01.9	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
VI	-	16.8	21.6	15.2	17.2	23.3	11.9	29.4	29	07.2	04	20	02.8	10	01.8	09	01.3	1	1	20	01.7	07	02.1	1	1	01	04.0	23													

Mesec	Oblačnost Nm (0-10)				Inkolacijs broj sati (Dnes)	Vlažnost vazduha				Padavine R mm				Broj dana n sati																							
	7	14	21	Sred. (Dnes)		7	14	21	Broj. Min.	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tn	Tx	P(0-12)	Nm(0-10)	R mm	•	•	*	*	Δ	Δ	▲	▲	□	□						
MCSTAR																																					
BR. ST. 136																																					
I	4.2	4.6	3.1	4.0	154.8	04.4	74	58	68	66	35	045	025.3	29	.	.	13	.	.	16	02	10	05	07	05	02	07	.	.	.	03						
II	3.4	4.0	2.9	3.4	184.7	03.9	59	45	53	52	30	010	008.0	14	.	.	05	.	.	19	07	15	05	04	02	.	04	.	.	.	03						
III	8.2	8.1	6.8	7.7	082.8	06.7	77	60	70	65	34	222	071.2	14	.	.	02	.	.	15	02	02	18	20	16	08	20	.	.	.	07	.					
IV	5.4	6.4	4.2	5.3	190.7	07.2	72	54	62	63	26	103	025.0	02	.	.	02	.	.	18	01	08	07	13	09	04	13	.	.	.	01	03					
V	5.8	7.1	5.3	6.0	190.4	10.9	78	56	72	69	29	099	023.0	07	.	.	14	03	.	07	01	05	1C	13	12	03	13	04	.				
VI	5.2	7.2	4.8	5.8	209.0	12.2	75	52	67	64	34	033	013.4	17	.	.	22	10	01	14	01	03	04	12	06	01	12	.	.	.	08	.					
VII	2.7	4.2	1.7	2.9	323.4	13.2	65	46	57	56	34	039	024.0	06	.	.	28	24	12	13	01	14	03	10	07	01	10	.	.	.	07	.					
VIII	5.1	6.1	3.3	4.8	235.3	11.9	64	48	59	58	33	122	041.0	26	.	.	27	13	04	12	02	04	05	12	04	05	12	.	.	.	07	.					
IX	2.6	4.7	2.0	3.1	253.8	13.6	82	53	74	69	43	049	030.5	13	.	.	27	08	03	06	02	12	02	07	06	01	07	.	.	.	04	.					
X	4.9	5.4	4.3	4.9	172.8	08.7	75	51	71	67	37	262	114.2	13	.	.	08	03	.	17	02	10	09	13	13	07	13	.	.	.	01	08					
XI	6.7	6.7	5.0	6.2	101.0	06.5	79	47	76	74	34	180	045.2	11	.	.	03	.	.	10	04	03	12	16	13	05	14	.	.	.	03	02					
XII	3.9	4.6	3.6	4.1	156.2	05.2	74	58	71	68	40	145	080.7	18	.	.	04	.	.	09	04	09	05	07	05	04	07	.	.	.	01	01					
GOD.	4.8	5.8	3.9	4.8	2295.1	08.7	73	54	66	64	26	1309	114.2	05X	.	.	27	125	61	22	145	29	95	85	134	103	41	134	.	.	.	01	01				
IVAN SECLO																																					
BR. ST. 137																																					
I	4.7	5.2	5.7	5.2	063.1	03.5	87	71	84	81	41	032	007.2	27	02	07	29	.	.	11	03	06	09	11	07	.	03	09	.	.	01	03	31				
II	7.4	6.3	5.2	6.3	036.4	03.0	84	68	77	76	26	016	004.3	15	02	12	26	.	.	12	.	05	11	10	06	.	02	08	.	.	06	28					
III	7.4	7.5	6.7	7.2	067.3	04.5	77	62	76	72	20	201	036.7	14	.	02	09	.	.	24	15	02	13	22	16	05	18	06	02	.	03	05	14				
IV	6.6	7.1	5.3	6.3	123.2	04.6	74	56	64	65	16	170	033.3	02	.	.	07	.	.	16	10	06	12	16	13	04	12	08	.	.	01	03	07				
V	6.0	7.6	5.9	6.5	115.0	07.7	80	55	76	70	29	084	016.6	19	.	.	02	.	.	08	01	.	09	14	12	03	14	.	.	.	05	11					
VI	7.6	8.1	6.7	7.4	078.5	09.3	85	64	84	78	46	110	037.4	26	.	.	02	.	.	08	02	02	15	17	14	03	17	.	.	.	07	11					
VII	6.0	6.0	4.1	5.4	126.9	10.0	84	57	78	73	35	066	022.6	06	.	.	03	.	.	04	01	05	07	11	10	09	11	.	.	.	09	08					
VIII	6.2	7.4	6.4	7.3	085.7	09.9	92	62	83	79	42	126	031.4	28	.	.	01	.	.	01	02	15	18	13	04	18	.	.	.	16	17						
IX	5.8	5.1	2.2	4.4	115.7	09.7	91	58	79	76	46	049	035.7	13	.	.	01	.	.	07	04	02	06	02	01	06	.	.	.	01	12						
X	7.5	7.0	5.9	6.8	025.0	06.4	93	67	86	82	40	202	057.1	13	.	.	01	.	.	05	02	05	16	18	14	08	18	.	.	.	05	14					
XI	8.0	7.0	6.9	7.3	033.7	04.7	90	76	85	84	49	135	038.6	11	02	05	12	.	.	12	04	03	19	18	16	03	14	.	.	.	01	10					
XII	6.7	6.6	5.9	6.4	059.9	03.8	87	74	82	81	46	081	049.1	18	.	08	28	.	.	09	02	05	15	11	08	02	03	.	.	.	01	09					
GOD.	4.8	6.7	5.6	6.4	942.4	06.4	85	64	80	76	16	1272	057.1	05X	.	06	34	112	08	.	.	117	40	47	143	172	130	38	138	47	02	.	.	01	46	315	167
BERKOVICI																																					
BR. ST. 138																																					
I	2.4	3.1	1.8	2.4	-	04.1	78	61	76	72	37	033	016.4	29	.	.	22	18	02	04	04	01	04					
II	3.6	2.9	2.1	2.9	-	03.7	73	53	66	54	32	009	040.2	15	.	.	20	.	.	03	.	16	05	04	04	04	04	22					
III	7.1	7.1	5.7	5.3	-	06.2	80	69	77	76	43	155	038.4	29	.	.	04	.	.	01	.	03	08	14	05	14	14	.	.	.	03	14					
IV	4.6	4.8	3.6	4.4	-	06.7	67	61	67	65	32	122	022.6	03	.	.	01	.	.	01	08	05	11	11	05	11						
V	4.7	5.7	4.1	4.9	-	10.2	77	68	76	74	47	114	035.2	15	.	.	04	.	.	07	04	10	16	04	10							
VI	3.6	5.3	3.3	4.1	-	10.5	71	62	69	67	40	047	008.4	25	.	.	16	.	.	01	.	08	02	10	10	06	10	.	.	.	10	05					
VII	1.8	2.8	1.3	2.0	-	10.9	63	43	63	58	23	061	017.4	02	.	.	24	07	.	01	.	18	C1	06	04	03	04	.	.	.	04	06					
VIII	3.1	4.0	1.9	3.0	-	10.5	64	51	63	59	32	083	018.4	26	.	.	26	06	.	01	.	12	01	08	04	03	04	.	.	.	03	04					
IX	1.5	2.5	0.9	1.6	-	11.2	76	57	70	67	40	058	025.4	13	.	.	23	02	.	.	.	21	01	05	09	02	03					
X	4.0	4.2	4.2	4.1	-	07.5	71	62	69	67	40	289	078.6	13	.	.	04	13	07	11	11	09	11	.	.	.	07	08					
XI	5.2	5.6	4.3	5.0	-	05.7	77	70	76	74	27	184	047.2	18	.	01	06	.	.	09	08	14	14	06	14	.	.	.	01	08							
XII	3.5	3.1	2.5	3.0	-	04.6	80	64	73	72	45	118	064.4	16	.	.	15	.	.	01	.	17	05	04	04	04	06	.	.	.	08	23					
GOD.	3.8	4.2	2.9	3.6	-	07.6	73	60	70	68	23	1273	078.6	05X	.	01	70	91	15	.	09	.	190	45	102	163	44	103				
BJELASNICA																																					
BR. ST. 139																																					
I	5.4	5.3	4.8	5.1	162.8	02.4	75	75	78	76	24	015	003.6	27	05																						

OC PER	Vrednost Pratisek PM	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра m/s, Fm (0-12)																		
		PM			N		NE		E		SE		S		SW		W		NW		C									
		7	14	21	Sred. (Dnev.)	N	NE	E	SE	S	SW	W	NW	C	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.						
$\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = +1h\ 14\ min.$															SARAJEVC															
I	716.0	-02.6	04.1	00.0	00.3	04.8	-03.8	10.6	25 -13.2	10	03	02.0	.	05	15	02.8	21	02.4	.	01	02.0	06	02.2	03	01.7	44				
II	711.2	-03.1	04.0	-00.2	00.1	04.8	-04.0	12.8	13 -06.8	28	01	04.0	04	02.5	25	02.6	09	02.2	02	03.0	05	02.0	10	01.9	01	02.0	27			
III	702.5	04.0	11.4	07.3	07.7	12.8	02.9	20.4	30 -05.3	01	02	02.0	02	01.0	16	02.6	15	02.9	22	03.0	07	02.4	15	02.2	06	02.0	08			
IV	705.9	06.6	13.0	09.1	09.4	14.9	04.4	23.9	07 -00.2	13	03	01.7	01	02.0	13	01.8	07	01.7	09	04.2	11	03.2	19	02.2	07	01.6	20			
V	705.7	11.6	20.1	14.5	15.2	21.1	09.6	26.2	22 04.0	01	03	02.0	02	03.0	12	01.8	07	01.9	03	02.0	03	02.0	14	01.8	07	01.3	42			
VI	706.3	13.7	19.8	15.4	16.1	21.1	11.6	28.5	30 05.3	06	01	02.0	01	02.0	10	01.5	12	01.4	04	02.0	07	01.6	09	01.6	04	01.5	42			
VII	706.8	15.2	24.3	17.8	18.0	25.3	13.0	32.8	19 07.4	27	04	01.8	02	02.5	17	01.6	19	01.7	03	01.3	06	01.7	13	01.9	10	01.7	19			
VIII	707.8	13.8	21.6	16.0	16.9	22.7	12.3	28.5	18 08.6	22	03	01.7	.	.	15	01.7	19	01.5	08	01.6	13	01.8	07	01.9	26	.	.			
IX	710.4	12.3	23.9	16.0	17.0	24.5	11.1	29.8	16 06.9	10	25	02.2	21	02.0	01	01.0	06	02.2	12	01.8	06	02.0	19			
X	709.8	06.3	14.4	08.8	09.6	15.3	05.4	27.9	01 -01.4	27	02	01.5	03	01.7	18	02.4	23	02.2	.	07	01.7	09	01.8	01	02.0	30				
XI	707.8	01.7	07.2	03.8	04.1	08.2	00.3	17.7	02.0 -14.6	26	02	01.5	.	.	13	02.5	14	02.4	07	03.1	05	01.4	16	01.6	04	02.0	29			
XII	710.9	-00.6	03.1	00.4	00.9	03.9	-02.0	15.6	17 -07.2	08	12	01.9	08	04.3	01	01.0	06	01.7	03	02.0	60					
600.	708.6	06.6	13.9	09.1	09.7	15.0	03.1	32.8	10W -14.6	26xi	24	01.9	15	02.1	191	02.2	175	02.0	56	03.0	67	02.0	142	01.9	59	01.8	366			
$\varphi = 43^{\circ}31' N$ $\lambda = 18^{\circ}27' E$ Gr. $\Delta G = +1h\ 14\ min.$															KALINOVIK															
I	672.0	-01.5	03.6	-00.6	00.1	04.1	-03.5	10.7	16 -12.2	10	03	02.3	11	02.4	12	01.7	14	01.3	11	01.0	08	01.2	25	01.6	01	01.0	08			
II	672.7	-02.8	00.7	-01.8	-01.4	01.5	-04.4	08.1	07 -10.2	28	03	03.0	13	03.1	40	02.3	05	01.0	03	01.0	06	02.0	10	01.7	01	01.0	03			
III	668.7	02.8	07.0	03.8	04.4	07.8	01.2	16.5	30 -04.4	26,01	02	01.5	05	02.0	08	01.8	09	01.1	09	01.0	37	03.2	21	02.5	01	01.0	03			
IV	669.9	05.5	09.5	05.9	06.7	10.6	03.0	21.8	06 00.0	27,13	18	02.3	08	01.5	10	01.6	06	01.0	02	01.0	26	04.1	17	02.1	01	02.0	02			
V	672.9	11.1	15.6	11.2	12.3	17.2	07.6	22.2	20 01.9	10	07	02.4	07	01.9	12	01.3	10	01.0	09	01.0	19	02.1	17	01.6	05	01.0	11			
VI	671.3	13.6	17.3	13.1	14.3	18.2	10.3	25.6	28 03.3	06	13	02.2	04	01.7	21	01.3	05	01.0	03	01.0	27	02.6	07	01.6	01	01.0	19			
VII	672.3	15.2	20.8	15.6	16.8	21.9	11.8	29.9	18 06.4	02	10	01.3	12	02.0	26	01.8	06	01.0	02	01.0	12	02.2	04	02.0	02	01.0	18			
VIII	673.5	13.4	18.9	13.8	14.9	19.8	10.8	25.9	12 06.7	23	09	01.9	14	01.9	17	01.5	11	01.2	08	01.0	12	01.8	04	01.2	03	01.0	18			
IX	674.0	12.2	20.6	13.6	15.0	21.0	09.5	26.9	16 04.4	25	03	02.0	02	01.5	21	01.8	06	01.0	05	01.0	13	02.2	11	01.8	01	01.0	28			
X	672.3	09.5	11.5	07.0	08.4	12.4	04.1	23.9	01 00.0	30,09	06	02.7	09	02.0	36	01.8	07	01.3	06	01.0	10	03.2	01	02.0	02	01.0	24			
XI	670.1	01.9	05.7	03.0	03.4	06.9	00.3	18.2	02 -12.9	24	05	02.0	10	01.9	23	01.8	04	01.2	03	03.7	12	03.5	07	02.0	02	01.0	24			
XII	672.3	-00.3	04.1	00.3	01.0	04.9	-02.1	11.3	24 -07.4	08	02	02.5	17	02.0	24	01.8	11	01.0	04	01.0	06	03.5	06	02.3	03	01.3	20			
600.	672.2	04.4	11.3	07.1	07.9	12.2	04.0	29.9	10W -12.9	26xi	81	02.2	114	02.1	248	01.8	94	01.1	65	01.1	176	02.8	130	01.9	23	01.1	164			
$\varphi = 43^{\circ}10' N$ $\lambda = 18^{\circ}33' E$ Gr. $\Delta G = +1h\ 14\ min.$															GACKO															
I	-	-04.1	03.3	-01.3	-00.9	04.1	-05.3	07.0	20.06 -10.8	10	27	03.3	C2	02.5	C6	02.0	.	.	03	02.0	.	.	.	14	02.4	38
II	-	-03.2	02.8	-01.3	-00.7	03.8	-04.6	10.3	19 -11.4	10	53	03.5	.	.	15	02.4	.	.	02	02.0	.	.	.	03	03.3	11
III	-	02.1	07.7	03.6	04.3	09.0	00.3	16.0	30 -07.0	02,01	16	03.6	.	.	33	02.9	06	04.0	10	03.7	.	.	.	03	02.3	25
IV	-	06.0	11.5	06.4	07.6	12.3	02.8	21.0	04 -02.0	13	27	03.6	08	01.5	24	03.8	06	02.0	05	02.8	23	.	.			
V	-	12.0	17.2	11.8	13.2	19.0	07.0	25.5	17 01.0	10,01	19	02.7	.	.	12	02.8	01	03.0	08	02.9	.	.	.	06	02.3	47
VI	-	13.9	18.9	13.2	14.8	20.2	09.1	26.0	20,15 03.0	10	35	03.4	.	.	07	03.1	01	03.0	07	03.9	.	.	.	01	03.0	39
VII	-	16.5	23.1	16.5	18.2	24.5	11.1	31.0	18 08.0	01	44	02.8	.	.	04	03.0	01	03.0	05	03.4	.	.	.	06	02.2	31
VIII	-	14.8	21.0	15.1	16.5	22.6	10.9	27.0	11 09.2	23	46	03.2	08	01.7	07	02.7	01	03.2	08	03.0	.	.	.	27		
IX	-	11.7	22.4	14.5	15.6	23.4	06.0	20.5	16 01.6	25	01	02.0	26	03.1	.	.	06	02.6	01	02.0	11	02.6	.	.	.	04	02.2	38		
X	-	06.5	14.1	07.9	09.1	15.3	03.6	24.0	01 -02.5	31,09	01	02.0	42	03.4	.	.	21	03.3	01	02.0	04	02.2	.	.	.	05	02.4	20		
XI	-	00.3	07.0	02.9	03.3	08.3	-01.8	18.3	04 -18.4	26	01	05.0	23	03.7	.	.	23	03.1	01	03.0	06	02.7	.	.	.	10	02.4	24		
XII	-	-01.7	05.5	00.7	01.3	01.3</																								

Mesec	Oblačnost Nm (0-10)				Temperatura srednja broj sati (Dnes)	Vlažnost vazduha				Padavine R mm		Broj dana na sat																									
	7	14	21	Sred. (Dnes)		Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Rm(0-10)	R mm	≤	<	<	≥	≥	≥	≤	≤	<	>	Σ	N	•	*	*	Δ	~	▲	▲	¶	T	≡	■
						7	14	21	Sred.	Min	Max	Cat.	10.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.00.0.0	9	Δ	*	Δ	~	▲	▲	¶	T	≡	■					
SARAJEVC																																					
$H_a = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																					
I 4.4 5.1 4.0 4.5	120.6	03.8	85	69	84	79	49	025	008.9	27	02	03	28	.	.	.	01	.	10	07	10	08	.	04	08	01	03	20					
II 5.9 4.6 5.4 5.3	134.5	03.4	81	60	75	72	33	013	007.2	15	.	.	24	.	.	.	03	.	06	08	05	03	.	02	04	02	03					
III 7.7 8.3 6.0 7.3	110.6	04.7	69	50	43	61	26	073	020.3	22	.	.	09	.	.	.	13	01	01	16	13	08	03	10	04	02						
IV 6.6 7.0 5.1 6.2	160.9	05.4	73	56	43	64	13	091	044.3	02	.	.	01	.	.	.	09	.	06	13	13	11	01	13	03	02	01	.					
V 5.8 7.4 5.6 6.3	190.1	08.8	82	52	72	69	31	106	021.9	27	.	.	.	06	.	.	02	.	03	11	15	11	04	15	01	07	.	.	.				
VI 7.0 7.8 8.6 7.1	092.7	10.4	84	63	80	76	32	137	042.6	04	.	.	11	.	.	01	.	02	13	22	18	02	22	02	10	01	.	.					
VII 4.7 5.9 3.8 4.8	235.9	11.2	82	52	75	70	29	048	015.2	02	.	.	18	03	.	01	01	01	17	11	08	03	11	04	11	01	11	.	01	06	.	.					
VIII 7.1 7.3 4.3 6.3	151.6	11.1	90	62	83	78	34	096	015.7	14	.	.	09	.	.	01	03	10	23	17	03	23	12					
IX 3.6 4.7 2.1 3.4	238.9	10.6	91	51	80	74	30	034	026.7	13	.	.	.	17	.	.	03	.	11	04	05	03	01	02	05	03	.	.	.				
X 7.2 6.1 5.1 6.1	128.7	06.9	91	59	82	77	36	113	023.8	21	.	.	01	02	.	.	03	01	06	13	16	11	05	16	03	03	.	.	.				
XI 7.3 6.6 4.6 6.8	078.9	04.9	86	65	81	78	38	079	017.7	11	03	04	09	.	.	04	02	03	17	13	02	14	05	02	01	07	06	.	.				
XII 7.0 7.2 5.9 6.7	057.6	04.0	88	73	82	81	41	030	012.3	18	.	05	25	.	.	02	03	12	08	05	01	03	04	01	14	06	.	.					
GOD. 6.2 6.5 5.0 5.9	1701.0	07.1	83	59	76	73	13	845	044.3	024	V	05	12	97	63	03	.	40	04	63	130	158	116	23	136	32	09	.	.	04	46	33	37				
KALINOVIK																																					
$H_a = 1073 \text{ m } H_b = 1073.7 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																					
I 4.6 4.7 4.4 4.6	-	03.8	89	69	87	82	24	020	007.9	27	02	05	26	.	.	.	09	08	11	05	07	07	27						
II 6.8 5.4 5.3 5.8	-	03.5	91	76	85	84	33	009	005.4	15	02	10	24	.	.	.	06	12	07	02	03	04	04					
III 7.5 7.3 5.6 6.8	-	05.2	86	76	81	81	36	099	030.6	29	.	.	06	.	.	.	04	03	14	17	12	04	14	04	.	.	.	07	.	04	.	.					
IV 6.8 6.5 4.9 6.1	-	05.8	86	72	80	79	30	128	036.8	02	.	.	05	.	.	.	09	05	12	12	08	04	11	06	.	.	.	05					
V 6.0 7.0 5.6 6.2	-	09.0	89	68	91	83	37	075	026.8	14	.	.	.	06	.	.	03	10	16	11	02	14	12	01	.	.	.					
VI 7.0 7.4 6.0 6.8	-	10.4	88	71	88	83	48	126	045.8	25	.	.	04	.	.	.	02	11	17	11	03	17	06					
VII 4.7 5.2 3.0 4.3	-	11.4	87	63	85	79	35	090	010.5	07	.	.	07	.	.	.	09	06	13	11	01	12	.	.	.	07						
VIII 7.5 6.8 4.7 6.3	-	10.9	91	72	90	85	37	103	029.3	28	.	.	03	.	.	.	02	07	17	12	03	17	09	02	.	.	.					
IX 3.4 3.6 1.9 3.0	-	16.9	95	64	92	84	39	025	012.5	13	.	.	.	03	.	.	11	01	08	04	01	08	03	02	.	.	.					
X 7.1 5.4 5.2 5.9	-	06.7	93	71	88	84	31	230	074.9	13	.	.	02	.	.	.	02	03	13	14	07	14	01	.	.	.	04	01	01	.	.						
XI 8.2 4.7 6.2 7.0	-	05.5	94	83	92	80	50	146	055.3	19	01	03	06	.	.	.	02	01	04	17	17	10	05	14	05	.	.	.	02	02	01	.	.				
XII 5.4 4.8 5.0 5.1	-	04.5	95	79	89	87	51	065	044.9	18	.	04	24	.	.	01	08	08	11	03	01	04	08	.	.	.	01	07	07	.	.						
GOD. 5.1 6.0 4.2 5.1	-	07.3	90	72	87	83	24	1079	074.9	13X	05	22	86	17	.	.	10	01	70	119	160	103	33	138	37	.	.	.	58	18	30						
GACKO																																					
$H_a = 960 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																																					
I 5.3 4.8 3.7 4.6	-	03.5	79	73	82	78	46	023	015.2	29	02	01	36	.	.	.	02	07	05	06	06	01	04	02	16							
II 4.5 4.8 3.6 4.3	-	03.2	78	63	80	74	24	009	004.7	14	02	02	25	.	.	.	01	10	08	03	02	02	01	01				
III 8.0 7.7 7.3 7.7	-	04.7	80	65	80	75	27	220	064.2	29	.	.	11	.	.	.	02	02	17	18	16	07	18	03	02	.	.	.	02	.	02						
IV 5.4 6.6 4.6 5.5	-	05.1	71	52	74	65	15	128	034.0	11	.	.	05	.	.	.	03	06	13	12	04	12	02	.	.	.	01	01	01	.	.						
V 5.4 7.7 5.3 6.1	-	08.0	75	55	76	68	28	065	016.7	19	.	.	03	.	.	.	01	06	08	04	03	02	01	.	.	.	01					
VI 5.1 7.5 5.6 6.1	-	09.2	74	59	77	70	38	080	028.6	18	.	.	04	.	.	.	02	01	05	12	10	02	12					
VII 2.0 5.1 2.3 3.1	-	09.5	69	49	69	62	24	039	017.5	02	.	.	17	01	.	.	01	14	03	09	06	02															

Meseč MM	Vrednost precisa PM	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, fm (0-12)																							
		Ta					N					NE						E			SE			S			SW			W			NW		
		7	14	21	Sred. (Dnev.)	N	NE	E	SE	S	SW	W	NW	C	E.	J.	S.	J.	E.	J.	S.	E.	J.	S.	E.	J.	S.								
$\varphi = 45^{\circ}46' N \lambda = 19^{\circ}09' E$ Gr. $\Delta G = + 1h\ 16\ min.$															SCHEMOR												BR. ST. 151								
I	-	-00.5	04.5	01.7	02.3	07.3	-01.4	13.6	19 -06.7	01	09	02.6	04	02.8	.	.	01	02.0	15	01.6	05	01.8	09	02.0	02	03.0	04	48							
II	-	-03.0	05.5	00.0	00.6	06.4	-04.2	13.9	13 -09.1	17	05	02.4	12	03.3	C3	02.7	05	01.2	07	01.4	01	02.0	08	02.2	04	01.8	39								
III	-	03.7	13.8	07.6	08.2	15.1	02.2	22.9	09 -04.4	01	06	03.8	03	03.7	C6	02.3	11	02.9	17	02.6	03	03.0	08	02.6	04	01.8	35								
IV	-	08.1	14.6	09.8	10.6	16.2	05.1	27.7	07 -01.4	12	13	03.2	07	02.7	C1	01.0	.	.	10	02.5	04	02.0	11	02.3	17	02.8	27								
V	751.9	15.2	22.2	16.4	17.5	23.4	11.1	26.6	20 06.9	05	11	03.2	09	01.7	08	01.8	05	02.2	07	01.9	04	02.2	10	02.0	04	02.0	35								
VI	752.3	17.0	23.2	17.8	19.0	24.5	13.5	31.3	24 08.6	06	10	02.6	04	02.2	C2	02.5	C1	03.0	09	01.7	04	01.5	09	01.8	15	02.5	36								
VII	752.6	19.3	25.4	19.5	20.9	27.1	14.8	30.9	16 08.8	28	13	02.6	02	02.5	C2	01.0	.	.	01	03.0	03	01.0	11	01.6	12	02.0	49								
VIII	753.0	17.1	24.8	18.5	19.7	25.8	14.2	30.5	11 08.4	15	15	02.1	06	01.2	02	01.0	02	03.0	05	01.6	02	01.5	05	02.0	06	01.7	50								
IX	756.6	14.6	25.1	17.2	18.5	25.9	11.9	30.7	16 06.3	10	05	02.2	01	02.0	02	01.0	09	02.0	04	02.0	04	02.0	03	01.7	03	01.7	58								
X	757.7	07.5	14.7	09.9	10.5	15.7	05.9	27.9	01 00.0	27	08	02.8	05	02.0	06	01.5	10	02.9	05	01.6	05	01.2	07	01.9	08	02.1	39								
XI	756.9	02.0	07.0	03.3	03.9	07.8	00.4	15.1	02 -10.4	26	07	03.1	05	03.4	11	02.1	25	02.4	05	03.2	05	01.6	02	02.0	01	02.0	29								
XII	759.7	-01.4	04.0	00.8	01.1	04.9	-03.1	10.7	17 -09.9	21	03	02.3	02	02.0	02	01.5	10	02.2	05	01.6	09	01.6	11	01.9	12	02.4	39								
GOD.	-	08.3	15.6	10.2	11.1	16.7	05.8	31.3	24 VI -10.4	26 XI	105	C2.7	60	02.5	45	01.9	79	02.4	90	02.0	49	01.7	94	02.0	88	02.3	485								
$\varphi = 45^{\circ}07' N \lambda = 19^{\circ}15' E$ Gr. $\Delta G = + 1h\ 17\ min.$															SID												BR. ST. 152								
I	-	-00.1	04.0	02.7	02.6	04.8	-01.0	15.0	06 -08.5	01	04	02.5	07	02.4	C3	01.7	54	02.5	.	.	02	02.5	02	02.0	19	02.7	.								
II	-	-02.0	05.4	01.0	01.4	06.2	-02.9	14.0	13 -08.0	17.0	05	03.6	24	03.2	C7	02.4	23	02.6	01	02.0	02	02.5	04	02.2	18	02.6	.								
III	-	05.3	14.4	08.6	09.2	15.5	03.7	22.0	31.0	-04.3	01	03	02.7	12	02.4	16	03.8	35	03.7	01	01.0	07	03.0	06	03.3	13	02.8	.							
IV	-	08.1	15.4	10.5	11.1	16.7	06.1	27.5	06	01.0	12	15	02.1	14	02.1	05	02.6	15	02.7	.	.	03	01.7	06	03.3	28	03.2	.							
V	-	15.2	22.1	16.3	17.5	23.3	12.0	26.5	22.2	07.0	01	04	C3.5	10	01.6	15	02.1	26	02.2	05	02.6	02	04.0	12	02.3	19	02.9	.							
VI	-	16.6	23.1	17.8	18.9	24.2	14.2	30.5	24	07.0	03	06	03.2	13	01.8	04	02.0	20	01.8	03	01.7	05	02.6	03	02.0	36	02.9	.							
VII	-	18.5	23.7	19.5	20.8	26.7	15.4	31.0	19.16	08.5	27	05	01.6	19	01.8	02	01.5	21	01.6	.	.	01	02.0	03	03.3	42	02.1	.							
VIII	-	17.0	24.3	18.3	19.5	25.9	15.0	30.0	11	11.0	22	07	02.0	22	01.7	07	01.9	19	01.6	.	.	07	01.3	04	01.8	27	01.9	.							
IX	-	15.4	25.1	18.1	19.2	25.7	13.7	31.5	17.16	07.5	14	03	02.0	16	01.4	14	01.9	36	02.4	02	02.0	07	01.3	04	02.5	08	02.1	.							
X	-	08.2	14.8	09.4	10.7	15.6	06.8	27.5	01 01.0	25	17	02.0	12	02.0	08	02.4	23	02.9	.	.	04	01.8	05	02.2	24	02.5	.								
XI	-	02.5	07.3	04.2	04.6	07.8	01.4	16.0	02 -11.0	26	04	01.5	12	02.7	07	02.7	53	03.1	01	03.0	.	.	01	05.0	12	02.7	.								
XII	-	-00.5	03.9	00.9	01.3	04.7	-01.7	11.0	01 -07.4	21	05	01.8	13	02.2	05	01.6	32	02.6	01	01.0	08	02.0	03	02.7	26	03.0	.								
GOD.	-	08.7	15.6	10.6	11.4	16.6	06.9	31.3	17.16	-11.0	26 XI	78	02.3	174	02.1	93	02.4	363	02.6	14	02.1	48	02.0	53	02.6	272	02.6	46							
$\varphi = 45^{\circ}22' N \lambda = 17^{\circ}34' E$ Gr. $\Delta G = + 1h\ 17\ min.$															BACKI PETROVAC												BR. ST. 153								
I	-	-00.4	04.9	01.6	02.4	07.5	-01.4	16.5	18 -06.5	01	04	01.0	02	01.0	07	01.0	06	01.3	08	01.1	15	01.2	11	01.5	12	01.5	28								
II	-	-02.3	05.5	00.2	00.8	04.2	-03.5	15.0	13 -09.0	17	15	C1.9	07	01.6	06	01.3	08	01.2	C6	01.2	08	01.8	06	01.3	08	01.6	20								
III	-	04.8	14.9	08.4	09.1	15.7	03.2	22.7	09 -03.6	01	07	02.4	05	01.4	09	01.6	21	02.3	10	02.5	14	01.6	08	01.8	09	01.5	11								
IV	-	08.7	15.6	10.2	11.2	16.9	05.9	28.2	07 01.5	27.19	10	02.4	03	02.0	03	01.3	06	01.3	10	02.0	06	01.8	13	02.1	16	02.1	16								
V	-	15.6	23.0	16.2	17.8	24.1	11.8	29.4	19.17	04.7	01	05	01.6	07	01.3	04	01.5	06	02.3	06	01.5	09	01.7	16	01.8	08	02.2	32							
VI	-	17.2	23.9	17.5	19.1	24.7	14.4	31.0	24 09.5	05	05	C1.6	04	01.5	04	01.3	08	01.8	06	01.3	07	01.4	10	01.9	17	01.9	29								
VII	-	18.9	24.4	19.4	21.0	27.4	15.5	32.6	19 05.7	27	01	02.0	07	01.0	05	01.2	06	01.5	14	01.4	08	01.6	08	01.8	22	01.6	37								
VIII	-	17.1	25.1	18.1	19.6	26.1	14.4	31.1	10 09.5	15	09	C1.4	03	01.3	06	01.7	08	01.4	02	01.0	09	01.3	10	01.2	12	01.5	34								
IX	-	15.2	25.9	17.4	18.0	25.6	12.6	30.8	16 06.4	14	06	04	08	01.0	08	01.2	14	01.3	09	01.3	09	01.3	10	01.4	10	01.4	40								
X	-	07.4	16.7	09.8	10.4	15.4	06.9	27.5	01 00.7	26	01	01.0	12	02.0	07	02.0	11	02.3	04	01.4	11	01.7	12	01.6	29	01.6	29								
XI	-	02																																	

Mesec	Oblačnost Nm (0-10)				Vlažnost varžduha %	Padavine R mm				Broj dana na sat																										
						U m e				Tn Tx Tn Tx Tn Tx Tn F(0-12) Nm(0-10) R mm				• * * * □ ▲ ▢ ▣ ▤ ▥ ▦ ▧ ▨ ▩ ▪ ▫ ▬ ▭ ▮ ▯																						
	7	14	21	Sred.		7	14	21	Sred.	Min	Σ	Max	Dat.	≤	<	≤	≥	≤	≥	≤	≥	≤	≥	≤	≥											
SOMBOR																																				
BR. ST. 151																																				
I	5.2	3.6	3.9	4.9	120.5	04.6	91	71	88	83	46	015	004.8	29	.	.	21	.	.	01	07	04	06	05	.	01	.	01	01	01	01	01				
II	4.2	4.7	3.9	4.2	145.7	03.7	88	59	82	76	33	002	001.1	03	.	.	26	.	.	04	01	11	09	03	02	.	01	.	01	01	01	01				
III	6.5	7.0	4.0	5.8	-	05.6	83	52	74	70	22	014	004.3	18	.	.	08	.	.	13	03	01	07	12	05	.	11	02	.	01	01	03	02	01		
IV	6.4	6.2	3.9	5.5	172.2	06.7	79	57	76	71	26	040	012.4	12	.	.	01	02	.	11	05	06	11	04	02	11	01	01	01			
V	5.2	6.8	5.0	5.7	231.1	11.1	83	57	81	74	36	079	014.6	25	.	.	15	.	.	06	02	02	06	13	11	02	13	01	11	01		
VI	6.2	6.8	6.5	6.5	184.3	12.5	85	58	83	75	36	055	010.5	19	.	.	18	03	.	06	01	02	12	20	13	01	20	09	03	.		
VII	2.9	6.0	2.8	3.9	236.5	13.9	82	57	84	74	41	133	037.2	07	.	.	26	04	.	03	01	09	05	10	08	03	10	05	01	.		
VIII	6.5	5.5	5.5	5.8	204.9	13.7	90	60	88	79	42	116	025.8	31	.	.	26	01	.	03	02	05	04	18	13	03	14	14	01	.		
IX	2.5	3.5	1.8	2.6	232.8	12.4	93	54	86	77	39	016	010.0	08	.	.	21	02	.	02	17	01	04	01	04	03	03	.				
X	6.2	7.3	4.5	6.0	111.6	08.0	92	70	87	83	36	062	024.8	19	.	.	02	.	.	04	07	14	11	08	01	11	01	06	.			
XI	8.1	7.3	6.4	7.3	049.9	05.3	90	73	87	83	44	032	012.6	11	01	01	11	.	.	04	01	03	19	07	06	01	07	02	01	.	.	04	.			
XII	6.0	6.5	5.6	6.1	075.5	04.3	92	75	87	85	48	007	002.8	27	.	.	24	.	.	04	04	12	05	03	.	03	04	01	.			
GOD.	5.4	6.2	4.5	5.4	-	08.5	87	61	83	77	22	571	037.2	07/VN	01	04	93	104	10	.	45	11	73	57	120	84	18	115	11	01	01	02	01	47	35	03
SIO																																				
BR. ST. 152																																				
I	7.1	7.5	7.3	7.3	-	04.7	92	76	87	85	25	027	009.5	09	.	01	20	.	.	01	01	11	07	05	.	03	03	02	.	.	.	05	.			
II	7.3	7.1	6.6	7.0	-	03.7	87	59	76	74	23	006	003.0	21	.	.	23	.	.	03	01	08	05	02	.	02	04	01	02	.		
III	8.5	8.0	8.0	8.1	-	05.9	80	51	72	68	29	019	005.7	25	.	.	04	.	.	09	01	17	11	04	.	08	05	.	01	01	02	.				
IV	8.9	7.7	7.4	7.9	-	-	-	-	-	-	-	052	019.5	02	.	.	02	.	.	03	.	19	14	09	01	14	01	01	.			
V	7.3	7.6	7.7	7.5	-	11.8	88	61	88	79	32	073	020.9	27	.	.	14	.	.	03	.	11	16	11	02	14	02	05	.			
VI	8.5	7.7	8.3	8.2	-	13.4	89	65	87	80	50	082	019.4	21	.	.	17	03	.	02	.	16	19	13	03	19	04	01	.			
VII	6.5	7.1	7.8	7.1	-	14.6	89	41	66	79	43	109	028.6	01	.	.	24	04	.	01	.	12	09	04	03	01	.	.	.	01	04	01	.			
VIII	8.2	8.1	7.5	7.9	-	14.7	95	69	93	86	48	139	043.9	17	.	.	21	01	.	02	01	14	16	13	04	14	07	10	.			
IX	-	-	-	-	-	-	-	-	-	-	-	043	019.8	02	.	.	22	02	.	04	.	07	05	01	07	01	09	.				
X	8.0	8.5	8.5	8.6	-	08.6	96	73	93	87	41	039	008.3	14	.	.	02	.	.	04	01	19	13	12	13	11	01	13	.			
XI	8.9	8.8	8.0	8.6	-	05.6	90	77	85	84	50	056	013.3	11	01	01	09	.	.	04	.	19	11	07	02	10	03	02	.	.	04	04	.			
XII	7.0	8.0	7.8	7.9	-	04.4	89	78	89	85	42	006	002.6	17	.	.	21	01	.	04	.	10	04	02	02	04	08	02	.			
GOD.	-	-	-	-	-	-	-	-	-	-	-	651	043.9	07/VN	01	03	81	102	10	.	32	03	-	-	134	91	18	121	19	04	01	.	03	26	34	07
BACKI PETROVAC																																				
BR. ST. 153																																				
I	5.1	5.1	4.1	4.8	117.7	04.9	92	77	92	87	50	018	008.6	09	.	.	22	.	.	04	05	06	04	04	05	02	01	12	01	.		
II	4.0	4.1	3.4	4.1	141.7	03.9	88	65	83	75	28	006	003.1	21	.	.	25	.	.	01	11	05	05	02	.	01	05	.	.	.	04	03	.			
III	6.1	6.4	5.4	6.0	140.0	-	-	-	-	-	-	019	005.4	25	.	.	06	.	.	01	01	07	08	05	.	07	02	.	.	.	01	02	06	.		
IV	6.5	6.0	4.0	5.6	186.5	07.3	81	60	79	73	36	036	011.8	02	.	.	02	.	.	03	.	06	08	11	05	01	11	01	02	.		
V	4.7	5.0	5.1	5.2	212.9	12.8	89	67	91	82	35	047	017.4	27	.	.	15	.	.	03	04	06	06	13	09	03	13	12	02	.		
VI	6.3	5.4	5.4	5.8	186.0	-	-	-	-	-	-	136	025.8	14	.	.	18	03	.	02	.	04	05	17	13	06	17	.	.	.	01	13	01	.		
VII	2.7	4.9	2.8	3.5	277.5	-	-	-	-	-	-	120	036.5	01	.	.	25	04	.	01	.	10	01	10	08	05	10	.	.	.	10	01	.	.		
VIII	5.2	5.9	4.8	5.1	202.8	-	-	-	-	-	-	205	051.3	30	.	.	22	04	.	01	01	06	05	16	15	08	14	17	05	.		
IX	2.8	2.6	1.2	2.2	246.4	-	-	-	-	-	-	025	011.3	01	.	.	23	02	.	01	.	13	08	05	01	08	04	-	.			
X	6.6	6.9	5.5	6.3	098.4	-	-	-	-	-	-	034	008.7	21	.	.	01	.	.	01	.	03	13	11	07	05	11	.	.	.	05	12	.	.		
XI	7.4	6.3	5.8	6.5	074.4	05.5	90	75	88	84	53	0																								

Mjesec	Vremenski prstitek ESE	Temperatura vazduha °C								Čestina pravaca i srednja jačina vjetra nD, Fm (0-12)																					
		Tm				Nis				Dat.				N				NE		Z		SE		S		SW		W		NW	
		7	14	21	Sred. (dies)	N	M	S	E	Dat.	M	S	E	Dat.	E.	j.															
$\varphi = 45^{\circ}20' N \lambda = 19^{\circ}51' E$ Gr.ΔG = + 1h 18 min.																															
I	758.5	-00.3	06.6	01.7	02.4	07.4	-01.4	14.3	18	-06.7	01	04	02.8	04	01.5	10	01.9	18	02.3	04	01.5	11	02.1	20	02.4	16	02.2	06			
II	760.6	-02.8	05.3	00.2	00.7	06.1	-03.8	13.6	13	-09.8	17	14	03.2	08	02.5	12	01.8	15	02.1	.	.	07	01.6	15	02.5	09	02.3	04			
III	749.5	04.7	14.7	08.2	09.0	15.7	02.9	26.7	31	-05.5	01	05	04.0	05	01.8	11	02.5	31	03.5	08	03.0	05	01.4	18	02.4	07	02.4	03			
IV	752.5	08.5	14.8	10.6	11.1	16.4	0.6	27.2	04	02.0	27.12	16	03.1	03	02.7	04	02.6	11	02.6	04	03.0	04	02.0	24	02.5	03					
V	751.0	15.2	22.2	16.7	17.7	23.5	12.1	26.6	17	04.2	01	08	02.8	07	02.0	04	02.2	26	02.6	01	01.6	08	02.0	23	02.0	10	02.4	12			
VI	752.4	16.9	23.1	18.1	19.1	24.2	14.6	31.1	24	10.0	03	10	02.9	03	02.0	05	01.8	14	01.9	01	01.0	08	01.6	22	02.0	13	02.4	14			
VII	752.5	18.7	25.7	20.0	21.1	26.5	15.3	32.5	19	16	05.3	27	04	02.5	05	01.2	06	01.8	02	01.5	06	01.5	29	01.8	17	02.1	16				
VIII	753.7	17.0	24.0	19.1	19.9	26.1	14.6	31.0	12	06.7	15	15	02.1	01	01.0	05	01.2	10	02.2	03	01.7	03	01.6	08	02.0	32	02.2	13			
IX	756.7	15.2	25.4	17.6	18.6	26.2	12.5	31.5	16	06.8	14	07	01.4	04	02.2	13	01.5	12	02.4	04	01.5	08	01.5	11	01.6	04	01.8	27			
X	757.4	08.3	14.7	09.7	10.6	15.8	04.8	27.2	01	00.6	30	25	05	01.6	04	01.8	09	02.6	02	02.5	07	01.4	30	01.7	16	01.9	02				
XI	756.8	02.4	07.3	03.5	04.2	08.1	00.8	16.6	03	-05.3	27	09	03.4	.	.	23	02.7	36	03.1	01	04.0	06	01.5	05	02.0	05	02.8	05			
XII	759.7	-00.5	04.2	00.9	01.4	05.3	-01.7	11.3	18	-07.6	21	07	01.7	01	01.0	09	01.7	18	03.9	01	02.0	04	02.2	33	01.8	13	02.2	07			
GOD.	755.2	08.6	15.7	10.5	11.2	16.8	04.6	32.5	19	NW	-09.8	47	11	04	02.7	45	01.9	111	02.1	211	02.8	31	02.2	17	01.7	241	02.0	144	02.3	131	
$\varphi = 45^{\circ}15' N \lambda = 19^{\circ}32' E$ Gr.ΔG = + 1h 18 min.																															
NCVI SAC-RIPSKI ŠARČEVI																															
BR. ST. 156																															
I	754.9	02.8	06.7	04.5	04.6	07.8	00.9	16.1	18	-04.3	01	04	01.2	06	01.3	13	01.9	07	02.3	02	01.5	27	02.1	17	02.3	13	01.5	04			
II	756.0	-00.4	05.0	01.9	02.1	05.8	-01.3	13.1	13	-06.2	17	13	01.8	09	01.6	13	01.8	05	02.2	05	01.4	14	02.1	14	02.2	09	01.9	.			
III	749.0	07.4	14.2	10.0	10.4	15.1	03.6	25.9	31	-02.0	22	06	02.0	10	01.5	19	02.9	05	03.8	09	04.3	21	02.5	15	02.3	04	01.0	.			
IV	748.9	09.4	14.6	11.8	11.9	16.4	0.7	26.9	04	02.7	27	07	02.0	02	01.5	06	02.3	04	01.8	08	02.9	18	02.5	18	02.1	01	01.0	.			
V	748.1	15.8	21.7	17.4	18.1	22.5	13.7	28.0	17	06.5	05	06	01.5	08	01.1	15	02.1	07	02.0	04	02.5	28	02.5	13	02.4	11	01.8	01			
VI	748.6	17.4	22.0	18.7	19.4	23.9	15.4	30.3	24	10.0	08	03	10	01.6	03	02.0	06	02.3	.	09	01.9	25	02.2	15	02.3	18	01.9	04			
VII	748.9	19.1	25.6	20.9	21.6	26.5	17.1	32.2	19	12.2	02	05	01.4	03	01.7	11	01.5	03	07	01.7	01.4	26	01.8	20	02.1	17	01.8	01			
VIII	750.0	17.6	24.1	19.4	20.2	25.1	16.3	30.0	12	12.0	14	10	01.8	03	02.0	13	01.8	02	02.0	11	01.3	28	01.8	11	02.1	12	01.4	03			
IX	752.0	16.8	24.5	19.5	20.1	25.1	15.4	31.1	16	06.5	09	06	01.5	03	01.3	27	02.1	07	01.9	10	01.5	31	01.7	03	01.7	03	01.0	.			
X	753.6	09.4	14.4	11.0	11.3	15.2	0.8	27.2	01	01.4	30	03	02.0	03	01.3	15	02.4	10	03.2	02	03.5	22	01.9	25	02.0	11	01.9	02			
XI	752.8	03.0	07.2	04.1	04.6	07.8	01.3	19.5	02	-06.3	27	09	02.4	03	02.7	26	02.8	18	03.5	06	01.5	07	02.3	05	02.6	08	02.0	01	01.0	.	
XII	755.8	00.7	04.3	01.8	02.1	05.1	-00.7	11.8	17	-06.7	21	09	01.6	03	01.7	17	03.1	08	04.0	03	01.3	23	02.1	19	02.6	11	01.5	.			
GOD.	751.4	09.9	15.4	11.4	11.8	12.2	16.4	08.3	32.2	18	NW	-06.3	27	11	07	01.8	56	01.6	191	02.3	80	02.9	76	02.1	270	02.1	177	02.3	141	01.8	17
$\varphi = 45^{\circ}08' N \lambda = 20^{\circ}00' E$ Gr.ΔG = + 1h 20 min.																															
GLAČENČ																															
BR. ST. 158																															
I	-	00.3	06.0	02.2	02.7	04.8	-01.0	12.4	06	-05.7	10	06	02.3	.	.	C1	02.0	C1	02.0	02	01.5	17	02.0	02	01.5	17	02.5	17	02.3	45	
II	-	-	-	-	-	-	-	-	-	-	09	-	-	-	-	C1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	05.3	14.7	08.1	09.0	15.3	03.8	23.2	08	-02.5	22	07	03.3	01	02.0	C8	02.6	19	03.1	02	03.0	07	02.6	01	01.0	11	02.5	37			
IV	-	08.5	14.5	10.1	10.8	15.7	06.3	27.2	04	03.0	27.11	35	02.9	01	03.0	02	02.0	05	02.4	11	02.5	09	02.9	28	02.2	13	02.3	07			
V	-	15.7	21.9	16.0	17.4	22.7	13.6	28.5	22	08.5	02	14	02.6	05	02.0	C5	01.8	06	01.6	08	02.1	09	02.0	13	02.3	31	02.2	13			
VI	-	-	-	-	-	-	-	-	-	-	07	-	-	-	-	C1	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	17.5	24.1	18.7	19.8	24.5	15.9	30.4	12	11.4	14	24	02.3	01	02.0	04	02.0	.	04	01.8	04	02.0	.	.	31	02.2	25	02.2			
IX	-	16.0	24.2	18.0	19.1	24.6	14.5	30.2	16	05.4	14	23	02.3	02	02.0	C2	02.0	02	01.5	07	02.3	05	02.0	16	02.2	26	02.1	11			
X	-	09.0	14.3	09.7	10.7	14.7	07.8	26.5	01	02.6	26	27	02.1	01	03.0	01	01.0	10	03.0	08	02.2	01	02.0	03	02.0	31	02.2	11			
XI	-	-	-	-	-	-	-	-	-	-	07	-	-	-	-	C1	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-	-	-	-	-	-	-	-	-	07	-	-	-	-	C1	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	08.5	15.7	10.4	11.2	16.6	06.7	31.8	19	NW	-08.4	27	11	03.7	01.7	08	01.7	163	02.7	142	02.2	68	01.8	125							

Mesec	Oblachnost Nm (0-10)	Insolacijja broj sati (Dnes)	Vlažnost vazduha			Padavine R mm			Broj dana na sat																		
									Tn	Tx	Tn	Tx	Tn	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	□	
	7	14	21	Sk.	Min	Σ	Max	Dat.	≤	<	<	IV	IV	IV	IV	IV	<	>	N	N	N	N	9	Δ	▲	▲	T
									30.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.0	10.0	•	*	*	Δ	Δ	▲	▲	□	
BR. ST. 156																									H = 86 m H _b = 87.0 m h = 2.0 m h _r = 1.0 m		
I 5.5 6.2 4.3 5.4	140.5	04.7 93 71 91 85 38	018 014.5	09	.	.	24	.	.	.	06	09	06	02	01	05	02	08	01	
II 5.7 4.9 3.2 4.6	148.4	03.6 89 55 77 74 20	003 001.4	03	.	.	25	.	.	02	07	05	04	01	01	04	01	01	02	
III 7.2 8.0 4.9 6.7	145.0	05.5 82 45 69 65 22	020 006.3	16	.	.	05	01	.	09	01	03	12	11	04	03	02	02	03	
IV 6.9 7.0 4.7 6.2	160.1	06.7 81 54 73 69 28	047 017.6	02	.	.	02	.	07	01	05	12	11	04	01	11	01	02		
V 5.3 6.9 5.8 6.0	231.4	11.3 88 56 82 75 36	064 020.8	27	.	.	14	.	05	03	09	13	10	02	13	01	10			
VI 7.2 7.2 6.6 7.0	188.9	13.2 89 61 87 79 44	078 018.6	01	.	.	16	02	04	02	13	14	12	02	16	08	01			
VII 3.5 6.2 3.2 4.3	292.9	14.4 88 57 84 76 40	119 045.0	01	.	.	25	03	01	05	04	07	07	04	07	03	05			
VIII 5.7 7.0 5.2 6.0	210.3	13.8 92 60 86 80 39	096 031.6	17	.	.	21	04	04	03	10	13	10	02	13	17	04			
IX 3.3 3.1 1.6 2.8	263.8	12.7 93 52 87 77 36	035 012.0	04	.	.	22	02	.	14	01	09	06	02	09	03	02			
X 7.3 7.4 5.5 6.7	104.6	08.2 93 70 90 84 39	034 010.2	15	.	.	01	01	03	03	15	12	07	01	12	02	06			
XI 8.0 7.3 5.7 7.0	078.8	05.4 90 72 88 83 37	037 012.7	11	.	01	10	.	05	02	14	08	04	02	07	02	01	08	03		
XII 6.1 6.9 6.3 6.4	087.1	04.3 91 75 88 85 55	003 001.1	17	.	01	20	.	03	03	14	05	01	03	01	03	01			
GOD. 6.0 6.5 4.8 5.8	2053.8	08.6 89 69 80 83 77 20	554 045.0	04W	.	02	84	102	13	.	43	02	56	118	115	72	17	104	11	02	.	.	01	01	48	32	07
BR. ST. 157																									H = 132 m H _b = 129.4 m h = 2.0 m h _r = 1.2 m		
I 5.2 5.7 3.6 4.9	142.7	04.2 73 43 68 68 21	016 011.7	09	.	.	16	.	07	08	06	06	02	01	04	02	01	03	02	
II 5.1 4.8 3.5 4.4	148.2	03.4 73 54 67 64 18	005 001.5	04	.	.	24	.	07	01	09	05	04	03	01	04	01	01	03	
III 7.1 7.5 5.7 6.6	142.1	05.1 66 44 59 56 18	013 007.2	25	.	.	03	01	18	08	01	13	09	03	07	07	02	02	02	
IV 6.7 6.4 4.7 5.9	165.1	06.0 68 51 63 60 16	046 015.3	02	.	.	02	.	18	05	04	11	12	04	01	12	01	01		
V 5.2 6.4 6.0 5.9	231.3	10.5 78 55 73 68 36	077 018.4	27	.	.	11	.	11	02	05	06	14	12	03	14	05	.		
VI 6.8 6.7 5.8 6.4	192.1	12.2 79 59 76 71 36	076 015.9	19	.	.	14	02	02	14	02	03	12	16	13	02	16	06	.	
VII 3.5 5.9 3.7 4.2	294.3	13.1 79 53 71 68 37	130 049.3	01	.	.	25	03	04	10	03	08	05	07	07	04	07	03	03	
VIII 5.4 6.8 5.8 6.0	210.6	13.3 87 60 80 76 40	128 034.6	31	.	.	20	01	10	03	03	10	19	12	04	15	16	04		
IX 3.2 3.0 1.2 2.5	264.7	12.1 82 54 71 69 36	027 012.6	01	.	.	19	01	04	15	01	08	05	01	08	06	.			
X 6.5 6.8 5.0 6.1	115.9	07.8 85 67 79 77 34	029 007.6	21	.	.	01	01	09	03	07	14	14	10	13	13	01	05		
XI 7.9 7.1 5.4 6.8	079.9	05.0 81 66 78 75 33	033 011.0	11	.	01	10	.	14	02	04	15	10	07	02	08	02	01	05	03	
XII 5.9 6.5 4.0 6.1	092.9	04.2 83 70 80 78 46	003 001.0	27	.	03	18	.	15	02	04	10	07	01	04	03	05	01		
GOD. 5.7 6.1 4.7 5.5	2084.0	08.1 77 58 72 69 16	583 049.3	04W	.	04	65	93	07	06	131	31	73	108	122	81	18	111	13	03	.	.	.	49	24	18	
BR. ST. 158																									H = 185 m H _b = - m h = 2.0 m h _r = 1.2 m		
I 5.9 5.2 3.0 5.4	-	04.5 89 71 81 91 37	017 009.1	09	.	.	20	.	01	05	07	05	04	04	02	01	03	02	07	05	
II - - -	-	- - -	- - -	007 003.2	04	04	.	03	01	04	01	.	04	03	
III 6.5 7.1 6.2 6.6	-	- - -	- - -	024 006.5	15	.	.	06	.	02	02	13	09	07	08	01	01	02	04	
IV 6.6 6.7 5.2 6.2	-	06.7 78 58 73 70 22	031 020.8	02	.	.	01	.	01	01	06	12	12	07	02	12	01	04		
V 5.0 6.6 5.7 6.0	-	11.2 81 60 81 74 35	078 021.0	27	.	.	11	.	01	01	03	08	19	11	04	13	30	02		
VI - - -	-	- - -	- - -	- - -		
VII - - -	-	- - -	- - -	- - -		
VIII 3.1 4.9 2.9 3.7	-	13.6 88 63 84 78 46	130 022.5	25	.	.	17	01	.	13	04	14	13	07	14	01	11			
IX 2.6 2.7 0.5 1.9	-	12.5 87 63 79 77 48	041 018.9	13	.	.	17	01	.	17	06	05	02	04			
X 5.9 6.7 3.9 5.5	-	07.9 89 70 82 80 44	028 012.5	11	.	01	09	.	05	03	04	07	12	04			
XI - - -	-	- - -	- - -	- - -		
XII - - -	-	- - -	- - -	- - -		
GOD. - - -	-	- - -	- - -	- - -		
BR. ST. 159																									H = 78 m H _b = - m h = 2.0 m h _r = 1.0 m		
I 4.7 4.8 3.9 4.4	140.6	04.5 90 70 87 62 45	C13 010.6	05	.	.	22	.	01	09	04	04	02	01	03	02	05	02		
II 4.6 4.4 3.2 4.0	141.1	03.5 89 53 79 74 21	005 002.0	03	.	.	26	.	01	01	11	05	05	02	.	05	04	03		
III 4.6 6.0 3.7 4.8	171.3	05.2 77 43 68 63 18	026 007.6	15	.	.	05	01	.	14	11	06	13	07	10	03	03	02		
IV 6.5 6.6 4.7 6.0	170.6	06.2 77 55 69 65 21	035 007.8	02	.	.	01	.	13	02	05	09	12	08	.	12	01	.		
V 4.2 6.2 4.6 5.0	240.9	11.0 81 52 80 71 30																									

Meseč	Vrednost pritisak Pa	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, fm (0-12)															
		TM				IM	MS	MX	Dat.	MS	Dat.	N	NE	E	SE	S	SW	W	NW	C							
		7	14	21	Stred. (Dnev.)							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.			
$\varphi = 45^{\circ}24' N \lambda = 20^{\circ}21' E$ Gr. AG = + 1h 22 min.																								ZRENJANIN			
I	-00.7	05.9	01.3	01.9	06.5	-01.1	13.0	06	-04.4	01	07	02.4	01	01.0	C1	01.0	18	02.1	36	02.1	06	02.2	15	02.2	06	02.7	03
II	-02.8	04.5	-00.1	00.4	05.4	-03.0	13.0	13	-08.2	17	07	03.1	15	02.5	C3	01.3	15	01.9	15	02.1	03	02.0	13	02.3	07	02.4	06
III	-05.3	14.3	07.9	08.9	15.2	03.6	26.0	31	-04.9	01	05	03.4	04	03.0	06	02.0	24	03.0	36	03.2	06	02.2	07	01.9	05	02.2	.
IV	-08.0	14.6	09.9	10.6	16.3	05.3	26.9	06	00.0	20	17	02.9	07	02.6	.	.	07	03.0	16	03.0	03	02.7	16	03.0	21	02.6	03
V	-15.3	22.5	16.4	17.6	23.6	11.6	28.4	19	04.6	01	06	02.7	13	01.9	01	01.0	16	01.9	12	02.4	10	02.2	14	01.9	13	02.3	08
VI	-17.3	23.2	18.0	19.1	24.2	14.3	30.9	24	07.3	07	12	02.9	07	01.9	C2	01.5	06	02.3	13	02.5	07	01.9	16	02.3	16	02.3	11
VII	-18.9	25.7	19.6	20.9	24.8	19.0	31.6	16	05.6	27	03	02.3	08	01.4	04	01.2	09	02.0	14	01.9	05	01.8	18	01.9	23	02.1	09
VIII	-17.2	24.9	18.5	19.7	25.6	14.5	30.0	12	09.7	15	09	02.2	10	02.1	C6	01.3	11	02.1	10	02.0	07	01.9	10	01.9	17	01.7	13
IX	-15.5	24.5	18.1	19.1	25.2	13.7	26.5	16	06.8	16	14	02.0	05	01.6	04	02.0	24	02.3	14	02.3	06	01.8	06	01.8	08	01.8	09
X	-07.8	14.6	09.2	10.3	15.2	06.5	25.7	01	00.5	29.7	06	02.0	09	01.7	C1	02.0	16	03.0	03	02.0	20	02.1	17	02.2	08		
XI	-02.5	07.4	03.5	04.2	08.0	01.2	15.2	03.02	-05.3	27	06	02.7	04	03.2	05	02.2	47	02.9	11	03.1	05	02.4	04	01.8	05	02.6	03
XII	-00.6	04.1	00.1	00.9	04.9	-02.5	10.2	17	-05.7	21	10	C2.0	C1	03.0	C4	02.0	23	03.3	03	02.7	03	02.0	23	02.3	17	02.1	09
600.	-	08.6	15.5	10.2	11.1	16.4	06.8	31.6	KOM -09.7	24.4	102	02.5	84	02.1	37	01.7	216	02.6	192	02.5	64	02.1	162	02.2	195	02.2	83
$\varphi = 45^{\circ}51' N \lambda = 20^{\circ}28' E$ Gr. AG = + 1h 21 min.																								KIKINDA	BR. ST. 162		
I	-00.8	04.0	01.4	02.0	06.6	-01.1	12.7	04	-07.0	01	08	02.4	.	.	01	01.0	23	02.1	31	02.0	12	01.5	07	01.6	08	02.1	03
II	-03.2	05.0	-00.3	00.3	05.7	-04.1	12.8	13	-09.0	04	22	02.5	03	02.3	01	01.0	06	01.8	16	01.9	06	02.0	07	02.0	10	02.4	10
III	-04.7	14.4	08.2	08.9	15.6	03.4	26.7	31	-06.0	01	03	05.0	07	02.6	04	02.2	28	02.8	19	03.3	05	02.4	06	02.2	09	01.8	12
IV	-08.0	14.7	10.3	10.8	14.5	05.4	27.1	06	00.0	18	19	03.1	C6	02.3	.	.	05	03.1	09	03.0	11	02.9	14	02.2	17	02.6	05
V	-15.4	22.9	16.7	17.9	23.9	12.3	28.9	19	05.0	01	07	03.1	16	01.9	07	01.9	14	02.4	12	01.8	06	02.2	06	02.0	21	01.9	04
VI	-17.1	23.6	18.5	19.4	24.8	14.4	32.1	23	08.2	07	10	02.7	10	01.6	C3	01.7	14	01.5	11	01.9	03	02.0	07	02.3	22	02.5	10
VII	-19.0	25.8	19.6	21.0	27.2	15.3	32.0	19	05.6	27	09	01.8	07	01.9	05	02.0	11	01.9	08	02.1	06	01.8	11	02.1	21	01.8	15
VIII	-17.1	25.1	18.5	19.8	26.2	14.5	31.3	11	05.2	14	14	C2.4	12	01.7	C4	01.5	13	01.9	05	01.8	05	01.6	04	01.2	20	02.0	16
IX	-14.6	25.1	17.8	18.8	25.8	12.7	30.0	16	05.0	10	10	C1.7	C5	01.4	C8	01.9	25	01.2	13	02.1	05	01.6	04	02.2	14	01.6	09
X	-07.5	15.3	09.6	10.5	16.0	04.1	26.6	01	00.6	28	08	01.9	10	01.9	C6	02.2	22	02.9	09	02.4	04	01.5	06	01.8	24	02.3	02
XI	-01.9	07.3	03.7	04.2	08.0	00.3	15.4	02	-10.0	27	07	03.4	03	01.3	09	01.8	44	02.2	07	04.3	06	01.7	01	03.0	04	02.2	09
XII	-01.1	03.7	00.3	00.8	04.4	-02.4	10.4	02.01	-08.7	21	05	C2.0	04	01.5	03	01.7	22	02.7	05	02.2	17	01.6	16	02.2	17	02.1	04
600.	-	08.4	15.7	10.4	11.2	16.7	06.4	32.1	KOM -10.0	27.1	119	C2.6	83	01.9	51	01.9	234	02.3	145	02.3	86	01.8	89	02.1	189	02.1	99
$\varphi = 45^{\circ}27' N \lambda = 20^{\circ}51' E$ Gr. AG = + 1h 22 min.																									JASA TOPIC	BR. ST. 163	
I	-00.4	06.4	01.6	02.3	06.8	-01.2	12.6	18	-06.5	01	08	C1.9	C1	01.0	C1	01.0	43	01.4	12	01.2	04	01.0	01	01.0	06	02.3	17
II	-02.2	05.2	00.5	01.0	05.7	-02.9	14.0	13	-07.4	09	19	03.3	13	01.1	C2	01.0	17	C1.6	C7	01.7	02	02.0	04	01.3	06	01.5	14
III	-06.1	15.4	08.7	09.7	16.1	04.4	27.0	31	-06.5	01	04	04.5	04	01.2	C2	02.5	36	03.4	09	01.7	01	03.0	02	01.5	04	02.3	09
IV	-09.0	15.7	10.5	11.4	17.1	03.6	27.5	06	00.4	19	23	C3.0	C7	02.4	.	.	20	03.6	04	01.5	10	02.8	02	02.0	16	02.7	08
V	-16.1	23.5	16.7	17.9	24.4	12.5	29.5	20	05.6	01	14	02.6	12	01.8	C2	01.0	22	02.3	06	01.2	13	01.4	01	02.0	03	01.2	18
VI	-18.3	24.2	18.4	19.8	25.4	15.1	32.8	24	08.0	07	16	C2.0	05	02.0	C1	01.0	13	01.9	07	01.1	06	01.8	05	02.8	15	02.7	18
VII	-19.7	26.9	19.6	21.5	27.6	15.6	33.2	15	10.0	27	11	C1.8	C6	01.2	C1	01.3	12	01.5	08	01.9	09	01.3	03	01.3	23	01.9	20
VIII	-17.9	25.3	18.4	20.2	26.3	12.1	31.5	11	05.4	14	14	C1.8	06	01.5	C5	01.2	23	01.6	03	01.3	07	02.0	01	01.0	11	01.9	23
IX	-15.2	26.0	17.6	19.2	26.3	13.3	30.5	17	06.6	10	10	C1.6	06	01.5	C5	01.0	31	01.7	02	01.5	05	01.6	04	01.2	02	02.5	23
X	-08.3	15.1	10.1	10.9	15.8	04.6	27.2	01	0C.4	24	03	01.3	11	01.2	C5	01.0	25	03.3	C7	01.1	08	01.1	05	01.6	04	01.9	15
XI	-02.3	07.8	03.8	04.4	08.2	01.0	16.6	02	-11.1	27	03	C2.7	12	02.0	C2	01.0	33	02.3	03	01.3	04	01.8	02	02.0	04	03.2	07
XII	-00.4	04.3	00.8	01.4	04.6	-01.4	10.6	01	-08.0	21	07	C1.7	C1	01.0	C4	02.0	25	03.4	C2	01.0	19	01.6	09	01.9	12	01.3	14
600.	755.4	05.8	15.7	11.2	12.0	16.7	07.5																				

Mjesec	Oblačnost Nm (0-10)			Inzolacije broj sati (Dnev.)	Vlažnost vazduha			Padavine R mm			Broj dana na godini																										
	7	14	21		Sred. Sred.	Max	Min	Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	+	•	Δ	•	▲	▲	■													
					7	14	21	Sred.	Max	Min	Dat.	30.00	0.0	0.025	0.30	0.20	0.6	8	2.0	8.0	0.1	1.0	0.0	0.0	0.0												
ZRENJANIN																																					
BR. ST. 161																																					
I	4.1	5.0	3.2	4.1	149.3	04.3	50	65	85	81	42	013	010.7	09	.	01	24	.	.	06	01	10	04	05	03	01	04	02	01	.	00	03					
II	4.9	5.2	3.7	4.6	140.9	03.6	88	60	80	76	24	003	001.3	02	.	01	25	.	.	06	02	07	06	04	02	01	04	.	00	02							
III	6.3	6.5	4.0	5.6	160.3	05.4	76	46	65	64	22	023	007.5	18	.	07	01	.	.	15	11	04	05	07	06	04	01	01	01	.	01	01					
IV	6.7	6.9	4.6	6.1	159.1	06.6	81	35	76	71	26	048	012.0	03	.	01	01	.	.	19	05	04	10	09	07	03	05	.	01	02							
V	5.6	6.8	5.2	5.9	232.2	11.1	84	54	82	74	34	083	020.8	27	.	01	11	.	.	15	07	03	05	15	10	03	12	.	00	03							
VI	6.4	6.1	5.8	6.1	213.2	12.8	84	40	83	76	41	070	016.0	11	.	01	18	04	.	12	05	02	08	16	13	02	14	.	00	01							
VII	3.0	3.3	3.6	4.0	312.4	14.5	86	58	88	78	45	138	032.9	13	.	01	24	04	01	12	02	08	03	07	05	07	.	00	04								
VIII	5.6	6.2	4.8	5.5	233.5	14.0	91	62	89	81	42	185	032.4	26	.	01	19	01	.	15	07	05	07	15	14	07	15	.	00	04							
IX	3.1	2.9	1.7	2.6	266.3	12.5	89	54	83	75	37	025	010.5	08	.	01	18	.	.	08	14	09	03	01	05	.	00	04	.	00	04						
X	6.5	6.1	5.5	6.1	118.1	07.8	80	48	89	83	36	028	008.5	15	.	01	01	01	.	11	04	05	11	14	06	04	14	.	00	01							
XI	7.5	6.7	5.3	6.5	074.9	05.2	86	70	84	80	50	035	015.4	11	.	01	07	.	.	21	04	03	14	08	06	01	04	03	01	.	00	01					
XII	6.3	6.5	5.3	6.0	088.4	04.3	90	76	90	85	53	006	002.6	18	.	03	23	.	.	14	07	02	11	05	02	04	02	.	00	01							
GOD.	5.3	5.8	4.8	5.3	2143.7	08.5	86	56	81	77	22	658	032.9	05VII	.	06	86	94	08	01	161	35	69	88	114	72	23	104	12	02	.	00	43	00			
KIKINDA																																					
BR. ST. 162																																					
I	4.3	5.1	3.4	4.3	129.4	04.5	50	72	87	83	41	089	004.8	09	.	01	25	.	.	01	08	04	02	03	02	01	.	00	07	03							
II	5.2	4.6	3.7	4.5	141.5	03.5	89	57	78	75	24	004	002.0	03	.	01	29	.	.	01	01	09	05	04	01	.	00	03	03								
III	6.0	6.5	4.5	5.7	162.2	05.4	80	46	65	65	25	021	004.8	25	.	06	01	.	.	07	01	03	08	11	04	10	03	02	01								
IV	6.3	6.3	4.7	5.8	163.5	06.5	79	53	72	68	24	035	000.0	02	.	01	01	.	.	07	06	07	11	07	11	01	.	00	01								
V	5.3	6.1	5.3	5.6	216.2	11.0	84	52	78	72	31	098	020.5	24	.	01	14	.	.	04	02	03	06	11	10	04	11	.	00	18	03						
VI	6.1	6.2	5.6	6.0	224.0	12.8	85	58	81	75	43	087	022.9	18	.	01	19	04	01	03	01	02	07	19	14	03	19	.	00	12	03						
VII	2.7	5.7	3.5	4.0	314.0	13.8	84	35	82	74	35	105	046.8	01	.	01	25	04	.	01	04	02	07	03	03	07	.	00	08	00							
VIII	4.8	6.2	3.6	4.9	237.3	13.2	89	54	85	77	35	095	029.7	27	.	01	22	04	.	.	07	09	15	09	02	13	.	00	17	04							
IX	3.3	3.5	1.5	2.7	259.9	12.0	91	30	80	74	36	067	035.0	13	.	01	22	01	.	01	14	02	05	05	02	05	.	00	01	04							
X	7.3	6.1	4.1	5.8	133.2	07.6	90	63	84	75	31	038	015.6	19	.	01	62	.	.	04	03	10	08	06	01	08	.	00	01	07							
XI	7.1	7.3	5.8	6.7	073.0	05.2	88	70	85	81	54	018	006.4	11	01	01	12	.	.	02	05	17	07	04	07	01	.	00	02	.							
XII	5.5	6.3	6.0	5.9	075.3	04.2	90	76	88	85	54	007	003.6	27	.	05	24	.	.	02	03	10	05	03	04	01	.	00	04	01							
GOD.	5.3	5.8	4.3	5.2	2145.7	08.3	86	55	81	75	24	584	046.8	04VII	.	02	08	72	106	13	01	34	05	70	84	107	72	15	100	12	04	01	.	00	54	40	10
JASA TCMIC																																					
BR. ST. 163																																					
I	5.4	4.5	5.2	5.1	-	04.4	08	68	85	80	40	015	010.8	09	.	02	21	.	.	02	08	12	06	02	01	05	02	.	00	03	02						
II	5.9	6.2	5.2	5.8	-	03.8	86	59	83	74	10	007	002.4	04	.	01	23	.	.	02	01	06	11	06	03	04	02	.	00	04	02						
III	7.0	6.9	7.2	7.3	-	05.6	75	45	69	63	19	020	007.0	25	.	05	01	.	.	08	04	02	13	11	05	11	01	.	00	01							
IV	7.5	7.4	6.9	7.3	-	06.9	78	25	75	65	26	039	011.1	03	.	01	01	.	.	10	03	04	18	08	07	01	08	.	00	01							
V	5.8	7.2	7.5	6.8	-	12.1	86	57	86	76	33	107	026.7	17	.	01	14	.	.	04	01	02	10	15	12	04	15	.	00	12	02						
VI	7.0	7.5	7.4	7.3	-	13.7	85	62	85	77	39	064	018.0	21	.	01	21	08	01	03	01	01	19	13	10	02	13	.	00	03	02						
VII	3.2	6.4	3.9	4.6	-	14.8	84	57	88	76	42	133	070.7	02	.	01	25	07	.	01	01	03	10	08	05	10	03	.	00	02	02						
VIII	5.2	7.5	6.6	6.4	-	14.1	88	60	88	79	39	140	030.2	08	.	01	23	04	.	03	02	02	19	19	13	05	15	.	00	01	14	04					
IX	3.5	3.6	3.2	3.4	-	12.7	90	53	83	75	36	052	025.3	06	.	01	21	02	.	.	13	04	07	07	02	07	.	00	06	07							
X	6.8	7.5	6.4	6.9	-	08.1	90	45	86	82	38	026	009.3	15	.	02	02	08	.	.	04	01	02	13	12	06	04	12	.	00	07						
XI	7.1	7.5	6.5	7.1	-	05.2	84	70	84	79	39	047	011.2	11	02	02	08	02	.	02	04	17	08	07	02	04	03	.	00	01	04						
XII	6.7	6.4	6.6	6.6	-	04.3	87	75	87	83	49	004	001.8	10	.	03	20	.	.	04	03	13	04	02	03	01	.	00	04	01							
GOD.	6.0	6.6	6.0	6.2	-	08.8	85	40	83	76	10	684	070.7	02VII	.	02	08	77	110	21	01	31	51	142	115	82	22	109	11	03	.	00	01	44	37	10	
VRŠAC																																					
I	5.8	5.5	4.6	5.3	126.7	04.0	77	63	73	71	23</td																										

Mjesec	Vazdušni pritisak hPa	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Fm (0-12)																			
		Ta				H	H15	H30	H45	Dat.	H15	H30	Dat.	N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)									E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.				
$\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. AG = + 1h 22 min.														BECGRAD												BR. ST. 171					
I	759.1	01.2	07.1	03.3	03.7	06.0	06.2	14.7	06 -05.1	01	04	01.8	.	.	13	01.9	33	01.9	04	01.5	10	01.6	17	02.1	10	02.3	02				
II	756.7	-00.5	05.0	01.9	02.1	06.0	-01.2	15.1	13 -06.6	05	09	02.3	06	02.2	14	02.3	20	02.0	02	02.5	13	02.2	13	02.1	06	02.3	01				
III	746.0	07.7	14.7	10.3	10.7	16.0	06.6	26.7	31 -01.7	01	02	03.0	04	02.0	22	03.0	31	02.8	10	02.4	09	02.0	09	02.2	06	02.2	.				
IV	748.8	09.6	15.3	12.0	12.2	17.4	07.8	28.6	06 03.1	11	08	02.6	01	02.0	05	02.2	16	02.6	05	02.2	09	02.1	21	02.3	24	02.5	01				
V	748.1	15.9	22.2	16.9	18.0	23.4	13.2	28.2	22 07.2	01	07	01.6	05	02.0	16	02.5	22	02.2	13	01.7	09	02.0	22	02.1	05	02.0	.				
VI	748.5	17.5	23.2	18.7	19.5	24.1	15.4	31.0	24 09.5	04	11	01.9	06	01.8	07	01.9	11	02.2	06	02.0	13	02.0	22	02.4	13	02.3	01				
VII	748.9	19.4	25.6	20.3	21.4	26.6	16.4	33.4	19 11.3	28	05	02.0	01	01.0	14	01.9	14	02.1	06	02.3	11	01.8	26	01.8	14	01.8	03				
VIII	750.0	17.9	24.5	19.1	20.1	25.5	16.2	30.6	12 12.0	15	03	02.0	04	01.8	08	01.8	18	01.6	09	01.4	13	01.4	22	01.7	13	01.8	03				
IX	753.1	16.5	24.8	18.1	19.5	25.6	14.5	30.9	16 08.1	10	08	01.9	04	01.8	14	02.0	27	02.2	05	01.6	09	01.8	14	01.7	03	02.0	06				
X	753.7	09.5	15.0	11.1	11.6	15.9	08.8	26.4	01 03.7	26	09	01.9	05	01.8	11	03.2	21	02.6	04	02.2	10	01.9	22	02.1	10	02.1	01				
XI	752.9	03.4	07.7	04.5	05.0	08.2	02.6	15.6	18.02 -08.0	26	01	03.0	02	02.0	27	03.3	32	03.2	03	02.3	06	01.8	09	02.3	10	02.1	.				
XII	755.8	01.0	04.6	02.1	02.4	05.7	00.2	12.9	06 -06.0	21	03	01.7	02	02.0	08	02.8	23	02.9	02	01.0	12	02.0	28	02.2	13	02.5	02				
600.	751.5	09.9	15.8	11.5	12.2	16.9	08.4	33.4	19M -08.0	26.XI	70	02.0	40	01.9	153	02.5	268	02.4	69	01.9	124	01.9	229	02.1	127	02.2	19				
$\varphi = 44^{\circ}02' N \lambda = 20^{\circ}28' E$ Gr. AG = + 1h 22 min.														GORNJI MILANOVAC												BR. ST. 172					
I	-	-03.3	03.4	-01.2	-00.1	06.0	-04.7	12.0	07 -11.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
II	-	-04.8	03.4	-01.6	-01.1	04.7	-06.1	11.0	13 -19.0	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
III	-	02.0	13.7	06.5	07.4	15.2	01.1	26.0	31 -06.8	02.01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
IV	-	06.2	14.3	08.5	09.4	16.6	03.5	27.6	06 -03.1	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
V	-	12.1	20.8	13.9	15.2	22.1	05.4	27.5	22 03.4	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
VI	-	15.1	21.3	15.2	16.7	22.9	12.0	30.2	30 05.5	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
VII	-	15.6	24.1	16.7	18.3	25.5	12.5	33.5	19 06.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
VIII	-	14.9	22.3	15.8	17.2	23.8	13.0	29.5	12 09.0	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
IX	-	12.3	23.0	14.6	16.3	24.8	16.9	30.0	16 05.4	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
X	-	06.7	14.6	08.3	09.5	15.7	05.6	26.0	01 -01.4	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
XI	-	00.9	07.1	01.9	02.9	07.5	-01.2	21.0	18 -20.0	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
XII	-	-01.7	04.6	-00.2	00.6	05.6	-03.0	12.0	17 -08.0	27.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
600.	-	08.4	14.6	08.2	09.4	15.6	04.4	33.5	19M -20.0	26.XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 44^{\circ}00' N \lambda = 20^{\circ}31' E$ Gr. AG = + 1h 21 min.														RUDNIK												BR. ST. 173					
I	-	01.6	04.4	02.2	02.7	06.0	-00.6	15.1	16 -09.7	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	-03.2	00.2	-01.9	-01.7	02.2	-04.8	09.2	13 -10.6	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	05.9	10.9	07.2	07.8	12.7	04.2	23.6	31 -02.0	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	06.6	11.2	08.2	08.6	14.3	04.4	25.3	06 -00.6	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	13.0	17.8	13.6	14.5	19.5	11.6	25.6	22 04.2	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	14.4	18.4	14.8	15.6	20.4	12.2	27.2	16 04.6	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	16.1	21.4	16.5	17.7	23.4	13.6	31.2	19 08.6	02.01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	19.3	19.7	15.4	16.4	21.6	13.5	27.7	16 09.8	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IX	-	15.5	21.2	16.6	17.6	22.6	11.4	28.0	22 04.3	04	02	01.0	02	0.5	01.0	01	01.0	05	01.2	15	01.3	16	01.4	17	01.5	18	02.5				
X	-	07.9	11.4	08.7	09.2	13.1	06.6	24.8	01 03.0	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-	02.7	04.8	03.1	03.4	06.5	00.6	17.4	18 -11.1	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII	-	00.4	02.2	00.6	01.0	04.4	-02.0	12.0	17 -10.1	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
600.	-	08.0	12.0	08.8	09.4	14.0	06.1	31.2	19M -11.1	26.XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 44^{\circ}18' N \lambda = 20^{\circ}33' E$ Gr. AG = + 1h 22 min.														BLKČVIČKA BANJA												BR. ST. 174					
I	-	-01.0	06.6	00.0	01.4	07.3	-02.7	14.5	06 -04.3	22	03	01.0	.	.	C5	02.0	13	0													

Mesec	Oblačnost Nm (0-10)			Insolacij broj (Diss.)	Vlažnost vazduha			Padavine R mm	Broj dana n s a:																							
	7	14	21		Sred. Sred.	Min	Max		Tn		Tx		Tn		Tx		Tx		Tn		F(0-12)		Nm(0-10)		R mm							
									≤	<	<	≥	≤	≥	≤	≥	≤	≥	≤	≥	≤	≥	•	*	*	Δ	Δ	Δ	Δ	T	III	
	7	14	21	Sred.	(Diss.)				-10.0	0.0	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	0.0	•	*	*	Δ	Δ	Δ	Δ	R	III		
BEEGRAC																																
BR. ST. 171	$H_a = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$																															
I 4.3 4.5 4.4 4.5	144.7	04.4	82	61	77	73	33	026	011.5	05	.	.	12	.	.	.	02	.	11	C9	C7	05	01	04	03	02	.	.	.	01	03	
II 5.2 4.7 4.6 4.8	141.8	05.3	77	54	65	67	25	029	C03.6	04	.	.	20	.	.	.	05	01	07	05	06	04	03	04	01	.	.	.	01	04		
III 6.1 7.0 4.8 6.0	149.4	05.3	67	44	58	56	17	039	C11.2	16	.	.	02	01	.	.	18	03	01	10	09	06	02	03	03	01	.	.	.	01	01	
IV 6.6 6.7 5.7 6.4	160.0	06.3	71	51	63	61	19	041	C09.3	02	.	.	02	.	.	.	01	18	01	06	15	11	08	.	11	.	.	01	02			
V 5.5 6.1 5.8 5.8	216.4	11.1	80	56	80	72	33	132	C45.2	27	.	.	.	14	.	.	.	11	01	04	05	16	15	03	16	12		
VI 6.5 6.3 6.1 6.3	200.5	12.6	82	55	79	73	38	105	C21.0	14	.	.	.	17	04	01	10	01	03	09	17	14	03	17	02	03		
VII 3.5 4.4 3.1 3.7	279.1	13.6	79	55	78	71	39	132	C47.3	06	.	.	.	24	07	01	08	02	09	08	04	05	08	01				
VIII 5.5 5.6 5.8 5.7	201.7	13.6	87	60	87	78	40	129	C07.2	29	.	.	.	16	02	.	08	01	03	06	19	17	05	19	.	.	.	01	19			
IX 3.6 3.2 1.9 2.9	234.7	12.7	86	54	84	75	33	022	C06.9	06	.	.	.	19	01	.	.	06	.	15	C2	08	05	.	08	.	.	.	05	01		
X 6.4 6.4 5.9 6.2	115.0	08.2	89	67	81	73	37	053	C12.6	15	.	.	.	01	.	.	.	11	05	05	12	15	12	01	15	.	.	.	02	03		
XI 7.1 6.4 5.4 6.3	079.3	05.3	85	67	82	78	39	045	C11.1	21	.	.	.	02	08	.	.	15	04	06	13	11	07	01	08	04	03	.	01	07		
XII 6.0 6.0 6.0 6.0	056.0	04.3	85	69	81	78	34	106	C01.5	27	.	.	.	03	13	.	.	12	04	04	10	07	03	.	04	03	.	.	05	01		
GOD. 5.5 5.7 5.0 5.4	2018.6	08.4	80	56	76	71	17	743	C07.3	06M	.	05	55	94	14	03	132	25	72	104	135	104	20	125	19	07	.	.	02	03	52	18
GORNJI PILANEVAC																																
BR. ST. 172	$H_a = 335 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																															
I 5.9 5.4 5.2 5.5	-	-	-	-	-	-	-	023	C006.5	02	01	.	29	.	.	.	08	11	04	06	08	03	01	01	16			
II 6.8 6.3 4.7 5.9	-	-	-	-	-	-	-	020	C005.7	03	05	01	28	.	.	.	01	07	13	08	07	05	07	02	03			
III 6.9 6.9 5.5 6.4	-	-	-	-	-	-	-	056	C025.4	22	.	.	11	01	.	.	.	03	10	06	06	02	05	03	01	02	03	
IV 7.2 6.6 5.7 6.5	-	-	-	-	-	-	-	022	C005.6	02	.	.	04	02	.	.	.	05	13	08	08	01	.			
V 7.0 6.5 6.0 6.5	-	-	-	-	-	-	-	140	C039.8	27	.	.	.	06	.	.	.	02	11	17	17	04	17	01	09			
VI 6.6 6.7 6.6 6.7	-	-	-	-	-	-	-	100	C017.2	06	.	.	13	02	.	.	.	03	12	17	17	03	17	01	09			
VII 6.1 6.7 5.7 5.5	-	-	-	-	-	-	-	075	C016.0	13	.	.	18	05	.	.	.	01	04	09	09	03	09	01	03			
VIII 8.6 6.7 7.1 7.5	-	-	-	-	-	-	-	163	C047.5	19	.	.	11	12	21	21	04	21	07	04				
IX 6.2 3.8 2.8 4.3	-	-	-	-	-	-	-	025	C013.2	05	.	.	15	01	.	.	.	06	03	07	05	01	07	03	13			
X 9.1 6.9 6.9 7.6	-	-	-	-	-	-	-	098	C031.4	13	.	.	03	01	.	.	.	01	17	15	14	04	15	07	09			
XI 8.9 7.6 7.7 8.0	-	-	-	-	-	-	-	052	C009.8	24	04	03	14	01	20	15	14	.	11	05	01	.	.	03	09			
XII 7.3 7.1 7.4 7.3	-	-	-	-	-	-	-	012	C003.2	07	.	.	03	27	.	.	.	04	19	10	03	.	09	04	03	.	.	08	04			
GOD. 7.2 6.3 5.9 6.5	-	-	-	-	-	-	-	786	C047.5	09M	10	07	116	67	08	.	01	.	42	147	139	129	21	136	22	06	.	.	02	22	44	30
RUCAINIK																																
BR. ST. 173	$H_a = 700 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$																															
I 4.5 3.1 4.1 4.6	-	-	-	-	-	-	-	035	C10.8	28	0	03	17	.	.	.	12	08	12	07	01	04	10	01	08	31		
II 5.3 5.9 3.9 5.0	-	-	-	-	-	-	-	021	C007.5	09	02	07	25	.	.	.	10	09	10	06	.	01	09	08	20			
III 5.9 6.1 3.6 5.1	-	-	-	-	-	-	-	064	C022.1	15	.	02	07	.	.	.	04	08	08	06	02	05	05	09	04	11		
IV 6.5 6.5 5.2 6.3	-	-	-	-	-	-	-	038	C008.5	02	.	.	03	01	.	.	.	05	12	14	09	01	08	.				
V 5.5 6.4 5.5 5.8	-	-	-	-	-	-	-	138	C035.8	03	.	.	03	.	.	.	03	10	18	17	04	18	01	02				
VI 6.2 6.3 5.9 6.1	-	-	-	-	-	-	-	197	C037.6	06	.	.	04	.	.	.	03	09	19	15	08	19	08	14				
VII 3.9 5.4 4.1 4.4	-	-	-	-	-	-	-	076	C017.0	02	.	.	10	01	.	.	.	08	05	13	10	03	13	06	.			
VIII 6.2 6.5 6.0 6.2	-	-	-	-	-	-	-	164	C020.8	14	.	.	07	.	.	.	02	10	25	21	04	25	11	24				
IX 2.6 3.4 2.2 2.7	-	-	-	-	-	-	-	016	C005.0	09	.	.	05	.	.	.	16	C2	05	04	.	05	03	.				
X 6.2 6.4 6.1 6.2	-	-	-	-	-	-	-	097	C030.3	13	.	.	03	.	.	.	06	11	15	13	03	15	07	.				
XI 6.7 5.7 5.2 6.0	-	-	-	-	-	-	-	059	C011.8																							

Mesec	Vrednost pritisak Pa mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																	
		Tm					Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21	Sred. (Dnev.)	E.							J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.				
$\varphi = 44^{\circ}39' N \lambda = 20^{\circ}55' E$ Gr. AG = + 1h 24 min.															SPECEREVC												BR. ST. 176		
I	-	00.5	06.0	01.7	02.5	06.8	-01.2	13.6	06	-04.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	-01.7	04.7	00.7	01.1	05.3	-02.5	12.0	13	-06.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	08.4	14.2	09.0	09.7	15.6	04.8	24.6	31	-05.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	08.4	15.7	11.1	11.6	17.7	06.4	28.0	06	01.0	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	14.9	22.8	15.5	17.3	23.6	11.8	29.4	20	04.8	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	16.8	23.4	17.1	16.6	24.0	14.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	18.1	26.4	16.7	20.5	26.5	15.0	32.5	19	05.5	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	16.9	25.0	16.4	16.7	25.5	15.3	30.2	12	10.6	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IX	-	15.2	25.1	17.2	18.7	25.5	13.6	25.6	17	14	06.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-				
X	-	08.5	14.9	10.2	10.5	15.6	07.0	25.2	01	00.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-	02.5	07.0	03.6	04.2	07.7	01.3	15.2	18	-12.4	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII	-	00.3	04.2	01.4	01.8	05.4	-01.4	11.2	06	-05.4	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	08.6	15.8	10.4	11.4	16.6	07.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 44^{\circ}02' N \lambda = 20^{\circ}56' E$ Gr. AG = + 1h 24 min.															KRAGUJEVAC												BR. ST. 177		
I	-	00.1	06.8	01.5	02.5	07.7	-01.7	13.2	25	-04.6	21	04	C2.2	*	*	01	C2.0	C4	C2.2	21	01.8	*	*	09	02.6	54			
II	-	-02.7	03.9	00.3	01.4	05.9	-04.1	12.8	13	-11.1	27	09	02.4	01	02.0	*	02	02.0	07	01.9	*	*	14	02.6	51				
III	-	05.7	14.8	08.5	09.4	16.2	03.0	26.4	31	-05.2	01	02	C3.0	*	*	16	03.1	20	02.4	06	02.0	*	*	07	02.7	42			
IV	-	08.6	15.0	10.3	11.1	17.4	03.4	28.8	06	-00.4	12	05	C2.2	03	02.0	*	01	02.0	13	02.5	11	02.6	*	17	03.0	40			
V	-	14.5	21.7	15.4	16.8	23.0	10.4	28.2	20	02.2	01	05	C2.0	01	02.0	*	*	C9	C1.9	07	02.0	*	*	10	02.2	61			
VI	-	17.0	22.9	17.4	18.7	24.0	12.7	30.6	24	08.8	07.0	06	01.9	02	01.5	*	02	02.0	12	02.0	*	*	23	02.3	52				
VII	-	18.4	25.3	18.8	20.3	26.9	14.1	33.2	19	08.1	28	11	02.2	02	03.0	*	01	04.0	07	02.1	11	02.0	*	12	02.2	49			
VIII	-	16.9	23.7	17.6	16.0	25.0	14.1	30.6	12	09.0	15	06	C1.7	05	01.8	*	01	02.0	14	01.4	05	01.8	01	02.0	04	01.8	57		
IX	-	14.5	25.1	16.6	18.3	25.8	12.2	30.6	16	05.1	10	03	C1.7	01	02.0	*	*	C5	C2.2	12	01.3	04	01.2	*	04	02.2	61		
X	-	08.1	15.5	10.0	10.5	16.3	07.0	26.0	C1	00.0	31	11	01.9	01	04.0	*	09	C4.0	05	02.0	01	01.0	*	08	01.8	53			
XI	-	02.7	07.5	03.8	04.4	08.8	00.6	21.4	18	-16.4	27	01	02.0	03	02.0	*	23	03.1	07	02.3	07	01.9	*	07	02.3	42			
XII	-	00.6	05.2	01.7	02.3	06.2	-01.4	12.6	04	-05.0	24.10	04	02.5	02	01.5	*	16	02.6	08	01.5	10	01.9	*	08	03.0	45			
GOD.	-	08.7	15.6	10.2	11.2	16.9	06.1	33.2	49M	-16.4	27X1	68	02.2	21	02.0	*	15	02.8	103	02.0	56	02.0	02	01.5	123	02.3	607		
$\varphi = 44^{\circ}22' N \lambda = 20^{\circ}57' E$ Gr. AG = + 1h 22 min.															SMEČEREVSKA PALANKA												BR. ST. 178		
I	752.9	-00.6	08.4	01.5	C2.2	07.1	-01.6	13.3	24	-07.3	05	01	C3.0	C3	01.7	21	01.5	25	01.8	02	01.6	04	01.0	10	02.3	12	02.6	15	
II	757.4	-02.7	04.4	00.4	00.6	05.4	-03.7	12.6	13	-16.0	27	10	02.0	09	01.9	10	02.2	12	01.8	02	01.0	04	01.5	13	02.2	11	02.5	13	
III	747.1	05.7	14.3	08.5	09.5	15.7	04.0	26.2	31	-06.5	02	*	05	02.6	18	02.8	35	02.3	04	02.5	07	01.7	11	02.5	09	02.6	05	02.4	13
IV	749.3	08.2	15.0	10.5	11.1	17.1	05.8	28.0	06	-00.4	12	03	C2.3	02	01.0	10	02.2	13	02.8	01	02.0	03	01.7	24	03.0	11	02.8	13	
V	748.9	14.4	21.7	16.0	17.0	22.5	11.4	28.0	22	04.4	01	04	C1.0	08	02.0	15	01.9	10	01.8	03	01.3	09	02.0	16	02.4	05	03.0	23	
VI	745.2	16.9	22.6	18.0	18.6	23.5	14.3	30.5	24	05.2	07	11	01.8	04	01.2	11	01.7	02	02.0	C5	01.4	06	01.7	22	02.3	08	02.4	21	
VII	745.7	18.0	25.3	19.6	20.6	26.6	14.7	32.6	19	06.1	28	05	C1.8	03	02.0	07	01.9	10	02.1	04	01.2	07	01.9	23	02.2	11	01.9	13	
VIII	750.7	16.9	24.0	18.3	19.4	25.0	14.7	30.0	12	08.2	15	08	C2.0	05	01.0	13	01.7	08	01.8	05	01.4	12	01.8	10	01.8	08	01.8	08	
IX	751.9	14.0	24.8	17.2	18.3	25.5	12.4	25.7	16	05.5	10	05	C2.0	05	01.4	17	01.8	14	01.9	C5	01.2	07	01.1	14	01.4	11	01.7	12	
X	754.5	08.0	15.2	05.6	10.7	15.5	04.7	26.1	C1	-00.5	28	07	01.6	07	02.3	20	02.4	04	02.0	*	04	01.5	24	01.9	09	01.9	18		
XI	754.0	02.5	07.3	03.6	04.3	08.2	01.0	20.0	18	-14.5	27	01	01.0	06	02.3	40	02.2	17	02.4	01	04.0	*	09	02.6	08	03.1	08		
XII	754.9	00.0	04.8	01.2	01.8	05.8	-01.6	12.0	06	-06.0	29	07	C1.6	01	01.0	16	02.6	16	02.3	01	01.0	26	02.2	16	02.1	16	02.1	30	
GOD.	-	07.5	15.4	08.8	10.1	16.5	03.7	31.0	24M	-15.5	26X1	101	C2.5	C9	02.2	17	02.0	165	04.6	154	C2.5	19	02.3	52	02.5	99	02.8	479	
$\varphi = 44^{\circ}56' N \lambda = 21^{\circ}05' E$ Gr. AG = + 1h 24 min.															FLAMUČA												BR. ST. 179		
I	-	-02.2	06.4	-01.0	00.6	07.2	-05.4																						

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm				Broj dana na sat:																								
	Indoljenje broj sati			Sred. (Dnev.)		7	14	21	Sred. (Dnev.)	7	14	21	Max.	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	A	A	R	T	≡	
	7	14	21	Sred. (Dnev.)		7	14	21	Max.	Min.	Σ	Max.	Dat.	≤	<	<	≤	≤	IV	IV	IV	<	>	IV	IV	IV	IV	•	Δ	Δ	A	A	R	T
SR. ST. 176																																		
SMEDEREVO																																		
I	4.9	4.5	4.7	4.7	-	-	-	-	-	024	011.6	05	-	02	18	-	-	-	-	-	11	C9	06	05	01	05	01	-	-	-	03	04		
II	4.9	4.5	5.6	5.0	-	-	-	-	-	011	006.5	04	-	01	24	-	-	-	-	-	C9	C8	04	03	01	02	03	01	-	-	02	02		
III	4.8	4.2	3.5	4.1	-	-	-	-	-	047	017.8	15	-	-	04	01	-	-	-	-	11	C8	07	07	02	05	03	-	-	-	01	01		
IV	6.1	5.4	4.2	5.2	-	-	-	-	-	039	009.4	02	-	-	02	-	-	-	-	-	04	C8	11	06	-	11	-	-	-	-	01	01		
V	4.6	4.1	3.4	4.0	-	-	-	-	-	105	019.5	27	-	-	-	14	-	-	-	-	-	10	C3	16	15	03	16	-	-	-	04	01		
VI	5.5	5.0	3.8	4.7	-	-	-	-	-	148	029.4	14	-	-	-	-	-	-	-	-	-	15	C4	07	15	-	-	-	-	-	01	04		
VII	2.4	3.5	1.9	2.6	-	-	-	-	-	090	029.0	02	-	-	24	07	01	-	-	-	15	-	09	08	03	09	-	-	-	08	-			
VIII	5.4	4.2	4.9	4.8	-	-	-	-	-	194	032.5	14	-	-	19	02	-	-	-	-	07	C6	18	14	07	18	-	-	-	01	11			
IX	3.2	1.6	0.8	1.8	-	-	-	-	-	030	015.7	06	-	-	-	21	-	-	-	-	-	20	C1	04	04	01	04	-	-	-	01	06		
X	6.4	5.9	4.7	5.7	-	-	-	-	-	061	011.2	15	-	-	-	01	-	-	-	-	-	C5	12	13	12	02	13	-	-	-	01	04		
XI	7.5	5.5	5.1	6.0	-	-	-	-	-	065	014.0	25	02	01	09	-	-	-	-	-	05	11	13	12	02	10	03	-	-	02	07			
XII	6.0	5.4	6.1	5.9	-	-	-	-	-	003	002.0	18	-	03	19	-	-	-	-	-	07	11	03	01	-	03	-	-	-	06	-			
GOD.	5.1	4.5	4.1	4.5	-	-	-	-	-	817	032.5	KJW	-	-	-	-	-	-	-	-	-	119	101	28	111	10	01	-	-	01	01	36	26	14
SR. ST. 177																																		
KRAGUJEVAC																																		
I	5.5	4.9	3.9	4.6	130.3	04.2	86	59	86	76	32	021	010.6	29	-	24	-	-	-	-	10	C8	05	04	01	04	01	-	-	-	01	03		
II	5.0	5.6	4.6	5.0	130.5	03.6	86	59	82	77	32	019	006.2	03	01	25	-	-	-	-	08	C8	07	05	02	05	-	-	-	01	02			
III	6.5	6.6	4.7	5.9	164.1	05.4	80	42	68	63	20	059	024.2	15	-	69	01	-	-	-	-	03	10	09	04	02	07	03	-	-	02			
IV	7.4	6.2	4.1	5.9	159.0	06.3	77	51	71	66	23	024	005.8	02	-	01	03	-	-	02	-	04	C9	12	07	12	-	-	-	01	-			
V	6.6	6.3	5.3	5.7	221.6	10.8	86	54	87	76	34	103	022.6	14	-	-	16	-	-	-	02	08	16	12	05	16	-	-	-	01	18			
VI	6.4	6.7	6.0	6.3	189.8	12.2	84	55	86	75	34	093	017.6	09	-	-	18	02	-	-	03	10	17	13	04	17	-	-	-	06	-			
VII	3.6	5.4	4.3	4.4	285.9	12.7	81	49	85	72	29	070	024.6	13	-	-	23	05	-	01	10	07	11	09	11	-	-	-	04	-				
VIII	5.5	6.8	6.4	6.0	183.8	12.6	86	56	87	77	32	255	034.0	13	-	-	15	02	-	02	06	11	20	17	09	20	-	-	03	10				
IX	2.9	3.2	2.5	2.9	244.5	11.3	88	44	86	73	30	013	006.6	13	-	-	20	01	-	-	14	02	05	04	-	05	-	-	-	04	-			
X	6.0	5.5	5.2	5.6	138.2	07.3	88	55	84	74	32	079	020.8	13	-	-	01	-	-	-	06	11	13	04	13	-	-	-	01	08				
XI	7.9	6.6	6.1	6.9	070.4	05.0	85	63	80	76	43	050	013.4	24	03	04	10	-	-	02	04	16	12	12	01	08	05	-	-	01	08			
XII	6.2	5.9	6.3	6.1	093.3	04.3	88	65	84	79	39	004	002.4	07	-	02	21	-	-	-	03	10	03	02	-	01	02	-	-	02	-			
GOD.	5.7	5.7	4.9	5.4	1994.6	08.0	84	54	82	73	20	790	054.0	15.VN	04	06	86	91	10	-	79	110	130	98	28	114	16	-	-	04	38	04	19	
SR. ST. 178																																		
SMEDEREVSKA PALANKA																																		
I	5.0	5.3	4.3	4.9	147.9	04.2	88	65	81	78	41	024	007.6	05	01	19	-	-	-	04	09	08	09	05	01	02	01	-	-	01	04			
II	5.1	5.9	4.9	5.3	130.0	03.6	86	58	78	74	28	009	002.8	03	01	23	-	-	-	04	02	06	09	06	04	02	05	-	-	02	04			
III	6.7	6.3	5.3	5.8	170.5	05.2	76	47	84	66	20	035	011.4	15	-	06	01	-	-	14	04	04	09	11	02	09	03	-	-	01	02			
IV	7.4	7.1	5.4	6.6	164.7	06.5	78	53	71	67	26	034	005.9	11	-	01	03	-	-	14	05	04	14	12	09	04	-	-	02	-				
V	6.2	6.5	5.9	6.2	234.6	11.2	90	55	83	77	30	130	024.3	27	-	-	08	-	-	-	16	03	04	10	18	16	05	17	-	-	14	07		
VI	7.0	6.4	6.1	6.5	199.0	13.0	88	55	85	79	44	137	029.1	11	-	-	18	03	-	-	10	03	11	19	13	05	11	-	-	01	16	02		
VII	3.3	4.5	3.1	3.6	288.5	13.7	87	57	82	75	40	086	021.2	02	-	-	24	04	01	11	04	11	02	12	09	04	12	-	-	01	09	03		
VIII	6.3	6.4	5.6	6.1	194.3	13.8	92	63	90	81	41	155	047.3	25	-	-	15	01	-	08	03	05	11	22	19	04	22	-	-	18	07			
IX	3.2	3.1	2.0	2.8	261.4	12.4	94	54	88	79	38	020	012.3	06	-	-	21	-	-	-	15	01	05	03										

Meseč	Vrednost pritisaka Pa MM	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Fm (0-12)																			
		Tm					Sred. (Dnes)					N		NE		E		SE		S		SW		W		NW		C			
		7	14	21			N	NE	E	SE	S	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		
$\varphi = 44^{\circ}54' N \lambda = 21^{\circ}25' E$ Gr. $\Delta G = +1h\ 25\ min.$																															
I	-	-06.7	06.3	01.4	02.1	03.1	-02.1	15.7	16	-05.7	01	č7	01.9	č4	02.0	06	01.5	10	01.1	07	01.6	39			
II	-	-02.1	04.7	00.5	00.9	05.6	-03.2	14.4	13	-11.5	05	01	02.0	04	02.8	č3	č2.7	03	02.0	05	01.6	04	01.2	10	01.3	21	01.7	33			
III	-	06.5	14.8	05.1	09.9	15.9	04.7	26.7	31	-06.7	01	č2	04.5	25	03.3	04	01.8	21	01.6	10	01.7	05	01.4	26			
IV	-	08.5	16.4	10.6	11.5	17.5	05.6	27.1	06	-06.5	12	01	č3.0	.	.	.	10	02.9	.	03	01.3	25	01.6	33	01.8	18					
V	-	15.5	22.7	16.2	17.7	24.2	12.2	26.5	22	04.1	01	01	01.0	.	.	.	č7	02.3	02	01.5	02	01.5	22	01.5	11	01.8	48				
VI	-	16.9	23.6	17.6	19.0	24.9	14.1	32.7	24	05.0	07	02	01.0	.	.	.	č9	01.1	17	01.6	03	02.3	10	01.4	01	01.0	21	02.2	37		
VII	-	18.3	26.2	19.5	20.9	27.4	15.0	32.7	24	05.0	28	02	01.5	01	01.0	01	01.0	č2	01.5	03	02.6	10	01.8	14	01.4	29	01.6	31			
VIII	-	17.8	25.1	19.0	20.2	26.2	15.1	30.8	12	05.5	15	01	02.0	.	.	.	č5	02.0	01	02.0	.	.	11	01.1	11	01.5	13	01.7	51		
IX	-	15.4	25.7	17.5	19.2	26.6	12.4	31.3	17	05.4	10	01	01.0	.	.	.	č8	02.5	03	02.3	08	01.6	09	01.7	07	01.4	34				
X	-	09.0	15.0	10.2	11.1	15.5	07.2	26.0	01	06.6	27	01	01.0	.	.	.	č3	03.3	17	02.9	01	01.0	.	.	15	01.1	14	01.4	42		
XI	-	03.6	07.8	04.6	05.3	08.9	01.6	18.1	18	-13.4	27	č5	03.4	34	02.5	08	01.9	04	01.5	04	01.0	12	01.2	23		
XII	-	-00.2	03.9	00.9	01.4	04.7	-01.5	11.1	06	-06.5	20	č3	02.0	14	02.4	01	02.0	.	.	08	01.1	19	01.4	48		
GOD.	-	09.0	16.0	10.7	11.6	17.1	06.8	32.7	84M	-13.4	27X1	10	01.5	05	02.4	21	02.3	135	02.6	24	01.6	79	01.5	139	01.4	192	01.7	470			
$\varphi = 44^{\circ}23' N \lambda = 21^{\circ}25' E$ Gr. $\Delta G = +1h\ 26\ min.$																															
PETROVAC																															
BR. ST. 182																															
I	-	-00.9	04.5	00.3	01.5	07.0	-	13.4	18	-	-	45	01.1	04	01.5	07	01.0	02	01.0	13	01.3	.	.	22		
II	-	-02.4	04.6	-00.6	00.3	05.3	-	13.2	13	-	-	01	01.0	04	01.5	42	01.3	.	08	01.2	04	02.5	12	01.6	.	.	13				
III	-	07.4	15.1	08.7	10.0	16.3	04.5	27.4	31	-	-	03	01.7	63	01.6	04	02.0	05	01.6	01	01.0	07	01.3	.	.	10					
IV	-	08.7	15.9	09.6	11.1	17.6	05.2	27.6	06	00.7	30		
V	-	15.1	22.5	15.7	17.3	23.5	11.6	28.0	22	08.0	04		
VI	-	17.5	23.4	18.0	19.2	24.4	14.1	32.0	24	07.4	07			
VII	-	18.0	25.5	18.4	20.1	26.8	-	33.0	19	-	-		
VIII	-	16.2	24.8	17.7	19.1	23.6	-	30.5	12.11	-	-			
IX	-	14.5	25.8	16.3	18.2	24.5	-	30.0	16	-	-			
X	-	08.9	15.4	09.2	10.7	16.4	-	26.5	01	-	-			
XI	-	02.2	07.6	02.8	03.6	08.6	-	19.0	18	-	-			
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VELIKE GRADISTE																															
BR. ST. 183																															
I	760.1	-06.6	05.9	01.1	01.6	04.4	-01.9	14.5	17	-03.1	11	12	02.3	14	02.3	07	01.3	13	01.5	47		
II	761.6	-02.6	04.9	00.3	00.7	05.5	-03.2	14.6	13	-06.6	10	03	02.7	01	01.0	09	02.2	11	02.1	12	01.6	.	.	04	01.2	17	02.4	39			
III	751.4	05.4	15.0	08.5	09.4	16.0	04.4	26.3	31	-08.2	01	02	01.0	.	.	23	02.9	27	02.8	01	02.0	01	01.0	03	07	02.1	29				
IV	753.4	08.3	16.5	10.6	11.5	17.8	04.2	27.4	08	-00.4	12	07	02.7	11	02.7	12	02.3	29	02.2	31			
V	752.7	14.9	22.5	16.0	17.4	23.4	12.5	28.1	23	04.4	01	01	01.0	.	.	13	02.0	17	02.0	02	01.6	06	02.5	32			
VI	752.7	17.2	23.4	17.8	19.0	24.7	14.2	32.2	24	05.4	07	08	02.1	08	01.5	13	01.5	13	01.8	03	01.3	12	01.4	15	01.7	11	01.8	37			
VII	753.1	18.0	25.7	18.8	20.3	26.8	14.8	31.0	19.18	07.7	28	05	01.8	05	01.0	16	01.5	14	01.9	03	01.3	06	01.5	13	01.7	12	01.5	39			
VIII	754.3	17.4	24.1	18.4	19.6	25.5	15.3	30.4	12	10.8	15	04	01.2	03	02.0	19	01.8	24	01.9	04	01.2	10	01.3	12	01.7	06	01.5	11			
IX	757.6	15.3	24.9	14.9	18.5	25.6	12.6	25.2	27	05.6	10	01	02.0	05	01.2	27	01.7	27	02.2	03	02.0	05	01.2	06	01.7	10	01.5	06			
X	758.4	08.8	14.3	10.0	10.8	15.1	07.1	25.4	01	00.4	26	03	01.7	08	01.1	21	03.0	18	03.6	03	01.0	10	01.5	12	01.8	07	02.0	11			
XI	758.2	03.2	06.4	04.1	04.5	07.2	01.8	15.3	18	-14.2	26	01	04.0	.	.	20	03.6	46	04.6	05	01.6	01	01.0	07	01.7	07	03.2	06			
XII	760.8	00.1	03.3	01.1	01.4	04.1	-01.4</																								

Meseč	Vrednost pritiska Pa mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vетра m/s, Fm (0-12)																			
		Tm				Min.	Max.	Dat.	Min.	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21	Sred. (Dnev.)						8.	9.	8.	9.	8.	9.	8.	9.	8.	9.									
$\varphi = 44^{\circ}41' N \lambda = 22^{\circ}25' E$ Gr.ΔG = + 1h 29 min.																						BR. ST. 186							
I	-00.3	04.6	01.5	01.5	05.6	-01.2	14.0	07	-05.2	18	01	C1.0	01	03.0	13	05.0	.	.	44	03.0	40				
II	-01.0	05.0	01.3	01.6	C6.1	-02.0	13.6	13	-07.0	18	10	C2.2	02	02.0	01	03.0	.	.	01	03.0	.	.	25	02.9	32				
III	-04.8	13.5	07.2	08.5	14.9	03.3	24.4	31	-01.8	02.0	24	C2.0	03	02.7	01	01.0	.	.	03	03.7	.	.	11	03.3	51				
IV	-05.6	17.0	11.3	12.3	18.4	06.7	25.4	30.0	03.2	12	21	C2.1	01	03.0	19	03.9	.	.	19	03.8	30				
V	-15.1	21.7	16.1	17.2	23.7	12.7	26.6	19	07.0	01	25	C2.1	04	03.0	.	.	01	03.0	.	.	01	03.0	.	.	09	02.3	53		
VI	-17.8	24.6	18.4	15.8	25.5	14.5	32.0	24	09.4	07	32	C1.8	02	02.5	.	.	01	04.0	.	.	10	03.8	.	.	18	02.9	27		
VII	-19.1	26.3	19.5	21.3	27.7	16.2	32.4	16	11.2	28	38	C2.0	01	03.0	04	04.2	01	02.0	20	03.2	27				
VIII	-17.7	24.2	19.1	20.0	26.0	15.4	30.6	18	11.6	15	24	C1.9	03	03.3	04	04.0	.	.	20	02.6	42				
IX	-15.4	25.5	17.6	15.0	26.2	13.5	36.0	17	05.4	10	23	C1.7	04	02.5	03	04.3	.	.	10	02.0	50				
X	-09.7	16.1	11.2	12.1	16.9	08.1	26.4	01	03.8	27	27	C2.1	05	03.6	05	04.6	.	.	20	03.1	32				
XI	-03.5	05.9	04.1	04.4	06.6	02.1	12.8	06	-09.6	27	22	C2.1	09	03.3	.	.	01	04.0	.	.	06	03.3	.	.	21	03.0	31		
XII	-01.0	04.7	02.1	02.5	05.6	-00.2	10.6	06	-03.4	01	32	C2.1	05	03.2	14	05.1	.	.	16	03.6	26				
GOD.	-	09.4	15.8	10.5	11.7	17.0	C7.5	32.4	KwM -05.6	27.4	279	C2.0	39	03.0	02	02.0	03	03.7	01	03.0	96	04.4	01	02.0	233	03.0	441		
$\varphi = 44^{\circ}14' N \lambda = 22^{\circ}33' E$ Gr.ΔG = + 1h 29 min.																						BR. ST. 187							
I	763.4	-00.1	05.1	01.1	01.8	06.0	-02.2	14.5	07	-06.5	15	09	C2.4	11	01.0	C5	01.0	03	01.3	03	01.3	05	01.2	21	03.0	26	02.7	10	
II	764.5	-01.4	05.4	00.6	01.5	C6.5	-03.0	15.4	12	-08.8	15	11	C2.0	09	01.9	12	01.8	03	01.7	03	01.3	07	01	01.7	19	03.6	18	02.7	62
III	755.4	03.0	13.6	07.1	15.0	01.6	24.4	31	-05.5	02	15	C1.3	18	02.1	10	01.7	06	01.7	06	01.3	05	01.4	11	02.7	15	02.3	87		
IV	756.0	10.1	17.3	11.4	12.6	19.0	06.6	25.0	07	01.2	13	08	01.5	08	01.5	C8	01.4	01	02.0	01	01.0	05	02.8	27	03.4	26	02.9	66	
V	755.8	16.1	22.6	16.4	17.9	23.6	12.2	24.0	19	06.4	05	17	C1.7	06	01.3	C7	01.6	05	01.6	03	01.3	04	01.0	14	02.0	23	01.6	11	
VI	755.6	16.8	24.9	18.5	20.4	26.1	14.9	32.3	24	08.8	11	16	C1.8	09	01.4	C8	01.6	.	01	02.0	01	02.0	22	02.8	22	02.3	69		
VII	756.0	20.1	26.4	20.7	22.0	27.8	15.7	32.3	19	12.4	27	04	02.2	07	01.3	C7	01.4	04	01.2	03	01.3	04	01.8	35	02.7	22	02.3	65	
VIII	757.5	17.9	24.7	18.6	20.1	26.3	14.7	30.4	11	-07.2	15	20	01.7	01	02.0	12	01.2	07	01.1	03	01.3	05	01.8	14	02.4	17	01.8	14	
IX	761.1	14.7	25.6	17.0	18.6	26.4	12.0	31.2	17	05.8	11	09	01.4	16	01.1	C6	01.3	01	02.0	01	01.0	03	01.0	15	01.7	12	01.5	23	
X	761.9	08.8	18.1	11.0	11.7	16.9	07.3	26.3	01	01.0	27	11	C1.5	11	01.5	15	01.5	.	03	01.7	03	01.8	27	02.7	14	01.9	67		
XI	763.1	02.1	04.7	02.9	03.1	05.3	01.1	14.0	04	-13.7	28	02	01.0	18	01.4	25	01.6	05	01.4	01	01.0	02	01.5	12	03.0	09	02.6	16	
XII	763.6	00.7	04.9	01.8	02.3	05.9	-01.3	13.0	06	-07.4	01	19	03.3	C8	01.1	04	01.0	02	01.5	.	.	06	03.3	36	03.4	11	02.4	121	
GOD.	759.5	09.2	15.9	10.7	11.6	17.1	06.6	32.3	42.4	13.7	141	C1.9	125	01.5	133	01.5	36	01.4	30	01.3	46	01.7	223	02.8	240	02.4	121		
$\varphi = 43^{\circ}55' N \lambda = 19^{\circ}26' E$ Gr.ΔG = + 1h 18 min.																						BR. ST. 188							
I	-06.2	00.6	-04.5	-03.6	01.4	-07.6	07.0	19	-17.4	01	32	01.5	24	01.1	37			
II	-08.9	-01.9	-06.6	-06.0	-06.8	-16.3	06.8	13	-22.6	09	49	01.4	09	01.6	26				
III	-00.5	06.0	00.3	01.5	07.4	-02.0	16.8	30	-14.0	01	09	C1.6	61	01.7	23				
IV	-02.1	08.2	03.6	04.4	09.8	00.6	20.2	07	-04.0	21	42	C1.1	26	01.5	22				
V	-07.9	14.4	09.8	10.5	15.9	06.2	21.6	22	-01.4	01	48	C1.4	13	01.2	32				
VI	10.8	15.5	11.5	12.3	16.5	08.4	24.4	30	02.5	06	35	C1.4	18	01.1	37				
VII	-11.6	18.2	12.6	13.8	19.3	09.1	24.6	19	04.0	28	47	C1.5	08	01.5	38				
VIII	-11.2	17.0	12.1	13.1	17.9	09.2	23.4	18	04.0	15	44	C1.1	15	01.1	34				
IX	-05.0	18.0	11.1	12.3	18.7	07.4	26.6	16	02.4	16	23	C1.4	03	02.0	.	.	01	03.0	18	01.3	45			
X	-06.6	12.6	06.6	08.2	13.6	04.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-02.8	00.8	-02.0	-01.5	02.5	-04.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII	-04.0	00.2	-03.4	-02.7	01.4	-06.0	09.4	17	-13.0	21	38	C1.5	22	01.5	33				
GOD.	-	03.0	05.1	04.3	05.2	C1.3	01.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 43^{\circ}44' N \lambda = 19^{\circ}43' E$ Gr.ΔG = + 1h 17 min.																						BR. ST. 189							
I	678.4	-03.1	01.6	-01.2	-01.0	02.3	-04.4	05.7	18	-12.2	10	17	C1.9	C1	02.0	05	02.8	41	02.8	07	02.1	01	01.0	01	
II	678.5	-05.6	-01.7	-04.1	-03.9	-06.4	-06.6	07.0	13	-13.7	09	15	C1.8	27	02.0	01	01.0	.	.	04	02.2	29	02.7	04	01.5	02	01.0	02	
III	678.9	02.7	08.1	04.1	04.7	C9.5	01.3	16.9	31	-07.3	22	10	C1.9	67	01.9	.	.	C4	02.8	25	03.4	43	03.3	01	03.0	.	03		
IV	672.5	04.8	C6.4	06.2	11.2	02.																							

Mesec	Oblačnost Nm (0-10)				Inkolacija broj sati (dies)	Vlažnost vazduha		Padavine R mm		Broj dana n sati:																														
	%		mm			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ															
	7	14	21	Sred. (dies)		mm	7	14	21	Sred.	Min	Σ	Mx	Dat.	=	<	<	IV	IV	IV	IV	IV	IV	IV	IV	IV														
TEKIJA																																								
BR. ST. 186																																								
I	8.0	4.9	5.8	6.2	-	04.3	88	74	81	81	43	001	000.8	29	.	01	20	.	.	04	01	03	11	01	.	01	.													
II	6.4	5.4	5.8	5.5	-	04.0	89	63	80	77	36	012	004.8	21	.	01	21	.	.	05	03	05	10	08	04	01	07													
III	8.4	6.5	6.1	6.9	-	05.8	84	55	73	71	28	051	C12.2	23	.	05	.	.	.	03	03	04	10	08	07	07	01													
IV	7.1	7.2	5.6	6.6	-	07.2	78	52	72	67	33	029	006.2	11	.	03	.	.	.	03	03	04	10	08	06	06	.													
V	7.7	7.1	6.9	7.2	-	11.8	87	63	87	79	41	166	040.5	05	.	01	12	.	.	01	01	12	18	17	06	14	.													
VI	6.8	6.6	6.4	6.6	-	13.4	84	61	81	75	45	197	060.2	21	.	01	21	05	.	01	03	13	11	11	04	11	.													
VII	4.4	5.8	3.9	4.7	-	14.4	84	59	82	75	31	070	025.4	13	.	01	25	07	.	04	07	06	06	03	06	04	.													
VIII	7.1	7.2	6.4	6.9	-	14.0	88	64	85	79	43	143	060.2	29	.	01	22	04	.	01	11	14	13	03	14	14	.													
IX	7.9	4.1	2.8	4.9	-	12.8	91	56	85	77	41	013	005.8	14	.	01	25	01	.	01	02	05	04	03	01	01	.													
X	7.8	6.5	6.3	6.8	-	08.2	86	64	82	77	36	119	019.8	14	.	01	01	01	.	11	11	11	07	11	10	02	.													
XI	9.3	9.0	8.8	9.0	-	05.3	88	75	84	82	49	077	011.8	23	.	01	10	.	.	01	02	24	10	10	02	07	04													
XII	7.8	6.2	6.0	6.7	-	04.4	88	73	81	81	48	006	002.2	18	.	01	15	.	.	02	03	02	13	03	03	02	01													
600.				7.4	6.4	5.9	6.5	-	08.8	86	63	81	76	28	884	060.2	29	VM	.	01	71	109	17	.	14	14	26	137	102	92	26	90	15	01	.	.	.	34	08	21
NEGOTIN																																								
BR. ST. 187																																								
I	6.6	5.8	5.2	5.9	104.6	04.0	03	66	79	76	35	006	002.4	09	.	04	25	.	.	14	03	07	11	03	03	02	01	01	01	01	05	01								
II	5.6	5.1	5.0	5.2	130.3	03.5	79	57	73	69	29	010	002.5	04	.	01	24	.	.	12	05	07	08	07	04	03	07	.	.	04	.									
III	7.3	6.5	5.3	6.3	151.4	05.6	87	55	73	71	25	050	016.2	22	.	01	12	.	.	07	02	03	12	08	05	02	07	03	01	02	01	04								
IV	5.9	5.9	3.5	5.1	200.2	07.0	73	50	68	64	27	025	007.8	27	.	01	.	.	.	17	04	05	06	11	07	11	11	01	04	.										
V	5.7	6.7	5.8	6.1	207.9	11.7	83	58	84	75	43	076	016.2	27	.	01	14	.	.	09	02	04	08	17	10	03	17	.	.	01	13	.								
VI	5.4	6.0	6.0	5.8	244.2	13.4	86	58	82	73	39	088	033.0	03	.	01	22	06	.	13	04	04	06	15	10	03	15	.	.	01	10	.								
VII	2.7	5.0	2.7	3.5	305.6	13.7	77	54	74	68	42	049	024.6	13	.	01	23	06	.	14	12	02	08	06	01	01	10	.	.	01	10	.								
VIII	4.9	5.7	4.6	5.1	219.8	13.7	88	59	85	77	39	158	052.1	29	.	01	21	02	.	04	01	06	04	15	11	09	13	.	.	01	18	01								
IX	2.5	2.6	1.3	2.1	232.0	12.2	92	51	84	76	37	027	014.0	13	.	01	24	01	.	02	16	06	03	01	06	01	03	03	.	.	03	03								
X	6.0	5.2	5.5	5.6	153.2	07.8	88	60	81	76	35	132	025.4	24	.	01	01	01	.	03	01	04	09	14	10	07	14	.	.	04	.									
XI	9.1	8.9	8.2	8.7	024.0	05.1	87	78	86	84	52	073	016.2	24	02	03	11	.	.	04	03	01	23	12	11	03	08	04	01	01	05	10								
XII	5.1	9.3	4.5	5.0	105.6	04.1	82	69	79	76	41	003	001.7	18	.	01	21	.	.	20	07	10	11	06	02	04	02	.	.	03	04									
600.				5.6	5.7	4.8	5.4	2075.6	08.5	83	59	79	73	25	699	052.1	29	VM	02	08	93	110	15	.	127	34	79	102	122	82	25	110	20	03	01	01	02	60	22	29
MITROVAC-TARA																																								
BR. ST. 188																																								
I	4.7	5.1	4.7	4.8	091.9	-	-	-	-	-	-	038	013.6	27	09	08	31	10	09	11	10	01	02	11	01	.	.	.	31							
II	5.2	5.2	5.5	5.3	091.7	-	-	-	-	-	-	025	005.4	27	16	15	28	10	11	10	08	02	09	01	01	.	.	.	28							
III	6.0	6.5	5.8	6.1	128.7	-	-	-	-	-	-	062	017.4	15	01	04	21	02	11	10	09	03	04	05	.	.	.	18								
IV	7.4	6.1	6.6	6.7	135.7	-	-	-	-	-	-	079	012.4	09	.	01	13	02	12	18	12	03	18	06	06	.	.	.								
V	6.2	6.9	7.1	6.7	152.3	-	-	-	-	-	-	188	026.2	15	.	01	01	01	01	12	18	17	07	18	.	.	.	08	08							
VI	6.7	7.0	8.0	7.2	134.5	09.4	91	75	92	86	33	152	036.4	19	.	01	27	02	14	18	17	07	18	.	.	.	05	06								
VII	5.2	5.2	6.2	5.5	209.6	-	-	-	-	-	-	107	018.4	06	.	01	02	03	08	13	12	05	13	.	.	.	02	06	.							
VIII	7.6	7.3	8.4	7.8	127.1	10.0	94	74	94	87	39	129	024.6	30	.	01	01	01	02	19	20	19	03	20	.	.	.	06	.							
IX	3.1	3.9	4.3	4.0	198.2	-	-	-	-	-	-	034	014.2	11	.	01	01	01	11	04	05	05	01	05	.	.	.	02	.							
X	6.0	5.9	6.3	6.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	01	03	.									
XI	7.8	7.4	7.7	7.6	038.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	01	01	09									
XII	7.3	6.7	7.4	7.1	070.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	07	16										
600.				6.1	6.1	6.7	6.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	102			
ZLATIBER																																								
BR. ST. 189																																								
I	4.8	4.7	4.3	4.6	146.9	03.1	80	66	76	74	20	030	010.4	27	03	07	29	18	.	12	09	10	08	01	02	11	01	.	.	0						

Mesec	Vrednost prirodak pm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s (0-12)																			
		Tm	7	14	21	Sred. (Ges.)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C								
													E.	J.															
$\varphi = 43^{\circ}16' N \lambda = 20^{\circ}01' E$ Gr.ΔG = + 1h 20 min.																													
I	678.2	-11.3	-02.6	-08.7	-01.4	-14.0	07.0	07	-22.6	11	02	C2.8	C1	01.0	C6	01.7	03	01.7	03	01.3	01	01.0	03	03.3	10	02.4	58		
II	677.9	-10.0	-02.9	-07.3	-06.9	-01.4	-11.6	03.7	12	-25.6	10	16	C2.2	C3	02.7	C4	01.5	C6	C1.3	C4	01.2	03	C3.3	01	01.0	10	01.8	37	
III	671.1	-00.5	07.5	01.8	02.6	04.7	-02.1	26.1	31	-17.3	C2.01	C4	C2.2	C3	01.3	C7	01.6	20	02.2	14	02.8	15	C3.1	04	01.8	04	01.5	20	
IV	673.9	04.1	10.2	05.6	06.4	12.0	01.5	22.0	07	-05.1	21	14	C2.7	C3	C1.7	C4	01.2	C3	C2.0	11	03.1	18	03.2	07	01.7	22	02.5	08	
V	674.5	08.8	14.3	10.6	11.6	17.8	05.5	22.5	22	-01.8	01	12	C2.5	C3	01.7	C7	02.1	C7	01.9	06	01.3	12	01.8	04	C1.5	09	02.2	27	
VI	675.2	11.7	17.3	12.3	13.4	18.8	08.2	24.9	30	00.6	10	15	C2.2	C9	01.4	C6	02.5	C4	01.5	C5	02.2	07	02.9	03	01.8	16	01.9	26	
VII	676.1	12.2	20.4	13.7	15.0	21.5	09.0	25.2	19	04.8	22	16	C1.5	C7	01.9	C9	01.4	C1	01.0	C2	02.0	06	02.3	08	01.4	17	01.8	27	
VIII	676.8	11.3	18.9	12.6	13.5	20.0	08.8	24.8	18	05.0	24	15	C2.1	C4	01.8	C6	01.5	C4	01.8	C7	01.7	09	02.2	03	01.0	17	01.6	28	
IX	675.6	08.1	20.4	11.1	12.8	21.3	06.1	27.5	16	01.3	25	08	C2.1	C7	01.3	C6	01.8	C7	01.3	04	02.0	04	02.8	05	01.8	08	01.4	39	
X	677.2	03.2	11.9	05.4	06.5	12.7	02.0	24.1	01	-06.6	30	17	C1.9	C5	01.6	C8	02.2	C4	02.3	C6	02.3	05	02.6	03	01.7	15	01.9	20	
XI	675.2	-01.9	03.5	-01.2	-00.2	04.9	-04.5	17.2	02	-26.2	26	04	C2.5	C1	01.0	C6	02.0	C3	01.9	07	03.1	06	02.3	03	02.3	08	01.9	32	
XII	677.6	-04.1	01.1	-02.7	-02.1	02.1	-05.6	12.0	17	-17.4	08	13	C1.7	C2	01.5	C5	01.2	C6	01.8	C9	01.4	*	*	01	01.0	14	02.1	33	
GOD.	676.1	02.6	10.2	#4.4	05.4	11.4	06.2	29.2	#9M	-26.2	26	XI	142	C2.2	48	01.6	E6	01.8	H8	01.9	78	02.2	86	02.7	50	01.7	150	02.0	395
$\varphi = 43^{\circ}51' N \lambda = 20^{\circ}02' E$ Gr.ΔG = + 1h 20 min.																						UZICKA POZEGA		BR. ST. 192					
I	739.3	-04.8	01.7	-02.7	-02.1	03.4	-04.1	12.3	25	-12.1	11	02	C1.0	C3	01.0	C3	C1.0	C6	01.2	C3	01.0	05	01.0	12	C1.2	30	C1.4	29	
II	740.2	-03.6	C3.0	-00.4	-00.4	04.6	-04.5	12.2	07	-17.3	09	06	C1.5	C5	01.2	C7	02.0	C6	07	C1.9	C1	01.0	04	01.0	08	01.5	30	01.5	16
III	730.4	01.2	14.0	06.7	07.2	15.6	00.2	26.0	31	-06.1	01	11	C1.3	C7	01.3	C2	01.9	C9	02.1	C1	02.0	11	C3.3	02	02.0	25	C1.6	12	
IV	733.3	05.8	15.5	09.4	10.0	17.3	03.6	28.4	07	-02.6	21	04	C1.5	C6	C1.3	C9	01.6	C1	02.0	C2	03.0	09	01.4	40	02.2	06			
V	732.8	11.9	21.4	19.0	15.8	22.6	10.5	27.8	22	06.5	01	03	C1.3	C5	01.4	C11	C2.0	C6	02.0	C1	03.0	02	01.0	13	01.2	33	C1.7	16	
VI	732.3	14.6	21.2	16.7	17.3	23.2	13.1	31.8	30	07.6	04	07	C1.3	C9	01.7	C5	01.6	C7	01.7	C4	C2.0	06	01.8	08	01.8	20	C1.5	14	
VII	733.8	15.4	24.8	18.3	19.2	26.3	15.5	35.6	19	05.8	27	05	C1.6	C5	01.4	C12	C1.3	C6	02.0	C5	01.8	C9	01.6	03	01.3	20	01.4	17	
VIII	734.6	15.1	22.9	16.8	17.9	24.3	14.4	30.6	12	11.4	15	06	C1.5	C6	01.5	C3	01.5	C6	01.6	C2	01.5	05	01.8	19	01.4	21			
IX	737.8	13.3	23.9	15.6	17.2	24.5	12.1	36.2	16	07.8	27	04	C1.5	C11	01.5	C6	02.1	C5	01.6	C6	01.5	05	01.8	05	01.2	19	01.3	27	
X	737.9	07.6	15.1	09.1	10.2	16.1	06.2	26.0	01	00.2	31	10	C1.7	C11	01.4	C9	01.3	C7	02.0	C6	06	01.3	09	02.0	04	01.0	18	01.5	23
XI	736.4	01.3	06.0	02.0	02.5	03.1	07.2	00.1	23.2	18	-17.2	27	02	C1.5	C9	00.9	C1	03.0	C12	01.6	C3	00.9	02.0	06	01.3	25	01.4	10	
XII	739.9	-01.3	02.0	-00.4	00.0	02.8	-02.3	08.6	23	-06.4	21	04	C1.5	C12	01.3	C6	01.5	C6	01.2	C2	01.0	04	01.2	11	01.2	26	01.4	19	
GOD.	735.9	04.4	14.3	08.5	09.6	15.7	01.2	35.6	#9M	-17.3	09H	64	C1.5	109	01.4	114	01.6	82	01.7	36	01.6	71	02.1	94	01.4	315	01.6	210	
$\varphi = 43^{\circ}35' N \lambda = 20^{\circ}14' E$ Gr.ΔG = + 1h 21 min.																						IVANJICA		BR. ST. 193					
I	-	-03.1	C4.6	-01.0	-00.1	05.8	-04.3	12.0	25	-11.2	10	12	C1.6	C8	01.4	C5	01.3	C7	01.9	09	02.0	*	*	01	02.0	04	01.5	37	
II	-	-03.8	03.6	-01.4	-00.8	04.8	-04.0	14.4	07	-13.3	09	14	C1.8	C7	01.7	C11	C6	11	C2.4	C1	02.0	02	01.0	07	02.7	30			
III	-	-02.8	14.2	04.5	07.5	15.4	01.4	26.2	01	12.0	01	15	C1.7	C3	01.3	C12	C1.3	19	C2.2	C16	02.8	04	02.5	05	03.0	03.0	16		
IV	-	07.2	15.0	08.7	09.9	16.7	04.6	28.0	07	-08.4	13	10	C2.6	C6	01.3	C4	01.4	C12	02.6	C1	01.0	06	02.8	11	03.1	13	02.4	17	
V	-	12.4	20.0	13.6	14.9	21.7	10.0	27.3	22	03.0	01	02	C2.5	C3	02.0	C2	33	C1.9	10	02.1	02	01.5	03	02.0	08	02.8	12	C2.1	20
VI	-	15.1	20.1	15.4	16.7	22.3	12.6	31.5	20	06.1	10	07	C1.3	C5	01.6	C15	C2.1	C9	02.0	C2	21	02.1	10	02.7	20				
VII	-	16.1	23.0	16.7	18.3	25.3	13.5	34.5	19	08.8	27	04	C2.0	C2	01.0	C27	C1.8	C8	02.8	C2	01.0	02	02.5	17	02.2	23			
VIII	-	14.9	21.9	15.7	17.1	23.3	13.3	29.0	16	16.12	09.5	15	C2.0	C10	01.6	C23	C1.7	C3	02.3	*	*	01	01.0	16	02.2	16	02.4	22	
IX	-	12.6	23.0	14.6	16.2	24.2	11.1	31.0	16	06.0	11	08	C1.4	C2	02.0	C3	01.8	C4	02.0	C6	*	*	01	02.0	17	02.8	10	02.2	15
X	-	06.8	14.5	08.3	05.9	15.4	05.8	24.9	01	00.0	30	05	02.0	C2	01.5	C26	C1.7	C6	03.8	C4	02.0	27	02.4	21	02.2	05			
XI	-	00.8	06.2	02.3	02.9	07.6	-00.6	20.2	18	-18.3	27	04	02.5	C4	02.2	C16	C1.6	C4	03.0	C1	01	07.0	01	05.0	30	02.4	16	02.2	14
XII	-	-01.2	03.5	-00.2	00.5	04.9	-03.0	16.0	17	-07.2	21	08	C1.2	C3	01.3	C19	C1.9	C7	02.1	C1	01.0	*	*	20	02.2	13	02.5	22	
GOD.	-	04.7	14.2	08.2																									

Mesec	Vrednost pritisak Pa MM	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, fm (0-12)																		
		Tm	7	14	21	Sred. (Dnev.)	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C	č.	j.	č.	j.						
			č.	j.	č.	j.	č.	j.	č.	j.	č.	č.	č.	č.	č.	č.	č.	č.	č.	č.	č.	j.	č.	j.						
$\varphi = 43^{\circ}06' N \lambda = 20^{\circ}31' E$ Gr. $\Delta G = + 1h 21 min.$																														
I	-	-04.5	64.2	-02.0	-01.1	05.0	-05.6	12.5	25	-10.5	05	-	-	-	-	-	-	-	-	-	-	-	-	-						
II	-	-03.8	63.7	-01.1	-00.6	04.7	-05.1	11.4	07	-12.5	10.09	-	-	-	-	-	-	-	-	-	-	-	-	-						
III	-	00.9	13.4	05.3	06.2	14.4	-00.4	22.0	31.30	-07.0	02	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV	-	06.2	15.8	08.5	09.8	16.5	03.8	26.4	07	-02.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-						
V	-	11.1	20.7	13.0	14.5	21.9	08.3	27.0	31.22	03.2	04	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	14.5	21.8	15.3	16.7	22.8	11.3	30.0	30	05.5	10	-	-	-	-	-	-	-	-	-	-	-	-	-						
VII	-	19.0	23.9	16.1	17.8	25.3	12.1	34.0	19	08.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	14.6	22.2	15.5	17.0	23.2	12.1	28.5	12	08.5	23.22	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	11.0	23.8	14.5	15.9	24.7	09.5	31.5	16	04.5	11	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	06.0	15.4	08.5	09.6	14.4	04.6	26.5	01	-02.5	31	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	00.9	07.0	02.6	03.2	07.9	-00.6	18.5	18	-16.5	26	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	-01.7	03.9	-00.4	00.3	04.5	-03.0	09.6	17	-07.5	10.06	-	-	-	-	-	-	-	-	-	-	-	-	-						
GOD.	-	05.8	14.6	08.0	09.1	15.6	03.6	34.0	19M	-16.5	26X	-	-	-	-	-	-	-	-	-	-	-	-	-						
$\varphi = 43^{\circ}44' N \lambda = 20^{\circ}41' E$ Gr. $\Delta G = + 1h 23 min.$																														
I	747.5	-01.4	05.6	00.9	01.5	06.5	-02.6	14.6	25	-06.6	05	01	02.0	01	01.0	C7	02.7	.	.	.	09	C1.3	02	02.0	73					
II	748.6	-02.3	04.0	00.7	00.7	03.7	-03.3	12.0	11	-12.1	09	02	01.5	.	.	C7	02.1	.	.	.	08	C2.1	01	02.0	64					
III	738.4	05.0	15.0	09.1	09.5	16.3	02.6	27.3	31	-04.9	02	C7	03.1	01	02.0	06	03.0	03	01.7	10	01.9	01	01.0	35		
IV	741.1	08.9	16.2	11.0	11.8	18.2	06.6	29.0	06	00.2	12	04	C1.5	01	03.0	C8	02.6	03	02.7	03	03.3	.	.	13	02.9	06	02.5	92		
V	740.4	13.9	21.7	15.6	16.8	23.2	11.7	28.9	22	03.7	01	03	C1.7	02	01.5	20	02.2	01	02.0	01	03.0	02	01.5	10	01.6	02	01.5	52		
VI	740.8	21.7	21.8	17.6	18.5	23.8	14.3	32.0	16	08.4	06	01	02.0	05	01.6	09	02.6	01	03.0	01	03.0	02	01.0	12	02.0	04	01.5	85		
VII	741.4	18.1	25.2	19.3	20.5	27.0	15.0	34.4	19	10.1	28	08	C1.9	.	.	C12	02.3	03	02.0	03	02.7	.	.	11	01.5	04	02.2	50		
VIII	742.4	16.4	23.9	17.6	18.8	24.9	14.1	30.6	12	10.0	15	02	02.0	01	02.0	12	02.8	02	02.0	02	01.5	03	01.7	05	01.8	03	01.7	63		
IX	745.9	14.0	25.0	17.4	18.5	25.6	12.2	30.6	17	07.3	11	01	02.0	01	02.0	14	02.6	03	02.0	02	01.0	.	.	06	01.3	02	01.5	61		
X	745.8	08.2	16.2	10.6	11.4	17.1	07.3	25.5	01	-00.8	30	02	02.0	01	01.0	17	03.7	02	04.5	.	.	03	01.3	07	01.3	01	02.0	60		
XI	745.1	01.8	07.4	03.9	04.2	08.3	00.4	22.6	18	-17.4	27	01	01.0	.	.	38	03.3	05	03.0	02	05.5	.	.	08	01.6	01	02.0	35		
XII	748.1	00.1	09.0	01.6	02.1	05.5	-01.3	11.4	17	-05.2	30	01	01.0	.	.	21	03.3	01	03.0	.	.	03	01.3	08	01.5	01	01.0	58		
GOD.	743.8	08.3	15.6	10.5	11.2	16.9	06.4	34.4	19M	-17.4	27M	26	C1.7	12	01.7	C22	02.9	22	02.6	21	02.9	17	01.3	107	01.8	30	01.9	658		
$\varphi = 43^{\circ}37' N \lambda = 20^{\circ}54' E$ Gr. $\Delta G = + 1h 22 min.$																														
I	-	-01.4	05.8	00.1	C1.2	06.4	-02.6	12.5	25	-04.6	20	24	C1.6	07	01.9	C2	02.0	03	01.0	17	01.4	.	.	01	02.0	10	02.2	29		
II	-	-03.2	03.6	-00.2	00.0	05.0	-03.8	11.4	13	-12.2	09	25	01.5	06	02.0	C1	02.0	02	01.5	17	01.4	.	.	01	02.0	09	02.7	23		
III	-	03.8	14.5	07.7	08.4	15.7	02.7	27.5	31	-03.5	02.01	16	01.9	13	02.2	08	03.1	06	02.3	31	02.0	02	02.5	01	04.0	04	02.2	12		
IV	-	08.1	19.9	09.7	10.9	17.5	05.7	29.0	07	-00.4	12	05	02.0	.	.	C2	02.5	02	02.5	26	01.7	02	03.0	04	02.0	25	02.2	24		
V	-	14.0	21.3	14.5	16.2	22.6	10.7	27.5	20	04.0	01	18	01.7	08	01.8	02	03.0	02	01.5	09	02.1	02	01.5	01	02.0	19	01.8	32		
VI	-	16.4	22.1	18.0	23.5	13.7	31.9	16	08.5	06	17	01.5	08	01.6	.	.	13	01.9	01	01.0	03	02.7	19	01.8	20	.	.	.		
VII	-	17.5	24.4	18.1	19.6	24.2	14.3	34.6	19	04.3	27.03	22	01.5	05	01.6	.	.	01	01.0	21	02.0	.	.	02	02.0	21	01.9	21		
VIII	-	16.1	23.0	16.5	18.2	24.2	14.2	29.4	12	08.8	15	21	01.6	01	02.0	01	02.0	02	02.0	13	01.5	.	.	02	01.0	20	01.8	33		
IX	-	13.5	24.5	16.2	17.6	25.1	12.2	29.1	16	04.0	11	08	01.6	17	01.8	C3	01.7	.	.	22	01.8	.	.	03	01.7	03	01.7	34		
X	-	07.8	15.8	09.5	10.7	16.3	07.0	24.1	01	01.5	31.27	09	01.7	08	01.8	C7	02.6	C2	02.0	13	01.3	01	02.0	01	01.0	22	02.2	30		
XI	-	01.8	07.2	03.2	03.9	08.2	00.7	23.3	18	-16.9	27	10	01.3	07	01.7	26	02.3	03	01.7	14	02.1	.	.	08	02.2	22	.	.	.	
XII	-	-00.5	04.7	00.7	01.4	C5.7	-02.1	11.4	01	-05.8	30	21	C1.2	03	01.7	13	02.5	C1	01.6	18	01.4	.	.	.	16	02.1	21	.	.	.
GOD.	-	07.8	15.2	06.5	10.5	16.4	04.1	34.6	19	M -16.9	27	M 196	C1.6	83	01.8	65	02.5	24	01.8	214	01.7	08	02.1	19	02.0	176	02.0	310		
$\varphi = 43^{\circ}27' N \lambda = 21^{\circ}04' E$ Gr. $\Delta G = + 1h 21 min.$																														
I	-	-00.4	06.2	C6.5	C1.5	07.0	-01.6	14.2	25	-04.6	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	-03.1	04.3	-00.6	00.0	05.4	-04.6	11.5	13	-12.4	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	05.7	14.1	07.9	08.9	15.6	03.2	29.5</																						

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati Sred. (dies)	Vlažnost vazduha			Padavine R mm			Broj dana nasa:																													
					U m s						Th	Tx	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	Δ	•	▲	▲	R	•	•	•	•	•	•						
	7	14	21		Sred.	Min	Max	Dat.	mm	7	14	21	Sred.	Min	M	Max	Dat.	mm	10.00.0	0.025.0	30.020.0	6	8	2.0	8.0	0.1	1.010.0	,	Δ	*	Δ	•	▲	▲	T	•	•	•	•	•
BR. ST. 196																																								
NCVI PAZAR																																								
I	4.5	1.9	2.2	2.9	-	-	-	-	-	012	003.1	05	08	.	28	.	.	C9	.	15	C2	C8	04	.	04	05	01	01	19			
II	5.5	3.2	4.1	4.3	-	-	-	-	-	007	C02.1	21	C3	G1	26	.	.	.	07	04	07	02	.	C2	05	05	.					
III	4.7	4.0	5.4	4.7	-	-	-	-	-	046	C15.2	22	.	17	.	.	.	17	.	04	02	C9	08	02	05	05	01	04			
IV	4.3	3.5	3.9	3.9	-	-	-	-	-	015	C06.4	02	.	04	02	.	.	.	08	02	07	04	.	C7						
V	4.7	4.4	4.9	4.7	-	-	-	-	-	103	C16.5	27	.	.	.	05	.	.	.	08	06	15	13	03	15	01	02					
VI	4.2	3.5	4.6	4.1	-	-	-	-	-	096	C25.2	15	.	.	.	14	01	.	.	.	09	03	14	13	03	14				
VII	3.7	2.5	3.7	3.5	-	-	-	-	-	082	C28.7	12	.	.	.	18	03	.	.	.	11	C3	10	05	03	10	01	.				
VIII	3.9	2.5	3.5	3.3	-	-	-	-	-	060	C24.2	25	.	.	.	11	.	.	.	10	C2	13	09	02	13	01	.				
IX	3.6	1.0	1.8	2.1	-	-	-	-	-	023	C22.2	13	.	.	.	14	01	.	.	.	16	.	04	01	01	04	02	07				
X	5.5	2.9	3.8	4.1	-	-	-	-	-	115	C43.2	12	.	.	06	03	.	.	.	10	03	13	12	03	13	02	07					
XI	-	-	-	-	-	-	-	-	-	055	C11.4	19	04	04	11	11	09	01	08	05	01	01	03	09	
XII	5.8	2.4	3.2	3.8	-	-	-	-	-	019	C17.5	18	.	01	24	07	.	02	01	01	01	C1	01	04	01				
GOD.	-	-	-	-	-	-	-	-	-	641	C43.2	15.X	15	06	118	67	05	115	87	19	98	21	02	.	.	.	01	.	29	38						
BR. ST. 197																																								
KRALJEVC																																								
I	5.5	5.3	4.8	5.2	109.8	04.1	89	45	84	75	46	018	004.8	02	.	23	.	.	.	10	12	07	05	.	05	64	01	04	04						
II	6.4	6.2	5.2	5.9	101.9	03.7	87	64	78	76	37	017	003.4	17	02	22	.	.	.	06	11	09	04	.	09	67	02	01	02						
III	6.1	7.1	5.3	6.2	163.6	05.4	78	44	66	63	22	094	035.7	22	.	07	01	.	.	07	02	01	11	08	04	04	05	02	.	.	02	.	02							
IV	7.3	6.8	5.5	6.5	148.0	06.2	73	45	66	63	20	027	011.3	02	.	03	.	.	04	01	05	12	09	08	01	09	01	03								
V	5.6	6.4	4.9	5.6	189.3	11.2	90	25	86	78	34	180	052.8	27	.	12	.	.	02	01	04	C8	18	13	04	18	01	13	11							
VI	6.9	7.2	5.6	6.5	156.9	13.1	87	69	81	81	41	150	C39.5	15	.	17	02	.	01	.	03	10	23	15	05	23	01	14	04							
VII	3.9	5.2	3.9	4.4	252.9	13.8	88	26	58	83	76	41	093	C29.3	31	.	23	05	.	02	.	08	06	13	09	04	13	11	02							
VIII	7.6	6.8	6.0	6.8	160.0	13.7	94	67	90	83	44	113	016.5	03	.	12	01	.	04	01	02	13	20	14	05	20	14	13								
IX	5.3	3.6	2.5	3.8	226.0	12.5	65	55	86	75	36	015	005.6	13	.	18	02	.	01	01	04	07	03	.	07	03	15									
X	7.4	6.5	5.7	6.5	142.9	08.0	91	61	83	78	33	109	022.6	03	.	01	01	.	04	04	15	12	05	15	04	04										
XI	8.1	7.4	5.5	7.2	061.3	05.2	80	28	65	83	80	31	078	017.0	24	03	02	10	.	01	01	03	17	13	11	03	05	.	.	05	08									
XII	7.5	6.4	5.9	6.6	079.7	04.3	87	71	82	80	47	006	002.2	07	.	01	24	.	.	03	12	07	02	.	06	03	.	01	.	.	09									
GOD.	6.5	6.3	5.1	5.9	1792.3	08.4	87	60	81	76	20	900	052.8	27V	05	03	81	88	10	.	36	06	41	129	151	106	30	138	25	03	01	.	03	78	70	16				
BR. ST. 198																																								
VRNJACKA BANJA																																								
I	6.1	4.6	4.4	5.1	132.6	04.1	91	63	88	81	44	020	C05.8	09	.	27	.	.	.	11	C9	08	06	04	06	64	02	01	07				
II	5.7	6.0	5.5	5.7	105.6	03.6	89	64	83	78	39	018	004.5	27	01	24	.	.	.	07	12	10	07	04	07	04	.						
III	5.8	6.9	4.7	5.8	164.2	05.4	83	45	74	68	20	078	024.5	15	.	06	01	.	.	01	03	10	09	07	03	08	05	02	.	04						
IV	7.0	6.1	4.8	6.0	162.6	06.4	77	50	75	67	18	041	C11.6	02	.	01	03	.	01	06	10	13	07	01	13	02	.	.								
V	6.0	6.5	4.9	5.8	217.3	11.2	90	25	88	80	25	118	028.6	03	.	07	.	.	.	02	08	23	13	07	22	13							
VI	6.1	7.2	5.5	6.3	183.0	12.8	88	67	88	81	39	178	107.2	19	.	16	03	.	.	03	10	22	13	03	22	13							
VII	3.9	5.2	4.3	4.5	263.4	13.8	88	6																																

Meseč	Vazdušni pritisak Pa mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, fm (0-12)															
		Tm			Sred. (Dnev.)	N	NE	E	SE	S	SW	W	NW	C													
		7	14	21										č.	j.	č.	j.	č.	j.	č.	j.	č.	j.				
$\varphi = 43^{\circ}59' N \lambda = 21^{\circ}14' E$ Gr. $\Delta G = + 1h 25 min.$																											
I	-	-00.9	04.3	01.7	02.2	06.4	-02.1	14.0	17 -06.4	21	-	-	01	04.0	-	-	02	02.5	-	-	01	03.0	-	-	12	02.2	77
II	-	-02.6	04.6	01.2	01.1	05.3	-03.7	12.9	13 -10.0	09	-	-	03	01.7	-	-	04	01.8	-	-	01	02.0	-	-	20	02.2	56
III	-	05.1	15.6	10.0	10.2	16.6	03.1	26.0	31 -05.5	02	10	02.3	-	-	-	-	17	03.6	10	02.8	01	02.0	-	-	-	-	55
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	19.0	26.1	20.2	21.4	27.5	14.6	34.0	19 08.0	27	39	01.7	-	-	-	-	04	02.0	07	01.4	-	-	-	-	-	-	43
VIII	-	17.5	24.3	18.7	19.8	25.4	14.5	30.0	11 05.0	15	29	01.6	-	-	-	-	01	03.0	04	01.5	02	01.5	-	-	-	-	57
IX	-	13.9	25.6	17.8	18.8	26.0	12.6	29.5	16 05.5	10	18	01.9	-	-	-	-	-	-	-	18	01.8	02	02.0	-	-	52	
X	-	08.4	15.3	11.0	11.4	16.1	06.6	26.0	01 00.5	29	14	01.6	-	-	-	-	-	-	-	19	02.2	12	02.3	01	02.0	47	
XI	-	02.0	07.6	03.7	04.3	08.3	06.3	20.2	18 -18.5	27	11	01.6	-	-	-	-	32	02.2	02	01.5	10	01.9	-	-	-	-	35
XII	-	00.2	04.7	01.9	02.2	05.4	-01.3	11.5	18.17 -06.5	24	27	01.6	-	-	-	-	12	02.2	02	02.0	01	04.0	01	06.0	-	-	50
600.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 43^{\circ}00' N \lambda = 21^{\circ}16' E$ Gr. $\Delta G = + 1h 25 min.$																									BR. ST. 201		
I	-	-02.8	04.0	-00.8	00.4	04.6	-04.1	13.4	07 -08.0	05	09	01.6	05	01.4	01	03.0	-	-	11	02.0	22	01.1	01	01.0	13	01.2	31
II	-	-04.3	03.9	-01.6	-00.6	04.9	-05.1	14.6	07 -14.8	04	18	01.6	09	01.2	-	01	04.0	06	01.8	22	01.1	-	-	18	01.7	10	
III	-	02.7	14.3	07.3	07.9	15.5	01.5	23.9	31 -05.4	01	04	02.2	04	01.5	01	02.0	11	02.6	18	03.1	38	01.3	-	-	07	01.3	16
IV	-	07.7	18.3	09.3	11.0	17.7	05.0	27.3	06 -01.4	12	16	02.2	07	01.6	-	03	03.3	09	03.0	24	01.5	01	01.0	09	01.8	10	
V	-	12.7	21.5	14.1	15.6	22.6	05.4	27.3	23 01.9	01	11	02.1	08	01.5	-	04	01.5	03	02.0	29	01.2	02	01.5	06	01.3	30	
VI	-	16.0	22.4	16.0	17.6	23.6	12.2	31.7	02 08.1	04	18	01.7	04	01.2	-	04	03.2	07	02.2	23	01.2	01	01.0	11	01.4	25	
VII	-	16.8	25.1	17.2	19.1	26.5	12.8	34.0	19 07.4	27	16	01.6	07	01.3	-	03	02.7	05	01.8	33	01.1	01	01.0	10	01.1	18	
VIII	-	15.0	23.9	16.5	18.0	25.3	12.7	30.2	18.16 06.5	15	13	01.8	07	01.4	-	-	05	01.8	33	01.2	02	01.0	16	01.2	17		
IX	-	12.2	24.7	15.0	16.7	25.9	10.7	30.1	16 05.4	11	14	01.4	07	01.3	01	02.0	02	02.5	06	01.7	37	01.2	05	01.2	05	01.2	13
X	-	04.8	16.1	08.7	10.1	16.9	05.6	27.1	01 -06.6	31	10	01.6	11	01.5	-	02	03.0	07	02.6	29	01.1	04	01.5	17	01.1	13	
XI	-	01.9	07.6	03.5	04.1	08.6	00.3	15.3	18 -14.3	26	22	01.1	05	01.4	01	01.0	-	07	01.6	23	01.3	-	-	22	01.1	10	
XII	-	-00.8	03.0	00.1	01.1	05.9	-02.7	13.3	18 -07.4	31	21	01.8	14	01.7	04	01.2	03	02.7	06	02.8	30	01.1	08	01.0	04	01.0	06
600.	-	07.0	15.6	08.8	10.1	14.6	04.4	34.0	19M -14.8	09H	172	01.7	88	01.5	08	01.6	33	02.7	87	02.4	345	01.2	21	01.2	138	01.3	203
$\varphi = 43^{\circ}34' N \lambda = 21^{\circ}21' E$ Gr. $\Delta G = + 1h 25 min.$																									BR. ST. 203		
I	-	-01.4	05.6	-00.1	01.0	04.4	-02.1	13.2	25 -07.4	05	02	04.0	01	02.0	03	03.7	-	-	02	02.0	-	-	02	03.9	06	04.2	77
II	-	-02.7	04.3	00.1	00.4	05.4	-03.3	12.6	13 -04.8	09	13	03.1	05	03.0	04	03.0	-	-	03	02.3	01	02.0	02	03.0	07	04.0	49
III	-	04.2	14.9	08.8	09.2	18.0	02.4	26.2	31 -05.3	02	06	02.7	03	03.7	10	03.1	05	03.2	13	03.8	02	03.0	03	02.3	02	03.0	49
IV	-	08.7	16.8	11.0	11.8	18.0	05.9	28.2	06 -01.4	12	10	03.9	02	02.0	-	-	17	03.4	02	03.5	09	04.4	14	04.2	86		
V	-	14.1	21.9	16.3	17.2	23.3	11.0	28.8	31 02.7	01	04	02.8	07	02.6	05	02.4	-	-	06	03.0	07	02.7	02	04.5	59		
VI	-	16.8	22.8	18.2	19.0	24.2	14.0	32.1	02 09.1	06	07	03.1	02	03.0	04	02.8	-	-	07	02.3	-	-	09	03.6	04	04.0	55
VII	-	17.9	25.4	19.1	20.4	26.7	14.9	35.2	19 06.7	28	08	02.8	02	02.5	02	01.5	02	02.0	09	02.3	01	02.0	05	03.0	08	03.1	56
VIII	-	16.1	23.9	18.2	19.1	25.1	14.4	31.0	12 08.8	15	06	03.0	01	02.0	02	02.5	03	02.0	01	03.0	06	03.0	03	03.3	59		
IX	-	13.3	25.8	16.8	18.2	26.3	11.6	30.6	16 05.5	11	05	02.4	05	02.2	05	02.8	01	02.0	01	03.0	-	-	01	03.0	03	03.3	69
X	-	07.4	16.0	05.6	10.7	16.6	06.2	26.8	01 -01.0	31	06	03.2	04	03.5	08	02.9	03	03.0	07	02.8	-	-	03	03.0	03	03.3	59
XI	-	01.4	07.7	03.4	04.0	08.7	00.0	21.4	18 -21.4	27	01	02.0	04	03.0	22	03.4	02	03.0	04	04.2	01	05.0	04	04.0	01	03.0	51
XII	-	-00.1	03.0	01.1	01.6	05.0	-01.5	11.7	18 -06.2	10	05	03.0	04	03.2	08	01.9	04	03.5	09	01.5	-	-	05	03.4	07	03.7	56
600.	732.3	08.3	15.7	10.1	11.0	14.8	06.1	33.4	19M -16.6	27H	189	02.5	17	02.0	21	01.2	1C1	03.3	131	02.4	53	02.1	03	02.0	48	02.5	532
$\varphi = 43^{\circ}14' N \lambda = 21^{\circ}36' E$ Gr. $\Delta G = + 1h 26 min.$																									PRKUPLJE		
I	-	-02.4	05.2	-00.5	06.5	C4.1	-03.4	11.4	25 -07.2	21	-	03.0	01</td														

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm	Broj dana na sata:																					
							Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	R	T	≡			
	7	14	21	Sred. (Dnev.)			7	14	21	Sred.	Min.	Σ	Max	Dat.	<=	<	<	IV	IV	IV	IV	IV	IV	IV	IV	IV		
SVEĆAREVC																												
BR. ST. 201																												
I	5.6	4.6	4.8	5.0	-	04.4	91	70	85	82	39	026	C11.4	29	.	01	22	.	.	.	12	10	06	06	01	03	01	
II	4.6	5.0	4.3	4.6	-	04.0	92	70	81	81	43	012	C04.5	03	01	.	24	.	.	01	.	10	06	05	04	03	04	.
III	4.9	4.3	4.8	4.7	-	-	-	-	-	-	-	-	-	-	-	08	02	.	.	02	.	08	08	-	-	-	-	02
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	4.1	4.9	4.7	4.6	-	15.1	88	45	82	78	45	070	C20.2	06	.	.	25	18	.	01	01	05	04	09	03	05	.	
VIII	6.4	6.3	5.7	6.1	-	-	-	-	-	-	-	154	C33.0	27	.	.	18	01	.	02	.	04	10	16	15	04	16	.
IX	4.0	2.9	2.2	3.0	-	12.5	92	55	85	77	38	040	C29.6	13	.	.	22	.	.	01	.	13	02	03	03	01	03	.
X	6.0	6.0	5.4	5.8	-	08.1	89	67	82	75	44	063	C14.4	13	.	.	01	.	.	01	.	07	14	09	03	03	01	.
XI	8.3	6.4	6.2	6.9	-	-	-	-	-	-	-	065	C10.4	25	03	02	10	.	.	01	.	03	16	12	11	02	08	03
XII	6.7	5.8	6.8	6.4	-	-	-	-	-	-	-	001	C01.0	08	.	.	18	.	.	01	.	06	14	01	01	01	01	.
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
KURSUPLJINA																												
BR. ST. 202																												
I	5.6	5.3	3.5	4.8	104.7	03.8	85	62	88	75	33	010	C03.0	31	.	02	28	.	.	.	16	09	10	03	.	04	07	
II	5.6	5.5	5.6	5.6	099.7	03.4	88	60	80	76	32	011	C02.5	04	02	03	24	.	.	.	07	11	09	03	.	04	07	
III	5.3	6.8	4.4	5.5	134.8	05.3	85	46	72	68	23	057	C16.3	15	.	.	10	.	.	01	.	04	07	08	04	02	04	
IV	6.4	5.8	4.2	5.4	150.2	06.0	74	45	69	63	23	C30	C14.2	02	.	.	03	02	.	.	01	01	06	11	04	01	05	
V	5.8	6.0	5.1	5.6	171.2	10.2	87	55	86	76	33	105	C20.8	14	.	.	07	.	.	01	04	07	14	14	03	19	.	
VI	5.3	6.2	5.3	5.6	150.8	12.1	84	43	88	78	38	082	C16.1	15	.	.	14	02	.	.	04	08	19	13	02	19	.	
VII	3.7	4.5	3.5	3.9	222.6	12.4	83	53	87	74	36	051	C28.7	13	.	.	22	04	.	.	08	01	16	05	02	10	.	
VIII	5.9	5.6	5.2	5.6	162.3	12.2	85	57	90	79	34	050	C27.6	25	.	.	14	02	.	.	02	07	20	12	02	26	.	
IX	3.2	3.2	1.8	2.7	222.3	11.2	93	52	91	75	31	033	C12.5	05	.	.	20	01	.	.	16	01	06	04	02	06	.	
X	6.4	5.5	4.1	5.3	131.4	07.5	92	59	89	80	35	080	C24.9	13	.	.	04	01	.	.	01	06	08	10	02	19	.	
XI	8.3	7.0	7.1	7.5	047.6	05.3	89	70	85	82	47	056	C10.8	16	03	03	11	.	.	03	19	18	12	01	13	07		
XII	7.0	5.4	4.5	5.7	049.7	04.1	87	69	86	80	47	014	C11.3	18	.	01	23	.	.	03	10	05	02	01	04	02		
GOD.	5.7	5.6	4.5	5.3	1667.3	07.8	86	57	84	74	23	623	C28.7	15	V	05	09	105	80	09	.	03	02	101	92	08	29	
KRUSEVAC																												
BR. ST. 203																												
I	6.4	5.2	4.3	5.3	106.6	04.1	91	65	92	83	44	012	C02.4	02	.	01	27	.	.	04	.	08	08	09	05	.	01	00
II	6.2	5.8	5.3	5.8	095.7	03.7	89	59	86	78	33	010	C06.1	04	.	.	24	.	.	10	.	08	12	09	02	04	01	04
III	5.9	7.1	5.3	6.1	151.4	05.8	90	46	74	70	23	057	C17.4	15	.	.	08	01	.	14	.	03	12	11	07	03	08	02
IV	7.1	6.1	4.6	5.9	157.6	06.7	80	47	75	67	21	025	C14.2	02	.	.	01	03	.	20	.	05	10	08	03	01	06	.
V	5.8	6.2	5.4	5.8	195.1	11.3	92	58	89	80	25	108	C45.6	03	.	.	11	.	.	07	.	02	06	18	14	02	16	.
VI	7.0	6.7	5.6	6.4	166.7	13.5	92	64	91	82	36	115	C45.1	19	.	.	17	04	.	05	.	02	11	17	14	02	17	.
VII	4.1	5.5	3.6	4.4	253.5	14.5	91	56	94	81	34	108	C40.5	13	.	.	21	04	.	09	.	08	04	11	10	03	11	.
VIII	6.6	6.7	5.7	6.3	166.0	14.3	98	56	87	87	37	088	C14.2	27	.	.	15	03	.	11	01	04	09	19	19	04	17	
IX	2.6	3.3	2.5	2.8	235.4	12.3	98	48	95	81	27	026	C12.5	13	.	.	22	01	.	05	.	13	02	06	09	01	06	.
X	6.9	6.1	5.1	6.0	121.0	08.3	98	63	94	86	38	070	C17.1	12	.	.	04	01	.	07	.	05	12	15	12	02	19	.
XI	7.7	6.9	6.7	7.1	044.8	05.4	92	69	89	84	35	069	C12.7	24	04	04	11	.	.	12	01	04	17	13	10	02	09	
XII	6.9	6.6	4.0	4.5	054.4	04.5	94	73	92	84	43	005	C01.4	07	.	.	03	23	.	11	.	04	13	09	02	01	01	
GOD.	6.1	6.0	5.0	5.7	1742.2	08.7	92	59	89	80	21	693	C045.6	05V	04	08	98	91	14	.	121	02	06	116	145	99	20	134
CUPRIJA																												
BR. ST. 204																												
I	5.5	5.1	5.0	5.5	132.0	04.2	87	66	84	80	44	015	C07.2	29	.	01												

Mesec	Vrednost pritisaka P ₀	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetrova dB, Fm (0-12)																		
		Ta					Hx	Hf	Mx	Mf	Dat.	Mj	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21	srđ. (100)	8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.							
$\varphi = 43^{\circ}39' N \lambda = 21^{\circ}51' E$ Gr. $\Delta G = + 1h\ 26\ min.$																														
I	-	-01.9	03.8	-00.7	00.1	04.6	-02.7	10.8	17	-07.6	11	-	-	-	-	-	20	03.2	-	-	02	01.5	04	02.0	02	02.5	-	-	55	
II	-	-03.0	03.1	-00.7	-00.3	04.2	-04.2	12.4	13	-10.5	19.10	01	02.0	-	-	-	-	-	-	-	02	01.5	04	02.0	02	02.5	-	-	55	
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19	03.2	-	-	-	-	09	03.4	11	02.8	-	-	50	
IV	-	07.6	14.9	11.7	12.0	17.6	05.5	27.4	06	-02.6	12	01	02.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	50		
V	-	11.4	20.9	15.8	16.0	22.6	10.2	27.5	31.30	02.8	02	01	03.0	-	-	-	05	03.0	-	-	02	02.5	02	02.0	10	02.1	-	-	73	
VI	-	14.7	22.4	17.6	18.2	23.6	13.4	30.1	02	07.3	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	73		
VII	-	15.2	25.2	18.8	19.5	26.7	13.5	34.4	19	07.6	20	01	03.0	-	-	-	07	02.6	-	-	-	-	06	01.8	09	01.7	-	-	70	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	70		
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
600.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}20' N \lambda = 21^{\circ}54' E$ Gr. $\Delta G = + 1h\ 26\ min.$																														
I	749.0	-01.5	04.5	00.1	00.8	05.4	-02.4	11.9	25	-05.9	20	03	03.3	-	-	12	01.2	02	01.0	-	02	01.5	06	01.0	16	02.7	52			
II	749.7	-02.4	04.5	00.5	00.8	05.7	-03.2	13.0	13	-08.6	10	02	01.5	06	03.2	15	01.8	04	01.8	05	01.2	03	01.0	19	02.3	26				
III	750.7	04.4	15.3	09.2	09.6	16.4	03.4	26.0	31	-04.9	02	-	-	02	02.5	15	01.7	14	01.6	15	01.6	07	02.1	20	02.1	26				
IV	742.6	08.3	17.0	10.8	11.7	18.7	05.6	28.3	06	-01.1	12	06	02.2	-	-	02	02.0	03	01.0	09	02.5	09	01.8	05	01.6	26	02.7	31		
V	741.9	14.4	22.2	16.1	17.2	23.7	11.7	28.4	31	01.6	01	-	-	03	01.3	09	01.4	01	01.0	04	01.2	05	01.6	06	01.3	18	02.0	47		
VI	742.2	17.1	23.3	18.2	19.2	24.5	14.3	32.4	02	06.1	07	06	01.8	01	01.0	10	01.3	04	01.0	03	01.7	03	01.7	05	01.2	20	02.2	31		
VII	742.7	18.4	26.2	19.7	21.0	27.3	14.9	34.8	19	09.0	27	11	01.7	01	01.0	07	01.3	02	01.3	01	01.7	01	01.0	01	01.0	24	02.3	45		
VIII	742.6	17.1	24.8	18.9	19.9	25.9	13.1	31.2	12	08.2	15	11	01.8	03	01.3	09	01.3	01	01.0	01	02.0	03	01.0	03	01.3	20	01.9	43		
IX	747.1	14.1	26.0	17.8	19.0	26.7	12.4	30.7	16	06.3	11	03	01.7	01	03.0	20	01.2	04	01.3	04	01.2	02	01.6	05	01.0	10	01.6	39		
X	747.4	08.6	16.5	10.6	11.7	17.5	07.4	27.0	01	00.1	31	07	01.4	01	01.0	19	02.6	03	02.0	-	04	01.0	04	01.2	02.1	02.1	21			
XI	747.0	03.0	08.0	04.4	04.9	08.8	01.6	21.0	18	-12.9	26	02	01.0	04	02.5	33	02.3	03	02.0	04	02.2	02	01.0	01	02.0	21	02.3	49		
XII	749.7	00.6	04.7	11.5	02.1	05.7	-00.9	13.4	18	-05.3	23	04	01.8	-	-	14	02.6	03	02.0	01	03.0	03	01.0	05	01.2	21	02.3	43		
600.	745.3	08.5	16.1	10.7	11.5	17.2	06.7	34.8	19W	-12.9	26X	55	01.8	22	02.2	145	01.8	46	01.5	47	02.1	46	01.4	20	01.2	210	02.2	484		
$\varphi = 43^{\circ}01' N \lambda = 21^{\circ}57' E$ Gr. $\Delta G = + 1h\ 26\ min.$																														
I	747.4	-02.3	03.7	-00.2	00.2	04.5	-03.2	11.0	25	-08.7	05	12	04.4	-	-	C1	01.0	12	01.3	09	01.6	02	01.0	-	03	01.7	54			
II	747.7	-02.8	04.2	00.1	00.4	05.3	-03.6	12.2	13	-09.7	10	19	03.1	04	02.2	05	03.2	07	01.7	03	01.3	02	01.5	02	01.0	06	02.5	34		
III	739.1	03.2	15.1	07.9	08.5	16.0	01.3	25.7	31	-06.0	02.01	08	03.6	02	02.0	01	01.0	19	01.9	18	01.7	14	01.9	04	02.0	01	02.0	26		
IV	741.0	07.5	17.3	10.7	11.6	18.8	04.7	28.6	04	-02.6	12	18	03.4	02	02.5	05	01.6	07	02.1	11	02.4	05	04.6	10	03.3	21				
V	740.4	13.8	21.8	15.6	16.6	22.2	10.6	29.0	31	01.6	01	10	03.0	02	01.5	C3	01.3	10	02.0	03	02.0	06	01.5	09	01.6	11	02.1	41		
VI	740.4	16.3	23.2	17.6	18.7	24.3	13.5	31.8	02	08.0	07	11	03.6	01	02.0	06	02.0	07	01.9	11	01.6	06	01.5	09	02.2	12	02.6	31		
VII	741.0	17.3	25.8	18.8	20.2	27.1	13.5	34.2	19	07.5	27	16	02.6	-	-	04	01.8	01	01.0	08	01.8	04	01.8	06	01.8	09	02.1	51		
VIII	741.9	16.2	24.8	18.3	19.4	24.1	13.5	30.7	18	08.7	14	20	02.7	01	01.0	03	01.3	02	02.0	11	02.1	03	02.3	22	02.3	42				
IX	745.4	12.6	26.0	16.6	18.0	26.6	10.5	36.2	16	04.4	11	08	02.1	03	02.0	02	01.5	04	01.5	06	01.5	04	01.5	06	01.5	04	02.2	34		
X	745.7	07.2	16.5	10.6	11.7	09.5	05.6	28.4	C1	-02.0	21	15	02.5	02	01.5	02	01.0	01	01.0	04	01.8	03	01.7	02	02.5	04	01.8	60		
XI	745.2	01.4	07.4	03.4	03.6	08.7	-00.3	20.7	18	-18.6	27	11	02.0	02	01.0	C8	02.2	04	01.8	04	02.0	01	01.0	01	01.0	02	01.0	57		
XII	748.0	-00.4	04.2	00.0	01.2	05.6	-01.5	14.0	16	-05.6	25	16	03.1	01	01.0	C4	01.0	14	01.8	03	01.3	05	01.6	04	01.5	04	01.5	49		
600.	-	07.4	15.7	06.5	10.2	14.5	02.0	35.2	19W	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 43^{\circ}34' N \lambda = 22^{\circ}16' E$ Gr. $\Delta G = + 1h\ 29\ min.$																														
I	-	-01.0	04.7	00.4	01.1	05.6	-02.2	16.6	07	-08.6	28	05	02.6	C5	02.6	C4	01.8	C3	02.0	C7	02.7	57	02.2	03	02.3	04	02.8	01		
II	-	-02.3	04.9	00.4	00.6	05.6	-04.5	15.0	13	-11.6	19	03	02.7	17	02.8	C4	03.2	C2	03.0	47	02.8	05	03.2	02	04.5	-	-	-		
III	-	03.7	13.6	07.0	07.7	14.8	01.6	29.9	31	-05.1	01	03	02.7	28	02.9	C6	03.0	C1	03.0	44	02.3	04	02.5	02	02.5	-	-	-		
IV	-	08.2	17.4	10.4	11.6	18.6	04.5	28.0	C8	-00.6	12	02	01.5	21	02.7	C1	04.0	01	03.0	45	02.6	42	03.9	30	03.5	-	-	-		
V	-	14.3	22.1	15.4	17.0	23.3	10.5	26.2	23	01.0	01	-	-	14	C2.3	10	02.9	C1	C3.0	C7	02.1	54	02.1	02	02.0	05	03.0	-	-	-
VI	-	17.0	23.8	16.0	19.2	25.2	13.2	31.3	16	07.3	07	01	02.0	13	02.0	C														

Meseč	Oblačnost Rm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																									
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. Min.			Tn	Tx	Tn	Tx	Tn	F(0-12)	Rm(0-10)	R mm	•	*	*	*	Δ	Δ	Δ	Δ	Δ	R	T	≡	□					
		mm	mm	mm		-20.0	0.0	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	20.0	9	△	△	△	△	△	△	△	△	△	△	△	△						
SEKCIJE NAJVIŠE VLAŽNOSTI																																					
BR. ST. 206																																					
I	5.7	3.6	6.4	5.2	-	-	-	-	-	006	C03.5	25	.	04	27	.	.	.	08	09	03	03	.	03	C2	02	.	.	.	19	01						
II	7.1	5.6	7.6	6.8	-	-	-	-	-	011	C05.6	27	02	02	25	.	.	.	01	.	03	19	07	03	.	01	04	.	.	.	05	03					
III	-	-	-	-	-	-	-	-	-	045	C18.0	19	-	-	-	-	-	03	-	-	07	06	02	04	03	03	01	02				
IV	-	-	-	-	-	06.2	75	46	61	60	07	-	-	-	01	02	.	.	02	01	-	-	-	-	-	-	-	-	-	-	11	-					
V	-	-	-	-	-	10.6	93	62	80	78	27	-	-	-	07	03	15				
VI	-	-	-	-	-	12.0	88	63	80	77	39	068	C14.3	23	.	.	.	14	02	.	.	01	-	14	12	02	14	01	08				
VII	-	-	-	-	-	12.4	85	55	77	74	-	043	C15.1	19	.	.	.	24	05	08	06	01	07	01	02	12			
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
NIS																																					
BR. ST. 207																																					
I	6.2	5.2	4.1	5.2	112.4	04.0	89	48	88	81	38	013	C04.5	09	.	02	25	.	.	01	.	08	11	11	04	.	06	07	01	01	.	.	03	07			
II	5.5	5.7	4.6	5.3	122.4	03.4	82	55	73	70	29	007	C02.3	04	.	.	23	.	.	02	.	07	10	09	03	.	C5	07	01	.	.	.	02	.			
III	6.2	6.9	5.2	6.1	158.5	05.3	82	41	62	62	19	070	C02.4	22	.	.	07	01	.	02	.	03	10	11	08	03	10	05	02	.	.	.	02	04			
IV	6.0	5.8	5.0	5.6	196.0	06.1	75	43	67	62	18	037	C017.9	27	.	.	01	03	.	07	.	06	09	11	07	01	11			
V	5.3	6.3	5.9	5.8	223.7	10.9	86	35	83	75	34	126	C031.6	27	.	.	.	13	.	.	02	09	21	15	06	21	01	19	.				
VI	6.8	6.1	5.4	6.2	208.7	12.5	85	62	84	77	36	125	C038.2	14	.	.	.	17	05	.	01	.	01	09	17	12	04	17	.	.	.	01	03	13	.		
VII	3.9	4.2	3.8	4.0	297.8	12.5	81	49	77	69	30	014	C055.9	13	.	.	.	23	08	.	03	.	07	02	06	05	06	08	.				
VIII	5.7	6.1	5.5	5.7	202.1	13.2	89	56	84	74	32	062	C016.1	29	.	.	.	21	04	.	03	.	04	08	17	11	02	17	14	01	.		
IX	3.3	3.2	1.4	2.6	245.7	11.4	92	47	79	72	32	013	C004.1	13	.	.	.	24	02	.	03	.	12	02	07	03	04	05	01	.			
X	7.9	5.7	4.7	6.1	142.2	07.7	88	57	81	75	36	059	C019.8	12	.	.	01	02	.	03	.	04	10	13	11	01	13	02	04	.			
XI	8.1	7.5	6.6	7.4	057.2	05.3	85	66	81	77	44	057	C055.6	20	02	04	08	.	.	02	.	04	18	14	11	07	04	06	.	.	.	02	08	.			
XII	7.0	5.6	6.3	6.3	081.2	04.4	87	70	85	81	46	007	C003.4	07	.	01	21	.	.	02	.	03	12	07	02	04	02	04	.				
GOD.	6.0	5.7	4.9	5.5	2048.1	08.1	85	35	78	73	18	590	C038.2	KLVM	-	02	07	103	18	.	22	.	39	108	143	92	17	127	29	04	01	.	01	04	61	15	24
LESKEVAC																																					
BR. ST. 208																																					
I	6.2	5.5	4.4	5.4	-	04.1	93	75	91	87	52	012	C005.5	09	.	04	26	.	.	04	02	08	11	10	04	.	06	03	01	01	.	.	07	16			
II	6.1	5.3	4.8	5.4	-	03.7	91	62	80	78	32	006	C01.8	15	.	.	26	.	.	03	.	06	10	08	02	.	04	06	01	01	.	.	01	04			
III	5.9	6.0	5.2	5.9	-	05.9	87	45	72	68	20	046	C14.4	22	.	.	09	01	.	04	01	05	09	11	07	02	09	03	03	.	.	02	.	04			
IV	6.4	6.3	4.0	5.5	-	06.5	83	46	69	64	22	038	C013.5	27	.	.	02	04	.	12	.	04	08	11	01	01	.	.	.	01	01	.	.				
V	6.6	7.0	5.7	6.6	-	11.1	91	57	85	78	34	095	C017.4	25	.	.	11	.	.	01	.	02	10	21	12	03	21	.	.	.	01	14	07				
VI	7.1	6.1	7.0	6.7	-	12.9	90	62	86	79	41	153	C033.2	21	.	.	17	03	.	06	.	01	11	17	13	05	17	.	.	.	01	11	04	.			
VII	4.6	5.1	3.7	4.5	-	13.4	89	53	83	75	36	028	C011.5	06	.	.	23	06	.	03	.	06	C3	07	07	01	07	.	.	.	01	10	09				
VIII	7.1	6.3	5.5	6.3	-	13.4	94	58	87	80	41	092	C025.9	29	.	.	20	04	.	04	.	01	08	14	11	02	14	.	.	.	01	20	19	.			
IX	3.6	3.6	2.4	3.2	-	11.5	97	47	84	76	29	013	C008.0	13	.	.	25	01	.	02	.	12	02	07	03	04	05	19	.				
X	7.2	6.0	4.8	6.0	-</td																																

Mjesec	Vrastunski pritisak Pa	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, Fm (0-12)																							
		TM					NIN					Dat.		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)							Dat.		Min		Dat.	C.	J.	C.	J.	C.	J.	C.	J.	C.	J.	C.	J.	C.						
$\varphi = 43^{\circ}04' N \lambda = 22^{\circ}26' E$ Gr.ΔG = + 1h 29 min.																									ESTERIŠICA		BR. ST. 211								
I	-	-03.2	04.4	-01.2	-00.3	05.2	-04.4	12.0	19.18	-05.4	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
II	-	-03.8	03.3	-01.4	-00.8	04.3	-04.6	12.0	07	-11.6	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
III	-	02.1	13.9	06.4	07.2	14.8	06.9	25.0	31	-05.0	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV	-	06.8	16.3	09.2	10.4	17.6	04.3	27.6	07	-02.7	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
V	-	12.4	20.6	13.7	15.1	21.9	09.4	28.8	31	00.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	15.2	21.9	15.7	17.1	22.2	12.1	31.0	02	07.2	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VII	-	16.0	25.0	17.1	16.8	25.9	12.9	33.8	19	08.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	15.3	23.2	16.4	17.8	25.1	13.0	29.5	24	06.0	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	11.0	25.3	14.6	16.5	25.9	10.0	30.0	16	05.4	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	06.6	15.6	08.4	09.9	16.2	02.5	27.0	01	-01.8	31	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	01.4	07.1	02.8	03.5	08.0	-00.1	18.4	19	-16.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	-01.2	04.2	-00.1	00.7	05.0	-02.8	11.1	18	-07.0	24,10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
600.	-	06.6	15.1	08.5	09.7	16.1	04.7	33.8	19M	-16.0	27.XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
$\varphi = 43^{\circ}09' N \lambda = 22^{\circ}36' E$ Gr.ΔG = + 1h 29 min.																									PIRKT		BR. ST. 212								
I	-	-01.7	04.4	-00.5	00.5	05.2	-03.5	13.3	19	-08.0	11	05	C1.4	-	-	01	01.0	C1	01.0	04	01.2	-	-	04	02.0	20	01.7	58							
II	-	-02.6	03.7	-00.8	-00.2	04.6	-C4.3	12.5	13	-16.0	10	16	C1.4	-	-	05	01.2	02	01.5	02	01.0	-	-	02	01.0	12	01.7	45							
III	-	04.4	14.4	07.3	08.3	15.3	01.7	26.0	31	-05.5	02	11	01.6	-	-	02	01.5	25	02.4	-	02	01.0	01	01.0	02	02.0	56								
IV	-	08.3	17.2	10.7	11.7	18.4	04.9	28.0	06	-01.0	12	12	C1.7	-	-	09	01.7	02	02.0	02	02.5	04	02.0	15	02.1	46									
V	-	13.4	21.1	14.9	16.1	22.3	10.2	28.0	31	01.5	01	C8	C1.4	05	01.4	C3	01.0	C3	01.7	-	-	03	01.3	01	01.0	70									
VI	-	15.4	22.5	18.1	24.2	12.7	30.5	16.02	06.5	09	08	C1.4	03	02.0	01	01.0	-	-	01	02.0	01	01.0	-	-	04	01.5	72								
VII	-	16.4	24.6	18.5	19.7	26.0	13.0	33.0	19	05.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	16.4	24.2	18.6	19.6	23.6	13.7	26.5	16.12	08.0	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	13.2	23.6	16.9	18.2	24.3	10.3	30.0	24	04.3	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	07.7	16.1	10.6	17.1	15.6	27.0	02	-01.0	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	03.2	07.6	04.2	04.8	08.7	01.4	19.5	18	-15.5	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	06.4	04.1	06.6	01.6	04.8	-01.4	12.3	18	-06.5	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
600.	-	07.9	15.5	09.9	10.8	16.5	05.4	33.0	19M	-15.5	27.XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
$\varphi = 43^{\circ}20' N \lambda = 22^{\circ}41' E$ Gr.ΔG = + 1h 30 min.																									TCPLI DC		BR. ST. 213								
I	-	-02.8	02.8	-01.1	-00.5	03.7	-04.4	10.0	19.18	-05.2	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
II	-	-04.9	01.2	-02.6	-02.2	02.2	-06.6	05.8	13	-13.5	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
III	-	02.7	11.4	05.7	06.4	12.2	01.5	22.8	31	-08.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV	-	07.0	14.1	08.4	09.5	15.3	04.3	24.8	07.06	-01.2	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
V	-	12.4	17.9	12.4	13.8	19.5	09.1	24.0	31	03.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	14.2	19.0	14.3	15.5	21.0	11.1	29.2	02	08.1	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VII	-	15.3	22.1	15.5	17.1	23.4	11.7	31.0	19	06.2	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	14.8	21.2	15.5	16.7	22.6	12.1	26.4	24.16	06.6	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	12.7	21.7	14.3	15.8	23.0	10.5	26.7	17	03.9	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	06.3	12.8	09.0	09.9	15.9	05.7	24.0	01	-01.6	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	01.4	05.3	02.2	02.8	06.6	-00.2	17.0	18	-12.4	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	-01.7	02.7	-00.3	00.1	03.6	-03.2	10.0	18	-08.6	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
600.	-	06.4	12.7	07.7	08.7	14.0	04.3	31.0	19M	-13.9	09.II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
$\varphi = 43^{\circ}01' N \lambda = 22^{\circ}45' E$ Gr.ΔG = + 1h 29 min.																									CIMITROVGRAE		BR. ST. 214								
I	726.9	-02.6	03.7	-00.7	-00.1	04.3	-03.8	11.4	19.07	-05.4	11	-	-	-	-	67	02.0	34	02.6	-	-	-	-	-	17	01.9	24	03.2	11						
II	727.2	-03.5	03.2	-01.2	-00.7	04.2	-04.6	11.0	13	-12.0	10	-	-	-	-	12	02.2	27	02.1	-	-	08	02.0	24	03.3	18									

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati • Hr	Vlažnost vazduha			Padavine R mm		Broj dana na sat																								
	7	14	21		7	14	21	Min.	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(O-12)	Nm(0-10)	R mm	•	*	*	*	Δ	Δ	Δ	Δ	R	T	III			
	Sred. (Dnes)											≤	<	<	IV	IV	IV	IV	IV	IV	IV	<	>	IV	IV	IV	IV	IV	IV	IV	IV	IV		
BABUŠNICA																																		
BR. ST. 211																																		
I	5.9	5.2	3.2	4.8	-	-	-	-	-	-	C08 C04.5	05	.	04	28	C8	C5	C4	C3	C2	C1	C0	C0	C0	C0	05	10		
II	6.4	5.4	4.3	5.4	-	-	-	-	-	-	016 005.0	15	02	03	26	06	10	07	05	03	02	01	00	00	00	04	04		
III	5.5	5.4	3.9	5.2	-	-	-	-	-	-	053 030.1	22	.	.	12	01	03	07	09	08	01	07	06	00	00	00	02	02		
IV	6.0	6.3	3.1	5.1	-	-	-	-	-	-	025 006.3	17	.	.	02	03	04	06	11	06	01	11	00	00	00	00	00	00		
V	5.9	7.0	4.9	5.9	-	-	-	-	-	-	098 C27.6	03	.	.	07	01	03	11	16	13	02	16	09	02		
VI	6.3	6.2	5.1	5.9	-	-	-	-	-	-	136 C25.0	21	.	.	14	01	02	10	17	14	04	17	15	08		
VII	4.8	5.5	3.2	4.5	-	-	-	-	-	-	025 016.0	23	.	.	22	04	06	05	09	05	01	09	00	00	00	00	08	08		
VIII	6.4	6.6	4.1	5.7	-	-	-	-	-	-	044 008.6	26	.	.	18	01	02	07	14	11	01	14	00	00	00	00	18	05		
IX	4.2	3.8	1.2	3.1	-	-	-	-	-	-	022 007.6	05	.	.	24	01	10	06	05	06	00	06	00	00	00	00	04	04		
X	6.3	5.7	3.8	5.3	-	-	-	-	-	-	079 015.6	12	.	.	04	02	06	07	13	11	02	13	00	00	00	00	03	03		
XI	7.9	7.2	5.0	7.0	-	-	-	-	-	-	078 C20.0	23	04	03	11	01	03	14	12	11	03	08	05	00	00	00	02	07		
XII	6.9	5.5	3.7	5.3	-	-	-	-	-	-	011 010.0	18	.	02	25	01	05	07	04	01	01	03	01	00	00	00	00	04	04	
GOD.	6.0	5.9	3.9	5.3	-	-	-	-	-	-	595 030.1	22.8	06	12	108	91	06	.	01	.	60	93	124	93	14	110	23	01	00	00	00	58	41	23
PIROT																																		
BR. ST. 212																																		
I	6.3	5.9	4.6	5.7	-	04.0	89	71	90	93	42	011 003.2	05	.	01	29	07	12	08	03	02	04	00	00	00	00	06	02		
II	5.6	5.0	4.5	5.0	-	03.8	89	69	86	81	42	027 014.2	17	01	02	26	10	11	08	07	01	03	07	00	00	00	00	01	06	
III	4.7	5.2	2.8	4.2	-	05.5	81	51	72	68	25	054 034.8	22	.	.	10	01	.	.	.	01	01	09	07	09	08	01	07	05	02	00	02		
IV	5.3	6.2	4.1	5.2	-	06.4	75	47	67	63	24	011 003.7	02	.	.	01	03	.	.	.	07	08	07	04	02	07	00	00	00	00	00	00		
V	4.5	5.5	5.8	5.3	-	10.5	86	59	83	76	31	105 025.6	14	.	.	08	00	.	.	.	07	07	17	14	04	17	00	00	00	00	10	02		
VI	4.7	5.4	5.9	5.4	-	12.2	88	63	82	78	36	162 C58.0	04	.	.	18	04	.	.	.	04	10	20	17	05	20	00	00	00	00	01	08	01	
VII	3.9	3.9	3.0	3.6	-	-	-	-	-	-	042 021.4	06	.	.	21	04	.	.	.	11	03	07	05	01	07	00	00	00	00	01	04	01		
VIII	7.0	6.1	6.3	6.5	-	-	-	-	-	-	064 023.0	29	.	.	30	01	.	.	.	01	11	13	13	02	19	00	00	00	00	04	02			
IX	2.7	3.2	2.7	2.9	-	-	-	-	-	-	013 005.2	13	.	.	24	01	.	.	.	14	02	06	04	00	06	00	00	00	00	01	02			
X	6.6	5.4	5.4	5.8	-	-	-	-	-	-	097 016.8	18	.	.	02	02	.	.	.	04	10	10	10	04	10	00	00	00	00	03	03			
XI	8.3	5.7	6.8	7.0	-	-	-	-	-	-	056 016.3	20	03	02	10	01	.	.	.	13	13	09	02	10	04	00	00	00	00	02	07			
XII	6.7	6.4	6.3	7.1	-	-	-	-	-	-	012 006.2	18	.	02	20	01	.	.	.	09	05	03	09	01	01	00	00	00	00	03	03			
GOD.	5.7	5.3	4.8	5.3	-	-	-	-	-	-	654 058.0	04.8	04	07	98	98	09	.	01	01	78	103	123	97	20	112	21	02	00	02	31	23	17	
TCPCLIĆ																																		
BR. ST. 213																																		
I	6.0	5.4	4.4	5.3	-	-	-	-	-	-	032 014.4	29	.	04	31	10	13	10	03	02	03	04	00	00	00	00	00	02	17	
II	6.3	5.5	5.5	5.8	-	-	-	-	-	-	030 016.7	17	03	10	27	05	10	09	05	01	02	07	00	00	00	00	00	22		
III	6.3	6.3	4.6	5.9	-	-	-	-	-	-	046 018.6	22	.	.	09	01	.	.	.	03	08	09	07	01	06	05	02	00	00	00	03			
IV	6.5	6.8	4.2	5.8	-	-	-	-	-	-	026 007.8	02	.	01	01	01	.	.	.	05	10	11	08	01	11	00	00	00	00	00	00			
V	6.0	8.0	5.8	6.6	-	-	-	-	-	-	120 029.7	10	.	.	04	01	.	.	.	02	11	22	16	04	22	00	00	00	00	00	00			
VI	6.3	6.1	6.7	7.0	-	-	-	-	-	-	150 028.2	26	.	.	05	01	.	.	.	01	13	22	20	06	22	00	00	00	00	00	00			
VII	4.2	4.2	3.1	4.5	-	-	-	-	-	-	080 022.0	07	.	.	04	01	.	.	.	05	02	12	10	04	12	00	00	00	00	01	09			
VIII	5.6	6.4	6.3	6.2	-	-	-	-	-	-	-	-	.	.	04	01	01	01	01	02	11	-	-	-	-	-	-	-	-	-	00	00		
IX	2.9	3.0	2.5	3.5	-	-	-	-	-	-	032 013.2	14	.	.	03	04	.	.	.	10	01	11	06	01	11	00	00	00	00	00	02			
X	6.9	5.7	5.2	5.9	-	-	-	-	-	-	124 026.2	18	.																					

Meseč Broj	Vrednost pritiska Pa	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, fm (0-12)															
		Tm					N	NE	E	SE	S	SW	W	NW	C												
		7	14	21	Sred. (Dnev.)	N	NE	E	SE	S	SW	W	NW	C													
$\varphi = 42^{\circ}26' N \lambda = 20^{\circ}21' E$ Gr. AG = + 1h 22 min.																											
I	-	-03.3	02.3	-02.0	-01.2	03.1	-04.2	11.5	07 -08.8	11	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	-02.4	04.5	00.1	00.6	-03.5	10.8	11 -11.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	03.3	13.0	07.3	07.7	14.2	01.6	21.6	31 -05.4	01	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	07.5	16.4	09.5	10.9	18.0	04.8	26.2	07 -01.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	13.9	21.8	15.2	16.5	22.5	05.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	17.4	25.0	17.9	19.7	27.1	12.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	17.0	26.3	16.4	20.0	27.0	13.3	33.8	19 07.5	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	17.2	25.6	18.6	20.1	27.2	-	32.5	17 -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	14.2	26.8	17.2	18.9	27.7	10.8	32.0	17.16	06.0	11	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	07.6	16.2	09.7	10.8	17.0	05.7	28.4	01 -06.2	21.30	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	02.8	07.7	04.6	05.1	09.2	01.2	21.2	18 -09.5	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-01.0	04.1	00.6	01.0	04.8	-01.9	13.0	18 -07.5	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	07.8	15.5	09.8	10.8	17.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}47' N \lambda = 20^{\circ}30' E$ Gr. AG = + 1h 22 min.																											
I	-	-01.9	03.1	-CC.8	-00.4	03.5	-03.4	10.4	07 -06.8	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	-02.3	04.8	00.4	00.8	05.6	-03.5	10.0	15 -09.8	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	04.3	13.7	08.1	08.5	14.3	03.0	23.2	31 -04.6	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	08.2	16.5	11.3	11.8	17.4	06.0	26.0	07 00.2	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	13.5	21.6	14.7	16.1	22.6	10.2	27.0	20 05.6	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	16.2	23.5	17.0	18.4	24.5	12.7	30.4	02 08.2	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	17.9	25.8	18.9	20.3	26.8	14.1	33.0	19 09.6	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	16.4	24.9	18.6	19.6	25.5	13.6	30.0	16 10.1	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	14.2	25.5	16.5	18.4	26.4	11.5	31.5	17 08.0	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	07.9	16.4	10.7	11.5	17.2	06.5	28.4	01 01.0	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	04.2	08.1	05.3	05.7	09.5	02.8	18.6	18 -07.6	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-00.6	04.4	00.9	01.3	05.3	-01.7	13.5	18 -06.5	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	08.0	15.7	10.2	11.0	16.6	06.1	33.0	19.VII -09.8	40.II	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 42^{\circ}38' N \lambda = 20^{\circ}34' E$ Gr. AG = + 1h 22 min.																											
I	-	-03.8	02.9	-01.2	-01.1	04.2	-04.5	12.0	07 -05.6	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-03.6	04.9	-00.5	00.1	02.9	01.1	-06.5	11.5	12 -11.8	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	02.5	14.5	C7.2	07.9	15.9	00.8	24.3	31 -08.2	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	07.2	17.1	10.4	11.3	18.5	04.6	27.5	07 -01.8	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	12.2	22.5	15.1	16.2	23.5	05.4	28.5	31.23	03.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	15.3	24.7	17.7	18.9	26.0	12.5	32.0	02 08.9	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	18.3	27.0	19.5	21.1	28.7	13.5	37.0	19 05.1	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	16.0	25.7	18.5	19.7	27.1	13.6	32.7	17 05.7	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	12.9	26.6	17.2	18.5	27.6	10.7	31.5	17.16	05.8	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	06.9	16.5	09.7	10.7	17.7	05.5	26.3	01 -01.8	31	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	02.9	08.4	04.6	05.1	09.5	01.6	26.5	18 -08.2	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-01.6	04.2	00.4	00.9	05.5	-02.5	13.5	18 -08.2	22.21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	07.1	16.2	09.8	10.8	17.6	05.1	37.0	19.VII -11.8	40.II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}04' N \lambda = 20^{\circ}39' E$ Gr. AG = + 1h 23 min.																											
I	-	-02.1	03.5	-01.4	-00.5	04.6	-04.3	11.0	15.06 -12.1	10	27	C1.9	C3	C2.7	21	C1.3	22	C1.8	12	C2.0	04	02.5	01	01.0	.03		
II	-	-04.7	-00.1	-03.4	-02.9	01.1	-06.5	10.1	07 -14.1	09	37	C3.0	06	C2.2	21	C1.4	06	C2.3	C6	C1.8	03	C2.0	.02	04.0	03		
III	-	02.7	C8.7	04.4	05.0	10.1	00.5	26.0	31 -07.0	26	13	C2.8	02	C2.5	27	C1.3	18	C3.2	19	C3.0	05	C4.6	03	C3.3	03	C2.3	03
IV	-	05.7	11.2	07.0	07.5	12.8	03.1	23.1	07 -01.0	28.27	26	C3.1	07	C2.0	09	C1.1	14	C2.6	10	C3.0	16	C3.4	02	C2.5	03	C3.0	03
V	-	10.7	21.2	11.2	12.3	17.3	07.7	24.0	30 03.1	10	11	C2.6	C6	C2.7	21	C1.2	16	C1.2	C6	C1.7	11	C3.6	01	01.0	09	C2.9	08
VI	-	13.2	21.3	13.5	14.5	21.5	05.6	27.2	30 03.0	06	23	C2.5	05	C2.0	25	C1.1	09	C2.2	C3	C1.4	09	C2.0	02	03.2	10	C3.2	07
VII	-	14.5	20.2	14.6	16.1	22.0	10.5	31.1	19 07.1	03	16	C2.4	C6	C2.0	34	C1.4	01	C1.0	04	C1.2	04	C3.0	04	C3.0	04	C3.1	08
VIII	-	13.4	19.3	14.1	15.2	21.6	10.0	24.1	18.16 07.0	05	31	C2.5	C7	C2.4	28	C1.4	05	C1.2	C5	C3.0	05	C3.0	04	C2.8	11	C3.0	02
IX	-	12.2	20.5	13.8	15.1	21.6	10.2	26.0	16 05.1	11	17	C2.5	C5	C1.8	31	C1.2	06	C1.0	C7	C1.4	03	C2.7	06	C2.7	07	C2.3	07
X	-	06.1	11.3	07.2	08.0	12.7	04.7	23.0	01 C0.1 27.65	32	24	C2.6	04	C1.5	20	C1.0	08	C1.9	17	C2.2	C2	C3.5	01	C3.0	04	C3.0	05
XI	-	01.1	C4.5	C1.8	02.3	04.2	-00.5	17.0	18 -11.1	26.25	33	C2.1	C6	C1.2	23	C1.2	07	C3.4	07	C2.1	05	C5.2	.05	C3.2	06	C2.0	06
XII	-	-01.8	C2.5	-00.1	C4.2	C1.1	12.1	18 -11.0	08	35	C2.4	12	C2.5	17	C1.2	11	C1.8	C5	C1.8	05	C2.0	.05	C2.0	.05	C3.3	05	
GOD.	-	C5.6	11.3	C6.6	C7.7	12.6	C3.4	31.1	19.VII -14.1	09.II	30.1	C2.6	69	C2.2	215	C1.2	126	C2.0	C17	02.3	61	C3.3	23	C2.7	66	C2.9	63
$\varphi = 42^{\circ$																											

Mesec 2	Oblačnost Nm (0-10)				Insektacija broj sati (tides.)	Vlažnost vazduha			Padavine R mm			Broj dana n sa:																				
							m	t				Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	□	■			
	7	14	21	Sred. (tides.)		mm	mm	mm	Sred. Min.	Max	Dat.	≤	<	<	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV				
SKIVJANE-CJAKOVICA																																
BR. ST. 216																																
I 6.5 5.7 4.8 5.7	-	-	-	-	-	-	-	-	-	C18 C12.0	25	.	09	25	.	.	.	-	09	14	03	03	01	03	01	-	.	12	01			
II 4.7 4.4 4.0 4.4	-	-	-	-	-	-	-	-	-	C16 C05.5	21	02	.	24	.	.	.	-	10	C7	G6	04	.	03	04		
III 5.2 6.0 4.1 5.1	-	-	-	-	-	-	-	-	-	031 C12.5	25	.	.	12	.	.	.	-	05	06	10	06	01	05	04	01	.	.	01	02		
IV 4.9 4.7 3.4 4.3	-	-	-	-	-	-	-	-	-	056 C24.0	02	.	.	03	02	.	.	-	01	09	06	12	10	01	12	01		
V 4.7 5.2 4.5 4.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.	03	.				
VI 4.0 5.5 4.4 4.6	-	-	-	-	-	-	-	-	-	036 C12.8	24	-	-	-	-	-	-	-	-	06	06	02	04	01	03	.		
VII 3.3 3.9 3.3 3.5	-	-	-	-	-	-	-	-	-	015 C06.0	12	-	-	24	06	-	-	-	11	02	07	05	.	07	.	.	.	03	.			
VIII 4.2 4.2 3.5 4.0	-	-	-	-	-	-	-	-	-	024 O04.8	08	-	-	24	05	-	-	-	09	02	09	09	.	09	.	.	.	05	.			
IX 4.6 4.8 4.3 4.6	-	-	-	-	-	-	-	-	-	012 C11.0	13	-	-	02	26	06	-	-	04	.	02	01	01	02	03	.		
X 5.4 5.3 5.6 5.4	-	-	-	-	-	-	-	-	-	134 O40.0	19	-	-	02	04	-	-	-	06	09	14	14	04	14	.	.	.	04	01			
XI 8.7 8.1 8.1 8.3	-	-	-	-	-	-	-	-	-	102 O24.5	17	-	-	01	09	-	-	-	01	23	10	10	03	08	03	01	.	01	09			
XII 8.4 9.6 5.9 6.6	-	-	-	-	-	-	-	-	-	054 O41.0	18	-	-	01	19	-	-	-	02	13	04	04	01	03	02	.	.	01	09			
GOD. 5.4 5.3 4.7 5.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.	01	27					
ISTEK																																
BR. ST. 217																																
I 6.5 5.6 4.8 5.6	-	-	-	-	-	-	-	-	-	014 O07.4	09	.	07	29	.	.	.	03	.	05	11	04	04	.	03	01	.	.	13			
II 5.4 4.6 3.6 4.6	-	-	-	-	-	-	-	-	-	003 O01.8	15	-	-	27	.	.	.	03	.	09	04	04	01	.	03	03	02	.	04			
III 4.8 5.6 3.5 4.6	-	-	-	-	-	-	-	-	-	038 O12.8	15	-	-	05	.	.	.	01	.	05	04	08	07	02	07	03	02	.	03			
IV 4.9 5.3 4.0 4.7	-	-	-	-	-	-	-	-	-	034 O21.4	02	-	-	02	.	.	.	04	.	05	03	07	09	01	07			
V 5.1 5.5 4.5 5.0	-	-	-	-	-	-	-	-	-	053 O13.8	14	-	-	10	.	.	.	02	03	13	13	01	13	.	.	.	02	01				
VI 5.0 5.7 5.2 5.3	-	-	-	-	-	-	-	-	-	067 C28.8	19	-	-	17	02	.	.	01	.	04	03	10	09	03	10	.	.	01	02			
VII 4.4 5.1 4.0 4.5	-	-	-	-	-	-	-	-	-	031 C12.8	13	-	-	23	04	.	.	03	02	06	06	01	06	.	.	.	01	01				
VIII 5.0 5.3 4.6 5.0	-	-	-	-	-	-	-	-	-	030	-	-	-	21	01	.	.	05	02	-	-					
IX 2.7 3.6 1.4 2.6	-	-	-	-	-	-	-	-	-	022 O15.2	13	-	-	23	03	-	-	14	.	03	02	01	03	01	02			
X 5.2 5.1 4.2 4.8	-	-	-	-	-	-	-	-	-	112 O25.4	19	-	-	03	.	.	.	02	.	07	06	11	11	03	11	.	.	.	02	07		
XI 7.7 7.2 7.0 7.3	-	-	-	-	-	-	-	-	-	045 O05.8	15	-	-	07	.	.	.	03	13	09	08	05	03	.				
XII 6.6 6.2 5.5 6.1	-	-	-	-	-	-	-	-	-	039 O35.0	18	-	-	21	.	.	.	04	12	03	03	01	02	01	.	.	.	12	01			
GOD. 5.3 5.4 4.4 5.0	-	-	-	-	-	-	-	-	-	482	-	.	07	93	94	32	-	-	48	63	-	-	-	-	-	.	03	-	43			
KLINA																																
BR. ST. 218																																
I 6.6 6.4 4.7 5.9	-	-	-	-	-	-	-	-	-	012 C07.4	25	.	06	29	.	.	.	-	07	12	05	02	.	03	02	01	.	.	12			
II 5.5 4.8 4.9 5.1	-	-	-	-	-	-	-	-	-	004 C11.6	15	03	.	27	.	.	.	02	.	08	G6	02	.	04	04	02	.	.	01			
III 5.9 7.1 3.8 5.6	-	-	-	-	-	-	-	-	-	038 O15.2	22	-	-	14	.	.	.	04	.	03	08	08	06	01	08	04	04	.	02			
IV 5.1 6.0 4.1 5.1	-	-	-	-	-	-	-	-	-	046 C22.3	02	-	-	04	02	.	.	05	.	08	08	11	04	01	11	.	.	01				
V 5.6 6.7 6.0 6.1	-	-	-	-	-	-	-	-	-	040 C05.0	14	-	-	15	.	.	.	02	01	08	17	12	.	.	02	07	02					
VI 5.4 6.2 5.6 5.8	-	-	-	-	-	-	-	-	-	060 C37.0	05	-	-	22	04	.	.	06	.	04	08	12	04	01	12	.	.	09				
VII 4.0 5.9 4.2 4.7	-	-	-	-	-	-	-	-	-	018 O08.2	31	-	-	26	10	01	07	03	10	04	.	10	.	.	07	01						
VIII 5.0 6.1 4.7 5.3	-	-	-	-	-	-	-	-	-	048 C15.3	28	-	-	24	05	.	01	.	05	05	10	07	01	10	.	.	04	01				
IX 2.7 3.7 2.2 2.8	-	-	-	-	-	-	-	-	-	016 C16.3	13	-	-	26	04	-	-	15	01	01	01	01	01	01	.	.	02	02				
X 6.0 5.8 4.6 5.5	-	-	-	-	-	-	-	-	-	143 C35.5	15	-	-	06	04	.	.	02	10	13	11	06	13	.	.	05	03					
XI 7.8 7.4 7.4 7.6	-	-	-	-	-	-	-	-	-	073 C15.2	17	-	-	09	.	.	.	02	04	20	11	09	04	10	01	.	.	01	03			
XII 7.9 5.4 5.7 6.2	-	-	-	-	-	-	-	-	-	042 C37.1	18	-	-	01	20	.	.	-	04	12	04	03	01	02	02	.	.	01	05			
GOD. 5.6 6.0 4.8 5.5	-	-	-	-	-	-	-	-	-	540 C37.1	18	XII	03	07	111	119	25	01	-	-	72	103	108	69	16	101	13	07	.	02	41	38
DRAGAS																																
BR. ST. 219																																
I 4.6 3.6 3.6 3.5	-	-	-	-	-	-	-	-	-	039 C12.7	02	04	06	25	.	.	.	02	.	14	04	07	07	02	01	07	.	.	03	31		
II 6.1 5.1 6.1 5.8	-	03.0	79	74	79	77	23	-	-	012 C03.4	17	06	13	24	.	.	.	04	.	13	07	09	C4	06	03	.	.	.	20			
III 5.0 7.5 5.4 6.0	-	04.2	75	55	69	64	22	-	-	030 O11.8	25	-	-	11	.	.	.	04	.	05	11	08	06	01	06	05	02	.	01	01	09	
IV 5.8 5.7 5.0 5.5	-	04.7	66	53	66	62	22	-	-	081 C18.2	27	-	-	05	.	.	.	C2	01	06	12	12	11	04	01	02	.	.	03			
V 6.4 7.0 5.6 6.3	-	07.5	81	60	77	73	35	-	-	116 C23.5	03	-	-	05	.	.	.	02	05	19	14	04	15	.	.	01	04	.	.			
VI 4.3 7.1 6.2 5.8	-	09.3	78	64	79	73	33	-	-	074 C16.7	04	-	-	05	.	.	.	02	08	13	11	04										

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																							
					U m t			e m			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	R	•						
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. Min.	Σ	Max	Dat.	<=	<	<	IV	IV	IV	IV	IV	<	>	IV	IV	IV	IV	T	•						
KCSCVSKA MITREVICA																																		
BR. ST. 221																																		
I	7.1	5.0	4.4	5.5	-	-	-	-	-	005	004.3	05	.	04	29	.	.	.	05	C8	03.01	.	02	03	01	.	.	09	02					
II	7.0	5.1	5.6	5.9	-	-	-	-	-	003	002.4	04	.	01	24	.	.	.	05	C9	03.01	.	01	03	.	.	.	02	.					
III	5.7	5.4	4.4	5.2	-	-	-	-	-	040	020.3	15	.	.	13	.	.	.	06	C7	06.04	01	06	04	01	.	.	01	-					
IV	6.1	5.4	4.1	5.2	-	-	-	-	-	034	021.4	02	.	.	03	01	.	01	07	C10	10.05	01	1C	01	.	.	01	01	.					
V	6.8	6.4	6.0	6.4	-	-	-	-	-	040	005.1	26	.	.	06	.	.	.	02	C10	15.10	.	15	05	02					
VI	5.9	5.9	6.5	6.1	-	09.6	100	64	81	82	035	013.3	20	.	.	16	01	.	.	03	C11	15.08	01	15	.	.	.	03	01					
VII	4.9	4.6	4.8	4.8	-	-	-	-	-	051	023.1	31	.	.	21	06	.	.	08	C9	10.06	01	12	01	06	.	.	01	03					
VIII	5.8	6.3	6.6	6.3	-	-	-	-	-	053	012.1	29	.	.	16	.	.	.	05	C12	12.08	63	12	.	.	.	01	03						
IX	5.0	2.5	3.0	3.7	-	-	-	-	-	-	-	-	.	.	-	-	-	-	-	-	-	-	-	-	-	-	.							
X	6.7	5.1	4.8	5.5	-	-	-	-	-	109	020.4	12	.	.	03	03	.	.	06	C12	14.11	05	14	.	.	.	02	01						
XI	9.2	7.5	7.4	8.0	-	05.8	92	78	80	86	44	055	010.2	14	01	03	10	.	.	02	C23	14.12	01	12	04	01	.	.	01	07				
XII	8.5	5.4	5.2	6.3	-	-	-	-	-	030	028.1	18	.	.	23	.	.	.	01	C10	03.01	01	03	02	01	.	.	05	.					
GOD.	6.6	5.4	5.2	5.7	-	-	-	-	-	-	-	-	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-							
PRISTINA																																		
BR. ST. 222																																		
I	6.6	5.2	4.2	5.3	098.0	03.6	90	79	80	87	48	017	009.5	09	.	06	29	.	.	07	06	08	13	04	.	03	04	01	.	13	06			
II	4.9	4.9	4.4	4.7	133.8	03.3	85	63	70	75	35	011	005.5	15	02	01	27	.	.	07	08	07	07	03	.	03	C5	01	.	04	.			
III	5.3	7.5	3.7	5.5	171.1	05.0	82	47	72	67	24	049	021.5	15	.	.	12	.	.	12	04	07	07	06	02	05	04	01	.	03	04			
IV	6.0	6.1	3.9	5.3	193.4	05.6	74	45	63	61	24	053	017.7	02	.	.	01	.	.	14	02	08	09	12	09	01	12	01	.	01	01			
V	5.8	7.2	5.3	6.1	204.6	05.3	87	55	75	72	31	066	017.6	03	.	.	04	.	.	C3	02	08	15	13	01	15	.	.	01	11	02			
VI	5.3	6.2	6.0	5.8	226.0	11.0	84	55	77	73	36	051	027.1	14	.	.	14	.	.	04	02	08	18	11	02	18	.	.	01	16	03			
VII	4.1	5.1	3.7	4.3	287.0	11.4	83	51	74	69	32	035	010.0	11	.	.	17	03	.	05	10	03	09	06	02	05	.	.	01	12	01			
VIII	6.0	5.7	4.2	5.3	224.8	11.1	87	51	73	71	33	031	011.4	08	.	.	16	.	.	01	04	04	15	06	01	15	.	.	01	10	04			
IX	2.8	3.7	1.5	2.7	255.5	10.2	89	44	73	69	26	022	017.2	13	.	.	18	01	.	01	15	02	07	03	01	07	.	.	06	02				
X	5.8	5.5	4.7	5.3	159.6	07.1	91	56	81	76	31	101	024.6	14	.	.	04	02	.	05	02	07	08	13	16	09	13	.	02	04				
XI	6.4	7.7	6.0	7.6	062.6	05.2	86	73	83	81	43	065	010.5	20	02	05	08	00	.	05	01	02	19	17	12	01	12	07	.					
XII	7.7	5.6	5.2	6.2	082.8	04.2	91	79	82	87	55	023	023.4	18	.	03	24	.	.	03	04	11	05	02	01	03	02	01	.	01	11			
GOD.	5.7	5.9	4.5	5.3	2099.4	07.2	85	58	77	73	24	567	027.1	14.VI	04	15	105	71	04	.	47	03	72	54	138	05	17	115	27	03	.	04	45	22
URCSEVAC																																		
BR. ST. 223																																		
I	7.7	4.3	2.6	4.8	113.7	03.2	87	73	88	83	52	025	012.2	05	11	03	30	.	.	.	05	C4	05.03	01	02	05	.	.	.	11	31			
II	5.2	3.3	3.6	4.7	127.2	03.4	88	70	84	81	48	017	009.3	21	02	03	27	.	.	.	08	C7	10.09	04	08	11				
III	5.9	6.3	2.4	4.7	159.4	05.5	87	56	70	74	31	041	016.6	22	.	.	11	.	.	02	05	04	07	07	02	05	04	.	04	.				
IV	6.0	5.4	3.5	5.0	205.0	04.0	91	77	51	69	25	086	016.0	02	.	.	01	.	.	04	02	07	08	13	12	05	13	.	.	.				
V	6.1	6.2	3.5	5.3	197.5	09.8	88	60	82	77	36	072	012.3	03	.	.	03	.	.	04	C5	20.15	01	26	.	.	.	01	07	.				
VI	5.6	5.6	5.4	5.6	217.7	11.8	89	65	85	80	44	286	032.0	20	.	.	16	.	.	04	07	19	14	05	19	.	.	01	11	01				
VII	5.0	5.3	2.0	4.1	256.9	12.2	87	56	84	75	37	031	014.5	07	.	.	17	03	.	08	04	07	05	01	07	.	.	03	.					
VIII	6.5	3.9	4.1	4.8	220.0	12.0	91	61	84	75	33	083	029.6	29	.	.	13	.	.	06	07	16	11	02	14	.	.	01	07	01				
IX	3.0	3.3	0.6	2.3	267.0	10.9	93	48	89	77	21	012	005.2	13	.	.	17	.	.	14	05	03	03	05	03	.	.	03	.					
X	6.2	5.6	4.2	5.3	157.0	07.5	96	63	86	82	35	146	043.2	14	.	.	01	02	.	02	05	07	08	10	14	07	18	.	01	.				
XI	6.3	6.6	6.1	7.0	080.0	05.4	92	79	87	86	37	064	014.0	23	02	04	10	.	.	01	02	16	12	10	02	07	06	01	.	02	09			
XII	8.4	5.8	4.8	6.3	083.6	04.2	91	79	82	87	55	023	019.9	18	.	03	24</td																	

Mesec	Vrednost pritisaka hPa	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Fm (0-12)																
		Tm			Sred. (°C)	Hm	Hf	Hg	Dat.	M	Dat.	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21																								
$\varphi = 42^{\circ}33' N \lambda = 21^{\circ}55' E$ Gr.ΔG = + 1h 26 min.																												
I	728.2	-03.0	01.7	-01.0	-00.8	02.7	-02.5	07.6	25 -06.4	11 04	C2.2	23 02.6	C8	02.1	01 01.0	01 01.0	16	01.4	02	02.0	01	01.0	31					
II	728.1	-02.9	03.8	-00.2	00.2	04.5	-03.6	09.9	12 -10.5	10 17	C2.6	32 02.8	C6	02.3	01 01.0	06	02.3	02	02.0	26						
III	720.8	03.2	13.4	08.1	08.2	14.6	02.1	22.2	31 -05.5	02 04	02.2	15 02.2	C5	02.2	06 02.8	24	02.7	12	03.0	27						
IV	722.5	07.5	16.1	16.5	11.3	17.4	05.2	26.0	08 -02.6	13 10	02.5	18 02.5	C6	02.7	02 03.5	16	02.8	14	03.4	03	02.3	21					
V	722.1	13.0	21.2	15.5	16.3	22.6	10.2	26.2	31 02.5	01 04	02.2	18 01.7	C8	02.1	01 01.0	01 01.0	11	02.4	06	02.2	05	02.0	29					
VI	722.2	15.8	22.6	17.7	18.4	24.0	13.1	31.3	02 08.0	06 05	02.2	36 02.3	C3	01.8	01 01.0	02 02.0	10	02.1	01	04.0	03	03.0	19					
VII	723.1	16.6	25.2	19.2	20.1	26.7	13.5	32.0	19 05.3	03 08	02.1	26 02.1	C1	02.0	01 02.0	04 02.0	01	01.0	01	04.0	03	03.0	30					
VIII	723.8	16.3	24.7	18.6	19.6	26.0	14.3	30.9	17 08.0	15 08	01.8	32 01.9	C6	02.2	01 01.0	03 02.0	06	02.3	03	02.3	01	01.0	23					
IX	727.4	13.1	25.5	17.7	18.5	26.5	11.2	30.1	16 05.1	11 36	C2.5	27 02.0	C7	02.6	02 01.5	06 01.7	06	02.5	01	02.0	01	02.0	34					
X	727.2	07.4	16.0	10.6	11.1	17.1	06.2	27.3	01 -01.4	09 07	C2.0	31 02.1	C5	01.0	03 02.0	10 01.9	03	02.7	21								
XI	726.4	02.8	07.6	04.6	04.9	08.6	01.6	16.0	18 -12.6	27 02	03.0	27 02.3	C10	02.4	05 01.6	11	02.6	12	02.8	23						
XII	726.9	-00.6	03.7	01.2	01.4	04.9	-01.6	11.8	18 -05.7	10 01	C2.0	28 02.5	C15	03.0	01 02.0	07	01.7	12	02.8	29						
GDO.	600.	725.1	07.4	15.1	10.3	10.8	16.4	05.7	32.0	49.W -12.6	10.XI	76	02.5	313	02.3	140	02.3	06	01.4	32	02.1	127	02.3	67	02.8	17	02.2	319
$\varphi = 42^{\circ}45' N \lambda = 21^{\circ}59' E$ Gr.ΔG = + 1h 27 min.																												
KUKAVICA																												
BR. ST. 227																												
I	-	-01.7	01.2	-01.5	-00.5	02.2	-02.4	12.5	15 -16.5	01 13	C2.4	05 01.4	34	C2.1	04	01.2	19	C1.8	18					
II	-	-05.7	-02.3	-04.6	-04.4	-06.6	-07.2	06.5	07 -14.0	09 12	C1.9	18 02.1	C6	01.3	C1	01.0	02	01.5	22	02.0	03	01.3	17	C2.5	03			
III	-	01.5	06.6	03.1	03.6	07.6	00.6	16.5	31 -07.0	22 22	C0.5	06 01.3	C0.1	01.0	C5	02.0	11	02.5	59	C2.1	04	02.0	03	02.3	01			
IV	-	04.4	08.9	05.1	05.9	10.0	02.4	19.5	06 -03.5	12 19	C1.9	06 02.3	02	02.5	04	02.5	36	02.5	10	02.3	22	02.4	01			
V	-	10.5	14.1	10.4	11.4	15.4	08.2	20.5	23 02.5	02 08	01.2	18 01.4	C1	01.0	03	01.0	06	01.2	25	01.4	04	01.8	13	C1.7	15			
VI	-	12.2	16.0	12.2	13.1	17.2	05.6	24.0	02 02.0	07 03	C1.3	26 01.3	C2	01.5	04	01.0	04	01.2	15	01.4	02	01.5	18	C2.2	16			
VII	-	14.2	18.0	13.5	14.5	16.6	11.3	26.5	19 06.0	03 15	C1.8	28 01.2	C0.2	01.0	03	01.3	10	01.2	01	02.0	14	C1.6	16	01.6	01			
VIII	-	13.2	18.0	13.5	14.6	19.0	11.5	23.5	17 08.0	15 07	C1.3	19 01.3	C1	01.0	05	01.4	15	01.3	01	01.0	33	01.8	01					
IX	-	13.4	18.5	13.5	14.7	15.2	11.6	24.5	16 06.5	10 05	02.0	30 01.4	C1	01.0	06	01.2	01	03.0	26	01.3	01	02.0	09	C1.4	11			
X	-	05.6	09.8	06.3	07.0	10.5	04.4	21.5	01 -00.5	26 02	C3.0	27 01.7	C2	01.0	07	01.3	03	02.7	31	01.7	04	02.5	12	02.0	05			
XI	-	00.2	02.5	00.4	00.5	03.7	-01.2	14.0	01 -12.5	26.25	04	02.5	27 01.3	02	01.0	04	05.2	32	01.8	02	01.0	09	02.0	10			
XII	-	-02.7	00.1	-01.7	-01.5	01.7	-04.5	09.0	24 -12.0	21 09	02.2	19 01.5	C3	01.0	06	01.5	03	03.3	32	01.9	03	01.6	09	01.8	07			
GDO.	-	05.4	09.3	05.8	06.6	10.5	03.6	26.5	49.W -14.0	09.II	89	01.9	229	01.5	19	01.1	43	01.3	46	02.3	337	01.8	41	01.8	178	02.0	113	
$\varphi = 42^{\circ}58' N \lambda = 22^{\circ}06' E$ Gr.ΔG = + 1h 29 min.																												
VLASOTINCE																												
BR. ST. 228																												
I	-	-00.6	04.9	00.6	01.3	05.6	-01.8	14.0	C7 -08.0	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	-01.3	03.9	-00.2	00.6	04.5	-03.1	12.0	13 -08.0	10.09	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	06.3	15.0	08.7	09.7	15.8	04.1	25.5	31 -02.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-					
IV	-	09.1	17.4	16.5	12.1	18.6	06.6	28.0	06 00.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-					
V	-	14.0	22.1	18.0	17.0	23.3	11.9	29.5	31 05.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-					
VI	-	14.5	23.4	17.3	18.6	24.3	13.8	32.0	02 05.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-					
VII	-	17.8	26.6	19.4	20.8	27.8	14.8	34.0	19 05.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-					
VIII	-	14.8	25.4	18.6	19.8	26.0	14.9	31.5	24 05.4	15	-	-	-	-	-	-	-	-	-	-	-	-	-					
IX	-	14.0	26.2	17.4	18.8	26.8	12.4	30.0	16 07.0	11	-	-	-	-	-	-	-	-	-	-	-	-	-					
X	-	08.8	16.6	10.2	11.4	17.6	07.0	29.5	01 00.5	31	-	-	-	-	-	-	-	-	-	-	-	-	-					
XI	-	03.3	08.1	04.8	05.2	09.2	01.1	21.0	18 -15.2	27	-	-	-	-	-	-	-	-	-	-	-	-	-					
XII	-	00.2	04.7	01.5	02.0	05.7	-01.1	15.0	18 -05.0	30.24	-	-	-	-	-	-	-	-	-	-	-	-	-					
GDO.	-	08.7	16.2	10.4	11.4	17.2	06.7	34.0	49.M -15.2	27.II	-	-	-	-	-	-	-	-	-	-	-	-	-					
$\varphi = 42^{\circ}50' N \lambda = 22^{\circ}08' E$ Gr.ΔG = + 1h 29 min.																												
PREDEJANE																												
BR. ST. 229																												
I	-	-02.3	03.7	-00.5	-00.1	04.2	-03.4	10.5	25 -07.5	05	19	C1.8	06	01.8	03	01.0	17	02.0	30	02.5	03	02.7	05	C3.2	10		
II	-	-02.8	03.6	-00.6	-00.3	04.6	-04.0	11.4	13 -11.0	10	26	C2.0	07	02.1	10	C1.6	12	01.9	05	02.0	02	02.0	09	C2.3	13		
III	-	03.1	14.9	07.4	08.2	15.6	02.1	25.0	31 -05.0	01	04	C1.5	08	01.9	10	01.3	33	02.1	19									

Meseč Mesec	Vršadunski Prstilan Pa. m	Temperatura vazduha °C										Čestina pravaca i srednja jačina vatra nD, fm (0-12)																					
		Tm				Min				Max.		Min.		Det.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)	Min	Max	Min	Max	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
$\varphi = 42^{\circ}44' N \lambda = 22^{\circ}21' E$ Gr.ΔG = + 1h 29 min.															VLASINA												BR. ST. 231						
I	-	-06.4	00.6	-04.8	-03.8	02.0	-05.3	07.5	07	-20.0	04	.	.	.	04	01.0	.	.	01	01.0	03	01.0	28	02.1	57								
II	-	-07.7	-01.8	-06.6	-05.7	-00.6	-10.4	07.3	07	-18.5	05	.	.	08	02.6	13	.	01.0	01.0	01	01.0	.	.	06	01.2	22	01.6	30					
III	-	-00.1	07.1	02.0	02.7	00.2	-02.5	17.6	31	-11.9	01	02	01.0	02	01.0	07	01.1	03	01.0	16	02.2	10	01.7	04	01.0	11	01.5	38					
IV	-	04.0	09.5	04.3	05.6	11.5	00.8	20.8	07.0	-06.8	12	03	02.7	01	01.0	01	01.5	05	02.8	12	01.9	06	02.0	37	02.0	21							
V	-	10.3	14.8	09.0	10.8	16.7	06.0	21.2	30	-00.2	01	01	02.0	03	01.0	04	01.8	03	01.3	04	01.8	03	01.3	13	01.4	23	01.7	39					
VI	-	12.1	16.9	10.8	12.7	18.5	07.9	25.0	02	02.6	07.0	06	07	01.7	03	01.7	05	01.2	04	01.2	05	01.2	08	01.1	07	01.1	26	01.7	25				
VII	-	13.4	18.9	11.5	14.0	20.6	08.7	27.5	19	04.1	03	04.1	02	01.5	02	01.0	04	01.5	05	03	01.7	11	01.4	39	01.4	28							
VIII	-	12.1	18.6	11.8	13.6	19.8	09.1	24.2	17	02.0	15	03	01.7	03	01.3	02	01.0	.	02	01.5	07	01.1	06	01.0	32	01.3	38						
IX	-	09.9	19.0	10.4	12.4	20.2	07.0	25.6	16	00.0	11	05	01.0	02	04.0	06	02.2	02	01.5	.	05	01.4	10	01.0	13	01.3	47						
X	-	03.8	10.8	04.7	06.0	11.8	01.8	21.5	01	-04.0	26.0	05	11	01.2	01	03.0	08	01.5	05	01.2	20	01.5	33										
XI	-	-01.4	02.6	-00.9	-00.2	04.0	-03.0	14.8	01	-12.8	26	04	01.2	05	02.2	17	01.2	08	01.1	10	01.7	04	01.5	05	01.4	27							
XII	-	-04.4	00.3	-03.4	-02.7	02.2	-06.7	05.6	30	-18.0	10	10	01.7	.	07	01.3	06	01.3	01	01.0	.	03	01.3	34	01.5	32							
GOD.	-	03.8	09.8	04.1	05.4	11.2	00.8	27.5	19	MVII -20.0	04.1	50	01.5	30	02.0	72	01.4	47	01.3	50	01.8	57	01.5	79	01.3	295	01.6	415					
$\varphi = 42^{\circ}30' N \lambda = 22^{\circ}28' E$ Gr.ΔG = + 1h 29 min.															BESILJGRAC												BR. ST. 232						
I	-	-05.5	04.8	-02.6	-01.1	05.3	-06.6	10.3	07	-13.2	04	24	01.4	.	.	10	01.6	.	.	01	04.0	58						
II	-	-06.0	02.8	-01.4	-01.8	03.2	-06.7	08.8	15	-13.0	10	.	.	01	02.0	.	.	32	01.9	.	.	12	02.4	.	.	02	03.5	37					
III	-	00.4	11.8	04.1	05.1	12.2	-03.2	22.1	31	-06.7	02	35	01.7	.	.	08	01.4	.	.	01	03.0	50						
IV	-	06.2	14.7	08.6	09.6	15.4	04.7	25.4	06	-06.1	13	.	.	01	02.0	.	.	22	01.6	.	.	24	02.1	.	.	01	03.0	42					
V	-	12.9	19.6	13.0	14.6	24.3	05.7	25.7	31	04.3	05	32	01.6	.	.	11	01.7	.	.	01	02.0	49						
VI	-	15.1	21.5	15.0	16.6	22.2	12.0	25.6	02	04.5	11	24	01.5	.	.	10	02.3	.	.	03	03.3	53						
VII	-	17.1	24.6	17.1	19.0	25.6	13.8	32.8	19	10.2	29	24	02.0	.	.	05	02.0	.	.	01	03.0	63						
VIII	-	14.8	24.6	16.6	16.1	25.1	12.9	26.9	16	08.9	06	26	01.6	.	.	17	01.7	.	.	01	02.0	56						
IX	-	11.5	23.7	14.8	16.2	24.6	05.8	31.1	16	02.6	11	.	.	02	02.5	.	.	26	01.5	.	.	13	01.5	.	.	01	02.0	49					
X	-	05.6	15.2	08.4	09.4	15.8	04.5	25.6	01	-02.4	05	34	01.6	.	.	14	02.8	.	.	01	03.0	45						
XI	-	00.2	06.0	02.3	02.7	08.6	-00.4	16.4	01	-14.9	27	.	.	02	01.0	.	.	19	01.4	.	.	23	01.7	.	.	01	01.0	45					
XII	-	-02.2	04.1	00.6	00.8	05.2	-02.9	09.5	30	-06.9	21	05	01.2	.	.	17	01.4	.	.	04	01.8	67						
GOD.	-	05.8	14.4	08.0	09.1	15.1	04.2	32.8	08	MVII -14.9	27	XI	.	.	06	01.8	.	.	297	01.6	.	.	164	01.9	.	.	14	02.6	614				
SR CRNA GORA															KRSTAC												BR. ST. 233						
I	-	-03.5	03.9	01.2	00.7	05.4	-04.8	05.4	18	-16.6	10	-					
II	-	-03.8	02.7	-00.6	-00.6	04.8	-05.0	11.0	19	-10.5	05	32	01.9	.	.	12	02.4	.	.	02	03.5	37						
III	-	02.6	07.3	04.8	04.9	03.8	00.9	16.0	08	-05.6	22	35	01.7	.	.	08	01.4	.	.	01	03.0	50						
IV	-	06.1	10.4	07.8	08.0	11.6	03.4	20.4	06	-02.0	13	22	01.6	.	.	24	02.1	.	.	01	03.0	42						
V	-	11.3	16.3	12.6	13.2	18.0	08.4	25.0	18	03.0	10	32	01.6	.	.	11	01.7	.	.	01	02.0	49						
VI	-	13.3	17.9	14.2	14.8	19.3	10.9	25.0	15	05.0	07	.	.	20	04.5	C2	02.0	25	02.4	C2	02.5	17	02.9	.	.	09	03.7	11					
VII	-	15.7	22.0	17.0	18.0	23.6	12.7	30.0	18	08.0	02.0	01	03.0	27	04.3	C1	01.0	16	02.0	01	03.0	09	03.0	18									
VIII	-	14.4	19.9	16.0	16.6	21.5	12.1	26.5	12	05.5	27	22	.	29	03.9	C4	01.8	21	02.7	04	01.8	12	02.3	03	02.0	04	02.0	16					
IX	-	12.1	21.5	16.5	16.6	22.2	10.4	28.4	16	07.0	14	.	.	49	02.9	C1	01.0	27	02.2	C1	03.0	18	02.4	02	02.5	08	02.5	24					
X	-	06.5	13.2	10.0	09.9	14.1	01.1	24.4	02	0.01	00.0	30	.	21	05.0	.	27	02.5	.	28	03.4	.	.	01	03.0	16							
XI	-	01.1	06.3	04.0	04.0	07.8	01.1	21.2	02	-03.8	04	26	.	30	04.3	.	30	02.7	01	02.0	13	02.8	.	.	01	01.0	15						
XII	-	-00.9	03.2	-01.3	-00.3	04.3	-03.4	15.0	02	-16.0	26	07	02.1	03	02.0	03	02.7	14	J4.3	01	02.0	01	02.0	05	03.0	53							
GOD.	-	04.1	10.1	08.5	03.5	04.7	06.8	06.4	26	MVII -18.0	09.1	01	02.4	33	02.0	37	01.8	77	03.0	113	02.9	43	03.5	13	02.1	57	C2.0	641					
$\varphi = 43^{\circ}09' N \lambda = 19^{\circ}08' E$ Gr.ΔG = + 1h 17 min.															PLJEVLJA																		

Mesec	Oblačnost Nm (0-10)	Indolacija broj sati (Dnes)	Vlažnost vazduha			Padavine R mm	Broj dana n s a:																						
			a _m	U _m	t		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	*	▲	▲	▲	▲	■				
			mm	7	14	21	Sred.	Streš.	Min	Σ	Max	Dat.				≤	<	<	≤	≤	≤	≤	≥	≥	≥				
BR. ST. 231	VLASINA	.																											
I 5.2 4.4 3.8 4.5	134.7	02.5	78	74	82	78	42	033	011.8	09	13	11	31	•	•	•	•	10	06	11	04	01	11	•	•	01 31			
II 5.8 5.5 4.5 5.3	129.0	02.6	80	75	84	80	47	034	008.1	15	16	16	28	•	•	•	•	07	09	09	08	03	03	09	03	03 28			
III 5.3 5.2 4.0 4.8	161.5	03.5	80	55	73	69	28	052	017.9	22	01	02	21	•	•	•	•	03	05	11	09	02	06	08	02	03 20			
IV 5.6 5.8 4.4 5.3	189.0	04.3	72	53	71	65	15	073	014.2	28	•	•	11	•	•	•	•	05	07	15	13	02	15	07	07	02 04			
V 5.1 6.5 5.9 5.8	203.4	07.6	84	63	87	78	39	161	024.3	18	•	•	01	•	•	•	•	07	20	18	06	20	•	•	•	08 01			
VI 5.1 5.9 5.5 5.5	185.0	09.3	87	68	90	82	38	186	047.0	21	•	•	01	•	•	•	•	06	18	17	07	17	01	•	•	07 03			
VII 3.8 5.4 3.0 4.1	240.5	10.3	86	69	80	82	39	044	010.0	31	•	•	01	•	•	•	•	05	C2	11	08	01	11	•	•	03	03		
VIII 5.0 5.9 4.3 5.0	201.7	10.0	94	66	93	84	40	040	014.4	06	•	•	•	•	•	•	•	02	03	19	08	01	18	•	•	04 01			
IX 2.3 4.2 2.2 2.9	239.4	08.5	90	54	89	78	19	022	008.4	25	•	•	01	•	•	•	•	11	•	07	04	07	07	•	•	01	•		
X 5.8 5.3 4.1 5.1	148.1	05.6	89	66	87	81	21	077	021.0	18	•	•	10	•	•	•	•	06	07	17	12	02	17	01	01	02			
XI 7.5 7.3 6.9 7.2	-	04.1	86	80	88	85	29	092	021.1	23	04	05	22	•	•	•	•	03	17	14	13	02	08	09	02	01 08			
XII 6.5 5.5 6.2 6.1	109.9	03.3	87	78	89	85	39	034	013.6	18	06	11	30	•	•	•	•	04	11	11	06	01	02	10	01	11 22			
GOD. 5.2 5.6 4.6 5.1	-	06.1	84	66	85	78	15	848	047.0	24 VI	40	45	154	03	•	•	01	•	56	80	163	122	25	124	94	16	•	23 35 116	
BR. ST. 232	BOSILJGRAD	.																											
I 3.3 4.4 3.2 3.6	-	03.4	82	68	86	79	48	008	006.3	29	03	01	31	•	•	•	•	10	04	02	02	02	02	•	•	•	•		
II 4.7 5.0 4.9 4.9	-	03.5	84	78	89	84	48	009	004.3	17	06	03	27	•	•	•	•	05	03	05	03	03	05	•	•	08 06			
III 5.0 6.4 5.5 5.6	-	-	-	-	-	-	-	040	014.0	23	•	•	16	•	•	•	•	02	C7	04	04	02	03	02	•	•	03 01		
IV 5.1 5.5 5.8 5.5	-	-	-	-	-	-	-	011	003.2	26	•	•	01	01	•	•	•	04	07	06	04	04	06	•	•	•			
V 4.5 6.2 5.9 5.5	-	09.6	80	66	75	74	31	089	022.5	25	•	•	01	•	•	•	•	02	07	13	12	02	13	•	•	04			
VI 5.3 6.3 6.1 5.9	-	11.0	83	65	77	75	32	269	052.2	21	•	•	11	•	•	•	•	04	04	16	16	08	16	•	•	09			
VII 3.6 4.6 3.6 3.9	-	11.6	77	55	76	69	01	046	020.4	06	•	•	17	03	•	•	•	08	01	08	05	02	08	•	•	01			
VIII 4.3 4.9 6.0 5.1	-	12.2	84	61	85	76	44	044	012.5	20	•	•	18	•	•	•	•	02	05	09	07	02	09	•	•	06 01			
IX 1.0 4.2 1.7 2.3	-	10.7	85	60	80	75	40	036	019.7	05	•	•	11	01	•	•	•	15	•	04	02	02	04	•	•	•			
X 5.9 5.9 5.9 5.9	-	07.3	87	71	78	88	48	114	022.3	18	•	•	06	01	•	•	•	03	10	13	13	05	13	•	•	01			
XI 8.7 8.5 8.7 8.7	-	05.0	87	82	85	85	25	076	024.0	20	03	01	12	•	•	•	•	01	23	10	09	03	07	03	•	•	16		
XII 6.5 5.5 6.2 6.1	-	-	-	-	-	-	-	014	006.0	07	•	•	26	•	•	•	•	07	10	03	03	01	02	•	•	28			
GOD. 4.8 5.6 5.2 5.2	-	-	-	-	-	-	-	756	052.2	21 VI	12	06	119	60	04	•	•	63	81	93	80	26	80	14	•	- - - -			
BR. ST. 233	KRSTAC	.																											
I 4.9 4.7 4.4 4.6	-	-	-	-	-	-	-	017	003.4	30	01	•	30	•	•	•	03	02	07	06	05	05	•	02	09	02	•	10	
II 5.3 4.3 4.9 4.8	-	-	-	-	-	-	-	010	005.5	15	02	03	25	•	•	•	04	•	07	08	03	03	03	02	•	•	01 06		
III 8.0 8.1 6.5 6.2	-	-	-	-	-	-	-	196	042.0	13	•	•	10	•	•	•	•	02	22	13	13	08	13	05	05	01	01	03	
IV 6.4 7.0 7.0 6.6	-	-	-	-	-	-	-	106	025.0	11	•	•	02	•	•	•	•	02	11	10	10	03	10	04	01	•	03		
V 6.0 7.7 7.1 6.9	-	-	-	-	-	-	-	091	023.0	09	•	•	01	•	•	•	•	13	10	16	05	10	10	•	•	02 01			
VI 5.9 7.7 6.7 6.8	-	-	-	-	-	-	-	052	008.5	20	•	•	01	•	•	•	•	05	03	•	10	09	09	09	09	09	02 02		
VII 3.5 5.5 3.7 4.2	-	-	-	-	-	-	-	038	018.6	02	•	•	13	01	•	•	•	05	02	02	05	05	01	03	01	01	04 06		
VIII 5.5 6.3 4.9 5.4	-	-	-	-	-	-	-	098	030.0	26	•	•	07	•	•	•	•	04	03	09	09	04	04	09	01	01	01		
IX 3.3 4.0 3.7 3.7	-	-	-	-	-	-	-	034	016.0	04	•	•	04	•	•	•	•	01	•	05	02	03	03	02	03	•	03		
X 5.9 5.7 5.7 5.8	-	-	-	-	-	-	-	190	030.5	14	•	•	04	•	•	•	•	09	04	04	12	11	11	08	11	•	01 02		
XI 7.5 6.6 6.6 7.0	-	-	-	-	-	-	-	243	100.4	19	01	04	05	•	•	•	•	08	03	02	16	09	08	03	08	02	01 02		
XII 4.8 4.4 4.0 4.4	-	-	-	-	-	-	-	118	070.9	18	•	•	25	•	•	•	•	11	16	07	06	04	03	06	01	01	01 01		
GOD. 5.6 6.0 5.6 5.7	-	-	-	-	-	-	-	1193	100.4	19 XI	04	•	•	26	01	•	•	50	20	41	111	93	92	41	05	20	11	•	04 08 23
BR. ST. 234	ZABELJAK	.																											
I 4.3 4.4 3.4 4.0	-	156.1	03.0	86	72	86	81	44	028	006.2	05	05	07	31	•	•	•	01	•	13	C5	10	06	06	02	10	01	•	31
II 6.1 5.4 5.2 5.6	-	124.0	02.6	85	80	85	84	33	019	006.6	17	16	13	28	•	•	•	•	07	12	10	05	05	05	10	05	•	20	
III 6.7 7.0 8.0 6.2	-	123.4	04.0	82	74	82	79	30	149	057.1	29	01	04	23	•	•	•	06	•	C3	C8	15	12	04	06	15	03	02	31
IV 6.5 6.3 4.7 5.8	-	158.0	04.4	81	67	79	76	27	221	051.2	02	•	•	17	•	•	•	06	03	07	14	16	14	06	11	10			

U č es e z	Oblačnost Nm (0-10)			Inovacije s tati č nosti broj	Vlažnost vazduha			Padavine R mm			Broj dana n sat:																						
	7	14	21		7	14	21	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	风	三					
	Std. (Dies.)				mm	mm	mm	mm	mm	dat.	=	<	<	=	=	=	=	≤	≥	≤	≥	≤	≥	≤	≥	≤	≥						
BIJELC FCLJE																																	
BR. ST. 236																																	
I	7.7	4.4	3.7	5.3	092.1	03.2	52	68	92	44	012	004.6.	29	11	04	30	.	.	01	.	06	C7	C7	C4	.	02	04	01	.	13	30		
II	7.2	5.1	4.2	5.5	097.5	03.1	88	53	77	72	24	J12	005.1	21	06	01	27	07	C8	C6	C3	.	02	02	01	.	01	05	
III	6.6	6.6	4.7	6.0	126.5	04.5	88	43	74	68	15	058	024.6	15	.	01	19	.	.	.	03	C5	C1	C0	C2	C7	04	01	.	01	03	04	
IV	6.8	6.0	5.0	5.9	167.2	05.3	80	44	66	63	13	054	012.4	02	.	01	34	01	.	01	05	11	11	05	01	11	.	.	02	03	.		
V	8.4	6.3	5.2	6.6	174.9	08.7	91	45	81	74	22	055	017.0	25	.	.	37	C7	C1	C0	C1	14	.	.	.	04	06	.	
VI	8.3	6.5	5.7	6.8	145.6	10.3	91	57	85	78	26	079	025.8	20	.	.	11	08	C1	09	02	C3	.	04	04	.	04	04	.
VII	7.8	5.0	4.9	5.9	218.1	11.1	91	45	86	75	27	035	013.4	02	.	.	18	02	.	.	.	C2	C7	11	C7	01	11	.	.	06	05	.	
VIII	9.0	6.5	5.4	7.0	156.2	11.0	94	53	91	79	31	112	030.4	08	.	.	10	12	19	16	03	15	.	.	02	07	.		
IX	9.9	3.1	1.7	4.9	200.9	10.1	95	48	91	78	26	021	014.2	13	.	.	22	C2	04	04	01	C4	27	.	
X	9.7	5.9	5.2	7.0	100.8	07.0	95	59	91	81	35	124	033.0	13	.	.	04	01	.	.	.	14	15	11	05	12	.	.	01	04	03		
XI	9.1	6.6	6.2	7.3	070.4	05.0	90	67	86	81	39	077	024.8	20	02	04	11	.	.	.	C1	01	15	13	10	03	10	04	01	01	04		
XII	9.2	7.0	7.3	7.8	044.9	03.5	89	71	84	81	34	014	010.7	18	.	03	23	.	.	.	14	06	03	01	07	C5	02	.	.	09	.		
GOD. 8.3 5.8 4.9 6.3 1605.1 06.9 90 55 83 76 13 653 033.0																																	
HERCEGNOWI-IGALO																																	
BR. ST. 237																																	
I	4.4	4.8	2.6	4.0	165.4	05.5	75	65	75	76	22	058	033.6	29	01	10	C2	C9	C2	C2	05		
II	4.0	4.9	3.1	4.0	162.3	05.0	66	53	66	62	23	074	046.8	15	.	02	.	.	.	04	01	12	C8	C6	C4	04	32	06	.	01	09	.	
III	7.9	8.5	7.5	7.9	088.9	07.5	76	65	73	73	27	250	034.5	16	01	03	03	20	16	15	09	18	.	.	01	09	.		
IV	5.2	5.6	4.2	5.0	219.9	07.7	67	57	68	64	27	069	019.0	11	02	01	07	08	09	C9	C3	C5	.	04	.				
V	5.5	6.1	5.3	5.6	236.2	12.4	84	68	83	79	37	066	024.8	14	.	.	05	.	.	.	C4	C9	11	C0	02	11	.	.	.	02	.		
VI	4.2	5.0	4.6	4.6	266.7	14.8	80	68	82	77	42	051	013.6	10	.	.	18	03	02	01	.	06	05	09	08	01	09	.	.	06	.		
VII	1.8	3.0	1.9	2.2	357.7	15.5	72	60	75	65	36	072	045.9	06	.	.	24	11	13	05	02	19	C2	C3	C3	02	03	.	.	04	.		
VIII	4.3	5.3	2.4	4.0	273.3	13.5	68	54	69	64	35	128	049.1	25	.	.	16	07	09	11	02	09	03	12	10	05	12	.	.	10	.		
IX	2.7	3.4	1.6	2.6	288.0	13.5	73	56	76	65	36	027	013.5	04	.	.	28	03	02	01	.	16	C2	05	03	01	05	.	.	04	.		
X	5.0	5.3	3.5	4.6	181.7	09.7	72	57	74	68	34	289	077.5	21	.	.	03	.	.	09	04	12	08	12	12	10	12	.	.	10	.		
XI	7.6	7.1	5.2	6.6	104.6	07.8	76	65	73	72	36	296	085.4	17	.	.	05	07	02	11	14	13	09	14	.	.	03	.	.	03	.		
XII	5.3	5.3	3.8	4.8	135.1	06.8	79	61	78	72	35	256	130.8	17	.	.	03	02	08	07	08	07	03	08	01	.		
GOD. 4.8 5.4 3.8 4.7 2483.6 10.0 74 80 74 65 22 1636 130.8																																	
GRADIVO																																	
BR. ST. 238																																	
I	3.5	4.0	1.6	3.0	-	34.2	86	71	91	82	43	088	044.6	29	01	.	25	.	.	.	02	02	16	C2	04	02	04	.	.	.			
II	3.9	3.9	2.6	3.5	-	04.4	88	76	92	85	35	C13	008.8	14	01	.	22	.	.	.	03	01	17	C6	09	05	03	01	01	01			
III	7.9	7.4	6.8	7.6	-	06.0	88	75	92	85	32	576	138.6	29	.	11	.	.	.	05	03	16	C8	17	10	18	02	02	01				
IV	4.6	5.8	3.6	4.7	-	37.1	80	72	83	78	53	191	048.2	11	.	04	.	.	04	09	06	12	11	05	12	.	.	01	02	01			
V	5.0	6.9	4.6	5.5	-	10.3	88	75	86	82	45	046	150.0	14	.	.	04	.	.	.	03	07	08	C7	08	07	02	.	.	.			
VI	4.1	6.3	4.8	5.0	-	10.6	77	65	83	79	39	082	022.8	28	.	.	12	.	.	.	03	04	09	C5	04	05	04	09	.	01			
VII	1.5	4.2	2.1	2.6	-	11.7	76	57	80	71	30	045	015.8	06	.	.	24	02	.	.	.	16	C1	07	05	02	07	.	.	03	.		
VIII	4.0	5.6	2.6	4.1	-	10.4	79	51	81	70	31	180	070.2	26	.	.	16	.	.	.	08	03	09	07	09	09	.	.	03	.			
IX	2.2	3.4	1.9	2.5	-	11.1	89	64	84	79	41	C92	052.4	04	.	.	12	02	.	.	.	17	C1	04	03	02	04	.	.	01	01	.	
X	4.5	4.9	4.0	4.5	-	08.3	90	80	85	86	36	583	164.2	13	.	08	.	.	.	13	08	13	12	09	13	.	.	01	02	01			
XI	6.9	6.4	5.8	6.4	-	05.7	92	76	92	87	39	929	195.6	19	01	01	17	.	.	.	02	02	04	13	14	11	06	14	03	02			
XII	4.1	3.2	2.6	3.3	-	04.5	87	70	91	83	39	230	124.6	18	.	05	25	.	.	.	14	06	05	03	04	05	.	.	03	.			
TIVAT																																	
BR. ST. 239																																	
I	3.2	3.7	1.5	2.9	-	05.3	86	57	83	75	31	040	C23.1	29	.	.	17	.	.	.	01	17	C1	05	01	05		
II	3.6	4.4	2																														

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha				Padavine R mm				Broj dana n s a:																							
	Indolacijski broj sati	Sred. (Dies)	7	14	21	U m %				Tn	Tx	Th	Tx	Tx	Tn	F(0-12)		Nm(0-10)		R mm	•	*	•	Δ	Δ	Δ	Δ	Δ	Δ	T	≡					
						e _m	mm	7	14	21	Sred.	Min	Max	Dat.	≤	<	<	≥	≥	≥	≥	≥	≤	<	>	≤	≤	≤	≤	•	Δ	•	Δ	Δ	Δ	Δ
CETINJE																																				
BR. ST. 241																																				
I 3.5 4.5 2.2 3.4 -	03.5	86	51	86	75	20	077	C44.0	29	.	.	29	14	C2	05	04	02	05	01	02	.			
II 3.9 4.4 3.2 3.8 -	03.4	88	51	80	72	20	080	C35.7	15	01	.	25	14	C0	08	08	02	04	02	06	04	.			
III 8.5 8.4 7.4 8.1 -	35.5	51	65	50	82	29	417	C76.5	28	.	.	13	.	.	.	02	.	02	11	21	18	11	19	07	03	01	07	05	03			
IV 8.8 5.5 3.9 4.7 -	35.7	77	47	73	66	20	236	C141.2	11	.	.	36	08	08	13	09	04	13	03	02	03	03	.					
V 4.6 6.5 3.8 5.0 -	09.3	80	58	86	75	36	117	C35.4	28	.	.	02	.	.	.	05	06	17	11	03	17	05	.	.					
VI 3.6 5.9 4.1 4.5 -	10.7	76	57	85	73	38	084	C33.4	24	.	.	11	.	.	.	03	.	06	04	13	10	03	13	07	01	.						
VII 1.5 3.9 1.5 2.3 -	11.8	76	51	86	71	28	090	C31.2	06	.	.	24	03	.	.	.	19	02	11	06	04	11	05	.	.				
VIII 4.2 6.1 2.4 4.2 -	10.6	83	47	82	71	29	112	C45.4	26	.	.	19	.	.	.	06	03	13	06	04	13	08	.	.					
IX 2.0 3.3 0.7 2.0 -	10.5	91	54	78	78	38	105	C43.3	04	.	.	12	02	.	.	.	20	01	06	05	03	08	03	.	.				
X 4.3 5.2 3.8 4.4 -	07.3	93	61	95	83	32	367	C74.3	14	.	.	05	01	.	.	.	13	09	13	13	10	13	06	01	.				
XI 5.8 6.7 5.0 5.8 -	05.8	92	74	93	86	41	361	C117.2	17	.	.	19	.	.	.	01	01	06	12	15	13	11	15	02	02	04	01	02				
XII 4.4 4.0 2.6 3.7 -	04.4	93	60	89	81	27	344	C214.1	18	.	.	26	.	.	.	16	06	05	04	04	06	01	03	.					
GOD. 4.3 5.4 3.6 4.3 -	07.4	85	56	86	76	20	2360	C141.1	48.XI	01	.	127	69	05	.	04	01	129	72	141	108	61	138	14	09	.	.	.	01	50	22	09				
NIKŠIĆ																																				
BR. ST. 242																																				
I 3.6 4.5 2.5 3.5 -	189.3	03.4	77	47	65	65	17	027	C28.4	29	.	.	22	.	.	.	05	08	13	03	04	04	01	04	02	.					
II 4.0 36.9 3.2 3.7 -	172.9	03.2	66	51	61	59	19	016	C07.6	15	.	.	19	.	.	.	18	10	15	07	06	04	05	02	01	.	.	.	03	.						
III 7.9 7.9 6.9 7.6 -	086.7	05.4	83	64	74	75	11	227	C55.0	29	.	.	08	.	.	.	22	07	02	18	18	15	08	17	03	.	.	.	01	04	01					
IV 5.0 6.1 4.7 5.3 -	184.9	05.6	70	53	64	62	18	166	C03.9	04	.	.	01	.	.	.	27	11	04	05	13	10	04	13	02	.	.	.	02	03	.					
V 4.8 6.5 4.4 5.2 -	203.7	09.2	79	55	77	71	22	076	C12.6	27	.	.	02	.	.	.	15	03	03	06	13	12	02	13	.	.	.	04	02	.						
VI 4.6 6.6 4.9 5.4 -	221.4	10.2	74	54	73	67	35	040	C10.0	17	.	.	12	.	.	.	22	04	04	04	09	09	01	05	.	.	.	04	01	.						
VII 1.0 3.7 2.2 2.6 -	319.3	11.1	65	45	66	61	29	024	C04.5	32	.	.	24	04	.	.	12	02	15	02	06	05	02	06	.	.	.	07	.							
VIII 5.1 6.0 3.2 4.7 -	223.5	10.4	73	53	67	64	27	148	C05.6	26	.	.	15	01	.	.	21	04	05	05	12	09	05	12	.	.	.	09	.							
IX 2.4 3.7 0.7 2.2 -	268.0	10.4	82	50	76	69	30	050	C33.0	13	.	.	14	01	.	.	08	01	18	C1	05	01	05	.	.	.	05	.	.							
X 4.9 5.5 4.2 4.8 -	171.2	07.0	79	57	75	70	26	495	C275.8	13	.	.	03	.	.	.	13	04	11	11	14	13	08	14	.	.	.	08	01	.						
XI 6.7 6.3 5.8 6.3 -	106.3	05.4	85	63	80	76	22	206	C76.3	18	.	.	01	08	.	.	09	04	04	12	13	10	04	12	02	01	.	05	01							
XII 3.7 4.0 3.4 3.7 -	162.3	04.2	80	57	77	71	27	110	C076.5	18	.	.	21	.	.	.	13	06	13	05	05	03	02	03	.	.	.	01	08	.						
GOD. 4.0 4.4 3.4 3.9 -	09.8	82	53	76	70	18	1738	C140.6	48.XI	-	.	-	126	63	-	-	24	10	161	EC	97	94	56	97	01	.	.	.	03	.09	.					
BAR																																				
BR. ST. 244																																				
I 3.8 3.3 1.6 2.9 -	195.1	35.5	65	58	72	66	18	028	C02.6	25	.	.	15	.	.	.	01	01	18	C4	04	03	01	04	.	.	.	01	02	.						
II 4.0 4.3 2.5 3.7 -	165.5	04.5	59	59	56	22	104	C70.4	15	.	.	02	.	.	.	02	01	16	C6	08	08	01	02	.	.	.	01	01	.							
III 7.7 8.0 6.8 7.5 -	108.8	J7.1	66	60	71	66	23	123	C02.6	22	.	.	01	.	.	.	14	01	03	17	13	11	05	13	.	.	.	01	08	.						
IV 5.2 5.0 4.6 4.9 -	233.1	07.6	60	60	67	62	24	046	C14.8	03	.	.	01	.	.	.	12	06	C9	10	08	07	01	08	.	.	.	01	04	.						
V 5.7 5.5 4.8 5.3 -	250.9	12.1	75	72	80	76	40	062	C22.5	08	.	.	02	.	.	.	04	02	06	C7	10	07	04	07	.	.	.	02	.	.						
VI 4.1 4.6 4.0 4.2 -	285.0	11.6	65	75	71	35	016	C06.2	17	.	.	11	01	.	.	07	03	10	05	05	04	05	03	.	.	03	.									
VII 1.8 1.9 1.5 1.7 -	360.4	15.3	65	68	70	34	034	C24.4	13	.	.	27	02	03	03	10																				

Mesec	Vadudjni pritisak pm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (0-12)																
		Tm			Sred. (Dnev.)	Mx	Mn	Mx	Mn	Mx	Mn	Dat.	N	NE	E	SE	S	SW	W	NW	C							
		7	14	21									č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.				
$\varphi = 42^{\circ}50' N \lambda = 19^{\circ}32' E$ Gr.ΔG = + 1h 18 min.																												
I	684.5	-06.4	04.3	-02.8	-01.5	05.2	-07.2	12.0	17	-14.6	11	28	03.3	14	01.4	51		
II	683.8	-05.0	01.8	-02.7	-02.1	02.8	-05.7	10.6	07	-15.0	10	48	03.2	14	01.4	03	01.0	.	.	.	19		
III	677.8	00.8	07.6	02.6	03.4	09.4	-00.6	18.2	08	-10.6	01	12	02.6	45	02.0	02	03.5	02	01.0	.	31		
IV	680.4	04.3	11.3	05.6	06.7	12.9	01.8	21.6	06	-03.6	13	34	02.1	31	02.2	01	04.0	.	.	.	24		
V	680.9	09.0	17.6	10.8	12.1	19.0	06.3	24.4	20	-00.4	01	12	02.2	32	02.2	01	02.0	.	.	01	02.0	47	
VI	681.5	11.2	18.1	12.0	13.3	20.3	08.2	26.0	29	03.4	10	24	02.5	23	02.5	02	01.5	.	01	01.0	43		
VII	682.2	12.7	22.3	14.2	15.9	23.6	10.0	30.0	18	04.9	28	31	02.4	15	01.9	05	02.6	01	02.0	04	02.0	37	
VIII	682.9	12.1	20.1	13.1	14.6	22.0	09.7	26.8	11	04.6	24	35	02.5	.	.	01	01.0	.	18	01.6	.	.	.	03	02.0	36		
IX	685.9	09.0	21.9	11.3	13.4	23.0	07.2	30.0	16	02.4	26.25	14	02.6	21	01.8	03	02.3	01	01.0	02	01.0	49	
X	684.0	04.2	12.8	05.9	07.2	14.0	03.1	25.8	02	-04.6	31	35	02.3	12	02.6	02	01.0	01	01.0	01	01.0	43	
XI	682.0	-00.3	06.8	01.3	02.3	08.0	-02.0	17.6	03	-19.2	26	28	02.3	12	03.4	05	02.2	.	.	.	45		
XII	684.0	-02.1	04.5	-00.6	00.3	05.0	-03.6	11.2	24	-10.0	08	33	02.4	01	01.0	.	.	.	11	01.6	02	02.0	.	.	.	44		
GOD.	682.5	04.1	12.4	05.9	07.1	13.8	02.3	30.0	M. IX	-19.2	26. XI	334	02.6	01	01.0	01	01.0	.	248	02.1	25	02.2	05	01.2	12	01.7	468	
$\varphi = 42^{\circ}50' N \lambda = 19^{\circ}32' E$ Gr.ΔG = + 1h 19 min.																												
$\varphi = 42^{\circ}50' N \lambda = 19^{\circ}32' E$ Gr.ΔG = + 1h 19 min.																												
I	705.6	-06.8	00.7	-04.9	-03.9	02.6	-08.2	10.3	25	-17.0	10	11	01.7	03	02.0	C1	02.0	.	02	02.0	02	01.0	.	07	01.3	67		
II	705.0	-04.3	02.7	-01.7	-01.3	04.0	-05.3	08.6	12	-12.6	10	24	01.7	08	01.8	01	01.0	02	01.0	01	01.6	03	01.0	17	01.8	23		
III	697.4	01.7	11.3	04.6	05.5	13.4	-00.5	21.6	31	-07.7	01	14	01.1	05	01.0	04	01.0	02	01.5	20	02.8	16	02.2	05	01.0	05	01.4	22
IV	699.0	05.6	13.5	08.1	08.8	15.1	02.8	24.4	07	-03.4	13	14	01.9	14	01.4	.	.	03	02.0	09	03.2	17	02.8	02	01.5	10	01.8	21
V	700.2	10.5	19.3	12.9	13.9	20.8	07.0	25.6	20	00.7	01	16	01.6	05	02.0	04	01.8	05	01.8	08	02.4	10	01.6	03	01.7	06	01.7	36
VI	700.0	13.3	20.8	14.1	15.6	22.1	09.3	28.6	02	02.5	10	12	01.3	07	01.4	02	01.0	04	01.2	05	02.2	06	02.3	06	01.2	05	01.8	43
VII	701.3	14.9	23.6	16.5	17.9	25.1	10.8	33.2	19	06.4	29	14	01.4	12	02.4	04	01.2	04	01.8	01	02.0	07	01.6	03	01.7	11	01.5	37
VIII	702.4	13.0	21.8	15.0	16.2	23.2	10.5	29.2	12	04.3	24	14	01.4	09	01.1	02	01.5	05	01.6	05	01.4	01	01.0	12	01.6	43		
IX	705.5	09.9	23.3	13.3	14.9	24.5	07.0	29.6	16	02.6	25	08	01.4	06	01.3	.	.	04	01.0	04	01.8	03	01.7	.	10	01.3	55	
X	704.5	05.3	13.9	07.3	08.4	15.1	03.5	28.2	01	-04.4	31	09	01.2	03	01.3	.	.	04	02.5	02	01.0	04	01.2	02	01.0	08	01.4	61
XI	702.6	00.5	06.6	01.8	02.7	08.1	-01.6	19.0	02	-17.5	26	06	01.2	04	01.2	.	.	03	02.0	03	03.3	01	04.0	.	06	01.3	67	
XII	705.4	-01.4	02.6	-00.5	00.1	03.5	-03.1	14.2	17	-04.7	08	11	01.5	01	01.0	.	.	03	03.0	01	02.0	01	01.0	11	01.3	65		
GOD.	702.5	05.2	13.4	07.2	08.2	14.8	02.7	33.2	M. VII	-17.9	26. XI	153	01.5	77	01.4	18	01.3	33	01.7	63	02.5	77	02.0	26	01.2	108	01.6	540
$\varphi = 41^{\circ}55' N \lambda = 19^{\circ}13' E$ Gr.ΔG = + 1h 17 min.																												
I	756.6	04.6	11.2	06.9	07.4	11.5	02.7	14.8	20	-01.8	05	01	02.0	28	02.6	47	02.2	03	02.0	05	02.2	.	04	02.0	04	02.0	01	
II	755.8	04.2	09.7	05.8	06.3	10.6	02.4	15.4	19	-03.6	09	.	.	29	02.9	45	02.8	04	03.2	.	01	01.0	02	02.5	02	02.0	01	
III	749.4	09.9	14.3	11.0	11.5	15.9	07.6	22.7	08	00.2	01	01	02.0	22	02.2	38	02.2	05	01.8	13	03.2	03	04.0	05	02.6	04	02.3	
IV	751.6	12.4	17.0	12.9	13.8	18.4	09.3	23.4	07	-03.4	13	04	02.2	16	02.3	26	01.9	04	01.5	04	03.2	04	02.2	14	03.0	17	02.9	01
V	750.9	17.2	21.7	16.8	18.1	23.0	14.2	25.6	18	10.4	01	02	02.5	17	01.9	27	01.9	04	01.8	02	01.5	.	.	18	02.3	22	01.9	01
VI	750.5	20.0	24.5	19.7	21.0	26.2	16.6	31.6	30	12.0	09	01	01.0	21	02.0	22	01.7	03	02.0	02	01.5	02	02.0	09	03.2	27	02.7	03
VII	750.4	22.9	27.8	22.7	24.1	29.5	19.1	34.6	19	12.3	02	01	04.0	19	02.0	25	01.9	01	01.0	01	02.0	02	01.5	16	02.8	25	02.7	03
VIII	751.3	22.1	27.3	22.2	23.4	29.0	19.0	31.4	11	17.0	21	.	.	17	01.9	36	01.9	01	02.0	03	01.3	03	01.7	12	02.1	27	02.7	02
IX	754.7	20.5	27.2	22.2	23.0	28.5	18.4	34.0	17	14.1	14	01	01.0	22	02.1	34	02.1	02	01.0	06	02.0	03	01.7	06	02.5	16	02.7	.
X	754.7	14.5	19.7	15.9	16.5	21.3	12.4	28.8	03.01	09.6	25	01	02.0	24	02.3	44	02.3	02	03.0	06	02.8	01	05.0	09	02.8	06	03.5	.
XI	753.6	09.5	13.1	10.2	10.8	14.5	07.3	20.7	03	-01.7	26	02	02.0	32	02.4	39	02.3	.	06	03.5	02	03.5	04	03.0	04	02.0	01	
XII	756.2	06.4	11.5	07.9	08.4	12.4	04.7	16.8	18	-01.3	21	.	.	36	02.7	50	02.6	02	02.5	01	02.0	02	01.5
GOD.	753.0	13.7	18.8	14.5	15.4	20.1	11.1	34.6	M. VIII	-03.6	09. II	14	02.1	283	02.3	433	02.2	31	02.0	50	02.6	22	02.4	101	02.6	147	02.6	13
SR MAKEDONIJA																												
$\varphi = 42^{\circ}01' N \lambda = 20^{\circ}53' E$ Gr.ΔG = + 1h 24 min.																												
I	-	-02.2	00.8	-01.7	-01.2	03.5	-04.5	13.0	17	-14.2	11	04	01.0	02	01.5	02	01.5	03	01.3	03	01.7	04	03.2	37	02.5	44		
II	-	-06.4	-03.6	-06.3	-05.6	-01.3	-09.3	06.9	06	-17.6	09	.	.	01	01.0	01	01.0	04	02.0	04	01.8	.	02	04.0	18	03.4	54	
III	-	-00.9	01.9	00.2	00.3	03.7	-02.9	10.0	31	-10.2	26	02	01.0	.	.	08	01.9	09	02.2	11	03.2	02	02.5	10	03.4	51		
IV	-	02.0	04.8	02.5	03.0	06.7</td																						

Mesec	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha		Padavine R mm				Broj dana na sa:																									
						U m s		R mm				Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	□	R	T	≡							
	7	14	21	Sred. (dies)		cm	mm	7	14	21	Sred. Hm	Hm	Σ	X	Dat.		≤	<	<	/N	/N	/N	/N	/N	<	>	/N	/N	/N	•	Δ	○	▲	□			
KLASIN																																					
BR. ST. 246																																					
I	5.2	5.0	3.7	4.6	-	133.9	03.2	90	60	86	78	23	046	020.9	29	13	03	31	-	-	02	-	11	07	11	08	01	04	09	01	-	-	-	01	31		
II	6.3	4.5	5.5	5.5	-	143.6	03.1	87	64	81	77	31	030	008.4	17	05	05	24	-	-	01	-	08	08	12	08	-	03	11	-	-	-	01	28			
III	8.0	8.3	6.4	7.6	-	108.3	04.6	87	63	86	79	27	210	056.7	13	01	01	16	-	-	01	-	03	18	21	14	04	17	08	-	-	-	01	09			
IV	6.5	6.7	4.7	6.0	-	168.8	05.5	84	60	82	75	26	231	054.6	11	-	-	06	-	-	02	-	07	12	14	16	07	14	06	01	-	-	01	01	01		
V	6.7	6.9	5.6	6.4	-	193.0	08.6	94	60	89	81	39	071	017.0	09	-	-	01	-	-	-	-	02	10	17	14	02	17	-	-	-	-	05	08			
VI	8.2	7.2	4.1	6.5	-	172.7	09.8	91	68	91	83	41	081	016.1	05	-	-	04	-	-	-	-	01	09	14	12	02	16	-	-	-	06	09				
VII	6.2	4.3	2.9	4.5	-	248.2	11.1	93	59	92	81	41	097	022.2	06	-	-	14	01	-	-	-	04	03	11	10	04	11	-	-	-	01	12				
VIII	7.3	7.1	5.8	6.7	-	173.2	10.5	93	65	92	83	33	129	046.8	28	-	-	07	-	-	-	-	02	14	14	13	04	16	-	-	-	08	06				
IX	6.6	4.0	1.3	3.9	-	231.9	09.7	95	57	95	82	33	016	006.8	04	-	-	07	05	01	-	-	04	02	05	04	-	05	-	-	-	04	16				
X	7.9	6.5	5.6	6.7	-	125.2	06.4	92	65	91	83	30	372	166.7	13	-	-	07	02	-	-	-	01	04	15	17	19	06	17	-	-	-	03	06			
XI	8.1	7.3	6.2	7.2	-	090.2	04.9	94	69	92	85	38	197	041.4	19	03	05	19	-	-	-	-	02	01	17	17	14	05	14	-	-	-	01	04			
XII	7.4	4.7	3.8	5.3	-	112.7	04.1	92	70	80	84	33	070	053.7	18	01	02	27	-	-	-	-	01	01	04	08	07	03	01	06	-	-	04				
GOD.	7.0	6.0	4.6	5.9	-	1901.7	06.8	91	63	88	80	23	1550	166.7	BR. ST. 246	20.X	23	16	131	34	02	-	10	02	57	123	164	131	36	142	39	02	-	01	03	39	71
IVANGRAE																																					
BR. ST. 247																																					
I	9.5	5.5	5.8	7.0	-	03.0	89	73	88	83	38	026	006.7	09	14	05	31	-	-	-	01	03	12	11	05	03	09	-	-	-	02	36					
II	7.9	5.9	5.6	6.4	-	03.1	85	58	77	73	37	010	001.8	04	03	02	27	-	-	-	01	03	13	09	05	02	07	-	-	-	02	03					
III	7.5	8.5	7.5	7.9	-	04.6	84	49	75	69	17	034	015.5	15	-	-	18	-	-	-	11	03	01	19	12	07	01	09	04	01	-	02	03				
IV	7.5	6.9	6.8	7.1	-	05.4	82	49	68	66	20	065	011.9	11	-	-	05	-	-	-	10	03	05	14	11	02	14	05	03	-	-	02	03				
V	7.1	7.8	6.7	7.2	-	08.6	89	51	80	74	34	068	010.3	27	-	-	01	-	-	-	01	-	13	17	15	01	17	-	-	-	01	05					
VI	6.6	7.8	6.5	7.0	-	10.2	86	56	86	76	29	085	020.5	26	-	-	10	-	-	-	02	10	12	08	04	12	-	-	-	01	11	00					
VII	5.9	5.8	5.1	5.6	-	10.9	85	49	81	72	28	051	017.3	31	-	-	17	03	02	-	02	04	07	10	07	02	10	-	-	03	04	04					
VIII	8.1	7.3	6.5	7.3	-	11.0	94	59	88	80	20	077	013.1	26	-	-	09	-	-	-	02	-	13	19	15	01	19	-	-	-	01	08	10				
IX	6.3	4.5	3.2	4.7	-	09.8	98	49	87	78	27	023	011.4	13	-	-	11	-	-	-	03	01	06	05	01	06	-	-	-	03	13						
X	8.7	6.5	5.9	7.0	-	06.8	93	60	89	81	36	024	027.7	13	-	-	07	02	-	-	01	14	19	14	07	19	-	-	-	01	11	00					
XI	9.6	7.8	7.1	8.2	-	04.9	90	72	88	83	41	093	024.3	20	03	04	18	-	-	03	02	-	19	14	11	03	11	04	01	-	01	01	13	03			
XII	9.3	7.1	7.2	7.8	-	04.0	89	74	88	84	47	019	013.3	18	04	04	27	-	-	01	-	19	06	03	01	04	01	-	-	-	01	13	03				
GOD.	7.8	6.8	6.2	6.9	-	06.9	88	58	82	76	17	733	042.7	BR. ST. 247	20.X	20	17	133	50	03	-	32	08	18	155	147	106	23	123	33	08	-	-	07	41	103	
ULCINJ																																					
BR. ST. 248																																					
I	3.8	2.9	2.2	3.0	-	197.0	05.1	71	55	69	65	26	032	019.0	29	-	-	03	-	-	-	01	-	15	02	05	04	01	05	-	-	-	01	03			
II	4.2	4.1	2.9	3.7	-	162.1	04.3	63	52	59	58	25	109	060.4	15	-	-	03	-	-	-	06	-	15	04	07	05	02	07	-	-	-	01	04			
III	7.6	7.5	6.2	7.1	-	098.6	07.3	73	64	77	71	29	099	018.8	15	-	-	17	-	-	-	06	02	03	11	14	12	04	14	-	-	-	01	04			
IV	4.8	4.0	4.0	4.6	-	233.7	07.9	70	59	69	66	30	048	014.4	03	-	-	05	-	-	-	05	04	07	10	07	01	10	-	-	-	01	05				
V	5.2	4.8	3.6	4.5	-	249.4	12.0	79	77	75	75	43	064	028.5	27	-	-	09	-	-	-	01	06	04	08	04	08	-	-	-	01	08					
VI	3.7	4.0	3.9	3.8	-	299.4	14.0	76	65	78	73	35	027	010.1	17	-	-	21	02	02	03	01	12	02	06	04	01	06	-	-	-	02	04				
VII	1.7	1.6	1.5	1.6	-	381.1	14.8	68	57	70	65	40	044	017.3	02	-	-	27	17	14	02	-	22	-	04	04	02	04	-	-	-	04	04				
VIII	4.1	3.1	2.5	3.2	-	307.2	13.7	65	55	68	63	27	088	003.4	25	-	-	31	08	10	-	11	-	05	03	03	05	-	-	-	03	05					
IX	1.7	2.3	1.3	1.8	-	278.4	14.2	70	60	71	67	37	026	017.8	13	-	-	30	06	06	02	-	22	01	05	03	01	05	-	-	-	01	01				
X	4.7	4.5	4.3	4.5	-	204.2	09.5	71	62	68	67	24	293	093.7	20	-	-	05	-	-	04	02	09	05	14	14	11	14	-	-	-	02	12				
XI	6.3	6.4	5.2	6.0	-	119.8	07.1	73	65	73	70	36	262	084.9	17	03	04	24	-	-	05	02	04	10	13	12	07	13	-	-	-	02	07				
XII	4.5	4.1	3.5	4.0	-	172.9	05.9	75	60	72	69	29	062	036.5	18	06	05	25	-	-	16	05															

Mjesec	Vrstdište Pm. MM	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Pm (0-12)																	
		Tm	7	14	21	Sred. (Dnev.)	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C	č.	j.	č.	j.					
												č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.					
$\varphi = 42^{\circ}08' N \lambda = 21^{\circ}43' E$ Gr. $\Delta G = + 1h 27 min.$																													
I	-	-02.9	02.3	-00.7	-00.5	03.2	-03.6	08.9	29	-06.8	16.11	20	03.6	10	02.4	03	01.0	31	01.0	02	01.0	02	01.0	02	01.0	06	02.3	17	
II	-	-02.2	05.4	00.1	00.8	06.4	-02.7	12.2	14	-05.2	11	32	03.6	11	02.2	05	02.0	16	01.1	03	01.0	02	01.0	01	01.0	14	02.1	.	
III	-	03.3	14.0	08.2	08.4	14.6	01.3	22.2	31	-05.6	03	12	02.5	01	01.0	06	01.0	30	01.5	22	02.2	06	02.0	03	01.0	13	02.4	.	
IV	-	07.9	17.2	11.3	11.9	18.5	05.8	28.0	08	00.0	13	35	03.6	04	02.2	.	.	15	01.5	19	01.6	08	02.4	01	01.0	06	02.0	02	
V	-	14.5	22.1	16.1	17.2	22.9	10.9	30.2	31	05.7	01	21	01.8	11	01.5	09	01.6	12	01.2	16	01.8	05	01.0	10	01.0	09	01.3	.	
VI	-	17.2	25.4	19.1	20.2	24.6	14.7	32.6	02	08.6	06	29	02.0	09	02.0	05	01.0	08	01.5	01	02.0	05	01.6	06	01.0	27	02.0	.	
VII	-	19.1	27.4	20.6	21.9	28.2	15.0	34.1	19	11.5	03	35	02.5	05	01.2	.	.	02	04.5	06	01.5	08	02.2	03	01.0	34	02.4	.	
VIII	-	17.7	27.1	19.9	21.1	27.9	15.5	32.0	17	11.0	16	37	02.4	12	02.1	.	.	06	01.2	04	02.2	08	01.8	01	01.0	25	01.8	.	
IX	-	14.5	27.2	19.0	19.9	27.8	12.6	32.0	16	08.0	11	26	01.8	13	01.5	03	01.0	10	01.3	09	01.3	09	01.2	05	01.0	14	01.3	01	
X	-	08.6	17.2	11.3	12.1	17.8	07.0	28.8	01	-01.0	09	20	02.8	11	01.8	.	.	05	01.9	08	02.2	09	01.2	10	01.2	24	02.3	02	
XI	-	04.4	08.7	05.8	06.2	10.1	02.7	17.8	01	-12.8	28	18	02.2	06	01.5	.	.	25	01.2	20	02.1	03	01.0	03	01.0	13	G2.3	02	
XII	-	-00.5	05.9	01.8	02.2	06.4	-01.5	14.0	03	-06.4	24	31	03.4	07	01.9	01	01.0	18	01.3	12	01.2	09	01.4	.	.	12	02.2	03	
600.	-	08.5	16.7	11.0	11.8	17.6	06.5	34.1	49.VII	-12.8	28.IX	31.6	02.7	100	01.9	32	01.3	182	01.3	122	01.8	74	01.6	45	01.0	197	02.1	27	
$\varphi = 42^{\circ}05' N \lambda = 22^{\circ}09' E$ Gr. $\Delta G = + 1h 29 min.$																									KRATOVAC		BR. ST. 251		
I	-	-02.0	03.6	00.6	00.7	05.0	-04.8	09.5	07	-05.3	22	06	01.5	16	01.4	15	01.4	07	01.7	04	01.0	15	01.9	02	02.5	11	02.1	17	
II	-	-02.2	04.4	00.5	00.8	05.5	-04.3	11.5	15	-11.7	10	06	01.8	10	02.2	11	01.5	05	02.0	03	01.0	04	01.8	03	01.7	08	02.5	34	
III	-	05.2	12.3	07.3	08.0	13.5	02.0	20.2	31	-03.6	26.4	04	01.8	03	02.3	10	01.7	25	02.5	05	01.2	08	02.1	02	01.5	05	01.8	31	
IV	-	09.2	15.9	11.0	11.8	17.4	05.2	25.2	07	-00.3	12	04	01.8	02	03.0	04	01.0	18	02.7	02	02.5	04	01.5	12	01.7	14	02.7	30	
V	-	13.8	20.4	16.0	16.6	21.5	08.8	27.2	23	03.8	01	02	01.0	03	01.3	14	01.1	06	02.5	07	01.0	15	01.9	12	01.5	06	01.8	28	
VI	-	14.0	23.6	17.8	18.8	25.2	12.6	30.3	02	07.5	07	02	02.5	01	01.0	16	01.2	05	01.2	04	01.0	06	01.3	10	01.7	07	02.0	35	
VII	-	18.3	26.3	20.1	21.2	27.6	14.6	33.2	15	09.0	03	.	.	.	15	01.2	05	01.2	03	01.0	11	01.6	04	01.5	06	02.2	16	01.9	35
VIII	-	17.6	24.9	19.4	20.4	26.6	13.1	31.2	17	08.5	15	01	02.0	02	02.0	15	01.5	18	01.6	04	01.0	08	02.0	05	01.4	04	01.0	34	
IX	-	15.7	25.4	18.6	19.6	26.5	11.3	30.5	17	07.2	11	.	.	15	01.7	20	01.5	18	01.3	04	01.0	01	01.0	04	01.5	02	01.5	26	
X	-	09.0	16.0	10.5	11.7	17.0	06.0	26.2	01	-01.0	26	03	02.0	07	01.9	19	01.4	12	01.6	04	01.0	07	01.7	07	01.7	10	01.9	22	
XI	-	03.8	08.4	05.4	05.8	09.4	01.6	17.1	18	-09.5	26	04	01.5	07	02.0	10	01.7	07	01.9	16	01.9	08	01.8	11	01.9	17	01.9	23	
XII	-	-00.1	05.0	02.1	02.3	06.3	-02.6	10.7	18	-08.2	22	12	02.2	06	01.7	03	01.0	09	01.7	04	01.0	.	.	27	01.9	09	02.3	23	
600.	-	08.7	19.5	10.8	11.5	16.8	05.3	33.2	49.VII	-11.7	40.II	44	01.9	72	01.8	154	01.4	142	01.9	53	01.2	95	01.8	108	01.7	93	02.1	334	
$\varphi = 42^{\circ}12' N \lambda = 22^{\circ}20' E$ Gr. $\Delta G = + 1h 25 min.$																									KRIVA PALANKA		BR. ST. 253		
I	704.7	-03.0	03.7	-01.9	-00.8	04.7	-04.3	09.8	07	-05.8	04	.	.	58	03.4	16	02.1	01	02.0	.	.	.	18	
II	704.5	-03.4	03.2	-01.3	-00.7	04.4	-04.2	10.4	15	-10.6	09	.	.	56	03.5	13	02.8	.	.	01	03.0	.	14		
III	698.5	03.1	12.1	04.2	06.9	13.4	02.1	22.3	31	-04.1	01	.	.	49	03.3	.	.	03	06.7	26	03.3	01	03.0	.	.	.	14		
IV	700.1	07.4	15.5	09.2	10.3	16.0	05.1	25.3	06	00.0	13	02	04.0	42	02.9	.	.	01	05.0	02	04.0	18	03.8	.	.	06	04.3	19	
V	700.2	12.6	20.1	13.3	14.8	21.3	09.4	26.0	31	04.6	01	.	.	52	03.0	.	.	02	01.5	.	.	21	03.2	.	.	02	04.0	16	
VI	700.4	15.5	22.3	15.8	17.4	23.6	12.3	29.8	02	07.5	06	.	.	57	03.2	02	03.0	.	.	.	12	03.3	02	03.5	03	03.7	14		
VII	701.1	17.3	24.6	17.5	19.2	26.1	13.7	32.7	19	08.7	03	.	.	65	03.4	.	.	10	03.4	.	.	02	02.3	16	01.9	07	07		
VIII	701.8	18.0	23.9	18.4	18.4	25.4	13.3	29.8	18	09.4	15	01.0	68	03.3	01	04.0	01	02.0	.	.	12	03.3	01	03.0	02	03.0	07		
IX	705.4	13.7	24.7	15.7	17.4	25.7	11.7	25.2	03	06.3	11	.	.	65	03.6	02	05.5	.	.	.	16	03.4	07		
X	704.4	07.4	15.3	09.0	09.6	16.4	06.1	26.6	01	00.5	26	01	03.0	64	03.5	01	02.0	.	.	.	03	05.3	17	03.0	01	04.0	.		
XI	703.4	02.7	07.0	03.4	04.1	08.0	01.3	18.0	18	-09.3	26	04	01.5	07	02.0	10	01.7	07	01.9	08	04.0	08	02.9	.	02	02.0	18		
XII	705.2	-01.1	04.2	06.0	06.8	05.1	-02.3	11.2	18	-09.6	22	01	01.0	51	03.2	15	02.7	01	04.0	.	.	25		
600.	702.5	07.4	14.7	08.6	09.8	15.9	05.4	32.7	49.VII	-10.4	09.II	05	02.6	685	03.3	06	03.8	04	02.5	12	05.7								

Mesec	Oblačnost Nm (0-10)				Insolacija broj sati em mm	Vlažnost vazduha				Padavine R mm	Broj dana na sat:																															
	7	14	21	Sted. (Dnes)		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ	R	T	≡																	
						mm	7	14	21	Sred. Mln	Max	Dat.	=	<	<	=	=	=	=	<	>	=	=	=	=																	
KUMANOVC																																										
BR. ST. 251																																										
I	9.1	6.9	5.9	7.3	-	03.5	92	82	85	86	48	006	004.1	09	.	04	27	.	.	04	.	01	14	02	02	.	02	17	06								
II	4.4	4.2	3.2	3.9	-	03.8	86	65	79	77	35	003	001.2	17	.	01	21	.	.	05	01	12	06	04	02	.	04	03	02	01	.	01						
III	3.6	3.5	3.5	4.2	-	05.5	64	48	70	67	22	052	016.6	15	.	09	.	.	03	.	10	06	08	06	02	08	02	02	.	01							
IV	5.0	5.8	3.8	4.9	-	06.3	78	46	62	62	09	023	008.3	02	.	.	03	.	10	11	09	12	06	12	06	01	.	.									
V	5.2	6.3	4.9	5.5	-	10.2	83	52	75	70	26	092	024.8	16	.	.	.	14	01	.	01	03	08	14	13	03	14	05	.	.							
VI	4.7	5.2	5.2	5.0	-	11.5	81	48	69	66	33	052	016.6	21	.	.	21	10	.	01	05	06	13	09	01	13	01	01	04								
VII	2.7	3.8	3.3	3.3	-	12.0	75	43	66	61	28	052	042.5	14	.	.	27	10	.	04	01	09	01	04	04	01	04	01	01	06							
VIII	4.3	3.5	4.0	3.9	-	11.8	81	42	69	64	27	014	004.6	08	.	.	24	12	.	04	09	02	08	05	04	08	.	.									
IX	0.7	1.9	2.7	1.7	-	10.5	86	37	67	63	04	020	011.5	14	.	.	27	03	.	20	01	04	03	01	04	03	.	.									
X	5.7	4.9	3.8	4.8	-	07.9	88	59	76	75	30	078	021.5	17	.	.	01	02	.	04	07	07	14	11	03	14	02	01	.								
XI	8.1	7.7	6.4	7.4	-	05.9	87	74	80	80	37	042	016.8	20	03	01	08	.	01	03	14	11	04	01	08	03	01	04	.								
XII	5.9	4.5	4.0	4.8	-	04.7	90	80	85	85	62	014	005.2	18	.	01	19	.	05	02	10	10	06	03	04	04	05	.	.								
GOD. 5.0				5.0	4.2	4.7	-					07.8	84	56	73	71	04	448	042.5	#xv	03	07	85	118	38	.	45	05	100	86	100	70	12	97	08	02	.	01	01	36	24	12
KRATOVAC																																										
BR. ST. 252																																										
I	4.0	3.1	3.5	3.5	-	03.7	83	67	79	76	41	031	018.3	26	.	03	31	.	.	09	01	04	04	01	01	03	03	10	.	.							
II	4.5	3.4	4.6	4.2	-	03.8	80	72	76	76	11	016	007.0	18	03	02	26	.	.	08	02	07	04	04	04	01	04	03	.	.							
III	4.5	3.1	4.4	4.0	-	05.8	76	43	74	71	35	108	024.6	11	.	07	.	.	09	05	11	11	04	11	02	01	.	.	.	04	01	.	.									
IV	4.5	3.4	4.2	4.0	-	06.5	66	56	63	62	20	014	004.1	23	.	01	02	.	.	12	06	09	05	04	04	04	.	.									
V	4.0	2.9	4.9	3.9	-	09.7	76	61	67	68	38	070	014.4	16	.	.	04	.	01	02	10	09	04	10	02	01	.	.									
VI	4.0	3.4	6.0	4.5	-	11.7	79	61	72	71	26	144	034.5	28	.	.	20	01	.	05	02	14	10	04	14	04	.	.									
VII	2.8	2.7	3.2	2.9	-	13.4	79	59	70	70	24	020	010.1	11	.	.	27	05	.	10	06	05	01	06	02	01	.	.									
VIII	2.6	3.1	5.0	3.6	-	12.0	75	57	68	67	32	015	004.8	30	.	.	21	07	.	04	01	06	04	04	04	04	.	.									
IX	1.4	2.6	3.7	2.6	-	11.1	76	52	65	64	31	038	022.4	14	.	.	24	02	.	12	06	03	02	06	01	.	.										
X	4.5	4.4	5.0	4.6	-	07.9	84	64	75	75	23	105	038.4	18	.	01	02	.	07	04	11	11	03	11	01	03	.	.									
XI	8.0	5.8	6.8	6.9	-	05.7	86	72	78	78	18	096	045.0	20	.	01	08	.	01	09	10	08	03	09	01	06	05	.	.								
XII	4.9	3.9	4.2	4.3	-	04.7	90	80	85	85	57	021	008.4	19	.	26	.	.	08	04	04	04	04	04	02	05	.	.									
GOD. 4.1				3.5	4.6	4.1	-					08.0	79	63	72	71	11	678	045.0	#xi	03	03	100	104	15	.	01	.	07	37	98	78	24	91	12	02	.	.	14	31	19	
KRIVA PALANKA																																										
BR. ST. 253																																										
I	5.0	5.0	2.3	4.2	-	150.2	03.3	79	60	82	73	26	028	013.0	01	.	03	30	.	.	05	.	13	06	05	03	01	02	05	02	.	.	04	19	.	.						
II	5.4	5.7	4.5	5.1	-	142.9	03.1	78	57	73	65	34	008	003.1	27	02	01	25	.	.	03	.	09	08	07	04	03	09	01	.	.	01	.	.	02	.	.					
III	5.8	6.7	4.0	5.5	-	165.2	04.0	79	49	68	65	26	072	024.0	22	.	.	06	.	.	03	01	06	11	11	08	03	10	05	03	.	.	01	01	.	02						
IV	6.3	6.1	3.5	5.3	-	207.3	05.4	71	42	61	58	17	027	006.6	28	.	.	01	.	.	06	03	06	08	13	07	.	13	.	.	.	01	.	.								
V	4.1	6.2	4.7	5.7	-	234.1	09.1	82	54	79	72	32	093	013.8	16	.	.	03	.	.	05	.	02	07	14	13	05	19	.	.	.	01	16	.	.							
VI	5.3	4.0	6.0	6.0	-	221.4	10.7	79	55	78	71	36</td																														

Mjesec	Vadudan pritisak Pa	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																		
		Tm		Sred. (Dnev.)	Max	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C														
		7	14	21																										
$\varphi = 41^{\circ}32' N \lambda = 20^{\circ}42' E$ Gr.ΔG = + 1h 23 min.																														
I	652.6	-03.7	02.8	-02.9	-01.6	04.5	-05.1	13.6	16	-14.1	10	11	C2.2	G9	01.9	18	01.6	08	02.1	04	01.8	04	C1.8	10	02.1	11	01.9	18		
II	651.6	-05.9	00.1	-04.4	-03.6	01.3	-07.2	06.7	06	-14.1	05	10	C2.6	G15	02.1	09	C2.1	02	01.5	02	03.5	10	02.8	09	02.8	11	02.5	16		
III	647.7	00.8	06.6	02.6	03.2	07.9	-00.6	17.2	31	-05.6	26	06	C2.3	G14	02.2	25	C2.3	11	02.9	09	02.7	05	02.4	12	02.2	04	02.8	07		
IV	650.0	03.9	09.4	05.0	05.8	11.2	01.3	20.6	06	-03.9	12	11	C2.8	G18	02.3	10	C2.5	09	02.8	09	03.2	03	03.0	11	03.1	05	03.6	14		
V	650.6	09.5	14.5	09.9	10.9	15.9	05.7	20.7	30	00.6	02	05	C3.0	G17	01.6	12	C1.9	06	02.3	03	01.3	04	02.8	07	02.7	11	02.3	28		
VI	651.1	12.1	17.4	11.7	13.2	18.5	05.1	24.8	02	03.4	06	19	C1.8	G04	02.0	18	C1.4	11	01.6	05	02.2	01	03.0	12	02.0	12	02.7	18		
VII	652.3	13.5	20.4	14.2	19.6	21.7	04.6	29.3	19	04.2	03	09	C2.4	G04	02.2	19	C1.8	19	C1.5	03	02.3	02	01.5	03	03.3	16	03.2	18		
VIII	652.6	12.2	19.5	13.2	14.5	20.7	09.3	25.1	17	05.7	21	08	C2.6	G16	01.9	13	C1.8	07	01.9	•	•	05	02.2	12	03.0	04	03.0	27		
IX	655.0	11.2	20.7	12.8	14.4	21.9	09.0	28.7	16	06.4	26	19	C16	G16	02.1	08	02.0	15	C1.7	09	C2.1	08	02.5	05	02.8	10	03.1	05	03.0	14
X	653.7	09.0	11.4	06.0	07.1	12.7	07.7	23.5	01	-00.9	25	25	C2.0	G10	02.3	03	02.0	03	03.3	07	02.7	11	02.5	11	02.2	09	02.1	21	02.7	18
XI	651.2	00.5	04.7	01.2	01.9	06.2	-00.9	14.7	03	-13.6	25	15	C2.5	G09	02.3	07	C2.6	04	02.0	09	01.8	06	02.2	14	01.7	17	02.6	09		
XII	652.9	-02.3	03.4	-00.9	-00.2	04.7	-03.7	12.7	23	-13.2	21	03	C1.7	G02	01.0	09	01.4	15	01.9	08	02.2	16	01.4	21	02.0	05	02.4	14		
600.	651.8	04.7	10.9	05.7	06.8	12.3	02.5	29.3	49.1	-14.1	09	11	C18	G2.3	126	02.0	158	01.9	104	02.1	67	02.4	72	02.2	123	02.4	110	02.6	107	
$\varphi = 41^{\circ}42' N \lambda = 20^{\circ}45' E$ Gr.ΔG = + 1h 23 min.																														
I	-	-03.6	03.6	-02.0	-01.0	04.6	-05.4	13.6	18	-11.5	10	•	•	25	C3.6	•	•	•	•	•	16	C2.9	•	•	•	49				
II	-	-07.0	-06.8	-04.4	-04.1	01.0	-08.1	10.4	07	-17.6	04	•	•	29	C2.8	•	•	•	•	•	08	C2.6	•	•	•	47				
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VIII	-	13.1	18.2	13.4	14.5	19.6	09.1	24.8	19	07.0	30	•	•	05	C3.2	02	01.5	•	•	06	C2.0	01	01.0	25	C2.0	•	•	54		
IX	-	13.4	19.3	13.2	14.8	20.7	08.9	25.0	16	07.0	19	•	•	07	C1.9	•	•	04	01.5	18	C3.2	19	C1.8	•	•	42				
X	-	06.0	10.4	08.5	07.3	12.0	04.2	21.0	01	01.0	31.0	•	•	03	C3.3	02	01.0	07	01.7	37	C3.4	05	C1.8	03	04.0	36				
XI	-	00.6	04.2	01.3	01.9	05.6	-00.5	14.0	18	-13.2	25	•	•	02	C3.5	•	•	05	03.8	07	01.7	41	C2.7	06	01.8	04	03.2	25		
XII	-	-01.0	02.6	-00.7	-00.2	04.1	-03.4	13.0	04	-11.7	22	•	•	11	C2.9	01	01.0	03	03.7	04	01.2	19	C2.5	05	01.0	01	06.0	49		
600.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 41^{\circ}07' N \lambda = 20^{\circ}48' E$ Gr.ΔG = + 1h 23 min.																														
I	698.0	-01.0	04.2	00.3	01.0	04.8	-02.2	04.4	26	-06.4	05	45	C2.1	G04	C1.8	C2	C3.5	•	•	09	C1.9	12	C0.3	01	01.0	11	01.7	09		
II	698.0	-01.2	04.8	00.8	01.3	03.0	-02.9	11.6	15	-09.4	09	36	C2.5	G07	C3.0	C0.6	C3.7	15	C2.2	04	C2.0	02	02.2	05	02.2	03	02.2	03		
III	692.9	03.5	11.1	06.9	07.1	12.3	02.2	20.3	31	-04.2	01	23	C1.7	G02	C1.0	C0.2	C2.0	06	C3.2	26	C2.5	14	C2.2	03	01.7	10	01.6	07		
IV	694.8	06.9	13.6	09.6	10.0	15.6	04.5	22.8	06	-00.8	12	23	C2.3	G03	C1.7	C0.3	C2.0	01	C2.0	23	C2.5	03	C2.0	05	01.8	12	01.7	09		
V	695.0	12.3	19.1	14.0	14.9	20.4	09.2	26.3	31	04.9	10	17	C1.8	•	•	02	C1.5	02	01.0	02	01.0	26	C2.0	12	C1.9	05	C1.8	03		
VI	695.1	15.5	22.1	16.8	17.8	23.5	11.8	29.6	30	06.6	06	19	C2.0	02.0	02	01.5	02	01.0	02	01.0	26	C2.0	12	C1.9	05	C1.8	03			
VII	695.5	17.6	24.6	19.5	20.3	26.4	14.4	31.7	19	07.2	03	32	C1.9	03	02.0	•	•	02	C1.5	21	C1.9	11	C2.3	05	C2.4	06	C1.3	13		
VIII	696.2	15.9	24.8	19.0	19.7	26.4	13.3	30.4	17	10.0	21	42	C2.3	04	C1.8	02	C2.5	•	•	18	C2.1	11	C1.9	05	C2.6	08	C1.8	03		
IX	699.0	14.5	24.6	18.1	18.9	25.9	12.8	31.3	17	10.2	27	38	C1.9	02	C3.0	C3	C2.3	01	C1.0	18	C1.9	11	C1.9	03	C2.3	10	C1.4	04		
X	698.5	08.4	15.8	10.3	11.2	18.9	07.0	25.7	01	02.4	27	37	C2.2	04	C2.0	01	C2.0	04	04.5	13	C2.0	08	C2.0	04	02.5	16	01.7	06		
XI	697.0	04.6	09.5	05.3	06.1	10.1	02.9	17.7	01	-07.0	26	27	C2.2	08	C1.4	02	C2.0	06	C2.8	18	C3.0	09	C1.4	04	01.8	09	02.0	07		
XII	699.0	01.0	04.0	02.3	02.9	06.8	-00.5	12.1	17	-07.2	21	36	C2.2	08	C1.8	02	C2.0	04	C3.2	10	C2.1	05	C1.4	12	01.7	11	01.7	11		
600.	696.7	08.2	15.0	10.3	10.9	16.3	06.0	31.7	49.1	-06.9	09	11	C375	G2.1	47	02.0	25	02.5	31	02.8	224	02.2	134	01.9	43	02.0	99	01.7	117	
$\varphi = 41^{\circ}48' N \lambda = 20^{\circ}55' E$ Gr.ΔG = + 1h 24 min.																														
I	-	-04.2	03.0	-01.0	-01.2	04.6	-07.0	09.3	25	-06.9	24	23	08	C2.5	04	02.2	•	•	02	03.0	•	•	01	07.0	•	•	06	02.5	72	
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	19.1	24.7	18.4	20.2	26.1	14.0	31.2	19	09.3	04	05	C2.0	06	C3.2	•	•	•	02	04.0	04	06.5	•	•	11	C2.7	65			
VIII	-	17.6	24.6	18.5	19.8	27.2	13.7	31.0																						

Meseč	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																
		Tm			Max	Min	Max	Dat.	Min	Dat.		N	NE	E	SE	S	SW	W	NW	C								
		7	14	21	Sred. (Dnes)							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.				
$\varphi = 41^{\circ}05' N \lambda = 21^{\circ}01' E$ Gr. $\Delta G = + 1h 24 min.$																												
I	-	-04.6	00.9	-01.8	-01.8	02.6	-07.2	05.0	12.11	-16.0	05	10	C2.2	07	02.6	C3	02.0	C1	01.6	C6	C1.3	03	01.3	02	01.0	02	02.5	39
II	-	-02.8	03.1	-01.1	-00.5	04.4	-04.4	05.2	15	-12.4	06	11	01.4	07	02.1	12	02.3	06	02.8	07	01.1	10	01.7	05	02.6	02	03.0	24
III	-	01.3	10.3	04.5	05.2	11.7	00.5	19.4	31	-06.5	02	12	01.5	05	01.8	C3	02.3	04	02.5	G9	C2.1	08	02.0	04	01.8	07	02.0	41
IV	-	06.2	13.8	08.2	09.1	15.2	03.1	22.5	06	-03.6	12	09	01.6	13	01.8	06	01.7	04	01.2	G8	01.9	12	02.0	08	03.0	01	02.0	29
V	-	11.4	18.4	12.2	13.6	19.6	07.0	25.7	30	02.6	10	11	01.2	07	01.6	C7	01.9	07	01.6	07	02.0	03	01.3	04	01.5	40		
VI	-	15.0	21.6	19.0	16.6	23.1	10.7	25.5	30	05.2	06	06	01.2	13	01.5	06	02.0	04	01.0	05	01.8	03	02.7	G5	01.0	03	02.0	45
VII	-	16.8	23.8	17.0	18.6	25.5	11.5	32.0	19	05.3	04	09	01.0	18	01.3	C9	02.0	07	01.4	02	01.0	01	01.0	06	02.2	40		
VIII	-	14.8	23.1	16.7	17.8	24.3	08.6	29.1	19	05.2	30	05	01.0	22	01.9	07	01.4	03	01.3	06	01.5	06	01.8	02	03.5	03	01.3	39
IX	-	12.6	23.9	15.2	16.7	25.0	08.1	29.6	16	03.2	24	06	01.3	13	02.0	10	01.5	05	01.8	03	01.7	07	01.6	01	02.0	05	01.8	40
X	-	06.3	14.8	08.0	09.3	16.0	02.9	24.2	01	-02.3	30	10	01.1	10	02.2	07	01.6	05	02.0	09	02.2	08	02.2	02	01.0	01	03.0	41
XI	-	02.9	07.7	04.1	04.7	09.0	-00.5	17.3	01	-15.5	26	07	01.1	08	01.9	18	02.2	02	02.5	10	01.5	08	01.8	03	01.3	03	01.7	31
XII	-	-00.3	04.9	01.1	01.7	05.9	-03.6	11.2	04	-12.2	22	09	01.3	11	02.2	16	02.0	02	01.0	03	02.0	04	01.5	.	01	01.0	07	47
600.	-	06.6	13.9	08.3	09.2	15.2	03.1	32.0	M9VW	-16.0	05.1	105	01.4	134	01.9	104	01.9	50	01.8	75	01.7	77	01.9	36	02.0	38	02.0	476
$\varphi = 41^{\circ}31' N \lambda = 21^{\circ}13' E$ Gr. $\Delta G = + 1h 25 min.$																									MAKEDONSKI BROD		BR. ST. 261	
I	-	-06.4	05.7	-05.1	-02.7	05.9	-07.4	10.0	20	-12.4	05	03	C6.0	.	.	C1	02.0	01	02.0	02	02.0	86
II	-	-04.8	06.2	-02.7	-01.0	06.5	-06.6	12.6	15	-13.6	10	02	03.0	.	.	C8	02.0	01	02.0	02	02.0	78
III	-	02.5	13.7	05.9	07.0	14.3	00.2	21.6	31	-11.0	01	01	C4.0	.	.	C2	04.0	07	C3.7	83		
IV	-	06.4	16.8	10.1	10.8	17.6	03.8	25.2	08	-02.6	12	07	04.9	.	.	C1	02.0	04	04.0	01	04.0	02	04.0	01	04.0	.	74	
V	-	11.0	22.3	13.3	15.0	22.6	08.6	29.6	31	02.0	01	07	02.3	02	02.0	.	.	01	06.0	.	.	83	
VI	-	14.2	24.9	18.3	17.9	25.5	10.8	31.8	02	04.8	08	02	C5.0	.	.	06	02.0	02	09.0	.	.	80	
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	13.3	26.8	16.4	18.2	27.3	08.8	32.0	16	05.0	27	02	02.0	.	.	.	08	02.0	03	02.0	77	
X	-	07.1	17.5	09.4	10.9	18.1	03.0	27.0	02	-04.4	27	02	03.0	91	
XI	-	02.4	09.9	03.9	05.0	10.2	01.3	19.2	01	-10.0	26	01	02.0	.	.	03	02.7	01	04.0	85		
XII	-	-02.8	05.9	-01.4	00.0	05.7	-03.8	11.0	03	-10.2	22	02	C3.0	.	.	01	02.0	01	02.0	09			
600.	-	07.0	11.4	07.6	08.4	12.5	04.6	28.0	M9VW	-12.3	09.11	26	03.7	443	02.3	162	01.7	109	02.7	33	03.0	91	03.4	61	03.8	73	03.7	77
$\varphi = 41^{\circ}22' N \lambda = 21^{\circ}15' E$ Gr. $\Delta G = + 1h 25 min.$																								KRUŠEVAC		BR. ST. 263		
I	-	-01.4	03.5	-00.6	00.3	04.4	-03.1	12.0	18	-10.0	04	03	C3.7	45	02.2	12	01.9	C1	01.0	C1	02.0	04	02.8	02	03.5	12	03.5	13
II	-	-04.3	00.2	-03.0	-02.5	01.3	-05.8	05.3	07	-12.3	09	02	02.5	47	02.6	13	02.1	C2	02.5	.	04	03.5	01	04.0	11	04.1	04	
III	-	02.4	07.4	04.2	04.6	08.4	01.1	17.0	31	-04.8	28	02	03.0	12	02.3	16	02.1	22	02.8	05	04.0	10	03.3	13	04.0	08	04.0	05
IV	-	06.3	10.7	06.9	07.7	12.0	03.4	15.9	06	-01.4	12	05	0.0	29	03.5	12	02.4	11	03.3	02	05.2	09	04.4	04	04.5	01		
V	-	12.0	16.0	11.8	12.9	17.0	08.7	23.4	31	04.0	03	01	C3.0	39	02.3	11	01.7	09	03.2	03	04.0	09	02.8	09	03.1	07	04.1	05
VI	-	15.0	19.1	14.2	15.6	20.0	11.2	26.0	02	03.3	04	03	05.7	35	02.6	16	01.9	09	02.6	02	03.0	11	03.5	04	04.8	09	03.4	01
VII	-	16.7	20.8	16.2	17.5	22.1	12.6	28.0	19	07.0	02	03	C2.3	41	02.1	16	01.5	06	02.0	03	02.3	09	02.9	04	05.0	06	02.3	05
VIII	-	15.4	20.3	15.9	16.6	21.4	12.4	26.8	18	08.2	21	04	03.5	46	02.4	15	01.5	06	03.5	04	03.2	05	02.8	03	03.0	08	04.6	02
IX	-	14.9	20.9	15.3	16.6	21.6	12.1	25.5	14	05.9	11	01	03.0	36	02.0	18	01.7	09	01.9	03	01.3	05	02.2	02	02.5	06	02.7	10
X	-	07.0	11.2	07.8	08.5	12.2	05.2	21.6	01	00.6	09	01	01.0	38	02.1	12	01.5	15	03.1	06	03.2	03	03.0	09	02.9	01	04.0	08
XI	-	01.6	04.3	01.9	02.4	05.1	-00.2	13.4	01	-10.0	25	01	03.0	19	02.0	26	01.5	09	02.2	03	03.3	11	02.7	02	05.3	01	02.0	18
XII	-	-01.0	02.7	00.1	00.5	04.0	-02.6	11.0	24.04	-12.0	21	.	.	56	01.6	15	01.2	10	01.9	01	01.0	03	03.0	03	03.3	.	05	
600.	-	07.0	11.4	07.6	08.4	12.5	04.6	28.0	M9VW	-22.6	05.1	201	02.0	67	01.8	41	01.6	105	02.5	133	03.3	37	01.8	68	03.4	98	02.2	245
$\varphi = 41^{\circ}03' N \lambda = 21^{\circ}22' E$ Gr. $\Delta G = + 1h 25 min.$																									BITCLA			

Mesec	Oblačnost Nm (0-10)				Insolacija broj sati (Dnev.)	Vlažnost vazduha				Padavine R mm				Broj dana na sa:																							
	7	14	21	Sred. (Dnev.)		em	m	s		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	T	≡										
						mm	7	14	21	Stred.	Min	Max	Dat.		30.00.0	0.025.0	30.020.0	6	8	2,0	8,0	0,1	1,0	20,0	9	Δ	*	Δ	▲	▲	T	≡					
RESEN																																					
BR. ST. 261	I	7.4	6.4	6.2	6.6	-	03.0	63	85	68	72	42	013	009.2	05	07	06	31	.	.	.	06	16	04	03	.	02	02	.	.	14	31					
	II	5.4	4.6	4.1	4.7	-	03.5	76	71	80	76	03	009	002.9	22	04	01	25	.	.	.	05	09	06	05	.	02	03	01	.	.	09					
	III	5.6	6.7	4.5	5.6	-	04.9	91	55	78	75	31	023	007.5	23	.	.	12	.	.	01	04	07	06	05	.	03	03	.	.	03						
	IV	4.9	5.2	4.1	4.7	-	05.6	73	51	73	66	05	051	026.3	11	.	.	03	.	.	01	01	10	10	08	08	02	08	.	.	.	01	.				
	V	4.7	6.8	3.2	4.9	-	08.4	82	52	82	72	27	060	C20.0	14	.	.	02	.	.	01	03	04	14	12	02	14	.	.	.	01	04	.				
	VI	2.8	5.5	3.5	3.9	-	05.7	76	50	75	67	19	038	008.4	26	.	.	13	.	.	08	02	09	08	09	.	09	.	.	.	03	.					
	VII	2.3	4.5	1.3	2.7	-	11.1	76	51	80	63	21	032	019.5	21	.	.	16	04	.	16	01	04	04	01	04	.	.	.	01	04	.					
	VIII	4.1	4.8	3.9	4.1	-	10.6	78	53	78	69	24	025	009.3	06	.	.	15	.	.	06	02	06	04	04	06	.	.	.	03	.						
	IX	2.6	3.5	1.4	2.5	-	08.9	82	39	72	64	25	024	013.5	05	.	.	13	.	.	16	01	04	04	01	04	.	.	.	03	.						
	X	5.4	5.6	3.9	5.0	-	08.8	85	56	87	76	32	163	C37.7	11	.	.	05	.	.	02	08	08	14	11	07	14	.	.	.	04	.					
	XI	7.1	6.7	5.9	6.5	-	05.0	80	68	76	75	10	086	030.0	20	03	.	13	.	.	06	17	13	11	01	12	01	.	.	01	05						
	XII	5.6	5.5	4.6	5.2	-	04.1	74	74	81	76	16	050	023.0	13	01	.	24	.	.	10	11	04	05	02	04	03	.	.	.	02	02					
	GOD.	4.8	5.5	3.8	4.7	-	06.8	78	58	77	71	05	574	037.7	Mx	15	07	115	59	04	.	05	01	102	88	94	80	16	82	14	02	.	.	02	29	14	30
MAKEDONSKI BROD																																					
BR. ST. 262	I	4.5	4.3	3.6	4.1	-	03.4	88	68	89	81	53	015	004.4	01	03	.	30	.	.	.	01	10	04	05	04	.	02	04	01	.	.	02	10			
	II	6.3	5.2	4.7	5.4	-	03.9	90	68	91	83	48	019	006.2	22	07	.	24	.	.	.	08	08	07	05	05	.	03	07	.	.	01					
	III	6.3	6.1	5.0	6.1	-	05.8	95	48	91	78	29	035	014.6	19	01	.	14	.	.	02	04	10	08	08	02	07	03	02	.	.	01					
	IV	5.8	6.0	3.9	5.2	-	06.7	92	50	70	71	23	034	009.2	02	.	.	03	02	.	02	01	04	08	10	09	01					
	V	8.2	6.9	4.9	4.7	-	10.3	97	56	88	80	40	035	008.6	14	.	.	07	.	.	01	09	09	08	05	.	.	.	02	11	.						
	VI	5.2	5.2	5.0	5.1	-	10.3	87	43	74	68	24	036	019.4	20	.	.	17	06	.	02	01	02	02	07	06	01	07	.	.	08	03					
	VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
	VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
	IX	3.0	4.0	2.4	3.2	-	10.9	90	43	79	71	34	017	011.0	13	.	.	22	05	.	.	11	01	03	01	03	.	.	.	01	01						
	X	7.7	6.3	5.9	6.6	-	08.2	97	59	93	83	30	165	C33.4	18	.	.	05	03	.	.	12	14	12	04	14	.	.	.	05	04						
	XI	9.1	8.4	8.4	8.6	-	04.0	92	74	93	84	15	043	012.6	20	01	.	09	.	.	02	11	11	08	01	09	03	.	.	.	05	04					
	XII	7.5	6.1	5.2	6.3	-	03.9	90	64	89	81	50	017	007.8	19	01	.	22	.	.	.	02	11	05	05	02	03	.	.	.	00	.					
	GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
KRUSEVO																																					
BR. ST. 263	I	4.7	3.9	2.3	3.6	-	03.2	72	44	69	68	26	058	045.4	01	01	04	23	.	.	03	13	05	05	01	05	.	.	.	03							
	II	5.7	5.2	3.7	4.9	-	03.0	78	74	72	74	33	049	C16.0	17	04	10	26	.	.	03	09	09	07	06	02	01	07	.	.	11						
	III	6.0	7.7	5.2	6.3	-	04.6	78	66	73	72	19	059	023.7	15	.	.	09	.	.	03	01	03	11	12	08	01	08	03	.	01	08					
	IV	5.6	6.0	3.0	4.9	-	05.1	69	59	66	65	29	058	019.5	11	.	.	05	.	.	10	02	08	08	11	02	04	03	.	.	08						
	V	5.2	7.2	3.2	5.2	-	08.3	76	65	76	72	38	083	023.2	25	.	.	07	.	.	02	05	05	15	11	03	15	.	.	01	08	09					
	VI	3.8	6.3	3.9	4.6	-	09.4	72	60	75	65	39	062	030.7	20	.	.	02	.	.	02	01	04	04	09	07	02	09	.	01	11	02					
	VII	2.6	5.6	2.5	3.6	-	10.4	72	60	73	68	41	071	014.2	21	.	.	06	.	.	01	09	03	07	06	02	07	.	.	01	09	.					
	VIII	4.9	6.0	2.4	4.5	-	09.9	77	57	78	71	48	015	009.9	26	.	.	03	.	.	03	02	01	08	02	06	04	02	.	04	02						
	IX	2.3	4.6	1.7	2.9	-	08.8	70	49	65	61	14	022	012.4	05	.	.	01	.	.	01	11	01	04	03	01	04	.	.	.	04	.					
	X	5.2	6.4	4.4	5.3	-	08.3	80	68	76	75	41	162	036.4	11	.	.	02	.	.	02	07	05	15	15	05	15	.	.	01	07	08					
	XI	8.3	7.8	6.6	7.6	-	04.9	88	82	87	86	54	085	043.5	20	01	03	12	.	.	02	04	20	16	09	02	11	09	.	.	01	20					
	XII	5.7	5.6	4.0	5.1	-	04.0	85	80	82	85	35	034	018.2	18	03	05	20	.	.	02	10	09	07	05	01	02	03	.	.	11						
	GOD.	5.0	6.0	3.6	4.9	-	06.5	76	65	73	71	14	758	045.4	01	04	22	95	12	.	04	02	05	116	85	22	89	34	.	.							

Mesec	Vadučki pritisak Pm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta ND, Pm (0-12)																			
		Tm				Sred. (Dnev.)				N		NE		E		SE		S		SW		W		NW		C			
		7	14	21		Max	Min	Max	Dat.	Min	Dat.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.		
$\varphi = 41^{\circ}59' N \lambda = 21^{\circ}31' E$ Gr. $\Delta G = + 1h 26 min.$																													
I	-	-02.9	02.3	-01.9	-01.1	04.0	-04.6	10.2	30	-08.0	05	01	01.0	02	01.0	.	.	16	01.0	05	01.0	18	01.0	.	.	06	01.5	45	
II	-	-02.7	06.8	00.3	01.2	08.6	-04.0	15.6	14	-10.6	10	01	01.0	10	01.2	.	.	12	01.0	01	01.0	15	01.0	02	01.0	06	01.2	37	
III	-	02.9	19.5	07.9	08.6	16.4	00.9	23.8	31	-06.4	02	.	.	05	01.0	03	01.0	31	01.2	02	01.0	16	01.0	.	.	08	01.2	28	
IV	-	07.3	19.3	11.5	12.4	20.1	04.6	25.0	08	-01.5	13	.	.	07	01.0	.	.	24	01.0	02	01.0	15	01.3	.	.	18	01.4	24	
V	-	13.3	24.2	16.5	17.6	25.0	10.6	31.4	31	03.5	01	.	.	05	01.0	.	.	23	01.0	02	01.0	14	01.0	.	.	17	01.2	32	
VI	-	16.4	26.5	18.7	20.1	27.3	13.5	32.2	03.02	06.4	08	01	01.0	04	01.2	.	.	20	01.0	01	01.0	20	01.1	.	.	14	01.1	31	
VII	-	18.5	29.0	20.3	22.0	29.7	14.7	35.6	19	10.2	25	01	01.0	04	01.0	02	01.0	19	01.0	.	.	13	01.1	01	01.0	11	01.2	42	
VIII	-	16.7	28.0	20.4	21.4	29.3	14.1	33.2	18	08.4	15	.	.	09	01.2	.	.	20	01.0	02	01.0	17	01.0	.	.	10	01.1	39	
IX	-	13.3	28.4	18.2	19.5	29.3	11.3	32.7	17	08.8	11	01	01.0	11	01.0	.	.	15	01.0	01	01.0	19	01.2	.	.	06	01.0	50	
X	-	07.5	18.5	10.4	11.7	19.0	05.9	25.6	01	-01.6	05	.	.	08	01.0	01	01.0	14	01.2	02	01.0	19	01.0	.	.	09	01.1	40	
XI	-	04.7	10.0	05.6	06.5	10.7	02.6	18.2	18	-06.0	27	.	.	12	01.0	.	.	16	01.0	02	01.0	11	01.0	01	01.0	09	01.1	39	
XII	-	-00.8	06.1	01.0	01.8	06.9	-02.4	12.0	03.02	-07.0	22	.	.	06	01.0	01	01.0	18	01.0	04	01.0	05	01.0	02	01.0	09	01.0	48	
GOD.	.	-	07.8	17.9	10.7	11.8	18.4	05.6	35.6	49M	-10.6	40.11	04	01.0	03	01.1	07	01.0	228	01.0	24	01.0	149	01.1	06	01.0	123	01.2	451
$\varphi = 41^{\circ}20' N \lambda = 21^{\circ}34' E$ Gr. $\Delta G = + 1h 26 min.$																													
PRILEP																													BR. ST. 267
I	707.1	-07.3	-01.9	-04.9	-04.8	-00.9	-08.5	05.8	08	-17.3	05	07	03.9	11	01.4	03	01.3	02	01.5	70
II	706.3	-03.0	03.2	-00.6	-00.3	04.3	-03.8	12.0	15	-10.6	10	09	03.8	25	03.0	.	.	01	03.0	08	01.5	03	01.7	38	
III	700.5	03.3	12.2	06.9	07.3	13.4	02.2	21.6	31	-04.8	01	07	02.9	06	02.3	02	03.5	.	.	10	03.8	15	02.9	08	01.6	01	02.0	44	
IV	702.2	07.8	15.3	10.4	11.0	16.7	03.4	25.0	08	-00.4	12	07	03.0	24	02.8	02	02.0	.	.	14	03.6	11	03.0	07	02.4	01	02.0	24	
V	703.2	13.3	20.6	15.0	16.0	21.4	10.1	29.5	31	06.9	01	10	02.5	13	01.8	30	03.7	.	.	09	02.4	12	02.3	08	01.9	.	.	38	
VI	702.3	16.4	23.4	18.2	19.0	24.5	12.7	31.6	02	06.0	08	11	02.6	17	03.3	C1	02.0	01	02.0	12	03.1	08	02.6	03	01.3	02	01.5	35	
VII	703.1	16.0	25.3	19.6	20.4	26.7	14.6	32.0	19	10.4	03	22	02.7	23	02.4	.	.	03	02.3	08	03.2	03	02.0	01	02.0	33			
VIII	704.7	16.8	25.2	18.3	20.2	26.6	13.9	31.7	17	10.1	15	08	03.1	27	02.7	01	02.0	01	03.0	11	02.5	04	02.1	03	01.7	04	01.8	30	
IX	707.2	14.6	25.6	18.7	19.4	26.8	12.7	30.7	03	05.8	27.11	16	02.9	16	02.7	.	.	03	02.3	07	02.0	03	01.3	.	.	45			
X	704.4	07.8	15.9	10.7	11.3	17.2	06.4	26.8	02.01	06.9	27	09	03.6	19	02.6	C1	07.0	02	03.0	10	03.5	09	02.2	04	01.5	.	.	39	
XI	704.5	03.6	08.2	04.7	05.3	09.3	04.5	18.7	18	-07.6	26	04	03.0	17	02.5	C1	02.0	.	.	09	03.4	08	01.8	02	01.0	.	.	48	
XII	706.2	-00.5	04.7	01.1	01.6	05.6	-01.6	11.9	18	-08.0	22	11	03.0	12	02.8	.	.	01	02.0	03	02.0	02	01.5	.	.	44			
GOD.	704.8	07.6	14.8	09.9	10.4	16.1	05.6	32.9	49M	-17.3	05.1	121	03.0	210	02.6	28	03.6	04	02.8	83	03.1	100	02.4	48	01.7	09	01.8	509	
$\varphi = 41^{\circ}43' N \lambda = 21^{\circ}46' E$ Gr. $\Delta G = + 1h 27 min.$																													BR. ST. 268
TITOV VELES																													
I	-	-02.5	02.6	-01.4	-00.7	04.0	-04.2	10.6	30.25	-08.5	11	.	.	02	01.0	.	.	04	02.0	.	.	24	03.0	43					
II	-	-01.1	07.1	01.4	02.2	08.4	-02.7	19.4	14	-10.0	10	.	.	02	01.5	.	.	03	01.7	.	.	39	03.0	36					
III	-	04.5	15.3	09.7	09.8	16.4	03.1	22.0	13	-07.2	02	.	.	03	01.3	.	.	17	02.9	.	.	22	02.7	36					
IV	-	09.9	16.4	12.6	13.7	20.5	06.8	28.8	08	00.5	13	.	.	01	01.0	.	.	11	03.0	.	.	30	03.8	38					
V	-	15.9	24.6	18.1	19.1	25.4	11.9	32.0	31	05.0	03	.	.	04	01.5	.	.	16	01.7	.	.	23	02.7	43					
VI	-	18.2	26.9	20.3	21.4	28.0	15.0	34.5	02	07.4	08	.	.	11	01.9	.	.	08	02.8	.	.	32	02.9	39					
VII	-	21.1	29.2	22.5	23.8	30.0	17.0	35.6	19	12.6	29	02	01.0	03	01.3	.	.	02	01.5	01	01.0	05	03.2	38					
VIII	-	19.9	29.0	22.2	23.3	29.9	16.7	34.0	18	12.2	15	03	01.7	08	01.2	09	01.3	01	02.0	09	01.1	01	01.0	41	02.2	21			
IX	-	16.8	28.7	21.2	22.0	29.7	14.3	33.0	16	07.6	11	.	.	07	01.7	.	.	11	01.5	01	03.0	18	01.3	.	.	.26	02.2	27	
X	-	05.5	18.5	12.5	13.3	19.3	08.2	29.2	01	-01.2	09	19	02.1	.	.	05	02.8	.	.	13	03.0	.	.	29	03.6	39			
XI	-	05.3	10.7	06.6	07.3	11.2	03.9	19.6	18	-07.6	27	02	02.0	04	01.8	.	.	18	03.1	.	.	05	01.8	.	.	18	03.2	43	
XII	-	00.8	07.2	02.4	03.2	08.3	-00.5	12.6	02	-06.0	24	30	02.0	.	.	09	02.9	01	02.0	04	01.5	.	.	26	02.4	49			
GOD.	-	09.0	18.3	12.4	13.2	19.3	07.5	35.6	49M	-10.6	40.0	09	01.7</td																

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sa:																							
	7	14	21		e _m	U _m	t	Tn	Tx	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	Δ	○	▲	▲	T	≡	■						
	Sred. (Dnes)	mm	mm		7	14	21	Sred.	Min	Σ	Max	Dat.	≤	<	<	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV						
TRUBAREVC																																		
BR. ST. 266																																		
I 7.8 6.6 5.0 6.5	-	03.4	85	67	88	80	28	018	010.5	05	.	04	25	05	12	03	03	01	02	02	01	.	.	08	03					
II 5.8 5.0 3.9 4.9	-	34.1	88	67	86	60	34	012	C06.3	17	01	.	26	07	07	03	03	01	01	03					
III 5.7 5.9 4.4 5.3	-	36.7	88	63	80	77	37	041	C20.0	15	.	.	14	05	07	06	06	01	05	01	.	.	.	03	02					
IV 5.8 5.5 3.0 4.8	-	07.3	79	50	73	67	26	021	009.0	24	.	.	03	04	.	.	.	07	07	05	05	.	05					
V 5.6 6.3 4.5 5.5	-	11.4	87	57	79	74	65	054	011.4	14	.	.	.	15	01	.	.	03	07	12	12	01	12	07	.					
VI 5.0 5.5 5.3 5.3	-	13.6	66	58	82	75	43	133	C31.0	24	.	.	.	23	11	.	.	05	C5	09	09	05	09	06	.					
VII 4.0 4.9 3.7 4.2	-	14.7	82	56	78	72	37	011	C06.4	06	.	.	.	30	13	.	.	07	02	02	02	.	02	.	.	.	02	.						
VIII 7.1 5.1 4.5 5.6	-	14.0	87	56	79	74	17	032	C13.0	30	.	.	.	28	13	.	.	04	04	04	01	04	04	.						
IX 2.6 3.9 3.2 3.2	-	12.3	88	50	79	72	35	016	010.0	13	.	.	.	30	11	.	.	11	02	03	03	01	03	03	.					
X 7.0 5.7 4.2 5.7	-	08.7	89	66	87	81	38	070	C16.0	11	.	.	06	04	.	.	04	C9	11	11	03	11	01	02						
XI 8.9 7.5 6.5 7.6	-	06.3	86	72	86	81	54	031	C11.0	23	.	.	09	.	.	.	02	17	05	05	01	05	01	01	.	.	02	02						
XII 7.6 5.6 4.9 6.0	-	04.5	87	74	89	83	50	013	C08.3	18	.	.	22	.	.	.	06	14	02	02	.	02	03	.						
GOD. 6.1 5.6 4.4 5.4	-	08.9	86	61	82	76	09	454	031.0	24M	01	04	105	138	45	.	.	62	93	65	65	14	61	07	02	.	.	26	17	09				
PRILEP																																		
BR. ST. 267																																		
I 5.7 4.8 4.1 4.9	083.5	03.0	93	83	53	85	50	015	006.4	01	12	20	30	.	.	.	02	01	12	10	06	04	.	01	05	.	.	14	31					
II 5.1 4.6 3.8 4.5	149.1	03.6	89	65	81	78	39	012	C06.6	17	01	01	25	.	.	.	02	01	11	08	07	03	.	C1	07	01	.	.	17					
III 5.5 6.7 4.3 5.5	162.4	05.4	87	51	76	72	27	047	C15.0	15	.	.	08	.	.	.	07	02	05	07	10	08	02	08	03	01	.	.	02	.	01			
IV 5.4 5.7 3.6 4.9	205.4	05.6	76	47	63	62	24	034	C11.4	26	.	.	01	01	.	.	04	02	07	08	09	05	01	05	01				
V 4.9 6.4 4.5 5.3	240.2	09.2	82	50	73	68	28	068	C16.8	14	.	.	.	03	.	.	.	02	01	04	06	17	08	03	17	.	.	.	01	01	13			
VI 3.5 5.8 5.0 4.8	252.8	10.5	78	48	69	65	26	114	C16.4	13	.	.	.	19	03	.	.	02	03	05	10	07	04	10	.	.	.	11	.	.				
VII 3.0 4.6 3.2 3.6	311.7	11.4	77	46	65	63	30	026	C13.9	14	.	.	.	24	05	.	.	03	01	08	03	04	03	01	04	.	.	.	10	.	.			
VIII 3.8 5.4 3.3 4.2	270.6	10.9	81	44	65	63	30	023	C09.8	20	.	.	.	21	09	.	.	02	07	02	06	05	04	.	.	.	02	.	.	02				
IX 2.2 3.3 2.3 2.6	278.9	10.4	85	41	66	64	24	008	C05.6	05	.	.	.	24	03	.	.	04	14	01	03	02	03	.	.	.	05	.	.	.				
X 4.3 5.4 4.2 4.6	178.8	06.9	85	51	72	69	29	104	C03.3	11	.	.	02	.	.	.	04	01	08	05	13	10	03	13	.	.	.	04	01	.	.			
XI 8.0 7.1 6.6 7.2	072.5	05.3	86	64	81	77	37	051	C04.2	20	.	03	07	.	.	.	02	.	03	17	11	06	01	08	04	.	.	.	01	.	02	.		
XII 5.5 5.2 4.8 5.2	114.0	04.1	87	65	82	78	45	019	C01.2	18	.	02	20	.	.	.	01	.	12	12	06	03	01	02	04	.	.	.	04	02	.	.		
GOD. 4.7 5.4 4.1 4.8	2320.7	07.2	83	54	73	70	24	523	C06.4	28M	13	14	26	91	94	16	.	37	09	94	84	102	64	16	82	24	03	.	.	01	01	48	18	93
TITOV VELES																																		
BR. ST. 268																																		
I 9.1 6.7 7.5 7.7	-	03.5	79	72	82	78	34	CC5	C02.4	05	.	05	28	.	.	.	04	.	15	03	03	.	02	01	07	02				
II 6.4 4.9 6.0 5.8	-	03.8	77	58	78	71	30	001	C00.6	05	01	.	21	.	.	.	07	.	03	C8	03	.	C2	01			
III 6.2 4.3 6.0 6.2	-	05.5	84	44	71	67	15	030	C18.0	15	.	.	06	.	.	.	03	.	02	11	06	04	01	C7	01			
IV 6.0 5.4 6.8 6.1	-	06.3	72	39	58	56	15	022	C10.6	24	.	.	05	.	.	.	05	03	02	11	05	01	10				
V 5.6 6.6 7.3 6.5	-	10.2	77	42	66	62	15	050	C11.2	14	.	.	.	18	02	.	.	04	02	10	17	11	01	17	.	.	.	01	.	.	.			
VI 6.2 5.7 6.5 6.8	-	12.4	79	47	69	65	23	101	C33.2	20	.	.	.	24	14	.	.	03	01	10	12	10	03	12	.	.	.	01	06	.	.			
VII 3.9 4.3 6.6 4.9	-	12.6	69	41	62	57	29	018	C15.3	07	.	.	.	30	18	04	04	.	07	C3	04	02	01	04	.	.	.	08	.	.	.			
VIII 5.3 5.4 7.6 6.1	-	12.2	73	40	61	58	23	023	C14.2	20	.	.	.	29	17	02	01	.	03	C8	05	02	01	05	.	.	.	04	.	.	.			
IX 1.8 3.9 4.7 3.5	-	11.3	76	38	64	55	25	005	C06.0	14	.	.	.	30	13	.	.	C3	.	08	03	02	02	.	.	.	03	.	.	.				
X 6.9 6.5 7.8 7.1	-	07.9	85	52	75	71	21	091	C28.0	11	.	.	04	.	.	.	06	.	08	06	13	11	10	03	11	.	.	03	.	.	.			
XI 8.7 6.2 9.0 8.6	-	06.3	86	67	83	79	43	054	C03.0	20	.	.	07	.	.	.	05	.	23	08	07	01	04	02	.	.	.	01	02	.	.			
XII 9.4 6.5 8.2 8.0	-	04.7	82	60	83	78	42	013	C06.7	18	.	08	.	.	.	02	.	16	04	03	04	.	.	.	02	.	.	.						
GOD. 6.0 5.9 7.2 6.4	-	08.1	78	56	71	66	15	417	C33																									

Mjesec	Vrsta i pritisak Pa MM	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra nD, Fm (0-12)																							
		Tm					N					NE						E			SE			S			SW			W			NW		
		7	14	21	Sred. (Dnev.)	N	NW	W	SW	Dan.	N	W	SW	Dan.	N	W	SW	Dan.	N	W	SW	Dan.	N	W	SW	Dan.	N	W	SW	Dan.	C				
$\varphi = 41^{\circ}45' N \lambda = 22^{\circ}11' E$ Gr.ΔG = + 1h 29 min.																																			
I	737.8	-03.2	02.0	-00.9	-00.7	02.9	-03.9	08.7	29	-07.6	12	04	02.8	.	.	01	01.0	02	03.0	06	01.2	05	01.6	04	02.0	20	04.6	46							
II	737.2	-02.2	05.6	01.1	01.4	07.2	-03.0	15.0	14	-09.4	10	07	03.1	09	03.2	.	06	01.8	05	01.8	09	02.2	04	02.5	24	03.6	20								
III	730.3	04.6	13.5	09.7	09.4	15.2	03.8	20.4	31	-04.4	02	03	01.0	04	01.5	04	01.5	37	04.7	05	04.2	06	02.5	03	02.0	12	03.6	19							
IV	731.9	08.8	17.6	12.3	12.8	19.0	06.9	28.0	06	01.0	13	10	03.1	.	.	01	01.0	22	05.5	03	03.0	02	03.0	04	03.8	28	04.5	20							
V	731.1	14.5	23.0	17.6	18.2	24.6	12.0	30.6	31	05.6	01	06	02.7	05	01.8	01	01.0	17	04.2	04	02.8	02	01.5	03	02.3	18	03.4	37							
VI	730.9	17.8	26.0	20.6	20.9	27.6	15.1	32.8	03	02	08.9	06	10	02.5	02	02.0	03	02.7	11	05.1	02	03.0	08	02.4	05	02.4	20	04.2	29						
VII	731.4	19.2	27.7	21.9	22.7	29.2	16.6	34.0	19	16.5	29	06	03.5	03	01.0	06	01.5	08	02.5	02	02.0	05	01.8	06	02.3	26	03.8	31							
VIII	732.1	17.7	27.0	21.6	22.0	28.9	15.8	33.0	13	12.2	06	04	02.0	04	02.2	04	01.5	14	04.5	05	02.6	07	01.6	01	04.0	19	04.0	35							
IX	735.4	15.2	27.9	20.7	21.1	29.3	14.0	32.1	03	08.6	11	07	01.7	09	03.0	.	.	12	03.7	04	02.5	02	02.0	10	03.1	38									
X	735.9	08.8	17.5	12.3	12.7	18.8	07.8	28.5	02	01.4	09	03	02.7	.	.	02	03.0	09	05.0	08	04.6	06	03.5	03	02.7	17	03.1	45							
XI	735.2	05.0	09.2	06.7	06.9	10.3	04.2	15.0	01	-07.6	27	03	01.0	02	01.0	03	01.0	23	03.5	09	05.3	03	02.3	01	04.0	16	04.2	30							
XII	738.0	-00.2	05.7	02.0	02.4	06.3	-01.1	11.8	18	-05.2	22	01	01.0	.	.	01	02.0	06	04.3	07	03.3	01	01.0	04	01.5	31	04.1	42							
GOD.	733.9	08.8	16.9	12.1	12.5	18.3	07.4	34.0	49VH	-09.4	10.II	64	02.5	38	02.3	26	01.7	168	04.3	60	03.3	66	02.2	40	02.4	241	03.9	392							
$\varphi = 41^{\circ}25' N \lambda = 22^{\circ}15' E$ Gr.ΔG = + 1h 29 min.																																			
DEMIR KAPIJA																																			
BR. ST. 272																																			
I	734.9	-05.1	00.6	-02.6	-02.4	01.3	-04.0	06.2	30	-12.2	11	01	01.0	02	02.0	C2	04.5	.	.	.	01	01.0	10	01.9	05	03.2	75								
II	735.7	-01.9	04.6	01.6	02.0	08.0	-02.4	15.9	15	-08.2	11	01	01.0	02	02.0	C4	01.8	01	02.0	03	02.3	04	01.5	09	01.9	16	02.1	44							
III	748.1	05.5	14.9	10.5	10.4	15.9	04.6	20.3	08	-05.0	02	01	01.0	02	02.0	38	04.6	02	03.4	02	02.0	.	10	01.3	06	02.3	29								
IV	749.1	09.8	19.0	13.3	13.8	19.6	07.9	25.8	06	01.4	13	01	02.0	01	01.0	23	05.2	02	03.0	01	02.0	02	01.0	14	02.3	30									
V	748.3	19.4	24.5	18.2	19.1	25.9	12.9	30.0	31	05.4	01	01	01.0	.	.	24	03.0	02	02.0	01	02.0	03	01.0	03	01.7	12	02.0	47							
VI	748.0	18.7	26.9	20.8	21.8	28.1	15.6	34.2	30	09.5	08	.	.	01	01.0	12	04.2	C9	02.8	02	01.0	.	.	09	02.0	15	02.4	46							
VII	748.4	20.6	29.2	22.8	23.9	30.2	17.5	35.4	19	13.0	29.0	03	.	.	.	09	02.7	02	03.0	03	01.0	.	09	01.7	12	02.2	58								
VIII	749.2	16.8	26.9	22.2	23.1	29.6	14.5	34.7	19	13.0	22.0	06	01.0	.	.	19	03.2	03	02.0	01	02.0	03	01.3	05	02.2	47									
IX	739.0	15.9	28.7	21.2	21.8	29.7	14.4	33.7	17	05.0	11	15	03.0	03	02.7	02	01.5	03	01.3	03	01.0	14	02.1	50							
X	733.6	09.1	18.4	12.6	13.2	19.3	07.9	28.4	01	00.5	09	01	01.0	01	03.0	19	04.0	01	03.0	06	01.5	02	01.0	07	02.1	50									
XI	733.9	06.1	10.6	07.7	08.0	11.4	05.1	18.7	20.18	-07.7	27	32	04.2	04	02.5	02	01.0	.	16	01.9	06	01.7	30								
XII	736.4	00.4	06.7	02.8	03.2	07.7	-00.5	13.2	18	-05.6	24.0	10	02.0	01	02.0	12	03.8	02	03.0	01	02.0	02	01.1	12	01.8	46									
GOD.	-	08.8	17.9	12.6	13.2	18.9	07.8	35.4	49VH	-12.2	M.I	07	C1.1	06	01.8	209	03.9	33	02.8	24	01.6	20	01.2	110	01.9	134	02.2	552							
$\varphi = 41^{\circ}55' N \lambda = 22^{\circ}25' E$ Gr.ΔG = + 1h 30 min.																																			
KOŠANI																																			
BR. ST. 273																																			
I	-	-03.0	03.0	-00.5	-00.2	03.5	-04.1	10.0	31.27	-07.6	12	05	02.6	03	02.0	.	.	.	10	02.8	.	.	.	02	02.0	71	
II	-	-02.0	06.4	02.2	02.2	07.4	-02.3	14.6	15	-09.4	10	15	03.1	10	02.3	C5	04.5	.	.	.	11	03.5	.	.	.	02	02.0	41
III	-	04.8	15.0	09.7	09.8	15.6	03.0	23.0	31	-05.0	01	31	02.7	05	02.0	.	.	.	13	03.0	02	03.0	.	42											
IV	-	08.6	18.9	13.5	13.6	19.6	06.2	28.5	06	-	-	35	C2.6	04	02.2	.	.	.	12	02.9	04	03.0	35				
V	-	14.9	23.4	17.6	18.4	24.1	11.5	25.2	31	05.0	01	17	02.4																						

Mesec	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																								
					U m m	t m m					Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	A	A	A	A	R	T	III						
	7	14	21	Sred. (0des)				Σ	Max	Dat.	≤	<	<	≤	≤	≤	≤	≤	>	≥	≥	≥	≥	•	△	*	▲	▲	▲	■					
BR. ST. 271																																			
STIP																																			
I	6.2	4.0	4.5	5.6	099.1	03.6	89	74	85	83	44	020	012.6	01	•	07	29	•	•	08	01	07	13	04	03	01	02	02	•	•	•	10	-		
II	4.8	4.6	3.8	4.4	145.0	03.4	84	51	67	68	28	008	006.2	17	•	•	24	•	•	10	10	08	04	01	•	02	04	•	•	•	03	03			
III	5.5	6.6	3.0	5.1	163.2	05.5	82	48	63	64	20	032	008.0	15	•	•	08	•	•	13	04	07	07	09	07	•	07	03	01	•	01	01			
IV	5.3	5.0	2.3	4.3	217.8	05.9	73	40	55	56	15	010	004.6	25	•	•	•	03	•	20	•	08	05	06	02	•	06	•	•	•	•	•			
V	5.3	5.6	4.0	5.0	246.6	09.8	81	45	68	65	24	070	026.0	10	•	•	•	17	01	•	10	01	03	05	13	05	02	13	•	•	10	•			
VI	4.5	4.9	5.6	5.0	242.2	11.1	76	43	63	61	27	098	030.0	28	•	•	•	23	11	•	11	01	04	04	12	09	04	12	•	•	12	•			
VII	2.7	4.2	2.9	3.3	319.3	11.9	74	42	60	59	29	042	036.3	07	•	•	•	29	12	03	07	10	01	04	04	02	04	•	•	01	12	•			
VIII	3.4	5.2	2.7	3.8	286.2	11.9	83	42	63	63	28	038	020.0	62	•	•	•	28	13	01	08	•	09	02	09	06	01	05	•	•	08	•			
IX	1.6	3.0	1.9	2.1	285.0	09.9	77	34	56	55	22	015	012.2	14	•	•	•	30	11	•	04	•	20	•	03	03	01	03	•	•	04	•			
X	4.9	5.3	3.6	4.6	182.8	07.6	84	53	72	70	24	089	025.0	11	•	•	•	04	•	•	04	03	09	08	12	10	04	12	•	•	05	•			
XI	8.3	7.3	6.6	6.6	072.9	05.9	83	67	77	76	40	042	043.3	20	•	•	01	07	•	•	09	02	02	17	09	04	01	07	02	•	•	02	•		
XII	5.9	5.2	3.5	4.8	117.7	04.4	88	66	82	79	45	009	004.5	19	•	•	01	19	•	•	10	02	10	10	05	02	•	03	01	•	•	08	•		
GOD.	4.9	5.2	3.7	4.6	2397.8	07.6	81	50	67	66	15	511	043.3	80.8	•	09	87	134	48	04	114	14	99	82	92	62	16	84	12	01	•	01	53	13	-
BR. ST. 272																																			
DEMIR KAPIJA																																			
I	7.4	7.0	4.2	6.2	-	03.4	92	79	89	87	49	071	055.4	01	03	10	28	•	•	01	•	04	11	05	04	02	03	04	•	•	16	36			
II	5.4	5.0	3.9	4.8	-	03.8	87	56	70	71	10	032	015.6	17	•	•	21	•	•	01	•	11	10	07	04	01	04	04	•	•	01	02			
III	9.4	6.6	2.7	4.9	-	06.1	83	49	65	66	24	025	008.1	25	•	•	04	•	•	08	01	08	04	00	03	•	06	01	•	•	01	•			
IV	5.4	4.8	2.4	4.2	-	06.3	72	38	55	55	19	016	004.6	18	•	•	•	01	•	05	•	10	06	09	05	•	07	•	•	•	•	•			
V	4.9	5.0	4.3	4.7	-	10.5	80	46	67	65	26	032	010.8	14	•	•	•	19	01	•	04	04	04	11	07	01	11	•	•	07	•				
VI	4.5	4.9	5.9	5.1	-	11.7	74	46	62	61	13	049	030.2	21	•	•	24	13	01	02	•	05	05	09	08	02	02	09	•	•	11	•			
VII	2.6	3.4	3.3	3.1	-	13.0	74	43	60	59	31	044	017.6	06	•	•	31	18	03	•	11	•	03	05	03	03	•	•	09	•	•	09	•		
VIII	3.7	4.7	2.1	3.5	-	12.4	79	41	62	61	28	021	008.5	01	•	•	29	17	01	•	12	02	04	05	•	06	•	•	•	•	04	•			
IX	2.0	2.8	1.9	2.2	-	11.1	82	38	59	60	25	011	006.7	14	•	•	29	11	•	•	19	02	04	02	04	04	•	•	04	02	•	02			
X	4.8	5.0	3.5	4.4	-	08.3	88	55	76	73	25	062	016.3	18	•	•	03	•	•	03	07	09	08	02	09	•	•	01	08	•	01				
XI	8.2	6.9	6.6	7.3	-	06.2	81	64	76	74	18	048	030.3	20	•	•	06	•	•	03	01	02	16	08	04	01	07	02	•	•	01	04	02	•	
XII	4.6	4.9	2.9	4.8	-	04.7	89	66	82	79	45	010	004.9	18	•	•	18	•	•	01	01	07	09	06	03	01	06	•	•	08	•	•	08	•	
GOD.	5.1	5.1	3.6	4.6	-	08.1	81	51	68	67	10	541	055.4	041	03	10	77	134	60	05	24	03	102	74	87	60	12	81	12	•	•	38	46	34	-
BR. ST. 273																																			
KOČANI																																			
I	6.2	5.8	4.9	5.6	-	04.0	87	83	89	86	68	018	011.3	25	•	07	29	•	•	08	11	02	02	01	02	02	01	02	02	01	02	07	•		
II	4.7	4.7	3.9	4.5	-	04.3	82	70	80	78	54	010	006.2	14	•	•	23	•	•	01	•	08	04	03	02	03	02	03	02	03	01	02	02		
III	5.4	6.0	6.1	5.8	-	06.7	78	65	72	72	36	051	019.5	25	•	•	08	•	•	03	08	07	07	03	07	02	02	02	02	02	02	•			
IV	5.6	5.2	4.9	5.2	-	07.5	80	53	64	66	30	021	007.0	22	•	•	03	•	•	08	09	04	04	06	04	06	04	06	04	06	04	06	•		
V	5.1	5.4	6.3	5.6	-	11.8	85	60	77	74	28	077	015.4	10	•	•	17	•	•	03	06	17	12	03	17	•	•	•	•	•	01	03	•		
VI	3.7	4.4	4.1	4.8	-	13.6	84	58	73	72	29	077	026.7	21	•	•	24	08	•	•	03	04	11	11	03	11									

Mesec	Vrstdinski pritisak mm Hg	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (0-12)											
		Ta					N					E						S					
		7	14	21	Sred. (O) deg.	N	NW	W	SW	S	SE	E	NE	N	S	SW	W	NW	C				
$\varphi = 41^{\circ}19' N \lambda = 22^{\circ}34' E$ Gr.ΔG = + 1h 30 min.																							
I	-	-00.3	07.1	11.8	02.6	07.7	-01.1	12.5	06 -04.2	15 . .	01 01.0 . . .	09 01.3 . . .	04 04.2	43									
II	-	01.0	08.0	03.6	04.2	09.0	00.0	17.6	15 -06.9	11 . .	06 01.3 . . .	01 01.0 . . .	02 02.5	23	03.5	23							
III	-	06.3	15.1	10.7	10.7	16.2	04.5	20.4	08 -03.6	02 01 04.0	10 01.5 . . .	11 02.5 16 02.6	02 01.0	01 03.0	14 03.4	38							
IV	-	11.0	16.5	15.2	15.2	20.4	08.3	26.0	06 04.2	04 02 02.5	06 02.3 01 01.0	03 02.7 07 02.9	02 03.5 . . .	04 03.6	23								
V	-	16.0	24.4	19.5	19.8	25.7	13.1	30.4	31 06.0	01 03 01.7	10 01.7 C1 01.0	02 02.5 11 02.1	03 02.0 . . .	23 03.1 40									
VI	-	19.2	27.9	22.0	22.8	26.8	16.4	34.3	30 11.4	06 01 02.0	09 01.7 . . .	06 01.7 08 02.0	04 01.8 . . .	29 03.5 31									
VII	-	21.4	29.7	25.4	25.5	30.9	18.8	35.6	17 14.4	03 01 02.0	06 01.7 . . .	01 03.0 07 01.6	09 02.6 . . .	01 01.0 43 03.2	25								
VIII	-	19.7	28.6	24.4	24.3	29.6	17.4	33.4	29 14.6	23 01 03.0	03 01.7 . . .	05 01.8 06 01.7	07 02.6 . . .	04 02.8 38 03.3	29								
IX	-	18.1	29.7	23.1	23.5	30.4	19.8	34.8	17 10.4	26 . .	08 01.8 . . .	06 02.2 10 02.5	08 02.1 . . .	15 02.9 43									
X	-	12.0	18.9	14.7	15.1	19.9	0.5	28.9	01 05.8	30 01 04.0	10 01.9 01 03.0	05 01.6 02 02.0	03 02.0 . . .	36 03.4 35									
XI	-	06.8	11.6	08.3	08.8	12.3	05.9	19.6	18 -05.0	27 . .	13 01.3 . . .	08 02.2 08 01.5	03 01.0 . . .	22 04.3 36									
XII	-	03.6	08.4	04.7	05.4	09.1	02.1	13.5	30 -02.5	22.21 . .	07 01.3 . . .	01 02.0 03 02.3	01 01.0 . . .	47 03.7 34									
GOD.	-	11.2	19.1	14.5	14.8	20.0	09.3	35.6	17W -06.9	H.N 10 02.5	89 01.6 03 01.7	49 02.1 87 02.1	46 02.2 06 02.5 369 03.5 400										
$\varphi = 41^{\circ}26' N \lambda = 22^{\circ}39' E$ Gr.ΔG = + 1h 31 min.																							
VALANCOVAC												BR. ST. 276											
I	-	-02.5	03.2	-00.1	00.6	06.2	-03.0	10.8	27 -03.8	24.12 08 03.0	* * C4 01.5	07 01.0 05 01.0	07 01.4 16 02.1	46									
II	-	-01.0	07.1	01.4	02.0	08.6	-02.4	16.8	15 -08.6	11 12 01.6	01 01.0 08 01.0	04 01.2 . . .	01 01.6 28 02.0	25									
III	-	03.1	14.8	09.1	09.0	16.0	02.1	22.4	31 -05.9	02 11 01.2	08 01.2 05 01.0	10 01.9 21 02.0	05 02.4 04 01.2	14 02.1 21 01.5	46								
IV	-	09.0	16.9	12.4	13.2	20.5	06.0	27.0	06 01.4	14.04 10 01.7	05 01.6 05 01.4	04 01.2 10 02.6	03 01.7 03 01.8	20 02.8									
V	-	19.0	23.6	17.3	18.3	29.3	11.4	30.2	31 04.3	01 06 02.0	04 01.0 02 02.0	07 02.3 11 02.3	07 02.1 05 01.2	17 01.9 34									
VI	-	18.8	27.0	20.3	21.6	28.2	14.7	33.4	02 10.4	08 06 01.2	03 01.3 . . .	06 01.3 13 01.3	03 01.3 10 01.6	18 02.4 31									
VII	-	20.0	28.7	21.6	23.0	30.3	15.3	34.6	19 10.0	03 02 02.0	03 01.0 01 01.0	09 01.9 06 01.5	05 01.0 05 02.0	22 01.6 40									
VIII	-	17.7	27.7	21.1	21.9	29.0	14.0	32.6	19 10.8	06 03 02.3	05 01.2 06 01.7	06 01.0 09 01.8	07 01.1 07 01.0	17 01.3 34									
IX	-	14.5	29.1	20.2	21.0	25.4	11.7	33.6	16 07.2	26.25 03 01.7	05 01.8 . . .	03 01.3 11 01.7	03 02.0 13 01.8	12 01.5 40									
X	-	08.0	18.4	11.3	12.2	19.2	06.2	28.6	01 -00.6	31.05 08 01.9	04 01.0 05 01.4	06 01.5 09 02.1	02 02.0 04 01.5	09 02.0 04 01.5	35 02.0								
XI	-	04.6	10.3	06.1	06.8	10.8	03.5	20.2	19 -07.2	27 04 03.0	07 01.0 11 01.2	08 01.2 05 01.4	03 01.3 03 01.7	03 01.7 14 02.1	35 02.1 35								
XII	-	-00.4	08.3	01.7	02.3	04.9	-01.2	11.3	18 -06.8	22 04 01.5	01 01.0 08 01.1	05 01.2 . . .	01 03.0 02 01.0	22 02.0 30									
GOD.	-	08.8	18.1	11.9	12.7	19.2	06.9	34.6	19W -08.6	H.N 14.11 77 01.8	46 01.2 53 01.3	75 01.5 100 01.9	40 01.7 73 01.6	213 02.1 416									
$\varphi = 41^{\circ}13' N \lambda = 22^{\circ}43' E$ Gr.ΔG = + 1h 31 min.																							
NCVI DOJRAM												BR. ST. 278											
I	-	01.1	06.8	02.9	03.4	07.6	-00.4	12.2	06 -05.3	27 . .	02 03.5 . . .	02 03.5 . . .	01 02.0 . . .	01 02.0 03 03.0	46	03.1 50							
II	-	01.3	07.5	03.1	03.6	08.6	0.2	17.2	15 -04.0	09 04 04.0	01 02.0 . . .	01 02.0 . . .	03 01.0 . . .	03 01.0 07 02.4	46	03.2 39							
III	-	06.8	13.3	08.4	09.2	14.4	05.0	18.3	17 -01.0	02 . .	04 02.8 . . .	04 03.2 . . .	01 02.0 . . .	01 02.0 03 03.0	46	03.3 67							
IV	-	11.3	18.4	12.5	13.7	19.6	08.8	24.5	09 05.0	05.04 . .	05 03.6 . . .	01 02.0 . . .	01 02.0 . . .	01 02.0 03 03.0	46	03.8 39							
V	-	17.0	23.6	16.9	18.6	25.0	13.5	29.4	20 07.5	01 . .	05 03.8 . . .	02 02.0 . . .	02 02.0 . . .	23 03.7 63									
VI	-	19.9	26.0	19.7	21.5	28.0	16.5	32.5	29.02 10.1	06 . .	02 02.0 . . .	02 02.0 . . .	02 04.0 . . .	01 03.0 29 05.1	56								
VII	-	22.1	29.1	22.6	24.1	30.2	19.1	33.7	20 15.3	07 . .	09 02.6 . . .	09 02.6 . . .	07 03.0 . . .	07 03.0 06 03.8	46	03.8 38							
VIII	-	21.0	28.4	21.5	23.1	29.6	18.3	34.0	30 15.0	16 . .	03 02.3 . . .	05 01.6 . . .	05 01.6 . . .	35 03.6 50									
IX	-	19.6	28.5	20.8	22.4	29.6	17.1	33.0	07.02 14.6	25.11 . .	04 02.8 . . .	04 02.8 . . .	04 02.8 . . .	14 03.3 72									
X	-	12.9	18.3	13.7	14.7	19.4	11.3	27.5	01 07.0	31 . .	18 03.6 . . .	18 03.6 . . .	01 02.0 . . .	45 04.0 31									
XI	-	07.1	10.4	07.5	08.1	11.3	05.8	17.1	20 -03.0	27 . .	23 04.0 . . .	23 04.0 . . .	04 04.0 . . .	17 04.5 50									
XII	-	03.2	07.3	04.2	04.7	08.3	01.0	12.2	30 -03.0	21 . .	09 04.0 . . .	09 04.0 . . .	01 02.0 . . .	45 05.6 39									
GOD.	-	11.9	18.2	12.8	13.6	19.3	06.8	34.0	30W -05.3	27.1 04 04.0	. . .	85 03.5	15 02.5	01 03.0 396 04.3 594							
$\varphi = 41^{\circ}58' N \lambda = 22^{\circ}46' E$ Gr.ΔG = + 1h 31 min.																							
CELCEVO												BR. ST. 279											
I	-	-05.4	04.3	-02.5	-01.5	04.6	-07.3	05.5	19.18 -14.3	04 13 02.5	02 04.0 08 01.2	05 02.2 01 02.0	07 01.6 03 03.0	53									
II	-	-03.7	03.9	-00.8	-00.3	04.5	-05.1	11.2	15 -12.5	10 14 03.4	13 03.2 04 01.5	03 01.0 07 02.4	10 02.1 04 02.8	29									
III	-	01.2	12.8	06.6	06.8	13.4	-00.1	22.0	31 -08.5	02 09 02.1	02 01.5 08 01.4	05 03.8 13 03.4	10 03.0 16 01.9	39									
IV	-	06.4	14.6	10.2	10.4	14.9	03.5	28.0	06 -02.0	13 12 02.4	08 03.1 02 02.0	03 03.0 14 02.6	06 04.0 12 02.3	03 02.3 24									
V	-	12.4	20.4	14.5	15.5	21.4	05.0	27.0	31 01.5	01 02 02.0	C1 02.0 01 01.0	09 02.1 12 01.6	04 02.8 09 02.2	04 02.5 31									
VI	-	16.0	23.6	17.5	18.6	24.5	11.4	31.0	02 04.5	07 09 02.7	C1 02.8 08 01.4	01 03.0 06 03.8	06 03.0 07 03.0	01 01.9 05 02.6	37								
VII	-	17.5	25.6	18.7	20.1	26																	

Meseč	Oblačnost Nm (0-10)			Inkolacijski broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																									
	7	14	21		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	≤	<	≤	≥	≤	≥	≤	≥	≤	≥	≤	≥	•	*	•	Δ	•	A	▲	□	T	≡	■
	Std. (Dles.)				7	14	21	Sred. Sv.	Min	Σ	Max	Dat.	30.00.0	0.025.0	30.020.0	6	8	2.08.0	0.1	1.010.0	,	*	Δ	•	A	▲	□	T	≡	■						
VALANDOVC																																				
BR. ST. 276																																				
I 4.5 2.7 1.9 3.0	-	03.9 75 59 75 69 33	065 053.0	01	.	.	19	.	.	03	.	15 03 03 03 01 02 01					
II 4.7 4.2 3.2 4.1	-	03.9 72 51 68 64 25	016 007.5	17	.	.	12	.	.	02	.	12 04 03 03 03 03					
III 4.8 6.0 4.5 5.1	-	06.3 81 52 66 66 21	047 017.2	25	.	.	03	.	.	02	.	07 07 07 06 02 07					
IV 4.7 4.2 3.3 4.1	-	06.7 70 40 51 54 23	008 006.0	02	.	.	01	.	.	13 04 02 02 02 02						
V 4.8 5.3 5.2 5.1	-	10.9 79 47 66 64	- 061 025.4	17	.	.	20	01	.	.	03 04 07 07 02 07						
VI 3.7 4.3 4.6 4.1	-	12.4 75 43 63 60 32	049 026.8	20	.	.	24	15	04 01	.	09 02 06 01 04 06						
VII 2.3 3.4 3.4 3.0	-	13.5 71 44 55 56 29	043 025.4	14	.	.	30	23	07 01	.	11 01 04 04 01 04						
VIII 3.3 5.6 3.1 4.0	-	12.8 74 45 56 58 29	060 022.5	03	.	.	25	16	04 01	.	10 03 06 06 02 06						
IX 1.8 2.7 2.1 2.2	-	11.4 73 37 55 55 23	008 007.8	14	.	.	30	18	.	.	17 01 01 01 01 01						
X 4.6 5.1 3.3 4.3	-	08.6 76 58 67 67 26	063 013.6	18	.	.	03	.	01	.	10 07 11 10 02 11						
XI 7.0 7.0 7.0 7.3	-	06.6 84 66 76 75 41	065 034.0	20	.	.	04	.	02	.	03 15 10 09 01 10 02	02	.						
XII 4.9 4.9 3.1 4.3	-	04.9 77 62 73 71 37	012 005.4	18	.	.	07	.	03	.	14 08 04 04 04 04					
GOD. 4.0 4.6 3.7 4.2	-	08.5 75 50 64 63	- 497 053.0	041	.	.	45	137	73 15 16	.	124 62 64 61 12 63 03	02	.							
STRUMICA																																				
BR. ST. 277																																				
I 3.5 4.2 2.2 3.3	136.5	04.0 84 71 89 81 46	031 015.2	01	.	.	27	.	.	01	.	13 02 03 03 01 02 01	06	.						
II 3.7 4.0 3.4 3.7	-	04.0 88 56 80 75 32	019 007.4	18	.	.	21	.	.	01	.	12 05 05 03 03 04 03	01	.						
III 5.0 6.2 4.1 5.1	156.6	06.2 92 51 74 73 25	096 053.2	22	.	.	07	.	.	02	.	04 04 08 08 02 08 01	01	01						
IV 4.8 4.9 2.5 4.1	220.0	06.7 78 43 60 60 23	020 007.2	02	.	.	03	.	04	.	12 05 08 03 03 04	01	.						
V 4.5 5.5 5.0 5.1	246.0	10.8 83 50 73 69 28	080 035.6	17	.	.	17	01	.	02	.	03 04 16 10 02 14	10	.							
VI 3.9 5.2 4.6 4.6	234.5	11.8 74 45 66 62 28	060 021.6	20	.	.	23	13	.	03	.	05 03 11 06 02 11	06	.							
VII 2.2 3.9 3.1 3.0	308.8	13.1 74 45 68 62 08	036 022.0	02	.	.	30	20	.	01	.	12 06 06 01 06	08	.							
VIII 2.6 4.6 2.9 3.4	259.6	13.1 85 50 70 68 27	028 009.4	20	.	.	28	15	01	.	11 04 08 05 05 08	07	.								
IX 1.1 2.9 1.5 1.8	273.0	11.0 92 35 63 63 07	016 012.2	06	.	.	29	12	.	01	.	18 05 03 03 01 05	04	.								
X 4.2 5.1 3.3 4.3	156.6	08.1 91 55 82 72 23	063 020.4	18	.	.	03	03	.	01	.	10 07 13 10 02 13	02	04								
XI 7.0 7.4 6.6 7.0	057.5	06.4 92 68 88 83 41	047 018.2	26	.	.	07	.	01	.	01 09 10 04 02 09	01	04								
XII 4.8 4.6 3.3 4.2	108.3	04.7 94 71 89 85 48	018 007.4	19	.	.	21	.	01	.	14 08 06 09 06 08	09	.								
GOD. 4.0 4.9 3.5 4.1	-	08.3 85 53 75 71 07	914 053.2	82N	.	.	86	133	59	.	13	.	115 93 99 64 13 97 11 08	01	39	24							
MCVI DCJRAK																																				
BR. ST. 278																																				
I 4.2 2.7 2.4 3.1	-	04.8 86 72 84 81 40	022 009.0	09	04	01	30	.	.	01	01 18 05 04 04 04 02 02	01	.							
II 4.6 3.2 3.9 3.9	-	04.8 86 68 81 70 36	036 015.0	18	.	.	11	.	.	02	.	12 05 05 02 04 03 03 02	01	02								
III 5.8 5.6 3.6 5.0	-	07.5 89 74 88 83 43	052 020.0	25	.	.	01	.	02	.	09 08 08 06 03 04 02 02	01	02								
IV 4.7 3.6 2.3 3.6	-	08.4 76 60 70 74 42	008 007.0	02	.	.	07	.	01	.	15 06 02 02 02 02							
V 4.7 5.0 5.2 4.9	-	12.8 82 65 85 77 45	084 028.0	14	.	.	20	.	02	01	07 09 07 07 07 03 07	04	.								
VI 3.9 4.7 4.9 4.5	-	14.3 77 60 76 71 34	134 036.0	20	.	.	23	13	03 04 03 08 08 07 07 05 07	09	.										
VII 2.0 3.0 4.0 3.0	-	15.0 73 58 73 68 47	051 028.0	02	.	.	31	28	13 08	.	16 03 04 04 02 04 04	04	.									
VIII 3.3 3.7 2.5 3.3	-	14.9 75 57 75 65 37	022 022.0	03	.	.	30	17	02 03	.	15 03 01 01 01 01	01	.									
IX 1.7 1.5 1.5 1.6	-	13.4 76 47 74 66 35	007 003.0	24	.	.	29	17	02	.	21 02 04 03 04 04	03	.									
X 4.2 5.1 4.1 4.5	-	10.2 82 73 83 60 47	059 017.0	11	.	.	03	.	10	.	11 08 09 02 09																									

