

SOCIJALISTIČKA FEDERATIVNA REPUBLIKA JUGOSLAVIJA — RÉPUBLIQUE SOCIALISTE FÉDÉRATIVE DE YUGOSLAVIE
HIDROMETEOROLŠKA SLUŽBA — SERVICE HYDRO-MÉTÉOROLOGIQUE

METEOROLOŠKI GODIŠNjak I

ANNUAIRE METEOROLOGIQUE I

GODINA 1974 ANNÉE

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B E O G R A D

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O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljaju se podaci 8 odabranih stanica, i to: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelashnica, Sarajevo, Beograd, Titograd i Skopje. U delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

φ = geografska širina, λ = geografska dužina od Griniča, ΔG vremenska razlika u odnosu na Grinič, H_s = nadmorska visina podnožja termometarskog zaklona, H_b = nadmorska visina rezervoara barometra, h_t = visina rezervoara termometra iznad tla, h_r = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebљene prema medjunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

P = vazdušni pritisak u mm visine živinog stuba, reducirane na 0°C ; T = temperatura u $^{\circ}\text{C}$; e = pritisak vodene pare u mm visine živinog stuba; U = relativna vlažnost u procentima; D = pravac vetra po ruži vetra od 16 ili 8 pravaca; F = jačina vetra po Boforovoj skali (0-12); v = brzina vetra u m/sek; V = vidljivost u km; N = oblačnost (0-10); insola - cija = trajanje osunčavanja u satima; R = padavine u mm; R_s = padavine u mm; h_s = snežni pokrivač u cm; W = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan medjunarodnim simbolima.

U rubrici "razvoj vremena" su potrebljene ove skraćenice:

n = u toku noći; a = pre podne; p = posle podne; i = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14, i 21 h po lokalnom vremenu računate su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente (P , e , U , N) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri su čitavani i uredjivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h predhodnog dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebљene su oznake $M_{\overline{ax}}$ i $M_{\overline{in}}$; za rubrike broj dana sa • ili •, ✕ ili Δ , i $\not\Delta$ prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Ažbučnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SFRJ sa naznačenim klimatološkim stanicama u 1974. godini čiji brojevi odgovaraju brojevima stanica sa podacima u tablicama B.

NOTICE EXPLICATIVE

L'Annuaire météorologique I a deux parties: A) Observations journalières et: B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd et Skopje. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

φ = latitude, λ = longitude E de Greenwich, ΔG = différence entre l'heure locale et l'heure de Greenwich, h_s = altitude du pied de l'abri météorologique, h_b = altitude de la ouverte du baromètre, h_t = hauteur, au-dessus du sol, du réservoir du thermomètre, h_r = hauteur, au-dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

La désignation des éléments météorologiques particuliers sont conformes aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

P = pression atmosphérique en mm (hauteur de la colonne de mercure réduite à 0°C); T = température en $^{\circ}\text{C}$; e = tension de vapeur d'eau en mm de la hauteur de la colonne de mercure; U = humidité relative en %; D = direction du vent en rose des vents de 8 ou de 16 directions; F = force du vent d'après l'échelle Beaufort (0-12); v = vitesse du vent en m/s; V = visibilité en km; N = nébulosité (0-10); insolation = durée d'insolation en heures; R = précipitations en mm; h_s = épaisseur de la couche de neige en cm; W = évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux.

Dans la colonne "Kazvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

n = pendant la nuit; a = avant midi; p = après midi; i = avec interruption.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4},$$

et pour les autres éléments (F , e , U , N) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7h, 14 h et 21 h.

Les lectures des thermomètres à maxima et minima suivies de leur amorçage, ont été faits à 21 h et les valeurs inscrites le même jour.

Les valeurs journalières des précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau, de la force du vent $F \geq 6$ (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air les indications $M_{\overline{ax}}$ et $M_{\overline{in}}$ ont été utilisées; dans les colonnes "Broj dana sa" (Nombre de jours avec) • ou , , * ou △, et × sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1974; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

A Z B U Č N I S P I S A K G T A N I C A
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

I

A Z B U Ć N I S P I N J A K S T A N I C A
PO SOČIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

II

S T A N I C A	Broj stanice 2	Nadmorska visina H, m. 3	Geografska širina φ, °N 4	Geografska dužina λ, °E Gr. 5	Pođ t e stanice	Vrednost prištak 7	Temperatura vazduha 8	Vlažnost vazduha 9	Vetar 10	Oblakost 11	Iznoslacija 12	Padavine 13	Broj karak- terističnih dodata 14
1													
Cres	76	10	44°59'	14°24'	ob		x	x	x	x	x	x	x
Crikvenica	49	2	45 10	14 42	ob		x	x	x	x	x	x	x
Čazma	62	144	45 45	16 38	ob		x	x	x	x	x	x	x
Beruvar	66	161	45 36	17 14	gl	x	x	x	x	x	x	x	x
Bonji Meljani	67	120	45 44	17 38	ob		x	x	x	x	x	x	x
Donji Miholjac	70	97	45 46	18 10	ob		x	x	x	x	x	x	x
Dubrovnik	100	49	42 39	18 06	ob		x	x	x	x	x	x	x
Djakovo	71	98	45 17	18 25	ob		x	x	x	x	x	x	x
Gospic	84	564	44 33	15 22	gl	x	x	x	x	x	x	x	x
Gračac	85	560	44 18	15 51	ob		x	x	x	x	x	x	x
Hvar	90	20	43 10	16 27	gl	x	x	x	x	x	x	x	x
Illok	74	133	45 14	19 23	ob		x	x	x	x	x	x	x
Karlovac	53	112	45 30	15 33	ob	x	x	x	x	x	x	x	x
Knin	86	234	44 02	16 12	ob	x	x	x	x	x	x	x	x
Komiža	88	6	43 03	16 05	ob		x	x	x	x	x	x	x
Koprivnica	43	141	46 11	16 49	ob		x	x	x	x	x	x	x
Korčula	97	15	42 58	17 09	ob		x	x	x	x	x	x	x
Kostel	40	270	46 11	15 45	ob		x	x	x	x	x	x	x
Križevci	42	155	46 02	16 33	ob	x	x	x	x	x	x	x	x
Lastovo	96	186	42 46	16 54	gl	x	x	x	x	x	x	x	x
Lidčko Lešće	83	463	44 48	15 19	ob		x	x	x	x	x	x	x
Lipik	65	154	45 25	17 10	ob		x	x	x	x	x	x	x
Makarska	92	2	43 18	17 01	ob		x	x	x	x	x	x	x
Mali Lošinj	77	53	44 32	14 28	gl	x	x	x	x	x	x	x	x
Ogulin	52	328	45 16	15 14	gl	x	x	x	x	x	x	x	x
Opuzen	93	2	43 01	17 34	ob		x	x	x	x	x	x	x
Orebic	98	6	42 58	17 10	ob		x	x	x	x	x	x	x
Osijek	73	89	45 32	18 44	gl	x	x	x	x	x	x	x	x
Pag	81	3	44 27	15 04	ob		x	x	x	x	x	x	x
Palagruž	94	98	42 24	16 16	ob	x	x	x	x	x	x	x	x
Parg	48	863	45 36	14 38	ob	x	x	x	x	x	x	x	x
Pazin	46	291	45 14	13 56	ob	x	x	x	x	x	x	x	x
Poreč	44	15	45 14	13 36	ob		x	x	x	x	x	x	x
Pula	75	30	44 52	13 51	ob		x	x	x	x	x	x	x
Puntijarka	55	988	45 55	15 58	gl	x	x	x	x	x	x	x	x
Rab	78	24	44 45	14 46	ob	x	x	x	x	x	x	x	x
Rijeka	47	104	45 20	14 27	ob	x	x	x	x	x	x	x	x
Rovinj	45	5	45 05	13 39	ob		x	x	x	x	x	x	x
Senj	79	26	44 59	14 54	gl	x	x	x	x	x	x	x	x
Sinj	91	308	43 43	16 40	ob		x	x	x	x	x	x	x
Sisak	61	93	45 30	16 23	ob	x	x	x	x	x	x	x	x
Škrad	51	675	45 26	14 59	ob		x	x	x	x	x	x	x
Sl. Požega	68	152	45 20	17 41	ob		x	x	x	x	x	x	x
Sl. kroc	69	88	45 10	18 00	gl	x	x	x	x	x	x	x	x
Slunji	54	258	45 07	15 35	ob		x	x	x	x	x	x	x

AKTUVČNI SFIŠSAK STANICA
PO SOCIJALISTIČKIM AC. UBLJEDAM

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A 1	Broj stanice 2	Nadmorska visina H.m 3	Geografska širina lat. 4	Geografska dužina lon. 5	Red stanice 6	Vrednost pritisak atmosfera 7	Temperatura vazduha 8	Vlažnost vazduha 9	Vetar 10	Oblačnost 11	Insolacija 12	Padavine 13	Broj karak- terističnih dani 14
Maoča	124	325	44°19'	18°59'	ob		x	x	x	x	x	x	x
Mlinište	110	1130	44 16	16 52	ob		x	x	x	x	x	x	x
Modriča	122	115	44 59	17 18	ob		x	x	x	x	x	x	x
Mostar	137	99	43 21	17 18	gl	x	x	x	x	x	x	x	x
Ponikve	125	970	44 11	18 22	ob		x	x	x	x	x	x	x
Potoci-Zeljuša	138	96	43 24	17 53	ob		x	x	x	x	x	x	x
Prijedor	109	135	44 59	16 45	ob		x	x	x	x	x	x	x
Prnjavor	118	150	44 52	17 42	ob		x	x	x	x	x	x	x
Prozor	133	800	43 50	17 38	ob		x	x	x	x	x	x	x
Rakitno	131	915	43 34	17 27	ob		x	x	x	x	x	x	x
Sanski Most	108	158	44 46	16 42	gl		x	x	x	x	x	x	x
Sarajevo-aerodrom	142	510	43 49	18 20	gl	x	x	x	x	x	x	x	x
Sarajevo	143	630	43 52	18 26	gl	x	x	x	x	x	x	x	x
Sokolac	147	872	43 57	18 49	ob		x	x	x	x	x	x	x
Srebrenica	129	550	44 02	19 19	ob		x	x	x	x	x	x	x
Teslić	119	225	44 36	17 54	ob		x	x	x	x	x	x	x
Travnik	117	581	44 14	17 40	ob		x	x	x	x	x	x	x
Tuzla	125	305	44 33	18 42	gl	x	x	x	x	x	x	x	x
Vlašenica	127	630	44 12	18 57	ob		x	x	x	x	x	x	x
Zenica	120	344	44 13	17 54	gl	x	x	x	x	x	x	x	x
S O C I J A L I S T I C K A R E P U B L I K A S R B I J A													
Al-Ksandrovac	202	360	43°27'	21°04'	ob		x		x	x	x	x	x
Babušnica	214	495	43 04	22 26	ob		x		x	x	x	x	x
Bačka Topola	156	100	41 41	19 39	ob		x	x	x	x	x	x	x
Bački Petrovac	155	89	41 22	19 34	ob		x	x	x	x	x	x	x
Bećej	161	78	45 38	20 02	ob		x	x	x	x	x	x	x
Bela Crkva	183	90	44 54	21 25	ob		x	x	x	x	x	x	x
Bele Vode-Golija	197	1500	43 25	20 17	ob		x	x	x	x	x	x	x
Beograd	173	132	44 48	20 28	gl	x	x	x	x	x	x	x	x
Bor	188	380	44 05	22 06	ob		x	x	x	x	x	x	x
Bosiljevac	235	830	42 30	22 28	ob		x	x	x	x	x	x	x
Bujanovac	228	400	42 27	21 47	ob		x	x	x	x	x	x	x
Bukovička Banja	176	265	44 18	20 33	ob		x	x	x	x	x	x	x
Čačak	198	250	43 53	20 19	ob		x	x	x	x	x	x	x
Čuprija	207	123	43 56	21 23	gl	x	x	x	x	x	x	x	x
Debeli Lug	187	290	44 22	21 55	ob		x	x	x	x	x	x	x
Dimitrovgrad	217	446	43 01	22 45	gl	x	x	x	x	x	x	x	x
Dragaš	222	1060	42 04	20 39	ob		x	x	x	x	x	x	x
Flamunda	181	160	44 56	21 05	ob		x	x	x	x	x	x	x
Gladnoš	160	185	45 08	20 00	ob		x	x	x	x	x	x	x
Gornji Milanovac	174	335	44 02	20 28	ob		x		x	x	x	x	x
Istok	220	465	42 47	20 30	ob		x		x	x	x	x	x
Ivanjica	196	465	43 35	20 14	ob		x	x	x	x	x	x	x
Jaša	165	80	41 27	20 51	ob		x	x	x	x	x	x	x

AZBUČNI SPISAK STANICA

PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

V

S T A N I C A	Broj stanice	Nadmorska visina H m	Geografska latituda 9°N	Geografska duljina 17°E Gr.	Rod stanice	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Imobilacija	Padavine	Broj karak- teristич- nih dani	
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Kikinda	164	81	45°51'	20°28'	gl		x	x	x	x	x	x	x
Klina	221	385	42 38	20 34	ob		x		x	x	x	x	x
Knjaževac	212	280	43 34	22 16	ob		x		x	x	x	x	x
Kos.Mitrovica	224	510	42 53	20 52	ob		x		x	x	x	x	x
Kragujevac	179	190	44 02	20 56	ob		x		x	x	x	x	x
Kraljevo	200	219	43 44	20 41	gl	x	x	x	x	x	x	x	x
Kruševac	206	166	43 34	21 21	gl		x		x	x	x	x	x
Kukavica	230	1250	42 45	21 59	ob		x		x	x	x	x	x
Kuršumlija	205	380	43 08	21 16	gl		x		x	x	x	x	x
Leskovac	211	224	43 01	21 57	gl	x	x	x	x	x	x	x	x
Loznica	167	121	44 33	19 14	gl	x	x	x	x	x	x	x	x
Ljubovija	168	170	44 11	19 23	ob		x		x	x	x	x	x
Mitrovac-Tara	191	1080	43 55	19 26	ob		x		x	x	x	x	x
Negotin	190	42	44 14	22 33	gl	x	x	x	x	x	x	x	x
Niš	210	202	43 20	21 54	gl	x	x	x	x	x	x	x	x
Novi Pazar	199	545	43 08	20 31	ob		x		x	x	x	x	x
Novi Sad-Petrovaradin	159	132	45 15	19 52	gl	x	x	x	x	x	x	x	x
Novi Sad-Rimske Šančevi	158	84	45 20	19 51	ob	x	x	x	x	x	x	x	x
Palić	152	102	46 06	19 46	gl	x	x	x	x	x	x	x	x
Pančevo	177	80	44 53	20 40	ob		x		x	x	x	x	x
Peć	218	498	42 40	20 18	gl	x	x	x	x	x	x	x	x
Petrovac	184	120	44 23	21 25	ob		x		x	x	x	x	x
Pirot	215	370	43 09	22 36	ob		x		x	x	x	x	x
Predejane	232	318	42 50	22 08	ob		x		x	x	x	x	x
Priština	225	573	42 39	21 09	gl	x	x	x	x	x	x	x	x
Prizren	223	402	42 13	20 44	gl		x		x	x	x	x	x
Prokuplje	208	265	43 14	21 36	ob		x		x	x	x	x	x
Rekovac	203	230	43 52	21 06	ob		x		x	x	x	x	x
Rudnik	175	700	44 08	20 31	ob		x		x	x	x	x	x
Senta	162	80	45 56	20 05	ob		x		x	x	x	x	x
Sijarinska Banja	227	455	42 47	21 36	ob		x		x	x	x	x	x
Sjenica	194	1015	43 16	20 01	gl	x	x	x	x	x	x	x	x
Skivjane-Djakovica	219	415	42 26	20 21	ob		x		x	x	x	x	x
Smederevo	178	120	44 39	20 55	ob		x		x	x	x	x	x
Smed.Palanka	180	121	44 22	20 57	gl	x	x	x	x	x	x	x	x
Sokobanja	209	300	43 39	21 51	ob		x		x	x	x	x	x
Sombor	153	88	45 47	19 05	gl		x		x	x	x	x	x
Sr.Mitrovica	169	81	44 58	19 38	gl		x		x	x	x	x	x
Surdulica	233	500	42 41	22 11	ob		x		x	x	x	x	x
Svetozarevo	204	115	43 59	21 14	ob		x		x	x	x	x	x
Šabac	170	80	44 46	19 41	ob		x		x	x	x	x	x
Šid	154	105	45 07	19 15	ob		x		x	x	x	x	x
Šušara	182	180	44 56	21 08	ob		x		x	x	x	x	x
Tekija	189	50	44 41	22 25	ob		x		x	x	x	x	x
Titovo Užice	193	440	43 52	19 51	ob		x		x	x	x	x	x

A Z B U Ć N I S P I S A K S T A N I C A
PO SOCIJALISTIČKIM REPUBLIKAMA

VI Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Nadzemna visina H, m	Geografska širina φ, °N	Geografska dužina λ, °E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblakost	Insolencija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Topli Do	216	700	43°20'	22°41'	ob		x			x		x	x
Uroševac	226	580	42 23	21 10	ob		x	x	x	x	x	x	x
Už. Požega	195	311	43 51	20 02	gl	x	x	x	x	x	x	x	x
Valjevo	172	174	44 17	19 55	gl	x	x	x	x	x	x	x	x
Veliko Gradište	185	79	44 46	21 31	gl	x	x	x	x	x	x	x	x
Vladimirci	171	120	44 37	19 47	ob		x	x	x	x	x	x	x
Vlasina	234	1190	42 44	22 21	ob		x	x	x	x	x	x	x
Vlasotince	231	270	42 58	22 08	ob		x	x	x	x	x	x	x
Vranje	229	433	42 33	21 55	gl	x	x	x	x	x	x	x	x
Vrbas	157	87	45 34	19 39	ob		x	x	x	x	x	x	x
Vrnjačka Banja	201	235	43 37	20 54	ob		x	x	x	x	x	x	x
Vršac	166	83	45 09	21 19	gl	x	x	x	x	x	x	x	x
Zaječar	213	197	43 53	22 18	ob		x	x	x	x	x	x	x
Zlatibor	192	1029	43 44	19 43	gl	x	x	x	x	x	x	x	x
Zrenjanin	163	80	45 24	20 21	gl		x	x	x	x	x	x	x
Žagubica	186	314	44 12	21 47	ob		x	x	x	x	x	x	x
S O C I J A L I S T I Č K A R E P U B L I K A C R N A G O R A													
Bar	247	1	42°06'	19°06'	gl	x	x	x	x	x	x	x	x
Bijelo Polje	238	560	43 02	19 45	ob		x	x	x	x	x	x	x
Budva	243	2	42 17	18 51	ob	x	x	x	x	x	x	x	x
Cetinje	244	655	42 24	18 56	ob		x	x	x	x	x	x	x
Građevno	241	710	42 39	18 41	ob		x	x	x	x	x	x	x
Herceg Novi - Igalo	240	40	42 28	18 30	gl	x	x	x	x	x	x	x	x
Ivangrad	250	670	42 50	19 52	ob	x	x	x	x	x	x	x	x
Kolašin	249	944	42 50	19 32	gl	x	x	x	x	x	x	x	x
Krtac	236	950	43 00	18 44	ob		x	x	x	x	x	x	x
Nikšić	245	647	42 46	18 57	gl	x	x	x	x	x	x	x	x
Pljevlja	239	784	43 21	19 21	gl	x	x	x	x	x	x	x	x
Titograd	248	49	42 26	19 17	ob	x	x	x	x	x	x	x	x
Tivat	242	5	42 26	18 42	ob	x	x	x	x	x	x	x	x
Ulcinj	251	97	41 55	19 13	gl	x	x	x	x	x	x	x	x
Virkapazar	246	14	42 14	19 05	ob		x	x	x	x	x	x	x
Žabljak	237	1450	43 09	19 08	gl	x	x	x	x	x	x	x	x
S O C I J A L I S T I Č K A R E P U B L I K A M A K E D O N I J A													
Berovo	283	824	41°43'	22°51'	gl	x	x	x	x	x	x	x	x
Bitola	267	586	41 03	21 22	gl	x	x	x	x	x	x	x	x
Debar	257	675	41 31	20 32	ob		x	x	x	x	x	x	x
Delčevo	282	630	41 58	22 46	ob		x	x	x	x	x	x	x
Demir Kapija	275	125	41 25	22 15	gl	x	x	x	x	x	x	x	x
Erdišelija	272	253	41 50	22 02	ob		x	x	x	x	x	x	x
Gevgelija	278	59	41 09	22 30	ob		x	x	x	x	x	x	x
Gostivar	262	525	41 48	20 55	ob		x	x	x	x	x	x	x
Kavadarci	273	265	41 26	22 02	ob		x	x	x	x	x	x	x

A) Dnevna osmafranja

$\psi = 46^{\circ}04'$, $N \lambda = 14^{\circ}31'$, E Gr. $\Delta G = +58$ min.

MK. St. 13

DG	Vzdušni pritisak P mm			Temperatura vzduha T °C							Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	742.4	742.0	742.3	00.0	00.7	00.0	00.2	01.6	-00.2	-01.1	04.1	04.3	04.0	89	90	88	89	NF	1	W	1	NE	1
2	741.4	740.3	740.0	00.0	00.9	00.4	00.4	01.6	-00.2	-01.2	04.2	04.4	04.6	91	90	98	93	NE	1	NE	1	-	0
3	739.7	739.1	739.4	00.3	01.6	01.0	01.0	02.2	00.2	-00.3	04.6	04.9	04.7	98	95	95	96	NNW	1	NNW	1	NW	1
4	741.9	741.0	743.4	00.9	02.5	00.8	01.5	02.9	00.5	-00.5	04.7	05.3	04.9	97	97	100	98	W	1	E	1	NE	1
5	741.0	742.0	741.2	00.4	01.4	01.1	01.1	01.8	00.0	00.0	04.6	04.9	05.0	98	97	98	98	NE	1	SW	4	NE	1
6	737.3	735.0	736.4	01.0	00.8	00.7	00.8	02.0	00.4	00.4	04.9	04.8	04.7	100	98	97	98	NNW	1	NE	1	NE	1
7	734.9	734.1	740.0	01.0	02.4	01.0	01.0	02.7	00.6	-00.4	04.8	04.8	04.7	98	97	95	93	E	1	NW	1	NNW	1
8	733.4	734.1	740.0	00.6	02.4	01.0	01.3	02.6	00.4	00.4	04.7	06.9	04.8	95	90	97	94	SF	1	W	1	NE	1
9	732.6	738.1	736.0	00.6	01.6	01.0	01.1	02.2	00.4	00.2	04.6	04.9	04.7	95	95	95	95	NW	1	NE	1	SE	1
10	736.2	738.1	740.9	01.0	02.3	01.3	01.6	02.7	00.6	-00.2	04.7	04.5	04.4	95	92	88	88	NE	1	SF	1	SE	2
11	742.2	742.6	743.8	00.4	00.9	00.9	00.8	02.7	00.1	00.0	04.2	04.2	04.5	89	86	91	89	SF	1	S	2	SE	1
12	744.8	744.9	745.6	00.0	01.0	01.0	00.8	01.7	-00.1	-00.1	04.5	04.8	04.7	98	98	95	97	E	1	W	1	E	1
13	743.8	743.5	744.8	-00.6	00.4	00.1	00.0	01.0	-00.7	-00.6	04.3	04.6	04.3	98	96	93	96	SSE	1	NW	1	SE	1
14	744.3	743.9	744.6	00.0	00.4	-00.2	00.0	00.7	-00.2	-00.8	03.8	03.7	03.5	84	79	81	81	SF	1	E	1	NE	1
15	743.7	742.5	742.2	-01.0	01.4	01.1	00.7	01.8	-01.0	-01.5	03.5	04.0	04.1	81	78	83	81	NW	1	NW	1	NE	1
16	741.2	741.7	739.0	00.7	05.4	00.6	01.8	05.9	00.2	-01.8	04.4	05.0	04.5	91	74	93	86	SE	1	-	0	NE	1
17	735.1	736.7	739.3	00.0	06.2	01.4	03.8	06.8	-00.3	-04.2	05.6	06.3	04.6	86	69	87	87	NW	1	NE	1	NW	1
18	739.9	738.3	739.2	-00.7	07.2	03.8	03.5	08.3	-01.7	-04.5	03.6	04.0	04.7	82	52	78	71	N	1	NE	1	N	1
19	740.1	740.1	740.3	01.4	05.9	02.0	03.2	07.1	01.2	-02.4	04.6	05.2	04.9	90	74	87	84	NF	1	SE	1	NW	1
20	740.3	739.1	741.5	-01.6	08.6	02.6	03.1	11.3	-02.0	-05.1	03.9	06.2	04.7	96	74	86	85	N	1	ESE	1	-	0
21	743.3	742.2	743.5	-02.2	06.4	-00.2	01.0	07.4	-02.4	-07.5	03.7	05.3	04.4	98	73	98	90	SF	1	SW	1	-	0
22	741.2	741.6	741.6	-01.4	00.2	-01.2	-00.9	00.4	-01.9	-06.9	04.1	04.5	04.2	100	96	101	99	-	0	ESE	1	ESE	1
23	744.2	743.3	741.9	-01.6	01.7	00.2	00.0	02.0	-01.9	-02.0	04.0	04.7	04.5	100	93	96	96	NF	1	NE	1	W	1
24	741.8	740.0	738.7	-01.8	00.1	-01.0	-00.9	00.7	-01.8	-01.7	03.8	04.1	04.2	96	90	98	95	SW	1	S	1	SW	1
25	739.0	738.9	739.0	-01.4	02.8	00.0	00.4	04.4	-01.6	-02.0	04.1	04.7	04.5	100	84	98	94	F	1	E	1	N	1
26	739.9	739.7	739.1	-00.6	00.7	-00.3	-00.1	00.8	-00.7	-00.5	04.4	04.7	04.5	100	98	100	99	SE	1	NE	1	NE	1
27	736.8	736.1	737.9	-00.7	02.1	00.7	00.7	04.6	-00.8	-00.8	04.3	05.0	04.6	98	94	95	96	ENE	1	-	0	NE	1
28	739.7	739.4	739.4	-00.2	03.4	01.5	01.6	04.0	-00.6	-01.9	04.5	05.4	05.0	100	92	98	97	-	0	S	1	NW	1
29	738.7	738.2	739.5	00.0	04.7	04.8	03.6	05.7	00.0	00.0	04.6	05.3	05.2	100	83	80	88	SW	1	SW	3	SW	3
30	741.8	741.9	741.9	01.1	04.7	04.0	03.5	05.6	00.2	-03.7	04.6	05.4	05.5	93	84	90	89	NE	1	NE	1	N	1
31	741.5	741.0	741.2	02.0	07.5	07.6	06.2	08.7	01.4	-03.2	05.3	05.4	06.4	100	82	82	88	NF	1	S	1	W	1
MES.	740.8	740.3	741.1	00.1	02.8	01.2	01.4	03.7	-00.4	-01.7	00.4	04.9	04.6	95	87	92	91	0.9	1.1	1.0	1.0	1.0	

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1	739.3	738.7	738.7	05.4	07.6	05.6	06.1	09.0	05.4	04.7	06.3	06.8	07.8	93	87	85	88	N	1	-	G	1	
2	738.3	737.7	738.3	05.3	10.0	07.8	07.7	10.8	05.0	04.9	06.5	07.6	07.5	97	85	95	92	-	0	NF	1	NE	1
3	736.7	734.1	733.2	05.4	10.0	06.9	07.3	10.3	05.3	02.2	06.7	07.5	07.5	100	81	97	93	N	1	NW	1	1	0
4	730.6	729.5	730.3	05.8	07.1	03.4	04.9	08.7	03.3	04.8	06.5	06.1	05.5	94	81	94	90	SE	1	SE	2	-	0
5	730.3	727.8	726.2	02.3	08.1	06.2	05.7	04.7	02.2	02.6	05.3	06.2	06.0	98	76	84	86	-	0	NE	1	SW	2
6	720.5	712.5	707.6	04.7	08.1	08.5	08.0	09.7	05.4	04.1	06.0	06.9	07.2	82	85	87	85	SW	2	SW	4	SW	3
7	712.7	715.5	719.7	01.0	07.7	01.2	02.8	01.6	00.8	-00.4	04.8	04.4	04.4	97	56	88	80	SF	1	SW	3	NE	1
8	727.5	731.9	736.0	-02.4	09.1	01.9	02.6	09.4	-02.4	-06.5	03.7	02.7	03.2	98	31	60	63	NE	1	NW	3	N	1
9	736.8	736.6	737.6	-02.4	11.5	05.4	05.0	11.7	-02.8	-07.4	03.2	03.7	04.0	85	36	59	60	N	1	K	4	W	3
10	737.8	738.7	738.9	02.4	11.7	06.8	06.9	12.3	01.4	-01.2	04.7	05.1	05.2	86	50	70	69	NW	1	SW	3	SW	3
11	736.2	733.9	732.3	06.3	09.8	08.7	08.4	10.8	00.7	-04.0	05.3	06.4	06.2	73	70	73	72	NW	2	SW	3	SW	3
12	730.6	730.3	729.3	08.4	11.6	07.9	09.0	12.5	06.9	06.4	06.4	06.0	05.7	78	59	71	69	SW	3	SW	3	MSW	1
13	726.8	725.2	725.7	04.8	09.8																		

HK. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Veličina 0-9	Oblačnost N (0-10)					Intenziteta broj sati	Padavine R mm	Snežni pokrov h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	5	10	10	-	10*	10.0	00.0	27.5	03	* ⁺ n-12 ¹ / ₂ i, 16 ³ -n; ⁺ n-19 ¹ / ₂ i
2	5	10*	10*	-	10	10.0	00.0	04.1	07	= ⁺ n-9, ⁺ n-4 ¹ / ₂ -20 ¹ , ⁺
3	6	10	10	-	10	10.0	00.0	01.6	08	= ⁺ n-5 ¹ / _{2-8¹/₂; *⁺n-5³/₄, 8⁴o, ⁺n-16⁴-17¹/₂, ⁺n-17¹/₂-19³/₄, ⁺}
4	3	10	10	-	10	10.0	00.0	01.0	05	= ⁺ n-17 ³ / ₄ , 12 ¹ / ₂ -17 ¹ / ₂ , ⁺ n-17 ¹ / ₂ -12 ³ / ₄ , ⁺ n-17 ³ / ₄ -18 ¹ / ₂ , ⁺ n-18 ¹ / ₂ -16 ³ / ₄
5	4	10	10	-	10	10	00.0	00.0	02	= ⁺ n-12 ¹ / ₂ , ⁺ n-12 ³ / ₄ , 15 ³ / ₄ , ⁺ n-12 ³ / ₄ -16 ¹ / ₂ , ⁺ n-16 ¹ / ₂ -18, ⁺
6	3	10	10	*	10	10	00.0	00.6	*	* ⁺ n-10 ¹ / _{2, ⁺n-10¹/₂-11¹/₂, *⁺n-11¹/₂-18¹/₂, ⁺n-5, ⁺n-10¹/₂, ⁺n-15-17³/₄, 10¹/₂-n, ⁺}
7	6	10	10	-	10	10	00.0	04.5	00	= ⁺ n-9, ⁺ n-17 ¹ / ₂ -17 ³ / ₄ , * ⁺ n-17 ¹ / ₂ -8 ¹ / ₂ , = ⁺ n-9, ⁺
8	5	10	10	-	10	10.0	00.0	00.1	00	= ⁺ n-20 ¹ , ⁺ n-20 ¹ , n
9	5	10	10	*	10	10	00.0	00.0	*	* ⁺ n-5, ⁺ n-n, ⁺ n-12 ¹ / _{2, ⁺n-15¹/₂-19¹/_{2, ⁺n-19¹/₂-n}}
10	6	10	10	*	10	10	00.0	02.1	00	* ⁺ n-4 ¹ / _{2, =⁺n-n, ⁺n-4¹/_{2-7¹/_{2, ⁺n-7¹/₂-10¹/₂}}}
11	6	10	10	-	10	10	10.0	00.0	00	= ⁺ n-7
12	3	10	10	*	10	10	00.0	00.0	*	= ⁺ n-4 ¹ / _{2, ⁺n-4¹/₂-6, 12¹/₂-19¹/₂, ⁺n-12¹/₂, 10¹/₂-n}
13	4	10	10	*	10	10	10.0	00.0	*	= ⁺ n-12 ¹ / ₂ , ⁺ n-7-8, ⁺ n-10 ¹ / ₂ , ⁺ n-13 ¹ / ₂ , ⁺ n-13 ¹ / ₂ -n
14	6	10	10	-	10	10	10.0	00.0	*	= ⁺ n-n
15	6	10	10	-	10	10	10.0	00.0	*	= ⁺ n-n
16	5	10	06	0	00	05.3	01.4	*	= ⁺ n-20 ¹ , ⁺ n-20 ¹ , ⁺ n-20 ¹ -n	
17	6	10	06	0	00	05.3	01.0	*	= ⁺ n-4 ¹ / ₂ , ⁺ n-4 ¹ / ₂ -15, ⁺ n-17 ¹ / ₂ -10 ¹ / ₂ , ⁺ n-18 ¹ / ₂ -n, ⁺ n-20 ¹ -n	
18	6	01	08	0	01	03.3	05.6	01.6	*	= ⁺ n-10 ¹ / ₂ , ⁺ n-8 ¹ / ₂ -9 ¹ / ₂ , = ⁺ n-10 ¹ / ₂ -n
19	6	10	08	0	00	06.0	00.4	*	= ⁺ n-9, ⁺ n-14, 18-n, ⁺ n-14-18	
20	4	02	04	0	00	02.0	04.2	*	= ⁺ n-6, ⁺ n-10, ⁺ n-10, ⁺ n-12 ¹ / ₂ , ⁺ n-12 ¹ / ₂ -9 ¹ / ₂	
21	5	10	00	0	10	06.7	04.0	*	= ⁺ n-4, 12 ¹ / _{2-15¹/_{2, 12¹/_{2-19¹/₂, ⁺n-7-11¹/₂, 19¹/₂-17¹/₂, ⁺n-12¹/₂, 10¹/₂-n}}}	
22	3	10	10	*	10	10.0	00.0	*	= ⁺ n-12 ¹ / ₂ , ⁺ n-12 ¹ / _{2-48, ⁺n-20¹-8¹/₂, ⁺n-8¹/₂-11¹/₂, ⁺n-13¹/₂-14¹/₂, =⁺n-14¹/₂-18}	
23	3	10	10	*	10	10.0	00.0	*	= ⁺ n-4, 12 ¹ / _{2-18¹/_{2, ⁺n-18¹/₂-11¹/_{2, 16¹/₂-18¹/₂, =⁺n-12¹/₂-16¹/₂}}}	
24	5	10	09	0	10	09.7	00.0	*	= ⁺ n-4, 12 ¹ / _{2-10¹/_{2, ⁺n-12¹/₂-10¹/_{2, ⁺n-12¹/₂-10¹/₂, ⁺n-12¹/₂-10¹/₂}}}	
25	4	10	08	0	10	05.3	01.5	*	= ⁺ n-12 ¹ / ₂ , ⁺ n-12 ¹ / ₂ -7 ¹ / _{2, ⁺n-7¹/₂-10¹/_{2, =⁺n-12¹/₂-10¹/₂, ⁺n-12¹/₂-10¹/₂}}	
26	2	10	*	10	*	10	10.0	00.0	00.2	00
27	5	10	10	*	09	05.7	00.7	00.1	*	= ⁺ n-5 ¹ / ₂ , ⁺ n-5 ¹ / ₂ -17 ¹ / ₂ , ⁺ n-7 ¹ / ₂ -10 ¹ / ₂
28	3	10	*	09	05	10	05.0	00.5	00.1	= ⁺ n-2 ¹ / _{2-12¹/_{2, ⁺n-13¹/₂, ⁺n-13¹/₂-18¹/₂, ⁺n-13¹/₂-18¹/₂, ⁺n-14¹/₂-18¹/₂}}
29	6	10	*	10	08	04.3	00.0	*	= ⁺ n-12, ⁺ n-12-12 ¹ / ₂ , = ⁺ n-12 ¹ / ₂ -17 ¹ / ₂ , ⁺ n-19 ¹ / ₂ -n, ⁺ n-19 ¹ / ₂	
30	6	10	*	10	10	10.0	00.0	*	= ⁺ n-n, ⁺ n-8 ¹ / ₂	
31	5	10	*	09	09	09.3	00.1	*	= ⁺ n-n, ⁺ n-5 ¹ / ₂ , 8 ¹ / ₂ -9, = ⁺ n-2 ¹ / ₂ -8 ¹ / ₂ , = ⁺ n-9-17, ⁺ n-16 ¹ / ₂ -17 ¹ / ₂	
MES. WRED.			09.4	08.9	09.3	08.9	19.3	44.6		

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1	7	10	08	06	08.0	00.5	C3.7	*	* ⁺ n-10 ¹ / ₂ , = ⁺ n-13, ⁺ n-18 ¹ / ₂ -n
2	8	10	10	10	10.0	00.0	05.1	*	* ⁺ n-5 ¹ / ₂ , ⁺ n-17 ¹ / ₂ -19 ¹ / ₂
3	8	10	09	10	09.7	01.1	C3.4	*	= ⁺ n-4 ¹ / ₂ , ⁺ n-6 ¹ / ₂ -9 ¹ / ₂ , ⁺ n-13 ¹ / ₂ , 5 ¹ / ₂ , 9 ¹ / ₂ , 10, 14 ¹ / ₂ , = ⁺ n-11 ¹ / ₂ , 17 ¹ / ₂ -n
4	6	10	09	07	08.7	00.7	07.7	*	* ⁺ n-6, ⁺ n-14 ¹ / ₂ -18 ¹ / ₂ , ⁺ n-14 ¹ / ₂ -n, ⁺ n-19 ¹ / ₂ -n
5	6	10	08	10	09.3	01.6	*	*	= ⁺ n-4 ¹ / ₂ , ⁺ n-8 ¹ / ₂ -10 ¹ / _{2, =⁺n-14¹/₂-8¹/₂, ⁺n-10¹/₂-n, ⁺n-12¹/₂-19¹/₂}
6	7	10	10	10	10.0	00.0	00.2	*	= ⁺ n-6 ¹ / ₂ , ⁺ n-15 ¹ / ₂ , ⁺ n-16 ¹ / ₂ -n, ⁺ n-19 ¹ / ₂
7	8	10	04	02	05.3	05.7	22.2	C2	* ⁺ n-16 ¹ / ₂ , = ⁺ n-13 ¹ / ₂
8	8	10	03	02	05.0	06.1	*	*	= ⁺ n-10 ¹ / ₂ , = ⁺ n-5 ¹ / ₂ , 5 ¹ / ₂ , 11 ¹ / ₂ -19 ¹ / ₂ , = ⁺ n-15 ¹ / ₂ , 10 ¹ / ₂ , = ⁺ n-25 ¹ / ₂
9	8	02	05	10	05.7	06.3	*	*	= ⁺ n-10
10	8	08	04	00	04.0	06.2	*	*	*
11	7	10	09	09	09.3	01.0	*	*	⁺ n-6
12	8	05	09	03	05.7	04.0	*	*	⁺ n-9 ¹ / ₂ , ⁺ n-11 ¹ / ₂
13	6	09	10	08	09.0	00.4	*	*	⁺ n-12 ¹ / ₂ , 19 ¹ / ₂ , ⁺ n-13 ¹ / ₂ -18 ¹ / ₂ , ⁺ n-18 ¹ / ₂ -19 ¹ / ₂
14	6	10	10	10	10.0	00.0	00.2	*	⁺ n-12 ¹ / ₂ , 19 ¹ / ₂ , ⁺ n-13 ¹ / ₂ -14 ¹ / ₂ , ⁺ n-13 ¹ / ₂ -19 ¹ / ₂
15	6	10	08	10	09.3	01.1	03.1	*	⁺ n-9, 19-n, ⁺ n-8 ¹ / ₂ , ⁺ n-11 ¹ / ₂ -14 ¹ / ₂ , ⁺ n-14 ¹ / ₂ -n
16	6	10	10	10	10.0	00.0	00.1	*	⁺ n-15, 18 ¹ / ₂ -n, ⁺ n-15-18 ¹ / ₂
17	7	10	10	09	09.7	00.1	CC.0	*	⁺ n-9 ¹ / ₂ , ⁺ n-10 ¹ / ₂ , ⁺ n-10 ¹ / ₂ -20 ¹ / ₂ , = ⁺ n-19 ¹ / ₂ -n
18	4	10	10	10	10.0	00.0	C1.0	*	= ⁺ n-5, 9-17 ¹ / ₂ , ⁺ n-3 ¹ / ₂ -6 ² / ₁ , ⁺ n-20 ¹ / ₂ , = ⁺ n-5, 17 ¹ / ₂ -n, ⁺ n-6 ² / ₁
19	7	10	06	03	06.3	04.6	02.0	*	= ⁺ n-11 ¹ / ₂ , ⁺ n-9 ¹ / ₂ -11 ¹ / ₂ , ⁺ n-11 ¹ / ₂ -n, ⁺ n-25 ¹ / ₂ , ⁺ n-9 ¹ / ₂ , = ⁺ n-12 ¹ / ₂ -8 ¹ / ₂ ui, ⁺ n-11 ¹ / ₂ -13 ¹ / ₂ , ⁺ n-13 ¹ / ₂ -19 ¹ / ₂
20	7	01	10	10	07.0	03.4	*	*	⁺ n-9, 19-n, ⁺ n-5 ¹ / ₂ -6, ⁺ n-6-9-19 ¹ / ₂ , ⁺ n-9-19 ¹ / ₂
21	7	10	09	08	09.0	01.2	CC.3	*	⁺ n-9, 19-n, ⁺ n-5 ¹ / ₂ -6, ⁺ n-6-9-19 ¹ / ₂ , ⁺ n-9-19 ¹ / ₂
22	7	10	10	00	06.7	00.2	00.0	*	⁺ n-10 ¹ / ₂ , = ⁺ n-5 ¹ / ₂ -12
23	7	10	01	00	03.7	06.2	*	*	= ⁺ n-11 ¹ / ₂ , ⁺ n-9 ¹ / ₂ , ⁺ n-10 ¹ / ₂ -14 ¹ / ₂ , ⁺ n-20 ¹ / ₂ -n
24	8	04	10	09	07.7	02.1	*	*	⁺ n-7-9 ¹ / ₂ , ⁺ n-9 ¹ / ₂ , ⁺ n-9 ¹ / ₂ -10 ¹ / ₂
25	6	09	10	10	09.7	0			

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 $\varphi = 46^{\circ}04'$ N $\lambda = 14^{\circ}31'$ E Gr. $\Delta G = + 58$ min.

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Dan	Vzdušni pritisak P mm			Temperatura vozduha T C°								Napon vodene pare e mm			Relativna vlažnost U%			Pravac i jačina vetro D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	737.0	736.0	734.7	-00.6	05.3	00.6	01.6	06.2	-00.8	-06.6	02.7	02.9	04.7	62	42	58	67	ENE 1	E 2	N 1
2	732.3	732.3	734.2	00.3	01.2	00.4	00.6	01.8	-00.2	-00.6	04.5	04.7	04.5	96	93	95	95	NF 1	NE 1	W 1
3	736.0	736.5	737.9	00.2	05.4	01.7	02.3	05.9	00.1	-00.2	04.5	03.5	04.1	96	53	79	76	N 1	S 1	E 1
4	736.9	735.7	734.1	00.4	01.3	00.6	00.7	02.0	00.4	00.1	04.6	04.7	04.7	96	93	98	96	NE 1	W 1	NE 1
5	732.4	733.3	733.6	07.0	03.7	02.0	02.4	03.8	00.5	00.0	05.0	05.6	05.0	94	94	95	94	NE 1	K 1	S 1
6	733.2	734.9	737.1	00.4	02.6	01.9	01.7	04.4	00.3	00.0	04.6	05.0	04.7	97	91	90	93	W 1	S 2	SE 2
7	737.6	734.1	739.3	02.2	04.6	02.6	03.0	06.0	01.9	00.4	05.1	04.5	04.4	95	71	80	82	W 1	SE 2	SE 3
8	739.2	736.8	740.9	01.2	02.7	01.1	01.9	03.3	01.0	00.6	04.3	04.5	04.6	87	81	89	86	SE 2	E 2	SE 1
9	733.7	736.9	741.0	01.0	03.7	01.2	01.8	04.3	00.7	00.0	04.6	04.1	04.0	93	69	80	81	SE 1	SE 3	SE 3
10	740.1	737.8	741.1	00.7	05.1	02.0	02.4	05.6	00.4	-00.9	04.0	03.3	04.4	84	51	84	73	N 1	E 3	SE 2
11	742.1	742.8	744.2	-01.0	05.4	02.8	02.8	07.4	-01.0	-05.4	03.8	04.0	04.6	89	56	83	76	NE 1	NE 3	E 1
12	744.0	743.1	741.0	02.2	04.7	02.9	03.2	05.6	01.8	-02.0	04.8	04.3	04.2	90	67	74	77	SE 1	E 2	E 2
13	739.1	736.0	735.4	01.0	08.3	03.4	04.2	10.6	01.4	00.8	03.6	03.8	04.3	71	47	73	64	NE 1	SE 1	SE 1
14	733.8	730.5	730.3	-02.6	12.5	06.3	05.7	13.7	-02.8	-07.5	03.8	05.4	04.8	100	49	67	72	NF 1	W 1	SSE 1
15	729.0	730.4	730.2	-00.6	10.1	04.6	04.6	10.8	-00.8	-06.5	04.1	05.7	05.0	95	62	80	79	NW 1	NE 3	SW 1
16	729.0	727.8	728.9	02.4	13.8	08.4	08.3	14.3	02.4	-00.6	04.8	03.9	04.3	89	33	53	58	W 1	SW 2	S 3
17	730.0	731.1	733.0	-00.4	15.9	10.2	09.0	16.8	-00.4	-04.9	04.2	05.8	04.8	95	43	51	63	NE 1	SW 4	WSH 3
18	734.0	733.2	733.9	02.2	12.0	11.4	09.5	13.7	01.4	-03.2	04.9	07.1	07.9	90	64	78	77	NF 1	SW 3	W 3
19	735.0	736.0	737.6	11.0	15.4	11.8	12.5	16.6	10.2	05.2	08.1	08.5	08.2	82	65	79	75	SW 2	SW 4	SW 2
20	737.0	732.1	739.6	11.4	16.2	11.8	12.8	17.1	10.9	08.2	08.5	07.6	07.6	84	55	75	71	NW 3	SW 3	SW 2
21	740.0	738.0	740.2	05.0	21.7	14.4	14.0	24.0	03.9	00.0	06.4	07.1	07.5	94	36	60	65	SE 1	NE 2	NW 2
22	740.0	737.6	736.4	04.9	22.8	14.4	14.1	24.4	04.9	-01.4	06.3	05.6	06.2	97	27	50	58	NE 1	NE 1	NW 1
23	736.3	736.0	737.8	07.5	19.2	12.2	12.8	19.4	07.2	03.2	06.5	05.2	07.3	83	31	68	61	N 1	SW 4	SW 1
24	739.0	737.5	737.3	04.4	20.2	14.2	13.3	21.2	04.0	-01.0	06.1	04.8	06.5	97	27	54	59	E 1	NE 1	SE 1
25	737.1	736.6	737.8	08.3	17.4	11.7	12.3	17.8	07.6	02.6	06.5	06.1	08.4	79	54	61	71	SW 1	NE 1	NE 1
26	737.7	734.9	734.3	08.0	19.0	14.6	14.1	19.3	07.0	02.6	07.5	08.7	07.9	94	53	63	70	NE 1	NE 1	NE 1
27	733.0	732.0	733.4	08.5	17.4	13.4	13.2	18.4	08.1	03.5	08.1	07.8	08.2	96	52	71	73	SW 1	SW 3	NW 3
28	734.5	734.3	735.7	06.1	14.4	09.7	10.0	18.6	05.8	00.3	07.0	05.2	08.3	99	67	92	86	E 1	2	NF 1
29	737.2	736.3	737.1	04.6	17.0	14.6	12.9	19.3	04.6	00.6	06.4	06.3	08.1	100	41	65	69	S 1	WSW 1	E 1
30	738.6	738.3	739.5	07.6	16.0	18.4	11.1	16.6	07.4	03.4	07.2	07.6	05.8	92	56	62	70	E 1	SE 1	E 1
31	738.5	736.1	736.4	05.5	14.8	10.6	10.4	15.3	05.3	01.1	08.4	04.6	05.5	94	37	57	63	NE 1	E 3	SE 3
MES.	736.5	735.0	735.6	03.6	11.4	07.6	07.4	12.4	03.0	-00.3	05.4	05.6	05.6	91	57	75	74	1.1	2.1	1.4
VRFD.	736.5	735.0	735.6	03.6	11.4	07.6	07.4	12.4	03.0	-00.3	05.4	05.6	05.6	91	57	75	74	1.1	2.1	1.4

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1	734.6	735.0	726.0	06.4	12.3	08.8	09.1	12.6	05.7	-0C.4	06.3	05.3	05.4	88	50	63	67	SE 1	SE 2	SE 2
2	736.5	736.3	739.4	07.2	11.2	09.2	09.2	11.8	06.6	05.6	06.7	06.1	06.2	88	61	71	73	SE 1	NE 3	E 1
3	740.4	739.1	739.3	02.2	16.1	09.0	09.1	16.1	01.5	-03.6	05.3	05.4	04.6	99	39	53	63	NF 1	SF 2	NE 1
4	738.7	735.7	735.2	01.6	16.6	09.4	09.3	17.1	00.8	-04.9	04.5	03.9	04.8	87	27	54	56	NF 1	SW 1	NF 1
5	735.2	734.5	736.5	01.6	16.2	10.4	09.7	17.1	00.2	-02.4	04.6	04.2	04.4	88	30	46	55	NE 1	E 3	N 2
6	737.5	736.4	737.6	03.6	16.1	09.6	09.7	17.0	02.5	-03.2	04.8	04.5	04.9	80	33	54	56	-	0	E 2
7	739.3	736.8	736.7	03.6	15.7	11.8	10.7	16.2	02.0	-03.3	05.0	05.6	05.6	85	42	54	60	E 1	NE 1	N 1
8	737.0	735.3	737.0	07.6	18.3	10.6	11.8	19.1	05.4	-01.2	04.8	04.4	04.7	97	28	49	55	NE 1	E 2	E 1
9	738.4	735.8	735.2	03.4	19.0	13.1	12.2	20.3	01.6	-04.1	04.8	03.7	06.6	82	23	58	54	E 1	N 1	SW 3
10	734.7	731.5	731.0	04.6	19.0	12.0	20.2	12.1	02.6	-01.7	05.6	04.7	04.2	88	27	40	52	N 1	SW 3	SW 3
11	728.8	727.2	726.7	05.7	12.7	08.9	09.1	14.0	04.0	-01.0	05.5	08.0	08.4	80	73	99	84	E 1	SE 2	NW 1
12	725.6	724.7	726.9	07.3	16.4	05.8	10.8	17.1	06.7	01.0	07.5	08.2	08.1	97	58	89	81	SW 1	SSW 3	St 1
13	728.2	729.6	730.7	09.4	12.8	10.6	10.9	13.5	08.4	07.0	08.6	09.0	08.8	98	81	92	90	SE 1	SW 1	SE 1
14	730.6	728.7	729.7	05.6	08.5	03.6	05.4	11.0	03.6	04.4	03.7	03.4	05.2	55	41	89	61	SE 4	SE 3	SE 1
15	728.8	725.9	727.9	03.2	13.5	09.2	08.8	13.7	01.6	-03.0	05.2	03.2	03.0	91	28	34	51	NE 1	E 3	SF 2
16	729.7	729.																		

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 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_f = 1.5 \text{ m}$

Dan	Veličina 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7	03	070	10*	06.7	05.7	.	.	.		
2	3	10*	10*	10*	10.0	00.0	06.0	06.	06		
3	7	10	060	10	09.7	02.8	09.5	11			
4	3	10*	10*	10*	10.0	00.0	01.5	01			
5	3	10	10*	10*	10.0	00.0	17.4	03			
6	5	10*	10	10*	10.0	00.0	14.5	03			
7	6	09	050	10	09.3	02.1	06.1	01			
8	6	10	10*	10*	10.0	00.0	00.2	.	.		
9	6	10*	10	10	10.0	00.0	00.3	00			
10	8	09	100	10	09.7	02.8	00.0	00			
11	7	02	09	09	06.7	03.5	00.0	00			
12	7	10	10	10	10.0	00.1	.	.			
13	7	09	020	00	03.7	07.6	.	.			
14	7	10*	000	00	03.3	07.6	.	.			
15	7	010	060	02	03.0	04.4	.	.			
16	7	08	080	06	07.3	05.9	.	.			
17	7	030	010	06	03.3	08.0	.	.			
18	7	050	10	10*	08.3	00.4	.	.			
19	7	09	040	01	04.7	04.6	00.0	.	.		
20	8	10	080	07	08.3	05.6	00.0	.	.		
21	8	00*	000	00	00.0	09.9	.	.			
22	8	000	000	00	00.0	08.6	.	.			
23	8	10	050	06	08.0	01.5	.	.			
24	8	020	070	03	02.3	09.7	.	.			
25	7	09	060	08	07.7	03.9	.	.			
26	7	10*	030	10	07.7	06.0	04.0	.			
27	6	050	100	05	06.7	06.9	.	.			
28	6	11*	100*	00	03.7	05.7	00.0	.			
29	7	10*	09	08	08.0	03.2	06.4	.			
30	7	10	10	10	10.0	00.0	.	.			
31	8	090	090	10	09.3	03.2	.	.			
32	8	070	070	06	06.8	11.7	00.5	.			
33	8	070	070	06	06.7	11.2	00.0	.			
34	8	000	010	00	00.2	11.7	.	.			
35	8	000	030	04	02.3	06.2	.	.			
36	7	10	10	10	10.0	00.0	.	.			
37	8	10	08	10*	08.3	04.0	03.3	.			
38	7	10*	10*	10	10.0	00.0	01.1	.			
39	8	10	10	10	10.0	00.1	01.2	.			
40	8	080	070	10	08.3	06.7	00.4	.			
41	7	060	09	03	06.0	09.4	00.0	.			
42	8	10	10	10	10.0	01.2	00.0	.			
43	8	070	10	04	07.0	02.0	.	.			
44	8	030	080	03	04.7	10.0	.	.			
45	8	000	010	00	00.3	12.4	.	.			
46	7	070	10	10*	05.0	02.6	.	.			
47	7	10*	050	06	07.0	02.2	00.0	.			
48	8	010	070	00	02.7	10.6	00.0	.			
49	6	080	090	09	08.7	02.4	.	.			
50	6	100	10	08	09.3	00.0	08.5	.			
51	7	070	10	10*	05.0	02.6	.	.			
52	7	10*	050	06	07.0	02.2	00.0	.			
53	8	010	070	00	02.7	10.6	00.0	.			
54	6	080	090	09	08.7	02.4	.	.			
55	6	100	10	08	09.3	00.0	08.5	.			
56	8	100	080	04	07.3	04.4	14.7	.			
57	7	030	10	10*	07.7	06.1	00.4	.			
58	6	10	10*	10*	10.0	00.0	02.8	.			
59	6	10*	090	08	09.3	00.9	18.9	.			
60	8	080	10	10	09.3	01.2	04.1	.			
MES.	MES.	06.1	07.5	06.1	06.5	161.6	55.5				

1	7	07	050	10	09.7	03.7	.	.			
2	7	10	10	07	06.0	00.4	00.1	.			
3	8	01*	050	01	02.0	08.1	00.0	.			
4	8	000	010	00	00.3	11.1	.	.			
5	7	000	060	06	04.0	10.2	.	.			
6	8	09	040	00	04.3	07.9	.	.			
7	8	030	10	09	07.3	01.3	.	.			
8	8	010	040	00	01.7	11.2	00.0	.			
9	8	000	010	00	00.2	11.7	.	.			
10	8	000	030	04	02.3	06.2	.	.			
11	7	10	10	10	10.0	00.0	.	.			
12	8	10	08	10*	08.3	04.0	03.3	.			
13	7	10*	10*	10	10.0	00.0	01.1	.			
14	8	10	10	10	10.0	00.1	01.2	.			
15	8	080	070	10	08.3	06.7	00.4	.			
16	7	060	09	03	06.0	09.4	00.0	.			
17	8	10	10	10	10.0	01.2	00.0	.			
18	8	070	10	04	07.0	02.0	.	.			
19	8	030	080	03	04.7	10.0	.	.			
20	8	000	010	00	00.3	12.4	.	.			
21	7	070	10	10*	05.0	02.6	.	.			
22	7	10*	050	06	07.0	02.2	00.0	.			
23	8	010	070	00	02.7	10.6	00.0	.			
24	6	080	090	09	08.7	02.4	.	.			
25	6	100	10	08	09.3	00.0	08.5	.			
26	8	100	080	04	07.3	04.4	14.7	.			
27	7	030	10	10*	07.7	06.1	00.4	.			
28	6	10	10*	10*	10.0	00.0	02.8	.			
29	6	10*	090	08	09.3	00.9	18.9	.			
30	8	080	10	10	09.3	01.2	04.1	.			
MES.	MES.	06.1	07.5	06.1	06.5	161.6	55.5				

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 $\varphi = 46^{\circ}04'$ N $\lambda = 14^{\circ}31'$ E Gr. $\Delta G = + 58$ min.

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Dan	Vzdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenih parov e mm			Relativna vlažnost v %				Pravac i jačina vetrova D, f (0—12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	718.3	719.0	722.3	11.4	18.8	13.7	14.4	19.1	10.9	08.9	05.3	06.8	05.6	92	42	48	61	SW	1	N	2	NW	1
2	724.7	726.8	727.9	10.8	13.4	10.6	11.4	16.4	07.8	02.6	07.3	08.2	09.1	75	71	95	80	SW	2	N	1	S	1
3	729.2	728.5	728.8	09.8	13.6	11.6	11.7	16.8	09.5	06.5	08.8	07.5	06.7	96	64	66	75	NE	1	W	2	SW	3
4	726.5	724.8	725.2	09.0	11.0	09.1	09.6	11.8	09.0	05.7	08.3	09.1	07.9	96	92	91	93	E	1	W	2	SW	1
5	724.6	725.3	726.5	08.6	12.2	10.8	10.6	13.4	08.0	07.0	08.0	07.5	07.9	95	70	81	82	E	1	W	2	SW	2
6	726.8	728.3	731.6	11.6	16.7	09.8	12.0	17.0	09.0	05.6	08.1	07.7	08.8	79	54	96	76	SW	1	SW	4	NE	1
7	733.6	734.6	735.8	09.4	10.1	10.5	10.1	12.0	09.0	08.1	08.6	08.6	09.0	98	93	94	95	NW	1	NW	1	SW	1
8	737.2	737.0	736.0	09.3	12.2	11.2	11.0	14.0	08.7	03.6	08.4	07.0	07.1	95	66	71	77	NE	1	NE	2	E	1
9	736.0	734.1	734.5	09.4	16.8	10.4	11.8	17.7	08.1	03.4	07.7	04.8	06.0	87	34	63	61	NE	1	SE	2	E	1
10	734.9	733.1	733.1	07.2	16.8	12.7	12.4	18.0	04.0	-00.2	06.3	07.3	06.4	83	51	58	64	NE	1	SW	4	W	1
11	733.8	734.3	735.3	09.0	16.0	13.0	12.8	18.0	07.9	02.5	07.6	06.8	07.0	88	50	62	67	N	1	SW	3	NW	2
12	736.2	735.8	738.8	12.4	21.7	15.0	16.0	22.0	10.6	08.2	08.0	05.7	08.8	74	29	69	57	NNW	2	NNW	3	SE	1
13	740.7	738.8	739.5	11.2	23.1	16.8	17.0	23.7	07.7	02.1	08.4	06.8	07.9	84	32	55	57	SW	1	W	2	SW	1
14	738.0	735.8	738.6	11.6	22.0	10.6	13.7	22.5	07.9	02.5	08.5	08.6	09.3	83	43	96	74	NE	1	SW	5	NW	2
15	737.9	734.5	734.2	09.1	18.2	11.7	12.7	19.0	07.6	03.9	07.8	06.1	07.7	90	39	75	68	ENE	1	NE	2	E	1
16	733.9	732.0	733.4	09.7	18.7	12.7	13.5	19.4	08.0	02.6	08.1	06.5	08.1	89	40	74	68	E	1	SW	2	SW	1
17	734.4	735.2	739.2	12.4	21.3	14.0	15.4	21.9	08.9	04.6	08.6	07.3	07.5	80	38	62	60	NNE	1	E	2	E	1
18	740.8	739.3	740.4	10.0	22.1	17.4	16.7	22.7	06.7	00.9	07.7	07.5	07.6	84	38	51	58	ENE	1	NE	2	NE	2
19	740.5	738.5	738.8	11.6	22.9	16.4	16.8	23.1	08.7	02.5	08.4	07.4	07.8	82	35	56	58	NE	1	ENE	3	NE	1
20	738.9	736.1	737.0	12.2	26.1	17.0	18.1	26.1	08.0	02.0	08.2	07.4	11.7	77	29	80	62	NE	1	SW	2	E	1
21	738.2	737.0	737.0	13.7	24.4	18.0	18.5	25.3	12.6	07.7	10.4	08.5	10.3	88	37	66	64	SE	1	NE	1	SE	1
22	734.9	727.9	729.0	13.2	24.2	14.2	16.5	24.5	12.5	07.6	10.4	09.7	09.2	91	43	76	70	SW	1	SW	4	ENE	2
23	730.2	728.8	728.8	10.3	14.2	11.0	11.6	17.9	07.5	00.9	08.3	07.3	07.4	88	60	76	75	NE	1	W	2	SW	1
24	729.1	729.3	730.4	07.9	09.4	07.0	07.8	11.2	06.2	00.3	07.9	08.4	07.2	87	95	96	93	N	1	NW	1	NW	2
25	732.1	734.9	736.8	07.1	14.6	10.9	10.9	16.9	06.2	05.5	07.1	07.8	08.1	93	62	83	79	W	2	SE	1	-	0
MES.	WRFED	733.7	732.7	733.6	10.7	18.5	13.4	14.0	19.7	08.7	04.5	08.4	07.8	08.3	87	51	72	70	1.2	2.2	1.4		

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1	733.9	736.8	738.5	15.0	15.6	14.4	14.9	18.2	14.4	13.3	12.4	11.5	11.4	97	86	93	92	NW	1	SW	2	S	1
2	740.8	740.7	742.4	14.4	22.2	17.0	17.7	23.6	12.5	08.4	10.9	07.5	09.6	89	37	68	64	-	0	SE	2	ESE	1
3	743.4	740.8	740.2	12.2	23.9	17.8	17.9	25.1	08.4	03.7	08.9	07.9	09.4	84	36	61	60	-	0	ESE	1	ESE	1
4	740.2	738.4	738.3	15.1	27.8	19.8	20.6	28.6	10.6	05.9	09.8	09.7	08.2	76	35	47	53	SE	1	W	3	SE	2
5	738.7	736.2	735.2	15.4	25.2	20.6	20.5	26.6	12.4	07.6	09.9	13.6	10.3	76	57	57	63	SW	1	NE	1	SF	1
6	734.1	734.1	734.7	16.0	18.8	15.4	16.4	23.0	13.4	07.4	10.5	12.3	12.1	77	75	92	81	S	1	SW	2	S	1
7	735.9	735.2	739.1	11.3	24.0	15.8	16.7	24.3	07.2	01.6	08.1	08.0	07.6	81	36	57	58	ENE	1	SE	1	SW	1
8	740.0	738.9	736.7	10.3	15.3	10.4	11.6	16.0	09.0	07.5	08.4	07.7	08.5	89	59	90	79	NE	1	SW	3	NW	1
9	733.2	731.3	730.9	08.2	17.3	12.7	12.7	18.3	06.9	02.2	07.9	08.5	10.8	97	58	98	84	SE	1	W	3	E	1
10	732.1	730.4	729.3	06.4	07.8	08.0	07.6	13.2	06.3	05.2	06.6	07.1	07.8	92	90	97	93	N	1	N	3	S	2
11	730.4	731.8	734.0	09.3	19.7	12.5	13.5	20.6	08.0	04.8	07.9	05.1	07.7	90	29	71	63	S	1	NW	3	SW	1
12	733.3	731.5	731.3	07.3	18.2	12.9	12.8	19.3	04.8	-00.4	06.6	04.6	04.4	86	29	39	51	N	1	N	2	NNW	2
13	728.5	728.8	729.2	07.8	16.3	13.5	12.8	18.7	05.7	04.6	06.4	06.4	07.5	81	46	65	64	NF	1	SW	4	SW	1
14	730.7	730.7	733.1	11.0	22.4	16.8	16.8	22.6	10.6	07.7	09.3	09.2	08.4	94	45	59	66	NE	1	S	4	SW	1
15	735.1	733.2	734.7	12.0	22.1	14.3	15.7	23.2	09.6	05.0	09.5	10.0	10.2	90	50	84	75	NE	1	SW	3	SW	2
16	734.3	732.8	733.9	12.0	23.7	16.2	17.0	24.6	09.9	04.5	09.6	08.6	10.7	91	39	77	69	NW	1	Nh	2	E	3
17	733.3	731.6	732.4	14.8	21.7	18.0	18.1	23.3	12.6	09.2	10.9	09.7	12.1	86	50	78	71	S	1	SW	2	SW	1
18	733.4	733.3	735.0	15.6	18.2	15.8	16.4	22.1	11.2	08.4	11.3	10.8	12.5	85	69	93	82	E	1	SE	2	S	1
19	737.2	737.6	738.3	14.6																			

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 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vidljivost 0.9	Oblačnost N (0-10)					Insolacija broj sati	Podzemne R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8	10	09.0	07	08.7	00.0	10.4	.	.	= n 4.2, tr-o-n 0.4	
2	8	04.0	02.0	01	03.7	10.9	10.9	02.0	.	= n 8.2, tr-o-5.4, 0.4, tr-o-M.4, -18.4	
3	7	10.0	09.0	10	09.7	05.0	02.3	.	.	= n 10.2, tr-o-5.4, 0.4, 13.0, 14.5, 0.4, tr-o-15.4	
4	7	10.0	10.0	10.0	10.0	00.0	01.3	.	.	= 2.5.4, n.4, = 3.4, n.4, tr-o-18.4, -10.2	
5	7	10	10.0	10.0	10.0	00.0	13.4	.	.	= tr-o-18.4, 17.4, -n.4, = n.4	
6	8	10	06.0	10.	08.7	01.0	00.4	.	.	= 2.16.0, 17.4, 19.4, -n.4, = 3.4, 6.4, 8.4, 12.4, 15.4, 19.4, 17.4, 18.4, 15.4	
7	6	10.0	10.0	09	09.7	00.0	2.6	.	.	= n 10.2, 20.0, n.4, tr-o-n.4, 13.4	
8	7	10	10	10	10.0	01.0	13.4	14.4	.	= n 4.2, 12.4, n.4	
9	8	07.0	06.0	00	04.3	10.4	.	.	.	= n 8.0	
10	7	01.0	08.0	04	04.3	09.5	.	.	.	= 2.2.0, 4.4, = 4.4, 8.4, 00.4, 12.4, 14.4, 0.4	
11	8	10	05	04	04.3	02.4	00.0	.	.	= n 12.2, tr-o-8.4, 12.4, = 3.4, n.4, 00.4	
12	8	08.0	07.0	08	07.7	10.4	00.0	.	.	= 2.12.4	
13	8	01.0	01.0	01	01.0	12.5	.	.	.	= n 12.4, 12.4, 12.4	
14	8	00.0	08.0	10.	06.0	10.2	.	.	.	= n 8.0, 12.4, 20.0, n	
15	8	00	06.0	10.0	08.3	06.4	00.0	.	.	= n 8.0, 12.4, 17.4, 20.0	
16	8	05.0	05.0	10	03.3	10.5	00.0	.	.	= 2.12.4, 12.4, 0.4, 20.0	
17	8	04.0	03.0	04	03.7	10.9	.	.	.	= 2.19.0, -n.4, = n.4, 00.4, 12.4, 14.4, 16.4, 18.4	
18	7	00.0	03.0	09	05.7	12.6	00.0	.	.	= 2.10.4, -n.4, 0.4, 12.4, 14.4, 16.4, 18.4	
19	7	01.0	03.0	00	01.3	12.9	.	.	.	= 2.12.4, = n.4, 00.4, 12.4, 14.4, 16.4	
20	7	00.0	08.0	04	05.7	11.8	.	.	.	= 2.10.4, 00.4, 12.4, 14.4, 16.4, 18.4, 12.4, 10.4, 12.4, 14.4, 16.4	
21	7	05	03.0	00	04.0	04.5	01.4	.	.	= n 10.0, 8.4, tr-o-3.4, 00.4, 2.4, 0.4	
22	7	05	03.0	04	05.3	05.5	00.4	.	.	= n 12.2, = n.4, 7.4, 8.4, 10.4, 12.4, 14.4, 16.4, 18.4	
23	8	03.0	06.0	10	04.3	05.4	00.2	.	.	= 2.10.4, = n.4, 00.4, 12.4, 14.4, 16.4	
24	6	10	10.0	10	10.0	00.0	00.0	00.1	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
25	8	10.0	03.0	07	04.3	07.1	21.0	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
26	8	10	03.0	00	04.2	10.9	01.0	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
27	7	00.0	03.0	07	03.7	12.2	.	.	.	= 2.10.4, -n.4, 0.4, 10.4, 12.4	
28	8	05.0	09	10	08.0	04.2	.	.	.	= n 12.2, = n.4, 0.4, 10.4, 12.4	
29	7	10.0	04.0	00	04.7	07.9	04.6	.	.	= 2.10.4, = n.4, 0.4, 10.4, 12.4, 14.4, 16.4	
30	7	10	09.0	05	09.3	08.9	00.0	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
31	7	06.0	10	10.0	08.7	03.7	.	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
MES. VRED.		01.5	06.7	06.5	06.6	207.4	169.0				

1	6	10	10	07	08.0	00.0	10.7	10.7	.	= 2.12.5, 5.2, = 5.4, 15.4	
2	8	08.0	02.0	01	03.7	10.9	16.9	.	.	= n.4, 2.4, 12.4	
3	7	00.0	01.0	00	00.3	13.0	.	.	.	= n.4, 0.4, 12.4	
4	8	00.0	02.0	01	01.0	13.7	.	.	.	= 2.10.4, = n.4, 0.4, 12.4	
5	7	04.0	02.0	05	03.7	08.6	.	.	.	= 2.10.4, = n.4, 0.4, 12.4	
6	7	05.0	10	10.	08.7	01.2	00.0	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4, 17.4, 19.4, 20.4, 22.4, 24.4, 26.4	
7	8	07.0	04.0	07	04.7	07.6	25.6	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
8	8	09	04.0	04	07.3	01.0	01.3	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
9	7	10	03	04	10.0	08.7	01.8	00.2	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
10	6	10	10.0	10.	10.0	00.0	32.9	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
11	8	09.0	04.0	01	04.7	11.8	4.1	.	.	= n.4, = n.4, 0.4, 10.4	
12	9	09.0	08.0	01	06.0	05.0	.	.	.	= 2.10.4, = 2.10.4	
13	8	09.0	10	C5	08.0	05.1	.	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
14	8	10.0	04.0	01	05.0	07.0	00.0	CC.0	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
15	7	07.0	06.0	07	04.7	04.4	00.0	.	.	= 2.10.4, = n.4, 0.4, 10.4, 12.4, 14.4, 16.4	
16	7	00.0	04.0	07	03.7	10.8	00.0	.	.	= 2.10.4, = n.4, 0.4, 10.4, 12.4, 14.4, 16.4	
17	7	02.0	06.0	03	03.7	07.9	11.1	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
18	7	02.0	10.0	10.	07.3	02.0	.	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
19	8	10.0	07.0	01	06.0	02.0	05.1	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
20	7	01.0	06.0	09	04.2	04.9	00.0	.	.	= 2.10.4, = n.4, 0.4, 10.4, 12.4, 14.4, 16.4	
21	8	10.	05.0	03	06.0	07.0	06.2	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
22	7	10	05.0	02	05.7	09.1	02.5	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
23	7	04.0	02.0	10	05.3	09.3	.	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
24	7	09.0	10	C9	05.3	00.2	05.0	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
25	8	06.0	04.0	05	05.0	08.7	20.4	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
26	8	09.0	05.0	04	06.0	07.7	.	.	.	= 2.10.4, = n.4, 0.4, 10.4, 12.4, 14.4, 16.4	
27	7	09.0	09.0	07	08.3	04.5	00.0	.	.	= 2.10.4, = n.4, 0.4, 10.4, 12.4, 14.4, 16.4	
28	7	10	05	10.	05.7	01.4	01.5	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
29	6	10	10.0	10.	10.0	00.0	11.7	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
30	8	02.0	04.0	08	04.7	11.8	49.0	.	.	= 2.10.4, 0.4, 10.4, 12.4, 14.4, 16.4	
MES. VRED.		06.8	06.2	05.7	06.2	189.1	245.2				

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 $\varphi = 46^{\circ}04'$, N $\lambda = 14^{\circ}31'$, E Gr. $\Delta G = + 58$ min.

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Dan	Vzdušni pritisak P mm			Temperatura vazduha T °C°							Napon vodenih pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	736.1	735.0	735.7	16.5	26.7	21.4	21.5	27.4	12.5	08.1	11.4	11.5	10.9	81	44	57	61	ESE	1	SW	4	SW	2
2	738.9	738.6	739.3	16.9	24.5	20.0	20.4	26.1	14.0	09.2	11.1	12.0	12.6	77	52	72	67	E	1	E	2	NE	1
3	738.9	733.7	733.4	17.4	26.2	17.6	19.7	27.8	12.9	07.7	10.3	11.9	13.7	69	47	91	69	SF	1	S	2	SW	1
4	735.5	735.2	736.2	14.9	22.5	18.4	18.6	24.0	13.3	09.3	11.6	11.3	11.4	91	55	72	73	NF	1	SE	3	E	1
5	738.0	736.9	736.2	16.8	24.6	20.8	20.8	25.6	15.4	11.9	10.9	11.3	13.2	76	48	72	65	NE	1	SE	2	SE	2
6	736.0	734.0	733.3	16.6	27.2	20.0	21.0	28.0	13.5	09.4	12.4	12.3	14.7	88	46	84	73	E	2	SW	3	N	1
7	733.8	736.4	737.5	17.2	30.1	15.8	17.2	21.0	15.8	15.0	13.5	10.6	09.9	91	60	73	75	NE	1	SE	4	E	1
8	739.5	737.2	738.3	11.4	22.6	17.7	17.4	23.3	10.2	05.3	09.0	07.0	09.2	97	34	69	64	NE	1	SW	3	NE	1
9	740.0	737.7	736.3	13.6	24.4	19.0	19.0	24.6	09.9	04.6	06.8	10.5	07.3	75	46	45	55	N	1	SW	3	SW	3
10	736.7	736.8	737.8	15.0	25.0	20.2	20.1	26.0	12.5	07.0	11.1	11.3	10.5	97	46	59	65	NW	2	S	2	E	1
11	733.5	736.6	737.4	16.9	27.3	22.0	22.1	27.7	16.0	11.5	11.6	12.4	13.1	80	46	66	64	E	1	SW	3	SW	3
12	736.6	736.2	736.6	21.1	27.5	22.8	23.6	28.5	14.2	11.2	11.6	14.2	13.0	62	52	62	59	W	2	SW	3	SW	2
13	736.4	734.9	734.2	19.4	29.0	24.0	24.1	30.0	17.0	12.7	14.1	15.3	12.1	83	51	54	63	S	1	SW	3	SW	3
14	734.4	733.5	734.2	18.6	29.1	22.8	23.3	29.8	15.7	10.7	12.0	13.4	11.7	74	44	56	58	NE	1	SW	3	W	2
15	737.1	739.1	739.3	10.4	19.0	17.2	18.2	22.9	17.0	12.9	12.7	11.8	12.9	75	71	48	78	SE	1	NE	2	N	1
16	737.2	735.0	733.8	15.9	26.4	21.7	21.9	30.6	14.0	09.6	12.7	13.3	17.7	94	46	65	68	NE	1	SW	2	-	0
17	732.5	730.0	729.8	18.7	29.4	24.0	24.0	30.6	14.8	09.7	12.1	13.0	13.2	75	42	59	59	SW	1	SW	3	SW	1
18	729.3	730.1	732.9	18.0	18.9	14.5	16.5	24.1	14.5	13.6	13.9	13.3	11.7	90	81	95	89	N	2	NE	1	NE	1
19	733.7	734.2	735.1	12.8	15.2	14.5	14.3	15.9	12.6	12.2	10.7	11.2	09.7	97	86	78	87	NW	1	S	1	-	0
20	735.6	734.6	734.6	13.0	19.2	15.0	15.6	20.0	09.4	11.9	08.0	07.5	06.4	71	45	65	60	SF	2	NE	3	SE	2
21	733.8	732.3	735.2	12.0	19.9	15.4	15.7	22.3	10.6	06.2	09.4	10.2	11.3	89	59	86	78	S	1	NW	3	SW	1
22	737.2	735.8	736.4	11.9	22.8	15.8	16.6	23.6	11.2	07.7	09.4	07.2	09.6	90	35	71	65	SW	1	NE	2	S	1
23	735.0	735.0	735.9	13.6	25.8	20.0	19.9	27.0	10.4	06.7	09.0	09.0	12.8	77	36	73	62	NE	2	NW	1	SK	3
24	736.6	735.1	734.2	15.4	25.5	20.4	20.4	26.3	12.9	08.7	11.4	08.9	15.0	87	36	72	65	NE	1	SW	4	K	1
25	732.8	737.1	739.9	17.9	12.6	13.4	14.3	20.6	12.4	05.8	14.6	10.2	10.3	95	92	89	92	NE	1	E	3	NE	1
26	740.1	738.7	738.6	12.1	22.2	17.7	17.4	23.1	09.8	07.5	09.7	08.2	10.1	91	41	66	66	NF	1	E	2	SF	1
27	739.1	737.1	737.4	11.2	25.5	18.9	18.6	26.0	10.0	07.1	09.9	11.1	12.5	99	45	76	73	-	0	FNE	1	-	0
28	739.2	738.9	740.0	13.3	27.0	20.4	20.4	28.1	12.0	07.5	11.1	12.0	15.9	97	45	87	76	E	1	E	2	-	0
29	741.7	740.0	739.5	15.4	28.6	22.0	22.0	30.0	14.3	10.4	12.9	14.0	15.2	90	48	76	74	NE	1	SF	2	NE	1
30	739.2	736.3	735.4	17.6	30.1	24.0	23.9	31.7	14.4	10.5	12.0	15.4	14.4	85	42	64	64	NF	1	NE	1	SW	1
31	736.1	735.0	735.0	19.2	30.2	22.4	23.7	30.7	16.1	11.7	13.5	15.8	14.0	81	49	68	66	E	1	NE	1	-	0
MES.	VRID.			15.8	24.4	19.4	19.7	25.9	13.2	09.4	11.4	11.4	12.0	84	51	71	65	1.2	2.4	1.7			

1974 AVGUST

LJUBLJANA BEŽIGRAD

1	736.2	734.6	734.9	18.5	20.0	24.4	24.2	30.8	17.4	11.8	15.5	15.9	19.4	97	50	84	77	ESE	1	NE	1	NE	1
2	735.0	734.8	735.2	20.2	21.6	24.2	25.1	31.7	18.9	14.4	16.8	16.4	20.0	95	47	88	77	NF	1	SE	2	SE	1
3	735.7	735.6	737.1	19.8	30.0	24.2	24.6	31.2	18.3	13.9	14.0	15.9	18.4	81	50	81	71	SF	1	NE	1	NE	1
4	737.5	735.4	735.6	20.1	32.4	25.0	25.6	32.1	18.6	14.1	15.8	13.8	13.4	89	38	63	61	NE	1	SE	3	SW	2
5	737.0	736.3	736.4	19.6	29.6	23.8	24.7	29.8	17.0	12.3	14.0	14.0	15.4	82	45	70	66	NE	1	SL	2	E	1
6	739.8	741.3	741.2	18.6	20.4	16.6	18.1	23.8	16.6	15.3	15.8	11.2	12.0	98	62	85	82	NE	2	NE	2	NE	1
7	739.5	736.6	735.4	17.3	24.0	19.4	18.8	24.9	12.1	07.4	10.5	10.4	10.9	98	47	65	70	NF	1	SE	1	SE	1
8	733.5	729.9	729.7	13.4	27.3	21.4	20.9	28.5	12.4	08.0	11.0	12.9	13.3	96	47	69	71	N	1	SW	2	SW	1
9	732.0	731.4	733.9	16.0	24.8	17.4	18.7	25.2	14.2	10.9	12.1	11.6	11.6	95	49	78	74	NW	1	SW	1	NW	1
10	735.4	732.7	732.0	15.2	23.7	17.5	18.5	24.0	12.2	09.1	11.0	11.9	14.2	85	54	94	78	SE	1	NE	2	NE	1
11	732.3	732.7	733.9	11.8	16.9	13.9	14.1	19.8	10.7	09.2	09.8	09.0	10.0	94	62	84	80	W	3	S	1	-	C
12	735.5	735.4	737.2	11.5	24.4	17.0	17.5	25.3	10.3	07.2	09.6	06.7	10.3	93	29	71	64	SW	1	SW	2	Nh	1
13	739.6	738.4	736.4	12.7	26.2	20.2	19.8	26.6	09.7	05.5	09.0	11.3	13.0	82	44	73	66	NE	1	SE	2	SW	1
14																							

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Instalacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	02 0	04 0	02	02.7	13.6	.	.	.	$\Delta^{\circ}n - 9^{\circ}2$, $F_{sw} 13-15$
2	8	09	04 0	02	05.0	09.2	.	.	.	$\Delta^{\circ}n - 9^{\circ}2$
3	8	00 0	04 0	09	04.2	11.2	.	.	.	$\Delta^{\circ}n - 9^{\circ}2 = n - 8, 00.8 - 9^{\circ}2, T^{\circ} - 10^{\circ}5 - 10^{\circ}2, F^{\circ} - 10^{\circ}10 - 20^{\circ}4$
4	8	03 0	04 0	02	03.0	12.2	05.0	.	.	$\Delta^{\circ}n - 10^{\circ}2, 10^{\circ}2 - 10^{\circ}4 - 20^{\circ}2, \bullet - 10^{\circ}2, 00^{\circ}4, 8^{\circ}2 - 0$
5	7	07 0	01 0	00	02.7	12.1	.	.	.	$\Delta^{\circ}n - 9^{\circ}2 - 0$
6	7	04 0	04 0	10 ●	06.0	07.2	.	.	.	$\Delta^{\circ}n - 9^{\circ}2 = n - 4^{\circ}2, 0^{\circ}2 = 1^{\circ}2 - 7^{\circ}, \Delta^{\circ}n - 9^{\circ}4 - 5^{\circ}4, 00^{\circ}9 - 10^{\circ}2, F^{\circ} - 10^{\circ}5 - 10^{\circ}2, \bullet - 10^{\circ}10 - 20^{\circ}2, \Delta^{\circ}n - 10^{\circ}2, 10^{\circ}2 - 10^{\circ}4, F^{\circ} - 10^{\circ}2, 00^{\circ}9 - 10^{\circ}2, \Delta^{\circ}n - 9^{\circ}2 - 0$
7	8	09	04 0	01	04.7	10.0	03.2	.	.	$\Delta^{\circ}n - 10 = n - 9^{\circ}2, 0^{\circ}2 = 1^{\circ}2 - 7^{\circ}, 00^{\circ}9 - 10^{\circ}2 - 20^{\circ}4$
8	7	08 0	04 0	01	04.2	11.1	00.0	.	.	$\Delta^{\circ}n - 9^{\circ}2, 0^{\circ}2 = 1^{\circ}2 - 7^{\circ}, 00^{\circ}9 - 10^{\circ}2 - 20^{\circ}4$
9	7	04 0	08 0	05	05.7	07.0	.	.	.	$\Delta^{\circ}n - 9^{\circ}2, 0^{\circ}2 = 1^{\circ}2 - 7^{\circ}, 00^{\circ}9 - 10^{\circ}2 - 20^{\circ}4$
10	7	06 0	05 0	06	05.7	08.2	00.1	.	.	$\Delta^{\circ}n - 9^{\circ}2, 00^{\circ}9 - 10^{\circ}2 - 20^{\circ}4$
11	7	10	03 0	07	06.7	08.4	00.0	.	.	$\Delta^{\circ}n - 8^{\circ}4, \bullet - 4^{\circ}2 - 5^{\circ}5, 00^{\circ}8 - 0$
12	7	01 0	04 0	01	02.0	12.5	.	.	.	$00^{\circ}n - 4^{\circ}2, 0^{\circ}2 = 1^{\circ}2 - 7^{\circ}$
13	7	00 0	02 0	01	01.0	12.0	.	.	.	$\Delta^{\circ}n - 8^{\circ}2, 00^{\circ}8 - 0$
14	7	01 0	03 0	01	01.2	13.8	.	.	.	$\Delta^{\circ}n - 8, 0^{\circ}2 - 0$
15	8	05 0	01 0	10	08.0	01.3	.	.	.	$00^{\circ}n - 9^{\circ}2, \bullet - 9^{\circ}2 - 10^{\circ}5 - 18^{\circ}4, \bullet - 4^{\circ}2 - 0^{\circ}4 - 12^{\circ}4$
16	7	10	03 0	00	04.2	08.5	00.8	.	.	$\Delta^{\circ}n - 9^{\circ}4, 00^{\circ}9 - 10^{\circ}2 - 18$
17	8	03 0	08 0	10	07.0	11.6	.	.	.	$\Delta^{\circ}n - 7^{\circ}2, 1^{\circ}2 - 10^{\circ}5, \bullet - 14^{\circ}2 - 15^{\circ}4$
18	8	07 0	09 0	10	08.7	04.3	04.8	.	.	$\Delta^{\circ}n - 4^{\circ}2 - 5^{\circ}8 - 10^{\circ}4, \bullet - 4^{\circ}2 - 0^{\circ}4 - 10^{\circ}5 - 15^{\circ}4, 10^{\circ}4 - 19, T^{\circ} - 18^{\circ}4 - 12^{\circ}2$
19	6	10	10	10	10.0	00.0	25.0	.	.	$\Delta^{\circ}n - 11, \bullet - 11^{\circ}2 - 11^{\circ}4$
20	8	03 0	09 0	10	07.3	06.3	01.1	.	.	$\Delta^{\circ}2n - 10^{\circ}2, \bullet - 2^{\circ}3 - 4^{\circ}4 - 17^{\circ}4$
21	8	08 0	10 ●	08	01.7	03.5	00.2	.	.	$\Delta^{\circ}n - 9, \bullet - 6^{\circ}2, 13^{\circ}4 - 16^{\circ}2, \bullet - 10^{\circ}2 - 13^{\circ}4$
22	8	09 0	07 0	01	05.7	08.4	00.1	.	.	.
23	7	06 0	02 0	05	04.3	11.3	.	.	.	$\Delta^{\circ}n - 9^{\circ}2$
24	8	04 0	06 0	10	06.7	08.1	.	.	.	$\Delta^{\circ}n - 8 = 0^{\circ}2$
25	4	10 ●	10 ●	10	10.0	00.0	00.2	.	.	$\Delta^{\circ}n - 15^{\circ}2, \bullet - 2^{\circ}3 - 15^{\circ}2, \bullet - 2^{\circ}12^{\circ}4 - 15^{\circ}4, \bullet - 2^{\circ}12^{\circ}4 - 15^{\circ}4$
26	8	C3 0	01 0	01	01.7	13.1	24.6	.	.	$\bullet - 6, 8^{\circ}3^{\circ}4$
27	8	10 0	01 0	00	02.7	11.5	.	.	.	$\Delta^{\circ}n - 9^{\circ}2, 0^{\circ}2 = 1^{\circ}2 - 4^{\circ}4, 7^{\circ}2 - 9^{\circ}2, \bullet - 2^{\circ}4^{\circ}4 - 6^{\circ}4, \bullet - 2^{\circ}6^{\circ}4 - 10^{\circ}2$
28	7	10 0	02 0	00	04.0	11.5	.	.	.	$\Delta^{\circ}2n - 9^{\circ}2, \bullet - 2^{\circ}4^{\circ}2, 7^{\circ}2 - 9^{\circ}2, \bullet - 2^{\circ}4^{\circ}4 - 6^{\circ}4, 7^{\circ}2 - 9^{\circ}2, \bullet - 2^{\circ}6^{\circ}4 - 10^{\circ}2$
29	7	00 0	01 0	00	00.1	14.1	.	.	.	$\Delta^{\circ}2n - 10 = n - 1^{\circ}4, 7^{\circ}2 - 9^{\circ}2, \bullet - 2^{\circ}4^{\circ}4 - 6^{\circ}4, 7^{\circ}2 - 9^{\circ}2, \bullet - 2^{\circ}6^{\circ}4 - 10^{\circ}2$
30	7	00 0	01 0	03	01.1	12.5	.	.	.	$\Delta^{\circ}2n - 9^{\circ}2, \bullet - 2^{\circ}4^{\circ}4 - 6^{\circ}4, 7^{\circ}2 - 9^{\circ}2, \bullet - 2^{\circ}6^{\circ}4 - 10^{\circ}2$
31	7	02 0	02 0	00	01.2	11.2	.	.	.	$\Delta^{\circ}n - 9 = n - 9^{\circ}2, 00^{\circ}9 - 10^{\circ}2 - 20^{\circ}4$
MES.										
MED.		05.3	04.4	04.4	04.0	227.4	86.1			

1. JUHIS JÄRNE, BEŽIGRAD

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1	7	00≡0	C10	06	02.3	11.2	.	.	$\Delta^2 n - 9^2 4_2 = n - 4^2 4_2 \cdot 2^2 4_2 - 9^2 4_2 \equiv -4^2 4_2 - 7^2 4_2 = -4^2 4_2 - 6^2 4_2, \text{ or } 9^2 4_2 - n$
2	7	030	020	00	C1.7	11.3	.	.	$\Delta^2 n - 8^2 4_2 = n - 8^2 4_2 \cdot 2^2 4_2 - 8^2 4_2 \equiv -8^2 4_2 - 5^2 4_2, \text{ or } 8^2 4_2 - n$
3	7	050	030	C1	03.0	10.1	.	.	$\Delta^2 n - 9 = n - 9^2 4_2, 20^2 4_2 - n; 00^2 4_2 - 20^2 4_2$
4	7	010	010	C1	01.0	11.6	.	.	$\Delta^2 n - 9^2 4_2 = n - 9^2 4_2, 00^2 4_2 - n$
5	7	050	020	01	02.7	11.5	.	.	$\Delta^2 n - 7^2 4_2 = 4^2 4_2 \cdot 8^2 4_2, 00^2 4_2 - n$
6	7	10●	090	00	04.3	C5.2	C1.2	.	$= n - 10^2 4_2, 0^2 - 4^2 4_2 \cdot 9^2 4_2$
7	7	10≡	070	CC	04.3	C1.5	C3.6	.	$\equiv n^2 4_2 - 7^2 4_2, \equiv -4^2 4_2 \cdot 6^2 4_2 - 7^2 4_2 = 7^2 4_2 - 9^2 4_2, 00^2 4_2 - n, 15^2 4_2, 20^2 4_2 - n$
8	7	020	080	05	05.0	C6.2	.	.	$\Delta^2 n - 9^2 4_2 = 4^2 4_2 - 9^2 4_2, \equiv -4^2 5^2 4_2, 6^2 4_2, 00^2 4_2 - 17^2 4_2, + 20^2 4_2 - n$
9	8	090	050	01	05.0	07.0	C5.2	.	$\Delta^2 n - 9^2 4_2 = 5^2 4_2 - 8^2 4_2, 15^2 4_2, 10^2 4_2$
10	8	040	050	CG	07.3	05.6	00.0	.	$T^2 14^2 4_2 - 15, \sqrt{14^2 4_2 - 2^2 15}, \sqrt{14^2 4_2 - 15}, F^2 15^2 4_2 - 15, \Delta 15^2 4_2 - 15^2 4_2$
11	8	10●R	C30	C1	04.7	04.8	28.7	.	$= n - 4^2 4_2, T^2 n, 8^2 4_2 - 9, \Delta^2 n - 2^2 4_2 - n, 9, 18 - 19^2 4_2, \sqrt{3^2 4_2 - 8^2 4_2}, \bullet^2 n - 9 - 12^2 4_2$
12	8	10	C30	0C	04.3	10.3	11.9	.	$\equiv n^2 4_2, 4^2 4_2 - 10^2 4_2$
13	8	090	050	01	05.0	12.1	.	.	$\equiv n - 4^2 4_2, \Delta^2 n - 10^2 4_2$
14	8	000	020	C1	01.0	11.7	.	.	$\Delta^2 n - 9^2 4_2 = n - 9^2 4_2, \equiv -4^2 4_2 - 6^2 4_2$
15	7	030≡	030	00	02.0	11.5	.	.	$\Delta^2 n - 9 = n - 10^2 4_2, \equiv -5^2 4_2 - 7, 00^2 4_2 - n$
16	7	00≡0	000	00	00.0	11.2	.	.	$\Delta^2 n - 9, \equiv -4^2 4_2 - n, 8^2 4_2, \equiv -4^2 4_2 - 6^2 4_2, = 6^2 4_2 - 9^2 4_2, 00^2 4_2 - n$
17	7	00≡0	010	00	00.3	11.3	.	.	$\Delta^2 n - 9 = n - 4^2 4_2, 8^2 4_2 - 10^2 4_2, \equiv -4^2 4_2 - 8^2 4_2, \equiv -2^2 4_2 - 6^2 4_2, = 6^2 4_2 - 10^2 4_2, 00^2 4_2 - n$
18	7	000	000	CC	00.0	11.6	.	.	$\Delta^2 n - 9^2 4_2, 8^2 4_2, \equiv -5^2 4_2 - 8^2 4_2, \equiv -4^2 4_2 - 8^2 4_2, = 6^2 4_2 - 8^2 4_2, 15^2 4_2 - n$
19	7	10≡	020	00	04.0	09.9	.	.	$\Delta^2 n - 9^2 4_2, 20^2 4_2 - n, \equiv -4^2 4_2 - 6^2 4_2, 8^2 4_2, \equiv -4^2 4_2 - 8^2 4_2, 8^2 4_2 - 9^2 4_2, 00^2 4_2 - 14^2 4_2$
20	7	00≡0	040	CC	01.3	11.0	.	.	$\Delta^2 n - 9, 20^2 4_2 - n, = n - 9^2 4_2, 19^2 4_2 - n, \equiv -4^2 6 - 8^2 4_2, 00^2 4_2 - 19^2 4_2$
21	7	090	-070	10R	08.7	09.1	.	.	$\Delta^2 n - 9^2 4_2 = n - 9^2 4_2, 6n - 4, 20^2 4_2 - 20^2 4_2, 00^2 4_2 - 7, T^2 20^2 4_2 - n$
22	7	C9	09	C9	C9.0	02.6	C0.1	.	$\equiv n - 10^2 4_2, T^2 n - 5^2 4_2, 3^2 4_2 - 4^2 4_2, 00^2 4_2 - 10^2 4_2, 6^2 19^2 4_2 - n$
23	8	10●R	060	09	C6.3	04.8	33.4	.	$\Delta^2 n - 5^2 4_2, 17^2 4_2, 18^2 4_2, \bullet^2 0 - 1, \Delta^2 n - 5^2 4_2, 8^2 4_2, 17^2 4_2, 17^2 4_2, = n - 6^2 4_2, \bullet^2 4 - 5^2 4_2, 8^2 4_2 - 10^2 4_2, \equiv -4^2 n, \bullet^2 7^2 4_2, = 5^2 4_2 - 6^2 4_2, \bullet^2 0 - 1, \bullet^2 6^2 4_2, \bullet^2 7^2 4_2, = 5^2 4_2 - 6^2 4_2, \bullet^2 0 - 1, \bullet^2 5^2 4_2, 14^2 4_2 - n$
24	7	10	10	03	C7.7	00.9	07.5	.	$\equiv n - 7^2 4_2, \bullet^2 5^2 4_2 - 6^2 4_2, \bullet^2 0 - 1, \bullet^2 5^2 4_2, 14^2 4_2 - n$
25	6	10●	10●	0?	C7.7	00.7	C1.5	.	$\equiv n - 7^2 4_2 - 6^2 4_2, \bullet^2 0 - 1, \bullet^2 5^2 4_2, 14^2 4_2 - n$
26	7	10●	090	09	09.3	02.5	C6.5	.	$\Delta^2 n - 9^2 4_2, \bullet^2 0 - 4 - 4^2 4_2, \bullet^2 0 - 4^2 4_2 - 11^2 4_2, = 9^2 4_2 - 13$
27	6	10●	09R0	06	08.3	01.4	05.2	.	$\equiv n - 15, \bullet^2 6^2 4_2 - 7, T^2 13^2 4_2, 14^2 4_2, 00^2 4_2 - 15, \bullet^2 2^2 4_2 - n, \bullet^2 21^2 4_2 - n$
28	7	10●	10	10●R	10.0	00.0	15.2	.	$\Delta^2 n, \bullet^2 6^2 4_2 - n, T^2 n, = n - 6^2 4_2, 10^2 4_2 - 13^2 4_2, 19^2 4_2 - n$
29	7	030	020	03	C2.7	11.2	37.4	.	$\equiv n - 10^2 4_2, \bullet^2 20^2 4_2 - n$
30	7	10≡	050	01	05.3	07.9	.	.	$\Delta^2 n - 10, 20^2 4_2 - n, \equiv n - 4^2 4_2 - 20^2 4_2, 7^2 4_2, \equiv -4^2 4_2 - 20^2 4_2, 7^2 4_2, = 7^2 4_2 - 12^2 4_2, 00^2 4_2 - n, \bullet^2 14^2 4_2 - n$
31	7	10≡	040	10	C8.0	06.2	00.0	.	$\Delta^2 n - 11, \equiv -2^2 n - 9^2 4_2, \equiv -1^2 n - 9^2 4_2, \equiv 9^2 4_2 - 11^2 4_2$

PES.
WRED.

1974 SEPTEMBER

LJUBLJANA BEŽIGRAD

 $\varphi = 46^{\circ}04'$ N $\lambda = 14^{\circ}31'$ E Gr. $\Delta G = + 58$ min.

BR. ST. 13

SD	Vzdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetroa D, I (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	734.8	734.8	724.7	16.1	20.6	14.6	17.6	21.3	15.4	13.6	12.5	13.3	13.9	91	73	97	87	S	1	SE	1	NE	1
2	735.3	734.9	735.2	15.9	25.0	17.6	19.0	25.6	15.3	13.5	13.0	12.4	12.1	96	52	80	76	NE	1	S	3	SE	2
3	735.3	734.0	714.1	14.6	26.4	20.8	20.7	26.7	13.1	9.8.5	11.4	12.7	14.0	92	49	76	72	NE	1	SW	2	SW	3
4	733.8	733.6	734.5	15.8	20.6	13.1	15.7	22.7	13.1	10.6	12.5	14.6	11.1	93	79	98	90	NE	2	NE	2	NE	1
5	740.4	738.3	736.9	10.6	21.7	14.8	15.5	23.0	10.2	08.0	09.2	10.6	10.8	96	54	86	74	NE	1	NE	1	NE	1
6	714.1	729.7	728.4	11.4	25.7	16.2	17.4	25.7	10.6	06.3	10.0	10.5	13.0	99	44	94	76	NE	1	NE	1	SE	1
7	717.7	731.5	733.4	12.2	16.6	12.4	13.4	18.7	11.7	10.0	10.2	10.0	10.1	96	70	93	86	NW	3	SE	1	-	0
8	736.8	737.9	739.5	10.0	22.8	14.5	15.5	23.5	09.9	04.7	09.2	10.6	11.4	100	51	92	81	NE	1	SE	1	-	0
9	741.1	739.4	738.9	11.0	22.7	17.7	17.3	24.3	10.7	05.9	04.7	13.0	14.8	99	63	97	85	N	1	S	1	SE	1
10	740.1	740.6	745.1	13.8	25.4	14.9	17.3	25.4	13.0	08.0	11.8	12.3	11.2	100	51	88	80	-	0	E	2	SE	1
11	745.7	746.2	744.8	13.1	20.2	14.4	15.5	21.4	12.5	08.4	10.6	08.3	10.4	94	47	85	75	N	1	NE	2	NE	1
12	743.5	742.4	742.0	13.3	19.7	16.4	16.5	20.2	11.9	06.5	09.6	11.0	10.8	84	64	77	75	NE	1	SE	1	SE	1
13	741.6	740.4	741.0	11.4	23.4	16.2	16.9	24.7	10.7	05.2	10.0	11.5	12.2	90	53	87	80	NF	1	F	1	SS	1
14	741.4	740.1	740.1	13.0	26.0	18.1	18.8	26.7	12.5	07.2	11.1	14.1	14.0	99	56	95	83	SE	1	NE	1	NE	1
15	739.6	737.8	739.8	14.8	25.4	18.4	19.3	25.7	14.8	10.3	12.4	14.7	15.0	94	61	94	84	SE	1	N	2	NE	1
16	739.6	739.3	740.2	15.0	23.1	17.5	18.3	23.8	14.6	10.0	12.5	12.4	12.6	98	58	84	80	NE	1	SE	2	E	1
17	740.0	738.8	739.2	14.0	24.4	17.0	18.1	25.4	13.0	08.8	12.0	12.1	12.3	100	53	85	79	NE	1	NW	1	-	0
18	739.0	737.6	736.2	13.8	24.6	18.2	18.7	24.8	13.4	08.2	11.6	12.3	12.0	98	53	77	76	S	1	SW	3	SW	3
19	739.6	738.7	739.0	14.4	22.2	15.8	17.1	22.3	12.9	08.4	11.9	13.0	12.5	97	65	92	85	NE	1	NE	1	NE	1
20	734.7	733.6	733.4	14.0	16.4	14.8	15.0	17.4	13.8	10.0	11.7	12.8	12.1	98	91	96	95	NE	1	SE	1	N	1
21	733.6	734.1	733.0	13.8	13.7	12.4	13.1	15.1	12.4	11.9	10.5	09.7	09.4	89	82	87	86	SE	1	NE	1	SE	1
22	731.7	733.0	734.1	11.8	15.9	14.8	14.3	17.0	11.4	07.7	09.8	10.3	12.0	94	76	95	86	-	0	NE	1	-	0
23	736.4	736.4	733.9	10.0	11.8	11.0	11.0	15.3	09.5	08.0	08.7	08.3	08.8	94	80	90	86	NW	1	N	1	SW	1
24	729.2	726.0	725.5	05.2	15.4	13.2	12.5	16.7	08.6	04.6	08.6	11.6	11.1	99	82	98	95	-	0	NW	1	NW	1
25	726.7	725.4	722.7	08.4	10.7	09.0	09.3	13.4	08.3	06.7	07.9	07.8	08.2	95	81	95	90	SW	1	ENE	2	N	1
26	721.0	723.6	729.4	08.0	15.1	07.8	09.7	16.1	07.3	01.5	07.9	08.1	07.3	99	63	92	85	NW	1	SW	2	E	1
27	735.7	735.4	736.3	03.4	18.3	09.3	10.1	19.0	03.4	-01.4	05.8	04.1	06.0	100	26	91	72	NE	1	NE	1	NE	1
28	734.9	733.1	732.9	05.6	20.6	13.8	13.5	20.6	04.2	-00.5	06.3	07.9	08.1	92	43	65	68	NE	1	W	3	SW	2
29	729.0	731.3	732.9	11.0	19.6	12.1	13.7	20.0	09.8	03.9	09.6	12.6	09.3	98	74	88	87	NW	2	SW	1	NE	3
30	734.6	734.8	735.5	09.7	11.1	09.2	09.8	12.8	09.1	07.7	07.6	09.0	08.6	95	81	99	88	E	1	NE	3	NE	1
MES.	WRIĐ.	736.0	735.4	735.0	12.0	20.2	14.6	15.4	21.2	11.2	07.5	10.2	11.0	11.3	96	63	89	82	1.0	1.6	1.1		

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LJUBLJANA BEŽIGRAD

1	735.7	735.3	736.2	07.2	13.2	07.4	08.8	13.3	06.5	05.0	07.4	07.5	07.3	97	66	95	86	SE	1	SE	2	NW	1
2	734.6	733.4	733.6	06.9	06.4	05.4	06.0	07.7	05.4	04.8	07.4	06.3	06.3	99	68	94	94	NE	1	NE	2	SW	1
3	736.4	736.2	735.7	04.0	10.4	08.0	07.6	11.7	03.1	-01.5	05.9	06.7	07.6	97	71	97	88	NE	1	SW	2	NE	1
4	733.8	735.7	737.4	10.6	11.4	06.7	08.9	12.0	06.7	05.6	09.0	09.9	07.2	94	98	97	96	N	2	ENE	1	SW	1
5	737.1	736.4	735.5	05.4	06.0	06.0	06.5	07.4	05.0	03.5	05.3	06.6	06.9	94	88	93	92	SE	1	S	2	N	1
6	734.8	735.6	736.4	06.3	09.2	04.0	05.5	10.0	04.0	03.4	06.8	05.8	05.9	95	67	97	86	SE	1	SE	2	NE	1
7	734.5	730.1	729.2	03.3	11.0	06.3	06.7	11.1	02.8	-03.1	05.8	06.1	06.8	100	62	95	86	NE	1	SE	1	N	1
8	725.7	728.3	731.1	06.6	07.2	06.0	06.5	07.6	05.4	-01.0	07.1	06.7	06.7	97	88	96	94	SW	2	N	2	NW	1
9	731.9	731.9	734.4	04.2	11.4	07.4	07.6	12.1	04.1	01.0	05.9	06.4	07.3	96	63	95	85	NW	1	SE	1	NW	2
10	737.0	736.6	737.4	04.0	10.9	04.8	06.1	12.2	02.8	-03.0	05.9	06.8	06.2	97	70	96	88	S	2	SE	1	-	0
11	737.0	736.5	737.3	04.2	09.9	08.1	07.6	10.1	03.6	00.5	06.0	07.5	07.9	97	82	97	92	N	1	N	1	SE	1
12	736.0	735.9	734.8	07.1	08.4	07.6	07.7	08.9	07.0	00.4	07.2	07.5	07.4	95	51	95	94	NE	1	N	1	N	1
13	734.9	736.0	736.6	07.1	07.9	06.6	07.1	08.3	06.6	05.5	07.3	08.8	06.9	96	85	95	92	NE	1	SSE	1	NF	1
14	735.5	735.3	736.2	06.0	08.9	05.5	06.5	09.0	05.4	03.5	06.6	05.7	06.1	94	68	90	84	N	1	SE	2	NE	1

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Insekcija broj sati	Podzemna voda mm	Snežni pokrovac h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7	05	10•	10	05.7	03.0	04.2	.		
2	7	10	040	05	06.2	08.4	11.0			
3	7	010	040	01	02.0	11.3	.			
4	7	070	08=	04	04.3	02.7	03.8	.		
5	6	050	010	01	02.3	10.3	03.4	.		
6	7	10=	020	02	04.7	05.7	00.0	.		
7	8	09•	050	06	06.0	01.2	42.2	.		
8	8	10=	020	00	04.0	09.8	00.1	.		
9	7	10=	080	02	01.7	06.4	.	.		
10	7	10=	040	10	08.7	06.8	00.1	.		
11	6	050	020	00	02.3	10.2	01.9	.		
12	7	10	10	09	04.7	00.4	.	.		
13	7	10=	000	00	03.3	07.9	.	.		
14	6	10=	010	00	02.7	08.9	.	.		
15	7	10=	010	00	03.7	07.2	.	.		
16	7	10=	080	06	08.0	04.7	.	.		
17	7	10=	030	04	05.7	06.6	.	.		
18	7	10=	040	00	04.7	06.2	.	.		
19	6	10=	09	02	07.0	01.2	00.0	.		
20	4	10=	10•	10•	10.0	00.0	03.8	.		
21	6	10•	10•	10	10.0	00.0	14.7	.		
22	6	10	10•	10	10.0	00.3	01.6	.		
23	8	10	10	10	10.0	00.0	35.4	.		
24	7	10=	10•	10•	10.0	00.0	01.8	.		
25	7	10	090	09	04.3	00.7	33.1	.		
26	8	09	050	01	05.0	04.3	06.2	.		
27	8	10=	030	00	04.2	09.1	.	.		
28	9	10	020	01	04.3	10.3	.	.		
29	7	10•	050	10	08.3	02.2	00.8	.		
30	8	10•	10	10•	10.0	00.0	05.3	.		
MES. VRKD.			09.2	05.0	04.0	06.5	145.8	165.4		

1	8	10•	070	09	08.7	01.9	11.3	.		
2	6	10•	10•	10	10.0	00.0	07.1	.		
3	7	10	09•	10•	09.7	02.3	09.9	.		
4	4	10•	10•	10•	10.0	00.0	10.2	.		
5	7	10•	10	10•	10.0	00.0	05.8	.		
.										
6	8	10•	05	00	06.3	02.2	04.0	.		
7	6	080	03	07.0	02.2	00.0	.	.		
8	7	10•	10	00	06.7	00.3	74.3	.		
9	7	10•	050	10•	08.3	04.3	10.9	.		
10	7	10=	030	00	04.3	04.4	16.4	.		
.										
11	7	10•=	09	10	09.7	01.0	00.2	.		
12	5	10	10•	10•	10.0	00.0	07.4	.		
13	7	10	10	10	10.0	00.0	12.1	.		
14	7	10	10	08	09.3	00.0	00.3	.		
15	7	10=	09	10•	09.7	00.0	.	.		
.										
16	6	10•	09•	04	07.7	00.0	02.3	.		
17	8	10=	020	02	04.7	05.8	06.4	.		
18	8	020	040	09	05.0	08.3	.	.		
19	7	10	10	10	10.0	02.4	.	.		
20	4	10•	10•	10•	10.0	00.0	05.6	.		
.										
21	7	10•	10•	10	10.0	00.0	37.5	.		
22	8	10=	040	10	08.0	06.3	03.4	.		
23	8	10=	030	01	04.7	06.2	.	.		
24	8	070	09	09	08.3	02.7	.	.		
25	7	04=	020	02	02.7	08.1	.	.		
.										
26	6	10	080	06	08.0	00.0	.			
27	7	10=	040	10	08.0	05.6	00.2	.		
28	5	10•	10•	10•	10.0	00.0	01.7	.		
29	6	10=	060	00	05.3	04.0	10.6	.		
30	6	10=	000	04=	04.7	03.4	.	.		
31	6	09	070	07	07.7	00.4	01.3	.		
.										
MES. VRKD.			09.4	07.3	06.9	07.9	71.9	283.4		

1974 NOVEMBAR

LJUBLJANA BEŽIGRAD

 $\varphi = 46^{\circ}04'$ N $\lambda = 14^{\circ}31'$ E Gr. $\Delta G = + 58$ min.

BP. ST. 13

Dan	Vzdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	732.1	732.3	734.7	-00.4	10.2	02.8	04.1	10.9	-00.1	-04.4	04.3	03.1	03.1	91	33	56	60	NF	1	NW	2	
2	735.2	733.7	736.2	-03.0	10.9	05.2	04.6	10.9	-03.0	-10.0	03.4	04.0	04.1	94	40	62	65	F	1	SW	4	
3	737.0	737.1	737.5	-02.8	12.9	04.2	04.6	14.8	-02.8	-08.7	03.5	03.5	04.4	94	31	71	65	SE	1	NE	1	
4	736.8	734.6	735.7	-01.1	09.9	04.2	05.3	10.3	-01.6	-07.3	04.0	04.7	06.3	95	52	89	79	NF	1	NE	1	
5	737.1	738.6	741.3	04.4	06.2	04.7	05.0	06.6	04.4	02.6	06.0	05.9	05.8	96	82	90	89	N	3	NE	1	
6	742.7	743.2	744.9	01.0	03.3	03.5	02.8	05.0	00.9	-01.5	04.7	05.4	05.7	95	94	97	95	NW	1	E	1	
7	744.5	742.9	742.6	04.0	05.2	04.3	04.5	05.3	03.5	-01.2	05.6	05.6	05.7	92	84	91	89	N	1	S	1	
8	741.4	740.5	742.0	03.3	07.2	01.7	03.2	08.3	01.2	-00.6	05.1	04.3	04.2	98	56	85	75	SW	1	SW	2	
9	742.3	740.7	741.0	-02.2	08.7	01.0	01.9	09.2	-03.6	-09.5	03.5	04.2	04.3	100	46	88	79	SF	1	SE	1	
10	740.1	738.2	738.7	-02.2	07.8	03.6	03.0	09.2	-03.6	-09.5	03.4	04.0	05.0	98	58	85	80	E	1	E	1	
11	740.7	740.0	739.9	00.7	11.3	03.3	04.7	12.3	00.2	-05.5	04.6	04.4	05.0	95	44	86	75	E	1	SW	1	
12	738.9	737.5	737.2	-00.9	10.7	04.0	04.5	11.4	-01.3	-06.5	04.1	05.4	06.3	96	56	79	77	NE	1	W	2	
13	737.9	738.7	739.0	05.3	09.9	08.3	08.0	10.0	04.0	00.0	05.6	06.5	07.5	85	71	91	82	N	1	E	1	
14	738.3	738.4	739.2	07.6	12.6	16.2	10.2	13.6	07.2	01.0	06.8	06.9	06.8	87	63	73	74	SW	1	WNW	2	
15	738.5	738.9	738.7	11.0	11.6	12.7	12.0	13.0	09.6	05.0	08.4	09.6	08.3	85	93	76	85	WSW	3	W	3	
16	737.6	736.8	738.0	12.7	14.4	12.8	13.2	15.3	12.5	10.3	07.9	07.0	08.2	72	57	74	64	SW	2	SW	3	
17	740.2	740.4	740.5	10.8	15.0	06.7	10.4	16.0	09.5	09.9	03.7	09.4	07.6	90	74	90	85	SW	1	NW	3	
18	739.7	739.4	738.0	10.2	14.4	12.9	12.6	14.8	05.8	00.0	06.9	07.4	08.0	74	60	72	69	W	3	SW	3	
19	732.6	732.2	737.9	09.9	10.1	04.8	07.2	13.0	04.6	07.9	07.2	05.6	90	78	87	85	-	0	N	3		
20	740.1	739.6	739.9	03.1	05.9	04.5	04.5	06.4	03.0	-00.5	05.5	05.9	05.8	97	85	91	91	SE	1	NE	1	
21	738.2	738.2	739.0	03.6	07.2	05.0	05.3	08.0	03.5	00.5	06.0	06.4	06.3	100	84	96	93	N	1	SW	1	
22	739.6	738.4	738.4	03.8	08.5	06.0	07.1	08.7	03.6	03.4	05.7	06.4	06.5	95	77	81	84	N	1	SW	1	
23	738.6	737.5	737.6	04.6	10.2	06.9	07.2	10.4	04.1	00.5	06.0	06.9	06.7	94	74	89	86	-	0	NW	1	
24	737.5	737.2	737.5	05.4	08.4	07.4	07.2	08.8	05.1	04.9	06.4	07.0	07.3	96	85	95	92	NNE	1	-	0	
25	735.0	731.7	731.2	07.2	09.4	06.4	07.4	10.2	06.2	05.6	07.4	07.1	06.5	97	80	91	89	SSW	2	NE	1	
26	734.1	732.9	731.5	03.4	08.3	02.1	04.6	08.6	02.1	02.3	05.2	04.6	04.9	89	56	92	79	N	1	S	1	
27	729.6	731.3	731.5	01.6	08.4	02.0	03.6	08.6	00.2	-04.2	04.7	04.9	04.5	92	59	86	75	NNE	1	SE	3	
28	721.4	720.6	723.8	02.3	02.4	02.0	02.2	06.1	00.4	-00.2	05.1	05.1	05.0	94	94	94	94	SE	1	SE	2	
29	725.1	726.0	729.1	-01.0	02.0	00.7	00.6	02.6	-01.4	-04.0	04.2	05.0	04.7	98	95	97	97	NF	1	ESE	1	
30	733.5	735.6	735.9	-00.3	01.1	-00.2	00.1	01.3	-00.4	-00.5	04.3	04.3	04.3	96	87	95	93	NW	1	N	1	
31	MES.	WRFD.	736.9	736.4	737.3	03.3	08.2	05.4	05.8	09.6	02.4	-00.4	05.5	05.8	05.8	92	68	85	82	1.2	1.8	1.2

1974 DECEMBAR

LJUBLJANA BEŽIGRAD

1	734.8	737.0	741.6	-00.7	07.4	02.2	02.8	08.0	-01.2	-01.5	04.1	05.0	05.0	94	65	94	84	N	1	-	U	SSW	1
2	741.6	732.7	745.3	01.4	05.0	01.2	02.2	06.6	00.2	-04.1	04.5	04.7	04.6	95	58	85	81	NE	1	NF	1		
3	745.9	746.1	746.3	-01.6	06.4	00.7	01.6	07.0	-01.6	-03.8	03.9	05.6	04.6	98	80	95	91	S	1	-	C	NE	1
4	745.3	742.6	740.0	-01.0	01.1	00.2	00.1	01.8	-01.3	-05.0	04.1	04.8	04.6	96	97	96	97	-	0	-	0	-	0
5	737.1	735.6	735.7	-01.5	-00.2	-00.3	-00.6	00.7	-01.7	-01.3	04.0	04.4	04.3	98	98	96	97	NE	1	SE	1	E	1
6	737.6	736.8	737.2	-01.3	00.4	00.0	00.2	00.6	-01.3	-01.3	04.0	04.6	04.6	98	96	97	97	SE	1	W	1	N	1
7	736.5	734.9	735.3	-01.6	-00.2	-00.8	-00.9	00.6	-01.7	-01.4	03.9	04.4	04.2	96	96	96	96	NE	1	NE	1	N	1
8	733.5	733.6	736.3	-01.6	07.5	02.0	02.9	08.4	-01.8	-04.4	03.8	05.9	05.3	94	75	94	88	NE	1	ENE	1	-	0
9	737.7	737.6	739.2	00.0	04.0	01.4	01.7	05.1	00.0	-05.1	04.4	05.7	04.9	96	94	97	96	-	0	N	1	-	0
10	738.9	738.6	739.7	00.0	01.4	02.6	01.7	02.7	-00.3	-00.2	04.5	05.0	05.3	98	93	95	97	ENE	1	E	1	NE	1
11	737.7	733.1	728.4	03.2	04.4	04.7	04.3	05.0	04.6	01.7	05.4	06.1	06.2	94	97	97	96	SE	1	N	1	NF	1
12	731.3	733.0	732.3	01.8	03.1	00.1	01.2	07.1	-00.6	-00.0	04.7	04.2	04.4	90	74	95	86	SE	2	SE	1	W	1
13	726.5	726.8	732.9	-00.9	03.7	02.3	01.9	04.1	-00.8	-05.4	04.2	04.3	02.3	96	72	42	70	SW	1	SW	2	ENE	1
14	739.0	738.9	740.2	-02.2	05.4	-00.6	00.4	05.6	-02.4	-03.2	02.5	02.6	02.9	68	39	68	58	W	1	SSW	1	S	1
15	739.5	737.8	737.5	-06.4	01.2	-01.7	-01.9	02.4	-06.7	-10.3	02.5	03.5	03.3	95	68	78	80	NE	1	N	1	NE	1
16	738.6	738.3</																					

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Veličina 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	9	06	010	01	02.7	07.8	.	.	.	$\infty 0-7^{\circ}14, \square^0-0-8^{\circ}12, 20^{\circ}2-24, \square^0-0-6, = 7^{\circ}14-10^{\circ}14$	
2	8	020	060	00	02.7	05.5	.	.	.	$\square^2-6, \square^0-5-6, = 6^{\circ}14-10^{\circ}12, \infty 10-12$	
3	9	020	040	02	02.7	07.3	.	.	.	$= 0^{\circ}-11^{\circ}, \square^0-0-10-12, 23^{\circ}-24, \square^0-20^{\circ}2-23, \square^0-23^{\circ}12-24$	
4	7	08	070	10*	06.3	05.6	.	.	.	$\square^0-0-8^{\circ}14, \square^0-0-10^{\circ}14, = 1^{\circ}12-3^{\circ}14, 22-24, \infty 18^{\circ}14-18^{\circ}14, \square^0-10^{\circ}24$	
5	7	10*	10	10*	10.0	00.0	03.8	.	.	$= 0-10^{\circ}12, 14^{\circ}14-24, \square^0-0-8^{\circ}14, 14^{\circ}20-24, \square^0-0-8^{\circ}12-9^{\circ}12$	
6	6	10*	10*	10*	10.0	00.0	15.7	.	.	$= 0-24, \square^0-0-12^{\circ}14, \square^0-0-6^{\circ}12, 10^{\circ}2-24, \square^0-0-6^{\circ}14-13, \square^0-13-24$	
7	6	10*	10	10	10.0	00.0	05.6	.	.	$= 0-24, \square^0-0-4^{\circ}12, \square^0-4^{\circ}12-10^{\circ}$	
8	7	09	050	00	04.7	04.7	00.0	.	.	$= 0-11^{\circ}12, 22-24, \infty 11^{\circ}12-16^{\circ}14, 19-22, \square^0-20-24$	
9	7	10	000	00	03.3	05.4	.	.	.	$\square^0-0-10^{\circ}12, 18^{\circ}14-24, = 0-2, 10^{\circ}3^{\circ}14-11^{\circ}12, 18^{\circ}12-24, \square^0-2-6^{\circ}14, 10^{\circ}2-10^{\circ}14, = 6^{\circ}14-10^{\circ}10$	
10	6	10	060	09	08.3	03.4	.	.	.	$\square^0-0-10^{\circ}14, = 0-5^{\circ}14, 18^{\circ}14-24, = 0-3^{\circ}5^{\circ}14, 10^{\circ}11, = 0-3^{\circ}5^{\circ}14-10^{\circ}10, \square^0-20^{\circ}24, \square^0-11^{\circ}12-14^{\circ}14$	
11	5	09	10	04	07.7	04.6	.	.	.	$\square^0-10^{\circ}14, = 0-7^{\circ}14-9^{\circ}12-13^{\circ}12-24, \square^0-4^{\circ}14-8, 19^{\circ}12-24, = 0-7^{\circ}9^{\circ}12, 00-13-18^{\circ}12$	
12	8	07	10	04	08.7	02.5	.	.	.	$= 0-42^{\circ}14, \square^0-0-10^{\circ}12$	
13	5	05	09	10	08.0	00.2	.	.	.	$= 6^{\circ}14-10^{\circ}10, = 7^{\circ}12-13^{\circ}14, 17^{\circ}14-24, \infty 10^{\circ}14-17^{\circ}14, \square^0-16^{\circ}5^{\circ}14-17^{\circ}12, \square^0-0-18^{\circ}25, \square^0-11^{\circ}12$	
14	7	04	08	02	04.7	05.0	00.2	.	.	$= 0-9^{\circ}12, \square^0-11^{\circ}14, = 0-19^{\circ}12-24$	
15	6	10*	10*	10*	10.0	00.0	00.0	.	.	$\infty 0-5^{\circ}12, = 5^{\circ}12-24, \square^0-6-15^{\circ}14, 19^{\circ}14-21^{\circ}12, \square^0-22^{\circ}14-24$	
16	8	09	09	04	07.3	00.4	00.2	.	.	$\square^0-0-3, = 0-6^{\circ}14, \square^0-0-4^{\circ}12, 4^{\circ}12-10^{\circ}14, = 7^{\circ}12-11^{\circ}12, \square^0-0-25, V 17^{\circ}14-18^{\circ}14, \square^0-12-24$	
17	8	10*	06	00	05.3	02.2	00.3	.	.	$\square^0-0-50, \square^0-0-8^{\circ}12$	
18	8	07	080	04	06.3	04.3	00.2	.	.	$= 5^{\circ}14-12^{\circ}12, 16-24^{\circ}12, \square^0-6^{\circ}25, 12, 18^{\circ}12-19^{\circ}12, T^{\circ}14-14^{\circ}52, \square^0-14^{\circ}52, 17^{\circ}12, F_{\text{W-W}} 15^{\circ}14-16^{\circ}14, \square^0-18^{\circ}12$	
19	7	09*	080	09	08.7	00.8	00.0	.	.	$= 4^{\circ}12, = 0-15^{\circ}12-7^{\circ}12$	
20	6	10	090	10	05.7	00.2	20.7	.	.		
21	5	10	10	10	10.0	00.0	.	.	.	$\square^0-3, 10^{\circ}12-20^{\circ}14, = 0-3^{\circ}4^{\circ}14, 9^{\circ}12-10^{\circ}12, 20^{\circ}14-20^{\circ}12, = 0-2-4^{\circ}14-9^{\circ}12, 20^{\circ}12-24, \square^0-0-9^{\circ}12-10^{\circ}12$	
22	5	10	09	09	09.3	00.4	00.1	.	.	$\square^0-4^{\circ}12, 19^{\circ}12-24, = 0-4^{\circ}2^{\circ}12, 2^{\circ}12-17^{\circ}12, = 7^{\circ}12-24$	
23	7	10	060	09	08.3	00.4	.	.	.	$\square^0-0-12, 20-24, = 0-13, 19-24, \infty 13-19$	
24	6	10*	10	10	10.0	00.0	00.5	.	.	$\square^0-0-2^{\circ}14, = 0-22, \square^0-2^{\circ}14-8^{\circ}12, \square^0-11^{\circ}12-12^{\circ}14, = 0-22-24$	
25	6	10*	10*	10*	10.0	00.0	01.5	.	.	$\square^0-0-10^{\circ}12, \square^0-15^{\circ}14-24, = 6-7^{\circ}12, 10^{\circ}12-24$	
26	8	10*	010	02	04.3	05.4	28.6	.	.	$= 0-7^{\circ}14, 19^{\circ}12-24, \square^0-3^{\circ}7^{\circ}14, \square^0-16^{\circ}3^{\circ}14-17^{\circ}14, \square^0-9^{\circ}17^{\circ}14-23^{\circ}14, \square^0-23^{\circ}14-24$	
27	6	08*	040	03	05.0	05.8	00.6	.	.	$\square^0-0-30^{\circ}19^{\circ}14-24, = 0-4^{\circ}14, \square^0-0-50, = 0-1^{\circ}14, \square^0-1^{\circ}14-19^{\circ}14, \square^0-0-30^{\circ}17^{\circ}14-19^{\circ}14$	
28	5	10*	10*	09	09.7	00.0	00.1	.	.	$\square^0-3^{\circ}14, \square^0-5^{\circ}14, = 4^{\circ}12-16^{\circ}14, \square^0-6^{\circ}14-12^{\circ}14, \square^0-12^{\circ}14-17^{\circ}14, \square^0-12^{\circ}14-13^{\circ}14-13^{\circ}14$	
29	3	C5	10	10	08.3	00.0	28.2	.	.	$\square^0-10^{\circ}12, \square^0-10^{\circ}12, = 4-6, 17^{\circ}12, 18^{\circ}14, = 6-7^{\circ}12, 10^{\circ}14-18^{\circ}12, = 0-7^{\circ}12-10^{\circ}12, 18^{\circ}12-24$	
30	4	10	10	10	10.0	00.0	.	.	.	$\square^0-10^{\circ}12, = 0-15^{\circ}14-18^{\circ}14, = 6^{\circ}14-24$	
MES. VR ED.	CR-3	07.5	06.5	07.5	72.4	106.5					

LJUBLJANA BEŽIGRAD

1974 DECEMBAR

1	7	05	020	10	05.7	05.0	.	.	.	$= 0-0^{\circ}14, 4^{\circ}14-12, 18^{\circ}12-24, = 0-0^{\circ}14-4^{\circ}14, \infty 13^{\circ}14-18^{\circ}14$	
2	8	04	07	01	05.7	00.7	.	.	.	$= 0-8^{\circ}14, 17^{\circ}12-24, \square^0-1^{\circ}14, 9^{\circ}14, \square^0-20-23^{\circ}14, \square^0-1^{\circ}23^{\circ}14-24$	
3	4	10	030	00	04.3	03.4	.	.	.	$\square^0-10^{\circ}14, 19^{\circ}14-24, = 0-5^{\circ}12, 18^{\circ}14-17^{\circ}14, \square^0-1^{\circ}14, 9^{\circ}14, \square^0-13^{\circ}14, 10^{\circ}14-13^{\circ}14, 11^{\circ}12-22^{\circ}12-24, \square^0-17^{\circ}12-14^{\circ}14$	
4	1	10	000	10	06.7	00.0	.	.	.	$\square^0-2^{\circ}14, \square^0-24$	
5	1	10	10	10	10.0	00.0	00.0	.	.		
6	3	10	10	10	10	00.0	00.0	.	.	$\square^0-2^{\circ}14, \square^0-10^{\circ}12-24, \square^0-20-20^{\circ}14, \square^0-20^{\circ}14-24$	
7	2	10	10	10	10	00.0	00.0	.	.	$\square^0-10^{\circ}10, \square^0-5^{\circ}12-5^{\circ}12, = 0-5^{\circ}12, 5^{\circ}12-13^{\circ}12, 17^{\circ}12-24, \square^0-20^{\circ}14-24$	
8	6	04	060	06	05.3	03.4	.	.	.	$\square^0-10-5^{\circ}12, = 0-1^{\circ}12, 16^{\circ}12-16^{\circ}14, \square^0-5^{\circ}12-11^{\circ}14, \square^0-11^{\circ}14-24, \square^0-12^{\circ}14-17^{\circ}14, \square^0-12^{\circ}14-13^{\circ}14$	
9	3	10	C50	10	07.3	00.1	.	.	.	$\square^0-2-12^{\circ}14, = 0-12^{\circ}14-16^{\circ}14, \square^0-12^{\circ}14-18^{\circ}14, = 0-16^{\circ}14-18^{\circ}14, = 0-16^{\circ}14-18^{\circ}14$	
10	3	10	10	10	10.0	00.0	00.5	.	.		
11	2	10	10	10	10.0	00.0	00.0	.	.	$\square^0-7^{\circ}14, 21^{\circ}14-24, = 0-7^{\circ}14-17^{\circ}14, \square^0-7^{\circ}14-17^{\circ}14, \square^0-12^{\circ}14-14^{\circ}14, \square^0-12^{\circ}14-14^{\circ}14, \square^0-22^{\circ}12-24$	
12	6	10*	090	09	05.3	00.0	26.1	.	.	$= 0-6^{\circ}12, 19^{\circ}12-24, \square^0-2^{\circ}12, 1^{\circ}12-17^{\circ}12, \square^0-2^{\circ}12-2^{\circ}12, 2^{\circ}12-2^{\circ}12, 2^{\circ}12-2^{\circ}12, 4^{\circ}12-15^{\circ}12, = 0-1^{\circ}12-24$	
13	7	10*	060	08	08.0	02.2	00.0	.	.	$\square^0-1^{\circ}12, 17^{\circ}12-24, \square^0-1^{\circ}12-17^{\circ}12, 17^{\circ}12-17^{\circ}12, 15^{\circ}12-15^{\circ}12$	
14	8	01	000	00	00.3	07.5	00.0	.	.	$\square^0-1^{\circ}12, 17^{\circ}12-24, = 3^{\circ}12-8^{\circ}14, 11^{\circ}12-12^{\circ}14, 20-24, = 0-8^{\circ}14-11^{\circ}12, 00-12^{\circ}12-20$	
15	6	03	030	10	05.3	04.1	.	.	.		
16	5	03	010	00	01.3	03.1	.	.	.	$\square^0-10^{\circ}12, 19^{\circ}12-24, = 0-12^{\circ}12, 18^{\circ}12-24, \square^0-12^{\circ}12-18^{\circ}12, \square^0-12^{\circ}12-18^{\circ}12$	
17	5	10	080	10	05.3	00.4	.	.	.	$\square^0-10-5^{\circ}12, = 0-1^{\circ}12, 18^{\circ}12-18^{\circ}12, \square^0-10-5^{\circ}12, = 0-1^{\circ}12-18^{\circ}12, \square^0-10-18^{\circ}12$	
18	4	10	10	10	10.0	00.0	02.6	.	.	$\square^0-8-5^{\circ}12, = 0-1^{\circ}12, 18^{\circ}12-18^{\circ}12, \square^0-10-18^{\circ}12, = 0-1^{\circ}12-18^{\circ}12, \square^0-10-18^{\circ}12$	
19	5	08	050	00	04.3	02.9	00.1	.	.	$\square^0-0-11^{\circ}12, 16^{\circ}12-16^{\circ}14, \square^0-11^{\circ}12-16^{\circ}14, = 0-2^{\circ}12-11^{\circ}12, = 0-2^{\circ}12-11^{\circ}12$	
20	7	05	030	06	04.7	06.4	.	.	.	$= 0-10^{\circ}12, \square^0-10^{\circ}12$	
21	7	05	080	00	04.3	06.6	.	.	.	$\square^0-1^{\circ}12-24, = 20^{\circ}12-24$	
22	6	01	000	00	00.3	03.4	.	.	.	$\square^0-0-12, 4^{\circ}12-24, = 0-20^{\circ}12, \square^0-10^{\circ}14-15^{\circ}14, = 0-20-22^{\circ}12, \square^0-21-24, = 0-22^{\circ}12-24$	
23	2	10	10	10	10.0	00.0	00.0	.	.	$\square^0-1^{\circ}12-24, \square^0-1^{\circ}12-24$	
24	6	10	10	10	10.0	00.0	00.0	.	.	$\square^0-1^{\circ}12-24, \square^0-1^{\circ}12-24, = 0-1^{\circ}12-5^{\circ}12, = 0-1^{\circ}12-5^{\circ}12, = 5^{\circ}12-17^{\circ}14$	
25	7	10	050	08	07.7	00.0	00.0	.	.	$\square^0-0-1^{\circ}14, \infty 12-18-18-24$	
26											

1974 JANUAR

ZAGREB GRČ

 $\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$

BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	755.0	754.6	754.7	01.3	02.1	01.3	01.5	02.5	00.6	-	04.3	04.8	04.6	86	88	92	89	NN	2	NN	2	NE	1
2	753.8	752.8	752.5	01.5	02.4	01.7	01.8	02.7	01.0	-	04.8	05.0	05.0	93	93	97	94	NN	1	E	1	NE	1
3	751.1	750.7	752.0	01.8	02.2	01.9	02.0	02.3	01.4	-	05.0	05.3	04.8	95	98	91	95	NN	1	SSE	1	SSE	1
4	753.8	754.9	756.8	01.1	02.1	01.4	01.5	02.2	01.1	-	04.8	05.0	04.6	97	93	93	94	SSE	1	SSW	1	SSW	1
5	756.3	754.6	753.8	01.5	02.7	02.9	02.5	03.0	01.1	-	04.8	05.0	05.0	95	90	91	92	SSW	1	SSW	1	SSW	1
6	750.0	747.5	748.9	02.4	04.0	02.9	03.0	04.2	02.2	-	05.3	05.6	05.3	96	91	94	94	SSW	1	NE	2	SE	1
7	752.0	752.4	752.4	02.3	03.8	03.3	03.2	04.0	02.2	-	05.0	04.8	04.9	92	77	85	85	SSE	1	WNW	2	WSW	2
8	751.2	752.2	753.5	02.8	04.4	03.2	03.4	04.4	02.5	-	04.8	05.3	05.0	87	86	86	86	NE	1	ENE	1	SSE	1
9	752.0	751.1	750.0	02.5	03.0	01.8	02.3	03.2	01.8	-	05.0	05.0	04.7	92	87	90	90	ESF	2	SSE	2	FSE	2
10	749.0	751.1	753.8	00.5	01.1	06.7	00.8	01.8	-00.4	-	04.6	04.6	03.9	96	91	81	89	ENE	2	ENE	2	ENE	2
11	755.6	755.6	756.4	00.3	01.0	01.4	01.0	01.4	-00.5	-	03.9	04.0	04.1	84	82	82	83	S	2	SW	1	SSW	2
12	757.0	757.2	757.6	-00.4	04.8	02.4	02.3	05.3	-00.4	-	04.0	04.8	04.6	91	75	85	84	ENE	1	ENE	1	WNW	1
13	756.8	756.8	757.9	-00.4	-00.3	00.4	00.0	02.4	-01.4	-	04.4	04.1	04.3	100	95	92	96	SSW	1	ENE	2	NNE	2
14	757.8	757.7	756.6	00.1	00.8	-00.5	00.0	01.4	-00.6	-	03.8	03.4	03.2	82	71	73	75	ESE	2	ESE	2	WSW	1
15	756.1	755.8	755.5	-00.3	01.5	01.2	00.9	01.7	-00.5	-	03.4	03.6	04.4	75	71	88	78	WSW	2	SSW	2	ENE	1
16	754.6	754.3	752.1	00.7	03.1	02.3	02.1	03.5	00.5	-	04.3	05.0	04.9	89	86	91	89	NE	1	SW	1	SW	1
17	747.0	748.3	751.5	01.2	02.8	03.7	02.8	03.9	00.9	-	04.6	05.4	05.6	92	96	93	94	SW	1	NNW	2	W	2
18	752.1	751.3	752.0	01.7	04.4	03.5	03.5	04.4	00.7	-	04.2	04.6	04.6	80	75	76	77	W	2	ENE	1	NNE	1
19	752.5	752.2	751.6	03.3	06.2	07.0	05.9	07.2	03.2	-	05.1	05.8	06.6	88	81	87	85	W	2	W	2	W	2
20	750.5	751.2	754.4	06.8	14.4	07.3	09.0	14.8	06.4	-	05.9	07.4	06.4	80	60	84	75	EN	1	ESF	2	NW	2
21	755.6	755.1	756.2	02.0	07.5	02.5	04.3	07.9	01.7	-	05.0	06.2	05.2	93	79	86	86	E	1	SSF	2	NNE	1
22	755.3	753.6	753.7	-01.5	03.1	00.7	00.8	03.9	-02.1	-	04.0	05.0	04.6	98	86	96	93	SSF	1	SSF	1	NNW	1
23	755.6	754.7	753.3	00.3	03.2	00.8	01.3	03.8	-01.2	-	04.4	04.4	04.4	93	76	92	87	WSW	1	WSW	2	WSW	1
24	753.5	752.7	751.2	-01.0	00.0	-00.8	-00.5	00.8	-01.0	-	04.1	04.6	04.2	96	95	98	96	SW	1	SSE	1	SSE	1
25	751.1	750.7	752.1	-00.0	02.5	01.3	01.1	03.4	-01.4	-	04.2	05.0	04.8	96	92	95	94	SSF	1	SSE	1	SSE	1
26	752.5	752.0	751.7	-00.4	00.5	-00.5	-00.2	01.3	-00.9	-	04.3	04.6	04.3	96	95	98	96	SSW	1	SSW	1	S	1
27	749.3	748.2	749.7	-01.2	01.1	01.3	00.6	02.3	-02.0	-	04.0	04.7	05.0	96	94	99	96	SW	1	SSE	1	WSW	1
28	752.2	751.9	751.9	01.2	03.5	01.8	02.1	03.7	00.7	-	04.9	05.5	05.0	98	94	97	96	NNW	1	WSW	1	WSW	1
29	751.2	750.4	751.4	00.9	02.1	02.4	02.0	02.8	00.6	-	04.7	04.8	05.2	97	90	96	94	SSE	1	SSE	1	NNE	1
30	754.4	755.0	755.0	00.8	03.3	03.3	02.7	03.3	00.5	-	04.8	05.4	05.6	98	94	96	96	NE	1	SSE	1	ENE	1
31	754.4	753.5	753.2	02.0	06.7	07.1	05.7	07.1	01.7	-	05.2	05.9	06.3	98	80	82	87	SF	1	SE	1	NW	1
MES.	MRED.			753.2	752.9	753.3	01.1	03.2	02.3	02.2	03.8	00.6	-	04.6	05.0	04.9	92	86	90	89	1.2	1.4	1.2

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1	751.5	750.5	750.1	05.9	08.5	08.6	08.0	09.6	05.7	-	05.8	06.1	07.4	85	73	82	82	ENE	1	S	1	W	2
2	749.8	749.4	750.6	07.0	13.3	10.2	10.2	13.4	07.0	-	06.7	07.2	07.0	89	63	75	76	S	1	SW	3	WSW	2
3	749.5	746.8	745.0	06.7	11.3	09.0	09.0	11.3	06.7	-	05.7	05.8	07.2	77	57	84	73	ENE	2	ENE	2	NNE	2
4	742.4	741.2	742.2	06.8	07.4	05.7	06.4	09.0	05.7	-	06.7	07.4	06.1	91	96	88	92	W	1	S	1	ENE	2
5	742.3	740.5	739.1	04.6	07.8	06.3	06.2	07.9	04.5	-	05.8	06.6	06.0	90	84	85	86	SW	1	S	1	WSW	2
6	732.3	725.2	719.8	06.8	11.4	10.7	09.9	11.5	05.4	-	05.5	05.9	06.6	74	58	69	67	WSW	2	SSW	4	S	2
7	724.5	727.2	731.1	01.0	07.1	05.1	04.6	10.7	01.0	-	04.6	05.8	03.8	95	75	67	79	W	2	WSW	2	NW	2
8	739.2	744.0	748.1	02.9	09.4	04.7	05.4	09.4	02.6	-	03.5	03.0	02.4	63	35	37	45	NNW	2	WNW	2	N	2
9	748.0	747.6	748.9	02.9	11.1	07.4	07.2	11.8	02.6	-	03.1	03.1	04.4	55	31	58	48	WSW	2	W	3	WSW	3
10	749.0	749.9	749.8	08.5	13.4	05.8	10.4	13.5	05.7	-	05.2	05.8	05.7	63	50	63	59	WNW	3	WSW	2	W	3
11	747.6	744.4	742.9	04.3	14.9	10.0	05.6	14.9	04.1	-	05.2	06.0	05.6	84	47	61	64	WSW	2	WSW	5	SW	4
12	741.5	740.6	740.4	10.7	14.7	10.5	11.6	14.8	09.5	-	06.0	05.8	06.1	62	46	64	57	WSW	4	WSW	5	WSW	2
13	738.9	737.3	737.4	05.1	10.4	08.2	08.0	10.5	04.9	-	05.8	05.3	07.2	87	56	88	77	NNE	1	NE	2	S	1
14	738.0																						

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 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Isolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	5	10*	10*	10*	10*	10.0	00.0	05.1	.	=n-n, *tr-6° 13° 15°, *6° 13° 15° n; █	
2	4	10*	10*	10	10.0	00.0	15.6	.	=n-n, *tr-7° 17°, █		
3	1	10	10	10	10.0	00.0	00.5	.	=n-8, 16° 7°, *tr-7°, 16-17; =8-16°		
4	4	10	10	10	10.0	00.0	00.2	.	=n-n		
5	5	10	10	10	10.0	00.0	02.1	.	=n-ni, *tr-6°, =0 10° 12°		
6	5	10*	10*	10*	10.0	00.0	00.4	.	*n-n, =n-8°, =8° n		
7	6	10	10	10	10.0	00.0	09.5	.	=n-n		
8	3	10	10	10	10.0	00.0	00.0	.	=n-n, *tr-7°, 8° 10°, =12° 14°		
9	6	10	10	10	10.0	00.0	00.0	.	=n-n		
10	4	10*	10	10	10.0	00.0	00.0	.	=n-n, *tr-9°, =n-ni, =8° 9°, *tr-15°, 16°		
11	5	10	10	10	10.0	00.0	00.0	.	=n-n		
12	4	07	07	07	05.7	03.3	.	.	=n-n		
13	2	10	10	10	10.0	00.0	.	.	=n-14, *tr-9°, =14-n, *tr-19° n		
14	5	10	10	06	08.7	00.0	00.1	.	=n-n, *tr-14°, 14°, *tr-0° 15° -n		
15	5	10	10	10	10.0	00.1	.	.	=n-n, *tr-14°, 14°, *tr-0° 15° -n		
16	4	10*	10	10	10.0	00.0	02.5	.	=n-n, *tr-7°, 8°		
17	3	10	10	10	02	07.3	00.0	00.1	=n-7°, 14°, =14° n, *tr-0° 8° 14°		
18	4	09	09	03	07.0	01.0	06.6	.	=n-7°, 10°, =n-ni, =8° 10°		
19	5	10	10	10	10.0	00.0	00.5	.	=n-7°, 10°, =n-ni, =9° 11°		
20	6	10	01	00	03.7	05.6	02.0	.	=n-10°		
21	5	00	07	04	03.7	05.6	.	.	=0-1 n-12°, =12° n		
22	3	10	00	10	06.7	04.3	.	.	=2 n-9°, 16°, =19° n, =19° 16°		
23	3	10	01	08	06.3	02.5	.	.	=n-7°, 13°, =17° 13°		
24	2	10	10	10	10.0	00.0	.	.	=0-1 n-12°, =12° n		
25	3	10	05	10	09.7	00.0	.	.	=0-2 n-13°, 16°, =13° 16°, *tr-9°, 11°		
26	1	10	10	10	10.0	00.0	00.0	.	=+2 n-n, *tr-7°, 9°		
27	4	10	08	10	09.3	00.1	00.0	.	=+2 n-11°, 17°, =11° 17°, *tr-0° 12°, 13°		
28	3	10	10	10	10.0	00.0	00.1	.	=+2 n-n, *tr-7°, 13°		
29	3	10	10	10	10.0	00.0	00.0	.	*tr-n, rj, =0-1 n-14°, 20°, =14° 20°		
30	3	10	10	10	10.0	00.0	00.0	.	=0-1 n-14°, 20°, =17° n		
31	4	10	09	09	09.3	01.2	.	.	=2 n-10°, *tr-8°, =10° 11°, 16°, 18°, =11° 16°, 18° n		
MES. VR.ED.		09.5	08.6	08.7	08.9	23.7	46.5				

1	3	09	10	10	09.7	00.3	.	.	=n-10°, 13°, *tr-8°, 11°, =0 10°, 13°		
2	7	03	09	06	06.0	01.1	00.0	.	=n-9°, 17°, n		
3	7	09	10	10	09.7	01.0	.	.	=n-7°, 15°, =0-1 n-16°, 20°		
4	3	10	10	10	10.0	00.0	01.5	.	=n-8°, 13°, n, =0 8°, 13°, *tr-10°, n		
5	5	10	05	04	06.3	02.5	05.5	.	=n-n		
6	8	10*	09	10	09.7	01.1	00.0	.	*tr-0°, 2°, 4°, 8°, 10°, 12°, 14°, 16°, 18°		
7	9	10*	06	03	06.3	04.2	14.0	.	*tr-1°, 7°, 10°, 13°, 16°, 19°, 22°, 25°, 28°, 31°, =7°, 10°, 13°, 17°		
8	8	06	01	00	02.3	08.4	01.5	.	=n-11°, 14°, 17°, 20°, n		
9	8	09	08	01	06.0	04.4	.	.	*		
10	6	05	04	00	03.0	07.0	.	.	*		
11	8	00	01	00	00.3	08.4	.	.	=n-7°, Fsw 13-17		
12	8	00	01	00	00.3	09.0	.	.	Fsw 11-12		
13	6	02	10	10	07.3	01.6	.	.	=0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°		
14	5	10*	10*	10	10.0	00.0	01.0	.	*tr-0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°, =n-12°, 18°		
15	5	10*	10	10	10.0	00.2	07.4	.	=0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°, =n-10°, n		
16	4	10	10	10	10.0	00.0	.	.	=n-n, *tr-17°		
17	6	10	07	04	07.0	01.6	00.0	.	=n-n		
18	3	10	10	10	10.0	00.1	00.1	.	*tr-0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°, =n-13°, 18°		
19	7	10	05	00	06.3	01.3	00.0	.	*tr-0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°, =11°, 13°, 17°, 20°, 23°, 26°, 29°, 32°, 35°, 38°, 41°, 44°, 47°, 50°		
20	6	04	09	10	07.7	03.0	01.3	.	=0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°, =n-n, *tr-8°, n		
21	6	10	05	09	09.3	00.2	.	.	=n-n		
22	5	10	05	09	09.3	02.5	.	.	=n-n		
23	5	10	10	10	10.0	00.0	.	.	=n-n		
24	5	10	10*	10	10.0	00.0	00.0	.	=n-n, *tr-0°, 6°, n, FNE 7°, 8°, 19°, n		
25	5	09	09	10	09.3	00.5	01.4	.	=n-n, FNE n-7°, n		
26	6	10	10	10	10.0	00.0	.	.	=n-n, *tr-0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°, =16°, 17°, 18°, 19°, 20°, 21°, 22°, 23°, 24°, 25°, 26°, 27°, 28°, 29°, 30°, 31°, 32°, 33°, 34°, 35°, 36°, 37°, 38°, 39°, 40°, 41°, 42°, 43°, 44°, 45°, 46°, 47°, 48°, 49°, 50°		
27	6	10*	05	10	09.7	01.1	00.1	.	=n-n, *tr-0°, 7°, 14°, 21°, 28°, 35°, 42°, 49°		
28	8	02	03	10	05.0	07.0	00.0	.	=n-n		
MES. VR.ED.		07.9	07.8	07.0	07.5	66.5	33.8				

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 $\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost v%			Pravac i jačina vetro D, f (0-12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	750.3	748.6	747.3	00.5	05.2	02.6	02.8	05.3	00.5	-	03.0	03.2	03.2	64	48	58	57	ENE 1	SSE 2	NE 1	
2	744.8	744.3	745.1	01.7	03.4	05.1	03.8	05.1	01.4	-	03.6	04.0	04.6	69	68	69	69	ENE 2	NNE 2	NNE 3	
3	747.6	749.1	750.5	01.1	04.7	03.0	03.0	05.1	01.1	-	03.3	03.7	03.8	65	57	67	63	ENE 2	SE 3	NNE 1	
4	749.6	748.4	745.9	02.6	03.4	06.0	04.5	06.0	01.8	-	04.0	04.6	06.4	72	79	91	81	ENE 2	ENE 2	NE 3	
5	743.4	744.4	744.8	06.0	07.4	06.1	06.4	07.5	05.2	-	06.1	06.6	06.3	87	86	88	87	NNE 3	NE 2	ENE 2	
6	745.0	746.8	749.1	03.2	03.5	04.0	03.7	06.1	02.5	-	04.8	05.1	05.0	84	86	83	84	ENE 3	NNE 3	NNE 3	
7	750.2	751.1	752.0	03.1	04.9	02.9	03.4	04.9	02.9	-	04.4	04.6	04.8	75	71	85	77	NE 3	NE 2	ENE 2	
8	751.4	751.2	751.7	01.7	03.0	02.5	02.4	03.2	01.5	-	04.8	04.5	04.6	92	80	85	86	SSE 2	NNE 3	NNE 2	
9	751.4	752.0	753.6	01.3	02.5	01.9	01.9	03.2	01.3	-	04.5	04.2	04.2	90	75	81	82	NE 2	NE 2	NE 2	
10	752.9	753.0	754.0	01.2	03.0	02.5	02.3	03.1	01.2	-	04.6	04.6	04.4	92	81	79	84	ENE 1	ENE 2	NE 2	
11	754.6	755.8	757.1	02.4	04.6	03.7	03.6	04.9	02.2	-	04.6	04.8	04.5	85	74	75	78	NE 2	ESE 2	NE 1	
12	757.2	756.1	754.4	02.4	05.6	04.6	04.3	05.6	02.4	-	04.7	04.3	03.9	87	63	61	70	ENE 1	E 2	N 1	
13	751.4	749.0	748.0	03.4	08.1	05.2	05.5	08.7	03.4	-	04.9	04.4	04.2	82	54	64	67	NE 1	S 2	NNE 1	
14	745.8	743.4	742.1	00.4	11.0	08.2	07.0	11.0	00.4	-	04.2	05.3	05.1	89	54	62	68	N 1	ESE 2	NE 2	
15	741.6	741.6	742.3	07.2	10.8	08.0	08.5	10.8	06.7	-	04.4	06.1	05.1	57	63	63	61	NNE 2	ENE 1	ENE 1	
16	741.8	739.6	740.5	04.8	12.2	10.4	09.4	13.1	04.2	-	04.5	04.9	04.9	70	46	52	56	NE 1	WSW 2	WSW 1	
17	741.6	742.6	743.8	05.2	14.5	12.8	11.3	16.0	04.9	-	04.3	05.2	06.0	65	42	54	54	SSW 1	WSW 3	WSW 2	
18	744.8	743.8	744.2	11.2	18.3	13.7	14.2	18.3	07.4	-	05.1	06.0	06.6	51	38	56	48	NW 3	WSW 4	W 4	
19	745.8	746.3	748.4	13.8	20.1	14.2	15.6	20.1	12.9	-	07.0	07.0	06.8	59	40	56	52	W 4	W 4	W 3	
20	749.6	749.4	749.8	10.2	19.2	16.0	15.4	19.9	10.1	-	07.2	07.9	07.9	77	47	58	61	W 2	SSW 3	NW 2	
21	751.5	750.5	751.1	08.8	21.9	19.1	17.2	22.5	08.8	-	07.0	06.2	05.8	83	31	35	50	W 1	E 2	NE 2	
22	751.3	749.5	747.8	10.2	22.7	19.2	17.8	23.1	10.2	-	05.7	07.2	06.9	61	35	41	46	N 2	E 2	N 2	
23	747.2	747.5	748.9	13.6	19.9	15.6	16.2	20.2	11.7	-	05.7	06.6	06.5	49	38	49	45	N 1	WSW 2	W 2	
24	750.7	749.6	748.9	09.1	21.2	18.1	16.6	21.4	09.1	-	06.8	06.4	06.6	78	34	42	51	SSE 1	SSE 2	NNE 3	
25	749.0	749.3	749.7	13.1	15.9	13.1	13.8	18.1	13.1	-	07.2	08.3	07.2	65	61	64	63	NE 3	ENE 2	NNE 1	
26	749.7	747.3	746.1	08.0	17.7	15.4	14.1	18.6	07.7	-	06.7	07.5	07.4	83	50	57	63	NE 1	ESE 2	NNF 2	
27	744.8	744.3	744.8	11.0	19.4	14.0	14.6	19.8	10.3	-	05.6	08.5	07.6	77	50	67	65	E 1	SSW 1	WW 2	
28	746.2	746.0	747.1	10.3	19.5	13.2	14.0	19.5	10.0	-	07.7	07.4	09.0	82	44	79	68	ENE 1	ESE 2	NNE 2	
29	748.7	748.3	749.3	08.9	19.1	16.0	15.0	19.6	08.3	-	07.5	08.0	07.5	89	48	55	64	ENE 1	SE 2	NNE 2	
30	751.2	750.9	751.4	09.5	14.3	11.5	11.7	16.0	09.5	-	04.8	05.7	05.3	54	47	52	51	ENE 2	E 2	NNE 2	
31	750.9	749.3	749.0	07.3	12.6	09.8	09.9	14.0	06.9	-	05.2	04.9	05.1	68	45	56	56	E 1	F 1	ENE 2	
MES.	VRED.	748.4	748.0	748.3	06.2	11.9	09.6	09.4	12.6	05.8	-	05.3	05.7	05.7	74	56	64	65	1.7	2.2	2.0

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1	747.8	747.6	748.7	08.2	10.9	08.5	09.0	11.0	07.4	-	05.6	05.9	05.8	65	60	69	66	ENE 1	ENE 2	ENE 2
2	749.2	750.2	751.7	08.1	14.0	10.3	10.7	14.1	07.9	-	05.4	05.7	05.7	66	47	60	58	ENE 2	ESE 2	NNE 2
3	752.3	751.3	751.4	05.8	15.3	10.6	10.6	15.3	05.7	-	05.0	04.3	04.7	72	33	49	51	ESE 1	ESE 3	NNE 2
4	750.3	748.4	747.2	05.7	16.2	12.1	11.5	16.7	04.9	-	04.5	03.5	03.3	66	25	31	41	SE 1	ENE 2	NNE 2
5	746.8	746.8	748.1	06.4	16.8	13.4	12.5	17.1	06.2	-	04.6	04.0	03.9	64	28	34	42	NNE 1	E 2	NE 3
6	749.3	748.3	749.1	10.9	17.5	13.3	13.8	17.7	09.4	-	04.4	04.4	04.0	45	29	35	36	NE 2	ESE 3	NNE 2
7	749.3	748.3	748.2	07.9	15.7	14.1	13.0	17.0	07.5	-	05.2	05.2	05.7	64	39	47	50	- 0	NNE 2	N 2
8	748.6	747.3	749.4	11.4	16.1	12.6	13.2	17.0	10.3	-	04.9	04.1	03.9	48	30	36	38	NNE 2	NNE 3	NNE 2
9	749.5	748.1	747.3	09.1	17.9	14.0	13.8	18.6	08.2	-	04.6	04.8	05.0	53	31	42	42	NW 1	S 2	NF 1
10	746.2	742.9	742.1	08.0	20.2	14.4	14.2	20.8	06.7	-	05.4	04.3	05.3	67	24	43	45	NNW 1	SSW 3	WSW 2
11	740.3	738.9	730.2	09.1	14.5	09.5	10.8	14.7	08.7	-	06.0	06.5	07.7	69	52	85	69	W 1	S 2	NNE 2
12	737.2	737.0	736.1	09.7	16.2	12.0	12.5	16.5	09.2	-	08.2	09.6	09.9	90	66	94	84	SSE 1	SSE 2	WW 2
13	739.8	741.4	742.6	12.0	12.4	11.3	11.8	13.6	11.3	-	09.0	06.9	04.4	86	82	44	71	NNW 1	N 2	NE 3
14	743.4	741.7	741.1	04.0	06.8	04.3	04.8	11.3	03.1	-	04.8	05.0	05.2	78	67	84	76	ENE 2	N 1	WSW 2
15	740.7	738.5	740.4	07.8	12.2	08.4	09.2	12.8	04.3	-	02.6	02.5	03.1	32	23	37	31	NNE 2	NE 3	NE 1
16	741.5	741.5	743.7	06.6	11.3	08.1	08.5	11.5	06.2	-	03.5	02.7	03.1	46	27	38	37	NAT 3	NE 3	NNE 3
17	744.6	743.1	744.2	04.0	10.4	09.4	08.3	10.8	03.6	-	04.3	02.9	03.1	70	31	35	45	NNE 3	NE 4	NNF 4

BR. ST. 57

 $H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Intencija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6	05	040	05	07.3	C4.5	.	.	.	= n-n	
2	6	10	10*	10	10.0	CC.0	.	.	.	= n-n, * tr n-p, tr 17° 17° 17°	
3	6	10	05	10	09.7	C1.3	00.0	.	.	= n-n, * tr 19° 20°	
4	6	10	10**	10**	10.0	CC.0	00.0	.	.	= n-n, * 8° 10°, * 13° 13°	
5	6	10*	10*	10*	10.0	00.0	07.7	.	.	= n-n, * n-n	
6	5	10*	10*	10*	10.0	CC.0	11.7	.	.	= n-n, * tr 15° 18° 18° 18° 18°	
7	5	10**	10	10	10.0	00.0	09.3	.	.	= n-n, * tr 17° 17° 17° 17° 17°	
8	5	10**	10	10	10.0	CC.0	CC.6	.	.	= n-n, * tr n-j 8° 11° 13° 13°	
9	6	10*	10	10	10.0	00.0	01.3	.	.	= n-n, * 8° 10°, * 8° 10°, * 8° 10°	
10	6	10*	10*	10*	10.0	CC.0	CC.3	.	.	= n-n, * tr 6° 17° 17° 17° 17°	
11	6	10	10	10	10.0	00.0	00.6	.	.	= n-n, * tr n-j, 8° 15° 9°	
12	5	10	10	10	10.0	CC.0	CC.0	.	.	= n-n	
13	6	09	030	00	04.0	05.6	.	.	.	= n-n	
14	5	00=	000	00	03.0	03.0	08.3	.	.	= n-n, * 10° = 10° n	
15	5	02=	09	04	05.0	CC.0	CC.0	.	.	= n-n, * 8° = 8° n	
16	6	000	010	08	C3.0	C7.1	.	.	.	= n-n	
17	6	C9	080	06	07.7	03.1	.	.	.	= n-n	
18	8	C30	10	C8	07.0	C4.2	.	.	.	= n-10°	
19	7	09	040	00	04.3	C5.4	.	.	.	= w 5-n	
20	7	10	C80	00	06.0	C7.2	.	.	.	= n-8°	
21	8	000	000	00	00.0	10.2	.	.	.	= n-9°	
22	7	000	000	00	00.0	10.2	.	.	.	= n-12° 17°	
23	6	10	10	10	10.0	CC.0	C2.5	.	.	= n-14°	
24	8	C70	080	C7	C7.3	C9.8	.	.	.	= n-n, -8° = 7° 9°	
25	5	C9	090	00	06.0	CC.0	06.3	.	.	= n-n	
26	5	C5	040	C2	C3.7	C7.2	.	.	.	= n-n	
27	6	09=	040	00	06.0	04.1	.	.	.	= n-n, * tr 17° 17° 17°	
28	6	08	C30	10	07.0	05.0	.	.	.	= n-11° 17° 17°	
29	6	C20	070	07	05.3	09.0	CC.7	.	.	= n-14° 17°	
30	6	09	10	10	09.7	00.0	.	.	.	= n-n	
31	6	10	070	00	0F.7	C1.6	.	.	.	= n-n	
MES.	VRED.	07.4	07.2	06.7	07.1	11C.8	32.2				

1	5	10	10	10	10.0	00.0	.	.	.	= n-n	
2	6	10	C50	C1	C5.3	C2.5	.	.	.	= n-11°	
3	7	000	010	00	CC.3	10.1	.	.	.	= n-9° 18°	
4	7	000	000	00	00.0	11.0	.	.	.	= n-11° 18°	
5	8	010	080	C4	04.3	10.5	.	.	.	= n-11°	
6	8	070	040	C0	03.7	C5.1	.	.	.	= n-11° 18°	
7	6	030	10	10	07.7	04.5	.	.	.	= n-p, * tr 19° 20°	
8	7	010	060	00	C2.3	11.0	00.0	.	.	= 19-n	
9	7	000	000	00	CC.0	11.6	.	.	.	= n-8°	
10	7	000	060	04	03.3	09.5	.	.	.	= n-8°	
11	8	10	10	10	10.0	CC.0	.	.	.	= n-12° 13° 13° 13° 13°	
12	6	10*	C9	10*	05.7	00.6	01.7	.	.	= n-13° 13° 13° 13° 13°	
13	5	09	10	10	05.7	00.0	05.8	.	.	= n-n, * tr 17° 17° 17° 17° 17°	
14	6	10*	10	10	10.0	CC.0	04.5	.	.	= n-n, * tr n-8°, * 6° 8°, * 8° 8° 9°	
15	8	10	C30	C8	07.0	06.4	CC.4	.	.	.	
16	7	10	080	05	07.7	C5.7	.	.	.	= n-12°	
17	7	10*	10	10	10.0	C3.4	CC.0	.	.	= n-9° 12° 12° 12° 12°	
18	7	10	10	10	10.0	01.9	00.0	.	.	= n-9° 18° 18° 18° 18°	
19	7	10	050	09	09.3	07.6	.	.	.	= n-8° 8° 10°	
20	8	000	080	06	04.7	10.0	
21	6	10	10	10	10.0	02.0	.	.	.	= n-n, * 19° 20°	
22	7	090	090	10	09.3	04.4	00.1	.	.	= n-12° 12° 12° 12° 12°	
23	6	010	060	03	03.3	C8.5	00.0	.	.	= n-9°	
24	7	000	10	10*	06.7	06.5	.	.	.	= n-7°	
25	5	10*	10*	10	10.0	CC.0	01.2	.	.	= n-n, * 6° 7°	
26	7	10*	080	09	09.0	02.4	12.9	.	.	= n-11°, * tr n-10°, * 15° 15° 15° 15°	
27	8	070	09	10	08.7	06.5	C2.5	.	.	= n-8°, * tr 13° 13°	
28	6	09	10*	10*	09.7	00.5	00.3	.	.	= n-n, * 13° 13°	
29	8	050	09	08	07.3	C5.7	C2.6	.	.	= n-14°, * 14°, * 15° 15° 15° 15°	
30	6	060	10	10*	08.7	01.2	CC.1	.	.	= n-j, * 13° 13°, * 17° 17° 17° 17°, * 20° 20°	
MES.	VRED.	06.3	07.6	06.9	06.9	154.3	36.5				

1974 MAJ

ZAGREB GRIC

 $\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1\text{h }04\text{ min.}$

BR. ST. 57

E D	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare φ mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21
1	729.7	730.8	733.7	11.0	12.6	12.2	12.0	15.9	10.8	-	09.3	10.0	09.2	95	91	86	91	FSE 1	EKE 1	WW 1
2	735.9	737.5	739.6	12.8	18.3	13.4	14.5	19.0	12.0	-	06.6	07.3	08.9	59	46	77	61	NW 2	SSE 2	NNE 2
3	741.3	740.1	740.7	12.5	18.9	12.9	14.3	19.5	12.2	-	08.5	07.6	06.5	79	50	58	62	NW 1	SSW 3	SSW 1
4	738.7	736.3	737.0	10.8	12.1	10.7	11.1	12.9	09.6	-	08.5	09.9	08.3	88	93	86	89	ENE 1	NE 3	SW 1
5	736.5	737.0	738.1	09.2	12.9	11.7	11.4	13.2	09.1	-	08.4	09.5	08.7	96	85	91	91	WSW 2	WW 1	W 2
6	738.3	741.3	743.7	11.0	14.0	10.5	11.5	14.2	10.2	-	08.3	09.6	09.2	84	80	96	87	WW 2	SSW 2	NNW 1
7	746.0	746.6	747.5	10.5	12.8	12.2	11.9	13.4	10.0	-	08.9	09.2	09.2	93	83	86	87	ENE 1	SSW 2	WSW 1
8	750.0	749.2	747.9	08.7	13.4	11.6	11.3	14.2	08.2	-	07.5	07.5	08.3	88	68	78	78	ENE 2	SSE 2	N 2
9	747.2	746.2	746.1	12.1	15.2	10.9	12.3	16.4	10.2	-	04.3	04.7	05.7	51	41	56	49	N 2	N 2	N 2
10	746.2	744.1	744.2	08.9	19.4	14.7	14.4	19.7	07.3	-	08.0	05.1	05.7	75	39	58	57	WSW 1	SSW 2	WSW 2
11	745.5	745.6	745.7	11.3	18.9	16.0	15.6	20.0	10.2	-	05.5	07.4	07.1	64	44	56	55	SW 1	SW 3	WSW 1
12	747.8	748.3	751.0	12.8	19.2	14.4	15.2	20.5	11.9	-	07.6	07.0	09.5	75	43	70	63	WW 2	ESE 2	NNE 1
13	752.7	751.7	751.4	13.4	20.3	17.2	17.0	21.1	10.2	-	08.4	07.9	07.4	76	47	60	61	SW 1	SE 2	NNE 2
14	750.1	747.1	750.5	13.3	23.4	10.8	14.6	23.9	10.8	-	09.5	09.7	08.7	83	45	90	73	ENE 1	SSE 2	ESE 2
15	749.3	746.7	746.2	10.9	16.9	10.7	12.3	17.4	09.4	-	08.3	06.8	08.9	84	47	92	74	WW 2	NNW 1	SSE 2
16	745.3	744.2	745.4	11.7	16.9	13.8	14.0	17.6	09.6	-	08.4	06.8	08.0	81	47	68	65	WSW 1	ESE 2	NE 2
17	746.5	748.4	750.9	11.4	16.7	12.6	13.3	18.1	10.2	-	07.2	07.6	07.7	71	53	70	65	ENE 1	ESE 3	NNE 2
18	751.5	751.6	752.2	13.1	19.1	14.8	15.4	19.5	09.6	-	08.1	08.7	09.7	71	52	77	67	WW 2	NE 3	NNE 2
19	751.8	750.5	750.0	14.6	21.1	17.7	17.8	22.0	13.5	-	07.9	07.8	08.0	63	41	52	52	WSW 1	NNE 3	N 2
20	749.4	748.1	747.8	16.5	24.6	18.4	19.5	25.2	13.4	-	08.9	09.0	10.4	63	39	65	56	WSW 1	ESE 2	NNE 1
21	749.3	749.3	749.4	16.9	21.0	17.5	18.2	22.7	13.7	-	09.9	10.1	11.6	68	54	77	66	NW 2	ENE 1	NNE 2
22	746.0	739.0	740.7	16.0	24.6	13.0	16.6	25.6	13.0	-	10.5	11.6	10.5	77	50	93	73	SE 1	WSW 3	S 1
23	741.4	739.6	740.4	13.0	18.4	11.9	13.8	18.9	10.9	-	08.9	05.3	07.8	79	33	74	62	NW 2	NNW 3	NE 1
24	741.1	740.8	741.8	11.9	13.4	11.8	12.2	14.2	11.2	-	06.8	07.6	08.9	65	66	86	72	NE 2	NNE 1	NE 1
25	743.3	746.4	748.7	10.8	14.6	12.5	12.6	16.5	10.4	-	08.5	07.1	07.9	87	57	72	72	NW 1	NNW 2	NNW 1
MES.																				
MRED.	745.2	744.5	745.2	12.7	18.4	14.2	15.0	19.4	11.1	-	08.5	08.4	08.7	77	54	73	68	1.4	2.2	1.5

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ZAGREB GRIC

1	745.6	747.5	750.0	18.4	19.2	16.1	17.4	19.3	16.1	-	11.4	11.4	11.2	72	68	83	74	WSW 2	SSW 1	NW 2
2	752.7	753.4	754.7	14.9	21.3	17.1	17.6	22.0	14.3	-	10.2	08.4	08.0	80	44	55	60	WSW 1	ENE 3	NNE 1
3	754.7	753.3	752.1	15.2	22.3	18.1	18.4	23.5	12.2	-	08.2	10.1	12.7	63	50	66	60	SSW 1	S 2	N 1
4	751.9	750.9	749.8	15.6	26.0	21.5	21.2	27.1	13.0	-	08.9	10.4	11.0	76	41	57	58	SSW 1	SSE 2	NE 2
5	750.0	748.5	747.2	18.9	25.1	21.5	21.8	25.7	15.5	-	12.1	12.9	13.5	74	54	70	66	E 1	ESE 2	NE 2
6	745.5	744.7	746.3	19.4	25.4	18.4	20.4	25.9	17.2	-	13.0	11.2	11.6	77	46	73	65	SE 1	WSW 3	S 2
7	747.6	748.4	751.5	14.6	18.0	11.4	13.8	19.2	11.4	-	08.1	09.8	09.2	65	63	91	73	SSW 2	SSW 3	E 2
8	752.3	750.6	748.3	13.8	17.2	14.5	15.0	18.9	10.0	-	09.1	06.4	07.2	77	43	58	59	SSW 1	SSE 2	N 1
9	744.8	742.1	743.1	12.4	21.5	16.2	16.6	23.3	09.0	-	07.8	10.4	11.5	72	54	83	70	WSW 1	WSW 3	NNW 2
10	743.7	742.1	740.8	11.0	11.8	12.1	11.8	16.3	10.1	-	08.5	09.0	09.7	86	87	91	88	NNW 2	SF 2	NE 1
11	742.2	743.4	745.5	09.7	17.9	14.5	14.2	19.7	05.1	-	08.3	07.5	07.1	91	49	47	62	NNW 1	NW 3	NNE 2
12	744.2	742.4	742.9	10.7	19.0	13.9	14.4	19.7	08.3	-	07.1	05.6	06.8	73	34	47	51	W 2	NNW 3	NNE 2
13	740.2	739.8	740.9	10.5	16.6	13.7	13.6	17.1	08.8	-	06.8	06.4	08.7	71	46	74	64	WSW 1	WSW 3	NNE 1
14	742.1	742.1	744.3	13.0	22.2	17.5	17.6	22.7	11.4	-	09.1	08.6	10.4	81	43	69	64	WNW 2	WNW 2	NNW 2
15	746.7	745.1	745.9	15.8	21.3	17.1	17.8	22.5	13.3	-	10.5	11.1	10.3	76	58	70	69	S 1	WSW 2	W 2
16	745.5	744.8	744.9	17.1	23.2	19.2	19.7	24.4	14.0	-	09.8	10.0	10.5	67	47	63	59	WNW 2	ESE 2	NNE 2
17	744.7	743.4	744.4	17.1	25.2	18.7	19.9	25.7	14.1	-	11.0	11.5	11.5	75	48	71	65	SE 1	S 2	E 1
18	744.8	743.9	745.7	16.5	24.6	18.2	19.4	25.0	14.8	-	11.0	11.4	12.5	78	49	80	69	E 1	SSE 3	NNW 3
19	748.9	749.2	750.3	15.2	21.6	18.3	18.4	22.2	14.9	-	11.9	10.3	09.5	92	53	60	68	SSW 1	NE 2	NNE 1
20	750.7	749.5	748.9	15.6	22.6	17.8	18.4	23.2	13.1	-	09.2	08.4	08.9	69	41	58	56	WSW 1	E 2	NNE 2
21	749.3	749.6	748.5	15.6	20.0	15.8	16.8	20.0	13.8	-	10.8	10.4	09.4	81	59	70	70	SSW 1	SSW 2	NNE 1
22	748.3	747.5	747.3	13.6	20.9	17.6	17.4	22.5												

BR. ST. 57

$$H_s = 157 \text{ m} \quad H_b = 162.5 \text{ m} \quad h_t = 6.0 \text{ m} \quad h_r = 2.0 \text{ m}$$

Dan	Vlaknost 0-9	Oblačnost N (0-10)					Inzolačija broj soči	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	6	10•	10•	10•	10.0	00.0	41.5	.	.	$\bullet^{n-1} n-n = rj-n$
2	8	C9	09	10	09.3	02.6	31.0	.	.	$\bullet^{tr-0} 10^{25} 17^{00} i$
3	7	10	040	02	05.3	06.5	00.4	.	.	$= n-10 \bullet^{\nabla} n$
4	5	10•	10•	10	10.0	00.0	00.6	.	.	$= rj-6 \bullet^{tr-1} rj-15^{50} i \nabla 14^{40} 14^{50} R^{0-1} 14^{35} 15^{45} Fw 14^{40} 14^{50}$
5	6	10•	10•	10	10.0	00.0	36.5	.	.	$\bullet^{tr-2} n-22^{45} i = 930 h$
6	6	10	10•	10•	10.0	00.0	11.8	.	.	$\bullet^{tr-0} 9^{38} ni$
7	6	10	1C•	10•	10.0	00.1	10.8	.	.	$= n-15^{45} \bullet^{tr-0-1} n-rj, 8^{40} 16^{15} i, 20^{32} n$
8	6	10	10	10	10.0	02.3	03.5	.	.	$= n-n$
9	7	040	08	0C	C4.0	09.2	.	.	.	$= n-9^{45}$
10	8	010	060	06	02.3	09.4	.	.	.	$= n-9^{45}$
11	8	1C	050	08	05.0	C3.0	.	.	.	$= n-9^{20}, n$
12	8	060	08	07	07.0	06.1	00.4	.	.	$\bullet n$
13	8	000	08	0C	C2.7	C8.9	.	.	.	$= n-830 \bullet^{\nabla} n-a$
14	7	000	10	10•	06.7	07.4	.	.	.	$= n-10^{45} 19^{15} n-a \bullet^{\nabla} n-a \nabla' 17^{16} 18^{36} \bullet^{\nabla} 18^{35} n, F_{NE-NNE} 17^{06} 17^{35} 15^{0-1} K^{35}$
15	8	010	06	1C	06.7	C8.2	22.1	.	.	$\bullet^{tr-0-1} 13^{02}, 18^{32} \nabla 18^{30} 21^{20} n, 18^{0-1} 17^{30} 18^{30}, 26^{45} 63^{02} n$
16	7	060	08	09	07.7	06.8	C3.3	.	.	$= rj-7^{30}$
17	7	10	090	09	C5.3	C5.0	.	.	.	$= n-9^{30}$
18	6	09	10	1C	C5.7	03.5	.	.	.	$= n-7^{30} \bullet^{tr-0} 18^{36} 20^{07} i$
19	8	010	040	0C	C1.7	11.1	00.1	.	.	$= 7^{15} 10^{30}$
20	8	000	020	10	C4.0	12.3	.	.	.	$= n-9^{15} \bullet^{\nabla} n, R^2 n$
21	7	05	05	C5	C6.3	05.3	C4.0	.	.	$R n, \nabla n = n-10^{30} 19^{30}$
22	5	10	09	1C	0C.7	02.9	.	.	.	$= n-14^{50} \bullet^{tr-1} 16^{45} 19^{05} R^{+2} 16-19$
23	9	C10	09	1C	C6.7	07.8	07.0	.	.	$\nabla^{\nabla} n, 14^{34} 19^{30} i$
24	8	10	10•	10	10.0	0C.3	C0.1	.	.	$= n! 7^{30} 13^{45} n, \nabla 7^{02} \bullet^{tr-0} 13^{35} 15^{40}$
25	8	10•	060	00	05.3	06.7	02.7	.	.	$= n-10^{30} \bullet^{\nabla} rj-925 R^{+2} 709 730$
26	8	000	010	10	C3.7	13.3	C4.7	.	.	$= n-8^{45} \Delta^{\nabla} n-a$
27	8	000	010	01	0C.7	13.2	.	.	.	$= n-11^{30} \Delta^{\nabla} n-a$
28	7	C10	090	1C	C6.7	C7.5	.	.	.	$= n-9^{45} \bullet^{\nabla} 19-ni$
29	7	080	070	04	0C.3	C6.5	08.3	.	.	$= n-12^{15} \bullet^{\nabla} n-rj$
30	6	000	050	1C	C6.3	10.3	.	.	.	$= n-13^{45} 16-n$
31	7	060	10	C9	0P.0	05.4	.	.	.	$= n-12^{15} \bullet^{\nabla} 10^{32} 1145$

1	8	10	10	10	1C+0	00+6	.	.	$\equiv 8^{46} \cdot 10^{-30} \cdot t^{n-0-1} 7^{33} pi$
2	6	10	07	00	05.7	04.8	02.3	.	$\equiv 10^{30} n$
3	6	00 0	04 0	00	C1+3	11.1	.	.	$\equiv n-7, \frac{1}{n-a}$
4	6	00 0	01 0	00	CC+2	12.6	.	.	$\equiv n-10^{30} \Delta n-a$
5	6	02 0	02 0	01	02+0	09.1	.	.	$\equiv n-n^1$
6	8	09	09	10	09.3	03.7	.	.	$\equiv n-9^{30} \cdot t^{n-16/2} \cdot 16^{44} \cdot 19^{06} \cdot 19^{10}$
7	8	10 0	07 0	10 0	05+0	C3+4	C4+8	.	$\equiv n-10^{45} \cdot t^{n-0} \cdot n^{630} \cdot 10^{154} \cdot 18^{04} n$
8	8	08	10	10	C5+3	C2+3	C1+5	.	$\equiv n-7^{15} \cdot t^{n-14/2} \cdot 14^{44} \cdot 14^{17}$
9	8	00 0	07	10 0	05.7	04+3	00+0	.	$\equiv n-10 \cdot t^{n-1-2} \cdot 13^{45} \cdot 17^{30} n i$
10	6	10 0	10 0	10 0	00+1	14.9	.	.	$\equiv n-n^1 \cdot t^{n-0-1} \cdot n^{-10^{45}} \cdot 13-n$
11	7	10 0	06 0	01	05+3	08.1	26.4	.	$\equiv n-8^{15} \cdot t^{n-9/2} \cdot 9^{30} \cdot 12^{30} \cdot 13^{0} i$
12	8	09	03 0	01	C4+3	07.5	CC+4	.	$\equiv t^{n-8/2} \cdot 8^{30} \cdot t^{n-6} \cdot 12^{42} \cdot 12^{52} \cdot 17^{22} \cdot 17^{31} \cdot 16^{30} n$
13	8	10	1C	10 0	1C+0	00.2	00.2	.	$\equiv 16-n, t^{n-20/2} n$
14	7	09	06 0	04	C6+3	C5+3	C0+2	.	$\equiv t^{n-0} 15^{22} 15^{57}$
15	7	09	08 0	10	09+0	02.6	.	.	.
16	7	01 0	02 0	06	C3+0	09+6	00+1	.	$\nabla^{n-19^{10}} 19^{30}$
17	7	01 0	06 0	02	C3+0	C9+1	00+1	.	$\nabla^{n-15^{10}} = 17-n$
18	6	01 0	1C	10	07+0	C8+0	CC+2	.	$\equiv n-n^1 \cdot n-0^n \cdot n-a, R^{-2} M^{45} \cdot 16^{15}, \nabla^{+2} 15^{36} \cdot 16^{35}, t^{+2} n$
19	8	10 0	09	05	07.7	01.2	12.2	.	$\equiv n-11^{15} \cdot t^{n-7/2} = 17-n$
20	6	00 0	04 0	10	04+7	11.7	CC+0	.	$\equiv n-n^1$
21	5	10	06 0	06	07.3	03.9	00.0	.	$\equiv n-n^1 \cdot t^{n-6^{30}} 11^{45} i$
22	6	10	03 0	00	C4+3	C5+1	CC+3	.	$\equiv n-18^{40} \cdot t^{n-0-1} 7^{30} 9^{45} 17^{05} 18^{20} i$
23	6	00 0	04 0	10	04.7	10.0	02.5	.	$\equiv n-14^{40} \cdot t^{n-14^{10}} 14^{40} 14^{10} n$
24	7	39	10	10	09.7	C1+6	C1+0	.	$\equiv n-8 \cdot t^{n-10/2} D \cdot 18^{0-10} - 10^{45} 22^{40} n, \nabla^{n-10^{45}} 10^{20}$
25	7	05 0	01 0	05	C3+7	07.9	07.7	.	$\equiv n-9^{45} \cdot t^{n-6/2} n$
26	7	C6 0	05 0	10	C7+0	C7+6	.	.	$\equiv n-9^{30}$
27	7	10	09	03	07.3	05.6	.	.	$\equiv n-9^{30}$
28	7	06 0	08 0	10	CE+0	C4+6	.	.	$\equiv 0-1 n$
29	7	10	10 0	10 0	1C+0	00.9	00.9	.	$\bullet 0-8 M^{32} n, R^{n-1} 13^{34}, 16^{30} 16^{20}$
30	9	07	03	00	C2+3	12.2	50.5	.	.

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 $\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1\text{h}04\text{min}$.

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	747.5	746.6	746.4	18.2	26.5	22.5	22.5	28.4	15.0	-	10.9	13.1	13.9	65	49	68	62	WSW 1	SSW 2	WNW 1	
2	750.8	750.9	751.7	18.6	24.0	20.1	20.7	25.3	17.6	-	12.4	11.6	11.0	77	52	62	64	ESE 2	SE 1	NNE 2	
3	750.5	745.9	743.9	18.4	25.2	20.2	21.0	26.7	16.8	-	08.6	12.0	12.8	54	50	72	59	NE 1	SE 2	NNW 3	
4	747.4	748.0	748.6	17.8	22.2	19.8	19.9	22.6	16.4	-	12.7	11.8	09.9	83	59	57	66	WNW 1	ENE 3	ENE 3	
5	749.7	749.4	748.4	18.3	24.0	20.3	20.7	24.7	17.1	-	08.1	10.7	12.4	51	48	69	56	NE 2	S 2	NNE 2	
6	747.5	745.9	744.5	18.6	27.3	23.5	23.2	29.4	16.5	-	13.2	13.6	14.1	82	50	65	66	S 1	SSW 2	NW 2	
7	746.9	749.6	749.9	15.6	18.0	15.0	15.9	23.5	14.8	-	12.2	09.4	10.0	92	60	78	77	ENE 2	SE 3	NNE 2	
8	751.0	749.8	750.5	14.4	20.5	16.6	17.0	22.1	12.4	-	09.8	09.5	09.9	80	52	70	67	NW 1	SSE 2	NNW 1	
9	751.4	749.5	747.8	15.2	24.0	20.0	19.8	24.2	12.9	-	09.6	11.2	11.9	74	50	68	64	NW 1	WNW 2	NNE 2	
10	748.0	748.8	750.2	19.2	25.0	20.1	21.1	25.2	16.5	-	10.9	11.7	09.2	65	49	52	55	W 2	ENE 2	ENE 2	
11	750.5	748.9	748.5	18.6	26.5	22.2	22.4	27.3	17.4	-	10.2	13.0	14.4	63	50	71	61	NNE 1	SSE 2	N 1	
12	747.9	747.1	747.9	20.3	30.0	24.2	24.7	30.6	18.5	-	13.1	14.3	14.8	73	45	65	61	SW 2	WSW 3	WSW 1	
13	747.8	745.8	745.2	20.7	30.8	25.4	25.6	31.4	18.6	-	12.8	14.4	11.7	70	43	48	54	WSW 2	WSW 4	MNW 2	
14	745.8	744.9	745.7	21.0	31.5	24.1	25.2	32.0	16.7	-	12.7	11.8	12.4	68	34	55	52	SW 1	SW 4	W 2	
15	749.3	750.6	750.8	20.9	24.0	19.2	20.8	25.0	19.2	-	12.3	11.5	10.4	66	51	62	60	ENE 3	SM 3	SM 2	
16	749.3	747.1	745.1	17.5	27.4	24.3	23.4	28.9	15.7	-	11.7	14.8	16.2	78	54	71	68	E 1	SE 2	NNE 1	
17	743.5	741.9	741.3	21.3	31.5	24.0	25.2	32.6	19.2	-	14.1	13.7	12.3	74	39	55	56	ENE 1	S 2	W 2	
18	742.4	741.5	744.3	18.3	23.4	17.3	19.1	25.2	16.4	-	14.5	14.7	13.1	92	68	88	83	ESE 2	WNW 2	ENE 1	
19	745.7	746.0	747.0	15.2	17.9	17.3	16.9	20.0	14.6	-	11.4	09.6	08.3	88	62	56	69	N 2	E NE 2	ENE 2	
20	747.5	746.9	746.4	15.4	19.6	15.5	16.7	19.9	15.0	-	07.6	08.2	08.3	58	48	61	56	NNE 2	NNE 2	NNE 1	
21	745.5	745.3	746.8	13.8	19.4	17.3	17.0	20.9	13.0	-	09.7	08.4	08.7	83	50	59	64	W 1	NNE 2	N 1	
22	748.6	747.6	747.5	15.9	22.0	19.6	19.3	22.6	14.5	-	08.7	07.5	07.4	64	38	43	48	NW 2	NEE 3	N 2	
23	746.9	747.2	747.3	17.6	21.6	20.1	19.8	24.1	17.3	-	08.7	11.4	11.5	57	59	65	60	NW 3	WSW 2	NW 2	
24	747.3	745.9	744.4	20.9	28.0	21.6	23.0	28.8	15.7	-	10.6	11.7	11.2	57	41	58	52	WNW 2	SSW 3	WSW 3	
25	745.3	748.4	750.3	20.3	14.8	13.5	15.5	21.6	13.2	-	12.7	11.5	10.8	62	91	93	92	NNW 1	NW 2	NW 1	
MES.	WRED.	748.3	747.6	747.6	18.0	24.7	20.6	21.0	26.1	16.1	-	11.4	11.8	11.8	73	51	64	63	1.4	2.3	1.7

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1	747.3	746.6	746.5	21.9	29.6	25.2	25.5	30.2	15.8	-	15.6	10.4	16.6	79	51	67	66	ENE 1	WNW 1	NNE 2
2	747.4	747.0	746.7	21.9	29.7	25.7	25.8	30.1	20.6	-	15.8	17.2	16.9	82	55	68	68	ESE 1	ENE 1	NNE 2
3	747.7	748.2	748.6	23.1	30.4	26.4	26.6	31.2	21.4	-	17.0	17.6	18.6	80	54	72	69	WNW 1	E 2	NNE 2
4	748.5	747.4	746.8	23.2	32.6	26.3	27.1	33.2	21.8	-	17.1	17.3	14.9	80	47	58	62	- 0	SSW 2	NNW 2
5	748.7	748.2	747.9	22.4	29.2	24.7	25.2	30.0	19.5	-	13.4	14.3	14.0	66	47	60	58	ESE 1	ENE 2	NNE 2
6	752.8	753.6	752.7	18.7	18.6	17.0	17.8	24.7	17.0	-	11.0	10.9	10.5	68	54	72	69	ENE 2	ENF 1	- 0
7	751.2	749.0	747.4	16.1	24.3	19.4	19.8	24.3	13.9	-	11.0	10.1	10.5	80	44	62	62	NE 1	SSE 1	NNE 2
8	745.0	741.8	740.9	16.5	26.4	22.4	21.9	27.4	14.7	-	10.8	12.8	15.9	77	50	78	68	E 1	SE 2	NNE 1
9	743.4	743.7	746.2	17.7	22.6	19.3	19.7	24.1	16.7	-	13.2	12.1	11.8	87	59	71	72	ENE 1	SSE 2	NE 2
10	747.5	744.9	743.3	15.7	25.2	20.8	20.6	25.6	14.8	-	12.4	12.0	12.0	93	50	65	69	ESE 1	SE 2	NNE 2
11	742.5	744.0	745.6	14.7	14.2	13.4	13.9	20.8	12.1	-	11.5	10.3	09.6	92	85	83	87	ENE 2	NW 2	NNW 2
12	746.7	747.4	749.0	15.5	22.9	16.6	17.9	23.7	12.0	-	09.6	07.4	09.2	73	35	65	58	NW 2	WSW 2	ENE 1
13	751.1	750.7	751.0	14.4	24.0	19.5	19.4	25.2	11.3	-	09.4	10.3	10.3	77	46	68	64	E 1	S 2	NNE 1
14	751.7	752.1	752.4	15.5	27.4	22.4	21.9	28.0	14.2	-	11.8	14.5	15.4	89	53	76	73	E 1	SSE 2	NNE 1
15	752.9	753.2	753.4	19.0	30.2	25.5	25.0	30.4	17.6	-	14.5	17.4	17.1	88	54	70	71	SSE 1	SE 1	N 1
16	753.1	752.0	751.4	21.7	31.7	26.5	26.6	32.1	20.1	-	16.0	16.4	17.7	82	47	68	66	SE 1	SSW 2	NNE 2
17	751.0	750.0	749.5	22.3	31.5	24.7	25.8	31.7	21.1	-	17.4	17.3	15.6	86	50	67	68	SSE 1	SSW 2	NNE 1
18	749.5	748.4	747.5	20.9	30.2	26.1	25.8	30.5	19.8	-	15.4	16.8	16.2	83	52	64	66	- 0	SE 2	NNE 2
19	748.6	748.5	749.3	21.7	31.5	26.5	26.8	31.5	20.3	-	15.4	14.5	14.9	79	44	56	60	NNW 1	E 2	NNW 2
20	750.3	749.5	749.3	21.4	30.4	26.7	26.3	30.6	20.7	-	14.9	16.9	15.8	78	52	60	63	S 1	ENE 3	NNE 2
21	749.4	748.2	747.3	22.7	29.4	24.8	25.4	29.5	21.6	-	16.8	17.2	18.8	81	56	80	72	SSE 1	ESE 2	NNE 1
22	749.0	747.5	747.3	20.2	23.2	21.2	21.4	26.0	18.5	-	14.9	14.5	15.1	84	68	80	77	WNW 1	S 2	NNE 2
23	7																			

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$$H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Isolacija broj sati	Padavine R mm	Snežni pokriven h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	070	020	00	03.0	14.3	.	.	= n-7 ³⁰	
2	7	10	090	01	06.7	06.5	.	.		
3	7	000	010	10.	03.7	11.8	.	.	•° 20 ³⁰ 21 ³⁰ 22, F-E 20 ⁴⁵ 21 ³⁰	•
4	8	040	07	08	06.3	06.4	01.6	.		
5	8	010	010	00	00.7	12.6	.	.	= n-8 ¹⁵	
6	8	000	030	07	03.3	11.5	.	.	= n-9 ⁴⁵ △° n-a, •'n, 18° 17 ⁴⁵ 23 ⁰⁰	
7	6	10.	10	03	07.7	04.7	18.4	.	•'n-9 ⁰⁰ 18 ³⁰ -n	
8	7	040	060	06	05.3	08.1	03.3	.	= n-10 ³⁰	
9	7	010	09	10	06.7	07.0	.	.	= n-10 ⁴⁵ △° n-a	
10	8	09	09	10	05.3	03.8	.	.	= n-10 ³⁰ △°-1 14 ²⁰ 14 ³⁰	
11	6	10	020	04	05.3	06.2	00.0	.	= n-n, •+6 ³⁰ 6 ⁴⁵	
12	6	010	060	00	02.3	12.3	.	.	= n-n △'n-a	
13	8	000	000	00	00.0	13.6	.	.	= n-16 ⁵⁰ △'n-a	
14	8	000	000	00	00.0	13.4	.	.	= n-8 ⁰⁰ △'n-a	
15	8	010	060	05	04.0	10.7	.	.		
16	7	000	000	04	01.3	11.5	.	.	= n-8 ³⁰ △'n-a	
17	8	020	010	08	03.7	12.4	.	.	= n-16 ⁴⁵ △'n-a	
18	6	10-R	060	10	08.7	03.5	01.8	.	= n-13 ¹⁵ △'n-a	
19	8	10.	10	10	10.0	00.2	15.3	.	•'n-8 ³⁰ / △'rj-5 ⁴⁵ , n; ▽ ⁰⁻² 5 ⁴⁵ 7 ⁴⁵ , 15 ⁴⁵ 17 ⁰⁰ ; 18 ⁴⁵ 5 ⁴⁵ 7 ³⁰ , 15-17, ▽ ¹ 15 ⁴⁵	
20	6	C9	07	06	07.3	05.0	00.2	.	= n-n	
21	6	10	09	10	09.7	03.8	00.2	.	•+n _i = 7 ³⁰ 18	
22	7	1C	05	08	05.0	06.2	.	.		
23	7	1C	08	04	07.3	02.0	.	.		
24	7	C10	09	10	06.7	11.1	.	.		
25	7	10	10.	10.	10.0	00.0	.	.	•-19 ⁵⁵ ni	
26	7	070	04	00	03.7	12.1	11.0	.	•°n = n-8 ³⁰	
27	6	000	000	00	00.0	13.3	.	.	= h-n	
28	7	000	010	00	00.3	12.5	.	.	= n-10 ³⁰	
29	7	000	000	00	00.0	13.2	.	.	= n-10 ³⁰ △'n-a	
30	7	000	000	00	00.0	12.7	.	.	= n-11 ⁴⁵ △'n-a	
31	7	010	040	00	01.7	11.6	.	.	= n-10 ³⁰ 17-n	
MES. VRED.		04.4	04.8	04.6	04.6	274.E	51.E			

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1	6	000	050	02	C2.3	11.6	.	.	= n-n, △°n-a
2	6	000	010	00	CC.3	11.5	.	.	= n-n, △°n-a
3	6	000	020	00	CC.7	10.1	.	.	= n-n, △°n-a
4	6	000	010	00	CC.3	12.1	.	.	= n-15° ³⁰ △°n-a
5	7	010	010	00	00.7	12.2	.	.	= n-7° ³⁰
6	7	10	10	00	06.7	01.0	.	.	
7	5	000	050	00	01.7	11.6	.	.	= n-15° ³⁰
8	6	000	05	09	04.7	10.0	.	.	= n-n
9	8	09	060	01	05.3	06.3	03.6	.	R°-10° ²⁵ , 17°-18° ³² , 9° ²⁷
10	8	10	C60	10	08.7	07.9	.	.	= n-11° ²⁵ , 17° ¹⁵ , n, 22-n
11	7	100R	100	C1	07.0	C1.5	06.8	.	= nj-12° ¹⁵ , 10°-17°, rj-15°, R°-16° ⁵⁰ , 10° ²² , 16° ¹⁵ , n
12	9	08	04	C1	C4.3	11.0	15.0	.	= 8-n
13	9	030	070	03	04.3	08.6	.	.	= n-17° ³⁰
14	7	000	020	C2	C1.3	12.8	.	.	= n-9° ³⁰
15	6	020	020	01	C1.7	11.7	.	.	= n-n
16	6	000	010	00	CC.3	12.5	.	.	= n-13° ¹⁵
17	6	000	000	00	00.0	12.5	.	.	= n-14° ³⁰ , 18° ¹⁵ , n
18	6	000	000	01	00.3	12.2	.	.	= n-n
19	5	000	010	00	00.3	11.8	.	.	= n-n, △'n-8
20	6	000	010	09	03.3	10.8	.	.	= n-n, R°w kv-n
21	5	000	010	00	00.3	09.7	.	.	= n-n, △'n-a, 8°-21° ⁵⁵ , n, R°-12° ⁴⁵ , 22° ²⁵ , 22° ³⁵ , F _{NNE-EVE} , 22° ³⁰ -23° ³⁵
22	8	08	10	04	07.3	06.3	47° ³	.	= n-7° ¹⁵ , 17° ²⁵ , n, 18°-22° ⁴⁵ , 14° ⁵⁰ , 24° ³² , 23° ⁵⁹ , 13° ⁵² , 14° ⁴³ , 18°-19°, 14° ⁵⁰ , 22° ²⁵
23	7	070	050	100R	07.3	08.4	09° ²	.	= n-14° ⁴⁵ , 17° ¹⁵ , n, 16°-19°, 20° ¹⁰ , 17° ¹⁵ , 20° ¹⁰ , F _{S-W-NW} , 20° ¹⁰ , 20° ³⁵ , R _{20°} , [20° ¹⁵ , 5° ²⁰ , 20° ³⁵]
24	6	10	090	10	09.7	03.1	15.4	.	= n-n, △'6° ³⁰
25	5	10	10	10	10.0	00.4	00.0	.	= n-n, 10°-12° ³⁰ , 14° ³⁰ , 19° ⁰⁵ , 21° ³⁰ , n, 8°-21° ²⁵ , 15° ³⁵ , 17° ²⁵ , 18° ⁴⁵ , R°-15°, 15° ³⁰ , L[21° ⁴⁵ , n]
26	6	10	09	08	C6.0	C1.6	05.9	.	= n-n
27	6	10	060	09	08.3	04.5	.	.	= n-n, △'2°n-a, 6°-19° ⁵⁵ , 21° ⁴⁵ , R°-21° ⁴⁵ , n, 8°-22° ²⁰ , n
28	5	100	10	08	09.3	00.2	09.7	.	= n-n, △'15° ¹⁵ , n-d ¹⁵ , 17°-17° ⁴⁵
29	5	000	020	01	01.0	10.4	04.8	.	= n-15° ¹⁵
30	7	010	020	00	01.0	10.6	.	.	= n-14° ¹⁵ , △'n-a
31	7	000	010	07	02.7	11.6	.	.	= n-10° ¹⁵

1974. SEPTEMBAR

ZAGREB GRČ

 $\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina vetroa D, I (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	746.6	746.5	746.2	17.7	24.3	20.3	20.6	24.4	17.2	-	13.9	13.2	14.3	91	58	80	76	SSW 1	SSW 2	NNE 2			
2	745.5	745.5	746.6	17.2	26.1	20.8	21.2	26.4	16.2	-	13.2	13.5	12.4	90	55	67	71	WSW 1	SSW 2	NW 1			
3	745.5	745.5	745.7	17.7	27.3	21.5	22.0	27.3	16.6	-	11.9	14.7	14.1	78	54	73	68	WNW 1	SSW 4	W 2			
4	745.2	746.6	750.8	19.0	19.0	13.9	16.4	21.5	13.9	-	15.4	11.1	11.2	93	67	94	85	NNW 1	NE 3	NNW 1			
5	752.2	750.6	749.0	12.1	20.6	16.4	16.4	21.1	10.5	-	05.8	10.0	05.8	92	55	70	72	W 1	S 2	NNE 1			
6	745.8	742.3	740.0	13.3	23.3	20.1	19.2	23.9	12.4	-	09.9	12.9	13.1	88	60	74	74	NF 1	SSE 2	NNF 2			
7	741.8	743.1	745.2	14.4	16.9	15.4	15.5	20.1	14.2	-	11.2	05.9	10.1	91	68	77	79	ENE 2	WSW 1	NNW 1			
8	749.5	749.8	751.1	12.8	21.8	16.6	17.0	21.9	11.6	-	09.3	10.2	11.2	84	52	79	72	NW 1	WSW 2	NNE 1			
9	752.7	751.3	750.4	14.8	22.6	18.5	18.8	23.4	13.3	-	11.3	13.0	13.9	89	65	84	79	WNW 1	SSE 2	N 1			
10	751.0	752.7	757.1	14.9	24.8	17.0	18.4	25.1	14.0	-	12.1	13.0	08.6	95	55	59	70	W 1	ENF 3	NE 1			
11	757.5	757.0	756.7	15.2	19.7	17.3	17.4	19.7	14.8	-	08.8	08.8	10.4	68	51	70	63	ENE 1	ENE 2	NNE 2			
12	756.2	754.3	753.4	16.7	22.0	18.5	18.9	22.5	16.4	-	09.8	10.3	12.7	69	52	77	66	ENF 2	NNF 1	N 1			
13	752.0	752.3	752.5	17.4	22.7	17.2	18.6	22.8	16.8	-	13.0	11.4	12.1	85	55	82	74	- 0	SSE 2	NNF 1			
14	753.0	752.0	751.6	14.3	24.1	19.6	19.4	24.5	14.2	-	11.3	14.3	12.7	92	63	94	80	NNW 1	SSW 2	NNF 1			
15	750.9	750.0	750.0	16.6	24.9	20.7	20.7	24.9	15.7	-	13.0	15.4	17.0	92	65	71	76	- 0	ESE 1	NNE 2			
16	751.3	751.5	751.5	18.0	23.7	20.0	20.4	23.7	17.5	-	12.0	12.9	12.1	77	55	69	63	ENE 2	ESE 2	NNE 2			
17	751.2	750.9	750.4	15.4	22.8	18.4	18.8	22.8	15.0	-	11.7	13.1	12.1	89	63	76	76	- 0	SE 2	NNE 2			
18	750.3	749.6	749.7	14.8	23.1	15.4	19.2	23.5	14.7	-	12.3	13.2	14.2	97	62	84	81	ENE 1	SSE 1	NE 2			
19	750.0	750.6	749.4	17.0	22.6	18.8	19.3	23.1	15.2	-	13.1	11.3	10.0	90	55	61	69	ENE 1	ENL 2	NNE 2			
20	746.3	744.5	744.6	16.4	18.7	16.1	16.8	18.8	15.3	-	10.6	13.4	12.4	76	56	90	84	ENF 1	NE 2	NE 2			
21	744.5	745.3	744.4	14.3	13.6	13.2	13.6	16.2	13.2	-	10.5	11.1	11.3	86	95	89	90	NNE 4	SW 2	SSE 1			
22	743.5	744.9	746.4	13.0	16.9	15.5	15.2	17.4	12.5	-	10.8	11.6	11.9	96	81	90	85	WSW 1	SSW 1	NE 2			
23	748.5	748.3	746.1	11.9	12.9	12.4	12.4	15.5	11.6	-	09.7	06.6	05.5	93	79	88	87	NNE 1	E 1	SSE 2			
24	741.7	739.2	737.6	11.9	17.1	16.1	15.3	18.0	11.5	-	09.6	12.0	11.0	92	82	80	85	SSE 1	ESE 2	NNW 1			
25	737.8	736.9	734.9	09.0	11.5	09.7	10.2	16.2	09.7	-	08.5	08.1	08.1	93	79	90	87	WNW 2	W 2	SSW 1			
26	732.1	735.5	740.8	06.9	14.6	09.8	11.0	14.7	05.3	-	08.7	08.2	07.8	95	65	87	82	NNE 1	SSW 1	NNE 2			
27	747.5	747.9	748.2	06.3	16.8	12.1	11.8	16.8	06.3	-	06.6	05.6	06.7	93	39	63	65	WSW 1	WNW 2	W 1			
28	746.1	743.8	743.5	06.2	21.1	14.0	14.6	21.1	07.6	-	07.1	09.2	07.5	87	49	60	65	WSW 1	WSW 4	KSW 3			
29	741.6	743.0	745.3	14.7	17.9	11.1	13.7	18.4	11.1	-	07.2	11.6	09.0	69	73	91	78	NNE 1	SSE 1	KSW 3			
30	745.8	747.3	747.7	10.1	10.4	10.2	10.2	11.2	09.2	-	08.9	09.0	08.8	96	95	94	95	SSE 1	ESE 2	ENE 1			
MES.	MREFD.			747.6	747.3	747.6	14.2	20.1	16.4	16.8	20.9	13.2	-	10.7	11.4	11.1	88	65	78	77	1.1	1.9	1.6

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1	747.2	749.0	749.7	09.5	10.1	08.1	09.0	11.3	08.1	-	08.5	06.9	07.1	95	75	87	86	WSW 1	WNW 1	N 1
2	747.1	744.9	744.3	07.7	07.6	05.8	06.7	08.8	05.6	-	07.2	07.0	05.9	91	84	88	89	NE 1	NE 2	W 1
3	740.3	748.6	747.8	04.6	12.4	09.8	09.2	13.5	04.6	-	06.1	06.6	07.2	96	61	79	74	WSW 2	SW 3	N 1
4	746.8	748.4	749.3	10.6	09.8	07.7	09.0	11.6	07.5	-	07.8	09.5	07.1	81	93	90	88	SSW 2	ENE 2	NE 2
5	748.7	748.2	747.3	07.6	08.4	07.6	07.8	08.5	07.5	-	07.5	07.0	07.2	95	84	92	90	WSW 1	ENF 2	NNW 1
6	746.6	748.1	748.4	06.6	06.7	06.2	06.4	08.6	06.2	-	06.9	07.0	06.4	95	95	91	94	SW 1	NNF 2	NNW 1
7	746.5	743.3	741.9	03.3	06.6	06.6	05.8	07.3	02.8	-	05.0	06.3	06.1	87	86	90	88	NNW 1	ESE 2	WSW 1
8	737.7	739.3	742.5	07.9	11.5	08.9	09.3	12.7	06.6	-	07.6	08.2	07.2	95	81	85	87	NNW 2	SW 2	N 2
9	743.5	744.3	745.9	06.9	09.0	08.1	08.0	10.0	05.5	-	07.2	07.7	07.6	96	91	94	94	ENE 1	WSW 1	ENE 1
10	748.5	748.5	749.2	06.4	13.9	09.4	09.8	14.0	06.4	-	07.0	06.4	07.1	97	54	79	77	W 2	SSW 2	NNW 2
11	748.8	748.7	749.2	07.2	10.4	08.9	08.8	10.4	05.8	-	07.2	08.1	07.9	95	86	93	91	ENE 1	SSW 1	NNW 1
12	748.4	747.8	745.5	07.2	09.6	05.7	05.0	09.9	06.9	-	07.1	08.7	08.7	92	96	96	95	ENE 1	FNF 1	NNW 1
13	746.9	748.0	748.9	08.3	08.6	07.5	08.0	09.7	07.4	-	07.1	07.6	07.3	87	91	94	91	NNE 2	S 2	WSW 1
14	747.6	747.9	743.6	07.3	07.3	05.9	06.4	07.5	10.1	-	07.1	06.2	04.1	97	69	82	82	W 1	NNE 2	NNW 1
15	749.0	746.8	745.1	04.9	06.3	06.3	06.0	07.3	04.3	-	05.9	06.4	06.5	90	89	90	90	SSE 1	WNW 1	NNW 1
16	744.7	746.8	748.1	06.2	06.7	04.5	05.7	06.7	04.9	-	06.5	06.8	06.0	93	93	94	93	NNW 1	WNW 1	NNW 2
17	749.6	749.7	750.1	02.1	11.0	07.5	07.0	11.6	01.7	-	05.2	07.1	05.9	97	72	76	82	SW 2	SW 2	WSW 2
18	7																			

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 $H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$

Dan	Vidljivost 0-9	Oblakost N (0-10)					Isolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	09	060	03	C6.0	C6.1	00.3	.	= n-10 ³⁰ • 0°5 ³⁰ 6	
2	7	030	080	06	C5.7	C5.4	.	.	= n-10 ⁶ • 0°1n-a	
3	8	020	020	C6	C3.3	C8.9	.	.		
4	8	09	10	C6	C8.3	C2.4	00.3	.	= rj-12 ¹⁵ △ ^{tr-2} 6-10 ²⁴ R ⁷⁰ 10 ¹⁵ F _{NN} 14 ⁰⁰ 16 ¹⁰ , 0°-15 ⁰⁴ 17 ²⁰ , 15 ²⁰ kV	
5	8	010	010	00	00.7	11.6	22.5	.	= 2n-a, = rj-6 ³⁰ , = 6 ²⁰ 10 ¹⁵ , 18-kV	
6	8	000	000	01	C6.2	11.1	.	.	= n-10 ¹⁵	
7	8	100	10	09	C6.7	C6.6	22.7	.	= n-8 ¹⁵ • 0°-1n-915	
8	8	000	060	00	C6.0	11.5	C3.9	.	= △'n-930	
9	6	010	07	10	06.0	08.4	.	.	= n-n, △ ² n-a	
10	6	000	020	10	C4.0	C7.9	.	.	= 2n-d, = n-930, = 930 10 ¹⁵	
11	7	00	010	00	C6.3	08.9	.	.	= n-8 ³⁰	
12	6	10	020	10	C7.3	C2.1	.	.	= n-14 ⁴⁵ , = 18 ³⁰ n	
13	6	09	010	00	C3.3	06.1	.	.	= n-n	
14	5	000	000	00	C6.0	09.4	.	.	= n-n, △ ² n-a	
15	6	08	040	00	C4.0	08.2	.	.	= △'n-a, = n-8 ¹⁵ , = 8 ¹⁵ n	
16	5	000	C10	00	06.3	07.9	.	.	= n-n, △ ⁰ n-a	
17	6	020	080	01	03.7	08.7	.	.	= △'n-d, = n-930, = 930 n	
18	6	10	020	00	C4.0	C4.1	.	.	= n-n, △ ⁰ n-a	
19	6	04	070	07	C6.0	C2.2	.	.	= n-n, △ ⁰ n-a	
20	3	C6	100	10	08.7	00.0	.	.	= n-n, △ ⁰ n-14 ⁴⁵ , = 18 ³⁰ n	
21	4	100	100	10	10.0	00.0	16.8	.	= n-n, • tr-0 n-915, 12 ⁵⁵ 14 ⁴⁰	
22	5	10	10	10	10.0	00.1	C2.9	.	= n-n, • 0°-1n-12 ³⁰ , 12 ⁴⁰ , 15 ⁴⁵ , 16 ³⁰	
23	7	100	10	10	10.0	00.0	15.5	.	= n-8 ⁴⁵ , • tr-0 n-815, 11 ³⁰ , 14 ⁴⁵ , R ⁰⁻¹³⁴⁰ , 5 ⁰⁶	
24	6	10	10	10	10.0	00.4	C0.7	.	= n-15 ³⁰ , • 0°-13 ³⁰ , 15 ⁴⁵	
25	7	100	10	C2	C7.3	C0.0	18.6	.	= tr-0 n-13 ⁰² , = 8 ³⁰ 10 ⁴⁵	
26	8	100	05	00	C6.3	C1.6	C7.7	.	= n-9 ³⁰ , • tr-0 n-815, 10 ⁰⁶ , 11 ¹⁶ , 17 ⁰⁵ , 18 ⁴⁵ , R ² 17 ²¹ , 17 ²⁰ , R ¹¹ 17 ⁰⁸ , 17 ²³	
27	9	C10	010	00	C6.7	10.0	C6.9	.	= △ ² n-a, = n-815	
28	8	000	010	00	C6.3	11.1	.	.	= rj-815	
29	7	10	10	10	10.0	00.7	C0.7	.	= tr-0 n-14 ⁴⁰ , ni, = 14 ³⁰ n	
30	5	100	100	09	09.7	00.0	17.7	.	= n-h, • n-14 ³⁰	
MES.										
WRED.	05.8	05.4	04.7	05.3	159.7	141.5				

1	5	100	090	08	05.0	00.2	11.7	.	= n-10 ¹⁵ , • 0°-1n-13 ³⁰ , R ^{0-14³⁰-15⁴⁰}
2	5	100	100	100	C6.0	C6.5	.	.	= n-n, • tr-0 n-n
3	9	010	080	10	C6.3	06.2	30.2	.	= n-n, • 0°-1n-8 ³⁰ , 11 ³⁰
4	4	100	100	10	10.0	00.0	00.5	.	= n-n, • 0°-1n-12 ³⁰ , • tr-0 n-15 ⁴⁰
5	6	100	10	100	C6.0	C6.5	.	.	
6	5	100	100	00	06.7	00.8	28.2	.	= n-15 ¹⁵ , • 0°-1n-14 ⁵⁰
7	5	10	10	10	10.0	C0.1	C6.1	.	= △ ² n-a, = n-10 ³⁰ , = 10 ³⁰ n
8	5	100	06	10	C6.7	C2.8	C4.2	.	= n-n, • 0°-1n-8 ³⁰ , 11 ³⁰
9	5	100	10	06	C6.7	C0.2	C4.8	.	= n-8 ³⁰ , • 0°-1n-8 ³⁰
10	8	010	010	01	01.0	09.7	02.7	.	= n-8 ³⁰ , • 0°-1n-8 ³⁰
11	4	10	10	07	05.0	C6.0	C0.1	.	= tr-0 n-11 ¹⁵ , = 0°-1n-10 ³⁰ , 17 ³⁰ , = 10 ³⁰ 17 ³⁰
12	3	10	10	10	10.0	00.0	00.2	.	= n-n, • 0°-1n-9 ³⁰ , ni, = 10 ³⁰ n
13	6	10	10	10	10.0	00.0	29.8	.	= n-n, • 0°-1n-12 ³⁰ , 16 ²⁵ , 20 ⁴⁵
14	7	10	10	02	07.3	00.2	03.2	.	= n-15 ¹⁵ , 15 ⁴⁵ , n
15	5	10	100	10	10.0	C0.1	.	.	= n-n, • 0°-1n-8 ³⁰ , • tr-0 n-18 ³⁰
16	5	10	100	02	C7.3	00.0	C6.4	.	= n-n, • tr-0 n-18 ²⁵
17	8	000	010	00	C6.3	06.7	C3.2	.	= n-11 ¹⁵ , △ ² n-a
18	6	000	050	00	01.7	07.5	.	.	= △ ² n-a, = n-9 ³⁰
19	4	000	000	09	03.0	C2.6	.	.	= tr-0 n-12 ³⁰ , 11 ¹⁵ , 12 ³⁰ , = 0°-18 ¹⁵ , 11 ³⁰
20	8	09	10	100	05.7	C0.0	C0.6	.	= tr-0 n-14 ³⁰ , 14 ¹⁵ , 14 ³⁰ , 17 ⁰⁵ , ni, = 11-14 ¹⁵
21	5	100	100	10	10.0	C6.0	34.5	.	= n-n, • 0°-1n-ni
22	8	080	09	00	05.7	05.3	C5.4	.	= n-10 ³⁰ , △ ² n-a, on
23	6	01	010	05	C2.3	C5.1	C0.1	.	= n-8 ³⁰ , △ ² n-a, on
24	8	08	09	04	C7.0	C1.1	.	.	= n-n
25	5	08	000	08	05.3	C6.8	.	.	
26	5	10	05	05	08.0	00.0	.	.	= n-n, • tr-0 n-19 ³⁵ , R ¹⁹ ¹⁵ , 19 ³⁰
27	8	050	050	C8	C6.0	C8.3	C6.5	.	= △ ² n-d, = 7 ¹⁵ 9 ³⁰
28	4	10	100	100	C6.0	06.0	.	.	= n-n, • 0°-17 ²⁰ n
29	8	10	080	00	C6.0	00.5	23.7	.	= n-10 ³⁰ , • tr-0 n-ni
30	7	10	060	08	08.0	C4.7	.	.	= n-13 ³⁰ , • tr-0 20 ⁵⁰ n
31	4	07	10	100	05.0	00.0	.	.	= n-n, • tr-0 20 ⁵⁰ n
MES.									
WRED.	07.7	07.6	06.5	07.3	74.9	224.0			

$\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0—12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	743.6	744.3	746.6	04.4	05.2	04.4	05.6	05.8	04.0	-	05.0	03.4	03.7	81	41	60	61	NNNE 1	NE 1	NW 1	
2	747.2	745.3	747.4	00.0	05.5	07.4	06.1	10.6	00.0	-	03.9	04.2	04.6	86	49	60	65	WSW 2	WSW 2	S 2	
3	749.3	749.5	749.9	05.2	12.7	05.2	09.1	12.8	02.6	-	03.8	02.9	04.1	56	28	47	44	NW 2	WNW 2	NE 1	
4	743.6	747.7	747.9	03.8	04.6	07.2	06.7	09.2	03.4	-	04.3	05.4	05.8	72	64	77	71	NNNE 1	SE 2	NF 2	
5	748.7	750.7	753.3	06.0	06.9	05.8	06.1	07.3	05.6	-	06.3	06.7	06.5	90	90	94	91	NNNE 1	WSW 1	WSW 1	
6	754.7	755.1	756.9	05.7	05.9	05.8	05.8	06.2	05.4	-	05.9	06.2	06.3	87	90	93	90	NNNE 1	SSW 1	SSS 1	
7	756.2	754.9	755.0	05.3	05.8	05.6	05.6	06.0	04.9	-	05.5	05.0	05.1	82	73	74	76	NNE 2	NNE 2	NNE 3	
8	753.5	753.4	754.2	05.0	06.8	06.6	06.2	07.0	04.8	-	04.7	04.4	03.8	72	60	55	62	WNW 1	ENE 2	NF 2	
9	753.8	753.0	753.1	03.3	05.8	04.9	04.9	08.9	03.2	-	04.5	04.4	04.6	80	53	74	65	WSW 1	SSF 2	WNW 1	
10	752.4	750.9	751.1	-00.2	08.3	04.0	08.4	-00.2	-	04.0	05.0	05.7	91	61	94	82	ENE 1	SE 2	ENF 2		
11	753.3	752.9	752.2	02.1	04.1	02.8	03.0	04.1	01.6	-	05.3	05.7	05.3	98	92	95	95	NNE 1	S 1	SSE 1	
12	750.6	749.1	749.8	01.7	11.1	10.6	08.5	11.8	00.8	-	05.1	06.9	06.8	98	69	71	79	WSW 2	SW 1	SW 2	
13	749.7	750.2	750.9	08.3	13.5	11.0	11.0	14.1	07.2	-	06.2	07.4	07.0	76	64	71	70	W 1	SSF 2	WNW 2	
14	750.1	749.8	750.1	10.1	14.7	11.6	12.0	14.7	06.5	-	07.0	07.0	07.3	75	56	67	65	WSW 2	SSW 4	WSW 2	
15	749.9	749.8	750.2	12.0	17.1	13.8	14.2	17.1	10.8	-	07.6	07.8	07.9	72	54	67	64	W 2	SW 5	WSW 2	
16	749.0	748.5	750.0	11.1	15.8	14.2	14.6	18.5	11.0	-	07.2	08.1	07.6	73	49	63	62	WNW 2	WSW 4	WNW 2	
17	752.4	752.5	752.2	11.2	16.2	13.0	13.4	16.2	11.2	-	07.3	08.2	08.5	73	55	76	69	SSW 2	SSW 2	WNW 2	
18	750.8	750.1	749.3	10.2	16.8	11.2	12.4	16.9	09.4	-	08.1	07.6	07.3	87	53	75	72	WNW 1	WSW 2	SSW 1	
19	745.2	744.4	740.3	08.7	11.4	07.1	08.6	13.6	06.9	-	07.1	07.8	07.0	85	77	93	85	ENE 2	SSW 3	SSW 2	
20	752.5	751.6	751.5	05.2	09.1	06.4	06.8	09.1	05.2	-	05.9	06.4	06.3	89	74	88	84	NNNE 1	S 1	N 1	
21	750.4	750.1	751.2	05.4	09.4	08.3	08.0	10.2	04.7	-	06.0	06.0	07.0	90	66	86	81	ENE 1	WNW 1	ENE 2	
22	752.1	750.5	750.1	05.6	06.8	06.2	06.2	08.3	05.4	-	06.2	06.5	06.7	90	88	94	91	E 2	SSE 1	SSW 2	
23	750.2	749.4	749.4	05.7	09.9	08.8	08.3	10.1	05.7	-	06.5	06.8	06.9	94	75	82	84	ENE 1	S 1	N 1	
24	749.4	749.6	749.9	07.7	09.6	06.8	03.7	09.7	07.7	-	06.8	06.7	06.9	87	75	83	82	ENE 1	E 1	ENE 1	
25	747.6	744.0	742.6	06.0	07.6	08.2	07.5	08.8	06.0	-	06.7	07.0	07.7	96	89	94	93	ENE 2	NNNE 1	ENE 1	
26	740.3	745.5	743.7	04.9	07.0	05.0	05.5	08.2	04.6	-	05.7	05.6	05.6	88	75	84	82	W 1	SW 2	W 1	
27	741.9	743.6	743.9	03.1	07.7	07.4	04.4	07.7	03.0	-	05.1	05.1	05.2	89	65	91	82	EKE 1	EKE 2	W 1	
28	733.3	732.7	735.9	02.0	04.6	00.9	02.0	06.2	00.6	-	05.0	05.5	04.8	73	86	99	93	WNW 2	NNE 2	WNW 1	
29	736.4	737.9	740.4	02.6	02.9	01.6	02.2	03.0	00.3	-	04.7	05.0	04.8	84	88	93	88	WSW 2	FNE 1	SW 1	
30	745.2	747.3	747.5	-00.1	05.0	03.3	02.9	05.0	-00.5	-	04.0	04.9	04.4	93	74	76	81	W 1	WSW 1	NW 1	
MES.	VRED.	748.8	748.5	749.2	05.4	05.5	07.2	07.3	10.0	04.8	-	05.7	06.0	06.0	R4	68	79	77	1.4	1.5	1.5

1	745.7	749.2	743.4	01.7	11.2	05.4	05.5	11.2	01.7	-	04.7	03.9	04.6	90	39	68	66	WSW 1	W 3	N 1
2	752.6	754.9	756.2	08.1	11.1	06.7	08.9	11.2	03.5	-	05.4	05.7	05.2	66	58	64	63	WNW 2	NNNE 1	WNW 2
3	757.4	757.6	757.8	06.6	12.4	04.2	09.4	12.4	05.9	-	06.1	06.0	07.0	84	56	73	73	ESE 1	SSE 1	WSW 1
4	756.5	754.4	751.3	04.5	10.2	06.6	07.0	10.2	04.3	-	05.5	06.4	06.2	67	69	87	81	ENE 1	SSE 1	NW 1
5	748.5	747.0	747.4	01.2	06.5	03.8	03.8	06.6	00.9	-	04.8	05.5	05.8	97	76	96	90	S 1	SE 1	ENE 1
6	749.4	748.7	749.1	03.6	05.8	03.6	04.2	05.8	03.3	-	04.9	05.8	05.3	85	83	88	85	ENE 1	SSE 2	NE 2
7	747.6	746.0	746.3	01.1	04.0	04.0	03.3	04.1	01.1	-	04.7	05.0	05.0	97	82	82	87	WSW 2	SSE 1	SSE 1
8	743.9	744.6	747.0	00.1	10.2	08.0	08.8	10.2	03.5	-	04.4	05.0	04.3	51	54	79	61	NW 3	NW 3	ENE 2
9	749.4	749.6	751.2	07.9	11.2	02.4	09.0	11.3	07.5	-	06.8	07.0	07.9	95	70	84	80	N 1	SSE 1	NNE 2
10	750.8	750.7	752.1	03.5	04.9	05.6	04.6	08.5	03.4	-	05.8	06.4	06.4	98	98	98	98	ENE 1	ENE 1	WSW 1
11	750.3	745.8	741.2	04.6	05.4	05.2	05.1	05.5	04.4	-	06.0	06.2	06.4	94	52	96	94	E 1	E 1	NE 2
12	744.9	745.5	744.4	01.4	02.6	02.6	02.3	06.4	01.2	-	04.8	04.8	04.7	95	87	89	89	ESE 2	WSW 2	WSW 1
13	733.9	733.7	734.1	-01.2	01.2	02.1	01.0	02.6	-01.2	-	04.2	04.3	03.0	98	86	57	80	WSW 2	WNW 2	NNE 2
14	751.5	751.7	752.6	02.3	04.2	-00.6	01.3	04.2	-00.6	-	03.1	03.4	03.0	57	55	69	60	N 3	NNE 2	WNW 1
15	751.1	749.9	749.7	-03.8	02.6	00.6	00.0	02.6	-03.8	-	02.9	02.9	03.0	84	52	67	67	WNW 1	WNW 2	SW 1
16	750.6	750.8	751.0	-02.2	02.6	01.8	01.0	02.8	-02.2	-	03.6	03.6	03.9	90	66	75	77	W 1	SSE 1	WNW 2
17	747.1	742.1	740.2	-01.4	02.7	08.5	04.6	08.8	-01.4	-	03.7	03.8	04.3	90	68	52	70	WSW 1	WSW 2	WSW 4
18	742.3	744.1	745.0	05.																

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 $H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Isotacija broj sani	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6	10	050	00	05.0	05.6	02.0	.	= n-12 ⁴⁶		
2	7	060	080	02	05.3	05.9	.	.	= n-10 ³⁰ , △ ⁰ n-a		
3	6	010	030	10	04.7	08.9	.	.	= n-n, = 0730 930		
4	4	05	09	100	08.0	00.8	.	.	= 0-11 ³⁰ , 16 ³⁵ ni, = 0n-11 ³⁰ , = 11 ³⁰ n		
5	4	100	10	100	10.0	00.0	03.6	.	• = 0n-10 ³⁰ , +r-0n25 ni, = 10 ³⁰ n		
6	4	10	10	10	10.0	00.0	01.0	.	= n-n, △ ⁰ n		
7	4	10	10	10	10.0	00.0	05.8	.	= n-n, +r-0n, 7 ⁴⁵ 745		
8	5	10	10	10	10.0	00.0	00.8	.	= n-n		
9	6	10	010	00	03.7	06.4	00.0	.	= n-n, △ ⁰ n-a		
10	5	02	020	09	04.3	05.9	.	.	= 1-2n-n, = 18 ⁴⁵ 20 ⁴⁵		
11	2	10	10	10	10.0	00.0	.	.	= 1-2n-930, = 930 11 ³⁰ , = 11 ³⁰ 14 ⁴⁵		
12	6	10	040	08	07.3	03.7	.	.	= 0-930, = 930 13 ⁴⁵		
13	6	08	050	05	06.0	07.1	.	.	= 745 13 ³⁰		
14	6	090	020	00	03.7	03.6	.	.	= Sw 12 ³⁰ 14 ⁴⁵		
15	9	07	060	06	06.3	06.7	.	.			
16	8	010	06	10	05.7	06.4	.	.	F _{WSW} a		
17	8	07	070	00	04.7	00.8	.	.	⊕ 13 ⁴⁵ 13 ³⁸		
18	8	07	09	07	07.7	00.7	.	.	= 0-745, = 745 11 ³⁰		
19	6	07	10	100	05.0	01.5	.	.	= n-n, △ ⁰ n-12 ⁰¹ 13 ³⁰ , 17 ⁰² n		
20	7	08	08	10	08.7	02.2	05.3	.	= 0-845, = 8 ⁴⁵ 12 ⁴⁵ , 16 ³² n		
21	5	10	09	10	05.7	00.1	00.0	.	= 0n-930, +r-745 10 ⁵⁰ , = 930 n		
22	4	10	10	10	10.0	00.0	.	.	= n-845, 11 ³⁰ , = 0g45 11 ³⁰		
23	5	10	090	08	05.0	01.4	.	.	= 0-12n-11 ³⁰ , = 11 ³⁰ n		
24	6	10	10	10	10.0	00.0	.	.	= 0-745, = 745 14 ²² ni, = 1n-11 ³⁰ , = 11 ³⁰ n		
25	3	10	10	100	10.0	00.0	00.1	.			
26	8	10	020	07	06.3	02.0	09.3	.			
27	7	10	010	08	06.3	04.5	00.4	.	• = n-745, = n-10, +r-1156, 15 ¹² * 2 15 ¹² , 17 ⁵⁰ , 17 ⁵⁰ 18 ³⁸ , n; R ¹⁴⁴⁰ 14 ⁴⁵ , = n-n, □		
28	5	10	10	10	10.0	00.0	CC.0	.	= 745 n, □		
29	4	09	10	09	09.3	00.3	29.0	06	= 0n-930, = 930 n, □		
30	4	06	030	08	05.7	06.0	06.0	02			
MES.			08.1	07.0	07.6	07.5	81.4	62.1			

1	6	08	000	09	05.7	04.0	.	.	= rj-n		
2	7	10	10	10	10.0	00.1	.	.	= rj-730, +r-0-1745 18 ⁰⁵		
3	6	10	020	09	07.0	06.0	00.0	.	= rj-745 10 ⁴⁵ 13 ⁴⁵ , = 0745 10 ⁴⁵		
4	5	01	000	00	00.3	00.6	.	.	= rj-730 10 ³⁰ n, = 0730 10 ³⁰		
5	3	10	10	10	10.0	00.5	.	.	= 1rj-845, = 845 13 ⁴⁵ , = 13 ⁴⁵ n		
6	4	09	10	09	09.3	00.0	.	.	= rj-n, +r-945 11 ⁵⁸		
7	5	10	10	10	10.0	00.0	00.0	.	= rj-745, = 0730 845, = 845 n		
8	6	10	10	10	10.0	00.0	.	.	= n-n, +r-10 ⁴²		
9	5	08	090	10	05.0	00.2	00.0	.	= 0-12n-1416 20-10 ⁴⁵ , = 1416 20-10 ⁴⁵ , = 945 n		
10	3	10	10	10	10	00.0	00.0	.			
11	4	10	100	10	10.0	00.1	00.0	.	= n-745 11 ³⁰ n, = 0745 11 ³⁰ , +r-0-1740 16 ⁴⁰ , = 19 ³⁰ n		
12	7	10*	100	10	10.0	00.0	10.3	.	= n-1156, +r-n-10 ⁴⁵ n, 10 ⁴⁵ ni, * 2 10 ⁴⁵ n, * 10 ⁴⁵ 18 ²⁴		
13	5	10	090	07	06.7	00.2	02.2	.	= 3n-10 ⁴⁵ , = 10 ⁴⁵ -n, * 2 10 ⁴⁵ 18 ²⁴		
14	8	06	010	00	02.3	07.2	00.0	.	= n-845 F _{NNE} 529		
15	7	01	010	00	00.7	07.0	.	.	= 1n-1145, = rj-10 ⁴⁵		
16	4	00	060	00	02.0	04.4	.	.	= n-n, △ ⁰ n-a		
17	5	02	10	10	07.3	00.0	.	.	= n-n, △ ⁰ n-9		
18	6	10	050	04	06.3	04.0	04.0	.	* 1n-845, = 1545 20 ³⁴ , = 20 ³² n		
19	1	03	10	10	07.7	01.0	00.4	.	= 1n-n, = 1045 20-10 ⁴⁵ , = 2-940 10 ⁴⁵ , 20-n, = 1445 15 ⁴⁰		
20	6	10	070	06	07.7	06.5	.	.	= 1n-10 ⁴⁵ , = 0-745 n, = 745 n		
21	6	09	030	00	04.0	06.0	.	.	= n-n		
22	4	03	000	00	01.0	06.5	.	.	= rj-n, +r-10 ⁴⁵		
23	1	10	10	10	10	00	.	.	= 1rj-n, = 10 ⁴⁵ n, = 11 ³⁰ 12 ⁴⁵		
24	2	10*	10	00	06.7	00.0	00.1	.	= n-n, +r-n-rj, △ ⁰ rj-11 ³⁰ , = 2rj-17 ³⁰ 20 ³⁰ n, = 217 ³⁰ 20 ³⁰		
25	5	10	10	00	06.7	00.0	00.1	.			
26	6	10	10	00	06.7	00.1	.	.	= 1n-8 ³⁰ , = 0830 930, = 930 16 ³⁰ , F _{NNW} 18 ³⁴ 19 ⁰⁵		
27	6	00	090	10	06.3	04.9	.	.	= n-n, +r-1212 20-10 ⁴⁵		
28	5	01	090	07	05.7	07.0	00.4	.	= n-n, +r-1172 20 18 ¹⁰		
29	8	04	030	10	05.7	04.1	00.1	.	= 1745 2, △ ⁰ 1845 n, F22 ⁴⁵ 23 ⁰⁵		
30	6	10	10	C5	08.3	00.0	04.6	.	= n-1445, +r-0-1745 12 ⁴⁵		
31	5	09	100	06	08.3	00.2	00.3	.	= n-1345, +r-1145 14 ⁴⁵ , +r-13 ⁴⁰ 13 ⁴⁰		
MES.			07.2	07.2	06.2	06.9	76.1	22.5			

1974 JANUAR

SPLIT MARJAN

 $\varphi = 43^{\circ}31'$, $N \lambda = 16^{\circ}26'$, E Gr., $\Delta G = +1h\ 06\ min.$

BR. ST. 89

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina vjetra D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	752.0	751.5	752.6	11.2	11.5	11.8	11.6	14.0	10.4	-	05.5	09.5	08.9	95	93	85	91	S	3	ENE 4	ESE 5	
2	752.5	751.7	752.5	10.3	11.5	10.2	10.6	12.0	09.6	-	08.7	08.6	08.6	93	84	92	90	E	4	ESE 4	ESE 4	
3	751.6	752.2	753.9	09.2	09.9	09.8	09.6	11.3	08.6	-	07.2	07.8	06.9	83	86	76	82	ENE 3	ESE 4	NE 2		
4	755.6	756.5	758.0	09.9	12.9	10.9	11.2	13.4	08.6	-	07.1	08.2	07.0	78	74	72	75	ENE 2	ESE 2	-	0	
5	757.6	756.8	756.6	08.8	10.1	09.4	09.4	11.2	08.1	-	06.6	07.4	06.2	78	80	70	76	N	1	SSW 1	WSW 1	
6	753.9	751.2	750.5	08.2	09.6	09.8	09.4	10.8	07.3	-	06.3	07.2	07.4	77	81	81	80	ENE 2	ESE 1	SF 2		
7	751.7	753.1	754.2	08.0	11.4	08.0	08.8	11.5	07.2	-	06.8	07.0	05.4	85	69	67	74	N	2	S 1	NE 1	
8	753.7	753.8	754.7	07.3	07.7	06.9	07.3	08.7	06.5	-	04.4	06.7	06.2	55	84	83	74	N	3	W 1	NNW 1	
9	754.4	753.4	752.0	06.0	09.7	08.8	08.3	10.4	05.7	-	04.1	05.2	06.2	5F	57	73	63	NE 1	ESE 4			
10	748.0	748.1	750.8	09.0	09.8	10.3	09.8	11.0	08.0	-	05.3	06.7	06.1	62	74	65	67	ENE 4	SE 1	N	1	
11	754.1	755.4	757.9	07.7	12.2	09.4	09.7	12.4	07.0	-	04.3	05.6	05.0	54	53	57	55	NE 1	-	0	SSE 1	
12	758.6	758.2	758.9	07.0	11.7	10.8	10.1	11.8	06.6	-	05.4	05.6	04.2	71	54	43	56	NNE 1	SSE 1	NNE 1		
13	756.7	755.5	756.0	09.0	11.8	09.2	10.0	12.0	04.5	-	03.3	04.1	03.3	36	40	38	38	NW 1	S 1	N	2	
14	756.9	756.8	757.2	05.7	09.2	06.8	07.1	09.7	05.1	-	02.4	03.7	03.2	35	42	44	40	NE 2	SSE 1	NW 1		
15	757.1	756.9	756.9	03.7	09.0	07.6	07.0	10.0	03.2	-	02.8	02.9	03.8	47	33	43	43	NNE 2	NNE 1	ESE 2		
16	756.8	756.7	756.1	07.6	10.0	08.2	08.5	10.5	06.6	-	03.8	04.8	04.5	48	52	55	52	-	0	-	0	
17	753.3	750.8	751.5	07.7	08.1	08.8	08.4	08.8	06.5	-	05.4	06.9	04.5	68	85	52	68	SSE 1	SE 1	NE 4		
18	754.3	753.4	753.4	06.6	10.4	09.4	09.0	10.5	06.0	-	04.0	02.9	04.2	54	31	43	44	NNW 3	NNW 3	N	3	
19	753.8	753.4	754.1	08.8	11.8	10.8	10.6	12.5	06.0	-	05.0	05.5	05.7	59	53	59	57	W 2	NNW 3	N	3	
20	752.7	752.2	754.2	14.2	17.2	13.8	14.8	17.4	10.6	-	05.6	05.4	04.7	46	37	40	41	N	2	N	1	
21	755.3	754.9	755.9	09.8	13.5	09.7	10.7	14.8	05.3	-	04.6	05.2	04.6	51	45	51	49	N	2	E 2	N 1	
22	756.5	756.3	756.5	06.5	11.6	08.8	08.9	12.4	06.4	-	03.6	04.7	04.9	49	46	58	51	NE 2	SSW 1	NW 1		
23	756.4	756.3	755.3	06.6	11.0	09.6	09.2	11.7	05.9	-	04.1	06.5	06.0	56	66	67	63	NE 2	N 1	N	2	
24	754.2	754.3	753.9	05.4	12.0	09.1	09.6	12.0	06.8	-	03.5	05.1	04.9	43	49	56	49	NE 3	SW 2	E 2		
25	753.0	752.5	752.7	06.3	10.0	07.1	07.6	10.1	05.2	-	04.0	05.4	05.5	56	59	73	63	N	1	SSW 2	NE 1	
26	754.3	754.6	754.5	05.6	11.0	08.2	08.2	11.0	05.0	-	04.8	06.1	04.9	70	62	61	64	NE 2	SSW 1	N 1		
27	753.1	752.0	752.4	06.6	09.6	07.8	08.0	10.6	05.1	-	04.8	06.5	05.8	66	73	73	71	ENE 2	ESE 4	ENE 2		
28	753.0	753.4	754.3	07.3	13.0	10.0	10.1	13.0	06.4	-	05.0	05.5	05.0	65	49	54	56	NE 3	SW 2	NNW 2		
29	754.5	754.8	755.4	06.7	11.4	09.0	09.0	12.6	06.3	-	04.2	05.7	06.5	57	57	76	63	NE 2	SW 1	ESE 1		
30	757.1	757.6	757.9	07.5	11.8	09.3	09.5	12.1	06.8	-	05.0	05.4	05.6	63	52	63	59	ENE 2	S 1	E 1		
31	758.4	758.0	758.1	08.2	11.2	09.5	09.8	11.8	07.7	-	05.7	06.2	06.6	70	63	72	68	E 2	ESE 4	ENE 2		
MES.	VrhD.	754.6	754.3	754.8	08.0	11.0	09.2	09.4	11.7	06.9	-	05.1	05.9	05.6	62	61	63	62	2.0	1.8	1.8	

1974 FEBRuar

SPLIT MARJAN

1	756.8	756.0	756.4	09.9	12.4	11.1	11.1	12.4	09.3	-	07.3	07.8	07.2	80	72	73	75	SE	4	ESE 4	ESE 4
2	755.8	755.3	755.3	10.2	13.0	11.4	11.5	13.3	09.9	-	06.9	07.7	08.2	74	69	81	75	E	2	SE 2	SL 5
3	753.2	750.7	748.4	10.5	12.4	10.3	10.9	12.5	09.0	-	06.0	08.8	08.1	84	81	86	84	SE	6	SE 6	E 3
4	745.1	745.3	746.4	09.4	09.2	09.0	09.2	11.0	07.7	-	07.7	07.9	06.5	87	90	76	84	SF	5	SW 2	NNW 1
5	746.3	744.5	743.7	07.5	10.8	07.2	08.2	11.8	06.4	-	06.1	06.4	06.4	78	66	84	76	NE	1	SE 3	F 3
6	740.2	735.6	730.2	08.9	10.8	11.2	10.5	11.7	06.8	-	07.3	07.2	08.4	85	74	84	81	SE	5	SE 6	SSE 6
7	728.5	730.9	734.4	08.0	10.6	07.8	08.6	11.6	07.5	-	04.8	03.2	03.6	59	33	46	46	NW	3	N	1
8	740.6	745.9	751.4	06.0	10.5	08.2	08.2	11.0	05.5	-	03.3	02.9	02.5	47	30	31	36	ENE	2	N	5
9	754.8	755.0	755.1	05.5	11.3	08.8	08.6	11.5	04.7	-	02.8	05.1	05.6	42	50	66	53	NE	2	S 2	ENF 1
10	755.3	755.3	755.3	07.9	12.4	10.0	10.1	13.2	07.4	-	04.7	05.8	06.6	59	54	72	62	ENE	2	ENE 1	WSW 1
11	754.1	752.4	751.4	08.8	13.2	10.0	10.5	13.7	08.5	-	06.8	08.2	07.8	80	72	85	79	NNE	2	SSE 1	ESE 2
12	749.1	746.9	745.5	08.2	12.8	10.8	10.6	12.8	07.9	-	05.9	07.4	07.6	73	66	78	72	ENE	3	SF 5	SE 5
13	742.0	741.2	740.3	11.0	14.7	12.4	12.6	15.0	10.8	-	08.0	08.2	08.6	82	66	81	76	SE	5	S 4	FE 4
14	738.7	741.6	743.6	10.1	11.9	12.0	11.5	12.5	09.5	-	08.7	07.8	07.8	94	75	74	81	SE	5	SE 5	ESE 3
15	743.5	744.0	744.5	11.2	13.6	11.7	12.0	15.0	10.4	-	07.3	07.0	06.2	73	60	60	64	SE	4	SSE 2	ENE 1
16	744.0	744.5	746.0</td																		

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	6	10•	10•	10	10•	10.0	00.0	32.4	.	R°n, 0°6°18°55'	
2	7	10•	10•	10•	10•	00.0	00.1	50.0	.	•n-n	
3	7	10	10•	09	09	09.7	C6.9	26.2	.	•n-0725, 8, 12°55' 15°45'	
4	8	09	04•	00	04•	04.3	C3.7	00.9	.	= 12°55' 13°30'	
5	7	07	09	09	08.3	00.9	.	.	.		
6	7	10•	10	10•	10•	10.0	00.0	00.7	.	0°-16°45' 13°45' 17°40' n	
7	8	10•	04•	00	04•	04.7	C6.0	C2.8	.	0°-16°30' 8°30' /	
8	8	10	09	00	06.3	00.2	02.0	.	.	• 19°45' 12°35'	
9	8	09	09	08	08.7	03.1	C2.0	.	.	0°-19°45' 17°30' /	
10	8	10	10•	10	10.0	00.0	.	.	.		
11	8	01	07•	00	02.7	C8.3	04.1	.	.		
12	7	03	02•	00	01.7	07.4	.	.	= 10°30' n	.	
13	8	01	05•	00	02.0	00.3	.	.	.		
14	8	04	08	00	04.0	04.6	.	.	• 12°35' 13, = 18°5 n	.	
15	7	00	05•	08	04.3	07.2	.	.	= 9°5 n	.	
16	7	10	10	00	06.7	00.0	.	.	• 18°30' 9°25' / = 13°40' 18°20'	.	
17	6	10	10•	06	08.7	00.0	00.2	.	• 0°-10°45' 17°30' /	.	
18	8	02	04•	01	02.3	C8.2	11.7	.	.	.	
19	8	09	06	03	06.0	06.0	
20	8	07	05	00	04.0	05.5	
21	8	01	00•	00	00.3	08.6	.	.	= 8°5 13°30'	.	
22	8	00	00•	00	00.0	C8.5	.	.	= 8- 9°45'	.	
23	8	00	09	02	03.7	03.8	
24	8	00	00•	00	00.0	C9.0	
25	7	06	09	10	08.3	01.9	
MES. WRED.					05.5	06.2	03.6	05.1	138.9	127.1	

1	8	05	07	10	07.3	C4.1	.	.	• 16°50' 17°20'		
2	8	08	07	04	06.3	C5.3	00.1	.	• 17°30' 13°30' 19°40' ; ESE 6°00' 18°45' 13°18°30' 19°40'	.	
3	7	03	10•	10	07.7	02.0	00.1	.	• 12°60' 7°25' 13°50' 14°30' ; • 17°25' 9°30'	.	
4	7	10•	10•	10	10.0	C8.0	C9.9	.	• 0°-6°20' 7°25' 10°20' 20°30' /	.	
5	8	10•	08	10	09.3	04.0	11.2	.		.	
6	8	09	10•	10•	05.7	00.0	02.4	.	ESE-SE 6°30' 12°45' / • 11°55' 17°05' 20°45' n	.	
7	9	10•	04•	04	06.0	08.1	11.7	.	• 0°-16°30' 7°	.	
8	8	04	04•	00	02.7	C8.4	
9	8	01	01•	00	00.7	09.2	
10	8	10	06•	02	06.0	C1.8	.	.		.	
11	6	10	07•	00	05.7	02.8	.	.	• 6°20' n	.	
12	8	05	04•	00	03.0	07.4	.	.	• 0°45° 7°30'	.	
13	8	10•	06•	05	07.0	03.7	01.0	.	• 0°45° 7°30'	.	
14	8	10•	09	09	05.3	C1.2	C5.3	.	• 0°-16°30' 15°20' /	.	
15	8	10	06	00	05.3	03.0	01.5	.	• 0°7°30' 8°10'	.	
16	8	10	09	04	07.7	03.0	00.1	.	.	.	
17	8	07	07	10	08.0	04.2	.	.		.	
18	8	09	10	10•	09.7	C0.0	.	.	ESE 6°10' n, • 17°20' n	.	
19	8	07	09	09	08.3	03.7	15.7	.	ESE 6°30' 11°30' ; • 10°30' 11°50' T 11°15' 11°20'	.	
20	8	03	07	00	03.3	07.6	00.7	.		.	
21	8	07	08	00	05.0	05.1	.	.	• 0°-18°30' 8°55' 12°20' 20°40' / ; FNE 23°22' 24	.	
22	6	10	10•	10	10.0	00.0	.	.	• 0°-18°30' 7°30' 10°40' / ; FNE 23°22' 24	.	
23	7	10	10•	10	10.0	00.0	08.8	.	FNE 0°-24	.	
24	8	07	05•	00	04.0	08.5	C6.4	.	F0-24	.	
25	8	01	00•	00	00.3	09.3	.	.	F0-24	.	
26	8	10	07•	09	08.7	03.4	
27	8	08	05•	00	04.3	08.2	
28	8	02•	03•	00	01.7	09.7	
MES. WRED.					07.4	06.8	04.8	06.3	131.7	75.1	

1974 MART

SPLIT MARJAN

 $\varphi = 43^{\circ}31'$ N $\lambda = 16^{\circ}26'$ E Gr. $\Delta G = +1h\ 06\ min.$

BK. ST. 89

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	750.7	749.7	749.1	05.3	12.5	09.0	09.0	13.0	04.9	-	04.0	05.8	05.5	60	53	64	59	NNE 3	SSW 3	ESE 1	
2	746.0	744.3	744.9	07.4	07.1	05.6	06.4	09.1	05.6	-	06.7	06.5	06.1	87	85	89	87	ESE 5	SE 6	S 1	
3	748.2	750.5	751.6	06.5	07.0	08.2	07.7	09.1	04.0	-	06.2	07.4	06.0	85	92	74	84	SE 3	SE 4	ESE 3	
4	750.5	749.3	746.9	10.7	10.2	10.2	10.3	11.7	06.1	-	06.1	08.2	08.2	63	88	88	80	SSE 7	SE 7	SE 8	
5	745.4	745.6	745.3	10.2	12.4	09.8	10.6	13.2	09.8	-	08.9	09.0	08.4	95	84	93	91	SE 7	ESE 1	SE 2	
6	742.2	744.2	747.1	09.5	08.6	06.2	08.6	11.0	07.8	-	06.1	06.4	06.4	68	76	79	74	ENE 4	ESE 7	ENE 1	
7	747.7	748.6	750.0	07.0	10.5	07.6	08.2	12.7	06.4	-	04.0	04.2	02.9	53	44	38	45	ENE 5	NE 5	NE 4	
8	749.9	749.8	751.0	06.8	11.5	07.2	08.2	12.4	06.2	-	03.5	04.3	03.6	47	42	47	45	NNE 5	ESE 2	NE 3	
9	751.4	751.9	753.1	05.8	11.2	08.2	08.4	12.2	05.5	-	03.5	04.4	04.6	50	44	56	50	NE 3	WSW 2	N 1	
10	752.7	752.3	752.5	06.2	12.4	07.8	08.6	13.0	05.8	-	04.5	04.8	04.1	64	45	52	54	NNE 1	WSW 2	NNW 2	
11	753.3	754.4	755.7	06.5	13.1	08.7	09.2	14.0	06.0	-	03.8	04.9	04.2	53	43	50	49	ENE 4	SW 2	ENE 4	
12	756.1	755.7	754.7	06.0	12.8	09.2	09.3	12.9	05.3	-	03.6	05.0	04.2	51	45	48	48	ENE 3	SW 2	ENE 1	
13	752.8	750.3	748.5	06.1	13.3	10.0	09.8	13.4	05.3	-	04.1	05.6	04.4	59	49	48	52	ENE 2	SW 2	NW 2	
14	744.7	740.4	739.8	08.0	15.4	12.6	12.2	15.7	06.2	-	03.4	06.5	05.3	42	50	49	47	NE 2	S 3	SSW 2	
15	759.1	730.0	742.1	10.4	15.4	11.8	12.4	16.1	05.9	-	02.5	03.5	03.6	27	27	35	30	NE 3	NE 5	NE 4	
16	743.1	743.0	744.0	09.5	15.2	11.0	11.7	15.5	09.0	-	04.0	05.4	05.7	45	42	58	48	NE 2	W 3	NNW 2	
17	746.6	748.2	749.5	08.4	15.1	11.4	11.6	15.4	08.0	-	05.2	06.7	08.1	63	52	80	65	ENE 2	SW 2	ESE 2	
18	750.9	750.6	751.4	09.9	15.9	13.7	13.3	16.0	09.0	-	05.0	06.5	06.3	54	48	53	52	NE 2	SE 4	SE 5	
19	752.6	753.4	754.1	12.9	14.8	13.2	13.5	15.0	12.4	-	08.9	08.6	08.2	80	68	72	73	SE 6	SE 6	ESE 5	
20	754.2	753.9	754.9	12.7	15.7	13.5	13.8	16.6	12.0	-	07.0	07.7	06.7	63	58	58	60	SE 5	SE 5	SSE 3	
21	755.1	754.7	754.4	14.1	19.5	15.0	15.9	19.8	13.2	-	02.4	03.6	05.6	20	21	44	28	ENE 3	SW 1	NW 1	
22	753.6	753.2	751.6	11.2	17.5	12.2	13.4	18.0	11.0	-	08.3	08.8	10.1	83	58	94	78	WSW 1	SSW 1	WSW 1	
23	752.7	753.1	753.0	11.2	17.1	12.7	13.9	17.3	10.6	-	09.4	08.8	08.0	94	60	68	74	SE 1	SW 2	NW 1	
24	753.1	752.4	752.0	11.4	16.8	12.6	13.4	17.7	10.6	-	07.5	09.8	09.5	74	68	87	76	ESE 1	SW 2	NNW 2	
25	751.4	751.6	751.5	11.8	18.0	15.8	15.4	19.0	10.5	-	07.9	07.2	06.1	76	46	45	56	ENF 1	SW 1	NNW 1	
26	751.2	750.1	749.3	14.0	19.0	15.6	16.2	19.6	13.7	-	06.3	07.3	08.0	50	44	60	51	ENE 3	SE 4	SE 4	
27	744.4	748.2	748.7	14.3	18.0	13.6	14.9	18.9	13.6	-	09.4	09.1	10.0	77	59	85	74	SE 3	SE 4	NW 2	
28	749.1	750.0	750.1	13.2	17.8	14.2	14.8	18.5	12.7	-	10.4	10.0	10.3	91	65	84	80	ENE 1	SW 3	W 1	
29	751.3	751.5	751.7	11.9	17.3	15.4	15.0	19.2	11.3	-	08.6	09.7	06.6	82	66	65	71	ENE 1	WSW 2	ESE 2	
30	752.3	751.9	752.2	15.0	17.4	14.6	15.4	18.4	14.0	-	08.3	08.4	08.0	65	56	65	62	SE 3	NNW 1	N 1	
31	751.3	749.9	749.9	12.6	15.9	13.1	13.7	16.8	11.4	-	07.9	07.9	09.4	72	58	83	71	E 1	SW 1	N 1	
MES.	WRED. 749.9 749.8 750.0			09.9	14.4	11.4	11.8	15.2	09.0	-	06.0	06.8	06.6	64	56	65	62	3.0	3.1	2.4	

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1	747.7	747.4	748.5	12.9	17.9	14.1	14.6	18.3	10.4	-	08.6	08.8	08.8	77	57	73	69	N 1	WSW 3	ENE 2
2	749.0	750.4	751.8	12.8	18.7	14.2	15.0	19.0	12.4	-	06.9	08.0	06.0	62	50	49	54	ENE 1	WSW 2	ENE 3
3	752.9	752.2	752.1	12.3	17.7	12.6	13.8	18.6	11.4	-	07.0	08.2	07.8	65	54	71	63	NNE 2	WSW 3	ENE 2
4	751.2	749.9	749.3	11.6	16.5	13.2	14.2	18.7	11.0	-	06.5	09.0	07.0	63	56	61	60	NNE 1	SW 2	NW 2
5	748.5	748.4	750.5	12.6	14.9	12.8	13.3	16.5	11.2	-	08.2	08.1	07.7	75	64	69	69	SE 3	SSE 5	ESE 3
6	747.9	747.2	748.5	13.7	19.9	15.3	16.0	20.5	11.9	-	03.9	03.8	03.4	33	22	26	27	NE 3	NNE 2	NE 4
7	750.2	749.1	749.4	13.6	18.8	14.8	15.5	20.4	12.7	-	03.7	04.9	04.1	32	30	33	32	NE 4	WSW 3	NE 4
8	749.1	748.7	749.5	13.2	17.4	13.9	14.6	18.0	12.5	-	05.4	05.0	04.3	48	33	36	39	NNE 2	NNE 2	NNE 4
9	751.2	750.6	750.7	12.0	18.3	14.1	14.6	18.7	10.7	-	04.1	05.0	07.0	39	31	58	43	WSW 1	WSW 3	N 2
10	750.5	748.8	747.3	12.5	16.3	13.1	13.8	16.7	09.9	-	04.9	06.5	06.6	45	47	58	50	NE 2	SE 4	SE 4
11	743.1	741.9	742.0	11.0	11.5	11.6	11.4	14.3	10.2	-	07.4	08.9	08.3	75	86	81	81	ESE 6	ESE 7	SE 5
12	740.8	741.2	741.7	11.4	12.6	13.4	12.7	13.8	11.0	-	09.5	10.0	10.5	94	91	91	92	SE 5	SE 4	ESE 5
13	743.4	744.2	743.4	13.7	15.2	13.2	13.8	16.8	12.1	-	08.4	09.0	09.2	71	70	81	74	ESE 4	SSE 4	ESE 1
14	739.2	736.4	737.0	15.0	13.6	11.8	13.0	16.5	11.5	-	08.2	08.5	05.5	64	73	53	63	SE 3	NE 6	NNE 5
15	738.0	738.9	740.5	10.6	14.8	09.1	10.9	15.0	08.4	-	03.7	03.9	05.7	39	31	65	45	NE 6	NE 4	NE 3
16	740.9	741.2	741.2	09.1	15.0	09.4	10.7	15.5	08.3	-	03.1	04.3	04.2	36	34	47	39	ENE 4	SSW 2	

BR. ST. 89

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijednost 0-9	Oblačnost N (0-10)					Intenzacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	05	050	09	06.3	07.3	.	.	.	• 14 ⁰ n-7 ⁰ 7 ⁴⁰ , F ESE 9 ⁰ 18 ¹²
2	7	10	100	100	10.0	00.0	02.6	.	.	• 18 ³⁰ 14 ²⁰ i
3	7	10	10	10	10.0	00.2	34.5	.	.	F- FSE-SSE 0 ⁴ 24, 0 ¹ 14 ³⁰ n
4	6	10	100	100	10.0	00.0	03.5	.	.	FSE 0-12, 0 ⁰ 26 ³⁰ ni
5	8	10	10	100	10.0	00.5	12.4	.	.	.
6	6	10	10	07	09.0	00.3	16.1	.	.	• tr-16 ²⁰ H ²⁰ i, F ESE 8 ²² 19
7	8	09	09	07	08.3	06.3	00.2	.	.	.
8	8	08	09	09	08.7	05.3
9	8	040	07	09	06.7	05.3
10	8	010	030	00	01.3	09.5
11	8	000	000	00	00.0	05.5
12	8	010	000	00	00.3	10.1
13	8	000	000	00	00.0	10.1
14	8	040	050	04	04.3	05.5
15	8	080	08	03	06.3	09.4
16	7	030	040	00	02.3	08.6	.	.	.	= 6 ³⁰ 12 ³⁰
17	8	000	030	05	02.7	09.4
18	7	020	020	07	03.7	09.9	.	.	.	FSE-SSE 6 ³⁰ 24i
19	7	060	050	00	04.0	05.7	.	.	.	FSE-SSE 0-10 ³⁵ i
20	8	06	08	00	04.7	09.7
21	8	010	000	00	00.3	11.0	.	.	.	Δ ¹ n-9
22	8	000	020	09	03.7	07.7	.	.	.	Δ ² n-9, = 7 ⁵ 12
23	8	10	070	00	05.7	05.7	.	.	.	Δ ² n-12, 19 ⁵ n; = 6 ³⁰ 11 ³⁰ n-18 ¹⁵ i
24	7	030	070	00	03.3	09.2
25	7	09	10	00	06.3	04.7	.	.	.	Δ ¹ n-8 ³⁰ ; = 6 ³⁰ 11 ³⁰ i
26	8	000	08	00	02.7	06.7
27	7	040	050	02	03.7	08.9	.	.	.	= n-n, Δ ¹ n-9
28	6	030	030	00	02.0	08.2	.	.	.	Δ ¹ n-17 ³⁰ i
29	6	010	08	07	05.3	05.7	.	.	.	Δ ¹ 0 17 ³⁰ i
30	7	10	10	10	10.0	00.2	.	.	.	• 0-10 ³⁰ 27 ³⁰ 23 ⁴⁰ 24
31	7	10	080	100	09.3	00.7	01.0	.	.	• 0-10 ²⁰ i, 11 ⁴⁰ 12 ²⁰ 17 ⁵⁰ ni
PES. VRED.		05.1	06.0	04.4	05.2	198.7	70.7			

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1	6	070	06	07	06.7	04.6	00.9	-	- 8-12 ³⁰
2	7	10	050	05	06.7	03.4	00.0	.	• 0-16 ⁴⁰ 7 ³⁰
3	8	000	010	00	00.3	10.5	00.0	.	.
4	7	06	06	00	04.0	07.6	.	.	= n-12 ³⁰
5	7	04	09	10	07.7	02.8	.	.	.
6	8	070	050	00	04.0	09.1	.	.	.
7	8	000	070	00	02.3	08.2	.	.	.
8	8	060	09	00	05.0	06.0	.	.	.
9	8	000	010	00	00.3	11.0	.	.	.
10	8	040	080	08	06.7	06.0	.	.	.
11	7	10	10	10	10.0	00.0	00.4	.	• 0-17 ³⁰ i
12	6	10	10	10	10.0	00.3	04.8	.	• 0-14 ²⁰ 15 ¹⁰
13	7	030	10	10	07.7	03.5	03.5	.	• 0-0 ⁵⁰ 27 ³⁰ 13 ⁴⁵ T ¹ 10 ⁴⁵ 11 ¹⁰ , FNE 12 ⁴⁰ 24
14	6	09	10	09	09.3	01.2	00.4	.	FNE 0-12 ³⁰
15	8	050	09	10	08.0	03.6	00.3	.	• 0-15 ³⁰ 15 ³⁰ FNE 17 ¹⁵ 24
16	8	040	10	09	07.7	06.1	00.1	.	• 0-15 ³⁰ 15 ³⁰ FNE 17 ¹⁵ 24
17	6	10	10	10	10.0	00.0	00.2	.	• FNE-ENE 0-24i, • 0-14 ²⁰ 19 ²⁵
18	8	10	050	00	05.0	08.0	00.2	.	• FNE-ENE 0-23 ³⁰ i
19	8	020	09	06	05.7	06.1	.	.	.
20	8	000	010	00	00.3	12.0	.	.	.
21	8	000	060	09	05.0	09.4	.	.	• tr-12 ⁴⁵ 12 ³⁰
22	8	040	090	04	05.7	07.2	.	.	.
23	8	010	020	00	01.0	12.4	00.0	.	• 0-11 ⁴⁰ 12 ¹⁰ 20 ⁴⁰ n
24	7	08	09	10	09.0	04.9	.	.	• 0-15 ³⁰ 19 ³⁰ i
25	7	10	10	06	08.7	00.0	01.7	.	.
26	8	10	040	10	08.0	07.7	01.4	.	• tr-27 ³⁰ 10 ³⁵ 18 ⁰ 9 ⁰⁴ 10 ⁵⁰ 9 ⁴² 9 ⁴⁰ 9 ³²
27	8	030	10	10	07.7	04.1	08.0	.	• FSE 16 ³⁰ 24i
28	8	050	10	10	08.3	03.2	.	.	• F-FSE 0-23 ³⁰ , • 0-13-13 ⁰⁵
29	8	060	060	01	04.3	10.3	00.0	.	.
30	6	080	10	100	09.3	00.0	.	.	• 0-19 ⁴⁰ n
PES. VRED.		05.4	07.2	05.8	06.1	169.3	21.5		

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 $\varphi = 43^{\circ}31'$, N $\lambda = 16^{\circ}26'$, E Gr., $\Delta G = +1h\ 06\ min.$

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DOF	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u%			Pravac i jačina vjetra D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	731.6	733.3	735.8	11.1	16.5	12.2	13.5	17.0	09.9	-	09.1	04.0	09.0	92	64	79	78	ESE 5	SSW 2	E 1
2	739.2	741.3	742.9	14.7	17.5	14.2	15.2	18.4	12.1	-	07.4	08.6	09.9	59	57	82	66	NNE 3	NW 2	SSW 1
3	745.1	746.2	745.8	13.4	16.8	13.8	14.4	18.0	12.7	-	10.5	10.8	10.1	91	76	85	84	S 1	SSW 3	SSE 5
4	741.3	742.0	742.7	13.2	14.3	13.2	13.5	16.6	12.5	-	09.6	09.5	06.2	84	78	54	72	SE 7	SSE 5	NNE 1
5	742.5	742.3	743.6	13.4	18.4	13.6	14.8	19.0	12.1	-	09.1	08.5	08.8	79	54	75	69	NNE 3	SW 3	SE 3
6	743.7	745.5	747.3	12.8	18.1	14.2	14.8	18.5	09.3	-	09.6	05.8	09.2	87	63	76	75	ESE 3	SSW 3	SE 3
7	749.1	750.1	751.2	13.2	15.0	14.1	14.1	17.9	11.4	-	08.1	08.6	09.2	71	69	76	72	ENE 2	ENF 2	SE 4
8	751.1	750.2	748.6	13.7	18.3	13.9	15.0	18.5	12.3	-	08.5	09.8	07.3	72	62	61	65	E 2	SSW 1	ENE 3
9	747.1	747.4	747.9	14.0	15.5	14.6	14.7	18.2	12.6	-	06.4	06.7	05.3	54	51	42	49	ENE 3	NW 2	NE 3
10	748.9	748.5	749.3	13.8	18.6	16.2	16.2	20.0	11.9	-	04.8	06.4	06.6	41	40	47	43	ENE 3	WSW 4	ENE 1
11	750.3	750.6	750.1	14.8	21.1	17.2	17.6	21.5	12.3	-	07.5	08.2	06.5	55	44	44	49	ESE 1	SSW 2	SE 5
12	751.1	751.6	752.8	16.8	21.7	16.6	17.9	22.4	15.6	-	08.6	10.0	09.7	60	51	68	60	SSE 5	WSW 2	SSE 2
13	754.2	754.5	754.6	17.0	21.0	19.1	19.0	22.6	13.7	-	08.3	10.7	08.4	57	58	51	55	E 1	WSW 3	WWN 1
14	753.9	753.0	751.4	17.3	22.8	18.6	19.3	23.3	15.4	-	10.3	10.2	08.4	70	49	52	57	E 1	SW 2	NW 1
15	749.5	748.7	747.7	15.4	16.8	15.0	15.6	19.2	11.0	-	07.4	10.3	06.7	57	72	52	60	NE 3	SSW 2	NNE 3
16	747.5	747.7	748.6	14.8	20.4	15.6	16.6	20.6	11.6	-	06.1	07.5	06.6	49	42	65	52	NNE 1	SW 3	ESE 1
17	749.6	750.7	751.7	15.8	20.0	15.8	16.8	20.1	13.5	-	09.3	08.7	08.4	69	50	62	60	ESE 1	SE 2	ESE 2
18	752.7	752.6	752.1	16.2	21.4	18.6	18.7	22.5	13.6	-	06.8	08.7	07.7	49	45	48	47	N 1	SW 1	NNE 5
19	751.7	750.5	751.4	18.5	23.2	19.4	20.1	23.7	16.6	-	08.2	08.7	07.7	52	41	45	46	NNE 2	NNF 5	ESE 3
20	751.6	750.4	749.9	20.2	26.1	21.0	22.1	26.2	18.2	-	08.1	08.9	09.0	40	35	48	43	NE 4	W 2	N 2
21	750.5	751.0	751.0	19.6	26.1	22.4	22.6	27.0	18.3	-	09.4	09.8	07.0	55	39	35	43	SSE 2	WSW 1	NNE 4
22	750.6	747.5	743.1	18.9	24.9	20.4	21.2	26.5	16.0	-	08.2	09.7	07.5	50	41	42	44	ENE 2	SW 2	ESE 3
23	742.7	742.6	742.1	15.6	22.2	17.3	18.1	23.4	11.0	-	08.0	07.4	09.1	60	37	61	53	NNW 2	W 3	WSW 2
24	742.3	742.3	742.8	17.2	17.9	17.4	17.5	20.0	14.6	-	10.3	09.9	11.6	70	64	78	71	SSE 1	SSE 5	SE 5
25	747.1	749.1	750.9	17.3	22.3	17.2	18.5	23.0	15.0	-	09.0	06.7	07.7	60	32	52	48	-	0	NNW 2
MES.																				
WRED.	747.8	748.0	748.1	16.0	20.4	17.0	17.6	21.6	13.7	-	08.7	09.6	08.7	64	54	60	59	2.1	2.5	2.5

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1	749.2	749.1	750.5	19.3	23.6	15.6	20.5	24.4	18.6	-	12.5	11.0	12.7	75	50	74	66	ESE 5	SE 4	NNW 1	
2	751.7	753.4	754.2	20.1	21.2	20.0	20.3	21.5	18.4	-	08.8	08.6	07.7	50	46	44	47	NE 5	NE 6	NNE 5	
3	754.4	753.4	753.3	18.9	25.4	21.9	22.0	26.0	18.2	-	07.3	06.9	08.0	45	28	41	38	NNE 4	NNF 1	NE 4	
4	753.6	753.3	752.2	21.0	27.0	20.0	22.0	27.2	18.5	-	09.0	11.0	13.8	48	41	78	56	NF 1	SSW 2	SSE 1	
5	752.2	751.8	750.7	21.1	27.4	23.1	23.7	28.5	18.2	-	11.8	12.0	11.6	63	44	55	54	ENE 1	SW 2	NNW 1	
6	748.7	749.0	748.0	21.7	24.4	22.0	22.5	24.7	18.0	-	12.2	11.6	10.2	63	50	52	55	ESE 1	SE 5	SE 3	
7	748.4	749.0	749.4	18.4	24.1	19.8	20.5	25.2	17.6	-	13.8	13.9	10.9	87	62	63	71	N 2	SW 1	NNE 2	
8	751.9	751.5	750.1	18.6	25.8	21.4	21.8	26.5	16.3	-	05.8	07.0	09.1	36	28	47	37	NF 3	SSW 2	NW 1	
9	748.5	746.7	745.8	17.2	23.5	20.9	20.6	24.2	16.8	-	11.3	09.9	10.4	77	46	56	60	ESE 4	SE 5	ESE 3	
10	745.3	744.9	742.2	19.8	22.7	19.9	20.6	23.2	19.0	-	13.4	12.0	13.9	77	58	80	72	SE 6	S 3	SE 6	
11	743.6	745.2	748.6	14.1	18.3	16.7	16.4	20.3	12.3	-	10.1	06.0	07.6	83	38	53	58	NNW 1	NNE 5	NNW 3	
12	747.6	745.5	745.3	17.0	21.7	14.5	17.1	22.3	14.3	-	04.9	09.3	06.2	33	48	49	43	ENE 3	WSW 4	NF 3	
13	744.2	744.2	745.1	16.2	21.8	16.7	17.8	23.0	13.1	-	05.6	07.0	08.1	40	36	56	44	NE 2	SSW 2	NNW 2	
14	746.7	748.1	749.1	17.0	21.5	18.0	18.6	22.3	13.9	-	08.7	10.2	11.8	60	53	76	63	ESE 3	SSE 2	SE 1	
15	750.5	750.3	749.0	17.3	22.5	17.0	18.4	23.0	14.6	-	09.6	09.2	13.0	65	45	89	66	ENE 3	ESE 2	SE 4	
16	748.6	747.8	747.8	17.2	22.8	19.0	19.5	23.7	15.5	-	12.0	11.6	12.4	81	56	75	71	ENE 1	SSE 1	W 1	
17	747.3	746.9	747.6	19.5	25.6	20.2	21.4	26.0	17.1	-	13.1	13.5	15.1	77	55	85	72	SSE 1	SW 3	ESE 1	
18	748.0	747.8	748.2	20.3	26.3	20.8	22.0	27.0	17.1	-	14.0	10.9	13.6	79	42	74	65	SSE 1	SSW 1	NN 1	
19	748.9	748.6	749.7	20.2	26.0	22.4	22.8	27.4													

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insekticija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	100	07	05	07.3	02.4	21.5	.	• 0-16 ³⁰ 9 ⁶ 15 ⁵⁰ 16 ⁴⁰	
2	8	100	10	09	06.7	00.0	05.5	.	• 0-16 ⁴⁰ 7 ⁴⁵	
3	7	100	10	08	09.3	C3.7	CC.0	.	• 16 ³⁵ 7 ⁴⁰	
4	8	10	05	04	07.7	02.2	00.7	.	FSE 6-16 ⁴⁵ , • 0-17, 6 ³⁵ 9 ⁵⁰ ; T ¹⁵ 17 ¹² i	
5	8	09	040	05	06.0	11.1	01.3	.		
6	8	100	060	05	07.0	08.0	00.4	.	• 0-2 7-8 ⁴⁰ R ¹ 7 ²⁰ 7 ⁴⁰ 7 ² 7 ⁴⁰ 8 ²⁰	
7	8	08	09	08	08.3	04.9	10.2	.	• 0-12 ²⁰ 12 ⁴⁰ T ¹ 13 ⁴⁰ 14 ³⁵	
8	8	09	09	06	09.0	00.0	00.2	.	T ¹ 10 ⁵⁵ 10 ⁵⁵ 10 ²⁵ 14 ³⁰	
9	8	10	10	09	09.7	C3.4	.	.	• 0-12 ⁵⁰ 13 ⁴⁵	
10	8	000	010	00	00.3	12.6	00.0	.		
11	8	05	C10	02	C3.7	11.2	.	.	= n-8	
12	8	09	030	00	04.0	10.0	00.2	.	✓ n 7 ³⁰ 7 ⁵⁰ T ¹ 7 ³⁰ 7 ³⁵	
13	8	000	030	01	C1.3	12.6	CC.1	.	= n-7 ⁵⁰ △ n-8 ³⁰	
14	8	060	030	07	C5.3	09.3	.	.	= n-9 ³⁰	
15	8	10	05	01	06.3	06.0	.	.	• 0-18 ²⁰ 11 ²⁰ 14 ⁴⁰ 14 ²⁰	
16	8	010	050	10	05.3	13.3	03.6	.	✓ 19 ⁴⁰ 20 ⁴⁰ i	
17	8	080	09	08	08.3	05.5	.	.		
18	8	040	06	01	C3.7	08.4	00.0	.		
19	8	070	C30	01	03.7	11.2	.	.		
20	8	000	020	C2	C1.3	13.2	.	.		
21	8	060	090	00	C5.0	10.1	.	.	FNE 23 ³⁵ 24	
22	7	10	050	03	06.0	06.4	.	.	FNE 0-5 ⁴⁵ T ¹ n, • 14 ¹⁰ 4 ³⁰	
23	9	C20	030	10	C5.0	09.1	00.4	.		
24	8	060	10	09	C8.3	C5.7	.	.	• 14 ⁵⁰ 5 ⁰⁰	
25	9	09	09	03	07.0	09.5	00.1	.		
26	8	050	010	00	02.0	13.4	.	.		
27	8	000	020	02	01.2	13.2	.	.		
28	8	030	09	09	R	C7.0	09.7	.	• 0-2 20 ²⁰ 24i, R ¹ 20 ²⁵ n, ✓ 12 ³⁰ 23 ⁴⁵	
29	7	10	090	05	08.0	04.2	12.0	.	• 0-0 ³⁰ 12 ⁵⁵ 15 ⁴⁰ i	
30	8	010	09	09	C6.3	C9.4	C1.7	.		
31	8	09	10	03	07.3	02.2	00.0	.	• 15 ⁵⁰ 6 ¹⁵	
MES. VRED.		06.4	06.2	04.8	05.8	241.8	67.5			

1	8	090	08	05	C7.3	C6.6	CC.9	.	Tn, • 0-12 ³⁰ 2 ⁵⁰ 6 ³⁰ 7 ⁰⁵	
2	8	040	060	00	02.3	11.6	00.1	.	FNE-NNE 6 ⁰⁵ -24	
3	8	030	010	00	C1.3	13.3	.	.	FNE NNE 0-12	
4	8	000	000	00	00.0	14.1	.	.		
5	8	000	010	00	00.3	13.3	.	.		
6	8	060	09	09	08.0	06.0	C1.9	.	Tn, • 0-13 ²⁰ 4 ²⁰ 23 ⁵⁰ 24; FSE 10 ⁴⁵ 14 ²² i	
7	7	09	040	03	C5.3	09.2	C2.5	.	• 10-6 ²⁰ i	
8	8	010	060	02	03.0	08.0	.	.	• 0-3 ⁵² 7 ⁴⁰ i, FSE 21 ³⁰ 24	
9	8	10	060	02	06.0	13.1	00.9	.	FSE 0-Mi, 16-22; • 17 ⁴⁰ 19 ³⁰	
10	8	09	08	10	09.0	C5.2	CC.0	.		
11	8	100	040	00	04.7	10.6	C6.3	.	• 17 ³⁰ 7 ¹⁰ FNE 13 ¹⁰ 16 ³³	
12	8	000	060	06	04.0	10.5	00.0	.	• 17 ⁴⁵ 17 ⁰⁰	
13	8	030	050	01	03.0	14.1	00.0	.		
14	8	10	05	01	C5.3	08.2	.	.	R ¹ 19 ⁴⁵ 11 ⁵⁵ i, • 1-2 10 ¹⁰ 10 ⁵⁰	
15	8	050	10	10	08.3	08.0	06.8	.	• 11 ⁴⁵ 11 ¹⁵ i	
16	8	10	09	07	08.7	C1.6	10.5	.	• 0-17	
17	7	000	010	00	00.3	13.7	.	.	△ n ₁ = 6 ³⁰ 13 ³⁰	
18	8	000	060	10	C5.3	11.5	.	.		
19	8	09	040	03	05.3	10.7	.	.		
20	8	030	060	C1	C3.3	11.6	.	.		
21	7	000	050	00	C1.7	10.6	.	.	= n-9 ³⁰	
22	7	070	030	08	C6.0	C9.5	.	.		
23	7	000	10	10	06.7	06.6	.	.	= n-9 ³⁰ , • 19 ³⁰ 20 ¹⁰	
24	7	09	040	10	C7.7	C8.4	.	.		
25	8	000	050	03	02.7	13.4	00.0	.		
26	8	090	060	00	C5.0	11.0	.	.	F-ESE 3 ⁵⁰ 17 ³⁰	
27	8	060	10	04	06.7	05.2	.	.	• 17-2 14 ³⁰ 19 ⁵⁵ i	
28	8	030	10	10	07.7	06.2	CC.9	.	• 17-2 14 ³⁰ 19 ⁵⁵ i, V ¹ 18 ¹⁵ 19 ⁰⁴ i, T ¹ 18 ⁵¹ 19 ⁴⁰	
29	7	09	10	09	09.3	01.0	.	.		
30	8	08	060	00	04.7	10.3	21.9	.		
MES. VRED.		05.1	05.8	04.1	05.0	284.8	52.7			

$\varphi = 43^{\circ}31'$ N $\lambda = 16^{\circ}26'$ E Cr. $\Delta G = +1h\ 06\ min.$

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D S D	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	750.2	750.7	750.9	22.6	26.8	24.0	24.4	28.2	20.0	-	09.5	02.1	10.8	46	12	48	35	NNE	2	SW	2
2	752.0	751.9	751.6	23.1	30.2	26.4	26.5	31.0	20.5	-	11.3	13.1	09.8	53	41	38	44	NE	1	SW	2
3	751.7	750.2	747.5	24.6	29.3	24.7	25.8	30.2	22.0	-	11.0	13.2	14.7	47	43	63	51	ESE	1	SSW	3
4	747.6	747.7	747.7	24.3	30.2	25.8	26.6	30.7	22.6	-	12.8	13.1	12.3	55	41	49	48	NNW	1	SW	2
5	749.6	750.3	750.5	24.7	29.7	26.2	26.7	30.5	22.0	-	12.9	14.0	14.0	55	45	55	52	ESE	1	SW	3
6	750.7	750.4	748.8	25.0	30.0	25.3	26.4	31.0	22.9	-	15.4	17.9	14.0	65	56	58	60	-	0	SSW	2
7	747.0	747.4	749.7	24.4	19.6	19.9	21.0	27.7	19.0	-	14.9	10.8	06.8	65	63	39	56	ENF	1	NE	6
8	751.9	751.2	752.9	18.6	23.5	20.2	20.6	23.8	17.9	-	06.5	06.5	05.9	40	30	33	34	NE	4	NE	4
9	754.3	753.3	752.4	19.8	24.5	22.3	22.2	26.5	16.6	-	07.3	07.1	09.9	42	40	49	44	NE	3	NNW	4
10	751.0	751.3	751.3	21.2	29.0	23.0	23.8	28.4	19.4	-	13.6	10.8	11.4	77	38	54	55	ESE	1	SW	2
11	750.7	750.7	750.8	23.5	29.3	24.6	25.5	29.6	20.2	-	12.1	11.2	12.8	56	37	55	49	SSE	1	SW	2
12	752.5	752.9	752.4	23.4	30.2	25.5	26.2	31.4	20.4	-	11.8	17.9	12.0	44	40	51	48	NNE	2	SSW	2
13	750.1	750.9	749.9	25.4	31.4	27.6	28.0	31.8	22.6	-	12.7	13.0	12.0	52	38	43	44	ENF	2	SW	3
14	749.8	749.8	750.2	27.6	31.3	27.7	28.6	31.9	25.4	-	10.4	10.6	11.7	37	31	42	37	SF	3	SF	1
15	751.2	751.9	751.3	27.5	34.0	28.8	29.8	34.6	24.6	-	11.6	10.5	12.5	42	26	42	37	NE	2	SW	2
16	750.4	749.9	749.7	28.0	35.3	26.3	31.0	35.8	26.0	-	11.7	10.5	12.2	41	25	38	35	ENE	2	WSW	2
17	747.1	746.2	745.1	27.9	34.3	29.0	30.0	35.3	25.8	-	12.0	13.5	12.4	43	33	41	39	ENF	2	SE	2
18	744.1	745.0	745.2	26.7	31.8	26.4	27.8	32.0	25.6	-	17.1	15.1	12.0	65	43	47	52	SE	3	SW	3
19	743.6	743.7	745.9	24.7	24.3	15.6	20.0	27.2	14.6	-	12.1	12.9	12.0	52	57	90	66	NE	3	ESF	5
20	745.1	746.1	746.0	19.3	21.0	18.8	19.2	21.7	15.0	-	07.5	07.2	06.5	47	39	40	42	NE	6	NE	5
21	746.1	746.8	747.7	18.5	20.7	19.8	19.7	22.6	17.4	-	06.7	07.0	07.5	42	38	43	41	NE	5	NNE	5
22	749.3	749.8	750.0	19.6	23.1	20.2	20.8	24.0	17.9	-	07.0	06.6	06.9	41	31	39	37	NNE	3	NE	3
23	750.1	751.0	751.2	19.5	21.0	21.2	21.0	24.6	18.4	-	06.6	08.6	12.2	51	43	64	53	NNW	1	NNW	2
24	752.1	752.0	751.1	21.3	27.2	22.0	23.1	27.7	18.9	-	11.3	12.9	12.3	59	47	62	56	NNF	1	SSW	2
25	750.1	749.5	749.4	22.2	26.1	23.7	23.9	26.6	20.2	-	11.9	13.2	13.5	59	52	62	58	SE	4	SF	2
26	750.1	750.6	751.4	22.3	29.1	23.8	24.8	29.7	21.0	-	10.2	11.7	10.3	51	39	47	46	NE	4	WSW	3
27	752.2	752.1	752.0	22.1	26.2	22.6	23.9	28.5	19.3	-	09.5	10.4	15.5	48	36	75	53	ENF	1	SW	3
28	752.5	752.1	752.4	22.6	29.3	27.2	26.7	32.1	20.0	-	09.7	13.1	11.0	47	42	41	43	NE	2	ESF	1
29	753.0	752.7	752.5	25.9	32.4	26.5	28.8	33.2	24.0	-	12.6	13.0	12.8	50	36	44	43	NE	1	WSW	3
30	751.8	750.7	749.8	26.8	32.7	27.1	28.4	32.8	25.0	-	13.4	13.6	12.3	51	37	46	45	ENE	2	WSW	3
31	749.3	748.8	748.3	26.0	31.7	29.3	29.1	32.3	23.2	-	11.5	14.5	11.0	46	41	36	41	ENF	1	SSW	2
MES.	VRED.	751.0	750.0	749.9	23.5	28.3	24.4	25.2	20.5	20.9	-	11.2	11.4	11.3	51	39	49	46	2.1	3.0	2.0

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1	743.5	748.6	748.6	27.1	32.0	29.7	33.6	24.6	-	14.3	17.5	12.6	53	49	40	47	ESE	1	SSW	2	NNW	1	
2	748.9	749.1	749.0	27.8	32.8	26.8	29.6	33.4	26.1	-	13.3	18.7	14.8	48	50	50	49	SE	1	SW	2	ESE	1
3	749.7	750.2	750.2	27.2	34.4	30.8	35.2	25.0	-	15.4	15.2	11.8	57	37	35	43	NE	1	SW	3	NNW	2	
4	751.0	751.1	750.5	28.4	34.2	30.7	31.0	34.8	26.3	-	14.5	15.7	12.4	50	39	37	42	ENE	1	SW	1	WNW	1
5	751.2	750.5	750.2	28.2	35.3	30.7	31.2	35.7	26.4	-	10.1	10.5	10.0	35	25	30	30	FNE	2	SW	3	NNF	1
6	750.0	749.9	750.4	29.2	34.4	24.6	28.2	36.1	24.4	-	08.9	12.1	09.9	29	30	43	34	NE	3	NE	4	NE	4
7	750.2	749.2	748.2	23.7	29.7	25.4	26.0	31.3	22.3	-	07.5	12.4	15.3	34	40	63	46	ENF	5	SW	2	E	1
8	747.4	746.1	745.8	24.8	30.3	25.2	26.4	31.0	22.6	-	13.3	14.5	14.3	57	45	59	54	ESE	1	SSW	3	NNW	5
9	744.5	745.0	746.9	24.8	29.3	24.8	25.9	30.6	23.0	-	14.4	15.3	12.8	61	50	55	55	ESE	2	SSW	4	NNE	3
10	748.9	748.1	746.4	23.0	30.1	25.4	26.0	30.6	21.7	-	09.6	13.3	11.1	46	42	45	44	ENE	2	ESE	3	SE	2
11	742.4	743.9	746.8	22.0	21.9	16.5	20.2	28.3	17.9	-	11.2	13.2	07.6	56	67	48	57	NNE	2	SSE	2	NE	5
12	749.4	749.2	750.9	19.8	27.0	22.1	22.8	27.0	16.6	-	08.1	07.9	07.2	47	29	36	37	NNW	1	NNW	3	NNF	3
13	753.0	752.9	753.6	20.6	27.3	23.6	23.8	28.0	19.0	-	07.6	10.0	13.3	42	37	61	47	NNE	5	SSW	3	NNW	2
14	754.5	754.8	754.8	23.4	29.4	25.5	26.0	30.8	19.2	-	11.8	16.5	13.5	54	54	55	54	W	2	SW	2	SSE	1
15	755.5	755.4	754.8	26.1	33.6	30.1	30.0	33.6	23.6	-	09.1	10.3	12.3	36	26	39	34	NNE	1	SW	2	ENF	2
16	754.9	754.3	753.1	28.7	34.6	30.1	26.9	35.0	26.4	-	12.6	11.0	11.7	43	27	37	36	ENE</td					

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivali h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	010	010	00	00.7	14.1
2	9	000	030	00	01.0	14.4
3	8	000	020	03	01.7	14.0
4	8	000	010	05	02.0	13.8
5	8	030	020	00	01.7	13.5
6	8	04	020	00	02.0	13.3
7	8	09	10	00	06.3	08.1
8	8	040	06	00	02.3	10.6	00.0	.	.	.
9	8	000	08	03	02.7	13.0
10	8	09	08	05	07.3	09.7
11	7	10	030	03	05.3	10.0
12	8	000	000	00	00.0	13.5
13	8	000	000	00	00.0	13.7
14	8	000	000	00	00.0	13.6
15	8	000	000	02	00.7	13.0
16	8	000	020	02	01.3	11.0
17	8	090	010	00	03.3	11.7
18	8	010	050	00	02.0	11.8
19	8	050	09	100	08.0	05.5
20	8	09	07	00	05.3	08.7	17.5	.	.	.
21	8	10	08	04	07.3	05.2
22	8	06	08	06	06.7	07.9
23	8	10	10	07	09.0	02.5
24	8	010	020	03	02.0	12.0
25	7	010	000	10	03.7	12.4
26	8	020	050	00	02.3	12.8
27	8	000	000	00	00.0	13.7
28	8	000	010	01	00.7	13.7
29	8	000	020	00	00.7	13.3
30	7	000	020	00	00.7	13.2
31	8	000	010	00	00.3	13.2
MES.										
VRED.		03.0	03.5	02.1	02.9	356.5	17.5			

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1	7	000	050	00	01.7	12.8	.	.	T 15 ³⁰ 15 ³⁰	.
2	7	000	010	00	00.3	12.5	.	.	= n-9 ³⁰	.
3	7	000	030	00	01.0	12.8	.	.		.
4	7	000	010	00	00.3	12.4	.	.		.
5	8	000	000	00	00.0	12.9	.	.		.
6	8	000	050	00	01.7	12.5	.	.	E NE 20 ⁴⁰ 24	.
7	8	000	000	00	00.0	12.9	.	.	E NE 0 ⁴⁰ 6 ⁴⁰	.
8	8	000	000	100	03.3	10.1	.	.	T 20 ⁴² 21 ⁴⁵ 0 ²⁰ 22 ⁴⁵	.
9	8	000	080	00	02.7	11.3	00.0	.		.
10	8	010	060	06	04.3	12.5	.	.		.
11	9	080	08	00	05.3	07.2	.	.	• 0 ⁷ 0 ³ 12 ³⁵ , T 18 ³⁰ 8 ⁴⁵ 11 ³⁵ , T 11 ⁵⁵ 0 ¹ 11 ²² 11 ²⁵	.
12	9	000	030	00	01.0	11.8	05.2	.		.
13	8	040	080	00	04.0	12.2	.	.		.
14	8	000	000	00	00.0	12.9	.	.		.
15	8	000	000	00	00.0	12.6	.	.		.
16	8	010	010	00	00.7	12.4	.	.		.
17	7	000	000	00	00.0	12.5	.	.		.
18	7	000	000	00	00.0	12.4	.	.		.
19	7	000	000	00	00.0	11.6	.	.		.
20	7	000	040	00	01.3	11.3	.	.	= n-12, T 15-15 ⁴⁰	.
21	7	010	020	00	01.0	12.0	.	.	= 8-12	.
22	8	000	050	060	03.7	11.3	.	.	• -2 24 ⁴⁰ 22 ⁴⁰ T +2 20 ⁴⁰ n	.
23	8	09	050	06	06.7	04.8	04.2	.	• T +0-1 0 ³⁸ 7 ⁴² 15 ²⁰ 18 ⁴⁰	.
24	8	090	080	07	08.0	04.8	00.1	.	T 12 ²⁰ 0 ⁶ 6 ⁵⁵ 12 ⁴⁰ 8 ¹⁹ 32 116	.
25	8	10	090	00	06.3	06.6	15.7	.		.
26	8	060	09	06	07.0	05.4	.	.	• 0-13 50 7 05 10 04 10 45 6 13 30, T 19 ⁴⁰ 19 ³⁰	.
27	8	100	060	08	08.0	04.6	06.4	.	T 10 ⁴⁰ 13 60 0 ¹³ 05 45 10 1	.
28	8	070	09	10	08.7	04.1	00.2	.	• T 17 ²⁵ 19, T 17 ⁴⁴ 18 ²⁵	.
29	8	07	070	09	07.7	08.2	00.1	.		.
30	8	000	030	00	01.0	12.0	03.1	.		.
31	8	020	000	04	02.0	10.6	.	.		.
MES.										
VRED.		02.4	03.7	02.3	02.8	324.0	25.0			

1974. SEPTEMBAR

SPLIT MARJAN

 $\varphi = 43^{\circ}31'$, N $\lambda = 16^{\circ}26'$, E Gr. $\Delta G = +1h\ 06\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, I (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	750.0	750.4	749.8	21.8	26.8	23.9	24.1	27.3	20.7	-	12.7	13.8	12.5	65	52	56	58	ESE 3	ESE 4	ESE 3	
2	750.0	750.5	750.7	23.0	29.0	23.6	24.8	29.0	22.2	-	11.8	16.9	17.5	56	56	80	64	ENE 2	SSE. 3	SE 1	
3	750.9	750.5	750.1	22.8	27.2	24.5	24.6	27.8	22.2	-	15.8	17.2	15.3	76	64	66	69	E 2	SE 4	SE 3	
4	748.8	748.6	749.8	24.3	27.9	24.1	25.1	28.5	23.7	-	15.2	19.0	18.8	67	67	83	72	SE 4	SE 3	WNW 2	
5	751.7	751.2	750.3	21.0	27.8	23.7	24.0	28.3	20.0	-	09.8	11.5	10.6	52	41	48	47	NE 4	SW 2	WNW 2	
6	748.5	746.1	743.9	20.7	27.8	23.0	23.6	28.0	19.6	-	09.4	12.1	12.4	51	43	59	51	NE 2	SSE 2	SW 1	
7	741.5	742.2	744.6	18.4	22.8	15.8	20.2	24.3	16.9	-	12.7	13.8	09.3	80	66	54	67	NNE 2	SW 2	NE 4	
8	747.7	749.7	751.7	20.2	26.9	23.5	23.5	27.1	18.4	-	09.9	11.6	14.1	56	44	65	55	NE 4	SW 3	ENE 2	
9	753.7	754.1	753.7	21.2	28.0	23.6	24.1	28.7	20.2	-	10.6	12.8	14.2	56	45	65	55	NE 2	SW 1	NNW 1	
10	754.0	754.1	754.1	21.3	28.0	23.4	24.0	28.6	20.9	-	12.2	14.2	14.0	64	50	65	60	NE 2	SW 3	NE 2	
11	754.6	754.7	754.8	21.6	28.7	23.5	24.5	29.2	20.6	-	10.0	10.7	10.5	52	36	47	45	NE 5	SSW 2	NE 3	
12	754.9	755.0	755.0	21.0	27.8	23.9	24.2	28.0	20.3	-	09.9	12.4	12.2	53	44	55	51	NE 3	SW 2	NW 1	
13	754.7	754.2	753.9	20.7	28.0	22.0	23.2	28.4	19.6	-	11.7	13.1	10.9	64	46	55	55	NNW 1	SW 2	W 1	
14	753.7	753.3	752.7	19.6	26.1	21.5	22.2	26.5	16.4	-	10.4	12.5	13.6	61	49	71	60	ENE 1	SSW 3	NNW 1	
15	751.8	751.0	751.0	21.1	28.7	23.4	24.2	28.8	20.5	-	09.5	12.7	13.7	50	43	63	52	NE 1	SW 2	- 0	
16	751.6	751.7	752.5	23.1	28.5	24.5	25.2	29.5	22.3	-	10.2	12.5	12.5	48	43	54	48	NE 1	WSW 3	NNE 1	
17	753.4	753.2	753.4	21.6	28.2	23.0	24.0	28.6	20.7	-	10.2	12.2	14.6	52	42	69	54	NE 1	SSW 2	- 0	
18	753.5	753.3	753.1	20.8	27.4	22.8	23.4	27.6	20.2	-	12.1	15.6	17.8	65	57	85	69	NE 2	SSW 2	SSW 1	
19	753.2	752.0	750.8	20.2	26.6	22.1	22.8	27.4	19.5	-	13.4	16.2	15.7	75	62	79	72	NE 1	SW 2	SSE 3	
20	748.4	747.4	745.4	21.4	18.9	18.6	19.4	22.6	17.5	-	15.9	15.0	14.5	83	92	90	88	ESE 5	SW 3	ESE 4	
21	745.7	746.3	745.6	19.4	20.5	21.4	20.8	23.6	17.8	-	13.4	14.8	15.0	77	82	78	79	NNE 2	ESE 4	SE 5	
22	746.9	746.5	747.4	18.8	24.3	21.5	21.5	24.6	17.0	-	13.5	14.0	15.2	83	61	79	74	ENE 1	SW 2	ESE 2	
23	749.0	749.1	749.2	19.3	23.1	21.0	21.1	23.4	19.2	-	13.1	12.6	14.9	78	60	80	73	NNE 2	ESE 3	SE 3	
24	746.4	745.3	742.5	20.0	21.9	19.6	20.3	22.5	17.7	-	12.5	11.8	13.5	71	60	79	70	SSE 4	SSE 4	SSF 5	
25	739.1	740.1	739.6	16.0	16.4	15.2	15.7	19.7	14.4	-	11.2	11.0	09.2	82	79	71	77	NNW 3	SSW 1	INF 2	
MES.	VRED.	749.3	749.5	749.7	19.9	24.7	21.3	21.8	25.7	16.6	-	11.4	12.9	13.0	66	56	68	63	2.6	2.7	2.3

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1	748.6	749.4	750.5	12.7	17.9	12.7	14.5	18.2	12.1	-	07.4	07.6	07.4	57	49	63	60	NNE 3	NNW 4	NNW 3
2	748.2	742.5	745.7	12.1	16.0	12.2	13.1	16.7	10.3	-	09.8	10.1	07.2	92	74	68	78	SE 3	SE 7	NW 1
3	751.9	754.0	753.7	09.1	16.0	13.6	13.1	16.1	07.9	-	05.8	07.2	08.1	66	53	69	63	NE 3	S 2	ESE 2
4	752.4	752.6	751.9	15.4	18.0	17.0	16.8	18.4	12.2	-	09.2	10.0	10.5	70	65	72	69	SE 6	ESE 5	FSE 4
5	749.3	748.2	745.9	15.5	18.9	18.8	18.0	19.5	14.4	-	11.4	12.3	11.4	86	75	70	77	ESE 5	ESE 5	SE 6
6	744.5	747.1	748.5	12.9	18.2	12.6	14.0	18.9	11.6	-	07.0	07.1	06.4	63	45	58	55	RNE 4	SW 2	NE 4
7	746.8	746.0	747.4	12.6	17.5	14.5	14.8	18.1	11.6	-	06.9	08.5	09.4	63	57	76	65	ENE 4	SSW 3	E 2
8	743.0	743.9	746.0	14.6	17.0	14.1	15.4	17.6	13.5	-	11.4	10.5	07.6	92	72	63	76	SSE 2	NE 1	NE 2
9	746.5	747.7	748.3	11.7	17.6	11.5	13.1	18.3	10.3	-	07.4	08.6	06.6	71	57	65	64	NF 3	SSW 1	SE 2
10	751.3	751.9	752.1	10.3	17.3	14.0	13.9	17.4	08.7	-	06.5	08.2	07.8	69	56	65	63	ENE 3	SSW 1	ENE 2
11	751.4	751.7	752.5	12.6	15.7	15.2	14.7	16.7	11.8	-	07.4	09.8	10.4	67	73	80	73	ENE 3	ESE 4	LSF 2
12	751.0	749.9	747.9	16.5	18.0	16.2	17.8	18.2	14.5	-	10.6	10.4	13.1	75	67	84	75	ESE 4	SE 5	SSE 4
13	746.4	746.8	746.8	16.1	17.0	14.8	15.7	18.3	14.6	-	13.2	13.4	12.1	96	92	96	95	ESE 3	ESE 2	E 2
14	746.2	747.3	747.4	13.2	13.3	13.0	13.1	15.0	12.0	-	09.2	09.2	08.8	81	80	79	80	NE 3	NNE 4	ENE 2
15	746.2	745.4	744.2	12.7	12.2	11.7	12.1	13.6	11.1	-	08.1	09.8	08.8	73	92	85	83	NE 3	NE 2	NE 2
16	748.1	749.7	752.0	09.6	14.5	09.2	10.6	15.3	08.0	-	07.7	07.3	06.7	86	59	77	74	WNW 3	SSE 2	NE 2
17	752.5	754.5	754.7	08.8	14.5	11.4	11.5	14.7	07.9	-	06.6	07.6	06.9	78	62	68	69	ENE 2	SW 1	NE 2
18	754.9	754.1	754.3	09.5	15.7	13.9	13.2	15.8	08.4	-	05.5	06.0	06.3	61	45	53	53	NE 4	WSW 2	NW 1
19	753.9	752.9	751.3	10.4	16.3	13.0	13.2	16.4	10.4	-	05.3	07.5	08.2	56	54	73	61	NE 3	SSE 1	NE 2
20	745.3	742.2	736.5	14.9	15.5	15.2	15.2	16.0	12.9	-	08.7	10.2	11.9	69	77	92	79	SSE 5	SSW 6	SSW 6
21	727.5	728.2	729.6	12.3	12.2	08.8	10.5	15.7	08.5	-	10.0	08.9	06.6	93	84	78	85	NW 2	SSW 2	NE 4
22	737.4	730.4	741.0	07.6	12.7	13.3	11.7	13.3	06.6	-	06.4	07.6	07.6	82	69	66	72	NNE 2	SW 4	SSW 5

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_1 = 6.5 \text{ m } h_T = 1.0 \text{ m}$

Dan	Vrijeme 0-9	Oblakost N (0-10)					Insolacije broj sati	Padavine R mm	Snežni pokrival h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnev				7	7
1	8 09	070	06	07.3	07.7
2	8 09	090	06	08.0	07.0
3	7 09	030	03	05.0	07.6
4	7 010	09	04	04.7	08.4
5	9 070	020	00	03.0	11.2
6	8 000	000	04	01.3	04.4
7	8 09	07	00	05.3	10.4	10.7
8	8 000	010	00	00.3	11.2	00.5
9	8 000	010	00	00.3	11.1
10	7 000	040	00	01.3	11.1	.	.	.	= 7 ³⁰ 9 ⁰⁵	.	.
11	8 060	000	00	02.0	10.1
12	8 000	000	00	00.0	10.9
13	8 000	000	00	00.0	11.2
14	7 000	000	00	00.0	10.8
15	7 000	000	00	00.0	10.7
16	7 000	040	00	01.3	09.6
17	7 060	050	00	03.7	09.3	.	.	.	= 8 ⁰⁵ 14 ³⁰	.	.
18	6 020	050	00	02.3	08.5	.	.	.	= 0-15 ²⁵	.	.
19	6 030	010	00	01.3	09.2	.	.	.	= 0-9 ¹⁵ , 0-14 ⁴⁵ 24i, R ⁰ 12 ³⁵ 13 ²⁰	.	.
20	6 09	100	100	09.7	00.0
21	8 080	090	09	08.7	06.3	26.0	.	.	12 12 ⁴⁰ 14 ¹⁰ 21 ¹⁵ 22 ¹⁵ , T ¹⁻² 13-13 ²⁰ 24 ³⁰ -24	.	.
22	8 07	060	10	07.7	09.2	12.8	.	.	0-4-4 ¹⁰	.	.
23	8 10	060	08	08.0	06.0	.	.	.	FSE-SW 15-24, 0-2 16 ²⁰ 17 ⁴⁰ 21 ³⁰ 24i, FSE 0-7 ²⁵ i	.	.
24	8 05	10	10	08.3	00.8	.	.	.	0-0-8 ³⁰ 13 ⁴⁵ 13 ⁵⁵ 20 ³⁰ 24i, FSE 0-7 ²⁵ i	.	.
25	7 10	090	100	09.7	03.5	11.4	.	.	1 ²⁰ 8 ²⁰ i, 8-3-7i, T ¹ 6 ³⁵ 7 ³⁰	.	.
26	9 100	040	00	04.7	06.9	40.5
27	9 000	010	00	00.3	10.8	00.4
28	9 000	010	00	00.3	10.7
29	8 09	09	100	09.3	02.8	.	.	.	0-16 ¹⁰ 16 ²⁰ 20 ⁴⁰ 21 ¹⁰ , 0-13 ⁴⁵ 9 ¹⁵ 12 ²⁵ 14 ²⁰ , T ¹ 6 ⁴⁰ 7 ¹⁰ T ¹ 7 ³⁰ , 8-10 ³⁰	.	.
30	7 100	100	03	07.7	00.4	08.2
MES. VRED.		04.6	04.4	03.1	04.0	237.8	110.9				

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1	8 05	030	00	02.7	07.4	24.4	.	• 0-0-15 ⁰⁵ 5 ³⁰ 10 ¹⁰			
2	8 100	10	090	09.7	00.0	07.4	.	• 0-13 ⁵⁰ 22 ⁰⁰ , E-ESE-SE 8 ¹⁰ 15i, R ¹ 14 ⁴⁰ 16 ⁴⁰ , 8-14 ⁵⁰ 17 ⁴⁰			
3	9 010	050	03	03.0	10.3	16.4	.	FSE 6 ¹⁵ -12			
4	8 09	05	08	08.7	04.1	.	.	FSE-SE 10 ² 5 ³⁰ 18 ³⁰ 24, 18 n-6 ³⁰ , 0-14 ³⁰ 6 ²⁰			
5	8 09	090	10	09.3	02.5	05.8	.	FSE 0-0 ¹⁵ , 0-0 ⁴⁰ 3 ³⁰ i			
6	8 08	050	00	04.3	08.3	03.8
7	8 09	050	06	06.7	04.6
8	8 100	060	00	05.3	04.2	C3.7	.	FSE-SSW 4-11 ³⁰ , 5 ²⁰ 12 ³⁰ , 18 n-11 ³⁰ , 13 ¹⁰	.	.	
9	9 020	07	00	03.0	08.4	15.6	.	0-12 ⁵⁰ 4, 16 ⁵⁰ 17 ³⁰ , 18 n-16 ³⁰ 18 ¹⁰ , A 16 ⁴⁰ 16 ⁵⁰ , 8-16 ⁵⁰ 16 ⁵⁰	.	.	
10	8 070	030	00	03.3	08.9	07.2	.	• 4 ³⁵ 5 ⁴⁰	.	.	.
11	8 070	09	06	07.3	03.6	.	.	• 0-10 ²⁰ 13 ⁰⁰ i			
12	7 090	10	10	09.7	00.0	01.1	.	• 0-14 ³⁰ 24i			
13	7 100	100	100	10.0	00.0	17.9	.	• 0-8 ³⁵ 12-17i			
14	8 10	10	06	08.7	00.0	32.0	.	• 18 ²⁰ 8 ¹⁰ 11 ⁴⁰ 12 ⁵⁰			
15	6 10	100	10	10.0	00.0	02.5	.	• 0-17 ⁴⁰ 19i			
16	8 09	08	03	06.7	05.5	13.4	.	• 0-17-8 ³⁰ , 17-19 ⁵⁰ , T ¹ 16 ⁰⁵ 18 ³⁰			
17	8 050	020	00	02.3	C8.1	C7.1	.	• 1n			
18	8 020	040	00	02.0	08.3
19	8 000	020	00	00.7	09.5
20	8 10	100	100	10.0	00.0	.	.	FSE-SSW 10 ¹⁰ 19, 0-2 10 ⁵⁰ 24i			
21	8 100	09	10	09.7	00.4	27.6	.	• 0-0-13 ⁰⁵ 16 ²⁵ 18 ⁵⁵ , T ¹ 16 ⁰⁵ 16 ⁵⁰			
22	9 100	07	10	09.0	03.2	06.3	.	T ¹ 9 ²⁰ 9 ⁴⁵ , 0-6 ³⁰ 10 ³⁰ , 23 ³⁰ -24, FSE 13 ⁴⁰ 23 ⁴⁰			
23	6 100	100	09	09.7	00.0	12.1	.	• 0-0-10 ²⁵ i			
24	9 08	030	00	03.7	07.2	03.0	.	• 0-0-6-6 ¹⁵ 11 ³⁰ 11 ⁵⁰ i			
25	8 010	010	00	00.7	09.6	00.0
26	8 04	100	100	08.0	01.4	.	.	• 0-13-12 ¹⁰ 20 ⁵⁰ 23 ²⁰ , ENNE-ENE 22 ²⁰ 24i			
27	9 010	010	02	01.3	09.7	03.5	.	ENE-ENNE 0-12 ²⁵ i			
28	8 040	10	10	08.0	05.8	.	.	FSE 14 ³⁰ 24 ²⁵ , 16 ⁴⁰ 22 ⁴⁰ i, • 16 ⁴⁰ 22 ⁴⁰ i, T ¹ 19 ³⁰ 19 ⁵⁰			
29	8 080	10	09	09.0	02.4	24.0	.	• 0-9 ⁴⁵ 13 ⁴⁵ i			
30	9 100	09	01	06.7	00.9	01.4	.	• 0-17-10 ³⁵ i			
31	8 10	10	10	10.0	00.1	00.5	.	• 8 ⁵⁰ 10 ⁵⁰ i, 14 ⁰² 16 ⁴⁰ , 19 ⁴⁰ 20, T ¹ 14 ⁴⁵ 20 ³⁰ i			
MES. VRED.		07.0	07.0	05.2	06.4	134.4	241.1				

$\varphi = 43^{\circ}31'$ N $\lambda = 16^{\circ}26'$ E Gr. $\Delta G = +1h\ 06\ min.$

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EGD	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0—12)					
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	741.8	744.6	749.1	07.3	09.8	07.2	07.9	10.3	06.2	-	04.6	03.6	03.3	60	35	44	48	NNE	2	NE	5	NNE	3
2	751.5	751.7	752.5	05.6	11.2	09.8	09.1	12.0	04.8	-	03.1	05.5	05.3	46	55	58	53	ENE	2	SSW	2	ENE	2
3	753.1	754.0	753.9	07.2	09.6	08.5	08.6	10.3	06.8	-	06.6	07.1	06.2	87	80	72	80	ESE	2	I	2	ESE	2
4	751.6	750.8	750.3	09.3	11.9	11.4	11.6	12.8	07.7	-	06.7	07.8	09.3	76	75	92	81	ENE	3	SE	6	SE	4
5	750.0	741.8	753.2	10.7	14.1	14.2	13.3	14.2	10.2	-	08.6	08.3	08.5	89	69	70	76	ENE	4	SSE	4	SE	3
6	754.2	754.3	754.0	14.5	16.1	15.8	15.6	16.5	13.0	-	04.6	09.9	07.9	78	72	59	70	SE	5	SE	5	FSE	5
7	751.3	750.5	750.3	13.4	12.2	10.4	11.6	16.6	10.3	-	05.9	05.9	05.4	51	56	57	55	ENE	6	ENE	6	EKE	6
8	749.8	749.0	750.1	10.3	13.0	10.8	11.4	13.5	09.2	-	04.5	04.6	04.3	46	41	44	44	ESE	5	ENE	6	NE	5
9	749.9	750.5	752.0	11.4	14.2	11.0	11.9	14.5	10.4	-	04.5	05.2	04.5	45	42	46	44	NE	6	NE	6	ESE	4
10	753.6	753.5	754.1	08.9	14.0	10.9	11.2	14.4	08.4	-	04.7	05.5	06.3	55	46	64	55	ENE	3	SSW	1	NNE	2
11	755.6	755.5	755.7	09.3	14.2	11.4	11.6	14.8	08.9	-	05.5	07.0	07.0	62	58	63	63	ENE	2	SSW	1	EKE	2
12	755.0	754.6	754.0	09.9	10.8	11.4	10.9	13.0	09.7	-	06.3	08.7	08.5	69	80	84	81	ENF	3	N	3	E	1
13	753.9	754.8	755.6	10.8	14.8	12.2	12.5	15.0	10.0	-	07.9	09.1	08.2	82	72	77	77	ENE	2	SE	2	ESE	2
14	755.9	756.0	756.6	11.0	14.4	13.3	13.0	15.0	10.2	-	07.7	09.0	09.2	78	73	80	77	E	3	SE	4	SE	3
15	756.5	756.7	756.7	11.7	15.8	13.2	13.5	16.0	11.2	-	07.5	09.0	08.0	73	67	70	70	ESE	3	SE	4	FSE	2
16	755.8	755.3	755.6	12.2	15.6	14.2	14.0	16.0	11.6	-	06.2	06.8	06.5	58	74	70	67	ESE	2	SE	5	SE	5
17	754.5	756.6	757.1	12.5	16.5	13.7	14.1	16.7	12.0	-	05.6	08.3	08.7	61	59	74	65	ENE	2	SSE	3	NNW	1
18	757.1	758.4	756.1	11.1	15.8	13.2	13.3	16.2	11.0	-	07.3	09.8	09.4	74	73	83	77	ENE	2	SSE	1	ESE	2
19	751.7	749.7	752.3	14.2	16.0	13.4	14.2	16.6	11.7	-	09.5	10.0	07.0	79	73	60	71	SSE	6	SSE	6	WNW	3
20	754.3	754.9	754.9	11.2	15.2	17.4	12.8	15.4	10.6	-	07.0	07.5	06.9	70	58	64	64	ENE	2	SWW	2	ENE	2
21	753.6	752.3	752.5	10.8	13.4	11.4	12.0	14.0	10.4	-	05.8	06.6	06.9	60	75	66	67	ENE	4	SSW	5	ENE	2
22	753.5	753.8	754.2	10.6	14.7	11.5	12.1	15.0	09.9	-	05.7	06.2	06.7	60	49	66	58	NE	3	SSW	2	ENE	1
23	754.4	753.2	753.3	09.7	13.1	11.6	11.5	14.1	09.4	-	06.7	08.0	06.9	74	71	67	71	ENE	2	SSW	2	ENE	1
24	752.5	752.7	753.5	10.6	14.4	12.0	12.2	15.0	10.4	-	06.1	07.9	06.8	64	64	64	64	ENF	2	SSE	2	E	2
25	752.1	749.4	747.6	13.4	14.0	14.3	14.0	14.4	11.4	-	08.3	10.7	10.6	72	90	87	83	SE	5	SSW	5	SSE	5
26	746.0	746.0	747.9	10.6	11.5	08.5	09.8	14.6	08.3	-	07.4	05.9	04.5	77	58	54	63	ESE	2	WNW	3	NE	3
27	744.7	743.8	745.3	08.7	09.8	09.2	09.2	11.0	07.3	-	05.8	07.5	05.2	68	82	60	70	ENE	4	NE	2	NE	3
28	742.2	736.8	736.4	09.0	13.4	08.4	09.8	13.8	06.5	-	05.9	09.2	06.2	69	80	75	75	E	3	SE	6	ENE	2
29	741.1	741.8	743.7	07.6	11.4	08.2	08.8	11.6	06.4	-	04.7	05.7	05.1	60	57	63	60	WSW	2	ENE	1	ENE	2
30	746.8	749.6	751.9	06.9	11.6	08.0	08.6	11.7	06.3	-	04.7	05.3	03.5	62	52	43	52	ENF	3	SW	2	ENE	3
MES.	VRED.	751.5	751.4	752.0	10.4	13.4	11.4	11.6	14.2	09.3	-	06.4	07.6	06.8	67	65	66	66	3.2	3.2	3.2	2.4	2.4

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1	752.1	753.7	757.0	07.6	10.5	08.2	08.6	11.5	06.2	-	04.5	05.8	05.1	57	61	63	60	ENE	3	ENE	2	NE	3
2	757.9	758.5	759.2	08.0	11.2	11.3	10.4	11.6	06.8	-	05.0	07.0	05.9	63	70	59	64	NE	1	NNW	1	NNW	2
3	760.1	760.0	760.3	11.4	15.0	13.9	13.6	15.6	10.3	-	05.7	06.6	05.7	57	52	48	52	NNT	2	NNW	2	NNW	2
4	758.9	756.6	754.9	12.2	16.2	12.5	13.4	16.5	11.3	-	05.8	07.2	07.3	55	52	67	58	NE	2	SW	2	SE	1
5	751.7	749.8	746.8	09.2	12.4	09.8	10.3	13.0	08.0	-	05.4	07.1	07.1	62	66	79	69	ENF	1	SSW	1	ENE	1
6	749.5	750.5	751.7	09.6	12.0	10.0	10.4	12.2	08.3	-	04.1	03.2	03.8	45	31	41	39	E	1	LNF	4	NNW	1
7	751.8	751.5	751.3	07.8	11.0	10.0	09.7	11.6	07.4	-	05.8	06.5	06.4	73	66	70	70	ENE	2	NNW	1	NNW	2
8	750.5	750.0	750.6	08.8	10.7	10.2	10.0	11.1	08.1	-	05.8	07.3	06.9	68	76	74	73	ENE	1	SSW	1	NNW	2
9	751.2	751.9	753.4	10.6	13.4	11.7	11.8	14.2	09.1	-	06.1	08.4	08.1	64	73	79	72	NNE	2	SSW	1	SE	1
10	753.9	754.5	755.4	09.2	13.5	10.6	11.0	13.5	09.0	-	05.8	08.4	08.8	67	72	92	77	ENE	2	SW	1	SSE	1
11	754.0	751.1	747.5	09.8	12.3	11.8	11.4	12.3	08.6	-	06.9	08.5	08.2	76	76	79	78	NE	1	SSE	2	SSE	4
12	743.5	742.9	743.2	11.8	08.3	04.2	07.1	12.6	04.2	-	08.2	05.5	05.4	79	67	88	78	SW	2	ENE	4	EKE	4
13	742.7	743.0	743.9	03.9	05.8	04.3	04.6	06.7	03.5	-	04.7	04.2	04.3	78	61	69	69	ENE	2	NNE	3	NNW	2
14	744.8	747.2	748.2	05.4	06.4	06.4	06.2	07															

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 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijnost O-9	Oblačnost N (0-10)					Insolitacij broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	050	050	00	03.3	06.8	03.1	.	.	.
2	8	020	040	10	05.3	08.2
3	7	100	100	08	09.3	00.1	03.3	.	.	.
4	8	10	09	10	09.7	02.4	02.9	.	.	.
5	8	09	10	09	09.3	00.0	27.9	.	.	.
6	8	08	10	10	09.3	01.8
7	8	10	10	10	10.0	00.0	00.4	.	.	.
8	8	060	070	01	04.7	07.8	00.2	.	.	.
9	9	020	010	00	01.0	08.9
10	9	010	010	00	00.7	09.1
11	8	05	08	04	05.7	07.1
12	8	09	100	100	09.7	00.8
13	8	07	070	00	04.7	02.3	19.6	.	.	.
14	8	02	07	07	05.3	05.2
15	8	01	020	00	01.0	07.8
16	8	00	060	00	02.0	07.5
17	8	08	040	02	04.7	07.7
18	8	07	090	06	07.3	05.9
19	7	07	09	01	05.7	02.2
20	8	08	06	02	05.3	06.4	00.2	.	.	.
21	8	10	10	09	09.7	00.6
22	8	01	030	04	02.7	08.1	00.2	.	.	.
23	8	08	08	10	08.7	04.7
24	8	10	080	09	09.0	02.2
25	7	10	10	100	10.0	00.0
26	8	090	040	06	06.3	05.9	05.4	.	.	.
27	8	10	10	00	06.7	00.0	01.5	.	.	.
28	8	09	09	100	09.3	01.8	02.0	.	.	.
29	8	09	070	09	08.3	05.1	08.9	.	.	.
30	8	05	020	00	02.3	08.1	01.0	.	.	.
MES. VRED.		06.6	06.9	05.2	06.2	134.5	76.6			

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1	8	10	060	00	05.3	03.7	.	.	$\bullet 7^{50} 10^{20} i$.
2	8	09	10	07	08.7	00.2	00.4	.	.	.
3	8	06	08	01	05.0	06.4
4	8	01	020	00	01.0	07.7
5	8	01	060	04	03.7	06.7
6	8	05	040	00	03.0	05.0
7	7	04	10	09	07.7	02.8
8	6	10	10	09	09.7	01.1	.	.	$=n-24$.
9	8	09	08	02	06.3	02.1
10	8	00	000	07	02.3	08.0
11	7	10	10	10	10.0	00.1	.	.	$\bullet 15^{45} 19^{30} i$.
12	8	10	10	10	10.0	00.0	01.2	.	$\bullet 0-12^{30} 4^{10} i$.
13	8	01	10	10	07.0	02.0	10.1	.	$\bullet 16^{22} 17^{50} i$.
14	8	07	040	00	03.7	05.8	00.1	.	$\bullet 0-24 i$.
15	8	03	060	00	03.0	07.6	.	.	$\bullet F NNE - NW 0-21^{30} i$.
16	8	05	010	00	02.0	06.3	.	.	$\bullet F NNE 12^{28} - 15 i$.
17	8	01	090	02	04.0	07.1	.	.	$\bullet 0-6^{16} 14^{20} i$.
18	6	10	10	05	08.3	00.0	00.2	.	$\bullet 12^{10} 12^{22} i$.
19	9	02	000	00	00.7	08.4	06.5	.	$\bullet 12^{42} 13^{32} i$.
20	8	07	000	00	02.3	07.3	.	.	$\bullet 12^{52} 13^{52} i$.
21	6	04	060	00	03.3	07.4	.	.	$\bullet n-15^{45}$.
22	7	00	000	00	00.0	07.7	.	.	$\bullet 12^{2} n-7$.
23	7	00	000	00	00.0	07.9	.	.	$\bullet 12^{2} n-7$.
24	7	00	010	10	03.7	07.7	.	.	$\bullet 12^{2} n-7$.
25	6	10	10	00	06.7	00.0	.	.	$\bullet 13^{30} n$.
26	7	04	080	10	07.3	03.9	.	.	$\bullet 9^{30} 14^{10} i$.
27	6	10	09	09	09.3	06.7	.	.	$\bullet 6^{12} 32^{17} 4^{10} i$.
28	9	100	030	07	06.7	07.4	06.1	.	.	.
29	8	01	070	05	04.3	06.7	00.2	.	$\bullet F-E NE 10^{30} 24 i$.
30	8	07	100	09	08.7	00.3	.	.	$\bullet F-E NE 0-20^{30} i$.
31	8	09	030	00	04.0	07.8	00.2	.	$\bullet F-E NE 0-20^{30} i$.
MES. VRED.		05.4	05.8	04.1	05.1	151.8	25.0			

$\varphi = 43^{\circ}43'$ N $\lambda = 18^{\circ}16'$ E Gr. $\Delta G = +1h\ 13\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenih parova e mm			Relativna vlažnost u %				Pravac i jačina vetrova D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	594.3	593.1	593.9	00.0	-00.4	-01.2	-00.7	00.9	-01.2	-	04.6	04.5	04.2	100	100	100	100	SW	10	SSW	5	S 8
2	593.3	593.0	592.4	-01.8	-01.6	-02.4	-02.0	-00.6	-03.0	-	03.9	04.0	03.8	98	98	98	98	S	8	S	4	S 6
3	591.2	591.4	593.3	-02.8	-03.0	-02.1	-02.5	-01.7	-03.4	-	03.6	03.6	03.8	97	97	98	97	SSW	7	SSW	7	SSW 6
4	595.4	596.2	597.5	-03.8	-01.4	-04.1	-03.4	-01.2	-04.3	-	03.3	03.9	03.2	94	95	94	94	SSW	2	-	0	- 0
5	596.5	595.4	594.9	-04.8	-01.6	-01.8	-02.5	-01.1	-05.1	-	02.9	04.0	03.9	91	98	98	96	N	1	SW	4	SW 5
6	592.5	590.0	589.8	-03.0	-03.2	-04.2	-03.6	-01.2	-05.2	-	03.4	03.5	03.2	93	97	96	95	-	0	SW	5	SW 6
7	591.1	591.9	592.3	-04.2	-04.9	-04.8	-05.7	-03.4	-07.4	-	03.2	03.0	02.4	96	95	89	93	-	0	N	1	- 0
8	591.3	591.6	592.0	-05.6	-06.2	-07.6	-07.0	-06.2	-07.8	-	01.9	02.7	02.4	68	92	93	84	N	7	N	2	N 6
9	592.2	592.0	591.3	-05.8	-08.0	-05.4	-06.2	-05.4	-08.4	-	02.7	02.1	02.6	90	85	86	87	SW	2	NW	2	SW 5
10	589.9	590.0	592.2	-03.4	-02.8	-04.6	-03.8	-02.8	-05.4	-	02.7	03.6	03.1	75	97	96	89	SW	7	S	2	NE 4
11	593.0	595.1	596.6	-06.0	-05.8	-04.8	-05.4	-04.4	-07.4	-	02.6	01.5	01.6	90	51	49	63	NNE	3	-	0	N 4
12	597.3	597.2	595.8	-01.6	-04.2	-07.4	-05.2	-01.4	-07.4	-	02.5	01.8	00.8	62	53	32	49	N	5	N	7	N 10
13	594.1	593.0	593.3	-09.0	-09.0	-11.0	-10.0	-07.2	-11.0	-	01.9	02.0	01.6	84	86	81	84	N	10	N	8	N 6
14	594.2	594.4	594.4	-09.0	-05.4	-06.6	-06.9	-05.2	-12.0	-	01.3	01.1	00.7	55	35	24	38	ESE	3	-	0	-
15	594.2	594.4	594.4	-08.0	-06.6	-06.0	-07.0	-06.0	-08.4	-	00.5	00.5	00.7	20	20	22	N	3	N	4	N 6	
16	593.8	592.5	595.0	-03.2	-02.0	-05.0	-03.8	-02.0	-07.0	-	03.5	03.9	03.0	97	98	95	97	N	8	N	9	N 3
17	592.0	590.4	589.3	-02.4	-02.8	-07.4	-05.0	-01.8	-07.4	-	03.5	03.6	02.4	90	97	93	93	SW	9	-	0	-
18	586.6	586.8	588.7	-09.4	-10.0	-09.1	-09.4	-07.2	-10.4	-	02.1	01.9	02.1	91	91	91	91	N	12	N	10	N 8
19	589.0	589.1	588.7	-10.0	-06.8	-05.4	-06.9	-05.4	-10.0	-	01.9	02.6	02.4	91	94	95	93	N	8	N	10	NNW 10
20	587.4	587.2	589.4	-03.8	-03.6	-04.7	-04.2	-03.2	-05.4	-	03.3	03.4	03.1	96	97	95	96	N	12	N	12	N 11
21	592.0	593.1	594.7	-01.6	-06.2	-06.6	-06.5	-04.7	-07.4	-	02.6	02.7	02.6	94	94	94	94	N	9	NNW	1	N 6
22	596.1	597.2	597.3	-05.0	-02.0	-03.5	-03.5	-01.5	-06.6	-	02.5	00.8	03.1	80	21	89	63	SW	5	N	2	SW 4
23	595.9	593.9	593.7	-03.4	-03.2	-03.7	-03.5	-02.4	-05.4	-	02.7	03.2	03.4	77	87	96	87	-	0	SW	6	NW 3
24	592.4	592.1	592.0	-08.4	-07.6	-08.4	-08.2	-03.6	-08.8	-	02.2	02.4	02.2	92	93	92	92	N	7	N	5	N 4
25	590.6	591.3	592.0	-08.0	-06.8	-07.6	-07.5	-06.4	-08.8	-	02.3	02.5	02.4	90	91	93	91	N	5	N	4	N 4
26	592.4	593.0	593.0	-08.2	-06.2	-05.5	-06.4	-05.4	-08.4	-	02.3	02.7	02.7	92	92	88	91	-	0	-	0	WSW 3
27	591.7	590.9	592.1	-04.6	-02.0	-05.8	-04.6	-02.0	-06.4	-	02.5	03.1	02.8	77	79	94	83	SW	6	N	1	-
28	592.1	592.8	593.5	-06.0	-05.7	-06.6	-06.2	-03.6	-07.2	-	02.8	02.8	02.5	94	95	89	93	N	4	N	5	N 4
29	593.2	593.3	594.3	-06.9	-02.8	-04.6	-04.7	-02.4	-07.2	-	02.5	03.4	03.7	91	91	83	88	-	0	SW	6	NW 3
30	595.3	596.3	596.8	-05.2	-03.4	-02.4	-03.4	-02.0	-06.1	-	01.8	03.1	03.2	59	87	82	76	N	2	S	1	SW 4
31	597.0	596.4	596.3	-04.0	-01.8	-02.4	-02.6	-01.4	-04.4	-	02.4	03.3	02.8	70	83	73	75	WSW	4	SW	6	SW 7
MES.	592.2	592.7	593.2	-05.3	-04.4	-05.2	-05.1	-03.3	-06.9	-	02.6	02.8	02.6	84	84	84	84	5.2	4.7	5.0		

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1	595.1	595.4	595.4	-04.2	-02.6	-04.0	-03.7	-02.4	-04.6	-	03.2	03.5	03.3	96	94	96	95	SW	9	SW	6	WSW 5
2	595.2	595.1	595.5	-03.6	-02.4	-04.4	-07.7	-02.1	-04.6	-	03.4	03.8	03.2	97	98	96	97	W	3	SW	5	SW 4
3	591.5	590.1	588.5	-04.0	-03.0	-02.0	-02.8	-02.0	-05.0	-	03.3	03.6	03.9	96	97	98	97	SW	9	SW	10	
4	585.5	584.0	585.9	-03.0	-04.2	-04.6	-04.0	-01.6	-04.8	-	03.6	03.2	03.1	97	96	96	96	SW	8	SW	10	WSW 4
5	585.1	585.0	583.7	-05.0	-03.9	-05.4	-04.0	-03.0	-06.2	-	03.0	03.3	02.9	95	96	95	95	SW	3	SW	6	SW 8
6	580.2	574.2	572.5	-03.6	-03.8	-02.8	-03.2	-02.8	-05.4	-	03.4	03.3	03.6	97	96	97	97	SSW	9	SW	15	SSW 12
7	569.9	572.5	576.0	-04.4	-04.4	-10.4	-07.4	-02.6	-10.4	-	03.2	03.1	01.9	96	94	90	93	S	9	W	5	N 5
8	579.3	583.5	588.2	-04.9	-09.6	-10.0	-09.8	-09.6	-11.4	-	02.0	02.0	01.9	91	91	91	91	N	8	N	9	N 8
9	590.9	592.9	594.0	-12.0	-06.4	-05.0	-07.1	-04.6	-12.2	-	01.6	02.7	03.0	89	94	95	93	3	NW	6	NE 4	
10	593.1	594.2	594.8	-06.4	-03.6	-04.0	-04.5	-03.6	-06.4	-	02.7	03.3	03.3	94	92	96	94	NW	6	N	6	N 1
11	593.6	592.3	591.7	-02.2	-02.8	-02.4	-02.7	-01.6	-04.2	-	03.4	03.2	03.2	93	86	84	88	-	0	NNW	5	W 6
12	588.4	588.7	586.9	-02.4	-02.0	-02.0	-02.1	-00.6	-02.6	-	02.7	03.0	02.6	71	76	67	71	SW	11	SW	6	MSW 8
13	584.0	583.9	583.7	-03.4	-03.2	-03.2	-03.2	-02.0	-03.6	-	03.5	03.5	03.5	97	97	97	97	WSW	7	SW	6	SSW 7
14	582.0	584.1	586.7	-03.4	-03.2	-03.2	-03.2	-02.8	-03.5	-	03.5	03.5	03.5	97	97	97	97	S	8	S	6	SW 8
15	586.5	586.0	587.6	-02.4	-01																	

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 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vjetar 0-9	Oblačnost N (0-10)					Insolacija broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	0	10≡	10≡	10≡	10.0	00.0	.	65	V 0-24, ≡ 0-24, F, F _{s-w} 0-24, [x]	
2	0	10≡	10≡	10≡	10.0	00.0	01.5	65	V 0-24, ≡ 0-24, F, F _{s-w} 0-24, * 3 ¹² 4 ⁴⁵ 22 ³⁵ 23 ⁴⁵ , + 22 ³⁵ 24, [x]	
3	0	10≡	10≡	10≡	10.0	00.0	01.8	66	V 0-24, ≡ 0-23, F _{s-w} 0-24, + 0-16, * 25 ²⁵ 24, * 10 ¹² 13 ⁴⁵ , [x]	
4	8	10	08	00	06.0	02.9	01.0	67	V 0-24, F _{s-w} 0-24, ≡ 0-24, [x], 0	
5	1	06	10≡	10≡	08.7	00.9	.	67	V 0-24, * 0-20 ¹⁵ , ≡ 9 ²⁵ 24, * 9 ⁴⁵ 10 ⁴⁵ , 15 ⁰² 16 ³⁵ , 19 ⁴⁵ 20 ³⁵ , [x], 0	
6	0	09	10≡*	10≡	09.7	00.0	01.0	67	V 0-24, ≡ 0-24, F _{s-w} 0 ²⁵ 14 ³⁰ 24, + 0 ³⁰ 24, + 12 ³⁰ 19 ⁴⁵ 23 ³⁵ 24, [x]	
7	0	10*	10≡	00	06.7	00.0	07.7	75	V 0-24, F _{s-w} 0-14 ⁵ , ≡ 0-17 ¹⁵ , * 0-9 ⁴⁵ , + 0-2 ⁴⁵ , * 17 ²⁵ 24, + 25 ³⁰ 24, [x]	
8	0	10	10≡*	10≡	10.0	00.0	00.4	75	V 0-24, + 0-24, * 0-24, F _n 0 ²⁰ 8 ³⁰ 16 ²⁵ 22 ⁴⁵ , ≡ 9 ⁴⁵ 24, * 11 ⁴⁵ 19 ⁴⁵ , [x]	
9	8	09	05	00	04.7	05.4	01.4	77	V 0-24, * 0-16 ⁵ , + 0-2 ⁴⁵ , ≡ 10 ⁴⁵ 10 ⁴⁵ , * 10 ²⁵ 24, F _{s-w} 20 ³⁰ 24, [x], 0	
10	0	09	10≡	10≡	09.7	00.0	.	72	V 0-24, * 0-9, F _{s-w} 0-10 ⁵ , ≡ 3 ²⁵ 24, * 12 ⁴⁵ 13 ⁴⁵ , [x]	
11	8	01	050	02	02.7	07.9	00.0	72	V 0-24, ≡ 0-2, * 2-24, [x], 0	
12	8	08	040	00	04.0	07.2	.	70	V 0-24, * 0-24, F _n 0 ²⁵ 24, [x], 0	
13	0	00	10≡	00	03.2	00.0	.	68	V 0-24, * 0-24, F, F _{s-w} 0-24, ≡ 7 ⁰⁵ 20, [x]	
14	8	02	050	00	02.3	08.9	.	66	V 0-24, * 0-24, F _n 0-24, [x], 0	
15	8	01	040	00	01.7	08.5	.	63	V 0-24, * 0-24, F _n 18 ³⁰ 24, [x], 0	
16	0	10≡	10≡	04	08.0	00.0	00.6	62	V 0-24, ≡ 0-24, F _n 0-18 ⁴⁵ , ≡ 10 ²⁵ 18 ⁴⁵ , * 4-5 ³⁰ , + 4-10 ⁴⁵ 14 ³⁰ , [x]	
17	0	03	10≡*	10≡*	07.7	00.0	.	60	V 0-24, * 0-7 ⁴⁵ , F, F _n 0-24, * 10 ²⁵ 23, + 4-18-24, [x]	
18	0	10≡	10≡	10≡	10.0	00.0	04.4	72	V 0-24, ≡ 0-24, F, F _{s-w} 0-24, + 4-0-11, [x]	
19	0	10≡	10≡*	10≡	10.0	00.0	.	72	V 0-24, ≡ 0-24, F, F _n 0-24, * 12 ⁰⁵ 15, + 4-12 ⁰⁵ 24, [x]	
20	0	10≡	10≡	10≡	10.0	00.0	01.7	76	V 0-24, ≡ 0-24, F _n 0-24, + 0-24, [x]	
21	0	10≡	10≡	10≡	10.0	00.0	.	74	V 0-24, ≡ 0-22 ¹⁰ , F, F _n 0-24, + 9, * 22 ¹⁰ 24, [x]	
22	9	00	000	00	00.0	09.6	.	74	V 0-24, F _n 0-17 ⁴⁵ , ≡ 10 ⁴⁵ 15 ⁴⁵ , [x], 0	
23	8	00	08	10≡*	06.0	04.9	.	71	V 0-24, * 0-12 ⁴⁵ , F, F _n 0-24, + 8 ³⁰ 14 ⁴⁵ , ≡ 14 ⁰⁵ 24, * 20 ⁴⁵ 23 ⁵⁰ , [x], 0	
24	1	10≡	000	00	02.3	02.7	00.5	71	V 0-24, ≡ 0-12 ⁴⁵ , F, F _n 0-17 ³⁰ , + 0-7 ⁴⁵ , * 12 ⁰⁵ 24, ≡ 12 ⁰⁵ 19 ⁴⁵ , [x], 0	
25	8	09	09	00	06.0	01.7	.	70	V 0-24, * 0-24, F _n 7 ⁴⁵ 10 ⁴⁵ , * 17 ⁰⁵ 18 ⁴⁵ , [x], 0	
26	8	00	000	00	00.0	09.6	00.0	68	V 0-24, * 0-24, [x], 0	
27	2	00	00≡	04	01.3	03.7	.	66	V 0-24, * 0-24, F _{s-w} 4 ⁴⁵ 14 ⁴⁵ , ≡ 10 ²⁵ 16 ⁴⁵ , ≡ 16 ⁴⁵ 18 ²² , [x], 0	
28	0	10≡	10≡	10≡	10.0	00.0	00.3	64	V 0-24, * 0-16 ⁴⁵ , ≡ 5 ³⁵ 14 ⁴⁵ , ≡ 5 ³⁵ 14 ⁴⁵ , F _n 9 ¹⁰ 14 ⁴⁵ , [x], 0	
29	9	00	000	00	00.0	09.8	.	62	V 0-24, * 0-24, F _n 11 ⁴⁵ 16 ⁴⁵ , [x], 0	
30	9	00	040	03	02.3	09.2	.	60	V 0-24, * 0-24, + 10 ⁰⁵ 23 ⁴⁵ , F _{s-w} 22 ⁴⁵ 24, [x], 0	
31	8	05	070	00	04.0	06.7	.	57	* 0-24, F _{s-w} 0-24, [x], 0	
MES. VRFD.		06.2	07.1	04.9	06.1	99.9	22.2			

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1	0	10≡	10≡	00≡	06.7	00.0	.	56	V 0-0 ⁴⁵ F, F _{s-w} 0-21, ≡ 0 ³⁵ 24, V 4 ⁴⁵ 24, [x]	
2	0	00≡	10≡	10≡	06.7	00.0	.	55	V 0-24, ≡ 0-24, F, F _{s-w} 0 ¹⁵ 6 ⁰⁰ , [x]	
3	0	10≡	10≡	10≡	10.0	00.0	.	54	V 0-24, ≡ 0-24, F, F _{s-w} 0-24, [x]	
4	0	10≡*	10≡	10≡	10.0	00.0	11.4	72	V 0-24, ≡ 0-24, F, F _{s-w} 0 ²⁵ 10 ⁴⁵ , * 20 ⁴⁵ * 20 ⁴⁵ 16 ⁴⁵ , + 0 ²⁵ 22 ⁴⁵ , R 1 ⁴⁵ 6 ⁰² , [x]	
5	0	04	10≡	10≡	08.0	00.0	00.3	74	V 0-24, ≡ 0-3 ¹⁰ 7 ⁵⁰ 24, + 3 ¹⁰ 7 ⁵⁰ F, F _{s-w} 8 ²⁰ 24, [x]	
6	0	10≡	10≡	10≡	10.0	00.0	.	74	V 0-24, ≡ 0-24, F, F _{s-w} 0-24, + 4-16 ⁴⁵ 24, [x]	
7	8	10≡*	080	02	06.7	01.6	05.0	79	V 0-24, * 0-9 ¹⁵ F, F _{s-w} w-nw 0-16 ³⁰ , + 4-12 ⁴⁵ , * 3 ¹⁰ 8 ⁰⁰ , [x], 0	
8	8	10≡	050	10≡	08.3	02.5	00.2	81	V 0-24, F, F _n 0-24, + 4-12 ⁴⁵ , ≡ 5 ³⁰ 17 ³⁰ , ≡ 20 ⁰⁵ 24, [x], 0	
9	9	000	080	01	03.0	06.6	.	78	V 0-24, F, F _n 0-22 ⁴⁵ 13 ³⁰ 14 ²⁰ , 21 ²⁰ 24, + 0-2 ⁴⁵ , ≡ 0-0 ⁴⁵ , [x], 0	
10	9	03	020	00	01.7	08.8	.	77	V 0-24, F, F _n 0-14 ⁵⁰ , [x], 0	
11	9	000	000	00	00.0	09.6	.	76	V 0-24, * 7 ¹⁰ 10 ⁴⁵ F, F _w 18 ⁴⁵ 24, [x], 0	
12	9	000	000	00	00.0	09.4	.	73	V 0-11 ³⁰ F, F _{s-w} b-24, [x], 0	
13	0	10≡	10≡	10≡*	10.0	00.0	.	70	F, F _{s-w} -wsw 0-24, ≡ 1 ²⁵ 24, V 8-24, + 8-15 ²⁵ 11 ⁴⁵ , + 8-24, [x]	
14	0	10≡	10≡	10≡	10.0	00.0	01.5	72	V 0-24, F, F _{s-w} -wsw 0-24, + 4-12 ⁴⁵ , ≡ 0-0 ⁴⁵ , [x]	
15	7	10≡*	08	10≡	09.3	00.0	09.5	81	V 0-24, ≡ 0-13 ⁴⁰ F, F _n 0-22 ⁴⁵ 10 ⁴⁵ 11 ²⁰ , * 5 ³⁰ 7 ⁴⁰ , 10 ²⁰ 11 ²⁰ , ≡ 20 ¹⁰ 11 ²⁰ , [x], 0	
16	8	06	08	03	05.7	00.0	03.9	84	V 0-24, F, F _{s-w} 3 ¹⁰ 24, ≡ 3 ¹⁰ 11 ⁴⁵ , 19 ⁴⁵ 24, [x]	
17	8	10≡	08	10≡	05.3	00.0	00.0	82	V 0-24, F, F _{s-w} -aw 0-24, ≡ 3 ¹⁰ 11 ⁴⁵ , 19 ⁴⁵ 24, [x]	
18	8	10≡	08	04	07.3	00.0	.	80	V 0-24, F, F _{s-w} -b-24, ≡ 0-11 ⁴⁵ , [x]	
19	0	10≡	10≡	10≡	10.0	00.0	01.7	81	F, F _{s-w} -b-24, ≡ 0 ²⁵ 24, V 1 ¹⁵ 24, * 2-4 ³⁰ 10 ³² 12 ⁴⁵ 17 ⁴⁵ , + 2-24, [x]	
20	0	08	10≡	10≡	05.3	00.0	01.6	84	F, F _{s-w} -0-13 ⁴⁰ 8-17 ⁴⁵ ; ≡ 0-2, H-24, V 0-24, + 4-12 ⁴⁵ , ≡ 12 ⁴⁵ , [x]	
21	0	05	10≡	10≡	08.3	00.0	01.4	86	= 0-24, V 0-24, * 4-5 ⁴⁵ 9 ⁴⁵ 10 ⁴⁵ 17 ⁴⁵ , * 5 ³⁰ 7 ⁴⁵ , [x]	
22	0	10≡	10≡	10≡*	10.0	00.0	01.7	88	V 0-24, ≡ 0-24, * 10 ⁴⁵ 12 ⁴⁵ K ₂₄ , + 20 ⁴⁵ 24, F _{s-w} 20 ⁴⁵ 24, [x]	
23	0	10≡	10≡*	10≡	10.0	00.0	07.7	100	V 0-24, ≡ 0-24, * 0-14 ²⁰ b2 ²⁰ 23 ⁴⁰ , + 0-15 ⁴⁵ , F, F _{s-w} 0-15, [x]	
24	0	10≡	10≡	10≡	10.0	00.0	01.4	102	V 0-24, ≡ 0-24, + 5-24, F, F _{s-w} 5 ³⁵ 24, [x]	
25	0	10≡	10≡	10≡	10.0	00.0	.	100	V 0-24, ≡ 0-24, + 0-14 ⁴⁰ , F, F _n 0-24, [x]	
26	0	10≡	10≡	10≡	10.0	00.0	.	100	V 0-24, ≡ 0-24, F, F _n 0-24, [x]	
27	9	10≡	000	00	03.3	09.3	.	100	V 0-24, ≡ 0-7 ³⁰ , F, F _n 0-11, * 7 ³⁰ 24, [x], 0	
28	9	000	000	00	00.0	10.7	.	98	V 0-24, * 0-24, ≡ 21 ²⁰ 24, [x], 0	
MES. VRFD.		07.4	07.7	06.8	07.3	58.5	47.3			

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 $\varphi = 43^{\circ}43'$, N $\lambda = 18^{\circ}16'$, E Gr. $\Delta G = +1h\ 13\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u%			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	589.5	589.5	588.9	-03.8	-02.8	-02.4	-02.8	-02.4	-05.0	-	03.3	03.6	03.8	96	97	98	97	S	3	S	3	S	3	
2	586.5	585.9	585.8	-02.2	-02.4	-01.6	-02.0	-01.6	-02.4	-	02.9	02.9	03.3	75	75	80	77	W	7	SW	6	SW	6	
3	586.7	589.2	590.7	-03.0	-01.6	-02.2	-02.2	-01.6	-03.0	-	03.4	03.3	03.5	93	80	90	88	SW	7	SW	7	SW	8	
4	589.9	589.7	588.0	-02.4	-03.2	-03.0	-02.9	-02.8	-06.0	-	02.6	03.4	03.6	67	93	97	86	SW	10	SW	13	SW	15	
5	587.1	587.2	587.4	-03.0	-02.4	-01.6	-02.3	-01.8	-03.4	-	03.6	03.8	03.9	97	98	98	98	S	12	S	7	S	7	
6	585.5	586.7	586.8	-01.4	-00.8	-04.2	-02.6	-00.6	-04.2	-	04.1	04.3	03.2	99	99	96	98	S	7	S	4	N	5	
7	586.8	588.2	588.3	-09.2	-08.3	-10.4	-09.6	-04.2	-10.4	-	02.1	02.3	01.9	91	92	90	91	N	5	N	6	NNW	7	
8	588.4	588.9	589.4	-10.2	-08.2	-08.4	-08.8	-07.4	-10.6	-	01.9	02.2	02.2	90	90	90	90	N	5	N	3	N	3	
9	589.3	590.0	591.6	-06.8	-05.6	-05.6	-05.9	-04.4	-08.8	-	02.6	02.8	02.9	94	92	95	94	N	1	ENE	2	E	4	
10	591.2	591.3	591.9	-05.6	-03.5	-04.6	-04.6	-03.0	-05.8	-	02.9	03.4	03.1	95	97	96	96	N	1	-	0	NNW	3	
11	592.1	593.7	594.1	-03.4	-05.0	-08.6	-06.4	-02.3	-08.6	-	03.5	02.9	02.2	97	93	92	94	S	1	-	C	N	2	
12	594.2	594.2	593.8	-08.0	-01.6	-04.6	-04.7	00.0	-09.0	-	02.1	02.3	02.4	82	57	75	71	N	1	ESE	3	-	0	
13	592.3	591.1	590.5	-06.0	-05.0	-04.0	-04.8	-04.0	-06.2	-	01.8	01.7	01.6	63	53	48	55	N	2	N	1	-	0	
14	588.0	585.7	584.6	-04.4	-04.0	-06.2	-05.2	-02.6	-06.2	-	01.2	02.7	02.7	35	80	92	69	E	4	N	4	N	4	
15	582.0	581.6	583.0	-07.0	-06.0	-07.0	-06.8	-05.6	-08.2	-	02.5	02.8	02.5	93	94	93	93	N	6	N	9	N	7	
16	583.0	584.6	585.7	-07.2	-05.2	-05.0	-05.6	-04.4	-07.3	-	02.5	03.0	02.9	93	95	91	93	N	4	N	2	W	3	
17	586.6	589.8	591.8	-05.0	-02.0	01.2	01.2	01.2	-05.6	-	01.4	02.7	02.1	45	68	41	51	N	5	W	2	NNW	2	
18	591.9	592.6	591.6	-00.5	00.0	00.4	00.1	01.3	-01.3	-	02.8	03.7	03.2	63	80	69	71	WSW	5	SW	7	SW	11	
19	592.9	594.5	594.5	00.6	01.6	01.2	01.2	02.2	-00.2	-	02.9	04.3	04.0	61	83	80	75	SW	10	SW	8	SW	9	
20	595.2	597.1	595.9	00.6	01.6	01.6	01.4	02.4	00.4	-	02.0	02.6	02.5	42	51	48	47	SW	9	WSW	6	SW	10	
21	598.2	599.0	599.5	01.0	05.0	02.4	02.7	07.4	00.8	-	01.8	02.9	03.1	38	45	56	46	SW	6	-	0	-	0	
22	590.4	597.8	596.3	06.4	04.4	03.6	04.5	06.8	02.4	-	02.4	04.1	03.6	33	65	61	53	-	0	E	2	S	5	
23	594.5	595.6	595.6	02.8	02.8	02.8	02.8	03.6	01.0	-	03.2	03.2	03.2	57	57	57	57	S	8	S	7	SW	5	
24	596.8	597.2	595.7	02.4	04.8	03.6	03.6	05.6	02.4	-	03.4	04.2	04.0	62	66	67	65	E	3	S	2	S	5	
25	594.4	595.6	595.6	02.2	03.8	02.8	02.9	04.0	02.2	-	03.2	04.5	04.5	59	75	81	72	SW	10	S	6	S	5	
26	594.9	594.6	593.0	02.4	04.6	03.2	03.4	04.8	02.0	-	04.1	03.8	04.3	74	60	75	70	SW	6	SSW	3	SSW	5	
27	591.9	591.9	592.4	01.8	05.0	00.8	02.1	05.0	00.2	-	03.9	04.0	04.2	74	61	86	74	SW	3	SSW	2	FNE	3	
28	592.0	593.1	594.0	02.4	04.0	01.0	02.1	04.4	00.4	-	04.6	03.6	04.3	84	59	86	76	SSE	4	-	0	-	0	
29	594.4	595.2	595.8	02.4	04.2	03.6	03.4	05.4	00.2	-	03.1	03.3	04.3	56	54	73	61	W	2	-	0	S	3	
30	595.4	594.6	595.0	00.8	01.2	01.8	01.4	03.6	00.6	-	04.5	04.9	04.4	93	98	85	92	N	3	N	3	SW	4	
31	593.5	592.7	592.2	01.4	01.0	-00.6	00.3	02.2	-00.6	-	04.8	04.9	04.4	95	100	100	98	SSE	3	-	0	NE	3	
MES.	WRED.	591.1	591.4	591.6	-02.0	-00.8	-01.6	-01.5	00.4	-03.2	-	02.9	03.4	03.3	74	78	80	77	4.9	3.8	4.7			

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1	590.2	590.6	590.9	-01.0	-01.0	-01.8	-01.4	01.2	-01.8	-	04.3	04.3	03.9	100	100	98	99	NE	2	-	0	-	0
2	590.9	592.5	593.4	-02.2	00.2	-02.4	-01.7	00.3	-02.4	-	03.8	04.7	03.8	98	100	98	99	-	0	-	C	N	1
3	593.5	593.9	593.9	-01.6	-01.4	-02.4	-02.0	00.0	-03.0	-	04.0	04.1	03.8	98	100	98	99	SSW	1	N	2	N	2
4	592.5	592.3	591.5	-03.6	-01.6	-01.8	-02.2	-01.0	-03.8	-	03.4	03.9	02.0	97	97	45	81	N	2	N	3	NF	3
5	590.7	591.5	591.5	-01.2	00.0	-01.4	-01.0	00.0	-02.2	-	04.0	02.6	02.0	96	56	48	67	E	2	E	2	NE	3
6	590.6	590.6	591.0	-04.0	-00.5	-03.6	-02.9	00.0	-04.4	-	02.0	02.2	02.1	58	45	55	55	NE	4	NNE	5	N	6
7	591.0	591.0	591.1	-04.6	-02.0	-03.6	-03.4	-01.6	-04.6	-	02.5	02.6	03.0	77	66	84	76	N	6	N	3	N	4
8	588.6	589.9	589.4	-04.2	-04.2	-04.4	-04.3	-03.6	-04.6	-	03.2	03.2	03.2	96	96	96	96	N	9	N	7	N	8
9	589.4	591.8	592.3	-06.2	-03.4	-04.0	-04.4	-03.2	-06.2	-	02.7	03.5	03.3	94	97	96	96	N	8	N	7	N	2
10	592.7	591.9	589.1	-03.4	00.0	-00.8	-01.2	00.0	-04.2	-	03.5	04.2	03.9	97	91	90	93	S	2	S	5	SW	7
11	586.0	585.0	584.6	-02.4	-00.8	-01.6	-01.6	00.0	-02.4	-	03.8	04.3	04.0	98	99	98	98	SW	10	SW	9	SW	9
12	584.6	585.0	585.5	-00.2	00.6	00.2	00.2	01.0	-01.6	-	04.4	04.6	04.7	97	97	100	98	SW	7	SW	7	SW	9
13	587.2	588.4	588.0	-01.2	01.2	00.8	00.4	01.4	-01.8	-	04.2	04.3	04.7	99	85	97	94	SW	7	SW	7	S	3
14	585.1	583.4	582.4	01.0	-00.6	-05.0	-02.4	01.4	-05.0	-	04.6	04.4	03.0	9									

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$$H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Instalacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	06	020	00	02.7	07.8	.	96	V0-24, $\equiv 0-4^{\circ}$, $\star 4^{\circ} 24$, $\boxed{60}$, \odot	
2	7	10	09	10 \equiv *	05.7	00.0	.	93	V0-24, $\equiv 0-4^{\circ}$, $\star F_{sw} 2^{\circ} 24$, $\equiv 06^{\circ} 11^{\circ} 16^{\circ} 26^{\circ} 24^{\circ} + 17^{\circ} 24^{\circ} + 17^{\circ} 24^{\circ}$, $\boxed{60}$, \odot	
3	0	10	10	10	10.0	00.0	00.2	98	V0-24, $F_{sw} 0-24$, $\equiv 0-8^{\circ}$, $\star 0-4^{\circ} 4$, $+ 0-14^{\circ}$, $\equiv \equiv 8^{\circ} 24$, $\boxed{60}$	
4	0	05	10	10	08.3	00.0	.	98	V0-24, $F_{sw} 0-24$, $\equiv 0-6^{\circ}$, $\equiv 0-6^{\circ} 24$, $+ 11^{\circ} 24$, $\boxed{60}$	
5	0	10	10	10 \equiv *	10.0	00.0	.	98	V0-24, $F_{sw} 0-24$, $\equiv 0-24$, $+ 0-24$, $8^{\circ} 17^{\circ} 23^{\circ} 24$, $\boxed{60}$	
6	0	10	10	10	10 \equiv *	10.0	00.0	15.5	117	V0-24, $F_{sw} 0-12^{\circ}$, $20^{\circ} 24$, $\equiv 0-24$, $\star 0-2^{\circ} 15^{\circ} 24^{\circ} + 0-24$, $\boxed{60}$
7	0	10	10	10 \equiv *	10	10.0	00.0	17.3	132	V0-24, $\equiv 0-24$, $+ 0-3$, $14^{\circ} 24$, $\star 0-2^{\circ} 11^{\circ} 17^{\circ} 23^{\circ} 24$, $\star F_{sw} 0-24$, $\boxed{60}$
8	0	10	10	10	10 \equiv *	10.0	00.0	07.6	145	V0-24, $\equiv 0-24$, $+ 0-4^{\circ} 24$, $\star 0-2^{\circ} 14^{\circ} 24$, $\star F_{sw} 0-6^{\circ}$, $\boxed{60}$
9	0	10	10	10	10	10.0	00.0	09.6	157	V0-24, $\equiv 0-24$, $\star 21^{\circ} 24$, $\boxed{60}$
10	8	10	00	00	10	06.7	05.8	01.6	163	V0-24, $\equiv 0-7^{\circ} 13^{\circ} 24$, $\star 0-2^{\circ}$, $\boxed{60}$, \odot
11	8	10 \equiv *	000	10	06.7	09.6	02.3	165	V0-24, $\equiv 0-7^{\circ} 18^{\circ} 24$, $\star 2^{\circ} 7^{\circ} 7^{\circ} 18^{\circ}$, $\boxed{60}$, \odot	
12	8	000	010	00	00.3	11.0	00.0	162	V0-24, $\equiv 0-2^{\circ}$, $\star 14^{\circ} 24$, $\boxed{60}$, \odot	
13	8	000	000	00	00.0	10.9	.	161	V0-24, $\equiv 0-13^{\circ} 24$, $\boxed{60}$, \odot	
14	8	080	09	00	05.7	06.6	.	159	V0-24, $\equiv 0-24$, $\equiv 15^{\circ} 20^{\circ}$, $\boxed{60}$, \odot	
15	0	10	10	10 \equiv *	10.0	00.0	.	158	V0-24, $\equiv 0-5^{\circ}$, $F_{sw} 3-24$, $\equiv 5^{\circ} 24$, $\star 9^{\circ} 21^{\circ} 24$, $+ 9^{\circ} 24$, $\boxed{60}$	
16	0	10	10	02	07.3	00.0	03.4	166	V0-24, $F_{sw} 0-6$, $\equiv 0-9^{\circ} + 0-6^{\circ}$, $\boxed{60}$	
17	8	000	030	00	01.0	10.9	.	164	V0-12^{\circ}, $F_{sw} 2^{\circ}$, $\boxed{60}$, \odot	
18	8	050	030	01	03.0	09.8	.	162	F_{sw} , $wsw 0^{\circ}$, 24 , $\boxed{60}$, \odot	
19	8	040	000	00	01.3	09.8	.	157	E_{sw} , $0-24$, $\boxed{60}$, \odot	
20	8	080	080	08	08.0	05.4	.	140	E_{sw} , $0-24$, $\boxed{60}$, \odot	
21	9	000	000	00	00.0	11.7	.	120	$E_{sw} 0-7^{\circ}$, $\boxed{60}$, \odot	
22	9	000	000	07	02.3	10.8	.	100	$E_{sw} 20^{\circ}$, 24 , $\boxed{60}$, \odot	
23	9	070	10	05	07.3	02.8	.	90	$E_{sw} 0-22^{\circ}$, $\boxed{60}$, \odot	
24	8	030	050	06	04.7	09.8	.	65	$E_{sw} 21^{\circ}$, 24 , $\boxed{60}$, \odot	
25	8	09	10	00	06.3	00.2	.	60	$E_{sw} 0-24$, $\boxed{60}$, \odot	
26	8	030	08	02	04.3	06.0	.	52	E_{sw} , $sw 0-10^{\circ}$, 21° , $\boxed{60}$, \odot	
27	8	040	080	04	05.3	07.4	.	46	E_{sw} , sw , $sw 0-5^{\circ}$, $15^{\circ} 15^{\circ} 20^{\circ} 18^{\circ} 20^{\circ}$, $\equiv 18^{\circ} 19^{\circ}$, $\boxed{60}$, \odot	
28	7	10	070	01	06.0	05.1	03.5	47	$\equiv 6^{\circ} 11^{\circ} 11^{\circ} 12^{\circ} 13^{\circ} 15^{\circ} 16^{\circ}$, $\boxed{60}$, \odot	
29	9	000	070	10	05.7	09.6	00.6	46	$E_{sw} 0-23^{\circ}$, 30° , 40° , 10° , $\boxed{60}$, \odot	
30	1	10	10	10	10.0	00.0	.	42	$\equiv 11^{\circ} 11^{\circ} 21^{\circ} 24$, $\star 21^{\circ} 23^{\circ}$, $\boxed{60}$	
31	0	10 \equiv *	10 \equiv *	10 \equiv *	10.0	00.0	00.8	40	$\equiv 0-24$, $\star 2^{\circ} 6^{\circ}$, $14^{\circ} 22^{\circ}$, $\star 10^{\circ} 11^{\circ}$, $\star 13^{\circ} 14^{\circ}$, $\boxed{60}$	

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1	0	10	10	10	10	10.0	00.0	01.2	41	≡ 0-24, * 10°5 M, \star	
2	C	10	10	10	10	10.0	00.0	00.0	40	≡ 0-24, \star	
3	1	00	00	10	10	06.7	06.1	.	40	≡ 0-6°20' 10°45' 24, # 32° 15°45' \star , \odot	
4	8	09	04	00	00	04.3	07.6	.	39	≡ 0-0° 10	
5	8	10	09	06	06	08.3	03.1	.	38	≡ 6°30' 17°30' * 18°05' 18°00' \star , \odot	
6	8	08	06	04	04	06.0	09.5	00.0	38	F _N -NNE-NE M-24, \star , \odot	
7	8	09	09	08	08	05.7	05.0	.	37	F _N 0-24, ≡ 22°24' 24, \star , \odot	
8	0	10	*	10	*	10.0	00.0	03.1	39	F _N 0-24, V 0-24, ≡ 0-24, * 0°25' 21°40' + 2° 0°3° 24, \star	
9	0	10	10	10	10	10.0	00.0	03.0	44	F _N 0-17°, ≡ 0-17° V 0-24, + 2° 0-14°, ≡ 11° 14°, \star	
10	9	00	00	07	07	04.7	08.1	.	40	V 0-24, F _{sw} 17°24', \star , \odot	
11	0	10	10	10	*	10.0	00.0	.	39	V 0-24, F _{sw} 0-24, ≡ 5°24, + 8°10' 10°45' + 2° 8°24, * 16°24, \star	
12	0	10	*	10	*	10.0	00.0	00.6	40	V 0-24, F _{sw} 0-24, ≡ 0-24, * 0-8°45' + 2° 0-11, + 12°20' 20°40' + 44°26' 16°30' \star	
13	9	02	08	10	10	06.7	02.0	02.2	44	V 0-24, F _{sw} 0-16° ≡ 0-9°, ≡ 16°24, * 16°40' 20°30', \star , \odot	
14	0	10	10	10	*	10.0	00.0	03.2	47	V 0-24, ≡ 0-24, + 14°24' 17°30' * 17°24' 18°05' * 18°05' 24, \star	
15	0	10	*	10	*	10.0	00.0	03.0	47	V 0-24, ≡ 0-24, * 0-8°45' 15°24, F _N 3°30' 14°24, + 2° 5°30' 14°24, * 21°45' 24, \star	
16	0	10	*	10	*	10	00.0	09.0	56	V 0-24, ≡ 0-24, + 2° 0-24, * 0-24, F _N 20°24' 24, \star	
17	C	10	10	*	10	*	10.0	00.0	13.6	72	V 0-24, ≡ 0-24, * 0-1, 13°24, + 2° 0-02°30' F _N -UNE 0-18° \star
18	C	10	*	10	*	10	10.0	00.0	14.2	83	V 0-24, ≡ 0-24, * 0-8°, 3°26' 26' 23°24, + 2° 9°24, F _N 14°52' 24, \star
19	0	10	10	*	10	10.0	00.0	09.9	92	V 0-24, ≡ 0-24, * 0-3, 13°26' 16°20' F _N 0-24, + 2° 0-24, \star	
20	8	10	02	00	00	04.0	09.6	01.4	94	V 0-15, ≡ 0-9°, F _N 0-7°30' 23°24, + 2° 0-4, \star , \odot	
21	8	00	06	10	10	05.3	10.3	.	86	F _N 0-8°, ≡ 18°24, * 19°24, 19°45' \star , \odot	
22	C	10	10	*	10	10.0	01.3	00.2	78	≡ 0-24, F _N 8°30' 10°40' 15°24, + 2° 7°24, 15°30' + 13°24, V 23°24, \star , \odot	
23	7	10	06	00	00	05.3	06.5	00.6	79	≡ 0-8°56' 12°20' 12°40' + 2° 0-8°45' F _N 0-7°20', V 0-10°, + 11°40' 13°, \star , \odot	
24	8	00	06	04	04	03.3	08.6	00.1	77	F _{sw} 9-24, ≡ 15°16' 18°45' \star , \odot	
25	8	10	10	10	10	10.0	00.0	.	73	F _{sw} 0-24, + 2° 8-9°30' * 8-9°45' 14°30' 23; ≡ 15-24, \star	
26	0	02	10	*	10	07.3	02.1	04.0	78	≡ 0-24, * 0°2 2, 10°32' 14°40' + 3°24' 24, F _{sw} 3°24' 24, V 8-24, \star , \odot	
27	8	10	10	10	10	10.0	00.0	03.6	84	≡ 0-9°16' 19°15' 24, V 0-15°20' 20-24, F _{sw} -ew 0-24, + 2° 0-9°16°20' 23; * 16°30' 17°45' \star	
28	8	09	10	10	10	05.7	01.6	01.4	83	≡ 0-0°15°24, V 0-9°, F _{sw} 0-24, + 15°17°30' 20-24, \star , \odot	
29	8	10	08	08	08	06.7	01.4	05.7	70	≡ 0-24, F _{sw} 0-24, + 4°25' 5° \star , \odot	
30	8	08	10	10	*	05.3	06.0	.	65	F _{sw} 0-24, + 10°20' 16°30' 24, ≡ 16°24, + 2° 17°24, V 18°24, \star	

$\varphi = 43^{\circ}43'$, $N \lambda = 18^{\circ}16'$, E Gr. $\Delta G = +1h\ 13\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodenih parova e mm			Relativna vlažnost v%			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	575.9	578.3	579.9	-02.4	-00.4	-00.6	-01.0	-00.4	-02.4	-	03.6	04.4	04.4	94	100	99	98	S	9	S	4	-	0
2	581.8	584.7	586.0	-00.4	00.0	-00.4	-00.3	00.0	-00.6	-	04.3	04.4	04.3	96	97	96	96	SW	6	NW	7	NW	3
3	588.3	588.7	587.8	00.4	01.0	00.4	00.6	01.8	-00.6	-	04.4	04.8	04.7	94	97	100	97	W	2	SW	7	SW	9
4	586.1	584.0	585.0	-01.8	-01.6	-01.4	-01.6	00.4	-02.0	-	03.9	04.0	04.1	98	98	99	98	SW	7	SW	9	SW	10
5	583.3	584.8	585.3	-01.6	-00.2	-00.8	-00.8	-00.2	-01.6	-	04.0	04.5	04.3	98	100	99	99	SW	9	SW	7	SW	7
6	585.6	587.0	588.0	-01.8	00.0	-00.8	-00.8	00.0	-02.4	-	03.9	04.4	04.3	98	97	99	98	SW	8	SW	8	SW	7
7	591.0	592.4	592.5	-00.8	01.2	00.0	00.1	01.4	-01.4	-	04.3	03.4	04.4	99	68	97	88	SW	7	SW	6	SW	7
8	593.0	592.7	590.6	-00.4	02.2	-00.6	00.2	02.2	-01.0	-	04.5	05.4	04.4	100	100	99	100	SW	2	S	2	N	6
9	589.2	589.4	589.9	-02.6	-02.0	-02.8	-02.6	-00.6	-03.0	-	03.7	03.9	03.6	97	98	97	97	N	8	N	6	NNE	6
10	589.7	591.7	592.3	<u>-03.2</u>	-01.4	-00.2	-01.2	00.0	<u>-04.0</u>	-	03.5	04.1	04.5	97	99	100	99	N	8	NF	4	WSW	3
11	593.0	594.6	594.7	00.2	01.0	02.4	01.5	02.8	-00.2	-	04.5	04.9	04.5	97	100	83	93	W	3	SW	2	SW	7
12	594.3	595.0	596.1	03.0	04.4	01.4	02.6	05.2	01.4	-	04.3	04.1	04.9	76	65	97	75	SW	10	SSW	5	N	3
13	596.3	597.7	598.2	-00.2	02.0	03.4	02.2	03.4	-00.2	-	04.5	05.1	04.1	100	97	70	89	N	5	N	2	W	2
14	597.1	596.7	595.5	03.4	07.6	05.0	05.2	07.6	02.4	-	04.1	04.3	04.4	70	55	68	64	NW	4	W	2	SW	4
15	593.0	590.7	589.1	01.4	-02.4	-02.3	-01.4	05.0	-03.0	-	05.1	03.8	03.8	100	98	98	99	N	2	N	5	N	5
16	588.5	589.6	590.8	-02.6	-00.6	-C1.0	-C1.3	-00.4	-C3.2	-	03.7	04.4	04.2	97	100	99	99	N	2	NW	3	NW	3
17	591.4	593.1	593.5	00.0	01.6	-00.4	00.2	01.8	-01.6	-	04.2	05.1	04.5	92	100	100	97	SW	3	SW	4	N	3
18	592.8	594.0	593.1	-01.0	00.0	01.0	00.2	01.0	-01.1	-	04.2	04.6	04.9	99	100	100	100	N	7	N	4	N	4
19	592.8	593.4	594.7	01.0	01.8	02.4	01.9	02.4	00.7	-	04.9	05.2	05.4	100	100	100	100	N	9	N	8	N	6
20	595.0	595.8	595.9	02.0	05.4	04.6	04.2	05.8	01.8	-	05.3	04.3	04.9	100	64	77	80	N	6	N	5	N	5
21	596.0	595.9	595.2	02.4	03.6	03.2	03.1	04.6	02.0	-	05.3	05.8	05.6	57	57	57	57	N	5	N	5	N	6
22	595.1	592.7	588.5	03.4	07.6	04.2	04.8	07.6	02.0	-	04.4	04.9	04.0	76	62	97	78	N	3	SW	5	SW	6
23	587.0	587.8	587.3	-02.8	00.0	00.6	-00.4	04.2	-02.8	-	03.6	04.3	04.6	97	94	97	96	NW	8	NF	3	NF	3
24	586.8	587.3	587.2	00.6	03.0	02.6	02.2	03.4	00.6	-	04.6	05.4	05.4	97	94	97	96	NF	3	SW	5	SW	6
25	589.7	592.2	593.6	01.4	03.4	01.8	02.1	03.4	01.4	-	04.9	05.2	04.3	97	89	83	90	SW	9	NW	4	-	0
26	595.4	596.4	596.3	00.0	04.0	04.2	03.1	04.8	-00.6	-	04.2	03.6	03.4	91	59	55	68	NW	2	C	-	0	0
27	595.2	595.6	594.8	03.6	06.5	05.8	05.4	07.4	02.8	-	02.6	02.9	03.5	44	40	51	45	NW	3	N	2	-	0
28	593.0	592.2	590.4	06.8	09.0	06.0	07.0	09.4	04.2	-	04.2	04.2	03.9	57	48	55	53	SW	4	SW	5	SSW	6
29	588.5	590.8	592.2	02.8	03.0	03.2	03.0	06.2	02.4	-	05.1	04.8	05.3	92	84	92	89	S	8	W	4	W	4
30	595.0	597.2	597.5	04.2	07.4	08.0	08.9	09.0	03.0	-	05.2	05.8	05.7	84	75	71	77	N	3	N	2	NW	4
31	597.3	587.7	597.5	07.8	<u>10.0</u>	06.8	07.8	<u>10.6</u>	06.4	-	05.4	05.6	05.3	68	61	72	67	SSW	7	SSW	8	SSW	7
MES.	WRED.			590.9	591.3	591.6	00.7	02.5	01.8	01.7	03.5	00.0	-	04.3	04.6	04.6	90	85	88	88	5.5	4.6	4.7

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1	595.4	594.9	595.8	05.2	07.6	04.2	C5.3	08.0	04.2	-	06.0	07.8	06.2	90	100	100	\$7	SSW	A	SW	C	WWH	7
2	595.9	596.0	595.4	03.0	02.2	02.0	02.3	04.4	01.4	-	05.7	05.4	05.3	100	100	100	100	N	8	N	2	N	3
3	595.7	597.7	596.2	01.2	02.4	02.6	02.3	03.0	01.0	-	05.0	05.4	05.6	100	100	100	100	NNE	0	N	9	N	7
4	598.3	600.0	594.6	03.4	08.4	09.0	07.4	09.0	02.0	-	05.8	05.7	03.6	100	69	42	70	N	7	NE	-	0	0
5	598.0	599.1	598.2	10.6	11.4	10.0	10.6	12.4	08.7	-	02.6	05.2	05.6	28	52	61	47	-	0	SW	1	-	0
6	597.0	596.0	594.5	10.6	11.0	07.5	09.2	12.0	07.5	-	02.6	06.0	05.2	28	60	66	51	SW	4	SW	6	WSW	6
7	593.3	594.6	595.3	06.0	06.8	02.0	04.2	07.6	02.0	-	07.0	07.4	05.3	100	100	100	100	SW	5	SW	2	N	3
8	596.1	596.8	596.0	-01.0	05.0	05.4	03.7	06.6	-03.0	-	02.3	04.8	04.5	57	73	67	64	N	3	NW	1	SW	2
9	594.7	593.2	592.4	05.0	08.4	06.2	06.4	08.4	04.7	-	03.9	05.2	04.2	60	63	59	61	SW	6	SSW	8	SSW	7
10	590.7	590.2	589.3	04.2	06.6	05.6	05.5	06.6	04.0	-	06.2	05.1	06.0	100	70	88	86	SSW	7	SSW	7	SSW	7
11	586.2	586.2	587.9	00.4	-01.2	-01.4	-01.0	05.6	-01.6	-	04.4	04.0	04.0	94	96	98	96	SW	3	NW	7	NW	0
12	589.2	589.4	588.6	<u>-02.8</u>	-00.4	-02.2	-01.9	-00.4	-02.8	-	03.6	04.3	03.8	97	97	98	97	NW	8	NW	3	NW	7
13	587.2	587.6	588.5	-00.6	01.6	00.2	00.4	01.6	<u>-03.4</u>	-	04.4	04.5	04.5	99	88	97	95	NNW	2	SW			

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 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Intenziteta broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena	
		14	7	14	21	Sred Dnes				7	7
1	0	10≡	10≡	08	09.3	00.0	04.2	67	F-Fs-sw 0-12 ⁰ ≡ 0-16 ³⁰ 22 ⁴⁵ 24; * 0-4 ³⁰ 9 ⁰ 16 ⁰ , 22 ³⁰ 24; + + 0-8 ⁰ , V0-24, # 30 ⁰ 16 ⁰ , [22 ⁰ ,]		
2	0	10≡*	10≡	03	07.7	00.0	02.2	68	≡ 0-15 ⁰ V0-24, * 8 ⁰ , F-NW 3 ⁰ 15 ⁰ , []		
3	0	03	10≡	10≡	07.7	00.0	.	66	V0-10 ³⁰ 22 ⁴⁵ 24, # 30 ⁰ 16 ⁰ , F-SW 1 ²⁰ 24, = 8 ³⁰ 24, []		
4	0	10≡*	10≡*	10≡*	10.0	00.0	00.0	62	≡ 0-24, F-Fsw 0-24, V0-24, * 5 ³⁰ 7 ⁴⁰ , M ²⁰ 23 ⁴⁰ , + + 7 ³⁰ 24, []		
5	0	10≡	10≡	10≡	10.0	00.0	05.0	67	≡ 0-24, F-Fsw 0-24, V0-24, + + 0-24, * 11 ³⁰ 15 ³⁰ 17 ³⁰ , []		
6	0	10≡	10≡	10≡	10.0	00.0	00.1	68	≡ 0-24, F-Fsw 0-24, V0-24, + + 0-24, A 4 ³⁰ 17 ³⁰ , []		
7	0	10≡	10≡	10≡*	10.0	00.0	00.0	65	≡ 0-10 ³⁰ 13 ³⁰ 24, F-N 0-24, + + 0-6 ³⁰ 16 ³⁰ 24, V0-11 ²⁰ * 16 ⁰ -23 ³⁰ , []		
8	0	10≡	10	10≡	10.0	00.0	01.4	68	≡ 0-24, F-N-SW 0-40, 17 ³⁰ 24, V0-9 ³⁰ 22 ³⁰ 24, + + 0-2 ³⁰ , A 15 ³⁰ 16 ³⁰ 18 ³⁰ , []		
9	0	10≡	10≡	10≡	10.0	00.0	00.4	67	≡ 0-24, F-N-NNE-NE 0-24, V0-24, A 15 ³⁰ 20 ³⁰ , []		
10	8	10≡	04○	00	04.7	10.0	00.5	68	≡ 0-8, V0-13 ³⁰ , F-N-NNE-NE 0-11 ³⁰ , [], ○		
11	8	01○	05○	00	02.0	11.0	.	64	F-Fsw 10 ³⁰ 24, [], ○		
12	8	00	05○	10≡	05.0	05.5	.	52	F-Fn-sw 0-16 ³⁰ 24, = 12 ³⁰ 24, + 20 ³⁰ 22 ⁴⁰ , [], ○		
13	8	10≡	08○	03	C7.0	02.1	C1.2	40	[] , ○		
14	8	04○	07○	03	04.7	09.5	.	36	≡ 0-24, F-N-NNE-NE 0-24, V0-24, A 15 ³⁰ 20 ³⁰ , []		
15	0	10≡*	1C≡*	10≡*	10.0	00.0	02.4	34	≡ 0-24, * 3-7 ³⁰ * 7 ³⁰ 14 ³⁰ 19 ³⁰ 22 ³⁰ , + + 12 ³⁰ 24, F-N 12 ³⁰ 24, V16 ¹⁵ 24, []		
16	0	10≡	10≡	04	08.0	04.2	05.4	43	≡ 0-14 ⁴⁵ + + 0-6, F-N 0-6 ¹⁵ , V0-24, # 7 ³⁰ 13 ³⁰ , [], ○		
17	0	08	1C≡	10≡	C5.3	00.0	02.3	42	≡ V0-8 ³⁰ F-N-wsw 0-9 ³⁰ 24, * 10 ³⁰ 10 ³⁰ , 9 ³⁰ 24, + 12 ³⁰ 13 ³⁰ , + 14 ³⁰ 18 ³⁰ , []		
18	0	10≡	10≡	10≡	10.0	00.0	02.7	40	≡ 0-24, F-E 0-24, # 3 ³⁰ 4 ³⁰ , 16 ³⁰ 22 ³⁰ , []		
19	0	10≡	10≡	10≡	10.0	00.0	00.9	37	≡ 0-24, F-Fn 0-24, []		
20	8	10≡	06	06	07.3	04.5	.	35	≡ 0-9 ¹⁵ , F-Fn 0-8 ³⁰ , [], ○		
21	0	10≡	10≡	10≡	10.0	00.0	.	34	F-N 0 ³⁰ 24, = 4 ³⁰ 24, * 7 ³⁰ 17 ³⁰ 10 ²⁵ 10 ³⁵ 16 ³⁰ 18 ³⁰ , []		
22	8	C6○	08	10≡*	08.0	08.1	02.3	33	≡ 0-5 ⁴⁰ , 20 ³⁰ 24, F-Fn-sw 0-24, + 19 ³⁰ 24, F-22 ³⁰ 24, [], ○		
23	8	00≡	C7	C7	04.7	04.7	03.8	35	F-Fn-sw 0-9 ³⁰ 24, = 0-11 ¹⁵ , 0-15 ³⁰ 15 ³⁰ 22 ³⁰ 24, V2 ³⁰ 12 ³⁰ , [], ○		
24	8	10≡	10●	10≡*	10.0	00.7	00.0	35	≡ 0-2 ³⁰ , F-Fsw 0-20 ³⁰ , * 4 ³⁰ 6 ³⁰ 7 ³⁰ 8 ³⁰ 11 ³⁰ , # 300-600 8 ³⁰ 12 ³⁰ , [], ○		
25	8	10●	00○	00	C3.3	01.4	04.3	35	≡ 2 ³⁰ 8 ³⁰ , [], ○		
26	8	10≡	01○	00	03.7	09.5	C1.3	32	F-Fsw 0-24, # 8 ³⁰ 17 ³⁰ , [], ○		
27	8	00○	02○	00	00.7	14.3	.	32	F-Fsw 0-24, # 8 ³⁰ 17 ³⁰ , [], ○		
28	9	02○	08	07	05.7	09.0	.	27	F-Fsw 0-24, # 8 ³⁰ 17 ³⁰ , [], ○		
29	0	10≡	10≡*	03	07.7	00.9	11.2	20	F-E 0-9 ¹⁰ = 1 ³⁰ 15 ²⁰ , * 2 ³⁰ 4 ³⁰ 12 ³⁵ 14 ⁵⁰ , ▲ 12-12 ³⁵ , [], ○		
30	8	02○	08	04	04.7	09.2	14.0	15	≡ 10 ³⁰ 13 ³⁰ , # 10 ³⁰ 13 ³⁰ , = 11 ³⁰ 12 ³⁰ , [], ○		
31	9	03○	08○	06	05.7	07.1	.	13	F-Fsw 0-24, [], ○		
MES.											
WRED.		07.4	08.0	06.6	07.3	111.7	65.7				

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1	0	10≡*	1C≡	10≡	10≡	1C-C	00.0	11.1	1C	F-Fsw-sw-wew-nw 0-24, ≡ 2 ³⁰ 24, ▲ 4 ³⁰ 4 ⁵⁰ , * 4 ³⁰ 7 ³⁰ 21 ⁴⁵ 24, []	
2	0	10≡*	10≡*	10≡*	10.0	00.0	14.9	08	F-N-NNE-NW-NNW 0-24, ≡ 0-24, * 0-2 ³⁰ , 9 ³⁰ 24, []		
3	0	10≡*	10≡	10≡	10.0	00.0	05.3	04	F-F 0-24, ≡ 0-24, * 0-8 ³⁰ , []		
4	8	10≡	04○	00	04.7	C8.1	.	C3	F-Fn 0-8 ³⁰ , []		
5	8	01○	04○	C6	C3.7	11.1	.	02	# 800-800 23 ³⁰ 8 ³⁰ 17 ³⁰ 17 ³⁰ , F-19 ³⁰ 22 ³⁰ , [], ○		
6	8	08	09	05	07.3	04.4	.	01	# 800-4 ³⁰ 8, F-Fsw 9-24, * 9 ³⁰ 10 ³⁰ , [], ○		
7	0	10≡	10≡	10≡	10.0	00.0	06.6	.	F-Fn-sw 0-8 ³⁰ 21 ³⁰ 24, = 1 ³⁰ 24, * 2 ³⁰ 19 ³⁰ 22 ³⁰		
8	8	00○	05○	00	01.7	10.8	05.9	.	= 0-3 ²⁵ , F-Fsw 4 ³⁰ 24, # 800-5 ³⁰ 7 ³⁰ , * 10 ³⁰ 10 ³⁰ , ○		
9	8	09	09	04	07.3	03.8	.	.	F-Fsw 0-24, ≡ 3 ³⁰ 11 ³⁰ , [], ○		
10	8	10≡	08	10	09.3	01.2	00.0	.	≡ 2 ³⁰ 6 ³⁰ 20 ³⁰ 24, Fsw 3-23, # 3 ³⁰ 4 ³⁰ 20 ³⁰ , [], ○		
11	0	10	10≡*	1C≡*	10.0	00.0	03.2	01	F-Fsw-sw-wew-nw 0-24, ≡ 1-6 ⁰ 9 ³⁰ 24, * 1 ³⁰ 10 ³⁰ * 1 ³⁰ 5 ³⁰ 18 ³⁰ 24, # 300-600 6 ³⁰ 9 ³⁰ 2 ³⁰		
12	8	10≡	05○	10≡*	08.3	03.7	00.2	01	F-Fn-sw 0-10 ³⁰ 4 ³⁰ , # 0-7 ³⁰ 16 ³⁰ 21 ³⁰ , * 0-16 ³⁰ 4 ³⁰ , L-10 ³⁵ V16 ²⁹ 24, + + 20 ³⁰ 24, []		
13	9	04○	04	10≡	06.0	08.1	00.1	01	E 21 ³⁰ ; V0-15 ³⁰ , []		
14	0	01○	10≡	10≡	07.0	04.4	C1.1	C1	Fsw 3 ³⁰ 23, # 3 ³⁰ 6 ³⁰ 4 ³⁰ 9 ³⁰ , = 9 ³⁰ 10 ³⁰ * 9 ³⁰ 11 ³⁰ , = 13 ³⁰ 23 ³⁰ , [], ○		
15	9	03	03○	10≡	05.3	07.5	.	.	= 2 ³⁰ 6 ³⁰ 20 ³⁰ 24, Fsw 3-4 ³⁰ 4 ³⁰ 20 ³⁰ , [], ○		
16	0	00○	00≡	00≡	00.0	03.7	00.0	.	≡ 0-2 ⁴⁵ 7 ³⁰ 24, [], ○		
17	8	10≡	08○	08	08.7	04.4	C1.3	.	≡ 0-10 ³⁰		
18	8	00○	07	04	03.7	05.1	.	.	13 ³⁰ 15 ³⁰ 16 ³⁰ , # 15 ³⁰ 15 ³⁰ , = 17 ³⁰ 18 ³⁰ , [], ○		
19	0	10≡	10≡	10≡	10.0	00.0	09.0	.	# 100-600 4 ³⁰ 4 ³⁰ 4 ³⁰ , = 4 ³⁰ 24, F-N 5 ³⁰ 24, # 13 ³⁰ 17 ³⁰ , [], ○		
20	0	10≡	1C≡	10≡	10.0	03.7	00.5	.	≡ 0-24, F-Fn 0-10 ³⁰ , [], ○		
21	0	10≡	10≡*	10≡	10.0	00.0	.	.	≡ 0-23 ³⁰ * 12 ³⁰ 17 ³⁰ , # 6 ³⁰ 23 ³⁰ , [], ○		
22	8	C2○	10	04	05.3	06.3	C1.8	.	F-Fsw 4 ³⁰ 24, [], ○		
23	8	08○	06○	08	07.3	06.0	04.0	.	F-Fsw 4 ³⁰ 24, ≡ 0-2 ³⁰ 5 ³⁰ , # 11 ³⁰ 14 ³⁰ 24, [], ○		
24	8	09	10	10≡	05.7	C2.6	.	.	F-Fsw 0-11 ³⁰ ≡ 0-4 ³⁰ 9 ³⁰ 10 ³⁰ , # 0-2 ³⁰ 9 ³⁰ 10 ³⁰ , [], ○		
25	7	09	08	08	08.3	00.0	01.7	.	* 6 ³⁰ 4 ³⁰ 9 ³⁰ , [], ○		
26	9	04○	04○	05	04.3	13.5	C1.1	.	F-Fsw 0-24, ≡ 15 ³⁰ 15 ³⁰ , = 22 ³⁰ 24, [], ○		
27	9	10	07	09	08.7	06.8	.	.	F-Fsw 0-12 ³⁰ 17 ³⁰ 24, = 0-17 ³⁰ 22 ³⁰ 24, * 0-2 ³⁰ 4 ³⁰ 22 ³⁰ , [], ○		
28	0	10≡	10≡	09	09.7	00.0	04.4	.	F-Fsw 0-24, ≡ 0-21 ³⁰ 13 ³⁰ 12 ³⁰ 24, [], ○		
29	0	10≡	10≡	10≡*	10.0	00.0	01.4	.	F-Fsw 0-12 ³⁰ ≡ 0-12 ³⁰ 14 ³⁰ 17 ³⁰ , [], ○		
30	0	10≡*	10≡	10≡	10.0	00.0	13.8	.	F-Fsw-sw-wew-nw 0-24, ≡ 0-12 ³⁰ 14 ³⁰ 17 ³⁰ , [], ○		
MES.											
WRED.		07.3	07.7	07.7	07.5	115.2	87.4				

$\varphi = 43^{\circ}43'$ N $\lambda = 19^{\circ}10'$ E Gr. $\Delta G = +1h\ 13\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°									Napon vodenе pare e mm			Relativna vlažnost u%			Pravac i jačina vetro D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	593.6	597.7	598.4	04.4	09.2	10.2	08.5	11.6	04.2	-	06.3	04.9	05.0	100	56	53	70	NW	7	K	5	-	0
2	599.0	599.5	599.1	10.6	11.0	08.2	09.5	11.6	08.2	-	04.3	05.8	08.2	45	100	100	82	W	2	-	C	N	3
3	599.5	597.8	595.5	08.6	13.2	10.2	10.6	13.8	05.4	-	02.4	05.4	06.8	29	47	73	50	N	2	S	3	SW	8
4	596.7	596.4	595.3	10.6	13.0	10.2	11.0	13.6	06.6	-	07.0	08.9	08.2	73	79	88	80	Sk	2	SW	2	SSW	2
5	597.2	598.6	598.9	10.4	12.6	11.4	11.4	13.4	08.6	-	06.5	08.6	08.9	69	78	88	78	NW	3	-	0	SW	3
6	598.6	598.9	596.6	13.4	15.0	10.6	12.4	15.2	10.0	-	07.2	07.2	06.6	63	56	65	63	-	0	S	6	SW	6
7	595.1	594.9	593.6	11.8	00.6	00.4	03.2	12.0	-00.2	-	07.3	04.8	04.7	71	100	100	90	SW	3	NNE	0	NNE	1
8	593.4	594.5	595.3	-00.3	01.2	00.8	00.6	01.6	-00.4	-	04.5	05.0	04.9	100	100	100	100	N	0	N	7	N	8
9	595.5	597.7	597.4	00.4	04.8	05.8	04.2	06.2	06.2	-	04.7	04.0	04.7	100	62	68	77	N	0	N	5	N	3
10	597.1	597.7	598.3	06.0	08.8	07.0	07.2	09.6	05.0	-	05.0	04.2	06.8	71	49	90	70	N	4	N	3	S	5
11	598.2	599.3	599.5	05.6	10.6	09.6	08.8	10.8	04.0	-	04.0	05.7	06.7	59	60	74	64	N	6	-	0	NW	4
12	599.2	600.2	600.8	10.8	14.8	12.6	12.7	14.8	09.0	-	05.5	05.0	06.0	56	47	55	53	SW	6	SW	5	SW	4
13	600.3	600.1	598.9	13.8	17.0	12.6	14.0	17.2	11.0	-	05.0	05.4	04.4	42	37	40	40	SW	3	SW	3	SW	5
14	599.1	599.7	599.3	14.2	17.0	12.8	14.2	17.2	10.8	-	05.6	06.7	05.4	46	46	49	47	SW	6	SW	7	SW	6
15	600.2	601.5	601.2	14.7	17.6	14.6	15.2	17.6	12.2	-	05.0	06.2	05.2	41	41	42	41	-	0	S	3	S	3
16	600.2	600.0	600.8	16.2	18.6	16.0	16.7	19.0	13.4	-	04.8	06.4	06.2	35	40	46	40	SW	4	SW	4	SW	4
17	598.0	598.4	596.1	15.2	18.0	14.6	15.6	18.4	14.6	-	05.4	05.4	04.9	41	35	39	38	SW	6	S	9	S	7
18	594.4	593.4	594.1	12.6	15.8	11.6	13.2	15.8	11.6	-	06.1	06.0	07.8	52	44	76	57	SW	4	S	9	S	8
19	597.3	592.3	592.3	10.8	12.8	07.4	09.6	13.0	07.4	-	09.5	07.7	07.5	98	70	98	89	SW	6	S	5	S	4
20	590.9	591.5	591.4	02.2	00.8	-00.5	00.5	07.4	-01.0	-	03.9	04.9	04.4	72	100	100	91	NW	7	NW	7	NW	5
21	589.8	589.9	590.2	00.6	00.8	01.4	01.0	01.4	-00.5	-	04.8	04.9	05.1	100	100	100	100	NW	7	NW	7	NW	7
22	591.9	592.5	592.3	01.6	01.6	01.8	01.7	01.8	00.8	-	05.1	05.1	05.2	100	100	100	100	NW	2	NW	8	NW	9
23	592.0	593.0	595.1	02.6	03.4	03.6	03.3	03.8	01.8	-	05.5	05.8	05.9	100	100	100	100	NW	8	NW	7	NK	7
24	596.7	598.4	596.6	06.0	09.0	08.4	08.0	10.8	03.6	-	06.8	05.9	06.8	97	68	82	82	NW	6	NW	3	NW	3
25	596.6	597.1	596.8	07.6	12.0	05.6	09.7	12.0	07.0	-	05.5	06.6	06.7	70	63	74	69	SW	6	SW	6	SW	4
26	597.1	598.0	598.0	06.4	06.0	05.7	05.7	09.6	05.2	-	07.0	07.0	06.6	98	100	100	99	NW	2	NW	2	NW	2
27	598.0	599.4	599.7	10.0	12.4	11.2	11.2	12.4	05.0	-	02.1	06.9	06.4	23	64	64	50	-	0	-	0	SW	2
28	599.7	600.4	600.6	11.6	13.0	11.6	12.2	13.8	09.6	-	04.4	08.1	06.6	43	68	64	58	SW	2	NF	2	NW	1
29	601.4	601.7	601.7	10.3	13.6	11.6	11.9	14.0	10.0	-	04.6	06.8	08.0	47	58	78	61	-	0	-	C	-	0
30	600.9	600.3	599.7	14.4	15.4	14.7	14.6	17.0	10.0	-	04.2	08.5	06.7	34	65	55	51	-	0	-	0	-	0
31	598.6	598.8	598.8	14.4	15.2	13.2	14.0	17.0	12.2	-	08.1	08.0	10.3	66	61	90	72	-	0	-	C	-	0
MES.	VRED.	596.7	597.4	597.2	09.0	10.8	09.0	09.4	12.0	06.7	-	05.4	06.3	06.4	66	68	76	70	3.6	3.8	4.0		

1	598.7	599.1	599.0	15.0	15.6	13.2	14.2	16.6	12.2	-	07.4	06.2	07.7	58	46	66	57	-	0	NN	?	-	0
2	599.7	599.7	599.9	14.2	16.2	12.8	14.5	16.4	12.0	-	06.7	07.6	07.7	55	55	65	58	N	3	ENE	3	-	0
3	599.7	600.9	601.2	15.2	17.0	14.8	15.4	17.8	12.6	-	05.9	14.5	12.6	46	100	100	82	N	2	ENE	4	ESE	3
4	601.0	601.4	601.9	15.6	19.6	15.6	16.6	16.8	13.6	-	06.4	07.7	06.4	48	45	48	47	S	3	-	C	NNW	3
5	601.1	601.1	601.4	15.8	17.4	15.4	16.0	17.6	14.0	-	04.4	07.3	06.1	32	45	46	42	-	0	-	0	W	3
6	600.2	600.2	599.7	11.0	09.0	06.0	08.0	15.4	06.0	-	09.8	08.6	07.0	100	100	100	100	N	4	I	?	N	5
7	598.0	598.0	597.7	05.0	09.4	11.0	09.1	11.0	03.0	-	04.7	05.7	03.5	72	64	35	57	N	3	N	2	W	7
8	596.0	596.0	594.8	13.0	16.0	12.4	13.4	16.2	10.0	-	04.3	05.9	06.5	38	43	60	47	SW	4	SSW	3	SW	5
9	594.1	593.0	594.3	10.0	11.0	06.0	09.2	13.8	08.0	-	05.6	06.5	08.0	61	66	100	76	S	2	SSW	7	N	5
10	596.5	596.5	594.8	05.4	12.6	09.8	09.4	13.0	04.0	-	04.7	05.6	04.0	70	52	44	55	NNE	2	S	2	SW	5
11	591.6	590.3	591.7	07.6	07.4	01.0	04.2	10.0	01.0	-	06.7	07.7	04.9	86	100	100	95	SSW	5	SW	4	N	7
12	590.8	593.8	594.5	01.8	03.8	02.6	02.7	04.2	00.8	-	05.2	05.1	05.5	100	84	100	95	N	8	N	5	N	4
13	595.0	598.0	599.1	02.2	06.6	07.0	05.7	07.0	02.0	-	05.4	03.9	01.9	100	54	26	60	N	3	N	7	N	7
14	599.6	602.2	602.1	08.0	12.6	11.4	11.0	13.0	07.0	-	05.5	05.1	04.7	65	47	46	53</						

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 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vrijeme 0-9	Obločnost N (0-10)					Insolacija broj sati	Precipitacija P mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8	10≡	040	00	04.7	05.5	02.7	.	.	F _{N-NW} 0-14 ⁰⁰ ≡ 0-8 ⁴⁵ 0 ¹⁵ 3 ⁰⁰ ○	
2	0	030	10≡	10≡	07.7	05.0	.	.	.	F _{N-NW} 0-12 ⁴⁵ 13 ²⁰ ≡ 9 ⁴⁵ 22 ⁰⁰ ○	
3	9	000	010	00	00.3	15.0	02.8	.	.	F _{NW} 17 ⁴⁵ 24 ⁰ ○	
4	1	050	10≡	10≡	08.3	05.1	00.7	.	.	F _{E-O} 0-3 ⁰ 2 ⁴⁵ 2 ⁴⁰ ≡ 50 ⁰⁰ 4 ²⁰ 7 ²⁰ 22 ⁴⁰ 24 ¹ ≡ 7 ³⁰ 22 ⁰ 22 ²⁰ 24 ¹ ○	
5	8	000	080	00	02.7	06.0	.	.	.	F _{N-NW} 0-9 ⁴⁵ 13 ²⁰ ≡ 0-8 ⁴⁵ 20 ⁰ ≡ 0-8 ⁴⁵ 20 ⁰ ≡ 9 ⁴⁵ 9 ⁵⁵ ≡ 15 ²⁰ 10 ⁰ ○	
6	8	000	080	00	02.7	11.2	.	.	.	0-17 ⁵⁰ ≡ 0 ⁰⁰ 2 ⁴⁵ 8 ²⁰ F _S 13 ²⁰ 24 ⁰ ○	
7	0	08	10≡*	10≡	05.3	00.0	.	.	.	F _{E-N-NNE} SW 0-24 ⁰ ≡ 8 ⁴⁵ 24 ¹ ≡ 9 ⁴⁵ 10 ⁰⁵ 18 ⁰⁵ 9 ⁵⁵ ≡ 10 ⁴⁵ 12 ²⁰ ≡ 12 ⁴⁵ 13 ³⁰ ≡ 13 ³⁰ 14 ⁴⁰ ○	
8	C	10≡	10≡	10≡	10	10.0	14.0	0.0	.	F _{E-N-NNE} 0-24 ⁰ V ₃₀₀ 9 ⁰⁰ ○	
9	8	09	050	01	05.0	04.7	.	.	.	F _{E-N} 0-16 ⁰⁰ ≡ 0-4 ⁵⁵ ○	
10	8	10	080	10	05.3	06.2	.	.	.	• 21 ⁴⁰ 24 ²⁰ ≡ 21 ⁴⁰ 24 ⁰ ○	
11	8	010	06	00	02.3	06.7	00.2	.	.	≡ 0-3 ⁴⁵ F _S 0 ¹⁰ 8 ⁰⁰ ○	
12	8	050	010	00	02.0	14.7	.	.	.	F _{NW} 3 ⁴⁰ 11 ²⁰ ○	
13	P	000	000	00	00.0	14.8	.	.	.	○	
14	9	000	000	00	00.0	14.6	.	.	.	F _{E-SW} 0 ²⁰ ○	
15	9	000	000	00	00.0	13.8	.	.	.	F _{E-S} 0-3 ⁰ ○	
16	9	000	010	00	00.3	14.5	.	.	.	○	
17	9	020	020	00	01.3	13.1	.	.	.	F _{E-SW} 1 ⁴⁰ 24 ⁰ ○	
18	9	000	040	00	01.3	13.5	.	.	.	F _{E-SW} 0-0.5 ⁴⁵ 23 ⁴⁵ ○	
19	8	10≡	10	10≡*	10.0	01.3	00.0	.	.	≡ 0.9 ⁴⁵ 14 ⁴⁰ 24 ¹ F _{SW} 2 ⁴⁵ 9 ⁰⁵ ≡ 2 ⁴⁵ 3 ¹⁰ 12 ²⁵ 44 ³⁵ 24 ²⁰ 23 ⁴⁰ ≡ 21 ⁴⁵ 24 ⁰ ○	
20	0	10≡	10≡*	10≡*	10.0	00.0	03.2	.	.	≡ 0.24 ⁰ ≡ 0 ⁰⁰ 3 ⁴⁰ 12 ⁴⁵ 23 ²⁰ ≡ 12 ⁴⁵ 23 ²⁰ ≡ 0-2 ⁴⁵ F _{SW} 4 ⁵⁰ 19 ⁵⁰ ≡ 17 ⁴⁵ 19 ⁴⁰ ○	
21	0	10≡*	10≡	10≡	10.0	00.0	00.3	.	.	≡ 0-24 ⁰ F _{NW} 1 ⁴⁰ 24 ¹ ≡ 2 ⁴⁵ 17 ⁴⁵ 14 ⁴⁵ 20 ⁴⁵ ○	
22	0	10≡*	10≡	10≡	10	00.0	01.0	.	.	≡ 0-24 ⁰ F _{E-SW} 0-24 ⁰ ≡ 2 ⁴⁵ 9 ²⁰ 21 ⁴⁰ 23 ⁴⁰ ≡ 15 ⁴⁰ 16 ⁴⁵ ○	
23	0	10≡	10≡	10≡	10	00.0	00.1	.	.	≡ 0-24 ⁰ F _{NW} 0-24 ⁰ ≡ 8 ⁴⁵ 11 ⁰⁵ ○	
24	8	10≡	07	01	06.0	05.4	00.0	.	.	≡ 0-70 ⁴⁵ F _{NW} 0-9 ⁵⁰ ○	
25	8	010	020	02	01.7	13.3	.	.	.	F _{E-SW} 0 ²⁰ 16 ⁰ ○	
26	C	10≡	10≡	10≡	10.0	00.0	00.0	.	.	≡ 6-24 ⁰ 5 ⁴⁵ 5 ⁵⁵ ○	
27	9	000	000	00	00.0	14.5	.	.	.	≡ 0-0 ³⁰ 1 ⁴⁰ 10 ⁰⁰ 5 ⁴⁵ 9 ²⁰ ○	
28	9	000	010	03	01.3	13.4	.	.	.	○	
29	9	010	020	00	01.0	12.4	.	.	.	≡ 18 ⁴⁰ 19 ⁴⁰ ○	
30	P	000	040	00	01.3	11.1	.	.	.	○	
31	8	000	050	00	01.7	11.2	.	.	.	≡ 2 ³⁰ 7 ³⁰ 21 ⁴⁰ 24 ¹ ≡ 15 ⁴⁰ 16 ⁴⁰ 18 ⁴⁰ 16 ⁴⁰ ○	
MES.	VRED.	04.4	05.4	03.8	04.5	256.4	15.8				

1	8	000	09	00	03.0	08.0	03.2	.	.	T 0-17 ³⁰ 21 ⁰⁰ 24 ¹ ≡ 0 ⁰⁰ 3 ⁰ 8 ⁰ T 10 ⁴⁵ 11 ⁴⁵ 14 ⁴⁵ 15 ⁴⁵ ≡ 15 ⁴⁵ 14 ⁴⁵ 14 ⁴⁵ ○	
2	8	000	020	00	00.7	14.1	02.5	.	.	≈ 0-7 ⁴⁰ 24 ⁰ ○	
3	8	000	040	00	01.3	13.6	.	.	.	≈ 0-7 ⁴⁰ ○	
4	P	000	050	00	01.7	10.8	.	.	.	○	
5	8	000	000	00	00.0	14.2	.	.	.	○	
6	0	10≡	10≡	10≡	10.0	01.1	.	.	.	≡ 5 ⁴⁰ 24 ⁰ ○	
7	8	000	020	00	00.7	12.5	.	.	.	≡ 0-6 ⁴⁰ F _N 3-5 ³⁰ ≡ 5 ⁰⁰ 3 ⁰⁰ 8 ³⁰ ○	
8	P	000	030	03	02.0	13.0	.	.	.	F _N 18 ⁴⁰ 24 ¹ ≡ 15 ²³ 24 ¹ ≡ 23 ⁴⁰ 24 ¹ ○	
9	6	09	10≡*	10≡	05.7	04.4	03.2	.	.	F _{E-SW} -SW 0-5 ⁴⁵ 15 ²⁴ 24 ¹ ≡ 15 ⁰² 13 ⁴⁵ 15 ⁴⁵ ≡ 0-1 ⁴⁰ 13 ²⁰ 15 ³⁰ ≡ 20 ⁴⁰ 15 ²⁰ 20 ⁴⁰ ○	
10	8	030	040	00	02.3	12.8	03.6	.	.	F _{E-SW} -SSW 0-5 ³⁰ 19 ³⁰ 24 ¹ ≡ 0-2 ³⁰ 5 ⁰⁰ 3 ⁰⁰ 9 ¹⁰ ○	
11	0	10*	10≡*	10≡	10.0	00.0	15.8	.	.	F _{E-SSW-SW} -SW 0-24 ¹ ≡ 4 ⁰⁵ 7 ⁰² 14 ⁴⁰ 14 ⁴⁰ 13 ⁴⁵ 6 ⁵⁵ ≡ 14 ⁴⁵ 5 ⁴⁵ 5 ⁴⁵ ≡ 8 ¹⁵ 24 ¹ ○	
12	8	050	08	10≡	07.7	07.6	09.1	.	.	≡ 0-4 ⁴⁰ 17 ²⁰ 24 ¹ F _N 0-24 ¹ ≡ 5 ⁰⁰ 4 ⁵⁰ 9 ²⁰ ○	
13	8	10	06	00	05.3	07.0	00.2	.	.	F _{E-N} 0-24 ¹ ≡ 0-9 ⁴⁰ ≡ 5 ⁰⁰ 8 ²⁰ ○	
14	8	00	01	00	00.3	13.7	00.0	.	.	F _{E-N} 0-24 ¹ ○	
15	8	00	04	00	01.3	12.8	.	.	.	F _{E-N-NNE} 0-24 ¹ ○	
16	7	10	08	10	05.3	04.9	.	.	.	F _{E-N-NNE} 0-24 ¹ ≡ 0 ⁰⁰ 13 ²⁰ 16 ²⁰ 24 ¹ ○	
17	8	00	01	00	00.3	13.3	.	.	.	≈ 0-8 ⁴⁰ F _{E-SW} 0 ²⁰ 7 ³⁰ ≡ 10 ⁰⁰ 4 ⁵⁰ 9 ²⁰ ○	
18	8	00	00	00	00.0	13.6	.	.	.	○	
19	8	00	01	00	00.3	13.2	.	.	.	○	
20	8	00	02	00	00.7	13.0	.	.	.	○	
21	8	04	08	04	05.3	06.7	.	.	.	T 13-15 ⁰⁵ ≡ 15 ⁰⁵ 16 ²⁰ ○	
22	8	00	02	03	01.7	12.2	00.8	.	.	≈ 0 ⁰⁰ 1 ⁴⁰ 9 ²⁰ T 20-12 ¹⁵ ○	
23	8	06	08	00	04.7	05.2	.	.	.	F _{NW} 2-23 ⁴⁰ ≡ 20 ⁰⁰ 10 ⁰⁰ 4 ⁵⁰ 8 ²⁰ ≡ 15 ⁴⁰ 15 ⁵⁵ ○	
24	8	08	06	10	08.0	03.3	00.0	.	.	F _{NW} 4 ⁰⁰ 12 ⁴⁰ ≡ 4 ⁵⁰ 24 ⁰⁰ 6 ⁰⁰ 17 ⁴⁰ ≡ 10 ²⁰ 12 ⁰ ○	
25	1	10	10	05	08.3	03.2	02.0	.	.	≈ 0-0 ⁴⁰ 13-19 ⁴⁰ ≡ 0 ⁰⁰ 12 ⁴⁰ 13 ⁰ 13 ⁴⁰ 16 ⁴⁰ ≡ 13 ⁴⁰ 17 ⁴⁰ 16 ⁴⁰ ○	
26	8	04	10	02	05.3	04.1	05.2	.	.	≈ 0 ⁰⁰ 0 ²⁰ 10 ⁴⁰ F _S 3-9 ²⁰ 14 ²⁰ 24 ¹ ≡ 15 ⁰⁵ 15 ⁴⁰ 23 ⁴⁰ 24 ¹ ○	
27	8	08	10	08	08.7	02.0	10.4	.	.	≈ 0-2 ⁴⁰ 16 ²⁰ 19 ⁴⁰ 23 ⁴⁰ 24 ¹ ≡ 15 ⁰⁵ 15 ⁴⁰ 23 ⁴⁰ 24 ¹ ○	
28	7	04	08	10	07.3	05.0	01.3	.	.	≈ 0-4 ⁴⁰ 12 ⁴⁰ 13 ⁴⁰ 16 ⁴⁰ 22 ⁴⁰ F _{E-SW} 0-11 ²⁰ 20 ⁰⁰ 14 ⁴⁰ ≡ 12 ⁴⁰ 13 ⁴⁰ 16 ⁴⁰ ○	
29	8	07	05	02	04.7	06.9	21.3	.	.	F _{E-SW} 0-24 ¹ ≡ 15 ²⁰ 19 ⁴⁰ 14 ²⁰ 16 ⁴⁰ 22 ⁴⁰ ≡ 24 ¹ ○	
30	0	00	10	10	06.7	07.6	14.2	.	.	F _{E-SW} 0-11 ²⁰ 20 ⁰⁰ 14 ²⁰ 18 ²⁰ 20 ⁰ ○	
31	8	00	03	02	01.7	09.9	.	.	.	≈ 0 ⁰⁰ 4 ²⁰ 11 ⁴⁰ 18 ²⁰ 24 ¹ ○	
MES.	VRED.	03.5									

$\varphi = 43^{\circ}43'$ N $\lambda = 18^{\circ}16'$ E Gr. $\Delta G = +1h\ 13\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pare e mm			Relativna vlažnost v%				Pravac i jačina veta D, f (0-12)				
				7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
		7	14	21																			
1	597.0	597.5	597.3	09.4	12.0	09.8	10.2	12.8	08.0	-	05.3	06.6	05.9	60	63	64	62	N	4	S	7	SW	7
2	596.9	597.9	598.4	09.0	12.4	10.0	10.4	12.8	08.4	-	07.6	07.1	08.4	89	65	91	82	SW	6	SW	7	SW	7
3	598.2	598.4	598.1	10.0	13.2	06.4	09.0	13.2	06.4	-	06.3	07.9	05.5	69	70	76	72	SW	6	SW	6	SW	6
4	597.0	596.8	597.0	11.8	14.6	05.0	11.1	14.6	06.4	-	05.4	07.4	06.9	52	59	80	64	SW	7	SW	4	SW	5
5	597.3	598.7	597.9	05.4	07.6	10.0	08.2	10.0	05.0	-	06.4	06.4	02.1	95	81	23	66	N	5	N	2	N	2
6	596.4	594.9	592.5	13.2	14.6	12.2	13.0	14.6	09.4	-	02.5	04.4	02.9	22	35	27	28	NW	1	-	0	SW	3
7	589.1	590.2	591.9	06.6	07.0	05.2	06.0	12.4	04.6	-	06.4	07.5	06.6	88	100	100	96	SW	7	SW	2	N	2
8	594.2	597.1	599.2	05.0	06.0	06.4	06.0	07.2	05.0	-	06.5	07.0	07.2	100	100	100	100	NW	4	N	2	SW	3
9	600.3	601.8	601.6	09.4	13.0	10.4	10.8	13.2	06.4	-	06.6	06.0	07.3	74	54	77	68	-	0	S	2	S	3
10	601.1	601.7	601.9	10.0	12.6	10.0	10.6	13.4	09.0	-	06.9	07.8	09.2	75	71	100	82	S	4	N	1	N	3
11	602.2	602.5	602.4	04.0	07.0	06.2	05.8	10.0	03.6	-	06.1	07.5	07.1	100	100	100	100	N	5	NNE	3	E	3
12	600.8	601.2	601.4	08.0	12.0	09.0	09.5	12.0	06.0	-	06.8	07.2	07.4	84	69	86	80	S	4	-	0	-	0
13	600.3	600.7	600.6	10.0	11.0	10.0	10.2	12.2	08.7	-	05.4	06.2	07.0	59	63	76	66	SW	2	N	1	-	0
14	600.2	600.4	599.5	08.8	10.0	07.2	08.3	12.0	07.2	-	06.1	08.0	07.6	71	87	100	86	S	1	-	0	N	3
15	599.3	598.6	598.9	08.6	09.4	07.8	08.4	09.6	07.2	-	03.0	07.2	07.9	35	81	100	72	NNE	5	R	4	N	3
16	599.4	599.3	599.6	06.9	08.2	07.0	07.2	08.4	06.4	-	07.4	05.8	06.0	100	71	80	84	N	4	NNF	2	E	3
17	599.1	599.9	599.6	08.4	11.4	08.4	09.2	11.8	06.8	-	05.0	05.6	05.5	61	55	67	61	SW	5	SSW	3	SW	5
18	599.5	599.7	599.5	08.8	11.2	09.0	09.5	11.2	07.4	-	04.9	05.8	07.3	57	58	84	66	SSW	3	SW	2	SW	2
19	598.8	598.7	598.2	07.6	09.4	07.2	07.8	09.6	07.2	-	07.6	06.6	07.6	98	74	100	91	NNW	5	N	4	-	0
20	595.5	594.3	592.7	07.8	10.4	06.4	07.8	10.8	06.4	-	06.5	06.2	07.0	82	65	98	82	SSW	5	S	7	S	11
21	592.5	593.2	593.2	05.6	07.8	07.2	07.0	08.2	05.4	-	06.8	07.9	07.6	100	100	100	100	S	7	S	7	S	7
22	592.4	594.3	594.9	07.0	07.2	06.8	07.0	07.4	06.2	-	07.5	07.6	07.4	100	100	100	100	SSW	8	SW	8	SSW	8
23	594.6	594.8	593.0	06.8	07.4	05.6	06.4	08.0	05.6	-	07.4	07.2	06.8	100	93	100	98	SSW	5	SW	8	SW	8
24	590.8	590.8	586.8	05.2	06.0	04.8	05.2	06.0	04.8	-	06.6	07.0	06.5	100	100	100	100	SW	10	SW	8	SW	8
25	584.7	583.6	592.5	04.2	03.0	01.2	02.4	05.0	01.2	-	06.2	05.7	05.0	100	100	100	100	SW	9	SW	8	SW	8
26	578.9	577.7	563.0	00.9	-01.6	-02.8	-01.6	01.8	-02.8	-	04.9	04.1	03.6	100	100	97	99	NW	8	NW	8	NW	0
27	587.5	592.8	595.0	-03.0	-02.2	-01.0	-01.8	01.0	-03.0	-	03.6	03.8	04.3	97	98	100	98	NW	10	NW	7	NW	2
28	594.3	594.1	594.0	00.9	03.6	03.0	02.6	04.6	-01.0	-	04.3	04.4	04.6	88	74	81	81	-	0	SW	4	SW	4
29	592.2	593.2	594.0	03.4	05.0	04.8	04.5	05.8	03.0	-	03.8	05.4	06.3	66	82	97	82	SW	8	SW	8	SW	9
30	593.1	593.1	593.2	05.0	06.4	04.2	05.0	06.4	04.0	-	06.5	07.2	06.2	100	100	100	100	SW	8	SW	9	SW	6
MES.	VRFD.			595.4	595.9	595.9	06.8	08.5	06.7	07.2	09.5	05.3	-	05.9	06.5	06.4	81	79	87	82	5.2	4.5	4.7

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1	592.1	592.1	592.1	01.8	C2.2	-00.6	C0.7	04.2	-00.6	-	05.2	C5.1	04.4	100	94	100	98	SW	5	S	4	S	4
2	590.2	598.5	587.9	-02.0	01.0	-00.6	-00.6	02.2	-02.0	-	04.0	04.9	04.4	100	100	100	100	SW	7	SW	8	N	2
3	591.5	593.8	594.6	-02.4	-01.2	-C1.4	-01.6	-00.6	-02.4	-	03.8	04.2	03.7	98	100	89	96	SW	4	SW	6	SW	8
4	593.7	595.2	596.2	-00.6	02.4	03.0	02.0	03.0	-01.4	-	03.4	05.4	03.6	78	100	63	80	SW	9	SW	6	W	3
5	593.6	593.1	592.0	03.4	04.0	04.3	04.0	04.3	02.4	-	05.8	06.1	06.2	100	100	100	100	SW	7	SSW	6	SSW	6
6	589.0	590.1	591.7	04.0	02.0	-00.8	01.1	04.4	-00.8	-	06.1	05.3	04.3	100	100	100	100	SSW	5	SSW	5	SW	5
7	590.0	589.4	589.0	01.0	03.0	04.0	C3.0	04.2	-00.8	-	04.9	05.7	06.1	100	100	100	100	SW	4	SSW	5	S	7
8	586.0	585.7	589.0	01.2	00.8	00.0	00.5	04.2	-00.2	-	05.0	04.9	04.6	100	100	100	100	SSW	8	SSW	12	SW	6
9	588.8	589.5	590.1	-01.0	00.1	-C0.2	-00.3	00.4	-01.2	-	04.2	04.4	04.5	99	95	100	98	SSW	11	SSW	11	SW	6
10	592.0	593.7	594.4	-01.6	-00.2	-01.8	-01.4	00.6	-02.8	-	03.7	03.8	03.3	92	84	82	86	SW	6	SW	5	S	5
11	593.7	594.3	594.4	00.0	01.2	00.6	00.6	01.6	-C1.8	-	03.7	04.2	04.5	81	84	94	86	SSW	4	SW	7	SSW	8
12	594.8	593.4	592.1	01.2	02.8	03.5	02.8	03.5	-00.2	-	04.9	04.2	05.9	97	75	100	91	SSW	7	S	8	SSW	11
13	591.5	592.0	592.0	05.2	04.8	03.2	04.1	05.4	03.0	-	06.6	06.5	05.8	100	100	100	100	SSW	8	SSW	6	SSW	

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$$H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Intensiteta broj sata	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w		
		14	7	14	21	Sred Dies				7	7	
1	8	07	08 0	04	06.3	06.9	.	.	.	0-8 ¹⁰ E E s-ssw-sw 0 ²⁰ 5 ³⁰ 11 ³⁰ 24 ⁰ 10 ²⁰ 10 ²⁰ 0		
2	8	10 ²⁴	08 0	C2	06.7	03.8	08.2	.	.	F _{sw} 0-24, $\equiv 4^{20} 10^{20} \cdot 4^0 19^{40} 24, 0$		
3	8	04 0	08 0	01	04.3	07.5	.	.	.	F _{ssw-sw} 0-24, $\Delta 0-8^{30}$		
4	8	06	06	10 ²⁴	07.3	09.1	.	.	.	F E s-ssw-sw 0-17 ⁴⁵ 13 ⁴⁵ 14 ²⁰ 20 ¹⁵ ▲ 19 ²⁰ 19 ⁴⁵ , $\equiv 17^{45} 24, 0$ 22 ⁴⁵ 22 ⁴⁵		
5	9	03 0	02 0	00	01.7	11.2	06.2	.	.	$\equiv 0-4^{15}, 0-1^0 0-15, \# 300-600, 20-1125$		
6	9	00 0	00 0	C1	00.3	09.4	.	.	.	# 300-600 5-15 11 ³⁰ E F _{sw} 21 ⁴⁰ 24, 0		
7	9	10 ²⁴	10 ²⁴	10 ²⁴	10.0	00.0	.	.	.	F F _{sw} 0-18 ⁴⁰ $\equiv 12^0 24, 0$ 8 ²⁵ 18 ⁴⁵		
8	9	10 0	10 0	10 ²⁴	10.0	00.6	03.3	.	.	$\equiv 300-600 0-1^0 0-20$		
9	8	00 0	02 0	00	00.7	12.1	.	.	.	# 300-600 7 ³⁰ 8 ³⁰ $\equiv 10^{40} 24, 0$ 19 ²⁰ 23, 0		
10	8	00 0	06 0	10 ²⁴	05.3	09.3	.	.	.	A 0-24 7 ³⁰ 8 ³⁰ $\equiv 10^{40} 24, 0$ 19 ²⁰ 23, 0		
11	0	10 ²⁴	10 ²⁴	10 ²⁴	10.0	00.0	07.4	.	.	= 0-24, F _{sw} 0-30 0-8 ⁰⁰		
12	8	02 0	05 0	00	02.3	08.8	.	.	.	= 0-5 ¹⁰ # 5 ⁴⁰ 11 ²⁰ 24, 0 20-24, 0		
13	8	00 0	03 0	00	01.0	10.1	.	.	.	A 0-8 ²⁰ 20 ³⁰ 24, 0 $\equiv 11, 20-24, 0$		
14	6	00 0	03 0	10 ²⁴	04.3	11.1	.	.	.	A 0-8 ²⁰ 0-1 ⁰⁰ 11-23-24, 0 $\equiv 10^{40} 23, 0$		
15	8	00 0	05 0	10 ²⁴	05.0	10.2	.	.	.	# 300-600 1-1 ⁰⁰ K ²⁴ , 0		
16	8	10 ²⁴	04 0	00	04.7	06.7	.	.	.	# 300-600 10 ²⁴ F _{ssw-sw} 0-24 8 ⁴⁰ 15 30 17 ²⁰ 24, 0 0-10 ²⁴		
17	8	02 0	09 0	00	03.7	08.6	.	.	.	F _{sw} 0-12 ²⁴ , 0 4 ²⁰ 24, 0 10 ²⁴ 12 ²⁴ 12 ²⁴ 12 ²⁴		
18	8	01 0	09	10 ²⁴	06.7	05.9	.	.	.	A 0-10 ²⁴ 0-20 ²⁴ 0-24, 0 $\equiv 15^0 24, 0$ F _{sw} 23 ²⁰ 24, 0		
19	8	00 0	04 0	00	01.3	06.0	.	.	.	A 0-10 ²⁴ 0-20 ²⁴ 0-24, 0 $\equiv 15^0 24, 0$ 20 ²⁰ 24, 0 $\equiv 20^{30} 24, 0$		
20	8	01	10	10 ²⁴	07.0	04.2	.	.	.			
21	0	10 ²⁴	10 ²⁴	10 ²⁴	10.0	00.0	21.4	.	.	F E s-24, 0 $\equiv 0-24, 0$ 0-8 ⁴⁰ 16 ³⁰ 17 ²⁰ 23 ²⁰ 24, 0		
22	0	10 ²⁴	10 ²⁴	10 ²⁴	10.0	00.0	22.5	.	.	F E s-24, 0 $\equiv 0-24, 0$ 0-3 ¹⁰ 13 ²⁰ 17 ²⁰ 0-3-5 ⁴⁰ 10 ²⁰ 12 ²⁰ 0-9 ²⁰ A ⁴⁰		
23	8	10	10	10 ²⁴	10.0	00.0	05.4	.	.	F E 0-24, 0 $\equiv 0-540 1430 21$, 0 3 ²⁰ 3 ³⁰ 8 ²⁰ 0 ²⁰		
24	0	10 ²⁴	10 ²⁴	10 ²⁴	10.0	00.0	00.0	.	.	F F _{sw} 0-24, 0 $\equiv 0-940 1220 24, 0$ 0-14 ²⁰ 0 ²⁰		
25	0	10 ²⁴	10 ²⁴	05	08.3	00.0	05.0	.	.	F F _{sw} 0-24, 0 $\equiv 0-2015 2320 24, 0$ 0-0 ²⁰ 0-8 ¹⁵ 0-20 ²⁵ 0 ²⁰		
26	0	10 ²⁴	10 ²⁴	10 ²⁴	10 ²⁴	10.0	01.4	02	.	# 300-600 10 ²⁴ F F _{sw-sw} 0-24 8 ⁴⁰ 11 ²⁰ 24, 0 0-10 ²⁴ 10 ²⁴ 10 ²⁴		
27	9	10 ²⁴	05	00	05.0	05.0	01.5	08	.	$\equiv 300-600 4^0 11^0 16^0$ # 0		
28	9	00 0	00 0	00	00.0	10.6	.	02	.	F F _{sw} 0-20 ²⁴ $\equiv 20^{16} 24, 0$		
29	9	04 0	10	10 ²⁴	08.0	04.4	.	.	.	F F _{sw} 0-24, 0 $\equiv 0-24, 0$ 10 ²⁰ 10 ²⁰		
30	0	10 ²⁴	10 ²⁴	10 ²⁴	10.0	00.0	.	.	.			

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$\varphi = 43^{\circ}43'$, $N \lambda = 18^{\circ}16'$, E Gr., $\Delta G = +1h\ 13\ min.$

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D G	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vетра D, f (0-12)					
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	582.7	583.6	585.1	-06.0	-04.2	-09.8	-08.7	-04.6	-05.8	-	02.8	02.1	02.0	94	91	91	92	N	2	N	7	N	10
2	583.6	584.1	590.6	-10.2	-05.0	-04.8	-06.2	-04.8	-10.4	-	01.9	03.0	02.9	90	95	92	92	NNW	5	WSW	0	SW	6
3	591.4	592.4	592.8	-06.8	-05.4	-04.8	-05.4	-03.6	-07.4	-	02.5	02.7	02.9	89	87	92	89	NNW	6	WSW	2	SW	2
4	591.4	591.4	591.1	-04.2	-02.0	-02.0	-02.6	-02.0	-04.8	-	03.2	03.9	03.9	96	98	98	97	SW	5	SW	7	SW	9
5	591.6	592.4	594.3	-03.4	-01.2	-01.2	-01.8	-01.2	-03.4	-	03.5	04.2	04.2	97	95	98	98	SW	0	SW	8	SW	8
6	596.0	596.4	598.3	-01.0	-00.8	-00.4	-00.6	-00.4	-01.2	-	04.2	04.3	04.4	95	99	100	99	SW	7	SW	8	NW	3
7	595.3	593.4	592.2	-01.6	-03.2	-03.4	-02.9	-00.4	-03.4	-	04.0	03.5	03.5	98	97	97	97	NW	4	NW	4	NW	5
8	591.1	589.6	591.1	-05.0	-06.0	-06.4	-06.0	-03.4	-06.4	-	03.0	02.8	02.7	95	94	94	94	NW	5	NW	7	NW	7
9	592.0	592.4	593.2	-05.8	-04.8	-04.8	-05.0	-04.4	-06.8	-	02.8	03.1	03.1	94	95	95	95	NW	9	N	8	N	8
10	594.2	594.2	594.5	-02.0	-02.0	-03.0	-02.5	-02.0	-04.8	-	03.2	03.2	02.9	82	82	80	81	-	0	SW	2	-	0
11	595.7	596.0	596.4	-04.0	-00.8	-00.8	-01.6	-00.6	-04.2	-	02.7	04.2	04.2	78	96	96	90	-	0	SSW	4	SSW	3
12	595.1	594.3	593.9	-01.0	00.0	00.0	00.0	00.0	-01.2	-	03.6	04.5	04.4	85	98	99	94	SW	7	SW	7	SW	8
13	594.6	595.5	596.6	-08.6	-00.2	00.0	00.2	00.0	-01.6	-	04.1	04.4	04.4	93	97	97	96	SW	5	SW	4	SW	4
14	590.3	590.2	596.6	-01.0	-00.2	-01.0	00.0	-02.0	-	04.0	04.4	04.2	98	97	99	98	SW	6	SW	8	SW	8	
15	597.7	597.8	598.3	-00.2	01.0	00.8	00.6	01.4	-01.2	-	04.4	04.6	04.3	97	94	88	93	N	4	SW	7	SW	5
16	597.5	596.4	597.9	00.8	01.6	01.0	01.1	02.0	00.6	-	03.8	04.4	04.1	79	85	83	82	SSW	7	SSW	8	SSW	7
17	599.1	599.3	599.3	03.0	02.6	02.2	02.5	04.2	00.6	-	02.1	03.6	03.1	37	65	58	53	N	3	SW	2	SW	3
18	598.5	598.6	598.1	02.2	05.0	05.2	04.4	07.4	01.2	-	03.5	02.4	03.9	65	27	58	53	SW	7	W	2	-	0
19	594.2	590.2	592.5	01.0	01.0	-00.2	00.4	05.2	-00.2	-	03.8	04.5	04.5	76	91	100	89	SSW	11	SSW	13	WSW	11
20	594.9	595.3	596.1	-02.0	-00.4	-01.2	-01.2	-00.2	-03.0	-	01.9	03.0	02.3	47	68	55	57	NW	2	SW	6	SW	5
21	595.4	593.6	593.5	-01.4	-01.0	-01.4	-01.4	-00.4	-02.4	-	03.4	04.2	04.1	P2	99	99	93	SW	5	SW	6	SW	4
22	593.6	594.4	594.6	-02.0	-01.6	-02.0	-02.2	-01.0	-03.0	-	03.6	04.0	03.2	97	98	80	92	N	3	WSW	2	W	5
23	594.7	594.3	593.4	00.0	01.6	00.2	00.5	02.2	-02.4	-	01.9	03.1	04.7	42	60	100	67	NWW	3	-	0	SSW	4
24	593.5	593.4	593.4	-03.5	-02.4	-01.2	-02.1	00.2	-03.5	-	03.4	01.8	04.2	97	98	99	98	NHE	2	-	0	SW	5
25	591.5	590.1	588.5	-02.0	-00.4	-00.4	-00.8	00.0	-03.2	-	03.9	04.5	04.5	98	100	99	99	SSW	8	SSW	9	SSW	10
26	587.8	587.1	587.9	-01.0	-02.4	-04.0	-02.0	-00.4	-04.0	-	04.2	03.8	03.3	99	98	96	98	WSW	4	SW	4	SW	4
27	585.0	584.6	586.8	-07.0	-03.6	-06.8	-06.0	-03.6	-07.0	-	02.5	03.4	02.6	93	97	94	95	SW	5	SW	4	-	0
28	580.9	573.2	577.1	-04.0	-02.2	-05.6	-04.4	-00.2	-06.8	-	03.3	03.8	02.9	96	98	95	96	SW	8	SW	14	NW	8
29	580.8	582.0	584.0	-09.2	-07.8	-05.2	-06.8	-05.2	-09.2	-	02.1	02.4	03.0	91	93	95	93	NW	6	W	3	SW	5
30	595.7	598.6	590.1	-07.8	-08.2	-08.2	-08.1	-05.6	-08.2	-	02.4	02.3	02.3	93	92	92	92	NW	7	NH	2	NH	3
MES.	VRED.	592.2	591.8	592.6	-02.9	-01.9	-02.3	-02.4	-00.7	-04.0	-	C3.2	C3.6	C3.6	86	90	91	89	4.9	5.5	5.4		

1974 DECEMBAR

BJELAŠNICA

1	589.8	592.5	595.1	-06.0	-06.0	-05.0	-05.5	-05.0	-07.8	-	02.8	02.8	03.0	94	94	95	94	SW	10	SW	7	NW	3
2	595.6	594.8	596.8	-05.6	-04.0	-04.0	-04.4	-04.0	-05.6	-	02.9	03.3	03.3	95	96	96	96	-	0	NW	8	NW	7
3	596.5	597.2	597.8	-04.0	-02.0	-01.6	-02.3	-01.4	-04.0	-	03.3	03.9	04.0	96	98	98	97	NW	9	N	9	N	9
4	597.5	596.5	595.5	-01.8	01.4	-02.8	-02.8	-02.1	-01.0	-	03.9	04.1	03.6	98	99	97	98	N	8	N	6	N	6
5	592.7	591.1	589.7	-03.7	-02.8	-00.5	-01.9	-00.8	-03.6	-	03.5	03.5	04.0	97	94	93	95	N	5	-	0	SW	5
6	589.2	589.6	589.8	-07.0	-09.0	-08.4	-08.2	-00.6	-10.4	-	02.5	02.1	02.2	93	92	92	92	N	7	N	5	N	5
7	583.7	590.3	590.2	-06.9	-05.6	-04.8	-05.5	-04.4	-08.4	-	02.6	02.9	03.1	94	95	95	95	N	7	NW	7	NNW	7
8	589.4	588.0	586.8	-03.4	-02.4	-03.2	-03.0	-02.0	-05.0	-	03.2	03.8	03.5	90	98	97	95	NNW	7	NW	11	N	12
9	589.8	591.0	593.1	-04.0	-02.8	-02.4	-02.9	-02.4	-04.4	-	03.3	03.6	03.8	96	97	98	97	N	8	N	11	N	9
10	594.6	595.3	595.9	-01.4	00.8	-02.0	-02.0	-01.6	-07.6	-	04.1	04.2	03.9	95	96	98	98	N	6	NNW	4	N	5
11	594.8	589.5	586.1	-01.0	-02.0	-02.4	-02.0	-01.2	-02.6	-	03.9	03.9	03.8	93	98	98	96	SW	5	SW	9	SW	9
12	586.1	585.5	584.1	-02.4	-02.4	-04.6	-03.5	-02.2	-04.6	-	03.8	03.8	03.1	98	98	96	97	SSW	9	-	0	SSW	6
13	581.2	582.1	582.0	-01.6	-04.0	-10.0	-06.4	-01.6	-10.0	-	04.0	03.3	01.9	98	96	91	95	SSW	8	NNW	7	N	6
14	583.5	583.2	584.1	-12.0	-12.4	-13.0	-12.6	-10.0	-13.0	-	01.6	01.6	01.5	89	89	88	89	N	11	N	10	N	11
15	583.5	584.8	585.3	-12.6	-11.4	-10.4	-11.2	-10.4	-13.0	-	01.5	01.7	01.9	88	89	90	89	N	11	N	10	N	10
16	586.3	588.6	589.1	-09.4	-09.4	-10.0	-05.7	-09.0	-10.4														

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 $H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vrijeme V. o.	Oblačnost N (0-10)					Intensitet sunc broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena	
		14	7	14	21	Sred Dnes				7	7
1	0	10*=	10=	10=	10=	10.0	00.0	07.8	68	V0-24, $\equiv 0-24, F_{N-SW} 0-24, + + 0-24, * 0-24, 8$, \boxed{B}	
2	0	040	10=	10=	10=	08.0	05.9	00.6	67	V0-24, $\equiv 0-625, 13.5-24, F_{N-SW-NW} 0-24, + + 0-24, * 0-24, 6-11.5-11.5, * 21.5-23, \boxed{B}, \circ$	
3	8	08	030	10=	10=	07.0	08.2	00.8	65	V0-24, $\equiv 0-2-20-24, F_{N-SW-NW} 0-24, + + 0-9.5$, \boxed{B}	
4	0	10=	10=	10=	10=	10.0	00.0	.	65	V0-24, $\equiv 0-24, F_{N-SW} 0-24, * 17.5-18.5, + + 0-18-24, \boxed{B}$	
5	0	10=	10=	10=	10=	10.0	00.0	00.1	65	V0-24, $F_{N-SW} 0-24, \equiv 0-24, + + 0-24, \boxed{B}$	
6	0	10=	10=	10=	10=	10.0	00.0	.	65	V0-24, $F_{N-SW} 0-18^{\circ}, \equiv 0-18-6, + + 0-18-6$, \boxed{B}	
7	0	10=	10*=	10=	10=	10.0	00.0	.	67	V0-24, $\equiv 0-24, + + 0-12.5-24, F_{N-SW} 0-24, \boxed{B}$	
8	0	10=	10=	10*=	10=	10.0	00.0	01.9	70	V0-24, $\equiv 0-24, + + 0-4.5-24, F_{N-SW} 0-24, + + 0-7.5-24, \boxed{B}$	
9	0	10*=	10=	10=	10=	10.0	00.0	03.3	78	V0-24, $F_{N-NW} 0-24, * 0-9.5 \equiv 0-24, + + 0-24, \boxed{B}$	
10	9	000	000	00	00	00.0	C9.4	00.1	78	V0-24, $F_{N-NW} 0-12.5 \equiv 0-12.5, + + 0-12.5-12.5, \boxed{B}, \circ$	
11	9	000	040	00	00	01.3	09.7	.	75	V0-10-20-30-40-50-60-70-80-90-100-110-120-130-140-150-160-170-180-190-200-210-220-230-240-250-260-270-280-290-300-310-320-330-340-350-360-370-380-390-400-410-420-430-440-450-460-470-480-490-500-510-520-530-540-550-560-570-580-590-600-610-620-630-640-650-660-670-680-690-700-710-720-730-740-750-760-770-780-790-800-810-820-830-840-850-860-870-880-890-900-910-920-930-940-950-960-970-980-990-1000-1010-1020-1030-1040-1050-1060-1070-1080-1090-1100-1110-1120-1130-1140-1150-1160-1170-1180-1190-1200-1210-1220-1230-1240-1250-1260-1270-1280-1290-1300-1310-1320-1330-1340-1350-1360-1370-1380-1390-1400-1410-1420-1430-1440-1450-1460-1470-1480-1490-1500-1510-1520-1530-1540-1550-1560-1570-1580-1590-1600-1610-1620-1630-1640-1650-1660-1670-1680-1690-1700-1710-1720-1730-1740-1750-1760-1770-1780-1790-1800-1810-1820-1830-1840-1850-1860-1870-1880-1890-1900-1910-1920-1930-1940-1950-1960-1970-1980-1990-2000-2010-2020-2030-2040-2050-2060-2070-2080-2090-2100-2110-2120-2130-2140-2150-2160-2170-2180-2190-2200-2210-2220-2230-2240-2250-2260-2270-2280-2290-2300-2310-2320-2330-2340-2350-2360-2370-2380-2390-2400-2410-2420-2430-2440-2450-2460-2470-2480-2490-2500-2510-2520-2530-2540-2550-2560-2570-2580-2590-2600-2610-2620-2630-2640-2650-2660-2670-2680-2690-2700-2710-2720-2730-2740-2750-2760-2770-2780-2790-2800-2810-2820-2830-2840-2850-2860-2870-2880-2890-2900-2910-2920-2930-2940-2950-2960-2970-2980-2990-3000-3010-3020-3030-3040-3050-3060-3070-3080-3090-3100-3110-3120-3130-3140-3150-3160-3170-3180-3190-3200-3210-3220-3230-3240-3250-3260-3270-3280-3290-3300-3310-3320-3330-3340-3350-3360-3370-3380-3390-3400-3410-3420-3430-3440-3450-3460-3470-3480-3490-3500-3510-3520-3530-3540-3550-3560-3570-3580-3590-3600-3610-3620-3630-3640-3650-3660-3670-3680-3690-3700-3710-3720-3730-3740-3750-3760-3770-3780-3790-3800-3810-3820-3830-3840-3850-3860-3870-3880-3890-3890-3900-3910-3920-3930-3940-3950-3960-3970-3980-3990-4000-4010-4020-4030-4040-4050-4060-4070-4080-4090-4100-4110-4120-4130-4140-4150-4160-4170-4180-4190-4200-4210-4220-4230-4240-4250-4260-4270-4280-4290-4300-4310-4320-4330-4340-4350-4360-4370-4380-4390-4400-4410-4420-4430-4440-4450-4460-4470-4480-4490-4500-4510-4520-4530-4540-4550-4560-4570-4580-4590-4600-4610-4620-4630-4640-4650-4660-4670-4680-4690-4700-4710-4720-4730-4740-4750-4760-4770-4780-4790-4790-4800-4810-4820-4830-4840-4850-4860-4870-4880-4890-4890-4900-4910-4920-4930-4940-4950-4960-4970-4980-4990-5000-5010-5020-5030-5040-5050-5060-5070-5080-5090-5100-5110-5120-5130-5140-5150-5160-5170-5180-5190-5200-5210-5220-5230-5240-5250-5260-5270-5280-5290-5300-5310-5320-5330-5340-5350-5360-5370-5380-5390-5400-5410-5420-5430-5440-5450-5460-5470-5480-5490-5500-5510-5520-5530-5540-5550-5560-5570-5580-5590-5600-5610-5620-5630-5640-5650-5660-5670-5680-5690-5700-5710-5720-5730-5740-5750-5760-5770-5780-5790-5800-5810-5820-5830-5840-5850-5860-5870-5880-5890-5890-5900-5910-5920-5930-5940-5950-5960-5970-5980-5990-6000-6010-6020-6030-6040-6050-6060-6070-6080-6090-6100-6110-6120-6130-6140-6150-6160-6170-6180-6190-6200-6210-6220-6230-6240-6250-6260-6270-6280-6290-6300-6310-6320-6330-6340-6350-6360-6370-6380-6390-6400-6410-6420-6430-6440-6450-6460-6470-6480-6490-6500-6510-6520-6530-6540-6550-6560-6570-6580-6590-6600-6610-6620-6630-6640-6650-6660-6670-6680-6690-6690-6700-6710-6720-6730-6740-6750-6760-6770-6780-6790-6790-6800-6810-6820-6830-6840-6850-6860-6870-6880-6890-6890-6900-6910-6920-6930-6940-6950-6960-6970-6980-6990-7000-7010-7020-7030-7040-7050-7060-7070-7080-7090-7090-7100-7110-7120-7130-7140-7150-7160-7170-7180-7190-7190-7200-7210-7220-7230-7240-7250-7260-7270-7280-7290-7290-7300-7310-7320-7330-7340-7350-7360-7370-7380-7390-7390-7400-7410-7420-7430-7440-7450-7460-7470-7480-7490-7490-7500-7510-7520-7530-7540-7550-7560-7570-7580-7590-7590-7600-7610-7620-7630-7640-7650-7660-7670-7680-7690-7690-7700-7710-7720-7730-7740-7750-7760-7770-7780-7790-7790-7800-7810-7820-7830-7840-7850-7860-7870-7880-7890-7890-7900-7910-7920-7930-7940-7950-7960-7970-7980-7990-7990-8000-8010-8020-8030-8040-8050-8060-8070-8080-8090-8090-8100-8110-8120-8130-8140-8150-8160-8170-8180-8190-8190-8200-8210-8220-8230-8240-8250-8260-8270-8280-8290-8290-8300-8310-8320-8330-8340-8350-8360-8370-8380-8390-8390-8400-8410-8420-8430-8440-8450-8460-8470-8480-8490-8490-8500-8510-8520-8530-8540-8550-8560-8570-8580-8590-8590-8600-8610-8620-8630-8640-8650-8660-8670-8680-8690-8690-8700-8710-8720-8730-8740-8750-8760-8770-8780-8790-8790-8800-8810-8820-8830-8840-8850-8860-8870-8880-8890-8890-8900-8910-8920-8930-8940-8950-8960-8970-8980-8990-8990-9000-9010-9020-9030-9040-9050-9060-9070-9080-9090-9090-9100-9110-9120-9130-9140-9150-9160-9170-9180-9190-9190-9200-9210-9220-9230-9240-9250-9260-9270-9280-9290-9290-9300-9310-9320-9330-9340-9350-9360-9370-9380-9390-9390-9400-9410-9420-9430-9440-9450-9460-9470-9480-9490-9490-9500-9510-9520-9530-9540-9550-9560-9570-9580-9590-9590-9600-9610-9620-9630-9640-9650-9660-9670-9680-9690-9690-9700-9710-9720-9730-9740-9750-9760-9770-9780-9790-9790-9800-9810-9820-9830-9840-9850-9860-9870-9880-9890-9890-9900-9910-9920-9930-9940-9950-9960-9970-9980-9990-9990-10000-10010-10020-10030-10040-10050-10060-10070-10080-10090-10090-10100-10110-10120-10130-10140-10150-10160-10170-10180-10190-10190-10200-10210-10220-10230-10240-10250-10260-10270-10280-10290-10290-10300-10310-10320-10330-10340-10350-10360-10370-10380-10390-10390-10400-10410-10420-10430-10440-10450-10460-10470-10480-10490-10490-10500-10510-10520-10530-10540-10550-10560-10570-10580-10590-10590-10600-10610-10620-10630-10640-10650-10660-10670-10680-10690-10690-10700-10710-10720-10730-10740-10750-10760-10770-10780-10790-10790-10800-10810-10820-10830-10840-10850-10860-10870-10880-10890-10890-10900-10910-10920-10930-10940-10950-10960-10970-10980-10990-10990-11000-11010-11020-11030-11040-11050-11060-11070-11080-11090-11090-11100-11110-11120-11130-11140-11150-11160-11170-11180-11190-11190-11200-11210-11220-11230-11240-11250-11260-11270-11280-11290-11290-11300-11310-11320-11330-11340-11350-11360-11370-11380-11390-11390-11400-11410-11420-11430-11440-11450-11460-11470-11480-11490-11490-11500-11510-11520-11530-11540-11550-11560-11570-11580-11590-11590-11600-11610-11620-11630-11640-11650-11660-11670-11680-11690-11690-11700-11710-11720-11730-11740-11750-11760-11770-11780-11790-11790-11800-11810-11820-11830-11840-11850-11860-11870-11880-11890-11890-11900-11910-11920-11930-11940-11950-11960-11970-11980-11990-11990-12000-12010-12020-12030-12040-12050-12060-12070-12080-12090-12090-12100-12110-12120-12130-12140-12150-12160-12170-12180-12190-12190-12200-12210-12220-12230-12240-12250-12260-12270-12280-12290-12290-12300-12310-12320-12330-12340-12350-12360-12370-12380-12390-12390-12400-12410-12420-12430-12440-12450-12460-12470-12480-12490-12490-12500-12510-12520-12530-12540-12550-12560-12570-12580-12590-12590-12600-12610-12620-12630-12640-12650-12660-12670-12680-12690-12690-12700-12710-12720-12730-12740-12750-12760-12770-12780-12790-12790-12800-12810-12820-12830-12840-12850-12860-12870-12880-12890-12890-12900-12910-12920-12930-12940-12950-12960-12970-12980-12990-12990-13000-13010-13020-13030-13040-13050-13060-13070-13080-13090-13090-13100-13110-13120-13130-13140-13150-13160-13170-13180-13190-13190-13200-13210-13220-13230-13240-13250-13260-13270-13280-13290-13290-13300-13310-13320-13330-13340-13350-13360-13370-13380-13390-13390-13400-13410-13420-13430-13440-13450-13460-13470-13480-13490-13490-13500-13510-13520-13530-13540-13550-13560-13570-13580-13590-13590-13600-13610-13620-13630-13640-13650-13660-13670-13680-13690-13690-13700-13710-13720-13730-13740-13750-13760-13770-13780-13790-13790-13800-13810-13820-13830-13840-13850-13860-13870-13880-13890-13890-13900-13910-13920-13930-13940-13950-13960-13970-13980-13990-13990-14000-14010-14020-14030-14040-14050-14060-14070-14080-14090-14090-14100-14110-14120-14130-14140-14150-14160-14170-14180-14190-14190-14200-14210-14220-14230-14240-14250-14260-14270-14280-14290-14290-14300-14310-14320-14330-14340-14350-14360-14370-14380-14390-14390-14400-14410-14420-14430-14440-14450-14460-14470-14480-14490-14490-14500-14510-14520-14530-14540-14550-14560-14570-14580-14590-14590-14600-14610-14620-14630-14640-14650-14660-14670-14680-146	

$\varphi = 43^{\circ}52'$ N $\lambda = 18^{\circ}26'$ E Gr. $\Delta G = + 1h\ 14\ min.$

BR. ST. 143

D D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	709.4	709.2	710.9	01.6	02.4	01.4	01.8	03.0	01.2	-	05.0	05.2	04.9	97	92	97	95	W NW	2	W NW	2	
2	710.3	708.8	709.2	00.8	03.0	02.6	02.2	03.1	06.8	-	04.8	05.3	05.3	98	94	97	96	-	0	W NW	1	
3	708.3	707.7	709.2	02.1	04.4	03.2	03.2	04.5	01.9	-	05.2	05.8	05.5	98	93	95	95	W NW	1	W SW	2	
4	712.1	712.2	714.1	00.9	03.2	02.2	02.1	03.5	00.0	-	04.7	05.4	05.3	97	94	98	96	-	0	SW	1	
5	713.2	712.0	711.5	00.0	03.6	02.6	02.2	04.0	-00.1	-	04.4	05.5	05.2	96	92	97	95	-	0	-	0	
6	709.2	706.8	705.8	01.8	05.2	04.2	03.8	05.5	01.5	-	03.0	05.9	05.6	95	89	91	92	ESE	2	-	C SSE	
7	707.6	709.1	704.5	02.9	02.6	02.5	02.6	04.6	02.2	-	05.6	05.2	05.0	100	94	90	95	W	1	W	1	
8	709.4	709.3	710.6	00.0	02.4	01.0	01.1	02.7	-06.3	-	04.4	04.9	04.8	96	90	97	94	E	1	-	0	
9	710.1	708.9	708.2	00.4	04.8	-00.1	01.2	05.6	-00.1	-	04.4	04.3	03.8	93	67	84	81	FNE	1	SE	3	
10	705.9	706.7	709.4	-01.4	01.4	01.2	00.6	01.9	-01.5	-	03.8	04.4	04.6	92	87	91	90	S	2	W NW	1	
11	711.9	712.6	714.9	-01.3	01.3	00.8	00.4	01.6	-01.4	-	03.8	04.3	04.0	92	85	83	87	-	0	SW	1	
12	715.6	715.1	715.5	-01.4	03.2	01.0	01.0	04.5	-01.5	-	03.6	04.3	04.6	92	75	93	87	-	0	-	0	
13	714.5	712.9	713.2	-01.6	-00.4	-01.8	-01.4	01.0	-02.5	-	03.8	03.0	03.7	92	85	92	90	SE	2	SW	1	
14	714.3	713.2	713.5	-05.0	01.3	-02.4	-02.1	02.5	-05.1	-	02.9	03.2	03.0	91	64	77	77	FSE	1	W NW	1	
15	714.0	713.0	713.5	-06.0	01.6	-02.4	-02.4	01.3	-06.4	-	02.8	03.2	03.2	94	65	84	81	SE	4	W	1	
16	712.8	712.4	711.9	-02.0	-00.1	00.5	-00.3	01.0	-03.0	-	03.4	04.1	04.3	87	91	91	90	-	0	C	NW	
17	706.5	705.9	709.3	-01.2	03.0	00.4	00.6	04.5	-01.5	-	04.0	05.1	04.6	94	91	96	94	E	1	-	0	
18	709.4	708.7	708.8	00.0	02.2	00.4	00.8	03.1	-00.5	-	04.4	03.8	04.1	96	71	86	84	-	0	SW	2	
19	709.9	710.2	710.5	-01.9	00.8	01.0	00.2	02.0	-02.5	-	03.7	04.4	04.6	92	40	93	92	-	0	-	0	
20	709.3	708.9	711.1	00.6	04.2	02.8	02.6	04.5	00.5	-	04.5	05.6	05.2	93	91	94	93	-	0	-	0	
21	712.8	710.4	713.5	02.2	03.0	02.2	02.4	03.6	01.6	-	05.3	05.1	04.9	95	89	90	92	SE	1	W	1	
22	713.3	712.1	711.6	-00.2	02.6	01.0	02.2	08.7	-04.2	-	04.4	04.5	04.2	93	62	85	80	ESE	1	W	1	
23	712.2	712.7	711.4	-04.2	-01.3	-00.1	-01.4	01.3	-04.5	-	03.2	03.9	04.4	96	93	96	95	ESE	1	W	1	
24	711.4	710.4	710.7	-00.4	03.4	-00.2	00.2	01.6	-00.5	-	04.5	04.3	04.2	100	85	93	93	-	0	-	0	
25	709.0	708.6	709.3	-03.4	01.2	-00.5	-00.8	01.6	-03.4	-	03.0	03.7	04.0	85	73	91	83	ESE	2	W NW	1	
26	711.2	710.5	710.2	-04.6	-00.2	-02.4	-02.4	00.0	-05.6	-	02.8	03.6	03.7	87	80	96	88	E	1	W	1	
27	709.4	707.7	708.3	-04.9	02.2	00.4	-00.5	03.6	-05.7	-	02.7	03.7	04.1	85	70	86	80	-	0	-	0	
28	709.5	710.1	710.5	-01.9	02.2	00.4	02.3	03.5	-02.4	-	03.8	04.6	04.6	96	85	96	92	-	0	SE	1	
29	710.7	709.7	710.5	-04.2	-00.7	-02.0	-02.2	00.8	-04.2	-	02.9	04.0	04.0	88	93	100	94	-	0	W NW	1	
30	713.4	713.2	714.1	-04.5	-01.0	-02.0	-02.4	-00.7	-04.5	-	03.1	03.9	03.9	94	91	98	94	SSE	1	-	0	
31	714.2	713.5	713.6	-03.8	02.0	-00.2	-00.6	03.6	-04.0	-	03.2	04.2	04.0	92	79	89	87	-	0	W NW	1	
MES.	VRED.	711.0	710.5	711.1	-01.3	02.1	00.6	00.5	03.0	-01.7	-	04.0	04.5	04.4	94	84	92	90	SE	2	0.7	0.7

1	712.3	711.1	711.2	-03.0	09.6	02.6	03.0	10.5	-04.4	-	03.3	05.3	04.6	86	89	82	77	ESE	2	W	1	-
2	711.3	710.3	711.4	00.4	12.2	03.2	04.8	12.4	-00.4	-	04.0	05.0	04.7	84	47	61	71	SE	2	W NW	1	-
3	709.7	707.9	704.8	01.8	10.0	04.0	07.4	10.6	-00.8	-	04.1	04.6	05.7	79	52	66	56	SE	4	SW	1	SE
4	702.6	700.0	701.0	02.5	09.6	03.6	04.8	11.0	00.9	-	05.2	05.0	05.0	95	56	85	79	SSE	4	SW	3	-
5	701.7	700.0	699.2	00.3	09.0	02.5	03.8	10.5	00.0	-	04.3	04.5	04.3	91	53	77	74	ESE	1	W	2	-
6	698.1	692.1	686.8	01.6	07.4	06.3	06.4	08.5	-00.2	-	04.3	04.0	05.2	83	52	67	66	SW	1	S	6	SSW
7	697.9	684.4	691.0	04.0	07.5	-00.1	02.8	09.5	-00.2	-	05.7	02.7	02.9	94	25	62	64	W NW	4	ESE	1	
8	698.5	702.2	706.9	-03.5	02.4	-00.6	-00.6	05.0	-03.9	-	02.9	04.1	03.2	83	74	77	82	SE	1	E	2	
9	709.7	709.0	709.7	-05.1	08.9	02.4	02.8	09.5	-05.6	-	02.6	02.4	03.2	84	28	59	57	ESE	4	W NW	1	ESE
10	710.1	709.8	710.3	-00.4	12.2	03.0	04.6	12.8	-00.9	-	03.4	04.2	04.3	72	40	75	62	SE	1	W NW	2	ESE
11	708.8	706.1	705.7	00.4	12.6	03.2	04.8	13.3	-00.2	-	03.8	04.9	04.5	81	45	78	68	ESE	4	W	2	SSW
12	704.1	701.7	701.3	01.0	14.2	04.2	05.9	15.8	00.5	-	03.7	04.4	04.2	74	36	68	56	ESE	3	W	1	E
13	699.4	698.3	698.0	04.8	10.3	07.3	07.6	12.0	01.5	-	04.6	05.4	04.8	71	56	75	67	NNW	1	S	4	ESE
14	697.0	698.6	701.3	06.4	11.3	05.8	07.2	12.6	05.5	-	05.3	04.8	04.6	73	47	67	62	ESE	2	SW	2	E
15	701.3	700.6	701.0	04.0	12.2	07.2	07.7	13.5	03.6	-	05.6	05.5	04.7	91	52	62	68	-	0	W	1	ESE
16	701.9	701.3	703.1	03.4	11.8	07.5	07.6	12.2	02.5	-	05.1	05.7	05.4	88	55	69	71	-	0	SW	1	SE
17	705.2	706.2	704.0	04.2	13.6	08.0	08.4	15.9	03.5	-	04.5	04.6	04.8	72	40	59	57	ESE	3	W	2	E
18	70																					

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$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vrijednost 0-9	Obločnost N (0-10)					Insolacijia broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	5	09	10•	10	05.7	00.0	00.7	.	n-n, 11 ²⁰ 14 ¹⁵ 17 ¹⁶ 19 ¹² n	
2	3	10•	10•	10•	10.0	00.0	00.6	.	n-16, 16-n, 19 ¹⁵ 21 ¹⁵	
3	2	10•	10•	08	06.3	00.0	00.4	.	n-19, 21 ¹⁵ n, orj-8, = 19 21 ¹⁵	
4	2	10•	10•	10•	10.0	00.0	00.1	.	n-n	
5	3	01•	06•	10	05.7	00.0	.	.	n-8, = n-7 ²⁰ , 13 ¹⁰ , = 7 ²⁰ 13 ¹⁰ , 11 ²⁰ 14 ¹⁵ , 15 ¹⁵ , = 15, 11	
6	5	10	10•	10•	10.0	00.0	00.2	.	n-n, 10 ¹⁰ n	
7	5	10•	10•*	10	10.0	00.0	05.5	.	•, n-8 ²⁰ 15-16; = n-n, 8 ²⁰ 13 ²⁰	
8	4	10	10	10	10.0	00.0	01.6	.	n-8 ²⁰ , = n-n, * 9 ¹⁵ 11 ²⁰ , 14 ¹⁵ K 15 10 ²⁰ 12, * 13 ²⁰ , 15 ²⁰	
9	7	06	09	00	05.0	02.2	01.5	00	= n-10, 20-n	
10	3	09	10•	10*	05.7	00.0	.	.	n-7 ²⁰ , = n-11 ²⁰ , 15-17, * 8 12 ²⁰ , 12 ²⁰ * 13 ²⁰ , 12, 18 ²⁰ , 12 ²⁰ , 11 ²⁰ , 11	
11	5	10	10	07	05.0	00.0	00.4	00	n-n, 9-n	
12	6	10	10	02	07.3	00.7	.	.	n-n, 9-n	
13	5	10•	10	10	10.0	00.0	.	.	n-n, 9-n, = 10-n	
14	5	05	03•	00	02.7	05.8	.	.	n-10 ²⁰ , = n-n, 12, 13-n	
15	4	10	00•	00	03.3	04.8	.	.	n-1, 17-n, = n-n	
16	3	10*	10•	10•	10.0	00.0	00.1	00	= n-7 ²⁰ * rj-10, = 7 ²⁰ n, A 14 ²⁰ 12 ²⁰ , * 12 ²⁰ 15 ¹⁵ , [X]	
17	2	02	10•	10*	07.3	00.0	02.0	C1	= 7 ²⁰ 12, 22-n, = 12-17, * 12 ²⁰ 17 ²⁰ , * 10 ²⁰ 17, * 11 ²⁰ 17, = 11 ²⁰ , [X]	
18	7	10*	09*	10*	09.7	01.6	16.4	14	* n-rj, 20-n, = 9 ²⁰ 12, [X]	
19	5	10	10*	10*	10.0	00.0	01.5	09	= n-n, * 8 ²⁰ n, [X]	
20	5	10•	10•	10•	10.0	00.0	17.5	19	•n-n, = n-n, [X]	
21	7	10•	10•	10	10.0	00.0	06.0	C7	= n-n, orj-7 ²⁰ , * 12 ²⁰ 15, [X]	
22	6	00	00•	00	00.0	00.0	08.1	05	= 8 ²⁰ 12, * 12, 18 ²⁰ , [X]	
23	3	03•	10•	10*	07.7	00.7	.	04	n-9, = 9-n, * 18 ²⁰ 21 ²⁰ , [X]	
24	4	10•	10	10	10.0	00.0	00.8	03	= n-12 ²⁰ , = 12 ²⁰ n, [X]	
25	5	10	10	09	09.7	00.0	.	C2	= n-n, [X]	
26	5	10	10	10	10.0	03.5	.	02	= n-n, [X]	
27	2	00	00•	04	01.2	04.7	.	02	= n-10 ²⁰ 17 ²⁰ n, = 10 ²⁰ 16 ²⁰ , = 11 ²⁰ 15 ¹⁵ , [X]	
28	2	10*	10•	00	06.7	00.0	00.3	02	= n-12, * rj-12, = 12, 18 ²⁰ , = 10 ²⁰ 19 ²⁰ , = 11 ²⁰ n, [X]	
29	3	10	10•	10•	10.0	00.3	00.5	02	= n-9, = 9 ²⁰ 12 ²⁰ , = 8 ²⁰ 12, [X]	
30	2	10	10•	10•	10.0	00.0	.	02	* n-8 ²⁰ n, = 8 ²⁰ 12, = 9 ²⁰ n, [X]	
31	3	10•	10•	00•	06.7	01.5	.	02	= n-14 ²⁰ , = 14 ²⁰ n, [X]	
MES.										
VRFD.	08.2	08.6	07.4	08.1	33.4	57.2				

1	4	03	01	00	03	02.3	07.7	.	02	$\equiv n-10, = 13-n$
2	6	02	06	00	02	02.7	07.7	.	.	$\sqcup n-9 = n-10, 10-21^{\circ}, \text{sw} 20^{\circ} 45^{\circ}, 21^{\circ} 30^{\circ}$
3	7	08	07	00	05	06.7	02.6	.	.	$\sqcup n-8^{\circ} = n-n, 8^{\circ} 55^{\circ} 03^{\circ} 17^{\circ} 30^{\circ} 18^{\circ} 5^{\circ}, 22^{\circ} 45^{\circ}, 21^{\circ}$
4	8	10	06	00	08	08.0	02.8	40.7	00	$\bullet 0-8^{\circ}, *n-j, 18^{\circ} 25^{\circ}, F_{SE}, 6^{\circ} 0^{\circ}, 0^{\circ} 4^{\circ}$
5	8	07	06	08	07.0	06.5	00.1	.	.	$\sqcup n-8^{\circ} = n-10, F_{SW}, 13^{\circ} 25^{\circ}$
6	8	05	10	10	08.3	03.3	.	.	.	$\sqcup n-8^{\circ} = n-17^{\circ}, 13^{\circ} 10^{\circ}, F_{S}, SW, 9^{\circ} 2^{\circ}, 19^{\circ} 15^{\circ}, 21^{\circ} 5^{\circ}, 22^{\circ}, 24^{\circ}$
7	8	10	06	01	05.7	03.3	09.8	.	.	$\bullet 0-8^{\circ}, F_{S}, 0^{\circ}, 2^{\circ} 0^{\circ}, 17^{\circ} 45^{\circ}, 14^{\circ} 0^{\circ}, *8^{\circ} 8^{\circ}, 0^{\circ}$
8	7	10	03	03	05.3	04.9	01.6	00	.	$*5^{\circ} 15^{\circ}, 5^{\circ} 45^{\circ}, 8^{\circ} 0^{\circ}, 12^{\circ}$
9	7	01	07	01	03.0	05.7	00.2	00	.	$\sqcup n-9 = n-n$
10	7	01	03	00	01.3	09.2	.	.	.	$\sqcup n-8^{\circ}$
11	7	00	00	00	00	00.0	09.6	.	.	$\sqcup n-8^{\circ}, = n-10$
12	8	00	01	00	00	00.3	09.4	.	.	$\sqcup n-10, = 9^{\circ} 20^{\circ}, 9^{\circ} 30^{\circ}$
13	8	08	08	10	08.7	05.5	.	.	.	$= 7^{\circ} 10, *9^{\circ} 9^{\circ}, 15^{\circ} 10^{\circ}, 18^{\circ} 5^{\circ}, n$
14	8	09	10	10	05.7	03.3	00.0	.	.	$= n-10, *n-j, 9^{\circ} 2^{\circ}, 10^{\circ} 30^{\circ}$
15	7	10	07	10	05.0	05.3	00.2	.	.	
16	7	10	08	09	09.0	02.3	00.0	.	.	$= n-n$
17	8	07	08	08	07.7	05.6	.	.	.	$\Delta n-8^{\circ}$
18	8	10	09	10	09.7	00.5	.	.	.	$\Delta n-10, F_{S}, 22^{\circ} 55^{\circ}, 24^{\circ}$
19	8	09	06	07	07.3	03.9	07.2	.	.	$F_{SE}, 0^{\circ}, 10^{\circ}, \bullet n-n$
20	7	05	08	08	07.0	03.4	.	.	.	$= n-n, = 8^{\circ} 10^{\circ}, *13^{\circ} 0^{\circ}$
21	5	10	10	10	10.0	00.0	00.0	.	.	$= n-n$
22	7	10	10	10	10.0	00.0	.	.	.	$= n-10, *7^{\circ} 55^{\circ}, 13^{\circ} 20^{\circ}, 17^{\circ} 24^{\circ}$
23	4	10*	10	10	10.0	00.0	10.4	04	.	$\bullet 0-4^{\circ}, 20^{\circ} 30^{\circ}, n-j, *12^{\circ} 10^{\circ} 30^{\circ}, \equiv n-10, = 10-n, \blacksquare$
24	6	10	10	10	10.0	00.0	00.7	00	.	$= n-n$
25	6	10	10*	10*	10.0	00.0	.	.	.	$= n-n, \Delta 8^{\circ}-n$
26	7	10	10	10	10.0	00.0	00.0	00	.	$= n-10$
27	7	09	01	02	04.0	08.5	.	.	.	$= 12^{\circ} n$
28	6	09	07	00	05.3	04.6	.	.	.	

$\varphi = 43^{\circ}52'$, N $\lambda = 18^{\circ}26'$, E Gr. $\Delta G = +1h\ 14\ min.$

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d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenog pore e mm			Relativna vlažnost %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21		
1	707.5	709.3	709.3	-03.0	07.0	01.5	01.6	08.6	-04.1	-	02.8	03.6	03.7	76	48	72	65	-	0	WSW 2	E 2	
2	703.1	709.9	701.2	-01.4	08.8	05.2	04.4	09.2	-02.6	-	03.5	03.7	04.5	85	44	62	66	ESE 3	-	0	NNW 2	
3	703.6	705.6	707.1	02.1	08.8	02.6	04.0	10.5	02.0	-	04.5	03.9	03.5	84	46	62	64	-	0	SW 2	ESE 3	
4	707.0	707.1	705.0	04.0	08.2	08.6	07.4	10.6	00.0	-	03.6	05.4	04.9	55	67	59	62	E 3	SSE 1	LSE 4		
5	703.2	704.4	702.4	08.2	09.0	06.1	07.4	09.6	05.1	-	05.1	06.3	06.6	62	73	92	76	ESE 5	ESE 5	-	0	
6	700.9	700.6	702.7	04.8	10.6	03.7	05.7	11.5	03.7	-	04.9	04.5	05.5	76	47	92	72	SE 4	SE 4	-	0	
7	705.2	707.4	707.7	00.0	04.6	-00.2	00.0	04.0	-00.3	-	04.3	04.2	04.0	93	88	89	90	NNW 2	-	C	NNW 1	
8	707.9	706.5	707.5	-00.2	02.0	01.0	01.0	02.9	-00.4	-	04.1	04.5	03.8	91	85	78	85	SF 2	WNW 1	ESE 2		
9	707.5	707.5	709.2	-00.4	03.6	01.4	01.5	04.0	-00.6	-	03.5	04.1	04.4	78	70	87	78	F 1	SSE 1	NW 1		
10	700.4	705.4	709.3	00.1	03.8	02.4	02.2	05.0	00.0	-	04.4	04.6	04.4	95	76	81	84	NW 2	SW 2	W 2		
11	710.3	711.6	713.1	00.2	02.3	02.1	01.7	02.9	-00.1	-	04.3	04.6	03.9	92	85	73	84	NNW 2	WNW 1	E 1		
12	713.0	711.1	711.3	01.0	05.6	03.2	03.3	06.4	00.6	-	03.8	04.1	03.9	78	60	67	68	ESE 3	S 3	SE 2		
13	708.9	705.2	705.4	-01.4	09.2	03.6	03.8	11.1	-02.2	-	03.4	04.0	04.6	93	45	76	68	ESF 2	W 1	ESE 2		
14	703.7	707.6	699.9	-02.0	06.6	04.0	03.2	08.9	-02.0	-	03.7	04.8	04.1	94	66	60	76	ESF 1	W 2	SE 2		
15	703.2	698.1	700.3	-01.2	08.0	02.6	03.0	09.0	-01.2	-	03.4	03.8	04.6	81	48	82	70	SE 1	ENE 4	F 2		
16	699.8	700.1	700.4	01.8	08.2	03.4	04.2	08.7	00.5	-	04.5	04.0	04.6	87	49	79	72	ESE 1	WSW 1	ESE 2		
17	702.4	703.3	704.2	00.0	16.4	05.2	08.7	17.0	-00.7	-	03.8	04.1	04.3	82	29	49	53	ESE 3	W 1	ESE 3		
18	705.8	705.0	706.3	04.0	19.3	13.6	12.6	19.5	02.7	-	04.1	05.0	04.2	68	30	36	45	SE 2	W 1	S 5		
19	708.5	707.5	709.6	09.8	20.2	10.9	12.9	20.7	08.4	-	04.2	05.5	04.9	47	31	51	43	SE 2	SSW 5	SSE 2		
20	710.3	709.9	711.0	00.8	20.0	11.6	13.0	20.2	05.7	-	03.1	03.5	04.4	36	20	43	33	ESE 2	SE 1	ESE 2		
21	712.2	710.1	711.0	06.2	27.0	12.6	14.0	24.7	04.3	-	02.4	02.3	03.6	34	10	32	25	SF 2	SW 2	ESE 2		
22	711.0	708.2	708.1	06.4	24.4	14.0	14.7	24.5	05.5	-	04.4	04.8	05.2	62	21	43	42	FSE 2	ENE 4	ESE 2		
23	707.9	703.4	709.4	09.1	18.1	12.2	12.9	19.5	07.0	-	05.5	04.2	06.3	63	27	59	50	F 3	SSW 2	E 2		
24	710.8	707.4	708.0	05.8	21.4	14.2	13.9	22.5	04.5	-	05.8	04.5	06.4	83	34	53	57	SF 3	W 2	SE 2		
25	708.4	707.7	708.3	09.1	19.2	13.4	13.8	19.8	06.6	-	06.0	05.5	06.6	69	33	57	53	ESF 2	-	E 4		
26	708.4	706.1	705.6	06.8	20.4	12.8	13.2	20.9	04.8	-	05.8	05.6	06.9	79	31	62	57	ESE 3	S 2	ESE 2		
27	704.7	703.5	705.4	08.2	15.5	10.4	11.1	20.0	07.3	-	06.4	06.6	07.9	79	50	84	71	SE 1	E 5	N 2		
28	705.9	705.2	707.1	07.6	17.3	05.4	10.9	19.5	07.2	-	07.2	05.8	07.8	92	39	88	73	SSE 1	-	0	ESE 2	
29	705.6	707.0	704.2	05.1	19.4	12.8	12.5	20.5	03.5	-	05.9	06.1	06.1	90	36	55	60	E 2	SF 3	ESE 3		
30	722.1	707.4	703.7	08.3	15.6	10.8	11.4	15.7	06.9	-	06.1	06.2	06.2	74	47	64	62	ESE 4	ESE 3	ESE 2		
31	708.3	706.9	704.6	07.2	09.7	07.0	07.6	11.0	06.2	-	07.0	07.2	06.9	92	83	92	89	-	0	NW 2	-	0
MES.	WRED.								WRED.								WRED.					
	706.8	705.9	706.7	03.7	12.3	07.2	07.7	13.5	02.5	-	04.6	04.8	05.1	76	49	68	64	2.1	2.2	2.0		

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1	704.9	704.8	706.0	06.2	08.2	06.6	07.0	09.3	06.0	-	06.7	07.2	06.4	95	86	87	90	-	0	F 1	I SE 3
2	706.6	707.5	709.4	05.7	09.5	07.4	07.5	09.8	05.2	-	05.8	06.1	05.8	85	65	75	76	ESE 2	-	C	SW 2
3	709.6	708.7	709.4	06.4	12.6	07.1	08.3	14.7	06.2	-	06.3	05.7	05.0	87	52	66	68	-	0	ENE 2	ESE 3
4	708.4	705.6	706.0	03.2	16.6	08.2	09.0	17.0	01.7	-	04.2	04.8	03.8	73	34	46	51	ESE 2	NE 1	ESE 2	
5	705.6	704.4	705.6	03.8	15.0	09.8	09.6	17.4	02.0	-	04.1	04.0	03.6	68	31	39	46	SF 2	W 1	E 5	
6	706.4	704.8	706.5	03.8	15.5	08.6	09.1	17.0	02.2	-	03.8	03.7	03.8	63	26	45	45	ESE 2	NE 3	E 3	
7	707.2	705.6	706.1	05.3	14.1	08.0	08.8	15.6	04.5	-	04.4	03.3	04.3	66	27	54	49	SF 3	NW 2	SSW 3	
8	705.7	705.4	706.4	05.9	08.2	05.9	06.4	09.2	04.0	-	06.7	06.5	05.9	96	79	85	87	E 2	WSW 3	-	
9	708.0	707.2	707.6	03.2	12.8	06.7	07.4	13.6	02.2	-	05.4	04.2	04.4	94	38	60	64	-	0	ENE 2	ENE 2
10	707.2	703.8	703.1	03.5	17.6	11.8	11.2	18.0	01.0	-	04.3	04.2	04.7	72	28	45	48	ESE 2	W 2	-	
11	700.0	698.7	698.6	07.4	11.9	09.0	09.3	13.0	05.8	-	04.9	06.2	07.3	63	59	85	69	ESE 1	WNW 1	E 1	
12	697.9	697.5	698.8	07.2	14.8	09.6	10.3	16.9	03.9	-	06.3	06.9	07.5	82	55	84	74	ESF 2	-	0	
13	700.3	699.9	700.9	07.8	18.0	10.5	11.7	18.5	04.3	-	05.9	06.3	06.8	74	41	71	62	-	0	S 1	W 2
14	697.9	696.5	698.1	08.2	05.1	00.7	03.7	11.0	00.6	-	07.8	06.2	04.6	95	94	95	95	NNW 2	NNW 1	SSW 1	
15	697.7	697.4	698.8	00.6	03.4	01.8	01.9	04.6	00.3	-	04.6	04.7	04.9	97	81	94	91	-	0	ESE 1	NW 2
16	699.3	699.3	699.8	01.0	04.3	02.2	02.4	05.1	00.4	-	04.8	04.9	05.0	97	79	94	90	W 2	SE 3	-</td	

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Den	Vrijeme 0-9	Oblačnost N (0-10)					Intenzitet broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6 10	020	00	04.0	C7.0	.	.	.	W n-9 = n-730 N-D, = 730 N		
2	7 08	06	10	08.0	C1.0	.	.	.	= n-7, 17-19.60		
3	6 10	06	00	05.3	C5.1	.	.	.	= n-D		
4	8 08	10	09	09.0	C0.0	.	.	.			
5	8 09	10	10	09.7	C0.0	00.1	.	.	• n-8 ^o 2015, FSE 2 ^o 2 ^o 4 ^o , 7 ^o 7 ^o		
6	8 09	08	10*	09.0	C3.2	04.3	.	.	• 16 ^o 23 ^o		
7	4 10*	10*	10	10.0	C0.0	C4.9	00	.	= n-7, *4 ^o n, □		
8	7 10*	10	10	10.0	C0.0	C4.3	02	.	*n-9 ^o , □		
9	7 10	10	10*	10.0	C0.3	00.1	00	.	= n-7, *2015 n		
10	5 10	10	10	10.0	C0.0	C1.1	01	.	*n-n, = n-n, □		
11	5 10*	10	10	10.0	C0.0	C1.3	01	.	*n 8 ^o = n-n, □		
12	8 09	09	09	09.0	C0.1	C0.1	00	.	= n-9 ^o		
13	6 02	000	00	00.7	C9.6	.	.	.	W n-8 ^o = n-n		
14	5 07	090	00	05.3	C1.7	.	.	.	W n-8 ^o = n-n, □ 13-15		
15	8 06	10	10*	06.7	C0.0	.	.	.	W n 8 ^o = n-10, F 11 ^o 13 ^o , • 17 n		
16	6 10	10	00	06.7	C0.9	C0.0	.	.	= n-n		
17	5 000	010	00	00.3	C9.5	.	.	.	W n-8 ^o = n-8 ^o		
18	8 010	010	08	03.3	C1.1	.	.	.	= n-8 ^o = 9 ^o N, F 6 21 ^o 23 ^o		
19	8 010	000	00	00.3	C0.9	.	.	.	= n-8 ^o		
20	8 040	070	00	03.7	C6.9	.	.	.			
21	8 000	000	00	00.0	C1.9	.	.	.	= 7 ^o 9 ^o		
22	8 000	00	00	00.0	10.8	.	.	.	△ 0-7 ^o 9 ^o = 7 ^o 9 ^o		
23	9 07	100	08	08.3	C2.7	.	.	.	• 13 ^o 13 ^o		
24	8 000	02	07	03.0	C8.7	C0.0	.	.			
25	8 08	10	02	06.7	C0.0	.	.	.			
26	8 07	09	04	06.7	C7.0	.	.	.	= 7 ^o 9 ^o N		
27	8 070	10	00	05.7	C5.1	.	.	.	= 7 ^o 9 ^o , F 13 ^o 14 ^o , • 14 ^o 14 ^o		
28	8 050	060	00	03.7	C4.1	C0.0	.	.	△ 0-7 ^o = 8 ^o 10 ^o 11 ^o 12 ^o 13 ^o 14 ^o		
29	8 000	050	06	03.7	C8.2	C1.4	.	.	= 5 ^o 9 ^o		
30	7 10	10	09	09.7	C0.0	.	.	.	= 5 ^o 9 ^o 12 ^o 23 ^o , W 2 ^o 12 ^o 14 ^o 18 ^o , = 12 ^o 15 ^o 18 ^o 22 ^o		
31	4 100	10	10*	10.0	C0.0	00.4	.	.	• n 12 ^o 17 ^o 23 ^o , W 2 ^o 12 ^o 14 ^o 18 ^o 22 ^o		
MES. VRRED.		06.4	06.8	05.2	06.1	126.2	18.0				

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1	6 10*	10*	10*	10*	10.0	00.0	01.4	.	= 0-18 ^o , • 2 ^o 16 ^o 20 ^o 23		
2	7 10	10	10	10	10.0	00.0	C1.0	.	= 0-11		
3	8 09	09	07	08.3	C2.3	.	.	.	= 0-9 ^o		
4	8 000	040	00	01.3	C1.7	.	.	.	= 0-9 ^o 14.45		
5	6 010	09	05	05.0	06.4	.	.	.			
6	7 050	010	00	02.0	C1.2	.	.	.	△ 2 ^o 8 ^o		
7	6 08	070	06	06.7	05.6	.	.	.	= 5 ^o 24		
8	7 09	09*	07	08.3	C0.4	C2.7	.	.	= 0-21 ^o , • 2 ^o 6 ^o 8 ^o 11 ^o 17 ^o 20 ^o , ▲ 11 ^o 14 ^o , ▲ 11 ^o 14 ^o 17 ^o		
9	8 10	06	00	05.3	06.0	C0.0	03.2	.	= 0-11 ^o		
10	8 000	080	02	03.3	C7.4	.	.	.	△ 3 ^o 8 ^o		
11	8 10	10*	10	10.0	00.0	.	.	.	• 13 ^o 20 ^o		
12	8 06	10	02	06.0	C2.5	C0.9	.	.	• 12 ^o 19 ^o		
13	8 030	050	08	05.3	C5.4	00.5	.	.	= 6 ^o 9 ^o = 18 ^o 20 ^o		
14	4 10	10*	10*	10*	10.0	00.0	C0.9	.	• 0-0 ^o 5 ^o 10 ^o 14 ^o 19 ^o , = 5 ^o 15 ^o 18 ^o 20 ^o , = 11 ^o 12 ^o 14 ^o 15 ^o , = 8 ^o 11 ^o 13 ^o 14 ^o		
15	5 10*	10	10*	10*	10.0	00.0	C4.9	00	* 0-11 ^o 21 ^o 24 ^o = 0-9 ^o 21 ^o 24 ^o , = 0-21 ^o 24 ^o , ▲ 14 ^o 12 ^o , ▲ 14 ^o 12 ^o 24 ^o		
16	7 10*	10*	10*	10*	10.0	00.0	C7.0	00	* 0-8 ^o 23 ^o 24 ^o = 0-8 ^o 23 ^o 24 ^o , = 8-23 ^o , ▲ 14 ^o 14 ^o 18 ^o		
17	6 10*	10*	10*	10*	10.0	00.0	C12.7	05	* 0-10 ^o 13 ^o 15 ^o 17 ^o 19 ^o = 11 ^o 13 ^o 15 ^o 17 ^o 19 ^o		
18	6 10*	10*	10*	10*	10.0	00.0	C6.5	02	* 0-4 ^o 5 ^o 4 ^o 12 ^o 12 ^o		
19	7 10*	10	08	05.3	C2.0	C8.4	00	.	* 0-5 ^o 6 ^o 5 ^o 10 ^o = 1 ^o 10 ^o 12 ^o 12 ^o , = 1 ^o 10 ^o 12 ^o 12 ^o 17 ^o		
20	7 030	050	10	06.0	09.5	C1.0	.	.	= 0-12 ^o , ▲ 14 ^o 8 ^o 4 ^o 6 ^o 3 ^o = 17 ^o		
21	8 000	09	10	06.3	06.1	.	.	.	= 7 ^o 9 ^o = 8 ^o 14 ^o 17 ^o		
22	7 09	09*	03	07.0	02.9	C1.5	.	.	= 5 ^o 12 ^o = 6-7 ^o 10 ^o 11 ^o 17 ^o		
23	8 09	08*	01	06.0	06.1	C1.7	.	.	= 3 ^o 23 ^o 24 ^o = 13 ^o 14 ^o		
24	8 000	060	10	05.3	08.9	00.0	.	.	= 0-7 ^o 5 ^o 13 ^o 15 ^o		
25	7 10	10	10*	10*	10.0	00.0	C0.0	.	* 3 ^o 4 ^o 9 ^o 14 ^o 14 ^o 14 ^o = 15 ^o 24		
26	7 000	07	07	05.7	06.6	03.1	.	.	• 0-0 ^o 11 ^o 14 ^o 15 ^o = 0-2 ^o 14 ^o 8 ^o 13 ^o ▲ 13 ^o 13 ^o F 12 ^o 12 ^o		
27	8 020	10	10	07.3	06.1	05.0	.	.	• 4 ^o 16 ^o		
28	8 09	10	09	09.3	02.0	00.0	.	.	F 2 ^o 19 ^o 13 ^o 13 ^o = 16 ^o 16 ^o		
29	8 09	09	00	06.0	06.7	C3.0	.	.	* 13 ^o 5 ^o		
30	8 09	10	08	09.0	00.0	00.3	*	.	F 13 ^o 9 ^o 9 ^o 17 ^o = 15 ^o 19 ^o 19 ^o , R 15 ^o 16 ^o		
MES. VRRED.		06.7	08.5	06.7	07.3	114.1	66.2				

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 $\varphi = 43^{\circ}52'$ N $\lambda = 18^{\circ}26'$ E Gr. $\Delta G = +1h\ 14\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	7	14	21
1	689.5	690.1	692.2	09.2	13.2	10.6	10.9	15.0	07.3	-	05.7	06.1	07.0	66	53	72	64	SW	1	SSW	3	-	0
2	694.1	698.3	699.1	08.2	09.2	08.9	08.8	10.1	07.5	-	07.8	07.7	07.3	95	88	86	90	W	3	WSW	1	-	0
3	701.2	701.1	702.0	08.6	16.8	11.3	12.0	17.2	06.7	-	07.2	06.5	06.5	86	45	65	65	SE	1	S	2	S	2
4	700.3	699.4	699.6	11.2	11.0	07.8	09.4	13.6	07.2	-	05.9	06.5	07.1	59	66	90	72	S	2	E	3	-	0
5	698.4	698.3	699.6	10.4	12.1	06.5	08.9	15.8	05.6	-	06.0	06.2	06.5	63	58	90	70	S	2	S	2	NE	1
6	699.5	701.9	703.5	07.7	11.6	08.6	09.6	14.1	04.0	-	06.0	07.3	06.9	77	71	77	75	-	0	SSW	1	-	0
7	705.5	705.4	707.7	08.2	16.4	10.0	11.2	16.7	05.4	-	06.5	06.1	07.3	79	44	79	67	ESE	1	SW	2	NNW	1
8	707.4	706.2	705.2	10.4	12.2	05.6	10.4	14.5	07.0	-	06.8	07.1	06.6	72	67	74	71	ESE	1	SE	1	ENE	4
9	704.3	704.4	705.1	08.4	10.4	07.6	08.5	11.8	07.4	-	06.5	05.6	06.3	78	59	80	72	WSW	2	-	0	-	0
10	705.7	704.4	704.6	05.6	16.8	10.8	11.0	18.0	03.6	-	05.9	04.8	05.3	86	34	55	58	-	0	SW	2	ESE	3
11	706.6	706.2	706.9	07.6	19.5	14.0	13.8	20.9	04.4	-	05.4	06.2	07.0	69	36	58	54	E	2	W	2	-	0
12	707.9	706.8	710.3	11.5	19.0	10.8	13.0	20.9	08.7	-	06.8	07.2	09.1	67	44	93	68	WSW	1	NW	2	-	0
13	711.6	711.7	711.4	10.2	15.3	10.6	11.7	17.6	07.0	-	08.5	07.2	06.5	91	55	68	71	-	0	NNW	1	SSE	2
14	710.6	707.6	707.3	09.2	22.7	16.6	16.3	22.9	06.2	-	06.9	07.3	07.4	79	35	52	55	SE	2	NW	2	NNW	2
15	707.8	706.8	705.4	07.7	05.4	06.6	06.6	16.6	05.1	-	07.6	06.4	06.7	96	94	92	94	WNW	2	E	3	-	0
16	704.3	704.6	705.1	06.4	09.8	05.1	08.6	12.5	05.5	-	06.8	06.8	06.3	95	75	73	81	-	0	W	1	SE	1
17	706.0	707.3	708.7	07.7	12.6	10.8	10.5	15.5	04.2	-	06.1	08.6	06.7	78	79	69	75	SE	1	M	1	-	0
18	709.6	709.6	709.7	08.2	10.9	10.0	09.8	11.3	07.6	-	07.3	08.6	08.6	90	88	93	90	-	0	-	0	-	0
19	709.0	708.5	709.0	10.0	15.7	12.6	12.8	17.0	05.3	-	09.0	07.0	07.1	98	52	64	71	-	0	SE	1	-	0
20	709.3	707.3	708.0	10.4	22.0	12.8	14.5	22.5	07.2	-	08.5	08.7	07.1	90	44	64	66	-	0	S	2	ESE	1
21	709.4	708.6	709.6	09.5	17.8	13.6	13.6	18.3	08.0	-	08.6	10.0	09.2	96	65	79	80	-	0	W	1	-	0
22	707.9	703.3	700.0	09.4	20.8	17.1	16.1	21.5	06.7	-	07.7	08.1	07.3	87	44	50	60	-	0	WSW	1	N	4
23	701.3	700.0	699.6	06.9	15.3	10.4	10.8	17.5	06.4	-	06.8	06.0	06.0	91	46	64	67	-	0	WNW	2	ESE	2
24	699.9	699.3	700.2	09.4	17.4	15.5	14.4	18.0	07.3	-	07.2	08.0	07.6	81	54	57	64	-	0	S	4	SW	2
25	703.6	704.1	707.0	09.0	16.9	13.0	13.0	19.1	04.3	-	08.2	06.8	07.0	95	47	63	68	SE	1	W	2	-	0
26	709.9	709.2	708.6	09.4	19.2	12.6	13.6	19.8	06.5	-	07.4	06.3	06.7	84	38	61	61	-	0	SW	1	ENE	1
27	709.8	706.5	705.7	08.6	22.4	14.7	15.1	22.4	05.5	-	06.6	07.3	08.0	78	36	64	59	-	0	W	2	ESE	2
28	704.5	701.7	701.0	11.1	22.8	16.2	16.6	23.1	08.3	-	07.8	07.9	07.7	79	38	56	58	-	0	W	2	E	2
29	701.3	702.0	704.5	11.1	14.1	12.3	12.4	18.6	10.1	-	08.9	10.5	09.7	90	87	90	89	W	2	NE	1	-	0
30	708.1	707.9	708.6	10.9	22.4	16.0	16.3	22.5	09.8	-	09.2	10.2	10.2	94	50	75	73	-	0	WNW	1	ESE	2
31	708.7	708.4	708.3	14.6	21.5	15.8	16.9	26.0	11.4	-	09.8	09.2	10.2	78	48	75	67	ESE	1	ESE	1	ENE	1
MES.	VRED.	704.9	704.4	705.0	09.2	15.9	11.7	12.2	17.8	06.8	-	07.3	07.4	07.4	83	56	72	70	0.8	1.6	1.1	1.1	1.1

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1	706.9	705.5	708.6	14.0	21.8	13.4	15.6	22.1	12.1	-	10.2	11.6	10.8	85	59	94	79	W	1	WSW	1	W	1
2	710.2	711.6	711.9	11.4	12.6	11.5	11.8	14.2	11.4	-	09.9	09.0	09.4	98	82	92	91	WNW	2	W	1	-	0
3	711.8	712.3	711.9	11.5	15.6	12.7	13.1	16.8	10.4	-	08.6	07.2	07.8	85	54	71	70	E	1	NNW	1	ESE	1
4	711.7	710.0	710.4	11.0	23.2	15.9	16.5	23.8	08.2	-	08.0	11.9	09.6	81	56	71	69	ESE	1	WSW	2	ESE	1
5	710.0	708.4	708.4	12.8	27.0	18.8	19.4	27.0	09.8	-	08.8	07.4	11.3	79	28	69	59	-	0	W	2	W	3
6	707.2	705.7	705.1	15.1	23.6	19.2	19.4	24.6	11.9	-	10.7	11.4	08.8	83	51	53	62	ESE	2	W	1	-	0
7	704.8	706.9	709.1	13.5	13.5	11.8	12.6	19.2	11.2	-	10.9	10.0	08.1	94	87	78	86	ESE	2	WNW	2	ESE	2
8	710.7	708.6	707.6	09.9	19.5	13.2	14.0	20.2	08.0	-	06.9	07.2	08.1	75	42	71	63	W	2	WNW	2	SE	2
9	705.7	703.8	703.2	11.1	22.1	19.2	17.9	22.7	08.2	-	08.3	09.6	06.9	83	48	41	57	-	0	WNW	2	S	4
10	702.4	701.5	700.2	17.6	20.4	18.4	18.7	21.5	13.2	-	07.4	09.0	08.3	49	50	52	50	S	4	ESE	4	S	2
11	699.1	702.5	704.8	08.8	09.9	07.1	08.2	19.0	07.1	-	08.1	06.6	07.2	95	72	95	87	E	2	W	3	-	0
12	704.2	702.0	703.2	06.9	16.4	07.7	09.7	17.1	05.2	-	07.1	05.4	07.2	95	39	91	75	-	0	W	2	-	0
13	701.0	700.2	701.7	06.9	12.0	09.3	09.4	16.8	05.0	-	06.5	07.4	07.1	87	71	81	80	-	0	-	0	SE	1
14	702.8	703.6	705.2	08.9	17.4	14.0	13.6	17.6	04.9	-	06.3	07.0	08.2	74	47	68	63	-	0	WNW	3	-	0
15	707.1	705.8	706.4	13.4	23.6	16.2	17.4	23.6	11.0	-													

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$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vidljivost 0-9	Oblakost N (0-10)					Instalacija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	8	09	09	09	09.0	01.2	06.6	.	.	• H ²⁵ H ⁴⁰ 13 ⁴⁰ 16 ²¹ 24 ²⁴	
2	5	10	10	08	09.3	00.0	03.0	.	.	• 0-12 ³⁰ = 4 ²⁴	
3	6	08	06	02	05.3	02.7	01.7	.	.	= 0-19 ³⁰ 15 ²⁰ 18 ²⁰	
4	7	09	10	10	09.7	00.6	00.3	.	.	F _{sw} M ¹¹ 25 ²⁵ • H ²⁰ 14, 17 ²⁰ 22 ²⁰	
5	8	06	09	05	06.7	03.1	02.9	.	.	• 12 ²⁵ 18 ²⁵ F _{sw} 13 ⁴⁵ , 18 ²⁵ 18 ²⁵	
6	8	04	08	09	07.0	04.2	02.2	.	.	• H-13 ⁴⁰ 16 ⁴⁵ 24 ²⁰ , F _{sw} 13 ⁴⁰	
7	8	04	04	10	06.0	05.4	01.6	.	.	• 16 ²⁰ 10 ⁴⁰ 19 ²⁵ 21 ²⁵	
8	7	04	10	09	07.7	01.2	00.3	.	.	• 10 ²⁵ 15 ²⁵	
9	6	10	10	10	10.0	00.0	CC.7	.	.	= 1 ²⁴ 15 ²⁵ 17 ⁴⁵	
10	7	00	03	00	01.0	11.8	00.2	.	.	= 0-2 ²⁵ , △ 1 ²⁵ 17 ⁴⁵	
11	7	01	08	00	03.0	09.7	.	.	.	△ 2-5 ⁴⁵	
12	7	05	08	10	05.0	04.7	.	.	.	• 7 ²⁵ 05 ²⁵ 18 ⁵⁰ 20 ³⁰ , R 48 ⁴⁵	
13	6	10	10	00	06.7	02.8	02.8	.	.	= 1 ²⁰ 20 ⁵⁰	
14	8	00	04	03	02.3	08.3	.	.	.	≤ 20 ⁵⁰ 22 ⁵⁰	
15	5	10	10	10	10.0	00.0	01.6	.	.	= 3-18 ⁵⁰ 20-24, • 3 ²⁰ 17 ⁴⁵ 20-21 ⁵⁰	
16	7	10	10	04	08.0	03.0	11.8	.	.	= 0-11 ²⁵ 1-5 ²⁵ 23-24, • 6 ²⁰ B ⁸⁰ 13 ²⁵ 13 ⁵⁰	
17	6	09	10	03	07.3	04.0	01.2	.	.	= 0-17 ⁵⁰ 6 ²⁵ 6 ²⁵ 6 ²⁵ = 6 ²⁴ 24, • 7 ²⁵ 44 ²⁰	
18	5	10	10	10	10.0	00.0	02.8	.	.	= 0-24, • 3 ²⁵ 13	
19	6	10	05	09	05.3	02.2	01.9	.	.	= 0-24, • 1 ²⁵ 5 ⁵⁰	
20	7	01	06	02	03.0	07.5	.	.	.	= 0-10 ²⁵ , △ 3 ²⁵ 7 ²⁵ 21 ²⁵ 24	
21	6	10	10	09	09.7	02.2	04.0	.	.	△ 0-4 ²⁰ 4 ²⁰ 9 ²⁵ 14-17 ²⁵ , = 6-21 ²⁵ , R _{NW} 14-14 ²⁰	
22	6	05	09	10	08.0	03.6	04.7	.	.	△ 2 ²⁵ 6 ²⁵ = 4 ²⁵ 20, • 17 ²⁵ 18 ²⁵ , 20 ²⁵ 24, R _N 20 ²⁵ , R _E 21 ²⁵ 23 ⁴⁵	
23	7	08	06	09	07.7	07.0	17.0	.	.	• 0-5, 23 ²⁵ 23 ²⁵	
24	7	09	10	10	09.7	04.9	00.4	.	.	= 10 ²⁵ 18 ²⁵ 24, • 2 ²⁵ 3 ²⁵ 13 ²⁵ 14, R _E 13 ⁴⁵	
25	8	09	03	04	07.0	04.9	07.6	.	.	= 0-5, △ 2 ²⁵ 6 ²⁵ , 12 ²⁵ 13 ²⁵ , R _E 5 ²⁵	
26	8	03	01	00	01.3	13.0	00.0	.	.	△ 23-24	
27	8	00	03	00	01.0	14.0	.	.	.	△ 0-8 ⁰⁵	
28	8	01	10	05	05.3	07.8	.	.	.	△ 23-24	
29	7	09	09	03	07.0	01.6	11.2	.	.	△ 0-2 ²⁵ 20 ²⁵ 24, = 0 ²⁵ 6 ²⁵ 23 ²⁵ 24, • 2 ²⁵ 6 ²⁵ 13 ²⁵ 16 ²⁵ , F _E 5 ²⁵ 6 ²⁵ , △ 13 ²⁵ 13 ⁴⁵	
30	7	10	04	09	07.7	05.8	03.4	.	.	= 0-10 ²⁵ , △ 0-10 ²⁵ 20 ²⁵ 24	
31	8	04	10	06	06.7	07.0	.	.	.	△ 0-7 ²⁵ , △ 18 ²⁵ 19 ²⁵	
MES. VRKD.		06.5	07.9	06.1	06.8	144.2	51.1				

1	7	10	09	10	C9.7	C2.2	CC.9	.	.	= 5-24, • 5 ²⁵ 10 ²⁰ 19 ²⁵ 24	
2	6	10	10	10	10.0	00.0	21.6	.	.	• 0-10 ²⁵ 15 ²⁵ 17 ²⁵ 19 ²⁵ 24, = 1-24	
3	7	09	10	08	C9.0	C3.0	C1.7	.	.	• 0-5 ²⁵ , = 0-9 ²⁵ 17 ²⁵ 24	
4	6	00	04	00	01.3	13.5	.	.	.	= 0-24, △ 9 ²⁵ 8 ²⁵	
5	7	00	01	10	C3.7	12.4	.	.	.	= 0-13 ²⁵ , △ 2-9, • 17 ²⁵ 10 ²⁵ 21 ²⁵ , R _E 19 ²⁵ 22 ²⁵	
6	8	06	09	C5	06.7	C4.7	C9.6	.	.	• 10-10 ²⁵ , R _E 10 ²⁵	
7	6	10	10	10	10.0	00.0	C5.7	.	.	• 1 ²⁵ 11 ²⁵ = 7 ²⁵ n	
8	8	00	03	00	01.0	13.0	04.3	.	.	= 0-1 ²⁵ △ 20-24	
9	7	04	05	C5	C7.7	03.3	.	.	.	△ 0-8 ²⁵ = 6-9 ²⁵ , 9 ²⁵ 10 ²⁵ F _E 20 ²⁵	
10	7	03	05	00	04.0	07.9	00.2	.	.	F _{sw} , 14 ²⁵ , 48 ²⁵ , 19 ²⁵ , 22 ²⁵ , 23 ²⁵	
11	7	10	10	10	10.0	00.5	C9.9	.	.	• 3 ²⁵ 6 ²⁵ H ²⁰ 12 ²⁵ 17 ²⁵ 19 ²⁵ = 3 ²⁵ 6 ²⁵ 18 ²⁵ 24, F _E -w 2 ²⁵ , 13 ²⁵ 18 ²⁵ 10 ²⁵ , R _E 4 ²⁵	
12	7	01	09	10	06.7	07.4	02.0	.	.	= 0-9 ²⁵ , F _{sw} 2 ²⁵ , • 14 ²⁵ 24 ²⁵ , 17 ²⁵ 21 ²⁵	
13	8	C7	07	03	C5.7	C9.6	C2.0	.	.	= 0 ²⁵ 8 ²⁵ 22 ²⁵ 24, = 5-9 ²⁵ , • 12-15 ²⁵ , 18 ²⁵ 18 ²⁵ , F _E 12 ²⁵ , R _E 13 ²⁵ 13 ²⁵	
14	8	01	07	09	05.7	04.5	01.6	.	.	△ 0-8	
15	P	01	04	10	C5.0	C9.4	.	.	.	△ 3-9-23-24, = 6-9 ²⁵	
16	7	01	10	10	07.0	07.4	.	.	.	△ 0-9 ²⁵ 20 ²⁵ 24, = 3-9 ²⁵ 23-24	
17	7	04	C5	07	05.3	C9.4	.	.	.	△ 0-7 ²⁵ , = 0-19 ²⁵ , R _E 15 ²⁵ 17 ²⁵ , △ 16 ²⁵ 19 ²⁵	
18	6	00	03	09	04.0	05.6	.	.	.	= 0-24, △ 0 ²⁵ M ²⁰ 12, 20-22 ²⁵	
19	6	10	10	10	10.0	00.0	02.1	.	.	= 0-24, △ 23-24	
20	6	04	10	10	08.0	04.1	00.5	.	.	= 0-24, △ 0-9 ²⁵ , △ 19 ²⁵	
21	6	C9	06	06	08.0	C1.4	.	.	.	= 0 ²⁵ 7 ²⁵ , = 0-19 ²⁵ , 18 ²⁵ 13 ²⁵ , △ 13 ²⁵ 14 ²⁵ , F _N 13 ⁴⁵	
22	5	C1	08	03	04.0	08.4	00.5	.	.	△ 0 ²⁵ 10 ²⁵	
23	7	07	06	04	05.7	08.5	C2.5	.	.	• 14 ²⁵ 4 ²⁵ 18 ²⁵ 18 ²⁵ 22 ²⁵ 24, F _N 18 ²⁵ 18 ²⁵	
24	7	09	07	09	C8.3	C3.3	.	.	.	• 0-5, 7 ²⁵ 14 ²⁵ , = 3-9 ²⁵ , △ 23 ²⁵ 24	
25	7	10	07	07	08.0	07.3	14.0	.	.	• 0-24, △ 0-9 ²⁵ , △ 19 ²⁵	
26	8	02	03	01	02.0	12.5	C1.2	.	.	△ 0-7 ²⁵	
27	8	10	05	08	09.0	05.7	.	.	.	F _N , 5 ²⁵ 5 ²⁵ 0 ²⁵ 12 ²⁵ 14 ²⁵ 15 ²⁵	
28	7	10	10	10	10.0	02.2	10.6	.	.	• 2 ²⁵ 6 ²⁵ 14 ²⁵ 5 ²⁵ 17 ²⁵ , △ 22 ²⁵ 24	
29	7	09	09	10	09.3	02.4	00.1	.	.	△ 0-7 ²⁵ , 7 ²⁵ 17 ²⁵ 24, = 19 ²⁵ 24, △ 19 ²⁵ 20, R _E 20 ²⁵ 22	
30	6	10	10	07	C9.0	01.4	31.1	.	.	• 0-0 ²⁵ , 3 ²⁵ 4 ²⁵ , = 0-10 ²⁵	
MES. VRKD.		05.8	07.6	07.0	06.8	175.4	122.7				

$\varphi = 43^{\circ}52'$ N $\lambda = 18^{\circ}26'$ E Gr. $\Delta G = +1h\ 14\ min.$

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D E G	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	707.7	708.0	708.4	12.6	23.4	16.5	17.4	23.9	10.6	-	09.5	09.9	05.5	87	46	66	66	-	0	W	2	-	0
2	710.3	710.2	711.3	13.9	23.3	17.3	18.0	24.0	11.7	-	09.4	11.0	09.0	79	51	61	64	-	0	-	C	ESE	3
3	711.0	707.1	705.5	12.9	26.0	19.6	19.5	26.4	10.2	-	08.5	06.1	05.4	76	24	55	52	W	1	W	2	-	0
4	706.9	707.1	707.5	17.2	20.3	18.0	18.4	20.8	15.3	-	11.5	10.8	10.6	78	61	69	65	-	0	SE	4	ESE	3
5	703.4	707.0	708.9	16.2	26.7	20.7	21.1	26.8	13.2	-	10.2	13.2	13.2	74	50	72	65	-	0	W	3	ESE	2
6	708.7	704.7	706.1	16.5	27.8	19.8	21.0	28.1	14.2	-	11.8	14.2	12.4	84	51	72	69	-	0	W	3	-	0
7	704.8	710.1	709.0	17.6	10.9	05.4	11.8	20.0	09.4	-	11.6	09.1	08.4	77	93	95	88	-	0	SW	2	-	0
8	709.7	704.0	710.0	09.2	14.4	09.5	10.8	16.9	07.0	-	08.3	07.1	06.9	95	58	75	76	-	0	NNW	3	ESE	2
9	711.4	709.9	709.2	08.8	20.6	14.4	14.6	21.3	06.9	-	07.3	07.7	07.8	86	42	63	64	-	0	W	3	ESE	1
10	708.8	708.9	708.4	17.0	21.2	17.6	17.1	22.0	10.4	-	08.9	09.6	10.6	85	51	70	69	W	1	NNW	1	SSE	2
11	710.5	709.6	709.9	15.6	24.2	16.8	18.4	24.8	13.7	-	10.5	08.5	10.1	79	37	70	62	-	0	NNW	2	-	0
12	709.5	709.4	709.7	16.4	29.8	20.5	22.0	29.8	12.6	-	10.4	10.5	12.0	74	33	65	57	ESE	2	W	3	-	0
13	710.3	707.9	708.1	17.0	31.0	21.2	22.6	31.0	13.6	-	10.6	12.1	10.5	73	36	56	55	ESE	1	W	2	-	0
14	708.3	707.5	708.2	18.3	30.8	21.2	22.5	31.0	13.7	-	09.2	09.8	11.7	58	29	62	50	ESE	3	W	2	-	0
15	709.7	709.2	709.8	16.8	32.0	22.8	23.6	32.0	14.0	-	09.4	11.3	11.0	66	32	53	50	E	3	NW	2	-	0
16	709.3	708.1	707.7	18.0	31.8	22.8	23.8	32.4	15.7	-	11.1	11.4	12.7	72	32	61	55	ESE	2	SW	2	-	0
17	706.2	704.1	703.7	20.4	33.0	25.8	26.2	33.1	16.7	-	11.2	09.0	05.8	62	24	40	42	ESE	1	WSW	4	-	0
18	702.5	701.9	703.2	20.4	29.6	20.1	22.6	29.8	17.8	-	10.5	09.3	10.5	58	30	60	49	-	0	SSW	4	-	0
19	702.8	703.7	704.2	17.5	14.4	12.9	14.4	20.2	12.8	-	12.9	10.8	10.7	86	88	96	90	W	1	-	C	WSW	1
20	704.5	705.6	705.6	11.5	10.8	10.8	11.0	13.2	10.3	-	09.7	08.9	05.3	96	92	95	94	NNW	1	W	1	-	0
21	710.4	707.9	704.6	10.4	11.9	10.8	11.0	12.9	09.8	-	08.8	08.6	09.3	93	83	95	90	-	0	W	1	-	0
22	706.2	707.3	707.1	10.7	12.5	11.2	11.4	13.3	10.3	-	05.3	09.0	09.1	97	83	91	90	W	1	-	0	-	0
23	706.0	707.2	708.6	10.8	12.9	11.8	11.9	13.0	10.2	-	09.3	10.6	09.9	95	95	96	95	-	0	W	2	SE	1
24	709.0	707.9	707.5	11.9	24.6	19.4	18.8	24.9	10.3	-	09.9	10.4	11.2	96	45	67	69	-	0	NW	2	-	0
25	707.6	705.9	708.3	14.6	27.2	16.8	18.7	27.2	11.7	-	09.3	11.2	11.4	75	41	81	66	SE	2	W	3	SW	2
26	710.3	710.4	710.8	12.9	18.4	13.2	14.4	18.5	12.8	-	08.5	10.2	08.8	76	64	77	72	ESE	3	SSE	3	E	2
27	710.8	709.2	709.7	10.3	25.0	17.6	17.8	25.4	08.7	-	08.4	11.3	10.9	86	48	72	69	-	0	W	1	S	2
28	710.6	709.6	711.2	14.0	27.8	20.5	20.7	27.8	10.8	-	09.5	11.8	10.7	79	42	59	60	ESE	1	W	1	-	0
29	712.5	711.2	711.9	15.2	27.8	20.9	21.2	28.4	13.2	-	10.9	15.5	11.9	84	55	64	68	SE	1	NNW	2	E	1
30	711.2	709.2	708.2	16.9	29.0	21.3	22.1	29.4	14.3	-	11.9	10.0	13.9	82	33	72	63	-	0	W	1	ESE	2
31	708.2	706.6	707.4	17.4	30.4	21.3	22.6	30.5	15.8	-	12.2	11.3	15.6	82	35	82	66	SSE	1	NNW	1	ESE	2
MES. MRED.	708.3	707.8	708.1	14.6	23.5	17.5	18.3	24.5	12.2	-	10.0	10.3	10.6	80	51	71	68	0.6	2.0	0.8			

1	707.8	707.1	707.8	18.8	28.9	20.5	22.2	28.9	16.6	-	13.1	14.9	13.7	81	50	76	69	SE	1	SW	2	E	2
2	708.4	707.3	708.0	16.7	30.4	22.1	22.8	30.4	14.8	-	11.6	13.3	13.6	81	41	68	63	ESE	2	WSW	1	E	2
3	709.9	708.4	709.3	17.4	32.1	23.0	23.9	32.2	15.6	-	11.7	12.0	13.3	78	33	62	58	-	0	WSW	1	E	2
4	710.2	708.7	708.9	18.2	32.6	23.7	24.6	32.4	16.0	-	11.8	10.1	13.7	75	27	62	55	ESE	1	-	0	SE	1
5	710.5	708.6	708.7	18.6	32.2	21.8	23.6	32.4	16.7	-	13.5	08.8	10.4	64	24	53	54	ESE	1	NW	1	-	0
6	710.8	711.7	711.9	16.8	20.5	16.6	17.6	21.8	14.7	-	11.7	11.0	09.8	81	61	69	70	-	0	E	1	NW	2
7	710.6	707.4	707.1	12.5	24.2	17.3	17.8	25.0	10.2	-	08.9	10.3	10.2	82	46	69	66	-	0	W	2	ESE	2
8	705.9	703.6	702.7	13.2	29.2	22.0	21.6	29.8	11.2	-	09.0	10.8	12.0	79	36	61	59	-	0	NW	2	-	0
9	704.0	701.6	705.9	16.0	27.5	14.8	17.0	26.1	14.3	-	11.6	13.3	11.9	85	65	94	81	N	1	WNW	2	-	0
10	708.2	705.8	704.6	13.5	25.1	17.8	18.6	25.4	10.3	-	09.5	10.0	10.5	82	42	68	64	E	1	E	2	ESE	2
11	701.9	700.5	706.0	13.5	16.9	11.6	13.4	21.2	11.6	-	11.2	12.7	08.1	97	86	79	88	ESE	3	W	2	W	3
12	706.7	706.6	708.3	08.0	17.7	13.5	13.2	19.3	06.9	-	07.6	07.7	08.2	95	51	71	72	-	0	W	4	-	0
13	710.5	710.3	711.8	12.6	22.0	13.5	15.4	22.2	11.4	-	08.9	07.5	08.9	81	38	77	65	-	0	W	2	-	0
14	713.0	712.2	713.1	11.4	27.0	16.7	16.0	27.4	08.2	-	07.8	10.4	08.8	77	39	54	57	ESE	1	WNW	2	SE	2
15	714.4	713.2	713.7	13.3	29.0	19.8	20.5	29.3	11.4	-	09.3	13.0</td											

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$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vrijeme 0-9 0-9	Oblačnost N (0-10)					Inadocija broj satni	Padavine R mm	Snožni pokriva h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	030	040	00	C2.2	11.2	02.2	.	= 0-10 ³⁰ □ 045.8 ³⁰ , 20 ³⁰ 24	
2	8	07	050	07	C6.3	04.1	.	.	△ 0-8 ³⁰	
3	8	000	000	00	CC.0	14.0	.	.	△ 0 ²⁰ 9, 21 ¹⁰ 24	
4	7	10	10	10	10.0	00.0	.	.	△ 0-9 ⁵⁰	
5	8	000	010	02	C1.0	10.2	.	.	= 1 ¹⁰ 9, □ 1 ²⁰ 9, 20 ³⁰ 24	
6	8	000	080	00	02.7	C7.5	.	.	△ 0-8 ¹⁰ 21 ³⁰ 24; □ 13 ⁴⁰ 13 ⁵⁵ □ 13 ⁵⁵ 14 ⁴⁵ □ 14-11 ⁰⁵	
7	6	06	10	00	C5.3	C3.6	00.6	.	△ 0-8 ³⁰ □ 9 ⁴⁰ 14 ⁴⁰ R 9 ³⁰ □ 10 ⁰⁰ ; = 10 ⁵⁰ 15	
8	8	10	10	01	07.0	02.1	13.0	.	= 1 ¹⁰ 8 □ 20 ³⁰ 24	
9	8	10	030	02	C5.0	C6.3	.	.	△ 0-9, 21 ⁰⁰ 24	
10	8	100	080	10	05.3	04.5	00.0	.	△ 0-6, □ 5 ⁵⁰ □ 20	
11	7	05	10	02	05.7	C8.5	CC.0	.	△ 0-9, 21 ¹⁰ 24	
12	8	040	000	00	01.3	13.5	.	.	△ 0-8 ³⁰ , 22 ³⁰ 24	
13	8	000	000	00	CC.0	14.0	.	.	△ 0-8	
14	8	000	000	00	00.0	13.9	.	.		
15	8	000	000	00	CC.0	13.2	.	.	△ 0-8	
16	8	000	010	03	01.3	12.1	.	.		
17	8	040	C10	00	C1.7	11.6	.	.	Fsw 14 ¹⁰	
18	8	000	010	02	01.0	11.2	.	.	△ 3 ⁵⁰ □ 7 ³⁰ Fsw 12 ⁰⁵ 12 ²⁵	
19	7	09	10	10	C5.7	C6.5	.	.	= 0-9, 14 ³⁰ 24; □ 0 ²⁰ 9, □ 10 ⁵⁰ 13 ⁴⁰ □ 14 ⁴⁵ 16 ⁰⁵ 18 ¹⁰ 24, □ 18 21 ¹⁰ 23	
20	6	10	10	10	10.0	CC.0	14.5	.	● 0-1 ⁰⁰ 18 ⁰⁰ 24; = 0-24, R b=1	
21	6	10	10	10	10.0	CC.0	C1.0	.	= 0-24, □ 0-6 ³⁰ 24 ³⁰ 24; □ 9 ⁵⁵ 10 ⁴⁵ 10 ⁵⁰ 19 ⁵⁰	
22	7	10	10	10	10.0	CC.0	11.4	.	● 0-9 ³⁰ 14 ⁵⁵ 15 ³⁰ , □ 20 ⁵⁰ 23 ⁵⁰ ; = 0-12, 21 ¹⁰ 24; □ 9 ⁴⁰ 11 ¹⁰	
23	7	10	10	09	C9.7	CC.0	04.2	.	= 0-20, □ 0 ²⁰ 11 ¹⁰ 16 ⁵⁵ 17 ³⁰	
24	8	10	010	00	C3.7	C9.6	C5.8	.	= 9-11	
25	8	000	030	07	C2.3	12.4	.	.	△ 0 ¹⁵ 8	
26	8	10	10	03	07.7	00.0	.	.	△ 22 ⁴⁵ 24	
27	8	000	000	00	CC.0	13.4	.	.	△ 0-8 ³⁵ 21 ⁴⁰ 24	
28	8	000	010	C1	CC.7	12.8	.	.	△ 0-7 ³⁰ , 22 ¹⁰ 24	
29	8	000	010	C1	CC.7	13.1	.	.	△ 0-9, 21 ³⁰ 24; = 8 ³⁰ 11	
30	7	000	010	00	CC.3	12.9	.	.	△ 0-9, 21 ³⁰ 24; = 8 ³⁰ 11	
31	8	000	010	00	00.3	12.6	.	.	△ 0-8, = 8 ³⁰ 11 ³⁰ , □ 15 ³⁰ 18 ¹⁵ , □ 17 ¹⁵ 18 ⁰⁵	
MES. MRED.		04.4	04.5	C3.2	04.1	252.2	C3.1			

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1	8	010	060	00	C2.3	C8.5	C1.7	.	△-0-8,23-24; = 8 ³⁰ 12, • 14 ³⁰ 14 ⁰⁰
2	8	000	010	00	00.3	12.9	C0.C	.	△-0-8,23-24; = 6-9
3	7	000	030	00	C1.0	12.8	.	.	△-0-8,23-24;
4	8	000	020	C1	01.0	12.0	.	.	△-0-7 ³⁰ , = 3 ³⁰ 7 ³⁰
5	8	000	000	00	00.0	12.6	.	.	△-0-8, = 5 ³⁰ 9
6	8	05	10	02	05.7	00.6	.	.	△-0 ³⁰ 8,22 ³⁰ 24
7	8	010	010	00	CC.7	12.8	.	.	△-0-8,20 ³⁰ 24; = 4 ¹² 9 ³⁰
8	7	000	010	03	C1.3	12.4	.	.	△-0-7 ³⁰ , = 2 ³⁰ 11, 23-24, 12 23 ⁴⁰ 24
9	8	09	10	C2	07.0	C6.5	C1.2	.	18.0-0 ³⁵ 10 ³⁰ 15 ³⁰ , = 0-6, • 0 ²⁰ 6 ³⁰ , 14 ⁰⁵ 15 ³⁰ ; △12 ³⁰ -13 ³⁵
10	8	010	040	00	01.7	12.6	05.C	.	△-0-9 ³⁰ 23-24
11	7	10	1C≡	10	1C.0	CC.9	C4.3	.	△-0-3 ²⁰ 18 3 ⁴⁵ 4 ⁰⁰ 11354 ³⁰ , • 3 ²⁰ 7 ³⁰ 124514 ³⁰ ; △124514 ³⁰
12	8	060	09	06	C7.0	05.1	06.1	.	△-0-9,23-24; = 6-8 ³⁰
13	8	06	040	02	04.0	C9.3	.	.	△-0-8,21 ³⁰ 24
14	8	000	010	00	00.3	13.2	.	.	△-0-8,21 ³⁰ 24
15	8	040	010	00	01.7	12.1	.	.	△-0-8,23 ³⁰ 24
16	8	010	07	00	02.7	C8.6	.	.	△-0-8,24 ³⁰ 24; = 22 ³⁰ D4
17	6	000	010	00	00.3	12.2	.	.	△-0-7 ³⁰ 20 ³⁰ 24; = 0-20
18	7	000	000	00	C0.0	12.7	.	.	△-0-8,21 ³⁰ 24
19	8	000	000	00	00.0	12.5	.	.	△-0-8,23-24; = 6-9
20	8	000	010	00	00.3	12.1	.	.	△-0-8,22 ³⁰ 24
21	8	03	050	08	C5.3	03.1	.	.	△-0-8,20 ³⁰ 18 14 ²⁰ 15 ³⁰ , • 14 ⁴⁰ 16 ³⁰ ; △14 ⁴⁵ 15 ¹⁰
22	8	000	010	02	C1.0	12.4	CC.5	.	△-3-8 ³⁰ , = 5-9, • 20 ³⁰ 22 ³⁰ , 18 22 ³⁰ 23 ³⁰ , • 22 ³⁰ 22 ³⁵
23	8	020	050	04	03.7	07.2	00.1	.	18 10 ³⁵ 15 ²⁵ 15 ³⁰ , • 16 ²⁰ 18 ³⁰
24	6	09	09	00	06.0	C2.0	C2.5	.	△-3-9 ³⁰ , = 7 ³⁰ 24, • 10 ³⁵ 13 ³⁵ 18, 12 ³⁰ 13 ³⁰
25	7	10	08R	10	09.3	03.2	01.0	.	= 0-9 ³⁰ 14 ⁴⁵ 18, 18 13 ⁴⁵ 3, 14 ⁴⁵ 14 ³⁰ 10 ³⁰ , • 14 ⁴⁰ 14 ⁴⁵ , 23-23 ³⁰ ; • 15 ¹⁵ 17 ³⁰
26	7	09	09•R	02	C6.7	C3.7	1C.5	.	△-5-9, = 8 ³⁰ 12, 18 13 ⁴⁵ 14 ²⁰ , • 13 ⁴⁰ 17 ²⁰
27	8	09	07	10•	08.7	04.5	CC.8	.	= 8-11, 18 14 ²⁰ 15 ³⁰ , • 14 ⁴⁵ 15 ¹⁵ 20 ³⁵ 21 ⁰⁵
28	8	10≡	100•R	10•	10.0	02.2	C3.3	.	= 5 ³⁰ 8, = 8-12, 12 ³⁰ 24, 18 12 ⁴⁵ 18, • 12 ³⁰ 22 ³⁵
29	8	050	06	03	04.7	09.1	15.2	.	= 0-11, 5-9, 22 ³⁰ 26
30	8	000	10	01	03.7	06.0	.	.	△-0-8,21-24, 18 12 ⁴⁰ 18 12 ⁴⁰ 13 ³⁰ , • 12 ⁴⁰ 13 ³⁰
31	7	00	C30	00	01.0	CC.0	13.1	.	△-0-11, 19 ³⁰ 24, = 7 ³⁰ 13 ³⁰

$\psi = 43^{\circ}52'$ N $\lambda = 18^{\circ}26'$ E Gr. $\Delta G = +1\text{h }14\text{ min.}$

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D E F G	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21		
1	707.8	707.1	707.2	13.1	25.4	17.4	18.3	25.4	12.1	-	10.2	11.7	11.5	91	48	77	72	ESE 2	-	0	SE 1	
2	707.9	708.1	708.2	14.8	25.4	17.8	19.0	26.2	13.6	-	12.0	12.6	12.0	95	52	78	75	SE 2	2	W 1	-	0
3	708.8	707.4	707.8	15.3	28.2	19.6	20.7	28.5	13.5	-	10.4	12.5	13.9	80	43	81	68	ESE 3	WSW 2	-	0	
4	706.6	705.2	708.5	16.6	28.6	15.4	19.0	29.6	14.6	-	11.3	11.4	12.2	80	39	93	71	-	0	SW 2	-	0
5	710.8	709.6	709.0	13.3	22.2	14.3	16.0	22.5	12.3	-	09.9	10.2	10.1	88	51	82	73	-	0	NW 1	E	2
6	707.6	705.0	701.0	09.6	26.0	17.2	17.5	26.5	06.7	-	08.1	12.3	05.8	91	45	66	65	-	0	-	C SSE 2	
7	698.8	700.6	703.2	15.0	14.7	13.2	14.0	18.1	12.8	-	08.7	11.4	10.9	68	91	96	85	SE 2	2	W 1	WSW 1	
8	707.0	709.3	711.1	13.0	17.1	14.2	14.6	18.5	12.4	-	10.8	11.3	11.2	96	77	92	88	-	0	-	0 E	1
9	712.7	711.4	711.2	11.9	24.4	16.8	17.5	25.0	11.5	-	10.1	13.5	12.5	97	59	87	81	-	0	W 2	SE 3	
10	712.0	711.0	713.1	13.2	26.7	15.8	19.5	27.0	12.2	=	10.9	12.8	13.2	96	41	78	71	-	0	W 3	=	0
11	715.5	714.5	715.1	13.2	18.3	16.0	15.9	19.8	13.2	-	09.2	10.5	10.1	80	66	74	73	-	0	-	0 SE 2	
12	713.7	712.1	703.0	13.3	23.4	16.1	17.2	23.8	12.8	-	10.4	12.1	11.9	91	56	87	78	-	0	WSW 2	-	0
13	712.4	710.8	711.7	15.2	25.5	16.7	18.5	26.0	15.0	-	11.4	12.1	11.9	88	49	83	73	ESE 1	WSW 1	-	0	
14	712.3	711.2	711.4	15.6	23.6	16.1	17.8	23.6	14.2	-	11.5	12.3	11.1	86	56	81	74	-	0	W 3	ENE 1	
15	711.0	709.4	710.5	11.6	23.2	16.6	17.0	23.6	10.7	-	09.6	12.5	11.3	93	58	80	77	ESE 2	NW 2	E	3	
16	711.0	710.0	711.4	12.8	23.4	14.5	16.3	23.8	11.5	-	10.3	10.6	09.9	93	49	80	74	SE 1	NW 1	ESE 2		
17	711.8	710.2	710.8	10.4	23.0	15.6	16.2	23.3	09.2	-	08.6	12.0	11.7	91	57	88	79	SE 2	WSW 1	-	0	
18	711.1	709.7	710.3	11.4	25.0	17.1	17.6	25.1	10.2	-	09.0	10.1	11.9	89	42	82	71	SE 2	WW 2	-	0	
19	710.8	709.4	709.2	12.5	23.2	15.8	16.8	23.7	11.5	-	10.4	11.3	11.4	96	53	85	78	E 1	WSW 1	ESE 2		
20	706.7	704.0	704.5	12.4	23.0	16.4	17.0	24.7	11.2	-	09.9	12.0	11.5	91	57	82	77	ESE 1	WSW 1	-	0	
21	703.9	703.6	704.2	13.8	20.0	15.3	16.1	21.0	12.5	-	11.3	12.0	10.8	96	65	83	SSE 2	N 1	-	0		
22	703.8	705.8	706.9	14.0	17.0	15.2	15.4	20.3	13.5	-	11.0	13.0	10.6	92	90	82	88	S 2	-	0		
23	706.0	705.9	706.0	12.6	20.6	14.6	15.6	20.8	12.4	-	10.2	10.9	09.2	94	60	74	76	SE 1	W 2	E 2		
24	703.7	702.4	700.2	14.9	18.3	14.4	15.5	20.5	11.7	-	09.2	09.4	09.8	72	55	79	70	N 2	SSW 5	-	0	
25	695.6	696.2	705.7	16.0	15.1	09.4	12.5	17.3	09.4	-	08.1	08.1	07.5	59	63	65	69	S 5	NW 2	-	0	
26	691.1	692.6	699.7	06.7	07.7	06.2	07.2	11.0	06.1	-	07.7	07.6	06.7	92	96	95	94	ESE 3	W 3	-	0	
27	705.9	707.3	708.7	06.0	14.7	06.4	08.4	15.0	05.0	-	06.8	05.3	06.2	97	42	85	75	-	0	W 2	E 2	
28	700.1	705.6	706.1	02.9	19.9	04.2	10.3	20.3	02.3	-	05.4	06.6	07.2	95	39	82	72	-	0	WSW 1	-	0
29	704.5	701.5	706.0	07.5	18.9	16.8	17.0	21.2	05.5	-	06.2	08.5	07.9	80	52	55	62	E 1	S 2	S 4		
30	705.4	703.7	716.3	17.2	18.0	09.6	13.6	20.3	09.1	-	07.8	10.7	08.8	53	69	98	73	S 3	ENE 1	NW 1		
MES.	VRED.	707.4	706.8	707.6	12.6	21.4	14.8	15.6	22.4	11.0	-	09.5	10.6	10.5	87	58	82	76	1.3	1.4	0.9	

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 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijnost O. -	Oblačnost N (0-10)					Insolacij broj sati	Podzemne R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	8	08	020	04	04.7	06.4	00.1	.	.	$\Delta 0-8^{30} 18^{45} 24, \bullet 5^{35} 6$	
2	7	09	070	01	05.7	08.7	05.5	.	.	$\Delta 0-5^{30} 20-24, 13^{45} 6^{30}, 8^{55} 5^{15}, \bullet 5^{35} 6^{30}$	
3	8	040	020	00	02.0	10.6	.	.	.	$\Delta 0-8^{30} 20^{25} 24$	
4	8	05	020	10	05.7	09.9	.	.	.	$\Delta 0-8^{13} 18^{45} 20^{45}, \bullet 18^{45} 19^{20}, \bullet 19^{20} 20^{25}, \bullet 20^{20} 21^{45}$	
5	9	030	010	00	01.3	11.8	14.6	.	.	$\Delta 20-24$	
6	8	000	000	07	02.3	11.0	.	.	.	$\Delta 0-9^{19} 24$	
7	6	08	100	10	09.3	00.2	.	.	.	$\Delta 0-8^{30} 9^{45} 24, 12^{30} 23^{45} 24, 18^{45} 10^{30}, \bullet 19^{30} 23^{45}$	
8	6	10	10	07	09.0	00.3	07.4	.	.	$\Delta 0-24, \bullet 0-4^{30}, 3^{25} 6^{30}, \Delta 20-24$	
9	7	000	010	00	00.3	00.3	.	.	.	$\Delta 0-3^{45} 6^{30} 11^{30}, \bullet 0-10^{30} 18^{30} 24, \equiv 3^{35} 6$	
10	8	000	010	10	03.7	05.8	.	.	.	$\Delta 0-1^{45} \bullet 7^{45} 11^{30}, \bullet 19^{45} 19^{20}, \bullet 21^{45} 23^{45}, \bullet 22^{45} 23^{45}$	
11	7	10	10	10	10.0	01.6	01.2	.	.	$\Delta 0-6^{30} \Delta 22^{30} 24$	
12	7	09	010	00	03.3	07.0	.	.	.	$\Delta 0-9^{30} 20-24, \bullet 6-11^{30} 21^{45} 23, \equiv 23-24$	
13	8	10	010	00	03.7	07.5	.	.	.	$\Delta 0-9^{30} 20^{30} 24, \equiv 0-6, \bullet 6-11, 21^{30} 24$	
14	6	09	040	05	06.0	05.4	.	.	.	$\Delta 0-8^{45} 19^{30} 24, \bullet 0-24$	
15	7	000	060	09	05.0	08.1	.	.	.	$\Delta 0-9, \bullet 19-24, \bullet 0-11^{35}$	
16	7	10	050	00	05.0	05.1	.	.	.	$\Delta 0-1^{45} 19^{30} 24, \bullet 5-13^{30}$	
17	7	000	030	00	01.0	09.1	.	.	.	$\Delta 0-9^{30} 20-24, \bullet 13^{45} 14^{30} 21^{30} 24$	
18	6	03	040	10	05.7	05.1	.	.	.	$\Delta 0-9^{30} 20-24, \bullet 5-11, 18^{45} 20^{30}, \bullet 19^{30} 19^{35}$	
19	7	10	0F	00	06.0	06.5	00.1	.	.	$\Delta 0-8^{45} 19^{30} 24, \bullet 5-11, 18-24, \bullet 13^{30} 13^{35} 15^{35} 16$	
20	8	000	09	10	06.3	06.3	00.0	.	.	$\Delta 0-6^{30} \bullet 0-12, \bullet 7^{30} 8^{30}, \bullet 15^{35} 16^{20}, 20^{35} 24, \bullet 16^{25} 16^{40}, 20^{40} 26^{45}$	
21	8	10	09	06	08.3	02.8	13.0	.	.	$\bullet 0-10, \bullet 0-4^{30}, 4^{30} 10^{30} \Delta 22^{35} 23$	
22	8	05	040	04	06.0	02.8	16.4	.	.	$\bullet 0-15, 3^{30} 11^{30} 13^{30}, \bullet 0-13, 12^{30} 24, \bullet 3-3^{30} 6^{45} 17^{30}, 9^{30} 10^{30}, \bullet 5^{30} 9$	
23	6	10	07	00	05.7	03.3	02.1	.	.	$\Delta 0-3, 19^{30} 24, \bullet 3-3^{30} 6^{45} 17^{30}, 9^{30} 10^{30}, \bullet 5^{30} 9$	
24	8	08	08	08	08.3	04.5	00.3	.	.	$\Delta 0-8, \bullet 16^{30} 24, 13^{30} 20-20^{30}$	
25	7	08	09	02	04.3	02.1	04.6	.	.	$\bullet 2^{30} 2^{30}, \bullet 7^{30} 8^{30}, \bullet 11-13, 15^{20} 15^{40}$	
26	5	10	10	10	10.0	00.0	03.8	.	.	$\bullet 4^{30} 7^{30} 10^{35} 24, \bullet 10^{30} 4^{30}$	
27	8	10	040	00	04.7	06.5	14.7	.	.	$\bullet 5-6^{35}, \bullet 18^{30} 24$	
28	7	000	000	00	00.0	10.6	.	.	.	$\Delta 0-10, \bullet 20-24, \bullet 7^{30} 12^{30}$	
29	8	010	09	09	06.3	06.8	.	.	.	$\Delta 0-8^{40}, \bullet 18^{30} 24, \bullet 13^{30} 13^{40}$	
30	7	080	09	10	09.0	02.3	.	.	.	$\bullet 18^{30} 19^{45}, \bullet 15-24$	
MES. VRED.			05.4	05.4	04.7	05.4	185.6	84.5			

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1	8	10	030	10	07.7	03.7	19.4	.	.	$\Delta 0-11^{30} \bullet 3^{25} 4, 10^{40} M, \bullet 6-7^{15} 9^{40} 10^{40}, \Delta 20^{35} 24$	
2	7	10	10	06	09.7	00.0	03.6	.	.	$\Delta 0-6^{15}, \bullet 6^{15} 7^{30}, 13^{45} 22^{20}, \bullet 15^{45} 16^{30}, \bullet 18^{45} 21^{40}$	
3	8	09	010	04	04.7	09.5	06.3	.	.	$\Delta 18^{30} 24$	
4	9	080	030	09	04.7	04.1	.	.	.	$\Delta 0-7^{30} 20^{30} 24$	
5	7	10	08	03	07.0	01.3	00.7	.	.	$\Delta 0-6^{40}, 20-24, \bullet 6^{40}, 7^{20}, 22^{20} 24, \bullet 5^{20} 24$	
6	7	10	10	10	10.0	00.0	11.8	.	.	$\bullet 0-0^{30} 3^{25} 11^{35}, \bullet 0-12^{30}$	
7	5	10	10	10	10.0	00.0	11.8	.	.	$\bullet 14^{30} 21^{30}, \bullet 5^{24}$	
8	7	08	09	00	05.7	01.4	02.2	.	.	$\Delta 0-3, 7-12^{30}, \bullet 11^{15} 12^{55}, 15^{15} 18^{30}, \bullet 16-16^{35}, \bullet 16^{20} 16^{35}$	
9	8	10	040	10	08.0	05.5	07.6	.	.	$\bullet 4^{30} 10^{45} 16^{35} 20^{35}, \bullet 17^{30} 21^{45}, \bullet 17^{30}, \bullet 18^{30} 19^{30}$	
10	8	06	040	00	04.0	09.1	02.3	.	.	$\bullet 3^{30} 4^{30}, \bullet 6^{30}, \bullet 6^{30} 7^{30}, \bullet 18^{30} 24$	
11	8	08	010	09	06.0	06.1	.	.	.	$\Delta 0-5^{30} 20^{35} 24, \bullet 4^{30} 6^{45}, 8^{30} 10^{30}, \bullet 5^{30} 7^{30}, \equiv 6^{30} 8^{30}$	
12	8	05	10	07	07.3	00.8	.	.	.	$\Delta 0-3^{45}, \bullet 3^{45} 7^{30}$	
13	6	10	10	10	10.0	00.0	07.3	.	.	$\bullet 2^{35} 22^{30}, \bullet 7^{30} 24$	
14	4	10	10	10	10.0	00.0	27.2	.	.	$\bullet 0-24, \bullet 0-11^{30}, 15-20^{20}, \bullet 11^{30} 15$	
15	4	10	10	10	10.0	00.0	06.7	.	.	$\bullet 0-15, 20^{20} 24, \bullet 2^{30} 7^{20}, 12^{50} 13^{20}, 20^{30} 21^{30}, \bullet 13^{20} 20^{30}, 22^{15} 24, \equiv 15-20^{35}$	
16	6	07	10	06	07.7	01.9	23.7	.	.	$\bullet 0-2^{35} 9^{40} 10^{35} 12^{45}, \bullet 14^{45} 16^{45} 22, \bullet 0-23, \bullet 8^{45} 10^{45}, \bullet 8^{45} 16^{40}$	
17	8	10	040	00	04.7	07.6	05.4	.	.	$\Delta 5^{30} 7^{30}, \bullet 23^{45} 24, \bullet 6^{40} 8, \bullet 8-11, 18-24$	
18	6	000	060	00	02.0	08.4	.	.	.	$\Delta 0-8, \bullet 6-7^{30}, 10^{30}, \bullet 24, \bullet 7^{30} 10^{30}, \bullet 18^{30} 24$	
19	6	10	040	00	04.7	06.0	.	.	.	$\Delta 0-5, 11-10^{30}, \bullet 0-2, 20^{30} 24, \bullet 3-10, \bullet 5-10, \bullet 10^{20}, \bullet 11^{30} 15^{45}, \bullet 15-24$	
20	7	10	10	06	08.7	00.5	.	.	.	$\bullet 11^{30} 15^{45}, \bullet 15-24$	
21	8	10	10	10	10.0	00.5	00.2	.	.	$\bullet 10^{15}, \bullet 6-7^{30} 10^{35}, \bullet 6^{40} 11, 17^{40}, 23^{45}, \bullet 23^{45} 24$	
22	7	040	040	10	08.0	00.6	15.5	01	.	$\bullet 0-3, \bullet 0-8^{30}, 14^{30} 24, \bullet 8^{30} 24, \bullet 13^{30}, \bullet 16^{30}, \bullet 18^{30}$	
23	4	10	10	10	10.0	00.0	27.1	.	.	$\bullet 0-24, \bullet 0-2^{45} 9-24, \bullet 24^{30} 9$	
24	8	010	030	09	04.3	08.4	36.4	.	.	$\bullet 0-1^{40}, \bullet 0-2, 6^{40} 11^{45}, \bullet 24^{30} 24$	
25	8	09	040	00	04.3	07.6	.	.	.	$\bullet 0-9, 18^{30} 24, \bullet 5^{24} 11$	
26	7	070	10	10	09.0	04.8	.	.	.	$\Delta 0-7^{30}, \bullet 7^{30} 12, \bullet 13^{45} 18^{20}, \bullet 18^{20} 24$	
27	8	010	050	00	02.0	06.4	11.5	.	.	$\bullet 0-2^{30}, \bullet 6-9, \bullet 2^{30} 8^{30}$	
28	6	08	030	10	07.0	04.7	.	.	.	$\Delta 0-0, \bullet 2^{30} 6-9, \bullet 15^{45} 24$	
29	6	10	10	10	10*	10.0	00.0	18.0	01	$\bullet 0-2^{30} \bullet 0-0^{30}, \bullet 2^{30} 3^{30} 8^{30} 9^{30} 12^{30} 17, \bullet 3^{30} 5, 8^{30} 9^{30}, 17-24, \bullet 3^{30} 24, \bullet 5^{30} 8^{30}, \bullet 11-19^{30}$	
30	3	10*	10*	10	10.0	00.0	11.8	04	.	$\bullet 0-20, \bullet 0-9, 15^{30} 23^{40}, \bullet 9-15^{30} \bullet 11-19^{30}$	
31	3	09	10*	10	09.7	00.0	06.0	04	.	$\bullet 5^{30} 11, 19^{30} 24, \bullet 10^{45} 18, \equiv 11-19^{30}$	
MES. VRED.			08.1	07.2	06.8	07.4	99.9	259.0			

$\varphi = 43^{\circ}52'$ N $\lambda = 18^{\circ}26'$ E Gr. $\Delta G = +1h\ 14\ min.$

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D e n g	Vazdušni pritisak P mm			Temperatura výzduchu T °C								Napón vodene pare e mm			Relativna vláznost u %			Pravac i jačina vjetra D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	709.7	702.0	705.0	00.0	00.6	00.0	00.2	00.8	-00.3	-	04.5	04.3	04.4	98	90	97	95	-	0	NNW	2	-	0
2	706.1	705.9	707.0	-01.6	05.1	00.9	01.3	06.0	-01.8	-	03.9	04.1	04.2	95	62	85	81	-	0	NNW	2	-	0
3	708.5	708.4	709.2	00.2	07.8	02.6	03.3	09.5	-00.2	-	04.3	04.0	04.5	91	50	82	74	-	0	NNW	2	ESE	2
4	708.1	707.2	707.3	02.3	08.6	06.0	05.7	09.3	01.5	-	04.6	05.2	05.3	86	62	76	75	ESE	3	S	2	E	3
5	707.2	708.5	710.6	05.2	11.6	06.4	07.4	12.4	05.0	-	04.8	06.1	05.8	73	59	80	71	ESE	3	E	1	ESE	2
6	712.2	713.8	712.6	02.6	15.0	06.7	07.8	15.5	02.5	-	05.3	06.0	05.7	95	47	78	73	-	0	SW	1	F	2
7	712.0	709.8	709.4	05.2	05.0	03.8	04.4	06.7	03.6	-	06.0	06.4	05.7	90	97	94	94	-	0	-	0	-	0
8	708.7	708.7	709.4	02.3	02.2	01.3	01.8	03.8	01.2	-	05.2	05.1	04.8	97	95	95	96	-	0	NNW	1	NW	2
9	709.7	710.0	710.7	01.7	03.4	03.4	03.0	03.8	01.7	-	04.8	05.2	05.4	94	88	92	91	-	0	-	0	-	0
10	710.0	709.0	709.8	02.7	09.7	02.1	04.2	09.7	02.0	-	05.3	05.4	04.7	95	60	89	81	-	0	ESE	2	ESE	4
11	712.0	711.0	711.0	-01.1	05.0	01.4	01.7	05.3	-01.1	-	04.2	05.5	04.5	98	83	97	93	-	0	NNW	1	-	0
12	711.1	709.9	709.8	-00.1	07.0	03.2	03.4	08.2	-01.0	-	04.2	05.6	05.0	96	71	86	84	E	1	-	0	L	1
13	710.1	710.4	711.1	02.6	08.4	06.4	06.0	08.5	01.5	-	04.8	06.1	05.7	88	74	80	75	ESE	2	-	0	ESE	2
14	711.1	711.5	712.2	00.4	13.6	04.6	05.8	13.6	00.1	-	04.5	05.4	05.2	95	46	82	74	SE	2	w	2	ESE	1
15	711.0	711.6	712.3	01.8	15.4	05.0	07.2	15.3	01.7	-	04.8	06.3	05.7	92	48	83	74	ESE	2	WSW	1	ESE	1
16	711.4	710.3	712.0	03.1	16.6	05.8	07.8	16.7	02.9	-	04.9	06.1	05.6	85	43	84	71	ESE	4	WSW	1	ESE	2
17	711.4	712.2	713.0	02.2	14.9	06.4	07.7	14.9	02.6	-	04.8	06.0	05.2	84	48	71	68	ESE	2	-	0	ESE	3
18	712.5	711.1	710.8	07.7	17.0	06.4	08.1	17.4	02.1	-	04.5	06.5	05.7	80	44	79	68	ESE	3	-	0	ESE	2
19	708.4	704.9	707.6	05.9	15.7	08.3	09.6	16.6	03.6	-	05.4	05.4	07.1	77	40	86	68	ESE	2	S	4	NNW	1
20	711.4	710.2	711.2	03.4	12.7	03.4	05.7	12.7	02.5	-	05.3	05.1	04.6	91	47	78	72	-	0	-	0	-	0
21	710.2	709.0	709.5	01.0	06.7	04.6	04.4	07.0	00.6	-	03.9	05.2	05.8	79	71	85	80	ESE	2	-	0	-	0
22	710.4	709.1	709.7	07.3	11.0	02.6	05.0	11.3	02.7	-	05.5	05.6	05.0	95	57	86	80	-	0	-	0	ESE	1
23	710.0	705.5	708.8	01.8	08.9	05.6	05.5	08.9	00.8	-	04.6	05.7	05.8	89	67	85	80	-	0	C	-	0	0
24	708.7	708.6	708.0	01.6	08.3	06.8	05.9	04.0	01.3	-	04.8	05.7	05.6	94	70	76	80	ESE	2	-	0	ESE	1
25	705.1	705.6	702.6	03.3	11.6	11.8	09.6	12.0	02.4	-	04.9	06.6	06.3	85	65	80	70	SE	2	S	4	S	2
26	703.0	703.9	704.1	06.9	02.8	02.2	03.3	11.8	02.0	-	06.4	05.3	04.8	93	54	85	92	-	0	-	0	N	1
27	701.3	701.2	702.7	00.5	02.7	-00.2	00.6	03.1	-00.8	-	04.4	05.1	04.4	93	95	95	95	-	0	-	0	C	-
28	697.1	697.6	698.6	-01.5	13.6	03.3	02.2	19.4	-02.4	-	03.6	05.5	04.6	88	58	98	81	SE	2	S	5	W	1
29	707.1	707.0	707.1	-01.2	-01.1	-03.0	-02.6	01.0	-03.5	-	03.4	04.0	03.5	95	54	95	95	-	0	-	0	-	0
30	703.6	106.1	702.1	-03.6	-02.2	-04.0	-03.4	-02.0	-04.0	-	03.3	03.7	03.3	93	56	96	95	NNW	1	-	0	ESE	1
MES.	708.2	707.5	708.4	01.7	08.5	02.7	04.4	09.3	01.0	-	04.7	05.4	05.2	90	67	88	81	I.	1	I.	1	I.	1

1	707.5	708.9	712.0	-05.6	02.2	00.5	-00.6	03.2	-06.5	-	02.9	04.3	04.6	95	80	97	91	-	0	-	0	-	0	
2	712.7	715.0	715.4	-02.0	0.0	00.8	00.1	01.0	-02.4	-	03.8	04.6	04.7	96	55	97	96	SSE	1	-	C	-	0	
3	716.4	716.4	717.0	00.9	02.2	02.2	01.9	02.3	00.7	-	04.7	05.3	05.3	97	98	98	96	-	0	-	0	-	0	
4	715.4	713.3	711.5	02.5	05.0	01.4	02.8	05.3	01.6	-	05.4	06.2	05.1	98	54	97	96	-	0	-	C	-	ESE	2
5	707.0	706.2	705.4	-00.6	01.4	00.6	00.5	02.0	-00.6	-	04.3	04.9	04.7	96	57	98	98	ESE	1	S	1	-	0	
6	707.0	707.1	707.3	00.6	04.2	01.0	01.7	04.4	00.0	-	04.7	04.4	04.0	98	72	82	64	CNE	2	w	2	ENE	2	
7	707.3	708.4	708.9	00.3	04.2	02.3	02.3	04.6	-00.9	-	04.3	05.1	04.7	91	82	87	87	-	0	-	0	-	0	
8	708.0	707.1	706.1	01.9	05.9	04.0	04.4	06.0	01.4	-	04.3	05.8	06.1	81	64	94	86	ESE	2	-	0	NNW	1	
9	707.1	708.9	710.3	04.5	04.0	04.6	04.3	05.2	04.3	-	06.1	06.1	06.1	96	94	94	95	NNW	1	-	C	-	0	
10	710.4	710.2	710.3	03.7	05.4	03.6	04.1	06.8	02.9	-	05.9	06.2	05.6	99	92	94	95	0	-	0	-	0	0	
11	703.7	707.4	703.5	00.2	04.6	08.0	05.2	08.1	-00.2	-	04.5	05.6	05.8	97	65	72	66	ESF	1	-	0	NW	2	
12	700.1	702.4	701.2	00.0	00.2	-00.9	01.8	02.1	-00.9	-	05.4	04.4	04.1	63	55	96	85	NNW	2	-	C	-	NNW	1
13	697.1	697.6	700.0	-02.1	0.0	00.4	-00.9	01.2	-02.1	-	03.7	04.4	04.1	94	53	96	94	NN	1	-	0	-	0	0
14	702.4	706.3	707.3	-02.3	-01.6	-02.8	-02.2	-00.6	-02.8	-	03.7	03.6	03.4	96	92	92	93	NN	2	w	2	NN	2	
15	703.0	706.5	706.0	-03.7	-02.6	-02.4	-02.4	-02.8	-03.7	-	03.2	03.3	03.2	91	86	85	87	w	2	w	2	-	0	
16	707.4	706.3	709.1	-01.4																				

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$$H_s = 630 \text{ m} \quad H_b = 637.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.0 \text{ m}$$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacij broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	3	10*	10*	10	10.0	00.0	04.2	06	= 0° 3° - 5° 30° 20° 24°	= 0° 3° 3,5° 20° 24° * 0° 25° 19° 25°
2	5	10**	01.0	09	06.7	05.9	05.4	10	= 0° 6° 8° 24°	= 6° 8° 24°
3	8	09	05.0	08	07.3	06.3	.	03	= 6° 12°	[X]
4	7	10*	10	06	08.7	02.1	00.0	.	= 4° 7°	= 4° 11° 23° 23° 23°
5	8	07	06	08	07.0	02.5	00.0	.		
6	8	09	07	08	08.0	04.5	.	.	= 7° 13° 22° 24	
7	3	10***	10***	10*	10.0	00.0	.	.	= 0° 6° 20° 24°	= 0° 20° 24°
8	5	10*	10	10*	10.0	00.0	09.4	.	= 0° 12°	= 0° 24°, 11° 13° 25° 22° 24°, 14° 16° 25° 20° 20° * 20° 20°
9	6	10*	10	10	10.0	00.0	01.6	.	= 0° 10°	= 0° 24°, 22° 24
10	7	10	01.0	00	02.7	02.9	00.0	.	= 0° 11°	= 0° 4° 18° 23° 25°, 23° 24
11	3	10**	00.0	10**	06.7	01.3	.	.	= 10° 8° 20°	= 10° 22° 24°
12	4	00**	00.0	07	02.3	03.2	.	.	= 0° 14° 17° 24°	= 0° 14° 17° 24°
13	3	09	10**	03	07.3	00.0	.	.	= 0° 8° 18° 24°	= 0° 9° 23° 24°, 8° 18° 20°, 12° 20° 14° 30°
14	6	00	03.0	00	01.0	07.2	.	.	= 0° 14° 30°	= 0° 3° 23° 24°, 13° 30° 8° 20°
15	5	00	00.0	00	00.0	06.8	.	.	= 0° 10° 15°	= 0° 15° 20°, 20° 24
16	5	00	00.0	00	00.0	07.1	.	.	= 0° 10° 0° 4° 20° 24	= 0° 20° 20°
17	5	03	05.0	00	02.7	05.0	.	.	= 0° 8° 15° 24°	= 0° 8° 15° 24°
18	6	07	03.0	00	03.3	04.0	.	.	= 0° 8° 21° 24°	= 5° 1° 40°
19	8	08	08	09	08.3	03.1	.	.	= 0° 8° 17° 18° 24°	= 11° 10° 11° 12°, 10° 10° 10°, 11° 10° 10°, 10° 10° 10°, 10° 10° 10°
20	9	10	00.0	01	03.7	05.7	03.0	.	= 5° 15° 20°	= 5° 8°, 20° 20° 24
21	4	05	10	10	05.7	00.8	.	.	= 0° 4° 15° 20° 24°	= 8° 11° 15° 20° 24°
22	6	08	03.0	00	03.7	04.4	00.0	.	= 0° 8° 11° 15° 20° 24°	= 0° 8° 11° 15° 20° 24°
23	5	08	09	10	09.0	00.7	.	.	= 4° 5° 24°	= 0° 3° 23° 24°
24	4	09	07	08	08.0	01.7	.	.	= 0° 24°	= 0° 11° 12° 20° 24°
25	8	09	10	10	05.7	00.0	.	.	= 0° 8° 12° 12° 24°	= 14° 10° 18° 20° 24°
26	5	10*	10*	10	10.0	00.0	15.2	.	= 0° 17° 15° 15° 21° 8° 11° 15°	= 8° 11° 15° 20° 24°
27	3	10*	10**	06	08.7	00.0	03.4	.	= 0° 8° 15° 20° 24°	= 24° 17° 11° 15° 20° 24°
28	8	08	10	10**	04.3	00.5	08.9	03	= 17° 2° 18° 18° 24°	= 11° 15° 18° 20° 24°
29	2	01	10**	10**	07.0	01.7	22.1	20	* 0° 3°	= 12° 5° 18° 20° 24°
30	3	10**	10**	02.0	07.3	00.0	.	14	= 0° 2° 16° 20° 24° 23° 24°	[X]

MES.
WREC.

SARAJEVO

1375-1376

1	5	07	08	10	06.3	00.5	.	07	$\equiv -0.11^{20} V_0 M_1 \equiv 11^{20} 24_1 \equiv 20-21^{\circ} [x]$
2	1	10	10	10	06.0	00.0	.	07	$\equiv 0-6^{20} V_0 9 \equiv 6-24_1 \equiv 11^{20} 24_1 \equiv 12^{20} 12_1 [x]$
3	0	10	10	10	10.0	00.0	03.0	05	$\equiv 0-24_1 \bullet 0-24_1 24_1 \equiv 23^{20} 24_1 [x]$
4	2	10	10	10	06.7	00.0	04.4	.	$\bullet 0-8^{20} 9 \equiv 16_1 \bullet 8^{20} 13_1 \equiv 11^{20} M_1 / 10-24_1 \equiv 13^{20} 14_1 [x]$
5	3	04	10	10	06.0	00.0	00.4	.	$\equiv 0-3^{20} 7_1 24_1 \equiv 23^{20} 6_1 \equiv 6-7^{20}$
6	6	10	07	08	08.3	01.8	01.8	.	$\equiv 0-0^{20} \bullet 11^{20} 24_1 \bullet 0-1^{20} 14_1 \times 10^{20} 5^{20} 8^{20} 8^{20} \equiv 11^{20} 24_1$
7	4	10*	10	09	09.7	00.2	00.0	.	$\equiv 2^{20} 24_1 \times 2^{20} 8_1 [x]$
8	5	10	10	10	10.0	00.0	00.0	.	$\equiv 0-28^{20} M_1 24_1 \bullet 11^{20} 24_1$
9	5	10	10	10	10.0	00.0	03.6	.	$\equiv 0-24_1 \bullet 0-1^{20} \bullet 11^{20} 17_1 \equiv 12^{20} 14_1 [x]$
10	3	10	10	10	10.0	01.7	01.0	.	$\equiv 0-2^{20} 19^{20} 24_1 \equiv 2^{20} 9_1 / 13^{20} 14_1 [x]$
11	5	09	09	09	09.0	00.2	.	.	$\equiv 0-8^{20} M_1 24_1 \equiv 2-4^{20} \equiv 8^{20} 11^{20} \bullet 47^{20} 24$
12	4	08	10*	10*	05.3	00.0	00.1	.	$\bullet 0-5^{20} 6^{20} \bullet 10^{20} \bullet 5^{20} 24_1 \equiv 10^{20} 24_1 \equiv 10^{20} 20^{20} \equiv 20^{20} 24_1 [x]$
13	6	03	10	10	07.7	00.2	16.7	12	$\times 0-3^{20} 17^{20} 24_1 \equiv 0-3^{20} \equiv 3^{20} 24_1 [x]$
14	6	10*	10	10	10.0	00.0	05.9	13	$\times 0-24_1 \equiv 0-24_1 [x]$
15	5	10*	10	10	10.0	00.0	01.6	19	$\times 0-24_1 \equiv 0-24_1 [x]$
16	5	10	10	10	10.0	00.0	01.8	10	$\bullet 0-3, 9^{20} 12_1 \equiv 0-24_1 [x]$
17	3	00	06	00	02.0	05.4	00.0	07	$\equiv 0-2^{20} 18^{20} 11_1 13-24^{15}_1 \equiv 11-18_1 [x]$
18	5	09	10*	10	05.7	00.0	.	04	$\times 0-5^{20} 5^{20} \bullet 12^{20} 12^{20} \bullet 12^{20} 16_1 \equiv 12^{20} 14_1 [x]$
19	6	10	09	10*	05.7	01.8	05.6	07	$\times 7^{20} 24_1 \times 9^{20} 10^{20} \times 19^{20} 24_1 [x]$
20	5	07	10	00	05.7	00.2	00.0	07	$\times 0-2^{20} \equiv 0-15^{20} 20^{20} 22^{20} \equiv 15^{20} 18^{20} \equiv 18^{20} 24_1 [x]$
21	3	02	08	10	06.7	00.0	.	04	$\equiv 0-13^{20} V_0 -12^{20} \equiv 5-7^{20} \equiv 18^{20} 24_1 [x]$
22	3	10	10	10	10.0	00.0	.	04	$V_0-24_1 \equiv 0-13^{20} 18^{20} 24_1 \equiv 13^{20} 18^{20} [x]$
23	3	10	06	00	03.3	00.0	.	04	$V_0-24_1 \equiv 0-9-23-24_1 \equiv 9-23_1 [x]$
24	3	10	06	00	03.3	00.0	.	04	$\equiv 0-9^{20} V_0 M_1 16^{20} 24_1 \equiv 9^{20} 24_1 [x]$
25	3	04	10	10	08.0	00.0	.	04	$\equiv 0-24_1 V_0 24_1 [x]$
26	3	10	06	08	06.0	00.1	.	04	$\equiv 0-6^{20} 9_1 18_1 V (1-10^{20}) \equiv 6^{20} 9_1 \equiv 18-24_1 [x]$
27	3	10	04	08	07.3	03.3	.	04	$\equiv 0-1^{20} \equiv 10^{20} 4^{20} \equiv 4^{20} 17^{20} [x]$
28	7	10	10	09	09.7	00.0	.	03	$\equiv 0-9^{20} 24_1 \equiv 9-19^{20} 10^{20} 13^{20} 14^{20} \times 19^{20} 20_1 [x]$
29	4	10	05	01	05.3	00.8	00.1	02	$\equiv 0-5^{20} 19^{20} 44_1 \times 18^{20} 24_1 \equiv 5^{20} 18^{20} [x]$
30	1	01	10*	10	07.0	00.0	.	*	$\equiv 0-14^{20} \bullet 9-10^{20} \bullet 10^{20} \times 10^{20} 23_1 \equiv 15^{20} 17^{20} f_8 18^{20} 22_1 [x]$
31	7	10*	10*	09	05.7	00.0	08.0	04	$\times 6^{20} 19^{20} f_8 19^{20} [x]$

PES.
IVRED.

$\varphi = 44^{\circ}48'$ N $\lambda = 20^{\circ}28'$ E Gr. $\Delta G = +1h\ 22\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenog parne v mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21
1	756.2	756.2	757.0	02.9	03.5	03.2	03.2	04.7	02.6	02.4	05.6	05.7	05.3	98	97	92	96	SW 1	WSW 1	ESE 2
2	757.3	756.3	755.4	02.0	02.8	01.6	02.0	03.2	01.4	00.9	04.2	04.4	04.1	79	78	80	79	ESE 4	ESE 5	ESE 5
3	753.8	753.7	754.8	02.0	06.1	02.6	03.4	06.6	01.4	00.4	04.2	04.6	04.5	79	65	F1	75	ESE 4	FSE 4	ESE 4
4	757.1	757.9	750.7	03.5	08.0	01.6	04.2	08.4	02.3	01.0	04.5	04.9	04.4	77	61	79	72	SE 4	SE 4	ESE 4
5	759.0	758.1	757.1	01.4	05.7	01.8	02.7	05.7	01.4	-00.5	04.1	04.7	04.3	81	66	82	77	ESE 4	ESE 3	ESE 3
6	754.6	752.3	751.5	01.4	05.3	00.8	02.1	06.0	00.8	00.4	04.2	04.8	03.8	82	72	78	78	ESE 2	ESE 2	ESE 4
7	753.2	755.1	756.6	-01.0	00.1	00.3	-00.1	00.8	-01.1	-01.2	04.0	04.3	04.4	94	93	93	93	ESE 3	ESE 2	SE 1
8	755.4	755.4	756.6	-00.2	01.0	-00.2	00.1	01.2	-00.4	-01.9	04.0	03.9	03.7	89	80	82	84	ESE 3	ESE 3	ESE 3
9	757.2	756.6	756.0	-02.0	01.1	-01.4	-00.9	01.7	-02.0	-02.0	03.0	03.0	03.3	76	60	80	72	ESE 4	SE 4	SE 5
10	752.6	756.0	756.5	-01.5	00.8	-02.2	-01.3	01.2	-02.2	-02.6	03.4	03.1	02.9	82	64	75	74	ESE 6	ESE 4	SE 4
11	759.2	750.5	740.9	-02.8	00.2	-02.4	-01.8	00.2	-03.1	-03.0	03.0	03.2	03.0	80	68	79	76	ESF 3	ESE 3	SE 2
12	759.2	740.1	740.8	-01.6	04.4	02.5	02.0	04.7	03.5	-04.2	03.5	04.4	04.4	85	71	79	78	SE 2	WNW 1	USE 2
13	760.2	760.3	761.2	01.0	02.0	-02.2	-00.4	02.5	-02.2	-03.0	04.2	03.7	03.1	85	65	79	78	ENE 1	-0	ESE 3
14	761.7	760.8	760.2	-04.6	01.6	-02.4	-02.0	02.3	-05.0	-06.1	02.6	02.6	02.4	81	50	62	64	ESE 3	SE 2	ESE 3
15	760.5	759.6	759.8	-05.9	01.9	-02.7	-02.4	02.2	-06.3	-09.8	02.5	03.1	02.6	83	60	68	70	-0	ENE 2	ESE 2
16	757.9	758.2	756.8	-05.3	-00.4	-00.2	-01.6	00.2	-06.1	-07.3	02.3	02.0	02.2	72	67	72	71	ESE 4	-0	-0
17	749.5	751.2	752.4	00.8	00.0	03.1	02.0	03.1	-00.9	-02.6	03.9	04.6	05.4	81	95	95	90	ESE 3	WSW 2	WSW 2
18	752.1	751.9	753.0	07.8	04.2	02.7	02.8	04.4	01.6	00.8	04.2	04.1	04.0	75	66	74	72	W 3	NW 4	NW 3
19	754.6	754.4	752.9	-01.4	03.7	03.2	02.2	04.6	-01.5	-04.4	03.8	04.4	05.3	92	74	92	86	WSW 1	W 3	NW 2
20	750.6	751.3	751.4	06.8	08.3	06.6	07.1	09.5	03.2	02.8	06.6	06.4	07.7	89	77	79	82	WNW 3	NW 4	NW 4
21	755.7	756.0	757.6	05.4	05.9	06.1	05.5	06.6	04.6	04.3	05.2	05.4	05.9	78	78	83	80	WNW 2	W 2	W 2
22	758.4	757.6	756.4	04.4	04.2	04.6	05.4	08.9	04.0	03.2	05.5	05.2	05.4	88	64	85	79	WNW 1	W 2	SE 3
23	755.7	757.2	755.2	-00.4	03.5	02.6	02.1	04.5	-00.9	-03.3	04.2	04.8	04.9	94	82	89	88	SW 1	W 2	NW 2
24	756.4	755.5	755.0	02.0	05.3	02.4	03.0	05.4	01.7	00.1	05.0	05.0	05.2	95	76	95	88	SSW 1	SSW 1	SE 1
25	754.6	753.2	754.3	-01.4	02.6	00.6	03.1	-01.5	-02.2	-04.0	04.0	04.9	04.6	97	89	97	94	SE 2	WNW 1	WSW 1
26	755.6	755.4	754.9	00.6	07.6	02.8	03.4	08.6	-00.4	-00.7	04.5	04.6	05.2	95	59	92	82	-0	WSW 2	ESE 2
27	753.1	751.9	752.2	00.4	08.8	03.4	04.0	09.7	00.4	-03.0	04.0	04.1	04.9	84	48	P3	72	SE 2	WNW 1	ESE 1
28	753.7	754.6	755.3	01.4	03.2	03.2	02.8	03.5	01.2	-02.7	04.7	05.1	05.0	93	84	86	89	NW 2	WNW 2	NW 2
29	755.7	754.7	755.0	02.8	04.0	03.8	04.6	08.3	02.7	02.0	05.0	05.6	04.5	89	70	75	78	ESE 2	SE 3	ESE 4
30	757.6	758.9	759.6	01.4	07.8	00.9	02.8	07.6	00.9	00.0	03.8	04.8	03.9	75	60	75	71	SE 4	SE 4	ESE 5
31	758.8	756.0	757.7	00.4	09.2	03.7	04.2	09.3	00.0	-01.2	03.7	04.5	04.5	79	52	76	69	ESE 4	SSW 3	ESE 3
MES.	756.0	756.0	756.4	00.5	04.2	01.6	02.0	04.8	-00.2	-01.4	04.1	04.4	04.3	85	71	82	79	2.5	2.4	2.6
VRFD.	756.0	756.0	756.4	00.5	04.2	01.6	02.0	04.8	-00.2	-01.4	04.1	04.4	04.3	85	71	82	79	2.5	2.4	2.6

1	756.0	755.0	754.5	C2.2	12.1	06.5	07.0	12.8	00.7	-04.0	04.1	05.2	05.0	76	45	67	64	SE 1	WNW 1	EST 2
2	754.2	753.9	754.2	07.4	12.0	04.7	05.9	13.2	06.2	00.5	05.2	06.6	06.0	68	60	66	65	SE 1	SSW 1	SE 2
3	754.1	752.4	756.5	06.5	16.3	10.0	10.7	16.9	06.5	00.0	04.8	05.2	05.3	66	37	58	54	SE 2	SSE 2	SE 2
4	747.0	744.4	744.0	10.0	11.1	07.6	09.3	12.6	07.8	07.0	05.5	06.6	05.5	60	64	70	65	SSW 2	SE 3	ESE 3
5	744.7	744.9	742.5	05.6	09.0	05.6	06.4	09.5	05.1	01.2	06.4	05.4	07.0	57	93	83	81	WSH 3	WSH 3	ESE 2
6	734.5	733.2	729.2	05.5	14.2	11.7	10.8	15.4	05.2	00.3	04.5	04.5	05.1	67	37	49	51	SSW 2	S 2	SSI 4
7	726.2	729.8	734.0	05.2	05.0	02.5	03.8	11.7	02.5	04.4	06.3	05.2	05.1	96	46	94	90	WSW 2	SSW 1	SW 1
P	741.4	745.6	751.1	01.2	05.4	02.4	02.8	07.0	00.5	-01.6	04.6	04.2	04.4	91	63	81	73	WSW 1	WNW 2	WNW 1
9	753.1	752.4	752.5	00.4	09.5	07.5	06.2	10.0	-00.4	-04.9	04.0	03.9	03.5	84	44	45	56	SE 2	SSW 2	SE 2
10	752.6	753.3	753.7	05.1	12.6	07.3	08.1	13.8	04.4	-00.6	03.6	05.6	05.6	54	52	73	60	SE 2	SE 2	SE 2
11	751.7	749.6	747.7	04.4	15.7	09.5	09.5	15.4	05.4	00.6	04.9	05.8	05.3	78	43	62	61	-0	ESE 2	SE 2
12	747.0	745.1	744.2	05.2	16.9	10.8	10.9	17.6	04.2	-01.9	04.9	05.3	05.3	74	37	55	55	ESE 1	ESE 1	ESE 2
13	743.1	742.0	742.3	06.8	15.6	07.7	09.4	15.8	06.6	03.1	05.2	05.3	05.3	70	40	67	59	SE 3	SE 3	ESE 4
14	742.5	743.1	744.8	05.4	10.6	06.7	07.4	11.6												

BECGRAC

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$$H_s = 132 \text{ m} \quad H_b = 132.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

Dan	Vlажност 0-9	Облачност N (0-10)					Изледача брой сали	Padavine R mm	Snežni покривач h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	5	10	10•	10	10.0	00.0	02.0	.	.	0-2°	0-22°
2	7	09	10	05	08.0	00.0	05.0	.	.	05°	6° 45° 11° 14° 17°
3	7	09	08	06	07.7	01.2	00.7	.	.	ESE 0-24°	ESE 0-24°
4	8	08	05.0	00	04.3	04.8	00.1	.	.	ESE 0-24°	ESE 0-24°
5	8	07	08.0	06	08.0	01.2	.	.	.	ESE 0-10°	ESE 0-10°
6	7	10	00.0	07	05.7	05.5	.	.	.	ESE 13°	ESE 13°
7	6	10*	10*	10	10.0	00.0	02.0	01	.	ESE 0-34°	ESE 0-16° 34°
8	7	10	05	10	09.7	00.0	01.2	02	.	0-0°	0-23° 24°
9	7	10	05	00	06.3	02.5	00.0	.	.	0-24°	0-24°
10	7	02	04.0	10	05.3	05.5	.	.	.	ESE-SE 0-4°	ESE-SE 0-4°
11	7	10	05	00	06.2	00.0	.	.	.	ESE 0-4°	ESE 0-4°
12	7	10	03.0	10	07.7	04.0	.	.	.	*7°	8°
13	7	10	05.0	00	05.0	02.2	00.0	.	.	0-10°	0-24°
14	7	00	03.0	00	01.0	07.5	.	.	.	0-2°	0-22° 24°
15	7	00	00.0	00	00.0	07.4	.	.	.	0-2°	0-14°
16	8	09	09	10	05.3	00.0	.	.	.	0-15° 6°	ESE 5°
17	6	C8	10•	10	05.3	00.0	.	.	.	0-19°	16° 22° 25° 23° 30°
18	7	10	10	05	08.3	00.0	03.1	.	.	WNW 55°	55° 83°
19	6	C4	10	10•	08.0	02.0	.	.	.	0-13° 9°	0-34° 24°
20	6	10	10	10	10.0	00.0	10.0	.	.	0-0-6°	22° 23° 30°
21	7	10	10	10	10.0	00.0	00.0	.	.	0-22°	0-24°
22	7	10	08	00	06.0	03.7	.	.	.	0-0-10°	0-26° 60° 0-15° 30° 30°
23	7	10	08.0	10•	09.3	01.3	.	.	.	0-23°	54° 17° 11° 22° 30°
24	7	10	05	05	08.0	00.7	01.1	.	.	0-2-0-10°	0-20° 26° 35°
25	5	C4≡	10	10≡	08.0	00.2	.	.	.	0-0-0-245°	0-245° 30° 0-23° 30° 30°
26	7	10	00.0	00	03.3	05.1	.	.	.	1-2-0-10°	0-26° 30° 24°
27	7	C2	00.0	00	00.7	08.3	.	.	.	0-0-0-23°	0-23° 24°
28	6	10	10	10•	10.0	00.0	.	.	.	0-0-0-15°	ESE 14°
29	6	10	00.0	00	03.3	05.6	00.0	.	.	ESE 0-24°	ESE 0-24°
30	7	C1	03.0	00	01.3	07.2	.	.	.	0-0-0-23°	0-23° 24°
31	7	01	05.0	03	02.0	06.1	.	.	.	ESE 0-10°	ESE 0-10°
MES.		VRED.		07.5	06.6	05.5	06.5	E3.4	76.5		

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1	8	C4	C20	C2	C2.7	CC.C	.	L ⁰⁻⁹¹⁶ = 0.30 12 ³⁰ 0.21 ³⁰ 0.1
2	8	10•	10	C8	C5.3	CC.C	.	L ⁰⁻⁶¹⁵ 24 ⁴⁵ 24 ¹⁵ 0.615 8 ³⁰
3	8	05	OC0	C6	C2.7	CC.6	.	L ⁰⁻⁵¹⁵ 0.515 14 ¹⁵ E ₁₅ 14 ¹⁵ 2 ¹⁵ 2 ¹⁵
4	7	10	10	C9	C5.7	CC.9	.	FES _E 0.014 14 ³⁰ L ⁰⁻⁰¹⁴ 10 ³⁰ C ₂₂ 12 ³⁰
5	7	10•	040	00	04.7	04.1	00.9	L ⁰⁻⁶¹⁵ 10 ³⁰ L ⁰⁻²²³⁰ 24
6	8	06	070	10•	C7.7	CC.C	C1.6	L ⁰⁻⁵¹⁵ FES _E 0.016 13 ³⁰ 24 ¹⁵ L ⁰⁻⁰¹⁶ 22 ³⁰
7	7	10•	10	C3	C7.7	CC.C	C9.5	L ⁰⁻⁰⁴⁵ 0.061 17 ³⁰ 26 ³⁰ L ⁰⁻⁰⁴⁵ 17 ³⁰
8	7	04	C10	C2	C2.3	C4.2	C3.6	L ⁰⁻²¹⁰ 0.210 12 ³⁰ 12 ³⁰ 0.210 8 ³⁰ L ⁰⁻²¹⁰ 12 ³⁰ 12 ³⁰ 0.210 8 ³⁰
9	8	02	05	05	05.3	03.7	C1.C	L ⁰⁻⁰³⁰ 0.030 24
10	8	01	030	00	C1.3	C7.4	.	L ⁰⁻²¹⁰ 0.210 12 ³⁰ 24
11	8	00	000	00	CC.C	C9.2	.	L ⁰⁻³³⁰ 20 ¹⁵ 24 ¹⁵ L ⁰⁻³³⁰ 8 ³⁰
12	8	00	000	00	CC.C	C9.1	.	L ⁰⁻⁴¹⁵ 24 ³⁰ 24 ¹⁵ L ⁰⁻⁴¹⁵ 8 ³⁰
13	8	04	010	10	C5.0	07.1	.	L ⁰⁻⁰⁷⁰ FES _E 10 ⁴⁵ 0.070
14	7	09	10	04	C7.7	C1.7	.	FES _E 0-04.0 0.045
15	7	09	10	00	06.3	01.9	00.CC	FES _E 0-6.1740, L ⁰⁻¹⁷⁴⁰ 8 ³⁰
16	7	04	030	00	C2.3	CC.3	CC.1	FES _E 0.016 24 ¹⁵
17	8	00	000	07	02.3	CC.8	.	FES _E 0-24.0 24 ¹⁵
18	8	09	08	10	CC.C	C2.C	.	FES _E -SE 0-24.0, FES _E 21 ³⁰ 23 ³⁰
19	8	09	060	04	CC.3	C2.3	.	FES _E 0-24.0, FES _E -SE 22 ⁰ 22 ⁰
20	8	08	10	10•	CC.3	CC.9	.	FES _E -SE 0-24.0, L ⁰⁻¹⁷⁴⁰ 24 ¹⁵
21	6	10•	10	10	10.0	CC.C	C4.4	L ⁰⁻¹⁰⁻¹²³⁰ 16 ⁴⁵ 17 ³⁰ = 0.1230 24 ¹⁵
22	6	10	10	C6	C2.7	CC.C	C1.8	L ⁰⁻⁰²⁴ 0.030 13 ³⁰ L ⁰⁻⁰²⁴ 13 ³⁰
23	7	10•	10	09	CC.7	CC.0	00.C	L ⁰⁻⁰³⁰ FES _E 10 ⁴⁵ 0.030, L ⁰⁻⁰³⁰ 8 ³⁰
24	7	09	10	10	CC.7	C2.7	CC.1	FES _E 0-1230
25	7	10	09	10	CC.7	CC.C	.	L ⁰⁻⁰⁹²⁰
26	7	10	060	10	CC.7	C4.4	CC.C	FES _E 10 ²⁰ 24 ¹⁵
27	8	000	06	00	CC.C	C7.7	.	FES _E 0-06.0 0.060 5. FES _E 12 ³⁰ 12 ³⁰ , L ⁰⁻⁰⁶¹⁵ 8 ³⁰
28	8	000	040	CC	C1.3	CC.8	.	FES _E 0-1230 24 ¹⁵ 0.1230 12 ³⁰ 0.1230 8 ³⁰

$\varphi = 44^{\circ}48'$ N $\lambda = 20^{\circ}28'$ E Gr. $\Delta G = +1\text{h }22\text{ min.}$

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D E S O	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	753.9	752.5	751.8	-01.4	06.6	01.0	01.0	07.0	-02.0	-03.3	02.8	02.8	02.8	68	35	58	55	ESE	5	ESE	4	ESE	4
2	748.9	747.7	746.5	-00.5	07.4	01.1	02.3	07.7	-00.6	-01.8	02.9	02.9	03.2	65	38	65	56	SE	4	ESE	5	ESF	5
3	749.8	751.9	754.4	00.5	07.4	02.4	03.2	08.0	00.1	-01.0	03.4	03.6	03.7	72	46	68	62	ESE	4	ESE	4	ESE	4
4	754.9	754.3	753.2	02.0	09.8	05.7	05.8	10.2	01.2	00.0	04.2	04.3	04.8	79	48	70	66	ESF	4	ESE	5	ESF	6
5	751.6	750.4	749.4	04.2	03.9	02.7	03.6	07.2	02.6	04.2	04.6	05.2	04.6	69	86	86	80	ESE	6	ESE	5	SE	5
6	749.3	748.9	750.5	02.4	02.9	01.5	02.3	04.6	01.7	01.0	04.1	04.8	05.0	76	84	95	85	ESE	5	ESE	5	ESE	2
7	751.6	752.9	753.7	02.4	02.9	02.2	02.4	03.4	01.4	01.0	04.8	05.2	04.2	89	92	77	86	E	2	ENF	1	ESI	2
8	753.9	753.4	754.3	-00.6	04.0	01.4	01.6	05.2	-01.0	-01.0	04.1	04.1	04.0	95	68	78	80	SF	2	ESE	2	ESO	3
9	754.7	755.0	756.1	-00.4	01.6	06.7	00.6	02.1	-00.6	-00.6	03.5	04.1	04.2	78	80	86	81	ESF	3	ESF	3	ESI	3
10	756.0	755.9	756.3	00.8	04.6	01.0	01.8	05.2	-00.3	00.0	03.9	04.3	03.8	81	67	76	75	ESF	3	ESE	5	ESI	4
11	757.7	759.0	760.2	-00.6	02.3	02.5	01.7	03.4	-00.7	-01.0	04.1	04.9	04.4	94	90	81	88	ESE	3	ESF	2	ENI	2
12	740.4	756.7	757.4	00.9	10.0	01.7	04.6	10.3	00.7	-01.4	03.8	03.8	02.8	78	41	47	55	E	2	SE	2	SE	3
13	754.6	752.0	750.7	01.3	11.1	04.9	05.6	11.9	00.4	-02.7	03.6	04.2	04.2	72	42	65	60	ESE	2	SSE	3	SE	3
14	748.5	746.2	744.9	01.2	11.5	07.8	07.1	12.7	00.6	-01.3	04.1	04.5	03.5	81	44	44	56	SE	2	ESE	3	SE	4
15	743.2	743.5	744.4	04.4	07.8	06.2	06.2	08.3	04.2	02.3	04.5	04.6	06.3	72	58	74	68	SSW	1	SSE	1	-	0
16	744.0	743.4	743.9	04.2	09.6	06.4	06.6	10.2	03.8	02.8	05.3	04.5	04.8	85	50	67	67	SE	1	SSW	1	SSF	2
17	744.8	745.7	746.9	03.5	16.0	11.4	10.6	16.8	03.0	-01.7	04.9	05.3	05.2	83	39	52	58	SSE	1	NNW	2	SW	2
18	748.0	747.0	746.8	09.8	20.6	15.7	15.4	21.8	08.2	04.2	05.5	04.9	05.6	61	27	42	43	SE	1	W	2	SE	2
19	750.2	749.8	750.4	11.8	26.2	15.5	19.0	26.6	10.0	04.4	06.1	04.6	05.4	59	19	32	37	SE	2	NW	2	S	3
20	753.6	753.0	753.2	11.0	23.5	17.0	17.1	24.4	10.0	03.4	03.9	04.8	04.9	40	22	34	32	SE	1	SW	2	ESI	2
21	754.9	754.2	754.6	12.8	25.0	18.0	18.4	25.9	11.5	03.6	04.7	07.0	05.9	42	29	38	36	SE	1	ESE	2	ESI	4
22	754.4	753.0	751.5	14.0	24.8	16.2	17.8	25.3	12.0	10.2	05.6	05.0	05.6	46	21	40	34	SE	4	SE	3	SSE	2
23	751.3	750.0	751.4	14.0	25.7	19.3	19.6	26.0	13.7	11.2	05.7	06.6	08.1	47	27	48	41	SE	3	SE	2	-	0
24	751.1	753.1	752.7	14.1	22.0	16.0	17.0	22.3	13.0	09.0	07.4	06.7	07.1	61	34	52	49	SE	3	SE	4	SE	4
25	753.4	753.0	753.3	08.2	13.7	08.0	09.4	16.0	08.0	07.7	05.5	05.3	04.7	68	47	58	56	SE	6	ESE	2	ESE	2
26	752.5	750.0	749.4	07.1	19.2	13.4	13.0	19.5	06.0	04.8	04.7	06.7	06.0	66	40	52	53	FSE	5	SE	2	ESE	2
27	747.6	746.8	747.6	09.8	20.0	15.2	15.2	21.5	08.6	06.1	05.3	06.7	06.4	58	37	45	48	SE	2	NE	2	ENI	1
28	749.6	749.6	751.0	10.2	20.3	13.5	13.5	14.4	20.5	09.0	05.0	06.0	06.0	64	34	45	48	ISE	3	ESE	3	SE	2
29	753.2	753.0	753.3	07.5	17.6	11.2	12.2	18.0	08.5	07.4	05.0	04.3	04.1	54	35	41	45	ESE	4	SE	2	ESI	2
30	754.9	756.0	754.4	07.2	11.1	09.1	09.4	11.3	08.0	06.7	03.7	03.6	03.6	46	36	42	41	ESE	4	ESE	5	ESI	2
31	751.1	752.5	752.1	07.7	10.7	09.2	09.4	11.0	08.3	06.7	04.5	04.0	04.8	53	41	55	50	SE	3	ESE	3	ESI	1
MES.	WRED.			751.8	751.4	751.6	05.6	12.9	08.6	08.9	13.7	04.8	02.8	04.6	04.8	04.8	68	47	59	58	3.0	3.0	3.1

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1	750.9	751.4	751.7	07.0	05.8	10.0	05.2	11.3	06.6	05.6	05.4	04.5	04.5	71	50	45	57	ESE	5	ESE	5	ESE	2
2	752.8	753.5	755.0	06.5	11.2	07.2	08.2	12.0	06.5	05.6	03.9	04.2	03.9	54	41	51	49	ESE	5	ESE	4	ESF	3
3	755.7	754.2	754.3	04.4	14.0	09.5	09.8	15.3	03.2	-00.8	03.7	03.6	03.6	60	29	40	43	SI	2	ESE	2	ESI	2
4	753.2	751.6	750.5	05.0	15.7	10.7	10.5	16.2	04.4	00.8	03.5	03.9	03.8	54	29	39	41	ESE	1	NNE	2	ENF	1
5	749.9	750.0	750.7	08.0	17.3	12.0	12.3	17.3	06.2	00.0	04.1	03.4	03.6	51	23	34	36	ESE	2	SE	2	NE	2
6	751.1	750.4	750.1	08.4	17.7	12.5	12.8	18.0	05.6	-00.9	03.9	03.7	04.5	47	24	41	37	SE	2	ENE	2	NE	1
7	750.2	748.4	748.5	07.4	17.1	13.5	12.9	18.2	06.9	03.7	04.6	04.2	04.3	59	29	40	45	NNW	2	NW	3	NW	1
8	748.6	748.0	749.5	07.9	14.4	10.2	10.7	15.6	07.5	06.0	06.3	04.0	02.3	78	33	35	49	NNW	3	NW	4	NNF	2
9	751.1	750.9	750.6	04.6	15.7	10.0	10.1	16.7	04.1	01.0	03.8	04.3	04.8	60	32	52	48	NNW	1	NW	2	ESE	1
10	750.4	748.0	745.7	10.0	20.6	14.7	15.2	20.7	07.8	01.6	05.0	05.5	04.9	52	30	39	40	SSE	3	ESE	2	ESI	2
11	743.9	741.8	741.5	10.9	20.2	14.0	14.8	20.2	08.8	06.6	04.8	05.5	05.2	50	31	44	42	FSE	3	SSE	3	SE	3
12	741.2	740.2	741.3	11.1	21.0	13.6	14.9	21.5	10.1	09.0	05.9	06.6	09.2	59	35	79	58	FSE	3	LSE	3	SSW	1
13	742.0	742.2	744.6	13.6	20.0	12.2	14.5	20.6	12.2	09.6	02.2	04.8	08.6	71	48	80	66	SW	1	NW	2	NNF	3
14	744.0	742.6</																					

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 $H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Dan	Vrijednost 0-9	Oblečnost N (0-10)					Instalacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7	00	020	00	00.7	CC.1	.	.	.	F ESE 2 ⁰⁸ 24i, F ESE 4 ³⁸	
2	8	00	040	C3	02.3	CC.8	.	.	.	F ESE 0-8 ¹⁶ i, F ESE 8 ⁴⁶ 24i	
3	8	04	040	00	02.7	CC.3	.	.	.	F ESE 0-8 ¹⁶ i, F ESE 8 ⁴⁶ 24i	
4	8	00	090	06	05.0	06.8	.	.	.	F ESE 0-4 ⁴⁸ i, F ESE 4 ⁴⁸ 24i	
5	7	09	100	100	05.7	CC.0	.	.	.	F ESE 0-2 ⁴⁶ i, 0 ⁹⁴⁵ 23 ⁴⁵ i	
6	7	09	05	100	05.3	CC.0	10-2	.	.	F ESE 0-15 ⁰³ X ⁰⁹⁰² 10 ⁵⁰ 15 ⁵⁰ 16 ⁴⁰ * ⁰ 12 ⁵⁰ 13 ⁵⁰ i, F ESE 15 ²³ 19 ¹⁰ 22 ¹⁶ , 0 ¹ 14 ³⁰ 17 ³⁵	
7	6	100	100	10	10.0	CC.0	06.0	.	.	* ⁰ 0 ⁷⁰ 10 ⁵ 16 ⁵ 17 ¹⁵ , 0 ⁸³² 10 ⁵ * ⁰ 17 ⁰⁵ 17 ⁴⁰ i, F ESE 16 ⁰⁵ 24i, [X]	
8	7	09	05	10	05.3	03.4	02.9	01	.	X ⁰ 11 ¹⁸ 5 ³⁰ F ESE 16 ⁰⁵ 24i, [X]	
9	7	10*	10*	10	10.0	CC.0	00.0	.	.	F ESE 0-15 ⁰⁵ X ⁰³⁰⁰ 9 ⁴⁵ M ⁵⁰ 24i	
10	7	09*	08	10	05.0	02.5	00.2	.	.	* ⁰ 0-3 ³⁰ 6 ⁴⁵ 11 ³⁰ F ESE 16 ⁵⁵ 19 ²⁶ 22 ⁰² 24, F ESE 19 ²⁶ 22 ⁰² 24, [X]	
11	6	10*	10*	10	10.0	CC.0	01.3	C2	.	F ESE 0-8 ²² 9 ²⁵ 10 ⁰⁷ * ⁰ 2 ³⁰ 13 ⁴⁵ X ⁰ 13 ¹⁵ 15 ¹⁵ , 0 ⁰ 22 ⁴⁶ 23 ¹⁵ , [X]	
12	8	000	010	00	00.3	09.3	00.8	.	.	= 0 ⁴³⁰ 8 ¹⁵ i, F ESE 17 ⁰⁹ 17 ⁴² i	
13	8	000	000	00	00.0	CC.0	CC.6	.	.	F ESE 7 ⁵⁰ 8 ¹⁵ i, △ 2 ³⁵ 24	
14	8	05	050	02	04.0	08.1	.	.	.	□ 0-8 ¹⁵ F ESE 20 ⁵⁵ 21 ⁴⁹	
15	7	10	10	100	10.0	CC.0	00.0	.	.	F ESE 0 ⁶ 2 ³⁵ i, 0 ²⁰ 24i	
16	7	10	08	00	06.0	00.9	00.0	.	.	△ 0 ¹⁹⁴⁵ 24	
17	7	00	030	C3	02.0	08.5	.	.	.	△ 0-2 ³⁰ 14 ⁵⁰ 2 ³⁰ 17 ³⁰	
18	8	040	020	04	03.2	09.4	.	.	.	△ 0 ³²⁰ 17 ³⁰	
19	8	090	020	00	03.7	09.5	.	.	.	△ 0 ³²⁰ 17 ³⁰	
20	8	010	050	03	03.0	06.7	04.2	.	.	△ 0 ⁴³⁶ 6 ³⁰	
21	8	000	000	00	00.0	10.1	.	.	.	0-1 ³⁰ 8 ⁴⁶ F ESE 14 ⁴³ 22 ⁵³	
22	8	000	000	00	00.0	10.4	.	.	.	F ESE 2 ³⁵ 18 ⁵⁰ i	
23	8	080	050	09	07.3	08.0	.	.	.	F ESE -8 ⁰² 10 ⁵⁰ i, 16 ⁰² 17 ⁵⁰ i, 0 ¹⁸³⁰ 19 ¹⁵ , 0 ⁰ 18 ⁴⁵ 18 ⁴⁹	
24	8	010	050	02	02.7	09.0	CC.1	.	.	F ESE 3 ²² 22 ²⁰ i, F ESE 22 ²⁰ 21	
25	8	06	08	00	06.7	04.2	.	.	.	F N6 0-24i	
26	7	02	000	00	00.7	CC.0	.	.	.	F ESE 0-4 ²⁹ i, F ESE 4 ²⁹ 10 ⁵¹	
27	7	050	000	00	01.7	CC.1	.	.	.	△ 0-2 ³⁰ 24	
28	7	000	000	00	00.0	CC.0	CC.1	.	.	△ 1 ² 0-6, F ESE 5 ¹⁶ 10 ⁴⁰ 16 ⁰² 24i	
29	7	000	000	00	00.0	CC.0	CC.0	.	.	F ESE -5 ¹⁶ 10 ⁴⁰ i, 16 ⁰² 17 ⁵⁰ i, 0 ¹⁸³⁰ 19 ¹⁵ , 0 ⁰ 18 ⁴⁵ 18 ⁴⁹	
30	7	10	10	10	10.0	CC.0	CC.0	.	.	F ESE 0-24i, F ESE 16 ⁵⁵ 19 ³⁸ 19 ⁴²	
31	7	10	10	10	10.0	CC.0	00.0	.	.	F ESE -6 ⁰ 14 ⁵⁰ i, 8 ⁵³ 24i, 0 ⁸³⁰ 19 ³⁰	
MES. WRED.			04.9	05.1	04.4	04.8	179.8	21.5			

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1	7	10	10	10	10.0	CC.0	CC.1	CC.0	.	F ESE 0 ⁰⁵ 1 ⁵⁰ 11 ⁴⁰ 24i, F ESE 1 ⁵⁰ 0 ³²⁰ 4 ⁵⁰ i	
2	7	10	0E0	03	07.0	01.8	00.0	.	.	F ESE 0-23 ⁶⁸ i, F ESE 2 ⁰⁶ , 0 ⁵⁴⁵	
3	7	020	020	00	01.2	1C.6	.	.	.	F ESE 9 ⁰⁸ 9 ²⁵ i	
4	8	050	000	00	01.7	09.4	
5	8	000	020	00	00.7	CC.0	CC.6	.	.	.	
6	8	000	030	05	02.7	10.0	.	.	.	△ 0 ²² 24	
7	8	030	060	100	06.3	07.9	.	.	.	△ 0-6 ⁴⁵ F N-NW 13 ⁴⁰ 16 ⁰⁰ i, △ 0 ¹⁵ 15 ⁵⁵ i, 0 ⁰ 19 ⁴⁰ 23 ⁴⁵	
8	8	08	060	01	05.0	07.5	00.1	.	.	△ 0 ²⁵⁰ 3 ⁴⁰ i, F N-NW 9 ⁴² 17 ⁰² i	
9	8	000	040	00	01.3	09.0	.	.	.	F NWW 14 ⁴⁰ △ 19 ⁴⁵ 24	
10	8	020	030	00	01.7	09.5	.	.	.	△ 0-10 ⁴⁵	
11	8	10	090	04	07.7	01.3	.	.	.	F SE -3 ²² 14 ⁴⁵ 17 ⁰⁴	
12	8	09	060	09	08.0	05.5	.	.	.	F NW 18 ⁵⁵ 19 ¹⁹ i, 0 ¹⁹⁰⁰ 22 ⁴⁰ i	
13	8	090	060	09	08.0	06.4	00.3	.	.	0 ⁰⁵ 1 ⁵ 6 ²⁰ 6 ⁴⁰ 12 ¹⁵ 12 ²¹ 14 ⁵⁵ 20 ⁴⁵ ; F W 12 ⁴⁰ , ♀ 12 ²¹ 12 ³⁰ , 16 ³² 16 ³⁷	
14	5	10	100	10	1C.0	00.0	02.1	.	.	0 ⁷⁸ 10 ⁵¹ 24 ⁴⁰ 25 ⁵ F ESE 15 ⁴⁵ 23 ⁴²	
15	8	100	100	10	1C.0	00.0	08.7	.	.	0 ⁰⁴⁵ 20 ⁵² i	
16	7	1C	090	04	07.3	02.8	01.1	.	.	0 ³²⁰ 8 ²⁰ i, 11 ⁴⁵ 21 ⁴⁵ 24i, ♀ 10 ³⁰ 10 ⁵⁷ i, F ESE 2 ⁵⁸	
17	7	1C	100	10	1C.0	00.0	09.5	.	.	0 ¹ 0-2 ⁴⁵ 24i, F ESE 16 ⁵⁴	
18	6	100	100	10	10.0	00.0	05.6	.	.	0 ⁶ 2 ²⁴ i	
19	7	10	10	10	10.0	03.1	05.0	.	.	0 ⁰ -2 ⁴⁵ 11 ⁴⁵ F NW 11 ⁴⁵ 16 ²⁰ i	
20	8	000	040	00	01.3	09.5	.	.	.	△ 0 ² 20 ⁴⁵	
21	7	C9	090	04	07.3	02.8	.	.	.	0 ² 0-7 ³⁰ 0 ⁴⁴⁵ 16 ⁰⁵ i, ♀ 0 ⁴⁴ 14 ⁴³ 14 ⁴⁷	
22	8	050	050	05	05.0	08.6	01.5	.	.	0 ⁴⁴ 16 ⁵⁶ 0 ⁵¹⁶ 16 ⁴⁰ i	
23	8	000	070	00	02.3	08.2	00.0	.	.	0 ⁰ -2 ⁴⁵ 9 ³⁰	
24	8	000	050	07	04.0	12.1	01.1	.	.	0 ⁰ -2 ⁴⁵ 8 ⁴⁵ i	
25	6	09	10	100	09.7	00.0	.	.	.	0 ⁰ -2 ⁴⁵ 8 ⁴⁵ , 0 ⁰ 15 ⁴⁰ 24i	
26	8	100	050	09	08.0	05.7	06.1	.	.	0 ⁰ -7 ⁵ 14 ⁴⁵ 16 ⁰⁵ i, F W 14 ⁴⁰ 14 ⁵⁶ 15 ³⁵ , ♀ 0 ²⁰ 20 ⁴⁰	
27	8	08	090	09	08.7	08.2	04.4	.	.	△ 0 ⁴⁴ 24	
28	8	040	080	10	07.3	08.6	.	.	.	△ 0 ⁰ -8 ⁴⁵ F ESE 10 ⁵² 24, 0 ⁰ 16 ⁴⁵ 18 ⁴⁵ i, 20 ⁴⁵ 20 ⁴⁵ i	
29	8	100	060	08	08.0	06.0	00.5	.	.	F ESE -5 ³⁹ 7 ⁴⁵ , 0 ⁰ 25 ⁴⁵ 7 ⁴⁵	
30	8	06	090	100	08.3	06.5	00.0	.	.	0 ⁰ 16 ⁵³ 24 ²⁰ i, ♀ 0 ⁴⁴ 21 ⁴⁰ 21 ¹⁰ i	
MES. WRED.			06.3	06.7	06.1	06.4	169.9	46.0			

$\varphi = 44^{\circ}48'$ N $\lambda = 20^{\circ}28'$ E Gr. $\Delta G = +1h\ 22\ min.$

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E O	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih pare e mm			Relativna vlažnost u%			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	732.4	732.1	733.2	13.8	20.1	14.0	15.5	20.4	10.6	05.7	07.3	06.8	07.5	62	39	63	55	SE	2	S	2	SSW 1
2	734.7	738.2	741.1	11.9	11.8	11.2	11.5	14.0	11.0	04.8	10.0	09.7	09.3	95	93	93	94	W	3	W	2	W 3
3	743.6	743.9	744.6	10.6	18.7	15.2	14.9	19.7	09.4	07.2	08.1	08.4	09.3	85	52	72	70	WSW	2	WSW	3	SSE 2
4	743.7	742.2	741.9	14.8	19.9	13.4	15.4	20.4	12.8	10.4	07.4	07.9	08.6	58	45	75	59	SSE	2	SE	2	S 3
5	741.6	739.6	740.9	13.4	20.4	11.2	14.1	20.8	09.5	05.8	07.3	06.6	08.9	63	36	89	63	S	2	SSE	2	NNE 2
6	742.2	742.8	746.2	13.2	17.2	11.5	13.4	19.7	09.1	05.4	06.7	07.2	08.9	55	49	88	65	S	2	S	2	WSW 2
7	749.3	750.3	750.6	10.4	15.1	12.6	12.7	15.8	10.0	08.5	07.0	07.7	08.1	75	60	74	70	NNE	1	NE	2	SSE 2
8	751.7	751.2	749.5	11.6	14.8	12.0	12.6	15.8	10.2	09.2	09.5	08.8	08.2	93	69	78	80	NNW	1	NNW	2	NW 1
9	747.2	746.9	747.3	09.1	16.3	12.0	12.4	16.8	08.7	07.6	06.4	05.7	06.6	73	41	63	59	NW	2	NNW	3	NW 2
10	748.0	747.8	748.2	09.9	18.2	12.4	13.2	19.1	07.4	04.4	06.8	06.1	07.0	74	39	65	59	W	2	NW	2	SSE 1
11	748.9	749.2	749.5	13.5	23.3	16.6	17.5	23.4	09.2	03.8	06.8	07.0	06.6	59	32	49	47	SE	2	NNW	2	SF 2
12	749.5	751.9	752.5	16.6	16.2	14.6	15.5	19.1	12.9	07.2	08.2	10.4	10.9	58	75	88	74	-	0	E	2	- 0
13	754.6	755.1	755.0	12.7	19.5	14.6	15.4	20.1	11.8	11.6	10.0	08.8	09.3	91	52	75	73	W	1	NW	2	SF 1
14	753.4	751.3	749.6	15.4	22.9	16.3	17.7	23.1	10.4	06.0	09.2	08.3	09.1	70	40	65	58	SE	1	NW	2	WSW 1
15	751.4	750.3	749.2	10.2	10.3	09.2	09.7	16.3	09.1	09.3	08.8	08.3	08.2	94	88	94	92	W	2	NNW	1	SW 1
16	746.5	746.5	747.4	09.4	11.5	11.7	11.1	12.9	08.2	08.0	08.0	09.1	09.2	90	90	89	90	WSW	2	W	2	SW 3
17	749.1	750.1	751.7	11.0	16.2	10.6	12.1	17.2	10.5	08.6	07.9	07.4	08.9	81	53	93	76	WSW	2	W	1	NW 1
18	752.5	753.0	753.0	10.0	14.9	13.4	13.1	16.8	09.9	09.7	08.9	10.5	10.4	93	83	90	89	W	2	NNW	2	NNW 2
19	752.0	751.6	751.1	12.0	20.6	16.2	21.7	11.5	11.0	09.2	10.4	10.2	88	57	74	73	NNW	2	NW	2	- 0	
20	751.2	750.0	749.3	15.0	24.5	17.0	18.4	24.7	10.2	06.5	09.5	09.0	10.2	74	39	70	61	WSW	1	NW	2	- 0
21	750.0	750.9	751.0	14.4	20.2	15.0	16.2	21.2	13.3	09.0	10.3	11.0	10.7	84	62	84	77	NNW	2	WSW	2	WSW 2
22	749.8	745.6	743.8	13.2	21.7	11.5	14.5	21.7	11.5	09.0	09.3	09.3	09.7	82	48	95	75	WSW	1	SSW	2	NNE 3
23	743.0	742.6	742.9	11.6	16.1	11.0	12.4	16.9	11.0	10.4	06.4	06.5	06.8	82	47	90	73	NNW	2	NW	3	SSW 1
24	743.6	744.0	742.9	11.0	18.6	15.5	15.3	19.6	07.5	05.5	07.8	07.6	09.7	77	47	74	66	S	1	SE	2	ESE 3
25	745.7	747.0	749.7	12.3	19.4	15.2	15.5	19.6	11.6	08.4	09.9	09.2	08.8	92	54	68	71	W	2	NNW	2	NNW 2
MES.	VRED.	747.5	747.3	747.5	12.0	19.1	14.2	15.2	20.1	10.8	08.2	08.7	08.5	09.3	77	53	77	69	1.7	2.1	1.5	

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1	748.5	748.8	750.2	21.4	22.8	17.4	19.8	24.4	17.3	15.4	13.6	12.5	14.2	71	60	95	75	NNW	1	W	3	WNW 2
2	751.6	753.0	754.0	14.9	13.9	13.4	13.9	17.4	13.0	13.5	10.8	11.5	11.0	85	97	96	93	WNW	2	WNW	2	F 2
3	754.3	755.1	754.6	13.8	16.7	15.4	15.3	18.1	13.2	12.3	08.0	09.4	11.3	67	66	86	73	NW	2	S	1	
4	754.6	753.6	752.9	16.4	24.0	18.6	19.4	25.2	11.7	09.2	10.2	10.1	12.1	73	45	75	64	SSE	1	NW	2	SSW 1
5	752.9	751.5	750.3	18.4	26.0	21.0	21.6	26.6	14.3	11.5	11.5	13.1	12.1	72	52	65	63	WSW	1	NNE	2	E 2
6	748.6	747.5	747.4	21.5	28.0	17.8	21.3	29.5	17.5	13.9	13.6	15.2	14.1	71	53	92	72	SE	2	SSF	2	NW 1
7	747.6	749.2	752.0	17.5	15.4	14.4	15.4	18.0	14.4	15.8	13.4	11.5	09.8	90	88	80	86	W	2	NNW	3	NNW 2
8	754.7	744.9	743.3	12.6	18.5	13.8	14.7	19.6	09.6	07.1	07.7	06.6	07.9	70	41	67	59	NNW	2	ESE	2	
9	748.4	746.5	744.7	15.3	24.9	20.6	20.4	25.6	11.6	08.4	08.0	10.7	12.0	62	45	66	58	ESE	3	SSE	3	SE 3
10	745.2	743.3	743.5	15.0	25.6	18.2	19.2	27.1	14.6	12.5	12.0	13.8	11.8	94	56	76	75	SSW	2	NNE	2	NNW 2
11	742.1	742.6	744.0	13.2	12.0	11.2	11.9	18.2	11.2	10.9	10.9	09.7	09.5	96	92	95	94	W	3	NNW	3	WNW 3
12	744.5	743.1	743.8	11.9	18.2	12.0	13.5	18.2	12.0	07.4	07.3	06.6	08.7	69	42	82	64	WNW	3	W	2	W 2
13	743.5	743.2	744.4	11.9	17.0	12.5	13.5	17.2	08.7	07.2	06.9	06.5	08.0	66	45	73	61	W	3	NNE	1	
14	744.8	745.5	746.7	13.0	17.7	14.6	15.0	18.7	11.5	10.5	08.6	08.3	10.8	77	54	87	73	SW	1	WSW	3	SW 1
15	749.5	749.5	747.7	14.0	21.5	17.0	17.4	22.7	13.5	12.8	11.4	09.8	13.1	95	51	90	79	W	2	NNW	2	ESE 1
16	748.4	747.9	746.8	15.0	18.1	17.4	17.0	22.6	13.2	12.1	11.4	12.9	12.7	89	82	85	86	WSW	1	E	1	NF 1
17	747.1	746.8	746.8	16.5	19.5	17.8	17.9	24.0	12.9	10.6	12.4	13.0	12.5	88	76	82	82	S	1	SE	1	- 0
18	747.1	746.7	747.0	18.7	25.6	20.0	21.1	26.3	14.1	11.4	12.3	09.7	09.8	76	39	56	57	SSE	1	WNW	2	NNH 1
19	748.9	748.9	750.9	17.8	24.2	15.7	18.4	24.6	15.7	13.3	12.6	13.6	13.0	82	60	97	80	W	2	NW	3	W 2
20	751.4	751.1	751.0	14.4	21.2	16.0	16.9	22.2	14.2	13.8	11.0	10.										

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 $H_s = 132 \text{ m}$ $H_b = 132.0 \text{ m}$ $h_t = 2.0 \text{ m}$ $h_r = 1.2 \text{ m}$

Dan	Vrijnost 0-9	Oblačnost N (0-10)					Intensitet broj sun	Padavina R mm	Snožni pokriven h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	9	050	070	08	C6.7	C6.4	C6.4	.	.	$\oplus^0 12^{55} 13^{12} \ominus^0 13^{02} 13^{40} \oplus^0 16^{40} 16^{55} 1, 23^{55} 24$	
2	6	100	100	100	10.0	00.0	06.7	.	.	$\bullet^0 20-22^1$	
3	7	000	060	09	C5.0	C1.5	C3.4	.	.	$\equiv 0^{45} 10^{30} \ominus^0 20^{45} 22^{45}, \oplus^0 22^{45} 24^1$	
4	8	09	10	08	C9.0	C0.2	00.0	.	.	$\bullet^0 0-15 14^{45} 18^{30}$	
5	8	060	070	07	C6.7	C8.2	C1.8	.	.	$\bullet^0 45 19^{45} 18^{30}, \oplus^0 17^{30} 18^{30}, \oplus^0 17^{40} 17^{50}$	
6	8	010	080	C7	C5.3	C8.0	C4.4	.	.	$\bullet^0 11^{55} 15 13^{20} 16^{45} 19^{45} 20^{45}, \Delta^0 13^{30} 8^{40}, R 14^{45} 16^{30}$	
7	7	10	090	C8	C9.0	C3.5	C4.6	.	.	$\bullet^0 20-22^1$	
8	7	10	080	09	C9.0	C1.8	C4.1	.	.	$\bullet^0 20-45 18^{45} 19^{45} \Delta^0 14^{30} 24^1$	
9	8	060	060	C2	C4.7	C1.3	.	.	.	$\Delta^0 0-936 20^{45} 24^1, F_{WW} 12 15^{35}$	
10	8	000	07	00	C2.3	11.6	.	.	.	$\Delta^0 10-0^1 20^{45} 24^1$	
11	8	000	030	00	C1.0	11.3	.	.	.	$\Delta^0 20-8^{30} 20^{45} 24$	
12	8	060	080	100	08.0	05.7	.	.	.	$\bullet^0 20-8^{45} 10^{30} 12^{25}, 20^{20} 24^1, F_W 8^{51} 10^{36}$	
13	7	10	060	04	C6.7	C4.4	C1.6	.	.	$\bullet^0 0-40 \equiv 0-2 5^{15} 11^{15} 10^{45} 19^{45} 24^1$	
14	7	060	080	03	05.7	C9.0	.	.	.	$\Delta^0 20-19^{45} 24^1, \Delta^0 20^{50} 24^{45}$	
15	6	100	100	10	C6.0	00.0	03.3	.	.	$\Delta^0 10-0^{45} 0-0^{45} 24^1, 10^{45} 24^1, \oplus^0 4^{20} 10^{45}$	
16	7	10	10	06	08.7	00.0	12.4	.	.	$\bullet^0 10-1^{30} 14^{45} 16^{45} 23^{30} 24, \oplus^0 13^{20} 14^{40} 1$	
17	8	100	060	100	06.7	C2.1	C2.2	.	.	$\bullet^0 10-0^{25} 6^{45} 8^{20} 19^{30} 20^{45}, F 12^{02} 14^{50}$	
18	7	100	09	10	05.7	C1.9	C3.6	.	.	$\equiv 0^{30} 6^{30} 6^{30} 8^{30} 14^{30}, H^{45} 12^{30}, \Delta^0 12^{30} 13^{10}$	
19	7	08	060	00	04.7	C9.1	01.1	.	.	$\equiv 0^{30} 12^{45} \Delta^0 19^{45} 24^1$	
20	8	000	060	05	03.7	11.4	.	.	.	$\Delta^0 20-0-8^{45} 19^{45} 24^1, T^0 17^{50} 18^{45}$	
21	7	09	040	100	C7.7	03.6	.	.	.	$\Delta^0 10-8^{20} 8^{40} 12^{55} 17^{40} 21^{30}, \oplus^0 17^{20} 20^{45} 22^{05} 22^{05}$	
22	7	010	09	10R	06.7	04.7	07.1	.	.	$\bullet^0 12^{35} 8^{30} \equiv 0^{35} 8^{45} 10^{45}, \Delta^0 10^{30} 11^{45}, \Delta^0 10^{30} 18^{45} 18^{45}, 21^{20}, F_N 12^{24} 12^{25} \Delta^0 12^{25} \Delta^0 12^{25}$	
23	8	020	060	00	C2.7	07.1	05.6	.	.	$F_{WW} 12^{45} 14^{30}, \Delta^0 15^{45} 15^{45}, 18^{45} 18^{45}, R 16^{45} 16^{45}, \oplus^0 14^{45} 14^{45}, \Delta^0 14^{45} 24^1$	
24	8	09	050	05	06.7	C6.1	C1.2	.	.	$\Delta^0 0-745 0-757 7^{45} 17^{45} 19^{45}, \Delta^0 20^{45} 22^{30}, F_{WW} 21^{21} 22^{25}, \Delta^0 21^{25} 22^{25}$	
25	7	10	050	04	06.3	06.7	04.8	.	.	$\bullet^0 10-34 7^{30} 9^{45} 11^{45}, \Delta^0 14^{30} 6^{30}, R 13^{30}, F_{WW} 14^{32}, \Delta^0 21^{18} 24^1, \Delta^0 21^{25} 21^{25}$	
26	8	000	050	00	C1.7	12.3	01.2	.	.	$\Delta^0 10-10^{30} 19^{45} 24^1$	
27	8	000	060	00	02.0	12.4	.	.	.	$\Delta^0 10-8^{30} 20^{45} 24^1$	
28	8	060	040	06	05.3	11.4	.	.	.	$\Delta^0 10-8^{30} 22^{30} 24^1$	
29	8	10	090	10	09.7	02.2	00.4	.	.	$\Delta^0 10-5 0-6-15 15^{45} 10^{45} 19^{45}$	
30	7	090	050	02	05.3	09.9	00.2	.	.	$\Delta^0 10-8^{30} 19^{45} 24^1, \Delta^0 20^{45} 20^{45}, R 20^{30} 22^{45}$	
31	8	040	050	06	05.0	09.7	.	.	.	$\Delta^0 10-8^{30} 19^{45} 24^1, \Delta^0 20^{45} 20^{45}, R 20^{30} 22^{45}$	
MES. VRED.		06.0	06.9	05.8	06.2	202.5	80.2				

1	8	09	09	100	C9.3	C3.5	C0.1	.	.	$\bullet^0 0-05 i, 19^{55} 21^{30}, \oplus^0 7^{55} 8^{40} 14^{30}, 14^{45}, 17^{35} 18^{40}$	
2	3	10	100	100	10.0	00.0	06.3	.	.	$\bullet^0 18^{30} 23^{30}, \oplus^0 10^{45} 10^{45}$	
3	7	10	10	05	C8.3	C0.0	14.1	.	.	$\bullet^0 245-35 \ominus^0 20^{30} 24$	
4	8	000	040	00	C1.3	13.4	.	.	.	$\Delta^0 10-9^{55} 20^{30} 24$	
5	8	09	050	00	04.7	10.2	.	.	.	$\Delta^0 10-8^{45} 19^{45} 24$	
6	8	010	080	10R	06.3	09.5	.	.	.	$\Delta^0 0-8^{30} 14^{45} 14^{45} 19^{45} 21^{30}, F_{WW} 19^{46} 19^{46}, \oplus^0 19^{45} 20^{45}, \oplus^0 120^{45} 21^{45}$	
7	7	10	10	04	C8.0	00.0	10.9	.	.	$\bullet^0 17^{30} 12^{30}, \oplus^0 10^{45} 10^{45}, F_{WW} 10^{32}$	
8	8	030	020	00	C1.7	13.6	C8.0	.	.		
9	8	000	080	C5	04.3	10.8	.	.	.		
10	7	10	070	C9	C8.7	C8.8	.	.	.		
11	8	100	100	100	C6.0	00.0	04.6	.	.	$\oplus^0 5-6^i, 13^{10} 13^{25}, \oplus^0 6^{40} 10^{45} 12^{45} 23^{45}, F_{WW} 12^{24} 21^{45}$	
12	7	000	070	05	04.0	07.7	18.9	.	.	$F_{WW} 12^{22} 16^{22}, \oplus^0 11^{45} 11^{45}, 14^{45} 16^{45}, \Delta^0 12^{22} 12^{24}$	
13	8	08	09	09	08.7	01.0	01.2	.	.	$\Delta^0 7^{45} \oplus^0 10^{45} 15^{45}, 15^{45} 15^{45}, 22^{45} 24^1$	
14	8	10	10	100	10.0	01.0	00.2	.	.	$\bullet^0 0-036 7^{45} 14^{45}, 18^{40} 24^1$	
15	8	10	050	10	08.3	09.2	01.1	.	.	$\bullet^0 20-0-0^{45}, 19^{50}, 24^1, \oplus^0 2-19^{45} 19^{50}$	
16	8	000	080	03	03.7	C9.6	C5.8	.	.	$\bullet^0 0-045 12^{55} 13^{45}, \oplus^0 12^{20} 12^{45}, \Delta^0 12^{20} 12^{45}$	
17	8	000	060	00	02.0	10.8	C4.3	.	.	$\Delta^0 3^{45} 6^{45} \oplus^0 11^{45} 13^{45}, \Delta^0 12^{20} 12^{45}$	
18	8	000	020	02	C1.3	C3.0	C1.6	.	.	$\Delta^0 2-0-10^{45} 15^{45} 21^i, \oplus^0 16^{20} 17^{45}, 21^{25} 22^1, \oplus^0 2-17^{55} 21^{45}$	
19	8	060	050	10R	07.0	08.4	.	.	.	$\Delta^0 5^{30} 8^{45}, \Delta^0 20^{30} 24^1$	
20	7	10	08	00	C6.0	03.1	38.3	.	.	$\Delta^0 2-0-0-9^i, 10^{45} 10^{45}, 24^1$	
21	7	020	050	10	05.7	10.9	.	.	.	$\Delta^0 2-0-0-9^i, 19^{45} 24^1$	
22	7	000	050	00	01.7	C1.7	.	.	.	$\Delta^0 2-0-0-9^i, R 16^{45} 16^{45}, \oplus^0 16^{52} 17^{45}, \oplus^0 22^{45} 24, \oplus^0 23^{45} 24$	
23	7	000	080	05	04.3	09.7	.	.	.	$\bullet^0 10-0-0^{45}, 17^{45} 11^{45}, \Delta^0 10-1^i, \oplus^0 2-0-0^{45}, 15^{45}, 15^{45}, R 16^{45} 16^{45}, F 15^{22} 15^{46}$	
24	8	10	060	07	C7.7	C3.2	C1.8	.	.		
25	7	100	060	00	C5.3	C6.9	12.6	.	.		
26	8	020	040	04	C3.2	12.8	C1.1	.	.	$\Delta^0 2-0-9^{50} 20^{30} 24$	
27	8	07	060	02	05.0	03.7	.	.	.	$\Delta^0 5-50 7^{30}, \oplus^0 6^{45} 6^{45}$	
28	8	100	05	09	C9.3	02.3	C0.0	.	.	$\bullet^0 16^{30} 17^{45}, 15^{45} 24^1, \oplus^0 16^{42} 16^{42}, \oplus^0 21^{40} 21^{40}, R 16^{40} 16^{40}, F_{WW-NW} 3^{45} 14^{45}, \oplus^0 14^{45} 16^{40}$	
29	8	100	080	10R	09.3	C1.8	C0.0	.	.		
30	6	100	100	06	08.7	00.9	43.8	.	.		
MES. VRED.		05.9	07.0	05.5	06.1	197.2	175.0				

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 $\varphi = 44^{\circ}48'$ N $\lambda = 20^{\circ}28'$ E Gr. $\Delta G = +1h\ 22\ min.$

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D DN	Vozdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost % %			Pravac i jačina vetro D, I (0-12)					
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21			
1	749.0	749.4	749.8	15.6	22.7	19.0	16.1	24.1	13.0	10.2	11.4	10.8	12.0	86	52	75	72	W	2	NNW	2	SW	1
2	752.7	754.5	754.0	17.6	20.2	16.6	17.8	21.7	16.6	12.6	11.6	11.0	11.6	77	62	62	74	N	2	NNW	2	SW	1
3	754.2	750.9	747.2	16.0	24.7	19.8	20.1	25.4	11.3	07.7	09.7	08.1	10.8	71	35	62	56	WSW	1	SSE	2	W	3
4	749.8	750.8	751.1	16.8	24.2	19.4	20.0	24.5	16.0	14.8	13.6	09.5	09.2	95	42	54	64	NNW	2	N	2	NNE	2
5	752.0	752.3	751.8	19.0	25.0	19.8	20.6	25.8	14.5	11.3	09.6	10.0	11.5	62	42	66	57	E	2	NNE	2	SE	1
6	750.7	749.0	747.0	20.1	29.9	23.6	24.3	31.0	16.4	12.3	11.2	15.2	15.3	63	46	70	60	SE	2	NNW	2	SSE	1
7	747.4	751.2	749.0	10.5	15.8	14.6	16.1	23.6	14.6	17.0	13.4	09.6	09.9	79	71	80	77	NW	3	NNW	3	NNW	2
8	751.4	750.8	751.9	13.6	20.8	16.0	16.6	21.3	10.8	08.7	09.5	08.6	07.5	82	47	55	61	NNW	2	NN	3	NNW	3
9	753.3	751.8	750.6	14.0	22.6	19.0	14.2	23.2	10.7	08.0	08.3	08.6	08.0	70	42	59	57	N	2	NNW	3	NNW	2
10	750.1	750.7	751.9	15.7	23.5	18.8	19.2	22.8	15.4	13.3	12.2	11.1	11.8	91	51	82	75	S	1	NNW	3	NNW	1
11	753.1	752.9	752.0	15.7	24.4	21.2	20.6	25.2	12.1	08.5	09.4	08.5	10.5	70	37	56	54	WSW	1	NW	2	SSE	1
12	751.6	750.7	751.1	20.0	29.8	23.2	24.0	31.0	16.0	13.0	12.2	12.0	15.0	69	38	70	59	ESE	2	NNW	2	ENE	1
13	751.0	750.0	748.9	22.5	32.5	26.2	26.8	32.8	19.0	16.1	14.9	13.9	15.9	73	38	62	59	-	0	SE	2	SE	2
14	749.3	748.4	747.3	25.1	31.6	24.0	27.7	34.4	21.0	16.0	13.1	10.6	15.2	55	27	60	47	SSE	2	NNW	2	SE	1
15	750.9	751.9	751.1	24.0	31.4	26.8	27.2	31.7	21.3	16.7	15.8	14.1	15.3	71	41	58	57	NNW	1	NW	1	NNF	2
16	751.9	750.3	749.4	19.8	19.6	25.0	25.4	31.1	17.8	16.3	12.0	14.5	15.1	75	46	60	60	W	1	NF	2	ESE	2
17	747.7	745.4	743.6	24.	23.3	28.5	28.9	34.9	22.7	19.0	16.3	16.5	16.1	72	46	62	60	SE	4	SE	3	SSE	2
18	742.9	752.9	745.4	26.	26.6	22.4	25.6	35.2	21.1	16.6	14.1	15.2	14.2	56	49	61	55	SE	1	NNW	4	NW	1
19	746.1	747.5	746.0	16.8	17.1	16.8	17.4	23.4	16.6	15.7	14.2	12.0	12.9	85	62	90	86	N	2	NNW	2	NNW	2
20	746.4	748.0	747.6	14.5	14.8	17.1	14.9	16.7	14.5	14.3	11.6	10.6	16.4	94	64	81	86	NNF	2	W	2	W	2
21	746.2	745.1	744.6	16.3	19.1	12.8	15.0	19.8	12.7	09.7	09.7	10.3	10.6	80	66	89	78	NNW	2	W	4	W	2
22	747.5	747.7	747.6	14.1	17.6	15.2	15.6	17.8	13.6	13.0	10.9	10.7	10.9	91	71	84	82	NNW	3	NNW	3	W	3
23	745.8	747.7	746.3	13.7	15.0	15.9	15.3	16.7	13.6	13.5	11.4	12.6	12.5	97	94	92	94	W	3	W	3	NNW	3
24	749.0	749.5	749.0	17.0	27.7	20.4	21.2	28.0	13.2	16.2	11.3	12.3	13.1	77	49	72	67	SE	1	NW	2	SE	2
25	742.6	747.6	751.8	21.0	29.5	16.5	21.5	30.0	16.8	12.9	11.9	11.1	11.2	57	36	78	57	SSE	1	S	2	N	2
26	754.5	754.0	754.0	14.8	21.8	16.8	17.6	22.7	14.2	13.9	11.3	09.6	10.0	90	49	65	65	W	2	NW	2	E	1
27	754.2	753.6	752.7	15.9	24.4	17.8	18.5	25.0	11.6	08.1	09.4	09.1	11.6	71	40	76	62	NNF	1	ESE	2	ESE	1
28	753.3	753.2	753.2	16.2	28.4	21.3	22.8	28.9	15.1	10.5	11.1	11.0	11.3	66	41	60	56	ESE	2	ESE	2	SE	1
29	754.5	754.6	754.7	15.7	29.7	21.6	23.2	30.2	16.7	12.0	12.9	12.0	12.8	75	39	66	60	SW	1	E	2	ESE	2
30	753.7	751.5	750.0	20.0	31.0	22.6	24.3	31.5	16.8	15.1	12.6	11.9	12.9	68	35	68	57	ENE	1	SE	2	ESE	1
31	749.5	749.4	749.6	21.5	31.3	23.2	24.8	31.8	16.6	17.3	12.7	11.9	14.9	66	35	70	57	NW	1	NF	2	E	1
MFS.	WRFD.	750.4	750.1	749.4	18.4	25.2	20.1	20.9	26.6	15.6	12.8	11.9	11.5	12.4	75	50	70	65	1.7	2.4	1.7	1.7	1.7

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BEDOGRAD

1	750.1	749.7	748.7	22.4	32.2	24.0	25.7	32.6	18.8	15.0	14.6	13.7	13.5	71	38	60	56	ESE	1	F	1	ESE	2
2	749.8	749.4	749.6	22.7	33.4	24.6	26.0	33.4	19.5	15.4	15.9	14.6	13.4	77	36	60	58	-	0	ESE	1	SE	2
3	750.6	750.6	750.7	22.8	34.2	24.6	27.0	34.3	19.8	15.9	14.8	14.4	13.7	67	38	58	54	SE	1	ESE	2	ESE	2
4	751.3	751.6	750.1	24.3	34.0	27.0	28.5	34.9	21.2	16.5	13.7	12.2	15.2	60	30	54	48	ESE	3	SE	2	SE	3
5	750.6	750.3	749.7	27.1	33.2	27.8	29.0	33.8	23.6	17.8	15.4	16.0	15.7	57	42	56	52	SE	1	NW	2	NL	2
6	751.7	754.2	754.0	21.8	25.8	19.6	21.2	27.8	19.6	14.0	12.0	11.1	09.6	61	50	56	56	NNW	2	NW	2	NNW	2
7	751.6	752.4	750.1	15.9	24.4	18.4	19.3	25.1	14.0	12.2	10.5	08.8	09.8	79	38	62	60	NNW	2	NNW	2	NNW	1
8	749.0	747.3	744.0	18.7	25.4	23.6	23.8	30.0	13.4	10.1	09.6	10.5	12.1	60	34	55	50	E	2	SE	2	SE	2
9	749.1	745.5	748.2	19.4	21.7	16.7	18.6	24.2	16.5	06.1	14.3	14.2	12.9	95	74	90	93	S	1	NN	3	W	3
10	750.6	749.7	747.5	16.7	24.4	19.2	19.0	25.2	14.4	12.7	11.2	09.4	11.6	76	41	70	63	W	2	NNW	1	ESE	2
11	744.0	742.4	746.1	17.9	19.6	14.6	16.7	20.2	14.6	12.0	11.3	12.0	11.2	74	76	90	78	SE	2	SE	1	W	2
12	746.7	747.2	748.4	14.2	15.0	14.2	14.4	17.1	12.8	12.5	09.2	11.0	11.4	76	86	94	85	NNW	3	NNW	4	W	2
13	751.2	752.3	753.4	14.3	22.4	17.6	18.1	23.6	13.6	13.4	10.2	11.0	11.4	81	54	75	70	W	2	NNW	2	W	1
14	754.4	7																					

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$$H_s = 132 \text{ m} \quad H_b = 132.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

1	E	000	020	C2	01.3	12.2	.	.	$\Delta^{+2} 0^{\circ} 8^{\text{35}} 20^{\text{15}} 24$
2	E	000	000	CC	00.0	12.2	.	.	$\Delta^{+1} 0^{\circ} 9^{\text{19}} 24$
3	E	000	000	CC	00.0	12.3	.	.	$\Delta^{+2} 0^{\circ} 8^{\text{35}} 20^{\text{15}} 24$
4	E	000	000	CC	00.0	12.6	.	.	$\Delta^{+0} 8^{\text{35}} F_{SE} 9^{\text{44}} 12^{\text{15}} 24$
5	E	000	010	00	02.3	10.9	.	.	.
6	E	070	C10	C2	02.7	09.9	.	.	$\Delta^{+3} -1^{\text{35}} 20^{\text{30}} 24$
7	E	000	010	CC	00.3	12.9	.	.	$\Delta^{+0} 0^{\circ} 9^{\text{05}} 23^{\text{25}} 23^{\text{45}} 15^{\circ} 23^{\text{45}} 24$
8	E	000	000	CC	00.0	12.7	.	.	$\Delta^{+0} 0^{\circ} 3^{\text{40}} 15^{\text{47}} 16^{\text{40}} 18^{\text{07}} 0^{\text{05}} 3^{\text{32}} 12^{\text{21}} 12^{\text{18}} 16^{\text{12}} 17^{\text{07}} \cdot 0^{\text{05}} 6^{\text{13}} 12^{\text{11}} 17^{\text{07}} 24$
9	E	10	10	10	10.0	03.3	12.6	.	$\Delta^{+2} 20^{\text{45}} 24$
10	E	040	030	00	02.3	11.0	03.8	.	.
11	E	060	10	10	0E.7	00.5	.	.	$\Delta^{+0} -4^{\text{30}} F_{SE-W} 3^{\text{42}} 4^{\text{42}} 18^{\text{18}} 2^{\text{31}} 0^{\text{09}} 18^{\text{24}} 12^{\text{34}} 22^{\text{13}} 18^{\text{12}} 24^{\text{17}}$
12	E	7	10	10	10	00.0	00.0	CP.7	$\bullet^{+1} 0^{\circ} 2^{\text{46}} 10^{\text{15}} 22^{\text{40}} \cdot F_{W-E} 6^{\text{42}} 17^{\text{04}}$
13	E	10	060	00	05.3	08.1	<u>17.4</u>	.	$\Delta^{+0} 20^{\text{13}} 24$
14	E	030	020	00	01.7	11.5	.	.	$\Delta^{+1} 0^{\circ} 0^{\text{00}} 20^{\text{30}} 24$
15	E	040	050	00	02.0	11.4	.	.	$\Delta^{+1} 0^{\circ} 0^{\text{00}} 19^{\text{45}} 24$
16	E	060	030	00	03.0	10.9	.	.	$\Delta^{+2} 0^{\circ} -9^{\text{30}} 24$
17	E	000	030	CC	01.0	11.8	.	.	$\Delta^{+1} 0^{\circ} 0^{\text{00}} 19^{\text{30}} 24$
18	E	000	000	00	00.0	12.1	.	.	$\Delta^{+0} -20^{\circ} 17^{\text{45}} 19^{\text{15}} 24 \cdot F_{SE} 11^{\text{02}} 12^{\text{46}}$
19	E	000	000	00	00.0	11.6	.	.	$\Delta^{+1} 0^{\circ} 0^{\text{00}} 19^{\text{45}} 24$
20	E	000	000	00	00.0	11.2	.	.	.
21	E	050	020	08	05.0	10.7	.	.	$\Delta^{+2} 0^{\circ} -7^{\text{15}}$
22	E	060	050	00	03.7	10.3	.	.	$\Delta^{+0} 0^{\circ} 0^{\text{26}} 4^{\text{30}}$
23	E	10R	000	09	06.3	06.3	00.0	.	$\Delta^{+2} 2^{\circ} 3^{\text{42}} 18^{\circ} 3^{\text{42}} 7^{\text{35}} 17^{\text{35}} 17^{\text{08}} \cdot 0^{\text{35}} 4^{\text{05}} 17^{\text{15}} 8^{\text{20}} 22^{\text{45}} 23^{\text{30}} \cdot 2^{\text{24}} 7^{\text{30}} 7^{\text{30}} 24^{\text{45}}$
24	E	060	09	05	06.7	06.6	12.2	.	$\Delta^{+2} 20^{\text{15}} 24$
25	E	050	020	06	04.3	10.4	.	.	$\Delta^{+0} -10^{\circ} 8^{\text{35}} 20^{\text{30}} 24$
26	E	030	000	C5	02.7	11.0	.	.	$\Delta^{+1} 0^{\circ} 17^{\text{30}}$
27	E	10	040	CC	07.7	06.7	00.4	.	$\Delta^{+0} 0^{\circ} 0^{\text{26}} \Delta^{+0} 22^{\text{30}} 24$
28	E	040	040	C4	04.0	10.8	.	.	$\Delta^{+0} 0^{\circ} 7^{\text{20}} 20^{\text{30}} 24 \cdot F_{SE} 9^{\text{32}} 16^{\text{30}}$
29	E	000	020	CC	00.7	10.8	.	.	$\Delta^{+0} 0^{\circ} 0^{\text{45}} F_{SE} 0^{\text{13}} 15^{\text{51}}$
30	E	080	060	10	08.0	03.5	.	.	$\Delta^{+2} 15^{\text{45}} 16^{\text{45}} 19^{\text{10}} 19^{\text{10}} 23^{\text{45}} 24$
31	E	010	020	00	01.0	11.2	03.1	.	$\Delta^{+0} 0^{\circ} 0^{\text{40}} \Delta^{+0} 20^{\text{30}} 24$

$\varphi = 44^{\circ}48'$ N $\lambda = 20^{\circ}28'$ E Gr. $\Delta G = +1\text{h }22\text{ min.}$

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S 8	Vazdušni pritisak P mm			Temperatura vazduha T C°						Napon vodenih parova e mm			Relativna vlažnost v%			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	750.3	749.8	749.6	17.5	20.5	21.4	21.8	27.7	15.4	11.1	09.5	09.1	10.6	63	35	55	51	SE	2	ESE	2	SE	2
2	749.3	749.5	750.3	19.6	27.8	19.4	21.6	29.0	17.0	13.1	10.6	13.5	16.8	62	48	94	68	SE	2	W	2	WSW	2
3	710.1	749.5	749.3	19.7	28.1	23.7	23.4	29.7	17.1	14.4	14.4	11.9	12.9	89	42	59	63	-	0	WSW	1	ESE	2
4	748.3	742.2	750.8	21.5	29.5	16.6	21.1	30.2	16.6	17.4	13.1	13.9	13.1	68	45	92	68	ESE	2	ESE	2	N	4
5	754.2	753.6	752.6	13.6	21.0	15.4	16.4	21.6	12.5	10.8	10.0	10.3	11.6	85	55	90	77	W	2	NNW	2	ESE	1
6	749.9	746.4	743.9	14.5	24.7	19.8	19.7	25.8	11.7	05.0	11.0	10.7	11.7	89	46	6E	68	ESE	2	ESE	3	SE	3
7	741.7	742.6	745.0	16.6	23.3	17.7	19.8	23.3	15.7	14.3	10.9	12.0	11.8	77	56	78	70	SE	4	ESE	3	S	2
8	749.6	751.7	754.0	15.0	22.8	19.2	18.6	23.3	14.0	12.5	11.7	13.2	13.6	92	64	88	81	WSW	2	W	2	W	1
9	755.7	755.3	753.8	16.5	26.2	19.4	20.4	26.6	14.1	11.4	12.0	11.5	11.6	92	45	70	69	-	0	E	1	ESE	2
10	753.8	753.7	754.9	20.1	28.6	22.0	23.2	29.0	18.7	14.2	12.7	12.9	15.6	72	44	79	65	SE	2	NNW	1	N	2
11	759.0	759.1	758.7	13.6	17.4	15.6	15.6	22.0	13.4	12.4	10.2	10.9	11.3	87	73	85	82	W	2	NW	2	WSW	2
12	758.2	757.2	756.2	16.6	23.7	19.0	19.6	24.3	15.4	11.9	11.5	12.0	09.7	81	55	59	65	ESE	1	SE	3	ESE	3
13	755.6	754.6	756.4	15.4	25.4	17.5	19.2	25.7	14.2	11.0	09.4	13.1	13.5	72	54	88	71	ESE	1	NNW	2	SW	1
14	754.9	754.0	751.7	15.4	24.7	18.6	19.3	25.1	14.5	11.5	12.6	12.6	13.2	96	54	82	77	SW	1	NW	2	W	1
15	752.0	751.7	751.9	17.0	25.4	19.8	20.5	26.0	15.6	12.6	12.3	12.1	12.4	85	50	72	69	WSW	2	N	2	NNE	2
16	754.0	754.6	755.5	14.5	21.2	16.6	17.0	22.5	14.0	11.9	11.1	11.5	09.5	90	58	70	73	N	2	ESE	2	SE	2
17	755.9	754.5	753.9	12.3	23.8	17.7	18.1	23.8	13.2	11.2	04.1	05.7	04.4	71	44	55	57	ESE	4	SE	3	SE	3
18	753.6	752.8	752.6	16.3	25.0	17.9	18.2	25.2	15.2	12.8	07.8	10.2	08.0	56	43	52	50	SE	3	SF	2	SSE	2
19	752.8	752.0	751.0	16.2	24.0	16.2	18.2	24.8	15.4	12.6	09.1	11.7	12.0	56	52	87	68	SE	2	NE	2	ENE	2
20	749.9	747.7	746.7	16.4	26.5	20.0	20.8	27.0	13.6	10.0	04.3	04.6	08.2	66	33	47	49	SF	2	SE	3	SE	3
21	748.7	746.1	746.0	17.4	22.6	18.0	19.0	22.7	17.3	15.0	06.2	10.5	11.8	55	51	76	61	SE	2	SSE	2	SF	2
22	746.6	747.1	746.3	18.1	24.7	19.5	18.6	25.1	15.2	11.7	12.3	12.0	12.5	79	51	95	75	SSE	3	SSW	2	SE	1
23	743.4	742.7	742.6	16.2	19.0	15.4	16.5	20.0	15.2	12.1	13.0	13.7	11.7	94	83	89	89	-	0	W	2	WNW	2
24	746.4	744.1	742.6	15.2	25.7	20.4	20.4	26.6	14.0	11.0	11.3	10.5	08.8	87	42	49	59	ESE	2	SW	2	SSE	3
25	739.6	739.4	738.8	16.5	14.5	11.8	13.6	20.6	11.8	14.3	11.0	11.1	09.6	78	90	92	87	SE	3	W	3	SSE	1
26	734.7	733.1	733.4	11.4	13.0	09.5	10.8	14.8	08.9	05.8	04.0	10.5	08.6	89	92	96	93	ESE	2	ESF	1	NW	3
27	740.2	740.5	751.0	09.0	15.6	09.6	11.0	15.7	08.8	07.5	07.1	04.4	06.6	83	48	74	68	W	3	NW	3	W	2
28	750.5	748.1	747.6	06.9	20.2	12.0	12.8	20.6	05.5	02.2	06.7	07.6	08.9	91	43	84	73	SE	1	W	2	SE	2
29	746.6	747.1	748.0	11.4	24.1	19.1	18.5	25.6	10.0	05.5	08.2	07.8	10.2	50	35	62	59	SE	1	SW	1	SE	2
30	747.3	747.9	749.6	16.4	19.5	12.2	15.1	25.6	12.2	11.9	04.4	11.6	09.9	67	68	93	76	SE	3	W	2	NW	2
MES.	NRFD.	750.0	749.1	750.1	15.6	23.2	17.2	18.3	24.3	13.9	11.4	10.5	11.1	11.1	79	53	76	69	1.5	2.1	2.0	2.0	2.0

1974. OKTOBAR

BEOGRAD

1	749.0	749.8	750.6	11.0	12.2	10.9	11.2	13.6	10.7	10.5	09.5	09.8	09.3	97	92	95	95	NNE	1	NW	1	WSW	1
2	750.6	747.5	744.4	07.7	12.2	12.6	11.4	13.2	07.5	06.1	07.2	08.2	09.8	91	77	88	85	SW	1	E	2	SSE	3
3	750.9	753.5	753.5	07.2	14.0	09.3	10.0	07.1	07.0	06.8	06.5	07.1	89	55	81	75	WSW	4	W	2	SL	3	
4	752.3	751.7	751.5	08.8	21.0	12.7	13.8	21.0	07.6	02.8	06.6	05.5	08.8	78	30	80	63	FSE	2	S	2	SE	2
5	750.3	749.9	749.0	09.1	18.7	10.2	10.0	12.4	08.5	05.7	08.4	08.7	09.7	98	91	93	94	SSE	1	WNW	2	W	2
6	746.4	747.8	751.7	09.5	24.5	07.6	08.3	10.2	07.6	09.5	08.7	07.9	06.9	98	95	88	94	SW	2	WSW	3	W	2
7	750.2	747.0	744.7	06.5	10.0	09.6	08.9	10.6	05.2	02.3	06.9	07.4	08.4	94	60	94	89	ESE	1	ESE	2	ESE	2
8	743.4	741.9	745.8	09.4	17.4	11.1	12.2	17.6	08.8	05.3	08.6	10.7	09.4	98	72	95	88	ESE	2	ESE	2	SSE	2
9	746.6	747.1	748.6	09.9	15.4	10.2	11.2	15.6	06.8	02.6	08.0	08.6	08.9	94	65	95	85	SE	1	WNW	2	SE	2
10	750.7	752.2	753.1	08.3	13.5	07.0	09.0	14.1	07.0	03.7	07.7	06.8	07.1	94	55	95	83	WSW	2	W	2	SF	1
11	752.6	751.8	752.4	06.3	17.6	11.5	11.7	18.4	04.5	00.7	06.9	07.6	07.5	96	50	73	73	ESE	2	SE	2	ESE	3
12	752.8	751.5	749.7	10.1	18.7	15.0	14.7	19.2	06.0	03.6	07.3	08.1	06.4	79	50	66	65	ESE	2	ESE	3	ESE	3
13	748.0	748.4	750.2	13.7	14.0	08.2	11.0	15.7	08.0	12.0	10.9	11.4	07.9	93	95	97	95	ESE	3	ESE	3	WNW	2
14	748.7	749.3	750.7	07.2	09.1	07.4	09.2	07.2	07.0	07.4	07.5	07.4	97	86	96	93	WNW	2	W	2	WSW	2	
15	750.1	749.1	746.0	06.2	09.2	07.8	07.8	10.0	06.2	05.8</td													

PP. ST. 173

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vlажност 0-9	Облачност N (0-10)					Изолација брз салі	Падавина R mm	Снеžни покривач h cm	Развој времена			
		14	7	14	21	Сред Dies				7	7	w	
1	8	050	050	09	07.7	06.7	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} F_{SE} 8^{\circ} 14^{\circ} 6^{\circ} 10 \cdot 19^{\circ} 22^{\circ} 23^{\circ}$			
2	8	C7	020	10•R	06.3	07.4	00.0	.	.	$\Delta^{+2} 0 \cdot 20^{\circ} 20^{\circ} 8^{\circ} 20^{\circ} 20^{\circ} 20^{\circ} 20^{\circ} 21^{\circ}$			
3	8	000	080	00	02.7	09.4	08.6	.	.	$\Delta^{+2} 0 \cdot 13^{\circ} 9^{\circ} 20^{\circ} 24$			
4	8	050	010	10•R	05.3	08.0	.	.	.	$\Delta^{+2} 0 \cdot 6^{\circ} 0^{\circ} 9^{\circ} 17 \cdot 17^{\circ} 22^{\circ} 22^{\circ} 24^{\circ} F_{SE} 0 \cdot 2^{\circ} 17^{\circ} 22^{\circ} F_{NW} 1^{\circ} 2^{\circ} 2^{\circ}$			
5	7	010	050	00	02.0	11.6	25.0	.	.	$F_{WW} 0^{\circ} \Delta^{+2} 0 \cdot 14^{\circ} 24$			
6	8	000	000	00	00.0	11.5	.	.	.	$\Delta^{+2} 0 \cdot 10^{\circ} F_{SE} 11^{\circ} 12^{\circ} 18^{\circ} 24^{\circ}$			
7	8	C9	050	00	04.7	06.2	.	.	.	$F_{SE} 0 \cdot 14^{\circ} 13^{\circ} 2^{\circ} 20^{\circ} \Delta^{+2} 0^{\circ} 19^{\circ} 24$			
8	7	10	060	00	05.3	05.9	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 19^{\circ} 24$			
9	7	000	050	01	02.0	10.8	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} 18^{\circ} 24 = 0 \cdot 130 10^{\circ} 45$			
10	7	000	060	03	04.7	07.8	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} F_{NW} 2^{\circ} 4^{\circ}$			
11	7	09	10	00	06.3	00.5	11.6	.	.	$\Delta^{+2} 0 \cdot 0^{\circ} 0^{\circ} 0^{\circ} 45^{\circ} 3^{\circ} 30^{\circ} 2^{\circ} 45^{\circ} F_{SE} 0 \cdot 35^{\circ} 3^{\circ} 0^{\circ} 24^{\circ} 24^{\circ} 24^{\circ}$			
12	7	10	040	00	04.7	05.1	.	.	.	$\Delta^{+2} 0 \cdot 8^{\circ} 18^{\circ} 24$			
13	8	000	010	00	00.3	10.0	.	.	.	$\Delta^{+2} 0 \cdot 20 \cdot 0^{\circ} 19^{\circ} 24$			
14	8	000	050	00	01.7	00.7	.	.	.	$\Delta^{+2} 0 \cdot 15^{\circ} 19^{\circ} 24 = 0 \cdot 15^{\circ} 10^{\circ} 30^{\circ}$			
15	7	000	040	00	01.3	01.8	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 0^{\circ}$			
16	7	000	040	00	01.3	00.3	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 0^{\circ} = 0 \cdot 13^{\circ} 13^{\circ}$			
17	7	000	000	00	00.0	05.6	.	.	.	$\Delta^{+2} 0 \cdot 30^{\circ} 30^{\circ} F_{SE} 3^{\circ} 3^{\circ} 12^{\circ} 18^{\circ} 21^{\circ} 0^{\circ}$			
18	8	06	030	05	04.7	07.0	.	.	.	$F_{SE} 6^{\circ} 0^{\circ} 0^{\circ}$			
19	8	04	040	03	03.7	06.5	.	.	.	$\Delta^{+2} 0 \cdot 18^{\circ} 0^{\circ} 0^{\circ}$			
20	8	05	020	09	05.3	07.3	.	.	.	$\Delta^{+2} 0 \cdot 7^{\circ} F_{SE} - SE 1^{\circ} 10^{\circ} 13^{\circ} 16^{\circ} 10^{\circ} 23^{\circ} 14^{\circ} 21^{\circ} 0^{\circ}$			
21	8	07	10	00	05.7	00.0	.	.	.	$\Delta^{+2} 0 \cdot 0^{\circ} 20^{\circ} 24$			
22	8	10	10	07	09.0	01.9	00.0	.	.	$\Delta^{+2} 0 \cdot 4^{\circ} 45^{\circ} 0^{\circ} 45^{\circ} 30^{\circ} F_{SE} 15^{\circ} 15^{\circ} F_{WW} 15^{\circ} 16^{\circ} 16^{\circ} 16^{\circ} 0^{\circ} 0^{\circ}$			
23	8	10	10	• 10	10.0	00.0	C5.4	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 10^{\circ} 15^{\circ} 13^{\circ} 24^{\circ}$			
24	7	050	060	08	05.3	08.2	00.0	.	.	$\Delta^{+2} 0 \cdot 30^{\circ} 30^{\circ} = 0 \cdot 45^{\circ} 6^{\circ} 0^{\circ}$			
25	7	10	10	• 10	10.0	00.1	C1.4	.	.	$\Delta^{+2} 0 \cdot 45^{\circ} 6^{\circ} 0^{\circ} 45^{\circ} 15^{\circ} 0^{\circ} F_{SE} 4^{\circ} 35^{\circ} 7^{\circ} 0^{\circ} 10^{\circ} 23^{\circ} 0^{\circ}$			
26	7	07	10	• 10	09.0	01.1	C3.4	.	.	$\Delta^{+2} 0 \cdot 11^{\circ} 23^{\circ} F_{N-NW} 16^{\circ} 23^{\circ} 6^{\circ} F_{NW} 16^{\circ} 18^{\circ} 18^{\circ}$			
27	7	10	060	00	05.3	10.6	<u>39.4</u>	.	.	$F_{WW} - NW 1^{\circ} 15^{\circ} 0^{\circ} 45^{\circ} 13^{\circ} 0^{\circ} F_{NW} 8^{\circ} 13^{\circ} 0^{\circ} \Delta^{+2} 0^{\circ} 19^{\circ} 24$			
28	8	000	000	00	00.0	10.6	.	.	.	$\Delta^{+2} 0 \cdot 9^{\circ} 15^{\circ} 18^{\circ} 22^{\circ}$			
29	8	000	040	05	04.3	09.5	.	.	.	$\Delta^{+2} 0 \cdot 20 \cdot 0^{\circ} 19^{\circ} 24$			
30	8	040	080	10	07.3	07.7	.	.	.	$\Delta^{+2} 0 \cdot 7^{\circ} 0^{\circ} 17^{\circ} 45^{\circ} 21^{\circ} F_{WW} 18^{\circ} 0^{\circ}$			

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1	7	10•	10	09	05.7	00.0	13.5	.	
2	7	060	10	10•	08.7	00.6	04.5	.	$\bullet 2^{\circ} 19^{\text{m}} 30^{\text{s}}$
3	7	10	C10	C2	04.3	05.9	08.4	.	$= 0^{\circ} 5^{\text{m}} 46^{\text{s}}$
4	8	06	020	05	04.3	07.9	.	.	$\bullet 0^{\circ} 1^{\text{m}} 23^{\text{s}}$
5	5	050	10	10	08.3	00.0	.	.	$\bullet 0^{\circ} 1^{\text{m}} 48^{\text{s}}$
6	6	10•	10•	10	10.0	00.0	C2.0	.	$= 0^{\circ} 0^{\text{m}} 18^{\text{s}}$
7	6	10	1C	1C	10.0	00.0	C2.7	.	$= 0^{\circ} 0^{\text{m}} 20^{\text{s}}$
8	7	10	10•	10	10.0	00.0	C2.5	.	$= 0^{\circ} 0^{\text{m}} 13^{\text{s}}$
9	8	070	020	09	06.0	06.0	02.3	.	$= 0^{\circ} 0^{\text{m}} 09^{\text{s}}$
10	8	060	040	00	03.3	07.0	C4.7	.	$= 0^{\circ} 0^{\text{m}} 07^{\text{s}}$
11	8	040	0C0	CC	01.3	09.4	00.0	.	$\bullet 0^{\circ} 0^{\text{m}} 02^{\text{s}}$
12	8	030	060	08	C5.7	04.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
13	7	10•	10•	1C	10.0	00.0	C2.5	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
14	6	10•	1C	1C	10.0	00.0	27.4	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
15	7	1C	10	10•	10.0	00.2	10.0	.	$= 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
16	7	09	1C	10	C5.7	04.1	20.2	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
17	8	000	030	01	01.3	08.9	03.5	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
18	8	00	0C0	00	0C.0	09.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
19	8	00	000	05	01.7	09.4	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
20	8	C5	1C	CC	08.0	04.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
21	7	10	10•	10	10.0	00.0	02.2	.	$F_{SE-W} 0^{\circ} 18^{\text{m}} 02^{\text{s}}$
22	8	C9	1C	10	09.7	02.8	C8.5	.	$= 0^{\circ} 0^{\text{m}} 44^{\text{s}}$
23	6	10•	10•	10•	10.0	00.0	C8.5	.	$= 0^{\circ} 0^{\text{m}} 13^{\text{s}}$
24	8	08	040	10	07.3	07.8	20.5	.	$= 0^{\circ} 0^{\text{m}} 34^{\text{s}}$
25	7	10	0C	00	06.3	02.5	00.0	.	$= 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
26	7	040	10•	10•	08.0	01.7	.	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
27	7	02	080	00	03.3	08.1	04.7	.	$\bullet 0^{\circ} 0^{\text{m}} 19^{\text{s}}$
28	8	05	060	05	05.3	05.0	.	.	$\bullet 0^{\circ} 0^{\text{m}} 10^{\text{s}}$
29	7	10•	10	10	10.0	00.0	C0.7	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
30	5	10*	10•	10•	10.0	00.0	16.8	03	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$
31	7	00	10•	10	06.7	00.0	C7.2	.	$\bullet 0^{\circ} 0^{\text{m}} 00^{\text{s}}$

$\varphi = 44^{\circ}48'$ N $\lambda = 20^{\circ}28'$ E Gr. $\Delta G = +1h\ 22\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih parova e mm			Relativna vlažnost u %				Pravac i jačina vetrova D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	741.9	743.4	747.0	04.9	04.9	04.0	04.4	07.0	03.5	04.4	06.3	04.8	05.2	97	74	85	85	NNE	2	NNW	3	W	3
2	740.2	748.2	749.0	04.0	10.4	06.7	07.0	11.2	03.1	00.9	04.7	03.6	04.8	78	39	66	61	W	3	W	3	WSW	2
3	750.5	751.9	753.1	05.2	09.1	06.0	06.6	10.2	04.3	-00.5	05.1	04.7	04.9	77	54	70	67	W	3	NNW	3	W	1
4	752.8	751.7	751.8	03.4	12.8	09.6	08.8	13.6	02.0	-03.0	04.8	05.0	06.1	82	45	68	65	SE	2	E	1	ESE	2
5	752.1	752.9	754.8	07.5	15.2	09.8	10.6	15.3	06.5	02.4	05.3	04.6	05.1	68	37	56	54	ESE	3	SE	3	SE	3
6	757.2	757.3	758.2	05.6	10.8	06.3	07.2	11.5	05.4	03.0	06.5	06.8	06.7	96	71	93	87	NNW	1	NNW	1	WSW	1
7	758.1	756.3	755.5	05.4	09.5	08.2	07.8	09.7	05.2	02.0	06.5	07.1	07.4	97	80	91	89	-	0	NNE	2	SE	2
8	753.6	753.9	755.0	05.4	04.6	05.0	05.0	08.2	04.6	05.2	06.5	06.2	06.4	97	97	97	97	NNE	2	NNE	3	NNW	1
9	755.1	755.5	756.2	04.4	05.4	05.2	05.6	04.4	04.2	05.9	05.8	06.2	94	86	92	91	NW	1	NW	2	SW	1	
10	756.0	756.0	756.0	05.1	09.8	06.8	07.1	09.8	04.4	03.2	06.2	06.2	06.3	94	68	85	82	SSE	2	SE	2	ESE	2
11	755.8	756.0	756.2	03.5	07.6	03.2	04.4	08.5	03.1	00.8	05.3	06.1	05.7	91	78	98	89	ESE	2	WSW	2	-	0
12	752.7	754.0	753.3	01.5	04.6	05.5	04.3	05.7	01.5	04.1	05.0	06.0	06.4	98	94	94	95	-	0	NNW	1	ESE	2
13	753.3	744.0	755.4	02.8	14.6	06.5	07.6	15.5	01.5	-01.3	05.3	06.2	06.8	95	50	93	79	-	0	NNW	2	SW	1
14	755.7	755.3	756.6	04.6	14.7	09.4	09.5	16.0	04.4	-00.2	06.1	07.1	06.5	96	56	74	75	SF	1	NNE	1	ESE	2
15	755.0	755.5	756.6	06.4	09.4	10.4	16.7	06.3	03.5	06.2	06.6	06.7	86	47	76	70	SE	3	ESE	2	SE	3	
16	754.7	753.3	754.0	07.3	18.4	11.4	12.1	18.4	07.3	04.8	06.1	07.6	06.6	79	48	65	64	ESE	3	SE	3	SE	3
17	756.0	756.5	756.2	06.9	15.1	10.6	10.8	16.2	06.9	00.7	06.7	06.8	07.2	95	53	75	72	-	0	NNE	1	ESE	1
18	755.5	754.5	753.4	07.1	11.8	11.8	11.8	16.8	06.6	-00.4	06.1	07.5	06.4	80	52	63	65	SE	1	-	0	ESE	2
19	750.7	747.3	751.4	08.2	17.5	10.6	11.7	17.7	06.0	04.2	05.7	06.0	06.8	70	40	72	61	ESF	3	NNW	2	-	0
20	756.3	755.7	755.7	07.1	10.4	08.9	07.6	10.8	06.0	03.1	06.4	05.2	06.5	90	55	87	77	WSW	1	ESE	2	ESE	2
21	754.2	753.9	754.3	04.9	11.1	06.5	07.4	11.1	04.5	00.4	05.7	06.7	07.0	88	68	93	83	ESE	2	-	0	W	1
22	754.6	744.1	753.9	06.0	09.6	06.1	07.0	10.1	04.4	04.4	06.4	06.8	06.6	92	76	93	87	NNW	1	NNW	1	SE	1
23	753.9	753.5	753.1	04.4	09.2	04.0	07.4	10.0	03.7	00.0	06.0	07.1	07.3	96	82	91	90	-	0	NW	1	-	0
24	753.0	753.8	754.8	07.2	07.5	03.8	05.6	08.2	03.8	05.2	06.5	05.8	06.7	86	74	79	80	ESE	2	ESF	3	SE	3
25	753.1	750.8	748.1	03.8	09.0	06.4	05.4	09.2	03.1	01.7	04.5	05.8	06.3	75	67	78	77	SE	5	SE	4	SE	4
26	746.5	748.6	746.3	07.2	C6.0	04.2	05.4	07.7	04.1	04.2	07.2	06.2	05.6	95	89	90	91	SSW	2	WSW	2	SSW	2
27	745.0	746.0	747.5	07.4	06.2	04.0	04.2	07.2	01.9	-02.0	04.7	05.0	05.8	87	70	95	84	SE	2	NW	2	WSW	2
28	739.3	736.0	731.6	02.8	10.4	01.0	03.8	11.8	01.0	-01.5	05.0	06.1	04.7	89	65	93	83	SE	2	NNW	3	-	0
29	739.4	740.7	742.1	01.2	C6.8	07.3	03.6	07.5	02.5	-00.5	04.7	04.6	04.1	95	62	71	76	SW	2	S	2	SE	2
30	747.3	749.8	752.0	00.9	07.1	02.4	03.2	07.8	00.5	-00.3	04.3	04.6	04.4	88	61	81	77	SSW	2	WSW	2	SE	2
MES.	VRED.			752.0	751.9	752.4	04.9	10.4	06.6	07.1	11.1	04.1	01.6	C5.7	06.0	06.0	88	65	82	78	1.8	2.0	1.9

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1	750.8	752.4	755.9	02.1	C8.6	06.1	05.7	08.8	01.5	-04.2	03.8	03.8	04.8	71	45	68	61	SE	2	SSW	2	NNW	2
2	754.2	756.9	758.7	06.4	08.0	06.7	07.0	08.1	06.0	C2.6	05.2	06.1	06.6	72	76	89	79	NW	2	WSW	3	W	2
3	749.6	750.7	750.3	06.6	08.8	08.6	08.2	08.8	06.2	05.6	07.1	07.4	07.6	97	88	91	92	W	2	WSW	2	-	0
4	758.7	757.2	755.2	07.4	05.0	06.9	07.6	10.2	06.9	05.6	07.0	07.4	07.3	91	86	97	91	WNW	2	NW	1	ESE	1
5	751.2	750.2	750.8	06.2	07.9	06.9	07.0	08.2	05.5	01.6	07.0	07.3	05.4	97	92	72	87	SF	2	-	0	N	2
6	751.5	751.6	752.0	02.8	05.6	02.4	03.3	07.5	01.4	C2.2	05.4	04.6	04.0	97	67	74	79	WSW	2	W	2	SSE	1
7	751.2	748.8	749.0	02.4	04.4	05.7	04.6	05.7	01.7	-00.9	05.1	05.9	06.5	94	94	94	94	SSW	2	WSW	3	NNW	2
8	746.4	745.8	747.8	05.6	06.1	07.8	06.8	07.8	05.1	04.2	06.2	06.8	07.0	91	96	88	83	SSE	1	WSW	2	NNW	2
9	752.5	753.6	755.7	02.4	04.2	02.0	02.6	07.8	01.5	01.0	04.6	04.6	04.7	84	75	88	82	N	1	NNE	1	ESE	2
10	755.5	754.4	753.9	01.2	08.0	03.8	04.2	08.1	01.0	-02.8	04.3	05.7	04.2	86	71	70	76	SE	2	ESE	3	SÉ	3
11	754.5	751.2	746.8	03.4	04.5	08.6	06.8	08.6	01.0	02.4	05.8	06.2	05.3	98	85	63	82	SSW	1	ESE	1	ESE	3
12	743.9	747.1	746.8	06.9	C3.1	01.4	03.2	08.6	01.1	05.0	05.1	04.9	04.8	68	86	95	83	ESE	3	N	2	W	2
13	742.0	742.7	745.8	01.1	01.0	01.2	01.1	02.4	01.0	00.6	04.8	04.7	04.5	97	95	90	94	WSW	2	WSW	2	W	2
14	750.3	750.5	751.4	01.2	00.8	00.3	00.6	01.4	01.0	00.5	04.6	04.4	04.5	91	90	96	92	NW	2	NNW	3	W	2
15	750.5	750.4	750.8	-00.3	-00.3	-00.7	-00.6																

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$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijeme O. 9	Oblačnost N (0-10)					Instalacija broj seti	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10•	10	07	09.0	CC.C	05.E	.	• ⁰⁻¹² 10 ¹⁵ E _{NW} 9 ¹³ 20 ⁰⁰	
2	8	10	01•	06	05.7	07.3	07.E	.	F _{w-wNW} 10 ¹³ 12-14 ⁴⁵	
3	8	09	05	04	07.3	02.4	.	.	F _{WW} 9 ⁰⁵ 15 ⁰⁴ , \sqcup 23 ⁰⁰ 24	
4	8	06	07•	06	06.3	05.1	.	.	\sqcup 0-7 ³⁰ F _{EE} 6 ¹⁴ 14 ²⁴ , 21 ²⁴	
5	8	05	07•	09	07.0	04.3	.	.	Δ ⁰⁻²⁰ 7 ⁴⁵ F _{EE} 6 ¹⁴ 14 ²⁴ , 21 ²⁴	
6	5	06	06	02	04.7	01.1	.	.	F _{SE} 0-0 ⁴⁵ \sqcup 0-6 ⁴⁵ 8 ¹⁵ 19 ³⁰ 24, \sqcup 0-2 6 ⁴⁵ 24, \equiv 0-2 6 ⁴⁵ 10 ³⁰	
7	5	09	10	10•	09.7	CC.C	.	.	Δ 0-6 ³⁰ \sqcup 0-6 ³⁰ 10 ³⁰ 24, \equiv 0-6 ³⁰ 10 ³⁰ 24	
8	5	10•	10•	10•	10.0	00.0	11.E	.	• ⁰⁻¹⁰ 24	
9	6	10	10	10	10.C	00.C	09.4	.	• ⁰⁻⁴ 45 \equiv 0-4 20 24, 9 ⁰⁹ 16 11 ⁴⁵	
10	7	10	07	04	07.0	CC.7	00.0	.	\equiv 0-4 0-11 ⁴⁵ 17 ³⁰ 24, \sqcup 21 ³⁰ 24	
11	7	00	03•	10	04.3	06.5	.	.	\equiv 0-10-8 ⁴⁵ \equiv 0-0-9 ⁴⁵ F _{SE} 1 ¹³ 24, \equiv 21 ³⁰ 24	
12	2	10	00	00	00	C3.3	01.6	.	\equiv 0-2 ³⁰ 6 ³⁰ 14 ⁴⁵ \equiv 2 ³⁰ 6 ³⁰ 19 ⁴⁵ , \sqcup 4 ⁴⁵ 7 ⁴⁵ 18 ³⁰ 24	
13	6	04	02	00	02.0	02.0	06.8	.	\sqcup 0-8 ⁴⁵ 22 ¹⁵ 24, \equiv 0-5 ¹⁵ 19 ⁴⁵ , \equiv 6 ³⁰ 7 ⁴⁵ , Δ 19 ⁴⁵ 23 ³⁰	
14	5	00	00	00	00.0	CC.0	08.3	.	\sqcup 10 ³⁰ 19 ⁴⁵ 24, Δ 0-17 ³⁰ 24	
15	6	00	00	00	00.0	CC.0	08.3	.	Δ 0-8 ⁴⁵ 19 ⁴⁵ 24	
16	8	00	00	00	00.0	CC.0	08.3	.	Δ 0-10-3 ⁴⁵ 21 ³⁰ 24	
17	6	05	04	00	03.0	C3.0	.	.	Δ 0-10 ³⁰ 18 ⁴⁵ 24, \equiv 0-4 ³⁰ 20 ⁴⁵	
18	5	03	03	00	02.0	C2.0	06.3	.	Δ 0-10 ³⁰ 18 ⁴⁵ 24, \equiv 0-4 ³⁰ 20 ⁴⁵	
19	8	03	05	00	10•	C6.0	02.9	.	Δ 0-19 ⁴⁵ 24	
20	7	08	00	00	02.7	C2.7	05.7	01.8	.	
21	8	03	1C	1C	C7.7	01.7	.	.	Δ 0-10-9 ⁴⁵ 20 ¹⁵ 22 ³⁰ , \sqcup 0-6 ⁴⁵ 8, \equiv 22 ³⁰ 23 ³⁰	
22	7	09	04	00	04.3	C5.6	00.0	.	Δ 0-18 ³⁰ 24	
23	5	07	10	10	05.0	00.0	.	.	\equiv 0-5 ³⁰ 12 ⁴⁵ 30 ⁰⁰ , F _{ESE} 9 ⁴⁵ , 12 ⁴⁵ 22 ³² , F _{SE} 22 ⁴² -24	
24	7	10	1C	08	09.3	C0.1	00.0	.	F _{SE} 0-10 ³⁰ 6 ⁴⁵ 9 ³⁰ , F _{SE} 1 ⁰⁰ 24, \equiv 0-4 ³⁰ 22 ³⁰	
25	7	04	10	10•	08.0	00.2	.	.		
26	7	1C•	10•	08	09.7	CC.C	05.7	.	F _{SE} 0-7 ³⁰ , \equiv 1 ¹⁵ 9 ¹⁵ 12 ⁴⁵ 18 ⁰⁰	
27	8	05	10	10	08.3	00.0	02.9	.	\sqcup 1-8 ³⁰ , \equiv 0-14 ³⁰ 18 ⁰⁰	
28	6	04	10	1C*	08.C	CC.4	C2.C	.	\sqcup 3-8 ³⁰ , F _{SE} 8 ⁴⁵ 7 ²⁵ , 15 ³⁰ 21 ⁴⁵ , \equiv 0-17 ³⁰ 22 ⁴⁵ , \equiv 0-19 ³⁰ 24, \boxed{x}	
29	8	08	06	05	06.3	05.8	16.0	01	* $0-20$ 24, \equiv 0 ³⁰ 0 ³⁰ , \boxed{x}	
30	8	06	01	00	02.3	C2.3	06.5	.	\sqcup 2 ¹⁵ 9 ⁴⁵	
MES.					06.1	05.8	05.3	05.8	96.4	63.0

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1	8	C9	10	07	08.7	00.7	.	.	\sqcup 0-4 ³⁰ 9 ¹⁰	
2	7	1C•	1C	10	10.C	00.C	00.0	.	• ⁰⁻⁵ 45 10 ⁴⁵ , 12 ⁴⁵ 16 ⁴⁵	
3	6	10•	10	10	10.0	00.C	00.P	.	\equiv 0-2 ³⁰ 7 ³⁰ , 16 ³⁰ 17 ³⁰ , \equiv 0-15-24	
4	7	10	10	09	05.7	CC.C	CC.1	.	\equiv 0-18 ³⁰ 23 ⁴⁵ , \equiv 0-18 ³⁰ 23 ⁴⁵ , \equiv 0-23 ¹⁵ 24	
5	5	04	05	10•	06.3	01.3	.	.	\equiv 0-0 ³⁰ , \equiv 0-0 ³⁰ 14 ⁴⁵ , 10 ⁴⁵ , 12 ⁴⁵ , \equiv 0-3 ⁴⁵ 19 ⁴⁵ , \equiv 0-19 ⁴⁵ 24, F _N 21 ⁴⁵ 21 ⁴⁵	
6	8	1C	04	05	06.3	C3.4	05.1	.	* ⁰⁻² 15, \equiv 3 ³⁰ 6 ³⁰ , F _w 11 ⁵⁰ , \sqcup 20 ⁴⁵ 24	
7	7	10	10•	10•	10.0	00.C	00.8	.	\sqcup 0-0-0-0, \equiv 0-0 ³⁰ 14 ⁴⁵ , 10 ⁴⁵ 24, F _{MSW} 12 ⁴⁵ 12 ⁴⁵	
8	6	10•	10•	10	10.C	00.C	C8.4	.	* ⁰⁻¹ 0-17 ⁴⁵ , 21 ⁴⁵ 21 ⁴⁵ , F _{WW} 12 ⁴⁵ 15 ⁰³ 16 ⁰³	
9	6	10	09	09	05.3	00.0	13.4	.	\equiv 0-19 ³⁰ 16 ³⁰ , \equiv 0-19 ³⁰ 16 ³⁰	
10	7	00	00	02	00.7	07.5	.	.	\sqcup 0-1 ³⁰ 9 ⁴⁵	
11	6	10	08	09	09.0	01.4	.	.	\equiv 1-2 ⁴⁵ 3 ³⁰ 11 ¹⁵ 17 ³⁰ , \equiv 0-13 ³⁰ 17 ¹⁵ , \equiv 17 ⁴⁵ 11 ⁴⁵ , \equiv 0-7 ³⁰ 10 ⁴⁵	
12	7	1C	1C	10	10.C	00.C	00.C	.	\equiv 0-4 ⁵ 5 ¹⁵ , \equiv 14 ³⁰ 17 ³⁰ , 20 ⁴⁵ 24, F _{ESE} 4 ⁴⁵ 5 ³⁴ , \equiv 0-6 ³⁰ 8 ³⁰ , \equiv 0-17 ³⁰ 20 ⁴⁵	
13	6	10	10	10	10.0	00.C	01.9	.	\equiv 0-2 ³⁰ 3 ³⁰ 7 ¹⁵ , \equiv 07 ¹⁵ 10 ⁴⁵ , \equiv 12 ⁴⁵ 20 ⁴⁵	
14	6	10	1C*	1C*	10.C	00.C	00.C	.	* ⁰⁻¹ 7 ⁴⁵ , 24 ¹⁵ , F _{WW} 11 ³⁰ 15 ⁴⁵ , \boxed{x}	
15	5	1C*	10*	10*	1C.0	00.C	21.C	16	* ⁰⁻¹⁰ 24, \boxed{x}	
16	7	1C*	10	10	1C.0	00.C	22.5	26	* ⁰⁻⁹ 15, \boxed{x}	
17	7	00	09	10	06.3	05.3	00.4	20	* ⁰⁻¹⁸ 45 3 ³⁰ , \equiv 15 ⁴⁵ 22 ³⁰ , \boxed{x}	
18	6	10	10•	04	08.0	00.C	.	15	\equiv 0-2 ³⁰ 3 ³⁰ 10, \equiv 03 ⁴⁵ 5 ³⁰ , * ⁰⁹ 30 11 ⁵⁰ , \boxed{x}	
19	7	07	07	10	08.0	02.8	07.C	12	\equiv 01 ³⁰ 29 ³⁰ , \boxed{x}	
20	6	10	10	05	08.3	01.1	00.0	11		
21	7	03	09	00	04.0	00.7	.	787	\boxed{x}	
22	7	03	00	00	01.0	C7.3	.	06	\sqcup 1-2 ⁴⁵ 9 ³⁰ , \equiv 0-2 ³⁰ 3 ³⁰ , 17 ⁴⁵ , \equiv 0-2 17 ⁴⁵ 18 ⁴⁵ , \equiv 2 ¹⁸ 45 24, \boxed{x}	
23	4	00	00	10	03.3	05.5	.	04	\equiv 0-18 ³⁰ 10 ⁴⁵ , 24, * ¹³ 45, \equiv 01 ³⁰ 18 ⁴⁵ , \equiv 2 ¹⁸ 45 24, \boxed{x}	
24	2	10	10	10	10.0	00.0	.	04	V ⁰⁻¹¹ , \equiv 0-20-24, \boxed{x}	
25	5	00	10	04	04.7	00.5	CC.C	04	\equiv 0-6 ⁴⁵ V ^{0-2³⁰ 8} , * ⁰²¹ 45, \boxed{x}	
26	7	02	10	09	07.0	01.9	.	04	* ⁰⁻³ 45 10 ⁴⁵ , \boxed{x}	
27	7	09	05	06	06.7	04.2	CC.1	02	\boxed{x}	
28	7	07	05	10	07.3	05.9	02.2	-	\boxed{x}	
29	7	10	09	00	06.3	01.3	.	.	* ⁰⁻⁸ 45 14 ⁴⁵	
30	7	10	10	05	08.3	00.C	02.5	.	* ⁰⁻¹⁴ 45 9 ⁰⁰ , 12 ⁵⁰ 14 ⁰⁵ , F _{WW} 10 ⁵⁵ 17 ¹⁵	
31	7	10	09	00	06.3	CC.6	CC.0	.		
MES.					07.5	08.0	07.2	07.6	51.8	90.2

$\varphi = 42^{\circ}26'$, $N \lambda = 19^{\circ}17'$, E Gr. $\Delta G = +1h\ 17\ min.$

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E D	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21		
1	761.5	760.6	761.5	07.9	09.6	09.6	09.2	09.6	07.3	05.9	07.7	08.9	08.7	96	98	98	97	-	0	-	C - C	
2	761.0	760.7	760.7	08.9	10.3	09.7	09.6	10.6	08.4	07.6	08.1	09.0	08.8	95	95	98	96	-	0	S - 2	- 0	
3	760.5	760.3	762.1	08.5	10.8	08.8	09.2	12.0	08.4	07.8	07.5	07.3	07.6	90	75	90	85	-	0	-	C NE 1	
4	763.6	763.1	765.0	07.0	09.5	05.8	08.3	15.0	05.8	05.1	07.3	09.7	06.7	97	70	97	88	-	0	SSW 1	- 0	
5	764.8	763.7	764.0	02.8	11.4	05.0	06.0	11.8	02.5	00.0	05.4	07.1	06.3	97	70	96	88	-	0	-	C - 0	
6	762.0	759.8	758.7	06.0	09.1	07.4	07.5	09.3	04.6	02.6	06.3	07.3	07.0	90	84	91	88	-	0	-	0 - 0	
7	758.9	759.6	760.9	07.2	09.1	06.7	07.4	09.5	06.1	06.2	07.4	08.1	07.3	97	94	99	97	NNE 1	-	C - 0	- 0	
8	760.9	760.3	761.2	04.2	07.9	03.6	04.8	08.0	02.9	01.0	06.0	06.7	05.7	97	63	95	92	ESE 1	-	0 - 0	- 0	
9	762.0	761.8	761.8	-00.2	09.8	02.7	03.8	10.3	-00.2	-01.9	04.3	04.5	05.1	95	50	92	79	-	0	WSW 1	- 0	
10	758.4	757.5	759.2	03.8	06.0	05.7	05.3	06.0	02.4	00.0	05.7	06.7	06.6	95	96	96	96	-	0	-	0 - 0	
11	761.3	762.7	765.7	05.5	11.2	04.4	06.4	11.3	04.0	03.6	06.5	07.3	05.7	96	73	91	87	N 1	S 2	- 0	- 0	
12	766.1	764.6	765.0	00.5	11.9	08.8	07.5	12.3	00.4	-01.5	04.7	06.5	04.3	98	62	50	70	-	0	SSW 2	NNE 3	
13	763.7	762.2	763.9	07.6	11.0	06.0	07.6	11.6	06.0	05.2	03.1	03.5	02.9	40	36	41	39	NE 4	NE 6	ENE 5	- 0	
14	764.6	763.8	764.4	03.0	10.2	01.4	04.0	10.2	01.0	-00.3	03.3	04.7	04.3	57	51	85	64	ENE 3	-	0 - 0	- 0	
15	764.9	763.9	764.1	-01.7	09.4	00.9	02.4	09.7	-02.1	-04.7	03.6	03.4	04.3	89	38	88	72	-	0	SSE 2	SSW 1	
16	764.8	763.9	763.7	-00.2	08.8	04.2	04.2	10.4	-00.8	-03.1	04.2	04.5	04.9	93	54	79	75	-	0	SW 2	- 0	
17	761.8	760.2	757.6	-00.4	04.5	04.4	03.2	05.1	-00.5	-03.0	04.1	04.8	05.9	93	77	94	88	-	0	C NNE 3	- 0	
18	758.8	758.5	759.6	07.2	10.2	02.4	05.6	10.6	02.3	03.8	04.3	03.9	04.1	57	42	74	58	N 2	ENE 5	NNF 2	- 0	
19	759.8	759.6	760.1	06.5	11.2	04.3	06.6	11.2	02.0	-02.0	03.4	04.0	04.3	47	40	69	52	NE 6	NE 5	- 0	- 0	
20	758.7	767.9	759.7	01.8	10.4	11.4	08.8	12.4	01.0	-01.6	04.5	05.3	05.8	87	56	58	67	-	0	ENE 5	- 0	
21	760.4	760.8	762.6	10.7	14.2	10.2	11.3	14.5	09.0	-01.8	04.4	04.4	03.9	45	36	42	41	NE 5	NE 6	NE 4	- 0	
22	763.7	763.2	763.7	03.5	14.5	04.9	07.0	14.6	03.0	00.0	04.7	06.2	04.7	80	50	73	68	-	0	SSW 2	- 0	
23	764.8	764.0	762.1	00.9	08.7	06.4	05.5	12.6	00.6	-02.6	04.6	06.2	06.0	95	75	84	85	-	0	S 2	- 0	
24	760.6	760.3	761.0	08.8	13.6	05.5	08.4	13.7	05.2	04.6	04.8	04.7	05.0	57	40	74	57	NE 5	ENE 6	FNE 3	- 0	
25	760.7	760.0	760.2	00.9	08.4	04.8	04.7	10.2	00.4	-02.8	03.9	04.1	05.4	79	46	84	71	-	0	S 1	- 0	
26	761.8	761.2	762.1	00.1	12.7	03.2	04.8	12.7	-00.2	-02.8	04.4	05.7	04.7	95	52	81	76	-	0	SSW 2	- 0	
27	761.8	759.9	760.1	01.4	12.4	05.6	06.3	12.7	01.0	-02.4	03.9	04.7	05.6	77	43	82	67	-	0	S 2	- 0	
28	759.9	759.7	760.8	02.8	12.8	08.0	07.9	13.4	02.5	-00.7	04.7	06.1	04.8	84	55	59	66	-	0	S 2	SSW 3	
29	761.8	761.4	762.8	01.9	13.9	03.6	05.7	13.9	01.0	-02.3	04.2	05.9	05.1	80	50	86	72	-	0	SW 2	- 0	
30	764.8	764.3	765.6	01.8	14.3	03.8	05.9	14.3	01.2	-02.0	04.4	06.3	05.1	85	51	85	74	-	0	SW 2	- 0	
31	766.9	766.5	766.7	03.0	12.4	03.6	05.6	12.8	01.9	-01.8	04.4	04.7	05.0	78	44	85	69	-	0	WSW 1	- 0	
MES.	VRED.	762.1	761.8	762.1	03.9	10.8	05.6	06.5	11.4	02.8	00.5	05.0	05.0	05.5	83	61	81	75	0.9	1.8	1.0	

1	765.8	765.0	764.3	05.4	11.0	08.0	08.1	13.1	03.0	-00.7	05.3	06.2	04.6	79	66	82	76	-	0	SW 2	- 0
2	764.7	764.8	764.1	06.0	10.4	07.8	08.0	11.0	03.5	01.0	06.0	07.3	06.7	86	77	85	83	-	0	C -	0
3	763.6	762.1	760.0	06.7	09.6	08.2	08.2	11.2	05.6	03.0	06.7	08.2	08.1	91	90	99	93	-	0	C E	2
4	756.1	754.0	753.1	08.2	12.2	07.8	09.0	13.6	07.5	01.5	07.4	06.2	06.4	91	58	81	77	SSE 5	5	5	0
5	754.3	753.0	751.5	05.5	09.8	07.1	07.4	10.5	05.5	04.3	06.2	06.3	06.9	92	70	91	84	-	0	WSW 2	- 0
6	749.5	747.9	747.7	06.9	09.0	10.2	09.0	10.6	06.5	00.8	07.2	08.2	08.4	97	94	90	94	-	0	C S	6
7	736.0	738.0	741.7	09.5	09.2	05.6	07.5	12.0	05.0	03.0	07.8	07.6	06.4	87	87	94	89	NW 2	W 2	- 0	
8	747.0	752.2	757.4	04.4	09.3	06.4	06.6	10.7	02.5	00.1	03.4	02.8	02.2	54	32	31	39	N 2	NE 6	NE 3	
9	761.4	761.9	763.7	02.4	11.6	04.8	05.9	12.2	02.1	-01.8	03.8	04.4	04.2	70	43	66	60	NE 6	S 3	- 0	
10	763.4	762.0	762.3	02.2	12.2	04.6	06.0	13.5	01.6	-01.5	03.7	04.9	05.2	70	46	81	66	-	0	SSE 4	- 0
11	761.5	759.5	758.8	02.4	13.8	05.0	06.6	14.0	02.2	-01.1	04.7	05.1	05.9	87	43	90	73	E 1	SSW 3	- 0	
12	757.5	755.0	754.1	02.3	14.7	06.9	07.7	15.1	02.2	-00.7	05.1	07.1	05.7	93	57	76	75	E 1	SS 2	- 0	
13	752.4	751.2	750.3	06.6	10.4	08.6	08.6	10.6	04.2	01.2	06.3	07.5	07.4	86	79	89	85	-	0	NF 2	- 0
14	748.6	751.4	751.2	07.6	08.4	08.0	08.1	10.3	07.4	06.2	07.2	06.6	07.0	92	78	87	86	ENE 2	NNE 2	NF 4	
15	751.0	750.3	750.9	08.0	15.7	09.2	10.5	16.4	07.5	05.9	07.6	08.9	08.3	95	67	95	86	N 3	S 1	- 0	
16	751.3	751.1	753.1</td																		

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrijednost O	Oblačnost N (0-10)					Insolascija broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	7	10	10	10•	10.0	00.C	05.5	.	• ⁰⁻¹⁴ ₁₄₋₂₀		
2	7	10•	10•	10	10.0	00.C	03.8	.	• ⁰ _n 19-25		
3	8	10	10	10	10.0	00.4	04.8	.	• ⁰ _n 5-14-20		
4	8	10	020	00	04.0	05.6	03.5	.	• ⁰ _n 24-24		
5	8	00	06	02	02.7	03.5	.	.	• ⁰ _n 24-18-20		
6	8	10	10	10	10.0	00.C	00.4	.	• ⁰ _n 5-14-20		
7	7	10•	10•	08	08	09.3	02.8	.	• ⁰ _n 24-14-20		
8	7	10	10	00	06.7	00.0	00.7	.	• ⁰ _n 5-14-20		
9	8	04	04	04	05.3	04.5	.	.	• ⁰ _n 24-14-20		
10	6	10•	10•	10•	10.0	00.C	01.2	.	• ⁰ _n 18-20-23		
11	8	10	040	00	04.7	03.2	17.4	.	• ⁰ _n 24-14-20		
12	8	02	030	00	01.7	06.3	.	.	• ⁰ _n 8-14-20		
13	8	00	020	00	00.7	08.3	.	.	• ⁰ _n 8-14-20		
14	8	00	010	00	00.3	07.7	.	.	• ⁰ _n 8-14-20		
15	8	05	000	00	01.7	07.6	.	.	• ⁰ _n 8-14-20		
16	8	10	10	00	06.7	02.3	.	.	• ⁰ _n 8-14-20		
17	7	03	10	10•	07.7	00.C	.	.	• ⁰ _n 24-14-20		
18	8	02	040	02	07.7	07.8	06.3	.	• ⁰ _n 8-14-20		
19	8	02	030	01	02.0	08.6	.	.	• ⁰ _n 8-14-20		
20	8	08	070	02	05.7	03.7	.	.	• ⁰ _n 8-14-20		
21	8	02	020	00	01.3	08.6	.	.	• ⁰ _n 8-14-20		
22	8	C1	000	00	00.3	08.8	.	.	• ⁰ _n 8-14-20		
23	8	C1	05	10•	06.7	04.0	.	.	• ⁰ _n 8-14-20		
24	8	04	01	00	01.7	08.4	00.6	.	• ⁰ _n 8-14-20		
25	8	07	07	10	08.0	04.7	.	.	• ⁰ _n 8-14-20		
26	8	00	000	00	00.0	08.6	.	.	• ⁰ _n 8-14-20		
27	8	C7	C30	10	06.7	07.6	.	.	• ⁰ _n 8-14-20		
28	8	C3	070	00	03.3	07.6	.	.	• ⁰ _n 8-14-20		
29	8	00	000	CC	00.0	05.1	.	.	• ⁰ _n 8-14-20		
30	8	01	060	00	02.3	08.6	.	.	• ⁰ _n 8-14-20		
31	8	08	070	00	05.0	07.1	.	.	• ⁰ _n 8-14-20		
MES.	VRED.	05.2	05.5	03.5	04.7	154.2	47.0				

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1	8	08	060	09	07.7	03.1	.	.	• ⁰ _n 12-13		
2	8	10	10	10	10.0	00.5	.	.	• ⁰ _n 12-24		
3	7	10	10•	10•	10.0	00.C	00.1	.	• ⁰ _n 12-24		
4	8	10•	R	08	10•	09.3	00.0	17.2	.	• ⁰ _n 12-24	
5	8	10	10	10	10.0	01.5	34.6	.	• ⁰ _n 12-24		
6	7	10•	10	10•	10.0	00.C	02.7	.	• ⁰ _n 12-24		
7	7	10•	10	08	09.3	00.2	52.6	.	• ⁰ _n 12-24		
8	8	10	070	00	05.7	05.5	10.5	.	• ⁰ _n 12-24		
9	8	00	01	00	00.3	09.5	.	.	• ⁰ _n 12-24		
10	8	04	000	00	01.3	09.5	.	.	• ⁰ _n 12-24		
11	8	00	000	00	00.0	09.5	.	.	• ⁰ _n 12-24		
12	8	02	000	00	00.7	09.8	.	.	• ⁰ _n 12-24		
13	8	10•	10	10•	10.0	00.3	.	.	• ⁰ _n 12-24		
14	8	10	10	07	09.0	00.4	07.5	.	• ⁰ _n 12-24		
15	8	10•	080	00	06.0	03.9	08.7	.	• ⁰ _n 12-24		
16	8	04	03	07	04.7	09.5	01.4	.	• ⁰ _n 12-24		
17	8	04	040	05	04.3	08.7	.	.	• ⁰ _n 12-24		
18	8	08	10	10	05.3	01.9	.	.	• ⁰ _n 12-24		
19	8	10	06	10	05.3	03.7	07.5	.	• ⁰ _n 12-24		
20	8	09	08	03	06.7	05.0	.	.	• ⁰ _n 12-24		
21	8	05	09	08	07.3	06.4	.	.	• ⁰ _n 12-24		
22	8	10	10	10•	10.0	00.C	.	.	• ⁰ _n 12-24		
23	8	10	070	07	08.0	03.2	08.3	.	• ⁰ _n 12-24		
24	8	C5	080	03	05.3	06.6	.	.	• ⁰ _n 12-24		
25	8	08	050	07	06.7	04.8	.	.	• ⁰ _n 12-24		
26	8	08	070	10	08.3	03.6	.	.	• ⁰ _n 12-24		
27	8	02	00	00	00.7	09.7	.	.	• ⁰ _n 12-24		
28	8	00	030	00	01.0	09.7	.	.	• ⁰ _n 12-24		
MES.	VRED.	07.0	06.5	05.8	06.5	126.9	151.5				

$\varphi = 42^{\circ}26'$, N $\lambda = 19^{\circ}17'$ E Gr. $\Delta G = +1h\ 17\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)							
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	758.6	756.8	756.2	01.6	12.2	05.2	06.0	13.7	01.4	-02.0	04.1	04.3	04.6	80	40	72	64	-	0	NW 3	-	0		
2	755.6	754.0	753.5	01.0	11.0	07.6	07.2	12.1	01.1	-02.8	04.4	05.9	07.4	85	56	95	79	-	0	SW 1	-	0		
3	756.0	758.2	760.3	06.2	13.0	07.0	08.3	13.4	06.0	-00.8	06.8	05.5	06.5	96	49	87	77	-	0	S 2	-	0		
4	761.5	750.3	760.8	05.6	11.3	07.6	08.0	11.5	05.0	02.0	06.1	07.0	07.6	89	70	97	85	-	0	-	0	-	0	
5	757.7	755.3	752.9	07.8	09.8	09.1	09.0	10.0	07.5	06.0	07.6	08.4	08.3	96	95	96	96	-	0	NNW 1	NNW 2	-	0	
6	752.6	753.3	753.8	07.8	09.3	08.0	08.4	10.7	07.5	01.5	07.1	07.6	07.6	90	83	94	89	-	0	-	0	NNE 2	-	0
7	754.8	755.2	757.1	06.0	10.3	07.4	07.8	11.5	05.9	05.2	06.2	05.9	03.5	89	62	45	65	-	0	SW 2	NE 4	-	0	
8	757.0	758.0	759.0	06.0	06.8	04.6	05.5	04.6	04.5	04.4	04.8	06.0	06.0	69	81	94	81	-	0	S 3	NN 1	-	0	
9	759.2	760.2	760.9	04.4	08.0	06.0	06.1	08.3	04.0	03.5	04.3	06.0	06.5	93	75	93	87	N	1	N 2	2	-	0	
10	759.8	757.9	759.4	03.8	14.5	08.4	08.8	15.0	01.5	-00.6	05.3	05.0	05.7	88	40	63	66	N	7	SW 3	-	0		
11	760.8	760.8	762.6	03.2	14.5	10.2	09.1	15.0	02.3	-00.5	05.3	05.0	05.0	92	48	51	58	-	0	SW 4	13	-	0	
12	763.3	762.4	762.4	08.2	14.0	04.4	08.0	16.2	04.2	00.0	03.0	03.4	03.0	88	45	81	81	3	3	3	3	-	0	
13	760.5	756.0	754.1	02.4	14.8	06.2	07.4	15.3	01.6	-01.4	05.0	05.1	05.6	92	40	78	70	-	0	SW 2	-	0		
14	750.8	746.5	746.0	03.8	18.0	13.4	12.2	18.4	03.0	-00.2	05.1	04.5	04.0	85	42	35	54	-	0	S 5	2	-	0	
15	745.2	745.8	748.0	10.0	12.0	09.8	10.4	14.8	05.8	08.5	04.0	04.2	04.1	44	40	46	43	N	4	NE 5	5	-	0	
16	749.5	749.6	751.0	08.6	14.0	10.1	10.7	14.6	06.5	06.6	05.1	04.4	07.2	51	52	78	66	NNE 2	55W 4	-	0			
17	753.2	754.1	756.9	06.8	16.4	05.4	10.5	16.6	04.5	00.7	02.3	07.1	08.2	85	51	93	76	N	3	S 5	4	-	0	
18	759.3	759.6	760.6	06.2	18.2	10.4	11.3	18.9	05.2	01.7	06.5	06.2	06.8	92	40	72	69	-	0	S 4	6	-	0	
19	761.9	761.7	762.0	08.0	19.7	10.9	12.3	20.2	06.5	02.0	06.3	09.3	08.4	78	56	67	73	ESE 2	53	3	-	0		
20	763.1	761.9	762.2	07.9	22.0	11.7	13.3	22.5	05.4	01.2	06.4	08.4	07.7	90	42	75	66	-	0	S 3	3	-	0	
21	762.5	760.0	760.7	07.8	24.8	12.6	14.4	25.0	05.4	00.9	06.0	06.6	05.7	76	28	51	52	-	0	S 2	-	0		
22	760.5	758.8	759.0	10.0	25.0	15.6	16.9	26.0	07.6	02.7	06.6	07.5	09.0	72	70	67	56	-	0	SW 2	-	0		
23	759.5	758.5	759.6	10.2	23.1	13.3	15.0	23.4	09.2	04.9	08.1	08.7	09.5	97	41	83	70	-	0	SSW 2	-	0		
24	760.2	758.7	758.5	09.4	23.6	15.8	16.2	24.0	07.3	03.3	07.8	07.2	08.6	88	34	64	62	-	0	S 5	2	-	0	
25	759.0	758.6	758.3	11.0	20.6	14.2	15.2	22.5	10.1	05.5	08.4	08.7	08.9	80	48	74	67	-	0	-	0	-	0	
26	759.0	756.6	756.7	14.0	22.8	14.6	16.5	23.2	11.4	05.9	07.4	05.4	04.6	62	45	77	61	N	4	55W 4	-	0		
27	755.9	754.3	754.5	11.6	21.0	14.6	15.4	21.3	10.0	06.3	04.7	04.5	04.2	94	51	74	73	-	0	NNW 3	-	0		
28	756.0	755.0	757.1	10.8	21.8	15.2	15.8	22.0	08.7	04.0	05.1	04.9	04.3	94	45	72	67	-	0	SW 3	-	0		
29	758.8	757.6	756.6	12.2	22.3	15.4	16.5	23.0	09.7	04.4	06.2	09.0	09.5	77	45	70	64	-	0	SW 4	-	0		
30	760.0	758.5	759.2	13.8	20.8	15.4	16.4	21.5	12.3	08.0	07.8	08.6	08.3	56	47	64	59	NE 2	5	1	-	0		
31	758.7	756.2	756.0	12.0	16.2	12.6	13.4	17.4	10.0	06.0	09.2	09.1	10.1	88	66	82	82	-	0	SW 3	1	-	0	
MES.	VRED.	757.7	756.8	757.3	07.6	16.6	10.6	11.4	17.3	06.4	02.8	06.4	07.0	07.2	81	51	75	69	0.7	2.4	1.0	-	-	0

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1	754.3	753.3	754.5	10.7	19.0	14.6	14.7	20.4	10.3	05.7	08.5	08.0	08.5	88	48	68	68	-	0	NN 2	13	-	0
2	756.1	757.2	756.3	12.8	18.4	13.6	14.6	19.4	12.0	10.0	08.8	08.4	09.2	80	53	73	71	NE 2	S 1	NE 1	-	0	
3	759.8	759.2	759.3	12.3	18.6	13.4	14.4	20.2	12.0	08.5	08.1	07.2	09.7	75	45	94	66	-	0	SW 4	4	-	0
4	757.9	756.0	756.4	13.3	19.4	12.3	14.3	20.0	10.3	05.7	08.0	08.0	08.3	53	53	77	61	NNE 3	S 5	6	-	0	
5	756.4	756.8	760.0	10.0	17.4	12.2	13.0	17.8	05.5	05.5	08.3	06.6	08.7	90	45	81	72	N	3	S 6	-	0	
6	754.7	753.1	754.6	10.4	18.0	14.4	14.3	20.0	07.0	03.0	04.8	04.3	07.0	72	41	51	57	N	1	SW 1	-	0	
7	755.9	754.3	755.5	13.6	19.4	16.0	16.4	21.2	17.1	04.8	05.5	06.3	05.3	47	36	34	41	NE 4	NE 5	4	-	0	
8	754.3	754.0	754.7	10.8	18.0	12.6	13.6	19.5	05.8	03.0	06.0	05.9	04.7	63	37	43	48	-	0	NE 4	5	-	0
9	756.3	756.0	757.1	11.4	19.0	14.4	14.8	19.4	08.6	03.0	05.1	04.2	04.8	53	31	39	41	NF 2	NE 4	4	-	0	
10	759.1	755.7	755.5	11.8	18.8	12.3	13.8	19.3	08.0	02.1	06.0	06.4	08.5	58	39	72	59	-	0	SSW 4	-	0	-
11	751.7	751.0	750.0	10.8	13.4	12.3	12.2	15.2	10.8	06.2	08.9	08.6	08.3	92	75	77	81	-	0	S 1	NN 2	-	0
12	749.5	750.1	750.1	11.5	12.0	11.9	11.8	13.7	11.0	09.5	08.9	09.6	09.4	88	91	90	90	FNE 1	-	0	EE 1	-	0
13	751.2	751.8	750.7	11.2	15.7	13.6	13.5	18.2	08.9	05.6	09.7	11.4	10.2	98	85	87	90	-	0	SSW 4	NDE 2	-	0
14	745.8	743.8	744.7	12.6	12.4	10.6	11.6	19.8	10.5	08.0	09.7	09.1	09.4	85	84	98	91	-	0	W 4	5	-	0
15	743.																						

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$$H_s = 49 \text{ m} \quad H_b = 50.6 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

Dan	Vidljivost 0-9	Oblačnost N (0-10)					Insolacia broj sadi	Padavina R mm	Snežni pokrívac h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	8	04	020	00	02.0	09.8	.	.	— ⁰ n-8	
2	8	040	08	10.	07.2	04.7	.	.	— ² n-8 ²⁵	• 17 ⁴⁵ 24
3	8	080	040	05	05.7	07.7	06.2	.	• ⁰ o-4, ¹ 20 ⁴⁵ 21 ⁵⁰	
4	8	10	10	10.	10.0	00.0	.	.	• ⁰ 14 ⁵⁰ 24	
5	8	100	100	100	00.0	14.7	.	.	• ⁰ 10-24	
6	8	100	10	100	10.0	00.7	28. ¹	.	• ⁰ 0-0 ²⁰ 14 ⁴⁰ 24	
7	8	10	10	10	10.0	00.1	08.7	.	• ⁰ 0-0-5	
8	8	10	10	100	10.0	00.6	.	.	• ⁰ 15 ¹² 24	
9	8	100	00	07	05.7	00.0	06.8	.	• ⁰ 0-10 ⁰⁵	
10	8	10	060	04	06.7	06.6	03.8	.	— ² n-8	
11	8	02	020	00	00.2	10.7	.	.	— ¹ 2n-9	FNE 18 ⁴⁰ 21 ¹⁰
12	8	BBB	BBB	BB	BB	18.2	18.7	.	— ¹ 2n-75 ⁰	
13	8	000	000	00	00.0	10.7	.	.	— ¹ 2n-9	
14	8	10	080	00	06.0	06.8	.	.	FNE 18 ⁰⁵ 24	
15	8	10	10	10	10.0	00.0	.	.	FNE 0-24	
16	8	10	05	05	06.7	05.0	.	.	— ¹ 2n-2 ¹⁰	
17	8	000	000	00	00.0	10.2	.	.	— ¹ 2n-74 ⁵	
18	8	040	000	00	01.3	10.4	.	.	— ¹ 2n-9	
19	8	01	000	00	00.3	10.9	.	.	— ¹ 2n-8	
20	8	060	060	00	04.0	09.3	.	.	— ¹ 2n-8	
21	8	030	050	00	02.7	11.2	.	.	— ¹ 2n-73 ⁰	
22	8	000	000	00	00.0	10.5	.	.	— ¹ 2n-73 ⁰	
23	8	020	040	00	02.0	09.5	.	.	— ¹ 2n-72 ⁰	
24	8	000	000	02	00.7	10.7	.	.	— ¹ 2n-71 ⁰	
25	8	06	10	00	05.3	02.7	.	.	— ¹ 2n-73 ⁰	
26	8	040	070	06	05.7	09.0	.	.	— ¹ 2n-73 ⁰	
27	8	06	030	02	03.7	09.1	.	.	— ¹ 2n-72 ⁰	FSEW 11 ²⁸
28	8	000	030	00	01.0	10.7	.	.	— ¹ 2n-72 ⁰	
29	8	000	060	02	04.7	10.2	.	.	— ¹ 2n-73 ⁰	
30	8	10	10	08	09.3	01.6	.	.	• ⁰ 10 ⁴⁰ 15 ³⁰	
31	8	10	10	10	10.0	01.0	.	.	— ¹ 2n-73 ⁰	
MES.	VREF	05-4	05-1	04-1	04-8	200-7	68-C			

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1	8	C6	OF	07	C7.0	02.3	CC.6	.	
2	8	1C	CPO	10	C9.3	C2.2	CC.C	.	
3	8	10	O8	C6	OP.0	03.5	00.6	.	
4	8	07	O6O	04	C5.7	C9.C	00.3	.	
5	8	10	O9O	02	C7.0	02.4	C3.8	.	
6	8	C7	1C	1C	C9.C	05.4	.	.	$\Delta^{\circ}n-8$
7	8	00	06	05	C3.7	09.3	.	.	FNE 10-1042
8	8	03O	03O	0C	C2.0	06.4	.	.	FNE 10-2450
9	8	06	01O	CC	C2.3	11.2	.	.	FNE 830-1725
10	9	02O	1C	10	C7.3	07.0	.	.	
11	7	10•	10	09	C9.7	00.0	00.6	.	
12	7	1C	10•	1C	1C.C	00.0	00.4	.	
13	8	03O	10	09	07.3	03.6	13.4	.	
14	7	09	10•	10•	09.7	02.2	01.2	.	
15	8	10	1C	1C	1C.C	05.3	1C.7	.	
16	7	10•	10•	10	1C.C	00.0	16.6	.	
17	7	10•	10•	10	1C.C	0C.1	42.C	.	
18	7	10•	10•	10	1C.C	01.0	24.3	.	
19	8	02O	1C	C3	05.C	08.2	C6.2	.	
20	8	00O	01O	00	00.3	12.4	.	.	$\Delta^{\circ}20-24$
21	8	C6O	03O	00	03.0	11.4	.	.	
22	8	10	OF	00	06.C	03.4	.	.	$\Delta^{\circ}0-530$
23	8	00O	01O	00	00.3	10.7	.	.	FNE 14.25-14.35
24	8	C2O	C4O	07	04.3	09.8	.	.	FNE 14.35-14.35
25	7	10	1C•	10•	10.C	00.C	.	.	
26	7	C4O	07O	00	03.7	05.3	06.8	.	
27	8	C4O	06O	06	C5.3	09.9	01.6	.	
28	8	10	1C	10	10.0	00.0	.	.	
29	8	C5O	02	00	02.3	10.3	21.5	.	
30	8	06O	10	10•	OP.7	05.2	.	.	
MES.									
VREF.		C6-4	C7-4	C5-9	06-6	159.3	150.6		

$\varphi = 42^{\circ}26'$, $N \lambda = 19^{\circ}17'$, E Gr. $\Delta G = +1h\ 17\ min.$

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D e n	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost v %				Pravac i jačina vjetra D, f (0-12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	741.6	741.3	742.1	11.0	11.2	10.6	10.8	17.4	10.3	09.3	09.3	09.7	08.9	94	98	93	95	S	7	7	5
2	745.6	748.0	749.5	11.2	11.0	13.0	13.0	15.4	10.0	09.5	08.9	09.6	10.0	90	75	89	85	-	0	0	0
3	752.6	753.8	754.8	12.4	17.4	13.9	14.4	17.6	12.0	11.2	09.7	09.0	07.2	90	61	60	70	-	0	SSW	3
4	753.7	753.0	750.7	13.0	12.6	12.2	12.5	14.5	11.0	07.8	08.2	09.5	09.8	73	87	92	84	NW	1	SSF	6
5	750.7	751.0	750.9	12.0	15.4	12.2	13.0	16.3	10.5	09.0	09.7	09.3	08.8	92	71	92	85	-	0	N	1
6	752.7	754.0	755.5	10.4	17.6	13.4	13.7	18.1	09.9	08.6	08.9	09.1	09.9	94	60	86	80	NE	1	SSW	4
7	757.7	758.6	759.3	12.0	16.7	14.5	14.5	18.5	11.0	10.6	09.6	10.0	10.0	91	79	81	84	-	0	S	3
8	758.8	756.4	755.1	13.2	19.4	12.0	14.2	19.5	11.5	10.8	09.9	08.5	10.0	87	50	95	77	-	0	SSW	3
9	754.0	752.7	753.5	11.6	16.8	13.6	13.9	18.2	10.4	09.7	08.4	09.6	07.4	82	67	63	71	-	0	S	4
10	754.3	754.2	756.2	15.2	20.1	13.4	15.5	21.3	13.2	10.8	06.8	08.2	08.6	53	46	75	58	N	5	SSE	4
11	758.0	757.6	758.6	14.4	21.6	14.0	16.0	22.2	06.3	05.5	06.6	06.9	05.3	70	36	77	61	-	0	0	0
12	758.9	758.0	760.5	15.4	22.8	15.8	17.4	23.0	10.7	07.0	08.8	07.6	08.6	67	36	64	56	-	0	SSE	4
13	760.8	760.2	761.1	15.4	22.2	17.2	18.0	23.7	10.1	07.5	08.8	10.7	12.0	67	53	81	67	-	0	SSE	2
14	761.0	758.8	758.5	16.9	24.2	18.2	19.4	24.7	11.5	08.3	08.1	10.9	11.2	57	48	71	59	-	0	S	4
15	757.3	754.1	752.1	13.8	17.6	12.3	13.0	18.0	11.4	12.6	11.0	10.9	07.0	93	94	65	84	N	1	NNW	1
16	753.8	754.0	755.6	14.7	16.4	14.8	15.2	19.3	10.5	06.9	07.9	10.0	09.7	63	72	77	71	-	0	NNW	2
17	757.2	757.0	758.9	13.8	21.2	14.0	15.8	21.3	05.5	06.5	08.4	08.4	11.2	71	44	94	70	-	0	S	4
18	759.0	756.6	757.7	14.7	21.8	16.6	17.4	22.8	10.8	08.0	07.5	06.8	06.6	60	35	46	47	NNW	3	NNE	6
19	756.3	755.4	756.6	17.5	23.4	19.0	19.7	24.0	15.2	09.4	08.9	09.1	07.7	59	42	53	51	N	7	N	4
20	756.8	755.2	756.6	20.2	25.7	20.6	21.8	28.2	15.2	10.3	09.0	08.8	07.8	51	35	43	43	-	0	NNE	2
21	756.2	755.6	756.8	20.1	19.6	18.6	19.2	27.4	17.0	14.5	09.6	13.2	12.1	54	77	75	69	SF	3	ESE	3
22	757.0	754.4	751.5	12.6	25.6	19.8	21.2	26.0	17.2	13.0	10.4	10.5	10.8	61	42	62	55	NN	2	SSW	3
23	749.0	749.1	748.5	11.0	19.0	15.6	15.3	21.4	10.5	09.3	08.3	10.8	11.1	84	65	83	77	NE	6	SSW	4
24	749.1	750.8	752.4	14.8	18.4	17.0	16.8	20.0	13.4	12.9	09.7	11.1	11.8	77	70	81	76	-	0	SW	3
25	754.8	756.1	757.3	15.5	16.8	16.5	16.3	19.2	14.5	14.0	12.1	13.2	13.4	92	92	95	93	S	2	-	0
26	758.0	757.6	757.7	17.2	25.0	17.6	19.4	25.3	13.5	11.5	10.4	07.8	09.4	71	33	62	55	-	0	SW	3
27	757.0	755.6	755.0	16.8	25.2	18.4	19.7	25.8	11.9	09.1	08.1	07.7	11.1	57	32	70	53	FNE	3	SSW	4
28	754.7	752.3	751.8	17.8	25.4	18.3	20.0	25.8	12.5	10.0	10.3	10.0	09.7	68	45	62	58	NE	2	S	4
29	751.7	752.5	753.6	15.6	19.6	14.4	16.0	20.3	14.0	09.5	10.4	12.1	11.3	78	71	92	80	NNE	4	ENE	2
30	756.5	756.5	758.0	16.8	25.8	18.6	20.0	26.1	11.5	09.8	10.6	10.1	12.9	74	41	80	65	-	0	SW	3
31	759.3	759.3	759.7	19.6	26.7	21.6	22.4	27.0	15.5	12.5	12.0	13.7	14.6	70	52	75	66	NNE	3	SW	3
MES.	VRF.D.	755.6	754.6	754.9	15.0	20.0	16.7	16.6	21.6	12.1	09.8	09.3	09.8	10.1	74	58	75	69	1.5	3.2	1.2

1	758.0	756.4	756.1	18.0	26.8	21.8	22.1	26.8	16.3	14.5	13.2	14.1	10.7	85	53	55	64	-	0	SW	3	SSE	2
2	756.6	757.2	758.8	21.6	24.6	19.8	21.4	25.8	16.3	13.2	10.8	05.3	07.1	56	40	41	46	NNE	3	NNE	7	NNE	3
3	758.7	759.7	759.1	19.3	21.4	19.4	19.9	22.5	18.5	15.5	08.0	07.8	08.7	47	41	51	46	NNF	5	NE	7	KNE	5
4	759.4	758.3	758.1	19.6	27.2	20.8	22.1	28.2	15.2	10.4	10.8	12.1	12.6	63	45	63	59	-	0	SSW	3	-	0
5	759.0	758.0	757.3	21.4	29.7	22.8	24.2	30.1	20.6	12.5	11.5	12.7	13.1	60	41	63	55	NE	2	S	3	NH	1
6	757.4	756.3	755.9	22.2	27.3	21.8	23.3	29.1	16.6	12.5	12.7	12.3	11.2	63	45	57	55	NNE	2	SW	2	SSE	2
7	754.9	755.4	755.4	20.0	22.8	19.3	20.4	24.5	17.7	13.5	13.0	14.9	14.2	74	72	85	77	-	0	NE	3	NE	3
8	758.3	757.0	755.6	19.8	27.2	20.6	22.0	27.6	17.8	14.0	07.8	08.9	11.5	45	33	63	47	NE	5	SW	3	NE	2
9	755.9	754.5	754.5	20.7	27.9	21.6	23.0	28.3	16.4	12.3	11.6	10.7	10.8	62	38	56	52	NNE	2	SW	5	SSW	4
10	754.4	753.8	752.7	22.4	25.2	20.6	22.2	26.4	15.5	13.0	09.4	11.0	10.0	46	46	55	49	SSE	5	SSE	7	KSW	1
11	747.9	749.8	752.1	20.2	18.8	14.6	17.2	22.1	14.5	14.5	13.2	12.0	06.8	74	74	54	67	SSW	5	FNE	3	NE	1
12	753.3	751.4	751.8	16.7	21.6	13.6	16.4	22.7	05.6	07.0	07.5	07.9	09.4	52	41	80	58	N	2	S	4	NE	3
13	752.0	751.8	752.3	12.4	17.8	13.6	14.4	18.5	11.7	10.0	09.8	08.8	08.8	91	58	75	75	-	0	SW	3	NE	2
14	753.5	754.1	755.8	14.6	21.6	17.2	17.6	22.5	10.2	07.1	08.4	08.2	08.2	67	42	55	55	NNE	2	SSW	2	S	2
15	758.4	757.0	757.4	16.2	25.0	16.6	18.8	26.0	10.8	07.4	09.1	10.5	13.9	66	44	96	69	-	0	SW	4	-	0

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 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Den	Vrijnost C-g	Obločnost N (0-10)					Intensitet broj sati	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	10•	10•	10•	10•	10.0	00.0	23.6	.	• 0-10-23 ³⁰ ; R 14 ⁵ 6 ²⁰ F _s 2 ³⁰ 13 ⁴⁰ ; 15-18 ³⁰ ; F _s 13 ³⁰ 15
2	8	10•	10	10•	10•	10.0	00.0	31.0	.	• 0-6 ³⁵ 10 ³⁰ 16 ⁰⁵ 17 ⁴⁰ 20 ³⁰ 23
3	8	10	10	10	10•	10.0	00.5	C3.0	.	• 0-15 ³⁰ 6 ²⁰ 16 ⁰⁵
4	8	10	10•	10•	10•	10.0	00.0	.	.	• 0-19 ³⁰ 23 ³⁰ ; F _s 12 ³⁰ 20 ⁴⁰ ; R 6 19 ³⁵ 19 ⁵⁵
5	8	09	10	07	08.7	08.7	02.0	19.4	.	F _s 9 ³⁰ 10 ³⁵ ; • 0-10 ³⁰ 14 ³⁰ ; 22 ³⁰ 23 ⁴⁰
6	8	10•	08	08	08.7	08.7	04.9	18.4	.	• 12-8 ³⁰ ;
7	8	09	09	10•	C5.3	04.2	02.7	.	.	• 0-19 ³⁰ 22 ³⁰
8	8	07•	10	10•	09.0	04.1	02.2	.	.	• 0-17 ⁴⁰ 24 ³⁰
9	8	10	09	10	05.7	03.1	04.8	.	.	• 0-10-4 ³⁰ 16-16 ⁴⁰
10	8	040	030	00	02.3	02.3	12.4	00.0	.	△ 20-7
11	8	000	010	00	00.3	13.3	.	.	.	△ 0-7 ³⁰ 0-12 ³⁰ 12 ³⁵
12	8	000	060	03	03.0	11.4	.	.	.	△ 0-7-6 ³⁰
13	8	010	04	03	C2.7	12.3	00.0	.	.	△ 17-6 ³⁰
14	8	000	030	00	01.0	11.3	.	.	.	△ 0-12 ³⁰ 20 ²⁰ ; F _{NW} -N 16 ⁴⁸ 17 ¹⁰ ; 20 ²⁶ 21 ⁰⁸ ; R 19 ³⁰ 20 ³⁰
15	8	10•	10•	04	08.0	00.0	07.0	.	.	• 0-13-13 ³⁰ ; R 13 ³⁰ 13 ²⁰
16	8	020	07•	08	05.7	10.5	16.2	.	.	• 0-13-13 ³⁰ ; R 13 ³⁰ 13 ²⁰
17	8	000	04	10•	04.7	07.7	00.7	.	.	△ 0-7-6 ³⁰ ; • 0-14-21 ²⁰ ; F _{NW} 14 ³⁶ 14 ⁴⁰
18	8	030	040	04	03.7	12.5	C2.6	.	.	△ 0-17-7 ³⁰ ; F _{NW} 8 ³⁴ 21 ⁴⁰
19	8	07	040	05	05.3	06.7	.	.	.	F _N 10 ⁴⁰ 18 ³⁰
20	8	000	040	00	C1.3	11.5	.	.	.	F _{NE} 7 ⁴⁰ 8 ²⁰ ; F _{SE} -UNW 12 ⁰⁴ 15 ⁵⁰
21	8	040	06•	05	05.0	09.9	.	.	.	• 0-13-14 ⁴⁰ ; R 13 ²⁰ 13 ³⁰ ; F _{NE} 13 ²⁵ 13 ³⁹
22	8	060	080	09	07.7	11.6	01.3	.	.	F _s 17 ⁵⁴
23	8	10	030	07	06.7	08.3	06.8	.	.	F _N -NE 2 ²⁰ 7 ²⁰ ; 8 ³⁰ ; • 0-25 ³⁰ 9 ⁴⁰ ; 23 ²⁰ 24; R 5 ¹⁰ 7 ⁴⁰ ; △ 5 ³⁰ 6 ⁵⁰
24	8	10	10	10	10.0	00.7	C5.9	.	.	• 0-10-2 ²⁰ 10 ⁴⁵ ; 10 ⁵⁸ ; 18-21 ¹⁰ ; 23 ³⁰ 24; F _s 21 ²³
25	8	10•	10	10	10.0	00.3	19.0	.	.	• 0-2-0-12 ³⁰
26	8	08	020	00	C3.3	11.2	06.5	.	.	△ 0-7 ³⁰
27	8	000	020	00	00.7	13.7	.	.	.	△ 0-7-7 ³⁰
28	8	020	030	09	04.7	11.8	.	.	.	△ 0-13-3 ³⁰ 6 ⁵⁰ 11 ³⁰ ; 16-16 ²⁰ ; F _N 7 ³⁵ ; R 9 ³⁰ 10 ⁴⁰
29	8	10	07	04	07.0	02.6	00.3	.	.	△ 0-17-7 ³⁰
30	8	000	050	03	C2.7	12.0	11.4	.	.	.
31	8	050	090	09	07.7	07.7	07.8	.	.	.
MES.										
MRD.		05.7	06.5	06.1	06.1	219.1	187.8			

1	8	10•	050	07	C7.3	C7.1	00.0	.	• 0-6 ³⁵ 7 ¹⁵ ;	
2	8	020	060	02	03.3	11.6	00.1	.	F _{NE} 8-23 ⁴⁵ ;	
3	8	08	030	CC	C3.7	08.5	.	F _{NE} 70 ² 11 ³⁰ 15 ³³ 22 ³ ; F _{NE} 11 ³⁰ 15 ³³		
4	8	000	010	00	00.3	13.5	.	F _{NE} 7		
5	8	020	020	CC	01.3	13.6	.	.		
6	8	040	07	04	05.0	11.1	.	.	• 0-10 ⁰⁵ 12 ⁵⁰ ;	
7	8	09	060	02	C5.7	02.2	.	.	• 0-17-7 ³⁰	
8	8	000	020	00	0C.7	13.7	C1.6	.	F _{NE} 1/2-7 ³⁰ ;	
9	8	050	060	00	03.7	12.5	.	.	F _s 6 ⁵⁰ -18 ³⁰	
10	8	08	080	03	06.3	11.7	.	.	F _s 15 ⁵⁰ 7 ⁰² 8 ⁰⁵ ; 0-05 ²⁰ 5 ³⁰ ; 0-17 ³⁰ 8 ²⁰ ; F _N 8 ³⁵ 0 ¹⁰ ; 0-19 ⁵⁰ 16 ²⁰	
11	8	10	060	03	C6.3	04.2	00.0	.	F _w 17 ³⁰ 1/9 ⁴⁰ ; 1/17 ⁴⁵ 19 ¹⁰ ; F _N 18 ⁴⁵ 18 ⁵⁵	
12	8	010	070	02	03.3	10.3	10.7	.	F _N 2 ¹⁰ 2 ³⁵ ; 0-19 ⁴⁵ 7 ²⁰	
13	8	10•	09	02	07.0	03.2	C2.0	.	△ 0-17-7 ³⁰	
14	8	000	070	05	04.0	10.1	C1.2	.	• 0-10-7 ¹⁵ ; 0-18 ¹⁰ 24 ³⁰	
15	8	010	030	10•	04.7	10.0	.	.	• 0-10-11 ³⁵ 12, 15 ⁴⁰ 19 ⁰ ; R 18 ¹⁵ 18 ³⁵	
16	8	060	080	10	08.0	05.1	07.4	.	• 0-10-8	
17	8	030	080	03	04.7	11.7	04.0	.	△ 0-17 ³⁰	
18	8	010	060	00	C2.3	09.9	.	.	• 0-13 ⁰⁵ 13 ⁴⁵ 13 ⁵⁵ R 13 ⁴⁵ 14 ³⁰ ; 0-13 ²⁰ 14 ¹⁵ , F _N 13 ²⁰ 21 ⁴⁵ ; 0-13 ⁴⁵ 14 ²⁰	
19	8	070	090	06	07.3	03.5	.	.	F _{NE} 7 ³⁵ 13 ⁴⁰ ; 15 ⁰² 22 ⁴⁰	
20	8	030	030	03	C3.0	12.4	06.7	.	• 22 ³⁰ -22 ⁴⁵	
21	8	020	070	06	C5.0	11.2	.	.	.	
22	8	000	030	00	C1.0	13.4	.	.	.	
23	8	000	040	07	03.7	10.5	.	.	F _s 9 ²⁰ 14 ⁴⁵	
24	8	090	040	05	06.0	08.7	.	.	F _s 13 ⁴⁰ ; • 14 ³⁵ 15 ²⁰ R 14 ³⁵ -14 ⁵⁰	
25	8	070	08	00	05.0	05.8	.	.	.	
26	8	040	030	00	C2.3	12.2	C1.1	.	△ 0-17-7 ³⁰	
27	8	09	060	03	06.0	09.0	.	.	F _s 12 ⁵² 20 ⁴	
28	8	09	050	03	05.7	C7.7	00.3	.	F _s 8-10 ¹⁵ ; • 0-22 ²⁴ 240	
29	8	08	060	10	08.0	07.7	.	.	• 0-10 ²⁵ 1 ⁰⁰ 8 ²⁰ 9 ²⁵ ; F _{NE} -NW 9 ³⁵ 14 ⁵ ; 14 ²³ 15 ⁰⁷	
30	8	030	060	08	05.7	07.1	08.4	.	.	
MES.										
MRD.		04.7	05.5	03.5	04.5	279.7	43.5			

$\varphi = 42^{\circ}26'$, N $\lambda = 19^{\circ}17'$, E Gr. $\Delta G = +1h\ 17\ min.$

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D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	755.4	755.6	756.8	22.8	30.0	24.6	25.5	30.5	18.0	13.0	08.9	10.7	10.7	42	34	46	41	N	3	NNF	4	NNF	3	
2	758.3	757.5	757.0	23.0	32.1	26.7	27.1	33.2	19.1	15.6	10.1	12.8	12.6	48	34	48	44	NNF	2	SSW	1	NE	7	
3	758.7	756.1	754.4	23.8	31.3	24.7	26.1	31.8	21.9	18.1	09.1	12.9	14.9	41	37	64	47	NNF	3	S	3	-	0	
4	754.2	753.9	754.3	23.0	32.3	25.2	26.6	32.9	20.3	16.2	13.6	13.4	14.0	64	36	58	53	NNF	3	S	4	-	0	
5	755.6	755.3	756.1	24.2	32.6	26.4	27.4	33.8	21.8	18.0	12.8	12.5	13.9	57	34	54	48	NE	1	SW	3	FNF	1	
6	757.4	756.0	754.7	24.8	34.0	25.7	27.6	34.4	21.7	18.5	13.0	12.2	13.1	55	30	53	46	NNE	2	WSW	3	-	0	
7	753.8	753.9	754.9	23.5	20.6	19.4	20.8	30.2	17.5	15.8	12.5	14.6	06.3	57	80	38	58	-	0	N	6	NNF	8	
8	756.7	756.3	757.3	19.3	23.5	19.0	20.2	24.5	17.2	14.4	07.5	07.9	07.9	44	36	48	43	NNF	6	NNE	6	N	3	
9	759.8	758.8	758.1	19.6	26.7	20.7	21.9	27.3	15.8	12.6	07.2	08.3	08.0	42	32	44	39	NE	4	NE	4	NE	2	
10	759.1	757.0	757.8	20.2	29.2	22.2	23.4	29.5	16.8	14.3	08.1	11.4	13.4	46	37	67	50	S	2	SW	3	-	0	
11	758.7	757.7	758.3	23.8	31.9	24.6	26.3	33.2	20.1	17.4	04.5	11.3	12.2	39	32	52	41	NNF	7	NNW	2	ENE	2	
12	759.5	758.7	758.8	23.4	33.0	25.0	26.6	33.5	19.8	15.8	11.9	12.7	15.0	55	34	63	51	NNE	3	SW	3	-	0	
13	759.1	757.0	756.0	24.0	35.2	25.4	27.5	35.9	20.0	16.3	13.4	10.6	13.7	60	25	56	47	N	2	S	3	-	0	
14	757.2	755.8	756.3	24.7	36.4	27.9	29.2	36.8	21.3	16.8	11.8	11.6	12.6	51	25	45	40	NNE	2	SSE	3	ENE	3	
15	757.8	756.5	757.2	25.9	37.7	25.5	30.6	38.3	22.1	18.4	10.8	12.7	14.7	43	26	48	39	N	3	SW	3	NF	2	
16	757.0	755.0	755.2	28.0	28.7	30.0	31.7	38.6	24.8	20.8	13.9	13.1	14.8	49	25	47	40	N	2	SW	4	-	0	
17	754.9	752.6	742.4	27.6	28.0	30.0	31.4	38.6	24.9	21.0	13.4	12.5	14.2	48	25	44	39	NNE	2	SSE	3	-	0	
18	752.3	751.6	751.4	26.5	34.1	27.5	28.9	35.5	22.0	18.9	14.4	12.3	15.4	56	31	56	48	ENF	2	S	6	-	0	
19	751.8	752.6	751.9	25.2	29.2	21.3	24.2	29.7	20.8	19.5	14.8	10.8	15.3	61	35	81	59	S	5	S	5	S	1	
20	750.9	750.1	750.9	20.6	27.2	26.6	22.2	28.4	18.1	16.7	12.7	10.9	08.9	70	40	49	53	N	1	SSH	4	NNE	6	
21	750.9	750.5	752.1	19.8	22.4	20.2	20.6	25.6	18.5	16.0	07.8	08.2	08.6	45	40	49	45	NE	6	NNE	6	N	2	
22	753.8	754.0	755.2	19.2	26.4	20.2	21.6	27.4	17.5	15.3	08.9	09.8	08.8	53	38	47	46	N	3	NE	3	N	5	
23	755.4	757.2	757.8	17.8	20.0	18.0	18.4	22.7	16.0	12.7	08.8	12.9	12.1	58	74	78	70	-	0	NE	2	-	0	
24	759.9	758.2	758.1	18.6	27.0	22.2	22.5	28.2	15.0	12.5	11.5	12.0	13.1	72	45	65	61	N	1	S	2	H	1	
25	758.1	755.7	755.8	20.6	30.2	24.2	24.8	31.0	16.6	12.4	11.9	12.4	12.4	65	39	55	53	NNE	1	S	3	-	0	
26	756.5	755.0	757.2	23.2	30.8	22.8	25.4	31.7	19.8	16.0	12.9	12.8	09.7	60	38	44	47	-	0	SSW	4	NNE	6	
27	758.6	757.2	758.0	22.4	31.2	24.2	25.5	32.4	19.9	18.0	11.0	15.2	14.3	54	45	63	54	Nw	2	W	3	-	0	
28	758.3	757.3	758.3	23.6	33.4	26.0	27.2	34.2	19.0	14.4	11.1	11.0	13.9	51	28	55	45	N	1	SSW	2	-	0	
29	759.1	757.7	758.3	24.1	35.8	30.6	30.3	36.1	19.2	16.5	13.9	13.3	14.2	62	30	43	45	-	0	SSW	3	NE	6	
30	758.3	755.4	755.4	27.2	36.0	29.6	30.6	36.0	25.8	23.4	16.1	12.7	14.0	59	28	45	44	N	2	SSW	4	-	0	
31	755.6	753.8	754.0	27.2	35.7	29.3	30.4	36.5	24.4	20.3	14.6	13.3	13.2	54	30	43	42	NNW	2	S	4	-	0	
MES.	VRED.	756.5	756.5	756.8	23.2	31.1	24.7	25.9	32.2	19.9	16.6	11.5	11.9	12.4	54	36	53	48	2.2	3.5	1.9			

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1	754.6	752.8	753.7	27.7	37.0	27.7	30.0	37.0	26.2	23.6	13.1	12.5	12.9	47	27	46	40	NW	4	SSE	4	-	0
2	754.5	753.7	753.7	28.1	37.0	28.6	30.6	37.8	26.0	23.3	12.7	11.0	13.6	45	23	46	38	N	3	S	4	-	0
3	756.2	755.3	756.1	28.0	37.0	28.6	30.6	38.0	26.2	22.5	10.2	07.9	13.9	36	17	47	33	NNW	4	SSE	4	-	0
4	757.6	756.1	755.8	28.2	38.3	29.4	31.3	38.4	26.3	21.6	14.1	11.7	12.7	49	23	41	38	NNW	3	SW	2	-	0
5	757.4	755.3	754.7	27.6	38.7	26.4	31.3	38.7	25.4	21.0	13.7	11.5	09.5	50	22	31	34	NNW	2	SSE	4	-	0
6	756.3	754.0	754.8	27.9	37.7	28.8	30.6	38.0	25.2	20.5	10.6	15.4	14.4	38	31	49	39	-	0	S	4	N	6
7	756.2	754.0	754.0	24.5	33.0	28.0	28.4	33.1	24.0	22.2	09.7	11.7	12.8	42	31	45	39	N	6	SSE	4	ESE	2
8	754.1	752.1	751.6	24.8	33.6	27.2	28.2	33.8	23.0	19.9	10.6	11.7	10.4	45	30	39	38	N	4	S	3	-	0
9	752.4	751.4	752.2	24.0	28.6	25.6	26.6	31.4	20.4	16.4	10.1	17.6	18.4	45	60	75	60	-	0	SSE	4	SE	2
10	755.4	753.8	753.0	24.2	31.7	24.6	26.3	32.6	23.2	20.6	12.1	08.3	14.0	53	24	60	46	N	4	SSE	4	-	0
11	751.5	750.6	751.3	22.7	26.8	22.6	23.7	28.8	20.5	15.6	10.7	14.5	14.4	52	55	70	59	-	0	S	6	NNW	2
12	754.1	753.9	756.2	21.0	27.2	22.2	23.2	28.2	18.5	15.0	06.5	06.7	06.6	35	25	33	31	N	4	NNE	4	NW	2
13	757.7	757.2	759.0	21.8	29.6	24.6	25.2	30.0	17.0	12.2	07.1	07.4	08.0	36	24	34	31	NW	5	NNE	4	NNE	4
14	760.9	759.6	760.3	21.8	33.0																		

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vyhřev 0-0	Oblačnost N (0-10)					Insolace sati breh	Podzvuk R mm	Snežní pokrývka h cm	Razový vývoj w
		14	7	14	21	Sred Dies				
1	8 030	040	00	02.3	13.8	00.3	.	FNE 9 ² -14 ²² i	.	.
2	8 000	020	00	00.7	14.0	.	.	FNNNE 22 ¹² -24i	.	.
3	8 000	020	00	00.7	12.9	.	.	FNNNE 0-3 ⁰⁴ i	.	.
4	8 030	020	00	01.7	13.3
5	8 030	020	00	01.7	13.5
6	8 000	010	00	00.3	14.0
7	8 030	090	01	04.3	08.8	.	.	• 0-11 ²⁵ -13 ¹⁵ , FNNNE 11 ¹² -14 ¹⁰ i, R 11 ⁵⁰ -13 ²⁰ , FNNNE 14 ¹⁰ -24	.	.
8	8 010	030	03	02.3	13.8	06.8	.	F-FNNNE 0-16 ¹⁰ i	.	.
9	8 000	040	00	01.3	14.1	.	.	FNNNE 5 ⁵⁰ -15 ⁵² i, FNNNE 9 ⁵⁰	.	.
10	8 030	030	00	02.0	12.7
11	8 10	030	04	05.7	10.3	.	.	FNNNE 9 ³⁰ -10 ³³ i	.	.
12	8 000	010	00	00.3	13.9
13	8 000	000	00	00.0	14.2
14	8 000	000	00	00.0	14.1
15	8 000	000	00	00.0	13.5
16	8 000	000	00	00.0	13.2
17	8 000	030	00	01.0	12.7
18	8 010	080	00	03.0	09.1	00.0	.	• 0-17 ²⁰ -7 ⁰ , 09 ⁴⁰ -9 ²⁰ , FSSSE 12 ⁰⁴ -14 ¹⁵ , FSSSE 12 ³⁴	.	.
19	8 070	020	09	06.0	09.1	00.0	.	FSSSE 14 ³⁵ -18 ⁰⁵ , 12 ³⁵ , FSSSE 18 ⁰⁵ -19 ¹⁶ , FSSSE 19 ⁵⁰ -20 ⁴⁵	.	.
20	8 080	060	06	06.7	11.4	03.5	.	FNNNE 18 ³⁰ -19 ³⁰ , FNNNE 22 ¹² -22 ⁵⁰	.	.
21	8 08	09	08	08.3	05.6	.	.	FNNNE 0-19i	.	.
22	8 040	050	02	02.7	08.2	.	.	FNE 15 ²⁰ -20 ⁴⁵ i	.	.
23	8 09	10	10	05.7	02.1	.	.	• 0-10 ²⁰ -10 ³⁵ , 13 ²⁰ -14 ³⁰	.	.
24	8 000	06	00	02.0	12.2	00.8
25	8 000	010	00	00.3	13.5
26	8 030	07	00	02.3	10.0	.	.	FNE 15 ²⁷ -22 ³² , FNE 16 ³⁶ -20 ²⁴	.	.
27	8 000	000	00	00.0	13.7	.	.	FN 040-140	.	.
28	8 000	000	00	00.0	13.8
29	8 050	030	05	04.3	12.6
30	8 000	030	08	03.7	11.9	.	.	FNNNE 0 ³⁰	.	.
31	8 000	030	06	03.0	12.7
MES.				02.3	03.3	02.0	02.5	368.7	11.4	
WRED.										

1	8 010	030	00	01.3	13.3	.	.	FNNW 15 ²⁵ -17 ²⁵ , FNNW 15 ²⁰	.	.
2	8 000	010	00	00.3	13.2	.	.	FNNW 14i	.	.
3	8 000	010	00	00.3	13.2
4	8 010	010	00	00.7	12.6
5	8 000	010	00	00.3	11.8
6	8 000	020	00	00.7	12.5	.	.	FN 17 ³⁵ -24, FN 18 ³⁰ -24	.	.
7	8 000	010	03	01.3	12.3	.	.	FN 0-10 ³⁰ , FN 0 ³⁰ -7 ⁴⁷	.	.
8	8 000	010	00	00.3	12.7	.	.	FSSSE 13 ¹⁴ -16 ³⁶ i	.	.
9	8 070	08	03	06.0	06.9	.	.	FN 05 ³⁰ -10 ²⁵ i	.	.
10	8 010	010	00	00.7	13.3	.	.	• 09-9 ¹⁰ , FSSSE 12 ²⁵ -17 ⁴⁰ i, 23 ⁵⁰ -24, • 0-11 ²² -12i	.	.
11	8 05	070	08	08.0	08.0	.	.	FN 0-19 ⁴⁰ i, FN 0 ³⁰ -10 ⁴⁵ i	.	.
12	8 010	050	05	03.7	12.9	06.6	.	FNNNE 8-22 ⁵⁵ i	.	.
13	8 000	050	03	02.7	12.0	.	.	FNNNE 11-12 ⁵⁵ i	.	.
14	8 000	010	00	00.3	13.2	.	.	FNNNE 13 ⁴⁵ -17 ⁰⁰ i, FNNNE 12 ⁴⁰	.	.
15	8 000	070	03	03.3	12.8
16	8 030	040	00	02.3	12.4	.	.	FSSSE 12 ¹³	.	.
17	8 000	060	00	02.0	12.3	.	.	FNNNE 8 ³⁰ -23 ⁴⁸	.	.
18	8 000	000	00	00.0	12.8	.	.	FNNNE 14 ¹⁵ -14 ⁴⁵	.	.
19	8 000	010	00	00.3	12.4	.	.	FNNW 14 ⁵⁵	.	.
20	8 000	030	04	02.3	11.3	.	.	• 19 ⁵⁰ -22 ⁴⁰ , T 20 ¹⁵ -21 ³⁰	.	.
21	8 05	070	03	06.3	04.8	.	.	FSE 17 ⁰² -12 ³⁷ , 6 19 ³⁰ -20 ⁴⁵ , T 20-20 ⁴⁰	.	.
22	8 000	050	03	02.7	11.6	.	.	FSE-N 0 ⁴⁰ -10 ²² , 15 ⁴⁵ -16 ⁰⁰	.	.
23	8 07	070	08	07.3	07.2	.	.	FSE-SE-NNW 14 ¹⁰ -14 ⁵⁵ , 6 ⁵⁰ -6 ⁵² , 17 ⁴⁵ -18 ⁰⁰	.	.
24	8 08	050	03	05.3	06.5	01.4	.	• 02 ⁴⁰ -3 ⁵⁰ , □ 20-20 ²⁰ , □ 20 ²⁰ -20 ²⁵	.	.
25	8 040	040	09	05.7	11.3	.	.	FSE 17 ³⁵	.	.
26	8 010	060	01	02.7	12.2
27	8 020	030	05	03.3	11.6
28	8 08	10 ⁰⁷	10	09.3	03.2
29	8 08	09	05	07.3	05.5	07.2	.	FNNNE-NE 6 ⁰⁰ -8 ²⁵ , 16 ⁵⁰ -17 ²⁰ , R 13 ⁴⁵ -15 ⁰⁰	.	.
30	8 09	040	00	04.3	07.3	00.3	.	FNNNE-NE 6 ⁰⁰ -8 ²⁵ , 16 ⁵⁰ -17 ²⁰ , R 13 ⁴⁵ -15 ⁰⁰	.	.
31	8 000	040	04	02.7	12.1
MES.				02.5	04.0	02.6	03.0	335.6	15.5	
WRED.										

$\varphi = 42^{\circ}26'$, N $\lambda = 19^{\circ}17'$, E Gr. $\Delta G = +1h\ 17\ min.$

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SD	Temperature (°C)			Humidity (%)						Wind (m/s)			Pressure (hPa)									
	7	14	21	7	14	21	Sred. Dries	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dries	7	14	21		
1	757.2	756.7	757.0	21.4	28.8	22.0	23.6	30.0	17.8	15.3	12.2	12.5	11.8	64	42	59	55	N	3	SSE 3	- 0	
2	757.3	757.2	758.1	22.4	30.4	23.2	24.6	31.2	20.6	16.8	11.8	11.1	17.2	58	34	R1	58	N	3	SSE 5	- 0	
3	758.3	756.8	757.3	22.9	32.6	24.8	26.3	32.8	21.0	18.8	13.5	14.5	14.4	64	39	61	55	N	3	SSE 4	- 0	
4	756.8	755.1	755.3	23.2	33.2	24.4	26.3	33.8	20.8	17.0	14.4	14.6	15.3	67	38	67	57	-	0	S 4	- 0	
5	757.3	755.3	756.3	24.2	32.4	24.5	26.4	32.5	22.7	19.8	12.5	11.7	11.6	55	32	50	46	NNW 3	SE 2	NE 2		
6	755.1	752.0	751.1	21.8	30.8	23.0	24.6	31.5	19.9	17.8	07.8	11.4	13.0	40	34	62	45	N	3	S 5	- 0	
7	748.1	749.2	750.3	20.8	18.2	17.6	18.6	23.0	16.8	14.5	11.8	14.5	14.2	64	93	94	84	N	2	SE 3	- 0	
8	753.7	755.0	758.1	16.6	29.2	24.6	23.8	29.6	14.4	13.4	12.5	12.0	11.0	88	39	47	58	-	0	NNE 5	NNW 3	
9	761.0	760.1	760.1	21.0	30.8	23.0	24.4	31.0	20.5	17.7	11.3	11.7	13.0	60	35	62	52	NW 1	SE 3	- 0		
10	760.9	759.2	759.7	21.4	31.2	24.7	25.5	32.4	20.0	16.6	12.9	14.4	14.9	68	42	64	58	N	2	SE 4	- 0	
11	760.8	759.8	761.0	25.0	31.4	25.0	26.6	31.4	23.5	19.6	11.4	10.4	11.1	48	30	47	42	N	6	NNE 5	NNE 5	
12	761.9	760.5	761.1	21.6	30.0	22.8	24.3	30.7	21.4	17.5	10.2	11.4	11.6	52	36	56	48	NW 1	SE 3	- 0		
13	761.2	759.0	759.4	21.0	31.0	23.4	24.7	31.4	20.0	15.5	11.4	12.4	11.3	61	37	52	50	N	3	SSE 3	- 0	
14	760.1	758.2	758.4	22.4	31.2	24.6	25.7	35.6	21.9	18.9	11.3	09.8	13.8	55	29	60	48	NNW 3	SSE 4	- 0		
15	758.0	756.1	756.7	22.7	30.0	23.8	25.1	30.5	21.7	18.5	10.3	11.9	11.1	50	37	50	46	NW 2	SE 4	- 0		
16	758.0	757.5	758.4	23.5	30.4	25.2	26.1	30.8	22.3	16.3	11.6	11.7	09.9	53	36	41	43	N	2	SSE 3	N 4	
17	760.3	759.9	760.2	20.9	29.0	22.8	23.9	29.5	20.8	17.5	10.0	11.2	15.2	54	37	73	55	SSW 3	ESE 2	- 0		
18	760.3	759.0	759.4	20.4	26.8	22.6	23.1	28.6	19.0	16.0	11.4	11.8	12.3	64	45	60	56	NNE 3	WSW 3	- 0		
19	759.4	757.4	757.6	20.0	27.3	22.4	23.0	29.3	18.5	15.0	12.8	12.3	11.6	73	45	57	58	-	0	ESE 1	NF 2	
20	756.2	754.3	754.2	19.4	28.8	23.5	23.8	29.0	18.4	14.3	10.2	10.7	16.8	60	36	77	58	NNE 4	SE 5	ESE 4		
21	754.4	755.5	755.0	18.5	18.0	18.7	18.5	24.0	16.3	17.5	14.9	14.5	14.8	94	93	92	93	-	0	-	0	
22	755.1	756.4	757.5	18.5	24.2	18.2	16.8	24.4	17.5	17.0	14.2	12.4	14.8	89	55	94	79	W 2	SE 5	-	0	
23	756.5	757.4	757.5	17.0	21.6	17.5	18.4	23.2	15.6	16.9	14.3	12.2	13.4	98	63	90	84	NW 2	-	0		
24	754.8	754.2	752.4	17.4	22.3	20.6	20.2	24.7	15.6	13.5	13.6	15.1	13.9	91	75	76	81	-	0	SE 2	SE 4	
25	749.9	747.6	747.3	15.4	13.7	13.0	13.8	22.0	12.8	14.5	12.6	10.9	10.6	96	93	95	95	-	0	NNNE 3	-	0
26	742.3	741.5	747.5	12.4	16.0	13.4	13.8	22.0	12.0	10.4	10.3	11.5	06.0	96	84	52	77	NW 2	-	0	NW 5	
27	754.3	756.2	758.3	10.6	21.0	12.6	14.2	21.2	07.5	04.5	07.3	05.7	06.4	76	30	58	55	-	0	NF 3	-	0
28	756.8	757.1	757.2	12.0	21.8	14.8	15.8	21.8	10.2	06.3	06.5	08.5	11.5	61	43	91	65	N	4	SSE 3	-	0
29	757.1	757.3	757.8	13.5	23.6	16.0	17.2	23.8	12.0	09.1	09.1	09.8	12.0	78	45	88	70	-	0	S 2	-	0
30	756.6	755.0	756.4	16.0	24.6	17.4	18.8	25.1	13.0	10.0	11.0	10.7	14.3	81	46	96	74	-	0	SE 5	-	0
MES.	VRRED. 756.7 755.8 756.6			19.5	26.7	21.0	22.0	28.2	17.8	15.2	11.5	11.8	12.6	69	47	68	62	1.9	3.2	1.0		

SD	Temperature (°C)			Humidity (%)						Wind (m/s)			Pressure (hPa)								
	7	14	21	7	14	21	Sred. Dries	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dries	7	14	21	
1	755.4	755.5	757.0	14.8	22.0	15.6	17.0	22.0	14.4	13.6	10.8	09.8	09.4	86	50	71	69	SE 1	SE 5	- 0	
2	756.6	756.4	752.5	12.6	19.0	15.0	14.2	17.6	11.0	08.4	08.1	10.5	09.7	74	87	76	79	-	0	WNW 2	SSW 5
3	759.3	760.0	761.8	11.4	19.4	11.4	13.4	20.0	10.4	08.0	09.3	06.5	08.5	92	38	84	71	-	0	S 3	- 0
4	761.3	760.0	760.1	10.7	20.4	12.0	13.8	21.8	09.2	05.3	06.7	05.1	08.4	69	29	80	59	-	0	-	0
5	758.4	756.4	754.9	13.2	21.4	15.0	16.2	23.0	11.0	07.2	06.0	07.8	10.5	61	41	82	61	NNW 2	-	0	
6	752.0	753.1	754.3	13.6	21.7	16.0	16.8	22.5	13.6	11.9	10.2	10.8	10.9	87	55	80	74	NE 1	SE 4	NE 2	
7	751.5	757.2	757.5	13.2	14.7	17.7	15.8	17.8	12.8	13.0	10.6	12.0	11.4	94	96	75	88	-	0	SE 5	
8	753.0	752.2	754.1	15.6	17.0	14.0	15.2	21.2	13.5	14.2	12.5	11.7	10.7	94	80	90	88	-	0	SE 5	- 0
9	755.2	755.3	755.5	11.8	20.6	15.2	15.7	21.4	10.5	07.5	09.3	07.4	09.9	90	41	76	69	-	0	SE 3	NW 1
10	758.9	758.2	759.1	11.8	21.2	12.2	14.4	21.4	08.6	05.9	07.4	05.9	08.0	72	31	75	59	N	3	W 1	- 0
11	759.4	759.2	760.4	10.5	20.4	13.8	14.6	20.8	09.6	05.5	06.4	06.3	07.3	67	35	62	55	N	4	SE 2	N 4
12	759.9	758.3	757.9	11.8	20.5	14.7	15.4	22.2	10.2	05.7	07.2	07.5	11.3	69	41	90	67	NW 2	NW 2	NNW 3	
13	756.5	755.0	753.3	14.0	15.4	15.2	15.0	16.6	13.5	13.6	10.7	11.8	11.4	90	90	88	89	-	0	NW 3	- 0
14	753.4	753.4	753.6	16.8	19.4	16.8	17.4	20.6	14.8	14.5	12.2	14.5	12.4	85	86	87	86	SE 4	SSE 1	- 0	
15	752.9	750.4	750.1	15.4	17.3	17.3	16.8	19.7	15.0	14.0	11.5	13.0	12.4	88	88	84	87	-	0	ESE 7	
16	755.3	757.7	758.8	13.2	19.6	12.6	14.5	21.2	12.6	10.4	09.7	06.7	09.0	85	39	83	69	-	0	S 3	-

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 $H_s = 49 \text{ m } H_D = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Dan	Opis	Oblikovanje					Srednji vremenski period	Srednji vremenski period	Razvoj vremena
		14	7	14	21	Sred Dnes			
1	8 050	070	03	05.0	C9.7
2	8 060	090	04	06.3	C9.7
3	8 040	020	00	02.0	10.6
4	8 020	020	03	02.3	11.2
5	8 020	040	00	02.0	12.0	.	.	FSE 1530 1706 FN 230 805 9480	.
6	8 000	000	00	00.0	12.0	.	.	FN 230	.
7	8 100R	05	03	07.3	00.0	.	.	R 540 1230 i FWW 1045 1056, 0-1-2 625 1220 i, FWW 1052	.
8	8 000	030	00	C1.0	11.2	14.4	.	FN 130 1320 i	.
9	8 000	010	00	00.3	11.6	.	.	FN 140	.
10	8 000	010	00	00.3	10.9
11	8 050	020	00	02.3	10.8	.	.	FN 430 2250 i, FN 940	.
12	8 000	010	04	C1.7	11.0
13	8 06	010	00	02.3	09.0
14	8 040	010	00	01.7	10.9
15	8 000	000	00	00.3	11.0	.	.	FN 800 840	.
16	8 000	020	00	00.7	10.7	.	.	FNNE 824 944	.
17	8 000	010	00	00.3	09.6
18	8 030	10	C6	C6.3	05.3
19	8 030	08R	02	04.3	C8.1	.	.	R 1245 1435, 0-1 1405 1415	.
20	8 010	010	08R	03.3	09.7	00.0	.	FESE 1330 7105 2410, R 2140 2150, 6 2150 n, 0-2 2140 24	.
21	8 100	060	080R	08.0	02.0	C7.2	.	0-2 0-1205 2050 2330, FESE 440 458 T 2050 n	.
22	8 100R	07	100	05.0	C1.7	45.7	.	0-0-330 1220 830, 0-1-2 0-2 0-2 925, 1505 1535 1810 24, R 1705 2010, 6 1930 24	.
23	8 100R	070	08	08.3	04.4	31.0	.	0-0-1040 1230, 0-1-2 1310 1330 2010, 124	.
24	8 10	070	100	09.0	06.6	15.1	.	0-0-1510 2320 24, FESE 030 1210, R 2150 1415, FESE 240 1240	.
25	8 100R	100	04	08.0	00.3	42.2	.	0-1-2 0-1450 1420 4510, FESE-NNE 945 1044 2040 2210, R n-1040, FESE 1010 1032	.
26	8 100R	09	C6	08.3	01.6	61.0	.	FN-ANNE 1100 1240, 2310-2330	.
27	8 030	010	00	01.3	11.1	32.4	.	FN 140 460	.
28	8 000	020	00	00.7	10.9
29	8 080	040	03	05.0	07.2	.	.	0-1-2 0-8, FESE 1330 1340 i, 0-1-2 1620 2010, R 1745 2020	.
30	8 070	070	10	08.0	07.0

MES.
WRED. 04.3 04.2 03.1 03.8 247.9 245.0

1	8 10	050	09	08.0	08.0	40.2	.	FSE 1119 1132 1144 △ 21-8, 0-2 1045 2310, FESE-SE 1435 1442 1659, 1744 2106; R 1820 n, FESE-S 1846 2010
2	7 09	10	100R	05.7	C0.8	.	.	△ 0-119-24
3	8 08	040	00	04.0	C9.2	11.3	.	△ 0-0-630
4	8 C50	070	02	04.7	09.2	.	.	.
5	8 080	090	06	07.7	C4.5	.	.	.
6	8 100	060	10	C8.7	C5.7	25.3	.	0-1-2 005 730 i, R n-6, FWW 049
7	8 100	100	10	10.0	00.0	06.4	.	0-1-2 1830 i, 21-2250, 1730 2230, FESE 2025 2330 i
8	8 08	100	100	05.3	02.9	40.5	.	FESE-SE 0040 042 820 1435, 1945, 10-2, 1400 2210, 1740 1850, R 19-17
9	8 10	060	07	C7.7	C6.8	10.3	.	0-1-2 7-9, 21-2140, FWW 12120 12124
10	8 030	030	01	02.3	10.3	06.4	.	△ 18-n
11	8 020	030	00	C1.7	10.4	.	.	△ 17-8 19-n
12	8 040	10	10	08.0	06.3	.	.	△ 0-119-1320 2150, R 805 020
13	8 100	10	100	10.0	00.0	C5.8	.	△ 0-1-1015 1045 1240 1245 1345 2245, FESE 342 400 R 1030 n, 1940 n
14	7 100	090	08	09.0	01.0	36.4	.	△ 0-2-0-0 60 1025 2410, FESE 1612 24, FESE 1646 1702, FESE 2305
15	7 10	100	100	10.0	00.1	20.5	.	0-1-2 0-540 1740 2030, FS 212 2211 10 1240 n, R 19-2010, 2010 n
16	8 040	040	06	04.7	07.6	97.0	.	△ 0-1-2 0-540 1740 2030, FS 212 2211 10 1240 n, R 19-2010, 2010 n
17	8 03	040	00	02.3	10.1	00.6	.	△ 0-1-2 17-8 19-n
18	8 06	080	00	04.7	07.2	.	.	△ 0-1-1830 24
19	8 02	040	00	02.0	10.0	.	.	△ 0-1-0-8, FESE 1412 1445
20	8 03	070	07	05.7	06.9	.	.	.
21	8 10	08	100R	05.3	C1.0	12.1	.	0-1-2 045 2410, FESE-S 434 2410, R 1510 n
22	7 C8	100	100R	05.3	00.5	52.8	.	0-1-2 0-2410, FESE-S 5030 5305 5305 2140, R 1110 1920, R 1520 n
23	8 100	100	090	05.7	C0.1	26.0	.	FESE 320 1130 1545, 1040 1910, △ 19-n
24	8 09	060	03	06.0	02.9	46.5	.	.
25	8 07	030	00	03.3	09.1	.	.	.
26	5 04	100	10	08.0	03.2	.	.	△ 0-1-2 0-730 0-1240 1610 2045 n, R 1320 1450, 0-1-2 2245 2340
27	8 03	020	00	01.7	10.0	00.8	.	FN 320 1410, FN 420 1410, △ 0-1-2 2010 2410, R 2245 24, FESE 2320 24
28	8 06	010	100	05.7	C9.7	.	.	△ 0-1-2 0-1030 1045 1940, △ 0-1-2 1740, R 19-1740, R 24
29	8 10	100	100	10.0	01.8	34.1	.	△ 0-1-4 180 0-730, 10-1740, FN 040 1130, △ 0-1-2 540 1830 i
30	7 100	100	07	09.0	00.2	32.5	.	△ 0-1-730 1910, △ 0-1-2 540 1830 i
31	8 10	100	10	10.0	00.0	16.6	.	.

MES.
WRED. 07.2 07.1 06.3 06.8 157.1 523.4

$\varphi = 42^{\circ}26'$, N $\lambda = 19^{\circ}17'$ E Gr. $\Delta G = +1h\ 17\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenih parova e mm			Relativna vlažnost v%			Pravac i jačina veta D, f (0—12)						
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21			
1	748.4	749.9	753.8	04.6	10.2	08.6	08.5	12.4	06.5	04.6	06.1	07.1	03.0	84	76	36	65	N	2	C	N	7	
2	750.3	750.2	750.3	04.6	12.6	05.6	07.1	13.0	04.2	-01.5	03.2	03.6	05.5	51	33	60	55	NW	3	SW	2	0	
3	760.9	761.3	761.7	05.6	12.6	08.2	08.6	12.8	04.5	00.2	05.9	05.1	06.7	86	47	82	72	-	0	SSE	2	-	
4	760.9	760.0	759.2	06.2	11.6	08.0	08.4	12.5	05.4	01.0	06.1	06.2	06.6	86	61	82	76	-	0	-	0	-	
5	759.9	760.4	762.4	08.6	12.6	10.0	10.3	14.6	06.2	03.4	06.3	06.4	07.7	75	58	83	72	N	2	N	3	-	
6	763.7	763.1	763.1	08.2	16.8	10.2	11.4	17.5	08.0	05.0	07.7	07.6	08.6	95	53	92	80	-	0	-	C	-	
7	760.1	758.0	758.0	05.2	11.5	10.2	10.3	12.5	09.2	07.2	07.7	08.7	08.2	88	85	88	87	-	0	-	C	-	
8	755.3	754.6	755.5	09.0	15.2	12.0	12.0	16.6	08.1	05.0	05.5	04.4	04.0	64	34	38	45	NW	3	NNE	7	NNE	7
9	755.7	756.1	758.9	11.7	14.2	11.4	12.2	15.5	11.2	08.4	03.8	04.3	04.1	37	36	41	38	NNE	7	NNE	8	N	7
10	760.1	759.8	761.1	05.6	15.6	07.2	08.9	16.0	05.3	00.5	05.5	05.5	06.4	80	42	84	69	-	0	SW	2	-	0
11	763.1	762.3	763.1	05.0	16.6	07.0	08.6	17.0	04.7	-00.4	05.4	05.7	06.5	83	40	87	70	N	3	SSE	2	-	0
12	763.0	761.7	761.7	06.2	14.2	08.6	09.4	16.5	04.7	-00.4	05.6	06.2	07.3	78	51	87	72	NNE	2	SE	1	-	0
13	761.6	762.1	763.5	07.5	15.0	08.5	09.9	15.4	07.0	03.5	07.1	06.7	07.5	91	52	90	78	-	0	-	C	-	0
14	764.4	763.7	764.0	07.4	16.7	07.6	08.6	17.5	06.9	03.0	07.3	06.8	07.2	95	47	92	78	-	0	SE	1	-	0
15	764.9	763.9	764.6	06.4	14.2	07.6	09.4	17.0	06.4	02.0	06.0	06.1	06.7	84	44	86	71	-	0	SSE	2	-	0
16	764.2	762.6	764.0	05.2	17.4	08.0	08.6	19.0	05.0	01.3	06.1	07.3	07.4	91	49	92	77	-	0	SE	2	NF	1
17	764.4	763.3	764.1	05.2	18.4	08.2	10.0	18.5	04.8	01.2	06.1	07.3	07.5	91	46	92	76	-	0	SF	2	-	0
18	764.6	763.4	763.5	04.4	17.2	08.2	09.5	17.4	04.4	00.6	05.5	06.1	06.7	88	41	82	70	-	0	SSE	3	-	0
19	767.5	760.2	759.7	05.4	16.0	11.2	11.0	16.9	05.3	01.5	06.2	06.4	06.3	91	50	93	78	-	0	-	C	W	2
20	761.6	761.1	762.5	10.4	15.0	09.8	12.4	19.1	09.5	06.5	08.4	08.2	08.4	86	50	93	76	N	2	SSE	2	-	0
21	761.7	761.0	759.8	08.0	12.6	05.6	10.0	14.0	07.9	05.0	06.6	07.9	07.9	82	72	88	81	-	0	-	C	-	0
22	759.8	754.7	761.0	08.2	15.8	07.6	09.9	16.2	07.7	06.6	06.9	06.8	07.1	85	50	90	75	-	0	SE	2	-	0
23	761.7	759.9	760.2	05.2	15.2	09.2	09.7	15.4	04.8	01.8	06.0	06.6	07.9	90	51	90	77	-	0	SE	2	-	0
24	759.8	759.8	760.5	05.0	11.8	08.2	08.3	12.0	05.0	01.5	05.9	07.2	07.5	90	69	92	84	-	0	-	O	-	0
25	761.1	760.1	758.1	07.4	09.6	09.4	09.0	10.8	06.8	02.5	07.1	07.2	08.3	92	81	94	85	-	0	-	C	NE	1
26	753.4	753.2	755.1	11.2	11.6	07.0	09.2	14.8	07.0	08.3	09.3	08.6	08.6	93	84	92	90	NE	2	KNE	3	-	0
27	754.3	751.9	752.5	05.8	08.2	08.6	07.9	09.2	05.0	02.5	06.3	07.1	07.3	92	87	87	89	-	0	NNW	2	N	4
28	750.6	747.3	741.0	08.9	10.4	14.6	12.1	14.7	08.1	05.7	07.1	08.0	09.2	83	85	74	81	-	0	-	0	SSE	6
29	747.0	748.3	752.1	06.2	14.0	06.8	08.4	15.6	05.5	02.5	03.7	03.6	06.5	52	30	88	57	N	3	S	2	-	0
30	753.6	756.8	759.4	04.5	12.2	07.3	07.6	12.6	04.0	00.6	05.1	04.7	03.2	81	44	41	55	N	2	S	1	NNW	4
MES.	759.4	758.8	750.4	07.0	14.0	08.6	09.7	15.1	06.3	03.0	06.2	06.5	06.9	82	55	81	73	1.0	1.7	1.3			
VRFD.	750.4	750.8	760.4	03.5	11.0	05.7	06.6	12.2	02.5	-00.4	04.5	04.7	04.7	82	55	81	73	1.0	1.7	2.2	2.0		

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1	760.1	762.6	764.3	03.4	06.0	03.0	03.8	09.0	02.5	-02.0	04.0	06.0	05.3	68	86	94	83	NW	3	-	C	-	0
2	764.7	764.6	765.0	00.8	10.0	05.6	05.5	10.6	00.5	-02.5	04.5	05.0	05.6	93	54	82	76	-	0	-	C	-	0
3	765.8	764.9	765.3	05.8	14.4	09.8	10.0	15.6	05.5	03.5	05.8	05.9	06.1	83	48	67	66	NNE	1	SSE	2	-	0
4	764.2	762.2	761.0	05.8	17.5	10.2	10.9	18.2	05.0	01.7	06.1	05.7	05.1	89	38	55	61	-	0	NNE	4	-	0
5	759.0	756.5	756.1	04.4	14.8	06.0	07.8	15.0	03.3	-01.0	05.2	04.6	06.2	82	37	89	69	-	0	SE	1	-	0
6	755.7	756.7	758.8	05.6	12.4	06.8	07.9	13.0	05.0	01.8	06.2	03.6	02.7	92	34	37	54	-	0	N	6	N	3
7	759.4	757.9	758.3	00.0	09.2	05.4	05.0	10.5	-00.4	-04.2	03.9	03.9	04.8	96	44	72	67	-	0	-	C	NE	2
8	757.9	756.8	756.4	04.6	08.0	06.4	06.4	08.4	03.8	-00.6	05.4	06.6	06.7	85	82	83	87	-	0	-	O	-	0
9	757.3	757.6	760.1	03.8	14.0	11.2	10.0	16.0	02.6	-00.4	05.3	05.0	04.6	88	42	46	59	WNW	1	NNW	2	N	3
10	761.4	761.3	762.2	02.4	14.4	04.8	06.6	14.7	02.0	-01.1	04.9	05.6	05.9	90	45	91	75	-	0	-	O	-	0
11	762.5	759.9	757.6	02.2	11.2	07.8	07.2	12.3	01.8	-01.3	04.8	05.4	06.7	90	54	85	76	-	0	-	C	-	0
12	753.5	752.4	750.9	09.8	10.0	10.8	10.4	12.0	07.0	07.0	07.6	07.7	07.6	83	83	78	81	SE	6	SE	5	SE	6
13	748.4	748.1	749.2	08.8	10.0	06.7	08.0	11.7	06.7	08.0	07.6	07.5	06.7	90	81	91	87	SE	3	SE	2	E	4
14	750.0	751.0	751.6	07.4	07.6	06.4	07.0	10.4	06.2	04.5	03.3	03.0	02.7	43	39	37	40						

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$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vremenska interv.	Oblačnost N (0—10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10	09	07	08.7	01.8	24.0	.	17-8 ³⁰ 0-1 ²⁰ 8 ¹⁰ 13 ¹⁰ 14 ²⁰ FN 16 ⁴⁴ 24 ⁴⁴ 17 ²⁰ 20, F 18 ⁴⁰ 21 ⁰⁵ , D 21.21 ⁴⁵	
2	9	03	00	06	03.0	02.8	21.2	.	F _N 0-1 ³⁰	
3	8	10	07	10	09.0	03.6	00.4	.	0-1 ²⁰ 3 ¹⁰	
4	8	07	10	04	07.0	02.1	.	.	0-1 ¹⁰ 8	
5	7	09	10	10	05.7	01.8	.	.	.	
6	8	08	08	10	08.7	03.5	00.3	.	0-2 ¹⁰ 2 ⁴⁰	
7	7	10	10	10	10.0	00.0	.	.	0-1 ⁸ 14 ¹⁰ , 18-24 ¹⁰	
8	9	06	07	00	04.3	09.4	04.5	.	0-1, F _{NNE} 8 ⁴⁵ 24, F _{NNNE} 11-23 ⁴⁹	
9	8	06	04	00	03.3	08.3	.	.	F _{NNNE} 0-23 ⁴⁰ , F _{NNNE} 0-08 20 ⁰⁸	
10	9	00	00	00	00.0	09.4	.	.	0-1 ¹⁰ 24	
11	8	00	00	00	00.0	09.1	.	.	0-1 ⁰ 8, 19 ³⁰ 24	
12	9	02	07	05	05.3	06.9	.	.	0-1 ⁰ 8, 19 ³⁰ 24	
13	8	05	08	02	05.0	01.7	.	.	0-1 ⁰ 8, 19 ³⁰ 24	
14	9	03	02	00	01.7	09.0	.	.	0-1 ⁰ 8, 19 ³⁰ 24	
15	8	00	00	00	00.0	08.8	.	.	0-1 ⁰ 8, 19 ³⁰ 24	
16	9	00	00	00	00.0	09.1	.	.	0-1 ⁰ 7 ³⁰ 19 ³⁰ 24	
17	9	05	06	03	04.7	08.9	.	.	0-1 ⁰ 7 ³⁰ 19 ³⁰ 24	
18	8	02	07	00	03.0	08.7	.	.	0-1 ⁰ 6-17 ³⁰ 20-24, D 17 ⁴⁵ 18	
19	9	08	08	10	08.7	04.1	.	.	0-1 ⁰ 8, 0-11 ⁵⁰ 16 ⁴⁰ , 0-13 ⁰ 14 ²⁰ , 21 ⁰⁰ 24	
20	9	10	04	03	05.7	06.3	01.1	.	0-1 ⁰ 20 ¹⁰ 24	
21	6	07	10	10	09.0	00.9	.	.	0-1 ⁰ -8, 0-1 ⁵⁰ 16 ⁴⁰ , 0-13 ⁰ 14 ²⁰ , 21 ⁰⁰ 24	
22	8	07	06	04	05.7	07.2	18.6	.	0-1 ⁰ -6 ¹⁰ , 0-1 ³⁰ 24	
23	9	03	03	04	03.3	08.0	.	.	0-1 ⁰ -7 ³⁰ 20 ⁰⁰ 24	
24	9	03	04	04	05.3	00.5	.	.	0-1 ⁰ -7 ³⁰ 19 ³⁰ 24	
25	8	10	10	10	10.0	00.0	00.4	.	0-0 ⁰⁰ 2, 0-0 ⁰⁰ 24, F _{ESE} 22 ³⁰ 23 ⁴⁰ , 23 ³⁷	
26	6	10	10	10	06	08.7	00.5	62.2	.	
27	6	10	10	10	10.0	00.0	06.3	.	0-1 ⁰ -7 ³⁰ 22 ⁰⁵ 22 ⁰⁹	
28	8	10	10	10	10.0	00.0	23.7	.	0-1 ⁰ -7 ³⁰ 18 ⁴⁵ , S 20 ⁵⁵ 22 ³²	
29	8	02	01	10	04.3	08.1	12.9	.	0-1 ⁰ -7 ³⁰ 19 ⁰⁵ 22 ⁰⁰ , F _{N-S} WNW 0 ³⁴ 2 ⁵⁴ , 19 ¹⁴ 19 ⁴⁰	
30	8	08	00	00	02.7	03.6	00.9	.	0-1 ⁰ -6 ³⁰ , 0-1 ⁴⁸ 24	
MES. VRED.		05.8	05.9	05.0	05.6	150.4	156.6			

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1	8	08	10	05	07.7	00.0	.	.	0-1 ⁵⁰ 12 ³⁰
2	8	05	03	07	05.0	02.6	01.1	.	0-1 ⁰ 7 ¹⁰
3	8	08	05	10	07.7	05.5	00.2	.	F _N 15 ¹⁰ 15 ⁵⁵ L
4	9	04	06	00	03.3	05.7	.	.	F _N 10 ⁴⁰ 11 ⁴⁸ L
5	9	04	02	00	02.0	08.6	.	.	.
6	8	10	05	00	05.0	04.0	.	.	0-1 ⁰ -7 ³⁰ , 0-1 ⁴⁵ 8 ⁴⁰ F _N 8 ²⁰ 14 ⁵⁰ , F _N 8 ⁵⁶
7	9	07	08	00	05.0	04.0	01.1	.	0-12 ³⁵ 18 ⁴⁰
8	7	07	10	05	07.3	00.0	.	.	0-19 ⁻ n
9	8	03	08	04	05.0	05.9	00.4	.	0-19 ⁻ n
10	9	00	00	00	00.0	00.0	08.5	.	.
11	7	00	09	10	06.3	04.1	.	.	0-1 ⁰ -8, 0-2 ²⁰ 18 ⁰⁰ L, n-7 ³⁰ F _{ESE} 5 ⁵³ 24, 10 ⁴⁰ 15 ³⁰ F _{ESE} 22 ⁵⁰ 23 ²⁹
12	5	10	10	08	05.3	00.0	17.6	.	F _{ESE} 0-1 ⁴⁰ 12 ⁰⁰ L, F _{ESE} 12 ⁰⁰ 24, 0-1 ⁰ 10 ²⁰ 21 ³⁰ L, n-14 ⁴⁵ 15
13	8	10	10	10	10.0	00.5	24.2	.	F _N 12 ²⁰ 20 ⁰⁵ L, F _N 20 ⁰⁵ 24, F _N 0-23 ⁴⁰ L, F _N 20 ⁰⁵ 24
14	9	10	07	03	06.7	00.0	07.3	.	.
15	8	09	05	03	05.7	03.6	.	.	F _N 0-23 ⁴⁰ L, F _N 20 ⁰⁵ 24
16	9	04	04	00	02.7	07.6	.	.	F _N 0-23 ⁴⁰ L, F _N 6 ⁴⁴ 17 ²⁵
17	9	00	05	08	04.3	07.5	.	.	0-2 ⁰ 6 ⁵⁰ 20 ⁰⁰ L, 0-12 ³⁰ n, F _{NW} 18 ⁵⁰ 20 ³⁴
18	6	10	10	08	05.3	00.0	23.3	.	n-8 ³⁰ , F _N 8 ²⁰ 12 ³⁰ L, F _N 17 ³⁰ n, F _{NW} 18 ⁵⁰ 20 ³⁴
19	9	03	03	00	02.0	08.5	23.3	.	.
20	8	00	04	00	01.3	07.2	.	.	.
21	8	03	03	00	02.0	08.5	.	.	0-1 ⁰ -7 ³⁰
22	9	00	00	00	00.0	08.3	.	.	0-1 ⁰ -8 ³⁰
23	8	00	00	00	00.0	08.6	.	.	0-1 ⁰ -8 ³⁰ 22 ⁴⁰
24	8	02	00	00	00.7	08.5	.	.	0-1 ⁰ -10 ²⁰ 20 ⁴⁰
25	9	00	06	08	04.7	07.6	.	.	0-1 ⁰ -10 ²⁰ 20 ⁴⁰
26	9	03	02	08	04.3	07.7	.	.	0-1 ⁰ -8 ³⁰ 22 ⁴⁰ , F _N 20 ¹⁰ 21 ⁴⁵
27	8	10	00	08	06.0	07.6	.	.	F _N 14 ⁴⁰ 17 ⁴⁸ L, F _N 21 ³⁰ 22 ⁴⁰
28	9	08	02	05	05.0	05.2	.	.	0-1 ⁰ -8, 19 ⁻ n
29	8	03	06	02	03.7	04.0	.	.	0-1 ⁰ -7 ³⁰ 14 ⁴⁵ 14 ⁴⁵ F _N 14 ⁴⁵ 24, 0-17 ⁰⁵ 18 ⁴⁰
30	9	02	06	10	06.0	04.1	.	.	0-1 ⁰ -7 ³⁰ 14 ⁴⁵ 14 ⁴⁵ F _N 14 ⁴⁵ 24, 0-17 ⁰⁵ 18 ⁴⁰
31	7	10	10	05	08.3	00.0	00.0	.	F _N 0-23 ⁴⁰
MES. VRED.		04.9	05.1	04.1	04.7	153.9	75.2		

$\varphi = 41^{\circ}57'$ N $\lambda = 21^{\circ}38'$ E Gr. $\Delta G = +1h\ 27\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min S cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	748.0	747.5	747.6	04.2	05.8	05.6	05.3	06.1	04.0	03.9	06.1	06.7	06.6	98	97	97	97	-	0	-	C	-	0	
2	747.0	746.7	747.1	05.7	08.2	06.4	06.7	08.5	05.4	05.3	06.7	07.3	06.6	97	90	92	93	ENE	1	SSE	2	SSE	2	0
3	746.6	745.7	747.3	06.4	06.8	07.0	07.3	09.5	06.1	05.6	06.0	06.4	05.9	84	75	79	79	SSE	3	S	2	SSF	2	0
4	748.5	749.0	750.4	05.4	08.0	05.8	06.2	08.0	05.2	05.0	06.2	05.4	05.7	91	67	P2	80	SE	1	ESE	2	ENE	1	0
5	749.9	748.7	749.7	04.4	07.2	07.2	04.0	07.4	01.5	03.8	05.4	04.9	04.8	85	64	R9	79	NNE	1	-	0	-	0	0
6	746.7	744.0	744.0	-00.2	04.9	03.6	03.0	05.1	-02.2	-04.1	04.4	05.1	05.6	96	78	94	89	-	0	-	0	-	0	0
7	743.8	743.8	745.6	03.4	06.4	04.2	04.6	06.6	03.4	02.1	05.7	05.9	05.3	97	81	85	68	-	0	SSE	2	NNE	3	0
8	745.7	745.0	745.7	02.4	05.8	02.6	03.4	05.8	02.3	02.1	04.4	04.6	05.2	81	66	94	80	ENE	2	NNE	2	NW	1	0
9	747.1	747.3	746.7	01.8	04.4	03.4	03.2	05.0	01.4	01.4	04.5	04.4	04.9	87	71	85	81	NE	2	NNE	1	SSE	2	0
10	745.3	745.5	746.7	02.6	02.6	02.4	02.5	03.4	02.4	02.5	04.8	04.9	04.8	87	89	89	88	SSE	3	S	3	S	1	0
11	748.2	749.1	751.1	01.0	04.0	02.8	02.4	05.0	00.5	00.2	04.6	05.0	05.2	93	82	94	90	SE	2	SSE	2	-	0	0
12	751.5	750.2	749.9	02.2	04.4	00.2	01.8	04.6	-06.2	01.6	05.0	04.0	04.3	93	74	93	87	-	0	NW	2	WNW	2	0
13	748.8	747.4	749.1	03.0	04.6	-01.5	01.2	05.3	-01.5	-01.4	04.1	03.8	03.1	72	60	75	69	N	5	N	7	E	1	0
14	750.7	749.9	749.9	-03.8	02.2	-03.2	-02.0	02.9	-05.4	-07.2	02.6	02.0	02.9	74	48	81	68	NNE	2	W	1	NE	2	0
15	750.2	749.4	749.5	-06.8	01.4	-04.1	-03.4	02.6	-07.7	-09.6	02.5	03.8	02.9	91	75	86	84	E	1	W	1	SE	1	0
16	749.9	748.6	747.9	-06.7	01.4	00.0	-01.3	03.0	-07.0	-10.6	02.6	03.4	03.8	92	67	82	80	SE	2	-	0	-	0	0
17	744.7	742.5	742.4	-05.0	04.7	01.4	00.6	05.7	-05.0	-07.2	02.7	03.6	04.2	87	56	83	75	-	0	NW	1	N	2	0
18	742.1	741.1	742.1	03.4	03.6	02.2	02.8	06.5	00.6	00.0	04.8	04.4	03.8	82	74	71	76	NNW	3	N	6	NNW	3	0
19	743.5	743.8	744.2	02.2	04.6	01.1	02.2	06.1	01.0	01.5	03.5	04.3	03.9	65	67	78	70	NW	3	NW	4	NE	4	0
20	741.3	740.3	742.0	00.6	08.0	07.8	06.0	09.4	00.1	-01.0	04.5	05.8	05.5	93	72	70	78	-	0	NNE	2	NNW	5	0
21	744.2	744.8	746.8	06.6	07.3	05.4	06.3	08.2	05.3	04.3	04.8	04.8	05.0	66	60	75	67	N	4	NNW	3	NNE	2	0
22	747.7	748.1	749.5	06.4	09.2	06.6	04.2	10.1	06.6	03.9	04.5	04.6	04.3	63	53	89	68	WNW	2	NNW	1	-	0	0
23	749.6	747.7	746.7	-05.0	05.4	00.8	00.5	06.8	-05.4	-07.9	02.7	04.8	04.4	87	72	90	83	-	0	N	2	E	2	0
24	745.9	745.6	745.9	00.4	04.7	01.9	02.2	05.3	00.1	-01.0	04.6	04.5	04.5	96	70	85	84	NNW	1	NNW	3	N	3	0
25	745.5	744.0	745.4	-04.4	03.7	-01.4	-00.9	05.2	-04.8	-07.0	03.2	04.4	03.7	96	74	90	87	-	0	ESE	1	ESE	1	0
26	746.3	746.3	747.0	-01.6	07.1	-00.6	01.1	08.5	-02.0	-03.5	03.9	04.5	04.0	96	59	91	82	ESE	1	SE	1	-	0	0
27	747.0	744.5	744.7	-05.0	06.2	-02.6	-01.0	07.4	-06.0	-08.3	02.9	04.6	03.6	93	65	96	85	E	1	W	1	-	0	0
28	745.6	745.0	745.9	-05.3	05.4	-00.5	-00.4	07.6	-06.5	-08.6	02.9	04.5	03.9	95	67	90	84	S	1	-	0	-	0	0
29	747.2	746.0	746.9	-04.4	08.4	-02.0	00.0	09.6	-05.6	-07.4	03.0	05.0	03.6	92	61	92	82	-	0	WSW	1	S	1	0
30	749.4	749.8	751.3	-05.0	07.0	-00.2	00.4	09.0	-06.0	-08.0	03.2	04.4	04.2	100	65	93	86	-	0	WSW	1	SSE	1	0
31	752.6	751.1	751.3	-00.5	08.1	00.0	C1.9	08.7	-02.4	-05.7	04.1	04.8	03.9	93	59	86	79	-	0	SSW	2	SE	1	0
MES.	WRED. 747.1 746.4 747.1 00.3 05.6 01.6 02.3 06.5 -00.9 -01.8 04.2 04.8 04.5 86 70 86 81 1.3 1.8 1.4																							

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1	750.5	748.0	748.3	-04.0	07.2	-01.4	06.1	09.4	-05.7	-08.2	03.1	04.3	03.8	92	57	91	80	SE	1	W	1	-	0
2	749.0	747.2	748.1	-04.8	07.2	-02.2	-00.5	09.2	-06.5	-08.6	02.9	04.3	03.7	91	57	96	81	-	0	WNW	1	E	1
3	748.8	746.8	746.2	-05.1	09.2	04.5	03.3	10.6	-05.8	-07.9	03.0	05.4	05.3	95	62	84	80	-	0	WNW	1	N	2
4	743.0	740.6	738.3	06.0	05.6	05.4	05.6	10.6	00.9	-00.7	06.0	06.2	05.8	86	92	86	88	SSE	1	NNW	2	SSE	4
5	737.5	737.1	736.1	02.0	05.4	03.7	03.7	06.0	00.7	-00.6	05.1	06.0	05.7	97	85	95	94	-	0	-	0	-	0
6	733.8	730.4	727.5	03.0	09.2	05.4	07.8	10.7	02.8	02.8	05.5	06.8	05.2	97	78	59	78	-	0	WNW	1	SSE	3
7	720.8	720.8	724.5	10.4	09.2	04.0	C6.9	13.0	04.0	07.5	05.8	06.0	05.0	61	69	82	71	S	5	WNW	5	NNE	2
8	730.5	735.5	741.5	03.2	06.4	02.0	C3.0	08.8	04.5	-00.1	04.6	04.0	04.2	80	55	75	70	NNE	4	N	5	N	2
9	745.4	745.5	746.1	-02.8	08.3	-00.4	01.2	09.8	-03.3	-06.0	03.1	03.4	03.8	83	41	85	70	NE	2	NNW	2	-	0
10	746.1	744.9	745.6	-03.1	10.7	00.8	02.2	12.0	-04.6	-07.3	03.3	04.2	04.1	91	45	P4	73	SE	1	-	0	-	0
11	745.4	742.4	741.4	-03.1	12.8	00.4	02.6	14.6	-03.6	-06.7	03.3	04.6	03.9	91	42	82	72	-	0	SW	1	-	0
12	741.2	738.4	738.0	-03.2	12.4	C1.9	03.2	14.3	-04.0	-07.0	03.4	06.2	04.6	93	57	87	79	SE	1	NNW	1	-	0
13	737.7	736.1	736.6	00.3	11.0	0																	

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$$H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$$

Dan	Vjetrost 0-9	Oblačnost N (0-10)					Intencija broj sat	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	3	10≡	10≡	10•	10.0	CC.0	C3.0	.	.	$\equiv^{\circ-10-4^{\circ}0} \equiv^{\circ-14^{\circ}24, \circ-4^{\circ}8^{\circ}24, 21^{\circ}24, \circ-18^{\circ}10^{\circ}19^{\circ}20^{\circ}40$
2	7	10	10•	09	05.7	CC.0	C2.1	.	.	$\equiv^{\circ-9^{\circ}30, \circ-17^{\circ}19^{\circ}i}$
3	7	10	05	09	C9.3	CC.6	C1.6	.	.	$\equiv^{\circ-10^{\circ}30}$
4	7	10	10	10	10.0	00.0	.	.	.	$= 7^{\circ}15, 21^{\circ}24, \square^{\circ-17^{\circ}20^{\circ}30^{\circ}i}$
5	6	10	10	04	CC.0	CC.0	.	.	.	$= 0-24 \sqcup^{\circ-10-10, \circ-10^{\circ}45^{\circ}45^{\circ}}$
6	6	10	08	10	05.3	00.0	.	.	.	$= 0-10^{\circ}6, 14^{\circ}15^{\circ}, \circ-15^{\circ}21^{\circ}40$
7	6	10•	10	10•	10.0	CC.0	C0.1	.	.	$\bullet^{\circ-16^{\circ}24}$
8	7	10	10	10•	10.0	00.0	01.8	.	.	$\bullet^{\circ-1-10^{\circ}i}$
9	6	10	10	10	10.0	00.5	04.3	.	.	$\bullet^{\circ-10^{\circ}18^{\circ}i}$
10	6	10	10•	10•	10.0	CC.0	.	.	.	$\bullet^{\circ-10-10^{\circ}45^{\circ}7^{\circ}15^{\circ}, \circ-17^{\circ}8^{\circ}15^{\circ}, 20^{\circ}25^{\circ}20^{\circ}45^{\circ}, \circ-19^{\circ}24^{\circ}}$
11	7	10•	10	10	10.0	CC.0	C0.8	C5.0	.	$\bullet^{\circ-10-10^{\circ}45^{\circ}7^{\circ}15^{\circ}, \circ-10^{\circ}24^{\circ}, \circ-12^{\circ}35^{\circ}4^{\circ}45^{\circ}, = 18^{\circ}24^{\circ}}$
12	7	10	10	10	10.0	00.0	00.2	.	.	$\equiv^{\circ-12^{\circ}20^{\circ}17^{\circ}30^{\circ}i, F_N 21^{\circ}24^{\circ}i}$
13	7	10	06	00	05.3	01.6	.	.	.	$F_N 6^{\circ}6^{\circ}14^{\circ}16^{\circ}5^{\circ}, \sqcup^{\circ-120^{\circ}24^{\circ}i}$
14	7	00	00	00	00.0	00.0	07.8	.	.	$\sqcup^{\circ-1-2^{\circ}6^{\circ}22^{\circ}24^{\circ}i}$
15	6	02	03	03	02.7	06.7	.	.	.	$\sqcup^{\circ-10^{\circ}10^{\circ}24^{\circ}i}, = 7^{\circ}24^{\circ}$
16	6	03	10	10	07.7	05.0	.	.	.	$= 0-24 \sqcup^{\circ-10-12^{\circ}0}$
17	7	00	09	10*	06.3	03.2	.	.	.	$= 0-12^{\circ}20^{\circ}17^{\circ}30^{\circ}i, F_N 13^{\circ}14^{\circ}45^{\circ}i$
18	7	10	08•	06	08.0	C1.1	C1.8	.	.	$F_N 3^{\circ}4^{\circ}11^{\circ}13^{\circ}5^{\circ}, \bullet^{\circ-17^{\circ}24^{\circ}11^{\circ}16^{\circ}08^{\circ}17^{\circ}i, 21^{\circ}22^{\circ}40^{\circ}i$
19	7	08	09	07	08.0	02.1	00.0	.	.	$\bullet^{\circ-10^{\circ}6^{\circ}25^{\circ}24^{\circ}i}, = 7^{\circ}9^{\circ}5^{\circ}$
20	8	10•	09	07	08.7	00.1	00.0	.	.	$\bullet^{\circ-10^{\circ}6^{\circ}25^{\circ}24^{\circ}i}, = 7^{\circ}24^{\circ}$
21	8	08	10	10	05.3	00.0	CC.1	.	.	$\bullet^{\circ-10^{\circ}25^{\circ}i}, \bullet^{\circ-15^{\circ}13^{\circ}F_N 3^{\circ}4^{\circ}5^{\circ}i}, 7^{\circ}10^{\circ}$
22	7	09	09	00	06.0	CC.5	.	.	.	$\sqcup^{\circ-10^{\circ}10^{\circ}3^{\circ}6^{\circ}12^{\circ}15^{\circ}24^{\circ}i}, = 0-1-2^{\circ}11^{\circ}6^{\circ}26^{\circ}, \sqcup^{\circ-2^{\circ}22^{\circ}24^{\circ}i}, \blacksquare$
23	7	06	08	10	08.0	01.4	.	.	.	$= 0-10^{\circ}6^{\circ}25^{\circ}24^{\circ}i, = 4^{\circ}24^{\circ}$
24	7	10*	050	07	07.3	C1.5	15.8	04	.	$= 0-4^{\circ}45^{\circ}i, = 0-9^{\circ}20^{\circ}24^{\circ}i$
25	6	01	060	02	03.0	04.5	00.0	.	.	$\sqcup^{\circ-1-2^{\circ}6^{\circ}24^{\circ}i}, = 4^{\circ}24^{\circ}$
26	6	06	030	00	03.0	C3.5	C3.5	.	.	$= 0-4^{\circ}45^{\circ}i, = 0-9^{\circ}20^{\circ}24^{\circ}i$
27	7	02	000	00	00.7	C7.5	.	.	.	$\sqcup^{\circ-1-2^{\circ}6^{\circ}24^{\circ}i}, = 4^{\circ}24^{\circ}$
28	6	01	020	00	C1.0	C5.9	.	.	.	$\sqcup^{\circ-1-2^{\circ}6^{\circ}24^{\circ}i}, = 0-16^{\circ}45^{\circ}$
29	6	08	010	00	03.0	07.5	.	.	.	$\sqcup^{\circ-10^{\circ}9^{\circ}20^{\circ}24^{\circ}i}, = 3^{\circ}24^{\circ}, = 6^{\circ}30^{\circ}655$
30	6	00	020	00	C0.7	C6.6	.	.	.	$\sqcup^{\circ-10^{\circ}8^{\circ}20^{\circ}24^{\circ}i}, = 0-15^{\circ}35^{\circ}19^{\circ}24^{\circ}i, \square^{\circ-17^{\circ}45^{\circ}21^{\circ}24^{\circ}i}$
31	6	09	050	08	07.3	05.4	.	.	.	
MES. WRED.		07.2	07.2	06.2	06.9	75.4	25.9			

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1	6	02	020	00	01.3	C7.3	.	.	$\sqcup^{\circ-10-9^{\circ}24^{\circ}i}, = 0-16^{\circ}20^{\circ}24^{\circ}i$	
2	5	02	020	00	01.3	06.7	.	.	$\sqcup^{\circ-10^{\circ}24^{\circ}i}, = 6^{\circ}20^{\circ}50^{\circ}$	
3	6	00≡	010	06	C2.3	C5.5	.	.	$= 0-6^{\circ}20^{\circ}8^{\circ}9^{\circ}20^{\circ}13^{\circ}5^{\circ}, \bullet^{\circ-19^{\circ}16^{\circ}i}$	
4	6	10	10•	08	C9.3	C1.0	.	.	$\bullet^{\circ-11^{\circ}20^{\circ}24^{\circ}i}, = 2^{\circ}3^{\circ}9^{\circ}24^{\circ}i, = 9^{\circ}23^{\circ}23^{\circ}, = 0-12^{\circ}23^{\circ}40^{\circ}i$	
5	6	10≡	10	10	10.0	CC.0	08.8	.		
6	6	10≡	03	10	07.7	03.4	.	.	$\sqcup^{\circ-10-10^{\circ}40^{\circ}i}, = 10^{\circ}30^{\circ}F_N 21^{\circ}24^{\circ}i$	
7	7	10	10•	06	08.7	00.0	.	.	$\sqcup^{\circ-1-2^{\circ}6^{\circ}24^{\circ}i}, = 0-24^{\circ}$	
8	8	09	09•	05	07.7	C5.5	C3.5	.	$\sqcup^{\circ-1-2^{\circ}6^{\circ}24^{\circ}i}, = 0-16^{\circ}45^{\circ}$	
9	8	01	010	02	01.3	C9.2	00.0	.	$\sqcup^{\circ-10-6^{\circ}20^{\circ}24^{\circ}i}, = 4^{\circ}24^{\circ}$	
10	7	08	070	00	05.0	C8.6	.	.	$\sqcup^{\circ-10-8^{\circ}24^{\circ}i}, = 21^{\circ}24^{\circ}$	
11	7	00	000	00	00.0	CC.0	C8.8	.	$\sqcup^{\circ-10-9^{\circ}20^{\circ}24^{\circ}i}, = 7^{\circ}12^{\circ}30^{\circ}$	
12	7	00	010	00	00.2	C8.2	.	.	$\sqcup^{\circ-1-2^{\circ}6^{\circ}24^{\circ}i}, = 12^{\circ}11^{\circ}F_N 21^{\circ}22^{\circ}59^{\circ}i$	
13	6	10	080	10	09.3	01.9	.	.	$\bullet^{\circ-1-6^{\circ}40^{\circ}7^{\circ}15^{\circ}11^{\circ}02^{\circ}45^{\circ}i}, F_N 7^{\circ}14^{\circ}20^{\circ}i$	
14	7	10	10•	10	10.0	CC.3	00.0	02.1	.	$\bullet^{\circ-1-6^{\circ}40^{\circ}7^{\circ}15^{\circ}11^{\circ}02^{\circ}45^{\circ}i}, F_N 7^{\circ}14^{\circ}20^{\circ}i$
15	7	10•	10•	10•	10.0	00.0	02.1	.		
16	5	10≡	07	03	06.7	C2.0	38.2	.	$\bullet^{\circ-0-20^{\circ}4^{\circ}5^{\circ}7^{\circ}24^{\circ}i}, = 5^{\circ}6^{\circ}7^{\circ}24^{\circ}i, = 6^{\circ}7^{\circ}7^{\circ}24^{\circ}i, = 0-19^{\circ}24^{\circ}i$	
17	7	05	08	05	06.0	06.7	.	.	$\overline{F_N 10^{\circ}39^{\circ}10^{\circ}39^{\circ}}i$	
18	7	10	05	10	05.7	CC.7	.	.	$F_N 17^{\circ}24^{\circ}15^{\circ}26^{\circ}i, \bullet^{\circ-17^{\circ}50^{\circ}9^{\circ}30^{\circ}i}$	
19	7	10	09	10	05.7	01.0	.	.	$\bullet^{\circ-1-2^{\circ}6^{\circ}45^{\circ}i}, = 7^{\circ}24^{\circ}$	
20	6	10•	10•	08	C9.3	00.0	15.2	.		
21	7	08	08	07	07.7	02.4	12.0	.	$\bullet^{\circ-0-20^{\circ}4^{\circ}5^{\circ}7^{\circ}24^{\circ}i}, = 6^{\circ}7^{\circ}7^{\circ}24^{\circ}i, = 0-19^{\circ}24^{\circ}i$	
22	7	10	06	10	C9.7	C2.5	.	.	$\overline{F_N 10^{\circ}39^{\circ}10^{\circ}39^{\circ}}i$	
23	7	10	05	08	CC.0	01.0	.	.	$F_N 17^{\circ}24^{\circ}15^{\circ}26^{\circ}i, \bullet^{\circ-17^{\circ}50^{\circ}9^{\circ}30^{\circ}i}$	
24	7	10	09	10	10.0	CC.1	.	.	$\bullet^{\circ-1-2^{\circ}6^{\circ}45^{\circ}i}, = 7^{\circ}24^{\circ}$	
25	7	10	10	10	10.0	CC.2	.	.		
26	7	10	06	10•	05.7	00.1	.	.	$\bullet^{\circ-20^{\circ}21^{\circ}i}, F_N 18^{\circ}22^{\circ}25^{\circ}i$	
27	8	10	06	C5	08.0	03.1	00.0	.	$\sqcup^{\circ-19^{\circ}24^{\circ}i}$	
28	7	C9	010	00	C3.3	C8.6	.	.		
MES. WRED.		07.6	06.8	C6.2	06.9	96.5	79.9			

$\varphi = 41^{\circ}57'$, N $\lambda = 21^{\circ}38'$, E Gr. $\Delta G = +1h\ 27\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)							
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	744.9	742.5	742.4	-05.0	07.0	-00.0	00.1	08.6	-05.4	-08.6	03.0	03.0	03.4	95	40	78	71	-	0	ENE 1	-	0		
2	741.5	739.2	739.6	-05.0	08.4	04.6	03.2	09.6	-05.0	-08.0	02.9	03.4	02.8	91	41	60	64	-	0	S 1	SSE 1			
3	741.7	743.9	746.7	-03.7	06.6	04.6	04.9	07.1	03.6	01.4	04.4	05.4	05.0	74	73	76	75	SSE 2	SSF 4	SSF 2				
4	748.5	748.3	748.3	02.6	07.7	05.2	05.2	08.2	06.3	-01.7	05.0	05.4	05.9	90	68	64	82	-	0	SSE 3	SSE 3			
5	746.4	744.5	742.9	05.0	06.9	05.0	05.4	07.0	04.8	04.2	05.8	05.8	05.7	86	75	87	85	SE 3	SE 4	SE 4	SSE 4			
6	739.6	736.6	739.5	05.0	04.4	03.6	04.2	05.7	03.6	04.5	05.8	05.5	06.4	86	84	91	88	SE 2	NNE 3	NF	2			
7	739.0	740.4	742.0	03.2	04.0	02.4	03.0	04.6	02.4	-02.4	05.2	05.0	04.1	91	82	74	82	N 1	NNE 4	NNE 4				
8	742.9	743.0	743.4	01.4	03.4	00.8	01.6	04.3	04.8	-00.2	04.2	04.9	04.6	83	85	95	88	NNE 2	-	0	ESE 1			
9	743.7	743.6	745.1	01.6	05.2	06.0	04.9	07.0	00.4	00.2	05.0	05.8	06.3	97	83	90	90	-	0	NW 2	SE 2			
10	744.9	744.3	744.6	05.0	08.9	06.0	06.5	09.4	04.4	04.1	05.8	05.4	05.1	88	63	73	75	E 2	SSE 2	NNE 3				
11	745.2	746.2	747.7	04.0	08.4	04.7	05.4	09.2	03.5	03.4	04.5	04.7	04.8	72	57	75	68	N 2	WW 2	NE 5				
12	748.9	747.7	747.1	02.8	09.7	01.4	03.7	09.4	01.4	02.8	04.4	05.2	04.4	78	60	87	75	NNE 4	WW 2	-	0			
13	745.7	745.2	740.9	-01.9	12.6	03.0	04.2	14.0	-02.4	-05.4	03.7	04.7	04.6	92	43	81	72	-	0	SW 2	E 1			
14	738.9	734.1	732.7	00.8	10.5	08.4	07.0	11.3	00.0	-02.0	04.4	05.1	04.3	90	53	52	65	ENE 1	NW 2	N 3				
15	731.3	732.1	733.6	03.8	06.8	05.0	05.2	08.4	02.7	03.6	05.6	05.4	05.9	92	72	90	85	NNW 1	WW 1	NNE 2				
16	734.2	734.9	736.4	03.8	07.8	04.4	05.1	08.7	03.8	03.5	05.1	04.8	05.2	85	60	82	76	NNE 3	NE 1	NNE 2				
17	737.2	736.9	739.7	-00.6	14.5	05.6	06.3	16.3	-01.7	-03.8	04.2	04.6	05.1	94	37	75	69	ENE 1	W 2	ESE 2				
18	742.6	740.9	741.9	00.9	18.6	11.8	10.8	21.1	-00.6	-03.0	04.3	05.8	05.9	88	36	57	60	-	0	S 1	SE 2			
19	745.3	743.5	744.7	02.1	20.6	14.0	12.8	23.0	01.7	-00.8	04.9	06.3	06.3	92	34	53	60	ESE 1	W 1	ESE 2				
20	747.1	744.9	745.6	04.6	22.6	10.8	12.2	24.2	03.0	00.0	05.8	06.4	07.0	91	31	72	65	-	0	NW 1	E 1			
21	747.1	744.7	745.6	06.7	23.6	11.2	13.2	25.2	04.6	01.7	06.3	06.9	06.9	85	32	65	62	-	0	WSW 1	-	0		
22	746.1	742.9	742.4	05.2	23.0	10.6	12.5	25.9	03.4	01.0	06.1	06.0	06.5	89	28	68	62	-	0	ESE 1	E 1			
23	743.9	741.7	742.2	06.0	23.2	14.1	14.4	25.2	04.6	01.9	06.2	05.4	06.6	89	28	55	57	-	0	SSW 1	ESE 1			
24	745.6	743.5	744.7	06.0	22.0	16.2	15.4	22.9	04.7	02.4	06.6	07.2	07.9	89	36	57	61	NE 1	S 3	SE 4				
25	746.0	744.2	742.9	07.9	19.0	13.0	13.2	19.9	06.2	04.2	07.1	07.0	07.3	89	43	65	65	NE 1	SSW 3	S 3				
26	746.1	742.4	741.7	05.8	17.6	10.6	11.6	18.7	06.9	04.1	07.0	07.6	07.1	83	50	74	65	SSF 2	S 2	SE 3				
27	740.5	737.2	736.8	06.4	16.6	13.4	13.0	20.2	06.4	05.1	07.2	07.0	06.3	87	56	81	75	SE 2	-	0	NE 3			
28	740.3	739.6	742.7	07.0	20.4	11.6	12.6	20.8	05.1	03.0	07.1	08.5	09.5	95	47	73	78	-	0	SSF 2	W 2			
29	744.7	745.0	745.2	10.4	14.4	09.2	10.8	15.7	09.2	08.8	07.5	07.0	06.8	79	57	78	71	SSE 2	SSE 3	SSE 3				
30	747.5	747.0	746.7	08.6	11.3	09.7	10.6	13.6	08.0	06.6	06.7	06.8	05.3	80	65	58	68	SSE 3	SSE 5	SSE 2				
31	745.9	745.3	745.3	07.2	14.2	09.2	10.0	16.0	06.6	04.5	06.5	06.7	06.2	85	38	71	65	SSE 2	N 2	ESE 2				
MES.	WRED.			741.3	742.0	742.3	03.9	12.0	07.6	09.0	14.2	02.8	01.3	05.4	0F.7	05.9	87	54	74	72	1.2	2.0	2.1	

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1	740.7	733.4	740.6	04.6	15.6	10.7	10.2	16.0	03.5	00.6	05.9	05.5	04.5	91	42	46	60	-	0	ESE 2	E 3		
2	742.1	741.7	744.0	06.1	15.8	08.0	09.6	15.9	04.0	01.5	05.1	05.9	04.3	73	44	52	57	ESE 1	SW 1	ENE 2			
3	744.1	743.9	743.9	03.4	14.0	05.0	06.6	16.0	00.3	-02.4	04.1	03.0	04.0	70	25	61	52	NE 3	SSE 2	SSE 1			
4	744.3	741.3	741.0	02.7	14.6	07.4	09.3	15.9	-01.8	04.4	04.3	05.4	04.8	80	43	62	62	SE 1	SE 2	E 1			
5	742.2	740.2	740.9	03.2	16.2	11.2	10.5	16.4	00.1	-01.7	04.9	05.9	06.1	84	43	61	63	-	0	SE 2	SSE 4		
6	742.0	740.7	740.3	05.0	13.1	09.0	09.6	13.2	03.6	02.0	06.6	07.0	06.5	82	62	76	73	NF 1	SSE 3	SE 2			
7	741.1	738.3	739.0	06.0	16.2	13.1	12.1	16.4	04.4	02.9	06.4	05.0	04.5	92	36	35	56	-	0	W 2	NW 3		
8	738.3	739.0	739.2	10.0	10.3	08.8	09.5	13.3	06.1	05.0	05.4	06.5	06.0	59	69	71	66	W 2	WW 2	WW 2			
9	737.8	740.7	742.2	05.8	12.4	05.8	07.4	14.7	04.0	01.8	05.4	04.8	05.2	78	45	75	66	NE 1	N 4	NNE 2			
10	743.0	740.2	739.0	03.9	17.8	12.1	11.5	18.0	01.0	-01.7	04.7	04.6	05.2	76	30	49	52	ENE 1	SSW 1	SSE 3			
11	737.7	737.4	736.5	05.6	10.2	07.4	08.6	13.6	07.4	05.4	05.8	05.9	06.3	65	63	82	70	SSE 2	SE 4	SE 2			
12	735.1	734.2	734.9	07.8	14.2	05.8	10.4	14.8	06.1	05.3	07.1	07.1	07.8	90	59	86	78	-	0	SSE 2	SE 2		
13	736.1	734.2	734.4	08.2	19.7	11.2	12.6	21.2	07.8	05.6	07.9	07.4	07.0	97	43	70	70	E 1	S 2	E 1			
14	732.7	728.3	729.3	11.1	16.0	09.8	11.7	18.7	08.0	06.4	08.3	08.5	07.8	84	62	85							

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$$H_s = 232 \text{ m} \quad H_b = 233.3 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.3 \text{ m}$$

Dan	Vlhkost 0-9	Oblačnost N (0-10)					Insolacia pri sadi broj	Padavina R mm	Snežní pokrývka h cm	Razoví vremena w
		14	7	14	21	Sred Dies				
1	7	03	C20	00	C1.7	07.4	.	.	L ⁰⁻¹⁰⁻⁹ 21 ³⁰ 24 = B ⁰⁻¹¹ 30 ⁰ 19 ²⁰ 21 ³⁰	
2	7	000	C30	10	C4.3	C7.2	.	.	L ⁰⁻¹⁰⁻⁸ 20 ⁰ = T ¹⁰ 15 ⁰ , D ¹⁸⁻²¹ 05 ⁰	
3	7	10	08	10	C9.7	C1.1	00.0	.	B ⁰⁻⁶ 35 ⁰ 11 ³⁰ 1	
4	7	10	10	10	10.0	00.0	C0.1	.	B ⁰⁻¹⁶ 00 ⁰ 24 ⁰	
5	7	10•	10•	10	10.0	00.0	CC.2	.	B ⁰⁻⁰ 22 ⁰ C	
6	7	10•	10•	10•	10.0	00.0	C1.7	.	B ⁰⁻¹⁴ 10 ⁰ 24 ⁰ L ⁰⁻¹⁷ 45 ⁰ B ⁰ 22 ⁰ 23 ⁴⁷	
7	7	10•	10•	10	10.0	00.0	09.5	.	B ⁰⁻¹⁰ 35 ⁰ 10 ³⁰ 18 ³⁰ i ¹⁰⁻¹ 00 ⁰ 10 ³⁰ i	
8	6	10	10	10*	10.0	00.0	00.3	.	* ⁰⁻¹⁶ 45 ⁰ 11 ³⁰ 20 ⁴⁵ 23 ⁴⁵ * ⁰⁻⁸ 95 ⁰ 9 ¹⁵ 9 ⁴⁵ * ⁰⁻¹¹ 30 ⁰ 12 ⁰ 18 ¹² 20 ⁴⁵ = 12 ⁰ 24.	
9	5	10•	10•	10	10.0	00.0	C6.1	.	= 0-20 ³⁰ * ⁰⁻²⁸ 0 ²⁵ 0 ²⁵ 0 ³⁰ 18 ⁵⁵ i ⁰⁻¹ 18 ⁰⁵ 21 ⁴⁰ i	
10	7	10	090	10	05.3	00.4	00.7	.	* ⁰⁻¹⁰ 20 ⁰ 19 ⁴⁰ / ⁰⁻¹⁹ 40 ⁰ 23 ⁴⁷	
11	7	10	08	10	05.7	00.0	00.1	.	B ⁰⁻¹⁰ 35 ⁰ FNE 18 ⁵⁰ 21 ³⁰ i	
12	7	10	09	00	06.0	C2.9	.	≡ 23 ³⁰ 24		
13	7	000	C20	00	00	C1.7	C4.8	.	≡ 0-14 ²⁰	
14	6	10	10	10•	10.0	00.2	.	L ⁰⁻¹⁰ 45 ⁰ 10 ³⁰ 22 ⁰ - 24		
15	6	10•	10•	10•	10.0	00.0	C1.3	.	L ⁰⁻¹⁰ 35 ⁰ 13 ²⁵ 24 ⁰ i ⁰⁻¹² 7 ³⁰ 10 ³⁰ i ⁰⁻²⁵	
16	7	10•	10	09	05.7	00.0	C1.8	.	B ⁰⁻¹⁰ 30 ⁰ 10 ²² 13 ¹⁵ i 17 ³⁰ 18 ¹⁰ i B ⁰⁻¹¹ 2 ¹⁷ 6 ³⁰ P05 ⁰	
17	7	09	020	00	C3.7	C4.4	00.0	.	L ⁰⁻² 30 ⁰ 8 ¹⁵ 0 = 5 ²⁰ 11 ³⁰	
18	7	030	030	00	02.0	10.2	.	L ⁰⁻⁵ 24 ³⁰ 24 ⁰ L ⁰⁻⁵ 07 ⁴⁵		
19	8	050	010	00	C2.0	C6.9	.	L ⁰⁻¹² 0 ²⁰ 24 ⁰ B ⁰⁻⁸ 24 ³⁰ 24		
20	8	000	050	02	02.3	09.3	.	L ⁰⁻⁶ 0 ²⁰ 20 ⁴⁰ 24		
21	9	070	010	00	C2.7	10.8	.	A ⁰⁻¹⁰ 8		
22	7	000	000	00	00.0	10.2	.	A ⁰⁻¹⁰ 8 ⁴⁵		
23	7	010	010	01	C1.0	10.4	.	A ⁰⁻²⁵ 9 ¹⁰		
24	8	000	020	02	01.3	09.9	.	A ⁰⁻³ 8 ⁴⁵ FSE 20 ⁰³ 20 ⁴⁶		
25	7	020	10	00	04.0	C5.7	.	A ⁰⁻⁴ 07 ³⁰		
26	7	10	010	01	04.0	07.6	.	L ⁰⁻³³ 7 ³⁰ 21 ³⁰ 24 = 5 ³⁰ 13 ²⁰		
27	6	10	030	10•	07.7	C5.4	.	L ⁰⁻⁰ 45 ⁰ = 3 ²⁰ 17 ²³ FNE 17 ²³ 18 ³¹ TS 17 ²⁵ 18 ³³ , FS 17 ⁵⁶ 18 ⁴⁵ □ ⁰⁻¹⁷ 55 ⁰ 18 ⁰ □ ⁰⁻¹⁷ 55 ⁰ 18 ⁰ □ ⁰⁻¹		
28	7	010	030	10•	04.7	07.0	03.1	.	FSNE 14 ⁵⁴ 16 ³⁰ , □ ⁰⁻¹⁵ 05 ⁰ 20 ⁴⁰ i, T K 17 ⁵⁶ [16-23-15 ⁵⁵]	
29	7	10	09	10	C5.7	C1.8	05.0	.	F ⁰⁻³³ 12 ⁵⁵ 14 ⁵⁰ i	
30	7	10	10	10	10.0	00.2	.	F ⁰⁻³³ 12 ⁵⁵ 14 ⁵⁰ i, □ ⁰⁻¹² 21 ⁴⁰		
31	7	10•	10	10	10.0	C3.4	00.0	.	• ⁰⁻⁶ 45 ⁰ B ⁰ 15-18 ³⁰ i, FSE 14 ⁴⁰ 16 ⁵⁰	
MES.		✓REFD.	06.8	06.2	06.0	06.3	137.2	29.9		

S&CP.JF - PETRO VAC

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$\varphi = 41^{\circ}57'$ N $\lambda = 21^{\circ}38'$ E Gr. $\Delta G = +1j 27$ min.

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D&T	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%			Pravac i jačina veta D, I (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	727.1	726.8	727.2	11.2	15.4	11.4	12.4	15.8	05.2	07.5	07.3	07.3	06.6	73	56	85	71	SSE 2	S 5	ESE 1
2	728.5	729.0	731.7	10.0	19.2	14.6	14.6	20.1	08.3	06.5	08.3	07.6	06.5	90	46	68	68	SSF 1	WNW 1	NNE 4
3	734.0	735.4	736.6	12.4	20.4	12.6	14.5	21.4	09.6	05.5	06.5	06.8	07.7	78	38	70	62	-	0	N 1
4	737.7	735.6	736.8	11.6	21.2	16.0	16.2	23.0	08.3	05.8	08.6	06.6	07.3	84	35	54	56	SSW 1	SSE 4	NW 1
5	735.2	734.8	734.9	11.6	11.1	07.2	09.3	16.1	07.0	10.5	09.8	08.6	07.0	95	86	92	91	S 2	SE 3	NE 1
6	736.8	736.7	738.3	07.4	14.2	12.0	12.4	14.6	02.6	00.9	07.5	08.1	07.3	97	52	70	73	NE 1	SE 2	ENE 1
7	740.8	740.1	741.1	11.0	20.5	14.6	15.3	21.1	08.4	05.1	08.7	06.5	08.2	88	36	65	63	SE 1	ESE 1	NNW 3
8	742.7	740.2	738.8	10.6	18.6	12.4	13.5	19.4	06.1	03.0	08.0	06.5	08.7	84	40	80	68	S 1	S 2	SSF 3
9	737.2	736.6	737.7	11.0	19.6	11.6	12.2	17.0	08.6	05.7	08.9	06.2	06.8	91	47	69	66	NW 2	N 5	NNE 4
10	733.5	737.9	739.9	09.6	15.0	09.3	10.8	15.8	09.3	08.4	08.1	06.7	07.0	90	52	79	74	-	0	WNW 3
11	741.3	740.3	740.6	07.2	21.6	12.2	13.3	23.2	01.8	-00.6	07.0	05.7	07.4	91	30	70	64	-	0	W 2
12	743.1	740.8	741.7	10.4	25.2	17.2	17.5	25.8	05.2	02.0	07.7	07.8	06.3	81	33	63	59	-	0	SSE 3
13	744.4	744.5	745.8	14.0	21.4	14.2	16.0	22.0	09.4	06.8	10.0	07.5	08.2	83	39	68	63	SW 1	NNE 5	ENE 3
14	745.9	742.9	741.9	11.0	23.4	18.0	17.6	24.2	05.5	02.9	08.3	08.3	09.0	84	39	58	60	-	0	ESE 2
15	741.7	738.7	739.9	12.2	16.3	13.0	13.9	18.3	09.6	07.5	09.4	11.1	10.5	83	80	93	85	-	0	NE 2
16	732.1	737.6	740.3	10.6	14.0	08.2	10.8	16.4	06.6	04.4	08.0	07.6	07.7	84	56	95	78	-	0	NE 2
17	742.1	740.5	741.8	08.0	20.0	15.1	14.6	21.0	04.1	02.0	07.4	07.4	09.1	92	42	71	68	-	0	ESE 2
18	742.3	737.0	737.0	12.3	16.2	13.4	14.0	17.1	10.4	08.6	09.5	08.3	07.5	89	58	65	71	-	0	NNW 4
19	741.2	741.0	741.0	10.4	14.2	12.9	12.6	18.0	10.0	09.2	10.1	09.9	98	84	89	90	N 2	NNE 1	WNW 1	
20	741.7	740.1	739.9	11.1	20.8	17.6	14.6	21.8	10.5	09.5	09.9	10.4	10.0	93	57	90	80	5	1	-
21	741.0	740.0	741.0	12.4	14.4	14.6	14.5	23.6	08.4	06.4	09.8	10.8	10.2	91	77	82	82	-	0	SW 1
22	741.7	739.1	739.5	14.1	23.5	17.6	17.7	24.1	10.1	08.3	10.4	09.1	10.3	86	42	73	67	-	0	N 2
23	734.7	735.7	734.9	10.9	11.3	09.8	10.0	16.7	08.8	09.4	08.6	08.7	07.9	86	86	92	88	N 5	N 1	SSF 2
24	735.9	736.9	737.7	10.4	17.2	12.6	13.2	18.7	08.6	06.0	09.0	09.9	10.2	95	67	93	85	-	0	N 1
25	732.2	731.0	731.0	10.6	21.4	17.4	16.7	23.2	08.0	06.5	09.4	13.9	13.6	99	73	91	87	-	0	NW 2
26	742.4	742.6	742.3	15.6	20.0	14.0	14.6	21.7	12.5	08.8	08.4	08.3	67	47	70	61	KNE 5	K 2	NNE 1	
27	742.0	740.5	742.5	12.9	23.2	18.8	16.9	24.6	07.9	05.1	09.4	09.2	08.9	85	38	66	63	-	0	NW 2
28	739.9	736.0	735.7	15.0	24.4	19.4	19.6	25.2	09.0	07.0	09.3	09.9	10.1	72	39	60	57	-	0	S 2
29	732.6	730.4	731.6	16.4	17.2	14.0	14.6	23.0	12.6	09.5	10.3	11.7	10.0	73	79	83	78	W 2	NNW 2	NNE 3
30	740.7	741.4	742.8	15.2	23.7	17.7	18.6	25.4	13.0	12.5	10.9	11.7	12.5	84	51	82	72	NNE 1	NW 2	E 1
31	741.0	739.0	742.2	15.6	26.0	20.3	20.6	26.7	12.3	10.4	11.8	13.0	13.0	90	51	73	71	ESE 1	SE 2	ESE 2
MES.	739.4	738.6	739.0	11.0	19.2	13.9	14.7	21.0	08.5	06.7	09.0	08.7	09.0	86	53	76	72	0.9	2.2	1.7

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1	741.4	739.6	739.0	10.6	24.8	21.2	22.0	28.2	14.6	10.1	12.9	12.4	13.6	75	47	72	66	-	0	ESE 2
2	741.4	739.2	739.8	10.4	20.0	15.2	17.6	22.4	15.6	14.9	12.9	11.9	09.6	81	68	71	73	NF 2	N 5	NE 3
3	743.5	744.0	745.6	14.8	16.7	14.4	16.1	16.7	12.9	13.3	09.1	08.2	08.6	72	57	72	67	NF 3	NNE 5	-
4	742.3	744.3	743.9	14.9	24.9	18.8	19.2	26.0	09.2	07.4	10.0	12.2	11.4	82	52	70	68	-	0	KSW 2
5	744.3	742.3	741.2	17.0	27.2	17.4	19.8	28.7	10.8	08.6	11.8	11.2	11.6	81	36	74	65	N 1	SW 1	-
6	741.8	740.4	739.0	17.0	28.4	22.4	22.6	29.6	11.6	09.2	11.5	11.8	10.7	79	41	53	58	SE 1	SSE 1	ESE 1
7	739.8	740.8	740.2	19.6	22.9	16.5	19.0	27.0	15.6	14.6	13.0	13.2	12.0	76	63	84	74	-	0	ENE 1
8	744.2	742.9	742.3	16.2	21.2	15.0	16.3	22.0	13.9	12.4	09.9	09.7	09.3	72	51	72	65	NF 2	NE 2	ESE 1
9	742.4	749.6	738.7	14.0	25.3	20.4	20.0	26.3	06.9	06.9	09.5	12.7	11.4	79	53	64	65	-	0	SE 4
10	739.3	736.9	736.4	19.3	26.6	20.4	20.6	27.0	15.0	12.4	10.9	11.2	12.6	63	43	70	59	S 1	SSE 4	SSE 2
11	732.4	731.3	735.7	20.4	16.0	14.0	16.3	26.0	14.0	11.5	10.1	09.3	07.4	56	65	62	61	SSE 4	NNW 6	NW 3
12	735.0	734.0	734.0	14.6	20.0	10.4	14.1	20.8	10.6	10.6	06.2	06.9	07.4	50	36	77	55	NW 4	NN 4	-
13	735.9	736.2	736.4	16.0	13.3	11.4	11.6	14.2	08.0	05.5	07.8	07.8	08.7	95	66	86	79	ESL 1	NNE 4	SE 1
14	737.6	737.5	738.6	13.4	22.5	13.6	15.8	23.6	09.8	07.7	08.9	07.0	08.1	77	34	65	60	-	0	E 2
15	741.6	740.2	739.1	12.7	24.4	16.8	17.9	26.6	05.2	03.2	06.1	07.9	10.2	73	32	71	59	E 1	S 2	E 1
16	739.5	738.1	738.4	17.1	25.4	17.0	19.1	25.6	14.4	12.5	11.2	11.5	13.7	77	47	94	73	ESF 2	SSW 2	SSW 1
17	739.3	737.2	738.2	16.6	24.3	15.4	19.4	25.0	16.0	15.3	13.3	11.5	13.3	94	50	79	74	NNW 1</		

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$$H_s = 232 \text{ m} \quad H_b = 233.3 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.3 \text{ m}$$

SKOPJE - PETROVAC

1974 J.L.H.

1	7	06	040	C2	05.0	05.2	.	.	$\Delta^{0-10-8^{\text{so}}}$	$20-24^{\text{so}}$	$= 5^{\text{so}} 9^{\text{th}}$	T 1407 1540	$\zeta 19^{\text{so}} 22^{\text{th}}$	
2	7	06	09	C0	08.3	02.7	CC.6	.	$\Delta^{+2-0-3^{\text{so}}}$	$\zeta 1^{\text{so}} 2^{\text{th}}$	F_N	NNE 158 425 1255 1810	T 2 420 $\bullet 0-13^{\text{so}} 4^{\text{th}}$	
3	7	10	10	C5	05.7	00.0	01.5	.	$F_{NNW} 10^{\text{so}} 16^{\text{th}}$					
4	7	03	06	C1	01	03.3	11.9	.	$\Delta^{+2-14^{\text{so}}}$	$\zeta 5^{\text{so}} 30^{\text{th}}$				
5	7	00	C1	CC	00.3	12.8	.	.	$\Delta^{+2-10-9^{\text{so}}}$	$\zeta 4^{\text{so}} 30^{\text{th}}$				
6	7	02	03	C2	02.3	11.9	.	.	$\Delta^{+1^{\text{so}} 8^{\text{th}}}$	$T 1245 1930$	$\zeta 19^{\text{so}} 23^{\text{th}}$			
7	7	06	05	R4	04	06.3	04.7	CC.1	.	$\bullet 0-12^{\text{so}} 0^{\text{th}}$	$\zeta 12^{\text{so}} 17^{\text{th}}$	$F_{N-NNE-S} 13^{\text{so}} 24^{\text{th}}$	$\nabla^{+2-12^{\text{so}} 1535^{\text{th}}}$	
8	7	02	04	C0	02.0	10.5	14.4	.	$F_{NNW} 0-3^{\text{so}}$	$\Delta^{+2-21^{\text{so}} 24}$				
9	7	00	C6	C3	03.0	12.0	.	.	$\Delta^{+2-0-8^{\text{so}}}$					
10	7	C2	07	C1	03.3	09.6	.	.	$\Delta^{+1^{\text{so}} 20^{\text{th}}}$	$F_{ESE} 1338 1430$	$\bullet 0-16^{\text{so}} 1700$			
11	8	040	10	05	07.7	05.9	00.0	.	$\Delta^{+0-10-5^{\text{so}}}$	$F_{ESE-W} 6-24$	$\bullet 0-12^{\text{so}} 14^{\text{th}}$	$20-20^{\text{so}}$		
12	8	06	040	C1	04.3	05.8	CC.2	.	$F_{NNW} 0-16^{\text{th}}$					
13	7	10	05	10	05.7	00.4	.	.	$\Delta^{+0-30-7^{\text{so}}}$	$\zeta 11^{\text{so}} 12^{\text{th}}$	$\bullet 0-745 10^{\text{so}}$			
14	8	070	04	C1	02.3	11.7	CC.6	.	$\bullet 0-30-3^{\text{so}}$	$\zeta 11-9^{\text{so}}$				
15	8	010	030	08	04.0	12.9	.	.	$\Delta^{+1^{\text{so}} 9^{\text{th}}}$					
16	8	10	07	10	09.0	05.4	CC.1	.	$\Delta^{+1^{\text{so}} 8^{\text{th}}}$	$\zeta 17^{\text{so}} 2325^{\text{th}}$	$T 1635 1915$			
17	8	10	030	08	07.0	07.8	06.1	.	$\bullet 0-18^{\text{so}} 7^{\text{th}}$					
18	7	040	040	10	06.7	09.5	CC.3	.	$\Delta^{+0-10-8^{\text{so}}}$	$\zeta 3^{\text{so}} 10^{\text{th}}$	$T 1412 1520$	$\zeta 1924 1936 \zeta 1915 22^{\text{th}}$	$F_{NW} 1030 2034$	
19	6	090	10	10	05.7	00.5	04.6	.	$\bullet 0-10-9^{\text{so}}$	$\zeta 632^{\text{th}}$	$\zeta 0^{\text{so}} 10^{\text{th}}$	$\zeta 1055 1107$	$\bullet 0-1440 21 1517^{\text{th}}$	
20	7	07	050	07	07.3	03.6	CC.4	.	$\Delta^{+0-7^{\text{so}}}$	$F_{NNW} 1420 19$	$T 1632 1730$		$L 12320$	
21	6	06	060	10	C7.3	06.1	.	.	$= 3^{\text{so}} 1540^{\text{th}}$	$T 1234 1855^{\text{th}}$	$\bullet 0-16^{\text{so}} 2042^{\text{th}}$	$R 1835 1940 \zeta 19^{\text{so}} 21^{\text{th}}$		
22	6	C10	020	C2	01.7	12.3	CC.1	.	$\Delta^{+0-3^{\text{so}}}$	$\zeta 332910^{\text{th}}$	$\zeta 2010^{\text{th}}$	$24, \Delta^{+20-15^{\text{th}}}$		
23	7	000	010	08	03.0	12.0	.	.	$\Delta^{+0-10-8^{\text{so}}}$	$\zeta 21-24^{\text{th}}$				
24	8	C20	040	C1	02.3	11.8	.	.	$\Delta^{+0-8^{\text{so}}}$					
25	8	030	070	04	04.7	10.9	.	.	$\Delta^{+0-0-8^{\text{so}}}$	$\zeta 8-21^{\text{th}}$	$F-E_{N-NNE} 13^{\text{so}} 1832^{\text{th}}$			
26	8	000	030	00	01.0	12.5	.	.	$\Delta^{+0-10-8^{\text{so}}}$					
27	8	C20	050	09	06.7	08.2	.	.	$\Delta^{+2-0-8^{\text{so}}}$	$F_N 1115$	$\zeta 161$			
28	7	090	060	05	06.7	CC.2	.	.						
29	8	020	060	09	06.3	11.9	.	.						
30	8	C9	09	C8	08.7	01.9	12.6	.	$\Delta^{+1-3^{\text{so}} 7^{\text{th}}}$	$\zeta 11^{\text{so}} 1220^{\text{th}}$	$T 1405 620^{\text{th}}$	$\zeta 945 1150^{\text{th}}$	$R 445 600^{\text{th}}$	$F_{NE-WNW} 1420 540$
													$L 1115 1135 1140^{\text{th}}$	

MES., WRED. 04.7 05.9 05.4 05.3 248.2 44.6

Σ = 41°57' N λ = 21°38' E Gr. Δ G = + 1h27 min.

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D	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost % .			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21	
1	738.0	739.4	741.0	19.3	26.0	18.6	20.4	25.7	12.9	10.5	09.0	09.3	10.2	52	35	62	52	NNW	2	NNW	5
2	744.2	742.5	743.4	17.4	28.6	20.0	21.5	29.7	10.8	09.2	12.0	10.9	10.3	80	37	59	59	-	0	N	2
3	745.2	742.0	749.9	18.2	25.6	17.9	19.9	26.8	14.1	11.7	10.7	09.1	11.2	68	37	73	59	-	0	N	2
4	740.1	739.6	740.6	16.4	26.9	21.1	21.5	28.9	10.4	08.9	10.8	12.5	11.9	77	42	64	61	SE	1	NE	3
5	742.3	741.3	742.1	20.0	28.4	23.6	23.9	29.7	14.8	11.6	11.6	12.7	13.0	56	44	59	56	-	0	E	1
6	744.1	740.6	739.6	20.4	26.6	23.6	24.5	31.8	15.2	12.5	13.2	13.5	14.5	74	41	66	60	-	0	SE	2
7	739.9	735.0	740.6	20.1	30.6	15.2	20.3	30.6	14.9	11.7	13.3	11.9	10.2	75	36	71	61	-	0	S	1
8	741.6	741.2	742.7	16.4	19.2	13.2	15.5	20.6	10.5	07.7	07.4	06.7	07.6	53	40	67	53	N	3	N	4
9	744.4	743.6	743.2	14.8	21.3	14.8	16.4	22.4	07.8	05.4	07.5	07.2	08.4	56	38	67	55	NW	1	N	3
10	744.1	741.7	745.2	12.4	24.8	18.6	18.7	26.8	06.9	04.8	09.1	09.2	08.8	85	39	54	59	-	0	NE	3
11	744.1	735.0	743.9	15.6	27.0	18.6	20.0	27.3	10.9	08.6	09.9	08.0	08.6	75	30	59	55	SSW	1	N	5
12	746.6	743.0	743.0	16.8	30.2	21.1	22.0	31.8	10.4	04.7	10.1	08.5	11.6	75	26	62	54	E	1	NNW	1
13	744.5	741.7	741.2	19.3	33.4	21.4	23.9	24.6	12.4	10.0	11.4	10.2	11.4	68	26	52	51	-	0	S	2
14	744.1	741.1	740.9	20.0	34.6	25.7	26.5	35.6	13.4	11.4	11.9	09.9	11.9	68	24	48	47	-	0	SSW	2
15	743.1	741.4	742.0	13.0	36.4	26.0	27.4	35.7	15.8	13.5	13.3	13.2	13.0	63	32	51	49	-	0	S	1
16	742.7	740.6	740.4	22.0	46.8	26.6	27.6	35.6	16.2	13.4	13.5	12.8	14.2	68	30	54	51	-	0	ESE	2
17	740.1	739.3	739.0	22.2	36.0	26.2	27.6	37.0	17.7	15.4	14.0	11.8	11.1	70	26	42	46	-	0	S	2
18	733.9	737.7	734.7	21.9	39.6	23.0	24.3	33.8	16.4	14.2	12.7	19.0	13.3	65	22	63	63	-	0	NW	1
19	736.6	734.8	735.0	19.8	32.6	23.4	24.8	34.0	14.7	12.0	12.6	08.9	10.1	73	24	42	46	SSE	1	SSW	1
20	735.6	735.6	735.3	20.0	26.9	18.0	20.7	27.3	16.0	15.6	11.9	12.2	11.4	68	46	74	63	NNW	3	N	5
21	735.8	730.6	730.0	16.6	19.0	16.8	17.4	20.1	15.4	14.0	08.5	08.5	08.6	56	51	60	57	N	5	N	4
22	737.4	730.4	740.0	14.2	23.0	17.1	17.6	23.0	13.6	11.9	10.4	07.9	05.8	86	37	67	62	-	0	NNW	4
23	732.9	730.2	741.2	14.0	21.4	19.0	17.8	23.3	11.5	09.7	10.5	01.8	10.0	87	46	65	66	E	1	NNE	5
24	742.4	741.7	741.5	16.4	27.0	20.5	21.2	28.0	14.2	11.5	10.5	09.8	10.8	75	37	59	57	-	0	NNW	2
25	740.4	740.0	740.4	17.4	30.8	24.6	24.4	31.9	11.7	09.6	11.3	11.2	10.2	76	34	49	51	-	0	WSW	1
26	742.0	741.3	740.4	20.0	24.4	19.3	20.9	25.2	16.7	14.4	11.1	10.8	08.6	61	47	51	52	NNW	5	N	6
27	745.5	741.3	740.1	16.6	26.8	21.4	21.6	29.0	11.5	08.2	08.7	05.4	11.5	61	35	60	52	NNE	1	SW	1
28	744.7	742.0	740.4	18.0	36.1	26.2	28.3	32.2	13.5	11.4	11.8	12.6	12.7	76	39	50	55	-	0	WSW	2
29	745.6	742.5	744.3	22.0	39.0	24.0	25.5	33.0	12.3	09.9	17.9	10.0	11.2	65	28	50	48	NNE	1	NNW	2
30	745.0	742.1	741.2	18.9	32.1	21.4	23.5	32.8	14.4	11.2	11.4	09.0	09.5	70	25	49	48	-	0	SE	1
31	741.0	739.4	739.3	17.4	32.7	22.2	23.5	33.6	13.0	10.4	10.2	09.0	11.7	68	25	56	50	-	0	WSW	1
MES.	741.0	740.1	740.0	18.3	26.4	20.5	22.2	26.6	13.3	10.8	11.1	10.5	10.8	70	36	58	56	0.8	2.4	1.7	
MES.	742.2	740.4	741.0	18.5	29.6	22.1	23.1	30.8	15.0	12.0	11.6	10.8	11.4	73	36	58	56	0.7	2.5	2.1	

1974 AVGVST

SKOPJE-PETROVAC

1	741.7	739.2	739.3	18.6	32.7	22.8	24.8	33.7	13.8	11.0	11.0	10.9	10.8	68	29	52	50	-	0	SSW	2
2	741.2	739.6	740.2	19.0	33.0	24.8	25.4	34.4	14.3	12.0	11.3	07.7	10.1	69	20	43	44	-	0	SE	2
3	747.5	741.6	742.1	19.6	34.0	23.6	25.7	34.8	14.1	11.2	10.8	07.2	11.8	63	16	54	45	-	0	SSW	2
4	744.0	742.6	741.7	19.4	35.1	22.8	25.0	35.7	14.3	12.2	11.4	08.4	09.4	67	20	45	44	-	0	E	1
5	744.3	740.8	740.6	19.0	35.3	25.2	26.2	36.2	15.3	12.5	10.8	09.0	11.0	65	21	48	44	-	0	NNW	1
6	742.0	739.7	742.2	21.2	34.8	24.4	26.0	34.1	16.8	14.2	12.4	15.7	11.1	61	40	48	51	-	0	NNF	4
7	742.9	740.4	740.3	21.1	28.0	23.6	24.1	29.0	18.4	17.4	09.5	10.5	10.7	50	37	49	45	N	4	N	2
8	740.6	737.7	737.4	17.6	31.0	25.0	24.6	32.0	14.9	11.9	12.6	11.7	13.5	63	35	57	58	SE	1	SSE	4
9	737.9	734.8	735.8	20.6	31.8	21.8	24.0	32.4	16.1	14.4	13.6	12.6	15.1	75	36	77	63	-	0	E	3
10	741.3	740.2	739.3	20.0	26.4	22.0	28.0	31.6	16.6	15.7	10.8	09.0	08.6	62	35	48	48	NNW	3	N	2
11	736.1	733.5	734.3	15.2	29.2	23.0	22.6	31.6	11.1	08.5	09.2	12.3	06.8	71	40	42	51	-	0	NW	2
12	738.9	737.7	740.2	17.8	24.4	18.3	19.7	25.6	15.1	13.4	09.3	07.6	07.6	61	33	48	47	KNE	3	N	5
13	741.0	742.1	744.2	17.4	23.0	16.8	18.5	24.4	12.8	10.9	08.4	09.6	08.8	56	46	62	55	NF	2	NE	1
14	745.9	745.3	745.3	17.7	27.4	22.4	22.5	29.0	11.0	09.1	08.9	09.6	10.4	54	35	51	48	NE	1	NNW	3
15	746.6	745.1	745.7	19.6	30.4	23.0	24.0	31.2	13.8	11.3	11.8	09.0	11.0	65	28	52	50	-	0	N	5
16	746.1	7																			

B.R. ST. 268

$$H_s = 232 \text{ m} \quad H_b = 233.3 \text{ m} \quad h_f = 2.0 \text{ m} \quad h_r = 1.3 \text{ m}$$

SKCP JF - PETROVAC

1974 AUGUST

1	8	000	010	00	00.3	12.9	.	.	Δ^0-7
2	7	000	010	00	00.3	12.7	.	.	Δ^0-6^{45}
3	7	000	010	01	00.7	12.8	.	.	.
4	7	000	010	00	00.3	12.7	.	.	.
5	7	000	010	01	00.7	12.1	.	.	.
6	7	000	010	09	03.3	10.7	.	.	F-E NNE-NE $12^{58} 24i$, $\Delta 21^{45} 22^{45}$
7	7	040	000	07	02.7	10.5	.	.	F NNE $0-10^{25}i$
8	7	000	010	00	00.3	11.4	.	.	$\bullet 0^0 17-19i$, T $18-19^{05}$, $\Delta^0-18^{20} 18^{23}$, F NNE $19-24i$, $\Delta 19^{05} 21^{10}$
9	7	000	070	04	03.7	09.4	.	.	F NNE $0-6^{45}i$
10	8	010	020	00	01.0	11.6	00.1	.	F W $10^{50} 11^{34}$
11	8	010	06	01	03.7	09.5	.	.	F NNE-WW $0^{34} 9^{25}i$, $12^{10} 20^{45}i$; $\bullet 0^0 22^{26} 0^{30}$
12	8	030	030	07	04.3	10.6	00.2	.	F NW $7-17^{35}i$
13	8	06	080	01	05.7	04.4	.	.	F NNE $15^{02} 19^{43}i$
14	8	030	040	00	02.3	12.1	.	.	F NNE $10^{08} 17^{40}i$
15	8	000	070	00	02.3	11.1	.	.	F NNE $11^{55} 17^{50}i$
16	7	000	06	01	02.3	11.2	.	.	F NNE $13^{55} 17^{00}i$
17	7	09	040	00	04.3	09.7	.	.	.
18	7	000	010	00	00.3	11.3	.	.	.
19	7	000	020	02	01.3	11.8	.	.	F N-E $15-17^{10} 21^{45} 22^{05}$, T $16^{30} 18$, $\bullet 0^0 17^{20} 17^{45}i$
20	7	000	020	00	00.7	10.6	.	.	.
21	7	000	030	07	03.3	09.7	00.0	.	T N-SE $14^{30} 16^{30}$, F-E $15^{30} 17^{40}$, $\Delta^0 17^{10} 17^{00}i$
22	7	010	020	03	02.3	11.8	00.0	.	T $13^{25} 15^{15}i$
23	7	010	07	02	03.3	07.4	.	.	T $13^{30} 18^{40}i$, F WW-NW $14^{40} 16^{15}i$, $\bullet 0^0 14^{43} 16^{12}i$, T $15^{40} 16^{00}i$
24	7	09	04	100B	07.7	04.6	00.1	.	$\Delta^0 0^0 17^{45} 17^{20} 18^{30}i$, T $18^{05} 19^{55}i$, F NW $19^{25} 20^{20}i$, T $19^{55} 23^{55}i$, $\Delta^0 21^{50} 22^{10}i$
25	7	06	020	02	03.3	09.9	21.4	.	$\bullet 0^0 1-2^0 17^{45} 18^{30}i$, T $15^{50} 18^{10}i$, V $0^0 17^{20} 17^{45}i$, V $19^{20} 20^{20}i$
26	7	000	03	03	02.0	10.5	03.1	.	$\Delta^0-10-8^{40} 23-24$, T $12^{35}-18^{20}i$
27	7	000	06R	02	02.7	09.0	.	.	$\Delta^0-2-7^{30} 12^{05} 15^{45}i$
28	7	09	08	09	08.7	09.2	.	.	$\Delta^0-4-20-7^{30} 13^{50} 14^{40} 2^{30} 23^{40}i$, $\bullet 0^0 13^{50} 14^{10} 22^{45} 24$
29	7	09	10	10	09.7	00.4	02.1	.	$\bullet 0^0-1-2^0 18^{55} 11^{20}i$
30	6	10	070	00	05.7	01.8	01.9	.	$\bullet 3^{50} 6^{40} 10^{55} 13^{00}i$, $\Delta^0 5^{20} 13^{30} 18^{40}i$
31	7	03	03	04	03.3	09.3	00.9	.	$\Delta^0-10-10^{45}i$, $= 6^{22} 6^{50}i$, F NNE $15^{50} 17^{23}i$
MES.									
VRED.		02.5	03.8	02.8	03.0	202.7	29.8		

$$\varphi = 41^{\circ} 57', \quad N \quad \lambda = 21^{\circ} 38', \quad E \text{ Gr.} \quad \Delta G = + 1h\ 27\ \text{min.}$$

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D D D	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %				Provac i jačina vetrova D, f (0-12)		
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	743.5	742.1	742.0	13.2	26.0	16.2	17.9	27.6	10.2	07.9	09.7	07.0	09.9	85	28	72	62	SSE 2	NW 2	SE 2	
2	741.2	741.5	741.9	13.4	28.3	19.8	20.3	29.6	10.9	09.1	05.8	09.7	12.3	85	34	71	63	- 0	SSW 1	S 1	
3	743.5	741.4	741.4	14.8	30.2	20.2	21.4	31.3	12.0	10.5	11.3	11.2	12.7	90	35	71	65	- 0	WSW 2	- 0	
4	742.5	739.5	739.3	17.3	31.8	24.4	24.5	33.0	13.4	12.2	12.3	11.8	11.4	83	33	50	55	- 0	SE 1	SE 2	
5	743.0	742.7	742.7	15.4	28.6	18.6	20.3	26.1	17.4	14.0	12.2	09.7	08.9	77	39	56	57	NNE 5	NNE 5	NNE 4	
6	742.2	738.3	736.2	13.4	27.2	16.4	18.4	28.6	09.6	06.5	09.6	07.0	07.4	83	24	53	54	- 0	C - 0	- 0	
7	739.4	732.3	735.9	14.4	27.3	15.4	18.1	27.6	10.1	08.6	09.6	12.3	12.6	78	45	96	73	- 0	SSE 3	W 1	
8	739.1	741.1	743.6	15.8	23.8	21.4	20.6	25.2	15.0	14.6	12.8	13.8	12.9	95	62	68	75	NNW 1	WNW 2	- 0	
9	746.7	745.8	745.6	16.2	26.4	18.6	20.0	27.6	14.6	13.7	12.7	11.9	14.0	92	46	87	75	NE 1	- C	WSW 1	
10	746.8	744.3	744.5	15.6	28.6	15.0	20.6	29.1	13.9	12.4	12.2	13.2	13.5	92	45	82	73	- 0	WSW 2	- 0	
11	746.5	745.7	747.2	15.4	25.8	16.6	19.6	26.0	13.3	12.4	11.8	11.6	11.0	90	46	68	68	- 0	NNE 5	NNE 2	
12	749.4	746.6	746.6	15.6	26.0	17.4	19.1	27.7	13.5	12.2	10.9	11.8	11.6	82	47	78	69	NNE 2	WNW 2	- 0	
13	746.9	744.5	745.1	13.7	27.8	17.0	18.6	29.0	11.9	10.5	11.1	10.9	10.7	95	39	74	69	- 0	SW 1	W 1	
14	745.9	743.5	743.6	13.2	27.6	19.6	20.0	28.3	10.9	09.5	10.4	11.4	10.5	91	41	61	64	- 0	SSW 2	- 0	
15	744.0	741.8	742.6	14.6	26.4	18.6	19.6	27.1	12.4	10.5	10.9	11.0	11.1	88	43	69	67	- 0	WNW 2	- 0	
16	744.2	743.7	745.1	15.0	26.0	20.0	20.2	26.2	12.6	10.9	11.5	10.0	10.8	90	40	62	64	E 1	N 1	NNE 2	
17	746.8	745.7	745.6	16.4	23.7	17.9	19.0	24.3	14.4	12.2	11.8	11.5	10.6	85	52	69	69	- 0	SSE 5	SE 3	
18	746.1	744.6	744.2	15.4	23.4	18.6	19.0	25.0	13.4	11.8	10.8	11.9	12.6	82	55	78	72	- 0	E 2	- 0	
19	744.4	742.1	742.6	15.6	26.1	15.6	18.2	26.9	14.1	13.0	11.4	10.8	12.1	86	43	91	73	- 0	N 2	- 0	
20	742.7	740.0	739.6	12.1	25.4	19.4	19.1	25.8	10.4	09.3	10.2	10.6	11.1	97	44	66	69	- 0	SSE 2	SSF 2	
21	740.2	740.2	740.4	15.0	22.0	17.4	18.0	23.2	13.2	11.6	11.5	10.4	11.2	90	52	74	72	SE 1	SSE 4	SE 1	
22	741.7	740.1	741.7	14.8	25.4	17.4	18.8	26.2	13.8	11.2	11.3	10.9	14.3	90	45	66	77	ENE 1	S 1	- 0	
23	741.9	740.4	740.7	16.0	23.2	16.4	18.0	23.5	14.1	12.2	12.8	11.7	12.1	94	55	86	78	- 0	SSW 2	S 1	
24	741.0	737.5	737.1	10.6	26.2	15.4	16.9	27.1	05.4	08.4	09.4	09.9	09.5	98	39	73	70	SSE 1	SSE 3	S 1	
25	735.3	731.2	731.0	11.2	22.9	13.8	15.4	26.2	06.7	08.8	07.5	10.3	10.7	98	36	87	71	- 0	S 5	NNE 3	
26	729.7	725.7	728.3	10.0	14.8	14.3	13.4	16.7	07.5	05.2	09.0	10.8	10.7	98	46	60	81	E 1	S 2	NNE 5	
27	735.7	734.5	742.6	12.4	17.2	09.4	12.1	17.4	08.8	08.2	06.7	05.6	06.2	62	38	70	57	NNW 5	NNW 1	NE 1	
28	742.0	740.5	740.0	03.6	19.9	10.0	10.8	21.1	01.4	-00.5	05.6	05.0	07.3	94	29	79	67	SSE 1	NW 1	- 0	
29	741.0	740.4	741.7	05.6	22.4	12.4	13.2	23.6	03.7	01.7	06.6	06.7	08.9	97	33	83	71	- 0	SSW 1	SF 1	
30	742.2	740.3	740.0	09.0	24.9	19.0	17.7	26.2	06.4	04.4	07.6	08.7	09.0	95	37	59	62	- 0	S 4	NE 2	

1974 EKTCRAB

SKOPJE - PETROVAC

	1	739.6	738.4	739.7	14.8	20.6	15.2	16.4	22.2	14.5	13.0	11.3	12.6	06.6	90	65	51	70	NW	3	E	1	NW	1
2	741.5	739.6	737.6	07.8	20.6	18.0	16.1	22.3	04.9	02.1	06.9	06.9	08.5	87	38	55	60	-	0	WNW	1	NW	2	
3	740.2	742.4	744.2	14.6	21.9	13.6	15.5	22.8	11.2	06.4	07.1	05.1	06.3	57	26	54	46	N	2	SF	1	E	1	
4	745.6	743.1	743.3	05.7	21.8	10.4	12.1	22.6	03.5	00.8	06.2	05.9	07.3	90	30	77	66	E	1	SSE	2	-	0	
5	743.3	739.8	739.8	07.2	23.4	14.2	14.8	24.2	05.6	04.0	07.2	08.3	08.5	95	39	70	68	-	0	S	1	ESE	1	
6	737.9	736.6	738.5	08.6	23.2	15.6	15.8	24.6	08.1	05.9	07.7	09.2	09.4	92	43	71	69	ESE	1	ENE	1	E	2	
7	739.6	737.9	737.6	11.8	19.0	18.6	17.0	21.2	11.4	09.3	08.8	10.8	09.8	84	65	61	70	NNW	2	NW	1	SE	3	
8	738.2	735.4	737.7	12.8	25.4	20.9	20.0	25.7	10.6	07.6	09.2	08.9	06.8	83	37	37	52	-	0	S	4	SSE	2	
9	739.3	738.9	739.8	12.1	17.9	14.6	14.9	20.9	11.0	09.0	10.5	09.5	09.0	94	62	72	78	NNE	2	-	0	NE	2	
10	741.9	741.0	742.3	08.0	21.2	09.6	12.1	22.2	06.5	03.6	07.6	05.9	05.8	95	31	65	64	-	0	ESE	1	SE	1	
11	743.8	742.3	743.6	04.2	19.7	05.6	10.8	21.0	02.7	00.1	05.4	06.2	06.6	88	36	74	66	-	0	SSW	1	-	0	
12	745.6	743.2	742.8	04.7	22.4	15.0	14.3	23.2	03.6	01.0	05.9	08.8	09.3	93	43	72	69	-	0	SSE	3	SSL	1	
13	742.3	740.6	739.6	10.4	19.4	15.8	15.5	19.7	05.2	07.2	08.8	12.2	10.8	90	72	80	81	-	0	NNW	2	E	2	
14	737.9	737.5	738.5	18.0	23.2	16.4	18.5	24.8	15.4	13.0	10.5	11.4	12.5	66	54	89	70	SSE	4	SSE	3	-	0	
15	737.9	737.1	735.5	16.0	19.4	18.2	18.0	22.0	15.9	14.0	13.1	12.8	12.3	96	76	78	83	WSW	1	E	2	SSE	5	
16	737.8	738.8	741.0	15.2	21.2	16.8	17.5	22.7	14.6	12.1	09.9	08.9	05.4	76	47	37	53	SE	1	WNW	3	W	2	
17	743.2	743.0	743.7	09.0	18.9	10.0	12.0	19.8	06.5	03.4	06.7	06.6	07.0	78	40	77	65	ENE	1	WNW	1	N	1	
18	745.9	744.3	745.4	02.8	16.7	11.1	10.4	17.0	02.2	00.0	05.2	06.7	05.9	94	47	59	67	-	0	SW	1	-	0	
19	746.0	743.0	743.2	03.1	18.0	07.5	09.2	18.4	02.6	-00.4	05.1	05.9	06.6	89	38	82	70	-	0	S	2	SSE	2	
20	740.5	735.9	733.0	03.2	20.2	16.2	14.0	20.4	02.6	00.0	05.6	08.1	10.4	97	46	75	73	-	0	SSE	5	SE	5	
21	724.7	720.5	724.5	14.2	15.7	10.0	12.5	16.9	10.0	13.1	10.9	11.4	07.0	90	85	77	84	SSE	4	WNW	2	WSW	3	
22	731.4	734.6	736.0	05.2	15.0	07.2	08.6	16.2	04.8	02.9	06.3	06.9	07.0	94	54	92	80	-	0	SSW	3	SF	1	
23	735.3	735.0	735.6	06.8	25.6	21.4	18.8	25.8	06.6	05.1	07.2	09.4	08.8	97	38	46	60	NNE	1	SSW	3	SF	5	
24	737.3	737.3	740.7	17.0	25.1	13.0	17.0	25.1	12.4	14.8	10.0	09.4	06.3	65	39	56	55	-	0	WSW	5	W	2	
25	743.3	743.1	742.7	06.4	13.9	06.0	08.0	14.9	04.9	02.4	06.2	06.0	05.3	86	51	75	71	S	1	NNE	5	-	0	
26	741.3	737.0	736.1	-00.3	14.2	05.2	06.1	15.2	-00.6	-03.4	04.3	04.7	05.7	96	39	86	74	-	0	SSW	1	SSW	1	
27	736.4	736.7	738.0	05.6	08.0	01.4	04.1	10.0	01.0	01.6	06.1	04.7	04.2	89	58	83	77	W	2	NNE	6	NAL	3	
28	736.8	733.5	732.6	-03.4	10.9	01.0	02.4	11.4	-03.6	-07.0	03.3	04.0	04.3	93	41	86	73	SE	1	SE	2	ESF	2	
29	728.7	728.6	729.0	03.8	13.7	07.6	08.2	14.6	-01.8	-03.7	04.9	07.6	07.3	82	64	93	80	WNW	2	S	4	-	0	
30	726.1	728.0	734.0	06.8	15.0	08.0	09.4	15.2	06.2	04.3	07.3	06.5	05.0	99	51	63	71	SSE	2	SSE	3	WNW	3	
31	737.6	736.5	735.5	00.0	09.0	06.4	05.6	11.4	-00.4	-02.4	04.4	05.9	06.9	96	65	96	86	-	0	NW	3	N	1	

ME 5-

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 $H_s = 232 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$

Dan	Vrijeme 0-9	Oblakost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnev.					
1	7 000	000	06	02	02.7	09.5	.	.	$\Delta^{+1} 0-7 22^{\circ} 24$		
2	7 060	020	02	02	03.3	05.1	.	.	$\Delta^{+1} 0-7 20^{\circ} 1$	$\Delta^{+1} 0-1425 M^{35}$	
3	8 010	020	00	01.0	11.0	00.0	.	.	$\Delta^{+3} 3-7 30^{\circ} 1$		
4	7 000	020	00	01.0	00.7	06.6	.	.	$\Delta^{+0} 0-7 30^{\circ} T 1427 16^{\circ} 1$	$\Delta^{+0} 1-1505 1506 1502 1500 1429 2045 2340 24$	
5	8 07	020	00	02.0	02.0	08.1	03.0	.	.	$\Delta^{+0} 0-7 30^{\circ}, F_{NNW-UNW} 0-18^{\circ} 20-58^{\circ} T 0403 35^{\circ}, \Delta^{+0} 1-100 310^{\circ}$	
6	7 000	000	00	00	00.0	11.6	.	.	$\Delta^{+1} 0-7 24^{\circ} 24$		
7	7 09	10	10	09.7	04.4	.	.	.	$\Delta^{+1} 0-8 0-1-2 14-15, 19^{\circ} 20^{\circ}, T 1520 19^{\circ}, R 15^{\circ} 19^{\circ}, F_{NNW} 1545 1640, \Delta^{+1} 5-1540 1940$		
8	6 10	080	09	09.0	02.6	45.6	.	.	$\Delta^{+2} 2630$		
9	7 000	010	00	00.0	00.3	09.6	.	.	$\Delta^{+1} 0-8 0-1830 24^{\circ} 24, = 4^{\circ} 12^{\circ} 21-24$		
10	7 000	020	00	00.7	10.2	.	.	.	$\Delta^{+1} 2-0-7 30^{\circ} 24^{\circ} 24, = 0-1340$		
11	7 020	010	01	01.3	05.8	.	.	.	$\Delta^{+2} 0-9, = 6^{\circ} 93^{\circ}, F_{NNW} 1018 1755$		
12	7 030	010	00	01.3	09.5	.	.	.	$\Delta^{+3} 730 20-24, = 530 1020$		
13	7 000	010	00	00.3	09.8	.	.	.	$\Delta^{+1} 0-7 2124, = 530 M^{30}$		
14	7 000	020	00	00.7	09.6	.	.	.	$\Delta^{+1} 0-7 2124, = 530 1230$		
15	7 000	020	00	00.7	09.0	.	.	.	$\Delta^{+1} 2-0-8 2124, = 4^{\circ} 12^{\circ}$		
16	7 010	020	08	03.7	09.4	.	.	.	$\Delta^{+2} 0-830 = 0-935$		
17	7 09	010	00	02.3	05.1	.	.	.	$\Delta^{+3} 0-830, = 1840, 1930$		
18	7 09	08	10	09.0	03.2	.	.	.	$\Delta^{+2} 0-740 = 6^{\circ} 20-1220, 2320-24, T 1420 1440, R 1440-1507, \Delta^{+1} 21450 1502$		
19	7 08	050	01	04.7	C7.0	.	.	.	$\Delta^{+0} 1036$		
20	7 000	010	00	00.3	08.5	04.0	.	.	$\Delta^{+3} 50-730 0-830 910^{\circ}$		
21	7 08	10	C3	07.0	00.5	.	.	.	$\Delta^{+1} 0-730, = 530 940, T 15-1705, \Delta^{+1} 1545 1625 1046, 1940, \sim 1620 1640$		
22	7 09	09	10	05.3	04.3	00.0	.	.	$\Delta^{+3} 0-945 T 1337 1445, \Delta^{+1} 1342 1435$		
23	7 10	09	05	08.0	C2.9	00.6	.	.	$\Delta^{+2} 0-945, = 330 7135$		
24	7 000	04	00	01.3	09.0	00.6	.	.	$\Delta^{+1} 0-830, F_{SSE-S} 1042 1440, \Delta^{+1} 1210 1225, 1630 1830$		
25	7 030	09	06	07.0	05.0	.	.	.	$\Delta^{+3} 0-30 0-1-1930 1520, 2030 2220, F_{NNW} 1950 21$		
26	7 08	06	10	08.0	02.4	00.5	.	.	$\Delta^{+3} 0-30, \Delta^{+1} 1930 1520, 2030 2220, F_{NNW} 1950 21$		
27	8 09	040	00	04.3	08.0	12.5	.	.	$\Delta^{+1} 2-0-930 2030 24$		
28	8 000	000	00	00.0	10.5	.	.	.	$\Delta^{+2} 0-20-930 1940 24$		
29	8 00	00	00	00.0	10.0	.	.	.	$\Delta^{+2} 0-830, F_{SSE} 185 1820, \Delta^{+1} 2135 22$		
30	8 010	080	07	05.3	08.7	.	.	.	$\Delta^{+3} 0-30, \Delta^{+1} 1930 1520, 2030 2220, F_{NNW} 1950 21$		
MES. VRED.		03.8	03.9	02.9	03.5	227.9	70.6				

SKOPJE - PETROVAC

1974 OKTOKTOBAR

1	7 100	08	05	07.7	C1.8	00.3	.	.	$\bullet 2^{\circ} 930 = 820 1020$	
2	P 040	05	04	04.3	C8.3	C1.3	.	.	$\Delta^{+1} 0-89, F_{SSE} 2225 2226$	
3	P 010	010	00	00.7	10.3	.	.	.	$\Delta^{+1} 0-730$	
4	8 010	050	04	03.3	08.5	.	.	.	$\Delta^{+0} 0-10$	
5	7 05	C40	06	05.0	C8.2	.	.	.	$\Delta^{+2} 0-830, \Delta^{+1} 1930 24$	
6	7 09	C50	04	06.0	05.8	.	.	.	$\Delta^{+1} 0-7$	
7	7 100	09	04	C7.7	00.3	C0.0	.	.	$\Delta^{+1} 0-86-80 1720 2220, \bullet 0-615 70, 2345 24$	
8	8 050	040	09	06.0	08.7	00.0	.	.	$\Delta^{+1} 0-86-80 1720 2220, \bullet 0-615 70, 2345 24$	
9	7 10	08	070	06.3	C1.7	00.4	.	.	$\bullet 0-86-80 1720 2220, 4925 2130$	
10	7 010	060	00	02.3	09.6	00.0	.	.	$\Delta^{+2} 22-24$	
11	8 08	030	00	C3.7	C8.6	.	.	.	$\Delta^{+1} 0-830$	
12	7 04	020	01	02.3	D8.4	.	.	.	$\Delta^{+3} 0-830$	
13	7 09	09	08	08.7	00.1	.	.	.	$\Delta^{+3} 0-830, \Delta^{+1} 1300 1230, T 1535 2025, \sim 2025 2240$	
14	7 08	090	09	08.7	04.3	00.2	.	.	$\Delta^{+2} 20-40, \Delta^{+3} 0-830 1230, T 1535 2025, \sim 2025 2240$	
15	7 09	100	080	05.0	C1.1	C1.7	.	.	$\Delta^{+1} 0-830, F_{SSE-W} 0-132 182, \bullet 0-1045 1105, \sim 1020 2125$	
16	8 03	050	01	03.0	05.2	04.7	.	.	.	$\Delta^{+1} 0-830, F_{SSE-W} 0-132 182, \bullet 0-1045 1105, \sim 1020 2125$
17	8 030	05	00	04.0	07.3	00.0	.	.	$\Delta^{+1} 0-515 1520, \Delta^{+1} 1030 1220$	
18	7 10	05	04	07.7	04.7	.	.	.	$\Delta^{+0}-1-0-430 2020 024, \Delta^{+1} 0-32 620$	
19	7 000	020	00	00.7	C9.0	.	.	.	$\Delta^{+0}-0-845, = 530 1130, F_{SSE} 24$	
20	8 09	040	04	C5.7	C9.2	.	.	.	$\Delta^{+1} 0-845, = 530 1130, F_{SSE} 24$	
21	7 100	100	08	09.3	00.6	05.5	.	.	$\Delta^{+1} 0-830, 20-2012 2320 24, \bullet 0-1045 1725, 20-2020, \sim 1745 1950, 2220 24$	
22	8 060	030	03	04.0	04.2	05.4	.	.	$\Delta^{+1} 0-110, F_{SSE} 0-099, \bullet 0-1120 305, \sim 20-24$	
23	8 03	050	03	03.7	07.6	.	.	.	$\Delta^{+0}-0-845, = 630 1240, F_{SSE} 902 1240, \sim 0-830 2146$	
24	8 08	050	09	07.3	06.1	.	.	.	$\Delta^{+1} 0-110, \Delta^{+0} 645 1240, F_{SSE} 902 1240, \sim 0-830 2146$	
25	8 020	08	00	C3.3	06.8	00.0	.	.	$\Delta^{+1} 0-110, \Delta^{+0} 645 1240, F_{SSE} 902 1240, \sim 0-830 2146$	
26	7 04	050	06	05.0	08.1	.	.	.	$\Delta^{+1} 0-830, \Delta^{+0} 645 1240, F_{SSE} 902 1240, \sim 0-830 2146$	
27	7 100	09	00	06.3	00.8	C1.9	.	.	$\bullet 0-830, F_{NNE-UNW} 530 545 90, 1545 1645; \Delta^{+0} 1-23-24$	
28	8 010	070	01	03.0	C7.9	00.0	.	.	$\Delta^{+1} 0-20-745 2020 024, \bullet 0-945 1640$	
29	7 07	07	08	07.3	02.8	.	.	.	$\Delta^{+1} 0-10-640, \Delta^{+0} 930 1020, \Delta^{+0} 705 820, \sim 1145-1300, 1640-1700, 2325 24, \sim 1300 1330$	
30	7 10	06	03	06.3	06.0	06.7	.	.	$\bullet 0-1045 1725, \Delta^{+0} 830 24$	
31	7 09	09	10	09.3	00.7	00.0	.	.	$\Delta^{+1} 0-110, \Delta^{+0} 830 24$	
MES. VRED.		06.1	06.2	04.2	05.5	172.7	32.1			

$\varphi = 41^{\circ}57'$ N $\lambda = 21^{\circ}38'$ E Gr. $\Delta G = +1h\ 27\ min.$

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Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pona e mm			Relativna vlažnost v%				Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21		
1	730.0	731.7	737.6	06.4	11.0	04.2	06.4	12.2	04.2	05.5	07.0	06.8	05.2	97	69	84	83	SSW 1	-	C	NF 5	
2	741.3	741.0	742.5	03.2	11.3	00.2	03.8	11.8	00.3	00.5	04.2	03.6	04.0	72	36	86	65	N 1	NW 2	-	0	
3	743.5	743.0	744.2	-00.4	12.8	03.6	04.9	13.4	-01.6	-04.4	04.2	04.7	05.0	94	43	85	74	SE 1	SSE 1	S	1	
4	745.6	743.9	744.4	-01.1	12.6	02.0	03.9	14.0	-02.0	-04.6	04.0	04.7	04.8	94	43	90	76	S 1	SSE 2	-	0	
5	745.6	745.2	747.2	-01.2	14.4	07.8	07.2	15.2	-02.0	-04.4	04.0	05.7	06.6	96	46	83	75	-	0	NNW 1	SE 1	
6	749.3	747.8	748.6	02.2	16.4	11.0	10.2	16.6	02.0	-00.6	05.2	07.4	06.8	97	53	69	73	SE 1	WSW 1	E	1	
7	747.5	745.4	743.4	09.6	09.8	08.2	09.0	11.0	07.6	05.6	07.2	08.2	07.7	81	90	95	89	E 1	-	C	E 1	
8	740.5	739.9	741.1	07.8	08.2	07.0	07.5	09.1	07.0	07.4	07.7	07.1	06.1	97	87	81	88	-	0	NNW 2	NNW 2	
9	741.5	742.0	744.2	07.0	10.2	07.8	08.2	10.2	06.4	05.6	06.6	06.1	06.1	88	66	77	77	WWN 3	W 3	N	3	
10	745.4	745.7	746.6	05.9	10.2	08.0	08.0	10.2	05.8	04.9	06.1	05.9	06.6	89	63	82	78	NNE 2	NNW 1	SSW 1		
11	747.4	746.5	747.5	04.8	14.3	04.4	07.0	15.1	04.3	04.7	06.1	06.2	05.7	94	51	91	79	SSW 1	SSW 1	S	2	
12	748.0	746.0	746.0	-00.6	12.6	05.4	05.7	13.4	-01.0	-03.0	04.2	06.5	06.2	96	59	91	82	-	0	-	0	
13	745.9	745.9	747.0	04.6	13.0	04.6	06.7	13.6	02.4	00.4	06.2	07.5	06.2	97	67	97	87	-	0	WSW 2	NNW 1	
14	748.5	747.4	748.6	01.4	09.7	03.2	04.4	11.4	00.9	-01.0	05.1	07.1	05.6	100	79	97	92	-	0	-	0	
15	749.7	748.7	749.0	00.4	06.4	02.2	02.8	08.6	-00.4	-01.4	04.7	06.6	05.2	100	92	97	96	-	0	SE 1	-	0
16	749.0	747.5	748.1	01.8	09.6	03.0	04.4	10.6	-00.6	-01.6	05.0	06.8	05.5	97	76	97	90	-	0	NW 1	-	0
17	749.1	748.5	749.0	03.2	05.2	04.1	04.2	05.4	-00.9	-01.3	05.8	06.4	06.1	100	97	100	99	SSE 1	-	0	-	0
18	749.4	748.7	748.7	02.4	03.6	02.8	02.9	04.3	02.0	02.8	05.4	05.8	05.6	100	97	100	99	NE 1	-	C	-	0
19	747.9	745.4	745.3	02.0	05.0	05.2	04.4	06.0	02.0	02.5	05.3	06.4	06.3	100	97	94	97	-	0	-	0	W 2
20	746.0	746.0	747.1	05.4	12.0	03.8	06.2	12.7	03.4	05.0	06.3	07.1	05.9	94	68	98	87	-	0	-	C	ENE 1
21	746.9	745.8	745.4	04.0	06.8	07.1	06.2	07.5	01.4	-00.4	06.1	07.0	07.2	100	95	95	97	-	0	ENE 1	ENE 1	
22	744.4	743.7	745.0	06.8	11.2	07.6	08.3	12.2	06.4	06.4	07.2	07.5	06.4	97	75	82	85	-	0	-	C	NE 3
23	746.0	744.7	744.5	03.2	05.8	05.6	05.0	08.0	01.0	-01.5	05.6	06.1	06.3	97	89	93	93	NE 1	-	0	NE 1	
24	744.0	744.3	745.7	05.3	08.5	03.8	05.4	08.6	03.4	05.3	06.2	06.8	05.8	93	81	97	90	-	0	W 1	-	0
25	746.7	745.2	744.8	05.6	09.4	07.8	07.6	10.0	03.8	00.0	06.6	07.3	06.9	97	83	87	89	-	0	NW 2	SSE 4	
26	740.8	738.6	737.9	08.2	08.2	06.6	07.4	09.7	06.5	02.1	06.9	07.9	07.1	85	97	97	93	SE 4	S 2	NNE 1		
27	738.5	736.8	736.2	03.2	06.9	05.2	05.1	07.1	02.8	00.6	05.5	06.6	06.4	95	88	97	93	NF 1	-	0	NNE 1	
28	735.9	732.2	727.6	01.2	09.3	06.2	05.7	09.8	01.2	-01.1	04.8	06.9	06.4	97	78	90	88	S 1	-	0	NNW 1	
29	729.3	732.9	734.9	04.4	10.5	00.6	04.0	14.5	00.2	03.3	05.4	04.8	04.1	85	50	86	74	NW 3	-	0	-	0
30	737.4	739.2	743.2	-02.8	07.7	01.8	02.1	08.1	-03.4	-05.6	03.4	05.2	04.4	91	66	83	80	-	0	NNW 4	NE 3	

MFS.
WRF0. 744.0 743.3 744.0 03.5 09.8 05.0 05.8 10.7 02.1 01.0 05.6 06.4 05.9 94 73 90 86 0.8 - 0.9 1.2

1	745.2	746.3	748.3	-04.4	04.0	01.4	00.6	04.5	-04.6	-07.6	03.0	04.5	04.7	92	73	92	86	-	0	NW 1	-	0	
2	749.0	748.5	749.2	-01.4	06.2	03.0	02.7	07.1	-01.9	-04.0	04.0	04.8	05.0	96	68	87	84	-	0	-	C	-	0
3	750.3	749.3	749.8	03.2	11.0	07.6	07.4	11.2	02.9	01.1	05.4	05.3	06.4	94	54	82	77	-	0	NNW 2	W 1		
4	748.9	746.9	745.8	08.0	11.0	08.4	09.0	11.9	06.4	05.4	06.8	07.4	06.4	85	75	78	79	NNE 2	-	0	NF 2		
5	743.3	741.2	740.4	00.6	12.0	06.4	06.4	12.4	00.0	-02.0	04.7	06.2	06.1	98	58	85	80	S 1	-	0	NF 1		
6	740.2	741.6	743.2	05.8	07.0	00.0	03.2	07.2	-00.6	00.3	04.5	04.7	03.7	65	62	80	69	N 5	-	0	NNE 2		
7	743.0	742.0	741.6	-04.0	05.1	01.8	01.2	06.0	-04.4	-07.0	03.2	03.6	04.4	94	54	85	78	ENE 1	SSW 1	NW 1			
8	740.9	738.3	739.6	00.0	07.4	04.3	04.0	07.6	-00.6	-03.4	04.3	05.1	06.0	93	65	97	85	NW 1	NNF 3	N	2		
9	740.5	742.6	745.7	02.9	09.4	03.4	04.8	09.4	01.3	-00.2	05.6	04.9	04.1	98	56	70	75	NW 3	NNE 4	NF 2			
10	747.4	746.7	747.4	-03.2	08.1	03.4	-00.5	09.1	-03.5	-06.2	03.4	04.6	03.2	93	57	89	80	-	0	-	C		
11	747.5	744.5	743.1	-05.6	06.6	-02.0	-00.8	07.4	-05.7	-08.3	02.8	03.9	03.3	92	53	83	76	-	0	-	0		
12	741.0	739.2	738.0	-02.4	04.2	00.4	00.6	04.6	-04.4	-06.9	03.5	04.2	04.2	90	68	89	82	-	0	-	C	E 1	
13	735.0	732.7	732.8	01.8	10.4	05.0	05.6	10.6	00.0	-01.6	04.7	06.0	05.8	90	64	88	81	N 1	W 2	NE 1			
14	735.9	737.2	736.2	02.6	01.6	00.2	01.2	05.6	00.2	02.0	05.0	04.5	04.5	90	87	96	91	W 2	NNW 2	NW 3			
15	736.8	737.2	738.6	00.9	01.8	00.4	00.9	02.4	00.0	00.0	03.8	04.2	04.4	78	80	93	84	NW 2	MSW 2	MSW 2			
16	740.1	740.8	742.5	00.2	02.0	01.6	01.4	02.3	-00.4	-00.6	04.0	04.3	04.3	86	80	83	83	NE 3	NNE 4	NNE 3			
17	743.4	741.5	741.1	02.0	05.1	-02.1	00.7	05.6	-02.2	-00.1	04.3	04.2	03.7	80	64	94	79						

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$$H_s = 232 \text{ m} \quad H_b = 233.3 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.3 \text{ m}$$

Den	Vlajka 0-9	Občačnost N (0-10)					Inocetija kraj seti	Padavina 2 mm	Snežni pokriva- k cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7	10*	08	10*	09.3	02.7	09.6	.	• 0° 0° 8° 30°, 18° 23° i, = 5° 7° 30°, Fne 18° 21°.	
2	8	04	020	00	C2.0	08.8	03.1	.	△ 0° 17° 20° 20° 24	
3	8	04	030	01	C2.7	08.2	.	.	□ 0° 10° 7° 22° 24	
4	8	06	020	00	02.7	07.8	.	.	□ 0° 2° 0° 8° 21° 24	
5	7	03	010	08	C4.0	07.1	.	.	□ 0° 2° 0° 8° 6° 7° 30	
6	7	04	060	09	04.3	04.1	.	.	= 5° 12° 30	
7	7	10*	10*	10*	10.0	00.0	00.0	.	• 0° 16° 24°	
8	6	10*	10*	10*	10.0	00.0	20.5	.	• 0° 10° 7° 21° 22° i, = 2° 9° 30° i, = 1° 2° 6° 7° 10°, 0° 1° 12° 15° 14° 10° 18° 21°.	
9	7	10	10	10	10.0	00.0	00.0	.	• 0° 14° 6° 8	
10	7	09	09	10	09.3	01.1	.	.	.	
11	7	09	010	00	03.3	07.7	.	.	△ 20° 24	
12	7	10	030	05	06.0	05.7	.	.	△ 0° 10° 8° 4° 5° 30° 7° 45° 12° 30° 16° 24°, = 5° 7° 45° 0° 1° 20° 24	
13	6	09	09	10	09.3	04.6	.	.	△ 0° 12° 9° 19° 24°, = 0° 12° 30° 12° 24	
14	6	10	00	00	03.3	02.9	.	.	≡ 0.5° 10° 11° 20° 12° 0° 12° 10° 25° 19° 24	
15	5	10	020	00	04.0	02.1	.	.	≡ 0° 0° 12° 22° 24°, = 0° 4° 11° 12° 22° 24°, ≡ 4° 11° 20° 2° 18° 21° 30°, 0° 21° 30° 2	
16	6	10	030	00	04.3	02.2	.	.	△ 0° 0° 5°, = 0° 0° 8° 30° 9° 30° 21° 20° 23° 30°, = 0° 0° 8° 30° 23° 30°, = 9° 21° 20° 120° 24	
17	5	10*	10	10*	10.0	00.0	00.0	.	≡ 0° 10° 6° 10° 10° 5°, = 0° 10° 0° 10° 10° 24°, = 10° 10° 15° 24°, = 15° 15° 10° 20° 24	
18	4	10*	10	10	10.0	00.0	00.3	.	9° 0° 0° 6° 10° 5°, = 0° 0° 9° 10° 15° 24°, = 19° 15° 15° 24	
19	3	10	10	10	10.0	00.0	00.0	.	≡ 0° 6° 15°, = 6° 15° 15°, = 6° 15° 10° 24	
20	6	10	02	03	05.0	04.1	00.3	.	≡ 0° 22° 15°, = 0° 0° 10° 5°, = 6° 18° 24°, = 22° 24	
21	3	10	10	10	10.0	00.0	.	.	≡ 0° 3° 9° 45° 14° 8°, = 0° 0° 9° 45°, = 0° 0° 9° 45° 11° 45°, = 14° 24	
22	5	10*	020	08	06.7	01.2	00.6	.	≡ 0° 18° 20° 0° 4° 12°	
23	5	10	10	10	10.0	00.0	00.2	.	= 4° 24	
24	5	10	09	10	09.7	00.0	.	.	= 0° 24°, = 0° 20° 20° 24	
25	6	10	10	10	10.0	00.0	.	.	= 0° 16° 12°, = 0° 10° 10° 30°, = 6° 15° 7° 10	
26	5	10	10	05	08.3	00.0	.	.	Fne 2° 2° 5°, = 0° 19° 20° 14° 15° 16° 15° 17° 45°, = 9° 23° 20°, = 21-22°	
27	6	10	10	10	10.0	00.0	07.7	.	= 7° 6° 24°, = 7° 7° 18° 18° 19° 21°, = 21° 22°	
28	7	07	09	09	08.3	01.5	CC.C	.	= 0° 10° 18° 20° 35° 124	
29	8	09	01	02	04.0	07.9	00.3	.	Fne -36° 0° 9° 15°, = 0° 4° 2° 5° 12°, = 9° 24	
30	7	08	09	02	06.3	01.8	.	.	△ 0° 10° 9° 21° 124, = 12° 12° 12° 40	

1	7	04	10	09	07.7	CC.0	.	.	
2	6	09	03	08	06.7	00.7	.	.	
3	6	09	080	08	08.3	02.4	.	.	
4	7	10	09	09	09.3	00.2	00.0	.	
5	6	03	07	10	06.7	05.1	.	.	
6	8	10	10	02	07.3	00.0	.	.	
7	7	04	05	05	04.7	03.3	CC.0	.	
8	7	10	10*	10*	10.0	00.4	00.0	.	
9	7	09	06	09	08.0	00.8	01.7	.	
10	7	02	000	00	00.7	07.5	.	.	
11	6	00	010	00	00.3	06.4	.	.	
12	5	07	10	09	08.7	00.2	.	.	
13	6	09	04	10	07.7	03.3	00.0	.	
14	6	10*	10*	10*	10.0	00.0	06.4	.	
15	6	10	10*	10*	10.0	00.0	14.2	07	
16	7	10*	10	10	10.0	00.0	C2.8	08	
17	7	10	000	02	04.0	06.5	00.0	04	
18	6	04	09	10*	07.7	CC.5	.	.	
19	1	10	00	09	06.3	01.0	08.2	01	
20	7	08	06	06	06.7	01.4	.	.	
21	7	05	010	09	05.0	05.4	.	.	
22	6	00	020	00	00.7	05.7	.	.	
23	5	00	000	00	00.0	06.6	.	.	
24	5	00	000	00	00.0	06.4	.	.	
25	5	00	000	00	00.0	04.4	.	.	
26	6	00	030	03	02.0	05.9	.	.	
27	5	09	08	01	06.0	01.9	.	.	
28	4	10	10	10	10.0	00.0	01.0	.	
29	4	10	08	10	09.3	00.0	00.0	.	
30	3	10	10	10	10.0	00.0	.	.	
31	5	10	10*	10*	10.0	00.0	C2.0	.	
MES.	NRED.	06.5	05.8	06.4	05.2	76.4	36.3		

**B) Mesecni i godišnji
pregled**

1974

Mjesec	Vrednost pritisak Pn mm.	Temperatura vazduha °C								Čestina pravaca i srednja jačina vatra nD, Fm (0-12)																									
		Tm			Sred. (tides)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C								
		7	14	21							E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.							
SR SLOVENIJA																																			
$\varphi = 46^{\circ}20' N \lambda = 13^{\circ}33' E$ Gr. AG = + 54 min.																																			
I	-	-06.6	04.5	C1.3	01.7	05.4	-01.0	12.3	20 -04.8	24 06	00.6	C4	01.2	C1	06.1	•	•	21	02.6	05	00.8	•	•	•	•	56									
II	-	C1.7	02.3	03.6	04.1	C6.2	04.9	12.7	21.20 -04.3	09 14	C1.8	10	03.5	C7	00.8	•	•	20	02.4	14	03.4	02	00.3	•	•	17									
III	-	03.2	11.8	06.0	06.7	12.6	02.0	23.8	22 -05.2	01 06	00.8	05	01.4	C7	01.2	•	•	33	03.9	23	04.0	01	00.2	•	•	18									
IV	-	05.5	13.3	08.4	08.9	14.2	03.4	19.7	12 -01.3	20 05	C6.6	16	05.4	11	C2.2	•	•	22	02.8	17	04.4	•	•	•	•	19									
V	-	09.9	16.8	11.4	12.4	17.6	07.5	24.3	21 02.6	15 04	C6.8	C2	00.5	17	C2.3	•	•	21	02.9	21	05.7	•	•	•	•	28									
VI	-	12.5	19.1	13.7	14.8	20.3	05.7	26.5	04 03.4	14 19	C3.3	C9	02.4	9	00.1	•	•	20	02.8	16	04.3	•	•	•	•	25									
VII	-	15.5	23.7	16.6	16.1	24.4	12.2	24.1	30 07.2	26 12	C1.4	C6	02.9	•	•	25	03.5	15	04.3	02	00.5	•	•	•	•	31									
VIII	-	15.9	25.8	17.8	19.3	26.5	13.5	32.7	16 05.2	13 04	C6.5	C1	00.4	C1	00.1	•	•	29	04.9	07	01.8	01	00.1	•	•	50									
IX	-	16.9	26.3	14.7	14.2	21.0	03.3	26.9	14 C1.6	27 03	C6.3	C1	00.8	•	•	•	•	23	03.7	10	02.4	04	C0.8	•	•	46									
X	-	03.3	09.8	04.7	05.6	10.6	C1.7	15.1	18 -03.1	30 31	C4.3	C9	01.8	06	01.7	•	•	21	02.7	05	01.4	03	00.5	•	•	22									
XI	-	03.0	09.1	04.1	05.1	04.8	01.3	12.9	08 -04.2	03 10	C1.3	C4	01.3	06	01.8	•	•	24	63.0	07	01.7	01	00.2	•	•	38									
XII	-	-01.0	05.7	00.5	01.4	06.5	-02.1	12.4	03 -07.1	15 10	C1.6	C5	01.4	12	C4.2	•	•	21	02.7	01	00.1	05	00.6	•	•	39									
GOD.	-	06.7	13.9	08.4	09.4	14.8	04.9	32.7	16W -07.1	15X	02.2	124	02.2	71	02.9	69	02.2	•	•	280	03.2	141	04.1	19	00.5	•	•	391							
VEDRIJAN																																			
$\varphi = 46^{\circ}01' N \lambda = 13^{\circ}33' E$ Gr. AG = + 54 min.																																			
I	-	04.1	C7.9	C5.3	05.7	09.2	C3.3	16.0	21 06.0	26.15	•	•	62	24.0	•	•	11	02.7	C2	00.4	09	C1.8	•	•	01	00.2	08								
II	-	05.8	09.4	C6.4	07.3	10.5	05.0	14.6	15 01.0	07	•	•	65	23.0	•	•	20	05.5	•	•	07	02.2	•	•	03	00.4	02								
III	-	07.1	12.9	08.7	09.4	14.0	06.2	25.0	22 00.5	11	•	•	48	22.8	•	•	12	03.0	01	00.2	25	05.9	•	•	03	C0.4	04								
IV	-	08.9	15.1	10.0	11.3	16.6	08.0	21.0	08 05.0	26.16	•	•	56	20.7	•	•	15	04.1	01	00.1	14	C3.8	•	•	04	C1.1	03								
V	-	12.9	18.3	13.7	14.7	20.0	11.2	26.5	21 07.4	24	•	•	42	12.6	•	•	18	04.7	C3	00.4	22	05.8	•	•	05	C1.3	03								
VI	-	15.2	20.6	16.4	17.2	22.1	13.3	28.0	05 07.5	10	•	•	41	13.3	•	•	23	06.0	•	•	18	04.4	•	•	06	C1.3	02								
VII	-	18.7	25.1	20.1	21.0	21.6	16.4	31.5	31 11.2	19	•	•	45	16.4	•	•	21	05.1	•	•	25	06.4	•	•	01	C0.3	03								
VIII	-	20.1	27.3	22.2	23.0	26.5	18.8	34.0	16 11.4	11	•	•	59	22.5	•	•	11	02.5	•	•	18	04.6	•	•	03	C1.4	02								
IX	-	15.4	22.0	17.2	18.0	23.2	14.6	25.6	14 07.0	27	•	•	59	25.5	•	•	10	02.8	•	•	13	02.7	•	•	01	C0.5	07								
X	-	07.1	12.0	08.0	08.6	19.2	06.0	17.5	07 02.4	31	•	•	55	22.1	•	•	15	04.0	01	00.1	16	03.7	•	•	03	00.9	03								
XI	-	07.1	11.0	07.8	08.5	12.0	06.1	15.8	11 02.0	02	•	•	39	15.5	•	•	22	05.3	•	•	20	04.8	•	•	01	C0.2	08								
XII	-	04.4	08.7	09.5	06.0	09.6	C3.4	15.5	03 -00.6	15	•	•	46	13.6	•	•	20	04.3	01	00.1	13	03.1	•	•	04	C1.3	09								
GOD.	-	10.6	15.9	11.4	12.6	17.1	09.4	34.0	16W -00.6	15X	02.0	10.0	605	20.0	•	•	198	04.5	09	00.3	200	04.6	•	•	32	C1.1	51								
RATECE-PLANICA																																			
$\varphi = 46^{\circ}30' N \lambda = 13^{\circ}43' E$ Gr. AG = + 54 min.																																			
I	-	69C.7	-03.3	C2.8	-02.2	-01.2	03.3	-04.6	04.2	19 -07.8	27.26	•	•	•	•	07	01.6	•	•	•	•	01	00.1	05	00.7	02	C0.2	78							
II	-	683.9	-02.4	04.3	00.1	00.8	04.9	-01.9	09.4	12 -05.4	09	•	•	66	00.9	C6	C1.0	04	00.9	03	00.3	06	00.6	09	01.4	•	•	50							
III	-	687.3	-01.0	07.7	01.3	02.3	08.5	-02.0	15.3	22 -07.0	12	•	•	04	00.7	06	01.4	01	00.1	04	00.7	01	00.1	10	01.2	•	•	67							
IV	-	684.3	00.8	09.8	04.1	04.7	10.8	-01.0	17.0	12.09 -06.4	26	•	•	07	02.1	13	C3.2	03	00.4	•	•	04	00.6	03	00.4	02	C0.3	58							
V	-	685.1	06.9	15.0	08.4	09.7	15.8	03.5	22.2	22 00.0	25.24	•	•	63	00.7	03	00.6	10	01.6	02	00.3	06	01.1	•	•	•	•	69							
VI	-	684.5	09.4	16.6	10.7	11.9	18.1	05.9	25.0	04 -01.4	12	•	•	62	00.7	C6	C1.3	02	00.3	06	00.6	07	01.9	02	00.2	68									
VII	-	685.1	21.4	13.9	15.4	22.1	06.6	27.0	30 02.8	26	•	•	61	00.4	16	C3.3	03	00.6	•	•	03	04.9	13	03.0											

Mesec	Oblačnost Nm (0-10)			Insolacije broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na mesec																							
					S m			U m s			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	△	■	≡	■					
	7	14	21	Sred. (Dnev.)	mm	7	14	21	Streš.	Min	Max	Dat.	≤	<	<	≥	IN	IN	IN	IN	≥	<	>	IN	IN	IN	IN							
BR. ST.1																											SR SLOVENIJA							
I	7.5	7.2	5.6	6.9	059.2	04.6	56	80	90	68	47	074	029.2	01	•	21	•	•	•	•	02	13	12	06	03	07	Ct	01	•	•	09	17		
II	6.7	7.6	7.1	7.0	072.5	05.0	89	71	86	61	36	243	061.3	07	•	10	•	•	•	•	02	15	13	12	06	13	•	•	01	01	01			
III	5.3	6.7	5.1	5.7	137.0	05.5	87	98	78	74	19	134	077.9	05	•	10	•	•	•	•	07	09	11	11	01	06	04	•	•	01	03	01		
IV	5.5	7.4	5.8	6.2	141.0	05.6	83	53	66	68	27	204	066.1	30	•	02	•	•	•	•	03	11	09	06	06	05	•	•	•	02	•			
V	6.4	7.0	6.4	6.9	130.9	08.5	90	64	82	75	32	101	021.6	25	•	•	•	•	•	•	13	18	16	03	18	•	•	•	01	07	02			
VI	6.7	7.5	6.7	7.0	132.1	09.7	86	61	83	77	31	370	076.2	30	•	02	•	•	•	•	02	11	19	16	09	19	•	•	01	11	01			
VII	4.5	6.3	6.4	5.7	211.7	11.8	84	56	83	74	35	222	082.6	16	•	14	•	•	•	•	04	03	12	10	06	12	•	•	01	06	01			
VIII	4.4	5.5	3.7	4.5	215.4	13.2	91	58	82	78	24	120	037.6	11	•	•	17	12	•	•	10	05	10	07	05	10	•	•	07	•				
IX	4.6	5.6	4.5	5.0	172.5	11.0	95	73	94	88	51	277	085.6	25	•	•	05	•	•	•	•	08	07	15	12	06	15	•	•	01	06	•		
X	6.6	7.7	6.6	7.0	084.5	04.0	93	73	93	87	44	236	055.4	21	•	12	•	•	•	•	02	15	20	17	06	20	02	02	•	04	•			
XI	6.8	6.6	6.4	6.6	075.7	05.8	94	72	86	35	196	068.2	20	•	13	•	•	•	•	02	12	12	09	06	12	•	•	01	01	01				
XII	3.2	5.0	3.4	3.9	077.4	05.9	84	62	84	78	16	021	017.2	12	•	25	•	•	•	•	12	05	04	03	01	03	02	•	•	01	01			
GOD.	5.7	6.6	5.7	6.0	1510.5	07.6	89	65	84	79	18	2200	085.6	25IX	•	•	93	38	12	•	•	54	119	155	125	58	147	14	03	•	06	49	15	25
BR. ST.2																											VEDRIJAN							
I	6.2	5.7	5.7	6.0	057.2	05.9	89	80	86	85	42	047	023.8	01	•	•	•	•	•	07	07	03	12	10	09	01	16	•	•	09	•			
II	6.0	6.7	5.5	6.2	091.7	06.5	87	78	86	84	43	162	037.4	01	•	•	•	•	•	06	07	03	11	12	12	05	12	01	01	01	05			
III	5.9	5.2	4.9	5.3	142.5	07.1	83	70	80	76	44	040	027.2	05	•	•	01	•	•	08	08	09	09	08	06	01	08	02	02	01				
IV	4.6	5.6	5.3	5.2	168.0	06.2	83	75	82	80	42	124	038.5	29	•	•	•	•	•	04	03	04	08	11	10	05	11	•	•	•				
V	5.6	6.5	6.1	6.1	175.5	10.6	86	76	85	83	37	131	033.6	25	•	•	04	•	•	03	02	01	12	14	13	04	14	•	•	02	•			
VI	6.0	6.9	6.6	6.5	168.7	12.8	88	81	86	85	59	224	075.1	30	•	•	07	•	•	02	02	03	03	12	17	08	17	•	•	02				
VII	3.6	4.5	5.7	5.7	282.6	15.7	85	78	84	82	48	122	048.9	26	•	•	23	03	02	03	03	03	07	07	03	07	03	•	•	04	•			
VIII	3.5	3.7	2.8	3.3	267.0	14.0	82	65	78	75	18	062	040.8	11	•	•	28	12	13	07	05	14	02	06	02	06	•	•	02	•				
IX	4.1	4.8	4.5	4.5	195.0	13.6	88	79	87	85	65	203	071.0	25	•	•	14	•	01	12	11	11	08	10	09	05	10	•	•	01	03	•		
X	7.1	6.5	6.1	6.5	095.2	07.5	88	81	88	86	51	202	047.4	21	•	•	•	•	•	08	07	02	09	16	14	07	16	•	•	01	01			
XI	7.3	6.7	5.8	6.6	073.2	07.4	90	82	89	87	50	097	018.1	06	•	•	04	03	02	13	10	09	04	10	04	01	04	•	•	06	•			
XII	9.8	9.3	9.2	9.4	102.2	06.1	88	82	86	85	49	023	013.9	12	•	01	01	01	01	05	09	04	04	01	04	01	04	•	•	06	•			
GOD.	5.5	5.7	5.4	5.5	1859.6	06.8	86	77	84	82	18	1443	071.0	25IX	•	•	01	76	15	16	67	58	65	108	125	115	46	125	03	03	•	02	17	27
RATEČE-PLANICA																											H_b = 864 m H_b = 865.1 m h_t = 2.2 m h_r = 1.5 m							
I	7.4	6.3	5.9	6.9	074.2	03.7	95	75	92	87	42	024	016.0	01	•	04	30	•	•	01	•	03	11	06	03	01	01	06	•	•	01	08	31	
II	7.8	7.8	6.4	8.0	056.5	04.1	92	71	89	84	45	098	032.3	07	•	03	17	•	•	•	•	17	15	08	03	11	07	01	•	•	01	02	21	
III	8.3	8.2	6.6	7.5	113.8	04.4	96	61	88	82	29	115	053.3	05	•	01	23	•	•	•	•	03	15	10	07	03	03	07	•	•	01	01	23	
IV	6.4	7.7	6.2	6.8	141.4	04.6	92	53	78	74	24	093	027.1	29	•	17	•	•	•	•	03	11	08	06	04	07	03	02	•	•	01	•		
V	6.5	7.0	6.6	6.8	164.1	06.6	89	50	82	74	31	068	019.6	25	•	•	04	•	•	•	•	02	13	15	10	02	15	•	•	03	01	•		
VI	6.0	6.5	6.2	6.7	161.2	06.0	90	56	83	76	32	248	093.0	30	•	02	01	•	•	•	03	13	19	15	07	18	02	•	•	06	01			
VII	4.5	5.2	5.3	5.0	261.7	09.2	84	47	80	70	27	160	034.4	25	•	•	08	•	•	•	•	05	02	10	09	07	10	•	•	06	02	•		
VIII	5.4	5.0	4.5	5.0	226.6	10.8	94	56	87	79	26	125	035.6	29	•	•	13	02	•	•	•	04	08	10	06	04	10	•	•	01	04	•		
IX	5.5	6.1	5.1	5.6	182.5	08.3	95	62	90	83																								

Mesec	Vrstdinski Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vatre ND, Pm (0-12)														
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW	
		7	14	21							E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.
$\psi = 46^{\circ}23' N \lambda = 13^{\circ}51' E$ Gr. $\Delta G = + 55$ min.																										
I	561.0	-05>3	-04+1	-05+1	-04+9	-06+1	-07+5	03+4	22 -12.6	18 03 02+2	04 02+4	04 01+3	10 03+8	02 00+4	02 00+5	07 03+3	45 24+8	16								
II	554.9	-08+7	-06+8	-06+2	-06+0	-05+6	-10+1	02+6	11 -15.6	07 12 00+6	03 01+2	05 01+5	26 10+1	02 01.0	01 00+4	30 17+1	05								
III	558.8	-06+0	-04+1	-05+7	-05+4	-03+1	-07+5	05+4	21 -13.3	11 06 02+3	03 01+1	02 00+6	44 17+6	02 00+8	04 00+8	18 08+2	14								
IV	556.8	-0+6	-04+5	-05+9	-05+7	-03+4	-0d+1	01+4	12+10 -14.7	17 05 02+8	03 01+3	02 00+7	26 09+6	03 01+7	03 01+2	05 01+7	26 10+5	17								
V	559.5	-01+7	00+1	-01+1	01+4	-03+5	07+1	14 -0+2	24 16 06+7	01 00+4	06 02+3	12 04+0	01 00+4	01 00+2	02 00+7	38 14+1	16									
VI	561.6	00+8	02+3	01+3	01+5	04+2	-00+8	10+2	06 -0+2	13+08 18	07+7 01	00+4	09 01+6	13 04+7	01+3 00+4	04 01+6	35 14+6	13							
VII	565+2	04+5	06+4	05+1	05+3	08+0	02+6	13+3	30 -0+0	20 11 04+7	02 00+5	05 01+5	13 04+1	02 00+9	44 19+2	16								
VIII	566.9	06+8	08+7	07+1	07+4	10+0	05+3	16+6	15 -0+0	11 07 02+4	02 00+5	03 00+8	37 12+3	02 00+9	01 00+3	19 06+8	22								
IX	563.5	03+2	04+4	03+4	03+6	06+5	01+1	12+2	06 -0+6	27 16 06+9	07 00+4	04 01+4	27 08+2	02 00+7	02 01+0	13 06+6	24								
X	555+1	-07+5	-05+8	-07+0	-06+8	-04+2	-0+0	-0+6	25 -12+9	31 28 12+8	02 00+7	07 02+8	11 04+0	03 01+7	02 00+6	03 01+4	26 11+6	11								
XI	556+7	-05+6	-04+9	-05+5	-05+3	-02+8	-0+0	03+0	23 -14+2	01 33 20+8	05 02+5	02 01+1	16 06+0	01 00+4	03 01+7	19 11+0	11								
XII	560.3	-05+5	-04+4	-05+3	-05+2	-02+3	-0+2	05+1	22 -17+7	13 13 08+4	01 00+4	03 01+5	05 01+5	03 01+1	63 35+9	05								
GOD.	560.2	-02+6	-01+1	-02+3	-02+1	00+6	-04+5	16+6	15+M -17+7	15 XII 168	10+1 29	01+3 48	01+6 240	09+6 17	01+0 12	12 00+7	35 01+7 376	18+7 170								
$\psi = 46^{\circ}01' N \lambda = 13^{\circ}55' E$ Gr. $\Delta G = + 56$ min.																										
I	-	00+1	02+2	00+2	00+2	07+3	03+4	-02+6	11+7	20 -0+0	14 01 00+1	17 01+8	07 00+7	01 00+1	05 00+5	62							
II	-	00+2	02+2	00+8	01+0	03+1	-01+3	05+1	04 -0+3	28	27 03+2	07 01+0	05 00+6	04 00+4	41							
III	-	01+6	05+1	02+4	03+6	03+0	06+1	-00+4	17+0	22 -0+1	01	40 04+1	08 00+8	02 00+2	43							
IV	-	03+5	07+3	04+4	04+9	08+1	01+0	13+1	09 -0+0	14 ..	03 00+6	33 03+8	02 00+2	02 00+3	50							
V	-	08+9	11+9	08+2	09+3	14+8	05+5	19+5	21 01+0	24 02 00+4	10 01+0	12 01+5	01 00+2	68								
VI	-	11+4	14+6	10+7	11+9	15+4	07+7	22+7	04 06+5	10	15 04+7	17 02+0	01 00+2	57								
VII	-	14+5	18+4	14+0	15+3	19+7	10+3	25+0	30 05+5	20 02+2	17 01+8	16 01+7	14 01+4	01 00+1	43								
VIII	-	15+3	19+7	15+8	16+6	20+8	12+6	27+7	17 05+5	11	28 02+9	04 00+4	01 00+1	60								
IX	-	10+7	14+3	11+0	11+8	15+9	08+2	23+3	13 02+5	27	01 00+1	27 03+1	08 01+0	01 00+1	53							
X	-	01+6	04+3	02+2	02+6	05+7	-00+2	09+5	04 -0+0	31+30 02 00+2	24 02+4	06 00+7	02 00+3	04 00+5	55								
XI	-	01+7	04+0	02+1	02+5	04+9	-00+1	10+3	17 -0+1	30	10 01+0	11 01+9	03 00+3	01 00+1	65								
XII	-	00+9	03+0	01+0	01+5	04+3	-01+6	11+0	29 -0+0	15 01 06+1	05 01+2	03 00+3	07 00+7	05 00+5	06 00+9	66								
GOD.	-	05+9	08+9	06+1	06+8	10+0	03+3	27+7	17 VIII -07+1	04 M 08	00+2	09 00+9	251 02+8	105 01+3	36 00+8	23 00+5 663								
$\psi = 46^{\circ}21' N \lambda = 14^{\circ}11' E$ Gr. $\Delta G = + 57$ min.																										
I	-	-01+2	03+2	00+4	00+7	03+7	-02+1	16+0	20 -0+4	23 18 02+7	13 02+6	06 01+4	10 01+2	01 00+1	10 01+9	35									
II	-	01+9	07+0	03+7	04+1	05+7	05+7	12+9	12 -0+0	09 11 01+4	16 03+3	11 02+5	07 01+0	04 00+6	07 01+3	28								
III	-	02+3	10+1	05+9	06+0	10+8	01+7	21+5	22 -0+0	11 11 01+2	17 03+6	13 03+4	04 00+6	03 00+4	04 00+5	40								
IV	-	04+6	12+1	08+4	08+4	13+3	02+3	19+1	10 -0+6	16 09 01+6	15 03+9	13 03+1	07 01+5	01 00+1	13 01+4	32									
V	-	10+3	17+1	12+2	13+0	18+3	07+2	24+4	21+20 -0+2	10 10 01+3	08 02+1	10 01+9	07 01+0	06 00+9	11 01+9	41								
VI	-	12+7	18+8	14+5	15+1	20+1	09+7	25+7	04 03+2	12 07 01+5	15 01+2	03+1	07 01+9	05 01+1	10 01+7	02 00+3	47							
VII	-	14+4	22+8	17+4	18+0	23+8	11+7	28+4	30 08+0	26+09 08	09 01+2	06 01+4	05 01+2	08 01+9	03 00+7	05 00+8	58							
VIII	-	15+7	23+6	17+1	16+5	21+8	12+5	26+8	31 07+7	26 14 02+7	29 05+7	07 01+3	17 03+8	05 00+2	02 00+5	07 01+0	42							
IX	-	11+0	18+3	13+2	13+7	17+9	10+3	23+6	14 01+3	27 11 Gl.6	34 05+6	C7 01+2	04 00+8	09 01+7	14 04+0	04 00+3	05 01+1	06 01+1	06							
X	-	03+6	08+8	04+2	06+7	07+9	02+0	12+6	25 -0+1	30 07 01+4	37 07+7	03 00+5	01 00+3	09 02+4	16 05+4	05 00+7	08 01+2	07 01+1	39							
XI	-	01+2	06+7	03+9	04+4	07+6	02+0	12+6	17 -0+1	29 11 Gl.6	24 05+2	03 00+9	01 00+3	10 02+6	22 09+0	07 02+6	07 00+9	05 00+9	55							
XII	-	01+3	06+0	02+5	03+1	06+6	00+0	13+6	0																	

Meseč.	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm	Broj godišnja																	
	7	14	21		mm	7	14	21	Sred. mm	Tm	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	Δ	○	▲	■	□		
					mm	7	14	21	mm	Σ	Max	Min	Sred.	Max	Min	0.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.0	0.0	
KREDARICA																										
BR. ST.6																										
I	6.2	5.5	4.7	5.5	109.1	02.0	71	66	69	69	13	647	C14.1	01	06	13	31	•	•	•	•	•	•	13	31	
II	7.3	7.5	6.4	7.1	057.8	02.1	87	66	86	86	20	083	004.7	07	14	26	28	•	•	•	•	•	•	01	23	
III	6.0	7.4	7.5	7.0	117.9	02.5	80	82	85	82	17	099	C26.1	05	14	45	30	•	•	•	•	•	•	02	24	
IV	6.9	7.9	7.2	7.2	106.0	02.5	84	80	86	F6	17	080	015.6	29	06	47	30	•	•	•	•	•	•	•	23	
V	6.3	8.2	6.4	7.0	142.5	03.4	80	81	84	82	20	094	C26.5	25	•	15	27	•	•	•	•	•	•	03	24	
VI	7.3	8.4	7.5	7.5	125.0	04.3	83	84	82	83	40	381	096.0	30	•	64	17	•	•	•	•	•	•	10	23	
VII	4.6	7.5	5.5	5.9	232.3	05.1	71	78	80	76	36	200	035.8	25	•	01	09	•	•	•	•	•	•	02	16	
VIII	4.9	7.1	4.7	5.6	189.2	05.7	71	78	73	74	15	200	074.0	24	•	•	02	•	•	•	•	•	•	04	19	
IX	4.8	6.4	4.7	5.3	172.7	04.3	75	78	72	75	17	240	C38.7	25	•	C3	10	•	•	•	•	•	•	01	15	
X	7.2	7.7	7.9	7.6	080.2	02.3	88	87	80	68	37	210	026.4	05	10	31	31	•	•	•	•	•	•	02	24	
XI	6.8	6.4	5.7	5.3	109.1	02.4	77	75	73	75	20	104	017.1	06	12	23	30	•	•	•	•	•	•	03	18	
XII	4.8	4.5	3.8	4.4	128.3	01.6	69	63	66	66	14	012	007.6	17	13	18	29	•	•	•	•	•	•	•	10	
GOD.	6.0	7.0	5.9	6.4	1571.1	03.2	78	78	78	78	13	1750	C96.0	26 VI	73	196	274	•	•	•	•	•	•	04	17	
VRJSKE																										
BR. ST.7																										
I	7.1	6.6	5.0	6.3	-	-	-	-	-	-	-	075	C39.6	01	•	04	27	•	•	•	•	•	•	12	31	
II	8.0	8.3	7.7	8.0	-	-	-	-	-	-	-	202	074.2	07	•	03	17	•	•	•	•	•	•	10	21	
III	7.5	7.8	6.7	7.4	-	-	-	-	-	-	-	100	C38.7	05	•	05	16	•	•	•	•	•	•	03	22	
IV	5.4	7.8	5.8	6.4	-	-	-	-	-	-	-	180	080.0	29	•	•	07	•	•	•	•	•	•	C2	C5	
V	6.1	8.1	6.4	6.8	-	-	-	-	-	-	-	127	C28.5	25	•	•	•	•	•	•	•	•	•	02	05	
VI	7.2	7.7	5.5	6.9	-	-	-	-	-	-	-	260	C45.0	07	•	•	•	•	•	•	•	•	•	01	01	
VII	4.6	5.4	4.7	4.9	-	-	-	-	-	-	-	100	C44.6	26	•	•	01	•	•	•	•	•	•	02	02	
VIII	5.8	5.4	4.4	5.1	-	-	-	-	-	-	-	137	C51.0	29	•	•	06	•	•	•	•	•	•	01	06	
IX	6.1	6.2	4.9	5.7	-	-	-	-	-	-	-	415	C165.9	25	•	•	•	•	•	•	•	•	•	02	05	
X	7.9	6.1	7.4	7.8	-	-	-	-	-	-	-	396	052.1	21	•	•	14	•	•	•	•	•	•	03	15	
XI	6.1	7.2	6.5	7.3	-	-	-	-	-	-	-	188	C51.3	20	•	•	17	•	•	•	•	•	•	02	15	
XII	4.9	5.3	4.4	4.8	-	-	-	-	-	-	-	044	C36.0	12	•	02	21	•	•	•	•	•	•	08	14	
GOD.	6.6	7.0	5.8	6.4	-	-	-	-	-	-	-	2224	C165.9	25 IX	•	18	119	07	•	•	•	•	•	•	43	108
RAČEVNIJICA																										
BR. ST.8																										
I	6.3	6.5	7.1	7.4	-	-	-	-	-	-	-	04.4	S58	93	40	42	041	C26.0	01	06	05	01	04	05	12	18
II	7.0	7.3	7.7	7.3	-	-	-	-	-	-	-	05.1	87	73	86	82	42	081	C46.0	07	•	13	•	02	05	02
III	6.5	6.7	6.4	6.2	-	-	-	-	-	-	-	05.5	26	66	81	77	33	089	C59.1	05	•	14	•	01	05	30
IV	5.3	6.8	6.0	6.0	-	-	-	-	-	-	-	06.5	88	70	79	79	36	101	C57.0	29	•	04	07	11	01	•
V	5.5	6.5	5.5	6.0	-	-	-	-	-	-	-	10.2	89	83	89	87	45	070	C22.0	25	•	01	03	09	16	•
VI	5.6	7.1	6.5	6.1	-	-	-	-	-	-	-	11.1	90	77	88	85	50	248	C72.1	30	•	01	03	16	14	•
VII	4.6	4.3	5.0	4.5	-	-	-	-	-	-	-	12.0	51	61	81	82	29	183	C65.0	16	•	04	06	12	09	•
VIII	4.9	4.8	4.5	4.8	-	-	-	-	-	-	-	13.3	91	61	88	80	33	092	C23.8	11	•	14	03	08	08	01
IX	5.1	5.5	5.7	5.4	-	-	-	-	-	-	-	10.5	93	73	92	86	48	213	C070.0	25	•	09	14	08	17	•
X	7.6	7.1	6.4	7.1	-	-	-	-	-	-	-	05.8	95	76	91	87	49	207	C054.5	05	•	09	14	20	13	•
XI	6.4	6.5	6.6	6.5	-	-	-	-	-	-	-	05.4	92	73	89	84	38	076	C022.1	20	•	15	01	10	11	02
XII	4.4	4.0	3.7	4.1	-	-	-	-	-	-	-	04.1	83	65	84	77	38	01P	C18.0	12	•	26	03	01	01	02
GOD.	5.5	6.1	5.6	6.0	-	-	-	-	-	-	-	07.8	90	71	86	82	29	1419	C675.0	25 IX	•	08	106	25	03	•
JAVORJE NAD PELJANAMI																										
BR. ST.9																										
I	7.8	7.5	5.6	7.1	-	-	-	-	-	-	-	04.4	90	84	87	87	35	061	C34.5	01	•	08	22	•	•	•

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																				
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21	Sred. (Dies)							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.			
$\varphi = 46^{\circ}13'$ N $\lambda = 14^{\circ}29'$ E Gr. $\Delta G = + 58$ min.																														
I	734.7	-01.1	02.6	01.3	00.5	03.4	-01.9	18.0	20	-07.5	22	04	00.5	03	00.4	13	01.6	C3	00.3	02	00.2	01	00.2	10	01.5	06	C1.0	51		
II	727.4	01.2	07.8	03.0	03.7	08.7	-06.3	13.1	12	-07.6	09	03	00.5	01	00.1	C9	01.5	10	01.7	C2	00.2	11	01.8	19	03.4	11	C1.9	18		
III	730.5	00.9	10.7	04.4	05.1	11.7	-00.3	23.8	22	-06.7	14	07	00.9	03	00.6	09	01.4	C4	00.9	05	00.6	09	01.2	16	02.5	07	C1.0	33		
IV	727.3	03.1	13.0	06.2	07.1	14.3	-06.2	19.4	10	-07.0	17	09	C1.6	04	00.9	11	02.6	11	02.0	04	00.7	04	00.6	14	02.3	08	C1.4	25		
V	727.6	06.8	17.5	10.7	12.2	19.0	05.0	25.2	20	-00.4	26	03	00.6	01	00.1	10	C1.9	C5	00.9	07	01.0	13	02.8	17	02.9	05	C1.0	32		
VI	726.4	12.1	19.5	13.4	14.6	21.1	08.1	27.4	04	-06.2	12	05	01.1	03	00.7	10	C2.0	04	00.7	08	01.6	10	01.8	08	01.5	04	00.9	37		
VII	730.5	14.5	23.5	16.3	17.7	24.9	09.8	30.7	20	07	01.7	01	00.1	14	C2.1	04	00.7	10	01.6	05	01.1	15	03.6	06	C1.2	31				
VIII	731.1	15.2	24.6	16.9	18.4	25.9	11.4	32.1	17.6	05.2	13	01	00.2	03	00.4	10	01.7	12	02.3	05	00.8	02	00.3	13	01.9	08	C1.5	39		
IX	730.1	10.3	19.0	12.2	13.4	20.4	07.6	25.6	14.0	-01.7	27	04	00.8	01	00.1	11	01.9	06	00.9	08	01.3	02	00.4	08	01.2	12	C1.7	38		
X	726.4	02.6	08.9	03.6	04.7	05.6	06.6	14.4	25	-05.7	30	*	*	01	00.1	11	C2.0	03	00.3	09	01.4	02	00.5	19	02.9	06	C1.3	42		
XI	730.9	01.1	08.1	02.6	03.6	09.2	-01.0	15.4	18	-07.2	09	02	03	00.3	C4	00.2	C1	00.1	06	00.6	04	00.5	04	00.9	15	02.2	08	C1.6	47	
XII	732.2	-03.3	04.5	-00.7	07	00.0	05.9	-04.7	16.7	29	-11.5	15	01	00.1	07	01.2	C8	01.1	02	00.4	02	00.5	08	01.1	21	03.2	05	C1.2	38	
GOD.	726.8	05.5	13.3	C7.4	08.4	14.5	02.9	32.1	17.6	VMM	-11.5	15	04	48	00.9	30	00.6	117	01.8	71	01.3	66	01.1	71	01.5	175	02.6	86	C1.4	431
$\varphi = 46^{\circ}21'$ N $\lambda = 14^{\circ}30'$ E Gr. $\Delta G = + 58$ min.																														
JEZERSKO																														
I	-	-C1.6	02.9	-06.6	00.0	01.3	C3.9	-03.2	13.3	20	-07.6	15	*	*	14	02.5	C5	01.2	14	03.5	*	*	03	00.7	*	*	01	C0.2	56	
II	-	00.1	04.3	00.7	01.5	05.6	C5.0	-01.6	07.9	16	-05.4	09	*	*	14	03.6	C7	01.8	C10	03.0	*	*	07	02.3	01	00.5	01	00.3	44	
III	-	-00.4	07.5	01.7	02.6	06.6	C6.4	-01.4	19.7	22	-08.4	11	*	*	26	05.2	C5	01.1	06	01.4	01	00.2	08	02.5	01	00.2	01	00.3	45	
IV	-	01.0	09.0	03.4	04.2	10.3	C3.3	-00.3	16.1	12.9	-06.2	20	*	*	26	06.4	C7	01.8	05	01.0	*	*	10	02.4	01	00.2	02	00.5	39	
V	-	06.2	13.9	07.7	08.0	15.3	03.2	20.8	20	-00.8	26	*	*	15	02.5	C6	00.9	15	04.0	*	*	10	02.9	02	00.7	01	C0.1	44		
VI	-	09.5	15.6	05.8	11.2	17.3	05.3	24.1	04	-06.2	12	*	*	18	04.0	C3	00.8	14	03.3	*	*	07	02.1	02	00.5	03	00.8	43		
VII	-	12.0	19.7	13.4	14.6	21.2	09.4	27.0	30	04.2	26	*	*	11	02.5	C5	02.1	18	05.9	*	*	10	03.1	01	00.3	05	C1.6	40		
VIII	-	11.8	21.8	13.8	15.3	22.6	09.4	25.4	15	03.9	13	*	*	11	02.6	C5	01.2	14	03.6	*	*	09	02.4	02	00.5	01	00.2	51		
IX	-	07.3	16.3	09.2	10.5	17.7	05.9	24.8	14	-00.3	27	*	*	11	02.4	C5	01.0	13	03.5	*	*	07	02.0	02	00.6	*	*	52		
X	-	00.3	05.6	01.7	02.2	07.1	-01.0	12.6	25	-03.3	23	*	*	26	05.9	C2	00.3	14	04.9	*	*	06	02.2	*	*	*	*	45		
XI	-	00.4	04.8	01.3	01.9	06.1	-01.3	12.6	18	-06.1	29	*	*	08	01.6	C2	00.7	30	10.3	*	*	02	00.4	*	*	04	00.7	44		
XII	-	-02.1	02.9	-01.2	-00.4	04.2	-03.0	11.4	08	-09.5	24	*	*	18	04.9	C1	00.3	13	03.9	*	*	01	00.5	*	*	03	00.6	57		
GOD.	-	03.7	10.4	05.1	06.1	11.6	C1.8	29.4	15	VMM	-09.5	24	*	*	198	04.2	56	01.3	166	05.0	01	00.2	80	02.3	12	00.5	22	C0.8	560	
LJUBLJANA-BEZIGRAD																														
$\varphi = 46^{\circ}04'$ N $\lambda = 14^{\circ}31'$ E Gr. $\Delta G = + 58$ min.																														
I	744.7	00.1	C2.8	01.3	01.4	03.7	-04.4	11.3	20	-02.4	21	07	00.7	29	02.9	C8	00.8	13	01.4	04	00.5	07	C1.2	30	C1.2	07				
II	733.3	03.5	C0.5	04.5	05.7	09.3	02.8	15.0	19	-02.6	09	C7	00.9	23	03.8	10	01.6	12	01.8	02	00.2	14	03.5	05	01.2	06	C0.9	55		
III	730.3	03.4	11.4	07.4	07.4	12.4	03.0	24.4	22	-02.8	14	04	00.4	24	02.9	13	02.2	17	02.9	05	00.8	17	04.0	08	01.0	04	00.7	01		
IV	733.1	05.3	13.9	09.4	09.5	14.8	03.8	26.3	09	-01.3	20	06	00.9	34	05.9	14	02.4	17	02.8	03	00.8	11	02.6	01	00.1	03	C0.5	01		
V	-	733.3	10.7	18.5	13.4	14.4	19.7	06.7	26.1	20	04.0	10	06	C1.0	21	02.9	13	01.6	07	00.8	01	00.1	28	06.1	08	C1.4	02			
VI	-	734.2	13.0	20.4	15.6	21.2	11.0	26.6	04	04.6	12	08	01.6	10	01.0	C8	01.1	11	01.6	16	02.2	24	06.8	07	01.2	02				
VII	-	736.2	15.8	24.4	19.4	19.7	25.9	13.3	31.7	30	05.4	20	04	00.5	24	03.0	14	02.0	09	01.9	06	00.8	23	05.6	03	00.5	04	00.7	06	
VIII	-	736.6	16.3	25.9	20.3	20																								

Nesec	Oblačnost tm (0-10)				Vlažnost vazduha % m	Padavine mm	Broj dana na s: Tn Tx Tn Tx Tn F(0-12) Nrm(0-10) R mm														H _s = 362 m H _b = 363,6 m h _t = 2,0 m h _r = 1,5 m															
	7	14	21	Sred. (Dnes)			Broj sati	7	14	21	Sum.	Mn	Σ	Nx	Dat.	<	<	<	<	<	<	<	>	<	<	<	•	*	Δ	Δ	Δ	▲	■	□		
					mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	30.00.0	0.0	25.0	0.0	20.0	6	8	2.0	8.0	0.1	1.0	0.0	•	Δ	*	Δ	Δ	▲	T	≡	■	
BR. ST.11																																				
I	9.4	8.5	8.0	8.6	032.0	04.4	58	88	94	93	24	037	021.2	01	.	C3	31	.	.	C1	.	01	23	12	C7	01	10	08	02	01	01	.	.	21	14	
II	8.0	7.9	7.6	7.8	080.4	05.1	95	67	87	84	30	051	C29.5	07	.	.	16	.	.	01	.	01	17	13	07	01	13	01	01	.	.	02	07			
III	7.1	7.3	7.1	7.2	115.9	05.3	96	58	90	83	30	055	C26.1	05	.	.	20	.	.	01	.	03	14	08	06	03	04	08	03	.	.	01	10	08		
IV	5.7	7.9	6.3	6.6	153.8	05.4	91	47	79	72	21	059	C26.2	29	.	.	19	.	.	02	.	02	12	11	C7	01	11	04	.	
V	5.5	7.0	6.4	6.3	197.3	08.1	90	55	86	77	23	080	C24.2	25	.	.	01	01	.	.	01	.	01	09	16	05	03	16	07	05		
VI	7.0	6.8	5.5	6.4	185.2	09.9	92	58	88	79	30	263	C52.2	30	.	.	01	03	.	.	03	.	02	08	17	15	08	17	12	06		
VII	4.9	4.9	4.5	4.8	285.4	11.4	89	52	86	76	35	122	C44.8	26	.	.	17	01	.	.	06	04	11	08	04	11	08	06				
VIII	4.6	4.5	3.5	4.2	246.5	13.1	95	59	94	82	30	122	C37.1	11	.	.	15	07	.	.	01	.	10	04	16	12	04	16	12	08		
IX	7.4	6.1	5.2	6.2	146.2	10.1	96	66	96	86	33	190	C73.1	25	.	.	02	02	.	.	01	.	03	10	14	11	05	14	01	07	15	
X	8.8	7.7	7.5	8.0	076.2	05.8	98	73	97	89	39	255	089.5	05	.	.	14	.	.	.	01	.	19	20	17	08	20	05	06			
XI	7.6	6.9	7.0	7.2	079.1	05.4	96	72	95	88	30	080	C16.5	20	.	.	19	.	.	.	01	.	16	14	08	04	14	02	02	.	.	01	08			
XII	5.9	5.9	5.4	5.7	087.8	03.9	93	75	88	85	18	010	010.5	12	04	.	28	.	.	05	.	04	06	01	01	02	01	01	01	14		
GOD.	6.8	6.8	6.2	6.6	1665.3	07.3	94	64	90	82	18	1326	C73.1	25X	04	03	151	38	06	.	16	.	34	142	156	10E	43	146	20	09	01	01	01	56	120	
JEZERSK																																				
BR. ST.12	H _s = 879 m H _b = - m h _t = 1,0 m h _r = 1,5 m																																			
I	7.2	5.5	5.7	6.1	-	03.9	91	75	89	85	33	033	C23.8	01	.	02	26	.	.	01	.	04	10	06	04	01	04	05	.	.	08	20				
II	7.9	7.6	7.4	7.6	-	04.3	89	70	87	82	36	112	C68.5	07	.	01	17	.	.	04	.	02	17	15	10	12	02	06	.	.	02	19	01			
III	6.5	6.9	6.3	6.6	-	04.5	93	63	87	81	31	089	C55.9	05	.	01	19	.	.	04	12	10	07	03	02	08	.	01	.	.	02	16				
IV	5.6	7.4	6.1	6.4	-	04.6	88	56	82	75	30	100	C45.6	29	.	.	17	.	.	04	12	11	08	03	05	02	01	.				
V	6.0	C 7.2	5.4	6.2	-	06.6	91	57	84	77	28	096	C23.2	25	.	.	02	.	.	01	.	12	17	12	02	17	02	.				
VI	6.1	6.9	5.4	6.2	-	08.2	89	64	88	80	31	321	101.7	30	.	.	01	.	.	01	.	03	20	17	09	20	02	C1	.	.	.	06	01			
VII	5.4	6.7	5.7	5.0	5.1	-	09.4	85	56	82	75	35	209	C46.4	26	.	.	02	.	.	04	05	13	12	06	12	05	01				
VIII	4.1	4.8	4.0	4.3	-	10.6	93	59	90	81	35	145	C32.1	11	.	.	13	.	.	08	06	15	09	04	15	06	01					
IX	4.6	5.5	4.5	4.6	4.9	-	08.3	95	67	93	85	42	283	112.4	25	.	.	02	.	.	01	.	68	66	15	15	05	15	01	05		
X	6.0	7.3	6.6	6.9	6.9	-	04.8	95	74	92	87	40	298	086.3	21	.	.	17	.	.	02	.	01	16	21	14	07	1E	05	01	.	.	02	07		
XI	6.5	6.3	5.6	6.1	6.1	-	04.4	89	71	86	82	37	104	049.7	20	.	.	21	.	.	01	.	08	12	09	03	12	06	04	.	.	.	07			
XII	5.1	5.4	3.4	4.5	4.5	-	03.5	85	67	83	78	36	020	019.4	12	01	27	.	.	05	04	04	01	01	04	01	24			
GOD.	5.9	6.4	5.4	5.9	-	06.1	90	64	86	80	28	1810	112.4	25X	05X	.	05	149	15	.	06	.	44	117	159	118	47	141	39	06	01	.	01	24	16	88
LJUBLJANA-BEŽIGRAD																																				
BR. ST.13	H _s = 299 m H _b = 297,6 m h _t = 2,0 m h _r = 1,5 m																																			
I	9.5	8.9	8.0	8.8	019.3	04.6	95	67	92	91	52	045	C27.5	01	.	17	.	.	.	25	15	C7	01	11	06	02	01	03	.	.	23	05				
II	8.8	8.1	7.1	8.0	042.3	05.5	89	67	81	79	31	049	C22.2	07	.	05	.	.	.	16	11	08	01	11	01	.	.	.	01	C7	01					
III	7.2	7.1	6.8	7.1	113.7	05.6	91	57	75	74	27	060	C17.4	05	.	06	.	.	.	02	15	16	07	02	07	01	03	.	.	02	10	06				
IV	6.1	7.5	6.4	6.5	161.9	05.6	83	46	66	65	23	056	C10.5	29	.	01	.	.	.	04	14	11	08	02	11	04	.					
V	6.5	6.7	6.5	6.6	207.4	08.1	87	51	72	70	29	109	C31.0	25	.	.	03	.	.	01	.	02	12	15	11	04	14	04	02			
VI	6.8	6.2	5.7	6.3	189.1	09.9	88	55	77	73	29	245	C49.0	30	.	.	06	.	.	02	.	02	08	17	15	09	17	12	04			
VII	5.3	4.6	4.4	4.8	287.4	11.6	85	51	71	69	34	086	C35.0	19	.	.	19	06	.	01	.	06	04	11	06	02	11	06	05			
VIII	6.3	4.6	3.2	4.7	243.8	13.7	94	54	82	77	29	168	C38.7	11	.	.	17	12	.	01	.	07	06	13	12	05	13	01	08			
IX	8.8	5.9	4.6	6.4	145.8	10.8	96	63	85	83	26	168	C42.2	07	.	.	07	.	.	01	.	01	11	17	13	05	16	05	14			
X	9.4	7.3	6.9	7.9	071.9	06.2	96	71	90	86	40	283	095.8	05	.	03	.	.	.	16	22	19	09	21	01	01	05	17				
XI	8.3	7.2	6.5	7.4	072.4	05.7	92	68	85	82	31	112	C28.6	26	.	.	09	.	.	02	.	17	15	07	04	15	03	03	02	12		
XII	7.5	6.4	6.7	6.9	056.9	04.5	92	77	84	84	39	031	C26.1	12	01	01	28	.	.	01	.	03	13	07	02	01	05	01	01	01	15	
GOD.	7.2	6.7	6.4	6.8	-	07.3	87	64	77	76	13	1287	C77.8	5X	.	02	70	32	06	.	05	.	45	158	142	112	43	131	21	05	.	.	02	24	94	30
SMARTNO PRI SLOVENJGRADU																																				
BR. ST.15	H _s = 452 m H _b = - m h _t = 2.0 m h<																																			

Mesec	Vazdušni pritisak Pr. mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра nD, Fm (0-12)																
		Tm				Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21	Sred. (Dies)							8.	15.	22.	29.	8.	15.	22.	29.	8.	15.	22.	29.	8.	15.	22.	29.	
$\varphi = 46^{\circ}04'$, $N \lambda = 15^{\circ}11'$, E Gr., $\Delta G = + 1h\ 01\ min.$																												
I	-	60.4	64.2	61.6	62.0	59.1	-60.7	16.1	20	-03.4	18	03	60.6	.	.	12	02.3	01	00.1	.	.	.	09	02.1	01	00.3	67	
II	-	64.6	64.4	65.6	64.3	60.2	67.7	14.2	12	-01.6	08	16	64.4	.	.	16	04.7	02	00.5	.	.	.	16	04.2	06	02.7	28	
III	-	64.4	62.0	66.9	67.5	62.7	64.8	25.0	22	-02.2	14	22	64.3	.	.	16	03.8	02	00.5	09	01.5	01	00.4	17	03.4	04	02.0	22
IV	-	65.9	64.2	66.0	69.5	15.5	63.5	21.6	10	-01.7	05	12	63.1	.	.	26	06.0	01	00.6	07	02.9	01	00.3	24	04.8	02	00.7	17
V	-	11.2	16.6	12.6	13.9	20.4	08.1	27.5	20	03.9	10	09	11.4	.	.	19	04.8	.	02	00.4	01	00.4	30	05.6	02	00.5	30	
VI	-	13.7	21.0	15.9	16.2	27.6	10.4	27.2	12	04.2	12	06	11.5	01	00.3	15	03.1	01	00.3	01	01.5	.	.	24	04.9	03	00.8	29
VII	-	16.0	24.5	17.6	18.4	26.2	12.7	31.8	14	05.4	09	11	01.1	.	.	12	02.8	01	00.3	07	01.4	.	.	30	05.8	02	00.9	30
VIII	-	17.7	25.9	18.9	20.8	15.0	12.8	17.6	13	06.6	13	06	11.5	.	.	24	05.8	.	05	00.9	.	.	19	03.9	06	02.8	33	
IX	-	12.2	20.4	13.9	15.1	21.6	10.5	26.0	C4	06.7	27	03	01.3	.	.	11	01.8	.	08	01.3	.	.	19	03.4	06	02.0	38	
X	-	04.5	10.3	06.0	06.7	11.4	02.0	16.5	25	-01.6	30	19	14.3	.	.	C1	00.2	.	11	02.1	.	.	19	03.9	*	.	43	
XI	-	04.0	10.4	05.5	06.4	10.0	02.2	17.2	17	-01.2	07	27	14.4	.	.	C6	01.3	.	04	0.9	.	.	17	03.5	04	C1.8	32	
XII	-	31.2	67.5	63.1	63.7	66.5	-90.6	15.1	29	-06.6	16	25	65.3	.	.	C3	00.4	.	07	01.1	.	.	09	02.3	06	C1.8	43	
GOD.	-	C6.0	14.0	09.7	10.5	16.0	05.4	37.8	M7	VM -06.9	Km	166	04.2	01	00.3	161	04.0	08	00.4	49	01.6	03	0L.4	233	04.3	42	C1.9	412
$\varphi = 46^{\circ}37'$, $N \lambda = 15^{\circ}11'$, E Gr., $\Delta G = + 1h\ 01\ min.$																												
RADUJE CB DRAVI																												
I	-	-60.8	64.1	60.2	60.9	59.2	-02.6	15.5	20	-06.4	23	22	C1	00.1	C1	00.1	C1	00.1	C3	00.3	*	02	00.2	03	00.3	04	C0.4	78
II	-	C1.9	C8.2	63.5	64.3	C9.4	06.3	15.0	12	-03.6	23	03	66.3	C3	00.6	*	05	00.6	02	00.3	08	01.2	03	00.3	06	C0.6	54	
III	-	02.9	11.4	14.7	15.2	15.5	06.3	12.1	01.7	24.2	22	-04.1	01	01	00.1	04	00.4	C2	00.2	04	00.5	05	00.6	07	01.0	01	00.1	56
IV	-	04.0	13.4	17.4	18.0	19.0	01.0	21.5	10	-03.0	05	01	00.2	C1	00.1	C2	00.2	05	00.5	03	07	05	00.6	11	01.3	56		
V	-	10.1	18.3	11.9	13.1	19.8	07.1	25.5	27	06.5	10	01	66.1	.	.	C2	00.3	10	01.4	01	00.1	06	00.9	02	00.2	04	00.9	67
VI	-	12.9	20.1	14.6	15.3	22.3	05.4	26.3	M7	05.0	04	02.6	12	03	C6.3	C1	00.1	C1	00.1	04	00.5	02	00.3	08	01.6	01	00.1	66
VII	-	15.1	24.3	17.1	18.4	25.4	11.7	36.8	30	07.6	C9	.	.	04	04.4	05	00.7	02	00.3	05	06.6	06	00.8	65				
VIII	-	15.6	25.3	18.0	19.2	26.5	13.6	33.4	16	07.3	13	01	00.1	.	.	C1	00.1	02	00.2	01	00.1	03	00.3	05	04.6	03	00.3	77
IX	-	11.6	19.6	13.3	14.4	20.8	05.8	27.9	14	03.0	28	05	05.5	.	.	C1	00.1	C3	00.3	03	00.4	04	00.4	05	00.6	05	C0.8	64
X	-	03.0	10.0	06.8	05.9	11.1	02.6	15.2	07	-02.8	24	01	00.2	02	00.2	C2	00.2	C2	00.4	02	00.4	01	00.1	04	00.4	06	00.6	73
XI	-	03.0	08.9	03.7	04.8	10.6	01.1	17.7	15	-02.4	04	01	00.1	.	.	C3	00.4	04	00.7	11	01.5	06	00.7	10	C1.3	55		
XII	-	-01.7	05.4	06.0	06.9	07.0	-03.4	11.0	09	-09.0	15	02	00.2	.	.	C7	00.2	C5	00.5	*	01	00.1	01	00.1	06	C0.8	76	
GOD.	-	C6.5	14.1	08.3	09.3	15.4	04.4	32.4	M7	VM -05.0	Km	45	20	00.3	12	00.2	18	00.2	51	00.7	25	00.5	61	01.0	47	C0.5	795	
$\varphi = 46^{\circ}15'$, $N \lambda = 15^{\circ}11'$, E Gr., $\Delta G = + 1h\ 01\ min.$																												
CELJE-LEVEC																												
I	-	-60.7	64.2	60.5	61.4	64.6	-02.6	16.5	20	-06.5	24	02	00.2	24	02.4	C1	00.1	C4	00.4	*	12	01.6	*	*	03	C0.3	47	
II	-	C2.9	C8.7	63.5	64.3	C9.4	06.3	15.0	12	-03.6	23	03	66.3	C3	00.6	*	05	00.6	02	00.3	08	01.2	03	00.3	06	C0.6	54	
III	-	02.1	10.9	09.6	06.1	11.7	00.5	23.5	21	-05.5	15	01	00.1	18	02.0	C1	00.1	C7	00.7	*	09	02.1	*	*	05	C0.6	52	
IV	-	03.5	13.7	07.6	08.1	14.5	06.5	24.2	10	-05.2	05	01	00.2	C6.2	18	03.6	C1	00.2	09	01.0	02	00.2	13	00.6	40			
V	-	10.4	18.6	13.6	13.5	19.6	06.6	25.8	20	-06.4	10	02	00.2	27	01.1	C1	00.1	14	02.4	*	28	03.9	*	*	09	C1.2	30	
VI	-	12.9	20.6	14.9	15.8	23.0	05.2	27.4	C4	01.5	12	03	66.3	C3	00.6	*	07	00.9	01	00.1	10	01.4	29					
VII	-	15.3	24.2	17.9	18.8	25.4	11.5	30.5	17	06.6	09	02	00.2	12	01.4	C1	00.1	17	02.2	*	24	04.0	02	00.2	13	01.6	22	
VIII	-	15.8	25.3	18.8	19.7	26.2	12.4	34.5	17	06.0	13	01	00.2	C6.2	16	02.2	C4	00.5	*	15	01.6	01	00.1	07	C0.7	47		
IX	-	11.3	19.8	13.6	14.6	20.6	05.0	27.1	03	-00.2	27	*	09	01.1	C3	00.3	06	01										

Mesec	Oblačnost Nm (0-10)				Insolacije broj sati (tjed.)	Vlažnost vazduha				Padavine R mm		Broj dana na sat																			
	7	14	21	Sred. (tjed.)		mm	7	14	21	Sred.	Mn	Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(O-12)	Nm(0-10)	R mm	●	★	▲	△	◆	▲	▼	■	
						mm	7	14	21	Sred.	Mn	Max	Dat.	30.00	0.0	0.250	0.020	0.6	8	2.0	8.0	0.1	1.0	0.0	●	★	▲	△	◆	▲	▼
BR. ST-16																															
RAĐEĆE																															
I 9.6 8.1 7.8 8.5	-	04.6 89 82 90 87 42	030 016.6	C1	21	10	06	01	06	02	11	04	
II 6.6 7.6 6.6 7.6	-	05.4 81 60 81 74 24	042 022.4	07	02	15	11	08	01	01	07	01		
III 7.5 6.4 6.1 6.7	-	05.5 83 55 78 72 16	C74 027.2	06	.	.	.	03	01	04	03	14	10	07	03	06	07	01	.	.	01	02	02	
IV 6.6 7.4 5.2 6.2	-	05.6 86 46 69 64 16	038 014.3	26	.	.	.	01	07	.	04	14	08	06	01	08		
V 4.6 7.3 6.9 6.6	-	08.6 85 52 82 73 30	170 C38.3	25	.	.	.	04	02	.	04	11	17	15	05	17	03	.	
VI 7.1 7.3 6.2 6.9	-	10.3 86 55 83 74 36	211 056.2	07	.	.	.	06	04	10	18	14	06	16	05	01			
VII 4.6 5.7 4.4 4.9	-	11.8 84 51 82 72 32	C98 047.5	26	.	.	.	21	05	08	06	07	06	04	07	04	03				
VIII 5.6 6.7 3.2 4.6	-	13.7 90 55 86 77 31	179 C46.5	11	.	.	.	18	11	01	01	01	01	01	01	07	13	11	07	13	04	03					
IX 7.7 6.1 5.6 6.5	-	10.6 92 41 91 81 30	193 C58.6	25	.	.	.	06	02	.	05	13	14	10	06	14	02	05		
X 9.4 7.7 7.4 8.2	-	06.2 93 70 90 84 42	303 069.3	05	.	.	.	02	C1	01	15	23	19	08	23	01	.	.	.	01	11			
XI 7.2 6.8 6.1 6.7	-	05.8 87 65 85 79 27	107 C38.2	29	.	.	.	06	04	01	03	10	08	03	10	01	01	.	.	02	07				
XII 6.1 5.4 5.4 5.7	-	04.6 80 65 80 75 32	017 014.4	12	.	.	.	16	01	.	04	08	04	02	01	04	04	.			
GOD. 7.0 6.7 6.0 6.6	-	07.7 85 59 83 76 16	1462 C69.3	53	.	.	.	53	55	16	01	15	02	45	146	145	112	46	138	12	02	22	62	07			
BR. ST-17																															
RADLJE OB DRAVI																															
I 9.7 6.6 7.4 8.0	-	04.3 95 71 93 86 47	034 C15.2	02	.	.	.	30	17	04	04	01	02	03	01	06	18			
II 8.8 7.5 7.3 7.9	-	05.1 80 66 88 61 44	042 030.0	07	.	.	.	14	15	06	07	01	07	03	06	04				
III 9.1 6.8 7.0 7.6	-	06.1 94 57 88 63 38	116 054.7	07	.	.	.	10	02	15	10	08	03	05	07	04	15	11			
IV 7.8 7.2 6.3 7.1	-	06.0 89 57 79 75 28	024 010.6	26	.	.	.	11	02	12	05	03	01	05	05	.					
V 7.0 7.0 6.6 6.9	-	08.6 90 57 82 76 36	080 016.8	25	.	.	.	01	01	08	14	11	04	14	04	03					
VI 7.2 6.8 7.1 7.0	-	10.5 91 63 86 80 36	183 051.5	30	.	.	.	06	C1	11	15	15	07	15	06	04					
VII 6.0 5.0 5.3 5.5	-	12.0 90 56 81 76 37	148 C28.4	07	.	.	.	20	02	04	05	11	11	05	11	06	03					
VIII 7.6 5.5 5.2 6.2	-	13.5 94 61 87 81 34	224 C43.7	11	.	.	.	17	07	C3	09	13	12	06	13	07	09					
IX 8.4 6.2 5.6 6.8	-	10.7 96 67 93 85 45	208 C49.7	23	.	.	.	07	02	13	14	13	07	14	04	10					
X 9.5 6.6 7.5 8.0	-	06.1 96 71 92 86 38	201 050.5	21	.	.	.	06	16	18	12	07	16	16	01	01					
XI 8.2 6.5 6.7 7.1	-	05.4 88 68 89 62 36	C53 C17.2	26	.	.	.	15	01	11	07	06	02	07	C1	.	.	.	06	01					
XII 6.7 5.0 6.8 6.1	-	04.0 89 65 88 81 40	007 004.5	12	.	.	.	29	04	08	03	02	02	01	C9	01					
GOD. 8.0 6.5 6.6 7.0	-	07.7 91 64 87 81 28	1920 C51.5	30	.	.	.	116	51	09	.	01	.	.	19	140	126	104	44	117	17	04	37	94	36		
CELJE-LEVEC																															
I 9.3 7.4 8.4 8.6	-	030.6 04.7 96 85 54 92 40	037 016.4	02	.	.	.	25	20	10	07	02	08	06	16	10				
II 6.6 7.5 7.4 7.8	-	050.7 05.6 91 80 88 62 43	040 026.6	07	.	.	.	13	01	01	13	09	04	01	C7	03	.	.	.	01	07	01			
III 8.2 6.7 6.7 7.2	-	105.0 05.7 94 65 85 61 41	085 026.2	05	.	.	.	15	03	13	11	08	03	08	06	03	.	01	01	02	06	09			
IV 6.8 7.4 6.9 7.0	-	138.9 05.8 88 53 73 72 28	029 009.6	26	.	.	.	15	02	15	09	05	05	05	03	.					
V 6.2 7.3 7.5 7.0	-	171.9 08.9 91 59 81 77	32 074 018.8	05	.	.	.	01	02	C1	01	01	10	10	16	02	16	.	.	.	04	.				
VI 6.8 7.0 7.0 6.9	-	172.0 11.1 93 64 86 61 41	236 026.5	30	.	.	.	04	C2	01	01	10	19	15	05	15	.	.	.	06	04				
VII 5.3 5.7 5.4 5.5	-	255.9 13.1 92 65 80 79 37	086 C25.6	26	.	.	.	19	04	02	04	04	12	08	04	12	.	.	.	02	02					
VIII 6.9 5.5 5.1 4.7 5.6	-	219.4 14.9 95 69 82 65 46	146 035.5	11	.	.	.	18	09	04	06	13	12	06	13	.	.	.	07	08						
IX 6.5 6.4 5.7 6.3	-	129.2 10.9 94 71 93 86 46	202 048.6	23	.	.	.	C1	04	01	01	C3	C8	13	10	06	12	.	.	.	02	11				
X 8.5 7.6 7.5 8.0	-	048.7 06.0 95 71 90 85 45	215 066.7	05	.	.	.	09	01	17	21	15	06	21	01	13					
XI 7.7 6.8 6.7 7.1	-	047.6 05.4 88 64 86 80 40	C66 C22.0	29	.	.	.	14	01	09	10	06	03	10	C1	01	.	.	01	04					
XII 6.2 5.8 5.5 5.8	-	042.9 04.3 93 63 87 81 27	013 C11.7	12	.	.	.	26	01	05	06	02	02	01	02	01	.	.	.	01	10				
GOD. 7.3 6.7 6.6 6.9	-	07.7 86 72 83 8C 32 1531 065.7	5 X	07	.	.	.	61	22	.	C1	14	01	35	160	155	109	51	136	25	02	01	.	.	01	24	29	53			

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C							Čestina pravaca i srednja jačina vetrova nD, Fm (0-12)																				
		Tm			Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		.		
		7	14	21							8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.
$\varphi = 46^{\circ}24'$ N $\lambda = 15^{\circ}39'$ E Gr. $\Delta G = + 1h\ 03\ min.$																													
I	-	-00.5	04.5	06.8	01.4	04.9	-01.3	14.2	20	-05.0	22	.	.	06	00.8	*	*	04	00.6	*	*	21	02.8	01	00.1	05	00.7	56	
II	-	03.1	09.0	04.7	05.4	09.5	01.8	15.3	12	-03.2	23	.	.	10	01.8	C4	00.6	10	01.4	*	*	30	08.0	01	00.2	03	00.7	26	
III	-	03.2	11.4	03.3	06.8	11.8	01.6	23.8	21	-02.5	01	.	.	19	04.3	10	01.4	02	00.3	*	*	18	04.8	03	00.3	*	*	41	
IV	-	05.5	14.1	09.1	09.0	14.8	02.6	22.0	10	-02.8	20.0	.	.	14	04.2	14	02.6	05	00.8	*	*	14	02.3	*	*	01	00.1	42	
V	-	11.0	18.5	12.1	13.4	19.5	07.6	26.0	20	01.7	10	.	.	C5	01.0	*	*	C3	00.6	*	*	32	06.0	*	*	*	*	48	
VI	-	14.0	20.7	14.5	16.0	21.9	10.0	27.0	04	05.0	12	.	.	C6	01.1	*	*	C3	00.6	*	*	21	04.2	02	00.3	06	01.2	53	
VII	-	15.9	23.9	17.6	18.8	25.2	12.4	31.2	31	07.8	20	.	.	C2	00.4	*	*	C4	00.7	*	*	25	05.2	01	00.2	07	01.2	54	
VIII	-	15.9	25.3	18.7	19.7	26.1	13.8	32.5	16	06.2	13	.	.	C3	00.6	*	*	C1	00.2	*	*	22	03.5	03	00.4	10	01.7	54	
IX	-	11.4	19.6	13.4	14.5	20.3	09.3	27.2	C3	01.2	27	.	.	C9	01.4	C2	00.2	C6	00.8	*	*	19	03.5	01	00.1	*	*	53	
X	-	03.8	10.0	05.6	06.2	10.6	01.1	16.0	25	-02.5	31.27	.	.	C6	01.1	*	*	C1	00.1	*	*	30	06.4	*	*	07	00.8	49	
XI	-	03.8	09.7	05.0	05.9	10.4	02.3	16.8	17	-04.6	09	.	.	C9	01.2	*	*	C1	03.2	*	*	27	05.5	*	*	11	01.7	32	
XII	-	06.2	17.5	02.4	03.1	18.0	-01.4	15.5	29	-02.0	15	04	C0.4	01	00.2	*	*	*	*	*	*	26	04.4	09	01.6	17	01.9	36	
GOD.	-	07.3	14.5	09.1	10.0	15.3	05.1	32.5	KvM	-08.0	15 XII	04	00.4	64	02.4	34	01.6	56	01.4	*	*	285	05.0	21	00.8	67	01.4	544	
$\varphi = 46^{\circ}38'$ N $\lambda = 16^{\circ}11'$ E Gr. $\Delta G = + 1h\ 05\ min.$																													
I	754.2	00.6	03.0	0.7	01.1	C3.0	-01.0	14.5	20	-05.4	22	C1	00.2	*	*	C7	01.3	07	01.4	08	01.7	01	00.2	C2	00.4	02	00.4	65	
II	742.4	02.4	04.5	04.9	C8.9	01.3	15.8	12	-03.1	11	C2	C3.0	06	C1.7	*	*	C8	01.2	09	02.8	05	02.1	05	00.9	03	00.5	46		
III	745.8	02.9	11.2	06.6	06.8	12.1	01.5	23.2	22.21	-04.8	01	02	00.3	07	01.8	C3	00.5	06	01.0	05	00.9	10	03.7	03	00.4	02	00.3	55	
IV	742.5	03.4	14.2	08.6	09.2	15.0	01.2	21.0	10	-03.6	04	09	C2.6	19	05.7	C5	01.2	05	01.0	07	01.6	03	00.9	02	00.6	03	00.3	37	
V	747.1	11.3	18.2	12.4	13.6	19.2	07.3	25.4	20	01.7	27	10	02.4	C7	06.4	C4	00.7	03	00.6	07	01.9	10	02.7	*	*	06	01.2	51	
VI	742.5	13.4	20.9	14.4	15.9	21.8	05.8	24.6	04	02.3	12	06	C6.9	04	00.4	C4	00.6	08	01.5	05	00.6	14	04.3	11	01.4	17	04.6	21	
VII	744.9	16.1	23.7	17.8	18.9	25.0	12.1	30.4	31	07.0	20	16	03.0	C8	01.0	C4	00.6	12	01.8	08	01.6	18	04.1	02	00.4	06	00.8	19	
VIII	745.7	16.8	25.6	15.0	20.1	26.2	13.5	32.4	16	04.0	13	03.0	C3	00.4	08	01.8	02	00.5	06	00.8	02	00.3	06	01.3	43				
IX	744.9	11.7	19.1	13.2	14.4	20.1	09.2	26.8	C4.0	C6.7	28	04	C1.2	10	07.0	C2	00.5	07	01.4	08	02.6	04	00.9	02	00.3	05	01.0	46	
X	741.2	03.3	10.1	05.5	06.1	10.7	01.9	14.9	25	-04.7	31	08	C1.6	07	01.2	C7	01.2	06	01.2	12	03.3	14	04.2	*	*	04	00.7	42	
XI	745.7	03.2	09.3	05.0	05.6	09.9	01.8	17.1	16	-05.4	09	08	C1.3	09	01.5	C4	00.8	06	01.2	21	08.3	12	03.5	*	*	04	00.5	41	
XII	747.9	-00.5	C6.3	01.5	02.2	06.9	-01.9	16.4	29	-07.7	15	08	C2.1	C5	00.7	C9	01.3	05	00.7	04	01.2	07	01.0	03	00.4	09	01.7	43	
GOD.	744.7	07.4	14.1	09.1	09.9	15.0	04.8	32.4	KvM	-07.7	15 XII	04	1.9	53	02.5	45	00.9	81	01.4	96	03.4	104	03.2	32	00.8	67	01.9	496	
$\varphi = 46^{\circ}28'$ N $\lambda = 16^{\circ}12'$ E Gr. $\Delta G = + 1h\ 05\ min.$																													
I	-	-00.4	C2.5	C0.8	00.9	03.2	-01.3	14.5	20	-04.0	15.13	.	.	38	05.2	C7	01.5	12	02.6	*	*	33	05.1	02	00.4	C1	00.2	*	
II	-	03.2	C7.5	04.7	05.0	C8.0	01.3	15.8	12	-03.1	11	02	C3.2	06	C1.7	*	*	C8	03.3	02	00.7	*	*	*	*	*	*	*	
III	-	04.4	10.4	07.7	07.5	11.2	03.3	22.5	21	-04.0	01	.	.	59	12.7	C1	00.2	03	00.6	*	*	29	06.2	*	*	01	00.1	*	
IV	-	07.0	13.2	09.1	09.6	14.2	04.4	20.0	10	-02.0	17	.	.	57	14.8	*	*	*	*	*	*	29	05.6	*	*	04	00.7	*	
V	-	12.1	17.3	12.7	13.7	18.1	08.7	24.1	20	01.5	19	08.7	08	02.3	13	02.7	C1	00.2	07	01.8	*	*	42	09.3	03	00.6	07	01.7	*
VI	-	14.6	20.4	14.7	16.1	21.3	11.3	26.0	26.04	05.0	12	04.7	25	04.0	05.0	12	01.2	01	00.2	*	*	58	12.2	01	00.3	15	03.8	*	
VII	-	16.7	22.7	18.1	18.9	24.0	14.0	30.0	17	10.0	20	.	.	17	04.7	C1	00.3	11	02.3	*	*	59	12.4	*	*	04	C1.0	01	
VIII	-	17.6	24.4	20.2	20.6	25.1	15.9	32.0	16	11.5	12	.	.	35	08.6	C1	00.2	10	02.4	*	*	42	07.7	*	*	05	01.2	*	
IX	-	13.1	18.5	14.6	15.2	19.4	11.3	26.5	03	04.5	27	.	.	41	08.9	*	*	C1	03.0	*	*	23	05.4	*	*	06	01.3	04	
X	-	04.7	09.3	05.7	06.4	10.4	03.8	14.5	25	04.0	31.30	.	.	36	07.9	*	*	C1	03.1	*	*	35	08.9	*	*	08	01.0	04	
XI	-	04.4	09.0	05.5	06.1	09.8	03.5	17.0	17.16	00.0	29.09	.	.	30	06.1														

Mjesec	Oblačnost Rm (0-10)				Insolacij broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na s: H = 251 m H _b = m h _t = 2.0 m h _r = 1.5 m																								
	e _m			l		m	t		Tn			In	Ix	Tz	Tn			F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	■	□								
	7	14	21	Sred. (0-10)		mm	7	14	21	Stv.	Min	Max	Dat.	30.00	0.0	0.25	30.0	20.0	6	8	2.0	8.0	0.1	1.0	10.0	•	Δ	*	Δ	○	▲	■	□			
PHAGERSKO																																				
BR. ST.21																																				
I 8.3	5.6	7.2	7.4	-	04.7	95	62	94	90	52	031	006.2	02	.	.	25	03	19	08	08	•	06	04	10	09			
II 7.8	7.0	6.6	7.1	-	05.6	88	68	88	81	48	037	C27.0	07	.	.	09	.	.	.	01	.	04	13	05	05	03	04	02	03	02		
III 6.7	6.5	5.9	6.4	-	06.1	92	67	85	81	45	076	C41.3	05	.	.	11	06	14	09	05	03	05	08	03	02	03		
IV 5.2	6.0	5.8	5.9	-	06.2	83	56	75	71	34	020	004.4	26	.	.	09	08	14	04	04	•	04			
V 5.8	7.2	6.5	6.5	-	09.5	90	64	89	81	44	128	C33.6	05	.	.	01	03	12	12	11	05	12	01	02			
VI 6.1	6.7	7.0	6.6	-	11.3	91	66	88	82	47	127	C32.6	30	.	.	04	02	14	13	13	05	13	02	.			
VII 4.7	4.7	5.1	4.8	-	13.0	93	63	85	80	48	062	C25.2	25	.	.	17	05	.	.	.	08	08	08	01	06	01	.				
VIII 4.4	3.8	4.5	4.2	-	15.7	97	77	93	69	54	194	C26.4	11	.	.	15	04	.	.	.	12	07	11	11	07	11	04	.			
IX 6.4	5.1	4.6	5.3	-	11.4	96	77	94	89	58	137	026.3	23	.	.	04	08	10	10	10	06	10	01	03			
X 7.2	6.9	5.7	6.6	-	06.6	96	82	94	91	64	185	C49.4	21	.	.	05	.	.	.	01	.	04	13	13	05	14	01	.			
XI 6.1	6.2	6.2	6.2	-	05.9	86	72	86	82	52	054	C15.3	24	.	.	09	.	.	.	01	.	04	11	10	08	01	10	02	.		
XII 6.0	5.6	5.8	5.8	-	04.5	84	67	82	78	44	010	004.6	17	.	01	20	08	11	02	02	•	02	04	.			
GOD.	6.2	6.1	5.9	6.1	-	08.4	90	70	87	82	34	1021	044.4	21X	.	01	80	41	14	.	02	.	70	144	106	102	34	95	14	C3	.	.	01	10	25	14
MURSKA SRPSKA																																				
BR. ST.22																																				
I 5.2	6.1	7.8	8.4	038.5	04.5	53	63	92	89	47	041	C12.2	02	.	.	19	02	24	11	07	02	08	05	01	13	07		
II 8.4	7.9	5.2	7.2	057.2	052.4	91	67	83	60	34	039	C20.4	07	.	.	09	.	.	.	02	13	11	06	01	10	02	05	02			
III 7.7	7.2	6.4	7.1	097.7	05.8	91	59	82	70	36	051	C17.0	08	.	.	08	.	.	.	03	17	10	05	02	06	06	01	04	01			
IV 5.9	7.1	4.6	6.0	171.9	05.9	63	45	72	68	26	018	009.1	26	.	.	11	.	.	.	04	11	08	04	•	06	01	.				
V 5.9	7.1	6.1	6.4	181.9	00.8	85	56	84	75	29	083	C24.8	02	.	.	02	.	.	.	01	03	08	17	11	02	17	04	01			
VI 6.2	6.0	6.2	6.2	196.5	10.0	83	53	83	73	35	111	C32.5	30	.	.	05	.	.	.	01	02	17	18	11	03	02	06	04	04	.		
VII 5.6	5.2	5.3	5.4	239.6	11.6	83	51	80	71	31	070	C24.6	07	.	.	16	04	.	.	05	04	13	12	04	13	02	04				
VIII 5.5	4.3	5.6	5.9	253.4	13.8	91	56	87	78	42	141	C34.0	28	.	.	15	06	.	.	07	07	14	12	05	14	05	07				
IX 8.1	5.8	4.5	6.1	145.0	10.3	94	64	90	83	32	112	C36.1	02	.	.	03	.	.	.	03	08	13	09	04	13	03	10				
X 8.4	7.7	7.3	7.8	084.4	06.0	95	69	90	85	37	182	C47.4	21	.	.	09	.	.	.	02	19	18	14	06	18	01	01	10	.		
XI 7.7	6.6	6.2	6.8	105.9	05.7	90	69	88	82	33	069	C13.9	29	.	.	11	.	.	.	05	01	10	10	06	02	10	07	.			
XII 7.6	6.9	5.2	6.6	074.8	04.7	94	73	91	86	50	014	C06.4	07	.	01	23	.	.	.	01	03	13	05	03	05	01	01	05	01		
GOD.	7.2	6.6	5.9	6.6	1646.8	07.7	89	62	85	79	26	912	C47.4	21X	.	01	90	41	12	.	14	.	37	141	148	100	30	135	15	03	01	.	.	18	71	10
JERUZALEM																																				
BR. ST.23																																				
I 8.6	7.1	6.1	7.2	053.1	04.5	93	90	93	92	55	051	C20.0	02	.	05	26	.	.	.	04	18	10	10	01	07	04	15	17			
II 8.4	7.4	5.4	7.0	057.4	05.5	86	77	84	63	43	043	C23.2	07	.	07	.	04	.	.	02	14	10	05	01	09	02	06	04			
III 6.1	6.5	5.2	6.0	103.9	05.9	84	69	74	75	45	067	C24.5	06	.	08	.	05	.	.	10	16	09	05	05	07	03	02	03			
IV 5.6	7.0	5.0	6.9	154.2	05.8	73	53	67	64	26	022	C16.0	26	.	01	•	•	•	06	11	08	05	01	08	02	01	01				
V 5.0	7.3	7.3	6.5	145.8	08.8	81	64	76	74	42	106	C28.0	02	.	.	02	.	.	.	03	13	18	10	05	18	01	07				
VI 5.5	6.5	5.8	6.8	169.4	10.7	83	76	78	78	50	117	C41.4	30	.	.	05	.	01	.	02	17	15	11	03	15	07	.				
VII 4.7	5.7	4.0	4.8	243.8	12.5	84	66	75</td																												

Mesec	Vrednost Pratiljk Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра m/s (0-12)																		
		Tm			Sred. (tjess)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.									
$\varphi = 45^{\circ}51'$ N $\lambda = 13^{\circ}40'$ E Gr. $\Delta G = + 55$ min.																														
I	-	64.0	68.1	64.9	65.5	68.6	62.5	14.5	21	-02.6	26	03	01.0	.	.	20	07.8	01	00.2	01	00.3	.	.	02	00.6	.	.	66		
II	-	65.5	68.7	66.1	64.6	69.5	64.0	13.0	20.15	-06.3	07	01	00.4	.	.	35	15.2	04	01.5	06	02.7	.	.	*	*	.	.	36		
III	-	66.9	71.5	67.7	68.5	72.2	65.0	22.6	22	-06.6	01	03	01.0	01	00.3	45	18.4	05	01.8	01	00.2	.	.	03	00.8	.	.	35		
IV	-	69.3	73.0	69.8	70.6	74.4	66.8	17.6	09	03.4	19	.	.	02	00.8	43	16.7	05	02.3	08	02.6	.	.	05	01.8	.	.	27		
V	-	72.9	77.1	71.7	73.9	78.2	71.4	24.0	21	07.0	05	01	00.3	.	.	15	14.9	01	00.4	11	03.3	.	.	06	02.9	.	.	59		
VI	-	75.4	79.6	75.7	76.6	80.5	72.6	26.5	05	04.6	12	21	07.5	02	00.5	06	01.7	01	00.3	11	02.0	.	.	54		
VII	-	79.2	84.0	79.4	80.5	84.8	76.0	30.0	30.29	11.7	25	22	08.0	.	06	02.2	.	.	13	03.8	.	.	52			
VIII	-	81.1	86.4	81.7	82.7	87.2	78.3	32.2	16	10.4	11	40	13.9	05	01.7	10	03.0	.	.	03	00.9	.	.	35		
IX	-	85.9	91.2	86.5	87.5	91.7	83.9	28.0	15	07.8	25	38	13.8	01	00.2	11	03.8	.	.	03	01.0	.	.	37		
X	-	87.1	90.8	87.5	88.1	91.6	85.5	14.7	07	02.0	17	02	CC.8	.	.	31	12.2	01	00.3	11	03.8	.	.	07	02.2	.	.	41		
XI	-	86.9	90.7	87.3	87.8	90.4	85.4	13.7	17	01.0	30	.	.	01	00.3	23	06.7	.	06	01.7	.	.	02	00.5	.	.	56			
XII	-	84.4	87.9	85.7	85.7	88.4	82.8	14.8	03	-01.0	15.14	.	.	01	00.4	09	02.6	01	00.2	03	00.8	79		
GOD.	-	10.7	14.9	11.2	12.0	15.6	8.6	32.2	KvM	-02.6	26.1	10	00.8	05	00.5	24	12.6	26	01.4	82	02.8	01	00.3	50	02.2	.	.	579		
$\varphi = 45^{\circ}32'$ N $\lambda = 13^{\circ}43'$ E Gr. $\Delta G = + 55$ min.																														
I	763.5	75.8	68.3	66.3	66.7	94.2	64.5	13.7	20	01.8	18	.	.	02	00.7	C5	01.5	14	02.8	.	04	00.7	10	02.3	08	01.8	50			
II	756.2	75.5	61.0	68.0	68.6	12.1	64.4	14.8	15	02.0	08	.	.	13	04.8	17	05.2	23	04.8	04	01.1	05	01.2	03	03.8	07	01.6			
III	755.0	75.9	12.8	69.0	69.7	13.9	64.9	22.2	26	01.1	01	.	.	14	04.6	25	07.7	11	02.2	01	00.4	03	01.0	06	01.7	07	C2.0			
IV	755.6	10.5	15.1	11.7	12.4	16.5	65.1	19.9	06	05.1	16	.	.	11	03.8	16	05.4	25	05.1	03	00.6	03	01.2	06	02.1	06	C2.0			
V	-	15.1	18.8	14.8	15.9	19.7	12.0	26.5	21	05.4	09	.	.	02	00.6	C7	02.0	28	04.5	06	02.3	04	01.4	07	01.8	18	C4.7	21		
VI	-	17.9	21.1	17.8	16.7	22.6	14.6	27.1	05	09.1	12	.	.	01	00.3	C5	01.5	17	03.4	03	00.7	01	00.3	05	01.4	19	C5.5	39		
VII	-	21.5	25.8	22.3	26.9	18.1	31.1	17	13.4	26	01	00.2	.	01	00.4	05	01.6	22	03.2	03	00.6	04	00.8	06	01.3	18	C3.9	33		
VIII	-	24.0	27.3	22.1	23.4	28.4	15.0	32.2	20	13.5	11	.	.	06	01.8	12	02.7	09	01.5	.	.	01	00.2	06	01.2	13	C3.4	46		
IX	-	17.5	22.7	18.1	19.1	23.6	15.8	25.7	14	05.2	26	.	.	07	02.1	C9	02.3	10	02.5	.	04	01.0	10	02.3	08	C1.7	42			
X	-	05.1	13.0	09.8	10.4	14.4	07.6	17.5	06	04.5	31	.	.	11	04.0	16	05.3	17	03.4	07	01.6	07	02.0	04	01.0	07	C2.1	24		
XI	-	05.3	12.0	09.1	12.9	17.7	18.5	17	02.0	30	.	.	09	03.2	12	04.1	19	03.8	C4	00.9	05	01.0	07	01.5	08	02.0	24			
XII	-	05.8	09.2	06.7	07.1	10.0	04.5	13.0	20.01	01.0	15	.	.	04	01.4	10	03.1	17	02.6	03	00.5	05	00.9	06	01.2	09	C2.1	39		
GOD.	-	12.5	16.4	12.9	13.7	17.5	10.5	32.2	KvM	01.0	45 XII	01	00.2	81	03.4	129	04.5	212	03.9	34	01.2	46	01.1	76	01.7	124	C3.3	382		
$\varphi = 45^{\circ}31'$ N $\lambda = 13^{\circ}52'$ E Gr. $\Delta G = + 55$ min.																														
I	-	22.3	68.6	63.6	64.5	65.6	04.5	05.7	15.3	21	-02.0	24.18	05	01.0	04	00.7	C7	01.6	13	02.0	28	06.0	17	01.8	69	01.4	.	.	60	
II	-	05.3	09.9	05.9	06.8	11.1	03.8	15.4	15	-03.0	08	01	00.2	.	.	24	08.1	08	01.5	38	07.2	10	01.5	02	00.4	C1.0	61	.	.	61
III	-	02.0	12.3	07.0	07.8	13.4	03.8	21.5	22	-02.8	13	03	00.7	.	.	25	09.3	09	01.3	30	05.2	08	01.1	07	01.0	01	00.1	.	.	61
IV	-	08.2	14.2	08.9	10.1	15.5	05.3	19.0	08.07	-01.0	20	14	03.0	07	02.2	16	05.0	10	01.8	30	05.9	04	00.7	08	01.3	01	00.3	.	.	61
V	-	13.4	18.0	11.9	13.8	19.7	05.3	25.6	21	04.0	10	07	01.7	04	00.8	08	02.3	10	02.3	38	06.8	08	01.7	16	02.6	02	00.6	.	.	61
VI	-	14.1	20.9	14.8	16.7	22.3	12.0	28.5	05	04.5	12	04	00.6	.	.	08	01.9	13	02.8	40	07.7	09	01.5	15	04.6	01	00.3	C1.3	61	
VII	-	18.9	25.5	17.8	20.0	26.4	14.2	30.5	31	08.0	19	13	03.1	02	00.6	14	04.5	07	01.6	16	02.2	17	02.1	21	04.0	03	00.7	.	.	61
VIII	-	19.0	26.4	18.8	20.8	28.3	15.5	33.5	16	11.0	11	16	03.3	C1	00.2	17	04.7	06	02.0	18	02.5	13	01.7	17	02.6	03	00.3	.	.	61
IX	-	13.8	22.5	14.9	16.5	23.3	11.9	29.5	14	04.0	27	11	02.7	01	00.2	08	02.4	11	02.1	31	05.4	12	01.7	14	02.1	02	00.4	.	.	61
X	-	06.4	11.5	07.0	07.9	13.1	05.0	17.0	07	-04.3	17	02	00.5	C3	06.9	17	03.3	20	06.9	06	00.9	08	02.0	.	.	61	.	.	61	
XI	-	06.2	11.0	06.6	07.6	12.1	04.3	17.8	17	-03.2	02	03	00.5	15	06.7	C5	01.0	02	00.2	05	02.7	44	07.4	10	02.1	06	01.4	.	.	61
XII	-	02.5	08.5	03.2	04.4	09.4	06.6	14.0	03	-03.5	15	16	03.0	05	00.8	08	03.0	06	01.2	23	03.5	13	02.0	22	03.6	.	.	61		
GOD.																														

Mesec	Oblačnost Nm (0-10)				Insolacija broj sati Sred. Dneš.	Vlažnost vazduha				Padavine R mm		Broj dana na sat																						
						Tn	Tx	In	Tx			•	*	*	Δ	▲	▲	▲	▲	▲	▲	▲	▲	▲	▲	▲								
	7	14	21	Sred. Dneš.		mm	7	14	21	%	mm	Σ	%	at	≤	<	IV	IV	IV	IV														
BR. ST.26																																		
NAVELC FRI TEPNICI																																		
I	7.4	6.0	4.4	5.9	089.9	05.5	EE	71	87	62	27	077	C45.7	C1	•	•	C4	•	04	11	08	06	01	06	•	•	05							
II	6.4	6.5	5.8	6.2	095.9	05.7	01	70	79	76	40	147	C39.7	C7	•	•	01	•	07	04	11	11	05	11	01	•	02							
III	6.0	5.5	4.7	5.4	151.1	06.4	78	65	77	73	43	037	C24.6	05	•	•	02	•	05	07	07	04	04	01	04	C2	01							
IV	4.9	5.8	5.8	5.6	172.0	06.1	65	56	67	63	30	100	C44.6	29	•	•	•	•	05	16	11	09	04	11	•	•	01							
V	5.3	5.4	5.6	5.7	190.7	05.6	79	67	82	76	46	092	C17.0	65	•	•	•	•	01	04	08	15	13	02	15	•	04							
VI	6.0	6.0	5.6	5.9	168.1	11.0	79	71	79	76	48	250	C45.7	11	•	•	C4	•	04	04	15	15	06	15	•	•	06							
VII	3.4	3.6	3.7	3.6	289.0	12.2	70	57	71	66	44	078	C34.5	26	•	•	16	02	01	10	C3	05	04	03	05	•	•	01						
VIII	3.3	3.5	2.5	3.1	190.0	14.0	71	57	71	c> 24	080	C35.5	11	•	•	24	11	11	C1	16	C3	06	02	06	•	•	02							
IX	4.0	4.0	3.5	3.8	008.0	11.4	79	64	82	75	21	254	C73.0	24	•	•	•	06	•	01	01	10	C3	13	11	06	13	•	03					
X	6.5	6.6	4.8	6.1	114.3	06.4	82	68	72	77	45	355	C121.0	15	•	•	•	•	02	06	19	17	07	19	•	•	04							
XI	7.1	6.8	6.5	6.8	073.8	06.5	P3	75	63	80	37	111	C63.4	26	•	•	•	•	03	12	11	10	04	11	•	•	07							
XII	5.2	4.6	2.9	4.4	094.5	05.3	79	71	79	76	36	026	C19.5	14	•	•	03	•	•	08	C6	05	04	01	05	•	•	06						
GCD.	5.5	5.4	4.7	5.2	1958.4	GE.3	77	66	78	73	21	1614	C121.0	05.X	•	•	04	50	13	13	27	•	76	94	123	110	45	122	C3	C1	•	29	37	01
KOPER-SEMEDELJA																																		
BR. ST.27																																		
I	7.5	6.8	6.1	6.8	070.2	06.0	EC	77	85	F1	43	059	C13.8	C1	•	•	•	•	01	01	13	11	07	01	11	•	•	06						
II	6.6	7.0	5.3	6.3	127.4	06.0	73	64	71	69	58	053	C11.0	C7	•	•	•	•	07	04	04	C5	11	10	C1	11	•	•	01					
III	6.0	5.6	5.4	6.0	165.6	06.3	72	59	72	66	31	027	C20.6	05	•	•	•	•	07	01	06	10	C5	C2	C6	•	•	01	C1					
IV	5.4	6.3	6.7	6.0	197.1	06.3	61	51	61	56	34	071	C75.0	29	•	•	•	•	07	01	05	10	11	09	02	11	•	•	C1	C1	04			
V	6.3	6.5	5.2	5.5	-	05.6	72	61	77	70	42	065	C13.7	05	•	•	02	•	01	04	10	15	10	C2	15	•	•	05						
VI	6.2	5.9	5.7	5.9	208.4	11.8	74	66	76	72	41	225	C53.0	07	•	•	06	•	01	C1	02	C8	15	05	15	15	•	•	01	04	05			
VII	3.4	3.4	4.5	3.8	335.1	13.2	66	54	71	64	31	081	C30.2	26	•	•	26	07	08	02	•	C8	C4	09	06	03	C7	•	•	04				
VIII	3.5	2.5	2.3	3.1	310.4	14.6	71	56	71	67	44	139	C64.1	11	•	•	30	11	14	C3	15	C2	06	03	06	•	•	04						
IX	4.3	4.6	3.4	4.1	215.7	12.0	75	62	74	70	26	217	C52.6	26	•	•	13	•	04	10	06	12	10	06	12	•	•	03						
X	7.3	6.5	6.3	6.8	094.3	07.2	79	68	77	75	40	216	C39.7	05	•	•	•	•	03	01	10	20	17	10	20	•	•	01	04	05				
XI	7.6	7.4	7.1	7.2	066.9	07.2	77	71	80	76	32	100	C33.4	70	•	•	•	•	02	03	14	11	09	05	11	•	•	01	10	01				
XII	6.5	5.9	5.5	6.0	072.0	05.9	79	73	79	77	26	031	C24.5	12	•	•	•	•	02	02	10	07	05	01	C7	•	•	01	07	01				
GCD.	5.5	5.5	5.2	5.6	-	08.9	73	E2	74	70	24	1304	C64.1	HVM	•	•	77	18	23	4C	05	A1	104	133	105	4C	131	•	•	06	06	42	22	
KUVED																																		
BR. ST.28																																		
I	6.6	6.9	5.5	6.6	-	-	-	-	-	-	-	063	C35.0	01	•	•	11	•	•	C4	13	11	08	04	11	•	•	05						
II	6.4	6.8	5.3	6.2	-	-	-	-	-	-	-	079	C22.6	C7	•	•	04	•	•	C4	16	10	C2	11	01	•	•	01	01					
III	5.0	5.4	3.6	4.7	-	-	-	-	-	-	-	048	C41.2	05	•	•	05	•	01	03	05	02	02	01	C1	01	•	•	01					
IV	4.7	5.9	5.2	5.3	-	-	-	-	-	-	-	078	C31.5	29	•	•	01	•	•	C6	07	09	06	03	05	•	•	01	03					
V	5.6	5.4	5.4	5.7	-	-	-	-	-	-	-	056	C30.0	05	•	•	01	•	•	05	09	14	11	03	14	•	•	04						
VI	6.3	6.5	5.0	6.0	-	-	-	-	-	-	-	250	C53.7	16	•	•	06	•	•	C3	05	14	13	06	14	•	•	04						
VII	2.4	4.0	2.8	3.1	-	-	-	-	-	-	-	093	C45.5	26	•	•	22	05	•	01	14	02	05	04	02	05	•	•	03					
VIII	2.5	4.2	2.2	3.0	-	-	-	-	-	-	-	179	C59.5	11	•	•	29	11	•	•	14	C1	07	07	01	04	04	•	•	04				
IX	4.0	4.6	3.3	4.1	-	-	-	-	-	-	-	192	C62.2	C7	•	•	15	•	•	11	04	12	11	07	12	•	•	04						
X	7.2	7.3	5.4	6.6	-	-	-	-	-	-	-	266	C45.5	05	•	•	01	•	•	05	17	16	07	17	17	•	•	01	01					
XI	6.0	6.8	6.0	6.4	-	-	-	-	-	-	-	100	C30.0	26	•	•	05	•	•	C1	03	12	09	04	05	•	•	01	01					
XII	5.4	4.7	4.4	4.8	-	-	-	-	-	-	-	139	C29.0	14	•	•	13	•	•	C1	05	08	06	01	06	•	•	01	07	01				
GCD.	5.3	5.8	4.6	5.2	-	-	-	-	-	-	-	1423	C95.5	HVM	•	•	38	74	16	•	0t	•	40	87	116	10t	41	118	01	01	04	18	18	
AJDEVSČINA																																		
BR. ST.29																																		
I	7.4	6.0	5.5	6.4	089.8	04.9	86	67	84	79	34	052	C15.0	04	•	•	14	•	•	C4	02	05	13	10	02	10	•	•	04					
II	7.2	7.0	5.6	6.9	069.7	05.6	77	65	76	73	37	051	C35.0	07	•	•	02	•	•	C7	02	12	11	01	02	11	•	•	04					
III	5.9	6.2	5.6	5.9	147.3	06.1	75	58	74	69	33	011	C03.1	06	•	•	03	01	•	11	01	04	10	07	04	07	•	•	02					
IV	5.3	6.5	5.6	5.8	162.4	06.4	70	53	68	64	37	052	C25.5	29	•	•	02	•	•	07	02	04	11	09	03	09	•	•	01					
V	5.6	5.1	5.6	6.2	154.0	09.3																												

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Mesec	Vardušni pritisak Pr. mbar.	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s (0-12)																			
		Tm			Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C		
		7	14	21							8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	
$\varphi = 45^{\circ}34'$, N, $\lambda = 14^{\circ}15'$, E Gr., $\Delta G = + 57$ min.																													
I	-	-66.3	66.9	61.5	02.6	07.6	-01.4	17.4	20	-04.4	22	12	C6.0	C6	00.4	C2	00.3	C1	00.4	14	03.1	C1	00.4	03	00.5	C6	C1.5	52	
II	-	63.0	67.7	65.0	05.4	09.5	01.6	12.4	16	-05.5	28	16	C6.1	C6	00.4	C4.2	04	C1.0	19	05.4	02	00.3	02	00.7	02	00.8	C2	23	
III	-	61.8	61.5	60.4	06.3	12.5	00.4	24.5	22	-06.1	C1	14	C7.8	C1	00.4	C4	01.3	C4	01.4	13	04.9	0.	01	01.3	06	01.5	C4	40	
IV	-	64.3	64.7	66.1	08.4	14.1	02.4	15.0	09	-04.5	20	21	11.7	11	00.5	C2	00.5	0.	01	14	03.9	03	00.6	07	02.1	0.	33		
V	-	65.0	66.7	61.6	12.0	16.1	06.4	24.3	20	02.0	10.05	18	C6.2	C1	00.2	C2	00.7	C3	01	01.2	21	06.1	03	01.1	02	00.4	C3	40	
VI	-	62.1	69.0	14.2	14.9	26.7	07.0	27.1	04	06.5	12	20	C6.7	C6	00.7	C2	00.7	C3	01	01.2	23	06.2	0.	02	00.5	01	01.3	C4	42
VII	-	63.6	24.0	17.3	18.1	24.4	04.1	30.4	30	04.9	27	24	C6.1	C2	00.5	C7	01.9	C6	01.7	16	04.4	0.	04	01.5	01	02.2	C4	40	
VIII	-	63.7	26.1	14.3	19.1	27.0	11.8	32.0	17	06.1	12	14	C4.4	C7	00.6	C3	00.7	C1	00.3	18	04.7	01	00.3	03	00.6	02	00.4	C4	49
IX	-	66.3	21.0	13.6	14.6	21.7	04.0	28.0	15	06.9	27	11	C1.2	0.	0.	C1	02.9	01	00.4	17	04.1	0.	0.	02	00.5	02	00.7	C4	46
X	-	64.4	05.8	06.3	11.2	02.2	14.8	07	-03.3	30	20	C7.0	C1	00.3	C5	1.5	C4	01.6	C2	03	07.0	01	00.3	01	00.2	02	00.3	C4	38
XI	-	64.1	65.6	65.3	06.1	10.3	02.5	14.9	10	-06.0	62	12	C4.2	C1	00.2	C6	01.2	C7	01.6	20	05.6	05	01.7	01	00.1	02	00.5	C4	36
XII	-	60.2	67.5	62.4	03.1	Cd.6	-01.1	15.0	04	-06.9	17	17	C5.4	0.	0.	C8	02.3	07	C2.5	09	02.4	C1	00.3	02	00.6	01	00.1	C4	48
GOD.	-	66.3	14.5	69.0	09.7	15.5	04.3	32.0	N/VW	-08.1	08	214	C6.6	10	00.4	66	02.3	38	01.6	207	05.1	17	06.9	29	01.0	27	C1.0	487	
$\varphi = 45^{\circ}38'$, N, $\lambda = 14^{\circ}22'$, E Gr., $\Delta G = + 57$ min.																													
I	-	-61.8	63.0	-01.1	-06.2	03.5	-03.4	13.3	20	-07.5	15	+	27	C3.7	0.	0.	01	00.1	19	02.4	C2	00.2	26	C2.8	18				
II	-	60.1	02.4	60.1	60.1	61.5	07.4	16	-07.9	08	+	38	06.6	0.	0.	C1	00.2	0.	30	05.1	0.	0.	02	00.2	13				
III	-	-00.4	05.2	00.5	01.4	C6.0	-01.7	16.0	22	-07.4	13	+	57	09.4	0.	0.	0.	0.	0.	07	01.0	0.	0.	0.	15	C1.7	14		
IV	-	62.0	02.4	02.8	03.6	07.5	-01.1	14.2	09	-05.2	20	+	56	10.2	0.	0.	0.	0.	0.	03	00.5	0.	0.	11	01.1	20			
V	-	60.4	12.1	68.3	16.3	13.4	03.5	15.5	30	06.0	26	+	19	07.3	0.	0.	C1	00.1	06	00.6	21	02.6	0.	0.	20	C2.0	26		
VI	-	64.1	14.1	68.5	16.7	16.0	06.7	20.4	04	-01.0	12	01	C0.2	15	02.3	0.	05	0.9	09.9	0.9	03.2	0.	0.	08	00.8	24			
VII	-	64.1	18.9	14.5	14.5	14.9	05.9	25.4	30	04.5	05	+	28	05.0	0.	0.	C8	01.1	02	00.5	07	C1.1	0.	0.	28	C3.2	20		
VIII	-	64.4	20.0	13.6	15.6	21.5	16.3	28.0	15	03.7	12	01	C0.1	31	03.9	C3	00.3	C5	00.6	02	03.0	00	01.2	0.	07	00.7	34		
IX	-	65.0	15.1	69.7	11.1	11.1	06.6	21.5	06	-01.5	27	+	25	03.9	0.	0.	C10	01.5	C8	00.9	18	02.2	0.	0.	05	C0.7	24		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	61.2	04.7	01.8	02.4	05.9	-06.4	12.1	10	-07.6	02	05	C0.7	19	06.1	C2	00.3	C1	00.3	0.	30	06.2	02	00.5	10	C2.0	21		
XII	-	-61.3	04.2	-00.9	00.3	05.1	-03.7	13.4	29	-06.9	17	+	12	01.9	C4	0.6	C1	00.1	01	00.1	10	03.0	08	02.2	02	09.7	05		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 45^{\circ}53'$, N, $\lambda = 14^{\circ}26'$, E Gr., $\Delta G = + 58$ min.																													
I	-	-61.1	62.2	60.0	00.5	C4.2	-03.1	14.8	20	-10.3	22	22	C3.6	C9	01.9	C8	C1.6	09	01.6	10	01.6	06	C1.1	11	01.8	16	C3.9	02	
II	-	60.9	04.1	01.8	02.2	01.1	-06.5	06.5	01	-10.6	08	21	C5.5	04	01.1	C9	C2.3	16	05.5	11	01.5	08	C2.1	05	C1.0	09	C2.6	0.	
III	-	60.8	07.0	02.9	03.4	C7.8	-05.5	20.6	22	-11.5	14	16	C3.3	13	01.0	C7	C1.8	17	04.0	17	04.8	08	C1.9	0.	0.	02.5	06	C1.5	0.
IV	-	62.0	09.2	03.6	05.1	10.4	-02.8	14.3	09	-05.6	20	09	C1.6	15	04.5	19	05.6	14	03.7	08	01.2	08	01.6	10	01.4	07	01.3	0.	
V	-	69.5	13.8	08.5	10.3	15.1	04.7	26.8	30	-01.2	26	15	C2.5	13	03.5	C4	C0.4	05	01.6	19	03.4	06	C2.0	09	01.4	17	C4.0	21	
VI	-	62.0	15.8	11.3	12.6	17.5	07.2	24.6	04	-01.4	12	11	C2.1	17	02.5	C5	05.5	12	03.1	06	01.0	06	01.3	12	02.0	24	05.6	02	
VII	-	64.8	20.3	14.2	16.0	21.7	07.5	27.0	30	02.9	27	10	C1.6	14	02.9	C16	03.9	11	02.7	14	02.8	07	02.0	07	01.2	13	C2.8	03	
VIII	-	63.4	21.5	15.0	16.5	22.7	05.9	28.5	17	04.6	26	15	C2.4	07	01.6	C7	01.0	22	03.2	04	00.6	14	01.7	07	01.4	04	C4	04	
IX	-	60.1	16.3	11.3	12.2	17.5	07.3	27.4	27	-01.2	27	01	C0.2	11	02.9	C7	01.6	05	01.6	15	02.7	08	01.4	10	02.6	09	00.7	28	
X	-	62.3	09.0	02.0	02.4	03.5	07.0	20.4	30	-01.7	30	01	C0.5	13	02.5	C3	00.7	12	02.2	08	01.4	05	02.3	04	00.3	24			
XI	-	61.9	06.5	02.7	03.5	07.4	00.1	1.6	30	-1.1	31	01	C0.3																

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha	Padavine R mm	Broj dana na sat																							
						Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	R	T	≡					
	7	14	21	Sred. (Gies.)	Insolacijs broj sati	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm					
ILIRSKA PISTRICA																													
BR. ST.31																													
I	6.7	6.1	5.7	6.8	-	054 C 97 75 93 88 34	076 029.4	01	•	•	20	•	•	•	•	C1	12	13	C0	02	12	•	•	•	•	12			
II	7.2	6.6	6.5	6.8	-	054 C 90 66 82 60 27	069 043.2	07	•	•	08	•	•	•	04	•	03	13	12	10	03	12	01	•	•	C1	05		
III	5.5	5.8	4.5	5.4	-	052 C 89 55 78 74 20	079 066.5	05	•	•	11	•	•	•	07	•	07	06	04	01	C4	02	•	•	•	•	C7	04	
IV	4.9	6.2	5.0	5.4	-	055 C 83 52 70 68 25	136 045.4	29	•	•	09	•	•	•	02	•	C7	05	09	04	05	•	•	•	•	•	•	•	
V	7.0	6.9	5.9	6.6	-	084 L 92 58 82 78 33	155 045.7	05	•	•	•	•	•	•	C2	•	01	11	18	14	06	16	•	•	•	•	01	C7	
VI	6.9	7.1	5.8	6.6	-	101 C 91 65 65 60 23	254 045.8	10	•	•	01	•	•	•	•	•	01	12	17	13	07	17	•	•	•	•	01	10	
VII	6.8	4.5	3.6	4.3	-	114 C 90 52 79 74 36	090 035.7	26	•	•	18	02	•	•	01	•	08	04	09	02	04	05	•	•	•	•	C1	11	
VIII	6.5	5.6	5.2	4.0	-	124 C 96 56 83 76 29	047 C 77.0	11	•	•	21	11	•	C1	•	07	04	10	08	02	10	•	•	•	•	09	10		
IX	7.5	5.0	3.7	5.4	-	104 C 95 60 90 62 34	150 031.7	23	•	•	07	•	•	•	•	C5	C7	16	11	06	16	•	•	•	•	06	17		
X	6.5	7.5	6.7	7.7	-	064 C 94 70 91 65 40	264 079.0	05	•	•	07	•	•	•	•	•	18	22	16	08	22	•	•	•	•	03	11		
XI	7.0	7.4	7.1	7.4	-	064 C 89 75 91 85 41	090 028.8	26	•	•	12	•	•	•	01	•	C2	18	12	09	02	12	•	•	•	•	C1	10	
XII	6.6	5.0	5.3	5.6	-	044 C 91 71 62 63 41	025 014.3	17	•	•	18	•	•	•	•	C6	C9	10	04	01	09	02	•	•	•	•	14		
GOD.	6.9	6.0	5.2	6.0	-	074 C 91 62 84 79 20	149 C 079.0	05X	•	•	85	45	12	•	14	•	48	126	154	111	45	151	05	•	•	•	02	46	105
MASUN																													
BR. ST.32																													
I	6.4	5.5	5.5	6.1	-	-	-	070 C 34.6	C1	•	04	26	•	•	•	•	04	13	08	07	02	06	C4	01	•	C4	15		
II	5.6	7.1	6.9	7.6	-	-	-	170 C 74.6	07	•	05	26	•	•	•	•	02	16	13	04	12	C7	C2	•	C1	06			
III	5.5	7.1	5.6	6.5	-	-	-	065 C 32.0	05	•	08	27	•	•	•	•	03	12	10	07	01	C2	08	•	•	C4			
IV	4.8	6.2	5.4	5.5	-	-	-	138 C 52.5	29	•	14	•	•	•	•	C6	12	13	10	04	13	C2	01	•	C1	01			
V	4.7	6.4	5.5	5.6	-	-	-	181 C 04.7	05	•	•	•	•	•	•	•	05	C7	17	15	05	17	•	•	•	•	C2	02	
VI	5.3	7.1	4.6	5.7	-	-	-	261 C 52.2	07	•	01	•	•	•	•	C4	16	21	16	05	21	•	•	•	•	C1	14		
VII	2.7	4.6	3.7	3.4	-	-	-	132 C 7.0	26	•	•	02	•	•	•	•	C2	13	C3	11	11	04	11	•	•	•	•	C1	07
VIII	3.1	4.0	2.8	3.3	-	-	-	165 C 3.0	29	•	•	06	•	•	•	•	C6	06	11	10	06	11	•	•	•	•	06	04	
IX	4.3	5.0	3.4	4.2	-	-	-	217 C 06.4	25	•	01	•	•	•	•	C1	11	14	12	06	15	•	•	•	•	C1	02		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	C1	16	23	20	14	20	04	•	•	•	•	C1	06	
XI	6.2	6.2	6.4	6.3	-	-	-	133 C 45.7	26	•	•	17	•	•	•	01	C4	11	10	09	04	C6	04	•	•	•	C1	06	
XII	5.6	5.2	4.0	4.6	-	-	-	067 C 40.3	12	•	03	27	•	•	•	•	C7	05	10	09	01	C8	05	02	01	•	C1	01	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
RAKITNA																													
BR. ST.33																													
I	7.4	7.3	5.5	6.8	-	-	-	045 C 25.7	C1	01	05	23	•	•	•	•	C3	14	03	C5	01	06	01	•	•	•	•	20	06
II	8.2	6.6	7.8	8.2	-	-	-	074 C 040.0	07	01	02	16	•	•	•	01	•	16	16	10	03	12	05	•	•	•	•	C4	06
III	7.2	7.4	5.6	6.7	-	-	-	075 C 21.1	05	01	05	20	•	•	•	•	04	16	11	08	03	03	05	•	•	•	•	C1	18
IV	5.2	7.0	5.4	5.9	-	-	-	076 C 01.4	29	•	16	•	•	•	•	•	07	10	12	09	01	11	C2	•	•	•	•	C1	03
V	5.1	6.5	6.1	6.0	-	-	-	150 C 27.4	25	•	03	•	•	•	•	•	C2	05	17	13	C7	17	•	•	•	•	C1	01	
VI	6.4	7.1	5.2	6.2	-	-	-	260 C 54.5	07	•	01	•	•	•	•	•	C2	08	14	14	C6	17	•	•	•	•	C1	14	
VII	3.6	4.8	4.0	4.2	-	-	-	180 C 045.3	26	•	•	05	•	•	•	•	C8	C3	10	07	02	10	•	•	•	•	C1	03	
VIII	4.4	5.1	4.2	4.0	-	-	-	164 C 73.0	29	•	•	12	•	•	•	•	•	12	C6	10	09	05	10	•	•	•	•	C1	12
IX	6.0	6.0	4.6	5.5	-	-	-	210 C 054.7	C7	•	01	•	•	•	•	C7	11	14	11	06	14	•	•	•	•	C1	11		
X	7.7	7.6	6.4	7.3	-	-	-	398 C 69.1	05	•	19	•	•	•	•	C1	16	23	20	14	20	04	•	•	•	C1	08		
XI	7.5	7.1	6.4	7.0	-	-	-	131 C 040.5	26	•	14	•	•	•	•	•	02	14	16	09	05	16	06	•	•	•	•	C1	07
XII	5.1	5.4	3.7	4.7	-	-	-	052 C 036.5	12	03	01	22	•	•	•	•	05	C4	09	04	01	07	02	•	•	•	•	C1	04
GOD.	6.4	6.6	5.3	6.1																									

Mesec	Vrijednost Prstenskog Prašnog	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																		
		Im				Dat.				Dat.				N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (mies.)	Max	Min	Max	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
$\phi = 45^{\circ} 18'$ N $\lambda = 14^{\circ} 32'$ E Gr. $\Delta G = +59$ min.														KLCJEVJE												BR. ST. 36				
I	-	-01.3	03.1	00.0	00.4	03.8	-01.5	15.4	20 -03.3	26 01	00.4	20	04.4	17	03.4	02	00.2	*	*	*	*	*	*	*	*	23	04.1	20		
II	-	03.1	07.3	04.2	04.7	07.5	00.0	13.4	10 -02.8	08 07	03.9	12	04.3	13	06.9	04	01.5	*	*	*	*	*	*	*	*	23	05.5	06		
III	-	01.5	09.9	04.7	05.0	10.5	01.0	24.4	21 -04.3	14 16	03.1	04	01.3	10	02.9	12	03.4	*	*	*	01	00.4	*	*	*	31	05.0	13		
IV	-	03.7	12.1	07.2	07.7	13.0	01.7	15.6	09 -03.7	09 06	11.7	15	05.5	17	04.6	07	01.6	01	00.4	02	00.3	*	*	*	*	20	04.4	12		
V	-	04.7	16.7	11.7	12.3	17.7	06.6	25.0	20 00.1	10 02	00.4	26	05.3	15	01.7	10	03.4	*	*	*	04	00.6	*	*	*	20	04.0	17		
VI	-	12.0	16.0	13.9	16.7	20.5	05.1	26.0	04 01.9	13 12	02	00.8	17	03.9	13	05.3	03	00.6	*	*	*	*	*	*	*	*	36	06.9	17	
VII	-	14.7	17.5	17.0	18.0	14.8	11.2	30.0	30 05.6	09	*	*	39	07.5	18	05.7	11	03.0	*	*	*	*	*	*	*	*	14	03.2	12	
VIII	-	14.5	19.4	17.8	18.6	20.4	1.6	32.0	14 00.0	12	*	*	14	03.7	15	01.4	13	03.7	*	*	*	*	*	*	*	*	31	06.2	25	
IX	-	11.2	19.5	12.6	14.5	20.4	05.8	25.4	14 00.3	01.3	27	01	00.1	24	04.7	12	02.5	03	01.1	*	*	*	*	*	*	*	14	02.2	21	
X	-	03.7	08.2	04.2	04.8	04.3	01.5	15.5	25 -03.7	31 09	02.0	27	04.5	20	05.0	03	01.2	*	*	*	*	*	*	*	*	15	03.3	19		
XI	-	02.9	03.3	04.4	05.0	04.2	01.5	14.5	18 -00.1	04 02.0	36	02.7	13	01.9	03	01.0	*	*	01	00.3	*	*	*	*	*	20	04.3	09		
XII	-	01.7	04.9	00.2	00.8	06.1	-03.0	05.9	08 -09.3	15 02	00.4	18	03.4	13	05.5	04	00.9	*	*	*	*	*	*	*	*	41	07.4	17		
GDU.	-	06.0	13.1	06.3	06.9	14.0	04.3	32.0	05VM -09.3	15XII 54	02.0	291	04.9	187	04.6	77	02.5	01	00.4	08	00.4	*	*	*	*	*	268	05.2	187	
$\phi = 45^{\circ} 18'$ N $\lambda = 10^{\circ} 11'$ E Gr. $\Delta G = +1h 01$ min.														NEVC MESTO-GOTNA VAS												BR. ST. 37				
I	74.6 -00.5	03.7	00.6	03.8	03.8 -00.9	16.1	20 -03.9	18	*	08	01.7	09	01.2	06	00.8	07	01.0	19	02.9	12	01.8	05	00.7	27						
II	74.6 03.0	05.4	05.4	05.6	05.4 02.3	14.0	11 -02.1	28 01	02.2	10	02.0	16	04.3	05	00.6	09	01.4	18	03.1	14	03.0	04	01.0	07						
III	74.4 -1.1	04.0	10.8	06.6	11.6	06.2	24.4	21 -03.7	14 03	00.4	12	02.4	15	03.0	12	01.4	15	02.9	14	04.7	14	01.9	06	01.0	02					
IV	74.6 04.0	13.0	05.5	04.9	14.3	03.0	26.9	16 -01.6	05 02	00.4	21	06.3	13	03.8	04	01.6	07	00.9	21	02.5	14	01.5	06	01.0	02					
V	74.6 16.6	16.6	12.8	13.5	14.4	06.1	25.9	22 03.0	10 06	01.4	13	02.8	04	00.9	01	00.1	10	01.7	27	05.0	21	04.0	08	01.9	03					
VI	74.1 13.2	16.5	16.1	21.1	16.6	26.6	26	04.1	12	02	00.5	07	01.4	11	02.0	03	00.4	14	01.9	15	02.4	26	04.2	11	02.0	01				
VII	74.2 15.1	16.9	16.9	15.3	25.6	12.1	31.4	17 06.6	09	02.0	09	02.6	10	02.6	08	01.3	12	02.1	25	04.6	17	02.5	06	01.1	02					
VIII	74.6 16.1	17.7	19.7	20.1	17.5	14.7	33.9	04 06.7	13 12	04	06.8	16	03.3	11	02.6	06	01.2	13	01.4	15	02.1	13	01.4	07	00.7	06				
IX	75.1 11.7	16.4	14.2	14.8	20.6	10.7	27.6	03 01.4	27	08	01.3	15	02.5	08	01.5	01	00.1	13	01.4	13	01.5	14	02.1	02	00.3	16				
X	73.5 05.7	05.2	05.2	10.3	02.6	15.7	25 -02.4	30 02	02.2	05	02.5	07	01.3	05	00.6	10	01.3	16	02.3	21	02.0	10	01.4	07						
XI	74.7 03.4	04.0	05.0	05.6	05.8	02.3	17.4	17 -06.0	29 01	00.2	14	02.3	09	01.6	03	00.4	08	01.0	28	05.1	17	03.1	03	00.3	07					
XII	74.6 -00.5	05.9	01.6	02.1	06.7	-01.5	12.2	03 -07.5	15 02	00.3	04	00.8	06	00.9	01	00.7	19	02.7	32	04.3	21	02.8	03	00.5	06					
GDU.	74.2 07.0	11.7	09.6	10.0	14.9	05.6	32.9	04VM -07.5	15XII 35	00.9	01.9	143	02.6	119	02.5	57	01.0	127	01.7	251	03.7	204	02.8	71	03.2	86				
$\phi = 15^{\circ} 04'$ N $\lambda = 15^{\circ} 12'$ E Gr. $\Delta G = +1h 01$ min.														CRNCMELJ												BR. ST. 38				
I	-	-00.5	03.0	00.6	01.0	03.8 -01.3	15.4	20 -05.6	22 05	00.6	10	01.5	10	01.2	*	*	08	01.1	02	00.3	06	01.0	*	*	52					
II	-	03.7	08.8	06.4	06.2	09.7	02.7	14.5	12 -10.3	09 15	02.8	11	02.4	09	01.8	*	*	02	00.4	15	05.2	10	01.2	*	22					
III	-	01.8	11.5	07.6	07.6	11.5	02.9	22.3	21 -04.6	14 17	03.6	03	00.7	07	01.6	02	00.3	05	01.0	15	03.9	15	03.1	*	24					
IV	-	05.7	14.0	09.7	09.7	15.1	03.7	22.1	10 -00.8	04 19	05.7	09	02.7	09	03.0	02	01.2	08	01.5	13	03.2	03	00.6	01	00.2	27				
V	-	11.4	18.8	13.4	14.3	19.9	06.6	25.4	20 01.9	10 05	01.1	05	00.9	07	01.4	05	01.3	05	01.2	14	04.4	07	01.4	01	00.4	44				
VI	-	13.9	26.8	16.1	22.6	21.1	27.3	26 03.8	13 02	04.4	08	01.6	08	01.6	06	02.6	03	01.3	07	02.6	09	02.9	10	04.5	07	00.4	42			
VII	-	15.4	24.9	19.1	19.7	26.3	13.3	31.6	17 06.1	09 02	05.5	11	02.2	03	01.3	05	02.6	04	00.8	13	03.5	09	01.7	01	00.2	36				
VIII	-	16.0	16.2	19.8	20.4	14.4	14.0	33.8	04 07.4	12 15	02.8	01.1	10	01.4	05	00.9	04	00.7	05	00.9	*	*	*	*	*	42				
IX	-	11.1	18.4	14.1	15.2	21.5	10.7	25.1	03 02.7	27 02	00.4	23	02.9	*	*	08	01.1	03	00.4	42	02.2	02	00.4	08	01.0	22				
X	-	04.1	10.2	05.9	04.5	10.4	02.7	15.7	25 -03.0	31	*	*	22	02.9	06	00.8	08	00.9	*	*	25	03.5	10	01.4	10	01.1	17			
XI	-	01.4	09.6	04.5	05.4	10.2																								

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha			Padavine R mm			Broj dana na sat																								
	7	14	21	Stred. (Dnev.)	Insolacija broj sati	mm	7	14	21	Sred. Min	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■		
KCCEVJE																																		
BR. ST.36																																		
I 5.5 7.3 6.6 6.6	-	04.4	55	87	95	52	58	043	C26.3	01	.	01	27	23	07	06	01	05	05	18	C6		
II 7.6 1.6 6.6 7.3	-	05.4	90	71	91	84	24	C78	C26.3	07	.	.	09	.	.	.	02	15	15	07	04	12	05	01	01	03	02		
III 8.3 7.0 5.6 7.0	-	05.4	93	65	85	81	36	C91	C30.1	05	.	.	16	.	.	.	01	12	15	11	08	04	02	10	01	04	15		
IV 5.9 7.1 5.2 6.1	-	05.9	90	57	84	76	30	092	C32.1	25	.	.	13	.	.	.	05	11	13	07	04	12	01	01	.	.	
V 5.5 7.0 5.7 6.1	-	08.2	94	58	83	76	29	151	C32.4	01	.	.	01	.	.	.	01	09	21	14	06	21	04	03	.				
VI 6.2 7.3 5.5 7.4	-	10.1	91	64	86	80	35	196	C34.2	30	.	.	01	.	.	.	02	09	20	14	07	20	01	05	04				
VII 4.8 4.3 3.0 4.0	-	11.3	88	56	77	73	37	112	C59.6	26	.	.	17	01	.	.	08	02	11	10	03	11	01	07	03				
VIII 7.9 4.8 3.6 5.5	-	12.9	96	62	84	81	35	293	110.2	29	.	.	15	07	.	.	05	09	11	08	06	11	10	12	.				
IX 9.2 5.6 4.6 6.5	-	10.5	96	67	89	84	28	208	C52.1	25	.	.	06	.	.	.	09	15	15	07	15	03	03	02	15	.			
X 9.1 6.0 6.0 7.7	-	05.8	96	76	95	89	38	334	C55.7	21	.	.	10	.	.	.	01	15	25	21	09	25	03	03	03	07	.		
XI 7.4 7.4 6.7 7.2	-	05.7	92	74	90	85	38	118	C37.1	29	.	.	13	.	.	.	02	15	16	09	05	16	02	01	01	02	04		
XII 6.6 5.6 3.7 5.3	-	04.4	93	79	93	88	49	032	C16.8	12	.	.	25	.	.	.	01	05	07	07	04	01	06	02	10	08	.		
GOD. 7.3 6.6 5.4 6.5	-	07.5	92	68	87	82	24	1748	110.2	29VM	.	01	113	40	06	.	07	.	32	139	172	123	57	157	28	05	.	.	04	01	38	E7	36	
NOVO PESTO-GOTVA VAS																																		
BR. ST.37																																		
I 9.6 8.8 8.0 9.8	019.3	04.6	97	89	97	94	48	032	C09.5	18	.	01	24	24	11	05	08	04	C1	21	C1	.			
II 8.1 7.8 7.5 8.0	072.1	05.5	90	68	83	80	29	033	C11.7	15	.	.	05	.	.	.	03	.	18	10	05	02	06	02	01	01	05	.	
III 7.6 7.3 6.8 7.3	115.6	05.7	93	61	79	78	33	078	C26.2	06	.	.	08	.	.	.	02	01	15	12	08	04	10	05	01	01	03	09	
IV 6.4 7.4 6.7 6.8	155.0	05.7	87	51	68	69	26	050	C15.2	26	.	.	05	.	.	.	03	02	12	11	09	02	11	01	01	C1			
V 6.2 7.1 7.1 6.8	200.6	08.5	89	55	80	75	25	145	C25.8	01	.	.	02	.	.	.	03	02	11	17	15	06	17	06	C5	.			
VI 6.7 7.1 6.2 6.7	182.3	10.4	89	56	84	77	28	163	C30.3	30	.	.	02	.	.	.	02	10	17	14	07	17	01	04	.				
VII 5.1 4.9 4.5 4.6	286.9	11.9	86	52	77	72	34	062	C33.4	26	.	.	19	04	.	.	01	07	05	11	07	01	11	07	03	.			
VIII 6.4 5.3 5.3 5.2	247.1	14.3	95	62	88	82	40	147	C05.6	26	.	.	16	04	.	.	04	14	10	10	06	10	05	14	.				
IX 7.9 6.1 5.2 6.4	160.4	11.2	57	69	96	87	41	160	C43.5	25	.	.	03	.	.	.	03	12	16	11	07	14	03	16	.				
X 8.5 7.9 6.5 7.6	074.5	06.3	97	76	95	90	39	275	C05.0	21	.	.	06	.	.	.	01	15	23	17	09	21	01	01	04	17	.		
XI 6.0 7.2 6.9 7.8	085.6	05.8	93	70	90	84	30	082	C23.3	29	.	01	10	.	.	03	01	11	12	07	04	12	01	01	02	07	02		
XII 6.9 6.5 5.5 6.3	092.9	04.7	96	74	91	87	25	029	C15.9	12	.	01	22	.	.	01	03	11	08	04	01	08	02	01	16	04	.		
GOD. 7.2 7.0 6.3 6.8	1692.3	07.9	92	65	85	81	26	1752	C55.0	21X	.	03	83	80	42	08	.	15	.	26	151	158	112	49	146	15	09	02	.	02	01	44	119	7
ČRACPELJ																																		
BR. ST.38																																		
I 5.7 8.7 8.5 9.0	-	04.6	96	88	96	94	36	048	C18.0	01	.	01	18	24	21	06	02	18	04	02	18	06	.		
II 6.0 6.1 7.9 6.0	-	05.6	89	72	82	81	32	041	C12.6	15	.	.	03	.	.	.	03	.	16	17	C5	01	15	02	04	.			
III 5.3 6.9 7.3 7.1	-	05.9	91	63	73	78	29	092	C22.5	05	.	.	04	01	.	.	02	14	12	08	04	09	11	04	03	01	06	04	
IV 5.9 6.6 6.9 6.3	-	06.0	84	52	68	68	22	061	C24.1	26	.	.	02	.	.	.	01	06	12	12	05	01	12	01	01	02	.		
V 5.6 7.1 7.5 6.7	-	08.7	87	54	77	73	29	162	C33.3	01	.	.	04	.	.	.	C1	01	11	17	13	07	17	07	01	.			
VI 7.7 7.2 6.8 6.6	-	10.8	85	60	81	75	41	168	C34.5	30	.	.	06	.	.	.	01	02	18	20	13	02	20	07	01	.			
VII 4.1 4.4 4.2 4.2	-	12.1	86	54	75	71	34	085	C35.4	26	.	.	21	05	.	.	01	10	04	09	08	03	09	05	04	.			
VIII 4.2 4.7 4.1 4.3	-	14.2	93	59	86	79	30	278	C07.1	26	.	.	19	10	.	.	11	06	10	10	05	10	10	11	.				
IX 6.6 5.6 6.3 6.2	-	11.3	56	88	90	85	46	186	C04.0	21	.	.	08	.	.	.	C1	04	12	14	12	07	14	05	16	.			
X 7.9 7.0 6.5 7.4	-	06.4	96	76	93	88	45	324	C04.0	21	.	.	08	.	.	.	C1	02	16	24	21	12	24	01	01	16	C7		
XI 6.4 7.3 7.2 7.6	-	06.2	92	74	87	94	34	105	C36.2	29	.	.	10	.	.	.	C1	01	16	13	08	04	13	01	01	01	10	C7	
XII 6.1 5.4 5.6 5.7	-	05.6	90	73																														

Mesec	Vardubljan pritisak mm Pm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																	
		Tm			Max	Min	Max.	Dat.	Min.	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21	Sred. (Dnev.)						8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.			
$\varphi = 41^{\circ}18'$ N $\lambda = 16^{\circ}23'$ E Gr. $\Delta G = + 1h 05$ min.																													
I	752.9	-00.1	03.4	01.0	01.3	03.9	-00.6	13.0	20	-04.3	22	11	01.8	01	02.0	14	01.8	10	01.8	28	02.7	07	01.6	12	01.7	04	01.5	06	
II	745.5	03.0	08.7	05.0	05.4	09.5	02.0	15.8	12	-02.5	28	10	02.5	11	02.4	14	01.7	04	01.5	15	02.8	14	03.4	11	02.7	02	01.0	03	
III	748.6	03.4	11.5	06.7	07.1	12.1	02.3	22.8	21	-03.2	01	14	02.2	16	02.3	21	02.0	01	01.0	10	02.1	13	02.5	10	02.4	02	02.0	06	
IV	745.4	06.2	14.3	09.4	15.1	03.1	03.1	10	10	-02.0	16	04	18	C3.0	12	02.9	11	02.4	*	*	18	02.6	07	02.1	14	01.9	07	01.9	03
V	745.2	12.3	18.0	12.6	13.9	19.0	08.6	25.4	20	02.3	10	11	02.2	07	02.1	08	02.1	03	02.0	17	02.6	09	02.8	26	01.8	09	01.9	03	
VI	745.8	15.0	11.2	15.4	16.8	22.2	11.1	27.0	26	04.0	12	10	02.7	C7	02.0	03	01.3	01	01.0	15	02.1	21	02.5	16	01.9	15	01.9	02	
VII	747.9	17.2	23.7	18.0	19.2	25.0	13.3	30.6	31	09.8	26	11	02.2	07	01.5	10	01.6	05	01.2	17	01.9	20	02.4	13	01.3	08	01.9	01	
VIII	748.4	17.4	25.6	19.3	20.4	26.5	14.4	32.4	16	07.1	13	15	02.0	08	01.4	10	01.9	03	02.0	12	02.2	09	01.7	16	02.7	05	01.6	15	
IX	747.7	12.9	19.7	13.9	15.1	20.6	10.6	27.2	14	02.8	27	12	02.0	04	02.5	17	01.5	08	01.6	10	02.3	08	02.9	16	01.6	04	01.5	06	
X	744.3	04.3	10.0	06.1	06.6	10.8	02.9	14.8	20	-01.8	30	11	02.3	08	01.9	05	02.0	03	01.3	09	02.9	26	02.4	17	01.6	08	01.5	06	
XI	748.7	03.7	09.9	05.5	06.2	10.4	02.6	17.7	16	-03.8	10	16	02.3	05	01.6	10	01.5	*	*	23	02.8	21	03.0	07	02.0	04	01.2	04	
XII	750.7	01.0	07.1	02.7	03.4	07.9	-00.3	16.4	03	-06.0	15	06	02.5	03	02.3	07	01.3	05	01.4	16	01.9	24	02.0	18	01.6	05	01.2	04	
GOD.	747.6	08.0	14.4	09.6	10.4	15.2	05.8	32.4	KvM	-06.0	15	XII	145	02.3	84	02.2	130	01.8	43	01.6	190	02.4	179	02.5	176	01.8	75	01.6	73
$\varphi = 46^{\circ}02'$ N $\lambda = 16^{\circ}33'$ E Gr. $\Delta G = + 1h 07$ min.																										KRIJEVCI		BR. ST.41	
I	754.6	-00.1	02.4	00.9	01.0	02.9	-00.8	14.0	20	-04.6	15	04	02.2	17	02.5	09	02.3	13	02.3	12	02.4	28	02.2	04	02.0	06	C2.3	*	
II	746.7	03.1	08.9	05.5	05.8	09.6	02.0	15.5	12	-02.5	09	10	03.7	28	02.9	04	03.5	01	03.0	10	02.6	20	03.3	03	05.0	07	C2.4	*	
III	749.8	04.0	11.6	07.8	07.8	12.5	03.0	22.9	22	-03.0	14	10	03.4	42	03.1	12	03.8	04	02.0	03	02.3	15	03.1	03	02.0	04	02.0	*	
IV	746.4	06.3	14.5	08.8	09.6	15.3	03.6	21.4	28	-00.5	24	24	03.4	24	03.8	08	04.0	02	04.0	10	02.2	06	02.3	03	02.7	13	02.7	*	
V	746.2	11.6	17.9	12.5	13.6	18.9	08.4	24.8	20	03.7	09	16	02.9	17	02.6	C3	02.3	06	02.3	10	02.4	20	02.9	07	02.4	14	02.3	*	
VI	746.9	15.0	20.5	15.7	16.7	22.0	11.2	26.7	26	06.0	12	09	12	04.1	12	03.3	05	02.4	11	02.5	22	02.9	06	02.7	20	02.5	*		
VII	749.0	16.9	23.8	18.2	19.3	25.0	13.0	31.5	17	06.2	21	18	03.2	12	03.1	07	02.4	09	02.7	20	02.8	04	02.5	16	02.8	*			
VIII	749.4	17.7	25.6	19.7	20.7	26.5	14.9	32.2	16	07.3	13	20	02.9	26	03.0	06	02.7	12	02.4	07	02.6	*	*	17	02.0	*			
IX	748.8	12.6	20.2	14.2	15.3	21.0	10.8	28.2	03	03.0	28	20	02.6	22	03.1	03	02.3	05	02.2	17	03.0	*	*	17	02.1	*			
X	741.6	04.3	09.9	06.3	06.7	10.5	02.8	14.5	20	-0.2	31	20	03.0	15	02.7	02	03.0	04	02.0	13	02.6	23	02.7	03	02.0	13	02.0	*	
XI	750.3	03.1	09.3	04.0	05.6	09.8	01.7	18.2	16	-0.4	10	13	03.5	11	03.4	04	02.0	04	02.0	14	02.8	33	02.8	03	02.9	09	02.2	*	
XII	752.3	00.6	05.3	02.3	02.6	06.2	-00.6	13.5	04	-05.5	17	16	01.9	03	02.5	03	02.0	19	02.2	30	02.2	06	02.2	12	02.2	*			
GOD.	748.8	07.9	14.2	09.7	10.4	15.0	05.8	32.2	KvM	-05.5	17	XII	174	C5.2	240	03.0	65	02.9	57	02.3	129	02.4	241	02.7	42	02.5	147	C2.1	*
$\varphi = 46^{\circ}11'$ N $\lambda = 16^{\circ}49'$ E Gr. $\Delta G = + 1h 07$ min.																										KOPRIVNICA		BR. ST.43	
I	-	00.4	03.0	01.1	01.4	03.7	-00.2	12.0	20	-04.5	15	04	01.2	09	01.0	10	01.7	16	01.4	21	01.4	23	01.6	01	01.0	09	01.6	*	
II	-	03.4	09.1	05.3	05.8	09.8	02.4	15.6	12	-02.4	28	12	01.8	18	01.9	04	03.5	04	01.0	10	01.9	27	02.3	02	02.0	07	01.4	*	
III	-	04.3	12.3	07.0	07.7	12.9	03.1	24.0	23	-23.2	01	10	01.5	36	01.8	08	01.6	07	01.4	17	01.8	04	02.5	04	01.8	*			
IV	-	07.0	15.3	08.9	10.1	16.0	04.4	22.5	28	-06.7	04	09	02.0	25	02.3	04	02.0	05	01.2	22	02.0	24	01.6	05	01.5	15	01.6	*	
V	-	12.5	18.8	12.9	14.3	19.6	09.7	26.2	30	04.5	10	04	01.2	13	01.8	C3	02.0	08	01.4	08	01.4	33	02.2	02	02.0	22	01.7	*	
VI	-	15.2	21.6	15.5	17.0	22.8	12.1	28.3	04	05.5	08	04	01.2	14	02.1	C1	01.0	05	01.0	07	01.0	36	01.9	03	01.7	20	01.4	*	
VII	-	17.5	24.7	17.9	19.5	25.6	14.1	32.0	17	10.0	27	24	02.0	16	01.3	C1	01.0	20	01.0	23	01.4	20	01.6	03	01.3	13	01.6	*	
VIII	-	17.6	26.6	19.5	20.8	27.6	15.2	33.0	17	16.6	07	13.0	13	01.0	22	01.4	04	01.0	10	01.2	10	01.1	23	01.4	02	01.0	15	01.4	*
IX	-	13.4	20.7	14.1	15.6	21.6	11.3	28.2	03	04.5	27	10	01.7	20	01.6														

BR.	Oblačnost Nm (0-10)				Vlažnost vzdušna % RH	Padavine mm	Broj dana na sat												H _a m	H _b m	H _t m	H _r m						
	Inkolastičnost broj (Dnes)						Tn			Tx			Tx			Tx			F(0-12)		Nm(0-10)		R mm					
	7	14	21	Srednji (Dnes)			Σ	x ₁₂	Det.	≤	<	<	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥		
VARAŽDIN																												
I	8.4	7.3	7.0	T.6	049.4	04.7	95	87	94	92	62	044	011.9	07	•	•	19	•	•	02	17	12	09	01	11	04	02	
II	8.3	6.9	7.1	T.4	074.8	05.5	88	89	84	80	43	036	016.9	07	•	•	06	•	•	06	03	02	13	12	04	01	11	
III	6.6	7.0	6.2	6.7	107.0	05.8	88	60	81	76	35	051	014.6	06	•	•	07	•	•	07	01	04	13	09	07	03	08	
IV	6.2	6.7	5.9	6.3	187.9	05.7	79	46	67	44	23	019	008.3	26	•	•	06	•	•	12	•	04	12	08	05	06	03	
V	5.5	7.3	6.7	6.5	194.2	09.0	82	59	83	75	40	129	033.1	02	•	•	01	•	•	05	02	02	10	16	11	07	16	
VI	6.0	6.9	6.3	6.2	211.8	10.5	81	57	79	72	38	133	036.5	30	•	•	07	•	•	06	01	06	14	15	04	06	03	
VII	5.1	5.3	4.9	5.1	266.6	12.2	81	56	80	72	38	051	023.1	07	•	•	14	04	•	06	05	06	12	07	01	12	04	
VIII	4.9	5.0	4.2	4.7	254.0	14.4	91	60	80	84	44	258	131.3	28	•	•	18	10	•	02	08	05	12	11	04	12	17	
IX	6.1	5.5	4.6	5.4	159.6	10.9	91	68	89	83	40	107	020.8	25	•	•	02	•	•	04	05	07	11	10	05	11	02	
X	7.2	7.7	7.0	T.3	095.6	06.3	93	73	88	65	51	208	035.6	21	•	•	06	•	•	06	04	06	19	16	07	19	07	
XI	4.4	5.9	6.5	6.3	114.1	05.7	88	67	84	80	17	056	023.3	29	•	•	08	•	•	06	03	10	07	06	02	07	01	
XII	6.0	7.9	6.4	6.7	084.8	05.0	90	73	86	83	45	033	012.0	12	•	•	17	•	•	06	01	12	11	06	02	11	01	
GOD.	6.5	6.5	6.1	6.4	1798.0	08.0	87	64	83	78	17	1125	131.3	36V	•	•	69	43	14	•	69	07	43	127	143	103	38	140
KRIŽEVCI																												
BR.	ST.42																											
H _a	=	155 m	H _b	=	140.0 m	H _t	=	2.0 m	H _r	=	1.0 m																	
I	9.1	9.0	8.4	8.8	017.2	04.6	97	88	95	93	56	050	013.2	07	•	01	17	•	•	•	24	12	09	01	11	02	01	
II	7.9	7.2	7.9	7.7	080.2	05.5	89	66	82	79	32	045	018.5	07	•	05	•	•	05	01	02	16	08	06	02	08	01	
III	7.0	7.0	5.7	6.6	132.2	05.7	84	58	73	72	36	024	012.3	06	•	05	•	•	06	04	14	08	05	01	06	02		
IV	6.1	6.8	5.5	6.2	170.0	05.6	76	44	68	63	23	023	010.5	27	•	01	•	•	09	05	10	07	04	01	07	•		
V	6.3	7.3	6.9	6.8	182.5	09.2	86	62	86	78	31	154	037.0	01	•	•	01	•	•	04	02	01	12	17	13	06	17	
VI	6.8	5.9	6.5	6.4	201.9	10.8	85	60	82	76	39	105	032.0	50	•	•	07	•	•	09	01	01	08	14	13	03	14	
VII	4.7	4.3	4.3	4.4	276.7	12.4	83	56	81	73	43	055	023.3	07	•	•	15	03	•	05	01	08	06	02	09	04		
VIII	4.6	3.7	4.0	4.1	263.3	14.8	90	61	88	80	45	053	015.3	12	•	•	18	09	•	01	12	05	12	07	02	12		
IX	7.0	5.5	4.5	5.7	156.1	11.0	93	65	91	83	39	104	022.8	05	•	•	06	•	•	08	07	12	10	10	05	10		
X	7.8	7.5	7.5	7.6	077.6	06.4	95	75	91	87	43	185	076.5	05	•	•	05	•	•	04	06	08	17	22	16	10	22	
XI	7.6	6.6	7.6	7.1	091.2	05.8	91	71	89	84	35	052	025.2	29	•	•	09	•	•	07	•	12	10	06	02	09	01	
XII	7.6	6.6	6.7	6.9	074.5	05.0	93	80	90	80	25	030	013.0	12	•	•	02	18	•	03	13	12	07	01	12	01		
GOD.	6.9	6.4	6.3	6.5	1723.4	08.1	88	65	84	79	23	880	037.0	04V	•	•	60	46	12	•	61	05	45	149	141	102	36	139
KOPRIVNICA																												
BR.	ST.43																											
H _a	=	141 m	H _b	=	-	-	m	h _t	=	2.0 m	H _r	=	1.0 m															
I	7.0	7.5	8.5	8.3	-	04.6	91	86	92	90	57	062	013.0	02	•	•	17	•	•	01	21	12	08	02	11	04	02	
II	7.2	7.2	6.8	7.1	-	03.6	87	69	83	80	41	042	018.2	07	•	•	03	•	•	03	13	09	02	08	03	02	01	
III	5.7	6.5	5.4	5.9	-	05.9	86	59	79	75	22	038	012.0	06	•	•	06	•	•	05	10	09	06	01	05	04	03	
IV	5.7	6.1	5.1	5.7	-	05.6	76	41	67	61	19	018	011.0	26	•	•	02	•	•	05	10	07	03	01	07	03	03	
V	6.2	7.2	6.3	6.5	-	-	-	-	-	-	-	113	033.0	01	•	•	04	•	•	01	10	15	12	03	15	04	03	
VI	6.4	6.1	6.2	6.2	-	-	-	-	-	-	-	111	032.2	30	•	•	09	•	•	01	05	16	11	03	16	04	01	
VII	3.7	3.9	3.3	3.7	-	12.1	78	53	80	70	38	059	020.2	07	•	•	19	07	•	12	04	10	04	03	10	03	01	
VIII	5.4	4.5	3.9	4.6	-	14.7	92	59	87	79	39	136	023.2	25	•	•	21	12	•	06	05	15	11	07	15	04	07	
IX	6.9	6.3	4.4	5.9	-	11.1	93	65	89	82	38	100	016.1	26	•	•	10	•	•	03	08	10	10	06	10	04	12	
X	6.9	7.0	7.2	7.2	-	06.4	92	74	90	86	39	201	039.3	05	•	•	01	•	•	03	15	23	17	09	23	02	12	
XI	5.7	5.7	5.8	6.1	-	05.8	88	68	85	80	36	041	023.7	29	•	•	04	•	•	03	12	09	04	02	09	01	02	
XII	7.2	6.1	6.6	6.6	-	05.0	88	75	85	83	18	042	016.1	12	•	•	12	•	•	03	11	11	07	01	09	02	11	
GOD.	6.4	6.2	5.8	6.2	-	-	-	-	-	-	-	963	035.3	05X	•	•	19	75	13	•	08	03	01	77	100	117	105	33
POREČ																												
BR.	ST.44																											
H _a	=	15 m	H _b	=	-	-	m	h _t	=	2.0 m	H _r	=	1.0 m															
I	7.5	7.7	7.5	7.6	-	06.4	87	81	90	86	59	045	022.7	01	•	•	01	•	•	02	17	10	04	0				

Meseč Vremenski Splitsak PM MM	Temperatura vazduha °C	Čestina pravaca i srednja jačina vетра m/s (0-12)																																					
		Tm						Dm						Dat.						N		NE		E		SE		S		SW		W		NW		C			
		7	14	21	Sred. (Dm)	Mx	Mn	Mx	Dat.	Mn	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.										
$\varphi = 45^{\circ}14'$ N $\lambda = 13^{\circ}56'$ E Gr. $\Delta G = + 56$ min.																				PAZIN		BR. ST. 46																	
I	735.6	01.8	09.4	03.8	04.7	10.5	06.4	16.4	21	-04.5	22	05	01.2	03	01.3	07	01.4	08	01.5	04	01.2	04	01.2	05	01.0	02	01.0	05	01.0	02	01.0	05							
II	732.5	03.7	10.3	05.5	06.3	11.1	02.0	14.5	20	-05.2	28	.	.	07	02.0	11	02.2	15	02.3	13	01.8	03	02.3	04	02.0	.	.	03	01.0	05	01.0	03							
III	735.3	02.8	13.1	06.6	07.3	14.0	01.7	24.3	22	-07.0	01	03	02.0	05	01.8	13	02.4	15	02.2	05	02.4	04	02.5	01	02.0	01	02.0	04	02.0	01	02.0	04							
IV	732.2	05.7	14.4	08.6	09.4	15.5	03.6	19.3	09	-01.6	20	03	02.0	09	02.0	12	02.2	18	01.8	08	02.5	06	02.8	03	02.7	01	03.0	03	02.7	01	03.0	03							
V	732.3	11.0	18.9	12.7	13.8	20.0	07.9	27.0	21	03.0	10	04	01.8	.	.	06	02.8	20	02.2	07	02.7	08	02.4	06	02.6	01	02.0	41											
VI	734.2	13.8	21.5	15.8	16.7	23.0	10.8	30.4	04	04.2	12	07	02.5	03	01.7	08	01.6	07	02.3	10	02.6	11	02.6	05	02.6	04	02.0	40											
VII	736.1	15.1	26.8	19.5	20.2	27.6	13.0	39.7	30.29	08.6	24	02	01.0	05	01.6	07	02.4	07	02.6	08	02.5	36	02.5	06	02.3	06	02.0	46											
VIII	736.1	15.3	26.7	20.2	21.1	30.0	13.5	35.0	04	08.5	12	03	02.3	04	01.5	07	02.3	07	02.3	04	02.5	02	03.0	04	02.0	03	02.0	09	02.0	03	02.0	03							
GOD.	735.2	07.7	16.6	10.3	11.2	17.6	05.7	35.0	04/VIII	-07.0	04/III	32	01.9	51	01.7	103	02.0	120	02.1	97	02.3	75	02.3	52	02.0	29	01.8	53	02.0	29	01.8	53							
$\varphi = 45^{\circ}20'$ N $\lambda = 14^{\circ}27'$ E Gr. $\Delta G = + 58$ min.																				RIJEKA		BR. ST. 47																	
I	756.7	05.6	10.4	07.0	07.5	11.3	04.5	20.0	20	01.4	15	03	01.0	38	01.7	05	02.0	01	01.0	03	01.0	09	01.0	.	.	01	01.0	33											
II	749.6	07.7	16.9	08.5	08.9	11.7	06.7	16.0	16	01.7	28	03	01.7	31	03.7	07	03.6	06	02.5	09	01.8	06	01.3	.	.	03	02.0	19											
III	752.4	07.6	12.7	09.7	09.9	13.9	06.7	21.7	22	-00.3	01	05	03.0	35	02.8	07	03.7	02	02.0	05	01.4	10	01.6	02	02.0	.	27												
IV	745.0	10.1	14.9	12.0	12.3	16.0	08.5	20.3	08	04.5	16	06	02.7	36	03.1	04	03.5	02	02.5	05	01.6	05	02.6	02	01.0	25													
V	745.9	14.1	18.4	14.7	15.5	19.8	11.6	26.3	21	08.0	09	02	02.0	14	01.9	04	02.2	04	01.5	05	01.4	17	01.4	05	01.6	02	03.0	40											
VI	750.3	17.2	21.1	17.5	18.3	22.6	14.6	27.9	04	08.6	12	04	02	17	02.6	02	01.5	02	02.5	06	01.5	11	01.4	02	02.5	01	01.0	45											
VII	752.1	20.4	26.0	21.3	22.2	27.2	17.7	32.7	30	14.2	25	01	01.2	26	02.6	04	02.2	02	03.5	05	01.0	21	01.5	02	01.0	.	32												
VIII	751.9	11.6	26.3	22.9	23.9	29.2	19.6	34.8	16	13.3	12	02	02.5	29	02.3	02	02.5	02	02.5	03	01.3	14	01.4	01	02.0	01	01.0	39											
IX	751.4	16.7	23.2	18.2	19.1	24.1	15.4	29.4	15	08.8	27	01	01.0	30	02.0	05	01.8	02	02.0	06	02.3	12	02.0	01	02.0	.	33												
X	748.4	08.9	12.3	09.6	10.1	14.0	07.2	17.2	07	03.3	17	.	.	45	02.2	07	02.1	03	02.3	06	02.8	09	02.0	01	02.0	.	22												
XI	753.4	09.0	12.5	09.6	10.2	13.3	07.7	16.0	14	02.4	02	05	02.0	26	01.7	05	01.8	02	02.0	13	02.0	07	01.4	.	.	32													
XII	755.8	05.7	10.5	07.1	07.6	11.4	04.7	16.2	03	01.3	13	04	02.2	31	01.7	03	01.3	02	01.0	05	01.4	02	01.0	46											
GOD.	751.8	12.0	16.8	13.2	13.8	17.9	10.4	34.8	4/VIII	-00.3	04/III	36	02.1	358	02.4	56	02.5	30	02.2	71	01.7	123	01.5	19	02.0	10	01.7	393											
$\varphi = 45^{\circ}36'$ N $\lambda = 14^{\circ}38'$ E Gr. $\Delta G = + 59$ min.																				PAG		BR. ST. 48																	
I	691.0	-00.4	02.7	00.3	00.7	03.9	-02.3	13.2	20	-06.9	15	02	01.0	06	01.3	03	01.0	50	01.2	25	01.3	05	01.6	.	.	02	01.0	.	02	01.0	.	02	01.0	.	02	01.0	.		
II	684.9	01.8	03.9	02.2	02.5	05.0	00.0	08.9	20	-04.0	08	.	.	01	01.0	01	04.0	24	01.4	20	02.5	32	02.7	01	02.0	04	02.2	01											
III	688.4	02.2	07.2	03.6	04.1	08.5	00.5	19.8	21	-04.9	14	01	01.0	04	01.5	02	01.5	53	01.5	20	01.3	10	02.6	.	.	03	01.0	.	03	01.0	.	03	01.0	.					
IV	685.1	04.4	09.0	05.5	06.1	10.7	16.6	03.9	03	-01.4	18	01	01.0	15	02.6	04	03.0	37	01.7	18	01.6	10	02.4	.	.	02	01.0	03	01.0	04	01.0	03	01.0	04					
V	686.5	08.8	12.7	09.0	09.9	14.7	05.3	21.2	20	01.6	09	02	01.0	08	01.8	05	01.8	41	01.7	14	01.4	18	02.4	.	.	03	01.0	02	01.0	03	01.0	02	01.0	03					
VI	687.8	11.6	14.9	11.4	12.3	17.4	07.7	23.9	04	02.4	11	06	01.2	09	01.7	04	01.2	27	01.7	21	01.6	17	01.9	.	.	03	02.0	03	01.0	04	02.0	03	01.0	04					
VII	690.7	14.4	19.6	14.5	15.8	21.2	10.2	27.9	30	06.7	27	02	02.0	07	02.0	01	01.0	41	01.5	28	01.6	08	01.8	.	.	03	01.7	03	01.0	04	02.0	03							

Meseč	Oblačnost Nm (0-10)	Inzocijacija broj sati (Dles)	Vlažnost vazduha			Padavine R mm	Broj dana na sa:												•	*	*	Δ	Δ	▲	▲	R	T	III	■								
			a _m	U m t			Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	III	■												
				7	14	21	Sred. (Dles)	Σ	Max	Dati.	≤	<	<	≥	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV											
PAZIN																																					
BR. ST.46																																					
I	7.7	7.1	6.2	7.0	-	05.3	93	66	91	83	30	070	040-1	01	.	.	16	02	15	14	07	01	13	16				
II	7.3	7.4	6.5	7.1	-	05.4	86	58	81	75	22	080	018-1	07	.	.	09	04	09	15	12	03	14	02	04			
III	6.7	6.6	5.5	6.1	-	05.5	89	48	78	72	12	171	160-4	05	.	.	10	04	09	05	03	01	05	01	01	04		
IV	5.6	7.0	5.0	5.9	-	05.7	81	44	69	65	18	104	046-8	29	.	.	05	05	09	09	08	04	09	02	.			
V	4.7	7.2	5.9	6.3	-	06.5	86	52	80	73	27	068	022-9	05	.	.	03	02	12	16	11	01	16	04	01			
VI	4.3	7.2	4.5	6.0	-	10.4	88	54	78	73	26	135	036-0	30	.	.	06	01	.	.	.	02	17	14	13	06	14	12	02			
VII	3.3	4.4	3.4	3.7	-	11.2	88	40	69	65	17	017	014-7	07	.	.	27	07	.	.	.	10	02	05	03	01	05	05	.			
VIII	3.0	4.9	3.5	3.6	-	12.4	93	40	77	70	17	080	039-8	11	.	.	26	16	.	02	01	13	02	09	06	02	09	01	16			
IX	4.8	5.4	3.1	4.5	-	10.7	93	49	87	74	26	162	043-8	25	.	.	15	08	06	11	10	05	11	01	11	04		
X	7.7	7.8	5.2	6.9	-	06.4	93	63	90	82	24	238	040-6	05	.	.	08	11	21	19	08	21	08	11				
XI	6.1	7.6	6.4	7.4	-	06.5	91	65	90	82	22	092	022-0	26	.	.	09	01	15	11	09	05	11	01	09			
XII	6.6	6.2	5.0	5.9	-	04.9	92	63	85	80	22	032	014-9	12	.	.	20	06	12	15	06	01	09	02	17			
GND.	6.1	6.6	4.6	4.9	5.9	-	07.7	89	53	81	74	12	1252	160-4	058	.	.	77	79	24	.	02	01	53	109	145	107	38	137	01	02	59	68
RIJEKA																																					
BR. ST.47																																					
I	6.7	7.0	5.3	6.3	084.7	05.6	75	65	74	71	37	058	022-2	01	.	.	01	.	01	03	12	13	09	02	12	02	.					
II	7.8	7.6	5.6	7.0	096.2	06.1	73	64	72	70	24	129	040-3	07	.	.	01	.	06	02	03	12	12	09	05	12	01	.				
III	6.4	6.8	5.4	6.2	143.8	05.9	70	54	65	63	22	096	079-2	05	.	.	01	.	04	05	11	05	04	02	05	01	.					
IV	6.5	7.4	6.2	6.7	166.4	06.2	63	52	59	58	24	167	048-4	29	.	.	01	.	01	05	15	09	07	04	05	03	.					
V	5.8	7.4	6.1	6.5	203.6	09.2	74	60	74	70	34	170	037-1	05	.	.	02	.	01	03	13	17	14	08	17	01	06					
VI	6.2	6.5	5.7	7.2	187.2	11.2	71	63	77	70	32	176	051-1	30	.	.	07	.	02	02	12	17	15	07	17	01	12					
VII	3.0	4.1	3.4	3.7	330.3	12.6	67	51	67	62	31	088	042-5	26	.	.	24	05	05	01	11	02	07	04	03	07	05	.				
VIII	3.4	4.0	2.4	3.1	302.5	13.0	64	45	64	58	29	067	025-1	11	.	.	28	14	16	02	01	16	C2	03	07	02	08	09	.			
IX	5.6	4.9	3.4	4.6	207.5	10.8	73	51	69	64	27	215	077-5	25	.	.	17	.	01	03	01	09	06	14	12	05	14	07	.			
X	7.6	8.3	5.9	7.2	101.3	06.4	74	60	72	69	32	257	049-6	21	.	.	07	.	02	02	12	17	17	08	21	01	05					
XI	6.1	7.3	6.7	7.3	080.0	06.7	74	63	72	70	26	118	038-4	26	.	.	01	.	01	02	16	16	11	03	16	02	.					
XII	5.4	6.1	5.0	5.5	094.2	05.5	73	63	70	69	29	033	016-2	12	.	.	01	.	01	06	10	10	05	01	10	01	01					
GND.	6.1	6.5	5.1	5.9	1999.7	08.3	70	57	69	66	22	1572	079-2	058	.	.	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01	01		
PARG																																					
BR. ST.48																																					
I	7.7	7.8	6.0	7.2	061.5	04.2	90	81	89	87	32	033	C10-0	01	.	.	07	28	.	.	.	04	15	14	05	01	08	07	11	18		
II	8.7	8.6	7.9	8.4	043.3	04.6	85	79	84	83	18	158	059-2	07	.	.	01	11	.	.	.	01	22	16	11	05	11	06	05	07		
III	7.6	7.5	7.5	7.5	100.3	05.1	89	70	86	82	35	085	033-1	05	.	.	01	16	.	.	.	03	20	11	10	04	04	10	01	19		
IV	5.9	7.3	7.8	7.0	133.7	05.1	76	72	74	71	34	120	039-7	29	.	.	06	.	01	01	05	15	09	04	12	06	03	08				
V	5.2	7.9	7.2	6.8	162.3	06.8	81	65	78	74	41	180	049-8	01	.	.	06	08	.	.	.	10	17	13	06	17	01	08	05			
VI	6.2	7.0	7.8	7.0	149.2	06.2	78	68	79	75	41	232	036-5	07	.	.	07	01	.	.	.	01	13	18	16	09	18	14	03			
VII	3.9	3.3	3.4	4.2	275.1	10.0	81	61	76	73	47	147	069-1	26	.	.	04	04	.	.	.	06	01	11	09	04	11	08	06			
VIII	4.9	5.4	4.2	4.8	236.8	11.9	66	87	84	79	42	206	065-6	29	.	.	13	09	08	12	11	05	12	11	03			
IX	5.9	6.6	5.5	6.2	162.6	09.3	88	74	88	83	48	227	087-9	25	.	.	12	01	.	.	.	06	12	15	15	06	1										

Mjesec M	Vrijeme prijevoda M Hr	Temperatura vazduha °C										Gestina pravaca i srednja jačina vjetra m/s, fm (0-12)																
		Tm				RH				W		E		SE		S		SW		W		NW						
		7	14	21	Sred. (Dnev.)	RH %	RH %	W	E	M.	M.	E.	W.	S.	E.	S.	W.	E.	S.	W.	E.	S.	C.					
$\varphi = 45^{\circ}25'$ N $\lambda = 14^{\circ}33'$ E Gr. AG - + 1h 00 min.																												
I	-	00.3	03.5	01.1	01.3	04.3	-01.4	19.2	20	-04.0	15	.	.	37	02.0	09	02.2	01	02.0	.	.	35	02.3	10	02.0	03	02.0	
II	-	02.4	05.3	03.6	03.0	06.1	01.3	09.8	20	.	.	35	02.4	06	02.2	02	02.5	.	.	27	03.2	11	02.3	03	02.0	.		
III	-	03.0	07.6	04.7	05.0	08.7	01.5	21.7	21	-04.4	01	.	.	38	02.3	14	02.4	03	02.0	.	.	29	02.5	07	02.8	04	02.0	
IV	-	05.4	10.3	06.8	07.4	11.3	02.5	16.3	10	-02.0	14	.	.	45	02.9	06	02.0	03	02.7	.	.	19	02.5	17	02.1	01	.	
V	-	10.6	15.4	10.7	11.9	16.6	06.9	23.0	20	02.8	10	.	.	26	02.4	12	02.5	04	03.0	.	.	42	02.5	13	02.5	06	02.2	
VI	-	13.4	18.0	13.5	14.6	19.4	05.7	25.0	04	03.5	13	.	.	27	02.4	09	02.6	01	01.0	.	.	46	02.4	07	02.4	04	02.5	
VII	-	16.0	22.0	16.8	17.9	23.2	11.7	26.0	17.16	05.3	13	.	.	26	02.5	09	02.4	01	03.0	.	.	40	02.4	15	02.2	02	02.0	
VIII	-	16.4	21.8	18.4	19.0	24.0	13.8	26.9	04	08.2	12.11	01	02.0	44	02.3	09	02.6	03	02.2	.	.	18	02.2	13	02.0	03	02.3	
IX	-	12.1	17.2	13.5	14.5	18.1	09.6	23.5	02	01.9	27	.	.	38	02.4	16	02.3	02	02.5	.	.	37	02.7	08	01.9	04	02.2	
X	-	03.4	06.6	04.0	04.5	07.7	01.0	13.8	04	-04.4	30	.	.	32	02.2	11	02.0	01	03.0	.	.	31	02.8	17	02.4	01	02.0	
XI	-	04.1	07.1	04.5	05.1	08.2	00.7	18.0	16	-08.5	28	07	02.9	18	02.2	05	02.4	01	01.0	79	02.9	12	02.0	15	03.0	03		
XII	-	02.5	05.2	03.3	03.6	06.9	-01.1	14.7	29	-04.8	15	01	01.0	11	02.8	03	03.7	15	02.3	.	.	05	01.4	22	02.8	34	03.0	02
GOD.	-	07.5	11.8	08.4	09.0	12.0	04.7	29.9	04W	-09.8	15XII	04	02.0	377	02.4	25	02.3	43	02.4	01	01.0	351	02.6	152	02.3	77	02.7	05
$\varphi = 45^{\circ}18'$ N $\lambda = 15^{\circ}14'$ E Gr. AG - + 1h 01 min.																								COULIN		BR. ST.52		
I	739.0	-00.6	04.1	00.8	01.3	05.1	-01.4	18.9	20	-05.6	26	06	01.9	11	01.7	11	01.4	10	01.5	07	01.7	06	01.8	10	01.7	13	C1.5	14
II	730.7	04.4	07.7	05.8	08.5	03.4	03.4	13.7	02	-01.6	08	07	02.1	18	02.0	01	01.7	08	03.2	14	03.2	16	02.6	10	C2.3	05	04	
III	733.7	03.7	10.2	06.4	06.7	10.8	02.9	24.0	21	-04.6	14	14	02.1	14	02.1	15	01.6	05	01.8	07	04.0	06	03.7	16	C2.7	08		
IV	736.4	05.1	12.3	08.6	07.7	13.4	03.9	19.6	29	00.3	04	14	02.6	18	02.7	10	02.2	03	02.0	02	02.0	05	04.0	15	02.4	16	C2.7	07
V	736.4	10.8	17.2	12.5	13.2	18.5	08.6	24.1	27	03.2	10	06	02.3	07	02.1	10	01.7	07	02.0	05	02.4	14	03.7	12	02.2	19	C1.4	19
VI	731.7	14.3	19.6	15.2	16.1	21.3	11.0	25.7	04	03.8	12	04	02.2	02	02.5	08	01.9	06	02.2	13	03.5	16	02.4	12	C1.9	19		
VII	733.8	16.1	23.6	18.4	19.1	25.0	12.9	30.0	17	08.0	27	04	02.7	13	02.2	10	02.0	04	01.8	06	02.5	11	04.0	16	02.4	17	C1.9	19
VIII	734.2	16.1	24.5	18.5	19.4	25.5	14.3	32.0	12	08.1	18	06	01.5	15	01.7	11	01.7	04	01.8	03	02.0	03	03.0	20	01.7	29	C1.6	01
IX	733.3	12.1	19.3	14.3	15.0	20.5	10.5	26.4	03	01.7	27	07	01.0	12	01.9	12	02.0	06	01.3	04	02.2	10	03.3	18	01.7	22	C1.5	04
X	729.7	04.2	08.8	05.4	06.0	10.4	02.4	16.0	25	-04.7	30	06	02.0	08	02.1	04	01.8	08	03.0	14	02.7	25	01.7	15	C1.9	04		
XI	734.3	04.9	09.2	05.8	06.4	10.3	03.4	17.0	19	02.5	10	09	01.4	08	01.9	09	01.2	07	01.9	07	01.1	20	02.2	16	02.5	14	01.9	04
XII	734.2	01.9	08.9	04.0	04.7	10.7	00.0	17.1	03	-09.8	19	04	02.5	11	01.9	02	01.5	03	02.0	05	02.4	14	04.2	26	03.0	20	C2.3	04
GOD.	733.1	07.8	13.8	09.6	10.2	15.0	06.0	32.0	06W	-09.8	15XII	04	02.0	137	02.1	93	01.8	71	01.8	66	02.4	130	03.4	212	02.2	157	C1.9	105
$\varphi = 45^{\circ}30'$ N $\lambda = 15^{\circ}33'$ E Gr. AG - + 1h 02 min.																								KARLOVAC		BR. ST.53		
I	737.3	30.0	02.8	01.3	01.3	03.5	-00.3	18.5	20	-03.8	22	02	01.0	30	01.1	02	01.9	.	.	05	01.2	01	01.0	01	01.3	50		
II	749.5	05.6	06.6	06.7	10.1	03.4	03.3	16.3	11	-01.1	20	08	01.2	24	01.6	04	01	03.0	.	.	23	02.3	.	07	02.5	28		
III	752.5	04.1	12.0	06.8	08.1	12.9	01.6	25.7	21	-02.6	14	04	01.2	37	01.6	06	01.5	.	.	09	02.4	.	01	02.0	41			
IV	749.0	05.5	14.6	10.2	15.6	04.6	2.2	21	10	01.0	20	04	01.5	37	02.1	02	01.5	.	.	03	02.7	.	.	03	02.0	41		
V	745.0	10.4	19.3	14.2	14.7	20.3	09.6	26.4	20	03.9	10	02	01.5	24	01.7	03	01.3	01	02.0	.	.	17	02.1	01	01.0	01	01.0	44
VI	749.7	14.1	22.0	17.4	17.7	23.3	12.3	28.2	24	04.5	13	03	01.7	14	01.7	01	01.0	01	02.0	26	02.0	01	01.0	04	01.7	34		
VII	751.7	16.3	23.6	20.7	20.8	27.0	14.4	33.2	17	10.0	09	01.0	36	01.7	12	01.0	03	01.0	03	01.0	11	02.0	01	01.0	13	01.6	34	
VIII	751.8	16.8	26.0	21.3	27.4	27.4	15.9	34.4	04	10.0	12	03	01.0	24	01.6	03	02.0	01	01.0	.	.	07	01.6	.	04	01.1	51	
IX	751.4	12.4	20.6	15.8	16.1	21.6	11.8	26.5	02	03.9	27	01	01.0	22	01.9	.	.	03	01.3	.	.	11	01.8	.	06	01.0	40	
X	748.4	10.2	16.2	07.2	11.3	03.7	17.0	29	-01.9	31.30	02	01.0	17	01.2	.	.	06	01.0	.	.	11	02.5	.	05	01.4	52		
XI	753.0	04.3	09.4	06.0	06.5	10.0	03.6	18.4	16	-03.5	29	02	01.0	23	01.1	02	01.5	01	02.0	17	02.2	.	01	01.0	44			
XII	755.4	00.3	05.6	02.4	02.7	07.1	-00.8																					

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine mm	Broj dana na sat																															
							Tn				Tx				Tz				F(0-12)		Nm(0-10)		R mm		•	*	•	Δ	•	▲	▲	R	T	≡	■			
	7	14	21	Sred. (Dnev.)			7	14	21	Stred.	Min	Max	Dat.	≤	<	<	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV						
SKRAD																																						
BR. ST.51																																						
I	7.3	7.7	5.4	6.8	-	04.3	88	81	85	84	36	046	015.7	01	•	04	25	•	•	•	04	14	15	07	02	11	07	03	•	•	•	•	15	19				
II	6.5	8.2	5.2	8.3	-	05.1	85	81	82	83	44	118	046.4	07	•	•	10	•	•	•	01	01	20	17	10	04	14	04	•	•	•	•	01	11	05			
III	7.5	7.4	7.4	7.4	-	05.0	82	71	74	76	27	111	030.2	05	•	02	15	•	•	•	01	17	15	12	04	04	11	•	•	•	•	01	06	19				
IV	5.6	7.3	7.2	6.7	-	05.1	75	56	68	66	19	144	044.5	26	•	•	05	•	•	•	•	04	13	15	09	05	13	04	02	•	•	•	•	03	07	03		
V	5.5	7.1	7.6	6.7	-	07.7	79	62	77	73	37	214	069.9	01	•	•	•	•	•	•	•	01	13	22	17	07	22	•	•	•	•	05	05	•				
VI	5.5	6.8	6.2	6.2	-	09.0	74	61	77	71	30	237	046.7	30	•	•	01	•	•	•	•	03	10	19	13	08	19	•	•	•	•	04	03	•				
VII	4.5	5.3	3.7	3.5	3.9	-	10.6	73	60	69	67	29	111	062.6	26	•	•	11	•	•	•	•	09	02	09	07	02	05	•	•	•	•	05	05	•			
VIII	5.3	4.9	3.8	4.7	-	12.6	63	66	78	76	39	234	069.2	29	•	•	14	•	•	•	•	09	07	10	09	05	13	04	02	•	•	•	•	05	08	•		
IX	6.7	5.3	6.0	6.0	-	09.6	88	72	83	80	43	220	068.4	21	•	•	•	•	•	•	•	05	13	13	11	08	13	•	•	•	•	04	07	•				
X	8.1	7.6	6.9	7.5	-	05.7	93	80	92	89	46	439	067.5	21	•	•	15	•	•	•	•	01	15	24	21	17	24	10	08	01	•	•	•	C2	13	08		
XI	8.3	8.1	7.6	8.0	-	06.0	92	87	88	89	54	146	037.9	26	•	•	14	•	•	•	•	01	12	13	11	04	02	10	03	•	•	•	•	03	10	07		
XII	4.8	5.3	4.2	4.8	-	05.7	90	92	91	91	33	059	033.1	12	•	01	17	•	•	•	04	•	09	07	09	06	01	05	03	•	•	•	•	01	06	•		
GOD.	6.5	6.6	6.2	6.4	-	07.2	83	72	80	78	19	2081	069.2	27	W	•	07	101	26	•	•	06	•	47	148	186	134	70	165	47	18	01	•	•	•	41	96	67
CGULIN																																						
BR. ST.52																																						
I	7.9	7.7	6.8	7.5	-	050.0	04.5	95	81	93	90	32	062	020.2	01	•	01	25	•	•	•	02	17	14	07	02	14	08	06	•	•	01	•	14	09			
II	9.8	6.6	6.0	8.5	-	056.4	05.5	82	72	82	80	27	100	025.8	25	•	•	05	•	•	•	08	02	•	21	16	10	04	12	05	01	•	•	01	02	03		
III	7.5	7.1	7.0	7.2	-	114.5	05.6	88	62	80	77	30	115	029.8	05	•	•	07	•	•	•	04	02	01	12	13	11	04	02	10	03	•	02	01	14			
IV	6.3	7.6	6.5	6.8	-	154.6	05.6	84	52	68	66	29	080	016.2	14	•	•	•	•	•	•	06	04	16	14	11	02	14	04	07	•	01	•	01				
V	5.5	7.5	7.1	6.7	-	199.1	08.3	86	57	79	74	38	176	053.3	01	•	•	•	•	•	10	01	02	13	21	17	06	21	•	•	•	•	03	01	•			
VI	5.5	7.4	5.4	6.1	-	205.6	10.1	81	59	79	73	39	185	039.3	25	•	•	02	•	•	•	01	04	08	19	14	06	19	•	•	•	•	06	01	•			
VII	4.0	4.2	3.5	3.9	-	309.6	11.6	83	55	73	71	40	101	026.5	19	•	•	15	01	•	•	04	01	12	04	09	08	04	05	•	•	05	01	•				
VIII	5.0	5.4	3.6	4.7	-	227.6	13.8	92	63	89	81	32	270	069.4	26	•	•	16	04	•	•	09	08	11	11	08	11	•	•	•	•	08	01	•				
IX	5.7	6.2	5.5	5.8	-	167.0	10.9	94	49	91	85	40	267	067.4	21	•	•	05	•	•	•	06	09	15	12	06	15	•	•	•	•	05	05	•				
X	7.5	8.1	6.1	7.2	-	082.1	06.1	92	75	86	84	46	458	063.2	29	•	•	05	•	•	•	03	01	03	15	26	22	14	26	04	04	04	04	07	05	03		
XI	8.2	7.6	7.0	7.6	-	065.9	06.6	93	73	86	82	31	181	047.6	26	•	•	05	•	•	•	06	03	02	19	15	11	08	15	05	04	01	01	02	03	07		
XII	5.4	5.6	5.0	5.3	-	108.8	04.9	84	64	79	76	29	082	036.8	12	•	04	14	•	•	03	04	07	09	08	02	07	03	02	01	01	04	07					
GOD.	7.0	6.4	6.0	6.4	-	1741.2	07.7	87	65	82	78	27	2021	069.4	26	W	•	01	61	38	05	•	62	15	52	152	181	142	67	171	35	22	02	•	04	41	38	42
KARLOVAC																																						
BR. ST.53																																						
I	5.5	5.2	8.1	8.9	-	021.0	04.7	97	90	94	94	44	052	C11.0	02	•	01	17	•	•	•	01	23	16	08	02	16	03	C1	•	•	•	•	12	C4			
II	8.2	8.6	6.2	7.5	-	061.3	03.0	90	70	84	81	28	045	010.8	25	•	•	03	•	•	•	01	15	12	09	01	12	03	03	•	•	01	02	01	01			
III	8.3	8.3	6.8	7.2	-	116.0	06.4	93	64	81	79	31	081	C21.0	06	•	02	02	•	•	•	03	14	10	08	03	05	C7	02	02	01	01	03	03				
IV	5.9	6.9	6																																			

Meseč vazdušni pratilac M E	Temperatura vazduha °C Tm 7 14 21 Sred. Sred. (Dana)	Čestina pravaca i srednja jačina veta m/s, fm (0-12)																																															
		N			NE			E			SE			S			SW			W			NW																										
		E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.	E.	J.	S.																								
$\varphi = 45^{\circ}36'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$																																																	
I	- 01.1 02.8 01.6 01.8 04.5 -00.1 11.4 20 -05.2 15.14 06 01.2 12 01.7 C7 00.7 21 02.5 08 01.5 18 02.3 03 02.3 13 02.5 05	STUBIČKA GORA																							BR. ST.56																								
II	- 03.0 05.4 03.4 03.8 06.4 02.1 11.6 12 -04.4 20 . . 24 02.3 07 02.9 18 03.0 05 03.0 14 03.9 07 02.9 09 02.1 .																																																
III	- 04.5 06.1 05.3 05.9 08.4 03.6 21.6 22 -03.6 03.01 . . 25 02.3 14 01.7 28 02.1 01 02.0 14 03.3 03 02.0 05 02.6 03																																																
IV	06.7 10.6 07.1 07.9 11.4 04.5 17.8 10 -01.8 17 01 01.0 44 02.8 05 02.2 16 . . . 10 02.5 02 01.0 00 02.5 02																																																
V	- 11.2 14.8 10.9 12.0 15.6 08.0 21.4 20 04.8 15 03 01.0 21 02.1 04 02.2 12 02.7 03 03.0 08 03.2 07 02.1 31 02.4 04																																																
VI	- 13.6 17.8 13.5 14.6 18.8 10.5 23.8 26 05.2 11.10 05 C2.0 12 02.6 06 01.5 14 02.7 . . 08 03.0 11 01.8 31 02.8 03																																																
VII	- 16.6 21.8 17.2 18.1 22.7 - 28.6 15 - . 07 01.3 16 02.4 06 01.8 14 02.9 04 02.5 12 03.2 14 02.3 19 02.4 01																																																
VIII	- 18.4 22.5 18.9 19.7 23.5 16.0 29.8 17 08.8 11 07 01.1 24 02.3 12 02.0 22 02.7 01 04.0 05 02.0 03 02.7 16 02.2 03																																																
GOD.	- 08.5 11.7 08.7 09.4 12.6 - 29.8 07.VM - 52 01.3 257 02.4 79 01.7 213 02.7 34 02.1 169 03.0 68 02.2 185 02.6 38																																																
$\varphi = 45^{\circ}49'$ N $\lambda = 15^{\circ}59'$ E Gr. $\Delta G = +1h\ 04\ min.$																									ZAGREB-GRIC																								
																									BR. ST.57																								
I	753.2 01.1 03.2 02.3 02.2 03.8 00.6 14.8 20 -02.1 22 05 01.4 18 01.2 08 01.6 15 01.3 16 01.2 16 01.2 12 01.5 03 01.3 .																																																
II	745.3 05.4 09.1 07.2 07.9 09.6 04.8 14.9 11 00.0 28 06 02.5 25 02.0 10 01.9 02 01.0 10 01.3 11 02.6 17 02.2 03 02.0 .																																																
III	746.3 06.2 11.9 09.6 09.4 12.6 05.8 23.1 22 00.4 14 13 01.9 35 01.9 18 01.6 04 02.5 04 02.0 06 01.7 11 02.7 02 02.5 .																																																
IV	744.9 08.3 14.5 11.2 11.3 15.2 07.3 20.8 10 03.1 14 18 01.9 29 02.4 07 01.9 05 01.6 06 02.2 09 01.8 11 02.0 04 01.5 01																																																
V	745.0 12.7 18.6 14.3 15.0 19.4 11.1 25.6 22 07.3 10 14 01.6 16 01.7 C8 01.6 07 02.0 09 01.8 19 01.7 10 01.6 10 01.8 .																																																
VI	745.7 17.7 21.7 17.4 22.8 13.3 27.5 26 08.3 12 11 01.6 09 01.7 09 01.7 05 02.0 12 01.7 18 02.2 15 01.9 11 01.9 .																																																
VII	747.9 18.0 24.7 20.6 21.0 26.1 16.1 32.6 17 12.4 08 14 01.7 18 01.8 07 02.1 09 02.0 08 01.9 09 02.2 10 01.9 14 01.7 04																																																
VIII	748.2 18.9 25.9 21.8 21.0 22.1 26.8 17.3 33.2 14 11.3 13 15 C1.6 21 01.7 16 01.6 13 01.5 08 01.9 04 01.2 03 01.3 08 01.5 01																																																
IX	747.5 14.2 20.1 16.4 16.8 20.9 13.2 27.3 03 06.3 27 11 01.5 23 01.6 07 01.7 06 01.8 11 01.5 10 01.8 13 01.5 06 01.2 03																																																
X	744.2 06.0 09.8 07.4 07.3 10.6 05.1 15.1 20 01.0 30 11 01.5 18 01.7 09 01.3 03 01.7 09 01.8 19 01.6 18 01.4 06 01.3 08																																																
XI	748.8 05.4 09.5 07.2 07.3 10.0 04.8 18.9 16 -00.5 30 06 01.3 19 01.4 04 01.4 06 01.8 17 01.6 17 01.9 18 01.6 07 01.6 08																																																
XII	750.9 03.0 06.2 04.6 04.6 07.5 01.8 13.6 29 -03.8 15 09 01.8 13 01.5 11 01.3 07 01.1 08 01.2 11 01.8 23 01.7 11 02.0																																																
GOD.	- 07.9 15.3 09.2 10.4 16.2 04.6 34.4 04.VM -08.6 45.M 84 01.5 103 02.0 97 01.6 147 02.1 47 01.8 187 01.9 97 01.5 167 01.7 206																																																
$\varphi = 45^{\circ}49'$ N $\lambda = 16^{\circ}02'$ E Gr. $\Delta G = +1h\ 04\ min.$																									ZAGREB-NAKSIMIR																								
																									BR. ST.59																								
I	756.4 00.2 02.8 01.3 01.4 03.5 -00.5 16.2 20 -04.9 22 09 01.4 13 01.3 14 01.4 15 01.1 18 01.2 04 01.0 08 01.4 03 01.0 .																																																

Mjesec	Oblakčnost Nm (0-10)			Vlažnost vazduha %	Temperatura °C	Podzemne R sna	Broj dana na sat																																	
							U m s			Tn			Tx			Ta			Tn			F(0-12)			Nm(0-10)			R mm												
	7	14	21	Sred. (Dias.)	Inzolacijski broj sati	mm	7	14	21	U	m	s	7	14	21	T	7	14	8	N	7	14	8	N	7	14	8	N	7	14	8	N	•	*	Δ	▲	▲	R	T	≡
BRa ST-56	STUBIČKA GOMA																													$H_s = 620 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 2.0 \text{ m}$										
I 8-3 7.7 5-7 7-2	-	04.3	86	63	80	83	52	054	021.4	02	.	07	17	03	17	07	06	01	06	04	01	11	15					
II 7.9 6.6 6-6 7-5	-	05.1	87	68	84	84	55	067	033.4	07	.	08	03	01	03	14	08	06	01	06	05	02	09	07					
III 6.7 6.6 5-9 6-5	-	05.3	79	69	75	74	34	049	016.3	06	.	04	02	01	04	13	07	07	02	03	06	01	07	13					
IV 5.8 7.2 5-4 6-1	-	05.2	68	57	66	64	30	045	013.5	26	.	02	05	11	10	08	02	09	02	01	01							
V 6.0 6.0 6-0 6-2	-	07.6	75	65	77	72	37	221	046.2	01	01	.	02	13	16	15	07	16	02	04							
VI 6.4 6.6 6-1 6-4	-	05.2	76	66	75	72	47	162	064.9	30	03	10	14	12	05	14	01	03								
VII 4.7 4.3 3-7 4-2	-	10.4	72	59	66	63	23	063	029.6	07	.	.	11	.	.	.	01	.	08	05	08	06	02	08	02	02							
VIII 3.8 5.2 3-4 4-1	-	13.0	78	78	76	79	49	171	045.1	28	.	.	14	.	06	.	12	06	10	10	05	10	04	09									
IX 5.6 6.1 4-2 5-3	-	10.4	84	77	84	82	49	169	039.8	21	02	.	08	09	12	10	06	12	01	11								
X 7.0 7.8 6-2 7-0	-	-	-	-	-	-	-	288	055.8	31	.	.	02	.	.	.	01	.	14	18	18	09	16	03	01	01	03						
XI 6.6 6.5 6-2 6-4	-	05.6	83	78	82	81	38	065	033.4	29	.	08	.	.	.	03	01	02	10	10	09	01	07	08	03	01	04						
XII 5.4 5.4 5-6 5-5	-	04.8	77	74	78	76	50	037	023.5	12	.	02	10	.	.	03	.	06	07	04	03	01	03	01	01	02							
GOD. 6-2 6-6 5-4 6-1	-	-	-	-	-	-	-	1392	064.9	30VI	-	13	-	25	.	-	16	03	59	129	124	110	42	110	26	09	.	.	.	01	13	73	62							
BRa ST-57	ZAGREB-GRIC																												$H_s = 157 \text{ m } H_b = 162.5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$											
I 9.5 8.6 8-7 8-9	023.7	04.8	92	86	90	89	60	046	015.6	02	.	.	12	04	.	02	15	10	08	01	10	03	02	20	01						
II 7.8 7.0 7.0 7.5	066.5	05.5	79	64	73	72	31	034	014.0	07	04	.	02	15	10	08	01	10	03	02	01	02							
III 7.4 7.2 6-7 7-1	110.8	05.6	74	56	64	65	31	032	011.7	06	01	.	02	14	08	04	01	08	06	04	01	03								
IV 6.3 7.6 6-9 6-9	154.3	05.5	67	44	56	56	21	036	012.9	26	02	03	15	11	07	01	11	02	01	02	02									
V 5.9 7.0 7.2 6-9	181.0	08.5	77	54	73	68	33	189	041.5	01	.	.	02	.	.	02	.	03	12	18	13	06	18	07	.								
VI 6.4 6.3 6-1 6-3	179.6	10.4	77	54	69	67	34	127	050.5	30	.	.	08	.	.	01	.	02	09	18	10	04	16	04	.								
VII 4.5 4.8 4-6 4-6	274.8	11.7	73	51	64	63	36	052	018.4	07	.	.	19	05	.	01	01	09	08	06	03	08	01	07											
VIII 3.8 4.4 3-5 3-9	266.5	13.9	83	57	72	71	35	118	047.3	22	.	.	18	11	08	02	.	14	06	09	09	03	04	02	06										
IX 5.8 5.4 4.7 5-3	159.7	11.0	88	65	78	77	39	142	022.7	07	.	.	03	.	.	01	.	07	09	13	10	06	13	01	03	04									
X 7.7 7.6 6-5 7-3	074.9	06.5	90	74	83	83	37	224	034.5	21	03	15	22	16	07	22	02	07	.											
XI 8.1 7.0 7.6 7-5	081.4	05.4	88	68	79	77	28	062	029.0	29	.	.	02	.	.	02	.	14	11	07	01	11	01	01	01	13	02								
XII 7.2 7-2 6-2 6-9	076.6	04.9	84	72	78	78	39	022	010.3	12	.	01	10	.	.	04	.	03	13	10	04	01	09	04	14	.									
GOD. 6-7 6-8 6-3 6-6	1649.8	07.8	80	60	62	73	72	21	1084	050.5	30VI	.	01	24	50	16	08	19	01	48	152	152	101	35	151	18	10	01	.	02	03	32	69	04						
BRa ST-58	TOPUSKO																												$H_s = 129 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$											
I 9.1 5-0 6-7 8-9	-	05.0	97	97	97	97	82	053	016.7	02	.	01	25	01	26	10	08	02	09	01	20	01							
II 7.7 7.7 7-2 7-5	-	06.5	97	94	96	96	73	035	007.3	25	.	.	10	.	.	.	01	01	16	10	09	.	10	02	11	.								
III 8.1 7.7 7-2 7-9	-	07.9	97	91	95	95	61	067	018.5	06	.	.	10	01	.	.	01	19	11	10	03	09	C5	02	02	18	C3								
IV 7.4 7.9 6-9 7-4	-	08.6	97	91	94	94	74	047	012.4	26	.	.	10	.	.	01	02	17	14	12	01	14	01	02	10									
V 6-4 7-6 6-2 6-7	-	11.7	98	86	96	93	35	124	025.2	23	.	.	06	.	.	.	03	13	16	15	05	16	05	02									
VI 6-9 7-4 6-3 6-9	-	14.5	96	89	96	93	34	137	040.3	30	.	.	12	.	.	.	01	11	15	12	04	15	04	04									
VII 4-5 5-2 3-9 4-6	-	16.9	98	88	95	94	75	076	021.0	07	.	.	22	06	.	01	06	05	08	08	03	06	04	06									
VIII H-2 6-5 4-4 6-4	-	18.6	97	92	96	95	57	157	037.4	24	.	.	20	11	.	.	02	10	12	10	06	12	05	20									
IX 8-1 6-1 6-2 7-0	-	13.5	99	92	97	96	79	153	055.0	30	.	.	09	01	.	.	01	11	11	10	05	11	01	18									
X 8-4 8-3 6-3 8-3	-	076.5	97	91	95	94	73	272	047.2	03	.	07	.	01	.	01	21	20	18	08	20	02	07										
XI 7-2 9-2 6-4 7-1	-	072.2	96	93	96	95	79	079	028.4	29	.	.	12	06	.	.	01	16	13	12	13	21	01	01	01	13	C7								
XII 8-5 6-7 7-6 7-6	-	06.0	97	94	96	96	83	040	013.8	12	.	03	17	.	.	01	16	06	06	01	05	02	01	12	01								
GOD. 6-5 7-0 5-6 6-6	1663.8	08.0	86	63	63	77	22	1091	052.9	30VI	.	03	54	51	17	.	04	.	45	144	145	102	41	144	12	08	.	.	03	04	42	55	05							
BRa ST-59	ZAGREB-PAKSIMIR																												$H_s = 123 \text{ m } H_b = 127.6 \text{ m } h_t = 2.0 \text{ m } h_r = 2.0 \text{ m}$											
I 9.2 5-0 8-5 8-9	020.0	04.7	95	68	93	92	52	042	011.8	02	.	.	16	.	.	.	04	.	24	11	08	02	11	01	01	7C	02						
II 7.9 8-1 7-1 7-7	067.7	05.6	87	65	80	77	31	039	014.1	07	.	.	03	.	.	.	03	14	07	04	01	06	04	03	01	02	01								
III 7-6 7-9 6-4 7-1	125.0	05.7	83	57	74	71	27	029	010.7	06	.	.	04	.	.	.	03	12	07	01	12	07	03	0											

Mjesec	Vrstdinski pritisak Pm hPa	Temperatura vazduha °C										Cestine pravaca i srednja jačina vjetra ND, Pm (0-12)																	
		Tm			Sred. (Dnev.)	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21							c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.	j.	c.				
$\varphi = 45^{\circ}30'$ N $\lambda = 16^{\circ}22'$ E Gr. $\Delta G = +1h\ 06\ min.$																													
I	757.4	00.3	02.9	01.5	01.6	03.5	-00.7	13.3	20	-03.7	22	04	01.8	03	01.0	13	01.1	07	01.6	02	01.0	.	02	01.5	.	62			
II	749.6	04.1	09.9	06.5	06.7	10.7	02.3	16.7	12	-04.4	28	11	01.8	07	02.0	10	01.6	04	01.5	04	01.5	10	02.2	04	02.5	03	01.2	31	
III	752.6	04.0	12.3	08.1	08.1	13.0	02.7	23.4	21	-03.4	14	11	01.9	17	01.8	04	01.0	04	01.3	.	05	01.8	02	01.5	01	01.0	47		
IV	745.2	06.4	14.6	09.8	10.2	15.7	03.5	21.7	10	-01.1	20	10	02.8	12	02.7	11	01.3	03	01.5	01	02.0	03	02.0	02	02.0	43			
V	749.4	12.7	19.1	14.3	15.1	20.4	09.1	26.1	27	22	05.4	09	07	02.4	08	02.6	09	02.2	07	02.3	03	02.7	08	02.2	14	01.6	08	01.8	29
VI	749.9	16.0	21.9	17.0	17.9	23.3	11.3	26.6	26	05.4	12	09	02.3	11	03.0	04	01.5	03	02.0	02	03.0	10	02.5	17	01.9	03	03.7	31	
VII	752.0	18.0	25.3	19.9	20.8	26.5	13.5	33.7	17	08.4	28	04	02.5	08	02.4	07	02.1	09	01.9	03	02.3	05	02.8	10	01.8	04	01.8	43	
VIII	752.3	17.8	26.3	20.8	21.4	27.4	15.1	34.1	04	08.8	13	13	02.1	11	02.4	06	02.0	05	01.8	01	03.0	01	03.0	09	01.7	06	01.5	41	
IX	751.7	13.1	21.0	15.7	16.4	22.0	10.9	29.2	03	02.3	27	12	02.4	07	02.7	06	01.8	03	02.0	03	01.7	02	03.0	07	01.6	03	02.0	47	
X	748.5	06.4	10.8	08.0	08.3	11.7	04.6	17.9	20	-02.6	31	13	02.0	07	03.3	05	02.2	03	01.7	05	01.8	06	02.5	06	01.9	04	01.8	42	
XI	753.1	04.0	09.9	06.3	06.8	10.4	02.9	19.4	16	-04.8	29	06	02.8	05	02.6	10	01.2	09	01.3	01	02.0	05	02.4	03	02.3	03	01.7	48	
XII	755.4	01.4	06.3	02.9	03.3	07.3	-00.5	16.3	29	-04.6	24	04	01.8	03	02.3	11	01.2	03	01.3	01	01.0	04	01.0	06	01.5	.	61		
GOD.	751.8	08.8	15.0	10.9	11.4	16.0	06.2	34.1	04.VII	-04.8	29.VII	104	C2.2	99	02.4	96	01.5	61	01.7	26	02.0	62	02.2	85	01.8	37	01.9	525	
$\varphi = 45^{\circ}45'$ N $\lambda = 16^{\circ}38'$ E Gr. $\Delta G = +1h\ 06\ min.$																									CAZMA		BR. ST.61		
I	*	00.7	03.3	01.5	01.5	03.9	-00.5	12.4	20	-04.8	14	13	01.2	12	01.2	11	01.5	09	01.4	25	01.7	17	01.6	05	01.4	01	C1.0	*	
II	-	04.4	09.6	06.2	06.6	10.2	02.6	15.3	12	-03.4	28	14	01.6	22	02.2	08	02.4	02	01.0	03	01.7	04	01.2	*	*	*	*		
III	-	04.3	12.4	08.1	08.4	13.1	02.4	24.3	22	-03.0	14.01	15	01.8	38	02.0	12	01.8	02	02.0	04	01.8	09	02.4	04	01.8	*	*		
IV	-	07.0	15.0	09.3	10.2	15.9	03.2	21.4	29	-01.4	16	27	02.3	16	02.4	14	02.2	02	02.5	08	01.8	12	02.4	04	02.2	07	02.3	*	
V	-	11.7	18.7	13.6	14.4	19.8	08.2	26.8	20	03.5	10	20	02.1	09	02.2	08	02.6	05	02.2	18	02.7	20	02.4	07	02.1	06	02.0	*	
VI	-	15.5	22.4	16.6	17.8	23.2	11.2	29.7	28	04.8	13	19	01.9	09	02.4	06	02.0	03	02.0	05	02.4	26	02.8	10	02.2	12	02.0	*	
VII	-	17.6	25.3	18.6	20.0	26.2	13.0	33.6	17	08.8	27	21	02.1	10	01.1	08	02.1	03	02.0	16	01.8	19	07.4	10	01.6	06	02.2	*	
VIII	-	17.9	27.2	21.8	22.1	28.2	13.7	34.6	17	08.6	13	30	02.0	13	01.6	02	02.0	01	02.0	18	02.1	13	01.9	*	*	*	*		
IX	-	13.7	21.6	17.1	17.4	23.2	10.5	28.9	01	04.5	27	19	01.8	10	01.9	07	01.9	05	01.8	14	01.9	12	02.0	11	01.6	12	01.9	*	
X	-	05.8	10.9	08.8	08.6	11.9	02.8	16.6	25	-01.7	31	28	02.0	14	02.0	06	01.8	05	02.2	08	03.0	16	02.2	05	02.0	11	C1.0	*	
XI	-	05.0	10.1	07.6	07.6	11.6	02.7	19.1	16	-03.7	10	22	02.1	04	01.5	04	02.0	02	01.8	22	02.3	25	02.3	01	02.0	04	02.0	*	
XII	-	01.5	06.4	04.1	04.0	07.6	-00.9	14.8	29	-06.2	23	09	02.1	06	02.0	06	01.5	09	01.7	14	01.9	40	01.7	09	01.4	01	02.0	*	
GOD.	-	08.8	15.3	11.1	11.6	16.2	05.7	34.6	17.VIII	-06.2	23.XII	236	02.0	163	02.0	103	C1.9	55	01.8	155	02.1	222	02.2	80	01.9	81	01.4	*	
$\varphi = 45^{\circ}54'$ N $\lambda = 16^{\circ}51'$ E Gr. $\Delta G = +1h\ 07\ min.$																									BJELOVAR		BR. ST.63		
I	754.6	00.2	03.0	01.2	01.4	03.3	-01.2	13.0	20	-05.4	15	11	01.0	21	01.1	10	01.1	11	01.0	09	01.0	16	01.0	10	01.0	05	C1.0	*	
II	746.9	0.9	0.9	0.6	0.6	10.5	0.2	17.0	10	-02.5	28	10	02.1	21	01.5	18	01.1	03	01.0	03	01.0	25	02.1	02	01.0	02	02.0	*	
III	749.9	0.9	12.6	07.9	08.1	13.5	02.4	24.5	22.21	-04.5	01	07	02.6	33	01.3	22	01.3	13	01.3	03	01.0	12	01.2	03	02.0	*			
IV	746.6	06.7	15.1	08.9	09.9	15.7	03.0	22.5	28	-02.0	22.20	22	02.3	20	01.5	17	01.1	04	01.0	07	01.0	09	01.2	06	01.3	05	01.4	*	
V	746.6	11.9	18.7	13.0	14.2	19.6	08.2	25.6	20	02.0	10	06	01.2	10	01.6	11	01.3	03	01.0	09	01.0	23	01.3	13	01.2	18	C1.2	*	
VI	747.2	15.4	21.8	16.6	17.3	22.9	11.9	26.5	27	05.2	12	14	01.8	03	01.0	05	01.0	02	01.0	03	01.6	15	02.4	10	01.8	01	01.0	*	
VII	749.4	17.7	24.8	18.8	20.0	26.0	13.1	33.5	17	05.2	27	21	01.8	09	01.4	08	01.0	16	01.0	21	01.2	13	01.0	05	01.6	*			
VIII	749.7	16.3	26.8	20.1	21.4	27.8	14.7	33.5	17	07.4	13	10	01.3	33	01.2	10	01.0	14	01.1	01	01.0	08	01.0	04	01.0	13	01.2	*	
IX	749.2	13.0	21.2	14.7	15.9	21.8	10.4	26.0	03	03.3	28	03	01.3	24	01.5	12	01.0	07	01.0	05	01.2	14	01.4	11	01.1	13	C1.0	01	

Meseč o	Oblačnost Nm (0-10)			Insolacija broj sati mm	Vlažnost vazduha			Padavine R mm	Broj dana na sa:																						
	7	14	21		7	14	21		Sred. Min	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	▲	■	■		
					mm	mm	mm		mm	mm	mm	mm	≤	<	≤	>	≤	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV				
SISAK																															
BR. ST.61																															
I 5.5 6.8 7.4 8.6	-	016.0	04.8	95 89 94 93 65	050	016.1	07	-	-	17	-	-	-	-	-	-	-	20	17	10	02	13	07	01	-	04	-	14	01		
II 7.8 7.7 6.5 7.3	-	076.2	05.8	87 67 80 78 36	037	012.2	05	-	-	-	-	-	-	-	-	-	-	02	13	14	07	01	13	01	-	-	01	01	03	-	
III 7.9 7.6 6.5 7.3	-	146.0	06.1	91 60 78 76 28	044	015.7	07	-	-	06	-	-	-	-	-	-	-	03	17	10	05	02	09	06	02	-	01	03	-	01	02
IV 6.2 6.0 5.6 6.6	-	157.8	06.3	84 50 70 78 27	034	012.1	26	-	-	05	-	-	-	-	-	-	-	03	12	12	10	01	11	01	-	-	-	02	03	-	
V 6.4 7.2 5.9 6.5	-	206.8	09.3	84 56 78 73 35	126	022.2	01	-	-	-	07	-	-	-	-	-	-	01	02	03	11	19	16	08	15	-	-	-	01	08	01
VI 6.3 6.7 6.5 6.5	-	111.5	83 59 79 74 41	108	034.9	30	-	-	-	-	10	-	-	-	-	-	-	01	01	01	01	12	09	05	17	-	-	05	02	-	
VII 4.0 4.5 4.0 4.4	-	300.1	13.0	81 54 78 71 40	047	C19.7	07	-	-	-	-	21	09	-	-	-	-	11	06	11	06	01	10	-	-	-	03	01	-		
VIII 5.3 4.4 3.1 4.3	-	252.1	15.3	92 62 87 80 41	065	029.0	24	-	-	-	20	10	-	-	-	-	11	06	12	09	01	12	-	-	-	12	14	-			
GOD. 7.0 6.9 5.7 6.6	-	1770.5	08.5	88 65 83 79 27	948	048.1	20IX	-	-	02	58	68	3	-	07	04	47	153	174	116	35	159	17	03	-	01	07	02	46	65	06
ČAZMA																											$H_s = 144 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$				
BR. ST.62																															
I 5.7 6.5 6.5 8.9	-	05.0	95 95 94 95 69	056	013.5	07	-	01	14	-	-	-	-	-	-	-	-	24	11	09	02	10	02	02	-	-	-	16	-		
II 7.5 7.9 6.6 7.3	-	06.9	93 90 91 91 61	041	016.8	07	-	-	03	-	-	-	-	-	-	-	03	17	09	07	01	09	01	01	-	-	01	04	-		
III 7.5 6.8 6.5 6.9	-	08.2	92 91 91 91 69	024	007.8	07	-	-	05	-	-	-	-	-	-	-	04	18	06	04	-	04	05	03	-	-	01	03	-		
IV 6.6 6.9 5.5 6.5	-	05.2	93 92 93 93 78	021	013.1	26	-	-	05	-	-	-	01	-	04	10	07	06	01	07	-	-	-	-	-	-	01	-			
V 6.4 6.7 6.5 6.7	-	12.1	93 92 93 93 73	149	036.8	01	-	-	02	-	-	-	-	-	-	-	04	12	17	13	05	17	-	-	01	06	-				
VI 7.0 7.3 7.1 7.1	-	15.2	94 94 94 94 85	114	045.2	30	-	-	11	-	-	-	-	-	-	-	02	12	14	11	03	14	-	-	01	01	-				
VII 3.8 4.3 5.3 4.4	-	17.4	92 92 93 93 77	068	023.8	07	-	-	21	08	-	-	-	-	-	-	10	04	08	07	03	08	-	-	02	02	-				
VIII 5.4 5.3 5.3 5.0	-	16.9	93 94 95 94 87	068	014.3	12	-	-	24	13	-	-	-	-	-	-	09	09	10	08	03	10	-	-	01	05	-				
IX 7.2 6.1 6.4 6.6	-	14.5	94 91 94 93 66	119	026.3	30	-	-	15	-	-	-	-	-	-	-	02	12	12	10	05	12	-	-	01	01	07				
X 8.0 8.3 7.7 8.0	-	07.9	93 92 94 93 76	222	C29.3	21	-	-	02	-	-	-	-	-	-	-	03	21	20	20	09	20	-	-	05	-	02				
XI 8.1 7.1 6.0 7.8	-	07.5	92 91 91 92 72	059	021.0	29	-	-	03	-	-	-	-	-	-	-	16	14	09	02	10	01	01	-	-	06	02	-			
XII 8.3 7.1 7.6 7.7	-	05.7	91 91 92 92 72	030	010.8	18	-	01	17	-	-	-	-	-	-	-	02	19	08	04	01	06	02	02	-	-	08	01	-		
GOD. 7.1 6.8 6.8 6.9	-	10.8	92 92 93 92 61	971	045.2	30VI	-	02	49	72	21	-	01	-	-	-	43	174	136	108	35	131	11	09	-	02	-	14	58	03	
BJELOVAR																											$H_s = 141 \text{ m } H_b = 142.4 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$				
BR. ST.63																															
I 8.8 8.8 8.4 8.7	-	04.8	55 65 56 53	056	015.8	07	-	01	19	-	-	-	-	-	-	-	01	24	12	09	02	12	03	02	-	-	01	14	-		
II 7.0 7.0 7.2 7.2	-	05.7	90 67 82 79 46	039	012.2	07	-	-	03	-	-	-	-	-	-	-	01	02	14	09	09	01	05	02	02	-	-	01	03	01	
III 5.5 5.7 4.6 5.3	-	06.0	89 61 75 75 23	020	010.5	06	-	-	09	-	-	-	-	-	-	-	09	13	06	05	01	05	04	02	-	-	01	02	-		
IV 6.0 6.7 5.4 6.0	-	06.2	83 49 70 67 27	022	010.8	26	-	-	03	-	-	-	-	-	-	-	05	11	08	03	01	08	01	01	-	-	01	01	-		
V 6.6 7.3 5.7 6.5	-	05.3	86 59 84 77 37	183	052.0	01	-	-	03	-	-	-	-	-	-	-	03	11	17	13	06	17	-	-	01	06	-				
VI 6.2 6.3 5.4 6.0	-	11.2	83 60 80 74 44	142	056.0	30	-	-	09	-	-	-	-	-	-	-	01	07	13	09	05	13	-	-	05	-	02				
VII 4.0 4.2 3.7 4.0	-	12.6	78 56 77 71 41	074	029.4	07	-	-	18	06	-	-	-	-	-	-	12	07	10	07	03	10	-	-	02	02	01				
VIII 5.0 3.9 3.7 4.2	-	14.9	87 58 86 77 42	077	020.7	12	-	-	24	12	-	-	-	-	-	-	14	06	08	07	05	08	-	-	04	01	-				
IX 6.6 5.2 3.9 5.2	-	11.2	92 64 88 81 42	097	C26.6	21	-	-	09	-	-	-	-	-	-	-	07	07	10	09	04	16	-	-	-	-	02				
X 7.8 7.7 6.3 7.2	-	06.5	94 75 91 87 48	176	027.5	21	-	-	05	-	-	-	-	-	-	-	01	17	20	17	08	20	-	-	06	-	01				
XI 7.3 6.0 5.7 6.3	-	05.9	92 70 88 83 41	051	023.0	29	-	-	09	-	-	-	-	-	-	-	05	17	20	19	08	20	-	-	07	01	-				
XII 7.7 6.5 5.4 6.5	-	05.0	93 78 92 87 48	040	010.8	18</td																									

Mesec	Vrstdusni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)																		
		Tm			Sred. (Dies)				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW	
		7	14	21	Sred. (Dies)	Max	Min	Dat.	Min	Dat.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.				
$\varphi = 45^{\circ}36'$ N $\lambda = 17^{\circ}14'$ E Gr. AG = + 1h 09 min.																									DARUVAR					
I	752.5	00.4	03.3	01.6	01.6	04.2	-06.3	13.0	31	-05.7	15	13	01.5	05	01.4	C7	01.1	03	02.0	08	C1.4	C3	01.0	06	01.3	20	01.0	28		
II	745.7	04.1	05.9	06.1	06.5	10.9	02.9	16.0	12	-04.5	20	20	02.0	08	01.9	C6	01.2	06	01.5	17	02.4	08	02.2	04	02.2	02	01.5	13		
III	748.6	03.6	12.5	07.6	07.8	13.5	02.7	25.0	22.1	-05.4	01	18	02.1	16	01.8	C5	02.2	06	01.8	03	01.0	01	01.0	05	02.0	05	01.2	34		
IV	745.1	06.2	15.0	08.8	09.7	16.1	03.7	24.0	29	-01.4	20	18	01.9	13	01.8	C2	01.0	06	01.0	05	01.0	06	01.3	04	01.5	06	01.3	30		
V	745.3	12.2	16.7	12.6	14.1	19.9	09.1	26.6	30	03.5	09	12	01.6	10	01.6	C7	01.0	13	01.0	10	01.4	07	01.3	02	02.0	11	C1.4	21		
VI	745.8	15.4	22.0	16.1	17.4	23.2	11.8	25.0	27	05.0	12	19	02.1	05	01.4	C5	01.4	05	01.0	08	01.4	10	01.7	C7	01.4	09	C1.3	17		
VII	746.0	18.2	25.3	19.0	20.4	26.7	13.8	35.4	27	09.2	16	16	C1.6	07	01.4	C8	01.0	14	01.1	11	01.3	05	01.4	07	01.1	09	C1.4	16		
VIII	746.2	18.0	27.1	19.6	21.1	28.0	15.0	34.5	04	08.7	13	13	01.3	19	01.5	C4	01.2	07	01.3	06	01.0	04	01.2	02	01.5	05	C1.2	33		
IX	747.7	13.0	21.0	14.8	16.1	23.0	11.0	30.6	03	06.6	27	20	01.6	08	01.5	C3	01.0	06	01.0	06	01.2	05	C1.4	03	01.0	08	C1.2	31		
X	744.6	05.3	10.7	07.0	07.5	11.9	04.1	17.6	04	-01.6	31	15	C1.5	C9	01.1	C2	01.0	06	01.2	18	C1.6	07	01.3	04	01.2	07	C1.3	25		
XI	745.4	04.4	10.2	05.5	06.4	11.1	03.1	15.6	10	14	01.6	04	01.2	C3	01.0	13	01.0	16	01.4	07	01.4	08	01.1	04	C1.5	21				
XII	751.4	02.8	07.2	03.9	04.5	06.2	01.3	16.6	29	-04.4	24	16	01.5	C4	01.0	18	01.1	12	01.2	09	01.1	04	01.0	06	C1.0	20				
GOD.	747.8	08.6	15.3	10.2	11.1	16.4	06.5	35.2	47V	-05.7	15.1	194	C1.7	108	01.5	56	01.2	106	01.5	72	01.4	56	01.4	92	C1.2	289				
$\varphi = 45^{\circ}44'$ N $\lambda = 17^{\circ}38'$ E Gr. AG = + 1h 11 min.																									DONJI MELJANI					
																										BR. ST.67				
I	-	CG.5	C3.3	01.6	01.6	04.7	-06.9	11.3	21	-07.0	29	07	01.6	07	01.1	25	C1.4	18	01.3	09	01.0	05	01.6	10	01.5	12	C1.8	.		
II	-	04.7	06.6	06.7	11.1	02.1	16.8	12.11	-02.8	28	10	C1.7	C3	01.3	14	01.6	C5	01.4	05	01.2	05	01.4	24	01.4	12	01.8	11	C1.5	.	
III	-	03.9	12.0	08.3	08.1	13.5	02.4	24.2	21	-04.4	01	10	02.3	05	01.8	23	02.0	24	C1.5	08	01.0	13	01.0	12	01.2	04	C1.2	01		
IV	-	06.5	14.9	10.2	10.4	16.5	04.0	24.8	26	-02.2	04	07	C2.1	C6	02.2	C5	01.0	12	C1.2	07	01.1	23	01.2	14	01.2	16	01.6	.		
V	-	13.1	16.7	14.2	15.0	20.4	05.5	27.4	21	05.0	09	10	01.9	04	01.8	C4	01.2	07	01.3	06	01.2	21	C1.4	23	01.5	18	C1.7	.		
VI	-	21.9	17.1	16.1	23.9	11.7	3.2	27	07.4	08	C9	C1.8	03	01.3	66	01.0	06	01.3	16	01.4	19	C1.7	27	04.0	01					
VII	-	19.2	25.4	20.2	21.2	27.2	13.5	34.5	14	08.2	27	08	01.9	06	01.7	11	01.1	09	01.7	02	01.0	32	01.1	11	01.5	21	C1.7	.		
VIII	-	26.6	20.8	22.1	29.0	14.9	35.8	04	09.0	08	16	01.6	04	01.0	14	C1.3	C6	01.2	06	01.0	20	01.0	14	01.4	13	C1.5	.			
IX	-	14.6	21.5	16.3	17.2	23.5	10.5	31.2	03	01.2	14	C9	01.7	10	01.2	14	01.1	09	01.3	07	01.3	15	01.0	11	01.1	15	C1.7	.		
X	-	06.1	11.1	07.3	08.0	12.9	03.6	17.5	19	-06.5	31	06	C1.7	C5	01.0	05	01.2	09	01.4	12	01.2	23	01.4	18	01.4	15	C1.3	.		
XI	-	05.9	10.2	07.0	07.0	12.3	02.8	22.4	16	-02.0	20	27	06	02.0	04	01.5	C5	01.2	22	01.4	06	01.0	33	01.3	07	01.4	07	C1.6	.	
XII	-	03.4	07.0	04.2	04.7	09.1	01.1	19.3	29	-04.2	25	C6	C1.8	05	01.0	07	C1.4	09	01.3	02	01.0	37	01.5	14	01.4	13	C1.9	.		
GOD.	-	09.3	15.2	11.2	11.7	17.0	06.3	35.8	04V	-07.0	29.1	97	01.8	64	01.4	133	01.4	136	01.3	74	01.1	252	01.3	165	01.4	172	C1.7	02		
$\varphi = 45^{\circ}20'$ N $\lambda = 17^{\circ}41'$ E Gr. AG = + 1h 11 min.																									SLAVONSKA PEŽEGA					
																										BR. ST.68				
I	-	06.2	04.0	C2.5	02.3	04.7	-00.6	11.1	20	-06.5	15	21	C1.2	14	01.1	21	01.2	C7	01.0	01	01.0	06	01.0	08	01.2	15	C1.1	.		
II	-	02.0	10.1	06.3	06.2	11.1	00.5	17.0	12	-04.3	29	12	C1.3	11	01.8	C7	01.3	06	C1.3	05	01.2	09	C1.4	17	01.7	17	C1.1	.		
III	-	02.9	12.0	07.9	07.9	13.6	01.7	24.5	22	-04.5	01	10	01.2	12	01.7	18	C1.4	C3	01.7	06	01.5	04	02.0	23	01.2	17	C1.2	.		
IV	-	06.2	09.7	10.2	16.0	16.0	03.2	23.5	29	-01.9	04	22	01.6	09	01.4	10	01.5	C4	01.7	07	01.3	16	01.3	13	01.2	10	C1.5	.		
V	-	11.7	19.4	14.3	14.9	20.2	08.4	26.5	31	02.8	10	13	C1.4	11	01.6	C6	01.2	03	01.3	12	01.1	14	01.2	25	C1.3	10				
VI	-	15.4	21.1	16.8	17.8	23.1	11.0	25.6	27	05.9	13	25	C1.5	C9	01.0	05	01.0	03	01.3	17	01.5	22	01.1	10	C1.3	.				
VII	-	17.3	25.3	19.6	20.4	26.3	12.3	34.0	17	06.1	27	11	C1.5	10	01.2	10	01.3	05	01.0	06	01.5	15	01.5	24	01.2	12	C1.2	.		
VIII	-	17.9	27.3	21.1	21.6	28.1	14.1	34.1	04	09.0	10	17	C1.2	C8	02.1	C3	01.7	17	01.8											

Mjesec	Oblačnost Nm (0-10)				Inovacije broj (Dnes)	Vlažnost vazduha				Padavine mm	Broj dana na sat																								
	7	14	21	Sred. (Dnes)		mm	7	14	21	Sred. min	Σ	Max	Dat.	Tn	Tx	In	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	III	II		
	≤	<	<	IV		IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV				
BR. ST.66																																			
CARUVAR																																			
I	8.5	8.7	6.5	7.9	034.1	04.6	96	86	94	51	070	014.7	07	•	01	17	•	•	•	01	17	11	09	03	11	•	•	01	•	13	•				
II	6.7	7.5	6.3	6.8	091.4	05.6	88	62	81	77	32	020	008.7	07	•	04	•	•	01	•	C2	11	09	07	•	05	C2	01	•	02	•				
III	5.7	6.5	5.3	5.8	127.8	05.8	92	57	78	75	26	020	008.4	05	•	07	02	•	•	05	13	07	05	•	06	04	01	•	•	01	•				
IV	5.7	6.4	5.2	5.8	143.5	06.0	87	42	73	68	23	019	004.7	26	•	03	•	•	•	•	06	11	12	05	•	12	•	•	•	•	•	01	•		
V	6.6	6.8	5.2	6.2	169.9	09.1	85	55	86	75	31	118	016.0	23	•	•	05	•	01	01	03	12	27	17	04	22	•	•	•	05	01	•			
VI	5.7	6.8	6.4	6.3	192.9	10.8	82	53	82	72	34	144	053.0	30	•	•	10	•	•	03	09	16	09	05	18	•	•	•	08	•	•				
VII	4.2	4.5	3.8	4.2	276.4	12.5	78	50	86	69	32	059	017.6	07	•	•	21	09	01	01	13	07	11	09	03	11	•	•	05	•	•				
VIII	3.9	4.3	2.8	3.6	263.4	14.4	89	54	86	77	35	060	019.4	12	•	•	23	13	•	01	13	04	11	08	02	11	•	•	08	•	•				
GOD.	6.2	6.5	5.4	6.0	1705.9	08.1	87	59	83	77	23	959	053.0	30VI	•	01	50	73	23	01	04	01	62	128	162	115	34	159	10	04	•	01	25	30	
BR. ST.67																																			
CGNJI MELJANI																																			
I	9.2	8.3	7.8	8.4	-	04.8	89	93	86	85	47	059	014.2	07	•	•	18	•	•	02	22	12	10	03	12	C1	01	•	•	21	•				
II	7.4	7.6	6.8	7.3	-	06.7	91	86	89	89	66	030	008.5	07	•	02	•	•	01	•	C1	14	09	06	•	08	01	•	•	07	•				
III	6.8	4.0	5.1	4.9	-	07.9	92	88	91	96	53	023	008.6	08	•	08	•	•	01	10	08	05	05	05	04	03	•	•	07	•					
IV	6.4	6.2	6.3	6.3	-	08.3	89	80	86	85	40	013	004.7	26	•	03	•	•	01	05	13	06	05	06	•	•	•	•	•	•					
V	6.8	7.5	5.3	6.5	-	10.3	83	73	80	79	40	122	040.2	01	•	•	05	•	•	02	12	15	14	04	15	•	•	•	•	•	•				
VI	5.8	6.4	4.8	5.7	-	11.8	83	60	82	75	31	173	070.5	30	•	•	13	01	•	05	07	12	10	05	12	•	•	•	•	•	•				
VII	4.4	4.1	3.6	4.0	-	13.6	78	61	73	70	20	075	042.0	07	•	•	19	10	•	11	06	09	09	01	05	•	•	02	02	•					
VIII	4.5	3.8	3.2	3.8	-	15.2	83	64	73	74	40	144	040.5	27	•	•	26	13	•	15	05	11	11	04	11	•	•	02	02	•					
IX	6.5	5.8	4.7	5.7	-	11.7	89	65	75	78	21	075	016.4	27	•	•	13	01	•	04	11	68	68	04	08	•	•	01	02	•					
X	8.3	8.1	6.5	7.6	-	06.8	90	79	80	83	26	218	038.5	06	•	01	•	•	01	•	02	16	21	15	09	21	•	•	04	•	•				
XI	6.7	5.5	5.0	5.8	-	05.9	86	74	75	78	42	061	021.4	26	•	05	•	•	01	04	10	06	07	02	06	01	•	•	13	01	•				
XII	5.5	7.0	5.6	7.2	-	05.5	86	81	84	84	47	077	027.4	18	•	12	•	•	01	01	15	12	11	02	11	05	04	02	•	07	01				
GOD.	6.6	6.3	5.4	6.1	-	09.0	86	74	81	81	20	1070	070.5	30VI	•	•	49	76	28	•	01	•	61	139	128	113	34	126	12	08	02	•	04	63	01
SLAVCIŠKA PG2EGA																																			
BR. ST.68																																			
I	8.4	7.8	6.5	7.6	-	05.0	93	87	93	91	60	064	017.6	07	•	17	•	•	01	17	12	06	03	11	02	•	•	•	•	17	01				
II	6.0	6.4	3.5	5.3	-	05.9	93	69	88	84	40	024	005.6	14	•	11	•	•	04	05	09	07	•	05	01	01	•	•	04	•	•				
III	6.0	6.5	4.1	5.6	-	06.5	90	65	86	81	31	027	009.8	06	•	09	•	•	05	08	07	06	•	05	04	01	•	•	01	•					
IV	6.0	7.0	4.4	5.8	-	07.2	89	56	87	77	33	018	004.2	26	•	04	•	•	01	05	09	11	06	11	C1	01	•	•	•	•					
V	6.3	4.3	4.5	5.9	-	10.1	89	63	85	79	45	069	010.2	12	•	04	•	•	02	01	06	20	12	01	20	•	•	11	01	•					
VI	5.4	6.0	5.1	5.5	-	12.2	86	65	85	79	48	136	036.6	11	•	10	•	•	03	03	19	11	05	18	•	•	07	•	•						
VII	3.4	4.4	3.1	3.6	-	13.9	87	60	85	77	44	053	013.3	19	•	21	09	•	14	06	10	07	03	10	•	02	•	02	01	•					
VIII	3.3	4.0	2.7	3.9	-	15.3	86	61	86	78	40	094	027.0	28	•	24	13	•	13	03	11	11	04	11	•	•	05	01	•						
IX	5.7	5.5	4.2	5.3	-	12.3	92	65	88	83	46	097	019.1	27	•	10	•	•	04	06	09	07	05	05	•	•	02	03	•						
X	7.3	7.5	5.6	6.8	-	06.4	93	76	91	87	44	208	035.1	06	•	05	•	•	04	11	19	15	08	19	•	•	01	04	•						
XI	7.1	6.3	5.1	6.7	-	06.1	92	73	89	85	45	047	018.6																						

Mjesec	Vrijednost Prstensk Br. m/m	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra nD, fm (0-12)																												
		Tm			Max.			Min.			Dat.			N			NE			E			SE			S			SW			W			NW			C		
		7	14	21	Sred. Dnev.	Max.	Min.	Max.	Min.	Max.	Dat.	Min.	Dat.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.			
$\varphi = 45^{\circ}17'$ N $\lambda = 18^{\circ}25'$ E Gr. $\Delta G = + 1h\ 14\ min.$																																LJAKOVO		BR. ST. 71						
I	-	00.0	03.0	01.4	01.4	03.6	-01.0	05.6	22	-06.6	15	14	01.5	6	01.3	C6	01.3	C6	01.1	04	01.0	16	01.3	C7	01.4	35	C1.5						
II	-	02.2	05.8	05.8	05.8	10.7	01.3	16.8	12	-02.5	28.01	18	01.7	6	01.7	C8	02.1	08	01.6	09	01.3	10	01.3	C5	01.8	17	C1.3						
III	-	05.8	13.0	07.6	08.0	13.4	02.3	15.0	22.1	-02.6	02	37	01.6	6	01.8	C4	02.6	05	02.2	.	11	01.4	02	01.0	16	C1.4							
IV	-	11.7	15.1	09.5	10.4	15.9	03.8	25.0	20	-01.0	04	32	01.8	5	02.4	C4	03.0	07	01.3	08	02.1	08	02.0	23	C1.9								
V	-	14.7	18.8	13.2	14.5	19.7	08.9	26.4	31	03.6	10	17	01.6	6	07.8	C1	02.0	09	01.3	16	01.8	15	02.3	27	C2.0								
VI	-	16.4	21.3	16.6	17.7	24.9	12.4	30.6	27	07.2	13	08	01.8	01	0.0	C3	01.7	06	01.5	04	01.8	14	01.7	17	02.3	37	C2.2						
VII	-	14.2	24.8	18.7	20.1	26.2	13.4	34.4	14	05.5	27	08	02.2	06	01.7	C1	01.0	18	01.4	04	01.8	12	01.8	11	02.4	33	C2.0						
VIII	-	18.9	27.2	19.9	21.4	28.0	15.5	33.5	04	10.5	10	09	01.9	06	09	02.0	14	01.9	08	01.5	03	01.3	09	01.4	34	C1.6							
IX	-	13.9	27.1	15.3	16.6	22.8	11.6	30.8	03	02.8	28	16	01.4	08	01.6	.	.	09	01.6	12	01.2	06	C1.3	C5	02.0	31	C1.7						
X	-	05.4	11.0	07.2	07.4	12.0	03.7	18.0	04	-01.0	31	11	01.5	02	0.5	C3	01.3	11	02.0	04	02.0	08	02.0	09	01.7	45	C1.7						
XI	-	02.5	09.7	04.5	05.3	10.2	01.3	19.6	16	-02.8	10	07	02.3	11	01.8	C1	02.0	22	01.4	10	01.5	03	02.0	05	02.0	31	C1.6						
XII	-	01.8	06.0	02.8	03.4	07.0	06.2	16.4	29	-04.6	23	04	02.5	03	02.3	02	02.0	20	01.4	04	02.0	30	01.6	07	01.9	23	C2.1						
GOD.	-	08.6	19.2	10.2	11.0	16.0	06.1	34.4	Fm	-06.6	15	181	01.7	68	01.8	45	02.1	141	01.6	69	01.4	137	C1.6	100	02.0	347	C1.8	03						
$\varphi = 45^{\circ}42'$ N $\lambda = 18^{\circ}44'$ E Gr. $\Delta G = + 1h\ 16\ min.$																																BREŠTOVAC-BELJE		BR. ST. 72						
I	760.0	00.0	03.5	01.4	01.6	04.1	-01.1	05.8	20	-06.6	15	03	03.7	09	01.6	23	C1.8	12	01.8	08	01.5	02	01.5	14	01.4	12	C2.1						
II	750.7	01.6	10.1	04.7	05.3	10.6	00.7	17.0	12	-03.0	28	06	01.5	12	01.7	16	01.6	05	01.6	17	01.5	16	01.6	07	01.4	05	C1.4						
III	754.6	01.4	13.3	07.5	07.9	11	01.1	25.5	21	-04.0	03	02	04	01.5	12	01.4	24	02.0	25	02.4	01	01.0	07	01.9	04	02.8	06	C1.3					
IV	752.1	07.1	15.2	09.9	10.5	14.0	04.1	24.5	28	-01.1	04	12	03.0	21	02.1	13	02.2	11	02.5	05	01.8	04	02.0	12	C1.7	11	C2.1						
V	751.4	12.5	19.9	13.4	14.6	20.0	09.2	26.0	31	04.0	10	10	02.6	03	02.0	05	01.8	05	01.4	09	01.6	08	01.9	23	C1.7	30	C2.6						
VI	752.3	16.0	21.4	16.4	17.6	22.6	12.4	30.0	27	06.9	08	14	C2.9	04	01.8	C5	01.6	05	01.2	04	01.8	10	01.5	16	01.6	30	C2.4						
VII	754.4	17.9	24.8	18.7	20.0	25.5	13.7	33.9	14	05.6	09	16	02.8	04	01.2	05	01.4	10	01.8	09	02.0	03	02.3	16	C1.6	30	C2.0						
VIII	754.8	18.8	27.0	20.1	21.5	27.0	15.0	34.0	03	10.1	07	08	01.8	23	01.7	18	01.9	05	02.0	07	01.9	08	01.2	10	01.1	14	C2.7						
IX	754.4	13.4	21.0	15.3	16.4	22.5	11.3	29.8	03	02.4	28	14	02.5	20	01.8	08	01.6	08	02.1	09	01.6	03	01.0	14	C1.9	14	C2.0						
X	751.6	05.7	11.0	06.7	07.4	11.6	03.8	17.5	12	-01.5	31	16	02.3	07	02.0	08	01.8	12	01.6	12	01.9	11	C1.6										
XI	752.1	02.5	09.7	04.2	05.4	10.1	01.5	17.6	17	-02.9	10	09	02.7	11	01.9	10	01.4	10	01.3	19	01.8	12	01.8	11	02.2								
XII	752.6	01.2	11.5	02.4	03.0	06.2	00.4	13.5	04	-04.3	23	09	02.8	05	02.0	07	01.7	05	01.6	15	01.5	10	01.6	27	01.6	14	C2.3						
GOD.	754.5	06.3	18.4	10.1	10.9	16.0	06.1	34.0	Fm	-06.6	15	121	02.6	142	01.8	164	01.8	109	02.0	116	C1.7	95	C1.7	173	C1.7	185	C2.7						
$\varphi = 45^{\circ}42'$ N $\lambda = 18^{\circ}44'$ E Gr. $\Delta G = + 1h\ 15\ min.$																																CSIJEK		BR. ST. 71						
I	760.1	-00.1	03.7	01.7	04.4	-01.0	16.4	22	-06.2	15	06	02.0	12	01.9	26	02.0	14	01.7	C5	01.6	04	C1.8	11	C1.5	13	C2.6							
II	752.4	01.5	10.2	05.0	05.6	11.0	00.9	27.2	14	-02.2	28	22	11	02.1	08	01.0	14	02.4	17	01.8	11	02.0	03	02.0	10	C1.6							
III	755.0	03.0	13.9	07.5	08.0	14.5	02.3	26.1	22	-02.1	02	09	01.9	15	01.9	23	02.5	14	02.3	07	02.1	03	02.3	08	02.0	08	C1.6						
IV	751.4	06.5	15.7	09.4	10.3	16.9	04.7	23.9	28	-06.6	16	20	02.2	11	01.5	03	03.1	16	02.3	05	01.8	15																		

Mjesec	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																							
	e _m	7	14	21		7	14	21	Stred. Sred. (Ukupno)			Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■		
	7	14	21	Sred. (Ukupno)	mm	7	14	21	Stred. Sred. Min	Σ	Max	Dat.	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<				
BR. ST.71																																			
DJAKOVAC																																			
I	8.7	8.1	7.5	8.1	-	04.5	87	86	90	89	70	061	C12.0	20	.	.	19	16	13	09	02	12	03	.	.	.	19	.		
II	7.6	6.2	5.5	6.4	-	06.1	84	80	88	84	47	025	006.6	05	.	.	09	01	06	10	07	.	09	01	.	.	06	.		
III	5.7	6.0	5.7	5.8	-	06.4	84	64	85	78	17	020	005.5	07	.	.	07	02	09	08	05	.	04	06	.	.	03	.			
IV	5.6	6.4	6.4	6.4	-	07.0	75	56	91	71	27	020	010.6	18	.	.	02	01	.	.	.	01	01	08	01	10	02	01	01	.	01	.			
V	6.0	6.5	5.5	6.0	-	09.5	82	61	83	75	40	082	C16.0	01	.	.	03	01	04	17	13	03	17	.	.	.	08	.			
VI	5.6	6.7	6.7	5.3	-	11.6	79	62	84	75	45	114	044.8	11	.	.	04	01	.	.	.	09	14	11	04	14	.	.	.	05	.				
VII	5.6	5.2	5.6	5.0	-	13.3	79	59	85	74	42	054	C09.6	20	.	.	21	08	.	.	.	04	06	12	09	.	12	.	.	.	02	.			
VIII	5.9	4.6	4.6	4.4	-	15.0	86	59	95	76	43	084	C28.0	26	.	.	24	12	.	.	.	02	02	04	07	04	05	.	.	07	01	.			
IX	6.7	5.7	4.8	5.7	-	11.9	84	69	88	81	46	060	C24.6	05	.	.	10	01	.	.	.	08	08	05	02	08	.	.	.	C1	05	.			
X	6.1	7.4	7.2	7.6	-	06.8	85	79	86	84	49	155	029.8	29	.	.	02	15	19	14	05	15	.	.	.	10	.				
XI	7.2	6.6	5.6	6.5	-	05.7	84	77	86	82	53	056	C18.0	29	.	.	07	10	13	11	02	13	01	.	.	.	10	.			
XII	7.2	7.2	7.0	7.1	-	04.9	83	76	85	82	26	050	006.9	12	.	01	16	.	.	.	11	16	11	.	14	02	.	.	.	07	G2	.			
God.	6.4	6.4	6.0	6.3	-	06.6	82	49	85	79	17	789	C44.8	44 VI	.	01	62	70	22	.	05	.	08	104	149	11C	23	143	15	01	01	.	24	61	02
BR. ST.72																																			
BRESTOVAC-BELJE																																			
I	9.1	8.0	7.5	8.2	041.0	04.6	93	83	91	89	62	034	C14.3	20	.	.	22	01	21	11	05	01	1C	03	01	01	.	19	01		
II	6.7	6.6	4.1	5.8	079.4	06.2	92	60	93	90	52	018	C06.0	24	.	.	13	06	07	09	04	.	06	01	.	.	.	07	.		
III	5.5	5.9	4.9	5.3	151.3	05.8	88	63	77	76	21	029	C09.0	06	.	.	09	01	.	.	.	09	11	06	07	.	05	05	.	.	.	08	01		
IV	6.1	7.0	6.0	6.3	155.0	06.0	77	47	67	64	27	025	005.7	18	.	.	02	06	14	12	06	.	12	.	.	.	01	C2	01		
V	6.5	7.5	6.6	6.8	169.5	09.4	84	55	82	75	37	072	C17.5	23	.	.	04	01	13	21	12	02	21	.	.	.	06	02	.		
VI	5.5	7.6	7.6	7.6	180.1	11.7	94	63	76	74	44	197	057.3	30	.	.	10	01	.	.	.	01	10	15	13	05	15	.	.	.	1C	01	.		
VII	4.4	4.7	6.0	5.1	245.8	12.8	81	53	82	72	37	055	C19.0	22	.	.	17	05	.	.	.	07	07	08	06	02	06	.	.	.	02	C1	.		
VIII	4.6	4.5	4.4	4.2	247.5	14.8	88	55	85	76	38	076	C22.0	27	.	.	24	12	.	.	.	11	06	12	08	03	12	.	.	.	08	04	.		
IX	5.5	5.5	4.3	5.1	161.7	11.3	92	61	88	80	42	019	007.6	27	.	.	05	06	05	08	05	.	08	.	.	.	01	11	.		
X	7.8	6.2	7.3	7.8	070.5	06.9	94	76	91	87	54	156	032.7	29	.	.	02	02	18	21	17	05	21	.	.	.	01	10	.		
XI	5.6	6.3	6.2	6.0	065.3	05.8	94	71	90	85	47	050	C15.6	26	.	.	04	07	12	13	09	03	13	01	.	.	.	12	.		
XII	9.3	8.2	7.4	8.3	047.2	05.0	90	80	89	87	54	050	C014.5	19	.	02	15	01	22	18	11	01	17	05	03	01	.	11	.		
God.	6.6	6.7	5.9	6.4	1616.3	08.4	88	65	84	79	21	781	C07.3	30 VI	.	02	67	65	18	.	.	53	151	156	105	22	150	15	05	02	.	33	90	01	
CSIJEK																																			
BR. ST.73																																			
I	7.9	6.0	6.5	7.5	046.3	04.9	96	87	96	93	63	032	C12.3	20	.	.	22	02	18	10	05	01	69	03	.	01	.	C3	C1		
II	6.4	6.4	4.6	5.8	087.4	05.9	97	72	89	86	47	020	C06.6	24	.	.	11	04	06	12	05	.	10	01	.	.	.	02	.		
III	5.5	6.4	4.4	5.3	160.9	06.2	95	61	79	78	23	021	006.4	08	.	.	06	03	.	.	.	01	07	11	08	05	.	06	04	01	.	C1	0!		
IV	6.0	6.9	5.3	6.1	161.5	07.1	90	50	56	60	73	26	045	C14.0	16	.	.	01	01	.	.	.	06	12	14	08	.	14	.	.	.	01	.		
V	6.5	6.5	4.4	5.8	173.4	10.2	92	62	89	81	43	074	C12.0	23	.	.	05	01	05	09	22	13	02	22	.	.	C1	05	C1		
VI	5.1	7.0	5.6	5.9	194.4	12.5	90	65	86	80	48	157	C04.6	11	.	.	12	01	.	.	.	03	10	18	14	04	18	.	.	.	06	.			
VII	3.6	4.2	3.5	3.8	251.0	14.0	89	58	85	77	42	062	C02.2	20	.	.	19	09	.	.	.	12	04	11	09	02	11	.	.	.	04	.			
VIII	3.0	2.7	3.1	3.2	257.1	15.9</td																													

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Pm (0-12)																					
		Tm			Max.				Min.			Dat.				N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)	Max.	Min.	Max.	Dat.	Min.	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\psi = 44^{\circ}58'$ N $\lambda = 14^{\circ}24'$ E Gr. $\Delta G = + 58 \text{ min.}$															GRES												BR. ST.76						
I	-	05.1	11.1	05.2	06.6	12.6	03.0	14.0	22	-04.5	18	22	C1.2	19	C1.6	+	+	03	03.7	13	01.4	01	01.0	14	01.0	15	C1.2	06					
II	-	07.9	12.4	08.0	09.1	13.3	06.5	16.0	18	01.8	09.8	17	C1.5	22	02.8	+	+	09	03.2	27	03.1	05	01.6	02	01.0	04	C1.0	03					
III	-	07.4	14.2	07.4	09.1	14.8	06.5	19.8	31	02.8	01	39	C1.3	09	04.3	+	+	03	05.0	20	02.2	03	01.0	10	01.0	09	C1.3	.					
IV	-	11.9	15.8	11.6	12.7	16.6	08.1	21.0	09	03.8	08	38	C1.2	01	02.0	16	02.2	12	02.6	06	01.7	01	01.0	10	01.7	02							
V	-	12.9	20.1	13.7	15.1	21.7	16.3	27.0	21	05.2	11	14	C1.1	08	01.8	+	+	11	02.2	01	01.0	13	01.4	33	01.2	.							
VI	-	16.4	23.0	16.6	18.2	24.1	13.7	28.8	05	05.0	12	24	01.6	06	02.0	01	01.0	15	02.4	06	C2.0	08	03.4	10	01.4	.							
VII	-	20.9	28.2	21.6	23.1	28.5	17.1	37.4	29	13.6	10	08	01.4	13	02.4	C2	03.0	08	02.5	05	01.6	04	01.0	18	01.4	01							
VIII	-	23.7	30.2	23.9	25.4	31.3	19.3	-	-	-	04	01.2	25	02.0	02.5	03	03.0	+	+	06	01.3	35	01.4	11	C1.1	07							
IX	-	18.5	25.1	18.6	20.2	26.3	16.4	32.0	16	11.0	30	23	C1.2	12	01.7	+	+	20	02.3	06	02.7	01	02.0	12	01.4	16	01.2	.					
X	-	08.5	14.1	08.7	10.0	15.3	06.1	18.8	05	02.7	17	07	01.8	35	02.3	C4	C1.2	15	02.6	06	01.5	08	01.5	05	01.6	06	C1.3	02					
XI	-	08.3	13.4	08.7	09.8	14.1	06.6	17.5	17	03.0	29	01	C1.0	25	01.7	35	02.3	05	01.8	14	01.4	+	+	04	01.0	06	.						
XII	-	04.7	10.5	04.9	06.2	11.4	02.9	13.5	03	-00.5	16	01	02.0	18	01.2	+	+	03	02.0	+	10	01.3	25	01.4	36	01.5	.						
GOD.	-	12.2	18.2	12.4	13.8	19.2	09.7	-	-	-	160	C1.4	230	02.3	10	02.3	145	02.5	101	02.3	79	01.7	161	01.4	182	01.3	27						
$\psi = 44^{\circ}32'$ N $\lambda = 14^{\circ}28'$ E Gr. $\Delta G = + 58 \text{ min.}$															MALI LOSINJ												BR. ST.77						
I	761.6	08.5	10.4	08.7	09.1	11.3	07.4	15.4	20	05.7	26	14	C2.6	16	02.5	C4	C1.5	18	02.7	04	02.8	+	+	10	01.9	12	C2.0	15					
II	754.2	09.2	12.0	08.8	10.2	12.7	08.4	15.9	16	05.2	07	06	03.0	17	03.0	C5	C2.2	27	03.4	08	03.1	05	C2.2	04	02.8	04							
III	757.0	09.0	12.5	10.1	10.4	13.6	08.3	16.6	21	04.8	16	09	03.2	27	02.6	C7	C2.1	11	04.3	11	03.6	06	02.2	03	03.7	14	02.4	06					
IV	753.5	11.4	14.8	12.1	12.7	15.9	10.5	19.0	07.00	06.9	17	09	03.1	29	03.0	C5	02.6	18	04.0	10	03.2	04	02.2	09	02.8	03	01.7	03					
V	754.6	15.0	18.3	15.4	16.0	19.4	13.0	25.7	21	05.9	01	05	02.4	16	02.8	C4	C1.8	02	03.0	25	03.2	12	02.8	16	02.4	06	C2.4	03					
VI	755.1	18.9	21.9	18.7	19.6	23.0	16.6	26.0	05	11.5	11	08	C2.5	28	02.4	C7	C1.9	05	02.0	21	03.3	10	02.8	08	02.6	05	C2.2	02					
VII	756.7	22.3	26.6	22.7	23.6	27.7	20.1	32.5	16	17.5	26	08	02.6	21	03.1	C7	C2.1	05	02.4	20	03.2	09	01.9	09	03.2	03	C2.0	11					
VIII	756.4	23.4	28.1	24.2	24.9	29.2	21.3	34.6	05	15.1	11	11	C2.6	30	02.2	C9	01.9	04	02.2	05	02.8	11	02.3	10	02.4	04	C2.5	08					
IX	756.1	19.2	23.5	20.0	20.7	24.3	18.0	28.5	16	15.15	25	15	02.7	71	C2.1	C5	02.2	11	02.5	11	C2.1	12	03.0	06	02.7	03	C2.3	06					
X	753.0	12.0	14.3	12.4	12.8	15.6	10.8	20.0	04	06.5	72	14	C3.1	20	03.6	C3	C1.7	10	02.4	20	03.0	16	03.3	05	03.4	03	C2.0	02					
XI	758.2	11.6	13.5	12.0	12.3	14.3	10.5	18.0	16	07.6	01	05	02.8	14	01.9	C6	C2.5	33	02.8	12	03.1	C9	02.8	04	02.8	03	01.3	01					
XII	761.0	09.1	11.0	09.4	09.7	11.8	06.7	14.4	04.00	-05.3	04.3	11	03.2	14	04.3	C3	02.0	06	02.7	02	01.5	19	02.5	10	01.7	12	C1.9	15					
GOD.	756.5	14.4	17.2	14.6	15.2	18.2	12.6	34.6	05.00	-05.3	05.0	113	C2.9	254	03.0	65	02.1	150	03.0	150	03.1	116	02.7	97	02.5	74	C1.2	76					
$\psi = 44^{\circ}45'$ N $\lambda = 14^{\circ}46'$ E Gr. $\Delta G = + 59 \text{ min.}$															RAB												PE. ST.78						
I	764.2	07.3	11.1	08.1	08.7	12.2	05.9	20.3	20	02.6	15	17	C1.8	08	01.0	C2	C1.0	18	03.2	03	01.0	07	01.4	28	.	.	.						
II	755.5	05.2	12.5	05.7	10.3	13.3	07.7	16.2	20	03.7	28	08	01.4	13	02.8	C7	02.3	34	05.0	06	C2.3	05	01.6	01	01.0	02	C3.5	08					
III	755.6	08.7	13.6	10.2	10.7	14.4	07.4	20.6	21	02.4	01	09	01.6	15	02.3	C5	C1.8	16	04.2	03	01.0	11	01.2	04	01.5	26							
IV	754.7	11.7	14.2	12.4	13.0	16.7	10.7	21.1	06.3	06	17	15	04.4	08	02.4	C4	03.7	05	03.0	07	02.7	02	03.0	17	.								
V	757.4	15.0	19.1	15.8	16.4	20.1	12.6	27.8	21	05.0	01	13	C2.7	04	01.5	C4	01.7	21	01.2	09	02.2	07	01.3	01	01.0	11	01.5	23					
VI	757.1	16.7	20.5	17.9	19.7	23.7	15.8	27.6	30	10.2	11	06	C2.8	04	03.0	C7	01.7	21	02.9	08	02.1	11	02.0	05	01.6	26							
VII	759.1	21.3	26.0	22.4	23.2	27.7	19.9	31.7	30	15.4	26	03	C1.5	14	01.6	C7	02.9	12	03.0	11	02.5	11	01.0	02	03.5	25							
VIII	758.9	22.4	28.0	24.0	24.8	29.7	20.1	35.6	20	13.2	11	14	C1.4	05	02.2	C3	02.3	04	02.2	02	01.1	06	01.3	06	C1.3	38							
IX	758.7	18.3	23.9	19.5	20.3	24.5	18.8	29.6	16	10.8	26	10	01.5	07	02.0	C2	03.5	23	04.0	02	03.0	11	01.3	04	01.2	25							
X	755.7	10.7</																															

Měsíc	Oblačnost Nm (0-10)				Intenzita hoří sítí (Index)	Vlhkost vzduchu				Padavina mm				Broj dana na rok:																				
						%				mm				Trn	Tx	Trn	Tx	Trn	F(0-12)	Nm(0-10)	R mm	●	*	♦	▲	▲	▲	▲	▲	▲	▲			
	7	14	21	Sed.		7	14	21	%	mm	Max	Min	Σ	Trn	Tx	Trn	Tx	Trn	F(0-12)	Nm(0-10)	R mm	●	*	♦	▲	▲	▲	▲	▲	▲	▲			
BR. ST.76																																		
CRES																																		
I	5.7	6.0	6.0	5.9	-	05.6	77	65	79	74	35	082	C36.5	01	.	.	02	.	.	.	10	14	C8	07	02	06			
II	6.8	6.3	6.4	6.5	-	06.6	77	65	77	73	37	066	C23.0	06	01	.	06	14	C6	06	03	06			
III	5.5	5.7	5.6	5.6	-	05.2	57	55	56	56	19	051	C30.2	05	09	12	03	02	02	03				
IV	5.6	5.6	5.5	5.6	-	04.9	63	57	63	61	30	102	C37.1	13	02	01	08	11	07	06	05	07	.	.	.	01	.			
V	4.6	4.6	5.1	4.8	-	08.2	63	60	63	62	29	115	C39.5	01	.	.	04	.	.	.	09	09	09	09	05	05	C5		
VI	5.6	5.8	5.6	5.7	-	09.3	62	53	60	58	21	093	C23.6	11	.	.	12	.	.	.	C5	C9	06	07	05	08	02	.		
VII	2.5	2.1	2.2	2.3	-	11.5	57	44	59	53	15	132	C14.3	26	.	.	29	09	05	.	21	C2	03	03	02	03	02	.		
VIII	1.7	2.3	2.0	2.3	-	13.3	57	49	54	54	-	031	C12.4	09	17	01	04	03	02	04	05	.			
IX	3.5	3.6	4.1	3.7	-	11.5	68	55	69	64	34	155	C34.6	30	.	.	22	04	.	.	12	C6	09	09	06	05	01	02	.	
X	7.6	7.7	8.1	7.8	-	07.0	79	67	77	74	23	262	C0.0	09	01	.	04	20	19	19	13	19	07	.		
XI	6.6	6.9	6.5	6.7	-	06.9	74	71	76	73	42	670	C26.4	26	04	14	05	05	03	05			
XII	4.8	5.5	5.5	5.3	-	05.3	74	67	74	71	47	028	C14.2	12	.	.	03	.	.	.	09	13	03	03	02	03		
GOD.	5.0	5.2	5.3	5.2	-	08.1	67	58	67	64	-	1107	C27.1	45W	-	-	-	-	-	04	01	114	123	84	79	50	84	.	.	.	01	20	.	
BR. ST.77																																		
MALI LOSINJ																																		
I	6.5	7.0	4.6	6.0	-	104.1	07.0	82	15	84	52	072	C20.6	07	01	.	04	C8	11	10	03	11	04	.		
II	6.9	6.8	4.0	5.9	-	120.1	07.0	78	65	77	35	071	C16.9	05	04	.	04	C5	12	08	02	11	03	.		
III	5.5	6.1	4.5	5.5	-	167.5	07.5	80	65	80	25	064	C23.5	05	04	.	06	10	07	04	03	05	.	.	.	01	02	.		
IV	6.3	6.0	5.2	5.8	-	187.9	07.5	73	57	69	24	080	C47.7	26	06	.	05	C9	06	09	04	05	.	.	.	01	02	.		
V	5.6	5.2	5.0	5.3	-	276.0	09.8	77	62	75	34	127	C34.2	25	.	.	01	.	01	.	C4	C8	14	11	04	14	07	.		
VI	5.6	5.3	4.5	5.1	-	275.5	12.4	74	63	77	29	094	C20.7	11	.	.	04	01	.	.	C6	C4	12	09	04	12	.	.	.	06	.	.		
VII	2.5	2.3	2.5	2.4	-	167.0	07.5	74	62	75	26	024	C10.6	06	.	.	.	27	06	14	02	16	C1	05	05	06	.	.	03	.	.	.		
VIII	2.0	3.0	1.8	2.5	-	336.0	15.3	74	52	68	24	054	C14.3	12	.	.	29	12	23	01	16	01	17	07	02	07	.	.	.	07	.	.		
IX	4.8	4.9	5.5	4.1	-	242.9	13.4	80	60	77	22	209	C66.6	21	.	.	15	.	06	02	12	C6	15	15	07	15	.	.	.	01	05	.		
X	7.3	7.7	5.7	6.9	-	117.0	07.8	74	65	70	37	222	C33.5	02	C5	.	01	12	18	14	08	18	.	.	.	01	01	IC		
XI	8.0	7.4	5.6	7.0	-	094.5	09.1	79	65	76	39	124	C21.4	07	C5	.	01	11	14	13	06	14	.	.	.	03	.	.		
XII	5.1	6.0	4.6	5.0	-	108.2	07.7	78	68	75	40	021	C05.1	31	.	.	02	.	.	.	C5	07	08	07	01	07	.	.	.	01	.	.		
GOD.	5.6	5.7	4.2	5.1	-	2408.6	09.6	77	62	74	24	1179	C66.5	29X	.	.	88	22	31	74	33	79	96	141	109	45	140	.	.	.	03	02	53	03
BR. ST.78																																		
RAD																																		
I	6.6	7.4	4.2	6.6	-	111.7	06.7	63	71	81	46	061	C17.8	01	01	.	04	C8	11	10	03	11	04	.		
II	7.4	7.4	4.6	6.2	-	125.6	05.5	73	62	69	31	079	C24.5	07	C5	04	02	10	10	10	03	10	.	.	.	04	.			
III	6.1	6.1	5.2	5.0	-	172.0	06.8	74	62	72	24	024	C10.6	02	04	01	05	C8	06	03	01	C5	.	.	.	02	.	.		
IV	6.0	5.9	4.4	5.4	-	157.6	07.1	68	57	63	25	098	C26.4	26	05	04	06	10	06	05	10	.	.	.	04	.	.			
V	5.6	5.4	5.4	5.7	-	158.6	09.9	72	67	73	36	052	C94.9	01	.	.	02	.	05	01	05	C9	13	10	04	12	.	.	.	07	.	.		
VI	6.2	5.9	5.0	5.8	-	243.6	12.4	74	63	73	34	105	C24.0	20	.	.	06	01	C6	04	05	C8	15	12	04	15	.	.	.	13	.	.		
VII	3.3	2.8	2.8	2.8	-	148.0	13.2	69	52	62	35	060	C44.4	26	.	.	30	06	09	05	02	14	C2	07	05	02	07	.	.	.	04	.	.	
VIII	3.0	2.7	2.6	2.6	-	320.9	15.0	70	52	64	33	054	C24.5	17	.	.	30	16	19	04	02	16	C1	06	04	02	06	.	.	01	02	.		

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Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																	
		Tm			Max		Min		Dat.		N		NE		E		SE		S		SW		W		NW				
		7	14	21	Sred. (Dnev.)	Max	Min	Max	Dat.	Min	Dat.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.				
$\varphi = 44^{\circ}27'$ N $\lambda = 15^{\circ}04'$ E Gr. $\Delta G = + 1h\ 00\ min.$																													
I	-	06.7	11.0	08.1	06.5	11.6	05.3	15.4	28	06.6	15	12	C1.0	C6	C1.0	C6	C1.0	C6	C1.0	C6	C1.0	C6	C1.0	C6	C1.0				
II	-	09.3	12.2	09.7	10.2	12.7	07.4	16.3	16.17	03.4	09	15	C0.2	C14	C0.4	C2	C1.0	C20	C2.8	C22	C2.6	*	02	01.5	09	C1.4			
III	-	08.7	13.7	10.9	11.0	14.3	07.6	20.8	26	04.8	01	18	C2.7	C1	C1.1	C6	C1.2	C17	C2.2	C11	C3.1	C4	C1.5	C3	C1.0	C1.4			
IV	-	12.4	15.2	12.8	13.3	16.5	09.8	20.8	30	05.7	21	19	C3.4	C15	C3.6	C6	C1.2	C17	C2.4	C13	C2.8	C2	C1.0	C5	C2.0	C1.5			
V	-	16.0	19.8	16.7	17.3	20.7	13.4	24.5	21	05.8	10	19	C1.7	C6	C0.2	C5	C1.0	C16	C1.9	C14	C2.1	C3	C0.9	C19	C1.6	*			
VI	-	19.6	23.5	19.9	20.7	24.4	15.9	28.1	05	11.7	11	14	C2.4	C6	C0.2	C1	C1.0	C19	C1.9	C14	C1.8	C8	C0.4	C19	C1.8	*			
VII	-	22.7	27.5	23.4	24.3	28.5	19.4	34.6	16	15.5	27	19	C2.3	C10	C0.3	C8	C1.4	C17	C1.8	C13	C1.9	C7	C1.9	C8	C1.6	C1.4			
VIII	-	23.9	29.0	24.8	25.5	30.2	20.5	36.4	20	13.5	11	20	C0.1	C9	C0.6	C12	C1.0	C11	C1.5	C8	C0.8	C4	C1.2	C6	C0.3	C25	C1.7		
IX	-	18.7	24.3	20.4	20.9	25.1	16.9	26.7	16	10.5	27	14	C1.9	C6	C0.7	C3	C1.2	C15	C1.6	C12	C2.2	C2	C1.5	C8	C1.6	C1.5	*		
X	-	10.9	14.1	11.4	11.9	15.0	08.8	19.0	04	03.8	31	19	C0.5	C13	C0.8	C5	C1.0	C19	C2.1	C17	C2.1	C3	C1.3	C10	C1.4	C9	C1.3		
XI	-	10.1	13.5	10.5	11.2	14.5	05.1	18.0	07	01.7	02	10	C0.1	C6	C0.4	C1	C1.0	C20	C1.8	C10	C1.9	C1	C1.0	C6	C0.8	C1.8	*		
XII	-	06.4	11.0	07.6	08.2	12.7	04.3	18.7	06	06.5	22	10	C0.1	C8	C0.5	C3	C1.0	C17	C1.5	C13	C1.5	C2	C1.0	C4	C1.0	C1.8	C1.4		
GOD.	-	13.7	17.9	14.7	15.2	18.9	11.5	36.4	00	00	29	00	196	C2.5	C111	C0.3	C8	C1.1	C17	C2.0	C178	C0.2	C1	C35	C1.5	C68	C1.5	C207	C1.5
$\varphi = 44^{\circ}08'$ N $\lambda = 15^{\circ}13'$ E Gr. $\Delta G = + 1h\ 01\ min.$																													
ZADAR													ZADAR																
BR. ST.R2																													
I	765.5	07.1	11.1	08.1	08.6	11.5	06.6	15.9	21	01.0	15	07	C3.0	C4	C1.7	C11	C1.7	C24	C1.8	C6	C1.3	*	03	C2.3	C17	C2.5	29		
II	756.5	08.2	12.7	09.4	09.9	13.5	06.5	16.6	18	02.1	28	02	C1.5	C10	C2.3	C17	C2.0	C30	C2.7	C6	C3.0	*	02	C2.5	C7	C2.3	10		
III	760.9	07.9	13.3	10.0	10.3	14.0	06.9	18.1	26	02.0	12.01	03	C2.3	C6	C0.5	C13	C1.9	C10	C3.5	C9	C2.8	*	01	C0.6	C19	C2.7	34		
IV	757.5	11.2	15.1	12.2	12.7	16.7	04.1	20.9	06	06.2	20.19	02	C0.1	C8	C0.7	C17	C2.7	C25	C0.5	C3	C0.2	C0	14	C2.4	C15	*			
V	758.7	15.3	18.8	15.8	16.4	19.8	14.4	24.5	21	05.5	10	01	C1.0	C5	C0.7	C0	C1.6	C11	C1.9	C16	C2.2	*	01	C0.2	C29	C2.6	25		
VI	759.1	19.5	23.0	19.6	20.4	24.0	16.0	27.4	20	10.4	13	06	C0.2	*	*	C3	C0.0	C21	C1.5	C1.7	*	06	C0.2	C17	C2.9	22			
VII	760.5	22.1	26.5	23.4	27.4	28.6	18.6	32.3	17	14.7	21	01	*	*	C3	C0.0	C2	C1.5	C13	C1.8	C7	*	06	C0.0	C22	C2.4	40		
VIII	760.1	22.3	27.7	23.3	24.2	28.9	18.5	32.7	17	14.0	12	05	C2.6	C2	C0.5	C15	C1.9	C09	C1.9	*	03	C0.3	C19	C2.2	38				
IX	760.0	18.0	23.8	19.8	20.3	24.5	16.5	28.1	15.04	11.0	26	02	C2.3	C5	C0.2	C21	C11	C1.6	C15	C1.5	C9	*	03	C1.1	C18	C2.6	26		
X	757.4	10.6	15.1	11.6	12.2	16.2	08.9	20.3	04	04.1	31	19	C0.7	C1.6	C0.5	C27	C1.4	C22	C1.9	C9	C2.8	*	07	C0.4	C17	C2.7	16		
XI	762.2	09.6	14.0	10.8	11.3	15.1	08.2	17.6	11	02.3	02	05	C1.4	C7	C1.9	C29	C1.5	C24	C2.2	C4	C2.2	*	02.0	C0	C1.5	C12	32		
XII	764.8	07.5	11.8	08.4	09.0	12.5	05.8	15.3	02	02.0	15.13	06	C3.7	C6	C0.3	C67	C1.9	C21	C1.5	C8	C0.8	C1	01.0	C4	C0.9	C2.6	31		
GOD.	760.0	14.3	17.7	14.3	14.9	18.7	11.2	32.7	07	00	19.0	01.0	C1.0	C1.0	C1.0	C70	C0.2	C129	C1.7	C25	C2.8	C0.5	C29	C1.5	C2.5	298			
$\varphi = 41^{\circ}48'$ N $\lambda = 15^{\circ}19'$ E Gr. $\Delta G = + 1h\ 01\ min.$																													
LICKE LESTCE													LICKE LESTCE																
BR. ST.R3																													
I	-00.7	03.3	00.2	00.7	03.6	-01.9	15.5	20	-05.8	22	15	C1.1	C1	C1.0	C4	C1.0	C7	C1.7	C11	C1.1	C6	C1.0	C3	C1.3	C1				
II	-03.7	07.7	04.3	05.0	06.7	01.5	14.3	12	-04.2	08	15	C2.2	C6	C1.8	C1	C1.0	C6	C2.8	C16	C2.9	C8	C2.2	C1	C1.7	C11				
III	-02.6	10.7	05.5	06.1	11.5	01.1	23.4	22	-04.8	14	21	C1.8	C6	C1.8	C2	C1.0	C9	C1.2	C7	C1.6	C4	C2.0	C2	C1.5	C18				
IV	-05.4	11.7	07.6	07.6	07.6	01.8	18.6	27	-03.1	20	18	C0.0	C11	C0.1	C7	C1.4	C9	C2.0	C6	C0.4	C1.0	C16	*	16	C1.5	*			
V	-	10.0	17.4	10.2	11.9	18.4	05.9	24.4	30	-01.4	10	19	C1.6	C6	C1.7	C7	*	*	C0.4	C1.4	C7	C0.6	C2.2	C2	C1.5	29			
VI	-	13.4	20.3	12.9	14.9	21.3	06.1	27.2	04	03.0	13	11	C0.5	C5	C0.2	C1	C1.0	C12	C2.2	C10	C2.7	C3	C1.3	C18	C28				
VII	-	15.4	24.8	15.4	17.7	25.6	10.3	31.0	30	05.1	27	12	C1.6	C6	C1.8	C2	C1.0	C9	C2.1	C7	C1.9	C2	C1.2	C26					
VIII	-	15.0	25.7	15.7	18.0	26.6	11.6	33.0	16	04.4	12	11	C2.0	C6	C1.5	C1	C1.0	C20	C0.3	C1.3	C1	C1.0	C18	C49					
IX	-	12.0	20.4	12.9	14.6	21.4	05.2	26.8	03	01.1	28	09	C1.7	C6	C1.8	*	*	*	C0.4										

Mjesec	Oblačnost Nm (0-10)			Insolacija broj sati Sred. (Dnev.)	Vlažnost vazduha			Padavine mm			Broj dana na se												•	*	*	Δ	Δ	▲	▲	T	III	II				
					em			Um R			Tn Tx Tn Tx Tn Tx F(0-12)			Nm(0-10)			R mm			•	*	*	Δ	Δ	▲	▲	T	III	II							
	7	14	21					7	14	21	Tn	Max	Min	7	14	21	Tn	Max	Min	7	14	21	Tn	Max	Min	7	14	21	Tn	Max	Min					
PAG																													$H_s = 3 \text{ m } H_b = - \text{ m } h_i = 2.0 \text{ m } h_t = 1.0 \text{ m}$							
I	6.6	6.5	4.4	5.9	086.6	06.3	80	68	78	75	36	095	C28.1	07	•	•	•	•	•	•	06	13	12	05	04	12	•	•	•	•	03	•				
II	7.8	6.2	4.6	6.2	087.3	06.5	71	63	71	68	39	095	C19.7	05	•	•	•	•	•	03	10	10	10	05	10	•	•	•	•	02	•					
III	5.7	5.4	5.1	5.4	162.0	06.7	74	56	69	66	29	055	C24.3	05	•	•	•	•	•	01	09	09	08	04	02	07	•	•	•	•	02	•				
IV	6.3	5.9	4.9	5.7	166.5	06.6	58	54	61	58	23	096	C27.7	26	•	•	•	•	•	05	08	12	09	08	04	05	•	•	•	•	04	•				
V	5.7	5.1	4.4	5.7	245.3	05.8	69	58	70	66	35	109	C46.6	01	•	•	•	01	•	•	06	08	11	05	04	11	•	•	•	•	06	•				
VI	4.7	4.8	5.1	5.9	258.6	11.9	69	56	64	56	36	084	C33.5	11	•	•	•	14	•	01	07	08	14	09	02	14	•	•	•	•	06	•				
VII	2.5	2.4	2.1	2.3	315.1	13.1	62	47	51	57	34	022	C00.6	16	•	•	•	27	10	12	01	17	01	04	04	•	•	•	•	05	•					
VIII	2.4	2.5	2.0	2.3	320.8	15.3	71	51	55	52	34	098	C26.6	10	•	•	•	29	15	17	•	18	02	08	07	05	08	•	•	•	•	06	01			
IX	5.7	5.3	3.7	3.9	326.3	13.1	75	64	74	70	34	154	C68.0	30	•	•	•	18	•	02	•	14	05	12	10	08	14	•	•	•	•	09	•			
X	7.6	7.4	6.3	7.1	108.5	07.6	76	62	71	71	27	071	C42.0	21	•	•	•	•	•	02	02	13	13	10	11	22	•	•	•	•	02	•				
XI	6.0	6.9	5.3	6.7	064.9	07.5	76	67	76	73	41	132	C30.6	27	•	•	•	•	•	02	03	12	11	10	05	11	•	•	•	•	04	•				
XII	6.4	5.2	5.0	5.5	081.5	06.3	82	66	79	76	38	030	C11.0	19	•	•	•	02	•	•	03	01	07	11	08	05	01	•	•	•	•	01	03			
GOD.	5.7	5.2	4.5	5.1	2165.8	05.2	72	58	70	67	23	1408	C42.0	218	•	•	•	02	05	25	32	12	01	09	104	127	103	52	127	•	•	•	•	03	54	06
ZADAR																													$H_s = 5 \text{ m } H_b = 7.3 \text{ m } h_i = 2.0 \text{ m } h_t = 1.0 \text{ m}$							
I	6.9	6.9	4.2	6.0	108.1	06.6	82	74	83	79	37	117	C33.1	07	•	•	•	•	•	05	10	09	04	05	•	•	•	•	•	•	•	•	•	•		
II	6.9	6.6	4.1	5.9	136.1	06.7	78	63	75	72	39	063	C16.6	05	•	•	•	09	•	02	02	07	11	00	02	11	•	•	•	•	03	•	•			
III	5.3	5.5	3.5	4.9	179.9	07.2	72	69	70	75	27	071	C28.7	05	•	•	•	•	01	01	06	06	07	05	02	07	•	•	•	•	01	06	•			
IV	6.4	6.2	5.5	5.4	175.1	07.5	65	63	70	67	27	075	C15.0	16	•	•	•	03	•	06	05	11	07	02	11	•	•	•	•	01	02	•				
V	5.7	5.2	4.5	5.0	276.7	10.7	79	66	79	75	41	124	C49.6	20	•	•	•	05	•	07	10	06	04	10	•	•	•	•	05	•	•					
VI	4.1	4.1	4.0	5.3	277.9	12.9	75	62	76	71	23	084	C14.7	11	•	•	05	01	•	04	05	07	06	03	07	•	•	•	•	06	•	•				
VII	5.4	5.5	4.7	5.7	316.1	14.3	68	56	72	65	34	034	C16.4	20	•	•	•	24	04	02	01	15	01	05	04	01	05	•	•	•	•	04	•	•		
VIII	5.7	5.0	4.7	5.2	315.7	16.6	77	61	76	72	35	041	C13.4	29	•	•	•	30	11	18	•	18	04	09	09	02	05	•	•	•	•	09	02	•		
IX	5.3	4.4	3.1	3.8	238.4	13.5	82	63	79	75	40	113	C26.4	16	•	•	18	02	01	•	17	05	12	10	04	12	•	•	•	•	05	•	•			
X	7.2	6.7	5.2	6.4	128.6	08.1	81	64	78	74	35	340	C104.3	06	•	•	•	01	•	03	10	26	17	09	20	•	•	•	•	01	10	•				
XI	7.5	7.2	4.2	6.4	110.7	07.6	80	65	78	76	42	086	C30.0	26	•	•	•	•	•	02	05	15	11	12	05	15	•	•	•	•	03	•	•			
XII	7.3	5.1	3.4	4.6	113.9	06.7	80	67	79	76	37	039	C21.7	29	•	•	•	•	01	•	04	07	05	01	07	•	•	•	•	01	01	•				
GOD.	5.4	5.4	3.7	4.9	2422.6	09.9	77	64	77	73	22	1186	C106.3	06	•	•	86	15	28	11	•	91	75	123	99	39	123	•	•	•	•	02	44	09		
LICKO LESCE																													$H_s = 463 \text{ m } H_b = - \text{ m } h_i = 2.0 \text{ m } h_t = 2.0 \text{ m}$							
I	8.6	7.7	7.0	7.8	-	04.2	87	79	87	F4	44	050	C24.4	01	•	02	27	•	•	•	02	18	12	07	01	11	06	C1	01	01	01	11	06	•		
II	8.1	7.8	7.5	7.8	-	05.0	80	73	75	T5	26	098	C29.4	07	•	•	09	•	02	01	16	17	06	14	06	01	01	01	01	01	02	02				
III	7.9	6.6	6.7	7.1	-	05.1	83	57	78	T3	26	051	C17.5	05	•	•	14	•	•	•	12	07	06	01	04	06	•	•	•	•	02	05	•			
IV	5.8	7.0	5.6	6.4	-	05.3	77	54	72	68	28	124	C45.2	26	•	•	11	•	•	05	11	17	11	04	16	04	03	•	•	•	•	01	01	01		
V	6.4	5.5	5.8	6.3	-	07.7	81	54	72	18	138	C11.7	1	•	•	01	•	•	01	11	15	10	05	15	•	•	•	•	03	05	•					
VI	6.2	5.2	4.6	5.7	-	09.4	80	55	83	26	118	C31.1	10	•	•	03	•	02	02	04	04	13	10	06	05	13	•	•	•	•	04	07	•			
VII	5.1	3.5	2.5	3.7	-	11.4	83	51	87	73	35	048	C19.3	26	•	•	20	05	•	01	05	03	06	05	02	06	•	•	•	•	01	04	06			
VIII	5.1	4.5	2.7	3.9	-	12.6	93	53	92	21	102	C20.3	24	•	•	20	09	•	•	02	07	1														

Mesec	Vadudni Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра nD, Fm (0-12)																		
		Tm										KNAJ																		
		7	14	21	Std. (Gies)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C	8.	9.	8.	9.	8.	9.				
$\psi = 44^{\circ}02'$ N $\lambda = 16^{\circ}12'$ E Gm, $\Delta G = +1h\,05\text{ min}$																									BR. ST. 86					
I	744.4	64.1	65.9	64.8	65.4	11.1	01.1	16.5	20	-03.6	15	31	65.0	02	01.6	06	01.7	03	02.0	02	01.0	03	01.7	34						
II	737.5	66.1	11.1	66.8	67.7	12.0	04.4	44.6	20	-02.3	09	33	64.0	04	03.0	03	02.3	07	02.4	16	02.4	*	02	01.0	03	C2.0				
III	736.7	65.6	15.2	68.9	69.6	16.0	04.6	25.6	22	-02.3	01	24	62.8	05	01.8	01	00.4	02.8	11	02.3	06	02.2	06	01.5	05	C2.2				
IV	736.4	66.2	14.9	16.4	11.1	16.4	06.5	21.6	09	06.3	21	42	63.0	03	02.7	04	02.5	08	03.0	13	02.3	02	02.0	03	01.7	02	01.5			
V	737.8	12.7	20.3	14.7	15.6	21.4	05.6	28.6	20	06.2	11	24	62.1	05	02.4	07	01.6	04	01.8	10	02.2	08	01.9	04	01.5	03	C1.7			
VI	738.4	16.5	23.7	17.9	19.0	24.6	13.4	31.0	04	06.5	13	23	62.5	06	02.5	10	01.8	03	01.6	14	02.4	02	01.5	02	02.3	05	C3.2			
VII	740.3	18.6	26.2	20.6	22.1	25.2	14.8	35.7	31	06.6	04	36	63.7	01	01.0	02	02.0	10	01.8	03	02.0	11	01.5	06	01.2	29				
VIII	740.0	19.3	29.2	21.6	23.1	31.4	16.1	36.7	16.0	03.0	12	31	61.8	02	01.0	04	01.0	05	01.6	02	01.5	09	02.1	03	01.0	05				
IX	735.7	14.8	24.4	17.0	19.3	25.5	12.4	31.1	15	05.8	28	45	67.1	02	01.0	05	02.0	06	01.8	07	01.0	05	01.6	04	01.8	24				
X	736.5	04.8	12.5	07.6	08.6	14.2	04.7	18.5	04	-01.4	31	50	63.3	07	01.1	03	01.3	04	03.0	11	02.4	01	02.0	05	01.2	04	C2.0			
XI	741.5	05.7	1.1	7.3	09.4	13.6	04.1	20.1	17	-02.5	02	23	61.7	06	01.3	08	02.1	*	18	01.7	01	01.0	02	01.0	01	01.0	31			
XII	741.5	01.6	6.9	04.0	04.6	10.2	00.1	16.4	04	-06.2	23	30	63.4	01	01.1	06	01.5	04	01.0	11	02.0	01	01.0	01	01.0	01	01.0			
GDU	735.6	66.6	17.6	11.8	12.6	16.8	07.7	36.7	K63VW	-06.2	23	72	61.6	42	02.1	57	01.7	48	02.1	131	02.0	32	01.9	53	01.6	40	01.9	320		
$\psi = 43^{\circ}44'$ N $\lambda = 15^{\circ}55'$ E Gm, $\Delta G = +1h\,01\text{ min}$																									SIBERIK					
																										BR. ST. 87				
I	755.2	06.8	11.5	06.1	08.6	12.7	04.5	15.4	20	00.6	15	17	62.9	17	01.9	08	02.5	*	*	*	*	01	02.0	03	01.7	37				
II	755.1	08.6	12.7	09.3	10.0	13.8	06.0	17.6	18	01.7	09	08	64.0	18	04.1	03	02.2	26	03.7	05	04.6	01	02.0	02	02.0	17				
III	755.2	08.7	14.3	10.5	15.5	07.0	21.7	26	02.4	13.0	17	62.7	19	03.7	03	04.0	17	03.4	02	03.5	06	01.8	07	01.4	05	02.8	27			
IV	755.9	11.7	15.7	11.7	12.6	17.2	05.3	21.0	06	05.7	21	16	64.0	10	03.0	19	02.5	*	*	*	*	09	02.8	04	02.0	05				
V	751.6	15.6	21.1	16.2	17.0	21.5	12.5	27.7	21	05.0	15	15	67.0	10	02.7	03	02.3	06	04.0	07	02.6	12	02.8	05	02.6	26				
VI	752.6	19.7	24.0	20.0	20.9	25.2	16.3	25.7	26	10.6	11	18	63.6	05	02.0	10	03.3	06	02.8	10	02.0	07	02.4	03	03.3	26				
VII	752.4	22.5	27.2	23.2	24.1	28.6	19.3	36.0	16	14.1	20	15	61.7	10	02.8	01	02.5	02	02.5	06	03.3	16	01.6	*	35					
VIII	752.4	23.4	28.8	24.4	25.2	30.4	20.4	36.6	01	12.5	12	14	61.4	11	01.6	17	01.0	02	01.6	10	02.0	14	01.0	03	02.0	29				
IX	752.8	16.8	24.0	20.0	20.7	25.4	16.4	25.0	16.0	10.4	20	19	61.2	07	01.1	10	01.4	11	01.5	06	02.7	07	01.0	02	01.7	45				
X	751.0	16.8	14.3	11.1	11.7	16.0	06.3	21.6	15	04.0	28	11	63.4	10	02.2	11	03.4	01	01.0	02	02.5	04	01.0	04	01.0	26				
XI	754.0	05.9	14.3	10.7	11.4	15.1	05.1	18.5	17	03.1	02	12	64.1	08	05.1	03	02.7	27	02.6	02	03.0	04	01.0	01	01.0	25				
XII	754.4	06.5	11.2	07.8	08.7	12.0	04.0	17.4	03	18.5	12	16	61.8	12	04.5	04	02.7	*	*	01	01.0	*	*	01	01.0	54				
GDU	754.1	13.5	18.2	14.4	15.1	19.5	11.4	36.0	05.0	00.6	16	171	61.2	100	03.8	06	02.2	150	03.2	37	03.5	53	02.2	02	01.1	34				
$\psi = 43^{\circ}04'$ N $\lambda = 16^{\circ}05'$ E Gm, $\Delta G = +1h\,01\text{ min}$																									RUMIJA					
																										BR. ST. 88				
I	-	06.8	12.0	04.7	10.5	13.7	06.7	16.6	20	03.1	24	16	61.7	01	01.9	21	02.2	26	02.4	04	01.9	*	*	*	01.0	14	02.4	05		
II	-	14.0	19.7	16.9	11.6	14.2	04.7	19.5	18	01.7	09	05	63.3	10	01.7	11	03.0	25	03.7	10	02.8	05	03.4	05	02.0	04	02.5	03		
III	-	11.2	14.5	11.1	11.5	15.3	07.5	18.9	21	02.2	08	01	63.1	07	01.5	04	03.5	30	03.4	04	02.5	*	*	*	01.9	20	02.4	14		
IV	-	11.0	16.2	11.6	13.6	16.7	04.9	19.7	04	02.6	19	11	61.8	10	01.4	10	03.5	20	03.6	04	02.5	*	*	*	01.6	09	02.0	05		
V	-	11.9	19.2	15.6	17.1	20.6	12.5	26.4	22	08.6	10	11	62.0	06	02.0	08	02.0	28	03.1	04	01.2	02	01.5	04	02.4	07	02.3	07		
VI	-	20.4	24.1	18.5	24.6	24.6	15.4	25.4	26	11.6	12	11	61.5	07	01.4	07	02.2	28	03.1	04	01.2	02	01.5	04	02.4	07	02.3	09		
VII	-	24.4	27.0	21.6	24.6	24.6	16.0	33.4	17	15.2	24	21	63.6	03	01.0	10	02.0	28	03.4	04	01.0	02	01.5	04	02.4	07	02.3	10		
VIII	-	24.5	26.1	21.4	25.5	25.5	16.2	33.2	06	16.1	12	10	61.7	07	01.4	10	02.5	28	03.1	04	01.0	02	01.5	04	02.4	07	02.3	11		
IX	-	11.4	22.3	14.6	17.6	21.6	06.7	25.5	16	12.6	26	05	61.1	07	01.2	07	03.4	26	03.5	04	01.5	03	02.0	05	01.8	01	01.0	12		
X	-	15.2	17.2	11.7	14.4	17.8	10.6	23.0	21	04.0	20	15	61.6	07	01.2	05	02.4	17	02.4	17	02.6	02	03.0	04	02.0	05	01.8	01	01.0	14
XI	-	11.7	19.5	11.4	12.8	16.1	05.6	17.6	15	04.6	30	05	61.4	07	01.2	05	02.4	17	02.4	17	02.6	02	03.0	04	02.0	05	01.8	01	01.0	15
XII	-	08.4	13.6	08.5	09.4	14.1	05.5	16.3	04	01.8	37	15	61.6	07	05.0	02	01.0	07	02.4	05	01.8	02	01.0	07	01.4	03	01.9	05		
GDU	-	15.4	19.2	14.0	18.8	11.7	35.2	06.0	02.2	15.1	93	01.2	25.9	02.9	14.9	02.7	22.0	03.6	72	02.4	14.3	02.0	49	02.0	57	01.7	09			
$\psi = 43^{\circ}31'$ N $\lambda = 16^{\circ}26'$ E Gm, $\Delta G = +1h\,06\text{ min}$																									SPLIT-MARJAN					
																										BR. ST. 89				
I	754.5	06.0	11.0	09.3	09.4	11.7	06.8	17.6	20	03.2	15	22	61.9	19	02.2	15	02.6	11	02.4	08	01.2	05	01.4	05	01.4	05				
II	747.6	06.9	12.0	10.0	10.3	13.0	06.0	16.6	20	04.0	20	24	62.0	06	03.0	12	03.2	26	04.5	06	02.2	03	01.0	03	02.0	05				
III	747.0	05.9	14.4	11.4	11.8	15.1	09.0	16.6	21	04.0	03	25	61.3	05	01.9	11	02.9	27	04.1	06	02.0	03	01.7	03						

Mjesec Z.	Oblačnost Nm (0-10)			Isolacijski Ljetni sati (dnev.)	Vlažnost vazduha			Padavine R mm		Br. n. j. d. a. n. s. a:																			
	e mm	m mm	t mm		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	★	●	★	▲	▲	▲	▲	▲	▲	▲					
	7	14	21	Sec. Sred. (dnev.)	7	14	21	Sec. Sred. (dnev.)	Hm	Mx	Dat.	10.00.0	0.0250	0.020.0	6	8	2.0	8.0	0.1	1.0	10.0	●	★	●	★	▲	▲	▲	▲
KNIK																													
BR. ST. 86																													
I 5.9 6.7 4.2 5.6	122.7	04.5	89 56 77 74 29	086 C23.0	02	•	•	11	•	•	•	•	•	•	C7	11	12	05	04	12	•	•	•	•	•	•	01	01	
II 7.0 7.5 4.8 6.7	113.6	05.5	74 56 75 69 23	092 C30.1	07	•	•	02	•	•	•	02	•	•	01	10	11	04	04	11	•	•	•	•	•	•	02	•	
III 5.7 6.5 4.1 5.4	103.9	05.5	76 43 70 63 14	062 C23.0	06	•	•	03	02	•	•	C1	•	•	C5	07	06	02	07	15	•	•	•	•	•	•	03	•	
IV 6.2 7.6 5.4 6.4	102.6	05.9	65 48 66 59 19	072 C22.1	13	•	•	•	•	•	•	03	•	•	03	12	13	04	03	13	•	•	•	•	•	•	04	•	
V 6.7 6.5 4.2 5.8	227.9	08.2	77 45 71 64 23	098 024.9	01	•	•	07	•	•	•	•	•	•	C3	05	37	13	05	17	•	•	•	•	•	•	07	•	
VI 5.4 6.9 5.1 5.9	236.7	10.3	74 46 68 63 28	171 041.6	11	•	•	15	01	01	•	•	•	•	C8	10	15	13	05	15	•	•	•	•	•	•	01	01	
VII 5.4 4.3 2.6 3.5	343.8	11.0	70 38 61 56 20	023 020.3	20	•	•	24	16	•	•	•	•	•	C10	C3	03	02	01	03	•	•	•	•	•	•	02	•	
VIII 3.2 5.3 2.3 3.6	318.9	12.5	75 43 66 61 18	052 012.7	28	•	•	30	18	01	•	•	•	•	C12	C3	09	08	02	05	•	•	•	•	•	•	11	•	
IX 4.5 5.5 2.5 4.4	223.9	11.1	86 50 79 72 21	264 058.1	25	•	•	17	06	•	•	•	•	•	C13	C8	17	10	06	11	•	•	•	•	•	•	07	02	
X 7.2 7.7 6.1 7.0	121.4	06.7	86 64 86 78 26	316 C78.0	06	•	•	01	•	•	•	02	•	•	C2	14	21	19	09	21	•	•	•	•	•	•	05	C3	
XI 6.9 7.2 5.1 6.4	126.2	06.2	83 57 80 74 30	072 C22.6	26	•	•	04	•	•	•	•	•	•	C1	13	11	06	03	11	•	•	•	•	•	•	02	01	
XII 5.6 5.8 5.2 5.9	127.7	04.7	89 60 77 73 30	052 C24.6	13	•	•	13	•	•	•	04	01	04	09	09	09	09	09	09	02	•	•	•	•	•	02	12	
GOD. 5.5 6.5 4.3 5.5 2325.6 07.7 78 50 73 67 14 1361 078.0																													
SIBENIK																													
BR. ST. 87																													
I 6.0 6.8 3.8 5.6	122.0	05.6	70 59 69 66 29	099 C25.2	02	•	•	•	•	•	•	04	•	•	C5	09	12	08	05	12	•	•	•	•	•	•	02	•	
II 7.1 7.0 5.6 6.6	123.3	06.0	66 56 67 64 22	070 C20.0	04	•	•	•	•	•	•	14	02	•	C1	10	13	02	13	13	•	•	•	•	•	•	01	03	
III 5.6 6.9 4.7 5.7	103.5	06.2	67 52 68 62 19	110 051.0	05	•	•	•	•	•	•	13	01	•	C4	07	07	04	07	17	•	•	•	•	•	•	02	66	
IV 5.6 6.8 5.3 6.1	178.3	06.1	57 49 58 54 17	034 C13.4	27	•	•	•	•	•	•	16	02	•	C5	11	13	05	01	13	•	•	•	•	•	•	01	01	
V 6.1 6.3 5.2 5.6	272.2	08.6	65 50 63 59 22	052 013.6	01	•	•	04	•	•	•	07	02	•	C6	13	06	02	13	13	•	•	•	•	•	•	06	•	
VI 6.0 6.0 5.0 5.7	277.5	10.8	62 48 63 58 26	046 C20.0	30	•	•	18	•	•	•	02	10	02	C5	04	06	01	12	12	•	•	•	•	•	•	02	C2	
VII 3.2 2.5 2.0 2.7	358.4	11.2	54 42 53 50 21	046 045.5	20	•	•	27	10	12	•	08	01	•	C1	01	01	01	01	01	•	•	•	•	•	•	01	01	
VIII 3.3 3.7 2.3 3.1	319.5	12.9	57 46 57 53 24	064 013.7	24	•	•	31	16	19	06	01	15	01	04	05	05	06	06	•	•	•	•	•	•	16	•		
IX 4.6 4.1 3.1 4.0	251.5	11.9	70 55 68 64 25	215 056.2	21	•	•	18	•	03	10	•	12	05	11	09	05	11	11	•	•	•	•	•	•	06	02		
X 7.0 7.5 6.3 6.9	124.9	07.2	73 60 71 68 25	247 G50.1	06	•	•	05	•	•	•	15	03	03	C4	12	24	15	17	24	•	•	•	•	•	•	04	12	
XI 6.6 6.6 5.2 6.4	127.4	06.9	72 58 70 67 26	054 012.0	26	•	•	•	•	•	•	05	01	04	05	14	08	02	14	14	14	•	•	•	•	•	•	01	10
XII 5.3 4.9 4.0 5.1	135.0	05.6	73 57 72 67 25	021 C08.7	13	•	•	•	•	•	•	06	04	07	C8	06	04	06	06	06	•	•	•	•	•	•	01	06	
GOD. 5.7 5.7 4.4 5.6 2462.5 08.2 65 52 64 61 17 1058 056.2																													
KENIZA																													
BR. ST. 88																													
I 3.7 4.1 3.2 3.6	-	07.1	77 68 76 73 45	138 C45.3	02	•	•	•	•	•	•	14	06	07	07	04	07	•	•	•	•	•	•	•	•	01			
II 4.6 4.0 4.5 4.3	-	07.3	72 63 74 70 28	101 050.7	23	•	•	•	•	•	•	C2	•	C7	04	07	03	07	•	•	•	•	•	•	•	02			
III 2.6 4.3 3.1 3.5	-	07.6	74 66 72 71 49	164 C60.7	05	•	•	•	•	•	•	02	01	C1	C5	04	05	06	06	06	•	•	•	•	•	•	02		
IV 5.0 4.6 4.2 4.6	-	07.9	68 61 70 66 34	112 055.6	18	•	•	•	•	•	•	04	•	C9	07	07	04	07	•	•	•	•	•	•	•	•			
V 2.5 2.1 2.5 2.4	-	09.0	63 52 66 60 36	056 C19.4	69	•	•	02	•	•	•	13	02	05	05	05	C3	C4	•	•	•	•	•	•	•	03			
VI 3.0 1.5 2.5 2.5	-	11.9	64 55 68 62 40	054 019.2	11	•	•	15	02	02	•	14	•	04	04	02	04	04	04	04	04	•	•	•	•	01			
VII 1.0 1.0 0.5 0.9	-	12.3	53 47 55 52 32	056 006.2	20	•	•	26	11	10	•	25	•	01	01	01	01	01	01	01	01	01	01	01	01	02			
VIII 2.5 1.0 1.2 1.5	-	13.8	58 53 55 55 27	073 C04.3	25	•	•	31	15																				

M	Vremenski pristupak 2m u m	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																			
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW			
		7	14	21	Sred. (dies)							E	J.	E.	J.	S.	J.	E.	J.	S.	J.	E.	J.	E.	J.	E.	J.		
M = 13 ⁰ 13 ¹ N = 16 ⁰ 40 ¹ E Gr. AG = + 1h 07 min.																													
I	-	02.4	05.9	04.9	05.5	10.6	01.0	15.6	20	-05.4	15	11	02.2	C7	02.7	C3	01.0	09	01.7	06	01.5	06	01.5	*	*	04	C1.2	47	
II	-	04.9	10.6	06.8	07.3	11.4	03.4	15.4	20	-03.8	09	10	03.4	C4	02.9	C1	C7.0	15	02.5	16	02.4	02	01.5	01	03.0	05	C1.2	20	
III	-	05.4	14.5	09.4	09.4	15.4	03.8	25.1	22	-02.5	01	14	02.4	C6	03.5	C3	01.0	10	02.4	16	02.1	07	02.6	*	*	04	C1.2	33	
IV	-	08.7	14.0	09.8	10.6	15.2	06.3	19.4	06	-00.8	21	16	C3.0	17	01.3	C3	01.0	09	02.9	15	02.3	C5	02.8	02	01.5	04	C1.5	15	
V	-	12.3	19.1	13.5	14.6	20.0	08.8	26.1	20	04.8	11	11	07.8	C9	05.1	C1	01.0	08	02.1	07	02.1	14	02.7	01	02.0	06	01.7	36	
VI	-	16.3	22.8	16.9	16.2	24.1	12.9	25.2	04	06.2	13	15	C2.5	C9	03.2	C2	01.5	06	04.0	06	03.7	16	02.1	02	02.0	07	01.9	27	
VII	-	19.4	27.3	20.2	21.5	28.2	14.4	34.8	16	08.8	09	15	C2.1	17	02.5	*	*	*	*	C1	03.0	18	01.9	03	03.0	05	C1.4	41	
VIII	-	19.6	28.9	21.9	22.8	30.1	15.3	35.4	02	05.8	12	08	C2.0	07	07.1	*	*	06	01.3	02	01.5	18	01.6	02	01.5	06	C2.8	44	
IX	-	14.6	24.2	17.5	18.4	25.3	11.9	30.4	15	10	02.1	C9	01.8	*	*	*	11	02.1	13	01.8	10	01.8	*	*	05	01.8	32		
X	-	02.9	12.7	08.4	09.1	13.9	04.6	17.4	04	-02.3	31	20	C1.8	C1	02.2	C7	C2.0	12	02.4	15	01.7	07	02.0	02	01.5	11	01.5	23	
XI	-	00.3	12.0	07.1	07.6	13.1	02.5	19.2	17	-02.1	02	07	04.0	07	04.0	*	*	14	01.6	18	01.4	01	01.0	C1	02.0	06	01.5	36	
XII	-	00.3	07.4	02.9	03.4	08.4	-01.8	17.3	04	-10.2	24	19	C2.8	C9	04.2	01.0	04	01.0	09	01.1	*	*	01	01.0	01	C1.0	49		
GOD.	-	05.4	17.0	11.6	12.4	18.0	06.9	35.4	02.8	-10.2	C2.1	160	02.5	107	C3.0	17	01.2	104	02.2	123	02.6	104	C2.0	13	01.8	64	C1.6	403	
M = 13 ⁰ 18 ¹ N = 17 ⁰ 01 ¹ E Gr. AG = + 1h 08 min.																													
MAKARSKA																													
BR. ST. 92																													
I	-	07.0	11.8	08.0	08.7	12.7	04.8	17.5	20	00.5	15	02	04.5	15	01.3	29	C1.3	32	01.1	C1	01.0	04	01.2	03	02.7	07	C3.6	*	
II	-	09.5	12.9	10.4	10.8	13.8	06.1	17.5	18	02.0	11	09	C1.0	14	02.0	31	C1.4	16	01.1	04	01.2	02	C2.0	*	*	14	03.6	*	
III	-	06.8	14.7	10.9	11.5	15.4	07.4	21.5	26	03.0	11	06	C0.5	07	01.3	35	C1.2	22	01.4	15	01.2	*	*	01	02.0	03	03.3	04	
IV	-	13.0	15.8	11.5	14.0	17.1	09.4	23.5	30	06.0	25	17	15	05.2	14	02.6	23	C1.2	19	C1.4	69	C3.1	01	02.0	*	*	01	03.6	08
V	-	16.8	19.8	17.6	17.6	21.0	12.7	26.0	22	05.5	11	07	C3.7	08	02.6	11	C1.1	10	02.0	54	01.7	*	*	*	*	02	03.0	05	*
VI	-	0.8	23.5	20.8	21.5	24.5	16.2	28.5	27	16.0	16	04	01	11	01.7	C3	C2.0	*	*	52	01.2	*	*	02	03.5	03	05.0	10	
VII	-	1.4	27.4	23.1	24.2	28.2	18.2	34.5	21	11.6	21	09	04.2	17	01.5	37	C1.0	11	02.0	09	01.9	16	C1.6	03	02.7	11	03.5	15	
VIII	-	1.4	28.7	19.8	25.0	30.0	19.8	35.5	20	16.5	14	01	04.0	18	01.6	C7	C1.0	19	01.4	16	01.6	07	01.7	12	02.0	20	C2.0	08	
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	12.7	19.1	15.1	15.5	20.2	-	36.8	02.8	-	05	04.0	07	C3.3	125	C3.1	503	C3.0	19	C3.6	120	C3.2	162	C3.2	24	C2.9	*		
OPUZEN																													
BR. ST. 91																													
I	-	05.6	11.7	07.5	08.0	12.4	-	17.0	20	-	-	00	02.5	11	02.2	72	C2.6	47	02.7	C7	02.0	*	*	*	*	02	C2.6	*	
II	-	08.5	13.4	10.3	10.6	16.2	-	18.5	16	-	-	01	02.5	18	C3.2	11	C3.6	42	02.8	*	*	10	03.2	01	04.0	01	C4.0	*	
III	-	09.7	16.0	11.9	12.3	17.0	07.2	24.0	21	04.0	14	09	*	*	14	01.9	34	C2.8	25	33.0	*	*	09	C2.4	16	01.4	01	C4.0	*
IV	-	13.0	17.3	14.1	14.6	18.0	09.4	22.6	09	07.2	22	*	*	14	02.2	C6	C3.1	02	03.1	12	03.0	05	C3.8	*					
V	-	15.6	20.3	17.6	17.6	21.0	11.3	25.4	28	06.4	01	01	*	04	01.6	C9	C3.4	26	C3.4	50	01.3	23	03.2	03	C1.7	*			
VI	-	19.5	24.6	21.2	25.6	15.6	25.0	29.0	05	10.4	14	02.2	12	04.9	11	C3.7	29	C3.4	01	02.0	07	03.4	01	04.0	*				
VII	-	21.1	28.5	19.3	24.0	29.4	18.0	34.8	16	13.4	10	05.0	04.0	04.0	01	03.7	28	C3.2	01	05.0	09	03.6	36	03.4	*				
VIII	-	21.4	30.7	24.1	25.1	31.7	19.1	36.8	06	14.8	13	02.0	04.5	*	07	C2.9	28	C3.0	23	03.0	31	03.1	*						
IX	-	18.1	25.6	20.6	21.3	27.0	15.7	30.5	21	10	*	03.0	C3	C3.7	50	03.1	01	02.0	20	03.2	13	03.4	01	C3.0	*				
X	-	11.0	16.7	14.0	13.9	17.7	05.0	21.2	13	03.3	31																		

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра m/s (0-12)																		
		Tm			Sred. (Dies)		Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		7	14	21									8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\varphi = 42^{\circ}40'$, N $\lambda = 10^{\circ}54'$, E Gr., AG = + 1h 08 min.																														
I	- 748.9	09.0	10.5	09.4	05.5	11.3	07.5	15.4	20	05.2	15	04	C1.5	14	01.9	12	02.1	23	02.8	*	C2	01.0	*	*	22	C1.8	16			
II	- 746.2	09.5	11.1	09.8	10.0	12.2	08.1	15.8	16	05.4	17	01	C1.0	16	03.4	16	04.5	34	03.7	04	02.8	*	C1	06.0	08	C1.5	12			
III	- 744.5	09.8	12.6	10.7	11.0	13.5	08.5	15.6	21	04.3	18	01	C1	12	01.9	10	01.5	28	05.5	01	05.0	01	01.0	01	01.0	28	C2.2	11		
IV	- 741.0	11.8	13.8	11.6	12.2	15.1	09.7	18.9	29	05.0	17	03	C1.3	10	03.1	18	03.0	34	03.4	03	02.7	*	*	01	01.0	24	C1.6	07		
V	- 742.7	15.2	18.0	15.1	15.6	19.3	12.9	24.4	22	05.2	09	01	C1.0	05	02.4	02	03.0	32	02.1	01	01.0	07	02.0	*	*	37	C1.9	08		
VI	- 743.3	19.2	22.5	18.9	19.8	23.7	17.0	27.6	26	11.2	13	02	C0.9	06	01.8	06	02.0	25	02.7	04	01.5	03	03.3	C2	02.0	33	C2.3	05		
VII	- 744.8	23.4	26.5	22.7	23.8	27.9	20.3	33.8	15	15.7	10	05	C2.4	05	02.0	C7	01.9	20	01.7	01	04.0	02	02.5	*	*	35	C2.1	18		
VIII	- 744.4	24.2	27.3	24.2	25.0	29.1	21.7	34.0	05	14.5	29	02	C2.5	01	02.0	08	01.4	16	01.9	01	03.0	02	01.0	*	*	45	C2.0	18		
GOD.	- 744.3	14.7	17.0	14.8	15.3	18.3	12.9	24.0	05	05.0	04.0	05	PM	28	C2.0	57	02.6	76	C2.1	330	C2.6	30	02.9	41	01.9	09	C2.2	355	C2.6	129
$\varphi = 42^{\circ}58'$, N $\lambda = 17^{\circ}09'$, E Gr., AG = + 1h 12 min.																									KUKČULA		BR. ST. 97			
I	-	08.7	12.0	09.3	09.6	12.8	06.4	16.9	20	03.1	15	02	C5.5	01	C1.0	23	C4.9	14	01.9	09	01.1	19	01.3	19	01.0	05	C3.0	01		
II	-	16.0	12.6	10.6	10.9	13.4	07.8	16.3	20	02.9	09	03	C2.5	04	05.5	40	C3.1	15	02.1	07	C1.6	08	C1.1	05	C2.0	03	C1.3	*		
III	-	10.6	14.3	11.3	11.9	14.9	05.0	18.8	30	03.3	05	*	*	C1	05.0	27	03.1	13	01.8	11	01.1	16	01.7	13	01.6	02	C2.5	*		
IV	-	13.4	15.7	12.7	13.6	16.6	09.5	18.9	06	05.4	17	02	C1.0	05	03.8	38	C2.3	16	02.1	02	01.5	09	01.2	15	02.1	05	C2.2	*		
V	-	17.2	19.4	15.6	17.1	20.0	12.5	25.3	21	05.4	26	*	*	C3	03.3	36	C2.4	12	02.1	03	01.0	06	01.3	17	02.0	06	C1.5	*		
VI	-	21.0	23.4	19.9	21.6	-	16.6	-	-	12.2	15	04	C3.0	01	01.0	39	C2.6	11	02.1	C2	01.5	02	01.5	24	C1.9	06	C2.3	01		
VII	-	24.4	26.5	23.2	24.3	27.4	19.3	32.7	16	16.5	23	05	C1.2	05	07.4	79	02.1	09	C0.4	03	01.0	06	01.3	35	01.8	11	C2.4	*		
VIII	-	25.0	28.1	24.5	25.5	29.5	20.9	34.5	06.0	16.6	12	05	01.0	05.0	26	C2.2	05	02.0	05	01.2	13	01.5	25	C1.9	06	C1.5	02			
IX	-	22.0	24.7	21.1	22.2	25.4	18.1	29.7	16	13.0	28	04	C1.8	*	*	*	C3.0	17	02.1	06	01.8	06	01.2	20	01.8	07	C2.4	*		
X	-	13.5	16.2	13.6	14.1	17.1	10.5	19.7	01	05.4	31	04	02.0	03	02.0	17	02.5	18	01.7	08	01.1	13	01.0	19	01.7	11	C2.5	*		
XI	-	12.2	14.2	12.2	12.7	15.1	05.4	18.7	07	04.2	02	*	*	C4	03.8	35	02.6	17	01.9	09	01.1	14	01.2	07	01.7	03	C2.7	01		
XII	-	09.1	12.0	09.7	10.1	12.8	05.5	16.1	04	02.8	17	*	*	C7	02.9	16	02.3	16	01.5	10	01.1	25	01.3	17	01.5	08	C1.8	*		
GOD.	-	15.6	18.3	15.3	16.1	-	12.1	-	-	02.8	PM	24	C1.4	39	03.5	364	C2.7	151	02.0	75	01.2	139	01.2	270	01.4	73	C2.2	05		
$\varphi = 42^{\circ}58'$, N $\lambda = 17^{\circ}10'$, E Gr., AG = + 1h 09 min.																									GREBIC		BR. ST. 98			
I	-	07.8	12.6	08.0	09.1	13.1	05.6	17.9	20	00.5	15	27	C1.3	18	07.5	C9	C2.7	12	02.7	*	04	02.0	04	02.5	13	C2.4	06			
II	-	05.5	13.0	05.6	10.3	13.6	07.4	17.5	16	01.0	05	15	C1.5	26	07.7	C5	C2.2	24	02.8	04	02.2	*	C1	03.0	04	C2.0	05			
III	-	05.7	14.6	10.0	11.1	15.1	07.2	15.6	25	03.0	11	01	C2.1	22	C1.5	13	C2.8	25	02.8	01	02.0	07	02.6	08	C1.4	09				
IV	-	13.5	15.5	11.7	13.1	16.9	09.5	21.1	06	05.8	17	09	C1.1	24	04.8	C9	C3.1	26	02.8	01	02.5	05	02.4	05	C1.6	05				
V	-	16.7	19.2	15.2	16.5	20.0	12.2	25.9	26	07.5	11	14	C1.6	12	02.4	C5	C2.0	26	02.4	02	02.0	07	03.1	11	02.8	07	C1.7	09		
VI	-	20.6	23.2	19.1	20.5	24.1	16.2	27.0	25	11.9	14	11	C1.9	19	C2.5	C3	C2.7	28	02.3	01	02.0	04	03.6	11	03.0	08	C2.1	05		
VII	-	23.9	26.5	21.4	23.3	27.8	18.3	32.0	16	12.2	09	22	C1.4	14	02.6	C2	C3.0	27	02.2	04	01.2	09	02.2	04	C3.1	02	C1.5	09		
VIII	-	24.4	28.7	23.2	24.8	29.5	20.9	35.5	16	16.0	14	12	C1.6	15	07.0	C6	C1.8	26	02.2	C3	01.7	07	C5.4	13	02.5	*	02			
IX	-	21.3	25.1	20.1	21.7	26.2	17.8	31.4	11	16.6	26	14	C1.3	17	02.9	C4	C2.5	28	02.9	02	*	08	02.8	10	C2.2	02	C1.8	*		
X	-	12.6	17.0	12.5	15.9	17.6	10.1	20.7	01	05.0	31	26	01.5	08	02.5	*	*	24	03.1	06	C2.3	04	03.0	13	02.5	07	C2.3	*		
XI	-	12.0	14.8	11.4	12.4	15.7	05.1	18.0	02.8	02	28	01.3	23	07.7	C7	C3.4	19	03.2	04	01.8	03	C2.3	02	03.0	02	C1.9	02			
XII	-	08.4	13.0	08.7	07.3	12.3	03.3	17.5	04	-02.0	24	27	41	02.5	05	02.8	C1	03.0	08	02.7	01	01.0	01	C1.0	07	01.3	09			
GOD.	-	13.4	18.4	13.4	14.6	19.7	05.4	37.5	05	05.0	51	263	C2.1	41	02.1	43	02.9	216	C3.2	53	C2.1	30	02.0	80	01.4	78	02.1	291		
$\varphi = 42^{\circ}50'$, N $\lambda = 17^{\circ}42'$, E Gr., AG = + 1h 11 min.																									STAKA		BR. ST. 99			
I	-	05.6	11.9	06.4	07.6	12.6	04.8	17.4	21	-02.0	15	42	C1.6	C4	C1.0	C2	C2.5	11	C3.2	04	C1.5	*	09	01.0						

Mesec	Udžačnost Rm (0-10)				Trsodajna Istočnost sati Sred. Odes.	Vlažnost vazduha				Padavine R mm		Broj dana na se																			
	7	14	21	Sred.		7	14	21	Sred.	Min	Tn	Tx	Tn	Tx	Tx	Td	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	☒	
LASTEVE																															
BR. ST. 96																															
I 5.6 6.1 7.9 4.7	118.0	06.6	76	71	76	74	39	106	040.1	03	02	.	10	05	10	08	03	10	*	*	*	01	*		
II 6.6 7.6 8.2 5.0	107.7	06.9	76	75	74	39	129	055.4	23	08	.	01	07	11	10	04	11	*	*	*	02	04			
III 5.2 5.7 4.4 3.5	160.4	07.3	78	69	72	73	24	086	031.2	05	05	02	09	09	07	04	04	04	*	*	*	02	01			
IV 5.7 5.7 4.5 5.4	161.9	08.0	76	69	79	75	36	087	036.4	18	05	02	12	16	12	02	16	*	*	*	03	*				
V 4.5 4.4 3.2 2.4	263.6	09.9	77	66	76	73	39	046	018.8	09	03	02	10	07	01	05	*	*	*	*	05	01				
VI 4.7 3.9 2.5 1.5	294.4	12.6	75	64	76	71	36	225	011.6	19	.	.	.	06	.	03	11	01	08	04	01	06	*	*	*	01	07	01			
VII 1.9 1.5 1.1 1.5	387.0	12.5	58	49	60	56	29	001	000.5	21	.	.	26	01	16	.	23	01	01	*	*	01	*	*	*	02	*				
VIII 2.5 2.4 1.9 1.3	320.8	14.3	64	55	65	61	19	051	017.1	25	.	.	28	13	22	03	18	09	07	03	09	*	*	*	*	11	*				
IX 3.4 3.2 2.7 2.2	256.8	14.4	80	67	78	75	36	047	030.1	21	.	.	14	01	15	05	15	04	08	04	01	08	*	*	*	*	01	08			
X 6.7 6.1 5.1 6.0	145.9	08.8	76	69	75	73	36	170	044.4	01	07	.	04	08	21	17	07	21	*	*	*	*	11	*			
XI 6.0 5.7 4.0 5.2	107.6	08.2	78	75	76	74	45	052	013.4	01	06	04	05	11	06	01	11	*	*	*	*	06	*				
XII 6.6 5.1 5.1 5.5	127.9	06.7	74	67	73	71	31	004	003.5	13	02	01	10	02	04	03	04	*	*	*	*	01	*				
GOD. 4.7 4.6 3.4 4.3	2456.8	09.7	74	65	73	71	19	012	055.4	038	.	.	.	76	21	53	45	03	122	56	118	85	28	116	*	*	*	07	*	60	03
KORČULA																															
BR. ST. 97																															
I 5.6 5.2 3.4 4.8	-	04.5	74	63	72	70	37	111	035.0	03	01	.	10	05	12	04	12	*	*	*	02	*				
II 7.8 6.4 5.9 6.7	-	07.1	75	66	74	72	33	222	059.1	04	02	.	01	14	13	11	05	13	*	*	*	04	*			
III 5.4 5.4 4.5 5.2	-	07.6	76	67	74	72	31	086	044.3	03	03	.	07	09	06	03	08	*	*	*	03	01				
IV 5.7 5.8 5.1 5.5	-	04.0	69	61	73	68	34	123	032.7	18	02	.	06	11	17	13	04	17	*	*	*	06	*			
V 5.7 4.7 3.9 4.7	-	10.3	72	62	75	70	41	126	043.6	09	.	.	01	.	02	.	08	06	11	05	03	11	*	*	*	03	02				
VI 4.9 4.2 3.5 4.1	-	13.5	72	65	75	71	36	063	012.5	30	.	.	.	03	.	10	11	08	01	10	*	*	*	06	*						
VII 1.9 1.7 1.5 1.7	-	13.1	57	53	58	56	31	006	006.3	20	.	.	27	03	11	01	22	01	01	*	*	01	*	*	*	01	*				
VIII 2.6 2.4 2.2 2.4	-	14.6	65	54	61	60	25	034	017.2	25	.	.	29	15	20	.	19	04	02	02	03	*	*	*	*	07	*				
IX 4.7 3.9 2.8 3.8	-	14.1	71	60	76	69	33	093	057.6	21	.	.	20	.	05	.	14	07	05	02	05	*	*	*	08	*					
X 6.9 7.1 5.5 7.5	-	09.2	78	68	76	74	34	280	044.6	06	.	.	.	07	.	04	13	21	18	12	21	*	*	01	01	CET					
XI 6.2 4.1 5.0 5.8	-	08.4	76	71	71	75	38	068	021.3	26	02	.	04	09	12	09	03	12	*	*	*	05	*				
XII 5.3 5.9 3.0 4.7	-	06.4	72	61	70	68	21	016	013.8	13	.	.	.	03	01	06	04	02	01	04	*	*	*	01	*						
GOD. 5.2 4.9 3.9 4.7	-	05.9	71	62	71	68	21	1220	059.1	058	.	.	.	35	15	01	111	85	121	93	40	121	*	*	*	04	01	96	03		
CREBIC																															
BR. ST. 98																															
I 5.7 5.5 3.9 5.0	-	06.1	74	55	74	69	23	13P	038.8	03	10	10	12	10	05	12	*	*	*	*	*					
II 6.1 6.6 6.2 7.0	-	06.8	72	62	76	70	31	229	072.5	04	02	13	12	06	12	*	*	*	*	03						
III 4.9 5.4 4.5 4.9	-	07.1	79	61	74	72	31	136	072.9	03	03	09	06	04	05	*	*	*	*	01						
IV 6.5 5.6 5.2 5.4	-	07.9	65	65	75	68	33	116	052.4	18	05	06	16	12	03	16	*	*	*	02	*					
V 5.4 4.6 4.4 4.8	-	10.1	72	63	75	70	23	145	042.3	05	.	.	02	.	01	.	06	05	10	09	04	10	*	*	*	04	*				
VI 5.0 4.4 3.8 4.4	-	12.4	65	61	73	66	37	045	014.6	30	.	.	14	.	02	.	07	03	01	01	10	*	*	*	02	*					
VII 1.9 2.2 1.6 1.9	-	12.7	57	53	60	57	33	002	002.5	20	.	.	28	07	06	.	21	01	01	01	01	*	*	*	02	*					
VIII 2.5 2.5 2.7 2.6	-	14.0	62	51	63	58	31	038	032.6	24	.	.	29	16	15	.	18	06	04	02	06	*	*	*	06	*					
IX 4.8 4.3 3.6 4.2	-	13.6	71	60	75	68	28	103	053.4	21	.	.	21	C3	05	01	14	07	08	04	02	06	*	*	*	06	*				
X 6.7 6.6 5.8 6.4	-	09.2	79	65	80	74	26	280	039.7	01	04	13	21	10	11	21	*	*	*	05	*						
XI 4.9 4.7 3.6 4.4	-	08.1	75	67	73	73	41	074	020.6	26	04	05	12	11	02	12	*	*	*	04	*						
XII 4.8 4.6 3.9 4.8	-	04.1	71	56	71	66	22	019	014.1	13	.	.	08	.	02	.	07	03	03	02	01	02	*	*	*	01	01				
GOD. 5.2 4.9 4.3 4.8	-	04.5	70	62	72	67	22	1335	072.9	038	.	.	94	26	28	04	106	81	120	95	42	120	*	*	*	01	35	*			
STON																															
BR. ST. 99																															

Mesec	Oblačnost Nm (0-10)			Isolacija Ljeto/ zimi	Vlažnost vazduha			Padavine mm			Broj dana na sata:																				
	7	14	21		em	m	%		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	★	▲	■	▲	▲	▲	▲	▲					
					mm	7	14	21	STEV. M	7	14	21	STEV. M	Max	Min.	30.00.0	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	10.0	0			
BR. ST.101 HLSANSKI NOVI SR BOSNA I HERCEGOVINA																															
I	9.5	7.9	7.4	8.3	-	-	-	-	-	-	-	-	-	-	050	013.4	01	-	-	14	-	-	-	-	-	-	-	-			
II	6.2	7.1	7.1	7.5	-	05.6	81	72	81	78	55	034	006.5	02	-	-	06	-	-	-	-	11	11	12	10	01	12	02	-		
III	7.1	6.2	6.5	6.6	-	05.6	75	65	72	71	29	046	014.0	06	-	-	06	02	-	-	-	04	04	07	06	02	07	03	02		
IV	7.0	6.9	7.0	7.3	-	06.0	81	56	74	70	26	057	020.1	14	-	-	04	-	-	-	-	11	14	05	01	14	-	-	28		
V	8.0	6.8	7.0	7.6	-	06.6	80	57	82	75	36	125	036.0	29	-	-	08	-	-	-	-	13	21	16	04	21	-	-	28		
VI	6.7	6.6	6.6	7.3	-	09.8	d2	56	71	71	30	089	010.0	07	-	-	12	-	-	-	-	01	17	16	09	03	14	-	-		
VII	7.7	5.6	3.4	4.9	-	10.9	73	52	66	64	22	079	015.4	07	-	-	22	10	-	-	-	04	04	10	07	05	10	-	-		
VIII	6.9	4.4	4.1	5.6	-	13.4	80	44	76	73	35	194	034.6	74	-	-	24	15	-	-	-	02	07	10	10	03	10	-	25		
IX	9.0	6.1	5.6	5.9	-	11.3	88	70	86	P1	50	151	059.8	30	-	-	13	01	-	-	-	07	14	11	06	14	-	-	-		
X	9.3	7.4	6.7	7.8	-	06.5	85	77	84	E2	55	273	045.6	06	-	-	02	-	-	-	-	17	20	16	09	20	01	-	21		
XI	6.8	4.6	5.6	7.0	-	05.6	85	72	R2	P0	53	066	017.2	29	-	-	07	-	-	-	-	01	14	12	11	02	12	01	01		
XII	7.6	5.9	5.0	6.3	-	04.6	87	76	86	B3	47	051	015.0	13	-	-	19	01	-	-	-	01	61	10	03	08	01	07	02		
GOD.	8.5	6.3	6.0	6.9	-	-	-	-	-	-	-	1120	059.8	50	-	-	60	R1	26	-	-	14	134	154	124	37	153	09	06		
BR. ST.102 BOSANSKA DUBICA																															
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
IV	5.7	7.3	5.9	6.6	-	06.5	86	55	82	74	28	037	006.5	13	-	-	03	-	-	-	-	04	13	10	10	-	10	-	C1		
V	6.6	6.9	5.0	5.2	-	05.8	89	62	98	80	43	101	016.0	23	-	-	07	-	-	-	-	04	10	18	14	02	18	-	-		
VI	5.1	6.0	6.5	5.9	-	11.8	35	62	86	70	40	150	040.6	11	-	-	14	-	-	-	-	01	07	14	12	05	14	-	-		
VII	4.2	4.1	3.6	4.0	-	13.6	85	56	67	77	23	066	019.5	20	-	-	07	-	-	-	-	12	C5	08	06	03	08	-	-		
VIII	3.9	3.6	3.7	3.7	-	15.4	91	63	90	81	49	101	017.0	18	-	-	19	12	-	-	-	16	08	10	10	04	10	-	-		
IX	7.4	5.6	4.6	4.9	-	11.5	94	67	92	84	44	137	010.0	30	-	-	10	01	-	-	-	02	02	C3	10	12	10	06	12	-	
X	9.0	7.7	7.0	7.9	-	06.9	91	79	94	P2	42	273	054.0	07	-	-	01	-	-	-	-	01	17	18	17	10	18	-	61		
XI	9.7	7.2	5.3	7.4	-	06.1	95	77	85	89	37	061	016.7	19	-	-	09	-	-	-	-	01	17	13	16	04	13	01	91		
XII	6.4	7.0	7.4	7.4	-	05.2	95	50	97	94	61	141	010.0	11	-	-	01	19	-	-	-	02	21	11	05	01	11	03	-		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
BR. ST.103 CERVENTA																															
I	9.0	P.3	6.5	P.5	-	04.9	96	67	56	G3	59	046	C73.6	20	-	01	18	-	-	-	01	23	11	05	02	11	01	01	13		
II	5.9	6.4	5.5	6.0	-	05.7	95	64	89	P3	41	030	C09.0	04	-	-	11	-	-	-	-	06	16	11	07	-	10	01	01		
III	5.1	5.7	6.0	5.6	-	05.9	90	58	92	77	20	021	C08.6	07	-	-	09	02	-	-	-	04	12	06	04	-	05	04	-		
IV	5.5	6.9	6.2	6.2	-	06.7	97	50	86	74	18	060	015.4	16	-	-	03	-	-	-	-	06	11	12	01	02	02	-	-		
V	5.9	7.0	4.7	6.6	-	10.0	90	59	92	80	40	086	C15.5	25	-	-	04	-	-	-	-	01	02	13	18	16	04	18	-		
VI	5.1	5.0	5.7	5.6	-	12.1	90	56	90	79	17	151	046.0	11	-	-	11	01	-	-	-	05	08	15	15	06	15	-	01		
VII	3.3	4.0	3.2	3.5	-	13.7	85	57	89	77	24	077	C22.4	20	-	-	17	08	-	01	-	16	06	11	11	03	11	-	01		
VIII	3.6	3.6	3.5	3.6	-	15.0	94	59	91	H0	38	079	017.6	09	-	-	19	12	-	-	-	13	04	12	16	03	13	-	06		
IX	6.0	5.1	4.5	5.6	-	12.4	95	66	94	P5	43	091	031.3	27	-	-	11	01	-	-	-	04	10	09	05	04	06	-	C7		
X	8.3	6.7	7.3	7.4	-	07.1	96	75	94	P9	43	200	034.5	06	-	-	02	-	-	-	-	01	15	20	18	06	20	01	01		
XI	6.0	6.6	7.7	6.7	-	06.0	96	77	96	90	39	074	020.4	29	-	-	09	-	-	-	-	04	15	11	11	02	11	01	01		
XII	5.0	6.3	6.7	7.0	-	05.2	94	79	93	89	52	062	G22.7	19	-	-	15	-	-	-	-	04	16	11	10	02	11	04	03		
GOD.	6.2	6.0	5.8	6.0	-	08.7	92	65	91	H3	17	996	046.0	80	-	01	67	64	12	-	02	01	71	143	147	120	34	145	15	11	
BR. ST.104 BIHAC																															
I	8.0	7.4	7.4	7.4	-	048.0	04.6	94	60	91	88	46	063	026.0	01	-	-	25	-	-	-	-	03	01	15	12	08	03	10	02	18
II	8.0	7.3	7.6	8.0	-	06.0	95	03.0	88	65	73	28	058	014.6	07	-	-	03	-	-	-	-	14	02	-	16	15	10	02	14	C1
III	7.2	7.2	7.4	7.6	-	095.9	05.4	86	60	75	73	20	079	021.6	05	-	-	07	-	-	-	-	03	02	14	11	08	03	07	01	
IV	6.8	7.0	6.1	6.9	-	128.8	05.8	83	53	69	68	26	102	034.4	14	-	-	02	-	-	-	-	05	02	14	15	02	01	02	C2	
V	6.6	5.7	5.7	6.6	-	187.6	08.0	79	50	74	66	30	115	C78.0	23	-	-	06	-	01	-	-	04	01	14	17	19	15	03	15	01
VI	5.9	7.7	5.8	6.5	-	15.3	09.9	56	73	62	35	115	C23.6	11	-	-	07	-	01	-	-	03	08	15	15	06	15	05	01		
VII	4.6	4.6	3.2	4.1	-	277.6	11.4	80	50	69	66	30	091	C35.2	20	-	-	23	06	02	05	-	11	05	13	09	03	13	-	03	
VIII	5.7	5.6	2.9	4.8	-	210.2	13.5	91	58	82	77	32	104	066.0	23	-	-	18	12	-	04	-	08	07	11	09	04	10	01		
IX	7.6	6.3	4.8	6.2	-	151.2	10.6	89	62	84	78	37	183	082.5	30	-	-	08	01	-	05	-	04	09	12	04	05	02	01		
X	7.8	A.1	6.7	7.5	-	082.9	05.9	77	65	79	75	40	270	068.0	21	-	-	05	-	02	01	-	17	21	20	09	21	05	02		

Mesec	Vazdušni pritisak Pr. mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																		
		Tm			Sred. (Cles)			Max	Min	Dat.	Min	Dat.	N		NL		E		SE		S		SW		W		NW			
		7	14	21									E.	J.	E.	J.	S.	J.	E.	J.	S.	J.	E.	J.	S.	J.				
$\Delta t = +1h\ 00\ min$																														
I	44°23'	N	1	16°24'	E	Gra.	ΔG =	+1h 00 min																						
I	723.7	-01.3	05.1	00.7	01.3	05.8	-02.2	13.6	20	-06.0	26	*	*	C1	04.0	*	*	03	02.0	04	02.5	01	02.0	02	02.5	01				
II	716.9	02.6	04.3	04.5	04.9	09.2	00.9	14.2	12	-06.0	09	13	04.2	05	04.3	*	05	03.4	16	03.2	04	03.5	01	03.0	02	02.5	37			
III	715.1	02.3	12.1	06.4	06.8	13.2	01.1	25.0	22	-06.6	14	03	04.6	06	04.7	C1	02.0	02	04.5	06	03.5	07	02.3	01	04.0	16	03.2	45		
IV	716.1	05.1	12.0	07.9	08.3	13.3	03.0	18.0	29	-02.8	20	17	04.5	14	04.7	*	*	05	03.2	09	04.6	05	03.6	02	03.5	40				
V	717.1	04.5	17.8	11.6	12.7	19.0	06.0	24.4	30	06.6	10	07	04.0	05	04.2	02	C1.0	07	03.1	07	03.4	02	04.0	02	03.0	54				
VI	716.0	12.6	19.0	14.7	15.4	21.7	09.7	28.2	05	02.0	13	17	03.4	07	03.7	*	*	05	03.0	02	05.5	09	03.6	02	02.0	51				
VII	720.3	14.0	24.6	17.1	18.2	25.6	10.6	32.8	16	04.1	09	11	03.4	05	04.5	*	*	02	03.5	04	03.4	06	03.0	01	04.0	10	03.2	55		
VIII	720.3	14.2	26.5	17.0	19.0	27.6	11.6	34.4	17	03.8	31	05	04.0	07	04.6	*	*	03	04.3	04	03.8	07	02.7	*	*	09	02.7	63		
IX	715.4	10.0	11.1	13.0	14.6	22.5	08.8	28.2	06.0	06.6	28	05	04.8	02	04.0	*	*	04	03.8	09	04.1	07	03.3	01	04.0	02	03.4	54		
X	715.6	03.5	09.8	04.7	05.6	11.2	01.6	17.8	04	-05.6	31	04	01.2	*	*	02	0.0	02	04.6	05	03.9	02	03.0	06	03.3	63				
XI	720.4	01.6	09.1	03.7	04.6	10.2	00.0	18.4	17	-05.2	02	03	01.8	*	*	*	*	*	04	04.8	11	03.4	*	*	01	03.0	66			
XII	711.6	-01.8	05.2	00.5	01.1	07.0	-03.4	12.6	10	-05.5	29	06	03.3	04	06.0	*	*	*	*	*	*	*	*	*	01	05.0	82			
GOD.	719.1	06.1	14.3	08.6	09.4	15.6	04.0	34.4	07.0	-09.5	94.0	43	14.0	11	04.0	C1	01.0	0	36	03.4	70	03.9	73	03.4	13	03.2	63	03.2	691	
$\Delta t = +1h\ 00\ min$																														
$\Delta t = +1h\ 00\ min$																														
I	-	44°01'	N	1	16°28'	E	Gra.	ΔG =	+1h 00 min																					
I	-	01.4	04.0	-00.8	-01.2	04.1	-03.5	05.5	20	-09.0	15	05	01.0	02	01.5	C1	01.5	*	*	13	02.1	C1	02.0	*	*	07	01.6	52		
II	-	01.9	05.6	02.0	03.1	05.5	-00.2	12.5	17	-05.0	08	03	02.0	12	03.0	12	02.0	*	*	49	03.2	*	*	*	*	*	*	08		
III	-	00.7	05.4	03.5	04.5	09.5	00.2	21.5	22.1	-06.0	14	03	02.5	03	02.0	*	*	*	*	17	02.8	*	*	02	02.0	06	01.8	35		
IV	-	05.4	05.4	05.3	06.1	10.8	01.2	16.5	29.10	-01.5	20	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*			
V	-	09.5	14.4	09.5	10.8	15.9	05.1	22.0	27	-04.5	10	02	03.0	14	03.1	*	*	*	*	46	02.3	*	*	*	*	*	*	31		
VI	-	13.6	17.6	12.9	14.2	19.3	08.4	24.0	05	01.0	13.12	15	04.5	06	04.7	*	*	*	*	36	02.5	01	04.0	05	02.8	*	*	27		
VII	-	14.9	27.1	15.2	16.0	22.9	09.7	30.0	16	03.5	09	15	01.0	05	01.0	*	*	*	*	22	02.3	*	*	*	*	*	*	46		
VIII	-	15.0	23.6	16.4	17.0	24.3	10.9	36.5	05	02.4	17	14	02.4	03	02.4	*	*	*	*	14	02.0	*	*	*	*	*	*	46		
IX	-	12.1	18.2	12.6	13.9	20.1	08.1	26.0	11	-06.5	27	16	07.0	*	*	*	*	*	*	21	02.3	*	*	02	01.5	*	*	57		
X	-	03.4	06.8	03.2	04.1	09.1	00.1	15.0	04	-06.5	31	01	02.0	*	*	*	*	*	*	01	02.0	15	03.2	*	*	03	02.3	01	02.0	72
XI	-	03.0	07.4	03.6	04.4	08.5	-00.3	-	-	-	20	03	01.0	*	*	*	*	*	*	25	02.4	*	*	*	*	*	*	67		
XII	-	-	-	-	-	-	-	-	-	-	20	03	01.0	*	*	*	*	*	*	22	02.5	*	*	*	*	*	*	59		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\Delta t = +1h\ 00\ min$																														
$\Delta t = +1h\ 00\ min$																														
I	-	44°46'	N	1	16°12'	E	Gra.	ΔG =	+1h 00 min																					
I	-	00.1	05.1	01.4	02.1	05.8	-06.4	14.0	20	-04.0	22	06	01.7	C4	01.5	02	01.0	01	02.0	02	02.0	05	01.4	06	01.7	08	01.9	59		
II	-	02.4	09.9	05.7	05.9	11.1	01.3	15.0	12	-04.0	09	10	01.3	01	02.0	05	04.5	05	02.4	03	02.3	03	02.3	10	02.1	36				
III	-	03.5	12.6	07.0	07.5	13.4	02.1	24.8	22	-04.4	02	04	02.2	06	02.0	C1	02.0	03	02.3	06	02.7	05	03.0	10	01.4	09	02.3	44		
IV	-	05.0	14.1	08.0	08.8	19.5	04.6	23.0	29	-01.6	20.0	09	02.6	08	02.4	02	02.0	01	02.5	03	02.2	05	02.2	05	02.2	50				
V	-	11.7	19.2	11.9	13.5	20.8	07.7	26.7	31	06.8	10	03	01.0	07	01.1	C3	02.3	08	07.1	08	03.2	02	01.5	12	02.2	46				
VI	-	14.8	27.1	15.9	17.2	24.3	10.8	30.4	27	01.6	12	05	02.6	02	02.0	C1	01.3	*	05	02.4	10	02.5	07	01.9	16	02.5	42			
VII	-	15.8	25.7	17.4	19.1	26.1	11.9	35.2	17	06.7	09	03	02.0	04	02.5	03	02.3	04	01.2	02	02.5	07	01.7	10	01.8	55				
VIII	-	16.2	26.6	18.4	19.5	27.7	12.7	33.0	04	03.6	12	14	01.6	04	02.8	C5	02.0	07	02.3	04	01.8	02	03.0	08	01.6	06	01.8	58		
IX	-	13.3	22.0	15.3	16.5	23.0	14.0	36.8	03	04.7	27	08	03.5	C1	01.0	01	03.0	04	02.2	04	01.2	04	02.5	09	02.1	06	01.5	50		

Meseč	Oblačnost Nm (0-10)				Insolacija broj sati em mm	Vlažnost vazduha				Padavine mm				Broj dana na sat															
	7	14	21	Sred. (Dnev.)		7	14	21	Sum. Min	Σ	Mx	Dat.	Tn	Tx	Tn	Tx	Tn	Tx	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	▲	▲
						mm	mm	mm	mm	mm	mm	mm	≤	<	≤	>	≤	>	≤	>	•	Δ	*	Δ	▲	▲	▲	▲	
DRVAR																													
BR. ST.106																													
I 8.0 6.6 6.0 6.9	-	04.5 96 75 93 88 49	068 023.6	01	•	01	25	•	•	•	•	•	01	15	11	09	02	11	03	02	•	•	•	•	•	14	05		
II 8.5 7.6 6.0 7.4	-	05.2 90 65 83 79 48	067 028.4	07	•	•	08	•	•	•	10	03	02	14	11	09	02	11	02	01	•	•	•	•	•	01	01		
III 6.7 7.0 4.5 6.1	-	05.3 88 57 75 73 20	036 011.4	06	•	•	11	01	•	•	07	03	02	11	07	06	01	07	02	•	•	•	•	•	01	02			
IV 5.8 8.0 6.1 6.7	-	05.6 82 55 70 69 35	050 009.8	14	•	•	08	•	•	•	10	02	03	13	12	10	•	12	02	01	•	•	•	•	•	01	02		
V 6.4 7.9 4.0 6.1	-	08.1 89 55 79 74 36	161 044.7	25	•	•	01	•	•	•	03	03	03	10	18	13	07	18	•	•	•	•	•	01	04	02			
VI 6.5 7.6 5.1 6.4	-	10.0 88 60 81 76 36	176 051.5	11	•	•	06	•	•	•	05	05	02	11	15	13	05	15	•	•	•	•	•	03	04	•			
VII 4.7 4.6 2.7 4.0	-	11.2 86 52 78 72 35	043 024.4	20	•	•	22	07	•	•	04	04	11	66	05	05	03	05	•	•	•	•	•	03	04	•			
VIII 4.5 5.1 2.0 3.8	-	12.8 96 52 88 79 27	074 022.8	24	•	•	20	15	•	•	02	01	10	04	11	10	03	11	•	•	•	•	•	13	08	•			
IX 7.6 5.7 3.5 5.6	-	10.6 97 63 93 84 41	180 039.8	30	•	•	15	•	•	•	01	01	05	08	12	10	06	12	•	•	•	•	•	07	14	•			
X 8.2 7.9 6.2 7.4	-	06.1 95 74 94 88 43	299 058.6	06	•	•	06	•	•	•	05	02	03	16	22	19	10	22	03	02	•	•	•	07	06	01			
XI 8.5 8.0 5.1 7.2	-	05.7 96 73 93 87 53	070 017.8	26	•	•	13	•	•	•	03	03	01	12	09	08	03	09	02	01	•	•	•	•	•	08	04		
XII 7.4 5.4 4.0 5.6	-	04.4 93 74 91 86 55	042 015.2	13	•	•	28	•	•	•	05	03	03	09	07	06	02	06	03	02	•	•	•	•	•	11	06		
GOD. 6.9 6.8 4.6 6.1	-	07.5 91 62 84 79 20	1306 058.6	06x	•	01	99	65	22	•	55	30	44	129	140	118	44	139	17	09	•	•	01	01	45	77	18		
DRINIĆ																													
BR. ST.107																													
I 5.4 6.7 4.6 5.6	-	04.2 91 86 91 89 63	065 025.0	20	•	04	30	•	•	•	•	•	06	09	08	03	06	07	01	•	01	•	•	•	06	31	•		
II 7.7 7.9 7.3 7.6	-	05.1 89 82 87 86 58	059 016.0	04	•	01	15	•	•	•	03	•	01	15	12	11	02	08	06	•	•	•	•	•	05	09	•		
III 6.3 7.9 6.1 6.8	-	05.1 86 66 87 80 27	043 019.3	06	•	01	15	•	•	•	01	•	02	15	07	07	01	03	05	•	•	•	•	•	04	10	•		
IV 6.5 8.3 6.5 7.1	-	06.5 84 87 88 86 62	071 029.0	14	•	•	14	•	•	•	03	13	11	11	02	08	05	01	•	•	•	•	•	01	04	•			
V 7.0 7.6 6.6 7.1	-	08.9 87 87 89 87 52	142 040.0	25	•	•	01	•	•	•	01	•	•	16	03	16	03	16	03	01	•	01	•	•	05	•	•		
VI 5.8 8.3 6.4 6.8	-	11.6 87 89 88 88 69	156 072.6	11	•	•	01	•	•	•	01	13	13	10	05	13	•	•	•	•	•	•	•	07	•	•			
VII 4.1 5.2 3.1 4.1	-	13.9 87 89 88 88 67	084 044.0	20	•	•	13	01	•	•	10	06	07	05	04	07	•	•	•	•	•	•	•	02	•	•			
VIII 3.0 5.0 3.7 3.9	-	- - - - -	132 031.1	24	•	•	16	03	•	•	14	05	12	11	05	12	•	•	•	•	•	•	•	01	08	•			
IX 5.2 5.8 5.5 5.5	-	11.5 91 90 91 91 79	169 044.9	30	•	•	01	04	•	•	07	05	10	10	06	10	•	•	•	•	•	•	•	03	03	•			
X 6.8 7.6 6.0 6.8	-	05.9 89 89 91 90 62	363 079.0	06	•	•	16	•	•	•	01	05	15	19	18	18	17	07	01	•	•	•	•	02	02	09			
XI 7.5 6.9 4.8 6.4	-	05.7 87 87 85 87 -	083 029.4	26	-	-	-	-	-	-	01	06	12	09	08	05	05	07	•	•	•	•	•	04	13	•			
XII 5.4 5.5 5.8 5.6	-	- - - - -	052 018.2	13	-	-	-	-	-	-	08	10	07	02	03	07	01	•	•	•	•	•	•	•	•	24			
GOD. 5.9 6.9 5.5 6.1	-	- - - - -	1421 079.0	06x	-	-	-	-	-	-	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
SANSKI MOST																													
BR. ST.108																													
I 9.3 8.1 6.9 8.1	043.5 04.9 96 81 95 91 56	C63 015.0	20	•	•	18	•	•	•	01	•	21	16	10	02	16	01	01	•	•	•	•	•	14	•	•			
II 6.8 7.9 6.2 7.0	085.9 05.5 93 64 84 81 34	041 006.7	04	•	•	10	•	•	•	02	01	02	13	17	12	•	17	02	01	•	•	•	•	06	•	•			
III 7.9 7.7 6.1 7.2	102.5 05.8 91 59 82 77 23	040 014.2	06	•	•	06	•	•	•	02	01	05	10	07	01	09	04	02	•	•	•	•	•	02	03	01			
IV 6.4 7.7 6.4 6.8	134.1 06.1 06.2 92 50 82 75 22	060 020.6	14	•	•	08	•	•	•	03	15	13	12	03	13	01	01	02	01	•	•	•	•	•	02	01			
V 6.5 6.6 5.1 6.1	192.1 09.0 87 55 89 77 31	108 030.3	23	•	•	06	•	•	•	04	01	03	09	17	14	03	17	•	•	•	•	•	04	•	•				
VI 5.9 7.2 5.7 6.3	191.1 11.1 85 57 84 75 38	125 050.1	11	•	•	11	02	•	•	02	01	02	08	13	10	03	13	•	•	•	•	•	04	02	•				
VII 5.6 4.5 3.2 4.3	273.4 12.7 84 54 87 76 28	088 029.5	20	•	•	22	09	•	•	02	09	06	11	06	03	11	01	03	09	•	•	•	•	03	12	•			
VIII 7.4 4.8 3.3 5.2	225.1 14.5 95 59 92 82 42	118 026.7	23	•	•	23	13	•	•	02	05	07	10	09	04	10	•	•	•	•	•	•	•	08	12	•			
IX 8.6 5.6 4.7 6.3	147.9 11.4 97 63 92 84 39	116 034.2	30	•	•	10	02	•	•	02	01	02	09	16	11	05	14	•	•	•	•	•	02	15	•				
X 8.5 7.8 6.2 7.5	081.3 06.3 92 69 91 84 36	293 061.5	04	•	•	06	•	•	•	01	01	•	16	21	18	18	20	04	03	•	•	•	03	07	02				
XI 8.0 7.0 5.4 6.8	079.1 05.8 93 69 90 84 35	077 021.0	29	•	•	10	•	•	•	02	02	03	12	14	10	02	14	02	01	•	•	•	•	09	13	•			
XII 7.5 6.6 5.6 6.6	078.6 04.9 93 74 91 86 53	066 021.5	13	•	•	23	•	•	•	01	01	02	12	12	08	02	10	05	02	•	•	•	•	09	08	•			
GOD. 7.4 6.8 5.4 6.5 6.5	-	08.2 92 61 87 80 21	1084 054.0	06x	•	•	59	72	22	•	86	17	36	133	130	118	36	128	11	07	•	•	•	07	119	07			
MLINISTE																													
BR. ST.110																													
I 7.6 7.6 8.1 7.8	-	03.5 74 74 75 74 56	069 016.4	19	•	07	28	•	•	•	•	•	18	07	07	03	03	04	01	•	•	•	•	•	11	31	•		
II 8.2 8.1 8.0 8.1	-	03.6 75 69 77 53 20	073 015.8	05	•	07	22	•	•	•	02	•	17	09	08	03	05	06	02	•	•	•	•	•	09	26	•		
III 7.2 7.9 8.0 7.7	-	04.0 68 61 71 66 2*	032 009.5	06	•	09	15	•	•	•	01	•	01	18	07	06	04	03	•	•	•	•	•	15	19	•			
IV 7.3 7.9 8.1 7.8	-	04.2 73 61 75 70 1	04 018.6	18	•	03	13	•	•	02	01	19	13	13	05	10	05	•	•	•	•	•	01	11	09	•			
V 7.6 7.7 7.7 7.8	-	06.1 72 6																											

Mjesec	Vazdušni pritisak Pr. mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova ND, fm (0-12)																	
		Tm			Sred. (Dnev.)	Max.	Min.	Max.	Min.	Dat.	Min.	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21									S.	J.	S.	J.	S.	J.	S.	J.	S.	J.	S.	J.	S.	J.			
$\varphi = 44^{\circ}03' \quad N \quad \lambda = 16^{\circ}52' \quad E$ Gr. $\Delta t = +1h\ 07\ min.$														GLAMCO												BR. ST. 111			
I	-	-01.3	04.1	-00.5	00.4	05.6	-04.4	05.2	30.12	-11.0	11	52	C1.0	01	07.0	03	05.7	03	02.3	19	03.2	15			
II	-	01.0	04.6	01.0	01.9	06.3	-01.7	11.2	17	-08.0	25	46	C1.5	06	01.3	.	.	03	07.0	01	07.0	.	.	28	01.9	.			
III	-	04.4	16.1	05.0	06.1	11.5	00.8	22.6	22	-06.2	08	50	C1.3	12	01.5	03	07.0	.	.	26	C2.2	.			
IV	-	09.4	09.6	04.4	05.7	10.9	01.5	17.2	30	-04.2	17	59	C1.6	09	03.0	22	03.0	.			
V	-	05.9	14.8	04.6	10.5	16.6	05.0	24.6	30	06.8	15	49	C1.3	09	01.4	25	02.0	.			
VI	-	15.3	17.1	14.2	14.4	19.9	07.	25.4	05	03.6	12	52	C1.1	03	02.7	02	07.0	33	07.3	.		
VII	-	11.5	17.1	16.1	17.8	23.4	16.1	31.2	16	03.6	22	40	C1.7	01	01.0	12	C2.7	.			
VIII	-	17.0	19.1	17.1	19.0	25.2	10.1	31.8	04	03.8	11	64	C1.4	04	01.5	25	C2.5	.			
IX	-	12.0	19.8	13.7	14.2	21.1	06.0	26.8	03	06.4	26	46	C1.3	01	07.0	43	03.6	.			
X	-	03.4	07.7	03.6	04.5	06.6	00.2	13.2	06	-07.4	31	30	C1.6	01	01.0	52	C2.2	.			
XI	-	05.4	10.1	06.7	01.7	05.5	-02.5	16.4	17	-14.6	29	14	C1.4	01	02.5	03	01.0	39	03.2	32		
XII	-	08.5	10.1	-05.4	-04.1	C1.4	-05.7	04.0	04	-18.0	23	55	C1.7	01	01.0	01	01.0	.	.	36	C3.3	.			
GOD.	-	10.2	11.7	05.6	07.7	13.1	02.0	31.8	04	VM -16.0	23	60	C1.4	36	02.4	.	.	03	07.0	03	05.0	07	05.6	20	03.0	362	02.7	47	
$\varphi = 44^{\circ}11' \quad N \quad \lambda = 17^{\circ}14' \quad E$ Gr. $\Delta t = +1h\ 09\ min.$														BANJA LUKA												BR. ST. 112			
I	17.6	00.1	04.1	01.1	01.8	04.8	-00.8	11.0	20	-04.9	13	28	C1.3	24	01.3	C1	C2.0	02	C1.0	02	01.5	04	C1.8	04	C1.0	30			
II	19.6	0.1	15.1	06.1	06.4	11.3	01.6	15.1	17	-04.0	09	13	C1.6	17	01.9	C1	C2.2	02	C2.0	10	03.7	05	C2.0	07	C2.0	27			
III	17.6	0.0	0.1	17.2	07.4	07.5	13.5	02.1	24.4	19	-03.9	02	19	C1.9	26	02.0	C1.3	C3.3	.	04	03.2	01	01.0	06	02.2	05	C3.0	24	
IV	17.4	0.7	14.1	08.7	09.4	15.7	03.3	22.7	29	-06.9	04	19	C2.2	18	02.6	C1.6	C3.0	05	01.0	01	02.0	01	01.0	13	C2.1	21			
V	17.6	0	11.9	19.9	15.1	14.4	10.5	08.3	27.4	31	03.2	10	16	C1.7	C1	C1.0	14	C1.9	03	01.7	10	01.6	06	03.5	14	C2.3	03	C2.7	25
VI	17.0	0.5	15.1	17.4	17.2	16.1	23.8	11.8	31.2	27	04.9	12	18	C2.1	10	C1.9	C2.4	08	01.4	09	01.3	05	03.0	11	C3.3	10	C1.8	14	
VII	17.6	0.1	17.4	15.5	16.9	20.7	26.4	13.0	34.2	27	06.0	13	11	C1.1	15	01.9	C1.9	C1.9	13	01.8	06	01.3	03	01.7	08	02.1	02	C2.5	26
VIII	17.1	0.9	17.1	19.3	19.3	20.7	27.4	16.1	33.4	04	07.7	12	07	C1.1	13	01.2	C2.5	07	01.1	05	01.8	.	.	04	02.0	04	C2.0	40	
IX	17.8	0	21.0	14.9	16.1	22.6	11.0	30.8	03	03.2	28	29	C1.4	14	01.1	C7	C2.0	02	01.6	07	01.9	01	01.0	06	02.6	07	C1.6	37	
X	17.5	0.8	11.3	06.5	07.3	12.8	02.8	22.0	04	-07.6	31	10	C1.3	10	01.7	C5	C2.3	02	01.5	08	01.4	08	02.5	15	02.0	02	C2.0	35	
XI	17.0	0.2	10.6	04.7	05.7	11.3	01.2	21.8	16	-04.1	29	18	C1.5	17	C1.2	C5	C1.0	01	01.0	06	02.8	05	01.6	04	C1.5	32			
XII	17.2	0.1	01.0	07.7	02.9	03.8	00.8	-06.9	15.4	29	-06.1	24	11	C1.5	14	01.4	C4	C1.5	05	01.2	10	01.2	08	02.1	02	01.5	04	C1.2	35
GOD.	17.6	0.1	15.6	10.1	11.0	16.6	05.6	36.2	07	VM -06.1	24	70	C1.9	167	C1.8	72	C2.0	50	01.4	78	01.7	51	02.7	93	02.4	63	01.9	341	
$\varphi = 44^{\circ}21' \quad N \quad \lambda = 17^{\circ}16' \quad E$ Gr. $\Delta t = +1h\ 09\ min.$														JAJCE												BR. ST. 113			
I	-	-06.2	-97.7	05.0	-65.7	04.6	-01.4	11.4	31	-05.2	27	*	*	*	*	C1	C1	02.0	.	*	03	02.7	C5	01.2	01	C2.0	82		
II	-	01.6	09.1	05.0	05.2	10.1	00.5	17.0	18	-04.6	10	06	C3.2	C3	01.0	13	C2.7	C2	01.0	02	07.0	02	02.0	05	03.0	47			
III	-	03.1	12.5	07.4	07.7	13.5	07.1	24.8	22	-21	-03.2	02	02	C3.5	C2	01.5	17	C2.8	C2	02.0	.	01	03.0	04	02.8	01	C1.0	64	
IV	-	05.1	17.9	09.0	08.6	14.1	03.1	27.8	29	-01.4	21	02	C4.0	C3	03.0	C6	C3.3	*	03	03.0	07	C4.4	06	02.8	01	03.0	63		
V	-	10.2	19.3	13.0	13.1	19.5	07.3	26.4	31	02.6	10	04	C5.0	C1	01.0	C6	C3.0	01	02.7	03	02.0	10	01.9	01	03.0	64			
VI	-	13.6	21.0	15.5	16.7	22.6	11.0	28.0	28	05	05.2	13	02	C3.0	C5	01.2	C7	C3	02.7	02	02.0	07	C2.1	*	.	55			
VII	-	15.5	24.9	18.0	19.1	25.5	12.1	34.8	16	07.8	09	*	*	00	02.6	C3	C2.5	*	01	03.0	03	01.7	14	C2.1	*	59			
VIII	-	15.0	23.6	18.0	19.7	27.1	13.4	33.0	03	07.8	12	04	C2.7	C7	05	C2.1	C1	01.0	05	02.0	04	01.5	03	C1.0	61				
IX	-	12.0	11.7	07.4	16.0	22.1	11.2	30.2	04	02.6	28	07	C2.4	C4	01.8	10	C2.9	C3	02.0	02	02.0	04	01.5	03	C1.3	61			
X	-	04.7	10.6	04.6	11.8	17.4	03.6	23.0	05	00.2	14	36	C2.7	C1	01.4	10	C3.4	C4	02.5	01	04.0	03	02.0	02	C2.0	65			
XI	-	07.2	19.1	04.2	05.0	01.1	01.1	19.0	16	-03.2	30	01	C1.5	C3	01.5	05	C2.2	*	01	02.0	04	02.8	02	03.5	*	73			
XII	-	-0.4	01.2	01.5	-02.1	02.6	-06.5	05.6	10	-15.4	19	24	C3.2	*	4	*	C5	03.2	01	04.0	04	04.0	12	C1.9	01	01.0	*		
GOD.</td																													

Meseč	Oblačnost Nm (0-10)	Temperatura Ljeto sati Srednje vrijednosti	Precipitacija Ljeto sati Srednje vrijednosti	Vlažnost vazduha		Podzemne vode mm	Projektni podaci na sat												R mm	•	★	●	△	▲	▲	▲	R	T	E																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
m	mm	mm	Tx	Nm (0-10)	R mm																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
				7	14	21	24	28	32	35	38	41	44	47	50	53	56	59	62	65	68	71	74	77	80	83	86	89	92	95	98	101	104	107	110	113	116	119	122	125	128	131	134	137	140	143	146	149	152	155	158	161	164	167	170	173	176	179	182	185	188	191	194	197	200	203	206	209	212	215	218	221	224	227	230	233	236	239	242	245	248	251	254	257	260	263	266	269	272	275	278	281	284	287	290	293	296	299	302	305	308	311	314	317	320	323	326	329	332	335	338	341	344	347	350	353	356	359	362	365	368	371	374	377	380	383	386	389	392	395	398	401	404	407	410	413	416	419	422	425	428	431	434	437	440	443	446	449	452	455	458	461	464	467	470	473	476	479	482	485	488	491	494	497	500	503	506	509	512	515	518	521	524	527	530	533	536	539	542	545	548	551	554	557	560	563	566	569	572	575	578	581	584	587	590	593	596	599	602	605	608	611	614	617	620	623	626	629	632	635	638	641	644	647	650	653	656	659	662	665	668	671	674	677	680	683	686	689	692	695	698	701	704	707	710	713	716	719	722	725	728	731	734	737	740	743	746	749	752	755	758	761	764	767	770	773	776	779	782	785	788	791	794	797	800	803	806	809	812	815	818	821	824	827	830	833	836	839	842	845	848	851	854	857	860	863	866	869	872	875	878	881	884	887	890	893	896	899	902	905	908	911	914	917	920	923	926	929	932	935	938	941	944	947	950	953	956	959	962	965	968	971	974	977	980	983	986	989	992	995	998	1001	1004	1007	1010	1013	1016	1019	1022	1025	1028	1031	1034	1037	1040	1043	1046	1049	1052	1055	1058	1061	1064	1067	1070	1073	1076	1079	1082	1085	1088	1091	1094	1097	1100	1103	1106	1109	1112	1115	1118	1121	1124	1127	1130	1133	1136	1139	1142	1145	1148	1151	1154	1157	1160	1163	1166	1169	1172	1175	1178	1181	1184	1187	1190	1193	1196	1199	1202	1205	1208	1211	1214	1217	1220	1223	1226	1229	1232	1235	1238	1241	1244	1247	1250	1253	1256	1259	1262	1265	1268	1271	1274	1277	1280	1283	1286	1289	1292	1295	1298	1301	1304	1307	1310	1313	1316	1319	1322	1325	1328	1331	1334	1337	1340	1343	1346	1349	1352	1355	1358	1361	1364	1367	1370	1373	1376	1379	1382	1385	1388	1391	1394	1397	1400	1403	1406	1409	1412	1415	1418	1421	1424	1427	1430	1433	1436	1439	1442	1445	1448	1451	1454	1457	1460	1463	1466	1469	1472	1475	1478	1481	1484	1487	1490	1493	1496	1499	1502	1505	1508	1511	1514	1517	1520	1523	1526	1529	1532	1535	1538	1541	1544	1547	1550	1553	1556	1559	1562	1565	1568	1571	1574	1577	1580	1583	1586	1589	1592	1595	1598	1601	1604	1607	1610	1613	1616	1619	1622	1625	1628	1631	1634	1637	1640	1643	1646	1649	1652	1655	1658	1661	1664	1667	1670	1673	1676	1679	1682	1685	1688	1691	1694	1697	1700	1703	1706	1709	1712	1715	1718	1721	1724	1727	1730	1733	1736	1739	1742	1745	1748	1751	1754	1757	1760	1763	1766	1769	1772	1775	1778	1781	1784	1787	1790	1793	1796	1799	1802	1805	1808	1811	1814	1817	1820	1823	1826	1829	1832	1835	1838	1841	1844	1847	1850	1853	1856	1859	1862	1865	1868	1871	1874	1877	1880	1883	1886	1889	1892	1895	1898	1901	1904	1907	1910	1913	1916	1919	1922	1925	1928	1931	1934	1937	1940	1943	1946	1949	1952	1955	1958	1961	1964	1967	1970	1973	1976	1979	1982	1985	1988	1991	1994	1997	1999	2002	2005	2008	2011	2014	2017	2020	2023	2026	2029	2032	2035	2038	2041	2044	2047	2050	2053	2056	2059	2062	2065	2068	2071	2074	2077	2080	2083	2086	2089	2092	2095	2098	2101	2104	2107	2110	2113	2116	2119	2122	2125	2128	2131	2134	2137	2140	2143	2146	2149	2152	2155	2158	2161	2164	2167	2170	2173	2176	2179	2182	2185	2188	2191	2194	2197	2200	2203	2206	2209	2212	2215	2218	2221	2224	2227	2230	2233	2236	2239	2242	2245	2248	2251	2254	2257	2260	2263	2266	2269	2272	2275	2278	2281	2284	2287	2290	2293	2296	2299	2302	2305	2308	2311	2314	2317	2320	2323	2326	2329	2332	2335	2338	2341	2344	2347	2350	2353	2356	2359	2362	2365	2368	2371	2374	2377	2380	2383	2386	2389	2392	2395	2398	2401	2404	2407	2410	2413	2416	2419	2422	2425	2428	2431	2434	2437	2440	2443	2446	2449	2452	2455	2458	2461	2464	2467	2470	2473	2476	2479	2482	2485	2488	2491	2494	2497	2500	2503	2506	2509	2512	2515	2518	2521	2524	2527	2530	2533	2536	2539	2542	2545	2548	2551	2554	2557	2560	2563	2566	2569	2572	2575	2578	2581	2584	2587	2590	2593	2596	2599	2602	2605	2608	2611	2614	2617	2620	2623	2626	2629	2632	2635	2638	2641	2644	2647	2650	2653	2656	2659	2662	2665	2668	2671	2674	2677	2680	2683	2686	2689	2692	2695	2698	2701	2704	2707	2710	2713	2716	2719	2722	2725	2728	2731	2734	2737	2740	2743	2746	2749	2752	2755	2758	2761	2764	2767	2770	2773	2776	2779	2782	2785	2788	2791	2794	2797	2800	2803	2806	2809	2812	2815	2818	2821	2824	2827	2830	2833	2836	2839	2842	2845	2848	2851	2854	2857	2860	2863	2866	2869	2872	2875	2878	2881	2884	2887	2890	2893	2896	2899	2902	2905	2908	2911	2914	2917	2920	2923	2926	2929	2932	2935	2938	2941	2944	2947	2950	2953	2956	2959	2962	2965	2968	2971	2974	2977	2980	2983	2986	2989	2992	2995	2998	3001	3004	3007	3010	3013	3016	3019	3022	3025	3028	3031	3034	3037	3040	3043	3046	3049	3052	3055	3058	3061	3064	3067	3070	3073	3076	3079	3082	3085	3088	3091	3094	3097	3100	3103	3106	3109	3112	3115	3118	3121	3124	3127	3130	3133	3136	3139	3142	3145	3148	3151	3154	3157	3160	3163	3166	3169	3172	3175	3178	3181	3184	3187	3190	3193	3196	3199	3202	3205	3208	3211	3214	3217	3220	3223	3226	3229	3232	3235	3238	3241	3244	3247	3250	3253	3256	3259	3262	3265	3268	3271	3274	3277	3280	3283	3286	3289	3292	3295	3298	3301	3304	3307	3310	3313	3316	3319	3322	3325	3328	3331	3334	3337	3340	3343	3346	3349	3352	3355	3358	3361	3364	3367	3370	3373	3376	3379	3382	3385	3388	3391	3394	3397	3400	3403	3406	3409	3412	3415	3418	3421	3424	3427	3430	3433	3436	3439	3442	3445	3448	3451	3454	3457	3460	3463	3466	3469	3472	3475	3478	3481	3484	3487	3490	3493	3496

Mesec	Oblačnost Nm (0-10)			Inovacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na se:																									
	7	14	21		L m s			Tn =	Tx =	Tn =	Tx =	Tx =	F(0-12)			Nm(0-10)			R mm			●	★	▲	▲	▲	T	≡	■							
					Sred. Sred. (tobi)	7	14	21	Sred.	Min	Σ	Nm	Dat.	10.00.0	0.0250.0	0.020.0	6	8	2.0.8.0	0.1.1.0.0.0	15	16	17	18	19	20	21	22								
BR. ST.116 BUGAĆIĆ																																				
I	9.7	8.0	6.3	8.0	-	042.8	043.3	53	81	92	89	54	049.011.6	20	-	01	22	-	-	04	01	20	15	68	01	12	16	04	-	-	18	05				
II	8.1	7.3	6.9	7.4	-	094.3	046.6	90	62	78	77	43	066.034.9	04	-	01	14	-	-	14	01	01	14	13	67	01	12	05	01	-	-	01	01			
III	7.4	7.3	6.1	6.9	-	124.7	048.8	89	51	74	71	16	019.004.6	07	-	01	19	-	-	06	01	12	14	69	04	06	03	-	-	-	02	03				
IV	6.4	8.1	7.3	7.3	-	124.8	052.8	86	52	71	70	30	033.007.6	16	-	01	10	-	-	11	01	15	15	69	01	15	04	03	-	-	-	01	05			
V	7.6	7.6	6.6	7.0	-	156.6	073.3	89	52	79	73	31	113.025.6	23	-	01	01	-	-	01	02	09	23	13	05	23	-	-	-	-	-	-	05	12		
VI	7.5	7.5	6.6	7.2	-	157.0	094.4	87	52	79	73	33	080.025.6	11	-	01	06	-	-	10	01	12	17	68	04	17	-	-	-	-	-	-	08	12		
VII	6.0	5.2	3.6	6.2	-	243.0	10.3	87	49	74	70	27	056.037.5	20	-	01	19	09	-	10	05	07	08	04	02	08	-	-	-	-	-	-	02	13		
VIII	6.9	5.0	3.4	5.1	-	239.0	11.3	94	46	83	75	23	064.015.6	27	-	01	14	11	-	06	01	08	10	68	04	10	-	-	-	-	-	-	11	21		
IX	8.7	5.3	4.6	6.2	-	155.6	10.2	94	57	88	79	41	076.012.4	08	-	01	06	-	-	09	01	01	07	15	10	03	13	-	-	-	-	-	01	07	13	
X	8.6	7.8	7.5	8.0	-	089.8	05.9	92	67	90	83	39	243.040.4	01	-	01	10	-	-	07	01	20	22	11	22	03	02	-	-	-	-	-	05	05		
XI	9.4	7.4	5.5	7.4	-	062.3	05.0	96	23	91	87	42	063.020.8	29	-	01	19	-	-	04	01	14	16	11	02	14	06	04	-	-	-	-	-	19	06	
XII	9.5	7.6	7.4	8.2	-	046.1	03.9	92	88	92	90	54	046.019.2	13	06	10	28	-	-	08	01	21	12	07	01	11	04	03	-	-	-	-	-	22	23	
GOD.	8.0	7.0	5.9	7.0	-	1530.0	06.9	90	60	82	78	16	908.040.4	0X	06	12	119	53	20	-	07	02	21	157	174	109	34	163	35	17	01	-	-	01	42	149
BR. ST.117 TRAVNIK																																				
I	9.0	6.9	6.2	8.7	-	04.1	91	87	89	89	58	082.029.2	20	-	06	-	-	-	-	-	01	23	12	09	04	08	07	01	-	-	-	20	07			
II	7.9	7.0	5.5	6.6	-	-	-	-	-	-	-	-	067.026.0	04	-	01	-	-	-	-	04	11	08	06	03	07	03	01	-	-	-	01	04			
III	7.0	6.7	5.5	6.6	-	05.4	83	58	80	74	-	051.015.0	06	-	01	-	-	-	-	04	12	08	07	02	05	04	-	-	-	-	02	04				
IV	5.8	5.5	5.7	6.6	-	05.6	86	59	76	74	32	044.008.0	14	-	04	-	-	-	-	04	11	15	12	-	15	03	03	-	-	-	01	01				
V	6.6	7.4	5.5	6.6	-	07.6	88	56	82	75	29	137.033.0	23	-	-	-	-	-	-	01	12	19	17	04	15	-	-	-	-	-	03	05				
VI	5.5	7.0	7.0	6.5	-	09.7	89	60	76	75	40	131.037.0	11	-	-	07	-	-	-	01	09	15	14	03	15	-	-	-	-	-	03	04				
VII	3.7	4.6	3.6	4.0	-	11.1	90	60	79	76	28	099.046.5	20	-	-	16	06	-	-	14	07	10	08	04	10	-	-	-	-	-	01	04				
VIII	4.1	4.0	2.9	3.7	-	11.8	90	53	83	76	18	059.020.2	24	-	-	18	09	-	-	12	04	09	07	03	09	-	-	-	-	-	05	05				
IX	7.6	6.0	4.0	4.2	6.0	-	10.4	94	64	83	80	43	074.014.5	26	-	-	06	-	-	01	-	03	09	12	11	02	12	-	-	-	-	-	03	14		
X	8.2	7.6	7.6	7.8	-	05.9	92	73	87	84	30	225.030.0	01	-	-	-	-	-	-	02	17	22	20	10	22	05	04	-	-	-	01	15	03			
XI	8.2	7.2	5.6	7.0	-	05.0	93	79	86	84	54	066.013.0	01	-	-	-	-	-	-	-	-	-	11	10	03	06	06	03	-	-	-	-	-	13	05	
XII	9.3	8.3	7.9	8.5	-	04.0	94	91	88	91	52	044.018.5	13	05	06	27	-	-	-	-	18	14	05	02	11	05	01	-	-	-	-	-	17	20		
GOD.	6.9	6.8	5.8	6.5	-	-	-	-	-	-	-	1059.046.5	20M	-	-	-	-	-	-	02	-	-	-	155	130	40	141	33	13	-	-	-	-	-	20	110
BR. ST.118 PRAJAVOR																																				
I	9.9	5.0	7.5	8.8	-	04.4	85	62	88	P5	51	077.020.0	20	-	01	17	-	-	-	05	19	13	11	02	13	01	-	-	-	-	-	21	-			
II	7.7	8.0	5.2	7.0	-	04.6	86	60	73	73	20	039.015.0	04	-	01	13	-	-	-	08	13	11	10	01	11	02	01	-	-	-	-	-	04			
III	6.6	7.2	5.4	6.4	-	05.2	81	52	74	69	12	056.023.0	07	-	01	08	02	-	-	03	13	06	04	02	04	06	04	-	-	-	-	-	01	01		
IV	6.5	8.0	4.0	4.9	6.5	-	05.5	80	47	67	65	18	093.024.0	18	-	01	03	-	-	-	02	08	11	10	03	11	01	-	-	-	-	-	04			
V	6.6	7.4	5.5	6.6	-	07.9	78	54	68	66	29	141.024.5	23	-	-	05	-	-	01	-	02	11	19	18	05	19	-	-	-	-	-	01	08			
VI	5.6	6.6	6.6	6.6	-	10.0	80	51	75	68	30	163.051.0	11	-	-	-	-	-	01	-	09	12	12	07	12	-	-	-	-	-	03	03				
VII	4.4	5.1	3.6	4.3	-	11.6	76	50	75	68	30	104.034.5	20	-	-	19	09	-	-	01	-	06	09	09	05	09	-	-	-	-	-	01	09	02		
VIII	3.2	4.2	3.9	3.8	-	12.9	87	52	76	72	29	089.037.0	24	-	-	20	12	-	-	01	-	12	20	10	02	10	-	-	-	-	-	01	04			
IX	7.6	6.0	5.6	6.1	-	10.6	91	60	78	76	38	130.031.0	21	-	-	10	01	-	-	04	-	10	13	12	05	13	-	-	-	-	-	04	11			
X	6.0	8.0	6.4	7.4	-	06.3	87	72	81	80	47	260.041.0	06	-	-	03	-	-	-	01	-	16	20	20	09	20	02	02	-	-	-	-	-	02	05	
XI	7.8	7.0	5.5	6.9	-	05.2	84	68	77	84	46	126.031.0	08	-	-	10	-	-	-	02	-	14	12	12	05	12	03	02	-	-	-	-	-	04	09	
XII	7.8	6.6	6.9	7.2	-	04.5	91	73	82	79	52	051.014.0	13	01	16	-	-	-	02	-	16	11	11	02	06	05	-	-	-	-	-	03	19			
GOD.	6.3	6.4	5.8	6.1	-	08.1	94	68	93	85	03	1243.070.2	20M	-	-	79	53	22	-	-	45	125	147	132	44	142	20	13	-	-	-	-	-	22	49	
BR. ST.120 ZENICA																																				
I	5.3	6.2	7.1	8.2	-	019.0	04.6	90	80	91	87	54	072.028.3	20	-	-	21	-	-	-	02	15	68	03	12	07	03	-	-	-	-	-	03	02		

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetroa mD, Pm (0-12)																
		Tm				Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21	Sred. (Dies)							8.	15.	22.	Dat.	8.	15.	22.	Dat.	8.	15.	22.	Dat.	8.	15.	22.	Dat.	
$\varphi = 44^{\circ}44'$ N $\lambda = 18^{\circ}06'$ E Gr. $\Delta G = +1h\ 12\ min.$																												
I	-	00.3	05.0	01.6	02.1	05.4	-00.4	11.2	31.27	-04.8	27	.	.	02	01.0	C8	01.6	C7	01.7	03	C1.0	08	01.1	12	01.6	02	C1.5	51
II	-	02.8	10.9	05.4	06.1	11.8	01.6	19.2	12	-04.2	28	01	C2.0	03	02.0	06	01.7	C4	02.2	07	02.3	11	01.4	09	01.2	02	C1.5	41
III	-	03.5	13.9	07.7	08.2	14.4	02.0	26.8	19	-03.4	02	02	01.0	10	01.7	13	02.6	08	01.6	02	01.0	01	01.0	02	01.0	08	01.9	47
IV	-	06.3	14.8	08.6	09.7	16.1	03.9	24.8	28	-01.2	04	02	C1.0	10	01.2	C1	03.0	03	02.3	05	01.8	01	02.0	08	02.0	57		
V	-	11.0	19.1	12.7	14.0	20.0	08.8	28.0	31	01.7	10	.	.	06	01.8	C3	C1.3	05	01.6	04	02.5	11	02.1	12	01.8	03	03.0	49
VI	-	15.3	22.3	16.5	17.6	23.5	12.3	30.5	27	04.5	13	03	C2.7	C2	01.5	02	02.0	10	01.4	06	01.5	26	02.0	06	02.2	39		
VII	-	16.8	24.9	18.6	19.7	26.3	13.6	36.5	17	06.8	03	02	02.5	06	02.0	C3	01.7	06	01.5	07	02.0	08	01.5	09	01.6	04	02.0	48
VIII	-	16.8	27.0	19.2	20.6	27.8	14.7	34.5	04	08.0	12	01	02.0	06	02.0	04	01.8	09	02.0	03	01.7	06	01.3	08	01.2	01	C3.0	55
IX	-	14.9	22.2	15.2	16.6	22.9	12.3	30.2	04	03.6	28	.	.	08	01.9	C3	02.0	10	01.6	01	01.0	03	01.3	05	01.4	13	C1.5	47
X	-	05.6	11.7	07.0	07.8	13.1	04.0	22.8	04	-01.2	31	.	.	04	02.0	02	01.0	04	01.8	07	01.9	07	01.3	17	01.7	04	C1.8	48
XI	-	02.9	10.9	04.4	05.6	11.6	01.7	21.3	16	-02.6	30	.	.	02	01.0	C4	01.5	08	01.8	08	01.5	12	01.3	05	02.0	03	01.7	48
XII	-	01.0	06.0	02.6	03.0	06.8	-00.2	13.4	29	-06.6	24	03	C1.3	04	01.5	04	02.0	16	01.6	02	01.0	02	01.0	01	02.0	06	02.2	55
GOD.	-	08.1	15.7	10.9	10.6	16.6	06.4	36.5	Pm	-06.6	24.VII	14	01.8	C3	01.8	53	02.0	82	01.7	57	01.7	80	01.5	101	01.7	60	01.9	585
$\varphi = 44^{\circ}59'$ N $\lambda = 18^{\circ}18'$ E Gr. $\Delta G = +1h\ 13\ min.$																										MODRICA		
BR. ST.122																												
I	-	00.5	02.9	01.3	01.5	03.9	-01.3	05.6	21	-06.8	15	00	C2.5	04	C2.0	14	01.5	10	01.2	01	01.0	04	01.5	04	01.5	16	C1.0	27
II	-	02.8	10.2	05.4	06.0	11.1	C0.8	17.5	12	-04.0	28	13	02.2	12	C1.8	C7	02.1	11	01.5	03	02.3	06	01.7	05	01.4	19	C1.3	49
III	-	03.8	12.9	07.2	07.8	13.5	02.0	25.5	19	-04.0	02	06	C1.3	18	C1.3	10	02.0	19	02.3	01	02.0	06	01.2	06	01.5	10	C1.3	17
IV	-	07.3	14.6	08.2	09.6	15.4	03.9	23.4	28	-06.4	04	07	C1.1	07	C3.0	18	01.9	08	01.9	.	.	15	01.3	12	01.5	11	C2.3	12
V	-	13.1	19.0	13.2	14.6	19.7	08.5	27.4	31	03.7	02	06	01.5	C8	01.5	C3	02.0	05	01.4	.	.	09	01.4	11	01.6	37	C1.9	19
VI	-	16.8	21.9	16.9	17.1	22.6	12.1	30.3	27	06.7	10.0	09	C3.0	C4	01.4	C3	01.7	03	01.0	.	.	05	01.2	11	01.4	36	C2.2	21
VII	-	18.5	24.6	19.2	20.4	25.7	12.8	34.8	27.14	05.2	27	04	01.2	07	C1.1	C3	01.0	12	01.6	01	01.0	09	C4.0	03	01.8	26	C1.8	26
VIII	-	18.8	26.6	20.7	21.7	27.3	13.4	34.0	04	10.4	29	05	04.4	12	C3.2	C5	02.6	11	01.9	01	01.0	03	01.3	02	01.5	29	C1.4	26
IX	-	14.6	21.5	16.5	17.3	22.2	11.5	30.2	C3	03.7	28	04	01.8	07	01.3	12	01.6	05	01.6	01	01.0	05	01.2	02	01.5	25	C1.3	27
X	-	06.0	11.2	07.8	08.2	12.2	C3.4	21.2	04	-02.1	31	05	C1.6	04	01.2	07	01.9	10	01.3	.	.	09	01.4	10	01.5	24	C1.4	24
XI	-	02.8	09.8	05.4	05.8	10.5	01.4	20.5	16	-02.4	28	01	01.0	07	01.8	05	01.0	04	01.0	01	01.0	09	01.3	07	01.7	40		
XII	-	02.1	06.2	03.1	03.6	07.0	-00.2	15.5	29	-05.4	25	10	C1.7	.	.	01	02.0	04	01.2	01	01.0	06	01.0	19	C1.3	30	C1.6	21
GOD.	-	08.9	15.1	10.4	11.2	16.0	05.7	34.0	Pm	-07.4	15.I	71	C1.4	04	01.6	54	01.8	102	01.6	10	01.8	85	01.3	92	C1.5	276	C1.7	269
$\varphi = 44^{\circ}11'$ N $\lambda = 18^{\circ}20'$ E Gr. $\Delta G = +1h\ 14\ min.$																										PONIKVE		
BR. ST.123																												
I	-	-02.8	04.3	-01.5	-00.3	05.5	-03.5	09.0	24	-10.0	13	24	C1.0	01	01.0	.	.	C1	01.0	05	C1.0	.	.	62
II	-	-01.8	04.4	-01.1	00.1	05.6	-02.5	05.5	17	-05.4	09	20	C1.0	08	01.2	13	C1.5	.	.	43	
III	-	00.0	09.8	02.9	04.9	11.0	-00.6	23.0	22	-05.0	12.0	01	01.0	09	01.0	05	01.0	.	01	01.0	.	07	01.0	.	.	64		
IV	-	02.6	11.4	02.7	04.9	12.0	01.8	21.0	06	-01.2	19	17	C1.1	07	C1.0	01	01.0	05	01.2	02	01.0	.	07	01.0	.	.	46	
V	-	06.4	15.1	05.2	06.0	16.7	04.4	23.4	26	02.2	10	04	01.0	09	01.0	02	01.0	02	01.0	02	01.0	.	.	13	C1.0	01	01.0	62
VI	-	10.2	17.4	11.6	12.7	20.7	07.8	28.0	31	02.8	10	01	01.0	01	01.0	18	01.6	C5	02.8	.	.	.	01	01.0	23	C1.3	40	
VII	-	14.8	20.9	14.4	16.1	22.1	11.0	30.6	27	04.2	13	.	.	03	01.0	C1	01.0	01	01.0	02	01.0	.	.	02	01.0	20	C1.3	37
VIII	-	16.0	23.7	16.1	18.0	25.1	12.3	35.0	17	06.0	09	03	C1.0	01	01.0	19	01.6	01	02.0									

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha em	Padavine R mm				Broj dana na sat:																				
	Temperatura Iznosljivosti Broj sati					Tn	Tx	Tn	Tx	Tn	Tx	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	R	—	■						
	7	14	21	Sred. (Dnev.)	mm	7	14	21	Stred. Min.	Σ	X	at.	-10.00.0	0.025.0	0.00.0.6	8	2.0	8.0	0.1	1.00.0.0	•	Δ	*	Δ	▲	▲	T	—	■	
BR. ST.121																														
DOBOJ																														
I	9.0	7.8	6.3	7.7	044.8	04.9	95	83	94	91	56	087	034.2	20	•	•	18	•	•	•	•	01	18	15	09	03	15	01	01	
II	7.0	7.6	6.9	7.1	089.1	05.6	92	63	85	80	40	030	035.4	04	•	•	08	•	•	•	•	02	13	13	06	01	13	•	•	
III	6.4	6.5	5.7	6.2	121.6	06.2	93	58	79	77	17	018	007.9	07	•	•	07	02	•	•	•	03	13	06	04	04	02	•	03	
IV	6.1	7.4	4.9	6.2	140.8	06.6	91	54	80	75	26	068	C13.4	14	•	•	05	•	•	•	•	01	63	C1	12	10	02	12	01	04
V	5.5	7.2	5.2	6.1	174.6	05.7	97	90	61	89	40	129	026.0	23	•	•	•	06	•	•	•	01	03	09	20	16	05	20	•	01
VI	5.9	6.6	4.8	5.8	160.3	12.0	89	60	88	79	44	177	042.0	11	•	•	12	01	•	•	•	02	10	13	13	08	13	•	05	
VII	3.9	4.4	3.0	3.8	249.3	13.1	87	57	85	76	37	121	049.4	20	•	•	19	09	•	•	•	13	04	12	09	03	12	•	04	
VIII	4.5	4.3	3.1	4.0	237.4	14.5	95	56	85	80	40	065	C24.8	12	•	•	22	12	•	•	•	10	03	12	06	12	12	•	09	
IX	7.5	6.0	4.1	5.9	141.1	12.3	97	66	92	85	43	106	C24.2	21	•	•	•	10	02	•	01	•	02	06	12	10	03	12	•	
X	8.6	7.0	6.6	7.4	091.1	07.0	95	73	92	87	44	159	C19.9	29	•	•	02	•	•	•	•	01	15	20	19	07	20	•	02	
XI	7.4	6.1	5.1	6.2	086.1	06.0	95	70	94	86	52	065	G13.1	29	•	•	09	•	•	•	01	01	04	11	11	12	03	03	11	
XII	8.8	6.1	6.5	7.2	062.5	05.2	96	80	92	90	59	058	C14.6	13	•	•	17	•	•	•	01	13	14	12	01	13	05	04	11	
GOD.	6.6	6.4	5.2	6.1	1598.7	06.6	92	65	88	82	17	1091	C49.4	20VI	•	•	66	71	24	•	04	02	45	124	161	125	38	158	14	11
MODRIČA																														
BR. ST.122																														
I	8.7	8.7	7.5	8.3	-	04.6	93	86	92	90	54	062	022.5	20	•	01	21	•	•	•	01	•	01	19	12	07	03	10	02	13
II	6.7	6.0	5.1	5.9	-	05.6	91	64	85	80	36	029	008.5	04	•	•	10	•	•	•	02	09	10	07	•	10	01	01	02	•
III	5.6	5.5	4.9	5.3	-	05.9	90	56	81	76	22	019	004.3	08	•	•	09	01	•	•	•	06	10	06	04	•	06	04	02	•
IV	5.5	6.2	6.5	6.1	-	06.5	82	51	84	72	28	085	C36.7	14	•	•	01	•	•	•	01	04	08	11	03	11	01	•	02	
V	5.3	6.0	5.1	5.4	-	09.6	84	60	83	76	41	078	022.5	25	•	•	•	04	•	•	04	01	04	05	18	15	02	18	•	05
VI	5.3	5.2	5.4	5.5	-	11.6	62	58	80	73	40	122	045.0	11	•	•	11	01	•	01	•	03	07	15	14	03	15	•	06	•
VII	4.1	4.2	4.7	4.3	-	13.2	63	57	80	73	25	086	032.0	20	•	•	17	07	•	•	12	06	11	08	02	11	•	04	•	
VIII	3.2	3.3	3.4	3.3	-	14.4	67	57	79	74	38	085	030.5	26	•	•	15	12	•	01	•	15	04	13	10	02	13	•	08	
IX	6.4	4.8	4.8	5.3	-	12.4	91	68	88	83	40	072	026.3	05	•	•	07	01	•	01	•	04	06	10	06	02	10	•	01	02
X	8.2	7.1	6.6	7.3	-	07.1	92	77	91	87	49	156	C24.6	06	•	•	03	•	•	•	02	18	20	17	07	20	•	02	05	
XI	7.5	6.2	5.3	6.4	-	06.0	94	74	90	86	45	061	016.9	09	•	•	07	•	•	01	•	05	13	10	08	02	10	01	•	
XII	8.1	6.5	5.3	6.7	-	05.3	89	79	92	87	49	065	C19.8	19	•	•	17	•	•	•	02	11	13	10	07	11	03	•	02	
GOD.	6.6	5.9	5.4	5.8	-	08.5	88	65	85	79	22	920	C45.0	44VI	•	01	68	59	21	•	10	01	60	115	149	118	28	145	14	01
PORNIEVE																														
BR. ST.123																														
I	6.5	6.4	6.2	6.4	-	-	-	-	-	-	-	148	035.0	16	01	•	27	•	•	•	03	12	12	11	04	07	08	•	•	
II	6.7	6.2	6.9	6.6	-	-	-	-	-	-	-	102	028.5	04	•	•	25	•	•	•	02	11	10	10	03	07	08	04	•	
III	4.9	5.2	5.2	5.1	-	-	-	-	-	-	-	048	010.2	08	•	•	15	•	•	•	08	09	08	08	01	02	06	•	07	
IV	6.0	6.6	6.7	6.6	-	05.0	91	50	93	78	24	101	C13.5	19	•	•	01	•	•	•	02	09	16	13	03	10	07	01	15	
V	5.6	6.0	6.5	6.0	-	05.9	86	41	93	73	23	194	C28.5	23	•	•	•	•	•	•	02	10	17	17	07	17	•	01	15	
VI	4.9	5.1	5.5	5.2	-	-	-	-	-	-	-	166	040.0	30	•	•	-	•	•	•	03	05	14	14	04	14	•	02	•	
VII	3.5	4.1	4.6	4.2	-	08.4	66	37	89	70	17	101	G20.0	22	•	•	16	07	•	•	11	05	10	10	05	10	•	01	01	
VIII	3.4	3.4	4.7	3.8	-	11.2	87	56	91	78	23	104	C17.5	26	•	•	15	07	•	01	06	01	13	13	06	13	01	04	04	
IX	5.9	5.6	6.8	6.1	-	08.5	90	48	92	77	23	097	C21.0	27	•	•	04	•	•	•	07	12	12	02	12	12	•	02	24	
X	7.5	7.5	7.7	7.6	-	-	-	-	-	-	-	186	024.3	24	•	•	-	•	•	•	14	18	18	18	08	14	05	26	05	
XI	5.5	5.6	6.9	6.6	-	-	-	-	-	-	-	084	023.0	29	•	•	03	•	•	•	08	09	09	02	02	08	06	•	17	
XII	7.1	7.3	7.2	7.2	-	-	-	-	-	-	-	136	G26.0	19	•	•	02	•	•	•	14	13	13	07	06	10	03	•	27	
GOD.	5.4	5.9	4.8	5.4	-	07.7	84	63	88	79	12	1330	058.6	02VI	•	01	56	57	22	•	05	02	90	108	170	129	51	159	36	17
MAGAČA																														
BR. ST.124																														
I	6.2	6.2	4.6	5.7	-	04.5	88	77	89	85	12	104	055.4	20	•	•	19	•	•	•	04	09	12	06	03	11	06	04	•	05
II	5.9	6.4	4.8	5.9	-	04.5	88	58	86	76	29	080	G27.2	04	•	•	08	•	•	•	05	09	12	04	02	08	04	•	06	01
III	5.6	5.5	4.6	5.2	-	05.5	80	53	82	72	13	017	005.6	08	•	•	07	•	•	•	10	11	11	04	06	07	02	•	02	01
IV	6.1	7.1	6.0	6.4	-	05.8	8																							

Mesec	Vardušni pritisak Pn mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova m/s, Pm (0-12)																						
		Tm			Max				Dat.			Min			Dat.			N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.							
$\psi = 44^{\circ}57'$ N $\lambda = 18^{\circ}50'$ E Gr. $\Delta G = +1h\ 15\ min.$																																		
I	-	01.2	03.4	01.7	02.0	-	-01.0	-	-	-06.8	16	03	02.3	*	*	01	03.0	*	*	03	02.7	18	02.5	*	*	06	03.0	47						
II	-	04.3	10.6	05.2	06.3	-	06.9	-	-04.0	28	02	02.0	02	02.0	16	02.8	02	02.0	01	02.0	05	04.8	06	02.2	01	03.0	47							
III	-	05.3	13.5	07.6	08.5	14.4	02.0	27.0	19	-04.0	02	*	*	39	03.2	06	03.7	07	02.0	*	*	04	02.6	*	*	42								
IV	-	08.4	14.3	09.5	10.7	16.6	-	24.6	29	-	-06	02.2	02	02.0	24	02.6	03	03.7	03	02.3	08	02.2	17	07.8	15	02.7	12							
V	-	13.7	19.1	13.0	14.7	20.6	-	28.5	31	-	-07	02.4	*	*	09	02.4	03	03.0	02	02.0	03	04.3	36	02.4	06	03.7	27							
VI	-	19.1	22.6	16.9	18.8	24.5	-	31.5	27	-	-07	02.3	*	*	02	02.5	*	*	11	02.5	03	02.0	32	02.6	13	04.1	22							
VII	-	19.5	25.5	18.6	20.6	27.0	-	36.0	17	-	-	02	02.0	22	01.7	05	01.8	04	01.5	09	01.7	34	02.5	02	02.5	15								
VIII	-	20.0	27.7	20.0	21.9	28.6	14.6	36.0	04	10.0	31.0	08	03.0	02	04.5	35	01.6	06	02.2	05	01.0	*	*	19	03.0	03	02.0	21						
IX	-	15.9	22.4	15.9	17.5	23.6	11.3	30.0	04.0	03	05.0	30.28	15	01.4	04	01.8	12	01.8	04	02.2	02	03.5	*	*	30	02.6	05	03.2	18					
X	-	08.1	11.7	07.4	08.7	13.1	03.7	22.0	04	00.0	20.18	01	03.0	*	*	22	01.5	04	02.6	06	03.8	07	02.4	44	02.2	*	*	09						
XI	-	04.3	10.6	04.1	05.8	11.3	01.3	21.5	16	-03.0	28	05	03.0	*	*	24	01.7	04	01.8	03	02.7	09	01.7	16	02.1	*	*	19						
XII	-	01.9	06.1	02.4	03.2	07.4	-00.3	14.0	27	-05.5	25	01	02.0	*	*	17	01.2	03	01.3	03	01.0	09	01.3	36	01.9	*	*	24						
GOD.	-	10.1	15.7	10.2	11.6	-	-	-	-	-	49	02.1	12	02.4	22.3	02.1	46	02.4	42	02.3	56	02.3	294	02.4	45	03.0	34							
$\psi = 44^{\circ}12'$ N $\lambda = 18^{\circ}57'$ E Gr. $\Delta G = -1h\ 10\ min.$																																		
I	-	00.1	02.6	00.7	01.0	03.5	-01.8	09.2	31	-06.8	17	*	*	04	01.0	08	01.0	06	01.0	12	01.1	14	01.2	15	01.4	68	01.6	26						
II	-	02.9	08.1	04.5	05.0	05.8	01.3	15.6	17	-06.0	28	02	01.5	09	01.3	10	01.2	14	01.7	05	01.2	14	01.1	11	02.4	08								
III	-	05.3	11.3	06.3	07.3	11.8	02.6	23.6	21	-05.6	01	02	02.5	19	01.1	20	01.4	15	01.4	15	02.8	04	01.5	10	02.0	05								
IV	-	07.3	11.7	07.0	08.2	12.8	04.2	21.6	28	-06.6	17	03	01.7	07	01.4	09	01.7	12	02.1	13	01.2	10	01.1	13	01.4	66								
V	-	12.4	16.2	11.5	12.9	17.5	08.1	23.0	31	04.6	16.10	03	01.3	16	01.4	06	01.3	06	01.7	07	01.3	14	02.5	15	01.3	13	02.1	13						
VI	-	16.2	18.7	15.0	16.2	20.1	11.5	28.0	27	05.6	13	01	01.0	06	01.0	04	01.0	08	01.4	04	01.0	20	01.8	21	01.4	10	01.9	16						
VII	-	18.1	23.1	17.7	19.1	24.0	13.3	36.4	17	08.4	20.09	04	01.0	10	01.4	06	01.3	03	01.0	05	01.0	19	01.1	16	01.2	07	01.6	19						
VIII	-	18.6	24.6	18.0	19.9	-	14.6	-	-05.4	12	02	01.5	10	01.1	04	01.2	05	01.0	14	01.1	13	01.2	16	01.1	14	02.5	13							
IX	-	14.9	19.8	14.5	16.0	20.9	11.4	26.6	28	05.2	*	*	*	*	*	*	06	01.2	08	01.1	07	01.4	15	01.0	07	01.4	15	01.0	05	01.7	26			
X	-	05.6	09.8	05.5	06.9	11.3	03.3	19.6	31	03	01.0	08	01.6	08	01.0	06	02.4	08	01.0	08	02.2	17	01.2	17	01.4	14								
XI	-	04.2	08.2	04.8	05.5	09.4	02.1	17.4	16	-03.8	28	01	02.0	04	01.2	06	01.5	14	01.5	07	01.3	13	01.5	17	01.2	13	01.4	15						
XII	-	01.8	04.1	02.3	02.7	05.0	-00.5	13.6	29	-05.8	18	04	01.2	07	01.6	04	01.0	07	01.4	12	01.4	16	01.2	23	01.3	07	01.7	15						
GOD.	-	09.0	13.2	09.0	10.1	-	05.8	-	-06.8	77	1	25	01.4	106	01.5	91	01.3	102	01.6	122	01.7	157	01.7	187	01.3	120	01.6	104						
$\psi = 44^{\circ}47'$ N $\lambda = 19^{\circ}16'$ E Gr. $\Delta G = +1h\ 17\ min.$																																		
I	-	00.1	04.4	01.6	01.9	05.2	-00.6	10.3	22	-06.6	15	01	02.0	02	01.5	27	01.4	06	01.2	01	01.0	01	01.0	07	01.1	07								
II	-	02.8	10.7	04.9	05.9	11.6	01.4	18.4	12	-05.2	14	*	*	*	*	06	01.7	05	02.2	09	01.2	19	01.6	13	01.0	07	01.1	21						
III	-	03.7	13.6	07.5	08.1	14.1	02.2	26.6	23.19	-03.3	13	*	*	05	01.0	25	01.8	15	02.2	08	01.4	*	01	01.0	*	*	17							
IV	-	07.3	15.0	08.9	16.0	16.3	04.3	23.7	29	-02.6	04	05	01.2	03	01.3	10	01.2	17	01.7	05	01.0	10	01.0	17	01.2	19								
V	-	12.8	19.1	12.5	14.4	20.5	09.3	25.4	31	03.4	10	07	01.0	05	01.4	02	01.0	02	01.0	07	01.1	09	01.1	19	01.1	19	01.1	21						
VI	-	16.2	22.4	16.3	17.8	23.9	13.1	30.7	27	06.9	13	01	01.0	*	*	01	01.0	18	01.2	04	01.0	16	01.2	23	01.6	22								
VII	-	18.0	25.8	18.6	20.2	27.4	14.0	36.7	17	05.8	28	07	01.0	04	01.2	02	01.5	01	01.0	15	01.0	06	01.0	10	01.2	27	01.5	21						
VIII	-	18.3	26.5	19.6	21.5	30.0	15.4	36.5	30	10.8	30	20	01.0	04	01.0	*	*	*	24	01.0	01	01.0	03	01.0	11	01.3	11							
IX	-	14.1	23.2	16.1	17.4	24.5	12.4	31.5	03	04.9	28	11	01.0	*	*	*	02	01.5	21	01.0	02	01.5	04	01.0	29	01.3	20							
X	-	06.1	12.1	07.4	08.2	13.3	04.7	22.3	04	-03.3	31	*	*	*	*	02	01.0	*	*	21	01.4	06	01.2	13	01.4	26	01.5	24						
XI	-	03.2	10.4	04.8	05.8	11.4	02.0	20.0	16	-01.2	30	04</td																						

Mjesec	Oblačnost Nm (0-10)				Insekticid broj sati	Vlažnost vazduha				Padavine R mm				Broj dana nesa:																						
						U m s				Tn Tx Tx Tx Tn				F(0-12)		Nm(0-10)		R mm		•	*	•	Δ	•	Δ	▲	▲	R	T	III	II					
	7	14	21	Sred. (Dnev.)		mm	7	14	21	Sred.	Min	Max	Dat.	10.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.00.0	0	Δ	•	Δ	•	Δ	▲	▲	R	T	III	II		
BR. ST.126																																				
BR. ST.126																																				
I	8.9	7.2	7.6	7.9	-	04.8	86	88	90	88	49	057	019.7	20	.	-	17	-	-	.	01	19	08	07	02	08	01	01	.	.	02	04	.			
II	6.6	5.8	4.9	5.8	-	06.3	80	81	85	82	46	033	008.3	23	.	-	08	-	-	.	01	01	04	07	08	08	.	08	01	01	.	02	04	.		
III	4.5	5.7	4.0	4.8	-	05.9	75	61	76	71	25	018	008.0	08	.	-	08	04	.	.	04	09	05	03	.	05	04	01	.	01	01	.				
IV	6.1	6.5	6.2	6.2	-	06.6	78	55	71	61	21	057	013.7	17	.	-	-	-	.	04	01	04	12	10	09	02	10	01	01	.	01	.	.			
V	6.1	6.6	5.4	6.0	-	06.7	79	64	83	75	38	129	019.6	07	.	-	05	.	-	05	03	04	09	14	16	14	.	.	01	07	.	.				
VI	5.3	6.3	5.8	5.8	-	12.8	83	61	84	76	41	117	031.2	11	.	-	14	01	.	05	02	08	09	09	05	03	.	02	02	.	.					
VII	3.9	3.7	3.6	3.7	-	13.5	81	54	84	73	32	077	026.3	20	.	-	21	11	.	01	13	06	11	11	02	11	.	.	04	.	.					
VIII	2.8	3.3	3.5	3.2	-	14.8	79	57	85	74	14	107	049.2	24	.	-	27	16	.	02	15	04	06	06	04	06	.	.	06	.	.					
IX	6.3	4.4	5.0	5.2	-	12.1	81	65	88	78	37	087	023.5	27	.	-	12	02	.	04	05	08	08	08	04	08	.	.	04	04	.					
X	6.8	7.2	6.6	6.9	-	06.9	76	74	86	79	35	199	019.3	16	.	-	03	.	.	05	17	18	17	07	18	.	.	01	01	.						
XI	6.8	6.5	4.3	5.8	-	05.7	84	68	80	80	39	061	013.0	08	.	-	04	.	.	02	05	12	10	10	02	10	01	.	07	01	.					
XII	8.1	6.6	6.6	7.1	-	04.9	84	79	88	83	47	058	014.6	19	.	01	12	.	.	02	01	15	12	12	01	12	03	02	.	.	05	01				
GOD.	5.6	5.8	5.3	5.7	-	08.7	80	67	83	77	14	940	049.2	26	m	-	-	-	-	32	05	68	126	119	114	35	119	11	06	.	02	.	26	44	03	
BR. ST.127																																				
BR. ST.127																																				
I	6.3	6.2	5.4	6.0	-	03.9	76	79	80	78	52	078	028.0	20	.	03	25	.	.	04	07	12	13	11	03	11	08	02	.	.	01	10	05			
II	7.4	5.8	5.7	6.3	-	05.0	77	67	77	74	38	062	022.6	04	.	-	06	.	.	01	04	09	11	09	01	09	03	01	.	.	01	04	02			
III	4.9	5.2	5.4	5.2	-	05.4	71	59	73	68	23	050	025.2	28	.	-	15	.	.	02	08	08	08	06	01	03	05	.	.	01	02	05				
IV	5.9	6.6	6.5	6.4	-	05.6	70	56	78	68	21	101	022.6	17	.	-	03	.	.	04	13	17	15	16	04	16	05	02	.	.	01	01	04			
V	5.4	7.2	7.4	6.6	-	08.5	73	70	77	73	37	132	030.2	23	.	-	05	.	.	01	05	12	22	18	03	22	.	.	01	.	.					
VI	4.2	6.8	6.7	5.9	-	10.4	72	70	79	73	35	120	033.0	02	.	-	01	.	.	.	-	14	12	03	14	.	.	01	06	.	.					
VII	4.3	3.9	4.0	4.3	-	12.3	73	65	70	72	25	054	013.5	08	.	-	14	05	.	.	13	06	13	10	02	13	.	.	01	03	.					
VIII	3.2	4.5	4.4	4.2	-	13.6	73	68	81	74	36	092	023.6	27	.	-	05	.	.	01	01	11	06	11	08	04	11	.	.	11	.	.				
IX	6.1	6.1	5.4	5.9	-	11.2	81	73	85	80	49	093	018.2	27	.	-	02	.	.	04	06	12	10	04	12	.	.	02	05	03						
X	6.4	6.6	6.4	6.4	-	06.3	83	75	86	81	39	213	029.2	24	.	-	02	.	.	01	01	07	14	19	18	08	18	03	01	.	04	02				
XI	5.4	4.8	4.2	4.8	-	05.4	77	73	81	77	43	096	023.0	08	.	-	09	.	.	07	05	11	10	04	07	07	03	.	.	04	06	.				
XII	7.4	6.5	5.8	6.5	-	04.5	80	77	79	79	52	092	016.2	19	.	02	18	.	.	02	11	13	13	04	07	08	02	.	.	04	21	.				
GOD.	5.6	5.8	5.7	5.7	-	07.7	75	69	79	74	21	1183	033.0	0461	.	-	80	.	-	01	06	02	-	-	164	140	41	143	39	11	.	03	04	30	33	45
BR. ST.128																																				
BR. ST.128																																				
I	8.8	7.0	7.2	7.7	045.6	047.7	91	82	90	88	65	036	017.5	20	.	02	18	.	.	05	18	12	06	01	11	03	01	.	.	01	04	.				
II	6.9	5.6	5.6	6.0	087.5	05.8	89	70	84	81	51	030	008.6	07	.	-	06	.	.	01	03	07	12	07	01	11	.	.	01	04	02					
III	5.6	4.7	4.6	5.0	143.3	042.8	88	64	73	75	39	014	005.1	06	.	-	09	03	.	.	08	08	10	03	.	08	04	01	.	.	01	01				
IV	5.8	6.0	5.9	5.9	143.3	07.0	82	64	72	75	26	062	009.7	17	.	-	03	.	.	03	08	16	10	.	16	01	.	.	02	.	02					
V	5.7	5.4	5.4	5.8	149.7	10.6	84	74	88	82	53	077	014.8	13	.	-	04	.	.	01	05	07	18	13	03	18	.	.	05	01	.					
VI	5.1	5.3	5.3	5.4	147.4	12.7	67	69	86	80	50	107	026.0	11	.	-	14	01	.	.	05	07	17	14	03	17	.	.	07	.	.					
VII	4.2	3.8	4.3	4.1	209.2	14.3	84	65	84	77	34	051	020.0	20	.	-	20	11	.	01	14	05</														

Mesec	Vrednost pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																			
		Tm				Sred. (Dnes)		Max		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Danes)	Max	Min	Max	Dat.	Min	Dat.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.				
$\varphi = 43^{\circ}34'$ N $\lambda = 17^{\circ}27'$ E Gr. $\Delta G = +1h\ 10\ min.$																															
I	-00.1	05.9	01.6	02.3	-	-	-	-	-	-	-	16	C2.2	01	01.0	•	•	04	02.0	•	•	07	01.6	•	•	65					
II	01.5	05.6	02.9	03.2	-	-	-	-	-	-	-	23	04.0	•	•	•	•	22	02.0	•	•	01	01.0	•	•	58					
III	-03.9	10.2	05.5	04.3	11.4	00.7	21.2	22	-05.2	13	17	03.8	03	03.7	04	03.0	•	•	17	03.1	•	•	02	01.0	02	03.5	48				
IV	-06.2	09.0	06.1	06.9	10.6	02.2	16.5	30	-01.6	24.17	36	C3.5	•	•	06	02.8	•	•	19	02.6	•	•	•	•	•	•	29				
V	-11.5	14.9	10.3	11.8	16.2	-	21.2	30.27	-	-	16	C3.3	•	•	C6	C4.0	•	•	08	02.5	•	•	02	03.0	•	•	61				
VI	-14.4	16.5	13.6	15.0	20.7	09.1	25.0	25	02.2	14	11	C2.8	01	03.0	C8	02.5	•	•	10	02.2	•	•	04	01.8	•	•	56				
VII	-16.9	23.1	16.3	18.2	25.1	12.7	32.0	16	06.2	08	26	C2.6	•	•	C2	01.5	•	•	02	01.0	•	•	01	01.6	•	•	41				
VIII	-18.8	25.2	18.3	20.2	26.3	14.3	32.2	02	08.2	12	19	02.2	04	01.2	C2	01.0	•	•	C1	C1.0	•	•	03	01.0	03	01.7	61				
IX	-14.7	19.4	14.3	15.7	20.7	10.8	27.4	06	03.6	28	21	02.4	•	•	C5	01.4	•	•	02	02.0	•	•	C2	01.0	05	01.0	55				
X	-04.7	08.7	05.3	06.0	10.1	01.9	14.0	11.06	-03.0	31	09	02.2	01	03.0	06	01.2	01	02.0	14	01.1	•	•	02	01.0	•	•	60				
XI	-C2.2	08.0	03.2	04.2	09.0	00.4	16.2	17	-05.0	29	17	C4.1	•	•	•	•	11	01.6	•	•	01	01.0	•	•	01	01.0	61				
XII	-00.6	04.7	00.4	01.2	06.1	-02.1	12.0	10	-07.0	22	19	04.3	•	•	C1	02.0	•	•	05	04.8	•	•	02	02.0	01	01.0	65				
GOD.	-	07.9	12.8	C8.2	09.2	-	-	-	-	-	-	C3.0	C3.1	10	02.3	40	02.4	01	02.0	115	02.3	•	•	28	01.5	11	01.6	660			
$\varphi = 43^{\circ}23'$ N $\lambda = 17^{\circ}36'$ E Gr. $\Delta G = +1h\ 10\ min.$																															
I	01.6	09.6	03.9	04.8	10.6	-00.5	15.0	20	-06.0	15	04	C1.8	•	•	•	•	•	•	•	•	•	•	•	•	•	69					
II	04.7	10.7	06.4	07.0	11.7	02.3	16.8	16	-04.6	09	11	C2.7	•	•	•	•	02	02.0	•	•	•	•	•	•	•	71					
III	-05.4	14.9	08.7	05.4	15.7	02.9	24.4	21	-02.4	13.12	06	C2.3	•	•	•	•	05	01.4	•	•	•	•	•	•	•	82					
IV	-09.0	14.4	10.0	10.9	15.8	05.7	21.0	30	00.0	21.20	17	C2.9	•	•	•	•	03	C2.3	•	•	•	•	•	•	•	70					
V	-12.6	18.7	13.4	14.5	20.3	08.3	26.4	30.20	04.8	18.11	05	C2.2	•	•	•	•	•	•	07	01.1	•	•	•	•	•	81					
VI	-16.2	23.6	17.3	18.6	24.8	12.1	29.4	26	05.4	12	11	01.7	•	•	•	•	02	01.5	•	•	•	•	•	•	•	77					
VII	-19.7	27.5	20.1	21.6	28.7	13.8	36.2	16	07.8	09	C9	C2.6	•	•	•	•	03	01.7	•	•	•	•	•	•	•	81					
VIII	-19.5	30.3	21.4	23.2	31.3	14.7	37.0	05	D9.0	13	07	01.7	•	•	•	•	03	01.7	•	•	•	•	•	•	•	75					
IX	-15.3	25.2	17.3	18.8	26.1	12.2	31.4	09	04.0	28	09	C1.9	•	•	•	•	04	02.0	•	•	•	•	•	•	•	77					
X	-07.5	13.4	08.6	09.5	14.4	04.7	19.2	06	-02.6	31	04	01.2	•	•	•	•	01	02.0	•	•	•	•	•	•	•	86					
XI	-04.7	12.4	06.6	07.6	13.2	02.0	19.0	17	-03.4	02	C7	C2.3	•	•	•	•	01	02.0	•	•	•	•	•	•	•	81					
XII	-01.3	09.2	03.0	04.1	10.1	-00.4	16.6	04	-05.0	24	17	05.8	•	•	•	•	01	02.0	•	•	•	•	•	•	•	75					
GOD.	-	09.6	17.5	11.4	12.5	18.6	06.5	37.0	05VM	-06.0	45.1	107	C2.8	•	•	•	•	01	02.0	32	01.6	•	•	•	•	•	955				
$\varphi = 43^{\circ}50'$ N $\lambda = 17^{\circ}38'$ E Gr. $\Delta G = +1h\ 10\ min.$																															
I	-01.5	05.6	00.1	01.1	06.7	-03.5	10.6	22	-05.4	15	06	C1.7	•	•	•	•	11	02.8	•	•	•	•	•	•	•	67					
II	00.3	06.7	02.2	02.9	07.8	-01.6	12.4	12	-06.6	09	08	02.0	•	•	•	•	12	02.4	•	•	•	•	•	•	•	53					
III	-01.4	11.8	04.9	05.8	13.2	-06.7	25.4	22	-05.6	02	16	C1.6	•	•	•	•	10	03.2	•	•	•	•	•	•	•	58					
IV	-05.0	10.9	05.9	06.9	12.4	01.8	19.4	30	-06.8	17	04	C1.5	•	•	•	•	13	C3.1	•	•	•	•	•	•	•	56					
V	-09.4	15.7	10.1	11.3	17.2	05.5	24.6	30	02.6	23.05	07	C1.7	•	•	•	•	C3	C2.3	•	•	•	•	•	•	•	74					
VI	-12.8	15.7	12.7	14.5	21.5	05.1	27.4	05	03.6	12	07	C1.9	•	•	•	•	02	02.5	•	•	•	•	•	•	•	67					
VII	-14.7	23.2	14.6	16.8	25.3	10.0	34.6	16	03.4	23.07	04	C1.3	•	•	•	•	01	03.0	•	•	•	•	•	•	•	71					
VIII	-15.5	25.8	19.3	18.0	27.6	10.9	34.4	04	04.8	12	06	C1.8	•	•	•	•	01	02.0	•	•	•	•	•	•	•	66					
IX	-10.7	20.6	12.4	14.1	22.7	07.0	29.4	10	-02.2	28	09	C1.7	•	•	•	•	07	02.6	•	•	•	•	•	•	•	54					
X	-02.7	09.6	03.8	05.0	11.3	00.3	18.6	19	-03.6	31	06	C1.7	•	•	•	•	17	02.4	•	•	•	•	•	•	•	42					
XI	-00.3	08.3	01.5	02.9	10.6	-01.6	17.8	19	-11.6	29	09	C1.8	01	03.0	•	•	07	02.3	01	02.0	•	•	07	01.9	•	•	48				
XII	-03.4	03.9	-01.4	-00.6	05.1	-05.7	14.2	05	-13.2	19	07	C2.1	01	02.0	•	•	07	02.1	•	•	01	03.0	02	02.0	01	03.0	74				
GOD.	-	05.7	13.5	08.1	08.8	14.3	03.9	18.5	17	-02.0	09	04	C3.2	09	02.7	C4	C1.8	12	03.7	C1	02.0	•	•	01	02.0	02.5	01	61			
V	-13.7	20.8																													

Mesec	Vrstdišni pritisak Pm mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (0-12)														
		Tm			Sred. (dies)			Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C				
		7	14	21										N	NE	E	SE	S	SW	W	NW	C				
$\varphi = 43^{\circ}09'$, N $\lambda = 17^{\circ}47'$, E Gr., $\Delta G = +1h\,11\text{ min.}$														GLMANOVICI												
I	-	62.8	12.4	6.2	6.2	11.2	8.4	11.6	3.8	11.6	01-02.0	11	11	01.4	02.2	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
II	-	56.4	12.9	6.2	6.9	13.1	6.4	11.9	1.8	11.9	01-02.0	05	21	01.7	02.2	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
III	-	52.8	12.5	6.1	10.7	14.2	6.5	12.5	2.2	12.5	01-02.1	08	17	01.3	02.2	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
IV	-	50.1	12.6	5.8	11.6	13.6	6.3	12.6	2.2	12.6	01-02.2	12	21	01.3	02.2	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
V	-	44.7	20.5	14.2	15.9	20.7	9.4	24.5	20	24.5	01-02.0	16	16	02.9	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
VI	-	39.4	20.4	16.8	20.6	25.5	13.6	29.4	05	27.0	01-02.0	12	20	02.8	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
VII	-	32.3	20.4	20.7	23.1	29.1	15.3	34.6	16	34.6	01-02.0	09	12	02.1	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
VIII	-	25.1	31.7	11.8	25.1	31.7	14.7	36.8	05	16.0	01-02.0	12	20	02.7	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
IX	-	11.4	16.6	15.6	20.6	14.6	9.4	24.5	01-02.0	27	10	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4			
X	-	10.0	15.9	10.2	11.4	16.0	21.5	01	02.1	01	01-02.0	31	07	02.1	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
XI	-	6.3	14.2	6.1	9.2	14.3	6.4	16.8	16.15	02.0	01-02.0	17	17	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
XII	-	0.4	10.6	0.7	0.5	10.7	01.1	15.5	04	02.2	01-02.0	20	23	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4	02.4		
GOD.	-	12.1	16.1	12.7	14.1	15.3	0.6	20.8	01-02.0	05	11	02.8	02.8	02.8	02.8	02.8	02.8	02.8	02.8	02.8	02.8	02.8	02.8			
$\varphi = 43^{\circ}21'$, N $\lambda = 17^{\circ}48'$, E Gr., $\Delta G = +1h\,11\text{ min.}$														MESTAR												
I	757.0	64.6	10.2	6.5	0.6	11.9	03.6	14.6	31	01.1	27	47	02.2	19	01.7	02	02.0	02	02.0	02	02.0	02	02.0	02		
II	756.5	65.9	12.0	6.6	0.6	14.0	05.0	18.6	16	00.1	09	29	02.7	13	04.8	03	02.3	07	02.4	04	01.5	02	02.5	02		
III	752.2	67.2	10.9	11.1	11.6	17.7	06.5	26.6	20.21	02.1	02	21	02.7	15	04.9	03	02.7	03	01.7	05	03.2	10	02.7	03		
IV	745.4	63.1	11.0	11.1	17.5	08.0	24.0	24	02.8	21	34	02.6	24	03.4	01	01.5	03	02.0	05	02.0	04	02.5	02	02.0		
V	756.1	13.7	20.4	16.2	16.2	21.7	10.6	24.6	30	07.0	11.06	03	02.2	16	01.2	02	02.0	03	02.7	02	01.5	11	01.6	02	01.0	
VI	756.5	17.5	16.2	17.1	20.5	26.0	16.4	36.6	05.04	06.2	14	29	02.2	11	03.0	03	04.0	07	02.1	11	02.7	03	02.0	03	02.0	
VII	751.0	21.0	17.5	17.9	17.9	30.7	13.3	37.9	16	12.0	09	26	02.0	11	03.1	02	01.5	06	01.5	01	05.0	03	02.7	09	02.0	
VIII	751.5	21.7	11.7	13.7	13.1	31.3	16.1	36.0	05.34	12.1	12	43	02.2	11	01.1	02	04.0	07	03.0	03	02.0	04	02.8	02	02.5	
IX	751.9	17.4	26.4	18.7	18.7	27.0	15.8	31.6	09	04.4	27	21	01.7	16	01.9	01	01.0	01	03.0	04	04.5	02	03.0	07	01.7	
X	745.3	08.9	14.2	10.2	15.2	20.4	01.2	20.4	04	01.2	31	26	02.5	19	01.3	04	01.0	07	02.7	05	02.2	08	02.0	03	01.7	
XI	754.4	15.6	12.6	9.9	12.6	16.0	04.5	18.6	17	00.0	02	31	02.0	19	01.4	01	01.0	02	01.5	01	01.0	06	01.7	27	01.0	
XII	746.0	01.7	09.4	0.8	0.8	10.7	02.8	17.8	04	01.4	24.71	31	04.9	13	04.5	01	02.0	04	01.3	03	01.3	08	01.7	02	01.0	
GOD.	752.0	11.4	15.8	13.3	14.2	19.6	0.6	20.0	01.4	00.0	05	11	02.0	11	01.4	01.0	01.0	01	01.0	01	01.0	01	01.0	01	01.0	
$\varphi = 43^{\circ}24'$, N $\lambda = 17^{\circ}51'$, E Gr., $\Delta G = +1h\,11\text{ min.}$														PETOCCI-ŽELJUŠA												
I	-	64.5	10.2	0.5	0.6	10.8	02.6	14.6	20	02.5	.9	14	01.4	21	02.1	.	03	01.7	02	01.7	02	02.4	02	02.5	04	
II	-	55.9	11.0	27.5	0.6	12.8	08.2	17.8	17	01.1	09	47	02.1	19	01.9	.	04	01.5	02	01.0	10	02.4	.	37	02.5	
III	-	57.4	16.6	0.9	16.9	17.4	05.2	25.6	22.21	00.7	13	01.0	10	01.3	22	01.4	.	02	02.5	02	03.2	18	03.0	03	02.4	
IV	-	50.0	10.4	11.1	17.4	06.9	22.0	29.28	01.8	21	16	01.3	16	02.1	01	01.7	*	04	02.6	*	36	02.7	*			
V	-	14.7	20.4	14.5	15.6	21.6	10.6	27.7	26	06.7	11	23	01.1	11	01.8	.	06	01.7	02	01.0	13	01.9	02	01.0	38	
VI	-	17.2	23.6	16.1	19.4	24.4	13.4	24.8	05	06.0	14	19	01.1	12	01.4	.	04	01.0	01	01.0	16	02.6	04	01.0	34	
VII	-	31.0	26.8	11.0	12.5	20.5	13.6	30.0	16.0	01.3	13	16	01.7	09	14	01.1	02	01.0	01	01.0	12	01.6	03	01.9	03	
VIII	-	17.0	31.7	12.1	14.4	31.0	17.7	34.1	09	12.8	12	13	01.0	11	01.5	01	01.3	10	01.3	01	01.0	04	01.8	01	01.0	03
IX	-	17.5	26.0	16.4	20.1	27.0	14.5	31.2	06.04	05.7	27	05	01.4	23	01.3	.	05	02.0	02	01.4	18	01.5	02	01.5	35	
X	-	5.2	14.5	0.7	16.0	15.6	0.6	20.0	04	00.5	31	04	01.0	16	01.2	.	08	01.4	02	01.6	11	01.6	02	01.7	02	
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 43^{\circ}46'$, N $\lambda = 18^{\circ}02'$, E Gr., $\Delta G = +1h\,12\text{ min.}$														IVAN SEDLO												
I	-	-01.8	01.0	-00.7	-00.5																					

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha			Padavine R mm			Prej dana na s:																	
	7	14	21	Sred. (Dnev.)	Inzolacijs broj sati	Inzolacijs broj sati	em	U m %			Tm	Tx	Tn	T ₁₄	T ₂₁	T ₂₄	T ₀₋₁₂	Sv (0-10)	R mm	●	★	▲	▲	R	T	III	
								mm	7	14	21	Sred.	Mn	N	Σ	Mx	dat.	8	2.0	8.0	0.1	1.0	6				
BR. 57-136	OCMANOVICI																										
I 4.5 4.0 3.7 4.0	-	05.3	84	95	81	73	23	056	417.1	19	-	-	10	-	10	01	-	10	08	09	02	03	01	02	03	04	
II 4.5 4.0 3.5 5.0	=	06.2	82	88	78	71	37	452	555.3	20	-	-	21	-	22	02	-	22	02	02	02	02	01	02	02	03	
III 4.4 4.0 3.5 4.0	=	08.3	18	44	73	65	26	047	026.0	21	-	-	21	-	21	02	-	21	04	04	02	02	01	02	02	03	
IV 5.2 5.7 5.4 5.4	-	07.9	65	58	83	76	26	199	933.5	18	-	-	21	-	21	02	-	21	02	02	02	02	01	02	02	03	
V 4.5 4.0 4.0 4.5 4.6	-	10.2	82	57	80	73	38	047	025.5	01	-	-	04	-	04	01	-	04	01	01	01	01	00	01	01	01	
VI 3.6 3.6 3.8 3.8 3.6	-	12.0	73	49	71	69	33	083	020.8	07	-	-	21	-	21	02	-	21	04	04	02	02	01	02	02	03	
VII 1.9 2.0 1.1 1.1 1.7	-	12.9	69	39	74	61	22	022	014.0	20	-	-	21	-	21	02	-	21	04	04	02	02	01	02	02	03	
VIII 1.6 1.6 1.4 1.4 1.6	-	13.3	67	33	70	57	22	018	008.0	24	-	-	31	-	30	02	-	31	03	03	02	02	01	02	02	03	
GOD. 4.2 4.0 3.7 4.0	-	09.1	79	53	78	71	22	1220	058.5	4	-	-	21	-	20	02	-	21	01	01	01	01	00	01	01	01	
MCSTAR																											
BR. ST.137	MCSTAR																										
I 5.3 6.0 3.7 5.0	122.8	05.2	77	60	70	69	41	682	031.0	02	-	-	01	-	01	01	-	01	01	01	01	01	01	01	01	01	
II 8.5 6.8 5.7 7.0	095.9	05.8	79	58	70	69	43	230	052.9	04	-	-	01	-	01	01	-	01	01	01	01	01	01	01	01	01	
III 5.5 6.7 4.6 5.7	179.3	06.5	74	51	64	63	32	054	027.3	06	-	-	02	-	02	01	-	02	01	01	01	01	01	01	01	01	
IV 7.0 7.0 7.0 7.0 7.1	145.2	07.0	75	75	75	75	28	073	017.7	27	-	-	01	-	01	01	-	01	01	01	01	01	01	01	01		
V 4.4 6.6 5.1 6.0	150.9	09.9	82	61	73	72	32	153	030.4	01	-	-	10	-	10	01	-	10	01	01	01	01	01	01	01	01	
VI 4.5 6.6 5.2 6.9	207.6	11.8	77	53	70	67	37	111	019.2	30	-	-	19	-	19	02	-	19	03	03	02	02	01	02	02	03	
VII 7.7 7.5 7.5 7.7	256.8	11.9	62	43	55	53	31	025	031.4	30	-	-	21	-	21	05	-	21	03	03	02	02	01	03	02	03	
VIII 2.6 4.4 1.8 2.0	311.1	12.9	62	43	55	53	27	074	032.6	12	-	-	30	-	21	12	-	31	01	01	01	01	01	01	01	01	
IX 4.4 4.6 4.4 4.4	214.4	11.8	56	50	67	64	37	155	041.0	22	-	-	19	-	19	02	-	19	01	01	01	01	01	01	01	01	
X 7.3 7.0 6.1 7.0	102.9	10.8	22	89	74	85	30	463	047.1	23	-	-	19	-	19	02	-	19	01	01	01	01	01	02	02	03	
XI 6.7 6.7 4.7 7.6	118.6	06.7	76	71	80	79	52	126	031.7	24	-	-	19	-	19	02	-	19	02	02	01	01	01	02	02	03	
XII 5.8 6.3 4.1 5.4	102.9	05.1	75	67	71	73	38	077	052.4	15	-	-	01	-	01	01	-	01	04	04	03	03	02	03	02	03	
GOD. 5.7 6.1 4.4 5.4	214.6	08.6	76	52	69	67	27	1639	059.7	4	-	-	08	-	08	10	-	08	11	11	10	10	10	10	10	10	
PETOČI-ZELJUSA																											
BR. ST.138	PETOČI-ZELJUSA																										
I 5.4 5.9 4.5 5.3	-	-	72	57	70	-	-	056	019.5	12	-	-	04	-	04	01	-	04	01	01	01	01	01	01	01	01	
II 7.9 7.1 6.2 7.1	-	05.5	74	58	69	67	28	200	045.8	04	-	-	01	-	01	02	-	01	02	02	02	02	01	02	02	03	
III 5.1 5.5 4.5 5.2	-	05.7	67	47	42	59	17	056	025.2	07	-	-	02	-	02	01	-	02	01	01	01	01	01	01	01	01	
IV 6.6 7.6 6.6 7.0	-	04.9	72	44	69	65	22	061	013.7	21	-	-	01	-	01	01	-	01	01	01	01	01	01	01	01	01	
V 6.5 7.1 5.5 6.3	-	04.4	72	54	49	65	31	135	026.5	01	-	-	08	-	08	01	-	08	11	11	11	11	10	11	11	11	
VI 6.0 6.6 6.2 6.3	-	11.8	74	56	72	76	34	148	034.2	30	-	-	21	-	21	05	-	21	03	03	02	02	01	02	02	03	
VII 2.5 3.7 3.3 3.2	-	12.7	63	50	64	59	29	041	014.5	20	-	-	21	-	21	06	-	21	05	05	04	04	03	04	04	05	
VIII 2.2 3.0 2.4 2.6	-	13.2	67	47	61	57	20	057	017.1	10	-	-	21	-	21	06	-	21	04	04	03	03	02	03	03	04	
IX 4.7 4.3 4.1 4.4	-	12.6	80	55	77	70	25	181	046.7	15	-	-	20	-	20	11	-	20	05	05	04	04	03	04	04	05	
X 7.1 8.0 6.5 7.2	-	08.0	62	73	86	81	27	510	016.4	13	-	-	01	-	01	02	-	01	01	01	01	01	01	01	01	01	
XI -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD. -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IVAN SFDOL																											
BR. ST.139	IVAN SFDOL																										
I 8.1 7.6 6.4 7.5	03.0	0.4	1.9	9.9	9.3	47	49	063	015.4	18	-	-	10	-	10	02	-	10	07	07	02	07	01	02	02	03	
II 7.7 7.4 7.1 7.5	05.8	0.4	3.3	7.0	7.0	70	43	144	014.1	04	-	-	01	-	01	02	-	01	15	12	10	07	11	01	02	02	
III 7.4 7.5 6.0 7.0	120.6	0.4	5.1	57	55	71	15	059	026.7	06	-	-	02	-	02	01	-	02	05	02	04	04	03	02	03	03	
IV 7.7 6.0 7.0 7.6	125.9	0.4	9.9	83	63	78	73	092	017.7	17	-	-	02	-	02	01	-	02	03	01	01	01	01	01	01	01	01
V 7.6 7.9 6.7 7.4	134.6	0.6	8.3	87	61	81	76	32	179	024.6	23	-	-	01	-	01	04	-	13	04	04	03	03	02	03	03	04
VI 6.6 7.6 7.0 7.4	125.1	0.8	9.9	85	61	81	76	47	111	038.2	30	-	-	21	-	21	05	-	21	04	04	03	03	02	03	03	04
VII 4.3 5.6 3.6 4.4	201.9	10.0	8.0	81	59	79	73	23	073	026.3	20	-	-	10	-	10	01	-	10	01	01	01	01	01	01	01	01
VIII 4.4 5.6 3.1 4.3	214.5	11.0	8.0	86	56	84	76	25	055	010.4	29	-	-	14	-	14	01	-	14	05	05	04	04	03	04	04	05
IX 3.0 7.0 6.4 7.4	122.8	0.9	7.2	64	80	77	44	077	030.4	18	-	-	15	-	15	01	-	15	02	02	01	01	01	01	01	01	
X 4.5 6.5 6.2 6.4	07.6	0.7	7.6	73	82	84	54	089	030.4	11</td																	

Mesec	Varduini Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																			
		Tm			Max			Min			Dat.			N			NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.	8.	J.				
$\varphi = 43^{\circ}43'$ N $\lambda = 18^{\circ}16'$ E Gr. $\Delta G = +1h\ 13\ min.$														BJELASNICA												BR. ST.141					
I	593.0	-05.3	-04.4	-05.3	-05.1	-03.3	-06.9	00.9	01	-12.0	14	44	06.2	02	04.5	01	03.0	.	.	08	05.1	23	05.6	.	.	03	02.7	12			
II	588.1	-05.2	-03.9	-04.4	-04.5	-02.9	-06.0	00.2	19.17	-12.2	09	23	04.9	06	03.5	01	04.0	.	.	14	07.0	29	07.4	08	04.6	02	06.0	01			
III	591.4	-02.0	-00.8	-01.6	-01.5	00.4	-03.2	07.4	21	-10.6	08	23	03.8	01	03.0	07	03.0	01	03.0	19	05.0	25	07.5	04	03.5	02	03.5	11			
IV	588.6	-03.5	-02.0	-03.1	-02.9	-01.3	-04.4	04.8	30	-08.6	19.18	42	05.1	04	03.0	02	02.0	.	.	11	05.3	25	07.0	06			
V	591.3	00.7	02.5	01.8	01.7	03.5	00.0	10.6	31	-04.0	10	30	04.9	04	03.2	06	06.5	35	02.6	05	02.2	08	04.1	05			
VI	593.9	04.9	07.0	05.4	05.7	07.8	03.6	12.8	27	-03.4	13	18	04.1	03	01.7	07	05.3	43	04.8	.	.	12	04.2	07			
VII	597.1	09.0	10.8	09.0	09.4	12.0	06.7	15.0	16	-01.0	20	15	03.5	01	02.0	09	05.4	28	04.6	01	02.0	22	05.5	17			
VIII	598.1	10.5	12.7	10.4	11.0	13.9	08.5	19.8	04	00.8	12	34	04.6	11	04.1	05	04.4	01	03.0	17	03.6	10	05.0	01	03.0	.	.	14			
IX	595.8	06.8	08.5	06.7	07.2	09.5	05.3	14.6	06.04	-03.0	27	16	03.1	01	02.0	02	03.0	.	.	13	05.4	41	06.2	01	04.0	08	05.8	08			
X	588.7	-01.1	-00.3	-00.1	-00.9	01.0	-02.6	05.4	13	-09.4	31.30	09	C4.1	15	06.9	61	06.9	02	03.0	05	03.4	01			
XI	592.2	-02.7	-01.7	-02.2	-02.2	-00.6	-03.8	07.7	18	-10.4	02	08	05.4	05	07.2	48	02.0	06	04.0	16	05.2	07			
XII	592.1	-04.7	-04.4	-04.9	-04.7	-02.7	-06.6	04.0	29	-14.0	31	44	07.5	01	06.0	16	06.6	04	05.5	24	05.6	04			
GOD.	592.6	00.6	02.0	01.0	01.1	03.1	-00.8	19.8	4VII	-14.0	31XII	306	05.2	33	03.4	18	03.3	02	03.0	125	05.6	384	05.9	32	03.8	102	05.0	93			
$\varphi = 43^{\circ}49'$ N $\lambda = 18^{\circ}20'$ E Gr. $\Delta G = +1h\ 13\ min.$														SARAJEVO-AERODROM												BR. ST.142					
I	722.2	-00.8	01.8	00.1	00.3	02.7	-01.8	06.6	22	-07.0	15	.	.	01	02.0	04	01.5	02	01.5	.	.	.	02	02.0	05	02.4	79				
II	715.2	00.4	08.9	03.7	04.2	10.0	-00.5	15.8	17.12	-05.7	09	02	02.5	04	01.5	03	02.0	08	03.8	05	03.6	03	03.3	07	01.9	05	02.0	47			
III	717.4	02.0	12.9	06.8	07.1	14.0	00.7	24.6	21	-04.4	02	.	.	04	03.8	01	03.0	09	02.6	02	03.0	01	02.0	11	02.0	09	C2.3	56			
IV	714.4	04.5	12.0	07.0	07.6	13.2	02.3	20.3	30	-02.4	21	01	C2.0	07	02.3	04	02.5	06	03.2	02	03.0	09	01.8	13	C2.5	45					
V	715.5	08.9	16.6	11.4	12.1	18.3	06.1	25.4	31	00.8	06	07	02.4	02	02.0	02	01.5	09	03.1	01	04.0	02	01.5	05	02.8	16	C2.0	49			
VI	716.3	12.9	20.8	15.1	16.0	22.4	05.9	26.0	27.23	03.2	14	03	01.7	01	02.0	05	02.2	17	02.2	03	02.3	.	.	02	02.0	22	02.4	37			
VII	718.7	13.8	23.9	16.8	17.8	25.2	10.5	33.8	15	-06.1	09	02	02.0	.	01	01.0	02	02.5	06	04.0	03	02.0	08	02.2	18	C2.2	57				
VIII	718.9	13.9	25.8	17.2	18.5	27.0	11.6	32.7	04	05.4	12	02	02.0	02	03.0	06	01.8	05	03.0	01	01.0	02	01.5	06	02.2	12	07.1	57			
IX	717.9	12.1	21.4	14.2	15.5	22.6	10.1	30.3	04	01.3	28	03	01.7	02	02.0	08	01.9	08	03.2	03	03.3	02	02.5	05	02.2	12	C2.1	47			
X	714.2	04.3	11.3	05.9	06.4	12.4	02.3	18.8	04	-03.2	31.28	01	01.0	01	02.0	05	02.8	09	03.4	02	02.0	01	03.0	06	02.3	10	02.2	58			
XI	719.2	00.1	08.1	02.8	03.4	09.1	-01.0	16.8	19	-08.0	29	01	02.0	03	03.3	01	02.0	.	.	03	02.0	04	03.0	78			
XII	721.2	-02.2	00.7	-01.4	-01.1	01.6	-04.0	05.4	12	-12.0	25	04	02.8	01	02.0	04	01.8	.	.	02	01.0	.	.	04	02.0	12	C2.2	64			
GOD.	717.6	05.8	13.7	08.3	09.0	14.9	03.8	33.8	4VII	-12.0	25.XII	26	02.2	25	02.4	43	02.0	78	02.9	24	02.9	17	02.3	70	02.1	138	C2.2	674			
$\varphi = 43^{\circ}52'$ N $\lambda = 18^{\circ}26'$ E Gr. $\Delta G = +1h\ 14\ min.$															SARAJEVO												BR. ST.143				
I	710.9	-01.3	02.1	00.6	00.5	03.0	-01.7	08.7	22	-06.4	15	.	.	01	02.0	04	01.5	02	01.5	05	01.0	15	01.2	05	C1.6	44					
II	704.2	01.8	08.8	04.0	04.6	09.8	00.6	15.9	17	-05.6	09	01	01.0	03	03.3	22	02.2	18	02.4	03	04.3	13	01.9	11	01.5	01	01.0	12			
III	705.5	03.7	12.3	07.3	07.7	13.5	02.5	24.7	21	-04.1	01	02	02.0	01	04.0	25	02.6	31	02.4	04	02.8	05	02.2	10	01.9	05	01.6	10			
IV	703.6	05.0	11.4	07.0	07.6	13.0	03.0	20.3	30	-01.0	20	02	C2.0	04	01.8	16	02.0	18	02.1	06	02.0	07	02.0	10	01.8	04	C1.8	23			
V	704.8	09.2	15.9	11.7	12.2	17.8	06.8	26.0	31	03.6	10	02	03.0	03	01.7	11	01.8	11	01.4	09	02.3	08	01.5	13	01.6	05	C1.4	31			
VI	705.7	13.2	20.1	15.2	15.9	21.6	10.7	27.3	27	04.9	14	03	01.3	.	.	14	01.7	10	01.6	06	02.8	03	02.0	26	02.0	04	02.5	24			
VII	708.1	14.7	23.5	17.5	18.3	24.5	12.2	33.1	17	-06.9	09	01	02.0	.	.	10	02.0	13	02.0	02	02.0	05	02.2	23	01.8	04	02.0	35			
VIII	708.2	14.7	25.7	18.2	19.2	22.6	13.1	32.6	19	06.9	12	02	C1.5	02	03.0	21	01.8	13	01.6	04	01.8	15	01.8	05	02.0	31					
IX	707.3	12.6	21.4	14.8	15.9	22.4	11.1	29.6	04	02.3	28	02	01.5	.	.	13	01.7	15	01.7	06	03.5	04	01.5	14							

Mjesec	Oblačnost Nm (0-10)			Indoklizacije broj sati (Dides)	Vlažnost vazduha			Padavine R mm			Broj dana na sat																										
	7	14	21		e _m	U m	t	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■										
	mm	7	14	21	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■										
BEJELAŠNICA																																					
BR. ST.141																																					
I	6.2	7.1	4.9	6.1	059.9	02.7	45	64	84	84	20	022	C17.7	01	04	30	21	•	•	•	27	12	C5	12	11	08	•	11	•	•	•	•	21	31			
II	7.4	7.7	6.8	7.3	058.5	03.1	54	56	93	93	67	047	D11.4	04	05	25	28	•	•	•	24	19	04	16	13	11	01	•	13	•	•	•	•	01	75	29	
III	6.5	6.5	5.7	6.2	151.0	03.2	74	78	80	77	33	063	C17.3	07	02	15	20	•	•	•	21	19	03	11	11	08	62	07	11	01	•	01	15	31			
IV	7.9	8.7	8.7	8.3	072.8	03.4	91	89	91	90	48	080	D18.2	10	•	16	29	•	•	•	26	20	15	02	02	18	02	•	•	•	•	•	28	30			
V	7.4	8.0	6.6	7.5	111.7	04.2	90	85	88	88	40	066	C14.0	36	•	04	16	•	•	•	27	21	01	13	19	15	02	12	12	01	•	01	03	31			
VI	7.3	7.7	7.7	7.5	115.2	05.6	61	80	86	83	21	087	C14.9	02	•	01	04	•	•	•	22	18	C7	17	19	03	16	04	•	01	•	03	04	25	10		
VII	6.4	5.5	3.8	4.5	255.4	06.0	65	68	76	70	23	016	C04.8	08	•	•	04	•	•	•	20	17	13	05	05	09	02	01	•	04	16	•	24	30			
VIII	3.5	5.6	3.5	4.2	279.7	06.3	52	62	71	65	20	097	C21.3	29	•	•	•	•	•	•	15	09	13	06	14	12	04	14	•	•	•	02	08	15	•		
GOD.	7.4	7.2	6.1	6.6	1553.9	04.3	82	87	85	83	20	887	D32.5	6.6	•	22	144	223	•	•	•	207	220	60	162	171	134	30	70	114	02	01	01	07	25	278	243
SARAJEVO-AERODROM																												$H_s = 2067 \text{ m } H_b = 2070.4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$									
BR. ST.142																																					
I	5.7	6.7	5.2	6.8	027.4	04.3	93	84	93	90	60	050	D15.8	18	•	03	23	•	•	•	24	15	C7	02	11	C8	01	•	•	•	•	•	21	6			
II	7.4	7.7	5.5	6.7	059.2	03.4	65	56	76	75	40	078	D35.2	04	•	15	•	•	•	07	•	03	11	09	C7	03	03	03	•	01	03	01	01	01	01	01	
III	7.3	7.1	5.8	6.7	121.1	05.3	83	52	74	72	12	025	D09.6	07	•	12	•	•	•	03	•	05	13	C8	05	•	04	04	•	01	01	01	01	01	01	01	
IV	7.0	8.1	6.4	7.6	121.1	05.7	83	57	76	74	34	078	D15.4	17	•	05	•	•	•	03	•	02	14	16	02	15	05	•	01	01	01	01	01	01	01		
V	6.7	7.3	6.4	7.6	147.7	07.7	86	54	78	73	34	092	C23.5	23	•	•	01	•	•	02	•	01	12	21	13	03	21	•	•	•	•	•	06	05			
VI	6.1	7.3	6.7	6.7	155.0	10.0	86	55	79	73	37	094	C27.7	30	•	•	08	•	•	04	•	03	10	14	12	02	04	•	07	04	•	07	04	04			
VII	6.3	5.1	3.5	4.7	264.6	11.0	87	53	81	74	25	057	C17.7	20	•	•	15	09	•	01	02	07	09	07	03	09	•	•	•	04	06	06	06				
VIII	6.0	4.9	3.8	4.6	259.6	11.9	93	51	84	76	30	055	D11.2	24	•	•	20	10	•	01	01	07	05	12	11	01	•	•	•	17	15	15	•				
IX	8.7	5.6	3.5	6.0	151.1	10.6	92	59	86	79	37	089	D15.6	22	•	•	08	01	•	04	01	•	05	12	10	05	12	•	•	•	01	01	14	•			
X	5.2	7.3	7.0	7.2	093.0	06.2	91	47	89	81	39	257	D06.2	24	•	06	01	•	16	20	20	10	20	02	02	02	•	01	01	01	01	01	01	01			
XI	5.2	6.7	5.5	7.1	071.3	05.0	94	70	80	85	46	073	D26.6	25	•	01	21	•	•	02	•	11	09	08	02	07	04	01	•	01	01	04	03	03			
XII	9.7	8.4	8.1	8.7	014.9	04.1	94	91	95	93	60	051	D27.1	13	02	11	29	•	•	07	24	12	07	01	09	06	01	•	•	•	22	22	22				
GOD.	7.4	7.4	5.6	6.6	1477.1	07.2	80	62	83	78	12	1005	D06.2	24	•	107	56	20	•	34	03	29	152	157	122	35	146	43	33	05	•	•	03	46	118	36	
SAHAJEVAC																											$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$										
BR. ST.143																																					
I	6.2	6.6	7.4	8.1	033.4	04.3	94	64	92	90	62	057	C17.5	20	•	01	21	•	•	•	02	20	19	06	02	13	10	01	01	01	01	01	16	15			
II	7.2	6.7	6.2	6.7	116.2	04.8	80	54	72	79	26	071	D40.7	04	•	12	•	•	06	01	03	12	09	C5	02	07	05	•	•	•	01	04	07				
III	6.4	6.8	5.2	6.1	126.2	04.8	76	49	69	64	30	018	D04.9	07	•	10	•	•	04	•	05	13	10	06	•	05	06	•	01	04	01	01	01	01	01		
IV	6.7	6.5	6.7	7.5	114.1	05.3	81	56	72	69	27	066	D12.7	17	•	02	•	•	04	•	01	14	18	15	01	18	06	05	•	02	01	07	02				
V	7.5	7.9	6.1	6.8	144.2	07.4	83	56	72	70	34	061	C17.0	23	•	•	01	•	•	03	10	23	16	03	23	•	•	•	•	•	07	•					
VI	7.6	7.6	7.0	6.8	175.4	09.3	81	53	73	70	28	123	C31.1	30	•	•	06	01	02	11	20	15	04	20	20	•	•	•	•	•	01	01	01	01	01		
VII	4.5	4.5	3.2	4.1	252.1	10.3	80	51	71	68	24	055	C14.9	20	•	•	16	06	•	•	14	07	08	07	03	08	•	•	•								

Mjesec	Oblačnost Nm (0-10)			Broj sati (dneve)	Vlažnost vazduha			Padavine R mm			Broj dana na mjeri																										
	7	14	21		U m s			Σ	Mn	Mx	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ	R	•	□						
					7	14	21	Sred.	Mn	Mx	Dat.	7	14	21	Dat.	≤	<	<	≥	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV							
BR. ST.140																																					
GENERAL																																					
I	6.2	7.0	4.7	6.0	100.3	03.7	83	74	86	81	28	044	C12+6	18	•	07	29	•	•	02	•	05	10	16	12	01	05	13	02	•	06	23					
II	7.8	7.6	5.5	7.1	083.7	03.9	91	71	86	84	46	195	052+3	07	•	03	22	•	•	04	03	02	12	16	12	06	06	14	03	•	02	28					
III	6.6	6.5	5.0	6.1	167.1	04.1	80	80	77	72	21	081	031+6	06	•	02	17	•	•	02	01	04	11	10	09	02	02	08	01	•	01	01					
IV	7.3	7.9	6.5	7.3	141.4	04.5	86	70	84	80	37	108	C19+4	17	•	01	15	•	•	08	04	01	15	16	13	05	11	06	02	•	02	09					
V	6.9	7.1	6.4	6.6	164.4	04.2	87	67	84	79	36	194	043+0	05	•	•	•	•	•	06	01	02	13	15	14	07	15	04	03	•	04	01					
VI	6.0	7.3	6.8	7.0	180.0	08.3	85	71	87	81	49	117	C32+7	30	•	•	•	•	•	05	02	03	16	18	12	05	16	•	•	•	05	02					
VII	3.6	4.7	2.5	3.7	275.7	05.1	79	61	78	73	34	031	010+4	08	•	•	04	•	•	03	10	03	07	06	01	07	03	•	•	03	02						
VIII	3.0	4.9	2.4	3.4	276.0	05.5	78	55	72	68	28	051	C04+7	10	•	•	•	08	•	01	•	14	03	11	09	•	11	•	•	•	10	01					
IX	7.0	5.3	4.5	5.6	173.6	08.6	88	83	85	79	30	202	C36+7	21	•	•	•	•	•	01	01	04	08	12	09	08	12	•	•	•	11	01					
X	7.9	8.0	7.1	7.7	091.5	05.5	88	79	90	86	49	569	060+4	23	•	01	12	•	•	06	05	01	19	22	16	19	07	03	•	05	04	06					
XI	6.9	6.9	5.6	6.5	108.1	04.4	87	74	87	83	42	153	C03+2	76	•	02	15	•	•	04	01	05	14	14	10	04	08	11	03	•	01	05					
XII	6.6	7.0	5.5	6.4	089.5	03.5	83	77	83	81	26	124	C95+7	13	•	07	27	•	•	03	01	06	13	13	10	04	03	11	01	02	•	01	04	23			
GOD.	6.4	6.7	5.5	6.1	1852.2	05.9	84	88	83	78	21	1869	C04+2	26.0	•	23	137	12	•	•	46	19	57	137	170	13H	59	118	74	16	04	•	01	01	45	93	133
BR. ST.147																																					
SKOKOLAC																																					
I	8.6	E.2	7.5	8.1	036.0	03.7	92	88	93	91	68	014	C05+6	20	03	10	31	•	•	•	•	21	11	04	04	06	•	•	•	•	05	14					
II	6.6	7.0	6.4	6.3	093.2	04.2	90	71	88	83	50	042	C26+7	04	01	•	22	•	•	C1	01	04	12	09	03	01	06	06	•	01	01	05					
III	5.5	6.6	5.6	6.2	144.7	02.0	85	84	84	85	35	036	C17+3	07	•	03	23	•	•	06	11	11	06	01	04	06	01	•	04	05							
IV	6.9	7.7	6.6	7.1	079.1	05.1	92	84	87	81	39	054	C14+4	17	•	•	16	•	•	02	14	14	10	01	09	07	•	•	02	05							
V	5.7	7.2	6.0	6.3	140.6	04.6	92	63	87	81	43	083	C23+4	23	•	•	02	•	•	01	•	03	09	12	09	03	12	•	•	01	04						
VI	5.9	6.7	6.3	6.3	144.2	02.8	88	59	80	76	41	099	C03+3	30	•	•	•	•	•	02	08	17	13	02	17	•	•	01	04	•	04						
VII	4.7	5.5	4.3	4.6	259.5	05.9	81	87	80	76	71	36	049	C12+3	01	•	•	14	03	•	•	13	10	08	07	01	06	01	•	•	03	•	03				
VIII	4.5	5.3	3.5	4.4	245.1	10.0	93	94	88	79	73	087	C02+1	24	•	•	15	03	•	01	01	12	05	10	10	04	10	10	•	•	02	03	15				
IX	7.7	5.7	4.2	5.8	181.7	08.2	93	51	80	75	37	062	C14+3	22	•	•	02	04	•	•	03	08	12	10	02	12	•	•	01	01	12						
X	6.0	7.1	6.5	7.2	091.9	01.1	91	67	86	81	43	229	C32+1	23	•	•	15	•	•	•	03	15	21	20	10	19	05	•	•	02	04						
XI	9.1	5.9	4.0	4.5	103.1	04.0	92	65	89	P3	14	074	C22+6	29	01	04	29	•	•	•	09	11	09	04	07	08	•	•	15	09							
XII	8.8	9.1	8.6	8.6	042.5	03.4	92	87	90	89	67	078	C15+5	19	08	14	31	•	•	•	21	15	12	02	06	11	•	•	14	26							
GOD.	6.6	6.7	5.6	6.5	1563.6	06.1	91	65	85	80	14	907	C32+1	28.0	•	13	31	171	32	06	•	03	02	48	143	152	113	31	117	51	01	•	03	07	86	68	
BR. ST.148																																					
GRADZDE																																					
I	8.4	E.7	8.7	8.6	-	04.9	94	88	94	92	61	051	C02+4	20	•	•	20	•	•	•	03	26	11	09	02	09	02	•	•	•	29	03					
II	5.4	7.0	6.5	6.3	-	05.5	93	71	88	83	50	030	C02+0	04	•	•	11	•	•	•	06	15	07	05	01	06	01	•	•	75	•						
III	3.4	6.5	4.7	4.9	-	06.6	95	65	87	82	36	025	C09+3	29	•	•	13	02	•	•	10	10	07	05	01	07	01	•	01	01	01						
IV	5.7	8.3	7.6	7.2	-	07.5	95	74	72	76	52	100	C08+6	18	•	•	04	•	•	•	15	15	14	03	15	02	02	•	01	01	01						
V	5.9	6.8	7.2	7.4	-	09.5	94	68	70	65	43	062	C26+8	11	•	•	06	•	01	•	04	13	15	11	02	16	•	•	26	•							
VI	6.0	7.8	6.3	7.4	-	12.1	94	67	87	83	39	069																									

Mesec	Vezduljani pričesak pm. min.	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nD, Fm (0-12)																			
		Tm		7	14	21	Sred. (dišes)	Max	Min	Dat.	Max	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C							
				8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.								
		$\varphi = 42^{\circ}41'N \lambda = 18^{\circ}20'E$ Gr. $\Delta G = + 1h\ 14\ min.$																											
I	-	00.3	08.8	02.9	03.7	09.3	-00.6	12.4	20	-05.6	15	.	.	03	01.0	C1	01.0	12	01.4	.	02	01.0	01	01.0	26	01.7	48		
II	-	03.4	10.8	05.1	06.1	11.5	02.0	17.0	16	-03.0	11.09	.	.	02	01.5	.	15	02.1	.	04	02.5	01	01.0	22	01.6	40			
III	-	04.3	14.7	07.5	08.5	15.4	02.5	23.6	22	-01.6	13	.	.	07	01.1	C4	01.0	12	01.4	28	02.5	42		
IV	-	07.8	15.1	09.6	10.5	16.1	04.9	20.6	29	-00.4	20	.	.	07	01.3	C1	01.0	25	01.6	.	.	.	01	01.0	17	02.2	39		
V	-	12.0	19.2	13.7	14.6	20.0	06.1	25.6	21	04.0	11	.	.	04	01.5	04	01.2	16	01.4	30	02.4	39		
VI	-	15.8	23.8	18.0	18.9	24.4	11.0	29.0	27	05.0	13	.	.	05	01.0	02	01.5	09	01.3	.	02	01.0	.	.	.	38	02.3	34	
VII	-	17.5	27.7	20.1	21.4	28.8	12.3	35.6	17	07.4	09	02	02.0	02	01.5	C1	02.0	01	02.0	39	02.3	47			
VIII	-	18.1	29.3	22.5	23.1	30.4	13.6	35.0	05	08.2	14	.	.	02	01.5	.	10	01.2	33	02.6	48			
IX	-	14.1	24.2	18.2	18.6	25.3	11.7	30.4	05	04.0	28	.	.	05	01.2	.	09	01.2	.	.	02	02.0	31	02.6	43				
X	-	08.1	14.4	09.7	10.5	15.0	06.1	20.6	12	-01.0	28	.	.	08	01.5	C3	02.7	17	01.5	.	02	01.0	01	02.0	23	02.0	36		
XI	-	03.2	11.8	05.5	06.5	12.3	02.1	16.0	06	-02.0	02	07	04.6	12	01.4	C3	01.0	14	03.3	.	01	01.0	01	02.0	19	01.8	36		
XII	-	00.8	08.2	02.1	03.3	08.7	-00.5	14.4	04	-05.4	24				
GOD.	-	08.8	17.3	11.2	12.1	18.1	06.1	35.6	F/V	-05.6	151	09	04.0	59	01.3	19	01.4	142	01.7	.	.	20	01.9	67	01.6	349	02.2	490	
		SR SRBLJA								LASTVA												BR. ST. 151							
		$\varphi = 46^{\circ}06'N \lambda = 19^{\circ}46'E$ Gr. $\Delta G = + 1h\ 18\ min.$								PALIĆ												BR. ST. 152							
I	758.5	-00.4	03.8	01.2	01.5	04.3	-01.5	10.5	20	-08.8	15	03	02.3	10	02.0	17	07.0	28	02.4	06	01.8	07	01.9	10	02.1	10	03.1	02	
II	750.8	01.9	09.9	04.7	05.3	10.6	00.8	16.4	17	-04.5	28	05	01.6	08	01.9	12	01.9	22	02.4	15	02.3	12	02.5	05	02.2	05	02.4	.	
III	754.1	03.5	13.1	06.8	07.5	14.0	02.2	26.0	21	-05.2	01	02	01.5	14	01.7	24	07.4	26	02.9	09	02.1	12	02.2	02	04.5	02	01.0	02	
IV	749.8	06.6	15.1	08.7	09.8	16.0	03.5	23.5	30	-02.9	16	17	02.7	15	02.1	10	02.5	20	02.6	05	02.0	09	01.9	07	01.9	05	02.0	02	
V	749.3	12.3	18.3	13.1	14.2	19.6	08.7	28.5	31	02.6	10	08	02.1	02	02.5	04	02.2	07	01.3	08	01.9	13	01.8	26	02.2	18	01.9	07	
VI	749.5	15.6	21.1	16.1	17.2	22.6	11.9	30.3	27	07.5	08	07	02.7	05	01.8	02	01.0	04	02.4	17	02.2	20	02.1	25	02.4	08	.	.	
VII	752.1	17.4	24.5	18.2	19.6	26.0	13.4	34.0	14	08.1	09	05	02.6	01	01.0	02	02.0	08	01.9	09	01.4	09	01.7	20	01.8	29	02.8	10	
VIII	752.7	18.9	27.3	20.1	21.6	28.4	15.7	35.5	04	09.6	08	05	02.0	09	01.6	21	01.6	12	01.9	03	02.0	03	02.0	13	02.1	10	02.3	07	
IX	752.2	13.1	22.3	14.9	16.3	23.6	09.9	30.5	03	00.6	28	10	02.1	15	01.6	15	01.5	05	02.4	06	01.3	08	01.0	10	01.8	14	02.4	07	
X	749.0	05.4	10.9	06.8	07.5	11.9	04.1	19.0	04	-01.3	31	10	02.1	06	02.3	09	01.8	08	01.6	14	02.0	16	01.9	20	02.0	09	01.6	01	
XI	754.0	02.3	09.7	04.3	05.2	10.3	01.5	19.1	16	-03.8	10	11	02.5	09	02.0	10	01.6	11	02.2	16	01.5	13	01.0	11	02.5	07	02.7	02	
XII	755.4	01.8	05.3	02.3	02.9	06.2	00.4	13.3	29	-04.2	24	14	02.3	03	02.3	06	01.7	05	01.8	08	01.6	19	01.9	18	02.4	20	02.4	.	
GOD.	752.3	08.2	15.1	09.8	10.7	16.1	05.9	35.5	F/V	-08.8	151	97	02.3	107	01.9	132	01.9	156	02.3	103	01.8	138	01.9	162	02.1	154	02.4	46	
		$\varphi = 45^{\circ}47'N \lambda = 19^{\circ}05'E$ Gr. $\Delta G = + 1h\ 16\ min.$								SCMBOR												BR. ST. 153							
I	-	00.1	03.6	01.4	01.7	04.2	-00.9	09.8	20	-05.8	15	04	04.5	04	02.0	08	01.9	23	02.8	03	01.3	02	01.0	05	01.6	08	03.2	36	
II	-	01.9	09.7	04.9	05.4	10.5	01.1	16.5	17.12	-03.7	22	05	01.5	03	02.7	07	02.0	14	02.9	17	02.1	06	02.5	02	02.0	03	03.7	30	
III	-	03.4	12.9	07.0	07.6	13.6	01.9	24.8	21	-03.6	14	04	02.2	.	.	11	02.6	43	03.8	04	02.0	04	02.0	05	02.4	.	24	.	
IV	-	06.6	14.9	09.2	10.0	15.8	03.7	24.0	28	-03.5	04	12	03.0	09	03.6	05	03.0	18	03.4	04	02.2	01	02.0	06	01.9	08	02.0	25	
V	-	12.4	18.5	13.5	14.5	19.6	09.0	27.9	31	03.5	10,09	11	02.5	01	03.0	02	02.0	03	02.3	05	01.6	06	01.7	17	01.8	18	02.6	30	
VI	-	15.7	20.9	16.6	17.4	22.4	12.3	29.8	27	08.2	08	08	03.1	02	02.0	02	01.0	01	02.0	05	01.6	06	02.0	11	02.2	22	03.2	33	
VII	-	17.8	24.6	18.6	19.9	26.0	13.7	34.1	17	09.2	27	17	02.9	.	.	01	01.0	02	01.5	11	01.5	02	02.0	13	02.0	16	02.6	31	
VIII	-	18.7	27.2	20.5	21.7	28.1	15.3	34.1	03	08.7	07	02	03.0	04	01.2	07	02.9	06	04.0	04	01.5	03	01.7	07	01.8	08	02.8	55	
IX	-	13.2	21.7	15.3	16.4	22.8	10.8	28.7	03	02.0	28	11	02.5	04	01.5	05	01.4	11	01.6	02	01.5	05	01.6	09	02.0	09	02.6	44	
X	-	05.3	10.5	06.4	07.4	11.8	03.9	19.2	04	-01.3	31	11	02.6	05	02.2	02	02.0	07	02.3	11	01.8	08	02.0	13	02.1	04	02.0	32	
XI	-	02.4	09.7	04.5	05.3	10.4	01.7	19.5	16	-02.3	10	06	02.2	07	02.6	01	02.0	09	01.6	13	01.7	06	01.3	03	02.3	08	03.2	37	
XII	-	01.6	05.3	02.4	02.9	06.1	00.3	12.3	29	-04.2	24,23	07	07	03	07	01.9	.	.	05	02.2	08	01.6	10	01.5	16	01.8	07	03.7	33
GOD.	-	08.8	15.0	10.1	10.8	15.9	06.1	34.1	F/V	-05.8	151	95	02.9	46	02.4	51	02.2	142	02.9	87	01.8	57	01.6	98	02.0	111	02.9	408	
		$\varphi = 45^{\circ}07'N \lambda = 19^{\circ}15'E$ Gr. $\Delta G = + 1h\ 17\ min.$								SIO												BR. ST. 154							
I	-	-00.3	04.1	01.6	01.7	04.9	-01.1	09.5	22	-22.20	-08.0	15	04	01.2	03	01.7	04	03.0	57	03.2	03	01.3	02	02.0	04	02.2	16	03.1	.
II	-	02.7	10.4	05.8	06.2	11.5	01.9	17.8	12	-02.5	28	09	02.4	04	01.5	06	03.5	55	03.4	02	03.0	02	02.5	02	01.5	04	02.2	.	
III	-	04.7	13.3	08.0	08.5	14.0	03.6	26.5	21	-02.3	01	01	03	00	01.7	18	03.2	52	04.4	04	02.1	05	02.0	05	03.0	07	02.0	.	
IV	-	06.8	14.9	09.8	10.3	16.0	05.2	24.0	28	-00.5	01	06	02.4	05	02.6	07	03.1	51	02.8	04	02.5	05	01.6	04	02.8	16	03.1	.	
V	-	11.9	19.0	13.4	14.4	20.1	09.8	28.5	31	05.0	10	06	02.8	10	01.9	03	01.7	14	02.1	05	01.4	04	01.8	18	02.0	35	02.9	.	
VI	-	15.9	21.9	16.8	17.9	23.2	12.9</																						

Mesec	Vazdušni Pritisak Pn. mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Fm (0-12)																	
		7	14	21	sred (Cles)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		V = 45°49'N λ = 19°39' E Grd. ΔGrd + 1h 18 min.										BACKA TOPOLA												BR. ST.156					
I	-	-00.2	03.8	01.4	01.6	04.5	-01.0	09.9	26 -07.5	15	*	*	10	01.1	*	*	48	01.6	*	*	10	01.0	*	*	16	02.4	09		
II	-	02.6	09.8	05.7	06.0	16.9	02.0	17.0	13 -01.8	28	*	*	09	01.2	*	*	48	01.7	01	01.0	13	01.2	*	*	10	01.2	06		
III	-	03.8	13.2	07.4	08.0	13.8	02.4	25.8	21 -03.0	03.02	*	*	10	01.3	*	*	57	02.1	*	*	13	01.5	*	*	03	01.7	10		
IV	-	06.1	15.1	09.4	10.0	16.2	04.3	23.7	26 -01.3	04	*	*	19	01.4	*	*	33	01.0	*	*	13	01.0	*	*	16	01.4	09		
V	-	11.8	18.4	13.9	14.5	20.0	09.3	28.6	31 04.0	10	01	01.0	04	01.0	*	*	12	01.2	*	*	27	01.1	02	01.5	32	01.2	15		
VI	-	15.5	21.7	16.9	17.7	23.1	12.7	31.4	27	06.5	08	*	07	01.0	*	*	09	01.1	*	*	30	01.1	*	*	30	02.3	14		
VII	-	17.0	24.8	19.7	20.3	26.4	14.1	34.3	17 09.0	09	01	02.0	07	01.0	*	*	20	01.1	*	*	12	01.1	*	*	41	01.8	17		
VIII	-	16.6	28.1	21.2	22.3	28.9	16.3	35.3	04	10.1	07	*	*	19	01.0	*	*	28	01.1	*	*	07	01.0	*	*	21	01.3	12	
IX	-	13.0	23.1	15.9	16.9	24.0	10.9	31.1	03 02.9	28	01	01.0	13	01.0	*	*	21	01.1	*	*	11	01.0	*	*	21	01.5	23		
X	-	05.7	11.0	07.4	07.9	11.9	04.2	20.4	04 -01.1	31	*	*	08	01.0	*	*	26	01.2	02	01.0	26	01.3	01	01.0	20	01.0	10		
XI	-	02.6	09.8	04.9	05.6	10.4	01.6	18.9	17 -02.8	10	*	*	15	01.1	*	*	37	01.2	01	01.0	10	01.2	*	*	14	01.5	10		
XII	-	01.4	05.0	02.6	02.9	05.7	00.4	11.6	25	*	*	11	01.0	*	*	17	01.1	*	*	32	01.0	*	*	31	01.6	10			
GOD.	-	06.2	15.3	10.5	11.1	16.3	06.5	35.3	04 00 -07.5	11	*	03	01.3	11.8	01.1	*	*	356	01.6	04	01.0	204	01.1	03	01.3	256	01.6	151	
		V = 45°34'N λ = 19°39' E Grd. ΔGrd + 1h 18 min.										VRBAS												BR. ST.157					
I	-	-00.4	03.8	00.8	01.3	04.6	-01.4	10.0	22.2	20 -08.1	15	02	01.5	09	02.6	13	02.5	22	03.5	*	*	01	02.0	12	02.4	05	05.0	19	
II	-	01.5	10.4	04.6	05.3	11.5	00.8	18.0	12 -03.6	09	03	02.1	02	01.0	20	04.0	20	03.3	06	02.5	05	03.0	02	02.1	02	02.5	18		
III	-	03.9	13.1	06.9	07.7	14.0	02.2	25.8	21 -04.0	03	02	01.5	33	01.1	33	03.7	04	01.6	07	01.6	03	02.0	02	01.0	12	02.0	08		
IV	-	07.1	15.3	08.8	10.0	16.3	03.9	23.8	28 -00.8	04	06	03.7	13	03.0	14	02.4	16	03.1	04	02.2	*	*	15	02.0	08	03.4	14		
V	-	12.7	18.8	13.5	14.6	20.1	09.0	28.4	31 03.6	10	08	02.6	02	04.0	03	01.7	03	01.7	05	01.8	32	02.6	05	03.6	32				
VI	-	16.0	21.2	16.5	17.6	23.1	12.2	30.7	27 06.5	08	02	04.0	04	02.0	04	02.2	04	01.5	02	02.5	06	02.0	25	02.7	17	03.7	26		
VII	-	17.6	24.5	18.6	19.8	26.1	13.2	34.5	17 07.0	09	04	03.2	02	01.7	05	01.4	03	02.3	02	02.0	04	01.5	19	01.9	30	03.0	24		
VIII	-	19.1	27.5	20.2	21.7	28.6	15.2	34.8	04 08.4	11	02	03.5	07	02.0	15	01.8	09	02.3	02	01.5	02	01.5	08	02.4	07	01.9	41		
IX	-	13.6	23.2	15.2	16.8	24.2	10.5	30.0	03 01.6	28	04	02.5	04	01.2	16	01.4	03	02.0	02	02.0	01	02.0	12	02.6	09	02.8	39		
X	-	05.9	11.5	06.8	07.8	12.6	03.7	21.0	04 -02.0	31	04	02.8	04	02.0	14	01.6	05	03.0	06	01.7	02	01.5	27	02.7	05	02.4	36		
XI	-	02.3	10.3	03.8	05.1	11.0	01.1	20.8	16 -02.9	10	05	03.0	03	02.3	22	01.9	07	01.7	04	02.0	01	02.0	13	02.9	05	03.8	30		
XII	-	01.1	05.0	02.1	02.6	05.9	00.0	12.0	29 -04.5	23	13	03.7	01	01.3	12	01.7	03	01.4	04	01.7	02	02.0	27	02.2	13	03.4	19		
GOD.	-	08.4	15.4	09.8	10.9	16.5	05.9	34.8	04 00 -08.1	11	01	58	03.6	59	02	13	181	07.1	124	03.0	18	01.9	31	02.4	187	02.4	130	310	
		V = 15°20'N λ = 19°51' E Grd. ΔGrd + 1h 18 min.										NOVI SAD-PITOVARAC												BR. ST.158					
I	755.8	-00.3	04.1	06.9	01.4	04.9	-01.1	10.7	22 -08.3	15	04	02.0	C5	01.3	10	02.6	37	04.0	*	*	04	02.0	12	02.4	11	02.3	05		
II	752.2	0.4	10.6	05.3	09.9	11.7	01.7	17.2	12 -03.0	28	01	02.0	04	02.2	15	02.7	57	04.4	06	02.0	02	01.5	02	01.6	03	02.7	03		
III	755.2	0.4	12.9	07.4	08.0	14.0	02.8	26.1	21 -03.2	03	07	03.6	09	02.9	10	02.5	28	04.5	03	02.0	06	01.8	12	02.3	10	02.3	03		
IV	751.0	0.6	14.9	09.1	09.9	16.0	04.4	23.6	28 -02.2	04																			
V	750.8	12.3	18.6	14.2	14.8	20.0	09.4	25.1	31 05.4	11	11	02.7	03	02.0	04	01.8	08	02.2	09	01.2	13	01.9	24	02.1	11	01.9	05		
VI	751.0	15.8	21.8	17.1	17.9	23.2	13.1	31.2	27 06.7	08	04	02.4	02	01.5	05	01.2	19	02.0	03	02.0	08	01.6	21	02.1	05	02.2	05		
VII	753.5	17.9	25.0	19.3	20.3	26.5	14.0	35.4	17 08.5	09	06	01.5	06	01.7	15	01.5	24	02.2	02	01.5	04	01.5	14	02.1	05	02.2	14		
VIII	754.0	10.7	27.8	20.8	22.0	28.9	15.8	35.3	04 11.0	07																			
IX	753.4	13.8	23.0	16.0	17.2	24.3	11.7	36.4	03 04.0	26	05	02.4	05	01.6	16	01.7	19	02.1	01	02.0	16	02.1	24	02.1	12	01.8	04		
X	756.0	0.6	11.4	07.6	08.2	13.0	04.7	21.0	04 -02.2	31	04	03.0	03	02.7	15	02.3	22	02.7	01	01.0	06	02.0	16	02.1	09	02.6	19		
XI	755.4	0.2	10.3	04.8	05.6	11.1	01.1	21.0	16 -03.0	28	04	03.7	03	02.7	06	01.9	06	02.7	01	01.0	11	01.9	31	02.4	14	03.0	15		
XII	757.1	0.1	05.3	02.8	03.1	06.3	00.5	13.0	29 -05.6	29																			
GOD.	753.7	0.8	15.5	10.4	11.2	16.7	06.5	35.4	04 00 -08.3	11	01	49	01.9	58	01.7	33	04.0	03	02.2	305	03.2	37	02.1	91	01.9	195	02.2	136	248
		V = 15°15'N λ = 19°52' E Grd. ΔGrd + 1h 18 min.										NOVI SAD-PITOVARAC												BR. ST.159					
I	755.7	0.0	4.1	01.6	01.8	04.8	-06.9	05.5	22 -06.8	15	02	03.0	01.1	02.0	11	02.6	37	04.0	*	*	01	02.0	11	02.4	05	02.0	03		
II	748.0	0.8	10.4	06.6	07.1	11.2	03.7	16.5	12 -02.2	28	01	02.0	04	02.2	15	02.7	57	04.4	06	02.0	02	01.5	02	01.6	03	02.0	01		
III	751.4	0.5	12.8	06.5	08.9	13.3	04.3	25.5	19 -02.6	01	09	02.2	02	01.9	16	02.6	28	04.5	03	02.0	08	02.6	08	02.2	01	02.0	01		
IV	747.3	0.7	14.6	10.4	10.7	15.3	06.7	23.4	28 02.5	09																			
V	747.3	13.0	18.4	14.8	15.2	19.7	11.1	28.2	31 07.6	09.05	04	01.4	01	01.0	10	02.0	*	08	01.9	33	02.5	22	02.4	15	02.1	*	*		
VI	747.6	16.3	21.7	18.1	18.5	23.0	13.8	34.5	27 06.2	12.08	05	02.2	03	01.7	12	01.6	07	02.1	03	02.0	08	01.6	23	02.1	16	02.6	05		
VII	750.0	18.4	24.7	20.8	21.2	26.3	15.8	35.7	17 10.6	09	01	02.0	06	01.7	16	02.2	11	02.2	02	01.0	20	01.9	09	02.8	11	01.9	05		
VIII	750.3	19.8	27.4	22.7	23.1	26.3	17.4	35.6	04 11.2	12																			
IX	749.7	15.0	22.3	17.																									

Mjesec	Oblačnost Nm (0-10)			Inzolacija broj sati	Vlažnost vazduha		Padavine R mm		Broj dana nasa:																										
					em	m			Tn	Tx	Tn	Tx	Tn	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	*	Δ	Δ	A	A	R	T	≡	H						
	7	14	21	Sred. (danas)		mm	7	14	21	Sum mm	Max	Dan.	<	<	<	<	<	<	V	V	V	V	V	V	V	V	V	V							
BR. ST.156																																			
BAČKA TOPOLA																																			
I	7.7	7.2	7.1	7.3	-	04.5	89	79	90	86	63	024	008.8	20	+	C1	20	+	+	+	C2	01	01	13	10	06	+	07	03	-	-	-	02	01	
II	6.6	6.8	4.0	5.8	-	05.3	85	64	77	76	37	016	012.7	24	+	07	07	+	+	+	06	08	09	01	01	08	01	-	-	-	-	-	02	01	
III	4.8	5.5	3.7	4.6	-	05.5	83	52	75	70	24	024	006.2	26	+	08	01	01	01	01	02	01	10	07	08	06	-	04	05	-	-	-	01	-	
IV	5.3	6.6	4.6	5.5	-	-	-	-	-	-	032	011.1	-	-	02	02	02	02	02	05	08	11	04	01	11	-	-	-	-	-	01	-			
V	5.9	6.9	5.4	6.1	-	10.2	89	71	87	82	41	110	C22.5	02	+	04	04	04	04	05	11	15	13	05	15	-	-	-	-	-	03	05			
VI	5.3	7.0	5.2	5.8	-	11.3	63	58	62	74	37	155	076.4	30	+	09	01	01	01	02	08	17	12	C2	17	-	-	-	-	-	06	01			
VII	4.8	6.6	4.0	4.5	-	12.7	83	93	76	71	36	041	007.8	20	+	18	09	09	09	08	07	17	10	05	17	-	-	-	-	-	03	-			
VIII	3.9	4.2	3.7	4.0	-	14.4	86	51	79	72	33	024	019.7	12	+	26	13	01	01	10	04	12	10	01	12	-	-	-	-	-	06	-			
IX	4.0	5.6	3.0	4.1	-	10.7	86	54	80	74	36	015	006.0	27	+	16	01	01	01	09	04	05	04	05	-	-	-	-	-	01	02				
X	7.3	7.8	5.8	7.0	-	07.0	93	76	91	87	40	101	021.0	29	+	01	01	01	03	12	20	18	02	20	-	-	-	-	-	03	-				
XI	7.3	6.4	5.4	6.4	-	05.7	92	69	90	83	45	028	011.5	26	+	05	05	05	05	01	11	09	04	02	09	-	-	-	-	-	02	-			
XII	8.5	7.9	6.4	7.6	-	05.0	91	79	90	87	42	050	014.0	08	+	01	12	01	01	16	15	11	01	14	03	02	-	-	-	-	-	05	01		
GOD.	6.0	6.6	4.9	5.7	-	-	-	-	-	-	638	076.4	80/VI	+	02	57	74	74	01	-	-	62	109	148	99	15	139	12	02	-	-	-	18	-	
VRBAS																																			
BR. ST.157																																			
I	7.5	7.2	5.4	6.7	075.1	04.6	93	83	93	90	67	021	009.4	20	+	01	22	+	+	C6	03	02	09	11	06	+	08	03	-	-	02	-			
II	6.4	6.0	5.7	6.0	106.5	05.5	92	65	86	81	40	013	009.2	24	+	11	05	05	05	11	09	02	02	09	01	01	-	-	-	-	-	01	-		
III	5.3	5.1	4.5	5.0	179.5	05.8	86	58	77	74	29	C32	016.8	06	+	10	04	04	11	06	11	C9	09	05	01	06	05	-	-	-	-	-	01	-	
IV	5.7	6.7	5.9	6.1	183.6	06.5	80	52	78	70	26	034	013.2	26	+	02	04	04	C8	11	09	04	01	05	-	-	-	-	-	-	-	-	-	-	-
V	6.0	7.2	5.5	6.2	224.5	04.7	85	60	87	78	39	087	022.6	12	+	04	04	04	05	02	C2	11	16	10	04	16	-	-	-	-	-	01	04		
VI	5.2	7.1	6.9	6.4	223.0	11.8	64	84	77	76	36	119	C25.3	24	+	11	01	01	12	05	01	08	17	13	04	17	-	-	-	-	-	01	05		
VII	4.7	4.6	3.8	4.4	296.5	13.3	87	57	84	76	30	C59	016.9	20	+	16	08	08	C5	11	06	12	01	14	-	-	-	-	-	02	-				
VIII	4.3	3.7	2.3	3.4	301.8	14.7	87	55	83	75	41	037	017.0	12	+	27	12	02	13	03	10	06	01	10	-	-	-	-	-	-	-	-	-	-	
IX	4.2	5.0	3.4	4.2	199.8	11.2	80	57	84	77	43	025	011.8	27	+	15	01	01	03	01	11	C4	07	04	01	07	-	-	-	-	-	01	02		
X	7.7	7.4	6.0	7.0	090.9	07.1	95	75	93	88	42	090	014.0	16	+	02	02	02	03	03	15	23	18	C2	23	-	-	-	-	-	03	-			
XI	7.5	5.6	3.9	5.7	099.2	05.8	95	71	92	86	46	027	008.0	24	+	08	08	08	05	03	10	11	07	07	09	-	-	-	-	-	06	-			
XII	8.6	7.6	5.5	7.4	049.4	05.1	93	83	92	80	53	058	014.0	19	+	01	16	01	01	07	01	01	14	20	10	04	17	02	-	-	01	-	09	02	
GOD.	6.1	6.1	4.9	5.7	2028.6	08.4	88	65	86	80	26	602	025.3	24/VI	+	02	71	74	27	+	76	23	68	111	156	97	17	145	11	01	01	02	-	23	23
NOVI SAD-RIMSKI ŠANČEVI																																			
BR. ST.158																																			
I	7.4	7.1	6.1	6.9	078.6	04.6	92	79	92	88	57	C17	C08.1	20	+	01	19	+	+	04	01	01	14	C7	05	05	06	02	02	01	-	-	02	01	
II	6.6	6.4	5.4	6.1	110.8	05.2	90	58	78	76	39	010	004.8	24	+	05	05	05	06	06	C9	08	02	08	01	-	-	-	-	-	01	-			
III	5.6	5.4	4.3	5.1	182.3	05.2	81	51	68	67	18	024	011.1	06	+	11	04	04	10	03	03	13	C8	03	01	05	05	01	-	-	01	01	03		
IV	5.9	7.4	5.6	6.4	164.0	06.0	81	41	67	69	28	C37	C11.4	17	+	04	04	04	04	01	11	08	05	02	08	-	01	-	-	-	-	01	-		
V	6.2	7.4	6.4	6.7	189.0	05.4	86	59	81	75	29	088	C26.5	23	+	03	03	03	03	02	15	18	12	C2	18	-	-	-	-	-	06	-			
VI	5.7	7.7	6.3	6.6	213.0	11.6	85	55	83	75	33	083	017.5	07	+	11	01	01	05	01	12	15	11	04	15	-	-	-	-	-	04	-			
VII	4.6	5.1	3.9	4.6	276.6	12.1	82	47	77	68	27	057	013.6	20	+	18	11	01	02	26	16	09	11	07	03	-	-	-	-	-	04	-			
VIII	4.4	4.0	3.1	3.8	286.1	13.8	86	47	78	71	29	056	016.4	12	+	26	12	01	04	14	02	10	08	02	10	-	-	-	-	-	05	-			
IX	4.7	5.5	3.3	4.5	193.6	11.0	91	53	84	76	36	C38	016.7	27	+	16	02	02	05	07	04	04	02	C6	-	-	-	-	-	02	01				
X	7.1	7.6	6.0	6.9	070.7	03.0	97	70	86	37	109	C14.6	16	+	01	01	01	02	04	13	23	19	03	23	-	-	-	-	-	04	-				
XI	7.5	6.9	4.4	6.3	091.2	05.6	88	69	88	39	032	007.0	29	+	07	07	07	01	01	03	10	06	C7	07	-	-	-	-	-	07	-				
XII	8.2	8.2	6.7	7.7	050.2	05.1	91	44	88	88	55	042	006.7	09	+	01	13	08	02	02	01	16	17	10	-	14	05	01	01	01	-	07	-		
GOD.	6.1	6.3	5.2	5.8	2001.2	07.6	75	57	69	67	21	663	034.6	27/IX	+	02	40	72	23	08	184	54	67	121	154	94	18	144	16	04	01	03	27	22	06
GLADNOS																																			
BR. ST.160																																			

Mesec	Vrstdani pritisak Em mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																		
		Tm			Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C		
		7	14	21						E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	
$\varphi = 45^{\circ}38'N \lambda = 20^{\circ}02'E$ Gr. $\Delta G = +1h\ 20\ min.$																												
I	-	-00.1	04.0	01.3	01.6	04.4	-00.7	09.8	20 -07.1	15	01	04.0	07	01.4	09	01.8	35	02.7	01	01.0	05	01.0	06	01.3	12	02.3	17	
II	-	02.8	10.2	05.8	06.1	11.0	02.4	16.7	18.16 -02.9	09	04	01.5	03	01.7	13	02.2	42	02.8	06	02.2	06	02.2	05	02.6	05	02.4	07	
III	-	04.4	13.1	07.8	08.3	13.9	03.7	25.8	21 -02.3	03	01	01.0	02	01.5	21	02.5	34	03.4	08	02.4	05	02.2	04	02.5	01	05.0	07	
IV	-	06.7	15.1	09.8	10.4	15.9	04.7	23.0	28 -01.2	06	15	02.4	10	02.2	08	02.1	24	03.5	13	03.2	04	01.8	06	02.7	07	02.7	03	
V	-	12.6	18.7	14.3	15.0	19.7	10.0	29.8	31 04.2	10	10	02.5	02	01.5	04	02.2	13	02.4	10	01.9	24	02.2	23	02.7	05			
VI	-	16.0	21.5	17.2	18.0	23.0	12.9	30.3	27 07.4	08	11	02.5	01	02.0	03	01.3	07	02.3	11	02.5	05	02.2	17	02.4	23	03.0	12	
VII	-	17.9	25.1	18.9	20.2	26.1	13.9	33.4	14 07.8	09	09	02.4	01	03.0	06	01.3	12	02.0	09	01.8	04	02.0	07	02.0	32	02.6	13	
VIII	-	19.1	27.7	20.5	22.0	28.3	16.0	34.0	03 05.5	07	06	02.3	05	01.4	12	01.7	20	02.3	06	02.0	01	02.0	05	02.4	12	03.1	26	
IX	-	14.0	23.3	15.9	17.3	11.4	30.2	03 03.6	28	05	01.8	06	01.3	05	02.0	27	02.7	11	02.2	05	01.6	09	02.0	13	03.1	09		
X	-	06.4	11.3	07.8	08.3	12.4	04.9	20.1	04 -00.4	31	02	07.0	05	01.6	05	02.0	17	02.5	18	02.6	06	01.8	19	02.8	27	02.4	09	
XI	-	03.4	10.0	04.9	05.8	10.5	02.0	18.4	18 -01.8	28,10	03	03.0	05	01.6	04	01.8	23	02.5	18	02.7	07	02.1	07	03.3	13	03.1	10	
XII	-	01.4	04.6	02.4	02.7	05.5	00.4	11.5	29 -04.4	25	12	01.9	01	02.0	03	01.3	10	02.7	11	01.9	26	02.5	14	02.8	09			
GOD.	-	08.7	15.4	10.6	11.3	16.3	06.8	34.0	03 05.5	-07.1	15	79	02.4	48	01.7	101	(2.0	255	02.8	125	02.5	65	01.9	135	07.4	167	02.0	120
$\varphi = 45^{\circ}56'N \lambda = 20^{\circ}05'E$ Gr. $\Delta G = +1h\ 20\ min.$																												
I	-	-00.2	04.0	01.4	01.6	04.6	-00.9	10.4	20 -08.0	15	06	02.2	03	01.7	12	01.2	25	02.1	08	01.9	10	01.6	03	01.3	14	02.8	02	
II	-	02.6	10.3	05.9	06.2	11.0	02.1	10.1	12 -02.0	28	04	01.0	03	02.0	10	01.9	03	02.3	07	02.1	01							
III	-	04.7	13.7	08.2	08.7	14.4	03.1	27.2	21 -03.8	01	01	01.0	11	01.9	10	02.5	41	02.3	14	01.9	05	02.2	02	02.5	03	02.0	06	
IV	-	07.6	15.4	10.3	10.9	16.4	04.7	23.9	30 -00.5	04	14	01.3	04	02.0	06	02.2	21	02.1	06	01.8	10	01.7	06	02.2	16	02.2	06	
V	-	13.0	19.2	14.5	15.3	20.3	09.8	29.3	31 02.5	10	*	*	C2	C2.0	C2	C2.0	07	01.7	07	01.7	18	01.8	23	02.0	25	01.8	09	
VI	-	16.5	22.2	17.1	18.2	23.8	12.9	31.5	27 08.2	08	01	01.0	05	01.2	*	*	02	02.0	05	02.2	22	01.7	13	02.5	30	02.3	11	
VII	-	18.1	25.3	19.6	20.6	27.2	14.5	35.0	17.14 -06.5	08	05	01.8	10	01.9	05	01.8	09	01.9	06	01.8	11	02.0	15	02.1	40	02.4	12	
VIII	-	19.3	28.3	21.1	22.5	29.6	16.3	36.4	04.03 10.8	08	05	01.8	10	01.9	05	01.8	09	01.4	06	02.2	07	01.6	13	01.8	23	01.7	15	
IX	-	14.2	23.8	15.9	17.5	24.8	11.3	30.5	03 02.1	28	05	01.4	05	01.6	07	01.6	15	01.9	*	*	10	01.8	08	01.2	17	02.1	23	
X	-	06.3	11.5	07.8	08.3	12.5	04.9	20.1	04 -00.7	31	06	01.2	03	01.7	12	02.3	06	02.5	23	01.8	16	02.2	11	01.6	10			
XI	-	03.3	10.2	05.2	06.0	10.5	02.5	18.1	17 -02.0	28,10	07	02	02.0	06	01.5	23	02.0	11	01.9	12	04.6	11	01.6	02				
XII	-	02.0	05.3	02.8	03.2	05.8	00.7	13.4	29 -03.6	25	06	02.2	01	01.7	02	02.0	11	01.7	19	01.9	19	02.6	23	02.4	01			
GOD.	-	09.0	15.8	10.8	11.6	16.7	06.8	36.4	04 08 VIII -06.0	15	49	01.8	58	01.7	51	02.0	231	02.1	98	02.0	156	01.8	132	02.2	222	02.1	98	
$\varphi = 45^{\circ}24'N \lambda = 20^{\circ}21'E$ Gr. $\Delta G = +1h\ 22\ min.$																												
I	-	-00.3	04.0	00.9	01.4	04.7	-01.4	10.0	22 -08.7	15	01	02.4	05	01.6	14	01.5	36	02.4	21	02.9	02	01.5	06	02.5	12	02.7	06	
II	-	02.4	10.2	05.3	05.8	10.9	01.9	16.9	16 -05.8	09	04	02.0	07	02.0	24	01.5	25	03.3	33	03.2	01	04.0	05	01.8	07	02.4	01	
III	-	04.6	12.8	07.4	08.1	13.6	03.2	24.8	23.21 -02.2	03	*	*	02	02.0	09	02.2	45	03.2	22	03.5	05	02.2	03	02.0	03	02.7	*	
IV	-	07.0	14.7	08.7	09.7	15.6	04.3	23.0	28 -03.7	04	03	03.6	09	02.4	04	02.8	23	03.1	18	02.9	06	02.0	09	02.1	10	02.5	03	
V	-	12.4	18.6	13.3	14.4	19.8	09.1	28.1	31 04.1	10	07	03.4	04	01.8	02	02.0	16	02.2	24	02.5	12	02.4	23	02.5	21	02.4	*	
VI	-	15.8	21.8	16.3	17.6	23.2	12.6	30.2	27 07.8	08	06	02.8	07	02.0	24	01.8	30	02.3	33	02.2	03	02.4	22	02.5	27	02.6	05	
VII	-	17.8	25.0	18.8	20.1	26.5	13.7	34.3	17 08.3	09	09	03.0	07	01.7	02	01.5	06	01.9	15	02.1	08	01.9	17	02.4	22	03.0	05	
VIII	-	19.4	27.8	20.6	22.1	28.9	16.1	35.4	04 09.0 08.07	06	06	01.0	04	01.5	12	01.9	20	02.0	19	02.3	04	02.0	13	02.5	05	02.5	05	
IX	-	13.7	23.5	16.2	17.4	24.7	11.4	30.4	03 03.4	28	06	02.0	07	01.9	08	02.1	25	02.4	13	02.3	05	02.4	13	02.6	07	02.0	16	
X	-	06.2	11.5	07.5	08.2	12.4	05.0	19.8	04 -00.1	31	05	01.6	05	01.8	05	02.2	18	02.4	17</td									

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha e _m mm	Padavine R mm				Broj dana na sat:																						
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. Min.	Σ	Max	Dat.	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	★	▲	△	▲	▲	■	□				
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. Min.	Σ	Max	Dat.	≤0.00.0	0.025.0	0.020.0	0.6	8	2.0	8.0	0.1	1.00.0	●	★	▲	△	▲	▲	■	□			
REČEJ																																
BR. ST.161																																
I 6.9 7.0 6.2 6.7	073.7	04.3	85	74	85	81	53	022	006.9	20	•	01	18	•	•	01	•	03	10	09	07	•	07	04	02	•	•	04	01			
II 6.8 6.5 5.4 6.2	109.6	04.8	82	55	71	69	31	016	010.5	24	•	•	04	•	•	02	•	06	10	08	02	01	08	01	•	•	•	•	01	03		
III 5.0 4.8 3.9 4.6	192.1	04.6	76	43	61	60	12	032	012.7	06	•	•	06	02	•	06	•	11	11	07	07	01	04	05	•	•	•	•	01	03		
IV 5.4 6.7 5.0 5.7	186.9	05.4	74	42	61	59	21	039	014.4	17	•	•	01	•	•	02	01	04	09	09	05	02	09	•	•	•	•	01	03			
V 6.6 6.5 5.8 6.3	216.4	08.4	91	53	80	71	25	084	019.0	23	•	•	04	•	•	13	•	05	11	17	12	04	17	•	•	•	•	01	03			
VI 5.2 7.1 4.3 5.6	215.5	11.1	81	56	80	72	35	100	021.5	30	•	•	10	01	•	03	03	04	17	13	04	17	•	•	01	09	•	•	01	03		
VII 4.3 4.2 3.1 3.9	285.8	12.0	80	46	78	68	28	082	022.1	20	•	•	15	09	01	01	01	12	03	16	12	02	16	•	•	•	•	01	02			
VIII 3.7 3.3 1.9 3.0	307.9	13.7	81	48	79	69	29	062	029.7	12	•	•	26	11	01	01	•	•	09	08	02	09	•	•	•	•	02	03				
IX 3.6 5.0 2.6 3.7	214.9	10.2	85	48	77	70	30	024	012.8	27	•	•	15	01	•	05	15	03	07	03	01	07	•	•	•	•	01	01				
X 7.8 7.5 5.6 7.0	092.2	06.9	92	71	87	83	39	107	017.4	16	•	•	01	•	•	02	01	02	13	23	18	01	23	•	•	04	•	04	01			
XI 7.9 6.0 4.5 6.2	101.8	05.5	87	65	85	79	43	023	007.7	29	•	•	05	•	•	09	02	04	10	09	06	•	08	•	•	04	02					
XII 6.4 8.3 6.9 7.9	047.2	05.0	93	83	90	89	49	053	011.1	08	•	02	11	•	•	07	01	01	19	15	10	01	13	03	•	•	•	•	02	02		
GOD. 6.0 6.1 4.6 5.6	2044.0	07.7	83	57	77	72	12	644	029.7	10/VII	•	03	46	72	22	02	52	06	•	•	146	103	19	138	13	02	•	•	04	18	21	06
SENTA																																
BR. ST.162																																
I 7.7 7.5 6.7 7.3	-	04.4	89	75	88	84	60	024	007.0	20	•	01	18	•	•	01	01	01	15	10	06	•	08	02	•	01	01	•	•	C3	01	
II 7.0 6.9 5.4 6.4	-	05.2	86	58	76	73	31	018	013.5	24	•	•	02	•	•	•	•	03	11	08	02	01	08	01	•	•	•	•	01	01		
III 6.1 5.8 4.6 5.5	-	05.7	79	48	68	65	19	026	006.0	08	•	•	06	03	•	•	•	07	10	07	07	•	05	05	01	•	•	•	•	C2	01	
IV 5.7 7.1 5.9 6.2	-	05.7	72	44	63	60	27	028	007.2	17	•	•	01	•	•	•	•	03	09	11	06	•	11	•	•	•	•	•	•	01	01	
V 6.5 6.5 6.7 6.7	-	09.5	82	58	79	73	30	124	029.5	23	•	•	05	•	•	•	•	03	16	18	10	05	18	•	•	•	•	04	01			
VI 5.5 7.3 5.7 6.3	-	11.7	81	60	80	74	36	165	078.4	30	•	•	14	02	•	•	•	02	08	18	11	04	18	•	•	•	•	10	01			
VII 4.4 4.8 4.7 4.6	-	12.6	81	51	75	69	31	046	012.2	20	•	•	20	11	01	•	•	10	06	14	09	01	14	•	•	•	•	02	01			
VIII 4.2 4.5 3.6 4.1	-	14.4	82	51	78	70	34	064	027.7	12	•	•	26	13	01	•	•	11	04	07	07	02	07	•	•	•	•	04	06			
IX 4.1 5.4 3.6 4.2	-	10.5	86	52	80	73	37	019	015.5	27	•	•	17	01	•	•	•	10	06	06	03	•	06	•	•	•	•	•	C1	03		
X 7.6 6.1 6.8 7.5	-	07.2	93	75	91	86	47	115	019.9	29	•	•	01	•	•	•	•	02	16	21	19	03	21	•	•	•	•	10	01			
XI 7.1 6.2 5.6 6.3	-	05.7	91	66	86	81	45	030	013.0	29	•	•	03	•	•	•	•	02	11	09	05	02	05	•	•	•	•	07	01			
XII 6.5 8.2 7.5 8.0	-	05.0	89	79	88	85	50	040	010.3	08	•	02	11	•	•	•	•	16	19	09	01	16	05	01	03	•	•	12	01			
GOD. 6.0 6.1 6.3 5.6	-	06.1	84	59	79	74	19	699	078.4	30/VII	•	03	42	85	27	02	•	•	54	130	148	94	19	141	13	02	01	04	•	23	48	C3
ZRENJANIN																																
BR. ST.163																																
I 7.3 7.0 5.4 6.6	083.8	04.3	86	73	86	82	58	019	005.3	03	•	02	21	•	•	11	03	04	12	08	06	•	06	02	•	01	01	•	•	C3	•	
II 6.7 6.2 4.5 5.8	125.4	05.0	83	58	74	72	40	018	007.2	07	•	•	05	•	•	14	07	05	08	09	04	•	09	•	•	•	•	•	•	•	03	•
III 5.2 5.3 4.5 5.0	193.4	05.0	75	50	65	63	24	033	014.9	06	•	•	08	•	•	23	07	09	11	07	04	01	06	05	02	•	•	•	•	01	03	
IV 6.3 6.8 5.4 6.2	136.2	05.9	77	49	70	65	33	036	010.7	18	•	•	03	•	•	21	07	01	13	12	06	01	12	•	•	•	•	01	01			
V 6.6 6.5 6.0 6.4	204.9	09.5	84	61	85	77	39	088	018.1	23	•	•	02	•	•	15	01	05	01	09	18	12	03	18	•	•	•	•	05	01		
VI 6.1 7.4 6.0 6.5	213.9	11.8	84	60	86	77	43	103	022.0	30	•	•	10	01	•	15	08	01	14	13	11	04	13	•	•	02	07	02	02			
VII 4.0 4.7 4.4 4.4	291.8	12.5	82	51	79	71	36	058	004.0	07	•	•	17	11	•	14	05	11	05	15	11	•	15	•	•	•	•	04	•	06		
VIII 4.1 3.5 2.1 3.2	298.1	13.5	81	46	80	77	68	030	051.8	1																						

Mjesec	Vazdušni pritisak Pn/m ²	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, fm (0-12)																
		Tm			Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	W.								
		7	14	21								5.	12.	5.	12.	5.	12.	5.	12.	5.	12.	5.	12.	5.	12.			
$\phi = 45^{\circ}09'N \lambda = 21^{\circ}19'E$ Gr. $\Delta G = +1h\ 25\ min.$																												
I	76.4	00.6	03.9	01.0	01.6	04.9	-01.6	09.0	27	-12.4	15	02	C2.6	C1	C2.0	C2	C2.5	30	C5.4	11	03.4	02	02.0	03	02.3	02	03.0	40
II	75.0	05.7	10.2	06.8	07.4	11.3	03.7	17.6	16	-04.1	09	-	-	01	02.0	-	-	38	C5.4	22	C3.6	02	02.0	03	02.7	-	-	18
III	75.6	06.7	13.1	09.1	09.5	14.0	04.4	26.6	21	-04.2	13	01	C2.0	04	C2.2	03	C2.0	43	C5.6	19	03.5	04	02.2	-	-	01	02.0	18
IV	75.1	08.0	14.5	09.5	10.4	15.5	04.9	22.6	30	-03.7	20	03	C1.2	06	C2.3	03	C2.7	25	C4.6	18	02.9	03	02.0	-	-	07	C2.3	23
V	75.1	12.9	18.3	13.5	14.5	19.6	08.6	27.2	31	01.6	10	05	C2.4	-	C1	C2.0	C9	04.0	15	02.7	02	02.0	15	02.5	07	02.7	39	
VI	75.1	16.6	21.6	16.7	17.0	23.2	12.4	29.3	27	06.3	09	02	C3.0	01	C2.5	01	C2.0	07	C4.7	14	02.7	09	02.3	09	02.3	11	03.0	35
VII	75.5	17.8	25.1	18.6	20.0	26.3	12.8	35.2	18	06.4	27	06	C2.3	06	C2.2	01	C1.0	09	C3.8	11	02.4	03	02.3	03	02.7	11	02.6	43
VIII	75.4	20.5	27.9	20.5	22.4	28.7	15.2	34.6	04	09.1	08	06	C2.7	05	C1.8	05	C2.2	21	C4.0	08	02.8	01	03.0	06	02.5	02	03.0	39
IX	75.7	16.8	23.9	17.4	18.9	24.8	12.3	31.1	04	01.6	28	02	C2.5	02	C3.0	C1	C2.0	34	C4.0	14	03.1	02	02.0	03	02.7	05	02.8	27
X	75.1	08.2	12.5	09.1	09.7	14.1	05.6	21.4	05	-02.5	19	-	-	04	C2.0	C1	C2.0	20	C5.4	16	03.1	08	02.2	14	02.1	03	02.0	27
XI	75.6	05.8	10.7	06.5	07.4	11.4	03.4	17.8	18	-02.2	30	01	C3.0	03	C2.0	C1	C2.0	26	C5.0	17	03.2	02	02.5	06	03.2	03	03.0	31
XII	75.7	01.9	04.5	03.1	03.2	05.7	00.3	11.4	29	-05.5	23	07	C1.1	01	C1.0	-	-	07	C4.4	24	02.8	04	02.0	10	02.5	02	02.5	38
GOD.	75.4	10.1	15.5	11.0	11.9	16.6	06.8	35.2	Tm	-12.4	H	35	C2.7	35	C2.1	19	C2.2	269	C4.9	189	C3.1	42	C2.2	72	C2.5	54	C2.7	380
$\phi = 44^{\circ}33'N \lambda = 19^{\circ}14'E$ Gr. $\Delta G = +1h\ 17\ min.$																									LICINICA		BR. ST. 167	
I	75.1	00.8	04.8	01.7	02.3	05.5	-00.2	11.3	27	-05.4	15	-	-	-	C3	C2.0	-	-	-	03	C2.0	02	C1.5	09	C3.1	76		
II	74.5	03.0	10.7	05.3	06.1	11.8	02.0	19.1	12	-03.8	28	04	C2.8	-	C7	C2.0	02	C2.0	01	C3.0	03	C3.0	02	C2.0	03	C1.7	62	
III	72.1	03.6	13.6	07.7	08.2	14.3	02.5	27.6	19	-05.0	02	01	C1.5	07	C7.3	15	C2.0	02	C2.0	-	02	C1.5	01	C3.0	-	C6	55	
IV	74.3	07.0	17.2	09.2	10.1	16.4	05.0	25.6	28	-00.4	04	05	C2.7	05	C2.0	08	C2.0	02	C1.5	-	11	C1.5	01	C4.0	03	C1.7	57	
V	74.6	12.4	19.3	13.2	14.5	20.7	09.4	30.0	31	04.8	10	04	C1.6	C3	C1.0	C1	C2.0	-	-	01	C1.0	10	C1.8	02	C3.0	09	C2.4	58
VI	74.0	15.8	22.6	16.9	18.0	24.0	13.6	30.8	27	08.4	13.0	09	C1.5	01	C2.0	-	-	C1	C2.0	06	C1.8	10	C2.6	08	C2.5	60		
VII	75.1	17.2	25.4	18.6	19.9	26.5	13.9	36.9	17	09.1	27	04	C1.0	02	C1.5	C7	C1.9	01	C2.0	-	08	C2.0	06	C2.3	09	C2.1	54	
VIII	75.1	18.1	28.0	19.4	21.2	29.2	15.2	36.0	04	10.7	30	07	C1.7	02	C1.5	06	C2.0	02	C1.7	-	06	C1.7	03	C2.3	07	C2.5	65	
IX	75.1	14.4	23.0	15.4	17.1	24.1	12.2	31.6	03	03.3	28	12	C1.6	02	C2.0	C4	C2.2	-	01	C2.0	01	C2.0	02	C2.5	05	C2.6	63	
X	74.2	06.2	12.6	07.4	08.4	13.9	04.6	22.7	04	-01.6	31	05	C1.6	-	01	C1.0	02	C1.5	01	C4.0	04	C2.0	05	C1.8	02	C2.4	73	
XI	75.2	03.4	11.0	04.7	06.0	12.3	02.1	22.8	16	-01.9	27	02	C1.5	-	01	C2.0	01	C1.0	06	C2.3	04	C2.0	02	C2.5	73	C2.5	63	
XII	75.0	02.1	05.6	02.9	03.3	06.8	00.6	14.4	29	-05.4	24	01	C3.0	-	-	-	-	01	C2.0	26	C1.8	03	C1.3	07	C2.6	55	C2.6	55
GOD.	75.1	08.7	16.0	10.2	11.3	17.2	06.7	36.9	Tm	-05.4	H	55	C2.0	22	C1.9	53	C2.0	02	C1.8	07	C2.3	86	C1.9	41	C2.3	59	C2.5	760
$\phi = 44^{\circ}11'N \lambda = 19^{\circ}21'E$ Gr. $\Delta G = +1h\ 18\ min.$																									LJUBČEVIA		BR. ST. 168	
I	-	00.0	04.9	01.3	01.9	05.5	-00.7	10.8	22	-05.4	14	01	C1.0	C1	C1.0	C5	C2.0	C3	C3.7	01	C2.0	05	C1.4	16	C1.4	20	C1.2	41
II	-	01.6	11.3	04.3	05.3	12.1	00.7	18.5	12	-04.0	01	07	C1.3	02	C1.0	C3	C1.0	05	C2.6	02	C1.0	01	C1.0	07	C1.2	41		
III	-	03.8	14.8	07.3	08.1	15.2	02.0	27.7	21	-03.8	13	02	C1.5	C3	C1.3	C8	C1.5	13	C3.2	-	-	01	C1.0	09	C1.2	16	C1.2	41
IV	-	05.3	15.0	08.2	09.2	15.9	04.1	24.0	29	-28.0	04	04	C1.2	C2	C1.0	C3	C2.0	-	-	03	C1.0	17	C1.2	10	C1.4	47		
V	-	10.2	19.0	12.4	13.5	20.0	08.7	29.1	31	03.5	05	05	C1.0	C3	C1.0	C4	C1.0	04	C1.0	01	C2.0	07	C1.9	08	C1.1	12	C1.1	51
VI	-	13.9	21.7	15.5	16.7	23.3	12.3	28.4	26.0	06.4	13	03	C1.3	C6	C1.0	C4	C1.0	05	C4.0	01	C1.0	08	C1.6	15	C1.7	09	C1.2	49
VII	-	14.7	25.2	17.0	18.5	26.0	13.2	34.9	17	06.7	09	04	C1.0	02	C1.0	06	C1.0	07	C3.1	02	C1.0	05	C1.0	07	C1.4	11	C1.5	50
VIII	-	15.7	27.4	18.1	19.8	28.5	14.7	35.0	04	C1.8	09	01	C1.0	05	C1.4	-	-	03	C1.0	10	C1.5	14	C1.8	27	C1.5	57		
IX	-	13.4	23.2	15.0	16.6	24.6	12.5	30.5	04	03.5	28	01	C1.0	03	C1.3	C6	C1.0	05	C1.3	01	C1.0	06	C1.2	03	C1.0	20	C1.3	51
X	-	05.6	13.0	07.1	08.2	14.4	04.8	22.0	08	-01.5	26	07	C1.4	-	-	-	-	03	C3.3	02	C1.0	02	C1.0	23	C1.3	41		
XI	-	02.0	10.0	03.7	04.8	10.9	01.0	18.1	16	-01.6	30	07	C1.3	-	-	-	-	02.7	01	C1.0	07	C1.0	17	C1.2	43			
XII	-	-00.9	02.8	06.4	00.7	03.9	-01.0	09.5	10	-11.6	25	06	C1.0	04	C1.0	03	C1.											

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha e _m mm	Padavine R mm	Broj dana na se:																												
	Insekticija broj sati						Tn	Tx	Tn	Tx	Tn	F (0-12)	Nm (0-10)	R mm	•	*	Δ	▲	▲	□															
	7	14	21	Sred. (Dles)	7	14	21	Sred.	Mn	Σ	Max	Dat.	=	<	<	<	<	>	>	>	>														
VRBAC																																			
I	7.4	7.1	6.5	7.0	073.5	03.9	77	67	79	74	30	019 005.2	18	01	.	19	.	.	18	10	02	15	10	06	10	03	05	.			
II	6.7	6.4	4.3	5.8	113.9	04.7	66	52	65	61	28	028 010.8	21	.	.	05	.	.	25	15	04	07	06	03	01	06	01	.			
III	5.4	5.4	4.3	5.0	184.8	04.4	62	42	53	52	18	015 004.8	07	.	.	07	05	.	22	16	10	10	05	04	05	02	01	01			
IV	6.8	6.9	5.2	6.3	159.5	05.4	66	46	61	58	24	039 009.7	16	.	.	03	.	.	21	10	.	06	12	08	12	12	02	.			
V	7.0	6.0	6.7	7.1	6.9	191.3	05.0	81	57	80	73	29	117 020.3	23	.	.	03	.	.	12	04	02	13	19	15	05	19	01	06	02	
VI	5.9	6.7	5.7	6.1	191.3	11.2	80	59	79	73	36	065 016.1	30	.	.	11	.	01	12	09	01	09	14	11	02	14	01	06	.		
VII	4.5	4.5	3.9	4.1	279.8	12.0	80	50	76	69	32	089 021.5	23	.	.	16	10	02	07	02	11	04	16	11	03	16	07	01	.		
VIII	3.8	4.0	1.7	3.1	286.0	12.5	71	45	72	67	29	057 024.2	13	.	.	28	12	02	17	11	12	02	08	05	02	08	05	02	.		
IX	4.6	5.1	4.1	4.6	203.8	09.9	68	47	69	61	28	083 035.2	27	.	.	16	02	01	22	13	06	04	06	04	03	06	02	03	.		
X	7.0	7.8	6.6	7.1	098.0	07.0	82	62	77	79	39	172 023.2	16	.	.	02	.	.	18	12	02	15	20	17	08	20	02	01	01	04	01
XI	6.0	6.1	6.0	6.3	107.2	05.5	78	62	76	72	32	054 019.4	29	.	.	03	.	.	21	11	04	09	12	07	01	12	01	01	05	02	.
XII	8.3	8.2	7.9	8.1	040.9	04.9	87	82	84	84	26	084 015.9	09	.	02	12	.	.	13	03	01	19	19	11	04	18	06	12	04	.	
GOD.	6.2	6.2	5.2	5.9	1930.0	07.5	75	56	72	68	18	822 035.2	270	01	02	51	79	24	06	210	116	55	115	147	103	29	146	14	02	.	.	02	33	36	04
BR. ST.167																																			
LGOZNICA																																			
BR. ST.167															H = 121 m H _b = 122.2 m h _t = 2.1 m h _r = 1.2 m																				
I	8.4	7.2	5.8	7.1	061.0	04.7	92	78	90	87	49	042 019.6	20	.	.	15	.	.	02	01	01	15	14	06	01	12	04	12	.		
II	6.8	4.8	4.6	6.2	111.8	05.3	88	58	79	75	32	028 008.0	07	.	.	06	.	.	03	02	03	10	12	08	01	12	01	03	.		
III	6.0	6.7	4.8	5.8	143.7	05.4	84	51	71	69	18	008 002.6	08	.	.	07	04	.	06	11	09	02	09	04	02	01	.				
IV	6.5	7.0	5.9	6.5	177.2	06.1	80	47	73	67	24	062 016.2	17	.	.	01	01	.	03	01	06	14	15	09	02	15	01	.			
V	6.3	7.2	5.6	6.4	206.3	09.1	82	55	83	73	29	089 012.6	13	.	.	05	01	.	04	01	05	09	18	15	02	18	01	10	.		
VI	5.4	7.3	6.2	6.3	204.8	11.4	81	56	81	73	34	113 027.7	25	.	.	13	01	.	04	03	04	05	15	12	04	15	14	.			
VII	4.5	4.3	3.9	4.2	276.1	12.4	81	51	81	71	28	034 010.3	20	.	.	19	13	.	03	01	13	05	12	08	01	12	05	.			
VIII	3.1	3.6	2.9	3.2	297.4	13.7	85	49	83	72	31	060 020.1	12	.	.	26	15	01	04	01	16	03	08	07	02	08	08	03	.		
IX	5.9	5.7	4.1	5.2	177.6	11.8	91	58	91	80	29	074 026.5	05	.	.	17	03	.	07	01	05	06	09	09	02	05	05	05	.		
X	7.4	7.0	6.5	6.9	112.3	06.9	92	66	90	83	35	146 022.2	24	.	.	02	.	.	03	02	03	13	20	19	04	20	02	06	.		
XI	6.4	6.4	4.5	5.6	097.5	05.7	91	63	70	81	34	065 017.9	08	.	.	05	.	.	02	01	03	08	10	07	03	10	01	05	.		
XII	7.7	7.9	5.8	7.1	046.9	05.0	88	76	86	83	46	065 014.1	13	.	01	11	.	.	02	01	05	17	17	13	02	06	01	07	07	.	
GOD.	6.2	6.2	5.1	5.9	1912.6	08.1	86	59	83	76	18	786 027.7	251	01	02	47	85	32	01	37	14	68	122	159	116	25	153	18	02	.	.	01	45	42	07
LJUBOVCIJA																																			
BR. ST.168															H = 170 m H _b = - m h _t = 2.0 m h _r = 1.2 m																				
I	8.4	6.5	5.5	6.8	-	04.7	94	78	92	88	42	080 034.7	20	.	.	17	.	.	03	14	18	07	03	18	04	03	13	.			
II	6.6	5.6	4.6	5.7	-	05.2	90	56	82	77	36	019 009.4	07	.	.	13	.	.	01	04	09	11	05	01	12	02	01	05	01		
III	6.3	6.5	3.7	5.5	-	05.5	87	49	76	70	19	008 003.7	07	.	.	08	05	.	01	06	05	09	02	07	04	01	01	04	01		
IV	6.6	7.0	5.4	6.5	-	06.1	90	49	79	72	20	064 016.7	19	.	.	06	.	.	03	11	16	11	02	16	01	01	02	05	.		
V	7.6	7.0	6.4	7.2	-	09.5	94	61	90	82	33	116 019.5	16	.	.	03	.	.	04	01	05	09	18	12	04	22	06	12	.		
VI	8.3	7.0	6.1	7.2	-	-	-	-	-	-	-	138 026.5	30	.	.	12	.	.	01	11	21	13	05	21	01	12	06				
VII	8.7	5.7	5.1	3.5	-	12.8	94	56	91	80	35	004 012.0	01	.	.	15	10	.	01	04	08	02	15	09	02	15	03	17	.		
VIII	8.9	4.3	2.9	5.4	-	13.8	96	54	89	80	32	082 025.8	28	.	.	24	15	.	02	05	20	08	03	14	12	21	.				
IX	9.1	5.9	4.4	6.5	-	-	-	-	-	-	-	070 020.5	08	.	.	15	02	.	01	08	16	08	02	16	07	16	.				
X	9.1	7.4	7.0	7.8	-	07.1	97	68	93	86	38	130 018.0	24	.	.																				

Meseč	Vazdušni pritisak Pm (mb)	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Pm (0-12)																	
		Tm			Max (Dnev.)	Min (Noc.)	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW	C			
		7	14	21							8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.					
$\varphi = 44^{\circ}37'N \lambda = 19^{\circ}47'E$ Gr. $\Delta G = 1h\ 14\ min.$																													
I	-	-00.1	04.5	01.6	01.9	05.0	-00.9	10.2	31	-07.2	15	10	02.9	.	.	.	06	02.2	10	03.6	67				
II	-	03.0	10.6	05.8	06.3	11.3	02.1	17.2	12	-04.0	28	16	02.1	02	03.5	.	01	02.0	04	02.5	61				
III	-	03.9	13.8	07.9	08.4	14.1	02.9	26.6	23	-03.0	01	27	03.5	09	07.3	.	01	02.0	.	01	03.0	55			
IV	-	06.7	15.2	09.3	10.1	16.0	05.2	23.5	29.2	-01.5	04	09	04.4	03	02.3	19	03.2	59			
V	-	12.8	19.3	13.4	14.7	20.1	09.6	30.0	31	06.0	11.0	06	02	02.0	.	.	02	03.5	.	.	.	03	02.7	15	03.3	71			
VI	-	15.6	21.9	17.1	17.9	23.3	19.0	25.0	27	07.5	13	03	02.0	01	03.0	.	.	.	23	03.5	63				
VII	-	18.0	25.3	18.7	20.2	26.6	13.8	35.0	14	05.5	27	01	03.0	04	01.5	07	02.7	79				
VIII	-	18.1	28.6	20.7	22.0	29.3	19.6	36.0	03	10.2	30	01	03.0	.	.	02	02.5	.	.	.	02	01.5	18	03.6	70				
IX	-	13.6	23.4	16.3	17.4	24.1	12.1	31.6	04	03.5	28	03	02.0	.	.	04	02.0	.	.	.	02	03.0	17	03.3	64				
X	-	06.0	11.9	07.5	08.2	13.0	04.6	21.5	04	-00.5	31	05	02.2	.	.	09	02.7	.	.	.	02	03.0	06	02.7	71				
XI	-	03.2	10.7	05.5	06.2	11.2	02.3	20.0	16	-01.0	11	04	02.2	.	.	07	02.7	.	.	.	04	02.5	06	04.0	69				
XII	-	02.0	05.3	02.9	03.3	06.3	00.2	17.0	29	-06.8	25	*	.	.	.	01	02.0	.	.	.	01	01.0	21	03.6	70				
GOD.	-	08.6	15.9	10.6	11.4	16.7	06.7	36.0	03	08.0	-07.2	45	19	02.2	.	.	87	03.0	11	06.6	01	03.0	01	02.0	30	02.2	147	03.4	707
$\varphi = 44^{\circ}17'N \lambda = 19^{\circ}55'E$ Gr. $\Delta G = + 1h\ 18\ min.$																													
VALJEVO																							BR. ST.172						
I	752.0	-00.1	04.9	01.1	01.8	05.7	-01.5	10.8	27	-07.0	15	01	04.0	03	01.3	06	02.2	01	03.0	.	01	02.0	07	02.7	04	02.8	70		
II	744.8	01.6	10.7	04.5	05.4	12.1	00.5	18.3	17	-06.4	28	.	.	05	01.2	07	02.1	04	03.0	02	02.5	02	03.5	07	01.6	.	57		
III	747.3	03.3	13.6	07.5	08.0	14.4	01.7	27.9	19	-04.7	02	02	01.0	06	01.2	20	02.0	06	03.0	01	02.0	.	02	01.5	55				
IV	743.5	06.5	14.2	08.4	09.4	15.4	04.0	23.3	28	-02.7	04	04	02.2	04	02.0	10	02.3	03	02.3	.	.	.	12	01.4	05	C1.8	57		
V	743.8	12.7	18.1	13.3	14.3	19.8	08.9	28.7	31	03.4	11	09	01.4	04	01.5	C4	01.8	.	.	05	02.6	.	.	14	01.4	01	C1.0	56	
VI	744.2	16.1	21.6	16.5	17.7	23.3	12.5	28.8	27	06.7	13	05	C2.0	.	01	02.0	.	.	04	02.2	.	.	16	01.9	05	C2.4	59		
VII	746.6	17.7	25.0	18.3	19.8	26.4	13.3	37.6	17	06.9	28	06	02.0	02	02.0	08	01.9	01	02.0	.	.	.	17	02.1	04	02.7	55		
VIII	746.7	18.1	28.2	19.7	21.4	29.1	14.9	34.8	05	04.0	08	04	01.8	05	02.4	16	02.1	02	01.5	.	.	.	11	01.9	02	03.4	53		
IX	746.1	13.6	23.6	15.8	17.2	25.0	11.3	32.0	04	00.7	28	04	01.5	05	01.6	C5	01.8	.	.	01	03.0	01	02.0	03	01.7	07	02.6	64	
X	743.4	05.6	12.6	07.3	08.2	13.8	03.9	21.5	12	-02.6	31	03	01.7	03	02.0	C4	01.8	02	02.0	04	02.2	02	01.6	04	01.8	67			
XI	748.2	02.0	11.0	04.2	05.4	11.8	00.8	20.2	16	-03.9	27	01	02.0	.	.	04	01.5	01	03.0	02	02.0	.	.	09	01.9	02	02.5	71	
XII	749.9	00.7	05.3	02.2	02.6	06.8	-01.4	13.0	29	-10.0	24	01	02.0	01	02.0	.	.	01	02.0	01	01.0	17	01.7	08	02.4	64			
GOD.	746.4	08.2	15.7	09.9	10.9	17.0	05.7	37.6	17	VII -10.0	24	41	40	01.8	38	01.7	05	02.0	20	02.6	20	02.3	08	02.2	118	01.8	44	02.3	722
$\varphi = 44^{\circ}48'N \lambda = 20^{\circ}28'E$ Gr. $\Delta G = + 1h\ 22\ min.$																							BR. ST.173						
BEOGRAD																													
I	756.1	00.5	04.2	01.6	02.0	04.8	-00.2	09.7	27	-06.3	15	.	.	01	02.0	22	C3.0	36	03.2	.	07	01.3	12	01.9	10	02.4	05		
II	748.8	04.5	10.8	06.5	07.0	11.6	03.9	17.6	12	-01.8	28	.	.	02	01.0	18	03.1	42	02.8	04	01.5	08	01.5	05	01.6	04	01.5	01	
III	751.6	05.6	12.9	08.5	08.9	13.7	04.6	26.6	19	-02.0	01	.	.	03	01.3	25	03.6	53	03.2	03	02.3	04	01.5	01	02.0	02	02.0	01	
IV	747.4	07.8	15.0	10.4	10.9	15.7	06.7	23.6	28	-02.7	15	01	02.0	06	01.8	18	02.7	28	02.8	01	01.0	10	01.4	13	01.8	11	02.2	02	
V	747.4	13.0	19.1	14.3	15.2	20.1	10.8	29.4	31	07.4	10	02	02.0	03	02.0	03	01.7	17	01.7	12	01.8	10	01.7	23	02.1	18	01.9	05	
VI	747.8	16.6	21.9	17.4	18.4	23.4	14.1	29.5	06	08.7	13	04	01.5	05	01.4	04	01.5	17	01.8	10	01.3	07	01.1	24	02.3	16	02.2	01	
VII	750.1	18.4	25.2	20.1	20.9	26.6	15.6	35.3	18	10.7	09	08	02.2	05	01.8	10	01.5	18	01.8	04	01.2	08	01.4	24	02.3	15	02.2	01	
VIII	750.5	20.3	27.9	21.7	22.9	28.7	17.9	34.9	04	12.8	12	04	01.8	03	01.7	22	02.0	33	01.9	02	01.0	14	01.9	09	02.4	05			
IX	749.9	15.6	23.2	17.2	18.3	24.3	13.9	30.2	04	05.5	28	05	02.4	02	02.0	10	01.9	39	02.2	01	02.0	07	01.6	16	02.0	07	02.1	03	
X	747.2	07.0	12.2	08.8	09.2	13.3	06.0	21.0	04	00.4	30	01	01.0	03	01.3	12	02.0	31	02.0	07	01.7	08	01.9	19	02.2	09	01.7	03	
XI	752.1	04.9	10.4	06.6	07.1	11.1	04.1	18.4	16	00.5	30	02	04.0	04	01.8	09	02.1	31	02.5	02	02.0	07	01.7	15	01.9	09	01.7	03	
XII	753.6	02																											

Mjesec	Oblačnost Nm (0-10)			Insolacije broj sati (des.)	Vlažnost vazduha			Padavine R mm			Broj dana nesna:																					
	7	14	21		em mm	U m s ⁻¹	t °C	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	☒					
	Sed. (des.)	7	14	21	Σ mm	Min	Max	1/1 0.00.0	< 0.0	< 0.0	> 0.0	> 0.0	> 0.0	8	2.0	8.0	0.1	1.00.0	IV	IV	IV	IV	IV	IV	IV	IV	IV					
VLADIMIRCI																																
BR. ST. 171																																
I	-	-	-	-	-	04.6	92	76	90	87	57	025	011.0	20	-	01	19	-	-	-	-	10	04	01	10	01	01	-	06			
II	-	-	-	-	-	05.4	87	62	79	76	37	020	009.1	07	-	05	-	-	-	-	-	08	05	-	08	-	-	-	04			
III	-	-	-	-	-	05.6	84	54	70	70	27	008	003.0	07	-	09	04	-	-	-	-	04	03	-	04	02	02	-	01			
IV	-	-	-	-	-	06.8	82	59	78	73	33	075	014.5	17	-	01	-	-	-	-	-	11	10	03	11	-	-	-	01			
V	-	-	-	-	-	10.0	86	63	87	79	38	060	011.0	23	-	-	03	01	-	-	-	16	16	02	16	-	-	-	-			
VI	-	-	-	-	-	-	-	-	-	-	-	140	053.7	30	-	-	13	-	-	-	-	13	13	04	13	-	-	-	01			
VII	-	-	-	-	-	12.9	81	54	81	72	23	046	009.0	24	-	-	19	13	-	-	-	11	11	01	11	-	-	-	-			
VIII	1.4	1.4	2.1	1.6	-	-	-	-	-	-	-	042	019.5	12	-	-	27	16	-	-	-	21	21	08	05	01	08	-	-			
IX	4.7	2.2	2.3	3.1	-	11.9	90	61	86	79	35	060	015.5	27	-	-	14	02	-	-	-	15	04	10	09	03	10	-	02			
X	5.4	5.6	5.3	5.5	-	07.0	93	72	90	85	38	157	031.4	24	-	-	01	-	-	-	-	10	11	15	19	05	19	-	05			
XI	6.7	3.5	3.7	4.6	-	05.9	92	68	87	83	39	060	014.5	09	-	-	03	-	-	-	-	08	06	09	03	01	09	01	12			
XII	7.0	2.5	5.2	6.1	-	051.1	88	61	87	85	53	066	015.0	15	-	02	15	-	-	-	-	06	12	14	16	10	13	05	03			
GOD.	-	-	-	-	-	-	-	-	-	-	-	781	053.7	30	-	-	03	53	8C	32	-	-	133	113	21	132	05	07	-	01		
VALJEVO																																
BR. ST. 172																																
I	8.1	7.4	5.4	6.9	-	064.8	04.6	92	75	91	86	46	050	024.1	20	-	-	20	-	-	-	01	-	02	13	12	09	01	02			
II	5.6	6.4	5.2	6.1	-	110.1	04.9	89	53	81	74	30	C19	006.2	07	-	-	12	-	-	-	04	-	06	11	10	05	04	02			
III	5.9	6.1	4.2	5.4	-	160.9	05.1	84	47	69	66	18	010	004.1	07	-	-	09	03	-	-	02	-	05	11	06	03	02	03			
IV	5.8	7.3	5.3	6.1	-	162.3	05.6	78	47	75	67	21	081	017.2	17	-	-	03	-	-	-	04	-	05	10	03	15	01	03			
V	6.6	7.1	6.4	6.7	-	187.1	09.1	80	58	84	74	29	144	020.8	08	-	-	01	-	-	-	04	01	02	11	20	16	05	20			
VI	6.2	7.6	6.7	6.8	-	183.2	11.6	82	57	88	75	35	177	054.1	19	-	-	13	-	-	-	02	-	03	13	20	17	05	20			
VII	3.0	4.6	3.9	4.1	-	217.6	12.3	80	58	84	71	25	042	011.1	01	-	-	19	11	-	-	01	-	11	08	11	08	01	11			
VIII	3.5	3.6	2.2	3.1	-	296.5	13.2	82	44	81	69	31	038	020.3	12	-	-	27	15	-	-	01	-	16	03	06	04	02	06			
IX	4.7	5.5	4.4	4.9	-	208.5	11.5	90	54	90	78	32	047	015.3	05	-	-	16	03	-	-	03	-	07	06	08	06	02	08			
X	6.3	7.2	6.6	6.7	-	114.0	06.9	92	66	92	84	36	175	049.0	24	-	-	04	-	-	-	01	-	15	14	19	19	02	01			
XI	6.7	6.6	4.8	6.0	-	107.6	05.5	92	62	91	81	34	097	023.4	09	-	-	13	-	-	-	02	-	05	09	11	09	04	11			
XII	7.0	8.4	5.6	7.0	-	054.6	04.7	89	73	86	83	46	078	013.2	15	-	01	01	20	-	-	-	01	-	03	15	16	13	05	01		
GOD.	5.9	6.5	5.1	5.8	-	1899.7	07.9	85	57	84	75	18	958	054.1	44	-	-	01	01	81	79	29	-	-	27	01	70	124	154	115	31	146
BEGGRAD																																
BR. ST. 173																																
I	7.5	6.5	5.5	6.5	-	083.4	04.3	85	71	82	79	48	026	010.0	20	-	-	15	-	-	-	17	03	04	10	09	07	01	08			
II	6.2	6.0	5.2	5.8	-	120.1	05.1	78	54	69	67	37	C24	009.8	07	-	-	03	-	-	-	18	02	04	10	09	06	05	01			
III	4.9	5.1	4.5	4.8	-	179.8	04.7	68	47	59	58	19	022	010.2	06	-	-	06	04	-	-	22	12	09	10	07	04	01	05			
IV	6.3	6.7	6.1	6.4	-	169.9	05.6	69	45	62	59	23	046	009.5	17	-	-	03	-	-	-	16	02	14	13	10	12	01	01			
V	6.0	4.9	5.8	6.2	-	202.5	08.8	77	53	77	69	32	080	012.4	16	-	-	03	-	-	-	06	01	02	09	20	18	01	26			
VI	5.9	7.0	5.5	6.1	-	197.3	11.3	79	58	78	71	38	175	043.8	30	-	-	13	-	-	-	02	06	01	04	11	16	06	18			
VII	3.6	3.4	3.5	3.8	-	289.1	11.9	75	50	75	70	65	27	041	019.2	24	-	-	18	12	04	-	06	13	10	04	10	06	10			
VIII	4.0	3.0	2.5	3.3	-	296.4	12.9	71	46	66	62	30	059	017.4	13	-	-	27	13	07	07	13	C3	07	06	03	07	05	01	05		
IX	4.5	5.3	4.0	4.6	-	208.7	10.9	79	53	76	69	33	099	039.4	27	-	-	16	01	-	-	12	04	07	04	07	07	03	07			
X	6.7	7.3	7.2	7.1	-	104.3	07.2	51	69	86	82	30	185	037.4	14	-	-	06	02	04	15	21	20	06	21	21	02	01	01			
XI	6.1	5.8	5.3	5.8	-	195.9	05.9	68	45	83	78	37	063	016.0	29	-	-	09	03	08	09	09	02	09	01	01	01	06	01	06		
XII	7.5	8.0	7.2	7.6	-	051.6	05.0	87	79	62	83	45	090	022.5	16	-	01	10	-	-	07	-	02	16	15	10	03	11	05	01		
GOD.	5.8	6.0	5.2	5.7	-	1997.2	07.8	78	57	74	70	19	910	043.8	30	-	-	01	34	81	26	13	141	30	71	110	145	119	27	138	16	
GORNJI MILANOVARAC																																
BR. ST. 174																																
I	-	-	-	-	-	-	-	-	-	-	-	-	055	022.3	20	02	-	23	-	-	-	-	-	11	08	01	08	05	01	-	03	
II	-	-	-	-	-	-	-	-	-	-	-	-	023	011.6	09	-	-	16	-	-	-	-	-	08	05	01	07	01	-	-	04	
III	-	-	-	-	-	-	-	-	-	-	-	-	016	003.5	16	-	-	15	02	-	-	-	-	09	08	04	05	01	-	-	02	
IV	-	-	-	-	-	-	-	-	-	-	-	-	065	017.5	19	-	-	10	-	-	-	-	-	13	09	03	13	01	-			

Mesec	Vazdušni pritisak Pr. mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, fm (0-12)																	
		Tm			Sred. (dies)			Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C							
		7	14	21										6	3	8	3	8	3	6	3	8	3	8					
$\varphi = 44^{\circ}18'N \lambda = 20^{\circ}33'E$ Grd. AG + 1h 22 min.														BUKOVICA BANJA															
I	-	-00.4	03.8	00.5	01.1	04.6	-02.6	10.1	31	-09.7	15	01	02.0	05	02.2	09	01.9	28	01.9	14	01.6	*	*	14	02.2	21	01.9	02	
II	-	02.3	05.8	04.3	05.2	10.7	01.3	16.4	02	-06.0	26	07	01.0	03	01.0	14	01.7	23	01.6	11	01.8	05	02.0	05	02.2	12	02.7	09	
III	-	03.7	12.3	06.0	07.0	12.9	02.6	26.0	19	-06.0	01	01	03.0	03	02.8	10	03.0	23	02.1	06	01.5	02	03.5	*	*	02	02.0	07	
IV	-	06.4	13.7	07.8	08.9	14.7	03.9	22.5	28	-02.5	04	02	01.5	02	02.0	10	01.4	20	02.1	03	01.3	01	03.0	17	02.1	12	02.9	13	
V	-	12.5	17.6	12.4	13.7	19.3	09.3	26.9	31	04.7	11	02	01.0	02	01.0	*	*	02	01.0	09	01.2	03	02.1	44	01.9	14	03.1	17	
VI	-	15.9	21.2	15.5	17.0	22.5	12.5	25.5	06	07.5	09	01	01.0	01	01.0	04	01.0	01	01.0	08	01.4	05	07.0	34	01.6	08	02.9	28	
VII	-	17.5	23.8	17.0	18.8	25.6	13.2	34.7	18	08.5	27	01	01.0	01	01.0	05	01.0	02	01.0	04	01.7	05	01.6	33	01.4	08	02.1	34	
VIII	-	17.8	27.8	18.4	20.6	28.5	14.8	34.5	04	10.5	30.0	04	01.0	01	01.0	15	01.3	01	01.0	05	01.0	*	*	17	01.9	08	02.8	47	
IX	-	13.9	23.5	15.0	16.8	24.7	11.5	33.0	04	02.5	28	*	*	01	01.0	10	01.1	07	01.3	05	01.2	02	01.0	20	02.4	04	02.0	41	
X	-	06.0	12.0	06.8	07.9	13.0	04.1	21.0	12	-02.0	31	01	01.7	01	02.0	09	01.0	02	01.0	12	01.2	*	*	19	01.7	14	02.1	33	
XI	-	02.9	10.6	04.6	05.2	11.4	01.4	18.5	19	-02.2	04	02	01.5	01	01.0	14	01.4	09	01.2	04	01.0	02	02.0	17	02.0	06	02.5	31	
XII	-	02.1	05.0	02.7	03.1	06.8	-00.4	16.0	29	-07.5	25.2	04	01.0	00	*	*	02	01.5	05	01.2	03	01.7	06	01.8	47	01.5	15	01.5	14
GOD.	-	08.4	15.1	09.2	10.5	16.2	06.0	34.7	28	-09.7	01	20	01.4	19	01.6	132	01.5	113	01.8	80	01.4	31	01.2	27	02.3	124	02.6	301	
$\varphi = 44^{\circ}51'N \lambda = 20^{\circ}40'E$ Grd. AG + 1h 22 min.														PANČEVO												BR. ST. 177			
I	-	-00.4	03.8	00.3	01.0	04.4	-01.9	09.4	20	-10.2	15	01	02.0	01	02.0	04	02.0	41	03.0	04	02.8	*	*	67	02.4	09	02.8	26	
II	-	01.7	10.7	04.1	05.0	11.1	00.4	16.6	12	-06.2	05	*	*	*	*	06	02.2	42	03.0	05	02.8	*	*	66	01.8	04	02.0	21	
III	-	03.4	12.6	06.5	07.3	13.8	01.8	25.9	19	-05.0	01	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*			
IV	-	06.7	15.0	09.0	09.9	16.0	04.5	22.6	28	-02.6	03	05	03.2	01	02.0	18	04.1	14	03.1	02	02.0	*	*	11	02.8	05	02.8	34	
V	-	12.5	19.0	13.6	14.7	20.4	09.7	29.3	31	04.5	11	02	07.5	*	*	04	01.5	05	02.7	03	01.0	27	01.6	10	02.7	40			
VI	-	16.4	22.1	16.9	18.1	23.7	12.9	30.2	27	08.0	09	*	*	01	02.0	01	02.0	04	02.5	04	02.2	02	01.0	24	01.1	10	02.4	43	
VII	-	17.8	25.3	19.0	20.3	26.6	13.6	34.5	17.14	08.5	27	06	01.8	*	*	02	02.5	02	03.0	01	01.0	*	*	21	01.8	10	01.2	51	
VIII	-	19.1	28.2	20.4	22.0	28.9	15.5	35.5	04	16.4	08	01	04.0	02	02.5	11	03.0	06	02.3	*	*	62	03.0	13	01.0	59			
IX	-	14.1	23.5	16.8	17.8	24.7	11.7	31.2	04	02.2	27	03	02.0	*	*	09	02.7	12	02.5	01	02.0	*	*	12	02.3	03	01.7	51	
X	-	05.9	12.2	07.9	08.5	13.3	04.6	20.0	12	-01.0	31	*	*	01	02.0	07	02.3	08	02.0	01	02.0	02	01.5	19	01.5	07	01.0	51	
XI	-	03.1	10.3	05.1	05.9	11.2	02.0	17.6	13	-01.5	30	01	03.3	01	02.0	11	02.8	11	02.9	*	*	01	02.0	11	02.8	02	02.6	50	
XII	-	01.2	04.2	02.3	02.6	05.7	-00.2	12.1	29	-06.2	25	*	*	05	03.0	06	02.8	*	*	02	02.9	71	01.8	04	02.8	49			
GOD.	-	08.5	15.8	10.2	11.1	16.6	06.2	35.5	28	-10.2	04	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*			
$\varphi = 44^{\circ}39'N \lambda = 20^{\circ}57'E$ Grd. AG + 1h 24 min.														SMEĐEVRETE												BR. ST. 178			
I	-	00.2	03.9	00.8	01.4	04.5	-01.0	05.8	27	-07.5	14	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*			
II	-	03.9	10.5	05.4	06.3	11.2	02.4	17.1	12	-03.5	27	27	*	*	*	*	*	*	*	*	*	*	*	*	*	*			
III	-	05.1	13.2	07.9	08.5	13.9	03.5	26.5	21.19	-05.0	01	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
IV	-	07.1	14.8	09.4	10.2	15.9	04.9	23.2	28	-01.7	04	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
V	-	13.0	19.0	13.3	14.6	20.1	05.8	27.5	31	05.0	10	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
VI	-	15.7	22.7	16.4	17.8	23.8	12.7	29.2	27	08.5	13	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
VII	-	17.6	25.7	17.7	19.7	26.8	14.1	35.2	18.14	09.5	27	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
VIII	-	18.1	28.1	18.9	21.0	28.7	15.7	34.5	05.04	10.0	08	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
IX	-	14.5	23.5	16.1	17.6	24.5	12.4	31.5	04	03.0	28	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
X	-	06.5	12.5	08.1	08.8	13.9	04.8	20.0	12	-02.0	31	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
XI	-	04.2	10.6	05.7	06.5	11.2	02.4	16.2	16	-01.8	04	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
XII	-	01.2	04.8	02.5	02.8	06.0	-00.6	12.5	29	-06.4	25	*	*	*	*	*	*	*	*	*	*	*	*	*	*				
GOD.	-	08.5	15.8	10.1	11.1	16.9	05.8	35.6	28	-10.4	01	58	02.2	24	01.8	06	01.5	139	02.3	90	01.9	02	01.0	128	02.7	515			
$\varphi = 44^{\circ}02'N \lambda = 20^{\circ}56'E$ Grd. AG + 1h 24 min.														SMEĐEVRSKA PALANKA												BR. ST. 180			
I	757.1	-00.4	03.5	00.6	01.1	04.3	-01.7	09.0	27	-10.2	15	05	01.0	03	01.0	26	02.0	29	02.4	05	02.0	01	02.0	12	02.6	10	02.4		

Mjesec	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha		Padavine R mm		Broj dana na snazi:																			
						U m t		R mm		Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	□	■	■	
	7	14	21	Sred. (Dnev.)		mm	7	14	21	Stred. Min	Σ	Max	Dat.	≤	<	<	IV	IV	IV	IV	IV	<	>	IV	IV	IV	IV	IV	IV
BR. ST.176 BUKOVICKA BANJA																													
I 9.0 7.0 7.1 7.7	-	04.2 87 76 85 F3 46	02F 006.4	20	.	01	22	.	.	.	CZ	.	C3	18	11	07	08	02	01		
II 6.1 6.0 5.3 5.8	-	05.0 86 57 82 75 24	030 015.4	07	.	09	04	06	12	05	01	11	02	01	01	03		
III 5.2 4.7 5.0 5.0	-	05.2 80 53 76 70 21	020 007.2	06	.	14	04	.	.	.	07	11	08	06	06	04	01	02		
IV 6.2 6.3 6.4 6.3	-	06.0 77 53 79 70 24	084 012.5	18	.	02	04	09	13	1C	05	13	05	02	.	.	01	01	03	01	01	01			
V 5.9 6.3 6.6 6.3	-	08.8 77 59 86 74 32	122 C17.5	19	.	02	.	.	.	01	C2	C5	19	14	09	14	09	06	01			
VI 4.8 4.7 6.1 5.2	-	11.2 81 59 86 76 38	129 025.6	20	.	09	.	.	.	C1	.	C5	20	16	05	20	05	.			
VII 3.5 3.4 3.5 3.5	-	12.8 80 61 87 76 35	046 014.5	24	.	17	10	.	.	14	05	13	13	07	02	13	01	01			
VIII 2.9 3.1 2.3 2.8	-	-	-	033 018.4	10	.	24	14	.	C1	.	17	03	04	C1	04	03	.				
IX 5.2 4.5 4.9 4.9	-	11.1 87 54 88 76 36	C61 C3E.7	27	.	04	.	18	04	C1	C4	C5	07	04	02	07	.	.	.	01	C1				
X 6.3 6.4 6.4 6.3	-	06.9 91 70 93 85 39	143 024.3	01	.	04	.	04	.	04	13	21	1P	05	21	02	C1	C6	01			
XI 5.8 4.8 4.5 5.0	-	05.9 90 71 89 83 41	069 016.1	09	.	06	.	01	.	01	07	05	09	09	04	09	02	02	13	01		
XII 7.6 6.7 5.5 6.6	-	04.9 86 80 85 84 42	048 015.8	09	01	17	.	01	.	02	12	17	14	03	13	07	10	.			
GOD. 5.7 5.3 5.3 5.4	-	-	-	-	848 038.7	27IX	.	02	72	74	28	.	06	01	73	1C3	154	114	32	144	27	1C	.	.	02	01	21	-	
BR. ST.177 PANČEVC																													
I 7.2 6.0 5.8 6.4	-	04.5 93 84 92 90 59	01P 003.8	18	01	23	.	01	.	C8	01	05	12	09	06	08	04	02	02	C6	02			
II 5.2 4.2 5.1	-	05.2 91 59 82 77	-	021 010.6	07	.	12	.	.	12	09	07	04	03	01	04	02			
III 4.7 4.0 3.4 4.1	-	05.3 71 36 58 55	-	025 014.2	06	.	12	03	.	07	01	15	C8	05	04	01	04	02	01	01	.		
IV 6.4 6.2 5.3 6.0	-	05.7 75 46 68 69 24	042 012.4	17	.	04	.	01	.	C2	04	06	09	09	09	01	05	01	.			
V 5.5 6.3 5.6 5.8	-	09.4 85 56 64 75 36	079 010.2	06	.	04	.	04	.	1C	03	C5	08	18	16	03	18	.	.	.	05				
VI 5.6 4.1 4.8 5.5	-	12.0 83 66 84 76 35	111 075.7	30	.	14	01	.	04	04	08	16	16	04	16	04	01	.	.	.				
VII 3.9 4.3 3.8 3.8	-	-	-	032 009.2	23	.	18	12	.	05	02	13	05	11	07	11	09	.			
VIII 2.8 2.3 2.5 2.5	-	-	-	059 024.5	13	.	17	13	01	05	18	C4	07	C7	C2	C7	03			
IX 4.3 4.6 3.2 4.0	-	11.0 85 54 78 72 34	093 031.2	05	.	16	03	.	1C	02	1C	04	07	07	03	07	C3	04	.	.	.			
X 6.3 7.1 6.6 6.7	-	07.1 93 65 90 84 40	164 030.1	14	.	03	.	03	.	03	04	15	20	2C	05	2C	02	01	03	.	.	.			
XI 6.3 5.7 4.6 5.5	-	05.8 91 67 89 82 34	056 015.6	08	.	05	.	03	.	03	04	09	09	08	02	05	01	01	09	.	.			
XII 9.0 8.1 6.3 7.8	-	05.0 93 85 90 89 64	069 014.0	09	02	15	.	05	.	05	01	17	18	10	03	13	06	01	17	.		
GOD. 5.6 5.5 4.7 5.3	-	-	-	-	781 031.2	05IX	01	02	74	82	25	01	71	17	98	108	133	110	75	126	15	05	02	.	.	.	17	40	
BR. ST.178 Smederevc																													
I 7.1 5.6 5.8 6.2	-	-	-	-	C27 013.0	20	01	18	06	14	08	07	C1	06	03	01	05	.		
II 5.9 4.5 4.9 5.1	-	-	-	-	C26 010.2	21	.	05	.	.	.	10	08	05	05	01	05		
III 3.1 3.1 3.8 3.6	-	-	-	-	041 020.0	06	.	08	05	.	.	18	C6	05	05	02	03	05	03	02		
IV 5.7 5.6 4.4 5.2	-	-	-	-	C58 C11.3	15	.	04	.	.	.	08	09	08	07	02	08			
V 4.6 5.0 5.4 5.1	-	-	-	-	094 013.0	01	.	03	.	.	C8	06	18	17	03	16	.	.	01			
VI 4.9 5.5 5.4 5.3	-	-	-	-	130 052.8	30	.	17	.	.	07	07	13	11	03	13			
VII 3.2 3.0 1.5 2.8	-	-	-	-	050 C14.0	23	.	18	13	.	17	C2	08	06	02	08	.	.	01	01	.			
VIII 2.1 1.9 1.4 1.8	-	-	-	-	055 034.0	13	.	28	12	02	.	23	C1	06	06	01	04	01	.			
IX 4.2 3.4 2.7 3.4	-	-	-	-	C78 040.0	05	.	15	03	.	13	05	C6	05	02	06	.	.	01	01			
X 6.4 6.7 6.1 6.4	-	-	-	-	176 027.0	30	.	03	.	.	03	13	21	21	02	22	C2	04	01			
XI 5.2 5.6 5.1 5.3	-	-	-	-	079 025.0	09	.	03	.	.	09	08	09	04	09	01	01	01	01	06		
XII 8.2 7.0 6.8 7.4	-	-	-	-	C95 C23.2	15	.	17	.	.	02	17	16	14	03	15	04	02	09	06		
GOD. 5.1 4.8 4.4 4.8	-	-	-	-	941 052.8	30VI	01	58	86	26	02	.	04	01	67	112	140	100	26	129	20	06	.	.	01	30	01	21	
BR. ST.180 SPEDEREVSKA PALANKA																													
I 7.6 6.5 6.0 6.7	-	074.7 042 88 75 86	E3 53	C42 G20.1	20	01	02	20	.	.	06	03	02	11	12	07	01	12	04	01	01	.	.	.	04	03	.		
II 6.2 5.6 6.2 6.2	-	121.2 047 83 52 73	23	027 CC4.7	21	.	10	.	.	01	06	10	07	05	04	11	09	06	09	01	01	.	.	.	01	01	.		
III 5.4 5.0 4.1 4.8	-	153.1 046 78 48 60	62 19	034 017.7	06	.	11	03	.	18	11	08	07	01	02	05	04	01	05	07	02	02	.	.	.	04	03		
IV 6.6 7.0 6.0 6.5	-	180.1 056 78 47 66	64 24	049 011.1	15	.	06	.	.	18	07	04	12	08	07	03	06	07	C3	06	04			

Mesec	Vrstdusni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednje jačina veta mD, fm (0-12)																
		Tm			Sred. (danes)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21								E.	J.	S.	D.	E.	J.	S.	D.	E.	J.	S.	D.	E.	J.	C		
$\psi = 44^{\circ}56'N \quad \varphi = 21^{\circ}05'E \quad E.G. = +1h 24 min.$																												
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	02.8	04.5	03.6	04.9	10.4	06.1	16.2	12 -11.9	09	0.1	02.0	01	02.0	-	-	43	04.0	13	02.2	01	02.0	01	02.0	03	02.3	20	
III	-	04.2	12.0	05.7	07.0	13.2	02.2	25.8	21 -05.2	15	-	-	-	01	03.0	65	04.0	03	02.2	01	03.0	01	02.0	03	02.0	23		
IV	-	05.8	14.5	06.3	06.2	15.4	01.2	23.0	30 -08.2	04	31	01.7	01	01.0	-	-	26	04.0	12	07.3	01	02.0	04	02.5	03	03.0	31	
V	-	12.1	18.7	11.7	13.5	19.7	06.1	27.8	31 -01.8	11	0.6	02.0	-	-	02	02.5	09	02.8	14	02.4	03	03.3	16	02.6	15	02.9	28	
VI	-	15.7	21.7	14.7	16.7	23.0	10.2	29.4	27 -02.0	09	0.5	01.6	-	-	07	02.7	10	02.4	05	03.0	12	02.6	12	03.4	35			
VII	-	17.2	24.8	16.2	18.6	25.9	10.1	35.0	18 -01.8	27	11	02.4	-	-	05	02.0	06	03.7	08	02.2	-	08	07.1	14	02.5	41		
VIII	-	18.3	26.9	16.8	19.7	27.6	11.5	33.0	04.0,07	04.0	08	0.6	02.6	-	-	03	02.3	16	02.6	10	02.9	03	03.0	02	02.5	06	03.6	46
IX	-	13.5	23.3	13.8	16.1	24.2	09.8	30.8	04 -02.0	28	0.2	01.0	01	04.0	05	02.2	20	03.4	15	02.5	01	03.0	03	01.3	09	03.1	34	
X	-	05.6	12.4	06.3	07.7	13.6	02.5	20.8	06 -05.5	19	0.2	01.7	-	-	05	02.8	14	03.3	18	02.7	06	02.3	08	02.6	05	02.6	34	
XI	-	02.5	10.5	03.7	05.1	11.3	00.3	19.0	17 -05.5	30	0.1	01.4	-	-	29	03.0	14	02.3	01	02.0	02	02.0	09	03.4	36			
XII	-	-00.2	04.5	01.8	01.8	05.4	-02.4	11.5	29 -11.0	23,10	1.6	02.1	-	-	02	02.6	20	02.5	-	10	01.2	07	02.1	16				
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\psi = 44^{\circ}56'N \quad \varphi = 21^{\circ}05'E \quad E.G. = +1h 24 min.$																												
I	-	-00.8	03.1	-00.3	00.4	03.7	-02.5	09.2	22 -12.2	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	02.0	09.0	04.3	05.1	09.9	01.2	16.0	12 -05.2	09	-	-	02	01.0	47	03.6	13	02.5	01	01.0	-	-	04	02.0	-	-	17	
III	-	04.2	12.0	06.8	07.6	13.0	03.1	25.8	19 -03.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	06.9	13.9	08.2	09.3	15.2	02.3	21.0	28,12 -02.0	23,22	-	-	03	01.0	26	02.4	06	01.0	-	-	-	11	01.6	06	03.3	24		
V	-	11.8	18.7	13.0	14.2	19.9	06.6	28.0	31 04.0	24,08	01	03.0	06	02.0	10	02.0	15	01.6	-	02	01.5	17	02.4	10	02.1	32		
VI	-	15.5	22.1	15.7	17.2	23.3	11.7	29.2	27 07.0	08	0.1	01.0	04	01.5	12	01.5	12	02.1	-	02	01.5	25	02.9	11	01.4	23		
VII	-	17.7	25.1	17.7	19.5	26.4	12.5	36.2	18 06.2	09	-	03	01.0	16	01.5	05	01.8	01	01.0	03	02.0	20	02.0	17	01.8	20		
VIII	-	19.4	27.6	19.4	21.5	28.4	14.7	34.7	03 09.2	07	-	-	03	01.0	22	01.7	22	01.5	-	-	-	11	02.0	07	02.6	26		
IX	-	15.0	23.4	15.4	17.3	24.3	11.1	31.0	04 01.2	28	-	-	01	01.0	19	02.2	25	02.4	02	01.5	02	01.0	10	01.1	07	03.2	24	
X	-	06.1	11.9	07.6	08.3	13.3	02.2	20.2	08 -01.2	28,27	-	-	02	01.0	03	02.7	20	03.0	-	08	01.5	05	01.2	09	01.4	46		
XI	-	03.4	09.4	04.5	05.6	10.4	02.2	17.0	18,17 -02.2	30	0.4	02.0	-	-	05	01.6	36	02.5	-	05	01.0	02	02.5	10	01.7	32		
XII	-	00.4	04.0	01.7	02.0	04.7	-00.8	10.0	29 -07.0	25	0.4	01.2	02	01.0	03	01.0	14	01.7	02	01.0	01	01.0	21	02.0	10	02.2	36	
GOD.	-	03.6	15.0	09.5	10.7	16.0	05.7	36.2	04,01 -12.2	45.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\psi = 44^{\circ}54'N \quad \varphi = 21^{\circ}23'E \quad E.G. = +1h 25 min.$																												
I	-	00.3	03.7	04.9	01.5	04.4	-01.2	05.4	22 -05.5	15	-	-	-	-	04	02.0	26	02.0	07	02.3	03	02.0	07	01.1	17	01.4	29	
II	-	03.8	16.0	05.9	06.4	10.8	02.1	17.0	12 -04.2	05	-	-	01	05.0	04	03.0	34	02.1	-	03	01.7	08	01.1	07	01.6	17		
III	-	05.9	13.0	08.6	09.0	13.9	04.2	26.0	21 -02.9	12	01	01.0	-	-	18	04.1	36	03.3	04	02.6	06	01.3	02	01.0	01	01.0	25	
IV	-	07.9	14.8	10.2	10.8	16.3	05.2	22.3	30 -01.2	22,20	05	01.6	-	-	11	02.9	16	03.2	06	01.8	04	01.0	06	01.8	13	01.5	29	
V	-	12.4	18.8	13.4	14.5	19.6	09.1	27.5	31 04.0	11	0.4	01.2	-	-	02	01.5	-	02	02.5	08	01.6	18	01.7	20	02.4	39		
VI	-	16.5	22.1	17.0	18.2	23.8	12.8	29.2	27 08.0	09	-	-	01	01.0	03	02.0	34	02.7	03	01.3	06	02.0	24	01.4	36			
VII	-	17.7	25.5	18.8	20.2	26.9	13.2	35.4	14 08.0	23	-	-	01	01.0	01	02.6	34	02.8	01	03.0	06	01.7	11	01.8	35			
VIII	-	20.0	28.5	20.8	22.5	29.6	15.7	35.7	04 11.2	07	0.2	01.5	03	01.0	03	02.0	35	02.2	05	01.6	05	01.4	10	01.4	19	02.1	36	
IX	-	15.8	23.9	16.6	16.4	25.4	12.3	32.6	04 02.1	28	0.1	01.0	-	-	04	01.8	18	02.7	06	01.8	09	02.7	09	02.6	36			
X	-	07.6	13.1	08.7	09.4	14.0	05.2	20.5	05 -00.6	31,28	-	-	01	03.0	02	01.5	34	02.9	08	01.9	03	02.0	15	01.4	09	01.3	41	
XI	-	04.1	11.0	06.5	07.1	11.7	02.9	18.8	18 -01.1	14	0.1	01.0	-	-	01	01.0	15	02.7	07	01.9	02	01.0	06	01.5	12	02.2	44	
XII	-	01.0	04.3	02.5	02.6	05.7	-00.4	12 -04.6	23	0.1	02.0	-	-	02	02.0	07	01.0	06	01.5	22	01.6	06	01.5	22	01.6	53		
GOD.	-	09.4	15.7	10																								

Mesec	Oblastnost Nm (0-10)	Insolacije broj sati (Gles)	Vlažnost vazduha e _m mm	Padavine R mm			Broj dana na sa:																												
				Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	R	T	≡	■												
	7	14	21	Sred.	7	14	21	Sred.	Max	Dat.	≤	<	<	≤	IV	IV	IV	IV	≥	<	>	≤	≥	•	Δ	Δ	▲	▲	R	T	≡	■			
BR. ST.181																																			
FLAMUNDA																																			
I	-	-	-	062.3	-	-	-	-	-	024	007.4	20	-	-	-	-	-	-	-	07	07	-	05	02	-	-	-	-	02	01					
II	5.7	5.8	4.5	5.3	119.0	04.8	80	59	79	73	36	024	009.8	21	01	-	11	-	-	06	07	07	04	-	07	-	-	-	-	-					
III	4.5	3.7	3.1	3.6	182.0	04.6	75	46	69	64	17	024	009.5	06	-	-	12	04	-	13	08	16	09	05	04	-	03	02	-	-					
IV	7.0	6.3	5.0	6.1	164.1	05.3	75	45	75	65	23	048	010.6	18	-	-	12	-	-	04	01	04	07	10	09	01	10	-	-	02	-				
V	6.4	6.1	6.5	6.6	178.1	08.9	86	57	84	76	03	072	013.2	01	-	-	03	02	-	01	01	03	09	16	13	03	18	-	-	04	01				
VI	6.1	6.7	4.2	5.6	166.7	11.4	86	60	88	78	38	081	025.6	30	-	-	11	-	-	01	05	07	15	12	02	15	-	-	06	-					
VII	3.9	4.2	3.1	3.7	-	12.3	84	54	86	75	32	134	106.5	24	-	-	15	07	-	11	04	11	06	02	11	-	-	-	-	VIII	3.3	2.7	1.5	2.5	
VIII	3.3	2.7	1.5	2.5	253.6	12.7	83	47	90	73	27	084	036.2	13	-	-	24	12	01	02	-	20	03	08	05	03	06	-	-	01	-				
IX	4.3	4.7	2.8	3.9	201.9	10.3	83	54	84	74	32	076	035.7	27	-	-	01	15	01	-	02	09	04	06	05	03	06	-	-	02	06				
X	7.3	7.8	6.1	7.1	102.6	-	-	-	-	-	175	030.2	16	-	-	10	-	-	01	03	16	20	17	08	20	02	-	-	03	02					
XI	6.4	5.5	5.2	5.7	110.7	05.3	89	64	85	79	39	076	021.2	29	-	-	14	-	-	04	07	11	09	09	04	08	01	-	-	04	02				
XII	8.2	7.4	7.1	7.5	043.7	04.8	92	83	90	88	52	087	018.5	15	02	-	16	-	-	03	19	16	13	04	13	05	-	-	-	-	14				
GOD.	-	-	-	-	-	-	-	-	-	-	905	106.5	94.7	-	-	-	-	-	-	30	10	-	-	130	104	30	122	12	-	-	-	-	19		
BR. ST.182																																			
SUSARA																																			
I	7.2	7.2	6.4	7.1	-	-	-	-	-	-	020	004.5	18	01	01	23	-	-	03	01	14	07	06	-	07	04	04	-	-	08	01				
II	6.0	5.8	5.1	5.6	-	-	-	-	-	-	026	011.5	21	-	-	09	-	-	03	03	07	07	04	01	07	-	-	-	-	01					
III	4.9	5.6	4.1	5.0	-	-	-	-	-	-	014	006.0	07	-	-	11	04	-	06	05	07	10	07	04	-	06	04	03	-	-	01				
IV	6.7	6.4	5.1	6.1	-	05.9	7.6	53	74	67	26	049	008.7	18	-	-	06	-	-	02	02	01	07	12	08	-	12	-	-	01	01				
V	6.5	5.9	6.1	6.2	-	09.1	88	57	84	76	30	084	C14.0	23	-	-	04	-	-	01	02	09	18	14	03	18	-	-	02	03					
VI	5.8	6.1	4.9	5.6	-	11.7	89	60	88	79	39	075	027.5	30	-	-	14	-	-	01	05	09	15	12	02	15	-	-	06	02					
VII	4.6	3.8	3.2	3.9	-	12.4	84	53	82	73	27	072	C38.2	24	-	-	17	11	01	-	11	05	10	07	02	10	-	-	04	01					
VIII	3.7	3.4	2.3	3.1	-	12.6	77	44	79	67	26	070	039.6	13	-	-	27	13	01	-	14	C2	06	05	02	06	-	-	04	01					
IX	4.6	4.9	3.1	4.2	-	10.5	80	51	82	71	31	086	C49.2	27	-	-	15	03	-	-	05	04	06	04	02	06	-	-	02	05					
X	6.3	7.6	6.4	6.7	-	-	-	-	-	-	187	027.5	30	-	-	04	-	-	02	13	20	18	16	07	22	02	-	-	02	04	02				
XI	6.4	5.7	5.1	5.7	-	-	-	-	-	-	061	C14.4	29	-	-	04	-	-	06	07	09	09	01	05	01	-	-	02	02						
XII	9.0	8.1	8.2	8.4	-	04.9	95	85	90	90	67	080	015.0	15	02	-	17	-	-	-	18	17	13	04	16	06	02	-	-	10	11				
GOD.	6.0	5.9	5.0	5.6	-	-	-	-	-	-	819	046.2	2711	-	01	01	74	81	27	02	15	08	57	105	134	105	25	132	17	09	-	01	21	37	17
BR. ST.183																																			
BELA CRKVA																																			
I	7.5	7.0	6.5	7.0	-	04.5	92	76	92	87	51	020	003.8	19	-	-	20	-	-	01	-	04	16	12	08	-	11	05	04	-	01	-	06		
II	6.1	5.2	4.3	5.2	-	05.7	86	68	83	79	41	035	C17.0	08	-	-	04	-	-	05	04	08	04	01	08	-	-	-	-	02					
III	4.9	4.8	4.1	4.6	-	-	-	-	-	-	002	001.3	06	-	-	05	03	-	05	01	09	07	05	01	-	04	02	01	-	-	01				
IV	6.4	6.5	6.1	6.3	-	06.3	73	54	67	65	33	038	009.6	27	-	-	02	-	-	03	02	02	08	14	09	-	-	-	-	01					
V	6.5	6.3	6.4	6.4	-	-	-	-	-	-	126	020.6	16	-	-	04	-	-	01	-	01	08	18	14	05	18	-	-	07	01					
VI	5.9	5.8	5.8	5.8	-	-	-	-	-	-	121	025.7	17	-	-	15	-	-	03	-	03	05	12	03	16	-	-	02	08						
VII	4.2	4.7	3.8	4.3	-	-	-	-	-	-	100	037.2	23	-	-	18	11	01	-	-	10	07	13	07	04	13	-	-	05	-					
VIII	3.6	3.5	2.7	3.3	-	-	-	-	-	-	048	015.5	12	-	-	26	16	03	-	-	11	C1	07	06	02	07	-	-	04	-					
IX	4.3	4.3	3.7	4.1	-	-	-	-	-	-	072	048.2	27	-	-	17	03	-	02	-	04	05	02	06	-	-	04	01							
X	6.5	7.5																																	

Mesec	Vazdušni pritisak Pn mbar	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Pm (0-12)																	
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW				
		7	14	21							č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.			
$\varphi = 44^{\circ}12'N \lambda = 21^{\circ}47'E$ Gr. $\Delta G = +1h\ 27\ min.$											ZAGURICA												BR. ST.186						
I	-	-02.0	01.6	-00.8	-00.5	02.4	-02.7	09.0	27 -12.0	15	31	02.4	11	02.7	10	01.9	.	.	41		
II	-	00.9	06.9	02.9	03.4	08.1	00.0	17.4	12 -06.4	01	.	.	09	02.6	21	03.0	08	02.8	02	02.5	.	.	04	01.2	.	.	41		
III	-	02.3	05.5	05.6	05.8	10.4	01.4	25.0	19 -03.0	01	.	.	22	02.5	26	02.3	34	02.0	.	.	01	02.0	03	01.3	.	.	27		
IV	-	05.1	12.9	08.3	08.6	14.0	03.4	21.4	13 -01.0	04	.	.	01	04.0	22	01.7	09	01.9	.	.	04	01.0	07	01.6	01	01.0	44		
V	-	09.8	17.2	12.9	13.2	18.5	08.5	24.6	31 02.4	11	02	02.0	02	02.5	21	01.5	06	01.0	62		
VI	-	13.7	20.1	16.9	16.9	22.1	12.3	27.2	27 06.0	09	01	02.0	09	01.8	01	02.0	01	04.0	27	01.8	05	01.2	46		
VII	-	14.3	23.1	17.9	18.2	24.5	12.0	34.0	18 06.0	27	02	02.0	01	01.0	03	01.3	28	01.5	05	01.4	52				
VIII	-	16.3	26.3	18.9	20.1	27.2	13.8	34.4	03 04.6	08	.	.	03	01.3	22	01.7	04	01.5	02	01.0	.	.	12	01.8	.	.	50		
IX	-	12.2	22.3	15.6	16.4	23.1	10.7	30.0	04 02.2	28	.	.	01	01.0	24	02.5	04	01.0	14	02.3	01	01.0	46		
X	-	05.9	13.2	08.4	09.0	14.9	04.8	23.0	08 -03.0	28	10	01.9	11	01.9	.	.	02	02.5	13	01.2	.	.	57		
XI	-	01.5	07.7	04.0	04.8	10.5	00.8	18.0	18.17 -03.0	30.21	18	02.4	07	01.1	.	.	01	01.0	08	02.4	02	02.0	54		
XII	-	-01.4	03.3	00.6	00.7	04.3	-02.5	09.0	29 -13.8	25	01	02.0	17	01.2	01	01.0	74			
God.	-	06.5	13.8	09.3	09.7	15.0	05.2	34.4	02.0 -13.8	45	15	02.3	179	02.3	101	02.0	06	01.7	13	01.7	14	01.6	21	01.2	596
$\varphi = 44^{\circ}22'N \lambda = 21^{\circ}57'E$ Gr. $\Delta G = +1h\ 26\ min.$																								DEBELI LUG					
BR. ST.187																									BR. ST.187				
I	-	-02.2	00.3	-01.5	-01.2	01.2	-03.7	06.0	22 -14.2	15	.	.	10	04.5	26	03.2	05	02.4	04	02.9	18	02.5	25		
II	-	00.8	05.7	01.5	02.4	06.8	-00.8	16.2	11 -04.0	11.0	.	.	08	04.8	23	02.6	17	02.6	.	.	.	02	02.5	04	02.6	30			
III	-	01.1	08.7	03.7	04.3	09.7	00.0	24.8	19 -05.0	02	01	01.0	06	04.7	47	03.4	11	02.8	01	01.0	02	03.0	25		
IV	-	04.0	11.7	06.5	07.2	13.1	01.8	26.5	13 -02.5	04.0	03	.	04	02.8	29	02.4	09	02.9	03	02.0	15	02.1	30		
V	-	10.0	17.2	11.2	12.4	18.5	08.3	24.7	31 03.0	12	.	.	07	01.1	01	06.0	02	01.5	.	.	.	06	01.3	22	02.5	55			
VI	-	13.4	20.7	14.3	15.8	22.0	11.0	27.0	29 05.1	09	.	.	03	02.3	04	01.8	01	01.0	30	02.1	52				
VII	-	15.1	24.8	16.3	16.2	25.8	11.8	.	-	-	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	15.3	26.3	17.6	19.2	27.1	13.1	34.2	03 10.1	29	01	03.0	.	09	01.6	09	02.2	11	02.4	63			
IX	-	11.3	21.9	13.3	14.9	22.6	10.0	29.5	03 06.0	20	.	.	02	02.0	10	02.2	07	02.7	12	01.9	59			
X	-	05.3	12.4	06.8	07.9	13.4	03.7	26.7	08 -02.8	28	.	.	03	02.7	05	02.0	14	01.5	26	01.7	45				
XI	-	-	-	-	-	-	-	-	-	-	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-				
God.	-	-	-	-	-	-	-	-	-	-	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 44^{\circ}05'N \lambda = 22^{\circ}06'E$ Gr. $\Delta G = +1h\ 28\ min.$																								BCK					
BR. ST.188																									BR. ST.188				
I	-	-02.1	-00.2	-01.9	-01.5	01.1	-04.4	08.0	28 -12.5	15	19	03.3	07	01.4	26	01.9	04	01.5	06	01.5	.	.	02	02.5	.	.	29		
II	-	01.2	05.4	01.7	05.2	06.6	-00.9	17.4	12 -05.6	28	05	01.4	05	02.4	23	01.8	06	01.7	06	01.7	01	04.0	02	01.5	03	02.0	23		
III	-	02.8	08.3	04.1	04.8	09.1	00.3	23.2	20 -05.8	28	02	01.0	07	01.0	51	02.4	06	01.5	05	02.2	.	.	02	02.0	20	.	20		
IV	-	06.2	12.2	07.4	08.3	13.3	03.1	22.0	13 -00.4	15	20	02.4	08	01.6	20	02.4	09	01.9	04	02.2	01	01.0	02	01.5	04	01.5	22		
V	-	12.9	17.8	12.7	14.0	19.2	08.7	26.2	31 04.0	11	40	02.2	01	02.0	02	02.0	02	03.5	08	01.9	06	01.5	05	02.8	04	01.2	25		
VI	-	16.5	21.4	15.6	17.3	22.6	12.1	26.3	29 06.9	14	17	02.3	03	02.7	04	01.8	04	02.2	06	02.5	01	01.0	06	02.1	17	04.1	35		
VII	-	19.1	24.7	17.5	19.7	26.0	13.3	33.8	14 05.4	09	20	02.5	01	03.0	03	01.7	04	01.5	03	02.0	05	01.8	17	02.9	37				
VIII	-	19.6	27.0	19.6	21.4	27.8	15.1	34.2	03 11.4	11	13	02.5	06	07.0	11	01.6	16	01.6	04	02.8	01	02.0	.	.	19	02.3	23		
IX	-	14.3	21.1	15.9	17.2	23.4	11.1	30.0	03 05.9	28	13	02.8	03	01.7	14	02.1	02	04.2	02	02.5	.	.	10	03.2	31				
X	-	07.6	13.3	08.0	09.2	14.6	07.8	20.8	08 -02.6	28	11	02.9	07	01.6	25	02.4	07	02.0	07	01.9	06	02.0	03	01.2	34				
XI	-	02.4	06.7	03.5	04.0	07.5	00.5	15.5	17 -04.6	27	10	01.9	04	02.8	08	01.9	09	01.8	07	01.6	02	02.5	03	02.0	35				
XII	-	01.2	04.6	02.4	02.6	05.8	-01.3	12.0	27 -06.2	25	24	02.2	01	02.0	00	01.3	06	01.2	03	02.0	01	03.0	05						

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha			Padavine R mm			Broj dana na sat																										
										Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	▲	R	T	III	II							
	7	14	21	Sed.	(Dnev.)	Inopacijalna broj sati	em	m	mm	7	14	21	Sed.	Min	Σ	Max	Dat.	≤	<	≤	IV	≤	IV	<	>	IV	IV	IV	IV	IV	IV	IV	IV			
ZAGUBICA																																				
BR. ST.186																																				
I	8.6	7.6	6.5	7.6	0.62±1	-	-	-	-	012	004.0	18	02	07	24	-	-	-	02	18	07	05	06	03	02	-	-	-	-	-	01	-				
II	7.3	7.0	5.8	6.7	0.90±6	04.4	85	64	78	78	24	039	020.2	21	-	01	12	-	-	04	13	09	05	02	09	01	-	-	-	-	-	01	-			
III	6.4	6.1	4.8	5.8	1.50±9	04.5	78	54	67	66	12	005	002.2	07	-	01	14	01	-	-	08	12	05	02	04	03	02	-	-	-	-	-	01	-		
IV	7.0	7.0	5.7	6.7	1.31±8	05.9	86	56	72	72	29	070	024.5	15	-	01	04	-	-	04	12	12	09	02	12	-	-	-	-	-	02	01				
V	6.5	6.0	6.5	7.0	1.54±6	09.1	97	62	86	81	32	152	033.0	13	-	-	-	-	-	02	15	25	19	04	25	-	-	-	-	-	03	06				
VI	7.1	7.3	5.9	6.8	1.71±3	11.4	93	64	85	81	34	090	015.9	22	-	-	08	-	-	08	10	16	13	04	16	-	-	-	-	-	04	-				
VII	4.4	5.3	3.5	4.4	2.56±1	12.4	94	60	85	80	33	067	016.2	23	-	-	14	09	-	09	06	10	07	03	10	-	-	-	-	-	03	-				
VIII	4.5	4.5	2.0	3.7	2.72±2	12.8	89	51	83	74	26	081	047.8	10	-	-	24	09	02	10	04	05	04	02	05	-	-	-	-	-	02	04				
IX	5.7	5.8	3.1	4.9	1.73±2	10.3	89	53	81	74	28	039	021.4	27	-	-	11	01	-	01	05	06	06	04	02	06	-	-	-	-	-	05	-			
X	7.8	7.3	5.0	6.7	1.06±3	07.1	94	66	88	83	34	134	032.6	15	-	-	05	-	-	12	18	16	04	18	-	-	-	-	-	01	01					
XI	7.1	6.3	4.8	6.1	0.87±1	05.4	94	66	91	83	34	056	013.0	09	-	-	15	-	-	05	11	10	09	02	09	01	-	-	-	-	-	07	01			
XII	9.0	7.0	7.0	7.7	0.24±9	04.5	93	82	94	91	01	108	024.6	09	02	01	21	-	-	02	17	15	11	05	12	06	02	-	-	-	-	-	07	18		
GOD.	6.8	6.6	5.0	6.2	1.68±1	-	-	-	-	853	047.8	40	NP	04	10	95	58	19	02	01	-	51	136	138	104	30	132	14	06	-	-	01	-	44	20	
DEBELI LUG																																				
BR. ST.187																																				
I	9.1	8.6	6.4	8.7	-	03.8	87	86	86	86	65	-	-	02	09	28	-	-	-	02	25	-	-	-	-	-	-	-	-	-	-	-				
II	8.0	6.9	6.8	7.2	-	05.1	88	75	88	87	-	038	017.5	21	-	01	14	-	-	03	16	08	06	01	06	02	-	-	-	-	-	01	-			
III	6.2	5.9	4.9	5.7	-	04.7	83	66	81	77	22	-	-	02	15	-	-	09	01	08	11	-	-	-	-	-	-	-	-	-	-	02	09			
IV	7.0	6.7	6.5	6.7	-	05.4	82	57	73	71	29	086	034.7	15	-	01	09	-	-	03	13	11	11	02	11	06	06	-	-	-	-	-	01	-		
V	7.3	7.1	6.1	6.8	-	08.9	92	63	90	82	31	123	022.0	03	-	-	-	-	01	01	-	12	19	18	04	19	-	-	-	-	-	01	08			
VI	7.0	6.0	6.5	6.5	-	11.0	88	63	89	80	43	118	038.0	30	-	-	10	-	-	01	11	18	16	03	18	-	-	-	-	-	01	03				
VII	9.1	3.4	2.1	2.9	-	11.9	87	52	87	75	-	-	-	-	-	-	-	-	01	-	-	-	-	-	-	-	-	-	-	01	-					
VIII	3.3	3.3	2.5	3.0	-	12.6	90	52	86	76	30	062	023.1	13	-	-	24	09	-	02	16	04	04	03	04	-	-	-	-	-	01	08				
IX	6.7	4.5	3.9	5.0	-	10.0	92	52	91	78	33	084	050.0	27	-	-	06	-	-	04	04	06	05	02	06	-	-	-	-	-	02	10				
X	8.4	6.6	7.1	7.4	-	06.7	93	63	90	82	33	142	022.6	14	-	-	01	-	-	01	14	18	16	07	18	-	-	-	-	-	01	12				
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
SCR																																				
BR. ST.188																																				
I	8.3	8.0	7.2	7.8	-	03.7	89	84	87	87	66	034	013.4	03	03	15	27	-	-	01	-	02	17	15	08	01	14	01	01	-	12	19				
II	7.1	7.4	7.0	7.2	-	04.6	86	73	87	62	17	023	011.8	21	-	02	18	-	-	02	15	16	03	01	11	06	01	-	-	11	-					
III	5.8	5.6	6.1	5.9	-	04.6	79	62	75	72	23	068	023.0	07	-	04	16	-	-	11	15	11	08	02	11	-	-	-	-	-	02	11				
IV	6.1	6.9	5.5	6.2	-	05.2	72	51	69	64	24	096	021.4	17	-	-	05	-	-	05	12	19	09	05	12	04	04	-	-	-	01	-				
V	5.4	6.2	6.0	5.9	-	08.1	71	53	77	67	30	107	023.4	09	-	-	01	-	-	05	05	15	14	04	15	-	-	-	-	-	02	-				
VI	5.5	6.0	3.3	4.9	-	10.5	75	56	79	70	30	030	015.0	30	-	-	09	-	-	02	07	06	15	12	02	15	-	-	-	-	-	02	-			
VII	3.0	2.9	2.1	3.0	-	10.8	64	47	74	62	17	019	011.0	07	-	-	17	11	-	01	17	03	04	01	04	04	-	-	-	-	-	01	-			
VIII	2.7	2.7	1.4	2.3	-	11.2	63	43	66	58	25	071	032.8	24	-	-	25	12	-	01	20	03	06	06	02	06	-	-	-	-	-	03	-			
IX	3.5	4.4	3.0	3.6	-	09.6	69	52	71	64	30	021	017.1	27	-	-	13	01	-	10	02	05	02	01	05	-	-	-	-	-	01	-				
X	5.5	5.6	6.8	4.5	-	06.7	79	61	81	73	23	122	018.9	30	-	-	03	-	-	01	07	11	15	12	06	15	01	-	-	-	-	-	03	-		
XI	8.7	7.6	6.7	7.7	-	04.9	86	71	85	81	27	095	020.2	09	-	-	15	-	-	01	18	18	10	04	14	06	01	-	-	12	09					
XII	6.7	6.8	7.5	7.0	-	04.2	80	69	78	76	26	056	016.8	16	-	01	21	-	-	01	03	15	10	07	03	08	05	-	-	-	-	-	06	12		
GOD.	5.7	6.0	5.1	5.6	-	07.0	76	60	77	71	17	785	032.8	04	NP	03	22	105	65	24	-	04	02	90	122	142	95	32	108	47	05	02	-	01	11	46
TERIJA																																				
BR. ST.189																																				
I	8.9	7.6	8.3	8.3	-	04.1	86	80	87	84	55	014	004.8	03	-	0																				

Mesec	Vazdušni Pritisak Pa	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра m/s (0-12)																
		Tm				Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW	
		7	14	21	Sred.	č.	j.	č.	j.	č.	j.	č.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		
$\varphi = 43^{\circ}55'N \lambda = 19^{\circ}26'E$ Gr. $\Delta G = +1h\ 18\ min.$																												
I	-	-03.9	00.5	-03.0	-02.4	01.0	-05.0	05.0	00.0	04.03	-14.0	14	51	01.1	+	+	+	+	+	06	C1.2	+	+	+	+	+	36	
II	-	-02.4	03.6	-01.7	-00.6	04.1	-03.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	06.4	10.9	06.9	07.8	12.0	03.5	19.0	31	-01.5	10.05	35	C1.1	+	+	+	+	+	56	01.2	+	+	+	+	+	02		
VI	-	10.1	14.5	10.5	11.4	15.9	06.9	23.4	27	03.0	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	11.6	17.2	11.1	12.8	18.6	07.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	09.1	16.4	10.6	11.7	17.8	07.0	26.0	04	-01.6	28	32	C1.2	+	+	+	+	+	29	01.2	+	+	+	+	+	29		
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}44'N \lambda = 19^{\circ}43'E$ Gr. $\Delta G = +1h\ 17\ min.$																												
MITROVAC-TARA													BR. ST.191															
I	-06.7	02.8	-00.3	-01.9	-01.7	00.9	-04.2	07.8	01	-09.2	14	19	C1.9	C8	01.5	C2	C1.5	C7	01.7	04	C2.2	42	C2.6	C3	C4.0	C4	C1.5	08
II	670.9	-00.1	04.2	01.5	01.8	05.4	-01.2	12.4	12	-07.8	29	06	C1.3	18	02.1	C3	C1.3	C8	02.1	15	C0.1	30	C3.7	01	C1.0	02	C1.5	01
III	673.5	01.5	07.0	03.5	03.9	07.8	-00.3	19.3	23	-07.9	01	11	C1.5	26	01.8	C4	C1.2	C10	10	02.6	19	C2.6	01	C2.0	01	C2.0	01	
IV	670.6	03.0	07.6	04.0	04.7	08.8	01.2	17.2	29	-3.7	21	19	C1.6	24	01.9	C3	C2.0	C4	02.0	12	C2.8	22	C2.7	03	C1.7	02	C1.5	02
V	671.9	08.2	12.1	09.1	09.6	13.8	05.5	23.0	31	02.0	10	22	C1.8	08	01.9	07	01.9	03	01.7	09	C3.3	34	C2.8	04	C7.5	05	C1.2	01
VI	674.2	12.3	16.0	12.7	13.4	18.0	09.5	25.5	27	03.1	13	23	C0.0	09	01.9	C4	C1.8	C3	01.7	07	C3.4	33	C2.8	05	C2.2	04	C1.8	07
VII	676.0	14.5	18.7	15.1	18.8	20.2	11.3	30.4	17	05.1	09	18	C1.7	15	01.9	C6	C1.7	C6	02.0	05	C2.4	34	C2.5	03	C1.7	07	C2.0	07
VIII	676.4	15.6	21.4	17.2	17.8	22.4	13.3	27.7	03	06.7	12	12	C2.1	26	02.1	14	C2.2	07	01.9	06	C2.0	15	C2.1	02	C1.5	05	C1.6	06
IX	675.1	11.8	17.3	13.2	13.9	18.6	10.0	28.2	04	01.8	28	12	C1.8	19	01.7	C4	C1.8	C2	01.5	13	C2.9	30	C2.7	07	C1.7	07	C1.5	03
X	670.7	04.3	05.0	05.6	10.0	12.2	15.6	08	-04.8	31	09	01.6	17	C1.8	C4	C1.2	C3	01.7	07	03.5	38	C3.2	05	C2.4	02	C1.5	02	
XI	674.5	01.0	05.6	02.2	02.7	07.2	-00.2	14.1	16	-08.2	30	12	C1.4	09	01.4	C1	C3.0	C2	02.0	09	C2.9	50	C2.8	05	C2.6	07	C2.0	02
XII	675.1	-02.5	-00.1	-01.2	-01.3	01.6	-04.4	07.4	12.11	-13.8	24	25	C0.2	01	02.0	02	01.5	03	06	03.2	50	03.1	04	02.5	02	C2.0	01	
GOD.	673.7	05.6	09.8	06.7	07.2	11.2	03.6	30.4	77M	-13.8	94M	187	C1.8	190	01.9	54	C1.8	51	01.9	111	C2.9	397	C2.8	43	C2.1	31	C1.6	31
$\varphi = 43^{\circ}52'N \lambda = 19^{\circ}51'E$ Gr. $\Delta G = +1h\ 21\ min.$																												
TITCWC UZICE												BR. ST.193																
I	-	-00.7	03.3	01.2	04.0	-01.2	09.8	22	-07.2	15	+	+	*	*	*	*	*	*	02	01.0	03	01.0	02	C1.0	C6	C1.2	78	
II	0.9	09.9	03.9	04.6	10.8	00.4	17.8	12	-05.0	09	+	+	02	02.0	C2	C1.5	C5	01.6	01.0	09	C1.7	01	C1.0	*	*	44		
III	-	02.3	12.4	06.4	06.9	13.0	01.8	25.5	21.19	-05.4	02	+	+	*	*	C2	C1.0	08	01.5	*	05	C1.2	*	04	C1.0	04		
IV	-	05.8	13.3	07.7	08.6	14.7	03.7	23.0	29	00.2	05	+	+	02	02.0	C1	C1.0	03	01.7	02	01.0	04	01.3	04	C1.0	40		
V	-	10.7	18.0	12.2	13.3	19.2	07.9	28.7	31	04.0	11	+	+	03	01.3	*	*	03	01.7	C1	0.0	08	C1.1	12	C1.1	03	C1.3	43
VI	-	14.0	21.6	16.0	17.1	23.0	12.1	29.3	27	07.0	14.13	+	+	*	*	04	01.5	*	07	01.6	15	C1.2	01	C1.0	61			
VII	-	15.9	24.4	17.7	18.9	25.6	12.8	35.2	17	07.5	09	+	+	03	01.0	C1	C1.0	03	01.0	*	03	C1.3	18	C1.1	01	C1.0	64	
VIII	-	16.3	27.4	18.9	20.4	26.3	14.3	34.0	03	10.3	08	+	+	07	01.0	01	02.0	07	01.1	05	04	07	01.4	07	C1.5	60		
IX	-	12.3	22.6	15.1	16.3	24.0	11.2	33.0	04	02.0	28	+	+	02	01.0	01	01.0	02	01.0	*	07	01.1	C8	C1.1	*	70		
X	-	04.7	12.2	07.0	07.8	13.0	03.8	20.0	04	-02.6	31	+	+	03	01.0	*	*	02	01.0	*	11	01.1	01	01.0	04	C1.2	72	
XI	-	01.7	08.6	03.5	04.4	09.4	00.8	15.6	19	-01.8	29	+	+	01	01.0	01	01.0	05	01.2	*	04	01.5	79					
XII	-	-00.1	04.4	01.7	01.9	05.4	-01.1	12.0	29	-08.7	24	+	+	01	02.0	*	*	01	01.0	*	03	01.3	16	01.0	07	01.3	66	
GOD.	-	07.0	14.8	09.3	10.1	15.9	05.5	35.2	77M	-08.7	94M	+	+	23														

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																
		Tm			Sred. (Dices)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.			
$\psi = 43^{\circ}35'N \lambda = 20^{\circ}14'E$ Gr. $\Delta G = + 1h 21 min.$																												
I	-	-01.2	03.3	00.3	00.7	04.2	-02.0	16.0	27	-08.5	15	14	C1.2	C3	01.3	C5	C2.0	12	01.2	C4	01.6	01	04.0	03	03.0	11	01.6	39
II	-	01.1	09.8	03.4	04.4	11.5	00.2	18.0	12	-06.8	09	10	C1.5	C3	01.0	C9	01.9	13	02.2	C13	02.3	•	•	03	01.0	10	02.6	23
III	-	01.6	12.4	05.1	06.0	13.6	00.6	25.7	20	-07.2	02	13	C1.7	C3	01.7	15	01.7	06	02.4	C8	04.9	•	•	02	01.5	12	02.5	29
IV	-	04.5	12.9	06.5	07.6	14.6	02.6	24.5	04	10	01.4	06	C1.5	15	01.9	17	02.0	04	04.5	•	•	03	02.7	14	02.1	21		
V	-	10.3	17.5	11.2	12.6	19.5	07.1	28.6	31	03.0	11	12	C1.7	C5	07.0	C8	C1.8	22	02.0	C7	C2.4	01	02.0	02	01.5	06	02.8	29
VI	-	15.1	21.2	14.7	16.4	23.3	11.4	30.2	29	06.0	14.09	12	C1.8	C7	03.0	C13	C1.5	19	01.8	C3	02.7	01	02.0	01	04.0	08	03.6	26
VII	-	15.8	24.3	15.9	17.9	25.7	11.5	36.2	17	06.1	09	07	C1.7	C2	04.0	C19	C1.5	24	02.0	C8	04.5	02	01.5	01	01.0	09	02.0	21
VIII	-	15.2	27.1	16.5	18.9	26.5	12.7	33.6	04	08	04.6	14	04	C2.0	06	C1.8	17	C1.5	19	C9	C2.4	•	•	03	02.3	07	02.7	26
IX	-	12.1	22.7	14.1	15.7	24.2	10.6	30.6	03	01.5	28	04	C1.1	C1	02.0	C4	01.8	22	02.0	C6	C1.7	01	03.0	06	02.7	05	02.2	37
X	-	05.4	12.9	06.5	07.8	14.6	03.6	21.5	08	-01.3	31	14	C1.9	C1	01.0	C17	C1.7	08	02.1	C4	C2.0	01	04.0	09	02.1	06	02.3	33
XI	-	01.6	09.8	03.3	04.5	11.4	00.2	18.5	19	-04.0	26	14	C1.1	C3	01.5	C16	C1.3	20	01.8	C4	C2.4	•	•	04	02.5	13	01.3	15
XII	-	-01.1	04.1	00.5	01.0	05.7	-02.4	12.6	05	-12.8	24	11	C1.6	C4	01.3	C10	C1.5	22	01.9	C7	C1.6	01	01.0	•	•	04	02.8	26
GOD.	-	06.7	14.8	08.2	09.5	16.4	04.7	36.2	MVII	-12.8	24	141	C1.6	47	01.6	C52	01.6	C20	01.9	77	C2.6	08	02.4	37	02.2	105	02.3	325
$\psi = 43^{\circ}25'N \lambda = 20^{\circ}17'E$ Gr. $\Delta G = + 1h 21 min.$																												
BELE VODE-GELIJA																												
BR. ST. 197																												
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	10.2	13.9	09.3	10.7	15.3	07.2	22.0	27.06	01.0	13.11	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	12.4	16.5	11.5	13.0	16.0	08.7	27.1	17	02.2	08.07	24	C1.1	C2	01.0	•	•	C1	01.0	•	•	12	01.8	07	01.1	33	02.1	14
VIII	-	13.4	19.1	12.7	14.5	20.1	10.2	26.0	04.03	04.0	12	31	C1.3	15	01.8	14	01.8	•	•	•	•	03	02.7	06	01.9	21	01.7	03
IX	-	09.4	15.6	09.8	11.1	16.3	07.4	24.0	04	00.0	27	18	C1.6	04	02.2	C7	02.6	•	•	06	C3.7	05	03.0	14	02.1	30	02.3	06
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	07.8	15.5	09.2	10.4	16.3	05.4	34.5	MVII	-09.0	24	15	C2.1	14	01.6	31	C2.2	37	C2.3	37	01.9	70	C2.3	128	02.1	13	02.3	750
$\psi = 43^{\circ}08'N \lambda = 20^{\circ}31'E$ Gr. $\Delta G = + 1h 21 min.$																												
NOVI PAZAR																												
BR. ST. 199																												
I	-	-01.2	03.7	00.1	00.7	04.3	-02.4	05.4	03	-05.4	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
II	-	-00.1	06.1	02.5	03.3	09.0	-01.2	15.5	17	-06.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	58			
III	-	02.7	12.4	06.9	07.2	12.9	01.7	25.5	19	-06.0	02	-	-	-	-	10	C0.5	21	C2.3	09	C0.2	02.1	C2.0	04	02.2	47		
IV	-	05.9	14.3	07.9	09.0	15.2	03.4	23.0	30	-02.0	04	-	C1.0	02.0	01	02.0	04	02.0	01	02.4	16	02.0	02	02.0	51			
V	-	12.0	18.6	12.3	18.5	19.8	08.1	29.0	31	03.5	11	13	C2.0	01	03.0	•	•	03	01.7	08	02.2	18	02.1	01	04.0	59		
VI	-	15.7	22.1	15.6	17.3	23.3	12.2	26.8	06	07.4	09	03	C2.0	•	01	02.0	01	02.0	01	02.0	09	02.2	17	02.1	01	03.0	57	
VII	-	17.1	25.4	17.2	19.2	26.3	13.0	34.5	18	08.5	27	•	04	01.2	•	01	01.0	•	06	01.8	07	02.0	01	03.1	62			
VIII	-	17.4	28.8	18.6	20.4	29.1	14.5	34.1	04	11.0	31.08	03	C2.3	•	04	02.0	01	02.0	05	02.4	13	02.1	03	02.3	63			
IX	-	13.4	24.1	15.7	17.2	24.6	11.2	31.8	04	02.0	28	01	C1.7	02	01.7	C1	02.0	C2	01.5	C3	02.0	03	02.7	03	C2.3	74		
X	-	05.5	14.3	07.1	08.1	13.8	04.0	21.5	08	-02.5	24	•	03	C1.3	C1	01.0	•	02	02.0	05	02.4	08	01.9	•	•	74		
XI	-	02.5	09.4	03.7	04.8	10.1	00.8	14.7	17	-02.0	30	•	04	01.2	•	01	01.0	•	03	01.3	06	02.3	07	02.3	74			
XII	-	00.6	04.6	01.6	02.1	05.7	-01.2	11.0	29.04	-09.0																		

Mesec	Oblačnost Nm (0-10)				Temperatura broj sati	Vlažnost vazduha				Padavine mm		Broj dana na sat																	
	7	14	21	Sred. (dies)		em	Um	%	Tn	Tx	In	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	□					
						mm	7	14	21	Sred. min	Max	Dat.	30.00.0	0.025.0	0.020.0	0.6	8	2.0	8.0	0.1	1.0	10.0	•	Δ	○	▲	□		
BR. ST.196																													
IVANJICA																													
I 8.2 6.0 7.1 7.7	-	04.4 94 83 93 90 56	C64 017.3	20	*	20	*	*	*	01	02	18	14	10	02	11	06	C2	*	*	*	*	*	11	04				
II 5.6 6.2 5.9 5.9	-	04.9 88 62 82 77 42	C20 005.7	22	*	13	*	*	*	C1	01	04	11	06	*	06	03	02	*	*	*	*	*	01	01				
III 6.2 6.3 5.6 6.0	-	-	-	-	022 004.0	28	*	14	04	*	*	C1	01	04	10	10	C7	*	04	06	*	*	*	C1	03				
IV 5.9 7.1 5.6 6.2	-	-	-	-	064 011.6	15	*	05	*	*	*	01	04	09	17	14	01	17	03	02	*	*	*	*	C2	02			
V 6.9 7.0 6.1 6.7	-	05.1 88 67 91 82 33	122 030.6	19	*	01	*	*	*	*	02	09	21	15	04	21	*	*	*	*	*	*	*	02	*				
VI 6.9 7.0 6.4 6.8	-	10.6 80 58 86 75 34	100 021.3	02	*	12	01	*	*	01	02	11	14	11	05	14	*	*	*	*	*	*	*	04	*				
VII 5.5 4.7 3.8 4.0	-	11.6 83 53 89 75 25	074 013.1	01	*	18	11	*	*	*	15	C8	10	07	02	10	*	*	*	*	*	*	*	02	*				
VIII 3.6 4.4 2.6 3.6	-	12.3 88 48 89 75 29	065 019.3	10	*	25	14	*	*	C1	01	12	05	06	04	05	*	*	*	*	*	*	*	01	07				
IX 5.9 5.4 4.6 5.3	-	11.0 54 55 91 81 36	C85 C28.2	27	*	16	02	*	01	*	05	05	13	08	02	13	*	*	*	*	*	*	*	02	01				
X 6.1 6.2 5.4 5.9	-	06.7 90 66 91 82 32	171 029.6	16	*	05	*	*	*	*	06	10	16	14	08	15	02	*	*	*	*	*	*	01	07				
XI 5.5 5.5 5.0 5.7	-	05.5 93 70 80 85 39	C94 C22.4	29	*	11	*	*	*	*	03	06	10	09	04	10	05	02	*	*	*	*	*	*	10	03			
XII 7.5 7.7 7.0 7.4	-	04.7 93 89 94 92 65	110 024.8	15	03	21	*	*	*	*	04	17	17	11	04	10	10	03	*	*	*	*	*	*	04	11			
GOD.	6.1 6.3 5.4 5.9	-	-	-	-	991 031.3	04W	03	*	89	76	28	*	05	05	63	121	159	116	38	140	35	12	*	*	01	22	34	33
BELE VODE-GOLIJA																													
BR. ST.197																													
I -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III -	-	-	-	-	136.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
IV -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI -	-	-	-	-	138.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII 3.8 4.6 3.4 3.9	242.3	08.3 78 65 81 75 25	11.1 054.0	01	*	05	*	*	*	*	15	C8	06	06	04	06	*	*	*	*	*	*	*	*	06				
VIII 4.0 5.0 2.3 3.9	266.9	09.2 80 55 82 74 30	067 017.0	25	*	02	*	*	*	*	10	03	06	08	02	06	*	*	*	*	*	*	*	*	06				
IX 3.5 5.9 4.3 4.6	185.0	08.2 86 68 88 61 40	020 C28.0	27	*	16	02	*	*	01	08	C6	12	12	03	11	02	*	*	*	*	*	*	*	04				
X -	-	133.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XII -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
GOD.	-	-	-	-	-	737 040.9	02W	*	02	89	75	29	*	*	*	94	107	136	104	23	132	16	12	*	*	00	05		
ČAČAK																													
BR. ST.198																													
I 8.0 7.0 6.3 7.1	-	04.4 91 81 88 86 59	03.1 012.9	20	*	02	21	*	*	*	*	04	16	10	07	01	10	02	02	*	*	*	*	*	C1	*			
II 5.5 6.2 4.2 5.3	-	04.9 90 63 85 79 32	C16 007.5	15	*	14	*	*	*	*	06	C8	08	02	*	C7	01	*	*	*	*	*	*	*	01				
III 5.1 4.6 3.7 4.5	-	05.3 83 59 71 71 27	C15 004.2	07	*	13	03	*	*	*	13	C9	08	05	*	05	03	*	*	*	*	*	*	*	01				
IV 6.2 6.2 5.3 5.9	-	05.8 80 42 75 68 24	C74 017.2	14	*	03	*	*	*	*	C4	C9	14	11	03	14	*	*	*	*	*	*	*	06					
V 5.8 6.4 5.1 5.8	-	09.0 81 58 85 75 34	090 C22.5	19	*	03	*	*	*	*	04	07	16	14	02	16	*	*	*	*	*	*	*	05					
VI 5.8 6.8 4.1 5.6	-	11.3 83 58 84 75 33	127 C40.5	02	*	12	*	*	*	*	05	C9	16	11	C4	16	*	*	*	*	*	*	*	02					
VII 3.7 4.4 2.8 3.6	-	12.3 80 54 82 72 36	050 010.4	08	*	16	12	*	*	*	17	05	11	09	01	11	*	*	*	*	*	*	*	02					
VIII 3.3 3.1 2.2 2.9	-	-	-	-	030 015.5	25	*	26	15	*	*	18	03	06	04	01	06	*	*	*	*	*	*	*	06				
IX 4.6 4.5 3.5 4.2	-	11.1 89 53 84 75 31	026 017.1	27	*	16	02	*	*	*	09	C3	08	07	01	08	*	*	*	*	*	*	*	C1					
X 6.8 6.7 5.2 6.7	-	07.0 93 68 80 84 31	132 023.5	16	*	05	*	*	*	*	04	11	17	14	04	17	02	02	*	*	*	*	*	01					
XI 6.1 5.7 4.6 5.5	-	05.5 91 65 89 63 33	076 019.4	08	*	13	*	*	*	*	06	C9	08	04	06	01	01	*	*	*	*	*	*	*	01				
XII 7.2 7.5 5.4 6.7	-	04.6 65 75 87 83 51	064 017.5	16	*	20	*	*	*	*	04	14	14	11	02	13	05	04	*	*	*	*	*	*	01				
GOD.	-	-	-	-	590 030.4	25W	C2	01	109	66	27	*	*	*	*	-	-	-	122	95	16	103	25	08	*	01	-15		
KRALJEVC																													
BR. ST.200																													
I 8.2 6.0 5.8 7.3	043.5	04.2 90 77 65 24 58	044 017.4	20	*	C3	18	*	*	*	06	*	03	13	12	09	01	11	05	02	*	01	*	*	07	07			
II 5.7 6.6 5.0 5.8	115.7	04.9 87 57 75 37	024 007.4	09	*	13	*	*	*	*	06	*	04	16	10	04	*	10	02	02	*	*	*	*	01	01			
III 6.2 5.4 4.3 5.3	162.6	04.6 87 59 64 65 21	019 005.2	28	*	10	03	*	*	11	01	08	12	08	07	*	02	05	*	*	*	*	*	01	01				
IV 6.2 7.3 5.6 6.4	161.8	05.7 77																											

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Pm (0-12)																			
		Tm			Sred. (Dnes)	Max	Min	Max	Min	Dat.	Max	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C	
		7	14	21										č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.				
$\varphi = 43^{\circ}37'N \quad \lambda = 20^{\circ}54' E$ Gr. AG = + 1h 22 min.															VRNJAČKA BANJA												BR. ST. 201				
I	-	-00.9	03.0	-00.1	00.4	03.8	-02.2	05.5	22	-16.7	16	09	02.1	20	02.0	10	02.8	C3	01.0	20	01.4	02	01.5	.	.	15	02.2	14			
II	-	01.5	09.4	03.5	04.5	10.6	00.3	15.8	12	-05.5	28	11	01.6	20	02.2	11	02.5	C2	01.5	20	01.4	.	01	02.0	05	C1.4	14				
III	-	02.9	11.7	05.6	06.3	12.7	02.5	25.5	19	-03.7	01	08	02.0	19	02.2	29	02.8	C6	01.7	12	01.8	01	03.0	.	.	02	01.5	16			
IV	-	05.7	13.4	07.7	08.6	14.8	03.5	22.8	28	-01.2	04	19	01.9	10	01.6	C5	02.8	05	01.6	12	01.6	.	.	01	01.0	11	02.3	27			
V	-	11.4	18.1	12.4	13.5	19.8	08.5	27.6	31	04.5	11	31	01.8	04	01.8	.	C3	01.0	13	01.8	02	01.5	.	.	08	02.1	31				
VI	-	15.6	21.6	15.9	17.2	23.3	12.3	28.9	27	06.8	14.13	37	01.6	04	01.5	C1	02.0	01	01.0	18	01.7	01	01.0	01	02.0	11	02.8	16			
VII	-	16.8	24.4	17.5	19.1	26.1	13.1	35.2	18	07.5	09	32	01.7	C5	01.6	C3	02.7	02	02.0	20	02.0	01	03.0	01	02.0	09	02.7	20			
VIII	-	17.1	27.6	18.7	20.5	28.4	14.8	33.5	04	11.4	08	24	02.0	14	02.4	C3	02.3	.	22	01.7	05	01.6	25				
IX	-	13.1	22.9	15.2	16.6	23.9	11.7	30.3	03	02.8	28	16	02.1	10	02.0	C5	02.0	C3	02.0	08	01.6	02	02.5	.	.	12	02.2	34			
X	-	05.9	13.4	07.6	08.6	14.8	04.5	22.0	08	-03.1	28	28	01.9	05	01.2	.	.	.	13	01.7	02	02.5	.	.	04	C2.0	41				
XI	-	02.0	09.0	04.1	05.0	10.8	01.0	16.9	17	-02.1	27	12	01.8	C4	02.5	C5	02.6	02	02.0	18	01.4	01	02.0	02	01.0	09	02.1	37			
XII	-	-00.2	04.8	01.6	01.9	06.0	-01.3	11.8	29	-11.0	24	26	01.8	07	02.0	.	05	01.4	15	01.5	01	02.0	01	02.0	14	02.0	29				
500.	-	07.6	15.0	09.1	10.2	16.2	05.7	35.2	PM		-11.0	PM		253	01.8	118	02.0	72	02.6	32	01.6	191	01.6	13	02.1	07	01.6	105	C2.2	304	
$\varphi = 43^{\circ}27'N \quad \lambda = 21^{\circ}04' E$ Gr. AG = + 1h 21 min.															ALFKSANDREVAC												BR. ST. 202				
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
III	-	03.6	11.0	05.6	06.4	11.7	01.9	24.5	19	-06.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV	-	07.4	13.2	07.8	09.1	14.5	03.2	23.4	30	-02.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
V	-	13.1	17.9	13.0	14.2	19.4	08.8	27.3	31	05.0	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	17.0	21.4	15.8	17.5	23.0	12.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VII	-	18.4	24.0	17.4	19.3	25.8	13.0	35.0	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	19.3	26.9	19.1	21.1	27.7	15.0	33.3	04	10.8	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	14.9	22.5	15.2	17.0	23.8	12.0	31.1	04	04.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
X	-	07.6	13.9	07.8	09.2	15.9	05.0	22.0	08	-03.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	03.8	10.5	05.3	06.2	12.0	01.8	16.2	18	-06.6	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XII	-	01.3	05.7	02.5	03.0	06.8	-00.2	13.5	29	-05.4	25.24	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
500.	-	07.7	15.6	09.3	10.5	16.6	05.1	35.6	PM		-10.8	45.1	17	02.0	10	01.7	25	01.4	27	01.7	85	01.5	09	01.6	45	02.1	116	C2.2	761		
$\varphi = 43^{\circ}52'N \quad \lambda = 21^{\circ}06' E$ Gr. AG = + 1h 24 min.															REKEVAC												BR. ST. 203				
I	-	-00.2	03.3	00.3	00.9	03.9	-01.9	08.8	22	-16.8	15	-	-	-	-	C1	01.0	C4	01.0	23	01.3	12	03.2	53			
II	-	01.8	09.4	03.7	04.6	10.3	-00.2	16.0	16.12	-07.1	28	02	01.0	C2	02.5	C2	02.0	05	02.2	17	01.5	01	C2.0	55			
III	-	02.2	12.1	05.6	06.4	12.7	01.1	25.3	23.21	-05.5	01	-	-	C2	02.0	C4	01.2	06	01.5	12	01.5	01	02.0	6R			
IV	-	05.4	14.1	08.0	08.9	15.2	02.6	23.4	28	-02.2	04	02	0.0	.	.	05	01.6	06	02.0	05	02.2	04	C1.8	13	C2.4	55	
V	-	11.8	18.4	13.1	14.1	19.7	08.1	27.7	31	02.5	11	03	03.3	.	.	C1	01.0	01	01.0	02	02.0	01	01.0	12	02.0	61					
VI	-	15.5	22.2	16.0	17.4	23.6	12.0	29.4	29	06.8	13	02	01.5	C2	01.0	C1	03.0	.	.	04	01.5	09	02.1	63			
VII	-	17.0	24.0	17.4	19.2	26.2	12.7	35.6	18	07.5	09	01	01.0	01	01.0	.	C1	01.0	01	02	04	15	01.5	66							
VIII	-	17.5	26.3	19.0	20.9	28.7	14.0	34.0	04.03	09.0	08	02.3	01.0	01.0	07	01.1	01	01.0	02	01.5	07	C3.1	69								
IX	-	13.2	24.0	15.0	16.8	24.8	10.2	31.4	04	06.8	28	-	-	C2	02.0	C1	01.0	.	.	C6	01.5	03	01.7	01	01.0	09	C2.4	68			
X	-	05.7	13.8	07.3	08.5	15.4	03.6	22.0	08	-03.6	28	02	01.0	.	.	C2	01.5	C2	02.5	03	02.5	03	02.2	12	C1.2	67					
XI	-	02.7	11.1	04.4	05.6	11.9	00.8	16.5	17	-02.5	04	-	-	C1	01.0	C2	02.0	02.0	10	01.5	02	02.5	04	02.2	12	C4.5	69				
XII	-	00.0	05.4	01.9	02.1	05.5	-01.3	10.1	11	-06.9	24	-	-	C1	01.0	.	.	.	01	01.0	01	01.0	23	C7.1	67		
500.	-	07.8	16.0	10.8	11.3	17.0	05.8	36.1	PM		-10.8	45.1	03	01.7	02	02.0	.	.	155	02.5	.	.	01	01.0	.	.	152	C2.4	782		
$\varphi = 43^{\circ}08$																															

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																										
		Tm			Sred. (Dnev.)		Max		Min		Max		Dat.		Min		Max		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21			Max	Min	Max	Min	Dat.	Max	Min	Dat.	Max	Min	Max	Min	Max	Min	Max	Min																
$\varphi = 43^{\circ}34'N \lambda = 21^{\circ}21' E$ Gr. $\Delta G = +1h\ 25\ min.$																									KRUSEVAC		BR. ST. 206											
I	-	-00.7	03.1	00.3	00.8	03.8	-01.8	09.6	31	-09.4	15	01	C2.0	06	03.4	22	03.0	02	02.5	01	01.0	.	.	06	02.3	06	04.0	49										
II	-	01.7	09.6	04.1	04.9	10.8	00.4	17.6	12	-06.1	28	02	C3.0	04	03.0	17	02.3	06	03.3	10	03.4	.	.	03	03.0	01	02.0	38										
III	-	02.6	11.8	07.2	07.2	12.7	01.8	25.4	23	-06.0	01	C3	C2.3	C9	03.6	31	03.4	06	03.0	02	03.0	.	.	03	02.0	.	.	39										
IV	-	05.7	14.0	08.8	09.3	15.3	03.2	23.1	28	-03.0	03	05	C2.2	05	03.4	10	03.4	06	02.7	07	03.1	01	03.0	08	03.1	05	03.6	43										
V	-	11.9	18.4	13.7	14.4	19.9	09.1	28.3	31	04.1	11	13	C3.2	C2	03.0	03	C2.6	03	03.3	17	02.8	01	02.0	07	03.0	05	03.8	42										
VI	-	16.0	21.9	16.8	17.9	23.7	12.8	30.2	27	07.6	14	08	C2.9	C3	03.3	02	C2.5	07	03.0	02	02.5	08	03.6	03	04.0	57												
VII	-	16.6	24.8	18.5	19.6	26.4	13.3	35.4	17	08.6	27	05	C5.2	C1	C2.0	C3	C2.0	01	02.3	03	03.0	13	02.8	09	03.6	48												
VIII	-	16.8	26.1	19.8	21.1	26.9	13.9	34.6	04	10.2	08	04	C3.0	06	02.8	C6	C2.7	04	02.5	06	02.5	03	02.3	03	03.0	56												
IX	-	13.2	23.8	16.3	17.4	24.9	11.0	32.7	04	02.2	28	02	C2.5	02	03.0	C7	C2.7	03	02.7	11	03.0	01	03.0	04	05.5	05	04.0	55										
X	-	06.7	15.2	09.4	10.2	16.9	05.0	25.1	08	-02.7	28	11	C2.5	C6	C2.5	C1	C2.5	13	03.6	.	.	04	02.5	06	02.5	46												
XI	-	02.2	11.1	05.1	05.9	12.3	01.1	17.6	17	-01.8	15	02	C4.0	03	03.0	C9	C3.2	05	03.4	01	04.0	01	04.0	09	04.2	02	04.0	58										
XII	-	-00.6	04.3	01.4	01.6	05.3	-01.6	10.0	05	-11.6	25	03	C3.3	01	02.0	C3	C2.7	04	03.0	03	03.7	08	03.1	03	04.0	69												
GOD.	-	07.7	15.5	10.1	10.9	16.7	05.7	35.4	FVII	-11.6	25	59	C2.9	47	03.0	117	C3.1	43	02.9	88	02.9	15	02.9	76	03.2	50	03.6	600										
$\varphi = 43^{\circ}56'N \lambda = 21^{\circ}23' E$ Gr. $\Delta G = +1h\ 25\ min.$																									CUPRIJA		BR. ST. 207											
I	757.1	-00.9	02.9	00.0	00.5	03.9	-02.1	09.6	27	-11.3	15	+	.	01	C2.0	24	C3.0	20	02.8	06	02.0	01	02.0	03	02.0	04	02.5	34										
II	75C.2	02.7	09.1	03.7	04.8	10.4	01.1	16.4	12	-05.6	09	.	.	C1	C3.0	34	C3.3	13	02.6	02	03.5	01	03.0	33										
III	752.8	03.4	12.3	07.1	07.5	13.5	02.0	26.4	20	-04.4	14	.	04	01.5	41	C3.3	05	02.4	02	02.5	41											
IV	748.2	06.2	14.5	08.4	09.4	15.4	03.1	23.8	13	-04.7	04	02	C2.0	C1	02.0	18	C3.0	05	03.0	04	01.8	01	02.0	05	02.6	06	03.0	48										
V	748.2	12.2	18.8	12.9	14.2	20.3	06.6	28.2	31	02.5	11	07	C2.3	.	.	C1	C2.0	07	02.1	15	02.1	03	02.3	04	01.8	14	01.9	42										
VI	748.5	16.2	22.0	16.3	17.7	23.7	12.2	30.0	27	07.0	09	17	C2.6	03	02.0	.	C2	03.0	07	C2.1	05	02.2	01	01.0	05	02.6	50											
VII	750.8	17.4	24.8	17.9	19.5	26.2	12.5	34.3	14	06.4	09	25	C2.3	C2	02.0	C2	C1.0	01	01.9	08	02.0	01	02.0	03	02.0	39												
VIII	751.1	18.4	28.2	19.7	21.5	28.8	14.2	34.5	03	05.3	C8	13	C2.4	C1	02.0	01	C3.0	13	02.6	06	02.0	07	02.3	01	02.0	05	02.2	46										
IX	75C.8	14.3	24.1	15.5	17.4	25.1	11.3	32.6	04	01.4	28	14	C2.4	.	.	C9	C2.6	19	02.4	05	02.0	02	01.0	02	04.0	39												
X	748.1	06.4	14.0	00.5	09.4	15.4	04.5	23.2	08	-02.3	28	18	C2.3	C3	02.0	.	C6	03.3	14	02.6	05	03.0	.	.	47													
XI	753.1	03.1	10.7	05.2	06.0	11.8	01.6	16.8	18	-02.6	21	11	C2.7	.	.	C6	C2.7	22	02.6	06	02.0	.	.	03	C2.0	36												
XII	754.5	-00.3	04.3	01.4	01.7	05.1	-01.5	10.1	05	-11.6	24	20	C2.7	01	01.0	.	C11	01.9	04	02.2	.	.	01	03.0	56													
GOD.	751.1	08.3	15.5	09.7	10.8	16.7	05.6	34.5	03	VII	-11.6	04	C1.0	127	02.5	17	01.9	121	C3.1	92	02.7	121	02.3	45	02.2	17	02.0	44	02.4	511								
$\varphi = 43^{\circ}14'N \lambda = 21^{\circ}36' E$ Gr. $\Delta G = +1h\ 26\ min.$																									PRKUPLJE		BR. ST. 208											
I	-	-00.5	03.5	00.5	01.0	04.4	-01.5	08.6	31	27	-10.3	16	-	.	C9	C2.2	.	.	C2	C1.0	C7	02.4	02	03.0	73									
II	-	01.1	09.4	04.2	04.7	10.8	-00.1	17.0	17	-07.1	28	08	C2.6	05	02.2	.	C8	02.2	03	03.7	C3	03.7	02	02.0	04	03.0	51											
III	-	02.3	12.1	06.5	06.8	13.0	01.5	26.0	21	-07.6	01	02	C2.0	18	C3.1	C1	C1.0	02	01.5	01	04.0	02	02.5	09	02.0	02	C1.0	62										
IV	-	05.1	14.1	08.5	09.1	15.4	03.1	23.9	30	-02.9	03	10	C2.9	03	02.3	.	C7	02.6	02	01.5	05	03.0	06	02.0	03	02.0	54											
V	-	11.0	18.2	12.9	13.7	19.8	08.7	28.0	31	03.0	11	05	C2.4	C1.0	01	01.0	C1	02.2	02	03.0	02	03.5	04	02.5	06	03.2	66											
VI	-	15.1	22.1	16.8	17.7	23.9	12.5	29.6	29	05.0	14	01	C3.0	03	01.7	.	C4	02.5	02	01.0	08	02.0	03	02.3	05	02.8	64											
VII	-	15.8	25.1	17.4	18.9	26.5	12.8	34.9	17	09.0	10	07	C3.9	07	01.7	.	C6	01.7	01	03.0	08	02.4	03	04.0	06	03.6	66											
VIII	-	16.3	28.3	19.4	20.9	29.1	14.3	34.0	04	10.9	08	01	C3.0	05	02.0	C1	C1.0	01	02.0	05	02.8	06	03.0	06	02.0	66												
IX	-	12.3	23.7	15.6	16.8	24.7	10.7	33.0	04	01.8	28	01	C3.0	C2	02.0	C3	C2.3	07																				

Mjesec	Oblačnost Nm (0-10)				Indeks broj sati (dnev.)	Vlažnost vazduha				Padavine R mm		Broj dana na sata:																									
						Um s						Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	Δ	•	Δ	▲	▲	R _t	•	■						
	7	14	21	Sred. (dnev.)		mm	7	14	21	U S	Min	Σ	Max	Dat.	≤	<	<	≤	≤	≤	≤	>	≤	≤	W	P	Δ	•	Δ	•	Δ	▲	▲	T	•	■	
KRUŠEVAC																												$H_s = 166 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$									
I	8.1	7.8	7.2	7.7	032.2	04.1	89	74	86	83	48	028	008.8	21	.	02	18	.	.	C2	.	02	19	13	08	.	02	08	.	01	.	01	.	03	05		
II	5.8	6.3	4.7	5.6	107.0	04.9	89	58	81	76	37	048	022.5	21	.	•	13	.	.	01	.	07	09	05	04	02	05	01	01	.	01	.	01	.	01	05	
III	5.8	5.6	4.8	5.4	146.3	04.9	89	86	50	66	68	028	010.3	07	.	•	13	03	.	.	01	.	09	12	09	05	01	04	06	01	.	01	.	01	.	01	05
IV	6.0	7.1	5.0	6.0	154.0	05.8	86	47	72	68	23	061	014.7	15	.	•	06	.	.	02	01	04	08	12	07	04	12	01	.	01	.	01	.	01	02		
V	6.5	7.3	6.3	6.7	183.2	09.0	86	54	84	75	26	112	023.1	09	.	•	02	.	.	01	.	02	11	20	17	04	20	.	.	.	02	01	06	02			
VI	6.4	6.8	5.9	6.4	165.7	11.4	83	59	86	75	32	162	C52.2	20	.	•	13	01	.	01	.	01	11	18	11	05	16	.	.	01	01	06	02				
VII	5.6	4.7	3.2	5.8	189.3	12.2	82	85	84	73	27	052	013.3	11	.	•	17	12	.	14	01	11	07	11	02	11	.	.	02	.	02	.					
VIII	5.3	3.9	2.5	3.2	272.7	12.5	88	39	80	69	22	048	018.4	10	.	•	25	14	.	07	13	04	08	07	02	06	.	.	01	03	03	.					
IX	5.0	5.3	3.5	4.6	168.7	10.6	89	45	84	73	28	027	012.5	27	.	•	17	02	.	12	02	08	07	03	01	07	.	.	.	02	02	.					
X	6.5	7.3	4.7	6.2	115.7	07.1	91	55	84	77	29	094	021.6	14	.	•	06	01	.	06	02	03	10	16	12	04	16	01	.	.	06	.					
XI	6.5	5.7	4.8	5.7	059.6	05.6	94	61	88	81	31	082	018.2	08	.	•	14	02	.	05	10	08	07	04	06	01	.	.	08	.	08	.					
XII	7.5	7.5	6.7	7.2	030.7	04.6	95	78	91	88	49	086	022.5	16	02	01	18	.	.	05	03	15	16	12	03	13	07	.	.	06	18						
GOD.	5.9	6.3	4.9	5.7	1745.1	07.7	88	55	82	75	22	828	052.2	206	02	03	88	78	29	.	55	08	69	123	143	100	32	130	25	02	01	03	02	23	32	28	
CUPRIJA																											$H_s = 123 \text{ m } H_b = 124.4 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$										
BR. ST.207																																					
I	8.3	7.2	6.6	7.3	058.7	04.1	89	76	87	84	52	034	010.4	20	02	01	19	.	.	03	16	14	09	01	11	06	C1	01	01	.	04	07					
II	5.7	5.8	4.4	5.3	138.4	05.0	80	84	81	76	41	047	029.6	21	.	•	13	01	.	01	07	09	05	02	05	01	01	01	.	01	01	.	01	03			
III	5.2	5.5	5.0	5.2	176.3	04.9	78	50	66	65	22	013	004.3	07	.	•	09	04	.	01	08	11	06	04	03	05	01	.	.	03	.	.	03	.			
IV	6.8	6.8	5.5	6.4	167.0	05.8	81	48	72	67	22	046	011.0	19	.	•	08	.	.	01	10	12	07	02	12	.	.	.	01	.	01	.	01	03			
V	6.2	7.1	6.8	6.7	269.2	05.6	87	59	86	77	22	143	026.8	30	.	•	02	.	.	01	03	12	24	15	06	24	.	.	.	01	01	09	01				
VI	6.0	6.5	5.8	6.1	203.5	11.9	85	61	86	77	36	107	027.6	25	.	•	13	01	.	01	03	06	10	16	16	03	18	.	.	01	01	11	02				
VII	3.4	4.0	3.1	3.5	291.7	12.6	83	56	83	74	34	066	029.8	24	.	•	17	11	.	04	15	06	12	08	02	12	.	.	02	.	02	.					
VIII	3.4	3.1	2.4	3.0	366.0	13.1	81	47	77	69	28	048	024.5	10	.	•	28	12	.	C3	01	16	03	05	05	01	05	.	.	03	.						
IX	5.4	4.5	3.1	4.4	200.3	10.5	83	49	80	70	31	030	022.6	27	.	•	18	02	.	02	08	04	04	03	01	04	.	.	01	02	.						
X	6.8	6.9	5.5	6.4	127.1	07.3	93	64	88	82	35	121	024.2	15	.	•	05	.	.	04	11	17	14	05	17	02	02	.	.	01	06	.					
XI	6.3	5.7	5.5	5.9	114.5	05.7	90	66	85	80	40	078	016.8	29	.	•	08	.	.	C6	06	12	04	07	04	06	01	.	.	04	02						
XII	7.5	7.5	6.6	7.3	030.2	04.4	97	81	91	88	48	098	025.4	09	02	•	19	.	.	01	04	17	13	12	03	16	04	.	.	01	19						
GOD.	5.9	5.9	5.1	5.6	2050.8	07.9	85	55	81	75	22	831	079.8	2414	04	01	81	82	26	.	30	02	81	117	147	105	30	139	24	04	02	02	01	02	30	21	31
PREKUPLJE																												$H_s = 265 \text{ m } H_b = - m h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$									
BR. ST.208																																					
I	8.7	7.1	6.2	7.3	-	04.2	86	75	86	83	58	031	010.2	20	01	03	21	.	.	02	01	-	10	04	.	06	06	03	.	.	.	12	15				
II	5.5	5.5	4.5	5.2	-	04.8	85	52	78	74	34	024	010.4	21	.	•	15	.	.	C1	.	09	10	08	04	01	08	06	.	.	06	.					
III	5.5	5.0	3.7	4.7	-	05.0	85	52	70	69	23	046	C18.2	07	.	•	13	03	.	01	07	04	02	07	04	03	.	.	01	06	02						
IV	5.9	6.7	3.6	5.4	-	05.5	82	47	67	67	15	048	016.8	15	.	•	08	.	02	06	08	06	02	08	06	03	.	.	03	.							
V	5.8	6.3	3.3	5.1	-	08.8	86	58	81	75	34	084	020.0	16	.	•	01	.	.	01	07	05	16	11	03	16	.	.	06	02	.						
VI	6.2	4.0	3.6	5.3	-	11.2	85	55	79	74	38	058	022.8	23	.	•	14	01	.	01	01	05	05	14	08	02	14										

Meseč Vazdušni pritisak mm	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta m/s, Fm (0-12)																	
	Tm			Sred. (dies)	Mn	Mn	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C	č.	j.	č.	j.					
	7	14	21								č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.				
$\varphi = 43^{\circ}01'N \lambda = 21^{\circ}57' E$ Gr. $\Delta G = + 1h\ 26\ min.$											LESKOVAC												BR. ST. 211					
I	748.0	-00.4	03.6	01.2	01.4	04.4	-01.3	08.8	03	-08.8	16	04	01.5	01	02.0	.	.	02	02.0	13	01.6	14	01.3	07	01.4	06	02.2	46
II	741.4	01.3	09.8	04.5	05.0	11.0	00.2	16.1	16	-05.6	28	08	02.8	01	03.0	07	02.9	07	02.0	14	01.8	12	01.3	04	02.0	02	02.0	29
III	743.6	02.9	12.9	06.8	07.4	13.8	01.8	25.9	23	-06.2	02	07	02.1	03	01.3	07	02.1	16	02.1	03	01.3	13	01.5	03	01.7	06	02.2	35
IV	739.4	05.6	14.1	08.5	09.2	15.1	03.1	24.2	30	-02.3	03	10	02.4	08	02.6	05	02.2	12	02.1	10	01.5	07	02.6	04	02.2	08	02.8	26
V	739.7	11.6	18.3	13.3	14.1	19.8	08.7	27.4	31	02.4	11	12	02.5	04	02.5	06	01.5	09	01.6	16	01.5	09	02.2	02	02.0	01	02.0	34
VI	740.0	15.8	22.2	16.9	17.9	24.1	12.2	30.1	29	04.3	14	16	02.9	01	02.0	02	01.5	09	01.6	16	01.6	06	02.0	05	03.6	06	02.8	29
VII	742.2	16.1	25.2	17.9	19.3	26.7	12.1	35.4	17	07.6	27	15	03.1	.	.	02	01.5	11	01.6	14	01.3	07	01.4	04	01.5	06	02.2	34
VIII	742.3	16.2	28.1	19.5	20.9	29.0	13.0	34.5	04	08.3	14	15	02.3	03	02.0	02	01.3	11	01.4	11	01.5	02	01.7	03	01.7	33		
IX	742.4	12.2	24.1	15.9	17.0	25.0	10.0	32.5	04	00.3	28	13	02.7	01	02.0	02	01.5	06	01.7	10	01.5	08	02.2	04	02.5	06	03.7	40
X	739.4	06.4	16.5	09.0	10.3	17.6	04.4	25.3	08	-03.7	28	08	03.1	08	02.4	03	02.0	16	02.1	08	03.0	03	03.3	02	04.0	02	02.5	43
XII	744.5	01.8	10.7	04.7	05.5	11.7	00.7	17.0	05	-04.1	30	07	03.7	03	02.7	01	01.0	05	02.2	08	01.0	01	02.0	05	02.0	01	01.0	59
GOO.	742.4	07.4	15.7	09.9	10.7	16.9	05.2	35.4	07.VII	-11.9	24.VII	127	C2.8	37	02.3	37	02.0	112	01.9	127	01.7	96	01.7	44	02.1	50	02.5	465
$\varphi = 43^{\circ}34'N \lambda = 22^{\circ}16' E$ Gr. $\Delta G = + 1h\ 29\ min.$																								BR. ST. 212				
I	-	-02.3	01.9	-01.2	-00.7	02.4	-04.3	09.6	27	-12.6	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-00.2	07.4	01.8	02.7	08.5	-02.4	16.8	11	-10.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	00.4	10.3	04.1	04.7	11.3	-02.0	25.9	20	-11.2	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	04.6	13.7	07.2	08.2	14.7	00.3	22.2	13	-07.6	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	11.6	19.0	12.3	13.8	20.4	06.9	28.7	31	01.1	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	15.6	23.0	15.9	17.6	24.2	10.6	30.7	27	04.9	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	16.5	26.0	17.0	19.1	27.2	10.3	35.4	14	04.5	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	14.8	28.1	18.1	19.8	29.0	11.4	34.4	04.03	07.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	10.7	24.4	13.8	15.7	25.2	08.0	32.8	04	00.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	05.3	15.6	07.8	09.1	16.3	03.8	24.7	08	-04.3	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	01.5	08.2	02.7	03.8	09.2	00.1	19.6	17	-03.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	00.1	05.6	02.0	02.4	06.7	-01.4	11.5	29	-07.2	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOO.	-	06.6	15.3	08.5	09.7	16.3	03.4	35.4	44.VII	-12.6	44.I	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}53'N \lambda = 22^{\circ}18' E$ Gr. $\Delta G = + 1h\ 29\ min.$																								ZAJECAR				
I	-	-02.3	01.2	-01.1	-00.9	02.0	-04.1	10.0	28	-16.0	15	06	02.3	37	02.9	06	02.7	06	02.5	*	21	02.2	10	02.6	07	03.4	*	
II	-	00.7	06.2	02.0	02.8	07.2	-00.7	18.0	12	-04.7	28	03	02.0	38	02.8	08	03.2	06	02.7	01	03.0	21	02.7	05	01.8	02	04.0	*
III	-	01.7	09.3	04.9	05.2	10.1	00.2	25.0	19	-06.5	13	04	02.0	51	03.0	14	03.2	02	03.5	01	03.0	18	02.2	03	01.7	*	*	*
IV	-	05.4	13.3	08.4	08.9	14.6	01.9	23.0	13	-05.5	03	05	02.6	25	02.7	09	03.2	03	03.0	01	02.0	37	02.6	03	03.0	*	*	*
V	-	12.3	19.4	13.7	14.8	20.8	08.6	27.4	31	03.6	11	01	03.0	08	02.5	02	03.0	03	03.0	06	03.0	58	02.3	08	02.9	07	03.0	*
VI	-	16.1	22.7	16.8	18.1	24.2	11.9	29.0	27	06.7	09	02	02.5	10	02.2	04	02.8	02	03.0	04	02.5	48	02.5	13	03.0	07	03.3	*
VII	-	17.7	25.8	17.7	19.7	27.1	12.0	35.5	14	07.1	27	02	02.0	13	02.4	03	01.7	*	03	01.7	51	02.2	17	02.4	04	03.2	*	
VIII	-	17.1	28.2	19.8	21.2	29.1	13.0	34.0	03	06.5	28	16	02.4	07	03.0	03	02.0	02	02.0	54	02.2	08	02.9	03	03.7	*		
IX	-	12.4	24.0	16.4	17.3	25.1	09.8	31.0	04	04.0	29	02	02.0	14	02.8	13	02.9	02	03.0	*	48	02.4	11	02.6	*	*	*	
X	-	06.1	14.9	08.6	09.5	16.0	04.1	23.3	08	-03.0	28	03	03.3	16	02.6	06	03.0	03	02.0	04	02.2	49	02.6	07	02.3	05	02.4	*
XI	-	02.6	07.7	03.8	04.4	08.3	01.0	16.0	13	-05.4	27	02	02.5	33	02.6	05	02.8	01	01.0	03	02.3	36	02.2	07	03.0	03	02.0	*
XII	-	-02.1	03.9	-00.2	00.4	05.1	-03.4	12.5	04	-13.5	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOO.	-	06.4	14.9	08.4	09.5	16.0	04.4	33.4	18.VII	-13.5	25.X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 43^{\circ}09'N \lambda = 22^{\circ}36' E$ Gr. $\Delta G = + 1h\ 29\ min.$																								PIRTY				
I	-	-00.8	02.9	00.6	00.8	03.9	-02.4	08.5	27	-12.9	16	14	01.9	01	02.0	01	01.0	14	02.5	*	*	*	*	*	16	01.6	47	
II	-	01.2	08.5	03.5	04.2	10.0	-00.6	16.4	17.12	-07.4	28</td																	

Mesec	Vazdušni pritisak Pm (hPa)	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, Pm (0-12)																				
		Tm			Sred. (dnev.)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C										
		7	14	21								8.	3.	8.	3.	8.	3.	8.	3.	8.	3.									
$\varphi = 41^{\circ}20'N \lambda = 22^{\circ}41'E$ Gr. - AG = + 1h 30 min.												TOPLI DU										BR. ST. 216								
I	-	-02.5	01.4	-01.5	-01.0	02.6	-03.9	06.5	22	-12.1	16	-	-	-	-	-	-	-	-	-	-	-								
II	-	00.2	06.8	01.5	02.5	07.6	-01.3	13.8	17.12	-08.1	28	-	-	-	-	-	-	-	-	-	-	-								
III	-	01.5	09.7	03.7	04.7	10.3	00.1	23.0	20	-08.2	01	-	-	-	-	-	-	-	-	-	-	-								
IV	-	04.4	10.4	05.8	06.6	11.3	02.1	22.0	30	-03.9	03	-	-	-	-	-	-	-	-	-	-	-								
V	-	09.1	14.0	09.7	10.9	16.0	06.7	23.8	31	02.6	11	-	-	-	-	-	-	-	-	-	-	-								
VI	-	14.0	18.0	13.2	14.8	20.3	10.0	27.8	27	04.3	14	-	-	-	-	-	-	-	-	-	-	-								
VII	-	15.0	22.0	15.1	16.8	23.0	11.5	31.8	17	06.7	27	-	-	-	-	-	-	-	-	-	-	-								
VIII	-	16.2	24.1	17.2	18.7	25.2	13.1	30.9	05	09.1	28	-	-	-	-	-	-	-	-	-	-	-								
IX	-	11.6	21.0	13.8	15.1	22.3	09.6	29.6	04	04.1	28	-	-	-	-	-	-	-	-	-	-	-								
X	-	07.6	14.1	08.8	09.8	15.3	05.4	20.5	08	-03.4	28	-	-	-	-	-	-	-	-	-	-	-								
XI	-	01.9	08.6	03.6	04.4	09.6	00.5	15.6	19	-03.2	30	-	-	-	-	-	-	-	-	-	-	-								
XII	-	-01.0	07.6	-00.3	00.2	03.6	-02.6	08.9	13	-08.0	10	-	-	-	-	-	-	-	-	-	-	-								
GOD.	-	06.5	12.9	07.6	08.6	13.9	04.2	31.8	Pm	-12.1	M	-	-	-	-	-	-	-	-	-	-	-								
$\varphi = 43^{\circ}01'N \lambda = 22^{\circ}45'E$ Gr. - AG = + 1h 29 min.												DIMITREVGRAD										BR. ST. 217								
I	727.6	-01.6	02.7	-00.3	00.1	03.4	-02.6	08.1	23	-13.6	16	-	-	-	-	-	-	-	-	-	-	-								
II	722.0	00.6	08.4	02.5	03.5	09.0	-00.5	15.4	17	-07.1	28	-	-	-	-	-	-	-	-	-	-	-								
III	724.4	01.7	11.6	05.3	06.0	12.4	04.8	25.1	20	-07.9	01	-	-	01	03.0	13	02.8	61	01.1	04.0	-	04								
IV	719.0	04.6	12.7	07.0	07.8	13.8	02.2	20.5	30	-03.5	03	-	-	03	01.3	15	02.7	33	02.6	-	04	02.2	19	03.0	14					
V	720.2	10.3	17.0	11.4	12.5	18.4	06.9	25.2	31	-00.4	11	01	C1.6	-	-	13	C1.7	18	01.9	-	-	13	01.9	23	03.0	25				
VI	726.9	14.6	20.9	15.4	16.6	23.1	10.7	25.9	27	04.8	14	07	02.0	01	01.0	08	02.5	22	02.0	-	01	01.0	06	03.7	27	03.3	23			
VII	723.1	15.6	24.7	16.7	18.4	25.5	11.1	34.4	18.17	06.2	10	01	C1.0	01	02.0	05	01.6	24	02.1	-	04	01.8	04	02.8	36	03.4	16			
VIII	723.7	15.8	27.0	17.8	19.6	28.0	12.1	34.2	05	09.3	29	-	-	03	07.3	15	02.3	38	02.3	02	01.5	01	02.0	03	02.7	17	02.6	14		
IX	723.4	11.6	23.7	15.0	16.3	24.8	08.9	31.7	04	01.4	28	01	02.0	02	01.0	09	02.1	40	02.5	01	02.0	02	02.5	06	01.8	18	03.7	11		
X	726.2	07.8	16.6	05.9	10.8	17.4	05.1	24.5	14	-04.3	28	-	-	01	02.3	12	02.3	41	02.2	02	01.5	01	04.0	08	01.8	17	02.6	06		
XI	724.8	02.1	08.6	03.4	04.3	09.4	00.7	15.0	06	-03.7	30	-	-	-	10	02.7	52	07.9	-	-	07	02.0	12	02.9	09	-	-	-	-	
XII	725.1	-01.4	03.5	00.5	00.8	04.3	-02.6	08.6	13	-05.6	24	-	-	-	06	C1.5	26	02.2	-	-	02	01.5	22	01.6	23	02.9	14			
GOD.	722.9	06.8	14.8	08.7	09.7	15.8	04.4	34.4	M	-13.6	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}10'N \lambda = 20^{\circ}18'E$ Gr. - AG = + 1h 21 min.												PEC										BR. ST. 218								
I	722.2	00.1	04.5	02.2	02.2	05.2	-00.5	05.9	20	-06.4	14	04	C2.0	10	01.8	06	01.7	C7	01.7	05	01.6	17	01.6	Q3	C2.3	34				
II	712.8	01.9	9.9	04.3	04.3	07.4	01.2	14.2	17	-03.0	01	14	C1.9	05	01.0	04	01.7	04	01.6	09	01.6	12	02.1	01	04.0	75				
III	716.2	04.5	11.4	07.9	07.9	12.3	03.6	22.6	21	-04.0	01	17	C1.0	08	01.8	05	01.4	07	01.3	05	01.2	08	02.3	03	01.7	72				
IV	714.5	07.1	12.8	08.9	09.4	13.6	05.1	20.9	30	01.0	19	10	C2.3	11	02.0	10	01.9	C5	01.6	08	01.9	10	02.4	08	01.9	07	02.1	19		
V	715.6	11.0	16.0	12.9	13.4	18.2	08.4	25.3	31	04.4	11	15	C1.1	16	07.2	10	01.6	06	02.5	14	01.6	11	01.5	05	02.2	03	02.3	13		
VI	716.2	16.1	21.6	17.3	18.1	22.8	12.7	28.2	27	04.4	14	03	C2.3	14	07.1	C8	04	02.0	12	01.6	07	02.4	16	03.0	07	03.1	19			
VII	718.4	17.9	24.7	20.0	20.6	26.1	14.5	32.9	17	09.7	10	06	C2.5	07	02.9	15	01.7	04	02.6	22	02.6	09	02.2	17	02.4	02	03.5	11		
VIII	716.6	19.0	26.6	21.1	22.0	27.7	16.3	32.8	05	09.9	14	10	02.0	00	02.4	12	02.0	10	01.9	15	02.2	14	03.4	-	-	-	-	-		
IX	718.4	14.0	21.9	16.8	17.4	22.8	11.7	30.7	04	01.8	28	03	C1.7	09	07.1	06	02.0	07	02.3	09	01.7	11	01.9	17	02.8	02	03.0	16		
X	716.9	07.5	13.7	09.6	10.1	14.7	05.9	19.4	01	-03.0	28	04	C1.2	17	01.8	04	01.5	04	01.5	08	02.4	11	01.7	13	02.4	-	34			
XI	719.6	02.9	9.9	04.1	05.6	05.8	02.1	12.8	17	-07.6	19	03	01.3	06	01.5	08	01.5	03	02.0	07	01.6	10	01.6	10	01.8	02	02.0	41		
XII	726.4	06.0	04.0	01.6	01.9	05.2	-01.0	12.6	04	-07.6	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	717.6	08.5	14.5	10.7	11.1	15.5	06.7	32.9	M	-07.6	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\varphi = 42^{\circ}26'N \lambda = 20^{\circ}21'E$ Gr. - AG = + 1h 22 min.												SKIVJANJE-ĐOJAKOVICA										BR. ST. 219								
I	-	-00.6	05.0	01.3	01.7	05.7	-01.4	10.5	22.21	-07.5	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	01.0	07.6	03.6	03.9	08.9	00.1	15.5	16	-04.6	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	03.3	12.4	07.0	07.4	13.4	02.1	23.5	23.22	-05.5	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	05.6	12.8	08.2																										

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha			Padavine mm			Broj dana na sat																					
								Tn	Tx	Tn	Tx	Tx	Tn	F (0-12)	Nm (0-10)	R mm	●	★	▲	◆	▲	■	■									
	7	14	21	Sred. (Dnevi)	Inzolacija Broj sati	em	m	t	Σ	Max	Min	7	14	21	Σ	Max	Min	7	14	21	Σ	Max	Min	7	14	21						
BR. ST.216																																
TEPLI CL																																
I	7.5	7.4	6.4	7.1	-	-	-	-	-	-	-	048	C13.6	03	03	07	27	*	*	*	*	02	16	14	09	01	06	12	04			
II	5.9	5.9	5.0	5.6	-	-	-	-	-	-	-	035	C12.0	08	*	19	*	*	*	*	*	06	11	07	05	02	06	03	02			
III	6.6	6.4	4.9	6.0	-	-	-	-	-	-	-	027	C07.0	05	*	17	*	*	*	*	*	06	14	11	05	03	03	09	01			
IV	6.7	7.0	6.3	6.8	-	-	-	-	-	-	-	126	C27.3	18	*	07	*	*	*	*	*	01	11	14	11	06	14	03	02			
V	7.2	7.5	6.6	7.3	-	-	-	-	-	-	-	139	C27.4	16	*	*	*	*	*	*	*	*	14	22	16	03	22	*	*	01		
VI	6.8	7.4	6.0	6.7	-	-	-	-	-	-	-	121	C19.3	07	*	*	0*	*	*	*	*	02	*	01	19	05	15	19	*	07		
VII	4.4	5.3	3.4	4.4	-	-	-	-	-	-	-	074	C36.6	24	*	*	14	04	*	*	*	*	09	09	07	06	03	07	*	01		
VIII	3.7	5.2	3.1	4.0	-	-	-	-	-	-	-	035	C17.4	13	*	*	17	02	*	*	*	*	10	04	05	05	01	05	*	06		
IX	3.7	5.4	3.2	4.1	-	-	-	-	-	-	-	073	C40.1	27	*	*	*	05	*	*	*	*	05	C1	06	05	01	06	*	*	01	
X	7.1	6.6	5.6	6.5	-	-	-	-	-	-	-	090	C21.3	12	*	*	03	*	*	*	*	*	01	11	17	13	02	16	02	01		
XI	6.1	5.4	4.9	5.5	-	-	-	-	-	-	-	082	C30.9	27	*	*	04	*	*	*	*	*	08	11	11	08	02	09	05	01		
XII	6.6	6.6	6.4	6.7	-	-	-	-	-	-	-	058	C27.0	09	*	03	26	*	*	*	*	*	06	13	14	11	01	07	11	03		
GOD.	5.8	6.4	5.1	5.9	-	-	-	-	-	-	-	908	C40.1	27	*	*	03	10	105	39	06	*	02	*	55	123	147	110	27	120	45	15
BR. ST.217																																
DIMITREVGRAD																																
I	7.3	7.8	6.5	7.2	064.5	03.8	86	70	86	80	48	037	C10.3	03	03	04	23	*	*	*	*	C2	*	C3	16	15	08	C1	06	06	01	
II	4.6	6.0	5.5	6.0	117.7	04.3	85	55	77	72	25	028	C12.2	21	*	*	13	*	*	*	*	05	*	04	12	05	04	01	03	01		
III	6.4	5.9	5.0	5.0	154.0	04.5	82	47	70	66	17	019	C05.5	07	*	*	11	01	*	*	*	04	*	08	14	10	04	09	06	03		
IV	7.0	7.0	4.4	6.1	152.3	05.3	E2	45	70	67	22	072	C26.6	19	*	*	06	*	*	*	*	06	*	C4	13	08	03	12	02	01		
V	6.3	6.7	5.7	6.2	197.1	08.1	86	57	82	75	34	128	C41.5	16	*	*	01	01	*	*	*	C1	*	C2	08	20	15	C3	20	*	01	
VI	6.3	6.3	5.1	6.0	212.1	10.5	E3	58	80	74	38	083	C22.6	08	*	*	14	*	*	*	*	05	*	02	03	15	11	03	15	*		
VII	3.7	4.0	3.1	3.4	316.7	10.6	79	46	78	68	23	050	C13.8	24	*	*	19	11	*	*	*	04	*	14	C3	08	07	03	08	*	01	
VIII	2.7	4.7	2.1	3.2	252.3	10.6	80	38	74	64	24	035	C13.4	26	*	*	24	19	*	*	*	02	*	01	15	C1	07	04	02	*		
IX	3.2	4.6	2.3	3.4	240.4	09.0	E4	46	76	67	25	022	C07.4	27	*	*	17	01	*	*	*	03	01	12	*	06	06	*	*	04		
X	7.0	7.1	6.1	6.0	158.0	07.1	86	51	82	73	26	065	C15.0	25	*	*	05	*	*	*	*	01	08	16	10	07	16	*	04			
XI	7.6	5.6	3.5	5.9	115.9	05.2	89	68	87	82	40	078	C17.5	05	*	*	11	*	*	*	*	02	*	05	11	08	07	03	01	*		
XII	6.5	6.2	6.4	6.4	087.5	04.0	E9	73	86	82	46	057	C13.0	15	*	01	24	*	*	*	01	*	05	10	05	03	10	02	01	*		
GOD.	5.8	6.0	4.5	5.5	2108.5	06.9	P4	54	78	72	17	674	C04.5	Kv	*	03	59	61	18	04	31	02	50	120	137	101	2P	130	17	06		
PEČ																																
BR. ST.218																																
I	7.0	7.5	5.9	6.8	087.1	04.4	E7	72	83	81	45	028	C04.5	03	*	*	16	*	*	*	*	C2	*	C3	14	12	07	10	04	01	*	
II	7.0	7.4	7.1	7.4	088.2	05.0	E7	70	80	79	45	066	C22.0	05	*	*	11	*	*	*	*	04	*	18	11	09	03	11	C1	*		
III	7.1	6.6	5.5	6.6	144.6	05.2	79	57	67	68	29	056	C017.0	29	*	*	06	*	*	*	*	04	*	13	13	10	01	11	07	02	*	
IV	7.3	7.9	6.1	7.1	136.7	05.4	72	50	64	62	27	082	C30.6	18	*	*	06	*	*	*	*	02	*	10	12	07	03	12	*	02		
V	7.0	7.5	6.6	6.8	174.2	07.5	80	57	70	69	40	111	C29.3	16	*	*	01	*	*	*	*	03	*	01	11	17	14	04	17	*		
VI	5.0	7.2	6.7	6.7	212.9	09.5	70	49	64	61	27	074	C26.7	17	*	*	05	*	*	*	*	05	*	06	12	07	02	12	*	01		
VII	3.5	5.5	3.1	3.6	300.4	10.1	87	47	55	56	23	044	C31.0	21	*	*	17	07	01	C7	02	11	05	07	05	01	C7	*	03			
VIII	2.8	4.9	4.1	3.9	295.1	10.4	63	41	55	53	29	030	C06.1	30	*	*	24	10	03	05	*	10	02	06	04	06	06	04	*	05		
IX	5.0	5.2	2.7	4.3	201.9	10.0	61	52	69	68	26	042	C24.7	27	*	*	10	01	*	02	*	08	04	08	06	01	06	*	07			
X	7.1	6.9	5.3	6.4	147.6	07.0	86	61	76	74	35	284	C02.1	16	*	*	01	*	*	*	*	03	*	10	17	17	09	17	01	01	*	
XI	6.5	6.9	5.4	6.3	090.4	05.5	89	69	81	80	37	107	C30.0	01	*	*	05	*	*	*	*	02	*	04	12	11	01	01	01	*	01	
XII	7.1	7.3	6.2	6.9	068.7	04.3	88	74	82	81	44	023	C00.7	13	*	03	20	*	*	*	02	*	03	15	11	07	08	05	01	*		
GOD.	6.2	6.7	5.4	6.1	1947.8	07.1	79	58	70	69	23	930	C02.1	Kv	*	03	59	61	18	04	31	02	50	120	137	101	2P	130	17	06		
SKIVJANE-DJARCVICA																																
BR. ST.219																																
I	-	-	-	-	-	-	-	-	-	-	-	024	C09.0	18	*	*	10	*	*	*	*	-	*	07	06	*	07	01	*	05		
II	6.4	5.3	5.4	5.7	-	-	-	-	-	-	-	074	C29.0	05	*	*	14	*	*	*	*	06	*	08	09	06	02	08	*	06		
III	5.8	5.0	5.1	5.7	-	-	-	-	-	-	-	059	C18.0	05	*	*	07	*	*	*	*	09	*	C9	C2	07	04	02	*	01		
IV	5.9	6.7	5.6	5.9	-	-	-	-	-	-	-	084	C23.0	18	*	*	-	*	*	*	*	-	*	10	09	03	10	*	*	02		
V	5.0	5.2	5.0	5.3	-	-	-	-	-	-	-	164	C04.5	16	*	*	01	*	*	*	*	03	*	03	12	12	06	14	*	03		
VI	5.0	5.3	5.0	5.7	-	-	-	-	-	-	-	085	C26.0	17	*	*	15	*	*	*	*	02	*	04	10	16	03	10	*	01		
VII	2.0	3.6	3.2	3.2	-	-	-	-	-	-	-	025	C11.2	2																		

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)															
		Tm			Sred. (Dnes)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW	
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.		
$\varphi = 42^{\circ}38'N \lambda = 20^{\circ}34' E$ Gr. $\Delta G = + 1h 22 min.$																											
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	00.9	08.3	03.9	04.3	09.3	00.2	16.9	16 -05.0	28.12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	02.8	13.1	07.2	07.5	14.0	01.6	25.0	21 -05.8	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	05.7	13.9	08.5	09.2	15.1	03.8	21.8	30 -02.0	71	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	10.8	18.4	12.3	13.4	19.9	07.6	27.0	31 01.1	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	15.9	22.8	17.0	18.2	24.3	11.8	29.0	27 04.2	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	16.8	26.2	18.5	20.0	27.5	12.6	34.4	17 07.4	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	17.0	28.5	19.6	21.1	29.7	13.2	34.7	05 09.5	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	11.9	23.8	15.4	16.6	25.1	09.9	32.7	04 -00.3	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	05.9	15.2	08.7	09.7	16.7	04.5	22.0	23 -03.6	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	01.9	09.8	04.6	05.2	11.0	01.3	16.4	15 -02.2	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-01.2	04.5	01.2	01.4	06.0	-01.6	13.5	04 -07.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
God.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}04'N \lambda = 20^{\circ}39' E$ Gr. $\Delta G = + 1h 23 min.$																											
I	-	-02.0	01.8	-01.2	-00.5	03.3	-03.4	-	-	-	19	02.0	08	02.0	26	01.2	04	02.2	02	02.0	03	01.7	02	01.0	19	02.4	10
II	-	00.3	04.5	01.3	01.8	06.0	-01.2	12.1	12 -06.1	28.09	10	02.2	06	01.5	20	01.4	20	02.1	10	02.4	04	03.0	01	03.0	13	03.5	*
III	-	01.8	07.3	03.4	04.0	08.3	00.8	19.0	23 -07.1	01	17	02.1	C5	01.8	33	01.2	05	02.0	02	03.0	01	05.0	01	02.0	25	02.9	04
IV	-	03.5	08.1	04.7	05.2	09.7	01.6	18.0	30 -01.1	24	24	02.4	02	02.5	17	01.3	07	02.7	11	02.4	C2	02.5	06	02.5	18	02.7	01
V	-	04.4	12.8	09.1	09.8	14.6	-	22.0	31	-	17	C2.6	06	01.8	15	01.1	12	01.4	16	02.8	14	03.1	*	*	05	02.4	08
VI	-	13.6	17.7	13.2	14.4	19.5	-	27.0	27	-	10	02.8	02	01.0	21	01.4	08	01.6	14	02.1	15	02.7	06	03.5	10	02.3	04
VII	-	15.3	21.2	14.8	16.5	23.0	-	32.1	17	-	22	C3.0	05	02.2	26	C1.5	14	01.1	05	02.4	05	03.8	02	03.0	08	02.8	06
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	12.0	18.4	12.6	13.9	19.7	09.3	28.1	04 03.0	28	12	C3.0	04	02.0	31	01.2	15	02.3	10	02.1	05	04.0	01	04.0	06	03.0	06
X	-	06.3	11.6	07.2	08.1	13.1	04.3	19.1	05 -03.4	28	10	02.6	03	02.3	17	01.2	15	02.7	22	03.1	18	03.8	05	02.2	03	04.0	*
XI	-	02.2	07.5	03.2	04.0	08.7	06.9	16.0	19 -05.1	02	24	02.3	04	01.8	17	01.2	11	01.5	12	02.5	12	03.4	03	01.7	03	02.0	04
XII	-	-00.3	03.4	00.3	00.9	05.1	-02.2	12.0	29 -07.1	20,19	13	02.7	13	01.9	13	01.2	23	02.2	07	02.0	08	02.9	02	02.0	11	04.5	03
God.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}13'N \lambda = 20^{\circ}44' E$ Gr. $\Delta G = + 1h 23 min.$																											
I	-	00.3	04.7	02.3	02.4	05.6	-00.4	11.8	23 -06.0	16	05	C1.6	09	02.1	C3	01.3	03	01.3	02	01.5	01	01.0	01	01.0	02	01.0	67
II	-	01.7	07.4	04.6	04.6	08.8	01.2	14.7	17 -03.1	28	04	02.8	07	02.9	02	01.5	04	01.5	01	02.0	04	02.2	06	02.2	*	56	
III	-	04.1	12.0	08.8	08.4	13.2	03.6	23.6	23 -04.1	01	02	C1.5	08	01.1	C1	02.0	06	01.7	*	03	02.3	01	02.0	02	03.5	70	
IV	-	06.8	13.6	09.8	10.0	14.7	05.6	22.4	30 -01.6	21	07	C1.3	03	02.3	06	01.7	04	01.8	01	02.0	05	01.6	06	02.5	03	C1.3	55
V	-	11.8	18.1	13.8	14.4	20.0	09.6	26.6	31 05.4	11	07	C2.1	05	C1.6	C1	02.0	06	01.8	09	01.6	11	01.8	12	02.5	02	01.5	40
VI	-	17.1	23.5	18.4	19.4	25.3	14.1	32.5	27 07.0	14	08	01.8	08	01.9	04	01.2	05	01.6	07	01.3	14	02.1	21	02.7	02	01.0	21
VII	-	19.1	27.0	21.4	22.0	28.9	14.9	37.6	17 09.5	09	18	C1.5	09	01.4	12	02.1	15	01.7	05	01.2	05	01.6	08	02.1	03	01.7	18
VIII	-	16.9	26.4	22.1	22.7	29.6	16.2	36.1	05 11.8	31	16	C1.8	19	01.9	06	01.8	09	01.3	06	01.3	07	01.1	01	01.0	20	*	01.0
IX	-	14.3	24.0	17.8	18.5	25.4	13.0	34.1	04 03.7	28	05	C2.4	11	01.6	06	01.3	11	01.8	08	01.9	08	01.8	07	02.3	03	01.3	31
X	-	08.4	15.7	10.9	11.4	17.0	07.0	23.9	23 -02.0	28	04	01.2	08	01.6	04	01.5	07	01.9	11	02.0	13	02.8	16	02.6	04	01.2	26
XI	-	03.1	05.6	05.8	10.2	15.1	29.28	-01.4	18	11	01.3	12	02.2	05	01.8	06	01.3	07	01.1	09	01.7	05	02.2	07	01.1	28	*
XII	-	-00.4	03.7	01.7	01.9	04.7	-00.7	12.2	04 -06.1	24	11	01.5	20	02.3	04	01.2	04	01.0	11	01.5	06	02.0	07	01.7	04	01.2	26
God.	-	07.0	14.8	09.1	10.0	15.7	05.0	34.0	05 08.5	06.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 42^{\circ}39'N \lambda = 21^{\circ}09' E$ Gr. $\Delta G = + 1h 25 min.$																											
I	715.8	-00.9	03.1	00.1	00.6	03.7	-01.8	08.0	03.02	-09.1	16	04	C3.0	07	02.9												

Meseč	Oblačnost Nm (0-10)			Isolacija bez sati Srednje vrednosti	Vlažnost vazduha			Padavine R mm			Broj dana na sa:																																									
	7	14	21		mm	m s			Σ	Max	Dati.	Tn	Tx	Tn	Tx	Tx	Tn	F (0-12)	Nm (0-10)	R mm	●	★	▲	▲	▲	▲	R	T	III	IV																						
						7	14	21		Srednje vrednosti	Min																																									
KLEINA																																																				
BR. ST.221																																																				
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-																							
II	7.3	5.8	6.0	6.4	-	-	-	-	-	-	-	013 003.0	11	-	-	-	-	-	-	-	-	11	07	-	11	01	-	-	-	-	15																					
III	-	-	-	-	-	-	-	-	-	-	-	048 C18.0	05	-	-	11	-	-	-	-	05	14	13	05	02	13	-	-	-	-	09																					
IV	6.3	6.8	4.6	5.9	-	-	-	-	-	-	-	015 007.2	09	-	-	09	01	-	-	-	-	08	04	-	07	03	02	-	-	-	-	05																				
V	6.4	4.5	4.2	5.7	-	-	-	-	-	-	-	129 064.4	16	-	-	02	-	-	-	-	03	06	17	11	03	17	-	-	-	-	03																					
VI	5.5	5.9	6.4	5.9	-	-	-	-	-	-	-	080 044.5	17	-	-	16	-	-	-	-	01	07	11	10	01	11	-	-	-	-	02																					
VII	3.2	4.1	3.0	3.4	-	-	-	-	-	-	-	035 011.7	08	-	-	23	12	-	-	-	13	04	09	07	02	09	-	-	-	-	02																					
VIII	2.5	4.5	2.8	3.3	-	-	-	-	-	-	-	014 006.3	24	-	-	27	17	-	-	-	13	02	06	03	-	04	-	-	-	-	02																					
IX	5.1	4.4	2.0	3.8	-	-	-	-	-	-	-	C43 024.3	27	-	-	01	19	02	-	-	10	02	07	05	01	07	-	-	-	-	06																					
X	6.1	6.1	4.9	5.7	-	-	-	-	-	-	-	191 025.4	16	-	-	06	-	-	-	-	05	C9	16	14	06	16	01	-	-	-	-	08																				
XI	7.0	5.9	5.5	6.1	-	-	-	-	-	-	-	092 026.2	26	-	-	15	-	-	-	-	04	12	10	09	04	10	-	-	-	-	01																					
XII	6.9	7.5	6.7	7.7	-	-	-	-	-	-	-	026 007.5	15	-	03	24	-	-	-	-	01	16	09	07	-	07	03	01	01	12																						
GOD.	-	-	-	-	-	-	-	-	-	-	-	734 064.4	K.v.	-	-	-	-	-	-	-	-	128	91	22	125	08	03	01	-	-	24																					
DRAGAS																																																				
BR. ST.222																																																				
I	6.5	6.5	6.4	6.5	-	-	-	-	-	-	-	044 020.1	24	-	-	-	-	-	-	-	01	01	07	16	12	01	07	16	02	-																						
II	6.2	5.6	5.6	6.1	-	04.0	80	69	79	76	38	048 G19.7	05	-	03	16	-	-	-	-	01	06	11	09	06	02	07	04	-	02																						
III	5.8	6.3	6.0	6.0	-	-	-	-	-	-	-	020 015.1	09	-	01	15	-	-	-	-	09	15	10	05	01	07	08	05	-	01																						
IV	7.4	8.3	6.8	7.5	-	04.8	02	62	74	73	22	043 015.6	17	-	-	05	-	-	-	-	02	01	15	13	10	01	12	04	-	01																						
V	6.8	7.4	6.9	7.0	-	-	-	-	-	-	-	06.7 78 64 77 73 30	164 041.1	16	-	-	-	-	-	-	01	-	02	13	17	16	05	17	-	04																						
VI	5.8	5.9	6.1	5.9	-	-	-	-	-	-	-	08.3 70 58 73 67 32	027 C20.0	20	-	-	-	-	-	-	01	-	06	11	13	10	03	13	-	05																						
VII	2.3	3.9	3.1	3.1	-	-	-	-	-	-	-	09.1 70 50 73 64 21	027 010.0	21	-	-	-	-	-	-	02	01	15	04	05	04	01	05	-	02																						
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-																							
IX	4.5	4.8	3.0	4.1	-	-	-	-	-	-	-	08.4 74 57 76 69 39	C36 016.5	27	-	-	-	-	-	-	01	-	08	05	05	03	02	05	-	03																						
X	5.9	6.9	4.9	5.9	-	-	-	-	-	-	-	05.8 75 60 74 70 30	168 033.2	15	-	-	02	-	-	-	-	02	01	19	17	08	18	03	-	-	03																					
XI	5.5	5.7	5.6	5.6	-	-	-	-	-	-	-	100 040.5	02	-	-	06	-	-	-	-	01	07	04	06	03	-	-	-	-	01																						
XII	6.2	5.6	7.3	6.4	-	-	-	-	-	-	-	C39 013.4	19	-	03	24	-	-	-	-	05	06	13	14	07	01	07	-	-	23																						
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-																							
PRIZREN																																																				
BR. ST.223																																																				
I	7.0	7.0	6.4	6.8	-	-	-	-	-	-	-	084.1 04.6 91 74 84 83 46	052 018.6	24	-	-	15	-	-	-	-	05	06	15	15	07	02	12	05	01	05																					
II	7.1	6.9	6.0	6.6	-	-	-	-	-	-	-	092.4 05.0 92 67 81 80 37	041 020.0	05	-	-	09	-	-	-	-	05	02	04	15	08	06	02	08	-	08																					
III	6.0	6.4	5.8	6.1	-	-	-	-	-	-	-	149.7 05.6 87 57 69 71 26	061 025.0	20	-	-	01	-	-	-	-	01	04	07	11	08	02	11	-	-	04																					
IV	7.3	7.6	5.6	6.0	-	-	-	-	-	-	-	051 013.5	17	-	-	-	-	-	-	-	06	01	12	15	10	02	15	-	-	01																						
V	6.5	7.0	5.1	6.2	-	-	-	-	-	-	-	184.4 07.9 77 54 67 66 27	159 048.7	16	-	-	04	-	-	-	-	08	01	02	09	17	16	04	17	-	06																					
VI	5.5	5.4	4.7	5.2	-	-	-	-	-	-	-	234.1 09.8 68 47 62 59 29	061 025.0	20	-	-	18	03	01	1C	03	04	07	11	08	02	11	-	04																							
VII	2.9	3.7	2.7	3.1	-	-	-	-	-	-	-	319.0 10.4 70 39 55 55 21	024 013.6	08	-	-	24	15	01	05	01	16	03	07	04	01	07	-	-	02																						
VIII	2.7	3.9	2.1	3.9	-	-	-	-	-	-	-	296.8 10.9 70 40 54 55 22	024 007.5	23	-	-	27	16	01	10	-	12	02	07	04	07	-	-	06																							
IX	4.9	4.1	1.9	3.6	-	-	-	-	-	-	-	214.0 09.8 80 44 65 63 27	031 015.1	27	-	-	20	03	-	09	-	10	02	06	04	02	06	-	-	04																						
X	6.8	6.5	4.5	6.0	-	-	-	-	-	-	-	158.9 06.9 83 52 72 69 27	155 025.4	15	-	-	01	-	-	16	05	02	07	21	18	05	21	-	04																							
XI	8.3	6.2	5.0	6.5	-	-	-	-	-	-	-	059.0 05.6 88 71 83 39	059 022.6	01	-	-	07	03	-	02	19	13	06	02	13	01	01	-	01																							
XII	6.3	7.8	7.8	8.0	-	-	-	-	-	-	-	052.2 04.6 90 81 89 87 54	060 033.0	19	-	04	20	-	-	09	02	02	20	12	08	02	09	06	01																							
GOD.	6.6	5.8	5.8	6.1	-	-	-	-	-	-	-	613 034.8	K.v.	-	-	86	70	25	-	01	-	56	142	120	94	23	110	17	03	-	02																					
KOSOVSKA MITROVIC																																																				
BR. ST.224																																																				
I	8.7	7.7	7.2	7.8	-	-	-	-	-	-	-	013 003.5	20	-	-	18	-	-	-	-	01	19	89	05	-	07	04	01	-	02																						
II	7.5	6.3	7.1	7.0	-	-	-	-	-	-	-	034 013.9	05	-	-	15	-	-	-	-	05	16	06	05																												

Mesec	Vazdušni Pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Pm (0-12)																		
		Tm			Sred. (Dles)	Max	Min	Max	Dat.	Min	Det.	N		NE		E		SE		S		SW		W		NW				
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
$\varphi = 42^{\circ}23'N \lambda = 21^{\circ}10' E$ Gr. $\Delta G = + 1h 25 min.$																														
I	-	-01.5	02.5	-00.5	00.0	03.1	-02.5	08.0	03 -08.8	25	18	C1.1	*	*	C2	C2.5	12	02.7	03	01.7	07	01.9	11	01.8	39	C2.1	01			
II	-	00.9	05.4	03.2	03.4	07.3	-00.1	14.0	17 -06.3	28	05	C1.4	05	02.0	C4	C1.5	21	03.4	07	02.5	08	02.0	15	01.9	22	C2.1	01			
III	-	01.6	10.9	05.5	05.9	11.6	01.1	22.9	23.22 -06.8	01	06	C1.3	06	01.7	02	02.0	26	03.5	04	02.0	09	01.7	09	01.7	31	02.0	*			
IV	-	05.2	11.9	06.9	07.7	12.9	02.7	20.0	29 -02.0	21	14	C1.6	09	01.6	04	01.8	26	03.5	01	02.0	12	02.6	05	02.0	19	02.4	*			
V	-	10.0	16.5	11.6	12.4	18.3	07.2	25.0	31 03.0	14	10	C1.6	C8	02.0	05	02.0	05	02.2	04	01.8	07	02.7	24	01.8	32	C2.1	*			
VI	-	14.4	21.0	15.6	16.7	22.7	11.3	28.5	29 04.4	14	13	C1.2	04	02.0	01	02.0	11	01.8	04	01.0	18	02.6	19	02.3	20	02.0	*			
VII	-	15.6	24.6	17.5	18.8	26.0	11.9	33.8	17 07.1	10	09	C1.7	04	02.0	02	02.5	01	02.0	06	01.5	13	02.4	25	02.2	33	02.6	*			
VIII	-	16.0	27.2	18.6	20.1	27.7	13.2	33.2	05 09.3	11	03	C1.3	G7	07.5	*	*	05	02.0	03	01.3	18	01.4	25	02.1	37	02.1	*			
IX	-	11.7	22.6	14.5	15.8	23.3	10.0	30.0	04 00.6	28	16	C1.5	C3	02.3	*	*	08	02.4	06	01.5	09	02.2	23	01.8	25	02.2	*			
X	-	06.3	15.2	09.0	09.9	16.5	04.6	22.6	23.08 -03.2	28	14	C1.6	C4	07.0	C1	C2.0	14	02.6	03	02.7	11	02.4	15	03.3	33	C2.5	*			
XI	-	01.4	07.9	03.7	04.2	08.8	00.4	14.1	06 -04.9	30	21	C1.8	04	02.0	*	*	11	03.1	07	01.4	08	02.5	14	01.5	23	01.9	02			
XII	-	-02.2	03.3	-00.1	00.3	04.3	-03.5	09.6	04 -14.6	25	27	C1.7	C3	02.7	*	*	07	01.9	01	02.0	09	01.8	16	01.9	30	02.2	*			
GOD.	-	06.6	14.2	08.8	09.6	15.2	04.7	33.8	Pm	-14.6	25	00	156	C1.5	47	00.0	21	02.0	147	03.0	44	01.7	129	G2.7	201	02.0	344	C2.2	04	
$\varphi = 42^{\circ}47'N \lambda = 21^{\circ}36' E$ Gr. $\Delta G = + 1h 26 min.$																														
I	-	-00.3	03.6	00.6	01.1	04.6	-01.9	09.0	01 -10.3	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
II	-	02.0	08.5	04.0	04.6	09.7	00.2	15.4	11 -07.3	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
III	-	02.1	11.4	05.3	06.0	12.3	00.7	24.9	23.21 -07.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
IV	-	04.7	12.6	07.2	07.9	17.0	02.7	-	-	-	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
V	-	09.5	17.0	10.9	12.1	18.8	06.9	25.9	28 01.9	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VI	-	13.9	21.3	15.0	16.3	22.9	10.7	28.2	29 03.9	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
VII	-	14.0	24.2	15.9	17.5	25.4	11.4	33.4	17 07.0	09	04	C1.2	-	*	*	*	01	02.0	03	01.7	*	*	*	*	*	05				
VIII	-	14.4	26.7	17.0	18.8	27.5	12.3	32.0	05.04	05.2	11	02	C1.0	-	*	*	05	02.0	04	01.2	*	*	*	*	*	02				
IX	-	11.7	21.9	14.3	15.6	22.8	09.5	30.4	04 00.4	28	02	C1.0	-	*	*	*	C1	01.0	14	02.1	*	*	*	*	*	73				
X	-	07.3	14.8	08.3	09.7	16.7	04.6	22.9	08 -03.5	28	09	C1.6	-	*	*	*	03	02.0	23	02.5	*	*	*	*	*	58				
XI	-	02.3	10.0	03.9	05.0	10.9	00.8	16.9	17 -02.1	30	04	C1.5	-	*	*	*	04	01.0	14	02.1	*	*	*	*	*	68				
XII	-	-00.6	04.9	01.2	01.6	05.7	-01.7	10.0	04 -07.3	24	03	C1.3	-	*	*	*	10	02.7	*	*	*	*	*	*	*	*	80			
GOD.	-	06.6	14.7	08.6	09.7	16.2	04.7	-	-	-	10.3	K1	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 42^{\circ}27'N \lambda = 21^{\circ}47' E$ Gr. $\Delta G = + 1h 26 min.$																														
I	-	-00.3	03.6	01.5	01.6	04.5	-	08.8	29	-	-	08	C2.0	C2	03.0	10	C2.4	05	01.8	17	02.3	04	03.0	C2	01.5	01	C2.0	44		
II	-	01.8	08.3	04.2	04.6	09.4	-	13.8	17	-	-	02	C2.5	C2	02.5	04	C2.8	03	03.0	37	02.7	01	01.0	02	02.0	*	*	33		
III	-	02.9	11.8	06.2	06.8	12.6	-	23.5	22	-	-	*	02	03.5	C5	02.4	08	02.5	23	02.7	05	01.8	01	02.0	*	*	49			
IV	-	05.3	13.0	07.9	08.5	14.4	03.2	21.9	30 -02.0	03	02	C2.0	06	02.0	11	01.7	02	02.5	30	02.7	*	*	01	01.0	02	02.5	36			
V	-	09.7	17.5	12.0	12.8	19.1	07.1	25.7	31 01.9	11	01	C1.0	07	02.4	08	C2.1	05	02.2	12	02.6	06	02.2	05	02.4	02	02.0	47			
VI	-	14.8	21.8	16.2	17.3	24.1	11.3	29.3	29 06.4	14	12	C2.5	01	04.0	06	C1.5	01	03.0	01	02.8	14	02.4	07	03.4	*	*	41			
VII	-	15.3	25.4	17.0	18.7	26.7	11.5	34.9	17 06.8	10	03	C3.3	06	02.8	07	02.0	01	02.0	08	01.8	06	02.0	04	02.2	03	04.3	55			
VIII	-	16.0	28.0	18.8	20.4	28.8	12.5	34.5	05 09.0	11	*	*	03	02.7	09	C2.1	02	02.5	15	02.0	*	*	08	02.6	*	*	56			
IX	-	11.8	23.3	14.7	16.2	24.2	09.8	30.9	04 00.2	28	03	C2.0	02	02.0	06	C2.3	02	03.5	19	02.4	05	02.4	03	03.0	01	01.0	49			
X	-	07.0	16.2	10.4	10.8	17.3	04.4	23.1	14,08 -04.5	28	01	C3.0	*	*	03	C2.0	01	03.0	41	02.5	06	02.3	02	02.5	*	*	39			
XI	-	01.8	09.4	03.8	04.7	10.4	00.6	15.0	06 -03.0	30	01	C3.0	16	02.1	C5	01.8	*	01	02.0	03	01.0	17	02.2	02	02.0	03	03.0	02	01.5	39
XII	-	-01.4	04.1	03.7	01.1	01.2	05.1	-02.2	10.7	13 -08.5	25	01	04.0	35	02.7	03	02.3	*	*	03	01.7	08	02.1	03	02.7	01	03.0	39		
GOD.	-	07.1	15.2	09.3	10.2	16.4	05.6	34.7	7. VII -08.5	25	00	93	C2.2	292	02.3	S1	02													

Mesec	Vardulni pritisak Pm, mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova m/s, Fm (0-12)														
		Tm			Sred. (Dnes)		Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C					
		7	14	21									8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.		
$\varphi = 42^{\circ}58'N \lambda = 22^{\circ}08' E$ Gr. $\Delta G = +1h\ 29\ min.$																										
I	-	00.5	03.8	01.7	01.9	04.7	69.4	09.5	31.03	-08.6	16	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	03.6	09.8	05.1	05.9	11.2	01.7	16.4	11	-03.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	05.0	12.9	08.2	08.6	13.9	03.0	26.4	27	-05.6	01	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	07.9	14.0	09.6	10.0	15.3	04.4	25.9	30	-00.1	04	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	12.0	16.3	13.1	14.1	20.1	09.6	28.4	31	05.5	11	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	16.4	22.2	16.7	18.0	24.3	13.0	29.9	29	06.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	16.8	25.5	17.9	19.5	26.6	13.4	34.9	17	08.5	04	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	17.2	26.0	19.7	21.2	29.3	14.3	35.4	04	11.0	07.06	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	14.0	24.4	16.1	17.7	25.2	11.9	32.4	04	02.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	09.7	16.9	10.4	11.8	17.9	06.1	25.1	08	-00.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	03.5	11.2	05.8	06.5	12.2	02.0	17.4	19	-01.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	00.3	04.6	01.7	02.0	05.3	-01.1	10.0	05	-05.5	25	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	08.9	16.0	10.5	11.4	17.2	601.7	35.4	04M	-09.5	25 VII	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 42^{\circ}50'N \lambda = 22^{\circ}08' E$ Gr. $\Delta G = +1h\ 29\ min.$																										
I	-	-00.4	03.6	01.0	01.3	04.5	-01.4	10.0	03	-05.7	16	36	C1.8	C6	01.7	C4	01.0	10	C1.9	13	C2.0	02	C2.5	-	C2	
II	-	01.7	09.8	04.0	04.9	10.9	00.5	16.9	17.16	-06.1	28	11	C2.1	C2	01.5	C5	01.8	22	C1.8	27	C2.1	03	C2.7	-	C2.6	
III	-	02.0	12.2	06.3	06.7	13.1	01.5	25.9	23	-06.4	01	18	C1.7	C7	02.1	C5	01.6	15	C1.9	17	C1.9	04	C2.2	02	C2.0	
IV	-	05.2	13.1	07.6	08.4	14.5	03.2	25.1	30	-02.8	03	17	C2.0	C4	01.3	11	C1.3	17	C1.9	14	C2.2	01	C2.0	-	C2.6	
V	-	10.8	18.1	12.1	13.3	19.2	08.5	27.2	31	03.1	11	11	C1.9	C6	01.8	13	C1.6	15	C1.8	16	C1.8	03	C2.3	-	C2.7	
VI	-	15.0	21.0	15.7	16.9	23.3	11.8	29.4	29	05.9	14	16	C2.1	C5	01.8	03	01.7	12	C1.9	16	C1.7	04	C1.8	02	C2.0	
VII	-	15.8	24.5	16.9	18.5	25.7	12.2	33.9	17.14	08.6	10	15	C2.6	C1	02.0	20	C1.2	09	C1.4	15	C1.9	01	C1.0	01	C1.7	
VIII	-	15.5	26.8	17.8	19.5	28.0	13.4	33.1	03	10.0	11	13	C1.8	C10	01.5	07	C1.0	25	C1.6	07	C2.0	01	C1.0	02	C2.0	
IX	-	12.4	23.5	14.3	16.1	24.4	10.7	32.4	04	02.5	28	13	C2.4	C3	01.3	04	C1.0	21	C2.0	09	C2.0	05	C2.4	-	C2.7	
X	-	07.2	17.1	08.6	10.5	18.0	05.4	25.0	08	-02.6	28	13	C2.2	C5	01.6	12	C1.2	20	C1.9	10	C1.2	01	C2.2	-	C2.3	
XI	-	02.4	10.7	04.0	05.3	11.5	01.1	17.7	06	-03.6	30	09	C1.4	C9	02.2	10	C1.2	21	C2.0	20	C2.2	04	C2.5	-	C2.0	
XII	-	-00.3	04.7	01.2	01.7	05.7	-01.2	11.4	13	-06.6	24	12	C2.7	C5	02.2	C6	01.3	17	C1.8	20	C2.2	04	C2.0	-	C3.0	
GOD.	-	07.3	15.4	09.1	10.3	16.6	05.5	33.9	F7	14.7	-09.7	46.1	184	02.0	65	C1.8	C10	01.3	204	C1.9	179	C2.0	32	C2.2	C7	C1.9
$\varphi = 42^{\circ}41'N \lambda = 22^{\circ}11' E$ Gr. $\Delta G = +1h\ 29\ min.$																										
I	-	-00.5	03.6	01.0	01.3	04.3	-01.3	08.8	29	-09.6	16	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	01.8	07.9	03.9	04.4	09.3	00.4	15.0	16	-05.4	03	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	04.0	12.0	07.2	07.6	13.1	02.7	25.1	21	-05.9	01	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	06.3	12.8	07.7	08.6	14.2	04.2	23.4	30	-00.6	21	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	11.3	17.5	12.2	13.1	18.7	08.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VI	-	15.9	21.0	15.9	17.2	22.9	12.3	29.5	29	05.6	14	-	-	-	-	-	-	-	-	-	-	-	-	-		
VII	-	16.8	24.3	17.9	19.2	25.8	12.9	33.9	17	08.5	10	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	17.6	26.7	16.3	20.7	27.6	14.8	33.9	05	10.9	11	-	-	-	-	-	-	-	-	-	-	-	-	-		
IX	-	13.2	22.7	15.8	16.9	23.7	11.0	31.5	04	04.1	28	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	07.9	15.7	10.3	11.1	17.1	06.2	24.0	08	-03.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-		
XI	-	01.8	05.3	04.6	05.1	10.6	00.8	15.2	06	-03.3	30	-	-	-	-	-	-	-	-	-	-	-	-	-		
XII	-	-01.1	03.8	01.1	01.2	04.9	-02.0	06.5	05.03	-08.2	25	-	-	-	-	-	-	-	-	-	-	-	-	-		
GOD.	-	07.9	14.8	09.7	10.5	16.0	05.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 42^{\circ}44'N \lambda = 22^{\circ}21' E$ Gr. $\Delta G = +1h\ 29\ min.$																										
I	-	-06.9	-01.6	-04.7	-04.5	-00.2	-08.4	06.6	17	-20.4	16	13	C2.2	C7	02.0	08	01.2	09	01.0	05	01.0	01	01.0	17	C1.4	
II	-	-03.7	02.0	-02.4	-01.6	03.3	-05.5	08.8	18	-13.7	11	-	-	04	02.0	13	C1.5	10	C1.4	03	C1.3	05	C1.8	08	C1.4	
III	-	-01.9	05.5	00.6	01.2	06.4	-03.6	17.8	23	-14.5	02	-	-	07	01.9	20	C1.6	16	C1.3	C8	C1.4	01	01.0	-	C3.6	
IV	-	01.4	06.7	01.9	02.0	04.4	-01.2	15.3	30	-05.6	05	04	C1.2	C1	03.0	04	02.2	14	C1.5	04	01.8	08	02.0	18	C1.7	
V	-	06.8	11.3	04.9	09.0	13.1	03.3	20.2	31	-01.3	10	01	02.0	-	-	05	C1.0	02	02.0	-	14	C1.8	02	C1.5	31	
VI	-	11.6	15.5	10.3	11.9	17.5	07.1	24.3	27	C1.2	14	-	-	04	01.5	01	02.0	07	C1.6	05	C1.4	37	C1.7	36		
VII	-	13.1	18.8	11.2	13.6																					

Mjesec	Oblačnost Nm (0-10)			Insolacije broj sati (Dnevi)	Vlažnost vazduha			Padavine R mm			Broj dana na mjeri												R _t	■																										
	7	14	21		Srednji mm	%			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	★	▲	▲	▲	▲	▲	R _t																									
						7	14	21																																										
VLASETINCE																																																		
BR. ST-231																																																		
I	7.7	6.6	7.6	7.8	-	-	-	-	-	-	055	C13.0	20	03	16	-	-	-	03	20	11	10	05	04	-	-	-																							
II	5.5	5.7	4.8	5.3	-	-	-	-	-	-	038	C14.5	21	-	10	-	-	-	06	10	07	04	02	07	-	-	-																							
III	5.6	5.6	5.6	5.5	-	-	-	-	-	-	C26	C10.2	07	-	08	04	-	-	07	11	08	04	01	06	03	-	-																							
IV	6.4	6.4	5.9	6.2	-	-	-	-	-	-	068	C16.5	19	-	01	-	-	-	01	05	11	10	03	11	01	-	-																							
V	6.4	6.9	6.5	6.7	-	-	-	-	-	-	122	C30.2	16	-	-	03	-	-	04	12	18	15	05	18	-	-	-																							
VI	5.9	5.9	5.2	5.7	-	-	-	-	-	-	083	C20.2	12	-	-	13	-	-	03	05	14	09	04	14	-	-	-																							
VII	3.6	4.0	3.7	3.8	-	-	-	-	-	-	075	C05.4	01	-	-	18	11	-	13	04	07	05	02	07	-	-	-																							
VIII	3.1	3.5	3.2	3.3	-	-	-	-	-	-	043	C25.5	13	-	-	26	14	-	12	04	08	05	01	08	-	-	-																							
IX	5.0	4.3	3.5	4.3	-	-	-	-	-	-	048	C25.0	27	-	-	17	02	-	-	-	06	05	02	06	-	-	-	03																						
X	5.6	5.6	5.0	5.4	-	-	-	-	-	-	057	009.0	30	-	-	01	01	-	03	06	16	21	14	16	-	-	-																							
XI	5.9	5.6	5.0	5.6	-	-	-	-	-	-	076	017.0	06	-	-	04	-	-	05	10	07	05	06	01	-	-	-																							
XII	6.9	7.0	6.4	6.8	-	-	-	-	-	-	095	C28.0	15	-	-	17	-	-	05	13	15	13	02	12	09	05	-																							
GOD.	5.6	5.7	5.2	5.5	-	-	-	-	-	-	786	C45.4	04.VII	-	03	56	83	27	-	-	-	126	98	28	121	19	10	-	01	-																				
PREDJANE																																																		
BR. ST-232																																																		
I	6.3	6.1	7.3	7.9	-	04.3	86	73	88	63	45	074	C04.1	21	-	02	19	-	03	18	15	12	03	11	08	02	-																							
II	6.6	5.9	5.1	5.2	-	04.9	86	57	77	74	31	040	C14.7	21	-	12	-	-	01	06	07	04	02	08	01	01	-																							
III	6.3	5.5	5.2	5.7	-	05.1	91	53	72	72	24	024	C09.5	07	-	12	02	-	03	10	07	04	04	04	-	-	02																							
IV	6.7	6.6	5.7	6.4	-	06.1	90	55	78	74	29	075	C23.3	18	-	05	01	-	01	03	11	15	08	04	15	01	-																							
V	6.5	6.5	6.4	6.4	-	05.3	95	60	85	81	33	140	C37.5	16	-	-	03	-	-	04	12	22	15	C5	21	01	-	07																						
VI	5.8	6.3	6.4	6.2	-	11.9	90	64	91	82	79	155	C34.2	20	-	-	12	-	-	02	01	06	16	12	16	01	11	03																						
VII	3.8	3.0	3.3	3.6	-	12.6	90	56	89	78	40	109	C06.0	01	-	-	16	08	-	01	14	C5	07	05	04	07	-																							
VIII	3.1	3.0	2.8	3.2	-	12.8	94	57	86	77	24	047	C30.7	13	-	-	25	12	-	03	14	04	08	04	01	08	-																							
IX	5.3	4.6	3.3	4.4	-	10.9	94	52	92	80	30	046	C31.2	27	-	-	15	02	-	01	08	04	06	04	01	06	-																							
X	6.9	6.1	4.3	5.8	-	08.0	95	60	92	63	31	071	C01.2	30	-	-	02	01	-	03	07	15	14	02	15	01	-																							
XI	7.0	5.8	4.5	5.7	-	05.8	95	66	93	85	39	095	C02.8	29	-	-	07	-	-	06	10	09	07	06	07	04	-																							
XII	7.1	6.4	7.0	6.8	-	04.6	94	77	93	88	41	131	C30.0	15	-	01	23	-	-	04	15	17	16	05	12	11	04	-																						
GOD.	5.1	5.8	4.9	5.6	-	08.0	92	60	86	79	24	1030	C60.7	04.VIII	-	03	80	76	22	-	05	72	111	145	105	38	130	31	10																					
SURDULICA																																																		
BR. ST-233																																																		
I	6.9	7.4	6.7	7.0	-	-	-	-	-	-	051	C10.5	18	-	01	21	-	-	04	15	15	10	01	09	07	-	01																							
II	5.6	5.2	4.4	5.1	-	-	-	-	-	-	039	C19.0	08	-	04	13	-	-	01	07	C5	07	04	02	01	-	02	01																						
III	4.6	5.1	4.8	4.8	-	-	-	-	-	-	024	C08.2	07	-	05	11	-	-	11	09	08	04	-	08	03	-	01																							
IV	6.2	6.5	5.2	6.0	-	-	-	-	-	-	085	C29.0	15	-	-	-	-	-	03	09	13	11	04	13	01	-	02																							
V	5.8	6.5	5.7	6.1	-	-	-	-	-	-	128	C37.4	16	-	-	-	-	-	-	21	21	02	21	-	-	01	-																							
VI	-	-	-	-	-	-	-	-	-	-	173	C03.2	08	-	-	13	13	-	-	13	13	06	13	-	-	02	-																							
VII	3.0	3.0	2.4	2.8	-	-	-	-	-	-	072	C35.4	01	-	-	17	10	-	01	16	C3	08	06	02	08	-	02	02																						
VIII	2.1	3.1	2.4	2.8	-	-	-	-	-	-	044	C18.0	13	-	-	24	12	-	04	14	C2	07	07	01	07	-	01	02																						
IX	3.3	4.5	2.9	3.6	-	-	-	-	-	-	034	C37.5	27	-	-	14	01	-	08	11	C1	07	06	01	07	-	01	-																						
X	5.5	5.5	4.1	5.6	-	-	-	-	-	-	079	C23.8	25	-	-	03	-	-	01	06	18	13	08	18	-	-	01																							
XI	5.5	5.5	4.1	5.5	-	-	-	-	-	-	056	C17.2	27	-	-	10	-	-	05	06	07	01	03	06	01	-	06																							
XII	6.3	6.1	4.5	6.3	-	-	-	-	-	-	087	C22.2	15	-	-	23	-	-	07	13	15	13	02	08	11	-	04																							
GOD.	-	-	-	-	-	-	-	-	-	-	874	C37.4	04.VIII	-	-	-	-	01	01	-	-	135	115	27	121	24	05	-	15																					
VLASINA																																																		

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																
		Tm			Sred. (Diss)	Max	Min	Dat.	Min	Dat.		N	NE	E	SE	S	SW	W	NW	C								
		7	14	21							8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.				
SR CRNA GORA																												
$\varphi = 43^{\circ}00'N \lambda = 18^{\circ}44'E$ Gr. $\Delta G = +1h\ 15\ min.$																												
I	-	-00.7	04.4	00.7	01.3	04.8	-02.1	09.6	22	-06.8	15	04	04.5	15	03.3	08	03.5	23	01.8	08	01.9	11	01.5	04	01.8	06	01.8	14
II	-	00.3	04.9	01.1	01.8	05.7	-00.7	11.4	16	-05.6	28	01	02.0	19	05.1	02	03.0	25	01.9	15	02.6	11	02.2	02	02.5	03	02.2	07
III	-	02.5	10.2	03.9	05.2	10.5	01.9	11.2	22	-04.4	12	02	01.0	13	03.1	01	03.0	33	01.9	04	01.6	18	01.8	*	04	01.2	14	
IV	-	04.7	09.1	05.2	06.0	09.7	04.0	19.0	30	-01.6	18	*	*	23	02.4	01	01.0	28	02.0	08	01.9	18	01.7	01	02.0	05	01.6	06
V	-	08.9	13.5	09.2	10.2	14.4	08.0	21.0	27	03.6	15	04	02.0	20	02.2	01	02.0	15	01.9	03	02.0	16	02.8	03	03.3	21	01.6	10
VI	-	12.8	17.6	13.3	14.3	11.8	26.0	05	06.4	12	02	13	01.9	08	01.6	14	01.9	08	01.5	14	01.9	*	*	16	02.1	15		
VII	-	15.4	22.3	16.8	17.8	23.4	19.9	30.4	17.16	09.0	20	07	02	04.0	24	03.1	01	01.0	22	01.5	01	01.0	06	01.5	*	08	01.2	29
VIII	-	16.1	23.8	19.0	19.5	25.5	14.9	30.6	05	10.4	31	01	02.0	21	03.0	02	04.5	16	01.6	03	02.3	08	01.5	04	01.8	04	01.7	34
IX	-	12.5	19.1	10.0	15.4	20.2	-	27.4	04	*	*	*	*	09	04.3	C1	03.0	25	03.3	*	*	27	03.2	*	*	*	*	26
X	-	05.5	09.8	07.5	07.6	11.2	-	15.0	24.12	-	*	*	*	*	*	*	*	36	03.3	*	*	46	03.9	*	*	*	*	11
XI	-	01.6	07.6	05.5	05.1	09.0	-	16.4	12	-	*	01	03.0	05	04.0	*	*	29	02.9	*	*	37	03.3	*	*	01	02.0	17
XII	-	-01.8	03.4	01.2	01.0	05.3	-	12.4	30	-	*	*	*	05	06.4	*	*	38	03.7	*	*	27	03.6	*	*	*	*	23
GOD.	-	06.5	12.1	08.2	06.8	13.2	-	30.6	-	*	17	02.6	167	03.2	25	02.5	304	02.5	54	02.0	239	02.8	14	02.2	AB	C1.7	207	
KRSTAC																										BR. ST. 236		
$\varphi = 43^{\circ}09'N \lambda = 19^{\circ}08'E$ Gr. $\Delta G = +1h\ 17\ min.$																										FABLJAK		
																										BR. ST. 237		
I	+46.4	-04.5	01.1	-03.2	-02.5	01.7	-07.8	06.2	22	-14.8	14	04	03.5	03	02.0	02	02.0	09	02.1	*	*	*	01	02.0	12	02.1	67	
II	634.8	-03.7	01.1	-02.2	-01.7	02.6	-06.2	08.8	12	-13.5	09	05	01.8	01	02.0	C1	02.0	09	02.2	11	02.7	03	02.0	*	*	53		
III	637.8	-01.9	05.6	00.2	01.1	06.6	-04.2	15.0	22.1	-11.5	13	*	02	02.0	05	01.2	07	02.1	12	02.5	04	02.0	*	*	01	02.0	62	
IV	635.4	00.8	04.6	00.6	01.7	06.3	-02.5	15.4	30	-08.0	20	06	C1.8	05	01.6	01	01.0	09	02.0	04	03.8	01	02.0	*	*	06	02.2	59
V	637.3	05.9	09.3	05.5	06.5	11.7	01.2	18.6	31	-02.5	17	09	02.3	03	02.0	C1	01.0	05	02.4	13	02.0	09	02.9	03	02.3	04	02.0	46
VI	639.0	10.1	13.9	09.8	10.9	15.5	05.5	21.4	05	-01.5	14	08	01.9	01	02.0	C2	01.5	04	04.0	17	02.5	08	02.0	01	04.0	08	02.5	41
VII	641.9	12.7	17.8	12.3	13.8	19.5	07.6	21.0	17	02.2	08.0	07	07	02.0	*	09	01.2	06	02.7	05	01.6	05	02.0	01	07.0	14	02.1	66
VIII	643.1	12.9	19.9	12.8	14.6	21.6	08.6	27.5	04	03.5	14.12	04	02.0	04	02.0	07	01.6	06	02.3	*	03	02.0	02	02.0	08	02.0	59	
IX	642.0	08.9	15.5	09.9	11.1	16.8	06.9	24.0	06	-01.0	28	05	02.7	*	*	06	01.3	05	02.2	18	02.6	06	03.0	*	*	02	02.5	48
X	636.2	02.4	08.3	02.7	03.5	08.1	00.5	13.5	10	-05.7	31	03	C1.7	*	*	*	*	02	02.5	34	03.0	07	03.6	02	01.0	*	*	45
XI	639.6	-02.0	03.8	-01.3	-00.2	05.2	-03.9	10.7	18.16	-06.6	30	04	01.2	*	*	*	*	03	02.0	25	02.8	*	*	01	01.0	02	01.5	56
XII	640.1	-04.0	01.1	-03.3	-02.4	02.3	-03.3	10.2	29	-14.0	19	14	02.3	*	*	*	*	05	02.4	02	02.0	01	02.0	09	01.7	09	02.2	53
GOD.	-	05.3	14.1	07.9	08.8	15.5	04.1	33.0	05.0	04.0	25.0	01	02.0	80	01.7	15	01.3	142	01.3	36	01.3	362	01.5	12	01.2	54	01.5	384
RIJELO POLJE																										BR. ST. 231		
$\varphi = 43^{\circ}02'N \lambda = 19^{\circ}45'E$ Gr. $\Delta G = +1h\ 19\ min.$																												
I	-	-02.0	03.8	00.2	00.6	05.0	-02.4	09.6	03	-08.2	14	*	*	06	01.2	C1	01.0	12	01.0	*	*	15	01.0	*	*	01	01.0	58
II	-	-00.2	01.1	02.5	03.3	10.4	-00.9	15.6	17	-06.9	01	*	*	13	01.9	C2	01.0	13	01.0	*	*	15	01.5	03	01.3	05	01.2	33
III	-	00.8	13.0	05.7	06.3	14.3	00.2	24.8	22	-06.2	01	01	02.0	06	02.5	01	02.0	14	01.4	01	03.0	39	01.4	01	01.0	06	01.5	24
IV	-	03.6	12.3	06.6	07.3	13.6	02.4	22.3	30	-02.4	21	*	*	10	01.8	C1	01.0	17	01.2	01	01.0	34	01.7	*	*	06	01.7	21
V	-	07.9	16.9	10.8	11.6	18.3	06.0	25.3	31	00.9	11	*	*	04	01.8	02	02.0	14	01.9	03	01.3	44	01.5	*	*	07	01.1	19
VI	-	12.4	20.9	14.6	15.6	22.5	10.0	27.4	05	02.9	14	*	*	05	02.0	02	02.0	08	01.2	05	01.6	45	01.7	02	02.0	03	01.3	22
VII	-	13.0	24.2	19.5	25.7	17.1	10.8	33.0	17	04.5	09	*	*	08	01.9	01	01.0	13	01.5	05	01.2	24	01.6	01	01.0	05	02.2	32
VIII	-	13.2	26.9	16.8	18.3	28.1	11.7	33.0	05.04	05.9	14	*	*	01	02.0	*	*	07	01.3	01	01.2	35	01.2	*	*	02	01.0	36

Mjesec	Vardušni pritisak Pn, cm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vjetra m/s, Pm (0-12)																				
		Tm				Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C											
		7	14	21	Spred. (Dies)						8.	1.	8.	1.	8.	1.	8.	1.	8.											
$\phi = 42^{\circ}49'N \lambda = 12^{\circ}41'E$ Gr. $\Delta t_m = +1h\ 15\ min.$																														
I	-	-00.9	06.9	06.8	01.9	07.8	-03.0	12.0	22.12	-06.2	15	02	03.0	02	02.0	*	*	02	01.0	05	01.2	03	01.3	06	02.3	04	02.5	09		
II	-	01.2	07.3	02.3	03.3	08.8	-00.8	14.5	16	-07.0	09	01	02.0	05	02.5	11	02.5	10	01.9	05	02.0	02	02.0	01	01.0	02	01.5	06		
III	-	01.7	11.9	03.3	05.0	13.1	-01.2	22.5	21	-06.2	10	02	04.5	03	02.3	10	03.3	09	02.0	06	02.5	*	*	*	*	02	02.5	04	02.5	01
IV	-	06.1	11.9	05.8	07.2	13.0	01.4	20.0	30	-03.2	24	*	*	03	01.3	15	02.0	12	02.2	04	02.5	*	*	*	*	01	01.0	02	01.5	05
V	-	11.0	15.6	09.4	11.3	17.3	04.0	23.2	20	00.0	11	01	03.0	04	02.0	14	01.9	09	01.6	08	02.0	01	01.0	*	*	02	02.0	04		
VI	-	14.7	20.3	12.9	15.2	22.2	07.2	26.0	05	00.5	14	*	*	04	03.0	09	01.9	11	01.6	05	01.0	02	01.5	*	*	02	03.0	05		
VII	-	17.0	25.4	16.1	18.7	27.3	09.1	34.0	16	04.2	09	05	01.0	03	01.7	01	02.0	07	01.7	06	01.3	*	*	04	01.8	06	01.8	01		
VIII	-	18.2	27.1	17.7	20.2	29.7	10.2	35.5	04	05.8	14	01	01.0	*	*	05	01.6	04	01.5	09	01.3	*	*	05	01.6	02	01.5	07		
IX	-	13.7	21.8	13.7	15.7	23.4	08.1	26.0	14.10	-00.5	28	*	*	01	02.0	15	01.4	09	01.6	04	01.2	03	01.3	*	*	02	02.5	06		
X	-	05.9	11.9	07.2	08.1	13.6	02.2	18.5	05	-04.0	28	*	*	02	03.0	07	01.1	09	01.8	09	01.3	02	03.5	01	02.0	*	*	03		
XI	-	06.6	09.7	03.6	04.4	10.9	-01.0	17.4	17	-04.8	02	*	*	01	01.0	01	01.0	*	*	01	01.0	*	*	05	01.6	01	03.0	03		
XII	-	-01.7	06.9	00.1	01.3	07.9	-03.7	13.0	04	-05.8	24	12	03.0	04	07.5	03	02.0	02	01.9	03	01.0	01	01.0	02	02.0	04	02.0	04		
GOD.	-	07.3	14.7	07.7	09.4	16.2	02.7	35.5	07	-06.8	24	*	*	02.7	21	02.6	51	02.0	08	01.8	65	01.6	14	01.7	24	01.8	26	02.1	74	
$\phi = 42^{\circ}26'N \lambda = 18^{\circ}42'E$ Gr. $\Delta t_m = +1h\ 15\ min.$																														
I	765.3	04.8	11.8	05.7	07.0	13.1	01.6	17.4	20	-03.0	15	05	02.2	09	01.9	*	*	07	02.0	04	01.5	06	02.2	01	02.0	06	02.2	55		
II	751.7	07.3	13.2	08.3	09.3	14.8	04.5	18.8	18.16	-00.5	10	01	02.0	12	03.8	01	01.0	12	02.8	05	03.0	09	02.1	*	*	06	02.0	36		
III	760.6	06.8	15.5	09.7	10.2	16.4	04.1	22.0	21	00.4	13.10	*	*	03	02.0	*	*	13	02.3	03	02.7	21	02.2	*	*	04	02.0	49		
IV	756.9	11.1	15.6	12.0	12.7	17.5	07.4	24.9	30	02.8	24	02	03.0	08	02.5	03	02.3	10	01.9	08	02.5	10	02.5	03	02.8	05	02.8	41		
V	751.1	19.6	15.6	16.5	20.4	26.9	11.1	26.4	20	06.2	11	05	04.6	02	04.0	*	*	02	01.0	16	02.4	19	02.3	01	01.0	02	02.5	46		
VI	755.4	20.3	24.9	20.6	21.3	26.0	14.8	30.2	27	07.9	14	05	02.7	07	01.7	03	01.0	04	03.8	17	02.1	04	02.8	05	01.8	39				
VII	760.4	22.0	28.6	21.9	23.6	29.9	16.0	36.0	15	12.4	24	03	03.7	09	02.8	00	01.0	01	01.0	02	02.5	22	02.2	01	01.0	03	01.7	50		
VIII	759.8	23.6	30.3	22.4	24.6	31.5	17.8	35.7	31	03	13.6	*	02.1	05	02.4	*	*	*	01	02.0	24	02.1	01	02.0	11	02.0	48			
IX	760.5	18.2	25.7	18.5	20.2	27.0	14.8	32.6	11	06.6	28	*	*	04	03.2	05	01.4	05	01.8	08	01.1	22	02.2	02	02.9	02	03.0	42		
X	758.3	11.6	17.5	13.8	19.0	08.2	02.3	22.5	05	01.8	28	02	01.0	03	00.0	05	01.0	03	02.0	13	02.7	11	02.6	04	01.7	01	01.0	49		
XI	763.3	07.4	14.9	6.2	10.0	16.2	07.3	19.0	07	-	*	-	05	01.4	08	04.6	01	01.0	03	01.0	02	02.6	09	02.2	03	01.7	*	56		
XII	764.3	05.0	12.4	06.7	13.9	01.7	19.1	04	-	-	*	08	05.1	11	02.9	03	01.3	02	01.5	03	01.3	06	01.0	05	01.8	04	02.0	34		
GOD.	760.5	12.8	19.2	13.5	14.7	20.5	09.0	36.0	08	-	*	*	40	03.2	81	02.0	72	01.3	64	02.1	72	02.4	176	02.2	23	01.9	50	62.2	567	
$\phi = 42^{\circ}17'N \lambda = 18^{\circ}51'E$ Gr. $\Delta t_m = +1h\ 15\ min.$																														
I	766.5	06.8	12.9	07.9	08.9	13.3	04.0	17.5	21	01.7	14	*	*	04	02.4	*	*	*	20	01.6	*	*	*	*	*	*	*	*	64	
II	760.1	08.4	13.4	09.2	10.1	13.8	07.5	18.5	16	03.0	09	*	*	08	02.4	03	02.0	06	02.0	37	02.0	*	*	*	*	*	*	*	31	
III	762.1	08.6	15.0	09.7	10.8	15.2	05.0	20.0	30.25	03.5	10	*	*	04	02.0	01	02.0	07	02.3	37	02.3	*	*	*	*	*	*	56		
IV	758.2	12.2	15.8	11.9	13.0	16.5	10.6	21.5	30	07.5	23	*	*	01	02.0	04	02.2	13	02.4	28	02.0	*	*	*	*	*	*	44		
V	755.0	16.1	19.4	15.3	16.5	19.4	13.8	27.3	20	10.2	14	02	02.0	01	03.0	01	02.0	07	03.4	27	02.5	07	01.4	01	02.0	02	02.5	47		
VI	760.0	21.6	24.9	19.5	21.1	25.4	16.1	29.6	30	12.5	15	01	05.0	*	*	*	*	31	02.0	04	02.5	*	*	07	02.0	*	29			
VII	760.8	23.3	28.4	21.7	23.8	29.3	19.0	33.6	17	16.0	25.09	*	*	09	02.0	01	02.0	06	26.17	03	01.7	06	02.5	*	*	54				
VIII	760.3	24.0	30.3	23.1	25.1	31.0	20.3	35.0	21	18.2	31.14	*	*	01	02.0	02	02.5	02	01.0	24	01.9	03	02.0	03	02.3	01	03.0	57		
IX	761.1	26.3	25.9	20.0	21.6	26.6	17.6	32.0	11	12.0	28.27	*	*	*	*	*	*	04	02.8	33	02.2	06	03.3	01	03.5	*	*	45		
X	758.6	13.4	17.8	13.6	14.7	18.9	11.5	23.6	05	06.0	28	*	*	02	02.0	*	*	03	02.3	53	02.8	04	02.5	*	*	31				
XI	763.3	09.7	15.4	10.6	11.4	16.1	09.1	20.4	08	04.0	02	*	*	02	04.6	01	02.0	03	02.1	02	02.0	*	*	*	*	46				
XII	764.5	07.1	12.9	08.4	09.2	13.2	06.4	17.4	04	03.7	22	11	05.1	*	*	01	02.0	01	05.0	29	01.9	*	*	*	*	51				
GOD.	761.3	14.2	19.3	-14.2	15.5	19.9	12.2	35.0	07	01.7	41	14	04.6	20	07.4</															

Meseč	Oblažnost Nm (0-10)			Vlažnost vzdušna e _m mm	Vlažnost vzdušna U m %			Padavine R mm			Broj dana u meseču																					
	7	14	21		7	14	21	Σ mm	X mm	dat.	Tn	Tx	In	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	•	Δ	○	▲	▲	R					
	Sred. (Dien.)	Ljeto	sest.								-30.00.0	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.0	10.0	9	△	●	▲	▲	T				
BR. ST.241																																
GRADIVO																																
I	4.5	5.3	3.3	4.4	-	04.9	88	86	90	86	40	154	059.6	02	.	.	24	11	06	06	06	04	06	01	01			
II	7.1	6.1	4.9	6.1	-	05.3	90	82	93	88	64	526	139.2	04	.	.	12	01	03	08	13	03	03	.	.			
III	4.8	4.8	3.2	4.3	-	05.9	85	74	90	83	14	268	108.4	06	.	.	20	03	15	69	07	07	05	07	05			
IV	5.6	7.5	5.2	6.1	-	06.7	87	77	91	85	52	192	052.6	18	.	.	06	03	11	16	14	03	16	.	.			
V	4.5	5.3	4.2	5.1	-	08.6	83	75	87	82	49	206	069.2	05	07	69	12	09	05	12	.	.			
VI	4.6	5.5	3.2	4.4	-	10.3	76	70	79	75	47	071	038.2	12	.	.	05	04	03	08	07	02	08	.	01			
VII	2.0	3.0	1.2	2.0	-	12.9	81	65	80	75	39	011	011.0	08	.	.	24	10	.	.	.	20	01	02	01	01	02	.	.			
VIII	1.5	3.7	1.2	2.1	-	12.5	71	53	77	67	31	053	023.6	30	.	.	28	17	.	.	.	20	05	04	02	05	01	.	.			
IX	3.9	4.6	2.9	3.8	-	10.5	82	62	83	76	28	399	084.6	22	.	.	01	16	.	.	.	11	04	09	09	07	05	.	.			
X	6.5	6.5	5.4	6.2	-	07.2	81	77	88	85	45	933	177.4	24	.	.	09	06	11	19	18	16	15	01	01			
XI	5.6	6.8	4.0	4.8	-	05.6	92	74	91	86	41	198	090.6	26	.	.	19	09	08	13	07	04	12	01	04			
XII	4.9	4.5	2.6	4.0	-	04.5	90	71	92	84	40	096	045.6	13	.	.	25	03	02	10	05	05	04	02	01			
GOD.	4.6	5.2	3.4	4.4	-	07.9	84	72	86	81	14	3107	139.2	07	.	.	116	73	27	.	.	07	02	119	75	115	98	59	114	14	04	
BR. ST.242																																
TIVAT																																
I	5.1	5.0	3.0	4.3	-	05.9	85	63	84	77	29	056	011.6	18	.	.	10	10	06	10	09	02	10	.	.			
II	7.3	6.7	5.5	6.5	-	06.7	80	61	85	75	31	202	050.4	07	.	.	01	04	11	14	11	07	14	.	.			
III	4.9	5.3	3.3	4.5	-	07.7	91	62	93	82	46	148	049.5	06	08	07	09	08	04	05	.	.			
IV	6.0	7.0	6.3	6.4	-	08.4	81	64	86	77	34	138	028.2	17	01	01	01	11	16	13	06	16			
V	5.1	5.5	5.2	5.2	-	10.9	81	63	89	78	33	295	101.0	02	.	.	04	01	07	08	18	14	08	18	02	05		
VI	4.3	4.7	3.5	4.2	-	12.5	71	51	75	65	34	047	025.1	20	.	.	24	01	01	01	01	07	02	10	07	01	10	.	.			
VII	1.8	2.2	1.4	1.8	-	13.3	67	43	72	61	26	004	003.7	21	.	.	30	17	01	.	.	20	05	01	03	01	03	.	C2			
VIII	1.9	2.7	1.3	2.0	-	14.0	66	42	73	60	24	028	026.2	24	.	.	31	20	03	.	.	21	01	04	02	01	04	.	01			
IX	3.8	4.1	2.5	3.6	-	13.9	86	57	89	77	26	447	165.7	23	.	.	23	05	.	.	.	01	01	11	02	09	09	07	09			
X	7.2	6.4	5.8	6.5	-	05.7	92	62	90	81	34	494	177.2	08	01	03	12	21	16	13	21	01			
XI	5.2	5.7	4.2	5.0	-	07.5	88	64	89	80	27	047	006.2	28	07	09	14	12	14	14	.	01			
XII	4.5	4.9	3.1	4.2	-	05.9	82	58	82	74	30	072	057.2	13	03	01	07	03	04	02	04	02			
GOD.	4.8	5.0	3.6	4.5	-	09.7	80	57	83	73	24	1978	165.7	231X	.	.	11	112	43	05	09	04	06	106	72	132	107	51	132	.	.	
BR. ST.243																																
BUDVA																																
I	5.4	6.1	3.5	5.0	-	129.1	06.8	82	68	83	34	049	009.6	18	10	07	13	06	13	12	.	.			
II	7.5	6.9	4.9	6.4	-	105.1	07.0	77	67	80	35	177	042.1	07	02	11	12	10	08	12	.	01			
III	5.4	4.3	3.7	4.5	-	186.6	08.1	63	73	85	40	116	044.1	06	10	09	08	09	03	08	.	01			
IV	6.4	7.5	5.6	6.5	-	125.0	05.3	73	68	77	36	188	045.7	17	02	11	15	12	06	15	.	02			
V	5.7	6.6	5.0	5.6	-	184.1	11.0	77	71	83	36	214	046.6	02	.	.	02	01	07	17	16	07	17	.	02			
VI	3.9	4.2	1.5	3.2	-	974.8	15.8	71	66	77	51	022	009.8	17	.	.	24	12	01	67	55	07	07	.	01			
VII	1.7	2.6	1.5	1.9	-	131.6	19.7	70	61	73	63	319	010.0	22	.	.	30	16	13	.	.	21	02	02	02	01	02	.	01			
VIII	3.1	2.8	2.0	2.7	-	284.6	16.0	67	57	71	65	28	011.0	06.0	.	.	31	20	24	.	.	18	01	04	02	04	02	.	02			
IX	5.0	5.1	2.8	4.3	-	218.3	15.5	82	71	82	78	33	434	187.9	23	.	.	21	05	01	.	.	09	05	09	08	07	09	.	10		
X	7.5	6.7	6.4	6.9	-	183.3	10.7	88	72	89	83	30	396	067.0	16	03	14	19	17	12	19	.	04			
XI	5.3	5.6	3.5	4.5	-	131.6	08.8	68	76	88	42	082	017.7	26	.	.	18	10	08	14	11	03	14	.	01			
XII	5.1	4.7	3.4	4.4	-	130.6	07.0	82	73	78	78	26	052	025.5	13	03	02	10	05	08	05	01	01			
GOD.	5.2	5.1	3.6	4.7	-	2236.7	10.7	78	68	90	75	26	1760	187.9	07II	.	.	104	62	24	.	.	09	06	90	96	153	123	72	152	13	10
BR. ST.244																																
CETINJE																																
I	4.9	5.6	3.1	4.5	-	04.4	90	68	87	82	34	118	038.6	11	.	.	24	11	06	11	10	04	11	02	03			
II	7.2	6.4	5.2	6.4	-	04.9	93	64	85	80	38	481	204.9	07	.	.	12	04	11	16	12	07	16	01	01			
III	5.5	5.3	3.7	4.8	-	05.2	91	54	80	75	23	228	104.5	06	.	.	12	09	09	07	05	09	04	01	02			
IV	6.5	8.1	6.4	7.0	-	06.1	86	65	80	77	26	250	061.2	17	.	.	03	02	15	21	16	08	21	01	01			
V	5.0	6.6	5.1	5.5	-	08.2	66	44	85	78	35	374	092.1	02	05	02	22	19	10	22	.	05			
VI	4.7	5.8	3.3	4.6	-	10.4	79	59	85	74	41	098	031.8	20	04	03	13</td								

Mjesec	Vardulski Prstisak Pm. num.	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Fm (0-12)																											
		Tm				Max		Min		Max		Min		Dat.		Max		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (dies)	Max	Min	Max	Min	Dat.	Max	Min	Dat.	Max	Min	Dat.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.									
$\lambda = 42^{\circ}14' N \lambda = 19^{\circ}05' E$ Gr. $\Delta G = +1h\ 16\ min.$																									VIRPAZAR		BR. ST.246												
I	-	02.2	09.2	04.2	04.9	00.2	14.0	04	-03.0	29	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*									
II	-	05.0	10.6	06.3	07.1	11.2	03.0	16.0	17	-01.0	28	03	01.0	27	02.6	*	*	*	*	10	02.2	C2	C1.0	30	01.6	06	01.0	*	*	06									
III	-	06.4	14.7	08.6	09.7	15.0	03.9	26.0	22	-00.5	01	*	*	21	01.1	*	*	03	01.7	02	C1.0	37	01.5	15	01.1	06	C1.3	09											
IV	-	09.0	15.5	11.2	11.7	15.9	05.5	19.0	28.27	02.0	20	*	*	08	02.0	02	01.0	03	01.3	03	C1.0	50	01.5	18	01.4	01	C1.0	05											
V	-	14.5	20.0	15.0	16.1	20.4	10.2	26.4	30.27	06.5	16	*	*	12	02.2	*	*	13	02.4	01	C1.0	49	01.8	07	01.3	04	C1.0	07											
VI	-	22.8	26.7	22.1	23.4	27.0	14.7	30.0	29	11.5	04	*	*	27	02.6	*	*	01	02.0	02	C1.0	39	02.3	14	01.0	03	C1.3	09											
VII	-	24.5	31.0	23.9	25.9	31.5	15.3	40.0	17.16	12.0	23	*	*	33	02.6	*	*	02	03.0	02	C1.0	28	01.4	13	01.1	*	*	15											
VIII	-	25.9	34.5	26.2	28.4	34.8	16.5	35.8	09	13.5	30	02	C1.0	37	01.8	*	*	01	02.0	07	C1.0	19	01.2	04	01.0	03	C1.0	21											
IX	-	21.4	27.1	20.3	22.3	27.5	11.6	33.6	04	06.5	28	*	*	18	01.8	*	*	05	03.0	C5	C1.0	33	02.2	09	01.1	05	C1.6	15											
X	-	10.0	14.6	10.8	11.8	15.0	06.6	20.0	16	01.5	28	*	*	11	02.0	*	*	11	02.0	03	C2.3	46	02.8	05	01.0	11	C1.8	06											
XI	-	05.3	12.7	06.6	07.6	12.9	03.0	16.6	13	01.0	30	02	C1.0	19	02.0	01	01.0	01	01.8	C3	C1.0	30	01.8	14	01.0	05	G3.0	11											
XII	-	01.6	10.4	03.8	04.9	10.6	00.0	13.0	10.02	-02.5	24	01	C3.6	33	02.9	*	*	06	01.5	04	C1.0	21	01.3	08	01.0	06	C1.2	10											
GOD.	-	12.5	18.9	13.3	14.5	19.3	07.6	40.0	F7K-VII	-03.0	29	*	11	02.1	241	02.3	03	01.0	60	02.1	34	01.1	301	01.6	113	01.1	44	C1.6	114										
$\lambda = 42^{\circ}06' N \lambda = 19^{\circ}06' E$ Gr. $\Delta G = +1h\ 16\ min.$																									RAR		BR. ST.247												
I	756.3	C7.4	12.3	07.7	08.8	13.2	03.9	16.9	01	-01.3	15	08	02.4	49	02.4	16	01.4	04	01.8	06	02.0	06	01.8	08	01.9	05	C2.4	01											
II	756.6	09.1	13.9	09.9	10.7	14.9	06.1	20.2	18	01.2	10	04	C5.2	38	01.6	12	C2.0	11	03.5	05	02.0	06	02.4	05	02.2	03	C3.0	*											
III	766.9	08.9	14.8	09.9	10.9	15.8	05.8	20.2	29	01.2	02	03	C7.0	42	02.0	19	01.7	*	03	02.7	07	01.9	16	01.1	03	01.7	*												
IV	757.2	12.9	15.9	12.4	13.4	17.7	08.7	26.2	30	04.0	21	11	C6.6	37	02.2	15	01.7	07	02.6	03	02.7	04	02.0	15	0.5	01	C4.0	02											
V	756.7	16.1	18.8	15.1	16.3	19.8	11.5	25.8	20	07.9	11	07	C2.1	36	01.7	68	01.5	05	03.4	10	02.7	10	02.1	14	02.4	*	*	03											
VI	756.9	20.6	23.5	19.3	20.7	24.7	15.2	29.6	27	09.1	14	05	C3.2	28	02.0	13	01.5	07	01.6	06	03.0	10	02.0	14	0.9	05	C2.6	02											
VII	766.0	22.8	26.2	21.0	22.0	27.4	16.6	34.7	18	12.4	10	*	*	28	01.7	26	01.5	02	03.3	C9	01.8	16	0.1	05	C2.0	04													
VIII	759.5	24.3	27.4	22.5	24.2	29.1	18.6	32.3	23	15.3	31	03	04.0	28	02.2	22	07.0	C2	01.0	03	01.7	08	02.1	21	02.3	05	C1.6	01											
IX	766.1	20.8	24.7	20.0	21.1	26.1	16.0	31.4	11	10.2	27	03	03.0	26	02.3	23	01.7	06	02.3	06	03.0	05	01.8	16	0.7	05	C2.8	*											
X	756.1	13.9	16.3	14.6	15.4	19.4	10.4	23.7	12	03.2	28	02	01.5	19	02.6	23	01.8	04	02.2	16	C3.6	13	04.0	15	0.9	01	C4.0	*											
XI	762.8	05.8	15.1	11.0	11.7	16.2	06.9	19.8	06	03.8	30	04	01.8	36	02.6	22	01.5	03	03.0	10	03.8	04	01.8	09	01.9	01	C3.0	01											
XII	763.7	07.1	12.3	08.1	08.9	13.2	03.8	17.8	04	01.1	23,21	05	C3.0	30	03.8	27	02.1	03	02.0	07	02.9	08	01.5	08	01.6	03	C2.3	02											
GOD.	766.4	14.5	18.6	14.3	15.4	19.8	10.3	34.7	48	07	-01.3	51	05	C2.7	382	02.4	226	01.8	54	02.5	78	02.9	90	02.2	157	02.5	37	C2.5	16										
$\lambda = 42^{\circ}26' N \lambda = 19^{\circ}17' E$ Gr. $\Delta G = +1h\ 17\ min.$																									TITCGRAD		BR. ST.248												
I	762.0	C3.9	10.8	05.6	06.5	11.4	02.8	15.0	04	-02.1	15	03	02.3	16	03.9	C3	04.0	*	*	11	01.9	06	01.8	01	C1.0	*	*	53											
II	755.6	06.6	12.6	08.0	08.8	13.0	05.4	19.4	16	-01.4	21	07	C2.1	19	04.7	C4	C1.2	02	02.0	11	03.2	06	02.3	03	02.7	*	*	C2.0	31										
III	757.3	07.6	16.6	10.6	11.4	17.3	06.4	26.0	22	01.1	02	04	C2.0	11	04.0	C2	C1.5	*	*	13	02.5	14	02.7	*	*	01	03.0	48											
IV	752.6	11.0	16.4	12.2	12.9	18.2	09.0	24.1	30	05.3	23	11	C3.0	27	03.1	C1	05.0	03	02.3	12	03.2	05	03.4	04	02.5	*	*	27											
V	754.8	15.0	20.1	15.6	16.6	21.6	12.1	28.2	20	05.3	11	13	03.2	08	02.9	02	02.5	04	04.0	14	04.5	09	03.2	01	02.0	03	C2.0	39											
VI	754.9	19.9	25.6	20.5	21.7	27.0	16.5	31.6	27	05.5	12	11	04.5	18	03.4	C2	02.5	03	02.7	17	03.8	12	03.2	02	01.5	03	C1.3	27											
VII	759.9	23.2	31.1	24.7	25.9	32.4	19.9	38.9	16	15.0	24	23	03.1	22	03.4	C1	03.0	01	03.0	15	03.6	09	03.1	02	02.0	01	C2.0	19											
VIII	755.5	24.9	32.9	26.2	27.5	33.9	22.6	36.6	05	17.0	13	27	03.3	01	03.6	18	03.6	01	07.0	27	03.6	01	03.6	02	03.0	*	*	24											
IX	756.4	15.5	26.7	21.0	22.0	28.2	17.8	35.6	14	07.5	27	14																											

Mesec	Oblačnost Nm (0-10)			Temperatura hod. (t) (°C)	Vlažnost vazduha U m t	Padavine R mm		Broj dana na sat:																										
	7	14	21			mm	7	14	21	28	Min	Σ	Max	Cat.	Tn	Tx	In	Tx	Tx	Tn	F (0-12)	Nm (0-10)	R mm	•	*	•	Δ	Δ	▲	▲	R	■		
	≡	≤	≤	≥	≥	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV	IV						
BR. ST.246 VIRPAZAR																																		
I 5.9 5.6 5.4 4.4 5.4 -	-	04.9	89	57	79	75	22	101	025.6	06	.	.	16	.	.	.	10	09	11	11	06	04	11	01	01				
II 7.4 7.4 5.8 6.9 -	-	05.9	87	63	82	78	38	271	125.0	07	.	.	01	.	.	.	01	04	15	08	06	08	01	02					
III 5.5 5.6 5.2 5.1 -	-	06.4	86	52	76	71	24	110	028.6	05	.	.	01	01	.	.	14	11	07	07	05	07	01	02					
IV 7.0 7.2 7.1 7.1 -	-	08.1	66	61	81	78	26	204	055.4	18	01	03	14	13	12	06	13	02	.				
V 6.2 6.6 5.8 6.2 -	-	11.5	86	72	85	81	50	407	096.4	02	.	.	01	.	.	.	02	02	03	14	17	17	11	17	01	.			
VI 3.0 4.0 2.4 3.2 -	-	17.3	75	74	82	77	37	039	014.0	11	.	.	26	01	.	.	02	03	13	01	06	06	02	06	01	.			
VII 1.3 2.4 1.1 1.6 -	-	17.6	72	58	80	70	32	019	010.0	19	.	.	29	21	03	01	21	02	03	01	02	01	02	01	.				
VIII 1.1 1.7 0.9 1.2 -	-	18.3	71	48	71	63	29	035	025.6	29	.	.	31	27	.	.	25	01	03	03	01	03	01	.					
IX 4.2 4.3 3.4 4.0 -	-	15.7	77	62	82	73	48	546	130.6	26	.	.	20	15	.	.	03	01	15	06	08	08	08	08	01	.			
X 8.6 8.6 8.5 8.6 -	-	08.6	85	71	87	81	51	746	118.4	08	.	.	01	.	.	.	04	02	07	20	23	23	17	23	01	.			
XI 4.5 5.8 3.9 4.8 -	-	05.9	88	50	85	74	31	155	070.4	26	.	.	01	.	.	.	02	01	06	05	07	07	02	07	01	11			
XII 5.3 4.9 3.8 4.7 -	-	04.2	86	39	76	67	23	069	025.6	13	.	.	14	.	.	.	02	02	09	08	07	07	03	07	01	01			
GOD. 5.0 5.4 4.2 4.9 -	-	10.4	82	55	80	74	22	2724	130.6	26	X	.	.	32	115	64	03	19	12	123	104	113	111	66	113	01	06	.	21
BR. ST.247 BAR																																		
I 5.6 6.0 3.6 5.1 -	142.2	05.5	70	60	76	69	37	052	017.6	18	.	.	01	.	.	.	01	07	07	11	10	01	11	04	.				
II 7.2 6.5 5.2 6.4 -	127.3	06.0	70	66	73	67	33	125	037.5	07	.	.	01	.	.	.	04	06	11	12	10	05	12	05	.				
III 5.1 5.5 4.2 5.3 -	195.6	07.4	77	65	78	74	45	057	020.5	06	.	.	01	.	.	.	06	05	03	05	03	08	02	01					
IV 6.6 6.7 7.2 6.9 -	163.5	08.0	67	64	74	68	23	124	021.7	19	.	.	01	.	.	.	04	02	14	13	11	05	13	01	06				
V 5.8 5.5 5.1 5.8 -	223.9	10.8	74	72	82	76	44	270	066.2	02	.	.	01	.	.	.	02	06	12	16	15	04	16	04	.				
VI 4.3 3.2 2.5 3.5 -	327.5	12.5	68	62	70	66	38	026	009.6	13	.	.	14	01	.	.	02	01	16	02	07	03	06	04	.				
VII 1.9 2.0 1.2 1.7 -	375.9	14.1	60	64	70	65	30	009	006.4	20	.	.	25	03	01	04	03	21	02	02	02	02	02	01	.				
VIII 2.1 2.4 1.7 2.1 -	330.7	14.4	57	62	66	72	30	016	014.0	29	.	.	30	13	04	01	20	03	02	01	03	03	05	.					
IX 4.7 4.1 3.6 3.9 -	237.2	14.1	72	68	76	72	31	275	064.5	24	.	.	21	01	01	01	10	06	10	04	09	09	08	09	06	.			
X 7.2 6.6 5.9 6.4 -	157.3	09.7	76	62	76	72	39	342	087.5	16	.	.	01	.	.	.	18	05	04	11	21	17	07	21	03	13			
XI 4.7 5.6 4.3 4.9 -	141.3	07.6	71	65	77	73	36	070	016.6	30	.	.	06	06	07	08	04	19	09	03	14	14	05	.					
XII 4.6 5.3 3.6 4.5 -	149.5	05.8	70	59	69	66	33	056	024.6	13	.	.	01	.	.	.	08	05	07	05	04	07	01	08	01	02	01		
GOD. 5.1 5.5 4.3 5.0 -	2558.6	06.5	72	50	70	64	15	1681	097.0	16	X	.	.	12	114	64	55	171	46	84	131	107	51	130	01	46	04		
BR. ST.248 KOLASIN																																		
I 5.2 5.5 3.5 4.7 -	154.2	05.5	83	61	81	75	36	047	017.4	11	.	.	05	.	.	.	10	09	06	01	11	08	01	11	03	.			
II 7.0 6.5 5.9 6.5 -	126.9	06.0	76	57	77	70	31	152	052.6	07	.	.	01	.	.	.	14	04	06	12	11	10	04	11	01	.			
III 5.5 5.2 4.1 4.9 -	107.0	06.9	81	51	75	69	28	048	024.3	06	.	.	02	.	.	.	05	09	08	06	06	02	06	03	06				
IV 6.4 7.4 5.5 6.6 -	159.3	07.5	73	56	73	67	31	151	040.0	17	.	.	01	.	.	.	16	02	02	12	16	11	06	16	02	.			
V 5.7 6.5 6.1 6.1 -	219.1	09.7	74	58	75	69	32	188	033.0	02	.	.	08	01	.	.	13	01	04	11	19	17	07	19	07	01			
VI 4.7 5.5 3.4 4.5 -	275.7	11.8	68	48	65	61	33	044	010.7	12	.	.	24	02	04	04	16	02	04	01	11	09	01	11	04	.			
VII 2.3 2.3 2.4 2.5 -	368.7	12.0	54	36	53	48	25	011	006.4	08	.	.	29	22	14	16	07	15	02	04	02	04	02	04	01	01			
VIII 2.5 4.0 3.4 3.0 -	335.6	11.7	49	31	50	43	15	016	007.2	29	.	.	31	26	24	21	06	12	01	04	03	04	04	05	05	.			
IX 4.2 4.2 3.1 3.8 -	247.9	12.0	69	47	68	62	29	249	061.6	26	.	.	20	14	13	21	04	11	04	08	08	07	09	02	.				
X 7.2 7.1 6.3 6.8 -	157.1	08.3	79	56	80	71	29	533	097.0	16	.	.	01	.	.	.	16	06	02	13	20	18	15	70	01	12			
XI 4.8 5.5 5.0 5.6 -	150.4	06.5	62	55	61	73	30	157	062.3	26	.	.	16	02	04	04	01	11	05	10	06	01	10	03	03				
XII 4.9 5.1 4.1 4.7 -	153.9	04.0	76	48	70	65	30	075	024.2	13	.	.	07	01	01	01	14	08	05	04	08	06	03	07	02	.			
GOD. 5.1 5.5 4.3 5.0 -	2558.6	06.5	72	50	70	64	15	1681	097.0	16	X	.																						

Mesec	Vazdušni pritisak pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Br. (1-12)																
		Tm			Sred. (Dnes)	Max	Min	Dat.	Max	Min	Dat.	U	NE	E	SE	S	SW	N	NW	C								
		7	14	21								E.	J.	E.	J.	E.	J.	E.	J.	E.	J.							
$\varphi = 41^{\circ}55'N \lambda = 19^{\circ}13'E$ Gr. AG = + 1h 17 min.																												
I	756.9	06.1	10.7	07.6	08.0	11.5	04.8	15.6	21	06.9	14	.	.	12	02.4	72	02.5	02	01.5	.	.	03	01.7	02	C1.5	02		
II	750.6	07.7	12.5	09.2	09.7	13.4	06.3	18.6	16	02.2	28	.	.	19	02.5	46	07.5	05	02.8	06	02.1	03	02.7	02	C3.5	01		
III	752.7	09.3	15.4	10.8	11.6	16.0	07.8	23.2	25	02.4	09	.	.	71	02.5	37	02.4	05	02.6	02	02.5	02	C2.0	09	02.7	08	C2.4	09
IV	749.4	11.6	15.8	12.0	12.9	17.0	09.2	24.6	30	05.6	20	01	03.0	17	02.2	33	02.2	04	02.0	05	01.8	06	02.3	12	02.8	09	C2.6	03
V	750.7	15.1	19.0	15.2	16.2	19.9	12.1	24.4	21.20	06.8	01	01	02.0	12	02.2	20	01.8	01	02.0	09	03.4	02	02.0	18	03.1	17	C2.8	04
VI	750.9	12.6	24.3	19.3	20.6	25.3	16.3	26.8	27	16.0	01	02.0	16	01.8	24	02.0	05	01.8	03	02.0	05	03.4	09	02.6	23	03.1	03	
VII	751.8	22.6	26.7	22.6	24.1	30.1	17.8	36.6	17	14.6	22.08	01	02.0	19	02.0	29	01.9	01	02.0	02	01.5	02	01.0	07	02.9	28	C3.3	04
VIII	751.5	24.2	31.1	24.3	26.0	32.1	20.7	37.3	04	16.4	29.28	.	.	10	02.2	26	02.0	03	01.3	01	02.0	02	02.5	13	02.8	22	03.1	06
IX	752.1	20.4	25.8	21.4	22.2	27.1	17.6	31.4	16	11.2	27	.	.	25	02.1	27	02.0	03	02.0	06	03.5	06	03.0	12	02.4	09	C3.6	02
X	749.7	13.1	16.0	14.8	15.2	19.1	10.9	23.2	05	04.9	28	01	01.0	17	02.1	23	02.1	03	02.3	10	04.2	03	05.0	19	04.1	13	C2.8	04
XI	754.4	05.4	14.4	11.7	15.5	15.7	07.5	18.4	15	04.3	02	.	.	20	02.3	48	02.2	01	02.0	08	02.6	02	03.5	05	03.4	06	02.7	.
XII	755.2	06.2	11.4	08.0	08.4	12.4	04.5	17.3	04	01.9	25.21	01	02.0	26	02.3	51	02.3	02	01.0	06	02.8	02	02.0	01	02.0	04	02.5	.
GOD.	752.2	13.8	16.9	14.7	15.6	20.0	11.4	37.3	08	06.9	41.1	08	01.8	224	02.2	436	02.3	35	02.1	58	03.0	34	02.7	111	03.0	143	C3.0	34
SR MAKEDONIJA																												
$\varphi = 42^{\circ}01'N \lambda = 20^{\circ}53'E$ Gr. AG = + 1h 24 min.																												
I	-	-04.4	-02.0	-04.6	-03.9	00.4	-07.0	06.6	23	-12.0	13	03	03.7	01	01.0	.	.	02	02.0	02	02.0	05	01.8	01	04.0	38	C3.2	41
II	-	-03.2	-01.1	-03.1	-02.6	01.0	-05.1	06.5	11	-12.6	28	01	03.0	11	02.7	11	04.2	.	.	19	C2.6	42
III	-	-01.2	01.8	-00.3	00.0	03.4	-02.9	11.5	27	-13.0	01	01	02.0	.	.	06	01.0	07	02.1	11	04.2	03	02.0	10	C1.7	55		
IV	-	-30.3	01.8	-00.2	00.5	03.6	-02.5	08.8	20	-06.9	20	02	02.5	01	02.0	02	01.5	11	02.2	08	02.2	06	02.2	05	03.4	18	02.7	37
V	-	04.8	06.8	05.1	05.4	06.6	02.0	15.2	31	-02.0	10	03	02.7	.	.	02	02.0	13	01.9	06	02.8	05	02.6	04	04.5	27	C2.5	34
VI	-	04.9	11.8	09.6	10.2	13.5	06.4	19.8	27	-00.2	13	.	03	01.3	03	01.0	12	01.9	03	03.3	01	01.0	05	04.4	26	C3.2	36	
VII	-	13.3	14.9	12.2	13.2	16.4	09.1	24.5	17	01.6	08	04	02.8	01	04.0	.	.	13	01.5	02	02.0	05	01.6	23	02.4	40		
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	10.2	12.6	10.3	10.8	13.9	06.9	21.5	04	-00.6	27	01	01.0	01	01.3	05	01.4	15	01.5	10	01.6	07	02.1	01	05.0	07	C2.7	42
X	-	04.0	06.1	03.6	04.3	07.7	06.9	14.0	04	-07.5	28	01	02.0	02	03.0	.	.	11	01.8	12	03.2	18	03.6	05	04.6	08	02.8	36
XI	-	-00.2	02.5	00.4	00.6	04.7	-01.7	11.7	16	-0.6	02	.	01	03.0	.	.	01	01.0	01	04.0	06	03.0	04	03.8	17	01.9	40	
XII	-	-02.1	-00.5	-02.1	-01.7	02.1	-04.9	10.5	24	-16.4	07	03	02.7	02	03.5	.	.	01	02.0	03	02.3	.	05	04.6	42	02.8	37	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
$\varphi = 12^{\circ}00'N \lambda = 20^{\circ}58'E$ Gr. AG = + 1h 24 min.																												
I	-	-01.5	C3.5	00.5	00.7	04.6	-02.1	12.0	20	-08.0	16	02	C1.0	C2	06.0	C1	01.0	C3	01.7	03	01.0	04	01.5	.	.	02	C2.5	7
II	-	01.5	07.0	04.3	04.3	08.3	01.1	13.5	11	-04.5	02.01	03	01.3	C9	02.0	C2	01.0	.	04	C1.2	03	01.7	01.0	17
III	-	03.2	11.6	07.9	07.6	12.9	02.8	23.5	23	-03.5	02	04	01.5	06	01.2	C1	01.0	02	01.0	01	01.0	01	01.0	01	01.0	01	01.0	77
IV	-	05.7	13.0	09.4	09.4	14.2	04.6	20.0	29	-06.5	10	07	01.9	09	01.2	C6	01.3	03	01.7	04	02.2	02	02.5	01	04.0	.	58	
V	-	10.3	17.4	13.1	13.5	19.3	06.0	25.5	31	02.5	11	11	01.5	05	01.0	.	.	02	01.0	02	02.0	06	02.7	01	01.0	01	01.0	65
VI	-	15.2	22.9	17.6	18.4	24.4	12.0	30.0	29	06.0	13	05	01.6	01	01.0	C1	01.0	02	03.0	05	02.2	06	03.2	09	01.0	27		
VII	-	16.1	27.0	20.4	21.0	28.3	12.6	35.0	17	06.5	10	17	01.9	08	01.4	.	.	03	01.3	04	02.2	07	01.5	61	01.0	02	C3.5	56
VIII	-	15.6	27.9	21.1	21.4	28.9	13.5	34.5	05	05.5	14	08	02.4	04	01.8	C6	01.0	05	01.2	02	02.5	01	01.0	04	01.2	61		
IX	-	11.5	23.2	15.6	16.5	24.0	10.2	36.0	04	01.6	28	09	01.6	04	01.5	.	.	01	01.0	01	03.0	.	.	.	01	C1.0	74	
X	-	C6.7	16.2	10.1	10.8	17.1	05.4	22.5	08	-03.8	28	07	01.6	03	01.3	C2	01.0	.	06	03.7	07	02.9	.	.	03	01.7	65	
XI	-	02.4	09.0	04.9	05.3	10.2	01.8	15.5	29	-01.5	30.15	01	02.0	03	01.0	C2	01.0	.	01	02.0	02	01.0	.	.	.	03	01.0	77
XII	-	-00.8	05.0	01.1	01.6	06.4	-01.8	12.0	04	-06.0	25	04	02.0	04	01.5	C1	01.0	02	04	01								

Meseč	Oblačnost Nm (0-10)				Aerosolacija Ljuljati Ljuljati sati	Vlažnost vazduha				Padavine R mm		Projekcija dana na sat																	
	7	14	21	Sred. (Dnev.)		e mm	U m s ⁻¹	m s ⁻¹	%	R mm	Tn	Tx	Tn	Tx	Tn	Tx	F(0-12)	Nm(0-10)	R mm	●	*	●	▲	▲	▲	▲	■	■	
	7	14	21	Sred. (Dnev.)		mm	7	14	21	%	2	8	2	8	2	8	0-10.0	0.0-25.0	0.0-20.0	6	8	2.0	8.0	0.1	1.0	0.0	1.0	0.0	1.0
BR. ST.251																													
I	5.2	5.7	4.1	5.0	-	150.8	05.0	65	55	63	61	25	079	027.3	0%	-	-	-	-	-	C1	05	09	11	11	02	11	-	-
II	7.0	6.0	4.7	5.9	-	128.3	05.8	71	54	67	64	28	195	036.2	07	-	-	-	-	-	C2	02	16	12	11	05	12	-	-
III	5.5	4.8	4.3	4.9	-	184.0	06.5	75	59	69	67	23	090	036.4	06	-	-	-	-	-	C3	09	09	08	07	03	09	-	-
IV	6.9	6.8	4.3	6.7	-	166.6	06.2	67	76	73	73	35	159	024.2	17	-	-	-	-	-	C4	01	02	12	15	14	07	15	-
V	5.8	5.7	6.4	6.0	-	217.6	10.4	77	66	78	74	43	159	036.4	0%	-	-	-	-	-	C5	04	10	15	12	05	15	-	-
VI	4.2	3.7	2.9	3.6	-	290.1	13.0	79	60	71	57	37	060	017.2	17	-	-	-	-	-	C6	01	10	01	08	07	02	08	-
VII	1.3	1.6	1.2	1.4	-	303.3	12.8	61	45	62	56	21	016	017.8	22	-	-	-	-	-	C7	02	03	03	01	03	02	-	-
VIII	1.6	2.2	1.6	1.9	-	13.4	56	43	60	53	49	19	007	004.7	29	-	-	-	-	-	C8	01	20	02	01	02	02	-	-
IX	3.6	3.6	3.1	3.5	-	239.4	15.4	71	62	71	68	25	187	044.8	27	-	-	-	-	-	C9	05	11	C10	07	08	05	-	-
X	7.0	6.3	5.5	6.2	-	164.9	05.6	82	64	73	73	23	094	055.1	01	-	-	-	-	-	C11	06	11	19	10	15	05	-	-
XI	4.7	5.6	4.3	4.9	-	142.8	07.6	79	67	75	73	46	097	042.2	27	-	-	-	-	-	C12	06	07	11	03	02	11	-	-
XII	4.4	4.8	3.6	4.2	-	157.1	05.4	69	58	64	64	28	067	026.4	13	-	-	-	-	-	C13	06	08	03	04	03	03	-	-
GOD.	4.8	4.7	4.0	4.5	-	09.3	71	58	69	66	19	146	055.1	0%	-	-	-	-	-	101	48	33	35	16	115	79	120	107	
BR. ST.252																													
PEREĆA SAPKA																													
I	5.5	5.3	3.9	4.9	-	04.5	73	70	74	72	14	035	010.1	24	05	15	31	-	-	C4	05	10	06	01	02	11	-	-	
II	6.1	7.2	6.2	6.5	-	03.1	78	51	53	51	29	056	018.4	15	02	11	27	-	-	C5	06	14	15	10	05	12	-	-	
III	5.0	6.1	5.7	5.6	-	02.4	75	79	76	75	33	061	024.2	17	02	11	15	-	-	C6	11	14	16	11	01	02	14	02	
IV	6.3	7.6	4.5	6.1	-	03.7	78	77	76	77	49	066	011.9	17	01	26	-	-	-	C7	02	17	04	01	01	01	04	03	
V	3.0	7.0	4.5	5.5	-	05.4	75	74	76	74	44	157	021.3	16	-	-	05	-	-	C8	02	19	17	05	15	13	02	-	
VI	4.6	5.8	3.9	4.6	-	06.4	76	67	66	68	25	073	014.9	20	-	-	01	-	-	C9	06	12	10	04	11	03	02	-	
VII	3.7	4.1	2.6	2.6	-	07.3	60	64	67	64	20	030	004.4	01	-	-	-	-	-	C10	15	02	04	01	02	02	03	-	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	3.2	4.7	1.9	3.3	-	06.1	61	70	69	69	26	069	046.0	17	-	-	01	-	-	C11	12	03	08	02	08	01	-	-	
X	5.2	5.4	5.1	5.2	-	04.5	67	71	71	69	21	159	026.1	14	-	-	01	-	-	C12	07	20	17	15	16	05	02	-	
XI	3.7	4.5	3.9	4.0	-	03.4	69	71	69	70	20	053	017.1	17	-	-	04	-	-	C13	11	05	10	02	02	10	01	-	
XII	4.5	4.6	4.7	4.6	-	02.6	65	65	65	65	15	017	005.9	15	02	12	30	-	-	C14	01	10	07	05	01	04	01	-	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
BR. ST.253																													
TETOVO																													
I	6.5	7.0	5.7	6.4	-	04.1	50	76	88	75	45	068	011.5	24	-	-	20	-	-	C1	01	06	14	13	02	06	01	-	
II	7.3	7.6	7.0	7.3	-	04.9	50	69	80	79	36	070	025.0	05	-	-	10	-	-	C2	05	19	11	11	02	05	06	-	
III	6.1	6.6	5.6	6.0	-	05.5	56	76	77	72	12	075	016.0	09	-	-	03	-	-	C3	05	16	16	02	05	02	02	-	
IV	7.7	6.2	7.2	7.7	-	06.1	87	59	73	73	19	063	017.0	17	-	-	01	-	-	C4	16	15	15	10	05	15	01	-	
V	6.5	7.9	5.8	6.9	-	08.1	57	51	71	71	26	071	024.6	16	-	-	01	-	-	C5	01	10	16	11	07	16	04	-	
VI	5.6	7.5	6.1	6.4	-	10.4	60	51	69	67	11	064	026.1	20	-	-	01	-	-	C6	01	10	10	05	01	10	06	-	
VII	3.2	3.8	3.4	3.4	-	10.3	77	57	58	58	26	072	024.5	01	-	-	26	-	-	C7	07	16	15	04	03	02	03	-	
VIII	3.1	4.5	3.4	3.7	-	11.5	84	44	64	65	17	019	024.9	25	-	-	01	-	-	C8	01	12	04	07	07	01	01	-	
IX	4.6	5.1	2.6	4.2	-	10.0	14	47	45	45	19	044	025.4	08	-	-	15	-	-	C9	02	07	13	07	02	13	06	-	
X	4.5	5.3	4.0	4.6	-	07.5	86	64	72	72	36	068	017.0	15	-	-	01	-	-	C10	03	07	06	02	06	04	05	-	
XI	7.5	6.1	6.6	6.7	-	05.5	91	71	71	71	26	040	020.0	08	-	-	01	-	-	C11	16	16	16	02	06	05	05	-	
XII	6.4	6.4	5.5	6.1	-	04.6	81	51	51	52	92	022	000.1	15	-	-	24	-	-	C12	05	15	09	04	02	07	05	-	
GOD.	5.3	5.4	5.0	5.2	-	07.4	83	58	77	73	17	129	027.4	0%	-	-	55	90	3										

Mesec	Vazdušni četvrtak utroba min.	Temperatura vazduha °C								Čestina pravaca i srednja jačina vетра m/s, Fm (0-12)																		
		Tm	7	14	21	Sred. Dneš	Max	Min	Dat.	Min	Max	NE	E	SE	S	SW	W	NW	C									
											8.	9.	10.	11.	12.	13.	14.	15.	16.	17.								
$\gamma = 42^{\circ}12'N \lambda = 22^{\circ}20'E$ Gr. AG = + 1h 23 min.																												
I	709.3	-01.4	02.9	-00.4	00.2	03.6	-02.2	07.5	01	-08.0	15	02	02.5	03	03.1	01	04.0	*	*	*	01	03.0	22					
II	708.1	01.0	01.0	01.0	01.0	01.0	01.0	01.0	01.0	-01.0	28	3	3	3	03.5	*	*	*	01	05.3	20	03.1	01					
III	702.3	02.4	10.0	02.4	00.1	41.7	02.2	45.0	22	-02.0	01	02.5	02.5	01	04.8	*	*	01	02.8	01	02.0	01	02.0					
IV	698.4	05.6	11.8	07.0	07.9	13.3	03.2	22.0	30	-00.8	03	04.5	02.9	01	04.0	02	03.5	01	03.0	22	03.0	03.7	04					
V	699.4	10.6	16.1	11.1	12.2	17.9	07.4	24.7	31	02.7	06	01	03.0	47	02.5	01	03.0	*	*	01	05.0	21	03.2	01	03.0			
VI	706.3	15.2	20.5	15.0	16.4	23.0	11.2	29.1	29	06.1	13	02	02.5	49	02.7	*	*	01	04.0	*	*	25	03.0	03	04.0			
VII	702.5	16.7	25.1	17.3	19.1	26.6	12.5	33.8	17	07.0	10	01	02.0	57	02.9	*	*	*	*	*	*	20	02.6	01	05.0			
VIII	702.8	17.0	26.1	18.2	19.9	27.0	14.1	33.3	05	10.6	31	0*	0	70	03.2	01	03.0	*	*	*	13	02.7	*	02	03.0			
IX	702.6	12.8	22.4	14.5	16.1	24.0	10.6	30.6	04	02.8	28	01	03.0	56	03.0	01	06.0	*	*	*	26	03.2	02	04.5	*			
X	695.9	08.4	16.4	10.0	11.2	17.2	06.4	23.2	14.0	-03.8	28	01	03.0	44	03.4	*	*	02	04.0	06	05.5	34	04.0	*	03			
XI	703.2	02.6	05.4	04.1	05.1	10.5	01.6	14.1	17	-02.4	03	0*	0	51	03.7	*	*	*	02	04.5	26	02.6	*	02	01.5			
XII	703.1	-00.7	04.9	00.3	01.2	05.9	-02.2	11.1	30	-05.6	18	01	03.0	53	03.3	*	*	*	*	*	14	01.9	*	01	04.0			
GOD.	-	701.6	07.6	14.4	08.7	09.9	15.8	05.4	33.8	0*	-08.0	41	09	02.7	647	03.1	06	03.8	05	03.8	13	05.1	248	03.0	11	03.8		
$\gamma = 41^{\circ}31'N \lambda = 20^{\circ}32'$ E Gr. AG = + 1h 23 min.																												
I	-	-01.7	04.7	01.9	01.7	05.5	-02.6	09.5	22	-07.5	25	01	01.0	*	*	02	04.5	*	*	37	01.5	*	*	41	01.7	*	12	
II	-	01.8	07.5	04.1	04.4	08.0	-02.2	14.0	14	-05.5	28	07	01.7	*	*	16	05.1	*	*	43	02.1	*	*	15	01.9	*	03	
III	-	03.9	11.6	06.7	07.2	12.8	01.3	23.0	24.2	-05.0	02.0	01	01.4	*	*	20	05.2	*	*	28	02.1	*	*	18	01.3	*	22	
IV	-	06.8	12.7	08.0	08.9	13.7	03.6	20.0	30.2	00.0	24	04	02.2	*	*	14	03.7	*	*	40	01.9	*	*	22	01.8	*	10	
V	-	05.0	16.6	11.7	12.5	18.3	06.4	26.0	31	01.5	11	*	*	*	*	01	03.0	*	*	56	02.0	*	*	19	01.9	*	17	
VI	-	15.6	22.4	16.1	17.6	23.8	10.7	30.5	27	05.5	12	*	*	*	*	*	*	*	55	01.9	*	*	21	02.1	*	14		
VII	-	17.1	26.9	19.2	20.6	28.3	11.7	36.0	17	06.0	10	07	02.5	*	*	*	*	*	54	01.9	*	*	22	02.0	*	15		
VIII	-	17.8	27.7	21.0	21.9	29.0	13.6	34.5	06	08.0	14	*	*	*	*	04	03.2	*	*	47	01.9	*	*	26	01.9	*	16	
IX	-	13.9	23.0	16.9	17.7	24.1	10.8	31.5	04	04.0	29.2	*	*	*	*	*	*	*	52	01.5	*	*	25	02.0	*	13		
X	-	07.9	15.0	16.0	10.7	16.7	05.6	23.0	12.0	-03.0	28	*	*	*	*	*	*	*	66	02.0	*	*	14	02.1	*	13		
XI	-	03.2	10.9	05.8	06.4	11.8	01.8	16.5	20	-04.0	30	*	*	*	*	*	*	*	63	01.9	*	*	14	02.0	*	13		
XII	-	-00.4	06.1	01.8	02.3	07.3	-01.8	12.5	04	-05.0	25.20	*	*	*	*	*	*	*	58	01.9	*	*	21	02.0	*	14		
GOD.	-	08.0	15.4	10.3	11.0	16.7	05.1	36.0	0*	-07.5	21	10	01.8	*	*	57	04.6	*	*	599	01.9	*	*	258	01.9	*	16	
$\gamma = 41^{\circ}11'N \lambda = 20^{\circ}41'$ E Gr. AG = + 1h 23 min.																												
I	-	-00.3	05.6	01.9	02.3	06.3	-00.9	10.3	04	-05.6	16	09	02.0	02	02.5	*	*	*	18	01.9	06	01.7	01	01.0	47	01.5	10	
II	-	02.3	07.0	04.0	04.3	08.0	01.1	12.4	18	-02.2	02	13	02.0	14	04.2	*	*	*	23	02.4	02	03.0	04	01.0	22	01.5	06	
III	-	03.2	10.6	06.4	06.7	11.6	01.9	20.8	24	-02.5	02	14	01.5	12	02.8	01	02.0	02.5	02	01.0	21	01.6	20	01.7	21	01.7	03	
IV	-	06.2	11.2	07.8	08.3	12.6	04.3	20.0	30	00.6	10	11	01.8	05	03.4	01	02.0	02.7	02.1	08	02.9	01	01.7	17	01.6	12		
V	-	10.4	15.7	11.8	12.4	17.3	07.1	23.0	31	02.0	11	12	01.8	02	02.5	02	01.5	03	02.0	31	02.5	02	02.5	05	01.2	20	01.3	14
VI	-	15.3	21.2	16.8	17.5	22.9	10.8	28.4	27	04.6	15	14	01.9	03	07.3	01	03.0	02	01.5	18	02.2	12	03.2	04	03.2	18	01.6	14
VII	-	17.1	25.6	19.2	20.3	26.8	12.0	33.5	17	06.2	10	12	02.7	01	02.0	01	03.0	*	*	24	02.1	01	01.0	07	02.3	22	01.6	25
VIII	-	17.4	26.4	19.2	20.5	27.6	13.7	31.6	04	08.8	13	12	02.0	*	*	01	02.0	*	*	19	02.2	06	02.2	01	03.0	37	01.6	06
IX	-	12.9	22.4	15.6	16.6	23.3	10.3	29.5	04	02.4	28	15	02.0	04	02.0	*	*	01	03.0	24	02.0	02	03.5	02	02.0	32	01.7	10
X	-	07.9	15.2	09.8	10.7	16.2	05.9	21.4	23	-02.1	28	06	02.2	*	*	01	03.0	*	*	28	02.7	12	03.4	10	02.6	28	01.6	08
XI	-	03.6	09.9	04.5	05.6	10.6	01.8	14.5	20	-01.6	04	13	01.1	02	03.0	*	*	23	02.2	04	03.0	03	02.5	32	01.5	14		
XII	-	-00.4	06.4	01.4	02.2	07.3	-01.7	12.5	04	-05.1	21	18	02.1	*	*	*	01	03.0	16	02.2	01	02.0	01	01.0	45	01.7	17	
GOD.	-	00.0	14.8	09.9	10.6	15.9	05.5	33.5	0*	-05.6	41	157	02.0	45	02.9	08	02.2	12	01.9	271	02.2	58	02.8	46	02.0	349	01.6	14
$\gamma = 41^{\circ}32'N \lambda = 20^{\circ}42'$ E Gr. AG = + 1h 23 min.																												
I	-	652.4	-04.1	00.8	-03.0	-02.3	02.0	-05.4	06.5	22	-12.1	14	07	02.0	02	01.5	16	01.5	07	01.7	*	*	01	01.0	08	01.9	37	
II	-	647.9	-01.8	02.2	-00.7	-00.2	03.5	-02.9	11.1	12	-11.8	09	02	01.5	01	01.0	08	01.8	26	01.6	15	01.0	03	02.0	*	01	01.6	23
III	-	650.2	00.5	06.5	01.9	02.7	07.4	-00.8	18.1	21	-08.7	02	01	01.0	01	01.0	07	01.6	17	01.6	21	01.6	10	01.4	02.8	01.8	06	
IV	-	647.2	01.7	06.0	02.4	03.2	08.1	00.0	14.6	30	-03.2	09	06	01.7	04	00.0	08	01.4	10	01.4	14	01.8	03	01.8	07	02.4	27	
V	-	645.5	07.3	11.2	07.7	08.5	12.8	04.2	18.8	20	00.6	11	11	02.9	05	02.6	04	02.0	11	02.3	08	02.3	04	01.8	07	03.0	16	
VI	-	651.4	12.0	16.5	12.2	13.2	18.5	07.7	24.4	27	06.1	12	17	02.5	09	02.8	05	03.2	16	01.8	15	01.4	02	02.0	02.4	01.4	14	
VII	-	653.5	13.7	21.0	14.8	16.1	22.2	09.8	29.6	16	02.0	09	09	02.8	09	02.7	21	02.6	11	02.2	03	01.7	07	02.1	10	02.7	07	
VIII	-	653.6	13.8	22.1	15.7	16.8	23.5	10.8	28.2	06	04.9	13	04	02.2	12	02.2	08	02.2	21	02.0	08	02.8	09	02.1	02	02.2	03	03.3
IX	-	653.2	10.2	17.7	11.6	12.7	18.6	07.8	25.5	04	01.0	28	07	02.4	22	02.0	16	02.1	08	02.5	05	02.0	06	03.2	02	03.0	06	03.0
X	-	645.0	04.8	09.7	05.4	06.3	11.0	02.4	17.7	04	-07.0	28	10	03.0	09	02.1	05	02.6	21	02.2	07	03.1	11	02.3	08	03.0	10	03.0
XI	-	651.9	00.5	6.67	01.																							

Mjesec	Oblažnost Nm (0-10)				Temperatura °C mm	Vlažnost vazduha				Padavine mm				Broj dana n s a:													
	7	14	21	Sred. (Dnev.)		7	14	21	Spec.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	□	■	■	
	Dnevi sati	Dnevi sati	Dnevi sati	Dnevi sati		mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	•	Δ	▲	□	■	■	■		
KRIVA PALANKA																											
BR. ST.256																											
I	7.4	7.4	6.0	6.9	084.6	03.7	62	67	80	76	31	025	006.6	24	•	01	24	•	•	02	•	05	16	09	06	04	
II	6.9	6.7	5.5	6.2	125.9	04.3	80	63	71	73	36	060	023.4	08	•	0	14	•	•	04	•	04	13	07	05	02	
III	6.9	6.3	5.5	6.2	150.5	04.8	77	55	71	68	19	937	033.2	9!	•	3	93	•	3	97	•	93	18	19	06	01	
IV	4.4	4.0	3.4	4.8	164.7	05.2	75	51	60	65	20	029	033.0	15	•	•	02	•	•	02	•	17	09	05	01	02	
V	6.2	7.2	5.6	6.4	198.0	07.6	80	55	78	71	34	134	C39.0	16	•	•	•	•	•	06	•	03	09	23	20	02	
VI	4.6	6.7	5.8	5.7	244.7	10.0	76	57	77	70	39	124	C25.2	02	•	•	08	•	•	04	02	02	06	14	11	06	
VII	2.5	4.0	2.5	3.1	335.5	10.1	71	43	67	60	25	023	012.9	01	•	•	21	09	•	14	03	07	03	01	07		
VIII	2.0	4.4	2.0	3.1	305.2	10.4	73	42	66	60	28	049	C13.7	12	•	•	24	09	•	04	01	13	02	10	06	03	
IX	3.5	5.0	2.4	3.6	243.4	05.2	80	48	74	67	29	019	C13.2	27	•	•	•	16	01	•	04	14	02	05	04	02	
X	6.5	7.2	4.8	6.2	191.9	06.9	81	49	73	68	30	065	C26.1	22	•	•	03	•	•	14	03	01	08	14	10	03	
XI	5.7	5.7	4.7	5.4	129.2	05.1	85	62	82	76	43	040	C19.2	01	•	•	04	•	•	07	09	06	01	06	01	05	
XII	5.7	6.4	6.1	6.1	105.5	03.8	83	61	81	75	20	045	C14.5	15	•	•	27	•	•	02	•	05	11	13	06	01	
GOD.	5.4	6.2	4.8	5.5	2279.1	06.8	78	54	74	69	18	640	C39.0	Ns-V	•	01	81	65	19	•	45	06	76	106	135	91	27
DEBAR																											
BR. ST.257																											
I	6.0	6.1	6.2	6.1	-	04.2	91	68	84	81	28	038	C20.0	18	•	•	23	•	•	01	•	09	14	05	05	01	
II	6.9	6.7	7.5	7.3	-	04.7	83	63	79	75	38	126	C42.0	07	•	•	15	•	•	05	01	04	16	07	07	04	
III	6.3	6.2	6.7	6.4	-	05.1	82	55	72	69	26	054	C15.0	09	•	•	10	•	•	04	02	07	14	07	07	05	
IV	6.7	7.3	7.1	7.0	-	06.3	82	62	78	74	48	083	C24.4	17	•	•	•	•	•	01	•	14	10	10	04	10	
V	6.5	6.9	6.5	6.6	-	07.6	85	55	76	72	26	233	C32.0	05	•	•	01	•	•	04	13	15	15	09	15	07	
VI	5.2	6.5	6.4	6.1	-	09.9	76	49	72	66	17	062	C32.0	17	•	•	14	01	•	04	10	07	07	01	07	07	
VII	1.6	3.5	2.8	2.6	-	09.8	69	35	63	56	20	-	-	-	•	•	25	19	•	19	02	•	•	01	06	02	
VIII	3.7	4.6	4.6	4.3	-	10.1	71	34	59	55	19	032	C13.0	25	•	•	25	17	•	12	06	05	05	01	05	07	
IX	4.3	4.7	4.7	4.6	-	10.3	87	49	73	70	25	038	C10.0	08	•	•	18	01	•	09	08	06	08	01	06	07	
X	6.5	6.5	7.1	6.7	-	07.3	86	60	80	75	15	192	C31.0	31	•	•	02	•	•	03	17	17	17	08	17	07	
XI	5.8	6.5	6.0	6.1	-	05.8	91	64	84	80	46	078	C04.0	01	•	•	05	•	•	05	14	05	05	05	05	03	
XII	5.1	4.9	5.6	5.2	-	04.5	89	67	90	82	52	029	C12.0	19	•	•	24	•	•	08	09	04	04	01	02	02	
GOD.	5.4	5.5	5.9	5.8	-	07.1	83	55	76	71	15	965	C42.0	07.0	•	•	93	70	31	•	11	03	85	137	90	90	07
STRUGA																											
BR. ST.258																											
I	6.4	5.9	4.9	5.7	-	04.4	51	67	84	81	36	046	C14.1	18	•	•	20	•	•	06	09	11	09	01	01	02	
II	7.2	7.2	7.2	7.2	-	05.0	66	67	82	79	36	101	C27.8	05	•	•	11	•	•	03	16	13	10	12	03	01	
III	6.1	6.6	5.2	6.1	-	05.4	88	59	76	75	27	063	C12.0	31	•	•	06	•	•	07	15	13	11	01	13	04	
IV	6.9	7.9	7.2	7.3	-	06.4	88	65	82	78	31	091	C19.5	16	•	•	•	•	•	01	12	18	14	04	18	04	
V	6.0	7.6	5.7	6.4	-	08.0	84	63	77	75	33	090	C16.6	02	•	•	01	•	•	02	14	16	13	04	16	07	
VI	4.4	5.9	4.3	4.9	-	10.0	78	24	70	67	25	044	C20.3	17	•	•	05	•	•	04	05	09	07	01	05	07	
VII	1.2	3.5	1.7	2.2	-	10.1	70	39	63	58	22	010	C05.0	01	•	•	22	06	•	20	02	03	02	05	02	02	
VIII	2.5	4.1	3.3	3.3	-	10.6	74	40	66	60	21	094	C27.0	29	•	•	25	06	•	14	02	09	07	01	09	10	
IX	3.2	4.9	3.4	3.6	-	10.0	88	48	78	71	26	038	C17.0	27	•	•	11	•	•	12	04	07	04	02	07	06	
X	6.4	7.9	5.0	6.1	-	07.5	89	60	81	77	34	195	C29.4	22	•	•	01	•	•	02	10	19	19	06	19	04	
XI	5.7	6.2	6.6	5.3	-	05.7	92	66	85	82	38	094	C26.8	01	•	•	04	•	•	02	12	10	08	05	10	02	
XII	5.2	4.5	4.2	4.6	-	04.4	88	67	80	74	46	023	C08.6	19	•	•	25	•	•	08	07	06	06	03	01	02	
GOD.	5.2	4.0	4.8	5.3	-	07.3	84	58	78	73	21	849	C29.4	22.X	•	•	67	67	12	•	05	•	81	108	137	111	28
LAZAROPCLE																											
BR. ST.259																											
I	6.6	4.5	4.7	5.9	-	03.2	85	68	83	79	30	056	C24.2	18	04	07	28	•	•	02	05	11	11	07	01	11	
II	7.5	8.0	6.0	7.8	-	073.4	03.7	67	81	80	29	122	C03.1	05	01	03	23	•	•	02	03	20	17	08	05	15	
III	6.4	6.8	6.1	6.3	-	132.8	04.3	85	64	80	77	21	052	C12.9	09	•	01	19	•	•	07	14	13	12	01	01	13
IV	7.1	8.7	6.7	7.5	-	110.4	04.4	86	64	81	77	39	115	C20.0	17	•	•	16	•	•	01	14	20	16	05	17	04
V	6.5	8.1	5.9	6.8	-	146.0	06.6	87	67	84	79	29	172	C27.3	16	•	•	01	•	•	02	13	17	15	08	17	04
VI	4.7	6.6	4.8	5.8	-	231.7	01.8	70	56	77	71	33	066	C02.4	17	•	•	05	•	•	01	06	07	03	08	02	02
VII	2.2	2.0	5.6	2.9	-	338.3	09.0	74	65	76	66	22	002	C01.7	01	•	•	22	06	•	13	01	04	01	04	04	03
VIII	3.2	5.3	2.0	3.6	-	278.5	09.0	76	45	73	65	21	057	C28.2	25	•	•	15	•	•	10	02	10	07	01	10	06
IX	3.9	5.8	3.1	4.3	-	209.1	08.2	85	54	84	74	34	065	C28.2	27	•	•	01	•	•	01	08	06	11	09	03	11
X	6.7	6.1	5.6	6.0	-	142.6	05.7	85	65	82	77	33	241	C03.6	22	•	•	09	•	•	01	10	20	15	10	17	

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																	
		Tm			Sred. (Siles)	Max	Min	Max	Dat.	Min	Dat.	N	NE	E	SE	S	SW	W	NW	C									
		7	14	21																									
$\varphi = 41^{\circ}07'N \lambda = 20^{\circ}48'E$ Gr. $\Delta G = + 1h 23 min.$																													
I	694.0	00.2	05.6	C1.9	02.4	04.2	-01.0	09.3	22	-06.4	16	37	C1.5	CR	01.9	C1	C2.0	02	02.0	10	01.7	09	01.2	01	01.0	13	C1.7	12	
II	693.9	02.7	07.0	04.2	04.5	08.3	01.0	12.6	17	-04.0	09	26	C2.0	09	02.4	CR	C2.5	04	02.6	16	02.7	08	01.5	03	02.3	09	C1.4	01	
III	696.0	04.0	10.4	06.9	07.1	11.7	02.7	20.9	23	-02.5	02	34	C1.7	08	02.2	C7	C2.4	04	03.0	16	01.9	11	01.9	06	01.5	08	01.5	09	
IV	692.5	06.1	11.3	07.7	08.2	12.7	04.0	26.0	30	06.3	09	17	C1.6	64	01.5	02	C2.0	04	02.5	20	02.3	14	02.1	10	02.3	06	C1.0	13	
V	694.2	10.8	15.9	12.0	12.6	17.5	07.5	23.3	28	03.1	11	08	C1.6	C4	02.5	C1	C2.0	01	02.0	34	02.3	22	02.0	06	02.5	02	01.5	15	
VI	695.2	15.5	21.0	16.8	17.6	22.9	11.4	27.4	27	06.3	15	17	C2.3	*	*	*	*	04	01.2	32	01.9	14	02.4	11	02.2	04	02.2	08	
VII	694.9	17.4	25.2	19.9	20.6	26.9	13.7	32.0	18	17	07.6	09	26	C1.8	04	01.2	*	*	01	01.0	23	01.6	14	01.9	04	02.8	08	01.2	13
VIII	697.0	17.6	26.2	19.7	20.8	27.9	14.9	32.3	06	05.3	13	43	C1.8	07	01.7	01	01.0	*	*	11	02.1	13	01.9	04	01.8	10	01.4	04	
IX	697.0	13.7	22.2	18.7	17.3	23.6	11.8	28.2	04	03.9	28	36	C1.8	C4	02.2	03	C3.0	01	01.0	16	02.0	09	01.9	09	01.9	11	01.5	01	
X	694.9	08.8	14.8	10.7	11.2	16.1	06.8	21.4	28	24	01.7	01	01.0	C2	C1.0	03	C2.0	26	03.0	21	C2.7	07	02.4	10	02.1	01			
XI	697.5	04.6	09.8	05.7	06.5	10.8	03.0	14.7	20	-06.7	30	34	C1.9	05	01.2	*	*	14	02.1	11	02.4	12	02.0	08	01.6	06			
XII	697.4	00.7	06.5	02.1	02.6	07.4	-01.1	14.0	04	-05.7	20	46	C2.3	07	07.5	*	*	09	02.0	12	01.5	C7	02.7	13	C1.7	04			
GOD.	696.0	08.5	14.7	10.4	11.0	16.0	C1.6	06.2	32.3	06.1	-06.4	N.1	336	C1.9	56	01.9	25	02.3	24	02.2	227	02.2	158	02.0	80	02.2	102	01.6	87
$\varphi = 41^{\circ}48'N \lambda = 20^{\circ}57'E$ Gr. $\Delta G = + 1h 24 min.$																													
I	-	-02.6	03.4	-01.1	-00.3	04.7	-05.6	10.0	21	-13.0	15	06	C2.0	05	C2.4	*	*	*	*	*	08	C2.4	*	*	08	C2.6	66		
II	-	01.6	C6.6	02.6	03.4	07.7	-00.8	11.4	12	11	-08.0	02	01	C2.0	03	C2.3	*	*	01	C2.0	*	*	14	C3.6	*	*	21	C2.6	43
III	-	03.8	11.0	05.4	06.4	12.1	01.3	22.4	23	21	-03.8	02	02	C2.0	08	C2.5	*	*	01	C2.0	*	*	12	C2.7	*	*	22	C2.3	48
IV	-	07.0	12.6	08.2	09.0	13.9	03.1	26.0	27	06.0	04	06	C2.5	08	C2.4	*	*	*	*	*	12	C3.5	*	*	24	C2.5	40		
V	-	12.8	17.2	12.2	13.6	19.4	06.2	25.0	31	03.5	16	01	C2.0	11	C2.3	*	*	04	04.2	*	*	34	C3.9	*	*	18	C2.7	25	
VI	-	17.2	22.6	16.4	18.4	24.0	10.1	28.4	46	07.2	13	03	C2.3	13	C2.4	*	*	01	C3.0	29	C3.9	*	*	22	C2.5	22			
VII	-	18.9	26.3	20.6	27.5	10.9	34.6	17	07.2	09	05	C2.4	13	C2.2	*	*	01	C3.0	00	C3.1	*	*	31	C2.3	34				
VIII	-	18.4	26.3	18.8	20.6	27.7	12.5	33.0	04	08.6	13	*	16	05.5	*	*	03	C3.0	*	10	C2.6	*	*	24	C2.4	40			
IX	-	13.7	21.3	15.7	16.7	22.9	08.4	27.6	04	01.0	29	28	C2.2	C8	07.2	*	*	C1	C2.0	*	*	10	C3.0	*	*	17	C2.3	49	
X	-	05.7	15.7	16.2	11.2	17.1	02.2	22.4	24	01	-04.2	28	05	C2.2	06	C2.5	*	*	01	05.0	*	*	39	C4.3	*	*	15	C2.2	27
XI	-	02.0	09.0	C3.7	04.6	10.1	-00.9	15.2	28	-04.3	19	*	08	02.5	*	*	*	*	*	15	C3.5	*	*	18	C2.4	49			
XII	-	-01.0	05.0	00.4	01.0	06.6	-04.2	11.6	04	-02.4	25	10	C4.8	06	C2.3	*	*	02	03.5	*	*	02	01.5	*	*	15	C2.3	60	
GOD.	-	08.3	14.8	C9.3	10.4	16.1	03.6	34.8	Max	-13.0	151	45	C2.6	105	C2.4	*	*	11	C3.3	02	C3.0	194	C3.6	*	*	235	C2.4	503	
$\varphi = 41^{\circ}31'N \lambda = 20^{\circ}58'E$ Gr. $\Delta G = + 1h 24 min.$																													
I	-	-00.9	04.7	C1.5	01.7	05.6	-01.7	09.5	22	21	-06.5	16	29	C1.1	12	C1.8	14	C1.4	16	C1.8	15	01.7	02	01.0	07	02.1	01	C2.0	07
II	-	01.7	C7.1	04.1	04.2	08.0	00.7	14.0	12	-04.6	01	30	02.1	05	C1.8	13	C2.3	*	*	14	C2.0	04	02.0	07	01.6	02	C2.6	09	
III	-	02.9	11.9	07.5	07.4	12.6	C2.2	23.8	22	-03.6	02	32	C2.0	07	C2.3	16	C1.6	C5	C2.2	14	C1.4	06	01.5	11	01.5	03	C2.3	09	
IV	-	04.9	13.2	08.7	08.9	14.0	04.0	19.5	30	29	-01.0	10	31	C2.5	07	C3.0	C5	C2.2	01	C3.0	34	C2.5	02	01.5	06	C1.7	07		
V	-	68.5	17.5	12.9	13.0	18.9	07.2	26.0	31	01.8	11	22	C2.3	C2	01.0	11	C1.8	02	C2.0	24	C3.2	03	01.7	11	C1.8	08	C1.5	10	
VI	-	12.8	23.6	17.7	18.0	24.7	11.1	30.8	27	05.0	13	12	C2.8	10	C2.4	11	C1.6	02	C2.8	02	C3.0	11	C1.5	07	C1.6	04			
VII	-	14.2	28.3	20.1	20.7	29.1	12.0	36.5	17	06.2	10	36	C2.1	17	C2.3	16	C1.6	02	C2.5	07	C2.1	04	C2.2	07	01.7	05	C1.4	07	
VIII	-	14.3	27.8	20.2	20.6	28.9	13.2	35.0	06.05	07.6	13	34	C1.7	08	C2.5	C5	C2.4	02	C1.5	06	C1.2	04	C1.5	09	C1.2	08	C1.6	13	
IX	-	16.9	23.3	15.4	16.5	24.1	16.1	31.5	04	01.2	28	21	C1.9	05	C1.8	C6	C1.2	01	C1.0	08	C1.4	02	C1.5	19	C1.4	18			
X	-	07.0	15.7	09.7	10.5	16.8	05.2	23.4	14	05.0	03.5	28	20	C1.4	08	C1.8	C6	C1.3	01	C1.0	15	C3.5	10	C1.4	16	C1.3	06		
XI	-	02.3	10.4	05.4	05.4	11.6	01.3	15.2	20	-02.5	30.4	28	C1.6	06	C1.8	C8	C1.4	04	C1.2	20	C2.0	03	C1.3	08	C1.6	06			

Meseč	Oblažnost mm (0-10)					Vlažnost vazduha			Padavine R mm			Broj dana na sat:																				
	Temperatura °C		Uvijet m s		Precipitation mm			mm			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	□						
	7	14	21	Sred. Sred. Sred.	Dnev. Dnev. Dnev.	mm	m	s	Σ	X	SD	D	%	30.00.0	0.0250.0	0.020.0	0.6	8	2.0	8.0	0.1	1.00.0	0.0	0.0	0.0	0.0						
CHRD																																
BR. ST.261																																
I 6.2 5.8 5.8 5.8 5.8	113.3	04.5	86	70	82	80	47	035	C09.7	18	•	•	21	•	•	•	05	11	11	C5	•	11	03	01	•	•	•	04				
II 7.5 6.8 7.0 7.1	085.4	04.9	83	66	77	76	47	090	C30.6	05	•	•	10	•	•	•	05	01	03	15	12	10	04	12	02	02	•	02				
III 6.5 6.6 5.5 6.2	141.6	05.4	83	60	75	73	32	040	C11.2	31	•	•	03	•	•	•	07	06	13	12	10	01	12	06	04	•	01	01				
IV 7.0 6.1 6.6 7.3	133.1	06.1	85	63	77	75	36	083	C15.2	16	•	•	•	•	•	•	04	01	•	12	18	16	02	18	•	•	01	04				
V 5.5 7.7 5.1 6.1	197.7	08.1	82	63	78	74	36	098	C34.0	05	•	•	•	•	•	•	03	11	15	10	04	15	•	•	•	01	04					
VI 4.3 6.1 4.6 5.0	265.1	10.5	78	58	72	69	42	042	C25.5	17	•	•	06	•	•	•	01	04	07	10	06	10	01	01	•	08	•	01				
VII 1.2 3.4 1.5 2.0	347.9	11.0	72	47	62	61	32	004	C01.8	01	•	•	22	07	•	•	19	C2	C3	03	•	03	•	•	03	•	03	•				
VIII 2.3 3.9 2.9 3.0	303.3	11.2	74	47	63	61	32	049	C14.4	28	•	•	26	08	•	01	•	15	C2	08	07	01	06	•	01	11	•	01				
IX 3.2 5.1 3.1 3.8	225.9	10.2	83	53	72	70	36	033	C14.7	26	•	•	11	•	•	01	01	10	C2	C7	02	02	07	•	•	•	06	•	01			
X 6.4 6.8 5.6 6.2	157.5	07.7	86	64	78	76	41	150	C26.0	22	•	•	01	•	•	•	07	03	01	08	21	19	07	21	•	•	05	•	01			
XI 7.0 6.2 4.9 6.0	109.8	06.0	90	68	85	81	50	077	C31.8	01	•	•	02	•	•	•	03	03	09	06	02	05	05	01	02	•	01					
XII 5.4 4.8 3.8 4.7	129.1	04.5	85	69	81	78	43	023	C08.6	19	•	•	23	•	•	01	•	08	07	05	05	03	01	•	•	01	02					
GOD. 5.2 5.9 4.7 5.3	2209.7	07.5	62	60	75	72	32	724	C04.0	65	V	•	•	60	65	15	•	25	06	77	98	133	106	24	131	15	08	•	03	45	03	
GOSTIVAR																																
BR. ST.262																																
H = 525 m H _b = - m h = 2.1 m h _r = 1.5 m																																
I 6.2 5.6 5.2 5.7	-	03.2	62	73	64	66	-	09	C22.0	24	04	•	31	•	•	•	07	11	11	16	04	05	06	•	•	•	03	31				
II 6.6 6.8 6.2 6.5	-	04.5	74	71	76	74	43	174	C30.0	05	•	•	16	•	•	•	02	•	06	14	18	17	08	18	•	•	02					
III 5.5 6.2 5.8 5.8	-	05.3	79	62	77	72	33	134	C17.0	09	•	•	08	•	•	•	08	12	11	11	09	08	06	04	•	•	04					
IV 6.5 7.4 6.9 6.9	-	06.2	79	59	76	71	26	664	C16.0	17	•	•	•	•	•	01	01	•	10	13	11	02	17	•	•	•	•	•				
V 5.5 7.1 5.4 6.0	-	08.2	72	59	72	68	39	088	C29.0	16	•	•	01	•	•	01	01	07	07	13	11	C3	13	•	•	•	•	•				
VI 4.6 6.1 5.6 5.4	-	10.4	70	54	68	64	32	052	C30.0	17	•	•	14	•	•	01	01	02	03	06	04	03	06	•	•	•	•	•				
VII 1.6 3.8 1.7 2.4	-	10.6	63	44	63	57	30	005	C03.0	08	•	•	25	09	•	•	15	•	02	07	•	02	•	•	01	01	•	01				
VIII 2.3 4.5 2.5 3.1	-	11.2	69	42	65	61	31	033	C18.0	25	•	•	25	10	•	•	13	03	05	05	01	04	•	•	•	01	01					
IX 3.8 5.4 C4.0 4.2	-	09.4	76	55	74	68	11	042	C11.0	27	•	•	08	•	•	04	06	C3	05	02	05	•	•	•	01	•	01					
X 5.2 5.6 4.3 5.1	-	07.0	76	56	72	68	10	13	C25.0	21	•	•	04	•	•	05	02	C5	C8	17	16	04	17	•	•	03	•	03				
XI 5.6 5.8 5.4 5.6	-	04.8	75	67	75	73	41	069	C30.0	27	•	•	20	•	•	01	01	C8	C8	08	02	08	•	•	•	01	12	•				
XII 4.8 4.3 4.5 4.5	-	03.6	65	71	71	69	32	018	C07.0	19	•	•	31	•	•	01	01	C8	C6	06	04	C2	04	•	•	01	16	•	01			
GOD. 4.6 5.7 4.8 5.1	-	07.1	72	60	71	68	-	516	C03.0	07X	04	•	110	73	19	•	12	06	R3	E5	115	106	36	102	16	•	•	02	05	46		
KICEVO																																
BR. ST.263																																
H = 620 m H _b = - m h = 2.1 m h _r = 1.5 m																																
I 6.8 6.1 6.2 6.4	-	04.4	92	72	88	84	48	055	C11.6	11	•	•	19	•	•	•	06	16	11	08	C2	C9	07	05	•	05	06	02				
II 7.7 7.1 7.2 7.4	-	05.0	90	67	84	80	21	094	C29.0	05	•	•	09	•	•	•	04	18	15	12	05	15	02	02	02	02	01	01				
III 6.9 6.4 6.7 6.9	-	05.4	90	57	72	73	20	053	C13.5	09	•	•	06	•	•	•	03	17	10	C9	01	05	07	06	•	01	08	02				
IV 7.9 8.5 8.1 8.2	-	06.0	88	55	73	71	29	111	C18.2	15	•	•	01	•	•	01	02	•	18	14	04	14	01	•	01	02	01					
V 5.5 6.3 7.0 6.9	-	06.0	87	60	74	74	28	095	C10.4	22	•	•	01	•	•	01	01	11	12	12	05	12	•	04	01	01	01					
VI 5.0 6.8 5.7 5.9	-	10.1	84	50	66	67	13	058	C16.3	19	•	•	16	01	•	•	01	06	11	10	02	11	•	01	07	03	•	03				
VII 2.0 2.9 3.2 3.4	-	11.2	84	43	66	55	27	076	C34.7	25	•	•	26	15	•	•	17	01	01	01	01	01	01	01	01	01	06					
IX 4.7 4.9 3.0 4.2	-	10.4	91	54	78	74	39	064	C32.5	27	•	•	13	01	•	01	09	04	06	06	01	C6	06	•	03	07	01					
X 6.6 6.9 5.2 6.3	-	07.5	89	61	82	77	29	124	C18.0	22	•	•	02	•	•	02	02	C2	04	02	04	02	04	04	03	03	04					
XI 7.0 5.2 5.0 5.8	-	05.5	90	63	84	75	48	076	C25.7	01	•	•	11	•	•	03	03	10	09	06	03	09	•	01	12	01						
XII 6.1 5.0 5.0 5.3	-	04.0	86	62	84	77	37	010	C03.9	15	•	•	24	•	•	04	09	11	04	03	•	03	02	01	01	01						
GOD. 5.7 6.2 5.4 5.8	-	07.4	88	57	76	74	13	817	C04.7	25X	V	•	•	72	62	33	•	05	02	68	122	120	116	32	116	19	14	•	01	01	32	56
PESEN																																
BR. ST.264																																
H = 881 m H _b = - m h = 1.9 m h _r = 1.7 m																																
I 6.2 6.4 5.4 6.0	-	04.1	80	75	83	81	37	046	C10.3	03	•	01	24	•	•	•	01	01	16	12	03	06	03	01	•	01	06	02				
II 7.3 7.6 6.3 7.1	-	04.6	81	73	87	81	23	109	C32.2	05	•	•	13	•	•	02	•	05	15	12	10	03	11	04	03	•	01	03				
III 7.0 6.3 6.0 6.5	-	05.0	87	60	83	77	26	058	C16.2	05	•	•	09	•	•	01	•	09	17	11	11	01	05	10	06	•	01	04				
IV 7.3 7.9 7.2 7.4	-	05.8	85	66	82	78	32	069	C13.3	17	•	•	02	•	•	01	•	13	14	12	02	14	•	•	02	02						

Mesec	Vazdušni pritisak Pr. mm	Temperatura vazduha °C								Čestina pravaca i srednja jačina veta nD, fm (0-12)																		
		Tm			Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C	
		7	14	21							8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.	8.	15.
$\varphi = 41^{\circ}22'N \lambda = 21^{\circ}15'$ E Gr. AG = + 1h 25 min.																												
I	-	-02.3	00.7	-01.5	-01.1	01.9	-03.9	07.5	18.17	-11.4	14	17	02.2	25	01.8	18	01.6	19	01.8	03	02.7	05	02.6	C6	02.2	C1	66.6	14
II	-	-00.1	02.4	01.0	01.0	03.6	-01.5	08.4	12.11	-07.0	29	07	01.0	30	01.8	11	01.2	15	02.7	01	01.0	09	03.9	05	04.0	03	01.7	08
III	-	02.2	05.9	03.5	03.8	06.4	00.8	16.4	19	-06.6	01	05	02.0	27	01.7	15	01.5	27	02.0	05	02.0	02	01.5	02	04.5	04	02.2	06
IV	-	03.8	06.8	04.5	04.9	08.1	01.4	14.5	29	-01.7	20	.	.	21	07.4	28	01.9	19	02.6	02	02.0	09	05.3	09	03.4	01	03.0	01
V	-	09.2	11.7	09.0	09.7	13.2	05.9	19.4	31	01.1	05	03	03.3	25	02.6	10	01.5	12	02.2	03	02.7	15	03.7	19	03.9	04	03.0	02
VI	-	14.0	17.8	13.4	14.6	19.0	05.8	24.5	27	02.2	11	09	05.0	13	01.7	12	01.9	08	01.0	01	01.0	29	03.3	12	03.7	16	03.8	.
VII	-	17.7	21.9	16.7	18.3	22.7	12.4	28.8	16	04.8	23	01	04.0	24	07.4	22	01.7	09	01.3	01	03.0	05	03.6	06	02.8	07	03.1	04
VIII	-	17.4	22.5	17.0	16.5	23.6	13.8	28.6	06	08.5	13	05	03.6	39	01.3	21	01.7	12	02.2	03	01.7	05	03.4	03	04.0	.	05	
IX	-	13.5	18.0	13.8	14.8	19.0	10.4	26.0	04	01.9	27	04	02.2	23	01.8	16	02.0	16	02.2	01	02.0	13	02.8	08	03.0	C5	03.6	02
X	-	07.0	11.2	08.2	08.5	12.3	05.1	18.5	28	03	04.0	06	01.8	C7	02.4	06	03.7	45	04.8	08	03.6	02	02.0
XI	-	02.6	06.4	03.8	04.2	07.1	01.5	13.7	19	-03.2	02	04	02.2	19	02.2	16	01.7	06	03.0	06	04.5	18	03.2	14	03.9	03	03.0	04
XII	-	-00.4	03.2	00.4	00.9	04.3	10.5	10.5	20	-07.3	20	08	02.5	47	01.8	07	02.3	02	02.5	07	03.1	07	04.0	04	04.0	05	05	
GOD.	-	07.0	10.7	07.4	08.2	11.8	04.4	28.8	4	-VII	46.1	05	02.8	30.9	02.7	162	01.7	164	02.2	36	02.5	153	03.7	59	03.5	50	03.3	57
$\varphi = 41^{\circ}03'N \lambda = 21^{\circ}23'$ E Gr. AG = + 1h 25 min.																												
I	714.3	-00.1	04.3	01.2	01.5	04.9	-01.3	08.0	21	-06.7	16	17	01.8	16	01.9	C2	01.5	04	01.2	11	02.9	05	04.0	02	02.0	11	01.4	21
II	705.0	01.9	06.9	03.8	04.1	08.3	02.9	13.1	12	-03.6	01	02	01.5	21	01.3	C5	01.6	02	01.5	20	03.9	05	03.4	C2	03.0	05	03.2	21
III	711.0	03.9	11.0	06.8	07.1	11.7	02.9	21.4	21	-04.0	02	10	01.6	18	02.1	C4	01.8	03	02.3	26	03.8	10	03.9	05	C4.2	04	01.0	13
IV	707.2	06.2	12.0	08.6	08.6	13.4	04.0	20.1	29	-00.3	10	01	02.0	17	02.8	C6	02.0	02.5	27	03.7	11	02.7	02	01.5	03	04.3	12	
V	708.3	11.5	17.4	12.9	13.6	19.2	07.4	24.2	31	02.0	11	14	02.1	14	02.1	C1	02.0	07	02.1	17	02.8	08	02.4	05	02.6	07	03.9	20
VI	705.0	16.1	23.0	17.6	18.5	24.5	11.6	30.2	27	05.6	15	13	02.8	15	02.1	C1	02.2	15	02.7	04	01.8	C5	03.8	14	04.3	10		
VII	710.9	17.4	27.8	20.2	21.4	29.1	12.0	36.9	17	05.6	10	19	02.1	22	01.5	C3	01.7	06	02.0	08	01.9	05	02.2	04	01.8	09	03.9	15
VIII	711.2	16.8	28.0	20.3	21.4	29.2	13.1	34.7	06	07.1	13	12	02.2	24	01.0	C1	01.0	05	02.8	06	02.5	02	02.0	04	03.3	24		
IX	711.4	12.5	24.0	16.6	17.4	25.0	10.3	32.2	04	03.4	28	18	02.2	07	02.0	C1	01.0	03	03.3	18	02.7	07	02.3	04	02.5	09	02.9	23
X	706.1	08.3	17.0	11.4	12.1	18.5	05.5	24.0	05	-03.6	28	11	02.5	C1	01.0	14	03.4	27	04.0	10	03.4	C9	03.2	07	02.4	12		
XI	712.3	02.2	09.4	05.4	05.6	10.2	01.4	16.2	28	-03.3	04	16	01.9	05	01.8	C4	01.5	07	02.0	10	03.5	04	01.0	07	02.6	07	03.3	30
XII	712.6	-03.8	02.0	-02.2	-01.6	03.1	-05.8	12.2	04	-15.7	18.17	29	01.9	08	01.6	C2	01.0	05	02.2	07	02.1	01	0.0	04	0.0	05	01.7	32
GOD.	710.4	07.7	15.2	10.2	10.8	16.4	05.2	36.9	IT-VII	-15.2	18.0	177	02.1	164	04.2	32	01.6	63	03.3	195	03.2	76	02.9	54	02.7	91	03.1	24.3
$\varphi = 41^{\circ}57'N \lambda = 21^{\circ}38'$ E Gr. AG = + 1h 27 min.																												
I	746.9	00.3	05.6	01.6	02.3	06.5	-00.9	10.1	22	-07.7	15	14	03.1	C8	02.0	07	01.4	12	01.8	01	01.0	04	01.0	11	02.4	25		
II	746.7	C2.3	08.9	04.6	05.1	10.4	01.1	14.6	11	-06.5	02	12	02.9	08	02.4	C7	01.0	19	02.1	10	02.9	02	01.0	03	01.6	08	02.0	18
III	742.6	03.9	13.0	07.6	08.0	14.0	02.2	22.6	22	-05.4	01	10	02.3	13	02.2	C6	01.5	22	02.3	14	02.4	02	02.0	05	01.6	06	01.6	16
IV	738.4	07.0	14.9	10.1	15.8	22.0	04.5	22.0	27	-06.4	04	10	03.0	14	07.6	C7	01.3	21	02.4	11	02.5	01	01.0	06	01.0	06	01.0	16
V	738.8	11.8	19.2	13.9	14.7	21.0	08.5	26.7	31	01.8	11	16	02.6	C9	04.3	06	01.3	13	02.4	08	01.0	03	01.0	C3	02.0	00	01.9	22
VI	735.6	16.9	24.2	19.3	20.6	26.4	17.7	32.1	29	05.2	15	16	02.5	C5	02.5	07	01.9	14	01.9	01	01.0	06	03.0	10	02.8	18		
VII	741.0	18.3	26.5	20.4	22.2	29.6	13.3	37.0	17	06.9	10	11	03.4	11	07.7	C7	01.3	10	01.5	09	01.3	01	01.2	01	02.0	05	02.2	25
VIII	741.2	16.5	24.6	22.1	23.1	30.8	15.0	36.2	05	11.0	14	15	01.6	C2	14	06.6	C7	01.7	06	02.1	06	01.5	08	02.0	05	02.4	21	
IX	741.5	13.6	25.1	17.3	18.3	26.1	11.4	33.0	04	01.4	28																	

Mjesec	Oblačnost Nm (0-10)			Insolacije broj sati	Vlažnost vazduha			Padavine R mm		Broj dana u nizu:																										
	7	14	21		e _m	U _m	%		Max	Dat.	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	▲	R	T	M								
					mm	7	14	21	Stred.	Min							≤	<	<	IV	IV	IV	IV	IV	IV	IV	IV									
KRUŠEVO																																				
BR. ST.266																																				
I	7.1	7.2	4.6	6.3	-	03.8	90	87	88	88	55	C65	C15.7	03	01	07	28	•	•	C3	•	09	12	16	09	03	05	14	•							
II	7.0	7.8	7.1	7.3	-	04.3	89	84	87	87	43	132	C30.4	05	•	05	20	•	•	03	01	05	18	17	13	04	07	15	02	•						
III	6.9	7.1	6.4	6.8	-	04.9	86	77	81	81	40	067	C12.5	28	•	01	18	•	•	05	16	16	13	01	02	14	•	•	02	20	•					
IV	6.6	6.4	5.9	7.0	-	05.3	84	78	79	80	51	094	C16.5	16	•	•	05	•	•	02	•	•	13	17	12	06	04	•	•	01	03	12	01			
V	5.6	7.1	5.6	6.2	-	07.1	75	74	79	77	55	130	C33.7	06	•	•	•	•	•	07	•	C3	06	15	15	04	15	•	•	•	03	05	•			
VI	4.7	6.2	4.3	5.1	-	08.9	72	66	71	76	43	085	C023.5	19	•	•	•	•	•	03	•	C3	06	12	07	04	12	•	•	•	01	04	C3			
VII	1.2	4.5	1.1	2.3	-	10.5	66	57	67	63	25	006	G02.8	18	•	•	09	•	01	01	•	15	03	02	03	02	•	•	•	02	•	•				
VIII	2.7	4.5	2.4	3.2	-	13.4	63	78	83	81	98	051	C23.2	26	•	•	14	•	•	02	•	11	C1	07	05	02	07	•	•	•	11	•	•			
IX	3.5	4.6	2.2	3.4	-	09.2	78	62	72	71	35	049	C21.0	27	•	•	01	•	•	03	•	11	01	06	04	02	06	•	•	•	02	C1	•			
X	6.2	6.9	4.4	5.9	-	06.4	79	69	74	74	42	116	C031.5	22	•	•	04	•	•	13	02	C2	08	19	17	03	17	04	•	•	•	01	04	•		
XI	5.5	5.7	4.6	5.2	-	05.0	86	74	82	81	38	097	C031.3	08	•	•	05	•	•	03	•	06	10	12	08	03	10	02	•	•	•	08	01	•		
XII	5.2	5.0	4.5	4.9	-	03.6	76	71	75	74	35	058	C19.4	15	•	03	25	•	•	02	•	05	08	08	07	01	02	07	•	•	•	05	•	•		
GOD.	5.2	6.3	4.4	5.3	-	06.9	81	73	78	77	25	950	C033.7	00V	01	16	105	24	•	01	43	03	75	101	148	112	30	103	60	07	•	•	02	34	160	•
BITOLA																																				
BR. ST.267																																				
I	6.6	6.8	5.2	6.3	09C.5	04.4	89	75	87	84	48	049	C010.1	25	•	•	20	•	•	C7	•	06	11	10	09	01	08	06	04	•	•	•	C3	C3		
II	7.0	7.2	6.4	6.9	082.4	05.0	89	69	84	81	37	119	C027.1	18	•	•	11	•	•	11	01	05	•	•	09	04	15	05	04	•	•	03	01	01	01	
III	6.7	6.5	5.7	6.3	139.0	05.6	87	60	78	75	31	051	C11.0	15	•	•	03	•	•	11	•	06	11	01	13	02	01	•	•	01	•	•	01			
IV	6.7	6.2	6.3	7.0	158.5	06.2	85	60	74	73	33	050	C06.4	19	•	•	01	•	•	11	01	01	11	16	13	•	14	•	•	03	•	•	•			
V	5.5	7.1	6.2	6.2	233.7	08.3	81	57	74	71	34	066	C024.8	30	•	•	•	•	•	14	01	C3	09	13	10	02	13	•	•	•	04	•	•			
VI	5.8	6.2	4.6	5.2	288.0	10.5	78	52	69	66	27	048	C029.8	17	•	•	16	01	•	19	01	03	08	06	01	08	06	04	•	•	07	01	•	•		
VII	1.7	4.0	2.6	2.8	369.3	10.1	71	35	57	55	24	001	C000.7	22	•	•	26	17	•	11	•	14	01	01	•	01	•	•	•	•	•	C2	•	•		
VIII	3.2	4.4	3.6	3.7	316.5	11.7	79	65	61	62	24	044	C25.4	25	•	•	25	16	•	05	•	09	02	05	04	02	05	•	•	04	•	•	04			
IX	3.4	4.5	2.9	3.7	245.2	09.8	88	64	70	67	31	015	C008.8	27	•	•	17	03	•	C9	01	10	C1	03	03	01	•	•	•	04	•	•	•			
X	5.5	6.0	4.5	5.5	166.0	07.4	86	52	71	70	25	055	C12.5	21	•	•	03	•	•	21	05	04	06	16	15	01	16	•	•	02	•	•	•			
XI	6.7	6.6	6.4	6.4	101.6	05.0	85	69	86	81	25	070	C036.6	08	•	•	11	01	•	07	02	05	11	15	08	02	11	•	•	12	•	•	12			
XII	7.1	5.2	6.4	6.2	098.7	03.7	90	77	88	85	51	059	C021.2	15	09	08	26	•	•	05	01	03	12	07	05	03	16	04	03	•	11	17	•			
GOD.	5.7	5.1	5.5	5.5	2291.4	07.3	84	57	75	72	24	627	C034.8	08X	•	•	64	105	40	•	117	11	69	107	120	74	16	116	10	04	•	•	01	46	30	05
TRUBAREVO																																				
BR. ST.269																																				
I	5.4	6.6	5.3	6.8	-	04.9	87	79	88	84	56	C29	C06.2	11	•	•	15	•	•	03	•	14	08	06	•	06	02	•	•	•	03	02	•			
II	8.1	6.1	5.6	6.8	-	05.0	87	69	85	80	41	056	C023.3	16	•	•	10	•	•	10	•	05	14	06	06	02	04	•	•	•	04	•	•			
III	7.2	6.2	5.5	6.3	-	06.8	87	68	82	79	50	C31	C009.7	29	•	•	05	02	•	07	•	05	14	06	06	02	02	02	•	•	02	•	•	02		
IV	6.9	7.2	6.0	6.7	-	07.5	84	68	82	78	44	050	C021.0	15	•	•	01	•	•	01	•	01	10	06	06	01	06	•	•	01	04	•	•			
V	5.7	7.3	5.6	6.0	-	195.9	08.9	86	53	76	72	30	092	C025.8	16	•	•	04	•	•	10	02	03	05	17	13	03	17	•	•	09	02</				

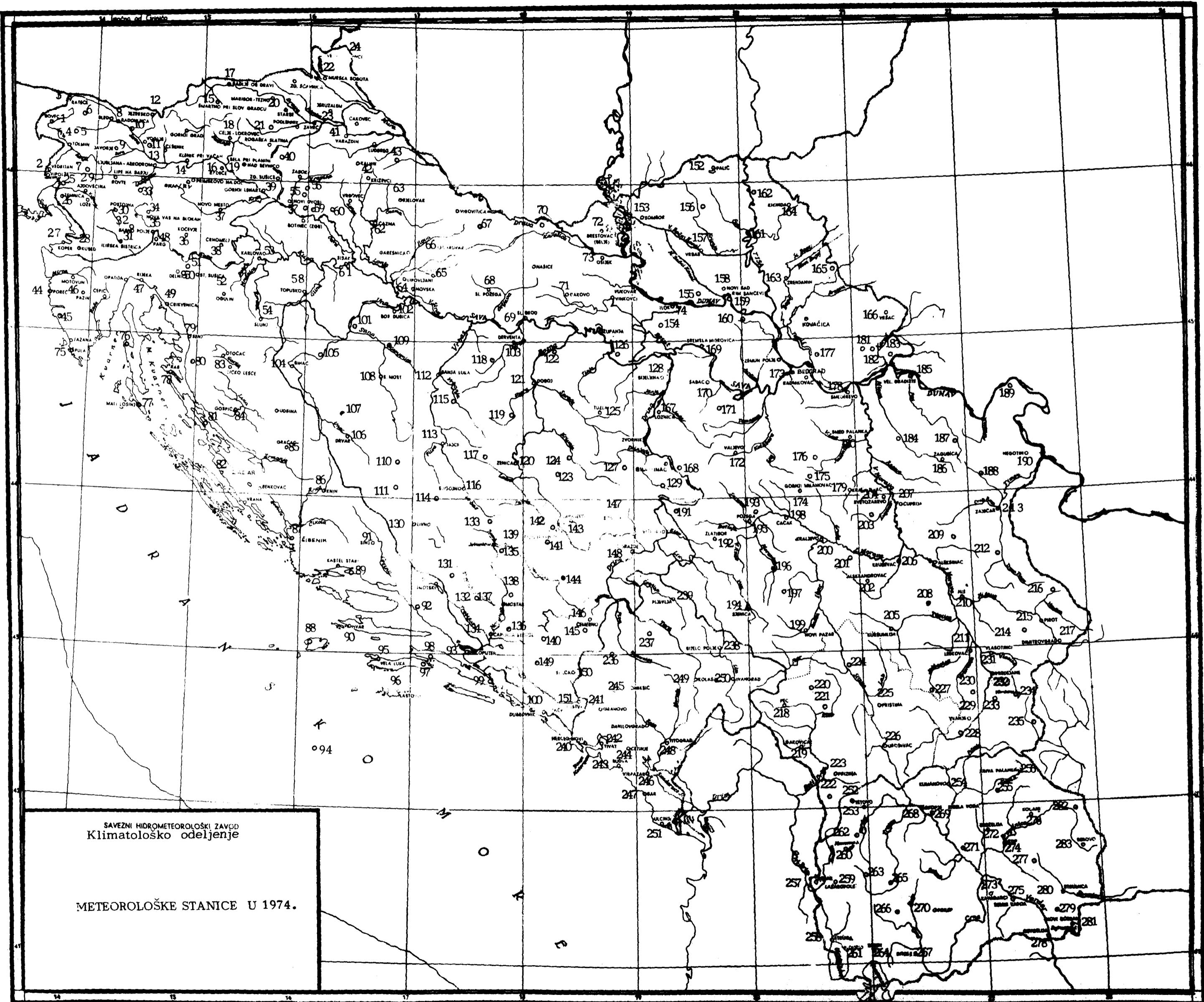
Mesec	Vazdušni Pritisak Fm mb	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, Fm (0-12)																
		Tm			Max	Min	Mx	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW			
		7	14	21							8.	13.	8.	13.	8.	13.	8.	13.	8.	13.	8.	13.	8.	13.	8.	13.		
$\varphi = 41^{\circ}43'N \lambda = 21^{\circ}46'E$ Gr. $\Delta G = + 1h 27 min.$																												
I	-	01.7	06.5	02.8	03.5	07.4	00.4	10.8	29 -07.0	15	.	.	C1	02.0	.	.	11	02.8	.	.	07	01.4	.	.	46	02.3	28	
II	-	03.2	10.1	05.7	06.2	10.9	02.4	14.8	06 -04.8	02	01	02.0	04	01.5	.	.	19	02.5	.	.	09	01.8	.	.	32	01.9	19	
III	-	05.2	13.8	09.0	09.2	14.5	04.2	25.6	21 -04.8	02	.	.	11	01.6	.	.	27	03.4	.	.	05	03.0	.	.	31	02.4	19	
IV	-	08.0	15.5	10.7	11.2	16.8	06.0	22.6	29 06.6	10	01	01.0	09	01.9	.	.	21	02.7	.	.	11	01.8	.	.	32	02.4	17	
V	-	13.5	20.4	15.4	16.2	22.0	10.4	26.2	31 05.5	06	.	.	03	01.7	.	.	C5	02.2	.	.	11	02.7	.	.	35	02.9	14	
VI	-	18.4	25.6	19.9	20.9	26.9	14.3	33.0	29 07.5	15	.	.	03	04.2	.	.	12	07.6	.	.	08	04.0	.	.	26	03.4	41	
VII	-	19.9	29.4	22.0	23.3	30.5	15.1	37.6	16 10.2	09	.	.	04	02.0	.	.	C5	01.8	.	.	02	01.5	.	.	32	02.9	40	
VIII	-	20.4	30.7	25.0	24.3	31.6	11.0	37.5	05 13.2	13.11	.	.	03	01.0	.	.	08	01.5	.	.	06	02.3	.	.	31	02.6	45	
IX	-	15.6	25.9	18.4	19.6	26.8	13.0	33.6	04 04.8	29	.	.	04	01.0	.	.	11	01.9	.	.	06	02.0	.	.	20	02.4	44	
X	-	10.1	19.7	12.7	13.8	20.7	07.2	30.0	08 -02.5	28	.	.	01	01.0	.	.	14	02.7	.	.	16	02.6	.	.	14	02.9	44	
XI	-	04.2	11.4	06.2	07.0	12.1	02.9	17.2	06 -03.0	30	.	.	03	01.0	.	.	C6	01.7	.	.	16	01.9	.	.	18	02.8	40	
XII	-	00.0	06.8	02.1	02.8	07.9	-01.2	12.6	13 -07.0	25	.	.	02	01.0	.	.	03	01.3	.	.	05	02.4	.	.	26	03.6	47	
GOD.	-	10.0	18.0	12.3	13.2	19.0	01.6	37.6	le VII -07.0	25	00	02	01.5	45	01.6	.	.	146	02.6	.	.	102	02.2	.	.	343	02.6	457
$\varphi = 41^{\circ}50'N \lambda = 22^{\circ}02'E$ Gr. $\Delta G = + 1h 28 min.$																												
I	-	C1.0	06.0	02.2	02.8	06.9	-00.9	10.5	22 -09.0	16	.	.	C1	02.0	.	.	02	02.0	.	.	02	02.5	.	.	19	03.5	69	
II	-	03.3	10.1	04.8	05.7	10.9	01.4	14.5	06 -06.4	02	01	02.0	01	02.0	01	03.0	09	02.6	01	06.0	01	03.0	.	.	11	02.5	59	
III	-	05.2	13.6	07.3	08.4	14.4	02.8	24.6	21 -05.0	02	.	.	02	01.5	.	.	19	01.9	.	.	02	02.5	.	.	12	02.8	60	
IV	-	07.9	15.1	09.0	10.3	16.3	04.3	22.5	29 -01.5	10	.	.	02	01.5	.	.	17	02.6	.	.	02	01.0	.	.	17	02.0	54	
V	-	12.8	20.1	13.8	15.1	21.2	09.1	28.0	31 02.5	11	.	.	02	01.0	.	.	05	02.4	.	.	03	02.3	.	.	25	03.3	40	
VI	-	17.7	25.8	17.8	19.8	26.5	11.7	32.2	28 05.5	15	01	04.0	01	04.0	01	03.0	07	03.7	01	02.0	22	04.8	57	
VII	-	18.2	28.9	20.6	22.1	25.9	13.4	37.4	17 06.8	10	05	04.0	01	04.0	01	03.0	01	03.0	03	02.0	20	04.8	49	
VIII	-	18.8	30.5	21.0	23.2	31.3	15.2	36.8	05 10.6	31	04	02.5	01	03.0	.	.	01	03.0	03	02.0	14	03.5	70	
IX	-	14.1	26.2	17.3	18.7	26.8	11.2	34.0	04 03.0	28	.	.	01	01.0	.	.	17	04.6	C2	04.0	01	03.0	.	.	01	02.0	63	
X	-	10.6	19.1	12.0	13.4	20.0	06.5	26.0	08 -04.5	26	.	.	C1	05.0	.	.	C3	04.3	.	.	01	03.0	.	.	07	05.4	74	
XI	-	04.2	10.3	06.5	06.9	10.8	01.6	15.0	13 -03.5	30	.	.	01	01.0	.	.	-	-	-	-	-	-	-	-	-	-		
XII	-	01.1	06.6	03.6	03.8	07.4	-00.3	12.5	13 -07.0	24	.	.	02	01.0	.	.	-	-	-	-	-	-	-	-	-	-		
GOD.	-	09.6	17.7	11.4	12.5	18.5	06.3	37.4	le VII -05.0	00.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 41^{\circ}26'N \lambda = 22^{\circ}02'E$ Gr. $\Delta G = + 1h 26 min.$																												
I	-	01.1	06.1	03.0	03.3	06.4	-00.7	09.8	03 -07.5	16	05	02.4	17	01.1	C1	01.0	01.0	C1	01.0	.	.	27	01.0	47				
II	-	04.5	10.3	05.9	06.6	10.6	02.2	15.2	17 -02.3	11	07	04.0	05	01.4	05	02.8	13	01.5	04	01.0	11	01.2	02	01.5	16	01.6	26	
III	-	06.7	13.5	09.2	09.6	13.8	04.3	24.5	21 -03.5	02	01	01.7	16	01.5	10	04.0	11	01.5	05	01.0	04	01.0	03	03.3	23	01.1	30	
IV	-	09.0	15.4	11.0	11.6	16.3	05.6	23.0	30.27 01.8	04	02	01.5	11	02.0	08	01.2	01	01.0	02	01.0	.	.	27	01.7	22			
V	-	14.5	20.7	15.8	16.7	21.8	09.4	27.0	31 05.8	17	02	03.5	07	01.4	C4	02.2	02	01.0	04	01.0	07	01.6	.	.	32	01.6	47	
VI	-	19.3	26.0	20.5	21.6	27.1	14.6	33.1	29 08.5	13	02	03.0	08	01.5	05	02.0	06	01.2	07	01.8	.	.	29	01.4	57			
VII	-	21.3	30.0	23.2	24.4	30.6	15.3	37.6	17 10.0	10	02	01.0	05	01.8	C3	02.0	03	01.0	05	01.0	03	02.0	01	01.0	25	01.7	47	
VIII	-	21.0	31.0	23.9	25.0	31.4	17.4	36.8	04 11.9	13	01	01.0	03	02.0	C2	03.0	04	01.0	02	01.0	06	01.0	.	.	23	02.1	54	
IX	-	16.2	25.7	18.8	19.9	26.2	12.8	29.6	10 06.5	28	.	.	08	02.2	.	.	06	01.6	01.0	01.0	03	01.7	01	01.0	20	01.6	51	
X	-	12.3	20.7	14.7	15.6	21.1	09.3	26.6	23 -01.1	28	.	.	12	01.3	C2	01.5	01.5	02	01.3	12	01.5	01	01.0	18	01.2	37		
XI	-	05.4	11.2	07.3	07.8	11.7	04.1	16.0	06 -00.6	04	02	01.0	10	01.4	C5	01.8	04	01.0	03	01.3	06	01.2	.	.	19	01.4	41	
XII	-	01.1	06.1	02.0	03.2	04.2	-01.3	12.0	04 -06.4	25.18	02	01.0	02	01.0	.	.	09	01.1	01	01.0	06	01.0	.	.	12	02.1	41	
GOD.	-	11.0	18.1	13.0	13.8	18.6	07.8	37.6	le VII -07.0	00.1	23	02.1	10.2	01.5	47	C2.1	75	01.2	30	01.1	73	01.4	08	02.0	266	01.5	411	
$\varphi = 41^{\circ}45'N \lambda = 22^{\circ}11'E$ Gr. $\Delta G = + 1h 29 min.$																												

Meseč	Oblačnost Nm (0-10)			Insolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sata:																			
	7	14	21		e m	U m	t	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	R	T	≡	■			
					mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm					
TITOV VELES																														
BR. ST.271																														
I 9.7 6.1 8.7 6.8	-	04.6 86 76 86 81 41	034 009.5	01	.	.	12	.	.	.	01	.	.	23	07	07	•	07	02	.				
II 7.2 6.1 7.2 7.0	-	05.4 84 62 78 75 29	030 031.3	16	.	.	09	.	.	C1	01	.	13	07	07	02	07	01	.					
III 6.7 6.3 7.2 6.7	-	06.1 86 55 74 71 27	022 007.5	06	.	.	03	02	.	C6	01	C6	17	11	C5	•	11	01	.					
IV 6.3 7.6 6.8 6.9	-	06.7 80 52 69 67 23	023 009.4	15	17	08	04	•	08	01	.					
V 6.5 7.1 6.3 6.6	-	05.9 80 70 76 72 33	074 C23.0	16	.	.	07	.	.	07	.	03	10	13	08	02	13	04	.					
VI 5.0 5.5 5.5 5.3	-	11.3 73 46 65 61 24	079 C30.0	19	.	.	22	07	.	C2	01	C1	06	08	08	04	08	02	.					
VII 2.8 3.0 3.8 3.2	-	11.3 67 34 56 53 23	010 006.6	08	.	.	27	17	01	C2	01	13	C2	01	03	02	03	02	.					
VIII 4.0 2.4 4.0 4.5	-	11.6 68 35 58 54 20	022 C11.0	24	.	.	29	21	02	C1	•	06	02	05	04	01	05	01	.					
IX 6.1 4.5 4.9 5.2	-	11.1 84 43 72 66 27	026 017.5	08	.	.	25	05	.	01	.	05	06	02	01	02	02	01	.					
X 7.4 7.0 5.4 6.6	-	06.3 82 51 75 70 28	052 C14.1	24	.	.	01	04	01	C2	•	08	12	09	02	12	05	.					
XI 9.3 6.5 7.5 7.8	-	06.2 91 67 86 81 35	027 C12.0	01	.	.	05	.	.	C2	•	16	05	04	01	05	05	.					
XII 6.8 5.6 7.4 6.6	-	04.6 85 66 88 81 31	022 C14.7	15	.	.	20	.	.	03	01	02	13	03	03	01	02	02	01	C2					
GOD. 6.6 6.6 6.3 6.3	-	08.1 81 53 74 69 20	471 C31.3	40.0	.	.	50	117	51	03	32	04	39	133	84	62	14	82	02	11	11	02			
ERDŽEĐELJA																														
BR. ST.272																														
I 6.7 6.3 5.4 6.1	-	05.2 90 65 90 88 56	039 C05.6	24	.	.	18	.	.	01	.	06	13	10	07	•	08	C2	01	C1	01				
II 6.0 5.5 5.2 5.6	-	06.2 91 80 87 96 47	100 C24.6	16	.	.	09	.	.	C1	•	C7	C9	C7	06	05	C7	01	.					
III 5.4 4.9 5.3 5.2	-	07.1 87 73 96 82 45	032 C14.6	07	.	.	05	.	.	01	•	12	14	10	06	01	10	C1	C1	01	.					
IV 5.0 5.7 4.9 5.2	-	08.3 86 83 86 85 45	049 C20.5	15	.	.	04	.	.	01	01	08	09	11	04	02	11					
V 6.0 6.5 5.6 6.0	-	11.3 88 85 85 84 47	087 025.0	14	.	.	03	.	.	01	.	03	10	15	10	03	15	01	.					
VI 2.8 3.3 4.2 3.5	-	12.8 62 51 74 72 33	052 040.0	2.	.	.	23	01	.	C5	01	14	C5	C6	05	02	06					
VII 1.5 2.3 1.5 1.7	-	13.7 63 51 74 70 25	008 077.9	09	.	.	26	17	.	C5	•	22	C2	C2	01	02	C2					
VIII 2.3 3.0 1.3 2.2	-	-	-	-	025 C21.2	25	.	26	21	.	C2	•	15	C1	C2	02	01	C2				
IX 1.1 2.6 1.6 1.8	-	-	-	-	-	045 016.5	06	.	.	23	03	.	•	20	C2	C4	C5	C2	06			
X 5.4 5.4 4.0 5.0	-	10.3 86 78 83 82 47	037 C14.6	15	.	.	02	04	.	C2	•	06	C1	C6	09	08	01	09	01	.					
XI 8.3 6.0 5.9 6.8	-	06.7 92 84 88 89 25	032 C23.0	04	.	.	07	.	.	C1	02	C2	14	04	04	01	04	13	.						
XII 6.2 5.8 5.8 5.9	-	-	-	-	-	013 C05.4	15	.	17	.	04	04	08	14	04	04	04	02	03	01	.	.	.	05	03					
GOD. 4.7 4.8 4.2 4.6	-	-	-	-	-	519 C30.0	021	.	62	107	44	.	23	08	125	101	86	47	16	83	04	03	.	.	01	01	21	04		
KAVADARCI																														
BR. ST.273																														
I 6.8 5.6 6.1 6.2	-	05.3 90 E3 91 P8 67	039 C08.7	24	.	.	19	.	.	07	16	11	C5	•	07	06	03						
II 6.2 5.7 5.5 5.8	-	06.7 91 82 91 E3 35	089 C08.7	16	.	.	09	.	.	C4	10	09	C7	C3	05	04	05	04	01	.					
III 5.6 5.3 5.8 5.6	-	06.9 89 66 H2 79	014 C05.1	07	.	.	03	.	.	09	13	C4	04	05	04	05	04					
IV 5.6 6.8 7.2 6.6	-	08.1 88 67 80 78 28	030 006.0	19	02	12	10	08	•	10						
V 5.4 6.4 6.4 6.0	-	10.8 81 66 77 75 34	076 C20.0	19	.	.	04	.	.	C1	•	04	09	14	12	03	14	01	.						
VI 3.6 4.9 5.1 4.5	-	12.0 69 51 65 62 33	058 C02.5	19	.	.	23	07	.	C1	•	C7	C3	C8	06	02	C6	06	01	.						
VII 1.5 2.9 2.5 2.3	-	11.9 62 40 57 52 30	031 C02.3	07	.	.	20	20	.	•	18	03	03	01	03	01	03	01	02						
VIII 3.0 3.0 3.3 3.1	-	11.7 65 37 49 50 23	050 C04.3	28	.	.	31	21	02	•	01	16	C2	C4	03	02	04	04	01	.					
IX 2.9 3.6 3.9 3.5	-	11.2 78 51 62 64 34	026 012.7	08	.	.	24	.	.	•	14	C3	05	04	01	05	04	01					
X 3.6 4.5 4.3 4.1	-	08.1 73 47 62 60 26	025 006.9	21	.	.	01	04	.	•	11	C5	06	07	06	06	07	06	02	.					
XI 7.1 6.2 6.1 6.5	-	06.2 86 67 79 77 43	043 021.1	08	.	.	05	01	.	•	07	14	09	06	02	05	04	02	02	.					
XII 6.3 6.5 5.5 5.6	-	04.6 88 66 78 75 51	043 016.4	15	.	.	21	01	.	•	08	04	15	08	05	02	06	06	05	03					
GOD. 5.1 5.6 4.3 5.0	-	250.6 09.9 80 84 61 21	052 C31.0	08	.	.	22	C4	.	•	09	02	13	C1	04	02	02	04	C4	.					
V 5.0 5.5 5.5 5.5	-	179.1 07.9 74 79 62 63 25	063 C22.5	22	.	.	01	01	.	•	16	02	C3	C5	11	05	03	11	04	01	04					
XI 7.1 6.2 5.5 5.4	-	122.0 06.1 86.1 70 76 84 82 41	040 016.4	08	.	.	02	02	.	•	08	04	15	08	05	02	06	06	12	.					
XII 5.5 5.9 5.5 5.6	-	104.3 04.4 51 69 85 82																												

Mesec	Vazdušni pritisak Pr. mbar	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta nD, fm (0-12)																				
		Tm				Dat.				N			NE		E		SE		S		SW		W		NW		C			
		7	14	21	Sred. (dies)	Max	Min	Max	Dat.	Min	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
$\varphi = 41^{\circ}55'N \lambda = 22^{\circ}25'E$ Gr. AG = + 1h 30 min.																														
I	-	00.5	05.9	02.6	02.9	06.3	-06.6	10.0	03	-06.8	16	26	C2.7	C3	02.0	.	.	.	12	02.2	07	02.1	45	
II	-	03.3	10.1	05.9	06.3	11.0	01.8	15.5	18	-03.5	02	17	C2.7	C3	03.0	C1	02.0	.	.	C4.2	01	02.0	33	
III	-	05.3	13.3	09.3	09.3	14.0	03.6	24.0	21	-02.0	02	24	C2.5	C7	02.4	.	.	.	C4.7	02	02.0	02	02.0	36	
IV	-	07.2	15.1	10.5	10.8	15.6	04.5	23.5	30	06.6	20	29	C2.9	C1	03.1	.	.	.	19	03.1	32	
V	-	12.6	19.4	14.9	15.5	20.4	09.6	27.2	31	04.5	11	28	C2.6	C6	02.5	.	.	.	15	02.9	02	02.5	42	
VI	-	16.9	24.9	19.1	20.0	25.6	13.7	31.2	27	07.6	13	24	C3.0	C3	02.0	.	.	.	16	C2.2	*	39	
VII	-	18.3	26.4	22.2	22.8	29.0	14.3	35.5	16	09.0	10	16	C2.9	C1	07.0	.	.	.	17	01.2	02	02.0	57		
VIII	-	19.2	29.7	25.2	25.8	30.2	16.4	34.5	08.0	11.5	31	16	C2.2	C5	02.8	.	.	02	03.5	14	02.3	01	03.0	.	.	01	03.0	54		
IX	-	13.5	25.2	18.5	18.9	26.0	11.6	32.0	04	02.5	28	24	C2.7	C1	03.0	.	.	.	14	02.4	01	02.0	50		
X	-	10.4	19.2	14.4	14.6	20.1	08.1	24.8	23	-03.2	28	26	C2.6	C1	03.0	.	.	.	C4.2	0.8	01	C2.0	44		
XI	-	03.6	11.4	06.8	07.1	12.0	02.2	17.0	06	-02.0	03	13	C2.2	C4	02.7	.	.	.	07	02.6	01	02.0	66		
XII	-	-00.3	06.3	01.9	02.5	06.9	-01.8	12.5	26	20	C2.6	C3	02.0	C5	02.0	02	03.5	01	02.0	.	.	.	62			
GOD.	-	09.2	17.4	12.4	12.9	18.1	07.0	35.5	KGW	-06.8	KGW	271	C2.7	C6	02.6	C1	02.0	02	03.5	191	02.6	20	02.3	03	02.0	01	03.0	50		
$\varphi = 41^{\circ}38'N \lambda = 22^{\circ}27'E$ Gr. AG = + 1h 30 min.																														
I	-	00.8	05.0	01.9	02.4	05.7	00.0	05.5	30	-06.5	16	12	C6.2	C1	03.0	28	C1.6	C3	01.7	C1	03.0	.	.	19	02.1	14	C4.3	15		
II	-	03.4	05.1	05.0	05.7	09.7	02.0	15.0	16	-03.0	28	04	C4.0	.	.	20	C2.2	C8	03.1	C4	02.0	.	.	22	02.4	06	C4.3	20		
III	-	05.1	12.1	07.5	06.1	13.0	04.1	24.0	23	-02.5	02	10	C4.4	.	.	24	C4.0	10	02.0	10	02.7	01	01.0	14	02.4	06	C3.0	19		
IV	-	07.1	13.9	09.1	09.6	15.1	05.1	21.5	30	01.9	20	09	C5.1	.	.	25	C2.2	11	C3.1	C7	C3.3	01	02.0	12	C4.4	14	04.9	11		
V	-	12.3	18.7	13.6	14.6	20.3	05.5	25.5	31	05.2	06	08	C4.5	C2	03.0	17	C1.1	C8	03.0	C3	02.0	04	03.2	19	02.1	16	C4.6	16		
VI	-	17.0	23.9	17.9	19.2	25.7	13.5	31.5	29	07.1	13	09	C5.1	C1	03.0	10	C2.0	C6	03.2	C2	02.5	25	03.3	21	04.3	12				
VII	-	19.4	28.5	21.0	22.5	29.7	15.1	37.5	17	09.7	10	16	C4.1	C1	03.0	14	C4.8	C6	03.0	C1	03.0	23	03.1	14	C5.1	29				
VIII	-	19.9	24.9	21.9	23.1	30.2	16.7	36.0	05	12.2	31	15	C3.1	C1	03.0	14	C2.8	C5	03.7	C5	03.8	03	03.7	16	03.2	09	04.8	27		
IX	-	14.8	24.8	17.4	18.6	25.6	12.5	31.5	03	06.0	28	05	C2.6	C2	01.0	13	C2.2	C3	04.6	C4	02.5	07	03.3	20	02.8	03	05.7	33		
X	-	10.5	15.7	12.9	13.6	19.1	08.8	24.4	15	-01.7	28	07	C0.4	03	02.3	23	C0.0	C8	03.4	C3	03.0	.	.	10	01.9	08	02.5	21		
XI	-	04.7	11.2	06.2	07.1	11.9	03.4	15.4	06	-06.6	03	10	C3.4	.	.	17	C1.7	C3	02.8	C4	04	04.0	.	.	22	02.2	10	03.6	24	
XII	-	01.0	05.8	02.1	02.8	07.0	-06.6	12.1	04	-05.5	18	25	C0.4	.	.	05	C1.4	C1	01.0	05	02.0	01	01.0	.	.	27	03.0	15	C3.6	19
GOD.	-	09.7	16.6	11.4	12.3	17.8	07.5	37.5	KGW	-06.5	KGW	170	C0.4	11	C2.6	110	C1.4	C5	C2.4	80	02.2	79	02.3	37	02.4	02	04.0	325	03.5	446
$\varphi = 41^{\circ}09'N \lambda = 22^{\circ}30'E$ Gr. AG = + 1h 30 min.																														
I	-	02.2	07.8	03.7	04.3	08.6	00.5	12.3	28.20	-06.6	15	15	C8.8	C2	01.5	C3	01.5	C7	04.3	C8	01.5	04	02.0	.	.	.	19	C4.5	37	
II	-	04.2	10.6	06.3	06.8	11.0	02.6	16.8	11	-06.4	02	09	C5.4	.	.	C1	03.0	19	C1.5	C3	01.7	08	01.5	01	02.0	18	03.2	25		
III	-	05.3	13.3	08.6	09.6	14.1	03.4	24.0	21	-04.4	02	07	C5.9	02	01.5	01	01.0	35	C1.6	07	01.9	06	01.0	04	01.8	09	C3.3	27		
IV	-	08.6	15.4	10.6	11.2	16.6	05.6	22.4	27	-06.3	10	09	C5.6	C1	01.0	06	01.0	38	C1.7	C6	01.8	03	02.0	.	.	.	11	03.9	16	
V	-	14.9	21.8	15.5	16.9	23.0	10.6	27.4	14	03.5	06	10	C2.1	C4	01.2	C5	01.0	16	C1.6	C6	01.4	01	02.0	02	02.5	19	01.7	22		
VI	-	19.6	26.6	20.2	21.6	27.6	14.0	34.0	29	09.5	15	20	C3.1	C2	02.4	C5	01.2	21	C1.8	C6	01.5	02	02.5	01	01.0	20	03.8	10		
VII	-	21.6	30.8	23.0	24.6	31.7	17.1	37.9	17	07.9	16	12.3	C1.1	C5	01.8	C7	01.1	18	C1.4	C3	01.0	05	01.0	05	01.2	07	04.0	22		
VIII	-	21.0	31.4	23.9	25.0	32.0	17.1	37.4	14	04.4	11	13	C1.3	C2	02.5	C5	01.9	25	C1.5	C6	01.6	06	01.5	06	01.0	08	03.3	13		
IX	-	16.2	26.8	18.1	19.8	27.5	12.7	32.1	03	03.6	29	06	C2.7	C4	02.6	C5	01.6	24	C1.6	C3	02.3	16	02.2	30	
X	-	11.0	21.4	13.3	14.8	22.1	08.2	27.1	16	-01.0	31	07	C3.0	C1	03.0	06	C1.2	26	C1.9	C3	C1.0	03	01.0	05	C2.6	31				
XI	-	04.7	13.9	06.7	08.0	14.4	02.6	18.6	14	-06.4	04	09	C3.6	03	03.3	C5	01.6	20	C1.2	C3	01.0	05	01.2	05	01.4	07	03.4	20		
XII	-	02.1	09.0	04.7	05.3</td																									

Mesec	Vazdušni pritisak: P ₀ : 1013 hPa	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, Fm (0-12)																
		Tm			Sred. (Dnev.)	Max	Min	Dat.	Min	Dat.	R	BL	E	SE	S	SW	W	NW	C									
		7	14	21																								
$\Delta G = +1h\ 31\text{ min.}$																												
I	-	02.7	06.1	03.4	03.9	06.6	01.2	22	-04.0	15	+	05.5	.	.	15	02.9	25	04.4	53				
II	-	05.2	09.3	04.3	06.8	10.2	03.8	15.0	16.11	-01.5	02	00	05.5	.	.	16	02.6	17	04.7	49			
III	-	06.4	11.6	07.9	08.4	14.6	05.1	22.0	23.21	-01.2	02	.	.	.	19	02.8	08	02.4	66			
IV	-	09.3	14.3	09.6	10.7	15.6	06.9	21.0	13	04.0	10	03	04.3	.	.	11	04.3	18	03.5	50			
V	-	14.6	20.7	14.8	16.2	21.9	11.8	26.7	31	07.6	06	.	.	.	14	03.5	36	03.7	67			
VI	-	19.7	25.8	19.4	21.1	27.2	16.3	34.0	29	05.6	13	.	.	.	08	02.1	.	.	03	01.3	.	.	27	03.7	52			
VII	-	22.0	29.8	22.7	24.2	31.2	17.3	39.4	16	14.0	09	.	.	.	01	07.0	.	.	03	01.7	.	.	35	04.1	54			
VIII	-	24.1	30.5	23.1	24.7	31.8	19.4	36.1	20.03	17.6	22.13	.	.	.	10	07.5	.	.	05	01.8	.	.	01	03.0	23			
IX	-	17.6	25.4	18.3	19.9	24.4	15.4	32.0	C3	05.5	29	.	.	.	C2	02.0	.	.	C4	01.0	.	.	17	03.3	67			
X	-	13.5	19.9	14.7	15.7	20.7	11.9	26.5	24	04.2	31	.	.	.	17	03.2	.	.	C9	02.9	.	.	15	02.9	52			
XI	-	07.4	12.5	06.2	C9.1	13.1	06.2	16.0	14.06	02.5	04	01	03.0	.	.	12	03.5	.	.	01	02.5	04	02.2	34				
XII	-	03.7	08.6	05.0	05.6	C9.6	01.9	14.0	04	-02.0	11	.	.	.	01	01.0	.	.	01	02.0	57	03.8	34					
GOD.	-	12.0	17.9	12.8	13.9	18.9	09.9	39.4	4.01	-04.0	C1.1	66	04.5	.	.	116	03.1	.	.	38	02.4	.	.	02	02.5	297		
$\Delta G = 41^{\circ}38'N \Delta L = 22^{\circ}46'E$ Gr. +1h 31 min.																												
NEVI DEJURAN																												
BR. ST. 281																												
I	-	-01.0	04.2	00.2	06.9	04.8	-03.0	08.6	23	-12.0	16	18	01.8	C3	01.7	C2	01.0	C1	02.0	C5	01.0	02	02.5	56				
II	-	00.4	06.3	02.2	03.4	08.8	-01.9	15.0	16	-06.0	02	15	C2.2	07	04.7	.	08	04.2	01	08.0	06	G2.2	08	01.6	02	01.5	36	
III	-	01.8	11.3	06.4	04.5	12.1	00.4	24.5	22	-08.5	02	20	C1.8	03	02.3	C9	C1.3	04	01.8	09	01.3	02	02.5	08	01.2	04	02.2	34
IV	-	03.9	12.9	07.7	08.1	13.5	01.5	21.5	10	-03.0	04	13	C2.2	08	01.7	10	C1.2	10	03.6	C6	02.7	03	03.7	10	02.4	06	02.7	28
V	-	10.3	17.5	12.5	13.2	18.2	04.2	23.5	26.12	01.5	26.16	07	C2.6	02	01.5	C9	C1.4	C5	03.7	08	C1.8	03	01.7	10	02.5	03	02.0	43
VI	-	15.1	22.3	16.3	17.5	22.6	09.5	24.0	28	03.0	17	06	C2.5	03	03.0	C4	C1.3	08	02.6	06	01.7	12	02.3	11	02.3	04	02.3	44
VII	-	17.0	24.6	17.6	15.8	27.1	10.6	35.5	18	04.0	10	15	C2.4	05	01.0	C4	C1.0	02	02.0	06	C1.5	03	02.4	05	03.0	43		
VIII	-	16.7	27.7	19.9	21.0	28.1	11.3	35.0	06	04.5	11	11	C2.7	08	01.9	06	C2.0	04	03.0	07	C1.7	04	02.2	07	02.0	05	02.4	41
IX	-	12.1	23.6	15.0	16.5	24.0	00.2	31.0	04	-01.5	28	06	02.3	04	04.0	C5	C1.6	06	02.0	18	C1.6	10	02.9	07	02.6	04	01.7	30
X	-	07.7	16.7	10.7	11.4	17.6	04.4	22.5	05	-04.5	28	01	02.0	01	03.0	05	01.2	06	04.8	21	03.0	04	02.8	18	02.0	02	02.5	34
XI	-	01.4	10.8	03.8	04.9	11.2	-02.3	14.6	20	-05.5	17.16	07	C2.7	03	04.0	C6	C1.8	C3	04.0	09	02.3	*	*	15	07.5	04	03.0	43
XII	-	-02.5	05.5	-00.5	06.5	05.9	-04.2	10.5	13	-10.5	25	17	C2.2	03	04.0	C4	C1.0	02	02.5	10	C1.5	*	*	06	01.7	04	C4.5	47
GOD.	-	06.9	15.6	09.4	10.3	16.2	03.4	35.5	35.7	-12.0	C1.1	119	02.2	44	03.2	C3	C1.4	59	03.2	104	02.0	54	02.7	109	02.1	50	C2.5	41
$\Delta G = 41^{\circ}13'N \Delta L = 22^{\circ}51'E$ Gr. +1h 31 min.																												
BERLVC																												
BR. ST. 283																												
I	682.6	-02.6	C2.6	-C1.1	-00.5	03.5	-04.3	09.0	03	-12.7	16	11	C1.8	C3	C1.3	*	*	G3	C1.2	C4	01.8	C2	02.0	*	*	07	01.0	56
II	688.2	-00.8	06.5	01.0	01.9	07.6	-02.5	13.2	12	-08.6	01	17	C1.6	C7	C1.5	*	*	15	02.9	C2	02.5	03	01.7	01	02.0	01	01.0	43
III	690.1	01.4	09.6	03.8	04.6	10.9	-00.5	22.0	21	-08.2	02	11	C1.3	C2	C1.5	*	*	14	01.8	05	01.4	10	01.5	02	01.5	04	01.5	45
IV	684.4	03.8	10.7	C5.2	06.2	12.1	00.3	15.8	10	-05.0	03	16	C1.7	04	02.0	*	*	14	02.6	C2	02.5	09	02.1	02	02.5	05	02.0	40
V	687.5	09.3	15.1	09.8	11.0	17.1	04.8	23.0	31	-00.7	06	15	C1.6	C2	C1.0	*	*	04	02.0	C8	C2.6	C3	C3.0	*	*	07	01.7	54
VI	688.6	13.3	20.3	15.7	15.2	22.0	06.8	27.6	29	01.3	13	19	C1.9	C7	C2.0	*	*	01	02.0	10	01.8	07	02.6	02	03.0	05	02.0	48
VII	690.7	14.4	24.3	15.9	17.7	25.3	09.3	32.4	17	03.4	10	22	C1.6	C2	C1.5	C3	C1.0	01	02.0	01	02.0	06	02.2	04	02.0	14	02.0	43
VIII	691.2	14.9	24.6	16.6	18.2	26.4	10.2	31.6	06	06.5	12	20	C1.7	04	02.0	*	*	03	02.0	04	02.0	02	02.0	01	02.0	07	02.0	57
IX	691.0	05.8	21.5	12.5	14.3	22.9	06.8	26.7	04	-02.0	28	04	C1.0	*	*	*	*											

Mjesec	Oblačnost Nm (0-10)			Insolacija Troj sati	Vlažnost vazduha			Padavine R/mm			Broj dana na sat																											
	7	14	21		mm	m	%	mm	mm	mm	Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R/mm	•	*	*	*	Δ	▲	R	T	≡	■									
	7	14	21								30	0.0	0.0	25.0	0.0	20.0	6	8	2.0	8.0	0.1	1.0	10.0	•	Δ	▲	R	T	≡	■								
BR. ST. 281																																						
I	6.8	6.0	5.0	5.9	-	05.5	91	85	85	88	55	C70	028.0	02	.	.	06	*	*	*	03	*	09	14	08	C8	C2	08	01	01	.	.	.	03				
II	6.6	6.0	5.5	6.1	-	06.4	90	78	86	85	60	C70	C24.0	20	.	.	04	*	*	*	03	*	06	13	06	06	04	06	.	.	.	01	.	.	.			
III	6.7	6.3	6.0	6.3	-	07.6	92	81	91	88	66	070	027.0	07	.	.	01	*	*	*	03	*	08	17	09	09	02	09	.	.	.	01	.	.	.			
IV	6.0	6.5	4.2	5.6	-	08.5	88	79	88	85	52	C66	C31.0	15	.	.	*	*	*	*	05	*	05	09	09	09	02	09	.	.	.	04	.	.	.			
V	6.1	6.0	4.3	5.4	-	11.3	82	71	84	79	49	065	014.3	30	.	.	*	*	*	*	05	*	05	09	08	08	03	08	.	.	.	05	.	.	.			
VI	4.2	4.6	4.6	4.4	-	15.1	81	71	80	77	51	C34	C13.0	17	.	.	*	*	*	*	07	*	09	05	07	07	01	07	.	.	.	01	07	.	.			
VII	1.1	1.5	1.7	1.5	-	16.2	73	61	69	68	42	011	006.3	01	.	.	*	*	*	*	23	*	21	02	02	02	02	02	.	.	.	01	.	.	.			
VIII	3.0	2.6	3.6	3.1	-	16.3	74	58	72	68	41	001	001.0	21	.	.	*	*	*	*	15	*	03	01	01	01	01	01	.	.	.	03	.	.	.			
IX	3.6	3.6	1.4	2.9	-	13.9	82	67	83	77	40	049	031.0	08	.	.	*	*	*	*	15	*	11	04	04	02	04	.	.	.	02	.	.	.				
X	6.4	5.5	3.5	5.1	-	10.9	83	70	84	79	35	036	C21.0	22	.	.	*	*	*	*	08	*	08	04	04	04	01	04	.	.	.	01	.	.	.			
XI	5.5	4.3	4.6	4.8	-	07.8	91	83	90	88	58	110	037.0	06	.	.	*	*	*	*	09	*	08	08	04	08	06	.	.	.	04	.	.	.				
XII	4.5	4.2	4.0	4.2	-	05.6	86	76	62	61	61	C14	C11.0	31	.	.	*	*	*	*	12	*	06	04	02	01	04	.	.	.	01	.	.	.				
GOD.	5.0	4.8	4.0	4.6	-	10.4	84	73	83	80	35	598	C37.0	18	*	*	*	*	*	*	124	*	95	70	68	22	70	01	01	.	.	01	24	07	.	.		
BR. ST. 282																																						
I	7.5	5.4	5.2	6.0	-	04.1	80	76	85	80	51	C44	C15.0	18	02	.	24	*	*	*	*	08	13	13	11	03	06	C5	01	.	.	.	07	.	.	.		
II	6.1	4.9	4.5	5.2	-	04.5	83	60	84	76	34	050	014.5	08	.	.	19	*	*	*	05	02	09	10	05	04	02	05	.	.	.	01	01	.	.			
III	7.2	5.2	6.2	6.2	-	05.3	87	75	77	74	25	050	C18.5	29	.	.	10	*	*	*	08	14	09	08	02	09	05	04	.	.	.	01	01	.	.			
IV	5.5	5.7	3.8	5.0	-	6.1	77	65	75	71	29	021	C06.0	17	.	.	09	*	*	*	01	01	07	07	06	04	06	*	*	*	01	.	.	.				
V	5.7	4.6	5.0	5.3	-	06.3	84	57	76	72	33	101	022.0	06	.	.	*	*	*	*	01	*	04	06	14	13	04	14	.	.	.	07	.	.	.			
VI	4.6	4.4	4.1	4.5	-	10.6	78	55	77	70	33	070	C12.0	02	.	.	*	*	*	*	02	*	06	02	12	11	03	12	.	.	.	04	01	.	.			
VII	3.3	3.1	2.2	2.5	-	12.2	74	54	75	68	31	024	012.0	01	.	.	*	*	*	*	15	*	03	05	05	01	05	.	.	.	01	.	.	.				
VIII	2.3	4.4	2.0	2.9	-	11.7	77	46	68	63	15	043	C14.6	25	.	.	*	*	*	*	13	*	07	05	02	07	07	.	.	.	05	.	.	.				
IX	2.5	3.6	2.2	2.8	-	10.2	86	51	79	72	28	034	C16.8	06	.	.	*	*	*	*	02	*	14	01	06	04	01	06	.	.	.	05	01	.	.			
X	5.1	4.9	4.2	4.7	-	08.1	88	66	80	77	27	076	040.0	22	.	.	*	*	*	*	04	*	01	03	03	14	10	01	14	.	.	.	01	01	.	.		
XI	7.3	4.6	3.8	5.3	-	05.6	90	69	89	83	40	060	015.6	01	.	.	*	*	*	*	05	*	08	06	06	03	06	.	.	.	09	.	.	.				
XII	5.7	5.0	4.7	5.1	-	04.2	84	78	91	84	49	035	C03.0	15	01	.	28	*	*	*	01	*	08	07	05	02	01	04	01	.	.	.	04	12	.	.		
GOD.	5.2	4.7	4.1	4.6	-	07.5	83	60	80	74	16	634	040.0	22	x	03	*	114	73	21	.	22	06	100	74	102	83	23	94	15	05	.	.	.	17	19	20	.
BR. ST. 283																																						
I	7.7	7.3	6.0	7.0	-	089.4	03.8	92	70	88	P4	36	048	020.2	02	03	02	26	*	*	*	*	06	17	12	08	01	04	C10	01	.	.	.	11	.	.	.	
II	7.1	6.8	4.5	6.1	-	112.7	04.4	92	64	87	81	30	055	017.7	08	.	.	23	*	*	*	*	05	10	08	05	03	07	04	02	.	.	.	01	01	.	.	
III	7.3	6.5	4.6	6.2	-	138.6	04.9	93	57	84	78	19	047	019.6	07	.	.	18	*	*	*	*	04	14	10	07	01	06	06	02	.	.	.	02	.	.	.	
IV	6.4	6.3	5.1	6.6	-	162.5	05.5	92	57	82	77	32	058	021.6	15	.	.	13	*	*	*	01	*	01	11	14	09	02	14	01	.	.	.	03	.	.	.	
V	6.6	7.9	5.1	6.5	-	212.9	07.7	89	58	85	77	28	082	019.0	19	.	.	01	*	*	*	*	07	09	18	13	07	18	.	.	.	14	01	.	.			
VI	5.6	7.3	4.6	5.8	-	278.6	09.7	66	53	85	74	35	150	036.6	19	.	.	04	*	*	*	01	*	03	06	15	11	05	15	.	.	.	07	.	.	.		
VII	2.3	5.3	1.5	3.0	-	368.0	10.0	84	42	75	67	28	023	C11.0	21	.	.	*	*	*	*	12	*	05	02	01	05	05	.	.	.	03	.	.	.			
VIII	3.1	5.8	2.5	3.8	-	311.4	10.1	83	43	72	66	27	027	014.2	25	.	.	*	*	*	*	07	*	02	08	05	01	08	.	.	.	10	.	.	.			
IX	3.1	5.4	1.9	3.5	-	260.0	08.5	91	43	82	72	24	011	004.7	26	.	.	01	02	*	*	*	*	08	01	06	03	06	01	06	.	.	.	03	.	.	.	
X	6.1	7.8	3.9	5.9	-	180.4	06.0	91	72	81	75	29	075	C25.7	22	.	.	09	*	*	*	01	*	10	15	10	03	15	.	.	.	01	.	.	.			
XI	6.1	5.5	4.0	5.7																																		



SAVEZNI HIDROMETEOROLOŠKI ZAVOD
Klimatološko odeljenje

METEOROLOŠKE STANICE U 1974