SOCIJALISTIČKA FEDERATIVNA REPUBLIKA JUGOSLAVIJA - RÉPUBLIQUE SOCIJALISTE FÉDÉRATIVE DE YOUGOSLAVIE
HIDROMETEOROLOŠKA SLUŽBA - SERVICE HYDRO-MÉTÉOROLOGIQUE

METEOROLOŠKI GODIŠNJAK I

ANNUAIRE METEOROLOGIQUE I

GODINA 1970. ANNÉE

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BEOGRAD 1972.

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O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljuju se podaci 8 odabranih stanica, i to: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd i Skopje. U delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

φ = geografska širina, λ = geografska dužina od Griniča, ΔG vremenska razlika u odnosu na Grinič, Hs = nadmorska visina podnožja termometarskog zaklona, Hb = nadmorska visina rezervoara barometra, ht = visina rezervoara termometra iznad tla, h_r = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebljene prema medjunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

P = vazdušni pritisak u mm visine živinog stuba, reducirane na $0^{o}C$; T = temperatura u ^{o}C; e = pritisak vodene pare u mm visine živinog stuba; U = relativna vlažnost u procentima; D = pravac vetra po ruži vetra od 16 ili 8 pravaca; F = jačina vetra po Boforovoj skali (0-12); v = brzina vetra u m/sek; V = vidljivost u km; N = oblačnost (0-10); insolacija = trajanje osunčavanja u satima; R = padavine u mm; h_s = snežni pokrivač u cm; W = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan medjunarodnim simbolima.

U rubrici "razvoj vremena" su upotrebljene ove skraćenice:

n = u toku noći; a = pre podne; p = posle podne; i = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14 i 21 h po lokalnom vremenu računate su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente (P, e, U, N) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri su očitavani i uredjivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h predhodnog dana do 7 h dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritiska vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritiska vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebljene su oznake M_{ax} i M_{in}; za rubrike broj dana sa • ili ⚲ , ✳ ili ⚠ , i ✳̇ prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Azbučnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SFRJ sa naznačenim klimatološkim stanicama u 1970. godini čiji brojevi odgovaraju brojevima stanica sa podacima u tablicama B.

NOTICE EXPLICATIVE

L'Annuaire Météorologique I a deux parties: A) Observations journalières et B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd et Skopje. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

φ = latitude, λ = longitude E de Grenwich, ΔG = différence entre l'heure locale et l'heure de Greenwich, H_s = altitude du pied de l'abri météorologique, H_b = altitude de la cuvette du baromètre, h_t = hauteur, au-dessus du sol, du réservoir du thermomètre, h_r = hauteur, au dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

La désignation des éléments météorologiques particuliers sont conformes aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

P = pression atmosphérique en mm (hauteur de la colonne de mercure réduite à $0^{o}C$); T = température en ^{o}C; e = tension de vapeur d'eau en mm de la hauteur de la colonne de mercure; U = humidité relative en %; D = direction du vent en rose des vents de 8 ou de 16 directions; F = force du vent d'après l'échelle Beaufort (0-12); v = vitesse du vent en m/s; V = visibilité en km; N = nébulosité (0-10); insolation = duré d'insolation en heures; R = précipitations en mm; h_s = épaisseur de la couche de neige en cm; W= évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux.

Dans la colonne "Razvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

n = pendant la nuit; a = avant midi; p = après midi; i = avec interruption.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4},$$

et pour les autres éléments (P, e, U, N) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7h, 14 h et 21 h.

Les lectures des thermomètres à maxima et minima suivies de leur amorsage, ont été faits à 21 h et les valeurs inscrites le même jour.

Les valeurs journalières des précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau, de la force du vent $F \geqq 6$ (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air les indications $M_{\overline{ax}}$ et $M_{\overline{in}}$ ont été utilisées; dans les colonnes "Broj dana sa" (Nombre de jours avec) ● ou ☂ , ✳ ou ⚠ , et ✳̊ sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1970; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

A Z B U Č N I S P I S A K S T A N I C A

PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

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S T A N I C A	Broj stanice	Nadmorska visina H_s m	Geografska širina φ° N	Geografska dužina λ° E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karakterističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
S O C I J A L I S T I Č K A R E P U B L I K A S L O V E N I J A													
Ajdovščina	28	110	45°53'	13°54'	gl	X	X	X	X	X	X	X	X
Babno Polje	34	756	45 39	14 33	ob		X	X	X	X		X	X
Bovec	1	425	46 20	13 33	ob		X	X	X	X	X	X	X
Brniki-letalište	11	362	46 13	14 29	gl	X	X	X	X	X	X	X	X
Celje-Levec	18	244	46 15	15 14	ob		X	X	X	X	X	X	X
Črnomelj	37	156	45 34	15 12	ob		X	X	X	X		X	X
Dom na Komni	5	1520	46 17	13 46	ob		X		X	X		X	X
Golnik	10	500	46 20	14 20	ob		X	X	X	X	X	X	X
Gomance	32	937	45 31	14 26	ob		X		X	X		X	X
Gornji Lenart	38	150	45 56	15 34	ob		X	X	X	X	X	X	X
Ilirska Bistrica	30	414	45 34	14 15	ob		X	X	X	X		X	X
Javorje nad Poljanami	9	695	46 10	14 11	ob		X	X	X	X		X	X
Jeruzalem	23	345	46 28	16 12	ob		X	X	X	X	X	X	X
Jezersko	12	879	46 24	14 30	gl		X	X	X	X		X	X
Klenik pri Vačah	14	560	46 07	14 51	ob		X	X	X	X		X	X
Kočevje	35	461	45 38	14 52	ob		X	X	X	X		X	X
Koper	26	33	45 33	13 43	gl	X	X	X	X	X	X	X	X
Kredarica	6	2514	46 23	13 51	gl	X	X	X	X	X	X	X	X
Kubed	27	262	45 31	13 52	ob		X		X	X		X	X
Ljubljana-Bežigrad	13	299	46 04	14 31	gl	X	X	X	X	X	X	X	X
Maribor-Tezno	20	275	46 32	15 39	gl	X	X	X	X	X	X	X	X
Murska Sobota	22	191	46 40	16 08	gl	X	X	X	X	X	X	X	X
Nova Vas na Blokah	33	722	45 46	14 31	ob		X	X	X	X		X	X
Novo Mesto-Gotna Vas	36	208	45 48	15 11	gl	X	X	X	X	X	X	X	X
Postojna Zalog	29	533	45 46	14 12	gl		X	X	X	X	X	X	X
Pragersko	21	251	46 24	15 39	ob		X	X	X	X		X	X
Radeče	16	230	46 04	15 11	ob		X	X	X	X		X	X
Radlje ob Dravi	17	365	46 37	15 13	ob		X	X	X	X		X	X
Radovljica	8	495	46 21	14 11	ob		X	X	X	X		X	X
Rakitna	31	787	45 53	14 26	ob		X		X	X		X	X
Rateče-Planica	3	864	46 30	13 43	gl	X	X	X	X	X		X	X
Sela pri Planini nad Sevnico	19	550	46 06	15 24	ob		X	X	X	X		X	X
Šmartno pri Slovenjgradcu	15	452	46 29	15 07	gl		X	X	X	X	X	X	X
Temnica	25	402	45 51	13 41	ob		X	X	X	X	X	X	X
Tolmin	4	180	46 11	13 44	ob		X	X	X	X		X	X
Vedrijan	2	258	46 01	13 33	gl	X	X	X	X	X	X	X	X
Veliki Dolenci	24	308	46 51	16 17	ob		X	X	X	X		X	X
Vojsko	7	1070	46 01	13 55	ob		X		X	X		X	X
S O C I J A L I S T I Č K A R E P U B L I K A H R V A T S K A													
Bistrac	54	160	45 49	15 42	ob		X	X	X	X		X	X
Bjelovar	63	141	45 54	16 51	gl	X	X	X	X	X		X	X
Božjakovina	60	110	45 49	16 17	ob		X	X	X	X		X	X
Brestovac-Belje	72	91	45 42	18 44	ob	X	X	X	X	X	X	X	X
Cres	76	10	44 58	14 24	ob		X	X	X	X		X	X
Crikvenica	48	2	45 10	14 42	ob	X	X	X	X	X		X	X
Čazma	62	144	45 45	16 37	ob		X	X	X	X		X	X

A Z B U Č N I S P I S A K S T A N I C A
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Nadmorska visina H_s m	Geografska širina φ°N	Geografska dužina λ°E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karakterističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Daruvar	66	161	45°36'	17°14'	gl	X	X	X	X	X	X	X	X
Donji Miholjac	70	97	45 46	18 10	ob		X	X	X	X		X	X
Dubrovnik	102	49	42 39	18 06	ob		X	X	X	X	X	X	X
Djakovo	71	98	45 17	18 25	ob		X	X	X	X		X	X
Gospić	84	564	44 33	15 22	gl	X	X	X	X	X	X	X	X
Gračac	86	560	44 18	15 51	ob		X	X	X	X		X	X
Hvar	92	20	43 10	16 27	gl	X	X	X	X	X	X	X	X
Ilok	74	133	45 14	19 23	ob		X	X	X	X		X	X
Karlovac	52	112	45 30	15 33	gl	X	X	X	X	X	X	X	X
Kaštel Stari	90	24	43 33	16 21	ob		X	X	X	X	X	X	X
Knin	87	234	44 02	16 12	gl	X	X	X	X	X		X	X
Komiža	89	6	43 03	16 05	ob		X	X	X	X		X	X
Koprivnica	42	149	46 10	16 50	ob		X	X	X	X		X	X
Korčula	99	20	42 57	17 08	ob		X	X	X	X		X	X
Kostel	39	270	46 11	15 45	ob		X	X	X	X		X	X
Križevci	41	155	46 02	16 33	gl	X	X	X	X	X	X	X	X
Lastovo	98	186	42 46	16 54	gl	X	X	X	X	X	X	X	X
Ličko Lešće	83	463	44 48	15 19	ob		X	X	X	X		X	X
Lipik	65	154	45 25	17 10	ob		X	X	X	X		X	X
Makarska	94	6	43 18	17 01	ob		X	X	X	X		X	X
Mali Lošinj	77	53	44 32	14 28	gl	X	X	X	X	X	X	X	X
Novska	64	136	45 21	16 59	gl		X	X	X	X		X	X
Ogulin	51	325	45 16	15 14	gl	X	X	X	X	X		X	X
Opuzen	95	2	43 01	17 34	ob		X	X	X	X		X	X
Orebić	100	6	42 58	17 10	ob		X	X	X	X		X	X
Osijek	73	89	45 32	18 44	gl	X	X	X	X	X	X	X	X
Pag	81	3	44 27	15 04	ob		X	X	X	X	X	X	X
Palagruža	96	98	42 24	16 16	gl	X	X	X	X	X	X	X	X
Parg	47	863	45 36	14 38	gl	X	X	X	X	X	X	X	X
Pazin	45	291	45 14	13 56	gl	X	X	X	X	X		X	X
Plitvički Ljeskovac	85	650	44 51	15 36	ob		X	X	X	X		X	X
Podravska Slatina	68	120	45 44	17 31	ob		X	X	X	X		X	X
Poreč	43	15	45 14	13 36	ob		X	X	X	X		X	X
Pula	75	30	44 52	13 51	gl		X	X	X	X	X	X	X
Rab	78	24	44 45	14 46	gl	X	X	X	X	X	X	X	X
Rijeka	46	104	45 20	14 27	gl	X	X	X	X	X	X	X	X
Rovinj	44	5	45 05	13 39	ob		X	X	X	X	X	X	X
Senj	79	26	44 59	14 54	gl	X	X	X	X	X	X	X	X
Sinj	93	298	43 42	16 41	gl		X	X	X	X	X	X	X
Sisak	61	98	45 30	16 22	gl	X	X	X	X	X	X	X	X
Skrad	50	668	45 25	14 55	ob		X	X	X	X		X	X
Sl. Požega	67	152	45 20	17 41	ob		X	X	X	X		X	X
Sl. Brod	69	88	45 10	18 00	gl	X	X	X	X	X	X	X	X
Slunj	53	258	45 07	15 35	ob		X	X	X	X		X	X
Sljeme	55	1007	45 54	15 57	gl	X	X	X	X	X	X	X	X
Split-Marjan	91	122	43 31	16 26	gl	X	X	X	X	X	X	X	X
Ston	101	2	42 50	17 42	ob		X	X	X	X		X	X
Stubička Gora	56	620	45 56	15 59	ob		X	X	X	X		X	X

A Z B U Č N I S P I S A K S T A N I C A

PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Nadmorska visina H_s m	Geografska širina φ°N	Geografska dužina λ°E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karakterističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Šibenik	88	77	43°44'	15°55'	gl	X	X	X	X	X	X	X	X
Topusko	58	129	45 18	15 59	ob		X	X	X	X		X	X
Varaždin	40	169	46 18	16 21	gl	X	X	X	X	X	X	X	X
Vela Luka	97	30	42 58	16 43	ob		X	X	X	X		X	X
Zadar	82	5	44 08	15 13	gl	X	X	X	X	X	X	X	X
Zagreb-Grič	57	157	45 49	15 59	gl	X	X		X	X	X	X	X
Zagreb-Maksimir	59	123	45 49	16 02	gl	X	X	X	X	X	X	X	X
Zalesina	49	750	45 23	14 53	ob		X	X	X	X		X	X
Zavižan	80	1594	44 49	14 59	gl	X	X	X	X	X	X	X	X
S O C I J A L I S T I Č K A R E P U B L I K A B O S N A I H E R C E G O V I N A													
Banja Luka	114	153	44°47'	17°13'	gl	X	X	X	X	X	X	X	X
Berkovići	141	537	43 06	18 11	ob		X	X	X	X		X	X
Bihać	106	246	44 49	15 53	gl	X	X	X	X	X	X	X	X
Bijeljina-Novo Selo	129	90	44 46	19 16	ob		X	X	X	X	X	X	X
Bileća	151	491	42 53	18 27	gl		X	X	X	X		X	X
Bjelašnica	142	2067	43 43	18 16	gl	X	X	X	X	X	X	X	X
Bos. Dubica	104	100	45 11	16 49	gl		X	X	X	X	X	X	X
Bos. Krupa	107	176	44 53	16 10	ob		X	X	X	X		X	X
Bos. Novi	103	119	45 03	16 23	ob		X	X	X	X		X	X
Brčko	127	96	44 53	18 49	ob		X	X	X	X		X	X
Bugojno	118	562	44 04	17 28	gl	X	X	X	X	X	X	X	X
Čapljina	135	10	43 07	17 43	ob		X	X	X	X		X	X
Čemerno	147	1305	43 14	18 36	gl	X	X	X	X	X		X	X
Derventa	105	105	45 00	17 55	ob		X	X	X	X		X	X
Doboj	123	146	44 44	18 06	gl		X	X	X	X	X	X	X
Domanovići	137	146	43 09	17 47	ob		X	X	X	X		X	X
Drinić	109	730	44 31	16 28	ob		X	X	X	X		X	X
Drvar	108	485	44 23	16 24	gl	X	X	X	X	X	X	X	X
Gacko	146	960	43 10	18 33	ob		X	X	X	X		X	X
Glamoč	113	1031	44 03	16 52	ob		X	X	X	X		X	X
Goražde	149	345	43 40	18 59	ob		X	X	X	X		X	X
Ivan Sedlo	140	970	43 46	18 02	ob		X	X	X	X	X	X	X
Jablanica	136	192	43 40	17 46	ob		X	X	X	X		X	X
Jajce	115	430	44 21	17 16	ob		X	X	X	X	X	X	X
Kalinovik	145	1073	43 31	18 27	gl	X	X	X	X	X		X	X
Kotor Varoš	117	266	44 38	17 23	ob		X	X		X		X	X
Kupres	116	1190	44 00	17 17	ob		X	X	X	X		X	X
Lastva	152	295	42 43	18 29	ob		X	X	X	X		X	X
Lištica	133	320	43 23	17 36	ob		X	X		X		X	X
Livno	131	724	43 50	17 01	gl	X	X	X	X	X	X	X	X
Ljubinje	150	413	42 58	18 06	ob		X	X	X	X		X	X
Maoča	125	335	44 19	18 26	ob		X	X	X	X		X	X
Mlinište	112	1130	44 16	16 51	ob		X	X	X	X		X	X
Modriča	124	115	44 59	18 17	ob		X	X	X	X		X	X
Mostar	138	99	43 21	17 48	gl	X	X	X	X	X	X	X	X
Potoci-Bijelo Polje	139	96	43 24	17 53	ob	X	X	X	X	X	X	X	X

• Nema barometra

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S T A N I C A	Broj stanice	Nadmorska visina H_s m	Geografska širina φ° N	Geografska dužina λ° E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karakterističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Prijedor	111	135	44°59'	16°44'	ob		X	X	X	X		X	X
Prnjavor	120	150	44 52	17 42	ob		X	X	X	X		X	X
Prozor	134	800	43 50	17 37	ob		X	X	X	X		X	X
Rakitno	132	915	43 33	17 27	ob		X	X	X	X		X	X
Sanski Most	110	158	44 46	16 42	ob		X	X	X	X	X	X	X
Sarajevo	144	630	43 52	18 26	gl	X	X	X	X	X	X	X	X
Sarajevo-aerodrom	143	518	43 50	18 21	gl	X	X	X	X	X	X	X	X
Sokolac	148	872	43 57	18 49	gl		X	X	X	X	X	X	X
Srebrenica	130	550	44 07	19 18	ob		X	X	X	X		X	X
Teslić	121	210	44 36	17 52	ob		X	X	X	X		X	X
Travnik	119	581	44 14	17 41	ob		X	X	X	X		X	X
Tuzla	126	305	44 33	18 42	gl	X	X	X	X	X	X	X	X
Vlasenica	128	680	44 12	18 57	ob		X	X	X	X		X	X
Zenica	122	344	44 13	17 54	gl	X	X	X	X	X	X	X	X
S O C I J A L I S T I Č K A R E P U B L I K A S R B I J A													
Aleksandrovac	204	360	43°27'	21°04'	ob		X	X	X	X		X	X
Bačka Topola	157	100	45 49	19 39	ob		X	X	X	X		X	X
Bački Petrovac	156	85	45 22	19 34	ob		X	X	X	X	X	X	X
Bečej	162	75	45 37	20 04	ob		X	X	X	X	X	X	X
Bela Crkva	184	90	44 54	21 25	ob		X	X	X	X		X	X
Bele Vode-Golija	199	1500	43 25	20 17	ob		X	X	X	X	X	X	X
Beograd	174	132	44 48	20 28	gl	X	X	X	X	X	X	X	X
Bor	189	380	44 05	22 06	ob		X			X		X	X
Bosiljgrad	234	830	42 30	22 28	ob		X	X	X	X		X	X
Bujanovac	227	400	42 27	21 47	ob		X	X	X	X		X	X
Bukovička Banja	177	265	44 18	20 33	ob		X	X	X	X		X	X
Čačak	200	240	43 54	20 21	ob		X	X	X	X		X	X
Ćuprija	209	123	43 56	21 23	gl	X	X	X	X	X	X	X	X
Debeli Lug	188	290	44 22	21 55	ob		X	X	X	X		X	X
Dimitrovgrad	217	446	43 01	22 45	gl	X	X	X	X	X	X	X	X
Flamunda	182	160	44 56	21 05	ob		X	X	X	X	X	X	X
Gladnoš	161	185	45 08	20 00	ob		X	X	X	X		X	X
Gornji Milanovac	175	330	44 02	20 29	ob		X		X	X		X	X
Istok	220	465	42 47	20 30	ob		X					X	X
Ivanjica	198	465	43 35	20 14	ob		X	X	X	X		X	X
Jaša Tomić	166	80	45 27	20 51	ob		X	X	X	X		X	X
Kikinda	165	81	45 51	20 28	gl		X	X	X	X	X	X	X
Klina	221	385	42 38	20 34	ob		X			X		X	X
Knjaževac	213	280	43 34	22 16	ob		X			X		X	X
Kokin Brod	194	570	43 31	19 50	ob		X	X	X	X		X	X
Kos. Mitrovica	223	510	42 53	20 52	ob		X	X	X	X		X	X
Kragujevac	180	190	44 02	20 56	gl		X	X	X	X	X	X	X
Kraljevo	202	219	43 44	20 41	gl	X	X	X	X	X	X	X	X
Kruševac	208	166	43 34	21 21	gl		X	X	X	X	X	X	X
Kukavica	229	1250	42 45	21 59	ob		X	X	X	X		X	X
Kuršumlija	207	380	43 08	21 16	gl		X	X	X	X	X	X	X

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S T A N I C A	Broj stanice	Nadmorska visina H s m	Geografska širina φ°N	Geografska dužina λ°E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karakterističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Loznica	168	121	44°33'	19°14'	gl	X	X	X	X	X	X	X	X
Ljubovija	169	170	44 11	19 23	ob		X		X	X		X	X
Mitrovac-Tara	192	1080	43 55	19 26	gl		X	X	X	X	X	X	X
Negotin	191	42	44 14	22 33	gl	X	X	X	X	X	X	X	X
Niš	212	202	43 20	21 54	gl	X	X	X	X	X	X	X	X
Novi Pazar	201	545	43 08	20 31	ob		X	X	X	X		X	X
Novi Sad-Petrovaradin	160	132	45 15	19 52	gl	X	X	X	X	X	X	X	X
Novi Sad-Rim.Šančevi	159	84	45 20	19 51	ob	X	X	X	X	X	X	X	X
Palić	153	102	46 06	19 46	gl	X	X	X	X	X	X	X	X
Pančevo	178	80	44 53	20 40	ob		X	X	X	X		X	X
Peć	218	498	42 40	20 18	gl	X	X	X	X	X	X	X	X
Petrovac	185	120	44 23	21 25	ob		X	X	X	X		X	X
Pirot	215	370	43 09	22 36	ob		X	X	X	X		X	X
Predejane	231	318	42 50	22 08	ob		X	X	X	X		X	X
Priština	224	573	42 39	21 09	gl	X	X	X	X	X	X	X	X
Prizren	222	402	42 13	20 44	gl		X	X	X	X	X	X	X
Prokuplje	210	265	43 14	21 36	ob		X	X	X	X		X	X
Rekovac	205	230	43 52	21 06	ob		X	X	X	X		X	X
Rudnik	176	700	44 08	20 31	ob		X	X	X	X		X	X
Sijarinska Banja	226	455	42 47	21 36	ob		X			X	X	X	X
Senta	163	80	45 56	20 05	ob		X	X	X	X		X	X
Sjenica	196	1015	43 16	20 01	gl	X	X	X	X	X	X	X	X
Skivjane-Djakovica	219	415	42 26	20 21	ob		X	X	X	X		X	X
Smederevo	179	90	44 39	20 54	ob		X		X	X		X	X
Smed. Palanka	181	104	44 22	20 58	gl	X	X	X	X	X	X	X	X
Sokobanja	211	300	43 39	21 51	ob		X	X	X			X	X
Sombor	154	89	45 45	19 06	gl		X	X	X	X	X	X	X
Sr. Mitrovica	170	81	44 58	19 38	gl		X	X	X	X		X	X
Surdulica	232	500	42 41	22 11	ob		X		X	X		X	X
Svetozarevo	206	115	43 59	21 14	ob		X		X	X		X	X
Šabac	171	80	44 46	19 41	ob		X	X	X	X		X	X
Šid	155	105	45 07	19 15	ob		X	X	X	X		X	X
Šušara	183	180	44 56	21 08	ob		X	X	X	X		X	X
Tekija	190	50	44 42	22 25	ob		X	X	X	X		X	X
Titovo Užice	195	440	43 52	19 51	ob		X	X	X	X		X	X
Topli Do	216	700	43 20	22 41	ob		X			X		X	X
Uroševac	225	580	42 23	21 10	gl		X	X	X	X	X	X	X
Už. Požega	197	311	43 51	20 02	gl	X	X	X	X	X	X	X	X
Valjevo	173	174	44 17	19 55	gl	X	X	X	X	X	X	X	X
Veliko Gradište	186	79	44 46	21 31	gl	X	X	X	X	X		X	X
Vladimirci	172	120	44 37	19 47	ob		X	X	X	X		X	X
Vlasina	233	1190	42 44	22 21	ob		X	X	X	X		X	X
Vlasotince	230	270	42 58	22 08	ob		X	X	X	X		X	X
Vranje	228	458	42 33	21 55	gl	X	X	X	X	X	X	X	X
Vrbas	158	87	45 34	19 39	gl		X	X	X	X		X	X
Vrnjačka Banja	203	235	43 37	20 54	ob		X	X	X	X	X	X	X
Vršac	167	84	45 09	21 19	gl	X	X	X	X	X	X	X	X

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S T A N I C A	Broj stanice	Nadmorska visina H, m	Geografska širina φ°N	Geografska dužina λ°E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Insolacija	Padavine	Broj karakterističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Zaječar	214	137	43°53'	22°18'	gl		X	X	X	X	X	X	X
Zlatibor	193	1029	43 44	19 43	gl	X	X	X	X	X	X	X	X
Zrenjanin	164	80	45 24	20 21	gl		X	X	X	X	X	X	X
Žagubica	187	314	44 12	21 47	gl		X	X	X	X	X	X	X
S O C I J A L I S T I Č K A R E P U B L I K A C R N A G O R A													
Bar	244	3	42°06'	19°06'	gl	X	X	X	X	X	X	X	X
Bijelo Polje	236	560	43 02	19 45	ob		X	X	X	X	X	X	X
Budva	240	2	42 17	18 51	ob	X	X	X	X	X	X	X	X
Cetinje	241	655	42 24	18 56	ob		X	X	X	X		X	X
Grahovo	238	710	42 39	18 41	ob		X		X	X		X	X
Hercegnovi-Igalo	237	40	42 28	18 30	gl	X	X	X	X	X	X	X	X
Ivangrad	247	670	42 50	19 52	ob	X	X	X	X	X		X	X
Kolašin	246	950	42 50	19 32	gl	X	X	X	X	X	X	X	X
Nikšić	242	647	42 46	18 57	gl	X	X	X	X	X	X	X	X
Pljevlja	235	784	43 21	19 21	gl	X	X	X	X	X	X	X	X
Titograd	245	52	42 26	19 17	gl	X	X	X	X	X	X	X	X
Tivat	239	4	42 26	18 42	ob	X	X	X	X	X		X	X
Ulcinj	248	97	41 55	19 13	gl	X	X	X	X	X	X	X	X
Virpazar	243	14	42 14	19 05	ob		X	X	X	X		X	X
S O C I J A L I S T I Č K A R E P U B L I K A M A K E D O N I J A													
Berovo	280	824	41°43'	22°51'	gl	X	X	X	X	X	X	X	X
Bitola	264	586	41 03	21 22	gl	X	X	X	X	X	X	X	X
Debar	254	675	41 31	20 32	ob		X	X	X	X		X	X
Delčevo	279	630	41 58	22 46	ob		X	X	X	X		X	X
Demir Kapija	272	125	41 25	22 15	gl	X	X	X	X	X		X	X
Erdželija	269	253	41 50	22 02	ob		X	X	X	X		X	X
Gevgelija	275	59	41 09	22 30	ob		X	X	X	X		X	X
Gostivar	259	525	41 48	20 55	ob		X	X	X	X		X	X
Kavadarci	270	265	41 26	22 02	ob		X	X	X	X		X	X
Kičevo	260	620	41 31	20 58	ob		X	X	X	X		X	X
Kočani	273	345	41 55	22 25	ob		X	X	X	X		X	X
Kratovo	252	640	42 05	22 09	ob		X	X	X	X		X	X
Kriva Palanka	253	691	42 12	22 20	gl	X	X	X	X	X	X	X	X
Kruševo	263	1230	41 22	21 15	ob		X	X	X	X		X	X
Kumanovo	251	338	42 08	21 43	ob		X	X	X	X		X	X
Lazaropole	256	1332	41 32	20 42	gl	X	X	X	X	X	X	X	X
Makedonski Brod	262	545	41 31	21 13	ob		X	X	X	X		X	X
Mavrovi Anovi	257	1240	41 42	20 45	ob		X	X	X	X	X	X	X
Nov Dojran	278	180	41 13	22 43	ob		X	X	X	X		X	X
Ohrid	258	760	41 07	20 48	gl	X	X	X	X	X	X	X	X
Popova Šapka	249	1750	42 01	20 53	ob		X	X	X	X		X	X
Prilep	267	673	41 20	21 34	gl	X	X	X	X	X	X	X	X
Radoviš	274	380	41 38	22 27	ob		X	X	X	X		X	X
Resen	261	881	41 05	21 01	ob		X	X	X	X		X	X
Skopje	265	232	41 57	21 38	gl	X	X	X	X	X	X	X	X

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1	2	3	4	5	6	7	8	9	10	11	12	13	14
Struga	255	695	41°11'	20°41'	ob		X	X	X	X		X	X
Strumica	277	224	41 26	22 39	ob		X	X	X	X		X	X
Štip	271	326	41 45	22 11	gl	X	X	X	X	X	X	X	X
Tetovo	250	462	42 00	20 58	ob		X	X	X	X		X	X
Titov Veles	268	175	41 43	21 46	ob		X	X	X	X		X	X
Prilep	266	233	41 59	21 31	ob		X	X	X	X		X	X
Valandovo	276	100	41 19	22 34	ob		X	X	X	X		X	X

A) Dnevna osmatranja

$\varphi = 46^{\circ}\ 04'$ N $\lambda = 14^{\circ}\ 31'$ E Gr. ΔG = + 58 min. BR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)					
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7		14		21	
1	725.8	722.3	724.1	-02.4	-00.4	-01.2	-01.	01.2	-02.6	-04.3	02.5	03.7	03.7	90	82	88	87	SE	1	NW	1	NW	1
2	726.3	728.0	730.1	-01.1	00.2	-00.3	-03.0	01.3	-05.3	-03.0	03.8	03.7	02.9	94	80	95	90	N	1	-	0	-	0
3	730.1	729.9	730.7	-03.2	-00.8	-00.2	-01.1	01.2	-05.5	-14.7	03.4	03.5	03.9	93	81	86	87	NE	1	N	1	NE	1
4	730.[illegible]	729.0	727.3	00.4	04.5	01.5	02.2	03.0	-01.0	-03.2	04.1	05.2	04.8	88	86	93	87	NNE	1	NW	1	-	0
5	724.0	719.8	718.9	01.1	02.4	02.8	02.3	03.1	01.1	00.4	04.5	05.2	05.2	91	95	94	93	N	1	-	0	E	1
6	722.8	725.2	730.3	03.8	01.0	00.4	01.4	04.5	00.4	01.2	05.6	04.5	04.4	97	91	93	94	-	0	NE	1	NE	1
7	729.[illegible]	732.1	730.4	-00.5	00.1	-01.2	-00.7	00.5	-01.2	-01.2	04.1	04.2	03.9	95	91	92	92	NE	1	E	2	ESE	2
8	741.[illegible]	74[illegible].1	744.5	-05.2	-04.[illegible]	-04.2	-04.7	-06.7	-10.4	-14.5	02.6	03.1	03.2	90	94	94	93	NE	1	ESE	1	ESE	1
9	743.[illegible]	741.[illegible]	744.1	-0[illegible].7	-02.3	-02.7	-03.4	-02.8	-05.7	-12.4	02.8	03.3	03.1	92	84	82	86	E	1	ESE	1	ESE	1
10	742.[illegible]	739.0	736.4	-03.6	-02.0	-02.0	-02.4	-01.5	-02.8	-04.5	03.3	03.2	03.4	92	81	85	86	SSE	1	NE	1	E	1
11	736.1	733.5	731.6	-00.6	01.7	01.4	01.0	02.3	-02.0	-02.5	04.3	04.6	04.8	98	88	95	94	-	0	-	0	SE	1
12	727.1	727.7	726.7	01.0	03.0	02.2	02.1	03.2	00.9	00.4	04.8	05.5	05.3	97	97	98	97	-	0	-	0	SSW	1
13	726.7	726.9	727.8	02.4	03.0	02.6	02.6	03.1	01.5	00.2	05.4	05.5	05.3	98	97	97	97	SW	1	W	1	-	0
14	729.1	728.3	725.6	02.0	03.5	07.0	05.0	07.4	01.8	00.1	05.2	05.6	06.0	95	97	80	92	WNW	1	-	0	SW	2
15	727.8	726.5	725.9	04.9	05.3	06.7	04.9	07.4	04.2	02.5	06.1	06.6	06.3	94	99	99	97	-	0	-	0	NNW	1
16	725.[illegible]	725.0	726.3	03.4	03.8	02.4	03.5	03.3	02.4	01.4	05.8	06.0	05.8	100	100	100	100	NE	1	SE	1	-	0
17	727.7	728.4	731.4	03.6	05.4	01.3	02.9	06.7	01.5	01.2	05.7	06.8	04.8	95	86	95	92	WSW	1	SW	2	ENE	1
18	735.1	735.5	737.1	00.8	00.6	-00.7	00.0	01.5	-06.7	-01.6	04.4	03.9	03.8	90	82	87	86	E	1	NE	1	E	2
19	739.2	739.8	741.6	-02.7	-02.6	-02.8	-02.7	-01.7	-02.9	-0[illegible].2	03.2	03.1	03.0	84	82	80	82	ESE	2	S	2	E	2
20	742.5	742.1	741.2	-02.7	-02.2	-02.8	-02.6	-01.0	-03.1	-03.2	03.0	03.0	02.9	80	77	78	78	SE	1	SE	2	NE	1
21	739.9	739.5	739.9	-03.0	-03.2	-03.6	-03.6	-02.4	-04.1	-04.7	02.9	02.9	02.9	84	81	82	82	E	2	ENE	1	SE	2
22	739.8	739.3	739.5	-03.3	-01.5	-02.6	-02.5	-01.2	-03.7	-04.3	02.8	03.0	02.8	77	73	73	74	ESE	2	SE	1	SE	2
23	739.7	739.3	739.7	-03.4	-02.4	-03.5	-03.2	-03.1	-02.6	-03.5	02.8	03.0	02.9	79	79	81	80	S	2	SSE	1	SE	2
24	739.4	738.6	738.8	-03.8	-02.0	-02.8	-02.8	-01.9	-04.0	-04.0	02.9	03.1	03.5	84	79	93	85	SE	1	SE	1	NE	1
25	737.8	739.6	740.2	-02.4	00.8	00.0	-00.4	01.[illegible]	-03.2	-03.2	03.4	03.9	04.1	88	79	89	85	SE	1	N	1	NE	1
26	739.9	740.4	740.6	-00.4	02.4	01.4	01.2	02.5	-00.5	-01.0	04.3	04.5	04.7	96	82	93	90	N	1	-	0	-	0
27	740.4	738.5	738.3	01.0	06.6	06.6	05.4	07.4	01.2	00.6	04.8	06.5	06.0	93	89	90	91	-	0	W	2	SW	1
28	737.6	736.8	737.5	03.4	03.8	00.0	02.3	04.2	00.0	01.5	05.8	06.4	04.4	98	93	96	96	NE	1	W	1	-	0
29	737.9	737.3	736.5	00.2	02.1	00.0	00.6	02.5	-00.1	-06.1	04.6	03.8	03.9	98	71	86	85	NE	1	E	1	-	0
30	732.5	730.4	730.4	-01.0	00.2	-00.4	-00.4	01.1	-01.1	-06.6	03.9	04.3	04.2	92	91	94	92	NE	1	NW	1	N	1
31	730.7	731.6	735.1	-01.0	00.8	-00.7	-00.4	01.2	-01.2	-02.0	04.0	04.4	03.8	94	90	87	90	-	0	NE	1	SE	1
MES. VRED.	733.7	733.5	734.2	-00.6	01.0	00.0	00.1	02.0	-01.5	-03.1	04.1	04.4	04.2	92	86	90	89	0.9		0.9		1.0	

1	735.9	734.6	734.9	-02.6	00.4	-02.2	-01.6	03.8	-03.1	-03.5	03.3	03.8	03.3	86	80	85	84	SE	1	NE	1	E	2
2	736.5	734.5	732.0	-03.6	00.2	-01.3	-01.5	04.[illegible]	-03.7	-05.0	02.5	02.8	03.1	72	60	75	69	E	1	NE	1	SE	1
3	728.6	727.4	728.8	-03.1	03.6	01.8	01.3	03.6	-01.7	-04.5	03.9	04.5	04.8	78	80	92	83	SW	3	SW	3	SW	1
4	731.1	729.7	728.8	-0[illegible]	00.4	01.8	00.6	02.1	-02.1	-07.5	04.0	04.6	04.8	97	96	92	95	N	1	-	0	SW	1
5	727.1	725.9	723.9	07.2	03.4	06.9	07.4	09.7	02.0	01.0	06.2	06.7	07.2	82	81	96	86	SW	2	NE	1	SW	2
6	728.4	730.4	732.6	03.1	11.4	03.4	05.[illegible]	12.0	02.4	-02.0	05.1	04.6	04.6	89	46	79	71	SE	1	SW	[illegible]	SW	1
7	734.4	734.6	734.2	02.2	02.2	01.8	02.0	03.7	-00.2	-06.0	04.1	04.5	04.5	76	84	87	82	E	2	E	1	NE	1
8	731.9	731.6	731.5	-00.5	07.8	04.1	03.9	09.4	-00.5	-05.0	04.1	04.8	05.1	93	60	84	79	N	1	SW	2	SW	2
9	731.0	723.8	727.0	00.9	07.7	08.8	06.5	03.8	06.3	-03.3	04.4	05.9	06.3	90	74	74	79	NE	1	NW	2	SW	3
10	723.2	724.8	726.9	03.6	01.6	01.2	02.4	03.1	00.9	04.5	06.6	05.0	04.6	97	97	91	95	NE	1	NE	1	N	2
11	725.9	723.3	726.4	-00.3	00.6	00.8	00.5	01.5	-00.4	-05.0	04.4	04.7	04.7	98	98	97	98	NE	1	N	1	SE	1
12	733.7	733.0	731.0	-03.4	-00.4	-02.4	-02.2	03.0	-04.1	-10.4	03.5	03.7	03.6	97	82	94	91	-	0	-	0	-	0
13	726.4	726.3	727.6	00.0	03.4	02.6	02.6	03.[illegible]	-02.5	-05.1	04.3	05.2	04.5	93	78	81	84	SW	1	SE	1	WSW	1
14	731.2	728.0	721.0	11.0	01.8	00.2	03.[illegible]	02.5	00.2	00.0	04.7	04.4	04.4	95	83	95	91	-	0	NE	1	NE	1
15	719.6	722.7	727.8	00.2	02.6	-00.1	00.9	03.0	-00.2	-01.0	04.5	04.5	02.8	96	81	61	79	NW	1	S	1	E	1
16	731.4	732.8	733.8	-05.0	-01.7	-06.9	-03.1	03.0	-07.0	-06.8	02.1	02.4	02.1	65	58	77	67	SE	2	[illegible]	1	NE	1
17	736.9	737.9	737.3	-12.6	-02.3	-06.9	-07.2	-03.4	-13.7	-22.2	01.6	02.0	02.3	92	51	84	76	NE	1	[illegible]	1	NW	1
18	733.9	733.5	735.5	-07.2	-02.0	-01.2	-02.3	-03.8	-09.8	-17.3	02.4	03.7	03.9	88	94	93	92	NE	1	E	1	N	1
19	739.0	740.4	741.8	-03.6	01.7	-03.4	-02.2	02.[illegible]	-04.3	-09.7	03.3	03.6	03.3	94	69	93	85	N	1	[illegible]	1	NE	1
20	741.5	738.3	734.2	-07.0	01.1	-01.9	-02.4	02.[illegible]	-07.0	-12.4	02.6	03.2	03.5	96	65	87	83	NE	1	ESE	1	NW	1
21	737.3	736.6	733.3	-05.4	02.2	-00.2	-00.9	03.7	-05.4	-13.5	03.0	04.2	04.0	97	79	89	88	E	1	SE	1	SE	1
22	732.0	732.2	732.0	-02.2	00.4	04.8	03.4	07.0	-02.3	-07.0	03.4	05.1	05.4	88	71	84	91	SW	1	SW	2	WSW	1
23	726.5	726.1	728.5	02.8	10.5	03.0	04.8	11.1	02.2	00.5	05.4	06.1	04.4	97	64	77	79	NW	1	S	2	SE	2
24	730.5	728.1	730.5	-04.4	07.5	02.4	01.9	03.5	-04.3	-10.5	03.2	03.9	03.6	98	51	67	72	NE	1	S	1	NE	1
25	732.2	731.1	731.7	-00.8	07.4	01.4	02.4	03.0	-01.2	-06.6	04.0	03.7	04.7	92	47	93	77	NW	1	SE	1	-	0
26	730.5	729.4	729.9	-00.2	05.[illegible]	02.7	02.6	03.7	-00.8	-02.5	04.1	03.6	03.7	91	53	67	70	NW	1	NNE	1	SE	1
27	729.7	730.1	732.4	-00.2	01.3	-01.4	-00.4	03.0	-01.5	-02.9	04.0	03.3	03.5	89	65	84	79	SE	1	SE	2	SE	2
28	733.3	733.7	735.5	-03.6	03.6	-00.2	-00.1	04.0	-03.8	-05.3	03.4	03.1	03.4	96	53	73	74	SE	1	SSW	1	NE	2
MES. VRED.	731.4	730.9	731.2	-01.1	03.4	00.7	00.9	04.7	-02.6	-06.1	03.9	04.2	04.1	90	71	84	82	1.1		1.2		1.3	

OB. ST. 13 H_s = 299 m H_b = 300.6 m h_t = 2.0 m h_r = 1.5 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srečl Dies		7	7	
1	4	10	10	10 *	10.0	00.0	05.7	18	*tr n-4^30 18^45 ni; = n-n, ⊠, ⊙
2	5	10 *	02 ⊙	10	07.3	00.8	00.9	17	= n-n, *o-tr n-14^35 i, ⌣tr 8¼-8¾, ⊙, ⊠
3	5	10	09	09	09.3	00.4	00.1	16	= n-n, *tr 12½-13¼, ⊙, ⊠
4	6	10	10	10 ●	10.0	00.0	00.0	16	= n-n, ●o-tr 18^35 19¼, ●tr 19¼-n, ⊠
5	2	10≡ ●	10≡ ●	09 ●	09.7	00.0	11.6	10	≡o-t n-11¾, 14½-18½; ≡ 11¾-14½, = 18½-n, ●tr-o-t-2 n-ni, ⊠
6	4	10≡ ●	10 *	10 *	10.0	00.0	20.5	05	≡o-2 n-8¼, ●o-1 n-9i, = 8¼-n, *o-1 9^01 10¾, *tr-o-1 10¾-n, ⊠
7	4	10 *	10 *	10	10.0	00.0	12.2	09	= n-n, △b n-3¾, *tr-o-1 3¾-17¾i, ●o-1 7½-8½, ⊠
8	1	10≡	10≡	10	10.0	00.0	02.2	11	= n-4½, 10^50 n; ≡o-1 4½-4^50 14-15½; ≡o-2 4^02 16^50 i, ⊙, ⊠
9	4	10	09	10	09.7	00.0	.	10	= n-8^05 11½-n; ≡o 8^05-11½, ⊙, ⊠
10	6	10 *	10	10	10.0	00.0	00.4	10	= n-n, △tr-o 5½-6½, *tr-o-1 6½-11¾, ⊠
11	3	10≡ ●	10≡	10≡ ●	10.0	00.0	04.4	11	≡o n-n, ⊠ n-12½, ●o-1 n-6¼, 16½-n; ●o 6¾-7¾, ●● 14^30-16½, ⊠
12	2	10≡ ●	10≡ ●	10≡ ●	10.0	00.0	08.7	06	= o-t-2 n-ni, ●o-tr n-17^45 i, ≡o n-9, ●tr 20^50 n, ⊠
13	3	10≡	10≡ ●	10≡ ●	10.0	00.0	01.9	05	≡t-2 n-12¾, ●tr-o 9^02 ni, ≡o-1 12¾-n, ⊠
14	5	10≡	09≡ ●	04	07.7	00.0	03.2	02	≡t n-10¾, ≡t-2 10¾-16¼, ●tr 12^40 15¼, = 15¼-15½, ⊙, ⊠
15	2	10 ●	10≡ ●	10≡ ●	10.0	00.0	00.1	.	= n-9¼, ●, ●tr-o 6^10 11¼ i; ≡o-1 9¼-13½, ●o 11¾-ni; ≡ 13½-n
16	1	10≡	10≡	10≡	10.0	00.0	13.1	.	●n; ≡o n-4½, ≡t-2 4½-n
17	6	10	08	10	09.3	00.4	00.2	.	≡o n-6¼, 19¾-20½; = 6¼-14¾, 18½-ni; ⌣o-1 20½-n, ⊙
18	5	10	09	10	09.7	00.0	.	.	⊠ n-8, ⌣o n-9, 20-n; ≡o n-5, = 5-n
19	6	10	10	10	10.0	00.0	00.0	.	= n-n, ●tr 4½-5½, *tr 10^45 11¼ i
20	6	10	10	10	10.0	00.0	00.0	.	= n-n
21	6	10	10 *	10	10.0	00.0	.	.	= n-n, ⌣o n-8, *tr 9-11, △tr 11-16¼
22	6	10	10	10	10.0	00.0	00.0	.	= n-n, ⊙
23	5	10	10	10	10.0	00.0	.	.	= n-n
24	6	10	10	10 *	10.0	00.0	.	.	= n-n, *tr-o-1 14½-n, ⊠
25	6	10	10	10	10.0	00.0	07.0	07	= n-n, * n, ⊠
26	3	10	10≡	10	10.0	00.0	.	04	= n-10½, 19½-n; ≡o 10½-19½, ●tr 16¼-16^40, ⊠
27	7	10	10	10	10.0	00.0	00.0	02	= n-12¼, 18½-n; ●tr 8^40 13½ i, 18-18½ i, 21^45-n; ⊠
28	3	10≡	07≡ ⊙	00≡	05.7	02.1	04.9	.	●tr-o n, 5¼-6^40, ●tr n-5¼, = n-5½, 14½-15¼; ≡ 5½-14½ i, 18¾-21½, ≡t-2 8^45-10½,
29	6	10≡	10	07	09.0	00.0	.	.	≡o-1 n-7, ⊠ n-9½, ⌣o n-9½, ≡o 7-7½, = 7½-16½, [21½-n; ⌣o 18-n, ⊠ 20½-n, ⊙
30	5	10	10 *	10 *	10.0	00.0	.	.	= n-n, ⌣o n-10, ⊠ n-7½, △o 8^20 10i, *tr-o 10-ni, *tr 16¾-19^45, ⊠
31	5	10 *	10	10	10.0	00.0	02.7	02	= n-n, *tr-o n-9¼, 16¾-20i, *o 17¼-18^20, ⊠
MES. VRED.		10.0	09.4	09.3	09.6	03.7	99.8		

1	5	10 *	10 *	09 *	09.7	00.0	09.5	02	= n-n, *tr 4½-ni, ⊙, ⊠
2	6	10	04	10	09.0	04.6	00.1	02	= n-n, *tr-o n, ⊙, ⊠
3	7	10	10	10	10.0	00.0	.	01	= n-9½, ●tr 8^55-14½ i, ⊠
4	2	10≡	10≡ ●	10	10.0	00.0	00.0	.	⌣ n-10½, = 4½-4¾, 17½-n; ≡o-1 4¾-11¾ i, 15½-17½; ≡o-1 5-9¼ i, ●tr 13½-15½
5	6	10	10 ●	10	10.0	00.1	00.0	.	= n-n, ●tr-o 13^20 ni, ▽o-1 17½-20^40 i, ⊠o-1 19^52-20¼, ⊙
6	7	02	04 ⊙	00	02.0	07.4	06.4	.	●n, = 6½-11¾, ⌣o 6½-8½, ⊠ 13^40-13^56 ⊙
7	6	10	09	10	09.7	00.0	.	.	= n-n, ⌣ n-7¾, *tr-o 7^50-13¾ i, △ 8¼-8¾
8	7	10	04 ⊙	01	05.0	04.7	01.4	.	= n-12½, ⊙
9	6	06	09	10	08.3	00.6	.	.	= n-15, ⌣o n-9½, ⊙
10	4	10 ●	10 *	05	09.3	00.0	07.9	.	= n-n, ⌣o 20½-n, ●tr-o-1 n-11^30, △ 11^32-11^40, △ 11^00-12½, * 12½-17¾, ⊠ 12^45-12^00
11	2	10≡	10≡ *	04 *	08.0	00.0	18.7	.	≡o-1 n-17½, ⌣o n-10, ⊠ n-8, *tr-o-2 11^40 17½, = 17½-n, ▽o-1 20¾-21¾, ⊠
12	5	10≡	09 ⊙	10	06.7	01.4	07.1	06	≡o-1 n-9½, ↔ 6¼-12½ i, ≡b 7½-12½, = 12½-n, ⊙, ⊠
13	4	10≡ *	07 ⊙	09	08.7	02.2	04.5	05	≡o-1 n-12½, *o-1 n-4½, △b-o-2 4½-9, △b 9-9½, △ ● 9½-10¾, = 12½-15½, ⊙, ⊠
14	6	10	10	10≡ *	10.0	00.0	07.1	08	= n-20i, ⌣ n, *tr-o-1 15¾-n, ≡ 16½-ni, ⊠
15	5	10 *	10	10	10.0	00.0	27.1	24	= n-n, *o-1 h-10^38 i, 16-16^34, △o 4½-4¾, ⌣ *tr 15^42 16, ⊠
16	7	10	07 ⊙	03	06.7	05.1	03.0	17	= 4½-6¼, ψ 17¾-n, ▽ 18¼-19¾, ⊙, ⊠
17	6	10	00 ⊙	00	05.3	04.8	00.0	17	≡o n-5, V b 4-9, ≡ 5-7¼, ≡o 7¼-11¾, *tr 7¾-8^40 = 11½-n, ⊙, ⊠
18	3	10	10≡ *	10	10.0	00.0	00.0	17	= n-13½, 18-h; *tr-o-1 7½-19i, ▽t 13½-15^25, ≡o 13½-18, ⊠
19	6	10≡	01 ⊙	02	04.3	05.0	07.6	32	≡t-2 n-9½, ≡o 9½-10½, = 10½-n, ⊙, ⊠
20	5	10≡ *	04 ⊙	10	08.0	01.0	00.0	21	⊠ n-11½, ≡t 2 n-11¾, V n-13½, *tr 6½-7, ↔o 9-10¾, ≡o 11¾-13¾, = 13¾-n, ⊠
21	2	10≡	10≡	04	08.0	00.0	00.2	26	= n-5½, 15½-n; * n, ≡t-2 5½-10¾, V o 6½-10, ≡o-1 10¾-15½, ⊠ 20-n, ⊠
22	7	08	09	08	08.3	00.0	.	18	= 6¼-13½, ⊙, ⊠
23	6	10≡	01 ⊙	01	04.0	04.5	01.3	11	●tr-o n-9¼ i, ≡o 6-11¾, = 11¾-19½, ⊙, ⊠
24	6	01	08 ⊙	06	05.7	05.4	00.1	10	= n-n, ψ n-4¾, ⊙, ⊠
25	7	06≡	08 ⊙	03	07.3	04.2	00.0	08	= n-6¾, 9½-13¾, 19½-n; ⊠ n-10½, *tr n, ψ 3½-5, ≡o 6¾-9½ i, ≡o-1 8^30-8¾, ●tr-o [19¾-19¾ i, ▽o 19^40-19½, ⊙, ⊠
26	6	10	06 ⊙	04	06.7	06.5	00.8	06	= n-15½, 19¾-n; ≃ n-9, ⊙, ⊠
27	6	10 *	10 *	07	09.0	01.3	00.0	05	= n-n, ≃ n-8^45 20-n; *tr-o-1 6^20-19i, ⊙, ⊠
28	7	10	09 ⊙	10	09.7	04.3	00.7	03	= n-12½, ∞ 12½-18¾, ⊙, ⊠
MES. VRED.		09.0	07.1	05.9	07.7	04.0	96.8		

$\varphi = 46^{\circ}\ 04'$ N $\lambda = 14^{\circ}\ 31'$ E Gr. $\Delta G = +\ 58$ min. PO. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21
1	736.8	735.7	735.3	-04.4	04.6	-00.4	-00.2	04.7	-04.6	-08.8	02.9	02.7	02.5	87	42	57	62	NE 1	NW 2	SE 1
2	731.8	727.0	723.4	-03.8	00.6	01.5	00.0	11.6	-04.8	-10.2	05.2	03.8	04.6	92	79	90	87	N 1	N 1	SW 1
3	720.6	719.7	720.3	00.4	01.2	00.1	00.4	11.6	00.0	-00.6	04.6	04.8	04.5	98	97	98	98	NE 1	SE 1	NE 1
4	720.3	717.5	715.0	00.0	01.2	00.4	00.5	11.4	-00.4	-00.6	04.4	04.8	04.6	96	97	96	96	- 0	NE 2	- 0
5	715.0	717.4	722.4	01.8	02.8	00.9	01.6	05.5	00.4	-01.9	04.4	04.7	04.6	83	84	95	87	SSW 1	SW 3	SE 2
6	729.6	731.9	724.2	-00.6	03.6	02.3	01.6	03.3	-00.8	-01.3	04.0	04.3	03.5	92	78	65	78	NE 1	SW 1	NE 2
7	735.5	734.0	736.9	-00.9	04.1	-01.2	00.2	04.8	-01.2	-01.5	03.9	03.0	03.7	90	49	68	76	S 1	SE 1	SE 1
8	737.4	735.1	724.7	-06.0	05.4	01.7	00.7	06.5	-06.7	-12.2	02.8	02.8	03.5	97	42	67	69	NW 1	NE 1	NE 2
9	735.7	734.3	736.3	-00.3	01.8	01.0	00.9	02.5	-00.4	-01.0	04.4	04.7	04.8	98	90	97	95	NE 1	NE 1	WSW 1
10	739.6	741.0	741.6	-00.4	05.0	00.6	01.4	06.2	-00.6	-03.1	04.5	04.1	04.3	100	63	89	84	NE 1	SW 1	N 1
11	740.3	737.9	736.0	01.0	03.9	01.0	01.7	04.3	00.3	-05.0	04.1	04.4	04.7	83	73	95	84	NW 1	WSW 1	N 1
12	731.9	732.0	734.1	00.4	02.0	01.5	01.6	04.5	00.4	-00.1	04.6	05.1	05.0	96	91	98	96	- 0	SW 1	SSW 1
13	738.9	746.0	739.9	00.0	07.8	02.8	03.6	08.9	00.4	-01.6	04.8	04.5	04.9	98	56	87	80	SW 1	SE 1	N 1
14	734.1	731.8	730.8	01.7	04.6	01.7	02.4	05.0	01.2	-00.9	04.8	04.3	04.9	92	68	95	85	- 0	E 1	E 1
15	729.2	729.9	732.5	00.6	02.6	00.8	01.2	03.8	00.4	-00.1	04.8	05.0	04.7	100	90	97	96	NW 1	S 2	SE 1
16	734.9	735.5	736.5	00.5	05.2	02.3	02.6	06.7	00.2	-01.8	04.4	04.0	03.9	93	61	72	76	NE 1	NE 2	SE 2
17	736.0	735.2	735.0	-01.8	04.8	02.3	01.9	06.0	-02.7	-08.1	03.6	04.2	04.1	91	66	76	78	NW 1	NE 2	SE 1
18	732.3	729.7	727.1	-00.6	07.9	03.4	04.5	08.5	-00.9	-04.5	04.0	04.7	05.6	90	59	83	77	SE 1	WSW 3	SW 2
19	725.2	727.3	730.4	00.6	04.6	02.1	02.4	06.5	00.5	00.3	04.8	05.3	05.0	96	87	93	92	E 1	W 1	SE 1
20	734.9	737.8	737.3	-00.4	11.2	04.0	04.7	12.7	-01.1	-02.3	04.5	02.3	03.3	100	25	55	60	SE 1	SE 2	- 0
21	738.6	737.5	737.9	-00.6	12.7	07.2	06.6	16.0	-00.7	-04.0	03.9	04.2	04.2	89	38	55	61	N 2	NNW 1	SW 1
22	737.6	736.7	737.7	-00.4	13.5	09.2	07.4	14.2	-00.9	-03.1	04.2	06.3	06.9	94	54	85	78	NE 1	SW 2	SW 2
23	737.1	737.0	737.1	04.0	09.5	06.4	06.6	16.0	03.5	00.0	05.2	07.7	07.0	85	84	97	89	NE 1	NW 2	NW 1
24	736.4	736.6	736.7	01.5	08.8	07.6	07.4	09.3	04.8	04.4	06.6	07.8	07.4	97	91	95	94	- 0	NE 1	NW 1
25	737.2	735.9	735.2	04.2	10.8	08.0	07.8	11.6	03.3	00.4	06.0	09.3	07.7	97	95	96	96	- 0	W 1	NW 2
26	734.6	734.2	733.6	05.8	08.4	03.5	07.8	09.1	05.7	04.8	06.5	07.6	07.8	94	92	94	93	NW 1	SW 1	- 0
27	729.2	725.5	725.0	05.0	06.9	05.9	05.9	09.4	04.8	04.0	06.4	07.2	06.5	99	96	93	96	SW 1	NE 1	NNE 2
28	726.8	727.4	728.5	-00.2	04.4	01.6	01.0	05.1	-00.2	00.0	04.4	03.9	04.1	96	62	80	80	NE 1	S 1	SW 2
29	730.6	730.2	733.7	-02.7	07.4	02.4	02.4	05.7	-03.3	-07.4	03.6	02.9	03.5	95	38	64	66	SE 1	SW 3	SW 3
30	736.3	734.4	734.4	-01.2	11.3	08.4	06.7	13.0	-02.6	-08.0	04.0	03.2	05.1	95	51	62	69	N 1	SW 4	SW 4
31	735.0	731.2	728.7	07.8	10.3	09.0	09.0	11.7	05.4	00.2	05.7	06.9	06.5	72	73	76	74	SW 3	S 3	SW 2
MES. VREDN.	732.7	732.0	732.4	00.5	06.1	03.4	03.3	07.2	00.0	-02.4	04.5	04.9	04.9	93	70	84	82	06.9	1.7	1.4

1	724.8	726.3	729.4	06.3	04.2	03.8	04.5	09.2	03.2	04.4	06.9	05.4	05.7	96	88	95	93	NW 1	NW 4	NW 1
2	727.4	725.4	725.6	04.1	06.2	00.6	02.9	06.7	00.4	01.2	05.9	06.2	04.6	95	88	96	93	NE 1	NE 2	NW 2
3	725.8	727.8	730.6	01.4	06.2	01.6	02.7	06.9	00.2	00.0	04.4	03.6	04.0	87	51	78	72	SW 1	S 11	SSW 1
4	731.1	729.8	730.9	-02.4	08.8	04.0	03.6	09.1	-03.6	-09.7	03.5	02.2	03.1	90	26	51	56	NE 1	SW 3	SW 2
5	731.1	730.8	731.3	00.0	01.1	00.6	00.6	04.1	-00.7	-02.2	04.5	04.7	04.6	98	95	96	96	N 1	N 1	NW 1
6	732.9	733.5	733.3	01.4	08.0	02.9	03.8	08.2	-00.1	-01.6	04.8	04.0	04.5	95	50	80	75	N 1	S 2	N 1
7	732.4	731.1	730.2	01.3	07.6	04.4	04.4	08.4	00.8	-04.3	04.8	06.2	05.4	95	79	85	86	NE 1	S 2	- 0
8	726.9	724.7	723.1	-00.4	07.7	05.4	04.5	08.2	-01.2	-04.8	04.5	05.4	06.3	100	68	94	87	SE 1	SE 1	NE 1
9	719.7	721.3	725.1	04.0	11.0	05.7	06.6	11.1	03.2	02.5	05.9	06.2	06.3	97	63	92	84	SW 1	SW 3	SE 1
10	729.3	730.6	732.7	05.8	13.0	06.9	08.2	13.7	05.2	00.9	06.0	04.5	05.2	86	40	70	65	SW 3	SW 4	- 0
11	734.0	734.5	735.6	01.7	06.7	04.4	04.3	07.5	00.7	-04.6	04.9	05.5	05.7	95	75	91	87	NE 1	ESE 2	NE 1
12	736.2	733.7	733.3	02.4	12.4	07.6	07.5	13.7	01.9	-01.2	05.4	04.0	04.5	98	37	57	64	N 1	NW 2	SW 2
13	732.7	731.7	731.5	02.2	11.7	07.8	07.4	13.7	01.0	-03.7	04.6	06.0	07.3	85	58	92	78	NNE 1	SW 4	- 0
14	733.2	734.1	736.2	00.8	13.6	09.0	09.6	14.0	06.5	05.0	06.5	04.3	03.9	95	37	45	56	SE 2	NW 1	NW 1
15	742.1	742.5	744.1	06.4	12.7	07.4	08.5	13.3	02.8	-04.2	04.0	0 .1	03.4	55	28	44	42	S 1	ENE 3	NW 1
16	745.9	742.9	744.0	02.0	14.4	10.2	09.2	16.1	00.0	-04.9	04.1	04.0	04.9	77	33	53	54	N 1	SE 1	- 0
17	743.8	741.7	740.5	06.8	16.2	14.4	13.0	18.6	05.4	01.7	05.8	06.8	05.8	79	49	47	58	NE 1	NW 1	SW 2
18	739.2	736.4	736.2	08.4	21.1	16.0	15.4	23.7	07.9	02.0	06.5	06.2	07.5	82	44	55	60	- 0	NE 1	W 1
19	736.3	733.0	732.6	08.0	25.7	16.7	16.8	26.0	05.7	-00.7	06.5	07.2	06.8	81	29	47	52	- 0	NE 1	SW 2
20	731.8	732.4	734.5	12.6	18.2	14.8	15.1	19.4	12.0	06.9	07.5	06.3	09.4	68	53	74	65	NE 1	SW 2	SSW 1
21	739.0	743.2	745.0	03.0	04.9	04.9	05.7	15.0	04.5	06.5	07.8	05.7	05.9	97	87	91	92	E 2	SE 2	NE 1
22	715.4	743.8	743.2	04.4	16.3	12.4	11.4	18.8	03.8	-02.0	05.7	07.2	05.8	91	52	54	66	NW 1	N 2	- 0
23	741.9	738.9	739.4	06.8	20.9	15.6	14.7	21.6	04.4	-02.3	06.6	06.8	05.4	89	37	41	56	NNE 1	SW 4	SW 3
24	737.5	735.9	737.0	12.0	21.5	16.4	16.6	22.0	10.9	07.6	08.4	07.6	08.1	80	40	56	59	NE 1	S 3	NE 1
25	736.2	733.6	731.6	12.4	17.6	13.3	14.2	18.2	11.1	08.7	08.5	09.3	09.2	78	62	80	73	W 1	NW 2	- 0
26	729.6	727.0	726.5	10.7	16.6	12.4	13.0	18.6	08.8	03.6	08.9	06.7	08.9	92	61	83	79	- 0	SW 3	SW 2
27	730.9	731.0	734.0	04.2	14.4	10.0	10.6	15.4	07.1	01.6	06.6	06.1	07.0	81	50	77	69	NE 1	NE 1	NW 1
28	734.6	734.3	733.0	07.5	08.6	07.5	07.8	10.3	06.8	05.2	07.2	06.7	07.1	92	80	91	88	NE 1	SE 2	NE 1
29	734.0	733.6	732.0	04.6	10.8	06.6	07.2	11.1	04.0	03.4	06.0	06.0	06.2	94	62	85	80	S 1	E 3	NW 1
30	735.0	736.4	738.1	01.6	07.3	05.6	05.5	10.3	00.7	-00.6	04.8	05.4	04.9	93	61	72	75	W 1	E 3	SE 1
MES. VREDN.	732.0	733.4	734.1	05.2	12.2	08.3	08.5	13.8	03.6	00.5	05.9	05.8	05.9	88	56	72	72	1.0	2.3	1.1

BR. ST. 13 H_s = 299 m H_b = 300.6 m h_t = 2.0 m h_r = 1.5 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	6	05	06⊙	00	03.7	07.1	.	04	= n-n, ⌣°n-9, ⊙, ⊠
2	6	10	10*	10*	10.0	00.0	.	05	= n-ni, *+-0 10^40 - 10^54, 13^50 n; = °18-20, ⊠
3	3	10≡*	10≡*	10≡*	10.0	00.0	12.5	14	*0-1 n-n, = n-5½, 11½-12½, = °5½-ni, ⊠
4	3	10≡*	10≡*	10≡*	10.0	00.0	37.4	45	= °n-n, *+-0-1 n-ni, *0-1 13½-19¼
5	6	09	10	10≡	09.7	02.1	21.0	41	= n-17½, *+-0-1 n, 8¼-8¾, 16^50-20^30, •+ 13^48-16^54 i, *° 16^35 16^40, = °17½-n, ⊙, ⊠
6	6	09	10*	10	09.7	00.0	03.4	30	= n-n, *+ 8¾-11½ i, ⊙, ⊠
7	7	10*	04⊙	00	04.7	05.3	00.1	27	= n-11¼, *+-0 15^40-9 i, ⊕ 16½-17½, ⊙, ⊠
8	5	10	08⊙	10	09.3	04.4	00.0	21	= n-17¾, 13-n; V° n-10½, = +-2 7¾-9¾, = +-2 9¾-13, ⊙, ⊠
9	4	10*	10*	10*	10.0	00.0	01.5	21	= n-n, *+-0 3½-11^30 18½-n; •° 14^50-15½, *+-0 15½-18½
10	7	10≡	08⊙	09	09.0	03.9	06.5	24	= ² n-9¼ i, *n, = ² 6¼-7¾, *+ 8^45-9 i, = 9¼-13¼, • 17-17½, ⊙, ⊠
11	5	10	10	10•	10.0	00.0	00.0	19	= n-n, •+-0-1 8¼-8¾ i, 15^40-18^40, *0-1 18^40 n
12	4	10≡*	10•	10	10.0	00.0	11.6	21	= n-5½, 11¾-n; *0-1 n-10¾, = °-1 5½-11¾, *° 10¾-11½, •+-0 11½-13, •+-0 13^50-16^50
13	6	10≡	09	10	09.7	04.6	03.7	21	= n-6¾, 9¼-11½, 18½-n; = °6¼-9¼, ⊙, ⊠ [⊠
14	6	10	10	10•	10.0	00.0	.	19	= n-n, •+ 7^25-9, 15^30-16¼, •° 16¼-n, ⊠
15	5	10≡*	10•	10*	10.0	00.0	03.1	18	= n-6½, 9½-n; •+-0 n-4½, 11^40-17^40; *+-0 4½-5¾; 8½-9½, 17^42 20½; *0-1 5¾-8½,
16	6	10	05⊙	06	07.0	04.9	04.8	13	= n-n, *n, ⊙, ⊠ [= °6½-9½, •+-0 9¾-11^40, ⊙, ⊠
17	6	09	08	05	07.3	01.6	.	11	= n-n, ψ 20-n, ⊙, ⊠
18	7	10	10	10	10.0	00.4	.	10	= n-n, •+ 16¾-16^55 20^20-20¾, ⊙, ⊠
19	6	10≡•*	10•	02	07.3	01.3	17.6	07	= n-5, 10¾-16½, 19½-n; •+-0-1-2 n-6¼, 9¼-10, 13¾-14¾; = °5-10½, *° 6½-9¾
20	9	10≡	05⊙	00	05.0	07.1	02.8	05	= +-2 n-9¾, = °9¾-11¾, = 11¼-12½, ⊙, ⊠ *0-1 7½-8½, ⊙, ⊠
21	8	04⊙	04⊙	03	03.7	07.4	.	02	⊙, ⊠
22	7	04⊙	01⊙	07	04.0	09.2	.	.	= n-6½, ⌣° n-7½, ⊙
23	6	10	10	10•	10.0	00.0	.	.	= n-n, •+-0 13^48, 14^50 13¼-n; •+-0 16^50-18¾
24	5	10≡•	10	09•	09.7	00.1	08.7	.	= °n-8½, •° n-5, •+-0-1 5-9½ i, 15^40 n, = 8½-n, ⊙
25	7	07≡	10•	10≡•	09.0	00.9	02.3	.	= n-5^20, 9¼-11¼, 15½-19½; = °5^20 9¼, 11½-n; •+-0-1 8¼-8½, 12¼-n; ⊙
26	5	10≡	10•	09	09.7	00.0	20.3	.	= n-ni, •+-0-1 n, 5¾-18 i; = °-1 5½-7¾ i
27	4	10≡	10•	10•	10.0	00.0	05.8	.	= °-1 n-5½, •+ n-5, = °5½-9½, •°-1 8^35-ni, = 9½-n
28	7	10≡*	06	00	05.3	03.5	32.0	04	•n, *° n-4¾, = °4½-9½, *0-1 4¾-10 i, = 9½-10½, ⊙, ⊠
29	9	10≡	08⊙	00	06.0	06.6	01.6	.	⌣² n-9½, = 4½-4¾, 7¼-11¼; = °-1 4¾-7¼ i, = °5-17, ⊙
30	8	00⊙	08	09	05.7	09.1	.	.	⌣' n-9¼, = 6¼-10¼, = 12¼-17½, ⊙
31	7	08	10•	10•	09.3	01.0	.	.	= n-6½, •+ 7^45-9¼ i, 13¾-ni; •+ 10^45-10¼, ⊙
MES. VRED.		08.9	08.4	07.4	08.2	80.5	196.7		

1	7	09	10*•	04	07.7	00.6	04.9	.	= n-12¼, 20-n; •+-0-1 n-12¾ ni, = 11^40-11^55 ⊽-1 15^40-16^50 i, ⊽ 13^40-14^50, ⊙
2	6	10	10•	10*	10.0	00.2	04.6	.	= n-n, •+ n, 19^35-19^50 i; ⊿' 15^40-15^50, *' 19^30-19^40, *+-2 19^50-n, ⊙, ⊠
3	7	10	10	00	06.7	02.5	33.0	07	= n-10¼, *+-0 n-5¾, ⊙, ⊠
4	9	01⊙	04⊙	06	03.7	08.1	.	02	= 5½-10, ⊙, ⊠
5	2	10*	10*	10*	10.0	00.0	12.6	13	= n-n, *+-2 n-n, ⊓° 14^40-14^30 i
6	8	09≡	04⊙	10	07.7	04.3	30.1	19	= n-5½, 9-11½, = °5½-9, ⊙, ⊠
7	5	10•*	09•	00	06.3	03.0	04.6	10	= n-n, •+-0 n-9^50 i, ⊿ •' 4^55! 5^40 *' 6-6^50 ⊽+-0 10^40-15^57, 18^42-18^51, ⊙, ⊠
8	5	10≡	10•	10•	10.0	00.3	01.5	04	= ² n-7¼, = °-1 7¼-9¼, = 9¼-n, •+-0 13¼-ni, •+ 14-14½, ⊙, ⊠
9	7	10•≡	05⊙	06	07.0	02.1	22.9	.	= °n-11½, •+-0-1 n-19½ i, = 11½-13¼, ⊓ 14-14½, ⊙
10	8	09•⊓	04⊙	04	05.7	09.1	08.3	.	•+-0-1 n, 4¼-9; ⊽+-0-1 n-4¼, 9-9½; ⊓° 6^30-7¼, ⊙
11	7	09	10•	10•	09.7	00.0	02.1	.	= n-12¼, •+-0-1 10^40 ni, ⊙
12	7	10≡	04⊙	00	04.7	09.8	07.0	.	= n-5½, 7¾-11½; •+ n-3¾, = °5½-7¾ i, = °6-7½, ⊙
13	7	08	10	10•	09.3	02.9	.	.	⊿' n-9½, = 5½-9, •+-0 16^40-ni, = 19½ n, ⊙
14	9	10•	07⊙	10	09.0	01.8	04.3	.	= n-9¼, •+-0-1 n-8 i, ⊙
15	8	08	04⊙	00	04.0	11.3	00.1	.	= 5¼-10¼, ⊙
16	7	01⊙	01⊙	05	02.3	03.3	.	.	⌣° n, 7¼, = 4¾-7¾, 20-n; ∞ 7¾-20, ⊕ 17-18¼, ⊽ 18¼-n, ⊙
17	6	08	10•	10	09.3	02.4	.	.	= n-9¼, ∞ 9¼-n, •+ 12^50-14¼, ⊙
18	7	10	06⊙	00	05.3	06.1	00.0	.	= n-12¾, ⊿° n-9½, ∞ 12-15, ⊙
19	9	01⊙	02⊙	07	03.3	10.1	.	.	⊿' n-9, = 4½-9, ∞ 9-12¼, 18½-n; ⊙
20	8	08⊙	09⊙	10	09.0	03.2	.	.	= n-9¼, ∞ 9¼-11½, ⊽+-0 20^45-20^55, = 20½-n, ⊙
21	6	10•	10•	10	10.0	00.0	26.3	.	= n-16½, •°-1 n-17½, T° 6^05
22	9	10	03⊙	04	05.7	06.9	25.0	.	= n-12, ψ 20-n, ⊙
23	8	04⊙	03⊙	00	03.0	09.8	.	.	= n-5½, ψ n-4¾, ⌣' n-7¼, ⊙
24	7	10	06⊙	03	08.0	05.6	.	.	= n-13, ⊿° n-9½, ∞ 13-16, ⊙
25	7	09	07	00	05.3	04.0	.	.	⊿' n-8, 20-n; •+-0-1 8-12^04 i, ⊙
26	7	04⊙	03•	09•	07.3	03.9	01.2	.	= n-9¼, 19¾-n; ⊿² n-9½, = SW 12½-13½, ⊽+-0 13^50 14¾, •+-0 14^45 ni, ⊙ 20¾-n, ⊙
27	9	05⊙	09•	10	09.0	06.5	03.4	.	•n, T° 12^05 12¾, ⊽+-0 12^20-20¾ i, ⊓°-1 14^45-14^55 18^45 ni; ⊙
28	7	10•	10•	10•	10.0	00.3	04.5	.	= n-9½, 13½-n; •+-0-1 n, 7¼, 14^50 ni; ⊙
29	7	10•	07	08	08.3	01.7	14.1	.	•+-0 n-9½ i, 12-12^05 18^45-19¾, ⊿ 20¼-n, ⊙
30	8	09	04⊙	00	04.3	03.3	26.7	02	= n-6, T n-5½, ⊽' n' 3½, ⊽° 3½-4^20, •° 4^20-5, ⊽+ 15^30-15^50, ⊿° 20-n, ⊙, ⊠
MES. VRED.		08.1	07.[illegible]	06.0	07.0	135.5	237.3		

$\varphi = 46^{\circ}\ 04'$ N $\lambda = 14^{\circ}\ 31'$ E Gr. $\Delta G =$ + 58 min. BR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	737.4	736.3	729.1	01.2	12.1	05.3	06.0	12.4	-06.4	-04.7	04.1	03.8	04.8	97	36	72	68	NE 1	NE 2	- 0
2	739.2	737.8	740.0	02.7	10.1	06.5	06.6	11.9	01.6	-06.1	04.9	05.9	04.5	87	42	61	62	- 0	ENE 1	E 2
3	741.2	739.5	740.1	02.8	13.4	09.2	08.5	15.0	00.2	-06.0	04.8	03.8	04.8	86	32	65	58	NE 1	E 2	- 0
4	739.2	739.8	734.5	04.2	17.6	11.2	11.0	18.8	01.4	-05.0	05.1	05.3	05.8	82	35	58	58	NE 1	NW 1	NE 1
5	731.5	730.1	731.7	06.7	10.9	09.0	08.9	15.7	04.4	-02.0	05.8	07.6	08.1	79	77	94	83	SE 1	E 3	NE 1
6	734.1	731.5	734.5	08.6	13.6	11.4	11.2	15.3	08.0	06.1	07.1	07.2	07.6	85	62	75	74	SE 2	N 1	NE 1
7	733.6	731.7	732.7	09.2	14.0	11.6	11.6	15.0	08.9	07.8	08.1	09.5	08.4	93	79	82	85	N 1	NW 1	- 0
8	732.8	732.1	723.9	11.0	16.3	10.4	12.0	18.6	10.0	07.0	09.3	10.2	08.6	94	73	91	86	NE 1	SW 2	SW 1
9	736.2	735.3	735.4	06.0	18.2	12.6	12.4	19.0	03.9	-00.9	07.0	05.1	05.2	100	33	48	60	N 1	SW 4	SW 3
10	732.8	729.3	729.6	10.6	21.2	13.0	14.6	23.0	07.5	01.8	07.1	07.2	10.1	74	37	90	67	NE 1	SW 2	NE 1
11	729.0	729.0	729.2	12.3	17.5	13.8	14.4	18.2	11.0	04.9	07.5	06.0	07.2	70	40	61	57	SW 3	SW 5	SW 1
12	729.7	729.2	731.3	11.8	16.4	10.9	12.5	17.0	10.9	07.6	07.4	07.1	08.8	72	51	90	71	SW 2	SW 4	SW 2
13	732.5	732.4	734.4	09.0	19.8	13.9	14.2	19.9	07.8	03.9	08.2	08.8	08.4	95	51	70	72	NW 1	SW 3	SW 2
14	736.5	734.8	734.8	05.7	21.7	15.6	15.6	22.4	06.7	00.6	08.0	03.4	08.0	89	43	60	64	NE 1	SSW 5	SW 2
15	736.5	731.3	731.4	15.6	19.5	14.2	15.6	19.7	12.4	05.0	06.7	08.2	09.4	66	50	78	65	SW 4	SW 4	SW 1
16	730.2	729.5	731.1	12.0	19.1	12.2	13.9	19.8	07.5	00.9	08.3	03.7	09.0	79	52	85	72	NE 1	SW 3	- 0
17	732.1	731.4	733.9	11.0	19.1	12.3	13.7	19.5	10.7	08.4	09.3	09.1	09.7	94	55	90	80	N 1	NW 2	SW 1
18	736.7	737.2	740.7	10.8	21.0	14.4	15.0	21.0	09.0	04.5	09.2	05.4	04.5	98	29	89	95	NE 1	N 3	NE 1
19	741.8	739.7	739.3	10.0	20.6	12.9	14.2	21.2	06.8	-01.2	05.8	05.5	06.9	60	30	62	51	SW 2	SW 2	- 0
20	738.1	735.7	735.6	10.6	22.1	16.4	16.4	22.7	05.5	-01.3	07.5	06.4	07.3	76	32	52	53	NE 1	E 1	NE 1
21	734.7	730.9	728.8	12.8	19.7	13.0	14.6	22.7	10.5	03.0	09.2	08.6	10.0	83	50	89	74	SE 1	SE 3	NE 1
22	730.1	731.2	732.1	07.7	10.2	09.4	09.2	13.2	07.3	06.6	07.5	07.5	08.2	92	80	93	88	SE 2	SE 3	- 0
23	737.1	738.1	741.4	03.2	14.0	08.2	08.9	17.3	04.4	-00.3	06.3	05.6	07.3	96	46	90	77	- 0	W 2	NE 1
24	745.0	745.0	744.5	05.5	17.8	12.4	12.0	19.0	04.6	-01.5	06.7	05.3	06.1	99	35	56	63	SE 1	NE 3	SE 1
25	744.6	740.5	739.8	06.8	20.5	14.6	14.6	22.0	04.2	-02.3	06.3	07.2	07.7	75	39	62	59	ESE 1	SSW 2	SSW 1
26	738.4	737.0	739.5	11.6	20.5	11.4	13.7	21.9	09.4	04.5	08.3	09.9	09.6	81	55	95	77	ENE 1	SE 2	SW 1
27	739.3	737.0	736.1	10.0	15.4	13.5	13.1	16.0	09.4	05.4	09.2	08.1	08.5	100	62	73	78	NE 1	NE 2	E 1
28	736.9	736.0	737.0	13.0	16.6	10.7	12.8	18.3	10.0	05.9	08.5	07.0	08.2	76	50	85	70	- 0	SE 2	NW 1
29	736.6	734.7	734.9	07.0	20.4	14.2	14.0	20.6	05.7	06.0	07.3	07.5	06.0	97	42	49	63	NE 1	SW 4	SW 2
30	734.9	732.7	735.9	09.6	14.0	12.7	12.2	15.3	07.1	01.0	06.9	10.1	09.9	77	84	90	84	N 1	SW 1	NE 1
31	737.8	737.2	739.0	12.6	20.6	14.6	15.6	22.9	11.0	09.0	09.7	08.3	09.5	89	46	76	70	W 1	SW 2	E 1
MES. VRED.	735.8	734.7	735.6	09.0	17.2	12.0	12.6	18.6	07.0	02.1	07.4	07.2	07.7	85	49	75	69	1.2	2.6	1.0

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1	740.7	739.7	739.3	12.6	20.6	17.0	16.8	23.0	10.3	04.0	09.7	03.4	11.0	89	46	76	70	NE 1	E 1	SSE 1
2	739.6	739.4	740.9	12.4	15.6	12.2	13.1	19.0	11.6	05.5	10.1	11.2	08.6	93	84	80	86	SW 1	NE 3	SE 3
3	742.1	740.1	739.7	09.1	17.1	13.2	13.2	18.8	06.1	00.6	07.3	06.8	07.8	84	46	69	66	SE 1	NE 2	E 1
4	738.1	736.7	736.8	10.8	19.1	14.6	14.6	20.0	08.4	02.7	09.3	06.3	07.1	95	38	57	63	NE 1	E 2	SW 2
5	736.2	735.5	735.9	11.0	20.2	15.6	15.6	20.6	06.0	00.4	08.0	08.6	06.3	82	49	47	59	N 1	SW 5	SW 5
6	736.4	736.1	736.2	13.2	21.0	16.2	16.6	21.4	12.2	04.5	09.2	10.6	10.6	81	57	77	72	N 1	SW 3	SW 2
7	735.7	735.3	735.3	16.1	20.8	18.4	18.4	22.0	15.0	11.8	10.9	10.7	12.4	80	58	78	72	SW 3	SSW 3	NE 1
8	735.9	734.8	735.9	16.6	23.6	19.8	20.0	24.6	14.5	12.1	12.8	12.7	13.9	90	58	80	76	SE 1	E 1	NE 2
9	736.1	735.2	735.5	16.7	22.5	19.4	19.5	23.5	15.2	09.8	12.7	13.7	13.1	89	77	77	81	SW 1	E 1	NE 2
10	734.8	733.1	734.0	15.2	24.6	16.4	19.2	26.2	14.3	08.4	12.4	10.7	12.9	96	46	81	74	NW 1	SW 4	NE 1
11	734.4	733.5	734.9	15.8	25.6	20.7	20.8	27.8	15.0	12.6	11.6	12.5	11.8	86	50	65	67	N 1	NE 1	SW 1
12	735.5	733.2	733.2	14.0	27.4	20.6	20.6	28.1	13.1	12.4	10.7	09.6	10.3	90	35	57	61	- 0	SW 2	W 2
13	733.4	731.6	732.5	15.4	25.8	21.0	20.8	28.0	12.3	06.5	10.7	12.3	13.1	81	49	70	67	N 1	SSW 2	SW 1
14	734.0	733.2	733.9	16.6	18.7	15.8	16.7	21.2	14.8	09.3	12.8	13.5	12.5	90	84	93	89	N 1	NW 1	S 1
15	735.6	735.4	736.6	14.3	25.9	19.0	19.6	26.4	12.9	08.0	12.0	12.9	14.4	96	51	87	79	- 0	SE 1	NW 1
16	736.4	735.5	735.9	16.3	27.3	21.8	21.8	27.7	14.7	10.6	13.1	12.8	13.9	94	47	71	71	E 1	SSW 4	SW 1
17	735.4	733.3	733.5	19.0	28.4	22.0	22.8	29.6	16.0	12.6	13.5	11.5	11.8	82	40	59	60	N 1	SW 4	S 1
18	732.3	731.4	733.4	19.3	20.7	19.9	17.0	25.0	13.8	10.9	12.4	14.0	11.5	74	76	97	82	- 0	E 2	NE 1
19	733.0	734.5	736.0	14.6	15.7	16.1	15.6	18.0	13.6	12.3	11.7	12.3	12.2	94	92	89	92	W 1	SE 1	- 0
20	736.7	736.6	739.1	15.5	25.0	18.8	19.8	26.0	14.4	12.2	12.2	10.1	11.0	92	41	68	67	- 0	S 1	SE 1
21	740.6	739.5	740.3	15.8	28.2	20.8	21.4	28.4	11.8	06.9	11.0	10.1	13.4	81	35	72	63	NE 1	NE 2	- 0
22	740.5	738.8	738.5	18.1	29.5	21.8	22.8	29.9	13.8	09.0	11.2	13.3	13.3	72	43	68	61	SE 1	SE 1	S 1
23	738.2	736.5	737.1	19.0	30.4	23.0	23.8	30.4	15.1	09.4	13.5	11.6	09.1	82	35	43	53	- 0	SW 4	SW 2
24	738.0	737.9	739.2	18.6	22.7	17.4	19.0	27.2	13.4	03.4	11.3	12.0	12.4	70	56	83	70	- 0	SW 2	SW 1
25	739.8	739.3	740.1	16.9	26.7	21.0	21.4	28.2	14.4	08.3	12.4	14.2	12.8	87	54	69	70	SE 1	NE 2	S 1
26	741.7	738.9	739.9	19.2	27.8	17.8	20.6	28.3	15.5	10.5	13.3	14.0	14.1	80	50	92	74	S 1	E 3	NE 1
27	740.0	738.0	737.4	16.0	28.3	21.1	21.6	28.8	15.4	12.1	13.1	14.7	14.2	96	51	76	74	SSW 1	E 1	SW 1
28	737.7	735.7	735.7	17.6	29.7	23.6	23.6	30.3	16.5	12.0	14.8	14.1	13.6	98	45	62	68	NE 1	SW 4	SW 2
29	736.2	736.0	736.8	12.0	21.2	17.8	15.7	24.0	15.9	10.6	12.9	13.9	13.2	93	74	86	81	- 0	NE 3	E 1
30	736.4	731.6	729.7	17.4	18.6	16.5	17.2	21.6	16.0	15.0	13.1	14.0	13.4	93	87	95	90	N 1	SE 1	SW 2
MES. VRED.	737.0	735.9	736.4	15.7	23.6	18.5	19.1	25.1	12.4	09.0	11.6	11.8	11.9	86	55	74	72	0.8	2.2	1.4

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BR. ST. 13 H_s = 299 m H_b = 300.6 m h_t = 2.0 m h_r = 1.5 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	9	10●	08	00	06.0	06.1	00.1	.	= n-3½, 6^55 8½; ⌣ n-5¼, ≡ °1 3½-3^55, 6½-6^55, ≡ 1 3^55-6½, ●^tr-16½-8¼i,
2	9	10	08	00	06.0	07.1	01.0	.	△ n-10¾, 19¾-n; ⊙ [✱ °7^40 7¾, ⊠
3	8	01⊙	03⊙	00	01.3	12.2	.	.	△ °n-9½, 20½-n; = 5¾-9¼, ⊙
4	8	00⊙	04⊙	00	01.3	11.9	.	.	⌣ °n-6¾, = 5½-11, △ °-1 20-n, ⊙
5	6	10	10●	10	10.0	01.8	.	.	△ 1 n-10¾, = 6¼-9½, 13½-n; Φ °-1 7½-11¼ i, ∞ 9½-12½, ⊙
6	7	10	10	10	10.0	02.9	06.1	.	●^tr-0 n-3^40, 20^40-20¼, ⊙
7	6	10	10●	10●	10.0	00.8	01.9	.	= n-n, ●^tr-0-1 n, 3½-15¼i, 19^28-n; ♈ 1 20, ⊙
8	7	10≡	07●	00	05.7	03.1	05.7	.	≡ °-1 n-5¾, ●^tr-0 n-5¾, 9-9^05 19^20 19^40 1, ≡ °5¾-8¾, = 8¾-13½, ♁^tr-0-1 12^40-14^40 i,
9	8	00≡⊙	05⊙	10	05.0	03.5	04.4	.	≡ 2 n-6^40, ≡ 2 6^40-8½, = 8½-9, ⊙ [17^45-18½, Tw 17^40, ⊙
10	8	05⊙	08⊙	10●	07.7	05.4	.	.	△ 1 n-9½, ●^tr 15^22-18^00 i, 20^45 n; ⊙
11	8	08	03⊙	08	06.3	07.6	05.2	.	●^tr n, 9½-9¾; Fsw 12½-16½, ⊙
12	7	09	09⊙	10●	08.0	04.5	00.0	.	♁^tr-d-1 8^mm-9, 16-17½ i; ●^0-1 17½-n, = 18½-n, ⊙
13	8	06	04⊙	01	03.7	09.3	04.7	.	● n, ≡ 1 n-4¾, ≡ °-1-2 4¾-6^58, = 6^58-10, ⊙
14	8	00⊙	04⊙	00	01.3	13.2	.	.	= n-9½ i, △ 1 n-10¼, ≡ °4-4¾, 7^05 7½°, ⊙
15	8	04⊙	08	02	04.7	08.7	.	.	△ °n-7, F 12½-13, ⊙
16	7	04	09	08	07.0	05.6	.	.	= n-7¾, △ 2 n-9½, ♈ °10^20 17¾ i, ♁^tr-0 12^34-12^45 16^55-17¼; ●^tr 17¼-19½ i, ⊙
17	7	10●	09⊙	08	09.0	02.4	01.8	.	●^tr-0 n-9^55 = n-10½, T °-1 14^26-14¾, ♈ 1 14¾-15^19¼, ♁^tr-0-1 14¾-15^59, 18^31-19^50, ⊙
18	8	03≡	05⊙	04	04.0	09.8	06.7	.	≡ 2 n-6^50 L, ≡ °-1 6^55-8½, = 8½-10½, ψ 19¾-20¼, ⊙
19	9	01⊙	05⊙	00	02.0	13.1	.	.	△ °-1 n-6½, 20-n; ⊙
20	8	03⊙	05⊙	09	05.7	10.4	.	.	△ 2 n-10½, ⊙
21	7	03⊙	09⊙	09	07.0	07.9	.	.	△ 1 n-8¼, ∞ n-15, ♁ K-16¼, ⊙
22	6	10●	10	08	09.3	00.1	23.4	.	= n-14, F n-5½, ●^lo-1 n-13^03, ♈ n, ⊙
23	8	08≡⊙	09	01	06.0	03.2	07.2	.	≡ °-1 n-6¼, △ 2 n-11½, ≡ °6¼-7½, = 7½-9¼, ♁^tr 13^35-16^20 i, Fsw 14^30-16, T 15½
24	8	10≡	04⊙	01	05.0	10.7	00.7	.	≡ °-1-2 n-8¼, ≡ °8¼-8½, = 8½-10½, ⊙ [15^50 ⊙
25	8	01⊙	03⊙	04	02.7	11.3	.	.	△ 2 n-9½, = 5½-8¾, ⊙
26	6	07⊙	06⊙	00	04.3	01.9	.	.	= n-n, △ °n-7¾, ●^tr 7¾-8^10 11^15, 11^25, ♁^tr 12^50-13^10 15¾-19^30, ♈ 15½-16½, ⊙
27	7	00≡	08⊙	07	05.0	05.7	17.3	.	≡ °-2 n-8½, = 8½-13½, ●^tr 11-13^10, ♁ 20½-n, ⊙
28	7	04⊙	07⊙	00	03.7	07.7	00.3	.	● n, = n-9½, ♁^tr-0 9-11^44 i, 16^34-17 i, ∞ 9½-16, ♈ 16^30-16^40, ⊙
29	8	00≡	07⊙	03	03.3	10.5	00.9	.	≡ 2 n-7¾, △ 2 n-10½, ≡ °7¾-8½, = 8½-10¾, ⊙
30	7	08	10	10●	09.3	01.0	.	.	△ °n-6½, ∞ n-9, ●^tr-6 10-10¾, 13¼-n; ● °12½-13¾, ⊙
31	8	09	04⊙	04	05.7	09.1	03.9	.	● n, = n-9½, ∞ 9½-12, ♈ °13^32-15^40, ♁^tr 17^50-18, ⊙
MES. VRED.		05.6	06.7	04.7	05.7	213.5	91.3		

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1	8	07⊙	08⊙	04	06.3	07.4	00.0	.	△ 2 n-10½, 20½-n; = n-9½, ⊙
2	7	10●	01♈	05	06.7	06.2	01.0	.	△ 2 n-3^50 = n-11½, ●^tr 3^50-8¾ i, ♁^tr-0-1 11^40-14 i, ♈ 1 13^35-14^20, ⊙
3	8	02⊙	04⊙	06	04.0	07.6	01.8	.	= n-7¾, △ 2 n-9½, ♁^0-1 10^50-12^50 i, 15^35-15^45, 18^02-18^10, ⊙
4	8	05⊙	04⊙	01	03.3	11.8	00.2	.	= n-9½, △ n-10½, ⊙
5	8	00⊙	02⊙	04	02.0	13.1	.	.	△ 1 n-9½, = n-8, Fsw 10½-13¾ i, ⊙
6	8	10	03⊙	09	07.3	09.1	.	.	= 6½-7¾, ⊕ 17-18½, ⊙
7	7	10	09⊙	10	09.7	04.0	.	.	⊙
8	7	10	08⊙	09	09.0	07.2	02.4	.	= n-10½, ⊙
9	7	10	09⊙	09●	09.0	02.1	00.3	.	△ 1 n-5^55 = n-12, ♁^tr-0 5^55-6^35, 13^03-13^50, 20^12-n; ●^tr-0 7^00-9½, ⊙
10	8	10≡	08♈	06	08.0	05.8	03.7	.	♈ n, 16^50-16^55, = n-4½, 8-9½, ≡ °4½-8 i, ≡ °-1 4¾-7¾ i, T °13^35-16¾ i, ⊙
11	8	06⊙	04⊙	04	04.7	10.4	00.0	.	△ °n-8½, ⊙
12	8	09	03⊙	03	05.0	10.3	00.0	.	△ 1 n-5¾, ●^tr 5¾-6, ⊙
13	7	01⊙	04⊙	05	03.3	11.3	.	.	△ 1 n-9¾, = n-9½, ∞ 9½-13½, ♁^tr-0-2 12½-13½, T °12^40-13¾ i, ♈ °-1-2 13-13^30, ψ 17¼
14	6	09	10♈	10	09.7	01.3	07.6	.	= n-17½, T °6^12-6^26 10^38-18¾ i, ♈ °-2 6^26-7¾ i, K^39-17¾ i, ♁ °-1 6^14-7½ i, 11^50-18^55; ⊙ [n, ⊙
15	7	10≡	06⊙	06	07.3	04.9	15.6	.	≡ °-1-2 n-7¾, = 7¾-12, ∞ 12-n, ♈ °14^31-15¾, ♁^tr-6 14^33-16½, ⊙
16	7	10≡	02⊙	06	06.0	08.5	00.2	.	△ 2 n-10, ≡ °n-7¼, ≡ °7¼-8½, = 8½-9½, ∞ 9½-n, ⊙
17	7	06⊙	02⊙	10	06.0	10.5	.	.	= n-10½, △ °n-8½, ⊙
18	7	02⊙	10●	10●	07.3	05.4	.	.	△ °n-8, = 6¼-9¾, 16½-n; ∞ 9¾-16½, T 12-13¾, ♈ 13¾-n; ♁^tr-0-2 12^46-n; ●^tr 18
19	6	10≡●	10	10	10.0	00.3	36.2	.	♁ °-1 n, ≡ °n-8¾, ●^0-1-2 5¾, 13½, 19¾-n; = 8¾-n, ⊙ [19½, ⊙
20	7	08⊙	02⊙	02	04.0	10.9	09.5	.	≡ °n-6½, ≡ °6½-7¾, = 7¾-10½, ⊙
21	8	10⊙	03⊙	00	04.3	13.3	.	.	△ 2 n-9½, ⊙
22	8	02⊙	03⊙	01	02.0	13.4	.	.	= n-5¼, △ 1 n-8½, ⊙
23	7	00⊙	04⊙	02	02.0	13.5	.	.	= n-11½, △ °n-9, ∞ 11½-19¼, ⊙
24	8	01⊙	07♈⊙	06	05.3	06.3	.	.	△ °n-8½, = n-6½, T °13^40-17½, ♁^tr 14^40-16¾ i, ●^tr 16¾-18¼, ⊙
25	8	05⊙	09	02	05.3	10.6	00.2	.	= n-9½, △ 1 n-9¾, T 14¾, ⊙
26	7	03⊙	05⊙	02	03.3	09.5	.	.	= n-10½, △ °n-8½, ♁^0-1 15^40-16¾, T 15^40-15^50, ♈ °-1 15^50-16^40, ⊙
27	7	10≡	04⊙	05	06.3	08.8	02.8	.	≡ °-1-2 n-7¾, △ 2 n-9^50 = 7¾-9^55 = 7^55-12, T °, 17^40 19, ⊙
28	7	10≡	04⊙	02	05.3	07.4	.	.	≡ 1-2 n-8^20, △ 2 n-3 = °-1 3^20-9, = 9-13¾, ∞ 16½-18½, ♁ 21^40-n, ⊙
29	7	07⊙	10⊙	10●	09.0	05.1	00.4	.	∞ n-9¼, ♁^tr-0-1 5^40-7^18 i, 10-11½, 20^50-21¼, ●^0-1 11½-12, 21-n; T °9¾-11^55, ♈ 1-2 10^20
30	7	09⊙	10♈●	10●♈	09.7	02.0	13.5	.	♁^tr-0-1 n, 7^45-7^50, 12^40-14¼, 19^50-n; = n-7¾, ∞ 7¾-n, ♈ 12^35-14¼, 17^30-n; ⊙ L 11½, ⊙
MES. VRED.		06.7	05.8	05.6	06.0	240.9	95.5		

φ = 46° 04' N λ = 14° 31' E Gr. ΔG = + 58 min. BR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	732.9	732.9	733.1	11.6	17.3	15.0	14.7	19.4	10.5	08.4	09.5	09.2	09.9	93	62	77	77	E 1	SSE 2	SE 1
2	732.6	730.9	731.2	11.0	24.4	19.2	16.4	24.8	09.3	05.0	09.6	10.1	13.4	98	44	80	74	NE 1	SW 3	SW 1
3	734.5	736.0	736.7	13.2	13.4	12.4	12.8	19.4	12.4	12.3	10.4	09.8	10.3	91	85	96	91	ESE 2	- 0	N 1
4	736.9	737.6	738.5	11.8	14.1	12.4	12.7	14.8	11.4	10.6	10.1	09.4	08.7	98	77	80	85	NE 1	ESE 1	SE 1
5	739.2	739.3	739.7	10.0	23.0	16.6	16.6	23.3	08.9	04.0	09.2	08.3	09.4	100	39	67	69	SE 1	N 2	SE 1
6	740.7	739.9	739.3	12.8	24.8	18.6	18.7	25.6	08.6	04.2	08.8	10.1	11.3	80	43	70	64	NE 1	NE 2	- 0
7	738.7	736.3	735.9	15.4	25.7	20.1	20.3	26.3	11.7	06.5	10.8	10.9	13.0	82	44	74	67	N 1	SE 3	E 1
8	735.5	733.6	733.5	16.4	26.6	22.1	21.8	27.4	13.7	09.2	12.1	13.6	15.7	86	52	79	72	- 0	ENE 2	E 1
9	734.2	732.8	734.6	16.8	30.1	22.2	22.8	30.6	15.5	11.9	14.1	13.8	14.0	98	43	70	70	NNE 1	SW 2	SW 1
10	737.7	738.0	739.1	19.0	27.3	23.2	23.3	28.3	15.6	11.4	13.3	13.8	15.0	80	49	70	66	E 1	SE 3	ENE 1
11	739.5	737.7	737.6	19.0	29.1	24.0	24.0	29.8	16.5	11.8	14.5	14.3	15.4	88	47	69	68	N 1	N 2	SE 1
12	739.9	738.8	739.2	19.0	28.1	23.0	23.3	28.8	17.3	14.1	14.5	14.5	15.1	88	51	72	70	NNW 1	SE 2	E 1
13	740.5	739.3	737.0	20.1	28.7	23.9	24.2	29.5	17.4	13.0	14.6	13.4	15.0	83	45	67	65	NE 1	ESE 2	E 1
14	735.3	731.7	730.5	19.4	30.1	24.3	24.5	30.6	17.0	13.0	14.8	13.8	12.3	87	43	54	61	N 1	SW 3	SW 2
15	725.2	722.3	731.6	21.5	25.9	08.8	16.2	26.6	08.0	14.7	14.3	13.0	08.1	75	52	95	74	NE 1	SE 2	NE 3
16	730.8	731.5	731.9	09.2	11.4	11.4	10.8	12.0	08.7	08.1	07.9	08.8	09.3	90	88	92	90	SE 1	SSE 2	SSE 1
17	732.1	732.4	734.4	11.1	17.2	13.8	14.0	21.0	10.3	09.0	08.9	08.8	05.8	90	60	49	66	SW 1	NE 1	NW 1
18	734.4	734.5	734.5	13.8	22.6	14.4	16.3	22.8	10.2	05.8	06.5	06.6	07.2	55	32	59	49	SW 1	NW 2	NW 1
19	735.4	731.6	731.8	11.4	23.3	17.9	17.6	23.5	08.2	03.7	07.5	07.7	07.1	74	36	46	52	NE 1	SW 4	SW 2
20	731.0	731.3	731.3	15.0	19.8	19.2	18.3	22.2	11.4	07.6	10.0	12.3	12.5	78	71	75	75	N 1	SW 4	SW 4
21	734.1	735.7	736.6	17.8	21.6	20.0	19.8	23.7	16.3	12.4	13.0	13.8	13.0	85	71	74	77	NE 1	SW 5	SW 1
22	736.1	736.6	737.4	17.0	29.7	22.8	23.1	30.3	13.9	09.5	12.1	12.5	14.0	83	40	67	63	NE 1	W 2	SW 1
23	739.6	737.5	737.9	19.3	31.2	23.7	24.6	32.4	15.8	10.7	13.0	15.2	13.8	77	45	63	62	SE 1	SE 1	- 0
24	738.2	735.7	733.6	20.7	30.8	24.0	24.9	31.2	17.1	12.9	13.7	16.3	16.2	75	49	72	65	NE 1	SE 2	NE 1
25	730.1	732.5	733.5	19.8	18.4	16.2	17.6	24.7	13.2	14.4	16.1	10.4	11.1	93	66	81	80	SW 1	SE 1	NE 1
26	734.7	735.1	736.3	13.8	22.1	18.3	18.1	23.7	10.4	07.5	10.8	09.0	11.1	92	45	71	69	NE 1	NE 1	NE 1
27	737.6	736.8	738.5	13.1	26.8	20.2	20.1	27.0	11.3	07.6	10.7	11.7	11.5	95	44	65	68	NE 1	SW 3	SW 1
28	740.1	738.4	738.0	17.3	28.4	22.7	22.8	29.0	14.0	10.3	11.8	14.1	15.6	79	49	75	68	SE 1	NE 3	SE 1
29	738.0	736.2	736.5	17.0	29.9	23.6	23.5	29.9	16.3	12.5	14.4	15.6	14.8	99	50	68	72	- 0	NE 1	E 1
30	739.6	738.9	739.6	20.8	28.3	21.6	22.1	28.4	18.3	14.7	15.9	13.2	14.6	86	46	75	69	NW 1	NE 3	- 0
31	740.1	738.4	738.8	18.9	27.7	21.7	22.5	27.8	17.0	13.2	14.0	12.0	14.8	86	43	76	68	NE 1	SE 2	E 1
MES. PRED.	735.9	735.1	735.7	15.9	24.4	19.3	19.7	25.6	13.1	10.0	11.8	11.8	12.2	86	52	72	70	1.0	2.1	1.1

1970 AVGUST LJUBLJANA BEŽIGRAD

1	740.2	738.6	739.2	16.4	29.1	21.7	22.2	29.3	15.4	11.9	13.7	13.3	15.8	98	44	81	74	N 1	SE 1	NW 1
2	738.6	736.8	736.4	17.7	26.8	20.4	21.3	28.1	15.7	12.0	13.6	15.8	14.0	90	60	78	76	NE 1	SE 2	NE 1
3	736.1	732.9	734.2	16.2	27.2	21.4	21.6	27.8	15.2	12.6	13.0	14.4	15.9	94	53	83	77	NE 1	N 1	S 1
4	735.2	734.1	736.0	18.2	27.8	20.4	21.7	29.6	16.8	13.6	14.2	12.7	14.6	91	45	81	72	SE 1	SW 1	N 1
5	737.4	736.8	737.6	16.4	30.4	23.3	23.4	31.0	15.1	12.8	13.6	12.3	13.9	97	38	65	67	N 1	SE 2	SW 1
6	737.9	736.6	736.3	19.1	31.3	24.8	25.0	31.7	16.2	12.5	13.8	15.2	14.7	83	44	62	63	NE 1	SW 4	SW 2
7	735.8	734.0	734.3	19.9	32.6	25.1	25.7	33.2	18.0	15.1	15.4	14.5	12.8	88	39	54	60	SE 1	S 4	NE 1
8	733.7	732.4	731.5	20.5	30.6	23.4	24.5	30.6	18.3	14.7	13.6	14.9	15.1	75	45	70	63	NE 1	SE 2	E 2
9	730.3	729.5	730.5	16.2	16.4	16.4	16.4	23.4	15.6	13.9	12.5	13.4	13.4	90	96	96	94	N 1	W 2	SE 1
10	731.6	732.1	733.3	15.8	23.7	13.2	19.0	25.0	15.4	13.2	12.7	12.6	13.4	94	57	85	79	SW 1	NE 1	NE 1
11	733.8	733.8	734.8	16.7	23.0	18.4	19.1	24.4	16.3	15.3	13.6	13.6	14.0	95	64	88	82	NE 1	W 1	S 1
12	737.8	737.8	737.8	16.7	24.1	19.2	19.8	24.5	16.2	14.6	12.9	13.5	13.2	90	60	79	76	NE 1	NE 2	E 1
13	738.9	738.6	738.4	16.0	21.5	18.8	18.8	23.0	14.0	11.6	13.0	12.6	14.2	95	63	87	82	NE 1	NE 1	NE 1
14	736.5	737.5	738.5	16.2	28.4	22.8	22.6	29.6	15.3	11.8	13.0	16.0	16.1	94	55	78	76	SW 1	N 1	SW 2
15	738.4	736.9	736.1	19.2	27.1	21.2	22.2	27.8	16.5	12.8	14.0	16.3	12.9	84	60	68	71	NE 1	SE 2	SW 2
16	736.2	733.9	732.8	17.0	26.3	22.4	22.1	27.7	15.0	11.8	13.4	14.1	18.0	92	54	88	78	S 1	SE 1	S 1
17	731.4	729.8	732.4	17.9	21.4	15.6	17.6	24.5	15.4	14.0	14.7	15.0	12.2	95	78	92	88	- 0	SE 2	SE 1
18	734.8	733.9	733.8	13.8	21.8	16.4	17.1	22.3	13.2	10.0	11.2	11.7	12.1	95	60	86	80	NE 1	SSE 3	E 1
19	734.7	733.3	733.5	13.4	23.0	21.9	20.6	24.4	12.8	08.9	11.4	12.0	15.6	99	50	79	76	SE 1	E 1	NE 1
20	733.6	732.0	731.7	17.4	29.2	22.4	22.8	29.9	17.3	13.4	13.8	14.9	18.0	92	49	88	76	SSW 1	SW 1	- 0
21	729.8	730.1	730.0	21.0	19.8	15.8	18.1	24.0	15.9	15.2	16.9	14.6	12.9	90	84	96	90	E 1	E 1	SSW 1
22	731.9	732.2	733.7	14.1	20.0	16.0	16.5	20.3	13.9	10.1	11.7	11.6	12.8	97	66	94	86	SW 1	SE 1	- 0
23	734.0	733.7	733.4	15.2	18.2	14.6	15.6	19.4	13.6	12.1	11.5	11.6	11.7	89	74	94	86	NE 2	N 2	- 0
24	731.8	731.9	732.4	13.9	14.8	13.0	13.7	15.5	12.8	11.1	11.5	10.7	10.6	97	85	95	92	NW 1	NW 2	NNW 1
25	735.8	736.4	738.3	11.2	23.2	14.4	15.8	23.6	09.9	06.9	09.5	08.4	10.3	95	40	84	73	- 0	SE 2	SE 1
26	740.2	739.6	740.5	11.4	23.4	15.5	16.4	24.6	10.9	06.3	09.9	08.6	12.0	98	40	91	76	SW 1	S 1	- 0
27	741.1	739.0	739.2	11.5	24.0	19.2	13.5	26.5	10.6	07.0	10.1	12.3	13.2	99	55	79	78	SE 1	NE 2	SE 1
28	738.2	737.1	736.8	14.2	20.6	19.0	19.2	21.2	13.2	10.0	11.0	14.2	12.0	97	78	73	83	NW 1	SE 1	SW 1
29	736.9	736.8	737.3	15.0	21.9	17.0	17.7	25.8	14.4	10.7	12.5	13.2	13.4	95	67	92	86	NE 1	SW 3	SW 1
30	735.6	736.2	736.4	15.7	17.6	16.6	16.6	17.8	15.0	13.4	12.9	13.7	13.6	97	91	96	95	SE 1	- 0	NE 1
31	736.5	736.2	736.9	15.4	21.2	16.6	17.8	22.1	15.8	14.1	13.4	13.8	13.2	96	73	92	87	- 0	S 3	N 1
MES. PRED.	735.7	734.9	[illegible]	16.1	24.2	19.1	19.6	[illegible]	14.5	12.0	12.9	13.2	13.7	95	60	83	79	0.9	1.7	1.0

GR. ST. 13 H_g = 299 m H_b = 300.6 m h_t = 2.0m h_r = 1.5 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	8	10	09	01	06.7	04.6	37.1	.	$\bullet^{+-0-1}n-5^{37}$ $\overset{\circ}{\nabla}^{+-2}n$ $\overset{\circ}{\Gamma}{}^{2}n$ $\overset{0-1}{\Delta}20^{3}/_{4}-n$ ⊙
2	7	10 ≡	06	10	03.7	05.9	.	.	$\equiv^{2}n-8^{3}/_{4}$ $\equiv^{0-1}8^{1}/_{2}$ $\Delta^{2}n-9^{3}/_{4}$ $\overset{\circ}{\nabla}^{+-02}19^{08}$ ⊙
3	7	10 ●	10 ●	10	10.0	00.0	04.7	.	$\bullet^{+-0-1}n$ 10^{40} $9^{36}-ni$ $\overset{\circ}{\Gamma}{}^{5^{40}}$
4	7	10 ●	10	08	09.3	00.2	11.2	.	$\bullet^{+-0}n-10^{35}$ $\equiv n-11^{1}/_{2}$ ⊙
5	8	10 ≡	07	04	07.0	09.0	04.2	.	$\equiv^{2}n-7^{1}/_{4}$ $\Delta^{2}n-9^{1}/_{2}$ $\equiv 7^{1}/_{4}-8$ $=8-9^{1}/_{4}$ ⊙
6	8	04 ⊙	05 ⊙	02	03.0	13.4	.	.	$\Delta^{1}n-9$ ⊙
7	7	01 ⊙	01 ⊙	00	00.7	13.2	.	.	$=n-9^{1}/_{4}ni$ $\Delta^{2}n-8^{1}/_{4}$ $\equiv 4^{1}/_{2}-5^{3}/_{4}$ ∞ $9^{1}/_{4}-n$ ⊙
8	6	00 ⊙	01 ⊙	00	02.7	12.2	.	.	$\equiv^{0}n-6^{1}/_{2}$ $\Delta^{2}n-9^{1}/_{4}$ $=6^{1}/_{2}-14^{1}/_{2}$ $\zeta 24-n$ ⊙
9	7	10 ≡	03 ⊙	02	05.3	11.2	.	.	$\equiv^{+2}n-4^{1}/_{4}$ $7^{1}/_{2}-7^{50}$ $\Delta^{2}n-9$ $\equiv^{2}4^{1}/_{2}-7^{1}/_{2}$ $=7^{50}-11^{1}/_{2}$ ∞ $11^{1}/_{2}-n$ ⊙
10	7	00 ⊙	03 ⊙	01	01.3	13.3	.	.	$=n-9^{1}/_{4}$ $\Delta^{2}n-9$ ∞ $9^{1}/_{4}-15^{1}/_{2}$ ⊙
11	7	00 ⊙	03 ⊙	03	02.7	12.8	.	.	$=n-9^{1}/_{2}i$ $\Delta^{1}n-9^{1}/_{4}$ $\equiv^{0}5^{50}-6^{1}/_{4}$ ⊙
12	7	04 ⊙	03 ⊙	02	03.0	12.6	01.2	.	$\overset{\circ}{\nabla}n$ ζn ⊙
13	7	00 ⊙	01 ⊙	01	00.7	13.4	.	.	$\Delta^{0}n-7^{3}/_{4}$ ∞ $9^{1}/_{2}-n$ ⊙
14	7	01 ⊙	03 ⊙	10	03.0	10.3	.	.	$\Delta^{0}n-8^{1}/_{2}$ $=n-9^{1}/_{2}$ ∞ $9^{1}/_{2}-12^{1}/_{2}$ ∪ $20^{1}/_{4}-n$ ⊙
15	7	03 ⊙	07 ●	10 Γ ●	06.0	04.8	.	.	$\Delta^{0}n-7^{1}/_{2}$ $=5^{3}/_{4}-9^{1}/_{2}$ $17-n$ ∞ $9^{1}/_{2}-17$ $\overset{\circ}{\nabla}^{+-0-2}12^{30}-ni$ $T^{0}14^{40}-18^{1}/_{2}$ F_{NE} $15^{1}/_{2}-16^{1}/_{4}$
16	7	10 ●	10 ●	10 ●	10.0	00.0	36.5	.	$\bullet^{+-14^{1}/_{2}}-ni$ [$\Gamma 18^{1}/_{2}-n$ ⊙
17	8	10	03 ⊙	06	03.0	03.8	09.4	.	$\bullet^{1}n$ ⊙
18	8	09	04 ⊙	04	04.3	07.9	.	.	$\Delta^{1}n-8^{1}/_{2}$ $20^{1}/_{4}-n$ ⊙
19	8	04 ⊙	01 ⊙	00	01.3	13.8	.	.	$\Delta^{0}n-8^{3}/_{4}$ ⊙
20	7	04 ⊙	10	09	09.3	04.6	.	.	$\Delta^{0}n-8$ ∞ $7-9^{1}/_{2}$ ⊙
21	7	09	10 ●	04	07.7	00.5	00.0	.	$=n-11$ ∞ $11-n$ $\bullet^{+-14-17^{1}/_{2}}i$ ⊙
22	7	03 ⊙	01 ⊙	02	01.3	13.5	00.2	.	$\Delta^{1}n-9^{1}/_{4}$ ⊙
23	8	03 ⊙	04 ⊙	03	03.3	12.8	.	.	$\Delta^{0}n-8$ ⊙
24	8	00 ⊙	01	00	00.3	13.4	.	.	$\Delta n-8^{1}/_{4}$ ⊙
25	8	10 ●	03 ⊙	01	05.3	08.0	.	.	$\Delta n-9$ $\equiv 3^{1}/_{2}-6$ $F 9^{1}/_{2}-11^{3}/_{4}$ $\zeta 10^{1}/_{4}-10^{40}$ $\Gamma{}^{1}10^{40}-13$ $\overset{\circ}{\nabla}^{0-1-2}10^{45}-11^{3}/_{4}$ $\bullet^{1}11^{3}/_{4}-13$ ⊙
26	8	04 ⊙	03	01	04.3	10.9	17.0	.	$\equiv^{2}n-4^{1}/_{2}$ $\Delta^{2}n-9$ $20^{1}/_{4}-n$ $\equiv 4^{1}/_{2}-6$ $=6-9^{1}/_{2}$ ⊙
27	7	02 ≡ ⊙	04 ⊙	02	02.7	11.6	.	.	$=n-4^{3}/_{4}$ $8^{3}/_{4}-12^{3}/_{4}$ $\Delta^{2}n-9^{1}/_{2}$ $\equiv 4^{3}/_{4}-8^{3}/_{4}$ ⊙
28	8	00	04 ⊙	00	01.3	13.9	.	.	$\Delta^{0}n-9^{1}/_{2}$ ⊙
29	8	10 ≡	03 ⊙	01	04.7	10.3	.	.	$\Delta^{0-1}n-9$ $=n-5^{3}/_{4}$ $9-9^{1}/_{2}$ $\equiv^{0-1}5^{3}/_{4}-9i$ $\equiv^{2}6^{3}/_{4}-7^{40}$ ⊙
30	7	07 ⊙	05 ⊙	00	03.3	12.3	.	.	$=n-9^{1}/_{2}$ ∞ $9^{1}/_{2}-n$ ⊙
31	7	01 ⊙	04 ⊙	00	01.7	12.2	.	.	$=n-13^{1}/_{2}$ $\Delta^{0}n-9$ ⊙
MES.									
VREDN.		05.0	05.1	03.6	04.6	227.0	125.5		

1	7	00 ≡ ⊙	04 ⊙	02	02.3	10.4	.	.	$\overset{\circ}{\nabla}n$ $=n-5$ $8^{3}/_{4}-9^{1}/_{2}$ $20^{1}/_{2}-n$ $\Delta^{0}n-7^{3}/_{4}$ $20^{3}/_{4}-n$ $\equiv^{0-2}5-8^{3}/_{4}$ ∞ $9^{1}/_{2}-20^{1}/_{2}$ $T 15^{1}/_{2}-$
2	6	03 ≡ ⊙	04 ⊙	02	03.0	10.8	06.2	.	$=n-6^{1}/_{4}$ $8^{1}/_{2}-18$ $\equiv^{0}6^{1}/_{4}-8^{1}/_{2}$ $T 11^{1}/_{2}-13^{1}/_{2}$ $\overset{\circ}{\nabla}^{+-12^{30}}13^{40}i$ ∞ $18-n$ $\zeta 20-n$ ⊙ [$-16^{1}/_{4}$ $\zeta 20^{1}/_{2}-n$ Γn ⊙
3	7	10	04 ⊙	04	03.0	05.4	00.1	.	$\Delta^{0}n-8^{1}/_{2}$ $=n-12^{10}i$ $\equiv^{0}4^{1}/_{2}-5^{1}/_{2}$ $\equiv^{0}5^{1}/_{2}-6^{1}/_{2}$ ⊙
4	7	06 ⊙	07 ⊙	00	03.3	03.3	.	.	$\Delta^{0}n-9$ $=n-9^{1}/_{2}$ ∞ $9^{1}/_{2}-16^{1}/_{2}$ ⊙
5	7	10 ≡	01 ⊙	03	04.7	09.2	.	.	$\equiv^{0-1}n-5^{40}$ $8^{1}/_{4}-13$ $\Delta^{2}n-9$ $\equiv^{1-2}5^{40}-7^{1}/_{2}$ $\equiv^{0-1}7^{1}/_{2}-8^{3}/_{4}$ ∞ $13-n$ ⊙
6	7	00 ⊙	02 ⊙	00	00.7	12.6	.	.	$\Delta^{0}n-8^{1}/_{2}$ $=n-9^{1}/_{4}$ ∞ $9^{1}/_{4}-n$ ⊙
7	7	00 ⊙	03 ⊙	03	02.0	11.8	.	.	$=n-9^{1}/_{2}$ $\Delta^{0}n-8$ ∞ $9^{1}/_{2}-14^{1}/_{2}$ $\zeta 20^{3}/_{4}-n$ ⊙
8	8	02 ⊙	03 ⊙	01	02.0	11.3	00.1	.	$\overset{\circ}{\nabla}^{+-0}3^{25}-4^{05}$ $\zeta 20-n$ ⊙
9	6	09 ●	10 ●	10	09.7	00.0	27.0	.	$\overset{\circ}{\nabla}^{0-2}n$ $3^{3}/_{4}-7i$ $12^{40}-13^{10}$ $=n-4^{1}/_{2}$ $13^{1}/_{2}-16^{1}/_{2}$ $\Gamma{}^{0-1}n-5^{1}/_{2}$ $\bullet^{0-1}4^{1}/_{2}-17^{05}i$
10	8	10	04 ⊙	09	03.3	05.1	00.7	.	$=n-9^{1}/_{2}$ $\bullet^{+}5^{1}/_{4}-5^{20}$ $\overset{\circ}{\nabla}^{+-0}15^{55}-15^{1}/_{2}$ $T^{0}16^{35}-17^{1}/_{4}i$ ⊙
11	6	10 ●	07 ⊙	04	07.0	03.3	00.2	.	$=n-14^{1}/_{2}$ $\Delta^{1}n-6$ $\bullet^{+}6-7^{40}$ $10^{20}-10^{30}$ $T 18^{35}-18^{50}$ $\Gamma{}^{0}18^{50}-20$ $\overset{\circ}{\nabla}^{0-1}19^{32}$ $20^{3}/_{4}$ $\zeta 20-20^{1}/_{4}$
12	7	10	07 ⊙	04	07.3	05.4	00.3	.	$=n-10^{3}/_{4}$ ⊙ [⊙
13	6	10	09	10	09.7	02.6	.	.	$\equiv n-n$ $\Delta^{2}n-9^{1}/_{2}$ $19^{3}/_{4}-n$ ⊙
14	6	10 ≡	01 ⊙	06	05.7	07.1	.	.	$\equiv^{0}n-8^{1}/_{2}$ $\Delta^{2}n-10^{1}/_{4}$ $=8^{1}/_{2}-n$ ⊙
15	7	07 ⊙	09 ⊙	04	06.7	05.9	.	.	$\Delta^{0-1}n-10^{1}/_{4}$ $=n-11^{1}/_{2}$ $\Theta 8-8^{3}/_{4}$ ∞ $11^{1}/_{2}-n$ $T 14^{3}/_{4}-15^{1}/_{2}$ $\zeta 20^{1}/_{4}-n$ ⊙
16	6	09	06 ⊙	07	07.3	07.0	.	.	$\Delta^{2}n-9^{1}/_{2}$ $=n-10^{3}/_{4}$ $20^{3}/_{4}-n$ ⊙
17	6	10 ≡	10 ● Γ	10 ●	10.0	01.8	.	.	$\Delta^{2}n-9^{1}/_{2}$ $=n-5^{1}/_{4}$ $7^{3}/_{4}-n$ $\equiv^{1-2}5^{1}/_{4}-7^{3}/_{4}i$ $\equiv^{0}6^{1}/_{2}-7^{1}/_{2}$ $\overset{\circ}{\nabla}^{+}11^{05}$ 12^{40} $T 14^{50}$ 12^{40} Γ 12^{10}
18	8	09 ⊙	00 ⊙	02	03.3	07.5	18.1	.	$\bullet n$ $=n-7^{1}/_{2}$ $\Delta^{1}20^{1}/_{4}-n$ ⊙ [$20^{1}/_{2}i$ $F 14^{05}$ $14^{1}/_{2}i$ $\bullet 17^{10}$ ⊙
19	7	10 ≡	00 ⊙	09	06.3	07.2	.	.	$=^{0-1}n-8$ $\Delta^{2}n-10^{1}/_{2}$ $=8-13^{1}/_{2}$ $\bullet^{+}12^{1}/_{2}-18^{50}$ ⊙
20	7	10 ●	10 ●	02	04.3	08.7	00.0	.	$=n-13^{1}/_{2}$ $\Delta^{2}n-7$ $\bullet^{+}7-7^{40}$ ⊙
21	6	08	09	01	06.0	03.9	00.3	.	$\overset{\circ}{\nabla}^{+-0-1}n$ 10^{55} 12^{40} 16^{30} $18^{50}i$ Γn 10^{40} $12^{1}/_{2}$ $16^{1}/_{2}-19i$ $=n-14^{1}/_{2}i$ $20^{1}/_{2}-n$ $\zeta 3^{3}/_{4}-4$ $19^{1}/_{4}-n$ $\equiv^{0}5^{1}/_{2}$
22	7	09 ●	09	09	08.7	01.3	19.9	.	$\equiv^{0-1}n-4^{3}/_{4}$ $\equiv^{1}4^{3}/_{4}-5$ $=15-8$ $\overset{\circ}{\nabla}^{0}5^{12}$ $7^{12}i$ ⊙ [$\zeta 4^{1}/_{4}$ $T 10^{10}-10^{40}$ 16^{0-2} $19^{1}/_{4}i$ ⊙
23	7	06 ⊙	07	10 ●	08.0	02.9	01.0	.	$\overset{\circ}{\nabla}n$ $11^{40}-14^{10}$ 16^{45} $=n-6^{1}/_{4}$ $\bullet^{0}11^{50}$ 15^{50} $20^{12}-n$ $\Gamma{}^{0}16^{20}-16^{45}$ ⊙
24	6	10 ●	10 ●	01	07.0	00.0	05.3	.	$\bullet^{0-1}n-19^{1}/_{4}i$ $=n-17^{1}/_{2}$ ⊙
25	7	09 ≡	05 ⊙	01	05.0	07.6	05.4	.	$\equiv^{0}n-10^{1}/_{4}$ $=10^{1}/_{4}-12^{1}/_{2}$ $\overset{\circ}{\nabla}^{+}15^{50}$ 16^{05} ⊙
26	7	10 ≡	04 ⊙	02	05.3	10.2	00.0	.	$=n-5^{1}/_{2}$ $7^{3}/_{4}-11$ $\Delta^{0-2}n-10$ $13^{1}/_{2}-n$ $\equiv^{0}5^{1}/_{2}-7^{3}/_{4}$ ⊙
27	8	10 ≡	03 ⊙	02	05.0	07.9	.	.	$\equiv^{0-1-2}n$ $9^{1}/_{4}$ $\Delta^{2}n-10^{3}/_{4}$ $\equiv 9^{1}/_{2}$ $11^{3}/_{4}$ $\bullet^{+}19^{50}-20^{40}$ ⊙
28	6	10 ≡	09 ●	06	08.3	02.5	00.1	.	$=n-4^{1}/_{2}$ $7^{3}/_{4}-n$ $\equiv^{0}4^{1}/_{2}-6$ $\equiv^{0}6-7^{3}/_{4}$ $\bullet^{+}12^{40}$ 16^{40} ⊙
29	7	10 ≡	09	10 ●	09.7	02.9	00.1	.	$=n-6^{1}/_{4}$ $9^{1}/_{2}-12^{1}/_{2}$ $\Delta^{2}n-10$ $\equiv^{0-1}6^{1}/_{4}-6^{1}/_{2}$ $9-9^{1}/_{2}$ $\equiv^{2}6^{1}/_{2}-9$ $\bullet^{+-0}15^{20}n$ ⊙
30	8	10 ●	10 ●	10 ●	10.0	00.0	02.2	.	$\bullet^{+-0-1}n-n$ $=n-n$
31	6	10	05 ●	05	06.7	04.5	26.1	.	$\bullet n$ $=n-n$ ⊙
MES.									
VREDN.		08.0	05.8	04.8	06.2	186.1	133.1		

$\varphi = 46^{\circ}\ 04'$ N $\lambda = 14^{\circ}\ 31'$ E Gr. $\Delta G =$ + 58 min. BR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha t °C							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21
1	736.8	735.0	734.7	14.2	25.4	18.6	19.2	25.4	14.1	09.4	11.9	12.1	14.6	98	50	91	80	NE 1	S 1	- 0
2	737.8	736.8	736.3	14.4	24.2	17.2	18.2	24.6	13.4	08.9	11.8	11.8	13.0	96	52	69	79	- 0	ESE 2	- 0
3	736.8	735.4	735.9	14.0	26.6	21.0	20.6	26.8	13.5	11.2	12.0	10.7	14.0	100	41	75	72	- 0	SW 2	S 2
4	738.0	737.1	739.2	16.0	24.4	17.6	18.9	25.7	15.4	12.7	12.8	11.7	12.8	94	51	85	77	NW 1	SW 2	SW 1
5	738.3	736.5	736.3	14.4	24.3	19.2	19.3	24.7	14.1	09.9	11.5	12.5	13.3	94	54	80	76	S 2	WSW 2	SW 2
6	736.3	735.6	737.1	17.0	25.0	18.8	19.9	26.1	15.7	11.6	13.8	12.6	14.2	95	53	87	78	NW 1	NE 1	NE 1
7	739.8	740.4	739.7	15.2	17.0	15.4	15.8	19.0	15.1	14.2	09.9	09.9	10.5	76	68	80	75	E 3	NE 3	NE 1
8	738.4	736.4	736.0	14.1	23.9	18.4	18.7	24.6	12.9	07.9	10.8	13.4	13.7	90	60	86	79	S 1	W 4	WSW 1
9	736.8	735.3	735.5	17.0	26.3	21.2	21.4	27.0	14.9	11.6	13.4	12.5	14.2	92	49	75	72	NE 1	S 3	SW 2
10	735.1	734.6	734.6	18.6	26.6	21.0	21.8	27.0	17.1	12.6	12.6	15.2	13.4	78	58	72	69	S 1	SW 4	SW 1
11	735.0	733.5	733.0	17.4	28.7	20.1	21.6	29.0	15.7	10.7	13.2	13.4	13.6	89	45	77	70	NE 1	WSW 4	W 1
12	732.9	732.3	731.8	16.6	26.0	19.0	20.2	27.0	15.7	10.8	13.2	13.0	14.8	93	51	90	78	NE 1	SW 2	SE 1
13	730.9	732.3	736.2	15.7	20.3	17.6	17.8	24.5	14.9	11.4	13.1	11.6	10.6	98	65	70	78	- 0	NE 4	NE 1
14	737.9	736.4	737.0	13.1	22.9	14.2	16.1	23.0	11.1	05.5	10.5	08.2	09.9	92	39	82	71	NE 1	NE 2	SE 1
15	738.0	735.6	735.6	09.6	23.7	16.5	16.6	24.8	08.9	03.6	08.9	11.0	11.1	99	50	79	76	NE 1	NE 1	SE 1
16	735.6	735.1	739.5	11.3	21.0	13.2	14.7	21.3	10.6	05.6	09.9	13.8	09.2	99	74	81	85	ENE 1	NE 2	NW 4
17	742.2	743.2	744.0	10.2	13.4	12.0	11.9	15.9	09.3	07.6	08.0	09.1	09.1	86	70	87	81	E 1	ESE 2	E 1
18	744.1	743.1	743.5	09.8	19.4	12.7	13.6	19.5	08.6	02.6	08.6	06.3	09.2	95	38	84	72	E 1	ESE 2	NE 1
19	743.1	741.7	742.5	08.5	22.5	13.2	14.4	22.6	08.0	02.4	07.6	09.7	10.4	91	47	91	76	E 1	NE 2	NE 1
20	741.9	739.7	740.3	11.0	24.5	17.6	17.7	24.5	10.3	04.0	09.6	10.8	12.8	98	47	85	77	- 0	SW 1	SE 1
21	739.6	738.9	739.1	15.6	20.0	14.8	16.3	21.4	10.4	11.4	12.2	13.0	11.8	92	74	94	87	W 1	NE 1	NE 1
22	738.9	739.7	741.0	13.7	16.6	14.2	14.7	17.3	12.8	07.8	11.6	10.3	09.9	99	73	82	85	NNW 1	SE 3	E 2
23	741.3	739.3	740.2	10.6	18.7	10.7	12.7	19.5	09.7	04.4	08.0	07.7	08.4	84	47	87	73	- 0	NW 1	N 1
24	741.7	740.0	740.6	07.0	18.2	10.2	11.4	18.4	06.4	02.0	07.3	06.8	08.2	97	44	88	76	SW 1	ESE 1	SE 1
25	740.8	739.4	739.8	06.1	19.4	10.8	11.8	19.7	05.2	-01.2	06.8	07.5	08.8	96	45	91	77	SSE 1	NE 1	NE 1
26	739.3	737.5	740.6	07.6	20.4	13.8	13.9	21.5	06.9	01.0	07.7	09.6	11.3	99	53	96	83	NE 1	NNE 1	NE 1
27	744.3	745.0	745.1	10.4	15.4	10.0	11.4	16.0	09.9	08.6	08.3	07.1	08.2	88	54	89	77	N 1	SSE 1	SE 1
28	747.5	747.2	746.8	06.9	16.5	08.0	09.8	17.1	05.4	-00.3	07.4	07.1	07.3	99	50	91	80	S 1	SE 1	- 0
29	748.4	747.3	746.1	03.5	15.5	06.0	07.8	15.5	02.5	-03.5	05.7	05.8	06.2	97	44	89	77	S 1	E 2	S 1
30	742.8	738.2	736.0	03.0	16.4	11.9	10.8	19.4	02.2	-03.6	05.7	07.1	07.1	100	51	67	73	- 0	NE 1	SW 1
MES. VRED.	739.3	738.2	738.9	12.1	21.4	15.2	16.0	22.3	11.0	06.7	10.1	10.3	11.0	93	53	84	77	0.9	2.0	1.1

1	732.1	729.5	732.4	11.0	14.0	08.2	10.4	14.6	08.2	06.2	09.6	10.1	08.2	98	84	100	94	N 1	SE 2	- 0
2	735.0	731.2	727.4	06.6	15.6	12.0	11.6	16.5	06.3	05.5	07.1	08.7	08.1	97	66	77	80	S 1	NW 1	NW 1
3	728.1	728.2	731.1	07.6	15.7	06.0	08.8	15.7	05.9	05.1	07.2	07.5	06.4	92	56	92	80	E 1	S 3	NE 1
4	731.9	731.8	735.7	03.6	17.6	07.4	09.0	18.6	03.5	-02.3	05.8	05.9	07.0	100	39	91	77	N 1	SW 2	- 0
5	737.4	735.5	736.5	06.0	18.8	09.1	10.8	19.0	04.9	-02.2	06.4	07.6	06.5	92	47	75	71	E 1	E 1	E 1
6	737.2	736.3	736.9	05.6	20.8	13.6	13.4	20.8	04.4	-02.6	06.4	09.4	09.0	94	51	77	74	NE 1	SW 3	NW 1
7	736.0	735.4	736.9	14.2	21.1	12.6	15.1	21.4	12.4	07.3	09.7	10.0	09.3	80	53	85	72	SW 1	SW 3	- 0
8	737.8	738.1	739.4	09.0	21.9	14.2	14.8	22.2	08.2	01.5	08.1	10.8	10.8	94	55	89	79	NW 1	SW 3	SW 2
9	740.3	739.4	740.7	09.6	24.7	15.6	16.4	25.0	09.0	03.2	08.4	10.7	11.6	94	46	87	76	E 1	SSW 4	NE 1
10	742.0	741.4	743.1	10.2	25.5	14.8	16.3	26.9	10.0	03.7	09.2	12.9	11.6	99	53	92	81	- 0	S 1	SW 1
11	745.0	743.9	744.9	10.4	22.6	17.0	16.8	24.9	10.3	03.5	09.3	13.0	13.4	99	63	92	85	NE 1	WNW 1	- 0
12	745.2	743.7	744.1	13.6	22.0	14.0	15.9	22.8	12.8	06.4	11.6	11.2	11.2	99	56	94	83	E 1	SSE 1	N 1
13	744.2	742.3	741.3	13.4	20.0	10.9	13.8	21.0	10.8	05.8	10.8	10.0	09.3	94	57	95	82	E 1	E 1	- 0
14	739.8	739.2	739.9	10.6	13.2	12.6	12.3	13.5	10.4	02.4	09.5	10.2	10.2	98	89	93	93	WNW 1	SE 1	NW 1
15	740.8	741.1	743.4	09.2	08.7	06.6	07.8	12.9	06.5	07.0	08.0	07.4	05.7	91	88	79	86	SE 2	SE 2	NE 2
16	745.1	744.3	746.6	00.4	11.0	03.8	04.8	11.2	-00.7	-08.2	04.2	03.9	04.6	89	40	76	68	NW 1	E 3	NE 1
17	746.0	743.9	744.4	-00.9	09.7	02.2	03.3	11.1	-01.7	-08.6	04.0	04.2	04.4	94	46	82	74	NNW 1	ESE 4	SE 1
18	742.6	740.8	742.2	01.7	11.9	03.5	05.2	12.4	01.5	-08.0	04.2	05.1	05.3	82	48	89	73	NW 1	SE 2	E 1
19	740.3	735.0	732.0	00.2	10.0	10.0	07.6	12.9	-00.8	-07.8	04.7	05.9	06.0	100	64	65	76	N 1	NE 1	SW 2
20	726.2	721.3	722.8	04.4	15.0	05.2	07.4	15.3	03.8	-02.8	05.7	07.8	05.8	91	61	87	80	N 1	SW 3	NNE 4
21	727.2	730.0	732.2	01.2	06.2	03.4	03.6	06.6	00.2	-01.5	04.7	05.8	05.6	95	81	95	90	NE 2	SW 1	- 0
22	735.1	735.3	736.5	01.9	10.5	03.0	04.6	10.6	01.2	-02.8	05.2	05.8	05.1	98	61	91	83	ESE 1	SE 2	- 0
23	736.3	734.6	738.0	01.0	10.1	05.2	05.4	16.6	00.6	-06.5	04.8	05.0	05.0	96	54	76	76	- 0	NE 1	NE 1
24	742.4	742.5	744.7	-00.6	10.7	03.4	04.2	12.0	-00.8	-08.2	04.1	02.8	03.9	93	29	67	63	NE 1	NE 2	SW 1
25	743.2	742.0	742.6	-00.6	11.4	06.2	05.8	14.4	-01.4	-08.3	04.1	04.5	05.2	93	45	73	70	N 1	NE 1	- 0
26	741.8	740.3	740.2	01.4	13.8	07.4	07.5	14.3	00.7	-05.4	04.7	05.9	06.3	93	50	82	75	NE 1	SW 2	SW 1
27	741.2	741.2	744.3	00.4	15.2	06.0	07.2	18.1	00.1	-07.0	04.6	06.6	06.5	96	47	93	79	NE 1	W 1	NE 1
28	745.4	743.0	742.4	05.6	13.2	10.6	10.0	14.3	03.5	-04.1	06.2	06.5	07.0	92	57	73	74	N 1	SW 1	SW 3
29	741.4	742.1	744.3	05.8	15.8	08.8	09.8	16.0	04.0	-02.2	06.1	08.0	07.6	89	60	90	80	N 1	SW 4	NE 1
30	744.8	743.3	742.6	04.8	14.0	10.6	10.0	14.6	03.6	-03.0	06.4	08.3	07.5	99	70	78	82	N 1	SE 1	SW 2
31	741.6	741.6	742.7	11.0	13.6	10.6	11.4	14.2	10.3	05.6	07.4	08.1	07.2	75	69	75	73	W 2	SW 3	SW 2
MES. VRED.	739.1	738.0	739.1	05.8	15.3	08.8	09.7	16.3	04.8	-00.9	06.7	07.7	07.5	93	58	84	78	1.0	2.0	1.1

BR. ST. 13 H_s = 299 m H_b = 300.6 m h_t = 2.0 m h_r = 1.5 m

Dan	Vidljivost 0–9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	6	10≡	04⊙	10	09.0	05.8	•	•	≡²n-9, ⌓²n-10, = 9-n, •°21¼-n, ⊙
2	7	09≡	05⊙	00	04.7	00.0	00.0	•	≡⁰⁻¹⁻²n-6½, ⌓²h-10¾, 20¼-n; ≡⁰6½-8¾, = 8¾-11¾, 19¼-n; ∞11¾-19¼, ⊙
3	6	10≡	00⊙	05	05.0	07.6	•	•	≡²n-9½, ⌓²n-10½, = 9½-11¼, 20¼-n; ∞11¼-20½, ⊙
4	8	09	04⊙	06	06.3	08.3	06.8	•	⛈n, ℞n, = n-12i, ≡°7¼-7¾, ⌓°20-n, ⊙
5	7	07	07⊙	00	04.7	07.0	•	•	≡ n-11¼, ⌓²n-10¾, ∞11¼-n, ⊙
6	7	10	09	09	09.3	05.2	•	•	= n-11¼, 18½-n; ⌓²n-10¼, ∞11¼-18½, T18¼-18²⁰, ⛈⁺ 18¼-19i
7	7	09	10	10	09.7	00.0	03.8	•	≡ n-6¼
8	6	07	05	00	04.0	08.6	•	•	= n-10¾, 18½-n; ⌓¹n-9½, 19½-n; ∞10¾-18½, ⊙
9	7	04⊙	04⊙	04	04.0	09.9	•	•	⌓²n-10½, = n-¹10¾, ∞10¾-12½, ⊙
10	7	00⊙	04⊙	00	01.3	08.4	•	•	⌓°n-9¼, 20-n; = 6¼-8, ⊙
11	8	01⊙	02⊙	01	01.3	10.5	•	•	≡ n-9¼, ⌓°n-10¼, ⊙
12	8	05	09	06	06.7	06.8	00.2	•	⛈⁺⁻⁰n, ⌓²⁻ 4⁰³, = n-10½, ⌓°20¼-n, ⊙
13	7	10≡	07	10	09.0	05.2	00.0	•	= n-½²⁰ 8¾-12½; ⌓²n-9¾, ≡⁰⁻¹⁻²4²⁰-8¾i, ≡ ¹⁻²4½-8i, ⊙
14	8	02⊙	02⊙	00	01.3	11.4	•	•	⌓¹n-9¾, 20½-n; = n-4¾, ⊙
15	7	10≡	01⊙	00	03.7	09.3	•	•	= n-4¼, 10½-11¼; ⌓n-9¾, ≡⁰⁻¹4¼-4½, 8¼-10½; ≡¹⁻²4½-8¾, ⊙
16	7	10≡	10•℞	10•	10.0	04.2	•	•	≡⁰⁻¹⁻²n-8¾, ⌓²n-10, = 8¾-11½, T12²⁰, ⛈⁺⁻⁰ 13³⁰-14²⁸, 20³⁰-n; ℞⁰⁻¹13⁴⁸-14¾,
17	8	10	09	10	09.7	01.3	04.6	•	•⁺n, 17⁵⁰-19¾, •⁺⁻⁰n 5, ℞n, = n-5½, ⊙ [ℓ 18½-n, ⊙
18	7	06⊙	02⊙	05	04.3	06.3	00.1	•	= n-10½, 19¼-n; ψn-4½, ⌓⁰⁻¹⁻²n-10¾, 19½-n; ⊙
19	7	03	00⊙	04	02.3	08.6	•	•	≡ n-11½, ⌓⁰⁻²n-10¼, 20-n; ⊙
20	7	10≡	04⊙	09	07.7	05.4	•	•	≡⁰⁻¹⁻²n-9¼i, ⌓²n-11¼, ≡⁰⁻¹9¼-10½, = ½-11¾, 19¼-n; ∞19¾-15¼, ⊙
21	6	10	09	00	06.3	03.5	00.0	•	= n, •9-10⁰⁵ ⊙
22	7	10≡	09	10	09.7	00.3	00.0	•	≡¹⁻²n-8½, ⌓²n-8¼, •⁺7⁵⁰-8¼, ≡ 8½-12, = 12-14, ⊙
23	8	06⊙	01⊙	00	02.3	10.2	00.0	•	⌓⁰⁻¹n-10½, 19½-n; = 20¼-n, ⊙
24	6	07≡	04⊙	00	03.7	09.3	•	•	⌓⁰⁻²n-9¼, 20½-n; = n-n, ≡°7¾-8½, ⊙
25	7	10•	01⊙	00	03.7	07.7	•	•	⌓⁰⁻¹⁻²n-10, 19¾-n; = n-12¼, 20-n; ⊙
26	7	10≡	09	09•	09.3	03.6	•	•	≡¹⁻²n-9¼, ⌓²n-11¼, ≡⁰⁻¹9¼-10½, = 10½-12¼, 17¼-n; ∞12¼-17¼, T18⁴⁵-18⁵⁰,
27	7	10	07⊙	00	05.7	03.8	06.6	•	⛈⁺⁻⁰ 18⁴⁵-20, ℞18⁴⁵-20, •20-n, ⊙ = n-10½, ⊙
28	7	10≡	04⊙	00	04.7	07.6	•	•	≡²n-6½, ⌓⁰⁻¹⁻²n-11½, 19¼-n; ≡⁰⁻¹6½-7¾, = 7¾-12, 19¼-n; ⊙
29	8	01	01⊙	00	00.7	09.4	•	•	⌣⁰n-8¼ = n-9½, 20¼-n; ∞9½-12½, ⌓°19½-n, ⊙
30	6	10≡	02⊙	09	07.0	05.5	•	•	≡¹⁻²n-10¼½, ⌓²n-10½, ≡⁰10½-11½, = 11½-14¼, ⊙
MES. VRED.		07.5	04.8	04.2	05.5	197.7	22.1		

Dan	Vidljivost 0–9	7	14	21	Sred Dies	Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
1	6	10≡•	10•	00≡	06.7	00.9	06.3	•	•⁺⁻⁰⁻¹⁻²n, 3²⁵-7³¼, 11⁴⁷-17¼i; = n-19½i, ≡⁰⁻²6¼-7¾, 19½-n; ⛈⁻¹⁻²14⁴⁰-16, ℞⁰⁻²14¼-16¾,
2	7	10≡	09⊙	06	08.3	03.9	25.8	•	≡⁰⁻¹n-9¼, = 9½-13½, ∞13½-14¾, ⊙ [F 15¼-15⁴⁰, ⊙
3	8	08	04⊙	00	04.0	06.2	13.0	•	⛈⁰⁻¹n-5⁵⁰, ℞⁰⁻¹⁻²n-5¾, 15¾-16; ℓ 15¼-15⁴⁰, ⌓⁰⁻¹⁻²19½-n, ⊙
4	8	10≡	04⊙	01	05.0	06.7	•	•	≡¹⁻²n-9½, ⌓²n-10¾, ≡ 9½-¹10, = 10¹-12, ⊙
5	8	10	06⊙	00	05.3	05.3	•	•	= n-9¼, ⌓²n-11¾, ⊙
6	8	01⊙	04⊙	00	01.7	09.6	•	•	⌣⁰n-6, = n-8¼, ⊙
7	8	08•	04⊙	00	04.0	07.6	00.0	•	⛈⁺⁻⁰6⁵⁰-7⁴⁵, ⌓°21-n, ⊙
8	8	03	04⊙	00	02.3	07.0	00.0	•	= n-9½, ⌓⁰⁻¹n-10¾, 20¼-n; F_SW 12²⁰-12³⁵, ⊙
9	7	01⊙	00⊙	00	00.3	09.1	•	•	⌓⁰⁻¹n-10½ = n-11½, ⊙
10	8	10≡	00⊙	00	03.3	07.1	•	•	≡¹⁻²n-9, ⌓²n-10, ≡⁰⁻¹9-9⁴⁵, = 9⁴⁵-11½, ⊙
11	7	10≡	01⊙	09	06.7	06.5	•	•	≡¹⁻²n-9¼, ⌓¹⁻²n-11½, 18½-n; ≡ 9¼-10¼, = 10¼-11¼, 18¼-n; ∞11½-18¼, ⊙
12	6	10≡	02⊙	00	04.0	05.6	•	•	≡¹⁻²n-10¾, ⌓⁰⁻¹⁻²n-10½, 19½-n; ≡°10¾-11½, = 11½-n, ⊙
13	6	08≡	00⊙	00	02.7	05.4	•	•	⌓⁰⁻¹⁻²n-10¾, 18¾-n; = n-16i, 18½-n; ≡ 6½-7½, ∞16-18½, ⊙
14	5	10≡	10	10•	10.0	00.0	00.1	•	•n-10¼, ≡⁰⁻¹⁻²n-10½, = 10½-n, •⁺17⁴⁵-17⁴⁶i, 19¾-n
15	6	10•	10	08	09.3	00.0	04.9	•	•⁺⁻⁰n-10½, = n-n
16	8	00⊙	00⊙	00	00.0	09.2	01.1	•	ψn-4½, ⌣²n-8¾, ⌓°20-n, ⊙
17	7	02	02⊙	05	03.0	07.1	•	•	⌣⁰⁻²n-9½, 20¼-n; = n-11½, 20¼-n; ⊙
18	7	03	03	00	02.0	09.0	•	•	⌣⁰n-8, 18½-n; = ¹6¼-7½, 18½-n; ⊙
19	3	10≡	01≡	00	03.7	04.8	•	•	⌣⁰n-6¼, ≡²n-11¼, ≡ 11¼-14½, = 14½-20, ⊙
20	7	08	10	10	09.3	00.4	•	•	= n-9¼, 14½-n; •⁺⁻⁰⁻¹⁻²10⁴⁰-11¼, 14¼-n; ¹F_W-SW-NW 19¼-20½, ℞⁴19⁵⁰-20¼, ⊙
21	6	10	06	10	08.7	00.5	33.7	02	*n, ⛈n, •⁺⁻⁰⁻¹n-6⁵⁵i, ℞n, = n-7, 10½-15⁴⁵, 18¼-n; ≡ 7-10½, ⌓⁰⁻¹19½-n, ⊙, [*]
22	8	10≡	04⊙	00	04.7	07.2	•	•	= n-5¾, 9½-10¾, 18¾-n; ⌓⁰⁻²n-10, 18¾-20; ≡ 5¾-9½, ⌣⁰20-n, ⊙
23	6	10≡	05⊙	10	08.3	02.4	•	•	≡²n-11½, ≡ 11½-13¼, = 13¼-13½, ∞13½-16½, ⛈⁺⁻⁰16½-16⁵⁵, ℓ 18¼-19½, ⊙
24	8	03	04⊙	00	02.3	08.0	00.1	•	⌣⁰n-9, = 4¼-9¼, ⊙
25	9	05⊙	04⊙	04	04.3	08.2	•	•	= n-6¼, ⌣¹n-¹7¾, ⊙
26	8	06	07	00	04.3	04.5	•	•	⌣⁰n-8¼, = n-8½, ∞12¼-12½, ⌓°20¼-n, ⊙
27	7	04≡	04⊙	00	02.7	07.6	•	•	⌣⁰n-9½, = n-6¼, 9¼-12½, 17½-n; ≡ 6¼-9¼, ∞11½-12½, ⌓¹18¼-n, ⊙
28	6	10	06	06	07.3	03.2	•	•	⌓²n-11, = n-n, ⊙
29	5	10	09⊙	00	06.3	00.6	•	•	⌓⁰n-10½, 20¼-n; = n-10¾, 19½-n; ∞10¾-19½, ⊙
30	5	10≡	06	05	07.0	03.2	•	•	≡⁰⁻¹⁻²n-11½, ⌓¹n-11½, ≡ 11½-12¼, = 12¼-14½, 18½-n; ∞14½-18½, ⊙
31	7	04	08⊙	00	04.0	00.4	•	•	= n-9½, ∞9½-n, ⊙
MES. VRED.		07.2	04.7	02.7	04.9	157.2	85.0		

φ = 46° 04' N λ = 14° 31' E Gr. ΔG = + 58 min. MR. ST. 13

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	[illegible]	740.5	740.7	[illegible]	14.2	10.4	10.2	15.[illegible]	04.9	-02.4	06.5	07.7	06.6	94	60	70	75	NE 1	SSE 2	SW 2
2	[illegible]	[illegible]	[illegible]	[illegible]	17.2	11.3	10.6	12.[illegible]	01.9	-04.0	05.3	07.9	07.8	97	54	78	76	NE 1	SW 1	SW 1
3	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	12.4	11.3	15.[illegible]	04.8	-02.4	06.4	08.5	08.0	97	67	73	79	- 0	SW 4	SW 3
4	[illegible]	739.9	740.2	09.6	16.7	15.3	11.7	17.1	09.4	02.5	07.2	08.4	08.4	81	59	89	76	SW 1	NE 1	- 0
5	[illegible]	[illegible]	739.9	06.5	12.4	12.6	11.0	14.2	05.2	-02.[illegible]	07.2	08.5	07.7	99	78	70	82	S 1	E 1	SW 3
6	[illegible]	[illegible]	[illegible]	[illegible]	12.6	9.0	07.5	14.2	04.9	-02.3	07.3	06.0	05.8	93	54	88	78	NW 1	SE 2	NE 1
7	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	03.2	09.7	-00.2	-[illegible]	04.6	[illegible]	05.4	95	64	80	80	NW 1	NE 1	- 0
8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	05.4	06.2	03.9	00.[illegible]	06.0	06.1	06.0	97	89	86	91	NE 1	SE 1	E 1
9	[illegible]	[illegible]	[illegible]	[illegible]	16.[illegible]	05.2	08.6	10.7	04.9	02.7	05.[illegible]	07.2	06.8	87	75	70	80	SW 1	SW 1	SW 1
10	[illegible]	[illegible]	[illegible]	[illegible]	11.7	05.4	07.1	13.7	01.7	-04.5	05.0	[illegible]	05.2	95	39	78	71	NE 1	SSW 1	- [illegible]
11	[illegible]	[illegible]	[illegible]	[illegible]	11.9	06.9	05.[illegible]	12.7	-02.[illegible]	-10.[illegible]	03.9	04.5	06.0	92	46	80	73	NE 1	- 0	SW 1
12	[illegible]	[illegible]	[illegible]	[illegible]	14.[illegible]	[illegible]	07.9	15.[illegible]	-00.4	-07.2	04.[illegible]	06.8	05.6	93	39	67	66	NNE 1	SW 2	SW 2
13	[illegible]	[illegible]	[illegible]	11.[illegible]	10.6	10.1	10.6	12.1	07.[illegible]	-[illegible]	07.0	08.0	08.2	69	64	85	80	SW 1	NW 2	NE 1
14	[illegible]	[illegible]	[illegible]	10.[illegible]	13.4	12.3	12.0	13.[illegible]	09.0	05.0	08.3	09.3	07.6	90	85	71	82	SE 1	NW 1	SW 1
15	[illegible]	[illegible]	[illegible]	06.4	07.1	[illegible]	03.5	13.0	05.5	-01.7	06.6	05.9	05.6	92	91	94	92	SW 1	SW 1	E 1
16	[illegible]	[illegible]	[illegible]	04.0	10.6	03.5	04.9	10.6	02.4	-0[illegible]	05.8	07.3	05.2	95	55	95	82	NW 1	SE 1	SSE 1
17	[illegible]	[illegible]	[illegible]	-11.2	[illegible]	03.0	01.9	04.[illegible]	-02.1	-09.2	04.0	04.5	05.0	100	76	87	88	NE 1	NE 1	NE 1
18	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	05.[illegible]	08.2	[illegible]	02.7	-00.5	05.4	06.9	08.0	80	83	90	84	- 0	NE 1	SE 1
19	[illegible]	[illegible]	[illegible]	13.4	[illegible]	12.4	12.4	15.[illegible]	05.[illegible]	[illegible].7	09.[illegible]	[illegible].2	09.7	78	63	90	77	SW 2	SW 2	SW 1
20	[illegible]	[illegible]	[illegible]	[illegible]	12.6	05.4	09.0	17.4	06.[illegible]	[illegible]7.0	09.4	03.5	07.2	96	88	100	95	NE 1	S 1	NE 1
21	[illegible]	[illegible]	[illegible]	[illegible]	05.2	07.2	06.2	07.2	03.9	02.6	06.3	07.1	07.6	100	100	100	100	- 0	S 1	- 0
22	[illegible]	[illegible]	[illegible]	[illegible]	[illegible].4	04.4	07.2	[illegible].1	06.[illegible]	02.2	06.2	06.5	06.6	84	74	92	83	W 1	SW 2	S 1
23	[illegible]	[illegible]	[illegible]	[illegible]	10.1	03.1	06.1	14.[illegible]	03.7	-03.9	05.0	04.5	04.8	77	39	84	67	E 1	NW 1	NE 1
24	[illegible]	[illegible]	[illegible]	-[illegible]	[illegible]	02.5	03.2	09.[illegible]	-01.[illegible]	-[illegible].7	04.1	04.8	05.0	96	57	90	81	[illegible] 1	S 1	[illegible] 1
25	[illegible]	[illegible]	[illegible]	[illegible]	05.2	05.7	05.4	06.[illegible]	02.4	-04.[illegible]	05.4	05.7	05.9	88	95	86	85	[illegible] 1	E 1	SW 1
26	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	01.4	04.0	09.[illegible]	-01.[illegible]	[illegible]	05.4	[illegible]	04.9	87	69	95	84	W 2	W 1	NW 1
27	[illegible]	[illegible]	[illegible]	-[illegible]	+1.2	00.0	00.2	02.[illegible]	-01.3	-0[illegible]	04.4	[illegible]	04.6	100	100	100	100	[illegible] 1	NE 1	E 1
28	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	01.6	01.4	02.[illegible]	-00.5	-0[illegible]	04.6	05.2	05.0	100	95	97	97	NE 1	- 0	NW 1
29	[illegible]	[illegible]	[illegible]	-1.2	[illegible]	[illegible]	07.3	11.3	-01.9	-[illegible].2	04.2	06.2	06.5	100	64	72	79	- 0	SW 3	SW 2
30	[illegible]	[illegible]	[illegible]	[illegible]	10.7	09.6	10.[illegible]	12.4	03.[illegible]	[illegible].6	08.2	09.3	08.5	79	96	9[illegible]	90	SW 2	NE 1	N[illegible] 1
Mes. Vrij.	[illegible].7	[illegible].1	[illegible]	[illegible].2	10.[illegible]	07.0	07.[illegible]	11.4	[illegible].1	-01.7	[illegible]	06.6	06.5	91	71	85	82	1.0	1.[illegible]	1.1

1	731.0	730.2	730.2	07.2	11.7	09.6	09.5	12.4	[illegible]	02.2	07.4	09.2	07.0	97	88	78	88	N 1	- 0	SW 2
2	730.0	732.0	73[illegible]	01.3	10.9	03.4	04.9	11.0	00.7	-0[illegible].2	05.0	06.5	05.5	98	71	94	88	NE 2	SE 1	SE 1
3	73[illegible]	73[illegible]	7[illegible].4	01.0	[illegible]	06.7	04.5	07.8	05.7	-04.8	04.9	05.6	05.7	100	94	77	90	SSE 1	SW 1	SW 3
4	73[illegible].7	740.[illegible]	742.[illegible]	02.[illegible]	1[illegible]	[illegible].7	06.2	13.2	00.[illegible]	-07.[illegible]	04.9	02.9	03.9	93	25	61	66	SE 2	SSE 1	NE 1
5	741.4	740.4	742.0	00.1	[illegible]	[illegible]	03.2	[illegible]	-06.[illegible]	-06.[illegible]	04.3	04.[illegible]	04.7	93	69	79	80	NE 1	NE 1	E 1
6	746.0	74[illegible].0	74[illegible].4	-01.4	[illegible]	-01.0	-00.7	04.0	-01.6	-09.1	04.1	04.7	04.3	100	98	100	99	- 0	SW 1	NE 1
7	741.8	740.2	741.2	-02.6	01.[illegible]	02.4	00.8	02.[illegible]	-05.[illegible]	-09.1	03.5	[illegible].1	05.4	97	98	98	96	SE 1	SW 1	NW 1
8	74[illegible].4	74[illegible].8	74[illegible].5	01.9	03.6	[illegible]	[illegible]	[illegible].3	01.3	-00.2	05.0	05.6	05.6	95	94	94	94	S 1	SE 1	SW 1
9	750.1	749.6	749.0	02.2	02.0	01.3	01.7	04.0	01.3	-03.1	04.9	04.7	04.9	92	88	97	92	NE 2	NE 1	NE 1
10	749.2	749.0	749.[illegible]	[illegible]	00.6	00.0	00.2	01.7	-00.3	-02.0	04.4	04.5	04.4	96	93	96	95	NW 1	NW 1	NE 1
11	750.2	749.9	749.[illegible]	-01.0	-00.4	-01.2	-01.0	00.4	-01.[illegible]	-03.0	04.1	04.1	04.0	96	93	96	95	NE 1	N 1	NW 1
12	748.2	747.2	747.[illegible]	-01.8	-01.0	-02.1	-01.8	-00.9	-02.1	-03.3	03.9	04.1	03.9	96	96	98	97	WNW 1	SW 1	SE 1
13	746.4	745.4	745.7	-02.5	-02.1	-02.7	-02.6	-02.0	-03.0	-04.5	03.7	03.9	03.7	98	98	98	98	N 1	NE 1	- 0
14	745.3	743.7	743.[illegible]	-03.0	-02.3	-03.2	-03.0	-03.0	-03.3	-04.6	03.6	03.5	03.4	97	93	95	95	S 1	NE 1	E 1
15	743.9	744.3	745.5	-03.0	-01.0	-01.6	-01.5	00.0	-03.6	-05.1	03.5	03.9	03.9	95	92	92	93	ENE 1	NE 1	NE 1
16	746.6	746.2	747.2	-05.6	03.[illegible]	-00.9	-01.0	04.5	-05.6	-10.1	02.9	04.2	03.9	95	72	91	86	N 1	SE 1	NW 1
17	747.1	745.3	743.7	-03.6	00.8	-00.8	-01.3	01.0	-04.5	-11.1	03.3	04.1	03.4	94	89	78	87	NE 1	- 0	N 1
18	742.1	742.2	743.[illegible]	-01.5	-00.8	-01.1	-01.1	00.0	-01.8	-03.6	03.5	03.4	03.5	85	80	83	83	NE 1	SE 1	SE 1
19	744.1	743.7	745.0	-03.4	-00.4	-04.1	-03.0	00.1	-04.2	-06.5	03.3	03.5	03.2	93	79	94	89	NE 1	ENE 1	- 0
20	74[illegible].3	743.4	742.3	-04.9	-03.3	-04.4	-04.4	-03.6	-05.2	-06.1	03.1	03.3	03.2	98	96	96	97	NE 1	SE 1	- 0
21	739.6	737.1	735.5	-06.4	-03.6	-03.4	-04.2	-02.9	-06.7	-07.6	02.7	03.4	03.5	96	97	97	97	NE 1	SE 1	NE 1
22	736.0	735.4	735.[illegible]	-01.4	00.5	-01.7	-01.1	01.4	-03.5	-06.0	04.1	03.7	02.9	99	77	73	83	NNE 1	S 1	ESE 3
23	733.3	730.6	730.2	-01.4	-01.9	-04.0	-02.8	-01.0	-04.0	-06.1	02.3	02.6	03.0	56	65	88	70	NE 3	NE 4	SE 2
24	731.9	733.3	73[illegible].7	-05.3	-03.1	-09.2	-06.7	-02.5	-09.3	-10.6	02.9	03.0	02.2	95	83	94	91	SW 1	SE 1	NE 1
25	735.0	733.5	732.9	-07.6	-03.0	-04.5	-04.9	-02.8	-09.4	-19.8	02.4	02.9	02.8	93	78	85	85	NE 1	SE 1	SE 1
26	734.4	735.8	737.2	-02.0	-02.2	-07.2	-06.2	-01.6	-09.0	-09.4	02.4	02.5	02.5	95	64	93	84	S 1	SE 1	SW 1
27	736.7	736.2	734.0	-05.6	-03.4	-03.4	-04.0	-03.1	-08.4	-16.0	02.8	03.3	03.4	92	93	95	93	NE 1	SW 1	E 1
28	72[illegible]	726.6	72[illegible].0	-04.2	-02.2	-02.5	-02.8	-02.0	-04.5	-06.8	03.2	03.4	03.6	96	86	94	92	SW 1	SW 1	W 1
29	730.[illegible]	728.1	724.3	-02.6	00.4	00.7	-00.4	01.1	-05.2	-06.3	03.3	04.6	04.7	94	96	98	96	NE 1	NE 1	NE 1
30	719.2	719.0	722.6	00.8	07.2	01.4	02.7	08.4	00.4	-01.7	04.7	04.9	04.6	97	64	92	84	- 0	S 3	NE 1
31	72[illegible].4	72[illegible]	721.4	00.0	00.6	-00.1	00.1	01.6	-00.6	-05.8	04.4	04.6	04.5	96	96	98	97	NW 1	NE 1	- 0
Mes. VREM.	739.8	739.0	739.2	-02.0	01.0	-00.8	-00.6	01.9	-02.9	-06.4	03.8	04.2	04.0	94	84	91	90	1.1	1.1	1.1

ZN. ST. 13 H_s = 299 m H_b = 300.6 m h_t = 2.0 m h_r = 1.5 m

Dan	Vidljivost 0–9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	5	09	02 ⊙	00	03.3	04.8	.	.	⌓°n-10¼, = n-10½, ∞10½-n, ⊙
2	4	06≡	09	00	05.0	05.8	.	.	≡°n-9½, ⌓°n-11¾, 20½-n; = 9½-11½, 18½-n; ∞11½-18½, ⊙
3	6	03≡	01 ⊙	09	05.7	04.0	.	.	= n-6¼, 10½-14¼; ⌓²n-10¼, ≡ 6¼-10½, ∞14¼-n, ⊙
4	5	09	09	05	07.7	03.2	.	.	⌓°6-13¾, 17¾-n; = 6¼-n, ∞11¾-12¾, ⊙
5	6	10≡	10	10	10.0	00.0	.	.	≡⁰⁻²n-10½, ⌓²n-13½, = 10½-14¾, ⊙
6	6	09	08	00	05.7	04.8	.	.	⌓⁰⁻¹n-8¼, 19½-n; = n-10, ⚲⁺⁺8¼, 13⁰¹-14½i; ∞16-n, ⊙
7	4	10	04 ⊙	10	08.0	02.4	00.1	.	⌓¹n-8¾, = 4½-13½, 17-n; ∞13½-17, ψ16¾-18½, ⌓°17½-n, ⊙
8	5	10≡	10	10	10.0	00.0	06.4	.	●⁺⁺⁻⁰⁻¹n-9¾i, = n-6, 9½-n; ≡ 6-9½, ●⁺⁺10-10¼i
9	6	10	09	10	09.7	00.0	00.4	.	= n-n, ⌓¹n-6²⁰, ●⁺⁺6²⁰-6⁵⁵
10	7	01	02 ⊙	07	03.3	07.4	.	.	⌓°n-9, = n-11½, 20-n; ∞11½-13½, ⌓°19¾-n, ⊙
11	7	01	00 ⊙	03	03.3	07.1	.	.	⌓¹n-8½, = n-12¼, 18½-n; ∞12¼-16¼ ψ18½-n
12	7	04	00 ⊙	00	01.3	07.4	.	.	⌓¹n-10½, = n-12¼, ψ n-4¾, ∞12¼-15, Fsw 14⁵⁰-15½, ⊙
13	7	10	10	10	10.0	00.0	.	.	●⁺⁺10¼-13¾, 14½-15¼; = 17½-n, ●⁺⁺17⁴⁵-18½
14	6	10●	09●	09	09.3	00.1	01.0	.	●⁺⁺⁻⁰⁻¹n-15i, = n-15¼, ⚲⁰⁻⁰4⁴⁸-4³⁰ ⊙
15	6	04	10●	10●	09.0	01.4	11.6	.	⚲n, ⚲n, ψ n-4¾, ●⁺⁺⁻⁰⁻¹10⁰⁰, 21i, ⚲⁰⁻¹14⁰⁹, 16¼-16¾i; ⚲16²⁰-16¾, ⊙
16	4	09	02 ⊙	00	03.7	05.1	32.0	.	●n, = 6½-11½, 14¾-n; ⌓°18¼-n, ⊙
17	5	10≡	10 ⊙	09	09.7	00.0	.	.	⌓¹n-10½, ≡ ²n-5, ≡ ⁰⁻¹⁻²5-11½, = 11½-n, ⊙
18	6	10	10●	10●	10.0	00.0	.	.	= n-n, ⌓⁶5½-11¹⁸, ●⁺⁺⁻⁰11¹⁸-n
19	7	09	10●	09●	09.3	00.0	06.4	.	●⁺⁺⁻⁰n, 10¾-n; = n-7¾, Fsw 10½-13¾, ⊙
20	6	10	05 ⊙	10≡	08.3	02.1	03.8	.	●⁺⁺⁻⁰⁻¹n-13¾i, = n-15¼, 19-19½; ≡ 19½-19¾, ≡⁰⁻¹19¾-n, ⊙
21	2	10≡	10≡	10≡●	10.0	00.0	11.7	.	≡¹⁻²n-18, ≡¹⁻²18-n, ●⁺⁺⁻⁰⁻¹17¼-n
22	3	10	10	10	10.0	00.0	29.2	.	●n, = n-5½, ●3½-4½, ⌓°20½-n, ⊙
23	9	06	02 ⊙	00	02.7	08.3	.	.	⌓¹n-10¼, ψ3½-6, = 19½-n, ⊙
24	7	00	00 ⊙	10	03.3	05.9	.	.	⌓¹n-10, = 5½-9½, ⌓¹18-n, ⊙
25	7	10	10	10	10.0	00.0	.	.	= n-n, ⌓°n-13½
26	7	10	00 ⊙	00	03.3	03.8	.	.	≡n-11½, 18½-n; ⌓°n-12, 19-20; ⌓¹20-n, ⊙
27	2	10≡	10≡	10≡	10.0	00.0	.	.	≡²n-n, ⌓¹n-10
28	3	10≡●	10≡	10	10.0	00.0	00.0	.	≡⁰⁻¹n-13¾i, ●4½-9½, ≡ 10½-16½, = 16½-n
29	6	10≡	09 ⊙	10	09.3	01.6	00.0	.	⌓°n-9, ≡ ¹⁻²n-10¼, ≡ 10¼-14½, = 14½-14¾, 18-n; ⊙
30	5	10●	10●	10●	10.0	00.1	00.2	.	= n-n, ●⁺⁺⁻⁰⁻¹n-9¼, ●⁺⁺⁻⁰⁻¹⁻²10¼-n, ⊙
MES. VREDN.		08.0	06.8	07.2	07.3	74.5	102.8		

1	4	10≡	04 ⊙	08	07.3	02.1	24.8	.	≡⁰⁻¹n-4½, 12-13¼; ≡¹⁻²4½-12¼, = 13¼-14½, 18¼-n, ⊙
2	7	03≡	04 ⊙	00	02.3	05.4	.	.	= n-6¾, 9½-13½, 17½-n; ⌓°n-9½, ≡⁰⁻²6¾-9½, ⌓¹20-n, ⊙
3	5	10≡	09	04	07.3	00.0	.	.	≡⁰⁻¹⁻²n-12¼, = 12¼-18½, ⊙
4	8	01	01 ⊙	01	01.0	07.2	.	.	= n-8½, 18¼-n; ∞11¼-13½, ⌓⁰⁻¹17½-n, ψ17½-n, ⊙
5	5	05	10	04	06.3	00.0	.	.	= n-n, ⌓¹n-10½, ●⁰⁻¹19½-20⁴⁵, ⊙
6	2	10≡	10≡	10≡	10.0	00.0	00.2	.	⌓¹n-13¾, = n-5²⁰, ≡⁰⁻¹⁻²5²⁰-5¾, ≡¹⁻²5¾-n
7	3	10≡	10≡	10●	10.0	00.0	00.0	.	⌓²n-10½, ≡²n-10¼, ↔ 7-7⁴⁰, ≡⁰⁻¹10¼-16¾i, ●⁺⁺⁻⁰⁻¹14½-19¼i, ●⁺⁺⁻⁰16²⁰-17⁴⁰19¼ n
8	6	10●	09	10	09.7	00.0	17.7	.	●⁺⁺⁻⁰⁻¹n-12¼i, = n-n, ⊙ [= 16¾ n
9	6	10	10	10≡	10.0	00.0	00.3	.	= n-20¼, ≡⁰20¼-n
10	4	10≡	10	10	10.0	00.0	.	.	≡°n-9¼, = 9¼-n
11	6	10	10	10	10.0	00.0	.	.	⌓¹n-7¾, ≡°n-4½, = 4½-n, ●⁺⁺7¼-10¼
12	3	10	10≡	10≡	10.0	00.0	00.0	.	= n-13¼i, ≡°7¾-9½, 13¼-n
13	2	10≡	10≡	10≡	10.0	00.0	.	.	⌓¹⁻²n-9, ≡⁰⁻¹n-17¼, 20½-n; ↔ 8-10¾, ≡⁰⁻¹17¼-20½
14	2	10≡	10≡	10≡	10.0	00.0	00.0	.	⌓¹n-13¾, ≡¹n-n, ●⁺⁺5½-6, ↔ 6-11¾
15	5	10	10	08	09.3	00.0	00.1	.	= n-21¼, ≡°21¼-n
16	5	00≡	01 ⊙	08	03.0	05.8	.	.	⌓¹⁻²n-11¼, 17¾-n; ≡¹⁻²n-6, ≡⁰⁻¹6-11½, = 11½-n, ⊙
17	5	10	10	10	10.0	00.0	.	.	⌓⁰⁻¹n-12¼, = n-n
18	6	10	10	10	10.0	00.0	.	.	= n-n
19	4	10	00 ⊙	10	06.7	02.8	.	.	= n-n, ↔ 9¼-10¾, ⌓¹17½-n, ⊙
20	2	10≡	10≡	10≡	10.0	00.0	00.0	.	⌓¹n-n, ≡¹⁻²n-n
21	3	10≡	05≡	10≡	08.7	00.0	00.0	.	⌓²n-n, V²n-n, ≡⁰⁻¹⁻²n-12½, 16-19¼; ≡°12½-16½, 19¼-n; ⊙
22	6	10	10	02	07.3	00.0	07.2	09	*⁰⁻¹n-5¼, = 5¼-18¼, ⊙, ⊠
23	7	10	10	10*	10.0	00.0	.	07	= 16½-n, *°18²⁰ n, ⊠
24	5	10*	09	00	06.3	00.0	00.8	06	= n-n, *⁺⁺7-7½, ↔ 7½-9¼, ≡° 7¾-9¼, ⊙, ⊠
25	4	10*	10	10	10.0	00.0	00.8	08	*⁺⁺⁻⁰⁻¹n-13¼, = n-n, ⊙, ⊠
26	6	10≡	00 ⊙	06	05.3	02.3	00.2	08	= n-6½, 8¾-n; ≡⁰⁻¹6½-8¾, ⊙, ⊠
27	4	10*	10	10*	10.0	00.0	00.6	08	= n-n, *⁺⁺⁻⁰3⁴⁰-n, ⊠
28	4	10*	10*	10*	10.0	00.0	13.9	17	*⁺⁺⁻⁰⁻¹⁻²n-16¾i, = n-n, T14½-16⁴⁰i, ⊠15-15¼, ⚠⁺⁺⁻⁰20⁵⁰ n, ⊙, ⊠
29	3	10	10≡*	10●≡	10.0	00.0	13.5	21	= n-12¼, ∞6½-7¼, ⚠●⁰⁻¹7¼-11i, ●⁺⁺⁻¹9½-10½, 16¼-n; ●11-12¼, ≡ 12¼-14¾, *12¼
30	5	10●	04 ⊙	08	07.3	01.3	22.3	29	= n-11½, 19¼-n; ●⁺⁺⁻⁰3¾-7, ●⁺⁺⁻⁰⁻¹7-11¼, 16-18⁴⁰, ≡⁵11½-12¼, *⁺⁺⁻⁰7⁴⁰ [19½, ≡⁰⁻¹14¾ n, ⊠
31	3	10	10*	10*	10.0	00.0	06.3	19	= n-n, ●°8¾-10½, ●⁺⁺⁻⁰10½-11¼, *⁰⁻¹11¼-n, ⊠ [-20⁴⁰, ⊙, ⊠
MES. VREDN.		09.0	07.9	08.0	08.3	27.9	109.2		

$\varphi = 45^{\circ}\ 49'$ N $\lambda = 15^{\circ}\ 59'$ E Gr. $\Delta G =$ + 1h 04 min. BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	735.9	734.7	736.4	-02.1	-01.3	-02.0	-01.8	-00.3	-02.1	-	-	-	-	-	-	-	-	SSW 1	ENE 1	WSW 1
2	738.9	740.5	742.6	-02.6	-00.9	-03.0	-02.4	-00.4	-04.9	-	-	-	-	-	-	-	-	NNW 1	W 1	WSW 1
3	742.6	742.0	742.9	-04.4	-03.8	-05.0	-04.6	-02.1	-05.4	-	-	-	-	-	-	-	-	SW 1	SSW 1	[illegible] 1
4	743.2	744.1	739.3	-03.1	02.2	02.2	00.9	04.6	-05.0	-	-	-	-	-	-	-	-	E 1	WSW 1	ENE 1
5	733.[illegible]	731.3	730.7	03.8	08.1	10.0	08.0	10.0	02.2	-	-	-	-	-	-	-	-	NE 1	W 2	WNW 2
6	736.1	742.2	743.2	03.2	01.2	00.0	01.1	10.9	00.0	-	-	-	-	-	-	-	-	NE 4	[illegible] 1	ENE 1
7	742.1	744.8	749.4	00.2	00.8	00.0	00.2	00.9	00.0	-	-	-	-	-	-	-	-	NNE 1	WSW 1	ENE 2
8	754.1	756.1	757.3	-04.8	-02.0	-03.4	-03.4	00.0	-05.4	-	-	-	-	-	-	-	-	ENE 1	S 1	NW 1
9	756.7	756.4	757.0	-04.0	-01.2	-02.5	-02.6	-01.0	-04.4	-	-	-	-	-	-	-	-	ESE 1	SE 2	ENE 1
10	75[illegible].3	752.5	751.0	-02.9	-01.0	-01.5	-01.7	-00.9	-03.0	-	-	-	-	-	-	-	-	ENE 1	SE 2	SW 1
11	747.8	745.3	743.7	-01.8	02.9	02.8	01.7	03.1	-02.1	-	-	-	-	-	-	-	-	SSW 1	S 1	ENE 1
12	739.6	738.0	738.5	04.0	03.9	02.4	03.2	04.7	02.4	-	-	-	-	-	-	-	-	NE 2	ESE 1	ESE 1
13	739.1	739.1	740.1	01.9	02.5	02.0	02.1	02.7	01.3	-	-	-	-	-	-	-	-	SE 1	SSW 1	SSW 1
14	740.0	739.9	740.6	01.0	01.7	00.5	00.9	03.1	00.[illegible]	-	-	-	-	-	-	-	-	WSW 1	WSW 1	SSW 1
15	739.6	738.4	738.3	03.1	05.7	06.8	05.6	07.9	00.1	-	-	-	-	-	-	-	-	W 1	ENE 1	NE 2
16	737.5	736.6	738.5	05.0	05.7	04.8	05.1	06.8	04.8	-	-	-	-	-	-	-	-	ENE 1	E 1	N 2
17	739.7	740.4	744.9	03.2	04.6	03.4	02.2	05.9	00.4	-	-	-	-	-	-	-	-	WSW 2	ENE 2	E 2
18	748.4	748.9	751.0	-02.4	-01.7	-02.6	-02.3	00.4	-02.6	-	-	-	-	-	-	-	-	SE 2	ESE 2	SE 2
19	752.6	753.1	755.2	-03.7	-03.0	-04.0	-03.7	-02.6	-04.1	-	-	-	-	-	-	-	-	SE 2	S 2	SE 2
20	755.6	755.3	754.3	-03.5	-02.7	-02.7	-02.8	-02.2	-04.4	-	-	-	-	-	-	-	-	SE 1	NW 2	SW 1
21	753.3	752.9	753.0	-03.3	-02.9	-02.9	-03.0	-02.4	-03.5	-	-	-	-	-	-	-	-	S 2	SE 1	SE 2
22	752.7	752.4	752.4	-03.4	-01.5	-02.1	-02.3	-01.5	-03.4	-	-	-	-	-	-	-	-	ESE 2	E 1	ESE 1
23	752.6	752.5	752.9	-02.5	-02.1	-02.8	-02.6	-02.0	-02.8	-	-	-	-	-	-	-	-	SE 1	ESE 1	SE 2
24	752.9	752.3	751.8	-03.6	-02.3	-02.7	-02.8	-02.0	-04.0	-	-	-	-	-	-	-	-	SW 1	SSW 1	NNE 1
25	751.1	752.4	753.3	-02.0	-00.2	-01.0	-01.0	-00.2	-02.8	-	-	-	-	-	-	-	-	NE 1	SSW 1	NE 1
26	753.0	753.1	753.0	-00.7	00.5	00.9	00.4	01.2	-01.2	-	-	-	-	-	-	-	-	NE 1	E 1	E 1
27	752.2	750.2	749.7	00.6	08.0	08.7	06.5	08.7	-00.7	-	-	-	-	-	-	-	-	NNE 1	W 2	NW 2
28	750.0	749.4	749.5	04.7	05.5	02.6	03.8	08.7	02.6	-	-	-	-	-	-	-	-	E 1	WSW 2	NNE 1
29	750.3	749.7	749.1	01.1	03.4	01.3	01.8	03.5	00.2	-	-	-	-	-	-	-	-	SE 1	SW 2	NNE 2
30	745.2	743.4	742.7	-01.0	00.2	00.5	00.0	01.3	-01.1	-	-	-	-	-	-	-	-	ENE 1	NE 1	NE 1
31	743.2	744.3	748.1	-00.4	01.2	-00.9	-00.2	01.4	-00.9	-	-	-	-	-	-	-	-	NE 2	NE 2	NE 2
MES. VRED.	746.3	746.2	746.8	-00.6	01.0	00.2	0.2	02.2	-01.6	-	-	-	-	-	-	-	-	1.3	1.4	1.4

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1	748.3	747.3	747.7	-01.1	-00.7	-03.0	-02.0	-00.3	-03.0	-	-	-	-	-	-	-	-	ENE 2	ENE 2	ENE 1
2	748.4	747.6	746.0	-04.2	-00.5	-03.0	-02.7	-00.4	-05.2	-	-	-	-	-	-	-	-	NNW 1	SSW 2	SSE 1
3	739.1	737.9	739.8	-01.2	05.7	06.5	04.4	06.6	-03.4	-	-	-	-	-	-	-	-	WSW 2	NW 4	WNW 4
4	742.5	741.2	739.8	01.7	05.2	03.5	03.5	06.5	01.3	-	-	-	-	-	-	-	-	NNW 1	ESE 1	SSW 1
5	738.5	738.0	736.5	08.8	10.4	09.7	09.6	10.4	03.5	-	-	-	-	-	-	-	-	WSW 2	WSW 1	WSW [illegible]
6	740.4	741.7	744.4	07.7	13.1	08.2	09.3	13.1	06.6	-	-	-	-	-	-	-	-	WNW 2	WSW 4	WNW 2
7	747.0	747.0	746.7	02.6	02.2	02.2	02.3	08.3	00.7	-	-	-	-	-	-	-	-	NE 3	ENE 2	ESE 1
8	743.7	743.0	742.8	01.1	09.7	06.1	05.8	10.4	01.0	-	-	-	-	-	-	-	-	WSW 1	WSW 2	WSW 3
9	742.0	739.6	738.1	03.4	13.9	10.7	09.7	14.0	03.3	-	-	-	-	-	-	-	-	W 2	WSW 4	SSW 4
10	735.2	736.9	739.0	09.4	00.9	01.5	03.3	11.4	00.6	-	-	-	-	-	-	-	-	W 1	NNW 1	WNW 2
11	738.0	735.2	739.8	-00.4	01.3	02.1	01.3	02.7	-00.9	-	-	-	-	-	-	-	-	ENE 1	WSW 2	NNE 3
12	745.4	745.7	742.9	-01.4	02.7	01.2	00.9	07.1	-02.4	-	-	-	-	-	-	-	-	W 1	SSW 2	SE 1
13	738.9	738.1	739.8	00.5	03.4	01.0	01.5	03.6	00.2	-	-	-	-	-	-	-	-	ENE 2	NNE 1	ENE 1
14	743.8	741.0	732.4	01.0	04.4	01.8	02.2	04.4	-00.6	-	-	-	-	-	-	-	-	ENE 2	ENE 2	NE 4
15	731.8	735.3	740.7	01.8	01.6	-00.9	00.4	02.0	-00.9	-	-	-	-	-	-	-	-	W 1	ENE 2	ENE 2
16	744.4	745.7	746.2	-04.5	-01.9	-04.3	-03.8	-00.9	-04.5	-	-	-	-	-	-	-	-	ENE 2	ENE 2	N 1
17	748.1	750.5	750.3	-05.6	-00.1	-02.1	-02.5	00.2	-05.7	-	-	-	-	-	-	-	-	NW 2	WSW 3	W 1
18	745.9	746.6	747.5	-02.9	-01.2	-00.4	-01.2	-00.2	-03.1	-	-	-	-	-	-	-	-	SSW 1	NE 1	NNE 1
19	751.7	753.1	754.6	-01.5	02.4	-00.8	-00.2	02.9	-01.9	-	-	-	-	-	-	-	-	SSW 1	SSW 2	WNW 1
20	753.8	751.0	746.7	-05.4	01.8	00.1	-00.8	02.4	-05.7	-	-	-	-	-	-	-	-	WSW 1	WSW 2	NE 2
21	749.7	748.9	745.5	-02.3	03.4	01.1	00.8	03.9	-02.3	-	-	-	-	-	-	-	-	NE 1	W 2	ENE 1
22	743.0	742.9	742.4	00.9	07.3	07.2	05.6	07.9	-00.1	-	-	-	-	-	-	-	-	WSW 2	W 3	WNW 3
23	737.8	737.9	740.5	06.2	09.9	04.0	06.0	10.4	04.0	-	-	-	-	-	-	-	-	W 2	WSW 3	NNW 1
24	742.6	741.3	743.0	01.2	07.3	04.2	04.2	07.3	01.2	-	-	-	-	-	-	-	-	ENE 2	ESE 2	NE 2
25	744.4	743.7	743.8	00.7	04.4	03.4	03.0	04.4	00.7	-	-	-	-	-	-	-	-	SSW 1	SSW 2	N 1
26	742.5	741.9	743.0	01.6	05.1	01.3	02.3	05.2	01.6	-	-	-	-	-	-	-	-	NW 1	SSW 2	ENE 2
27	743.4	742.9	745.8	-02.5	01.0	-00.2	-00.5	01.4	-02.5	-	-	-	-	-	-	-	-	ENE 3	ESE 1	NE 3
28	745.7	746.7	748.5	-01.2	01.5	-00.7	-00.3	01.5	-01.2	-	-	-	-	-	-	-	-	ENE 2	SSE 1	ESE 2
MES. VRED.	743.4	743.2	743.4	00.5	04.1	02.2	2.2	05.1	-00.7	-	-	-	-	-	-	-	-	1.6	2.1	1.9

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BR. ST. 57 H_s = 157 m H_b = 162.5 m h_t = 6.0 m h_r = 2.0 m

Dan	Vidljivost 0–9	Oblačnost N (0—10)				Insolacija broj sat	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	5	10	10	10	10.0	00.0	20.2	04	$*n_1 = n-n_1$ ⊠
2	4	10*≡	10	00	06.7	00.0	00.4	03	$*^{0-1}n-12^{30} \equiv n-11^{30} \equiv 11^{30}-n_1$ ⊠
3	3	10≡	00≡	00≡	03.3	00.0	03.8	03	$V^0n-n_1 \equiv {}^0n-13^{30} \equiv {}^{1-0}13^{30}-n_1$ ⊠
4	4	09≡	09	09	09.0	01.2	•	00	$\equiv {}^0n-12 = 12-n$ ⊠
5	4	10	09	10	08.3	00.4	•	22	$= n-15^{30}, \bullet^{tr-1}9^{45}-12^{50}i_1$ ⊠
6	5	10●	10*	10*	10.0	00.0	04.0	16	$= n-n_1 \bullet^{0-1}n-7^{40}$ FNE $6^{40}-6^{50}, *7^{40}-7^{55}, *7^{55}-n_1$ ⊠
7	4	10	10*	10*	10.0	00.0	12.2	16	$= n-n_1 *n_1 10^{15}-ni$ ⊠
8	3	00≡	10≡	10≡	06.7	00.0	03.9	19	$V^0n-n_1 \equiv n-8^{30} \equiv {}^{0-1}8^{30}-n \leftrightarrow 9^{30}-14^{30}$ ⊠
9	4	10≡	10●	10	10.0	00.0	•	17	$\equiv {}^1n-12^{30}i \equiv {}^{0-1}7^{40}-8^{30} = 12^{30}-n_1$ ⊠
10	5	10	10	10	10.0	00.0	•	17	$= n-n_1 \sim^{tr}9^{40}-11^{45}$ ⊠
11	4	10≡	10	10	10.0	00.7	00.1	15	$\equiv {}^0n-11^{30} \equiv 11^{30}-n_1 \bullet^{tr}15^{15}-15^{25}$ ⊠
12	2	10●	10●	10≡	10.0	00.0	00.1	12	$= n-8^{40} \bullet^{tr-0}6^{20}-14^{30} \equiv {}^{0-2}8^{40}-17^{30} \equiv {}^2 17^{30}-n_1$ ⊠
13	1	10●≡	10≡	10≡	10.0	00.0	07.8	08	$\equiv {}^2n_1 \bullet^{0-tr}n-a \bullet^{0-tr}12^{50}-ni \equiv {}^{1-2}13^{30}-n_1$ ⊠
14	2	10≡	10≡	10≡	10.0	01.1	03.3	06	$\bullet n_1 \equiv {}^{1-2}n-ni \equiv {}^{0-1}10^{30}-17^{45}i_1$ ⊠
15	5	10≡	10●	09	09.7	00.0	•	05	$\equiv {}^{0-1}n-15^{30} \bullet^{tr-0}12^{20}-14^{45}, = 15^{30}-n_1$ ⊠
16	1	10≡	10≡	10	10.0	00.0	03.3	00	$\bullet^{tr-0}n-a, 18^{45}-19^{45}, \equiv {}^0n-9^{30}, \equiv {}^{1-2}9^{30}-17^{30}, = 17^{30}-n$
17	5	10	09	10	09.7	00.0	•	•	$= n-n$
18	5	10	10	10	10.0	00.4	•	•	$= n-n$
19	6	10	10	10	10.0	00.0	•	•	$= n-n_1 \Delta^{tr}15^{30}-16^{45}i$
20	6	10	10	10	10.0	00.0	00.0	•	$= n-n$
21	5	10	10	10	10.0	00.0	•	•	$= n-n$
22	6	10	10	10	10.0	00.0	•	•	$= n-n$
23	6	10	10	10	10.0	00.0	•	•	$= n-n$
24	5	10	10	10*	10.0	00.0	•	•	$= n-n_1 *^{tr-1}15^{45}-n_1$ ⊠
25	5	10	10	10	10.0	00.0	09.3	08	$= n-n_1 *n_1$ ⊠
26	4	10	10	10	10.0	00.0	•	08	$\equiv n-7^{15}, \equiv {}^{0-2}7^{15}-11^{30}$ ⊠
27	3	10≡	10≡	10	10.0	00.1	•	05	$\equiv {}^{0-1}n-15^{30} = 15^{30}-n_1 \bullet p-n$ ⊠
28	3	10●	09	00	06.3	01.7	08.3	•	$\bullet^{tr-0}n-7^{45}, \equiv n_1 12^{15}-p; \equiv {}^{0-12}n-12^{45}$
29	6	10	03⊙	00	04.3	04.3	00.3	•	$= n-13^{15}, \sim^0 20-n$
30	4	10	10*	10*	10.0	00.0	•	•	$= n-9, \sim^0 n-9, *8^{15}-8^{30}11^{30}-n_1$ ⊠
31	5	10*	10	10*	10.0	00.0	03.1	02	$= n-n, *^{tr-0}n-13^{45}, 15^{45}-ln_1$ ⊠
MES. VREDN.		09.6	09.2	08.6	09.2	10.4	80.3		

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1	4	10*	10	10*	10.0	00.0	00.7	04	$= n-n_1 *^{tr}n-n$
2	5	02	00⊙	10	04.0	05.8	00.7	04	$= n-n$
3	5	10	10	02	07.3	00.0	•	03	$= n-n_1 \bullet^0 16^{20}-16^{35}$
4	3	08≡	10≡	10	09.3	02.2	00.4	•	$\equiv {}^0n-n$
5	6	10	10	10	10.0	00.0	•	•	$= 8^{30}n_1 \bullet^{tr}12-12^{30}$
6	7	01	02⊙	00	01.0	00.4	00.0	•	$= n-13^{30}$
7	5	10	10	10	10.0	00.0	•	•	$= n-n_1 *^{0-1}0^{15}-11^{45}$
8	6	10≡	03⊙	00	04.3	06.1	01.9	•	$\equiv {}^{1-2}n-9 \equiv {}^{0-1}9^{30}-10^{45}, = 10^{15}-13^{45}$
9	8	00	06⊙	10	05.3	06.7	•	•	$= n-9^{30}$
10	3	10●	10*	10	10.0	00.0	00.2	•	$= n-n_1 \bullet^{tr}n-11^{25}, 14^{30}-n; *^{1-2}11^{25}-13^{20}i, *^{1-2}11^{55}-14^{30}i, 15\ 11^{55}-11^{58}$
11	4	10≡	10*	10	10.0	00.1	25.2	00	$\equiv {}^2n-11^{10}i, \equiv 9^{20}-12^{30}i, = 12^{30}-n_1 \bullet^0 12^{45}-13^{19}, *13^{19}-20^{45}$
12	6	00≡	00⊙	03	01.0	07.3	14.7	04	$\equiv {}^0n-9^{45} = 9^{45}-n$
13	5	10	10	01	07.0	00.0	•	03	$= n-n_1 *^{tr-1}7^{20}-9^{05} \bullet^0 9^{05}-13^{30}$
14	6	10	10	10	10.0	00.0	02.7	02	$= n-n *^0n_1 19^{13}-n; \bullet^0 18^{35}-19^{13}$
15	5	10●	10	10	10.0	00.0	12.0	03	$= n-n_1 *\bullet n-n_1 \bullet 8^{35}-9^{45}, *^0 9^{45}-9^{45}, *^{tr-0-1}9^{45}-14^{45}i$
16	4	02	10	09	07.0	01.1	03.6	07	$= n-n$
17	5	01	00⊙	00	00.3	00.3	•	05	$= n-n$
18	4	10	10*	10	10.0	00.0	•	04	$= n-11, \equiv 8^{30}-10^{45}, *^{tr-1}9^{50}-20^{12}i$
19	4	10≡	05⊙	00	05.0	06.0	05.2	13	$\equiv n-9^{30} = 9^{30}-n$
20	4	00≡	09⊙	10	06.3	01.8	•	10	$\equiv {}^0n-11^{15}, = 11^{15}-n$
21	5	03≡	09	10	07.3	01.6	00.2	10	$*n_1 \equiv 6^{45}-7^{30} \equiv {}^{1-2}7^{30}-11^{45}, = 11^{45}-n$
22	7	10	10	00	06.7	01.4	•	05	$= n-12^{15}, 16^{30}-n$
23	5	00●	00⊙	00	01.7	03.0	00.9	•	$\bullet^0n-7^{15}, = n-n$
24	6	01⊙	02⊙	02	02.0	00.6	00.1	•	$= n-n$
25	6	05	10●	10	09.3	00.1	•	•	$= n-n_1 *^{tr-1}8^{35}-9^{40}, \bullet^{tr}13^{45}-ni$
26	6	09	10	10*	09.7	01.2	00.1	•	$= n-n_1 \bullet^{tr-0}19^{24}-19^{54} *^{tr-0}19^{54}-n$
27	6	10*	10	10	10.0	01.2	01.4	02	$= n-n_1 *n-8^{30}-19^{24}-20^{38}$
28	5	10	10	10	10.0	01.5	00.3	•	$= n-n_1 *^{tr}14^{10}-ni$
MES. VREDN.		08.5	07.6	06.7	08.0	73.4	71.3		

VIDLJIVOST OSMATRANA U 13 ČASOVA

$\varphi = 45^{\circ}\ 49'$ N $\lambda = 15^{\circ}\ 59'$ E Gr. $\Delta G =$ + 1h 04 min.

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Srednja	Max	Min	Min 5 cm	7	14	21	7	14	21	Srednja	7	14	21
1	749.4	749.0	749.6	-01.9	02.1	-01.7	-00.8	02.1	-02.2	-	-	-	-	-	-	-	-	WNW 2	SSW 2	ENE 1
2	744.9	739.4	735.6	-04.2	03.0	01.8	01.6	04.1	-04.2	-	-	-	-	-	-	-	-	NNW 1	WSW 2	WSW 2
3	732.9	731.6	732.3	00.9	01.3	02.6	01.8	03.8	00.9	-	-	-	-	-	-	-	-	ENE 2	NE 3	ENE 1
4	731.3	728.5	725.6	04.6	07.5	05.4	05.7	07.6	02.4	-	-	-	-	-	-	-	-	NE 3	ENE 3	NE 2
5	727.2	729.8	733.8	02.2	03.7	02.7	02.8	03.4	01.5	-	-	-	-	-	-	-	-	W 2	ESE 2	W 1
6	741.7	743.5	746.3	02.2	06.4	01.7	03.0	07.1	01.7	-	-	-	-	-	-	-	-	ESE 1	NE 3	NNE 3
7	747.3	748.4	749.6	01.4	02.7	00.9	01.5	02.7	00.9	-	-	-	-	-	-	-	-	NNE 2	WNW 2	WSW 2
8	749.5	748.1	747.5	-02.0	04.4	02.4	01.8	04.8	-02.0	-	-	-	-	-	-	-	-	ENE 1	ESE 2	NE 2
9	746.1	746.3	748.7	00.4	04.5	02.3	02.4	04.6	00.4	-	-	-	-	-	-	-	-	ENE 1	S 1	WNW 1
10	752.0	753.6	754.2	02.4	05.4	03.7	03.8	05.5	02.1	-	-	-	-	-	-	-	-	S 1	S 1	NW 2
11	752.7	749.9	747.8	04.1	07.2	04.5	05.1	07.2	03.1	-	-	-	-	-	-	-	-	NE 2	ENE 2	ENE 2
12	743.7	743.5	746.0	00.6	02.3	02.5	02.0	04.5	00.4	-	-	-	-	-	-	-	-	W 1	WNW 2	W 2
13	747.7	748.5	748.2	00.6	08.0	06.3	05.3	08.5	00.4	-	-	-	-	-	-	-	-	W 1	SSW 2	NNE 2
14	746.3	743.8	742.1	05.9	04.7	03.3	04.1	06.3	03.2	-	-	-	-	-	-	-	-	NE 3	NE 4	NNE 4
15	740.9	742.1	744.9	02.4	02.6	01.6	02.0	03.5	01.6	-	-	-	-	-	-	-	-	NNE 3	NNE 2	NE 2
16	747.2	748.1	749.3	02.4	06.6	04.1	04.3	06.6	01.3	-	-	-	-	-	-	-	-	NE 3	ENE 3	ENE 2
17	748.4	747.5	746.8	03.0	03.9	02.7	03.1	04.1	02.7	-	-	-	-	-	-	-	-	NNE 1	WNW 2	WNW 2
18	744.4	740.0	739.6	01.5	09.0	06.9	06.1	10.6	00.6	-	-	-	-	-	-	-	-	WNW 2	WSW 2	W 2
19	737.2	738.6	741.9	03.8	05.7	04.1	04.4	06.9	02.9	-	-	-	-	-	-	-	-	ENE 2	WNW 2	NW 2
20	747.2	748.4	749.7	03.2	10.0	06.0	06.3	10.6	02.0	-	-	-	-	-	-	-	-	NNE 2	SE 2	W 1
21	750.3	749.9	749.4	02.1	12.9	09.6	08.6	14.7	02.1	-	-	-	-	-	-	-	-	SSW 1	SSE 1	NNW 1
22	749.2	748.4	749.3	03.2	15.3	10.0	09.6	15.8	02.7	-	-	-	-	-	-	-	-	W 2	WSW 3	W 2
23	748.7	749.2	748.5	08.1	15.8	11.7	11.8	16.0	06.4	-	-	-	-	-	-	-	-	WNW 2	WSW 4	W 1
24	747.9	747.6	747.8	09.5	17.6	13.6	13.6	18.3	08.8	-	-	-	-	-	-	-	-	WNW 1	WSW 4	WSW 2
25	748.3	747.3	746.3	11.0	17.0	12.1	13.0	18.1	10.4	-	-	-	-	-	-	-	-	WNW 2	SSW 3	WNW 1
26	746.5	745.8	745.0	10.4	11.0	09.9	10.3	12.1	09.9	-	-	-	-	-	-	-	-	SSW 1	ENE 2	NE 1
27	740.8	737.2	736.9	09.4	10.2	09.1	09.4	11.0	09.1	-	-	-	-	-	-	-	-	E 1	ESE 2	W 2
28	740.8	739.3	740.7	02.8	09.8	02.7	03.5	09.1	02.5	-	-	-	-	-	-	-	-	ENE 1	NNE 2	WNW 2
29	742.0	741.8	745.5	-00.4	09.7	05.6	05.1	10.3	-00.5	-	-	-	-	-	-	-	-	WSW 2	WSW 3	NW 2
30	746.3	746.5	746.2	01.6	13.0	08.9	08.1	13.7	01.0	-	-	-	-	-	-	-	-	NW 1	WSW 5	WSW 3
31	745.1	742.0	740.6	08.1	13.8	10.5	10.7	14.7	07.5	-	-	-	-	-	-	-	-	WNW 2	WSW 4	WNW 2
MES. VRED.	744.7	744.0	744.3	03.2	07.8	05.5	5.5	08.8	02.6	-	-	-	-	-	-	-	-	1.7	2.4	1.9

1	737.1	737.1	741.1	09.6	09.2	05.8	07.4	14.9	05.8	-	-	-	-	-	-	-	-	NE 2	NNW 4	SE 1
2	740.0	737.4	736.4	06.3	12.1	07.2	08.2	13.7	03.5	-	-	-	-	-	-	-	-	ENE 2	NE 2	WSW 1
3	737.4	740.4	742.7	01.8	03.9	03.5	03.1	07.2	01.5	-	-	-	-	-	-	-	-	WSW 2	NNW 2	W 1
4	743.0	741.7	742.8	00.9	10.0	05.9	05.7	10.7	-00.1	-	-	-	-	-	-	-	-	WNW 2	W 3	WSW 2
5	743.6	742.0	741.9	02.8	08.6	04.7	05.2	08.7	02.5	-	-	-	-	-	-	-	-	SSW 2	NE 2	NNW 2
6	743.8	745.3	745.7	05.2	08.2	06.3	06.5	09.4	04.3	-	-	-	-	-	-	-	-	N 3	NW 2	WSW 1
7	744.4	743.1	741.8	05.6	12.9	09.7	09.5	13.4	04.0	-	-	-	-	-	-	-	-	SSW 1	WSW 3	WNW 2
8	738.7	736.4	734.6	07.3	08.9	08.4	08.2	09.9	05.6	-	-	-	-	-	-	-	-	ESE 1	ESE 1	NNE 1
9	731.5	733.1	737.7	08.0	14.0	08.7	09.6	14.5	07.5	-	-	-	-	-	-	-	-	SSW 1	WSW 4	WNW 2
10	741.6	742.6	744.6	09.0	13.9	10.3	10.9	15.6	07.6	-	-	-	-	-	-	-	-	WNW 2	W 3	WNW 2
11	746.1	746.9	747.6	07.0	06.1	05.1	05.8	10.4	05.1	-	-	-	-	-	-	-	-	NNW 1	NE 2	ENE 1
12	747.4	745.7	745.4	05.6	11.8	08.3	08.5	13.1	04.6	-	-	-	-	-	-	-	-	WNW 1	NE 2	SE 1
13	744.4	742.8	743.2	06.0	15.2	10.9	10.8	15.7	04.3	-	-	-	-	-	-	-	-	WNW 2	WSW 4	W 2
14	745.2	746.3	750.1	07.3	11.1	09.3	09.2	11.8	07.2	-	-	-	-	-	-	-	-	NE 2	SSW 2	NE 3
15	754.4	754.9	756.7	07.3	10.0	07.6	08.1	11.2	06.9	-	-	-	-	-	-	-	-	NE 3	NNE 3	NE 2
16	758.0	755.5	755.7	06.1	12.5	09.5	09.4	13.8	05.1	-	-	-	-	-	-	-	-	NNE 2	ENE 2	NNE 1
17	755.9	753.6	752.0	07.9	16.1	15.8	13.9	17.8	06.0	-	-	-	-	-	-	-	-	NNW 1	SW 2	W 2
18	749.5	747.6	747.2	15.3	24.5	16.7	18.3	24.8	12.5	-	-	-	-	-	-	-	-	WNW 2	WNW 2	N 1
19	747.3	744.9	743.6	13.1	24.9	19.0	19.0	25.6	12.2	-	-	-	-	-	-	-	-	ENE 1	SE 2	W 2
20	743.4	743.7	746.2	14.2	21.7	16.0	17.0	21.9	13.6	-	-	-	-	-	-	-	-	W 1	WSW 2	S 1
21	751.5	754.6	756.6	09.1	08.0	07.8	08.2	16.0	07.8	-	-	-	-	-	-	-	-	ENE 2	S 1	ENE 1
22	757.2	755.5	755.0	06.4	15.2	14.1	12.4	18.0	05.3	-	-	-	-	-	-	-	-	WNW 1	W 2	S 2
23	753.2	750.0	749.0	10.4	23.7	18.0	17.5	24.8	09.1	-	-	-	-	-	-	-	-	W 1	WSW 2	WNW 3
24	748.9	747.4	749.6	17.2	22.7	15.0	17.5	24.2	13.9	-	-	-	-	-	-	-	-	WNW 3	SSW 2	ENE 2
25	748.1	745.3	743.3	13.7	19.0	16.7	16.5	21.0	12.0	-	-	-	-	-	-	-	-	SW 1	ESE 2	WNW 1
26	741.1	739.4	737.4	14.3	21.1	16.6	17.2	22.8	12.8	-	-	-	-	-	-	-	-	WNW 1	WSW 4	NW 1
27	742.9	743.7	745.7	09.6	17.0	11.5	12.4	17.9	08.7	-	-	-	-	-	-	-	-	ENE 1	ESE 2	NE 1
28	746.4	746.0	744.7	10.1	10.8	08.9	09.7	12.6	07.8	-	-	-	-	-	-	-	-	N 1	NNE 1	NNE 2
29	745.8	746.3	744.2	07.1	09.6	07.4	07.9	11.0	06.4	-	-	-	-	-	-	-	-	SW 2	SSW 2	W 2
30	747.8	749.2	749.8	03.0	06.9	05.6	05.3	09.4	02.5	-	-	-	-	-	-	-	-	ESE 2	SSW 2	NW 2
MES. VRED.	745.5	745.2	745.7	03.2	13.7	11.3	10.7	15.4	06.9	-	-	-	-	-	-	-	-	1.6	2.2	1.5

BR. ST. 57 H_s = 157 m H_b = 162.5 m h_t = 6.0 m h_r = 2.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnevni		7	7	
1	6	10	10	10	10.0	02.5	00.1	01	= n-n, *tr-o 15^15 ni
2	4	08≡	09	10	09.0	03.4	00.6	01	≡ 1n-9^30 = 9^30 n
3	4	10*	10*	10●	10.0	00.0	00.5	-	*0-1n-15^45, *°15^45-16^30 ●°16^30 ni
4	6	10	10	10●	10.0	00.0	03.1	.	●tr-°14^20-n, = n-ni, ≡ 1°16^15-17^30
5	6	09	10●	10	09.7	02.7	10.2	.	= n-8^30, 11^30-n; ●tr-1 11^05-15^20, 18^21-20^40
6	6	07	09	10●	08.7	03.6	04.6	.	= n-n, ●tr-°18^21-22, * 22-n
7	6	10	10	00	06.7	02.0	02.6	.	= n-n, *tr-°8^15-11^25
8	6	01⊙	01⊙	00	00.7	08.0	00.1	.	= n-n, ⌴1n-9
9	6	07≡	10	10●	09.0	00.9	.	.	≡°n-9^15, = 9^15-n, ●tr-°16^31-17^51, 20^13-24^15
10	6	10	10	09	09.7	00.2	01.7	.	= n-n
11	6	10	10	10●	10.0	00.0	.	.	= n-n, ●tr-°17^50-n
12	6	10*	10	10●	10.0	00.0	25.2	06	= n-n, *0-1n-8^10 ● 8^40-9^05, 19^30-n
13	6	00≡	03	10	04.3	07.7	01.3	02	≡°n-8^30, = 8^30-13^30, 17^15-n
14	6	10	10	10●	10.0	00.0	.	.	= n-n, ●tr-°15^40, n
15	5	10●	10*	10	10.0	00.0	05.6	.	= n-n, ●0-1n-12^15, *0-1 12^15-13^45, 18^15-n; *° 13^45-18^15
16	6	10*	06⊙	10	08.7	04.4	01.7	.	= n-n, *tr n-7^45
17	5	10	10	00	06.7	00.9	00.0	.	= n-n, *tr 8^50-10^30
18	7	08	08⊙	10	08.7	04.2	00.0	.	= n-10^30 15^45-n; ●tr-°22^30-ni
19	5	10●	10	00	06.7	00.3	02.4	.	= n-18^30 ●0-1n-11^45 i; *0-1 7^55-8^30
20	7	01⊙	05⊙	00	02.0	08.5	09.2	.	≡°n-8^30, = 8^30-12^15
21	7	02	05⊙	09	05.7	05.1	.	.	= n-12^15, 18^45-n; Φ 19^45 n
22	7	00⊙	04⊙	06	03.3	09.7	.	.	= n-11, 17^30 n
23	8	09	09	10	08.3	03.9	.	.	= n-11^00 16^45-19^30, ●tr 15^44-ni
24	8	09	07⊙	00	05.3	03.5	00.0	.	= n-10^30
25	8	09*	09	10	09.3	01.4	.	.	= n-11^30, ●tr-o 14^20-20^15
26	5	10●	10●	10	10.0	00.0	01.7	.	= n-n, ●tr-o-1 6^40-20^10
27	4	10≡	10●	07	09.0	00.0	13.4	.	≡°n-9^50 = 9^50-n, ●0-2 9^55-19^06
28	8	10	09	00	06.3	01.1	15.1	.	= n-10^30 ● * n, *1tr 12^52
29	8	00⊙	05⊙	00	01.7	10.2	00.0	.	= n-10^30, ⌴°n-8^15
30	9	00⊙	04⊙	00	01.0	11.0	.	.	= n-9^15, F sw 13^25-19 i
31	8	05⊙	09	01	05.0	01.4	.	.	= n-8, F sw 11^20-16^50 i
MES. VRED.		07.2	08.1	06.5	07.3	96.6	105.6		

1	8	09	09	04	07.3	01.8	.	.	= n-9^30 ●tr-o 12^45-13^30 17^14-17^30 i; ● 16^45-16^27
2	6	10	05⊙	10	08.3	05.0	03.1	.	= n-13^45 17^15-n; ●tr-o 12^05-12^20, 18^22-21^04 i
3	7	10*	10	00	06.7	01.8	12.5	.	= n-12^45, *1-2 n-1 10^30 i
4	8	05	04⊙	01	03.3	09.3	00.4	.	= n-9^30 ⌴°n-7^45
5	7	10*	10	10	10.0	00.8	00.1	.	*6^40-7^15, ●0-1 19^25-20^30
6	8	09⊙	10	01	06.7	07.7	00.5	.	= 18^30-n
7	7	10≡	08⊙	03	07.0	05.7	.	.	≡°n-7^40 = 7^40-9^15
8	4	10●	10●	10●	10.0	00.0	00.2	.	●0-1n-7^50 i, 11^15-n, = n-ni, ≡ 1 8^15-10^15
9	9	10≡	08⊙	02	06.7	04.4	23.1	.	●0-tr n, 9^45-6^45 18^35, ≡°n-7^45, = 7^45-11^15, F wsw 13-19
10	9	01⊙	07⊙	02	03.3	07.9	01.0	.	F 0-0^30, ●°9^02-9^16
11	6	10	10●	10●	10.0	00.0	00.1	.	= n-n, ●°n-22 i
12	7	01⊙	06	00	02.3	08.9	04.9	.	= n-11^15
13	8	10	10	10●	10.0	03.9	.	.	= n-12^15 F wsw 13-16, ●tr-1 20^03-21^31
14	7	10●	10	10	10.0	00.0	29.0	.	= n-11^30, ●0-2 n-9^30 12^48-13^25
15	6	02⊙	09	01	04.0	06.2	00.4	.	= n-n, ●tr 11^03-11^18
16	6	09	03⊙	09	07.0	07.1	00.0	.	= n-n
17	6	08⊙	09	10	09.0	02.5	.	.	= n-n
18	8	10	00⊙	00	06.0	06.4	.	.	
19	7	01⊙	01⊙	06	02.7	10.8	.	.	= n-13
20	7	09	10	10	09.7	02.2	.	.	= n-12^15, 18^30-n; Φ 7^45-8^45 i, ●tr-o 14^20-15^40 i
21	5	10●	10●	10●	10.0	00.0	00.6	.	= n-n, ●tr-o-1 n-ni
22	7	05⊙	05⊙	02	04.0	10.7	09.9	.	= n-12^30 18^45-n
23	7	08⊙	07⊙	03	06.0	10.6	.	.	= n-10^30 ⊕ 8^30-9^45
24	7	10	10⊙	02	07.3	07.3	.	.	= n-12, 1F NE 18^31-18^55
25	7	10	04⊙	00	04.7	07.8	.	.	= n-12^15, ●tr 11^10-11^20
26	8	07⊙	03⊙	10	06.7	06.4	00.0	.	F w 13^50-14^30 ●tr-o 17^28-19^48 i, n 17^50-18^09
27	8	09	02⊙	06	05.7	07.1	05.5	.	♀0-2 0^45-1, 1 ♃+2 0^15
28	5	09	10	10●	09.7	00.3	01.2	.	= n-n, ●10-1 n, 10^05-13^30 16^44-ni
29	6	10●	10	05	08.3	00.6	2 .7	.	= n-n, ●tr-1 n-12^15 i, 18^22-18^50
30	8	10●	09	00	06.3	02.8	11.4	.	= n-10^45, ●0-1 n, 7^05-8^45; * n-7^05
MES. VRED.		08.1	07.6	05.2	07.0	144.0	145.5		

VIDLJIVOST OSMATRANA U 13 ČASOVA

1970 MAJ ZAGREB GRIČ

φ = 45° 49' N λ = 15° 59' E Gr. ΔG = + 1h 04 min. BR. ST. 57

I	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred. Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	749.2	750.0	751.4	04.2	06.3	05.6	05.4	09.0	01.6	-	-	-	-	-	-	-	-	WNW 1	NNW 2	NNE 1
2	751.0	750.2	751.8	04.0	10.0	06.0	06.5	10.6	02.0	-	-	-	-	-	-	-	-	WNW 1	N 3	WNW 2
3	753.0	751.9	752.2	06.4	13.2	09.2	09.5	14.3	03.9	-	-	-	-	-	-	-	-	NNW 1	ENE 2	NNE 2
4	750.8	747.9	746.2	06.5	16.1	13.3	12.3	17.6	04.6	-	-	-	-	-	-	-	-	- 0	SSW 2	NNE 2
5	742.8	742.5	744.0	11.6	10.0	08.7	09.8	13.6	08.7	-	-	-	-	-	-	-	-	W 1	SSE 2	SW 1
6	746.2	746.7	746.5	08.1	14.9	12.5	12.0	16.1	07.7	-	-	-	-	-	-	-	-	SSE 1	SSW 2	NE 2
7	745.5	745.2	744.6	11.7	18.2	16.4	15.7	18.5	10.8	-	-	-	-	-	-	-	-	ENE 2	ESE 2	NE 3
8	744.5	743.6	745.4	12.8	22.2	13.4	15.4	22.3	11.5	-	-	-	-	-	-	-	-	- 0	ESE 2	NW 3
9	747.7	746.7	746.5	11.1	20.5	16.4	16.1	21.5	09.3	-	-	-	-	-	-	-	-	NNW 1	SSW 3	NW 2
10	744.4	741.3	740.2	13.8	21.5	17.3	17.5	23.0	12.8	-	-	-	-	-	-	-	-	W 2	S 2	NNW 2
11	740.6	740.6	740.9	13.8	19.7	14.5	15.6	20.5	12.8	-	-	-	-	-	-	-	-	WSW 1	WSW 4	WNW 2
12	740.3	740.3	742.4	12.9	18.7	14.2	15.0	19.2	11.9	-	-	-	-	-	-	-	-	WNW 2	WSW 5	WNW 2
13	743.4	743.3	745.4	13.3	20.4	16.7	16.8	21.8	12.3	-	-	-	-	-	-	-	-	WNW 2	WNW 3	WNW 2
14	747.1	746.2	745.8	15.5	23.0	17.4	18.3	23.8	14.3	-	-	-	-	-	-	-	-	NW 3	WSW 3	WNW 3
15	743.8	742.7	742.8	16.5	19.1	16.4	17.1	20.9	13.4	-	-	-	-	-	-	-	-	W 3	WSW 4	W 2
16	741.6	740.9	742.6	14.1	14.5	13.9	14.1	21.7	12.1	-	-	-	-	-	-	-	-	W 2	NNW 3	ENE 2
17	743.3	742.7	744.7	12.6	17.7	13.0	14.1	18.0	12.5	-	-	-	-	-	-	-	-	NE 1	SSW 3	NW 2
18	747.7	749.9	752.7	13.9	17.8	15.8	15.8	19.1	12.8	-	-	-	-	-	-	-	-	NNE 3	NNE 4	NNE 3
19	753.0	751.7	750.7	14.9	19.8	15.6	16.5	20.8	13.7	-	-	-	-	-	-	-	-	NNE 3	ENE 3	NNE 2
20	749.1	747.4	747.2	13.4	22.4	16.9	17.4	22.9	10.9	-	-	-	-	-	-	-	-	E 1	NE 2	ESE 2
21	746.1	742.8	740.9	15.5	20.5	16.0	17.0	21.7	14.7	-	-	-	-	-	-	-	-	ENE 1	ENE 2	NNE 1
22	741.3	742.7	744.2	09.6	10.1	10.1	10.0	16.4	08.8	-	-	-	-	-	-	-	-	NNE 3	W 2	NNW 2
23	748.4	749.8	753.7	11.8	16.7	09.6	11.9	16.9	09.0	-	-	-	-	-	-	-	-	NNW 2	NNW 2	ENE 1
24	756.3	756.1	756.5	08.3	15.5	12.4	12.2	16.7	06.3	-	-	-	-	-	-	-	-	WNW 1	NNE 3	NNE 2
25	756.1	753.5	752.0	10.4	18.8	14.6	14.6	19.8	07.8	-	-	-	-	-	-	-	-	NE 1	WSW 2	ESE 1
26	750.4	749.2	750.4	11.7	19.8	15.0	15.4	20.4	09.8	-	-	-	-	-	-	-	-	NE 1	ESE 1	SSW 2
27	749.7	748.9	749.0	12.2	16.0	13.2	13.6	16.0	11.3	-	-	-	-	-	-	-	-	NW 1	ESE 2	SSW 1
28	749.1	748.2	748.7	10.8	16.6	11.9	12.8	17.0	08.0	-	-	-	-	-	-	-	-	N 1	SE 1	NNE 1
29	748.5	746.7	746.1	10.2	20.9	17.0	16.3	21.8	08.3	-	-	-	-	-	-	-	-	ESE 1	SSW 2	S 1
30	746.2	745.8	746.5	13.8	20.0	17.3	17.1	20.7	11.0	-	-	-	-	-	-	-	-	SW 1	WSW 3	NW 2
31	749.4	749.8	750.7	13.3	17.5	14.0	14.7	19.2	12.3	-	-	-	-	-	-	-	-	NNE 1	SSW 3	NNW 1
MES. VRED.	747.3	746.6	747.2	11.6	17.4	13.7	14.1	18.0	09.9	-	-	-	-	-	-	-	-	1.4	2.5	1.8

1970 JUN ZAGREB GRIČ

1	752.4	751.9	751.4	13.9	19.3	17.1	16.8	21.0	11.9	-	-	-	-	-	-	-	-	E 1	WSW 2	WNW 1
2	751.4	750.7	753.8	14.4	16.3	12.0	13.7	17.3	12.0	-	-	-	-	-	-	-	-	E 2	SSE 2	NE 2
3	753.5	751.6	751.1	10.8	16.3	14.1	13.8	17.8	08.7	-	-	-	-	-	-	-	-	WNW 2	NNE 3	NNE 2
4	749.9	748.9	748.4	11.6	18.2	14.8	14.8	19.3	10.0	-	-	-	-	-	-	-	-	SSW 2	NNE 1	NNW 2
5	747.2	746.3	747.3	12.8	21.2	15.8	16.4	21.6	09.4	-	-	-	-	-	-	-	-	W 2	WSW 3	W 3
6	747.6	747.3	747.7	15.0	23.0	18.7	18.8	24.2	12.3	-	-	-	-	-	-	-	-	WSW 2	WNW 2	NNW 4
7	747.3	747.3	747.4	17.0	20.8	19.0	19.0	22.4	15.3	-	-	-	-	-	-	-	-	W 2	SSW 2	ESE 1
8	747.0	747.3	747.7	16.7	22.0	18.8	19.1	22.8	16.2	-	-	-	-	-	-	-	-	ENE 2	ENE 2	NNE 2
9	747.4	747.0	746.9	18.0	23.2	20.3	20.4	24.0	15.6	-	-	-	-	-	-	-	-	NNE 1	WSW 2	WNW 2
10	746.2	744.4	745.3	17.8	25.8	19.9	20.8	26.0	16.4	-	-	-	-	-	-	-	-	SSW 2	WSW 2	SSW 2
11	745.4	745.4	746.0	18.2	22.0	21.0	20.6	25.0	15.8	-	-	-	-	-	-	-	-	SW 1	NW 2	NNE 1
12	746.0	744.9	744.6	20.8	26.0	20.8	22.1	26.8	16.1	-	-	-	-	-	-	-	-	NNW 1	NNW 1	NE 1
13	744.1	742.8	743.7	20.5	27.8	21.4	22.8	28.9	17.6	-	-	-	-	-	-	-	-	W 2	WSW 3	NE 1
14	745.2	744.6	744.5	19.8	20.9	19.0	19.7	21.0	18.6	-	-	-	-	-	-	-	-	ENE 2	WSW 1	W 1
15	746.7	747.0	747.6	18.7	26.3	21.9	22.2	26.8	15.9	-	-	-	-	-	-	-	-	ENE 2	SE 2	NNW 1
16	748.0	747.1	746.8	20.6	27.7	23.1	23.6	28.8	18.4	-	-	-	-	-	-	-	-	NNW 1	WSW 3	WNW 2
17	746.1	744.8	744.8	21.3	29.2	23.6	24.4	29.5	18.4	-	-	-	-	-	-	-	-	WSW 2	WSW 3	ENE 2
18	743.8	743.3	743.9	20.2	22.6	16.8	19.1	23.7	16.8	-	-	-	-	-	-	-	-	ENE 2	NE 3	E 3
19	743.7	745.1	746.5	15.7	21.3	17.5	18.0	21.7	15.2	-	-	-	-	-	-	-	-	WNW 2	W 1	WNW 2
20	747.0	748.1	749.9	18.8	24.7	21.2	21.5	25.4	16.2	-	-	-	-	-	-	-	-	NNE 1	NE 3	NNE 2
21	751.0	750.9	751.1	19.4	27.5	23.1	23.3	28.5	17.3	-	-	-	-	-	-	-	-	SE 1	ENE 2	N 2
22	751.0	750.4	749.5	21.4	29.2	24.0	24.6	29.4	18.8	-	-	-	-	-	-	-	-	NE 1	S 2	NNW 1
23	749.2	748.1	748.0	20.8	29.9	24.9	25.1	30.5	18.6	-	-	-	-	-	-	-	-	NNW 1	SSW 2	NNW 2
24	749.3	749.2	749.7	21.8	27.9	21.9	23.4	28.1	18.6	-	-	-	-	-	-	-	-	NNW 1	SE 2	WSW 1
25	750.9	750.7	751.6	21.3	26.9	22.3	23.2	27.0	18.6	-	-	-	-	-	-	-	-	SE 1	E 1	ENE 1
26	752.7	751.0	750.9	22.1	28.0	23.7	24.4	28.1	19.9	-	-	-	-	-	-	-	-	NW 1	SE 2	NNE 2
27	751.2	750.1	749.1	21.4	28.6	23.8	24.4	28.9	19.5	-	-	-	-	-	-	-	-	ESE 2	SE 2	ENE 1
28	748.9	747.5	746.6	21.1	29.5	25.8	25.6	30.5	20.0	-	-	-	-	-	-	-	-	E 2	SSE 2	ENE 2
29	747.6	747.8	748.1	21.5	23.0	18.1	20.4	26.3	17.2	-	-	-	-	-	-	-	-	ESE 1	E 3	N 1
30	746.0	743.0	741.6	18.0	23.8	19.0	19.4	24.5	16.5	-	-	-	-	-	-	-	-	ENE 1	ESE 2	ENE 3
MES. VRED.	748.1	747.5	747.7	18.4	24.3	20.1	20.7	25.2	16.1	-	-	-	-	-	-	-	-	1.5	2.1	1.8

BR. SI. 57 H_s = 157 m H_b = 162.5 m h_t = 6.0 m h_r = 2.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	6	09⊙	10●	02	07.0	03.2	01.0	.	$= 8^{30}\ 10^{30}, \bullet^{0-1} 8^{34} 9^{40} 13^{42}\ 14^{07}$
2	5	04⊙	05	02	04.7	06.4	01.0	.	$= n\text{-}9^{15}, \bullet^{tr-0} 18^{29}\ 18^{36}$
3	7	02⊙	04⊙	00	02.0	07.0	00.0	.	$= n\text{-}a$
4	5	00⊙	01⊙	01	00.7	12.6	.	.	$= n\text{-}n$
5	8	10	10●	10●	10.0	00.0	.	.	$= n\text{-}n, \bullet^{tr-0} 9^{50}\text{-}18^{30}, \bullet^{1} 18^{30}\text{-}n$
6	6	10	09	03	07.0	05.1	10.0	.	$= n\text{-}n$
7	5	10	09	08	09.0	01.0	00.1	.	$= n\text{-}n, \bullet^{tr} n, 8^{40}\text{-}9^{05}$
8	6	04⊙	09	09	07.3	06.0	00.1	.	$= n\text{-}n, \overset{\bullet}{\nabla}{}^{tr-1} 15^{46}\text{-}16^{33} i, \bullet^{0} 16^{46}\text{-}16^{24}$
9	9	00⊙	04⊙	10	04.3	09.1	00.9	.	$\overset{\bullet}{\nabla}{}^{2} n\text{-}d, \bullet^{tr} 16^{04}\text{-}16^{08}$
10	9	01⊙	07⊙	05	04.3	05.9	00.0	.	$\overset{\bullet}{\nabla}{}^{tr-0} 16^{30}\text{-}17^{35} i, \bullet^{0} n$
11	7	04⊙	07⊙	06	05.7	10.2	01.0	.	$F_{SW}\ 10^{44}\text{-}11^{55} i, 14^{10}\text{-}16$
12	6	10	08	10	09.3	05.7	.	.	$= n\text{-}8^{45} F_{WSW}\ 10^{44}\text{-}17^{30}, \bullet^{tr}\ 20^{15}$
13	8	08	09 ⚐	04	07.0	06.0	00.0	.	$= n\text{-}8^{30}, ⚐^{1}{}_{SW}\ 13^{34}\text{-}14^{05}, \bullet^{tr-0}\ 14^{15}\text{-}15^{28} i$
14	7	01⊙	01⊙	00	00.7	12.6	00.0	.	$= n\text{-}9^{15}$
15	6	07⊙	10	02	06.3	04.1	.	.	$F_{WSW}\ 8^{30}\text{-}11^{50}, 14^{30}\text{-}17^{10} i; \bullet^{tr}\ 13^{35}$
16	7	06⊙	09	10	08.3	07.0	00.0	.	$⚐^{0-1}{}_{NW-E}\ 11^{50}\ 13^{20}\ 19^{31}\text{-}19^{45}; F_{NNW}\ 12^{40}\text{-}12^{20}\ \bullet^{0} 12^{45}\ 13^{05}, \overset{\bullet}{\nabla}{}^{1} 12^{50}\text{-}13$
17	7	10●	10	10	10.0	01.3	03.6	.	$= n\text{-}10^{15}, \bullet^{tr-0} n\text{-}10^{20}, 15^{05}\text{-}n i, \overset{\bullet}{\nabla}{}^{2} 15^{15}\text{-}15^{30}, \blacktriangle^{0} 15^{40}\text{-}15^{15}, ⚐^{1} 14^{50}\text{-}16^{30}$
18	7	06⊙	06	01	04.3	11.8	09.5	.	$F_{NNE}\ n\text{-}a$
19	7	09	05⊙	03	05.7	10.4	.	.	$F_{NE}\ 7^{40}\text{-}10^{30}$
20	7	06⊙	03⊙	09	06.0	08.7	.	.	$= n\text{-}10^{30}, 17^{45}\text{-}n$
21	7	09	08⊙	09	08.7	06.6	.	.	$= n\text{-}10^{30}$
22	6	10●	10●	10	10.0	00.0	18.3	.	$= n\text{-}n, \overset{\bullet}{\nabla}{}^{1-2} 5^{03}\text{-}6^{04}, ⚐^{1} 5^{46}\text{-}6^{08}, 19^{28}\text{-}20^{15}; \bullet^{0-1} 6^{04}\text{-}n i$
23	8	05⊙	06	01	04.0	07.1	10.[illegible]	.	$\bullet^{tr-0} 16^{35}\text{-}17^{09}$
24	8	07	04⊙	00	03.7	10.6	00.1	.	
25	8	00⊙	01⊙	01	00.7	13.2	.	.	$= n\text{-}8^{30}, \oplus 13^{38}\text{-}17^{55}$
26	8	10	09⊙	01	06.7	01.6	.	.	$= n\text{-}5^{30}, \oplus 8^{30}\text{-}9^{45}$
27	6	10	10	10	10.0	00.1	.	.	$= n\text{-}n, \bullet^{0} 10^{45}\text{-}11^{20}\ \overset{\bullet}{\nabla}{}^{1} 21^{20}\text{-}22^{40}, ⚐^{0} 21^{32}$
28	8	05⊙	09	00	04.7	06.5	04.6	.	$= n\text{-}12^{15}, \bullet^{tr-0} 9^{45}\text{-}10^{05}$
29	8	00⊙	06⊙	03	03.0	10.5	00.5	.	$= n\text{-}9^{45}$
30	8	09	10⊙	09	09.3	04.6	.	.	
31	8	10●	07⊙	06	07.7	02.9	05.5	.	$= n\text{-}12^{30}, \bullet^{0-1} n\text{-}9^{45}, ⚐^{1} 15^{50}\text{-}16^{30}, \overset{\bullet}{\nabla}{}^{1} 15^{58}\text{-}16^{47}, \cap 16^{45}\text{-}17^{15}$
MES. VRED.		06.2	07.0	05.0	06.1	199.6	68.0		

1	7	01⊙	10	05	05.3	06.7	08.1	.	$= n\text{-}9^{30}, \bullet^{tr} n, 10^{15}$
2	6	10●	10●	04	08.0	01.9	00.2	.	$= n\text{-}n, \bullet^{tr-0} n\text{-}12^{50}, \overset{\bullet}{\nabla}{}^{0-2} 13^{55}\text{-}14^{57}, \blacktriangle^{0} 14^{06}, ⚐ 14^{30}\text{-}15^{15}$
3	6	10	06	02	06.0	05.0	16.9	.	$= n\text{-}10^{30}, \bullet^{tr} 6^{51}$
4	6	00⊙	03⊙	03	04.0	08.3	.	.	$= n\text{-}n$
5	8	00⊙	08	05	03.7	11.2	.	.	$= n\text{-}9^{15} F_{WSW}\ 14^{50}\text{-}16^{50} i$
6	8	05⊙	06⊙	03	06.7	10.2	.	.	$= n\text{-}9^{30}$
7	7	10	10	10	10.0	01.2	.	.	
8	7	09	07	06	07.3	05.2	11.7	.	$= n\text{-}n, \bullet^{0-2} n\text{-}6^{30}, ⚐^{1} n\text{-}a$
9	6	10	10	09	09.7	02.2	.	.	$= n\text{-}n, \bullet^{tr-0} 7^{25}\text{-}7^{50}\ 14^{34}\text{-}15^{15} i; ⚐^{0} 14^{59}\text{-}15^{20}$
10	8	09	04⊙	10	07.7	06.4	00.8	.	$= n\text{-}7^{45}, ⚐^{0}{}_{W-NW}\ 14^{34}, \overset{\bullet}{\nabla}{}^{0} 14^{35}, \bullet^{tr} 17^{04}, F_{NNW}\ 17^{25}\text{-}17^{35}$
11	8	09	08	04	07.0	06.4	00.0	.	$\bullet^{tr-0} 11^{34}\text{-}12^{40}$
12	8	04⊙	04⊙	04	04.0	11.1	00.0	.	$\overset{\bullet}{\nabla}{}^{0} 12^{57}\text{-}13^{04}$
13	8	05⊙	01⊙	01	02.3	12.7	00.0	.	$= n\text{-}9^{15}$
14	7	07⊙	10	10	09.0	01.9	.	.	$\bullet^{tr-0} 8^{50}\text{-}9^{30}, T\ 7^{45}\text{-}9^{45}$
15	6	00⊙	05⊙	03	05.7	08.5	00.4	.	$= n\text{-}n$
16	6	05⊙	03⊙	05	04.3	11.5	.	.	$= n\text{-}n$
17	8	07⊙	04⊙	10	07.0	06.2	.	.	$= n\text{-}10^{45}$
18	6	09	10	10● ⚐	09.7	01.1	.	.	$= n\text{-}n, ⚐^{1}{}_{S-SW}\ n, 15^{10}\text{-}15^{30}, 19^{05}\text{-}n; \bullet^{tr} 9^{35}\text{-}a, 15^{15}\text{-}15^{50}, 18^{30}\text{-}18^{45}, \overset{\bullet}{\nabla}{}^{1} 19^{48}\text{-}n$
19	6	10●	09	10	09.7	00.9	00.8	.	$= n\text{-}n, \bullet^{tr} 7^{20}\text{-}n i$
20	6	04⊙	03⊙	00	02.3	13.0	00.3	.	$= n\text{-}13^{30}$
21	8	00⊙	01⊙	01	00.7	13.8	.	.	
22	6	00⊙	01⊙	03	01.3	13.1	.	.	$= n\text{-}16^{30}$
23	8	00⊙	01⊙	04	01.7	13.7	.	.	$= n\text{-}9^{45}$
24	7	00⊙	02⊙	10	04.0	10.2	.	.	$= n\text{-}11^{15}\ 18^{30}\text{-}n$
25	6	07⊙	09	09	08.3	07.5	.	.	$= n\text{-}n, \bullet^{tr-0} 12^{50}\text{-}13^{06}, ⚐^{0} 13^{22}\text{-}13^{50}$
26	6	00⊙	05⊙	01	02.0	01.6	00.1	.	$= n\text{-}15^{45}$
27	6	05⊙	04⊙	01	03.3	12.7	.	.	$= n\text{-}n$
28	6	00⊙	01⊙	03	01.3	11.9	.	.	$= n\text{-}15^{15}\ 19\text{-}n$
29	6	05⊙	10●⚐	10	08.3	05.2	.	.	$= n\text{-}14^{30}, \overset{\bullet}{\nabla}{}^{0-1} 13^{45}\text{-}15^{06} i, \bullet^{tr-0} 14^{20}\text{-}15^{57} i, ⚐^{0-1} 13^{52}\text{-}16^{30} i, F\ 14^{45}\text{-}14^{25}$
30	7	08	09	09	08.7	06.7	09.9	.	
MES. VRED.		05.0	06.1	05.6	05.6	235.1	77.4		

VIDLJIVOST OSMATRANA U 13 ČASOVA

$\varphi = 45^\circ\ 49'$ N $\lambda = 15^\circ\ 59'$ E Gr. $\Delta G =$ + 1h 04 min. BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	744.4	744.5	744.5	14.4	18.6	15.5	16.0	19.6	13.0	-	-	-	-	-	-	-	-	WSW 2	ENE 1	W 2
2	744.0	742.6	742.2	14.2	23.5	21.1	20.0	24.3	12.1	-	-	-	-	-	-	-	-	WNW 1	ESE 2	ENE 2
3	746.9	747.5	747.6	13.1	14.7	15.2	14.6	21.0	13.0	-	-	-	-	-	-	-	-	E 1	WNW 2	NNW 1
4	748.0	748.6	750.0	14.0	14.7	12.7	13.5	15.2	12.7	-	-	-	-	-	-	-	-	NW 1	NNE 2	NW 1
5	750.6	750.1	751.3	13.4	22.0	17.9	17.8	22.4	12.0	-	-	-	-	-	-	-	-	NNW 1	NNE 4	NNE 2
6	751.7	750.6	750.5	17.4	24.1	20.4	20.6	24.7	14.2	-	-	-	-	-	-	-	-	N 1	NNE 3	NNE 2
7	749.5	747.8	747.1	17.4	24.8	21.2	21.2	25.8	16.9	-	-	-	-	-	-	-	-	SSW 1	ENE 2	NNE 1
8	746.3	745.4	745.0	19.8	27.7	22.6	23.2	28.0	18.1	-	-	-	-	-	-	-	-	ENE 1	S 2	NE 1
9	745.4	744.5	745.8	20.7	28.7	24.6	24.6	29.5	18.3	-	-	-	-	-	-	-	-	ENE 1	SSE 2	NW 1
10	749.2	749.7	750.7	20.5	28.3	24.1	24.2	28.8	18.5	-	-	-	-	-	-	-	-	WNW 1	E 2	NNE 2
11	750.9	749.4	749.0	21.4	29.6	25.2	25.4	30.1	19.4	-	-	-	-	-	-	-	-	ENE 1	S 2	NNE 2
12	751.3	750.7	750.5	22.2	28.4	24.1	24.7	29.0	20.3	-	-	-	-	-	-	-	-	ESE 1	NE 2	NNE 2
13	751.7	750.2	748.8	21.6	27.7	24.5	24.6	28.9	20.5	-	-	-	-	-	-	-	-	E 1	ESE 2	SSE 1
14	746.9	743.8	741.3	21.0	30.0	24.6	25.0	30.5	19.4	-	-	-	-	-	-	-	-	ESE 1	S 2	WSW 2
15	736.8	736.2	742.8	21.9	22.3	11.6	16.8	27.9	11.6	-	-	-	-	-	-	-	-	WNW 2	ENE 4	SSW 2
16	742.9	742.8	742.7	10.0	13.6	13.0	12.4	15.3	09.6	-	-	-	-	-	-	-	-	WSW 2	NW 1	NNW 2
17	743.3	743.8	745.5	12.3	16.3	14.8	14.6	18.0	11.3	-	-	-	-	-	-	-	-	WNW 2	WSW 2	NW 1
18	745.9	746.5	745.9	13.7	19.1	15.7	16.0	20.2	13.3	-	-	-	-	-	-	-	-	W 1	NNW 1	NNE 2
19	744.1	742.7	742.8	14.0	24.2	18.3	18.7	25.2	11.6	-	-	-	-	-	-	-	-	WNW 2	WSW 2	WSW 2
20	742.6	742.6	742.4	16.8	23.1	19.8	19.9	24.0	14.3	-	-	-	-	-	-	-	-	W 2	WSW 4	WNW 2
21	745.9	746.7	747.2	20.5	26.2	22.1	22.7	27.0	18.7	-	-	-	-	-	-	-	-	WNW 2	WSW 3	NNW 2
22	749.0	748.2	748.2	19.8	28.6	25.0	24.6	29.6	17.3	-	-	-	-	-	-	-	-	S 1	SSW 2	NNE 2
23	749.8	749.3	748.8	22.4	30.0	26.0	26.1	30.3	19.0	-	-	-	-	-	-	-	-	WNW 2	SSE 2	NNE 2
24	749.4	747.1	745.3	21.3	29.7	2[illegible].5	25.5	30.0	18.9	-	-	-	-	-	-	-	-	W 1	S 2	NE 2
25	741.3	743.5	745.4	22.6	17.9	15.8	18.0	27.9	15.8	-	-	-	-	-	-	-	-	E 1	N 4	WNW 2
26	746.2	747.3	748.2	14.5	21.8	18.2	18.2	23.1	12.4	-	-	-	-	-	-	-	-	NW 1	E 2	NNE 2
27	749.4	748.8	750.1	15.5	25.5	22.5	21.5	26.5	13.5	-	-	-	-	-	-	-	-	ENE 1	SSW 2	NE 2
28	751.6	750.7	749.9	20.4	26.8	23.3	23.4	28.0	18.6	-	-	-	-	-	-	-	-	NE 1	SSE 2	NE 2
29	749.4	748.5	748.2	21.5	28.3	24.1	24.5	28.8	20.0	-	-	-	-	-	-	-	-	ENE 1	SSE 2	NE 2
30	750.4	750.8	751.0	21.2	26.7	24.1	24.0	28.0	19.1	-	-	-	-	-	-	-	-	NNE 1	ENE 2	NNE 2
31	751.4	751.0	751.1	21.9	28.7	23.5	24.4	28.8	19.9	-	-	-	-	-	-	-	-	ENE 1	SSE 2	NE 2
MES. VRED.	747.3	746.9	747.1	18.1	24.2	20.5	20.9	25.8	15.9	-	-	-	-	-	-	-	-	1.2	2.2	1.8

1	750.9	750.0	750.3	20.6	26.9	22.8	23.3	28.9	19.6	-	-	-	-	-	-	-	-	NNW 1	NNW 2	NNE 1
2	749.7	748.1	747.6	20.3	27.1	23.1	23.4	27.7	18.5	-	-	-	-	-	-	-	-	ENE 1	ESE 2	NNE 2
3	747.4	746.0	745.7	19.1	27.2	22.9	23.0	27.2	18.7	-	-	-	-	-	-	-	-	NE 1	ESE 2	NE 1
4	746.2	745.7	747.2	20.5	28.6	23.0	23.8	29.1	18.5	-	-	-	-	-	-	-	-	NNW 1	SSW 2	ENE 1
5	748.5	748.3	748.8	20.4	29.2	25.1	25.0	30.2	18.7	-	-	-	-	-	-	-	-	ESE 1	SSW 2	NE 1
6	748.8	748.0	747.2	21.8	31.0	27.5	27.0	32.0	20.0	-	-	-	-	-	-	-	-	WNW 1	WSW 2	NW 2
7	746.6	745.7	746.6	21.7	30.7	21.3	23.8	32.0	20.5	-	-	-	-	-	-	-	-	SW 1	WNW 2	NNW 2
8	745.1	744.8	743.2	20.0	27.9	24.1	24.0	28.2	18.8	-	-	-	-	-	-	-	-	WNW 2	ENE 2	NNE 2
9	741.5	740.4	741.0	17.0	20.4	18.3	18.5	24.1	14.0	-	-	-	-	-	-	-	-	NW 3	NNE 1	WNW 2
10	742.7	743.6	744.1	17.7	19.2	18.3	18.4	20.8	16.2	-	-	-	-	-	-	-	-	WSW 1	S 1	W 2
11	745.3	745.9	746.6	17.8	21.0	17.9	18.6	22.0	16.2	-	-	-	-	-	-	-	-	W 2	SSW 2	W 2
12	749.4	750.2	749.6	16.6	23.0	18.8	19.3	23.0	14.8	-	-	-	-	-	-	-	-	WNW 1	SE 2	N 2
13	750.6	750.9	751.4	18.2	22.6	19.0	19.7	23.0	16.6	-	-	-	-	-	-	-	-	NE 3	E 2	NNE 2
14	750.0	749.3	749.7	17.6	26.0	22.6	22.2	26.9	16.5	-	-	-	-	-	-	-	-	- 0	S 2	NNE 1
15	749.6	748.2	747.3	20.2	28.2	23.1	23.6	28.4	19.6	-	-	-	-	-	-	-	-	NW 1	SSE 2	NNW 2
16	747.6	745.9	744.3	18.4	25.7	22.5	22.3	26.0	16.9	-	-	-	-	-	-	-	-	NW 1	S 2	NE 1
17	742.6	741.0	743.2	19.8	23.6	19.1	20.4	26.0	19.1	-	-	-	-	-	-	-	-	NE 1	NW 2	ENE 1
18	746.9	746.2	745.9	16.4	21.7	17.7	18.4	21.8	15.3	-	-	-	-	-	-	-	-	ENE 2	S 2	NNE 2
19	746.1	745.6	745.5	16.9	23.5	21.7	21.0	24.4	15.9	-	-	-	-	-	-	-	-	NE 1	ESE 2	NNE 2
20	745.1	744.0	743.2	19.1	27.9	24.2	23.6	27.4	18.5	-	-	-	-	-	-	-	-	ENE 1	ESE 2	NNE 2
21	741.5	741.0	740.5	20.9	25.1	21.4	22.2	26.1	20.4	-	-	-	-	-	-	-	-	ENE 1	WSW 2	WNW 2
22	742.1	743.8	745.7	17.4	19.0	17.9	18.0	21.8	15.4	-	-	-	-	-	-	-	-	W 1	NNE 3	ENE 1
23	745.8	745.3	744.7	16.0	20.0	17.0	17.5	21.2	14.7	-	-	-	-	-	-	-	-	N 1	SSW 1	NNW 1
24	743.7	743.0	744.3	15.6	19.2	15.2	15.3	17.0	14.1	-	-	-	-	-	-	-	-	NNE 1	ENE 1	NNE 2
25	746.6	747.7	750.0	15.6	21.8	19.1	18.4	22.8	14.2	-	-	-	-	-	-	-	-	NW 3	NNW 2	ENE 1
26	751.5	751.4	752.0	14.6	22.1	17.3	17.8	22.1	13.3	-	-	-	-	-	-	-	-	WNW 1	S 1	NNE 1
27	752.3	751.3	751.2	14.3	23.0	18.8	18.7	23.2	13.3	-	-	-	-	-	-	-	-	S 1	S 1	NNE 2
28	750.0	749.3	748.8	15.8	23.7	19.9	19.6	22.8	15.4	-	-	-	-	-	-	-	-	E 1	ESE 2	NNE 2
29	748.5	748.4	749.1	16.9	25.0	18.7	19.8	25.1	16.5	-	-	-	-	-	-	-	-	NE 1	SSW 3	W 2
30	747.8	747.6	747.7	16.7	21.0	18.0	18.4	21.1	16.6	-	-	-	-	-	-	-	-	NE 1	ESE 2	NNE 2
31	747.6	747.8	748.2	18.0	21.1	19.0	19.3	21.5	17.0	-	-	-	-	-	-	-	-	ENE 1	NNE 3	NNE 1
MES. VRED.	747.0	746.6	746.8	18.1	24.1	20.5	20.8	25.0	16.9	-	-	-	-	-	-	-	-	1.2	1.9	1.6

BR. ST. 57 H_B = 157 m H_b = 162.5 m h_t = 6.0 m h_r = 2.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	5	10	06	00	05.3	02.3	35.4	.	∇1-2 n, ●tr n-6^30, R^1 n
2	8	00⊙	07⊙	10	05.7	11.2	.	.	F NE 23^40 n
3	7	10●	10	10	10.0	00.0	04.0	.	●3 n-7^25 F NE n-0^50
4	6	10●	10	10	10.0	00.0	00.7	.	= n-17, ●0-1 5^40-21^30 i
5	5	10	03⊙	01	04.7	08.6	05.6	.	● n, = n-9, F 12^34-14
6	8	00⊙	04⊙	01	01.7	13.3	.	.	= n-n
7	6	00⊙	04⊙	00	01.3	13.5	.	.	= n-n
8	7	00⊙	00⊙	00	01.0	10.0	.	.	= n-n
9	7	00⊙	00⊙	03	02.0	09.2	.	.	= n-15^45 19^30-n, ∮^0 20^30-n
10	5	05	02⊙	01	03.0	12.8	.	.	= n-12^36
11	7	00⊙	01⊙	01	00.7	13.9	.	.	= n-11
12	8	01⊙	01⊙	01	01.3	12.8	.	.	= n-14^45 18^45-n
13	6	04	06⊙	01	04.7	11.9	.	.	= n-11, 18^30-n
14	7	00⊙	00⊙	06	02.0	12.1	.	.	F 13^30-16^20, R^0 14^40-20^45 i, ●0 14^50-ni, ∇ 15^54-16^32, = 18^30-n
15	7	00⊙	03	10●	09.3	06.9	.	.	
16	6	10⊙	10⊙	10●	10.0	00.4	35.2	.	= n-n, ●tr-0-1 n-14^45 18^50-21^30 i; R^0 9^03-9^40 i
17	8	10⊙	10	10	10.0	00.5	18.2	.	●tr-0 n-15^30, 18^38-18^54
18	8	10	10	06	09.7	02.7	00.0	.	
19	8	09	02⊙	00	03.7	11.2	.	.	
20	5	00⊙	05	09	05.7	10.1	.	.	F SW 10^40-17^30, = 19^45-n
21	7	02⊙	06	00	07.3	10.1	.	.	= n-9^30
22	5	00⊙	00⊙	00	00.0	12.9	.	.	= n-10^30 20-n
23	7	00⊙	00⊙	01	00.3	13.0	.	.	= n-8^45 R^1 p-n, F-F p-n
24	6	00⊙	01⊙	02	01.0	13.3	.	.	= n-14^36
25	8	08	10●R	01	04.3	05.6	.	.	= n-12^30, F 11^08-13^40 i, R^0-1 11^50-15^15 i, ●0-1 13^40-14^30
26	5	02	04⊙	01	04.3	08.5	00.5	.	= n-10^15
27	8	03⊙	06⊙	02	03.7	12.3	.	.	
28	6	08	06⊙	02	05.3	12.2	.	.	
29	7	00⊙	02⊙	01	01.0	13.2	.	.	
30	6	00⊙	04⊙	00	01.3	12.3	.	.	= n-12^45, 15^30-n
31	6	02⊙	05⊙	03	04.7	09.1	.	.	= n-n
MES. VREDN.			04.5	04.9	03.3	04.2	233.9	100.0	

1	6	00⊙	09⊙	09	06.0	06.5	.	.	= n-n, ∇tr 12^30-12^35, R^0 13-17^40 i
2	6	02⊙	07⊙	06	04.3	08.7	00.0	.	= n-n
3	7	00⊙	06⊙	05	03.7	07.9	.	.	= n-12^30
4	7	00⊙	07⊙	00	02.7	08.4	.	.	= n-11^30, 17^30-n
5	6	00⊙	01⊙	02	01.0	11.6	.	.	= n-n
6	5	09	00⊙	00	02.7	10.9	.	.	= n-n
7	6	00⊙	06⊙	10●R	05.3	09.7	.	.	= n-n, ●tr-1 20^02-22 i, ∇ 20^42-20^56
8	7	09	02	01	04.0	10.3	17.8	.	= n-11^45 16^45-n
9	6	10●R	09	04	07.7	03.3	00.0	.	● ∇▲ n-5^40 ●0-1 5^40-11^30 = n-14^45 R^1-2 n-8^45 F 4^50-5
10	6	09	10●R	10	09.7	01.9	24.7	.	= n-n, ∇ ● n, ●0 12^45-16^14, 21^25-n; ∇ 19^03-19^45, R 19^44-20^45
11	6	10	10	10●	10.0	02.2	11.0	.	●tr-0 n-6^30, 19^06-22^45, = n-n, T 18^52, R^0-1 19^45-19^50
12	7	09	05⊙	07	07.0	07.7	00.0	.	= n-10^45, ●tr n-6^45, 9^05-9^20
13	6	09	02⊙	00	03.7	09.3	00.2	.	= n-n
14	6	00⊙	01⊙	01	00.7	11.6	.	.	= n-n
15	6	01⊙	05⊙	09R	05.0	08.4	.	.	= n-n, ●tr 17^05-17^20, T0-1 16^45-21^45 i
16	7	00⊙	03⊙	06	03.0	11.2	00.0	.	= n-12^30 ⊕ 15^55-16^30
17	7	07	09R	10●	09.7	04.8	.	.	= n-n, ●0-1 12^28-16^26, 19^02-n; R^0-1 13^30-16^30, T 18^20-19^35
18	8	06⊙	01⊙	01	02.7	11.5	00.0	.	
19	8	00⊙	00⊙	01	00.3	12.2	.	.	= n-11^30 19^45-n
20	7	00⊙	00⊙	00	00.0	12.2	.	.	= n-12^45, 18^50-n
21	6	05⊙	09⊙	05R	07.3	07.1	.	.	= n-n, ∮ 19^35-ni, R^0-1 20^04-21^30, ●tr 22^05-22^19
22	7	00⊙	09	09	06.0	05.7	00.0	.	= n-10^30
23	5	01⊙	09⊙	10●	06.7	08.1	.	.	= n-n, ●tr-0 11^58-13^45, 18^45-21^30; R^0 18^43-19^30
24	6	10●	10●	10	10.0	00.0	13.0	.	= n-n, ●0-1 n-n
25	8	09	08⊙	10	09.0	06.3	10.4	.	
26	7	05⊙	05⊙	00	03.7	10.3	.	.	= n-9^45
27	6	04	02	02	04.7	10.1	.	.	= n-14^30 18^45-n
28	6	09	09⊙	10	09.3	01.5	.	.	= n-n, ●tr 16^47-16^33
29	7	10	08⊙	10●	09.3	05.6	00.0	.	= n-11^30 17^45-n; ●tr 16^23-19^19 i
30	6	10●	10	10●	10.0	04.6	06.4	.	= n-n, ●tr-1 n-7^50 14^50-n
31	5	10●	10	07	09.0	00.2	20.2	.	= n-n, ●tr-0-1 n-7^30, 11^37-n
MES. VREDN.			04.9	06.0	05.7	05.0	22.7	174.5	

VIDLJIVOST OSMATRANA U 13 ČASOVA

1970 SEPTEMBAR ZAGREB GRIČ

φ = 45° 49' N λ = 15° 59' E Gr. ΔG = + 1h 04 min. BR. ST. 57

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21
1	747.5	746.7	747.0	16.0	23.9	19.1	**19.5**	24.0	15.1	-	-	-	-	-	-	-	-	NNW 1	S 2	N 1
2	749.3	749.0	748.5	16.9	23.8	19.0	**19.7**	24.0	16.6	-	-	-	-	-	-	-	-	NNW 1	SSE 2	NNE 1
3	747.9	747.4	747.0	15.4	25.0	20.1	**20.2**	25.5	14.5	-	-	-	-	-	-	-	-	WSW 1	S 2	ENE 1
4	749.5	749.4	751.3	16.8	23.0	16.3	**18.1**	24.4	16.2	-	-	-	-	-	-	-	-	WNW 2	SSW 2	NE 2
5	749.7	748.4	748.1	14.3	23.0	19.9	**19.3**	24.0	14.2	-	-	-	-	-	-	-	-	SW 1	SSW 2	NNE 2
6	748.3	748.0	749.0	17.9	22.2	19.3	**19.7**	22.4	17.7	-	-	-	-	-	-	-	-	NE 2	ENE 2	NNE 1
7	752.4	752.7	751.6	14.1	19.2	14.8	**15.5**	19.3	14.1	-	-	-	-	-	-	-	-	NE 2	ENE 2	NNE 2
8	750.1	748.7	746.7	13.0	22.9	20.2	**19.1**	24.3	11.9	-	-	-	-	-	-	-	-	E 1	S 2	W 2
9	748.1	746.9	746.6	18.8	26.1	20.9	**21.7**	26.6	17.6	-	-	-	-	-	-	-	-	NE 1	SSW 3	WNW 2
10	746.1	745.4	745.2	19.4	28.1	23.0	**23.4**	28.2	18.0	-	-	-	-	-	-	-	-	WSW 2	SW 4	WNW 2
11	745.4	744.4	744.1	18.9	29.1	22.8	**23.4**	29.6	18.6	-	-	-	-	-	-	-	-	WSW 2	WSW 3	WSW 1
12	744.3	744.0	743.5	19.3	27.2	22.2	**22.7**	27.6	18.5	-	-	-	-	-	-	-	-	ENE 2	WNW 1	NNE 2
13	742.4	744.4	747.7	18.8	21.7	17.9	**19.1**	22.2	17.9	-	-	-	-	-	-	-	-	E 1	ENE 3	NNE 2
14	749.4	748.1	748.4	17.0	22.1	17.6	**18.6**	22.3	15.6	-	-	-	-	-	-	-	-	NE 2	ENE 2	N 2
15	748.9	747.5	747.3	14.4	23.1	19.1	**18.9**	23.2	13.8	-	-	-	-	-	-	-	-	ENE 1	SSE 2	NNE 1
16	746.9	746.5	749.9	14.8	25.4	16.1	**18.1**	25.6	13.9	-	-	-	-	-	-	-	-	N 1	WSW 1	NE 2
17	754.5	755.6	755.7	13.7	15.9	15.0	**14.9**	16.1	13.2	-	-	-	-	-	-	-	-	N 1	NE 1	ENE 2
18	755.5	755.3	755.2	13.6	17.8	15.9	**15.8**	18.2	13.6	-	-	-	-	-	-	-	-	NE 2	NE 2	NNE 2
19	754.9	753.9	754.1	12.8	20.9	15.9	**16.4**	21.1	12.8	-	-	-	-	-	-	-	-	ENE 1	ENE 1	NNE 2
20	752.9	751.8	752.1	13.1	22.4	18.3	**18.0**	22.4	12.9	-	-	-	-	-	-	-	-	NNE 1	SE 2	N 2
21	751.3	751.2	750.7	14.9	17.9	15.1	**15.8**	18.3	14.8	-	-	-	-	-	-	-	-	NE 1	ESE 1	WNW 2
22	750.9	752.1	753.4	14.4	16.1	14.7	**15.0**	16.6	11.8	-	-	-	-	-	-	-	-	ENE 1	ENE 1	NE 2
23	753.4	751.6	752.2	10.3	17.1	12.9	**13.3**	17.8	10.2	-	-	-	-	-	-	-	-	E 1	SE 2	NNE 2
24	753.6	752.5	753.0	08.2	17.3	12.8	**12.8**	17.5	08.2	-	-	-	-	-	-	-	-	ESE 1	SE 2	NNE 2
25	752.5	751.6	751.4	08.0	17.2	14.4	**13.5**	17.9	07.7	-	-	-	-	-	-	-	-	ENE 1	SSW 2	N 1
26	750.8	749.8	753.0	10.0	18.6	12.5	**13.4**	19.4	09.5	-	-	-	-	-	-	-	-	ENE 1	ESE 2	ENE 2
27	756.9	757.7	757.5	10.8	14.1	09.7	**11.1**	14.7	10.7	-	-	-	-	-	-	-	-	NNE 1	ESE 1	NNE 1
28	759.4	759.8	760.8	06.3	15.2	11.3	**11.0**	15.5	05.9	-	-	-	-	-	-	-	-	NNW 1	ENE 2	N 2
29	761.2	759.3	758.2	06.4	13.3	08.9	**09.4**	13.5	06.2	-	-	-	-	-	-	-	-	NE 1	SSE 2	NNE 2
30	754.5	750.7	747.3	04.3	14.6	12.1	**10.8**	15.5	03.8	-	-	-	-	-	-	-	-	NE 1	SSE 2	N 1
MES. VRED.	751.0	750.3	750.6	13.8	20.8	16.6	**16.9**	21.2	13.2	-	-	-	-	-	-	-	-	1.3	1.9	1.7

1970 OKTOBAR ZAGREB GRIČ

1	743.9	741.8	743.6	11.0	13.3	11.4	**11.8**	13.5	08.9	-	-	-	-	-	-	-	-	W 2	SE 1	E 1
2	745.9	742.8	738.4	07.0	15.1	12.9	**12.2**	16.3	06.9	-	-	-	-	-	-	-	-	SSE 1	SSW 3	WSW 2
3	740.4	740.8	742.7	08.8	12.7	08.4	**09.6**	12.9	08.8	-	-	-	-	-	-	-	-	S 2	SSW 2	NE 1
4	743.2	743.8	747.5	06.0	15.4	10.3	**10.5**	16.1	05.8	-	-	-	-	-	-	-	-	WSW 2	W 2	N 1
5	749.0	747.5	747.9	07.1	13.1	10.8	**10.4**	15.0	06.0	-	-	-	-	-	-	-	-	W 1	S 1	ESE 1
6	747.3	746.8	747.5	09.0	20.4	14.4	**14.6**	21.0	08.0	-	-	-	-	-	-	-	-	WSW 2	WSW 2	WSW 3
7	747.3	746.9	748.0	11.8	20.7	15.2	**15.7**	20.9	11.8	-	-	-	-	-	-	-	-	WSW 2	WSW 4	WSW 2
8	749.4	749.2	750.5	12.9	22.7	17.2	**17.5**	22.9	11.7	-	-	-	-	-	-	-	-	WNW 2	WSW 4	WSW 2
9	751.6	751.2	752.2	13.5	22.6	19.4	**18.7**	22.9	12.8	-	-	-	-	-	-	-	-	WNW 1	S 2	NNE 2
10	753.3	753.5	754.5	13.4	22.0	18.5	**18.1**	22.6	13.4	-	-	-	-	-	-	-	-	NE 1	SSW 1	NNE 2
11	756.2	755.9	756.5	12.8	19.8	16.0	**16.2**	20.5	12.8	-	-	-	-	-	-	-	-	NE 1	ESE 1	NNE 3
12	757.1	756.5	756.3	12.2	15.8	13.8	**13.9**	16.0	11.9	-	-	-	-	-	-	-	-	- 0	ESE 2	ENE 1
13	756.2	754.9	753.7	11.4	13.8	12.2	**12.4**	13.9	11.0	-	-	-	-	-	-	-	-	SSE 1	ENE 1	SSW 1
14	751.8	751.5	752.3	11.8	13.1	11.8	**12.1**	14.1	11.3	-	-	-	-	-	-	-	-	NNW 1	SSE 1	ENE 2
15	753.0	753.2	755.8	09.1	11.1	06.5	**08.3**	11.8	09.1	-	-	-	-	-	-	-	-	NE 1	NNE 2	NNE 2
16	757.4	757.5	759.0	03.9	09.0	05.6	**06.0**	09.6	03.6	-	-	-	-	-	-	-	-	NNE 3	ENE 3	NNE 2
17	758.3	756.9	756.5	03.4	08.8	07.0	**06.6**	09.0	02.6	-	-	-	-	-	-	-	-	ENE 1	ENE 3	NE 1
18	754.9	753.9	754.5	05.9	09.8	04.9	**06.4**	10.2	05.6	-	-	-	-	-	-	-	-	ENE 1	ESE 2	N 1
19	752.3	747.5	743.6	01.0	10.1	07.8	**06.7**	11.0	00.9	-	-	-	-	-	-	-	-	SSE 1	SSW 1	NE 1
20	738.7	734.2	733.0	04.6	14.2	12.0	**10.7**	16.9	03.2	-	-	-	-	-	-	-	-	ENE 1	NNE 1	NNW 2
21	739.1	742.0	744.2	03.6	09.8	07.3	**07.0**	12.0	03.3	-	-	-	-	-	-	-	-	WNW 1	SSW 2	ENE 1
22	746.6	747.8	748.3	06.0	08.4	05.7	**06.4**	08.6	05.7	-	-	-	-	-	-	-	-	N 1	SSE 2	N 1
23	747.6	747.1	750.0	02.3	09.0	05.3	**05.5**	09.2	02.2	-	-	-	-	-	-	-	-	SW 1	SSE 2	WNW 2
24	754.0	754.8	757.1	04.4	08.8	03.7	**05.2**	09.1	03.7	-	-	-	-	-	-	-	-	SSE 1	NNE 2	NNW 1
25	755.0	754.2	754.2	02.4	12.0	09.0	**08.1**	12.3	01.7	-	-	-	-	-	-	-	-	SW 2	SSW 2	NNW 1
26	753.6	751.8	751.5	03.8	14.1	09.3	**09.1**	14.2	03.8	-	-	-	-	-	-	-	-	NE 1	SSW 2	W 2
27	752.4	753.3	756.6	05.2	14.1	11.0	**10.3**	14.5	05.2	-	-	-	-	-	-	-	-	NE 1	ESE 1	NE 3
28	757.6	755.1	753.9	08.7	12.3	09.0	**09.8**	12.5	08.7	-	-	-	-	-	-	-	-	NE 1	SSE 1	W 2
29	751.6	752.7	757.0	11.8	17.3	10.9	**12.7**	17.3	07.4	-	-	-	-	-	-	-	-	WNW 4	WSW 3	ENE 2
30	756.9	754.3	753.1	06.5	14.5	12.6	**11.6**	15.3	06.5	-	-	-	-	-	-	-	-	NW 1	SW 2	WNW 3
31	751.9	751.5	752.9	12.4	17.8	12.9	**14.0**	17.8	11.1	-	-	-	-	-	-	-	-	WNW 3	WNW 3	WNW 3
MES. VRED.	750.8	750.0	750.7	07.9	14.3	10.7	**10.9**	14.8	07.3	-	-	-	-	-	-	-	-	1.4	2.0	1.7

ZAGREB GRIČ — 1970 SEPTEMBAR

BR. ST. 57 — H_s = 157 m H_b = 162.5 m h_t = 6.0 m h_r = 2.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	5	00⊙	09⊙	08	04.3	08.2	00.2	.	= n-n
2	6	06	06⊙	00	04.0	09.6	00.5	.	= n-n, ●°n
3	8	02⊙	00⊙	01	01.0	09.8	.	.	= n-11^30 17^30 n
4	7	10	07⊙	01	06.0	04.2	02.4	.	= n-11^30, ●^tr-0 n-6^40 15^54-17^15, ▽^2 16^04 16^19
5	7	10≡	08⊙	02	06.7	02.6	03.4	.	≡^1 n-7^36, ≡ 17^30-8^45, = 8^45-12^45 18^15-n
6	6	10	09⊙	09	09.3	03.9	.	.	= 9^45-n, ●^tr 15^50-16^03
7	7	10●	04⊙	01	05.0	03.8	00.5	.	= n-12^15, ●^0-1 6^38-7^28
8	6	00⊙	01⊙	00	00.3	10.5	00.3	.	= n-n
9	6	03⊙	01⊙	01	01.7	10.3	.	.	= n-14^45
10	7	00⊙	00⊙	00	00.0	10.7	.	.	= n-13^15
11	7	01⊙	01⊙	01	01.0	10.8	.	.	= n-11^45
12	6	08	05⊙	00	04.3	05.6	.	.	= n-n
13	9	10	04⊙	08	07.3	05.6	00.4	.	= n-n, ●°n-a, 11^38
14	9	09	01⊙	00	03.3	09.5	.	.	= 18^15-n
15	7	00⊙	01⊙	00	00.3	11.0	.	.	= n-11^30
16	6	00⊙	03⊙	09	04.0	07.4	.	.	= n-11^30 ●^tr-1 15^09 ni, ▽^0-2 17^39-18^24 i, ▲^2 17^45-17^55
17	6	10	10	10	10.0	00.0	16.9	.	= n-9^30 ●^tr-0 n, 8^05, 9^24, 15^37-15^50
18	6	10	09⊙	05	06.3	01.5	00.1	.	●^tr 6^30-6^56 9^30, = 16^30-n
19	6	07⊙	00⊙	00	02.3	08.8	.	.	= n-ni
20	6	01⊙	01⊙	10	04.0	06.8	.	.	= n-n
21	6	08	10	08	08.7	00.0	.	.	= n-n
22	6	10	10	08	09.3	00.1	00.0	.	●^tr n
23	6	08	01⊙	00	03.0	09.0	.	.	= n-14^15, 18^30 n
24	6	01⊙	03⊙	00	01.3	08.2	.	.	= n-n
25	6	00⊙	01⊙	10	03.7	09.9	.	.	= n-n
26	6	01⊙	05⊙	10●	05.3	05.8	.	.	= n-n, ●^0-1 18^30-n
27	7	10	09	00	06.3	01.2	08.5	.	
28	7	03⊙	02⊙	00	01.7	08.0	.	.	= n-12^15
29	7	00⊙	01⊙	00	00.3	09.9	.	.	= n-10^15
30	7	00⊙	01⊙	09	03.3	09.5	.	.	= n-13^30, 17^45-n
MES. VREDN.		04.9	03.8	03.7	04.1	202.2	38.2		

ZAGREB GRIČ — 1970 OKTOBAR

1	5	10●	10●	09	09.7	00.0	07.5	.	= n-7^45 10^45-n, ●^0-1 5^53-11^30 13^40 18^45 i; ≡^0-1 7^45-10^45
2	7	01⊙	09	09	06.3	05.5	11.6	.	≡^1 n-8^30 ≡ 8^30, 10^30 18^45-n
3	9	10●	03⊙	00	04.3	04.3	29.3	.	●^0-1 n-8^45 = n-10^45
4	8	09	07	02	06.0	03.7	00.2	.	= n-7^30, 17^45-n; ●^tr 12-12^20
5	6	10	10	03	07.7	01.8	.	.	= n-14^30, 17^45-n; ●^tr 12-12^20
6	7	01⊙	00⊙	00	00.3	09.6	00.0	.	= n-10^30
7	8	00⊙	01⊙	00	00.3	09.6	.	.	F wsw 13^40-13^55
8	8	00⊙	01⊙	00	00.3	09.7	.	.	= n-8^30 F wsw 13^45-13^55
9	7	01⊙	00⊙	00	00.3	09.3	.	.	= n-10^45 17^30-n
10	6	01⊙	00⊙	00	00.3	07.9	.	.	= n-8^40, ≡^0-1 8^40-n
11	6	00⊙	00⊙	01	00.3	08.4	.	.	= n-n
12	3	00	10≡	10≡	06.7	00.0	.	.	= n-8^40 ≡^0-1 8^40 n
13	2	10≡	10≡	10●≡	10.0	00.0	00.0	.	●^0-1 n-11^30 i, 18^45-n; ≡^0-1-2 n-n
14	5	10●	10●	10●	10.0	00.0	00.2	.	= n-n, ●^0-1 n-7^45, 12^30-14^45, 18^30-n
15	6	10	09	00	06.3	00.2	03.8	.	= n-n, ●^0 n-6^33
16	6	02	04⊙	00	02.0	06.5	.	.	= n-n
17	5	07≡	07	10	08.0	04.0	.	.	≡^0 n-8^15 = 8^15-n
18	7	10	02⊙	01	04.3	03.9	.	.	= 13^30-n
19	6	01≡	07⊙	00	02.7	07.2	.	.	≡^1 n-8^30 = 8^30-n
20	4	09≡	10	10	09.7	00.8	.	.	≡^0 n-10^45, = 10^45-14^45, ●^tr-1 15^56, 21^20-n; F nnw 21^30-21^30
21	8	10	08	10	09.3	03.2	20.0	.	●^1 n, 21^18-n, = 16^45-n
22	4	10	09	09	09.3	00.0	00.9	.	= n-n
23	6	01≡	01⊙	10●	04.0	04.9	.	.	≡^0-1 n-11^30 = 11^30-n, ●^tr-0 20^09-n, R^0 20^42-n
24	8	08	08⊙	00	05.3	04.4	03.0	.	= n-7^30, 16^50-n
25	8	09	08	09	08.7	03.8	.	.	
26	7	09	10	00	06.3	03.5	.	.	= n-11^15 15^45-n
27	6	09≡	03⊙	00	04.0	08.1	.	.	≡^0-1 n-19^45, = 9^15-n
28	6	04	10	00	04.7	04.0	.	.	= n-n
29	6	09	10	00	06.3	00.0	.	.	= n-n, F wnw 11^40-11^45
30	6	01	00⊙	00	00.3	08.5	.	.	= n-n
31	6	04	04	00	02.7	08.2	.	.	= n-n
MES. VREDN.		05.7	05.8	03.6	05.0	141.8	76.0		

VIDLJIVOST OSMATRANA U 13 ČASOVA

φ = 45° 49' N λ = 15° 59' E Gr. ΔG = + 1h 04 min. BR. ST. 57

I	Vazdušni pritisak p mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	752.2	750.6	751.0	07.4	17.5	12.6	12.5	18.0	07.2	-	-	-	-	-	-	-	-	WSW 2	WSW 3	WNW 3
2	751.5	750.1	749.9	10.0	16.3	12.3	12.7	16.3	08.9	-	-	-	-	-	-	-	-	WNW 2	SSW 2	W 2
3	750.2	747.1	746.7	09.3	18.0	14.0	13.8	18.2	09.3	-	-	-	-	-	-	-	-	E 1	SSW 3	WNW 3
4	748.7	750.4	752.0	13.5	19.3	14.5	15.4	19.9	13.0	-	-	-	-	-	-	-	-	WNW 4	ESE 2	NE 2
5	751.9	748.2	745.8	11.0	14.6	12.1	12.4	15.1	10.8	-	-	-	-	-	-	-	-	ENE 1	SW 2	WSW 2
6	747.1	748.4	750.7	10.8	10.8	06.7	08.8	13.3	06.7	-	-	-	-	-	-	-	-	NE 2	SE 2	WNW 1
7	750.8	750.0	749.6	04.3	05.9	06.2	05.4	08.2	03.2	-	-	-	-	-	-	-	-	S 1	ENE 1	NE 1
8	750.8	752.9	753.8	04.7	07.1	06.1	06.0	07.2	04.7	-	-	-	-	-	-	-	-	E 1	ENE 1	ENE 1
9	749.1	745.3	744.0	05.6	09.8	07.1	07.4	10.2	05.6	-	-	-	-	-	-	-	-	WNW 1	WSW 2	ENE 1
10	744.3	745.4	748.8	06.2	12.7	07.9	08.7	13.0	05.5	-	-	-	-	-	-	-	-	ENE 1	SSW 2	NNE 2
11	752.0	751.9	751.2	05.3	11.7	07.8	08.2	11.7	05.3	-	-	-	-	-	-	-	-	NNE 1	SSW 2	WNW 1
12	750.6	748.7	748.7	06.5	16.1	11.0	11.2	16.1	05.4	-	-	-	-	-	-	-	-	W 2	WSW 4	WSW 3
13	748.4	748.0	747.5	10.3	15.6	11.0	12.0	15.8	09.6	-	-	-	-	-	-	-	-	WSW 3	WSW 4	WSW 2
14	743.8	739.3	739.2	08.6	18.5	13.6	13.6	19.1	08.6	-	-	-	-	-	-	-	-	ENE 2	S 5	WSW 2
15	737.8	735.3	734.1	08.5	15.6	09.3	10.7	15.7	08.4	-	-	-	-	-	-	-	-	SW 1	ESE 2	ENE 1
16	737.2	739.3	743.2	07.1	08.8	05.7	06.8	09.3	05.7	-	-	-	-	-	-	-	-	S 1	WNW 2	N 1
17	745.6	745.5	745.5	01.9	08.1	06.5	05.8	08.1	01.8	-	-	-	-	-	-	-	-	SW 2	WSW 1	W 2
18	745.9	745.7	745.5	10.3	14.3	11.5	11.9	14.8	06.5	-	-	-	-	-	-	-	-	W 3	WSW 3	W 1
19	743.0	742.2	742.1	13.1	17.0	14.4	14.7	17.0	11.5	-	-	-	-	-	-	-	-	W 2	WSW 4	SW 2
20	743.0	744.3	746.7	12.4	13.8	09.7	11.4	14.9	09.7	-	-	-	-	-	-	-	-	NNW 1	NNW 2	ENE 1
21	745.4	743.5	739.6	06.6	08.0	10.3	08.8	10.5	06.1	-	-	-	-	-	-	-	-	WSW 1	ENE 2	NNE 3
22	737.3	740.6	745.0	08.2	06.6	06.7	07.0	10.5	06.6	-	-	-	-	-	-	-	-	NW 3	WSW 2	ESE 1
23	748.9	750.5	753.4	08.7	10.7	07.3	08.5	10.7	06.7	-	-	-	-	-	-	-	-	NW 2	N 2	NNW 1
24	754.3	754.1	754.6	05.4	07.8	06.8	06.7	07.8	05.2	-	-	-	-	-	-	-	-	NNW 1	WSW 2	NNE 1
25	755.3	755.8	756.8	06.6	08.7	07.9	07.8	08.9	05.7	-	-	-	-	-	-	-	-	ENE 1	ESE 2	S 1
26	758.4	758.5	758.9	05.0	09.8	04.7	05.8	08.9	04.7	-	-	-	-	-	-	-	-	ENE 1	SSE 2	N 1
27	758.7	758.2	756.2	-00.1	03.8	04.6	03.2	04.9	-00.1	-	-	-	-	-	-	-	-	ENE 1	SSE 1	WSW 1
28	755.5	753.6	752.2	04.4	06.0	04.6	04.9	06.0	03.9	-	-	-	-	-	-	-	-	ENE 1	WSW 2	WSW 2
29	749.6	747.7	747.3	02.9	11.3	10.3	08.7	13.4	02.6	-	-	-	-	-	-	-	-	WSW 2	WSW 2	W 3
30	746.6	746.4	746.1	13.0	14.0	13.1	13.3	14.0	09.6	-	-	-	-	-	-	-	-	W 4	W 1	WSW 2
MES. VRED.	748.5	747.9	748.3	07.6	11.9	09.2	9.5	12.6	06.6	-	-	-	-	-	-	-	-	1.7	2.2	1.7

1	748.0	747.1	747.0	09.5	10.0	07.3	08.9	13.1	07.3	-	-	-	-	-	-	-	-	NNE 2	WSW 1	W 1
2	748.0	749.2	751.1	07.0	10.8	08.7	08.8	10.9	04.9	-	-	-	-	-	-	-	-	WNW 2	ESE 1	ENE 1
3	750.0	746.5	743.2	04.9	05.3	07.3	06.2	08.7	03.7	-	-	-	-	-	-	-	-	SE 1	WSW 2	W 3
4	750.7	753.1	755.1	06.7	10.3	09.3	06.9	10.4	05.2	-	-	-	-	-	-	-	-	WNW 1	SSW 2	NE 2
5	753.9	752.3	754.3	03.5	06.9	05.4	05.3	07.9	02.2	-	-	-	-	-	-	-	-	NE 1	S 1	NE 1
6	757.8	757.0	755.7	04.6	08.9	05.1	05.9	09.0	03.8	-	-	-	-	-	-	-	-	NW 2	WSW 2	WSW 1
7	753.9	752.6	753.3	00.3	04.9	05.7	04.2	06.1	00.3	-	-	-	-	-	-	-	-	ENE 1	ENE 1	WNW 1
8	757.1	759.3	763.3	05.0	05.9	03.0	04.2	05.9	03.0	-	-	-	-	-	-	-	-	ESE 1	S 1	N 1
9	763.2	761.4	761.5	-00.3	01.5	01.6	01.1	03.2	-01.2	-	-	-	-	-	-	-	-	ENE 1	ENE 1	NNE 1
10	761.6	761.1	761.6	01.2	02.4	00.5	01.2	02.5	00.3	-	-	-	-	-	-	-	-	W 2	WSW 2	ENE 1
11	762.4	762.4	762.1	01.8	04.4	02.5	02.8	04.8	00.5	-	-	-	-	-	-	-	-	WSW 2	WSW 2	W 2
12	760.7	759.9	760.1	00.8	00.8	-00.1	00.4	02.5	-00.1	-	-	-	-	-	-	-	-	SW 1	S 1	S 1
13	759.1	758.2	758.6	-01.1	-00.9	-01.4	-01.2	-00.1	-01.4	-	-	-	-	-	-	-	-	WSW 1	SW 1	S 1
14	757.9	756.6	755.7	-01.7	-00.9	-01.0	-01.2	-00.8	-01.9	-	-	-	-	-	-	-	-	WNW 1	SSW 1	SSW 1
15	756.2	756.8	758.2	-01.2	01.7	-00.6	-00.2	01.8	-01.4	-	-	-	-	-	-	-	-	WSW 1	WSW 1	NW 1
16	759.0	759.1	759.9	-02.6	04.0	02.1	01.4	04.1	-02.8	-	-	-	-	-	-	-	-	WNW 1	NE 2	NE 1
17	759.4	758.2	756.6	01.4	02.4	01.3	01.8	02.5	01.2	-	-	-	-	-	-	-	-	NNE 1	SSE 2	S 2
18	754.7	754.9	755.6	-00.1	00.7	-00.8	-00.2	01.3	-00.8	-	-	-	-	-	-	-	-	NE 1	SE 2	WNW 2
19	755.9	756.3	757.5	-02.7	00.6	-00.2	-00.8	00.6	-02.7	-	-	-	-	-	-	-	-	NE 1	SSE 1	NW 1
20	757.3	756.2	754.7	-03.4	-00.9	-02.2	-02.2	-00.2	-03.5	-	-	-	-	-	-	-	-	ENE 1	ESE 1	SSW 1
21	751.7	749.7	747.9	-04.0	-03.6	-03.6	-03.7	-02.2	-04.6	-	-	-	-	-	-	-	-	SE 1	WSW 1	NW 1
22	748.7	747.8	748.2	-01.4	02.2	-00.6	-00.1	02.3	-03.6	-	-	-	-	-	-	-	-	E 1	NNE 3	NE 3
23	745.4	742.6	741.7	-01.9	-02.2	-02.7	-02.4	-00.6	-02.9	-	-	-	-	-	-	-	-	NNE 4	NNE 4	NNE 4
24	744.2	745.8	748.2	-03.6	-01.5	-04.4	-03.5	-01.4	-04.5	-	-	-	-	-	-	-	-	W 2	WNW 2	NE 1
25	747.2	745.3	744.8	-04.4	-02.2	-03.5	-03.2	02.1	-04.4	-	-	-	-	-	-	-	-	NE 2	NNE 3	SSW 1
26	746.7	748.3	749.8	-04.0	00.3	-04.0	-02.9	00.3	-04.4	-	-	-	-	-	-	-	-	W 1	SSW 2	ENE 1
27	749.4	748.6	747.2	-04.0	-02.5	-03.0	-03.1	-02.0	-04.8	-	-	-	-	-	-	-	-	W 1	WSW 1	ENE 1
28	740.0	738.9	740.4	-01.8	-00.3	00.0	-00.5	00.3	-03.5	-	-	-	-	-	-	-	-	ENE 1	W 1	SE 1
29	742.2	739.6	736.2	03.0	03.9	03.8	03.6	04.2	-00.1	-	-	-	-	-	-	-	-	WNW 2	SSE 1	NE 2
30	730.9	730.6	734.6	01.4	02.4	02.7	02.3	04.5	01.0	-	-	-	-	-	-	-	-	NE 1	WSW 2	W 2
31	737.3	735.0	733.2	04.2	04.0	-00.6	01.8	04.5	-00.6	-	-	-	-	-	-	-	-	W 2	NNE 2	NNE 3
MES. VRED.	752.0	751.3	751.5	00.6	02.6	01.1	1.3	03.4	-00.5	-	-	-	-	-	-	-	-	1.4	1.6	1.5

ZAGREB GRIČ — 1970 NOVEMBAR

BR. ST. 57 — H_B = 157 m H_b = 162.5 m h_t = 6.0 m h_r = 2.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnevni		7	7	
1	7	06	01⊙	01	02.7	07.2	.	.	= n-n, F NW 19^{55}-20
2	6	08	09	10	09.0	05.8	.	.	= n-n
3	6	04	03⊙	00	02.3	05.9	.	.	= n-n
4	7	08	06⊙	08	07.3	05.5	.	.	= n-n, F WNW n
5	4	09	08⊙	10	09.0	04.2	.	.	= n-n
6	6	10	09	00	06.3	00.9	.	.	= n-n, ● $^{0}11^{55}$-12^{25}
7	4	10≡	09	10	09.7	01.5	00.1	.	≡ $^{1-2}$n-12^{30}, = 12^{30}-n, ψ 16^{45}-20^{30}
8	5	10●	10	10	10.0	00.0	03.5	.	= n-n, ● ^{0}n-11
9	6	10	01⊙	08	06.3	04.4	01.5	.	= n-n
10	6	06≡	02⊙	07	05.0	07.5	00.0	.	● ^{tr}n, ≡ ^{0}n-9^{45}, = 9^{45}-n
11	4	01≡	02⊙	06	03.3	08.3	.	.	≡ ^{0}n-n, Φ 19^{30}-20^{45}
12	8	08	01⊙	00	03.0	08.5	.	.	= n-11^{45}
13	8	02	10	06	06.0	02.5	.	.	= n-8^{30} F WSW 12-12^{20}
14	9	09	09	10	09.3	04.1	.	.	= n-10^{45} F S-SSW 13^{30}-15^{30} ● $^{tr-1}$ 16^{53}-ni, ♁ 17^{22}-17^{36}
15	6	01	09	10●	06.7	04.1	03.0	.	● $^{tr-1}$ 14^{14}-ni, = 15^{45}-n, ♁ ^{0} 19^{10}-19^{50}
16	7	10	10	02	07.3	00.0	14.4	.	= 15^{45}-n
17	7	02≡	10	09	07.0	02.9	.	.	≡ $^{0-1}$n-8^{30}, = 8^{30}-12^{45}, 17^{30}-n
18	8	10	09	04	07.7	01.2	.	.	
19	9	09	09	10	09.3	00.4	.	.	
20	5	10●≡	09	03	07.3	01.3	01.6	.	● ^{0}n-7^{45}, 10^{40}-13^{30}, ≡ ^{0}n-7^{30}, = 7^{30}-ni
21	2	10≡	10≡	10●	10.0	00.0	03.5	.	≡ $^{0-2}$n-13^{30}, ≡ ^{0}13^{30}-14^{45}, = 14^{45}-n, ● $^{tr-0}$ 15^{11}-15^{40}, 18^{44}-n
22	5	10●	10●	10	10.0	00.0	19.2	.	= n-17^{30}, ● ^{1}n-9^{45}, 12^{30}-16^{40}
23	6	10	10	10	10.0	00.0	02.2	.	= 8^{30}-n
24	5	10	10	10	10.0	00.0	.	.	= n-n
25	6	10	10	10	10.0	00.0	.	.	= n-n
26	5	10≡	04⊙	00	04.7	02.9	.	.	≡ ^{0}n-8^{30}, = 8^{30}-n
27	3	10≡	00≡	10≡	06.7	00.5	.	.	⌣ ^{0}n-11^{45}, ≡ $^{1-2}$n-11^{30}, 14^{30}-n; ≡ ^{0} 11^{30}-14^{45}
28	6	10	10	10	10.0	00.0	.	.	= n-n
29	6	10≡	05	03	06.7	03.0	.	.	≡ ^{0}n-10^{45}, = 10^{45}-14
30	8	10	10	10●	10.0	00.7	.	.	F WSW n, ● ^{0}20^{50}-21^{20}, n
MES. VRED.		08.1	07.2	07.0	07.4	03.1	48.8		

ZAGREB GRIČ — 1970 DECEMBAR

1	2	07	10≡	00	05.7	01.9	01.8	.	= n-9^{30}, 20^{30}-n; ≡ $^{0-1}$$9^{30}$-$20^{45}$
2	6	01	01⊙	09	02.7	06.2	.	.	= n-ni, ≡ ^{0}7^{30}-9^{30}
3	3	08≡	10≡	03	07.0	00.0	.	.	≡ ^{1}n-7^{45}, 14^{30}-n; ≡ 7^{45}-14^{30}, F NW n
4	9	00	00⊙	03	01.0	07.8	.	.	= n-9^{30}, F NW n
5	6	05	09	10●	08.0	02.3	.	.	= n-n, ● $^{tr-0}$ 17^{22}-17^{50}, 20^{30}-20^{45}
6	6	05	01⊙	00	02.0	07.4	00.5	.	= n-17^{30}
7	3	05≡	10≡	10	08.3	01.3	.	.	≡ ^{0}n-8^{45}, 11^{30}-14^{30}; = 8^{45}-11^{45}, 14^{30}-n
8	3	10≡	10●	00	06.7	00.0	01.6	.	● $^{tr-0}$n-15^{45}, ≡ ^{0}n-15^{15}, = 10^{45}-ni
9	2	10≡	10≡	10≡	10.0	00.0	00.3	.	≡ $^{1-2}$n-ni, = 14^{30}-16^{43}
10	4	10	09	10≡	09.7	00.0	.	.	= n-15^{45}, ≡ $^{1-2}$ 15^{45}-n
11	5	10	10	10	10.0	00.0	.	.	= n-n
12	4	10	10	10	10.0	00.0	.	.	= n-n
13	4	10	10	10	10.0	00.0	.	.	= n-13^{30}, 20^{45}-n; ≡ ^{0}13^{30}-20^{45}
14	4	10	10	10	10.0	00.0	.	.	= n-n
15	6	10	10	10	10.0	00.0	.	.	= n-n
16	6	05	09	03	05.7	02.2	.	.	= n-n, ⌣ ^{2}n-10
17	6	10	10	10	10.0	00.0	.	.	= n-n
18	6	10	10	02	07.3	00.0	.	.	= n-n
19	3	01	10	10	07.0	00.0	.	.	⌣ n-11, = n-8^{30}, 13^{30}-n; ≡ 8^{30}-13^{30}
20	3	10≡	00≡	10≡	06.7	00.0	.	.	≡ ^{2}n-11^{30}, 14^{30}-n; ≡ $^{0-1}$ 11^{30}-14^{30}, V ^{0}8^{30}-13^{30}, 17^{45}-n
21	2	10≡	10≡	10≡	10.0	00.0	00.2	.	≡ $^{1-2}$n-n, V $^{0-1}$n-n, ↔ $^{0-1}$n-10^{30}
22	6	10	10	10*	10.0	00.0	05.5	07	* $^{0-1}$n-a, 19^{45}-n; = n-n, F NNE 22^{45}-n, ⊠
23	5	10*	10*	10*	10.0	00.0	00.3	04	* $^{0-1}$n-n, = n-n, F NNE n-n, ↑ ^{0}a-14^{30}, ⊠
24	6	02	04⊙	06	04.0	04.7	02.2	06	= n-n, ⊠
25	4	10*	10*	10	10.0	00.0	02.6	09	= n-n, * $^{0-1}$n-20^{30}, ⊠
26	6	10	00⊙	00	03.3	05.5	02.9	12	= n-n, ⊠
27	4	10	10*	10●	10.0	00.0	.	12	= n-n, * $^{0-1}$$17^{14}$-$18^{40}$, ∿ 18^{40}-19^{32}, ♁ ^{0}19^{32}-n, ⊠
28	5	10●	09	10	09.7	00.0	21.2	10	= n-n, ∿ n-9^{30}, ● $^{0-1}$n-8^{50}, 14^{25}-14^{35}, * $^{0-2}$ 12^{20}-15^{20}, i, ⊠
29	5	10	10	10	10.0	00.0	07.5	16	= n-n, ● ^{0}10^{40}-n, ≡ $^{0-1}$$14^{45}$, 16^{30}, ⊠
30	4	10≡	09⊙	02	07.0	01.0	02.5	10	≡ $^{1-2}$n-11^{30}, i, ≡ $^{0-1}$$9^{20}$-$9^{50}$, ● $^{0-1}$$10^{45}$-$18^{40}$, i, = 11^{30}-18^{45}, ⊠
31	6	05	10	10*	08.3	00.0	03.6	07	= n-ni, ≡ ^{0}9^{30}-10^{30}, ● ^{0}15^{25}-16^{20}, * $^{0-1}$$18^{30}$-n
MES. VRED.		07.9	08.1	07.4	07.3	40.3	51.4		

VIDLJIVOST OSMATRANA U 13 ČASOVA

1970 JANUAR SPLIT MARJAN

$\varphi = 43^{\circ}\ 31'$ N $\lambda = 16^{\circ}\ 26'$ E Gr. $\Delta G =$ + 1h 06 min. BR. ST. 91

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	737.4	736.4	737.2	09.4	07.0	07.0	07.6	12.8	06.4	06.4	07.6	06.7	05.9	85	89	79	84	NW 2	NNE 3	NNE 2
2	739.0	741.1	744.1	06.2	08.6	05.7	06.6	09.0	05.2	00.5	05.0	04.7	04.4	70	57	64	64	NNE 1	W 2	NW 2
3	746.4	746.4	747.2	03.3	06.0	08.5	06.6	08.5	03.0	-01.0	03.8	04.5	06.2	65	64	74	68	NNE 3	NE 3	ESE 2
4	747.4	746.2	744.8	07.0	10.3	10.6	09.6	11.0	02.9	03.6	05.9	08.0	08.6	79	85	89	84	NNE 3	ESE 4	ESE 6
5	740.5	738.7	738.7	12.8	14.0	15.0	14.2	15.0	10.3	08.0	09.4	10.4	10.7	85	86	84	85	ESE 6	ESE 6	ESE 5
6	738.2	740.0	741.1	14.0	15.8	13.6	14.2	16.2	13.1	11.0	10.0	10.1	10.0	83	75	85	81	ESE 5	E 5	ESE 5
7	737.1	740.2	745.6	11.0	08.8	04.8	07.4	14.2	04.5	09.0	08.6	07.6	05.4	87	90	84	87	NNE 4	NNE 5	NNE 7
8	751.0	753.5	755.3	04.8	07.6	04.4	05.3	08.2	04.3	01.8	03.2	03.4	02.7	50	43	43	45	NNE 6	N 2	NNE 4
9	756.0	756.0	756.1	04.1	08.7	07.0	06.7	09.0	03.2	00.4	05.4	05.0	04.7	55	59	62	59	NNE 2	SSW 1	NNE 3
10	755.0	754.4	753.5	07.1	11.6	12.0	10.7	12.0	06.0	01.5	05.3	07.1	08.0	70	69	76	72	ENE 1	ESE 2	ESE 5
11	751.7	749.6	748.0	12.7	12.9	12.5	12.6	13.8	11.6	09.5	08.1	08.6	08.5	73	77	78	76	ESE 6	ESE 6	ESE 6
12	742.6	741.4	740.2	13.4	14.6	13.6	13.8	16.0	12.3	10.7	10.3	10.2	10.6	89	82	90	87	SE 6	SE 4	ESE 5
13	738.9	740.1	742.2	10.8	13.0	12.4	12.2	14.1	10.4	08.5	08.4	10.3	08.9	86	91	83	87	N 5	ESE 6	E 2
14	743.2	744.3	746.0	11.8	12.3	11.0	11.5	12.7	10.6	08.8	09.4	09.8	09.7	91	91	88	90	ESE 3	ESE 1	ENE 2
15	744.6	743.1	743.2	11.2	12.0	12.8	12.2	13.0	09.4	05.0	08.2	09.8	10.6	82	93	96	90	E 4	ESE 5	ESE 4
16	740.8	738.3	738.4	12.4	11.4	08.8	10.4	13.0	08.8	10.5	10.3	09.6	07.9	96	95	92	94	ESE 3	- 0	WSW 2
17	740.4	741.7	745.1	09.2	11.4	10.8	10.6	12.0	06.6	03.6	04.8	05.3	04.6	55	53	48	52	NW 2	NNW 3	NNW 2
18	747.7	748.9	749.7	09.0	11.8	08.6	09.5	12.2	08.3	04.5	03.8	03.4	05.1	44	33	61	46	NNW 3	WNW 3	WSW 2
19	749.7	749.8	751.3	06.3	07.2	04.8	05.8	09.2	04.2	03.7	03.6	02.7	02.9	50	35	44	43	NNW 4	N 6	NNE 4
20	753.0	753.0	753.1	03.4	08.4	05.6	05.8	08.6	01.9	01.0	02.7	03.5	02.9	46	43	42	44	NNE 4	SE 2	NE 2
21	751.5	750.8	750.6	03.4	08.8	05.2	05.6	09.0	03.0	-00.6	02.9	04.4	03.7	49	51	56	52	NNE 2	SE 2	NNE 3
22	750.6	750.9	751.1	02.0	07.3	03.7	04.2	07.5	01.6	-01.0	03.2	04.0	03.1	60	52	51	54	NNE 4	SSW 2	NNE 3
23	751.7	752.0	753.2	01.6	08.0	06.0	05.4	08.2	01.5	-01.4	03.1	04.1	04.0	60	51	57	56	NNE 3	SSE 1	WNW 2
24	753.7	754.5	754.7	03.2	09.0	07.6	06.8	09.2	02.5	-03.0	03.8	05.3	04.7	66	62	60	63	NNE 3	SE 2	E 3
25	751.7	753.4	754.6	07.8	08.8	07.4	07.8	09.5	05.8	04.4	07.1	06.6	06.1	90	78	79	82	ESE 5	NE 2	NNE 2
26	755.5	757.1	757.5	05.8	07.9	08.4	07.6	09.4	05.4	00.7	05.4	05.5	05.7	78	69	69	72	NE 2	NE 2	NE 2
27	757.9	756.9	755.3	09.4	11.6	11.0	10.8	11.6	08.4	06.0	07.1	07.7	07.4	81	76	75	77	E 4	ESE 5	ESE 4
28	752.5	750.3	749.5	11.0	11.6	08.8	10.0	12.2	08.4	07.3	07.6	08.2	07.0	77	80	83	80	ENE 2	NW 2	NNE 2
29	749.2	750.2	750.8	06.7	10.0	06.2	07.3	10.3	05.5	03.7	02.9	03.4	03.5	40	37	50	42	NNW 6	NE 2	NNE 3
30	747.3	745.3	743.1	05.8	08.0	06.6	06.8	08.5	05.0	02.0	03.6	05.6	06.1	52	70	84	69	NNE 4	ENE 3	ENE 4
31	740.9	741.0	742.9	08.4	12.4	07.8	09.1	13.0	05.8	03.7	05.6	05.8	03.8	68	54	48	57	NNE 3	N 2	NNE 5
MES. VRED.	747.2	747.3	747.9	07.9	10.2	08.6	08.9	11.2	06.3	04.2	05.9	06.5	06.2	70	67	70	69	3.6	3.1	3.4

1970 FEBRUAR SPLIT MARJAN

1	744.3	744.7	746.2	04.0	06.6	02.0	03.6	08.0	02.0	01.4	02.6	02.5	02.3	42	34	43	40	NNE 6	NNE 3	NNE 3
2	748.7	749.3	749.9	00.8	05.8	03.4	03.4	06.2	00.6	-02.0	02.3	02.9	02.4	48	42	41	44	N 4	WSW 1	NNW 2
3	748.2	746.0	745.0	03.0	05.8	07.8	06.1	09.2	00.5	-04.8	03.1	05.4	06.1	54	78	77	70	NNE 2	E 3	NE 2
4	746.7	747.1	746.5	08.2	13.0	13.0	11.8	13.2	07.6	04.7	06.7	08.2	08.8	82	73	79	78	NE 2	ESE 2	ESE 4
5	744.6	744.4	743.8	12.0	14.7	13.0	13.2	15.3	11.2	08.5	08.8	08.2	09.2	83	66	82	77	ESE 6	SSE 6	ESE 6
6	746.8	748.3	749.4	12.2	15.8	11.6	12.8	16.0	11.6	07.5	08.9	05.6	06.7	84	42	65	64	NE 2	WNW 2	ESE 2
7	749.0	749.8	750.0	10.8	09.0	07.9	08.9	11.9	07.7	04.6	06.6	07.0	06.1	68	82	76	75	NW 2	N 2	N 3
8	749.5	749.7	750.1	07.5	13.0	09.7	10.0	13.7	06.7	02.4	06.5	07.5	07.5	83	67	83	78	E 2	SSE 2	E 2
9	750.2	747.7	746.5	09.2	13.2	12.2	11.7	13.2	09.0	04.3	06.8	08.1	08.3	78	71	78	76	ENE 2	ESE 4	ESE 6
10	741.9	740.4	742.2	11.2	14.8	09.6	11.3	16.0	09.4	07.9	07.5	08.2	04.2	75	65	47	62	ESE 5	SSW 3	WSW 2
11	743.3	739.0	736.1	07.0	10.6	08.0	08.4	11.0	07.0	-00.9	04.4	06.3	07.3	59	66	91	72	NNE 2	SE 6	WSW 2
12	745.3	747.8	748.5	04.5	08.8	06.4	06.5	09.2	04.0	00.5	02.7	03.2	03.4	42	37	48	42	NNE 6	SSE 2	ENE 3
13	745.3	742.7	743.7	09.4	11.2	09.2	09.8	12.4	05.8	02.5	05.7	08.2	06.4	65	82	74	74	ESE 7	SE 5	SSE 2
14	744.9	741.8	735.6	07.7	11.8	11.1	10.4	12.2	07.6	02.6	05.6	05.7	09.1	71	55	92	73	NE 2	ESE 6	S 9
15	737.2	736.6	737.7	09.2	08.8	07.0	08.0	11.3	06.5	04.9	06.6	06.8	05.7	76	80	76	77	S 5	SSW 5	N 2
16	739.2	742.5	743.4	01.4	00.3	-01.8	-00.5	07.2	-01.9	-01.4	03.2	03.4	02.1	64	74	53	64	NNE 6	NNE 4	NNE 5
17	746.7	752.5	755.0	-02.0	02.9	00.3	00.4	03.5	-02.4	-04.8	01.5	01.7	01.7	38	30	37	35	N 7	N 3	NNE 3
18	752.1	748.8	744.8	-00.4	04.8	03.8	04.0	05.9	-01.6	-04.0	02.3	05.2	06.1	52	80	89	74	ENE 4	ESE 6	ESE 6
19	746.5	750.5	753.4	03.0	04.8	04.0	04.0	05.8	01.0	-00.5	02.6	02.4	02.1	46	36	34	39	NNE 8	N 7	N 5
20	754.5	752.7	751.1	01.4	08.5	06.4	05.7	09.0	01.2	-01.4	02.4	02.9	02.8	48	35	39	41	NNW 2	SSW 2	E 2
21	750.5	750.8	750.5	02.0	08.8	06.8	06.1	09.2	01.6	00.0	05.0	04.6	04.0	95	55	54	68	NE 2	SE 1	ENE 2
22	749.4	749.3	749.1	04.4	11.3	08.4	08.1	11.7	04.2	00.0	03.6	05.6	04.9	57	55	60	57	NNE 3	SE 2	NE 3
23	744.6	740.8	742.1	08.8	09.0	08.3	08.4	10.2	07.8	05.3	07.3	07.4	06.1	86	92	74	84	E 3	NNE 4	NW 3
24	744.0	742.8	742.8	07.5	11.4	08.0	08.7	12.2	07.0	00.3	02.7	03.6	03.2	35	36	40	37	NNE 3	SE 2	NNE 5
25	743.0	744.0	744.0	06.0	08.2	05.3	06.2	08.6	05.2	03.0	02.6	02.2	02.8	37	27	42	35	NNE 7	N 5	NNE 4
26	743.7	743.8	744.7	03.2	07.4	04.0	04.6	07.5	02.8	-00.4	02.5	02.1	02.6	43	27	42	37	NNE 6	NNE 4	NNE 4
27	742.5	741.2	742.9	02.8	06.8	02.0	03.4	07.7	01.7	-00.4	02.2	02.0	01.6	39	27	30	32	NNE 4	NNE 5	NNE 6
28	744.6	746.2	748.4	00.6	05.2	02.0	02.4	05.6	00.3	-02.0	02.0	02.0	02.0	42	30	37	36	NNE 5	NNE 4	NNE 5
MES. VRED.	746.0	745.8	745.8	05.6	09.0	06.8	07.0	10.1	04.4	01.4	04.4	05.0	04.8	60	55	60	59	4.1	3.6	3.8

BR. ST. 91 H_s = 122 m H_b = 128 m h_t = 6.5 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednja		7	7	
1	7	10●	10●	01	07.0	00.0	14.6	.	●$^{0-1}$ 0-15^{55}i
2	8	09	04	00	04.3	02.9	14.3	.	
3	8	08	10	07	08.3	02.1	.	.	
4	8	10●	10	10	10.0	03.8	00.1	.	●^{0} 6^{30}-7^{30} F$_{ESE}$ 17-24
5	8	10	10	09	09.7	00.2	01.3	.	F$_{ESE}$ 0-24i, ●^{0} 0^{30}-5
6	8	08	03⊙	06	05.7	06.4	.	.	F$_{ESE}$ 0-2^{45}i
7	7	10●	10●	10●	10.0	00.0	09.8	.	●$^{0-1}$ 3^{30}-22^{30}i, F$_{NNE}$ 13^{58}-24
8	8	01	00⊙	00	00.3	08.1	12.3	.	F$_{NNE}$ n-a
9	8	09	09⊙	08	08.7	01.9	.	.	⌓^{tr} 18-24
10	8	05	09	10	08.0	02.4	.	.	⌓^{tr} 0-9, F$_{ESE}$ 19^{30}-24i
11	8	09	10	10	09.7	00.3	.	.	F$_{ESE}$ 0-24
12	8	10	09	08	09.0	00.3	.	.	F$_{ESE-E}$ 0-12, 22-24; ●$^{0-1}$ 17^{35}-19^{30}
13	7	10●	10	10●	10.0	00.0	12.0	.	F$_{E}$ 0-8, $_{SE-ESE}$ 11^{47}-15^{48}; ●$^{0-1}$ 2^{30}-21^{42}i
14	8	10●	09	05	09.0	00.1	24.4	.	●$^{0-2}$ 6^{30}-8^{30}, 11^{45}-12^{30}
15	6	09	10●	10	09.7	00.0	14.0	.	F$_{E-ESE}$ 5^{55}-17^{45}; ●^{tr} 10^{50}-19^{30}i
16	7	10●	10●	10	10.0	00.0	25.0	.	●$^{0-1}$ 2^{35}-20^{30}; ≡ 7^{30}-9^{30}
17	8	08	09⊙	10	09.0	04.8	24.8	.	
18	9	08	02⊙	04	04.7	08.5	.	.	
19	8	09	07⊙	03	06.3	04.4	.	.	F-F$_{N-NNW}$ 9^{22}-24i
20	8	00	00⊙	00	00.0	08.4	.	.	F$_{NNE}$ 0-2^{15}, 8^{30}-9
21	8	06	01⊙	00	03.0	06.4	.	.	
22	7	04	00⊙	00	01.3	07.5	.	.	
23	7	00	00⊙	00	00.0	07.9	.	.	⌴$^{0-1}$ n-8^{30}
24	7	02	09⊙	10	07.0	05.7	.	.	⌴$^{0-1}$ n-9, ●^{0} 22^{15}-24
25	8	10●	03	00	04.3	02.9	00.7	.	●^{0} 0-9^{45}i
26	8	09	10	10	09.7	00.0	09.8	.	
27	8	09	09	05	07.7	00.3	.	.	
28	8	09	09	10●	09.3	00.6	.	.	●^{0} 11^{30}-13^{30} 20-24i
29	9	01	01⊙	00	00.7	08.9	01.7	.	F$_{N-NNE}$ 5^{45}-7^{50}
30	8	10	10	10●	10.0	00.0	.	.	●^{0} 9^{45}-11, 19^{40}-24i
31	8	10	09	01	06.7	02.4	02.3	.	●^{0} 1^{45}-5i, F$_{NNE}$ 20^{40}-24
MES. VRED.		07.6	06.8	05.7	06.7	97.2	167.1		

1	8	02	10	00	04.0	03.4	.	.	F$_{NNE}$ 0-10^{50}
2	7	00	01⊙	00	00.3	08.3	.	.	
3	7	09	10	10	09.7	00.0	.	.	⌴ n-8, ●^{0} 7^{45}-9
4	7	08	07⊙	10	08.3	02.6	00.1	.	
5	8	09	09⊙	04	07.3	06.3	.	.	F$_{ESE}$ 6^{30}-10^{30}, 13^{40}-22^{45}i
6	8	09	02⊙	00	03.7	06.1	00.2	.	●^{0} 2^{50}-3^{30}
7	8	10	10●	00	06.7	00.0	.	.	●$^{tr-0}$ 7^{05}-15^{50}i
8	8	06	06⊙	06	06.0	07.6	02.3	.	●^{0} 4^{30}-4^{40}
9	8	06	07⊙	02	05.0	06.0	.	.	⌓^{2} n-8, F$_{ESE}$ 17^{05}-22^{40}i
10	8	07	06	06	07.0	05.6	.	.	●^{tr} 15^{40}-15^{50}
11	8	02	10	10●	07.3	01.3	00.0	.	⌓^{1} n-9, F$_{ESE-NNE}$ 11^{57}-18^{54}i, 23^{20}-24; ●^{tr} 11^{55}-21^{30}i, F$_{NNE}$ 18^{58}-19^{20}i
12	8	01	00⊙	09	03.3	09.2	07.2	.	F-F$_{N-NE}$ 0-2^{05}, 5^{05}-8^{30}
13	8	10	10	05	08.3	00.0	.	.	F$_{ESE}$ 2^{40}-16^{40}, ●^{1} 17-18^{30}
14	9	09	09	10●	09.3	01.5	04.9	.	⌓^{2} n-9, F-F$_{ESE}$ 12^{45}-22^{40}, ●^{1} 17^{04}-24
15	7	10	10●	10●	10.0	00.0	07.0	.	F$_{S}$ 1^{30}-2^{30}, $_{SSW}$ 12^{37}-16^{40}i, $_{NNE}$ 21^{30}-24; ⌓^{2} 9^{30}-9^{57}, 14^{40}-18^{51}i; ⌓ 9^{57}-10, ●^{1} 12^{44}-ni
16	8	10	10✱	04	08.0	00.0	06.2	.	F-F$_{NNE}$ 0^{06}-20^{30}i, ✱^{2} 1-6^{40}i, ✱$^{0-2}$ 7^{20}-16^{15}, ⌓^{1} 17-24, ⊠
17	9	10	00⊙	00	03.3	08.2	01.3	.	⌓$^{+2}$ 0-12, 18-24; F-F$_{N}$ 3-11^{45}i
18	6	09	10●	10	09.7	00.0	.	.	⌓$^{1-2}$ 0-12, F-F$_{ESE}$ 9^{34}-21^{45}, ✱$^{tr-1}$ 10^{30}-12^{40}i, ●^{0} 13^{40}-14^{40}, 17^{40}-20
19	8	04	00⊙	00	01.3	08.5	06.9	.	F-F$_{NNE-N}$ 2^{05}-21^{25}i
20	8	01	10⊙	06	05.7	07.5	.	.	⊕ 11^{45}-13^{15}
21	8	10	09	07	08.7	03.0	01.6	.	● 3^{45}-4^{30}, ●^{0} 4^{30}-6^{40}, = 7^{30}-8^{45}
22	8	10	10	10	10.0	00.1	.	.	
23	6	10	10●	01	07.0	00.0	.	.	●$^{0-1}$ 10^{02}-15^{40}
24	9	01⊙	09	00	03.3	06.6	11.3	.	
25	8	05	08⊙	00	04.3	05.0	.	.	F-F$_{N-NNE}$ 2^{45}-22^{53}
26	8	01	01⊙	00	00.7	09.2	.	.	F$_{N-NNE}$ 5^{10}-9^{20}
27	8	01	00⊙	00	00.3	09.6	.	.	F$_{NNE}$ 12^{05}-24
28	8	00	06⊙	00	02.0	07.3	.	.	F$_{NNE}$ 0-7^{25}, 21^{30}-24; ⌓^{0} n-9
MES. VRED.		06.1	06.8	04.3	05.7	127.6	49.0		

1970 MART SPLIT MARJAN

$\varphi = 43^{\circ}\ 31'$ N $\lambda = 16^{\circ}\ 26'$ E Gr. $\Delta G =$ + 1h 06 min.

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i brzina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21
1	749.9	750.0	749.8	01.2	05.0	01.8	02.4	05.6	00.4	-01.4	01.9	02.2	02.0	38	33	38	36	NNE 6	NNE 4	NNE 4
2	748.1	745.7	743.5	00.0	06.8	05.4	04.4	07.4	-00.6	-05.3	01.8	02.2	03.4	40	30	51	40	N 2	SSE 2	ESE 5
3	737.6	735.8	736.2	05.2	07.7	10.4	08.4	10.6	04.7	02.2	05.9	06.5	06.7	89	82	71	81	ESE 6	SE 6	SSE 7
4	733.8	731.4	729.7	10.4	08.6	04.4	07.0	10.9	04.1	07.2	07.4	08.0	05.7	78	95	91	88	SE 7	ESE 6	NNW 2
5	734.4	735.8	739.9	03.1	09.4	07.0	06.6	10.6	01.9	-01.0	05.2	07.3	05.9	91	83	79	84	ENE 3	S 7	WNW 2
6	744.2	745.7	745.7	06.2	07.6	08.4	07.6	10.1	05.6	01.0	04.8	06.2	05.2	68	79	63	70	NNE 3	SE 2	ESE 5
7	747.6	750.2	752.3	04.0	07.9	04.5	05.2	08.9	03.6	00.2	04.8	05.2	03.4	79	65	53	66	NW 3	NW 2	NNW 3
8	751.3	749.8	748.9	02.0	10.2	07.6	06.8	10.3	09.5	-01.8	02.8	04.1	03.0	52	44	39	45	NNE 2	SSW 2	NE 2
9	747.2	747.9	750.0	05.6	12.4	09.4	09.2	12.6	04.2	-00.6	02.6	04.1	04.2	39	38	47	41	NNE 2	S 2	- 0
10	752.5	753.5	753.4	07.4	14.2	10.5	10.6	14.4	06.6	-00.4	05.1	05.3	04.0	65	43	42	50	- 0	SSW 2	ENE 2
11	752.0	751.3	748.9	08.8	10.0	10.4	09.9	10.7	08.1	04.4	04.5	06.2	08.1	52	68	86	69	NE 2	ENE 3	ESE 6
12	745.4	746.9	749.9	06.2	08.0	05.9	06.5	10.6	04.2	02.5	05.0	06.4	05.5	70	80	79	76	NNE 2	S 2	N 1
13	751.4	751.2	749.2	06.2	12.0	09.4	09.2	12.6	05.6	00.3	05.8	06.3	04.8	82	59	55	65	ENE 2	SSE 3	NE 3
14	743.0	739.4	739.8	12.8	09.4	10.0	10.6	13.0	09.7	06.8	03.9	07.8	08.3	35	88	90	71	ENE 3	NNW 2	SE 4
15	740.8	742.2	743.5	08.6	09.3	08.7	08.8	10.4	07.5	06.0	08.0	06.2	07.0	95	70	83	83	SW 2	NNW 1	NE 2
16	744.5	745.4	745.5	06.4	09.9	06.3	07.2	10.7	06.0	03.7	03.7	03.8	03.2	52	42	45	46	NNE 5	NNE 5	NNE 6
17	743.7	745.9	747.3	06.0	09.0	05.8	06.6	09.5	05.3	02.9	03.0	03.2	02.9	43	38	42	41	NNE 7	NNE 6	NNE 5
18	747.9	746.4	745.5	04.0	11.2	08.6	08.1	11.5	03.5	-00.2	02.9	04.1	04.9	48	41	59	49	NNE 2	SSE 2	ESE 3
19	740.7	737.8	739.5	07.4	08.2	08.4	08.1	10.8	07.0	04.4	05.7	07.5	03.7	74	92	45	70	ENE 4	S 1	NNE 7
20	745.7	748.2	752.6	07.3	09.4	07.6	08.0	09.6	06.7	04.0	03.2	02.8	02.7	41	32	34	36	N 5	N 6	N 3
21	753.6	753.8	753.9	07.2	14.0	09.6	10.1	14.0	05.5	-01.5	03.4	05.7	06.7	45	47	75	56	NNW 2	SW 3	S 1
22	754.0	754.0	754.3	09.1	15.2	11.8	12.0	15.7	08.0	01.0	04.3	07.1	06.6	50	54	63	56	NE 2	S 2	E 3
23	754.2	753.4	753.2	11.8	13.0	13.1	12.8	13.5	11.4	07.4	07.9	08.6	08.1	76	77	72	75	ESE 4	ESE 5	ESE 4
24	752.6	752.4	752.7	13.1	15.2	13.6	13.9	15.8	12.7	10.3	08.9	08.4	08.8	79	65	75	73	ESE 6	ESE 5	ESE 5
25	753.1	752.0	750.8	13.2	15.1	15.1	14.6	15.4	12.6	10.1	08.3	08.7	07.0	73	68	54	65	ESE 5	ESE 6	ESE 6
26	749.6	747.8	747.3	14.7	15.4	14.6	14.8	16.0	14.3	11.6	07.5	08.6	07.8	60	65	63	63	ESE 5	ESE 6	ESE 4
27	744.7	742.3	739.1	13.2	14.2	14.3	14.0	14.8	12.5	11.0	10.3	09.9	09.9	90	82	81	84	ESE 4	E 4	ESE 6
28	737.9	738.6	741.2	09.3	11.4	08.2	09.3	14.5	07.5	06.0	07.2	06.8	03.7	82	67	46	65	NNE 4	SW 1	NW 3
29	743.6	744.7	748.6	05.7	11.0	07.4	07.9	12.3	04.9	02.0	02.9	01.7	03.8	43	17	50	37	NNE 3	WNW 3	NW 3
30	753.0	753.7	753.3	06.4	13.4	09.6	09.8	13.6	05.2	04.0	02.6	04.7	04.4	36	41	49	42	NNE 2	S 3	ESE 4
31	751.8	749.8	747.1	10.3	11.7	11.5	11.2	12.2	09.0	06.0	06.0	07.2	08.0	64	69	79	71	ESE 5	ESE 6	ESE 6
MES. VRED.	746.8	746.5	746.8	07.5	10.8	09.0	09.1	11.9	06.6	03.3	05.1	05.9	05.5	62	60	61	61	3.5	3.6	3.8

1970 APRIL SPLIT MARJAN

1	742.9	742.5	743.5	11.6	15.9	13.4	13.6	16.1	10.2	08.8	09.1	10.1	09.1	89	75	79	81	ESE 4	SSE 3	E 3
2	742.7	741.5	739.4	12.2	15.0	12.4	13.0	15.2	11.5	07.2	08.8	09.0	08.7	82	71	80	78	ESE 2	S 4	ESE 5
3	739.4	741.7	744.4	06.9	07.6	04.8	06.0	12.7	03.4	02.0	04.7	06.2	03.7	64	79	58	67	NE 2	E 2	NNE 5
4	746.2	747.4	748.1	04.4	10.4	07.2	07.3	11.4	03.8	-02.7	03.2	03.3	03.6	51	35	47	44	SSE 1	SSW 4	NW 1
5	746.7	744.7	744.3	06.8	08.7	04.7	06.2	09.7	04.7	-00.4	04.0	05.1	05.2	54	60	81	65	ENE 3	ESE 7	NNE 4
6	746.4	749.1	750.8	04.4	09.1	08.2	07.5	10.5	03.6	01.0	05.3	05.8	05.9	84	66	73	74	NE 3	E 1	SE 3
7	749.7	747.9	745.1	09.0	11.2	11.0	10.6	11.6	07.4	04.1	05.6	06.9	08.9	65	69	91	75	ESE 4	ESE 6	ESE 5
8	739.9	738.6	737.0	12.4	11.6	12.6	12.3	13.0	10.3	08.9	10.3	09.9	10.3	96	97	94	96	ESE 6	ESE 7	E 3
9	736.7	740.9	744.5	12.2	13.5	11.2	12.0	14.5	10.8	10.6	10.1	07.6	05.8	94	65	58	72	S 3	WSW 4	ENE 2
10	747.7	748.2	748.6	11.0	15.4	12.8	13.0	16.1	09.6	02.2	08.3	08.6	06.9	84	65	62	70	ESE 3	SSW 3	E 3
11	747.4	746.8	747.2	12.1	16.4	13.3	13.8	16.9	11.5	07.8	05.7	06.9	08.4	54	49	73	59	ENE 2	ESE 2	N 1
12	745.7	744.8	747.3	10.1	14.2	11.4	11.8	14.5	09.3	04.3	05.0	04.1	03.7	54	34	37	42	NNW 4	NNE 5	NNW 4
13	749.8	750.4	749.6	09.2	13.2	11.9	11.6	15.1	07.8	00.5	04.3	05.6	07.2	49	49	69	56	NE 2	SSW 2	ESE 5
14	745.2	745.5	748.4	11.5	10.6	11.4	11.2	12.0	07.8	06.5	09.8	06.1	04.5	97	64	45	69	SSE 3	NNE 4	N 6
15	750.8	752.7	755.8	08.0	10.8	09.5	09.4	11.5	07.5	05.7	02.6	03.3	03.4	33	34	38	35	NNE 8	NNE 7	NNE 6
16	757.3	755.3	756.5	09.0	12.4	10.4	10.6	13.0	07.7	03.6	03.0	02.8	03.3	35	26	35	32	NW 3	NNE 6	NNE 5
17	757.1	756.3	755.3	10.2	15.7	13.4	13.2	16.4	07.8	00.7	03.9	06.0	07.2	42	45	62	50	NNE 2	SW 3	SE 1
18	753.7	751.9	751.1	12.7	19.2	16.8	16.4	21.0	11.4	04.5	08.0	09.6	07.4	72	58	52	61	ENE 1	ESE 1	SW 1
19	750.9	750.2	748.8	14.2	20.2	17.3	17.2	20.6	12.8	04.2	08.2	09.1	08.5	68	52	57	59	SE 2	SSW 3	N 1
20	748.3	749.3	750.5	17.1	19.0	17.0	17.5	19.6	14.9	08.9	07.9	09.5	09.0	54	58	62	58	ESE 5	ESE 6	ESE 5
21	751.9	752.9	755.8	16.8	18.0	17.5	17.4	19.0	15.8	12.0	06.9	08.9	07.8	48	57	52	52	ESE 6	ESE 6	E 4
22	757.5	758.4	759.0	16.5	19.8	14.0	16.1	20.7	13.8	08.5	06.9	10.0	10.0	49	58	83	63	NNE 2	SSW 3	WSW 1
23	757.2	755.7	754.8	12.2	17.6	15.9	15.4	18.9	11.4	04.5	10.4	11.1	10.6	98	73	80	84	- 0	SSW 2	WSW 1
24	753.9	753.0	751.7	14.2	21.0	16.4	17.0	21.2	13.1	05.9	10.8	11.1	11.0	89	60	79	76	ESE 1	SSW 2	ESE 2
25	749.9	748.8	747.6	17.2	23.0	19.8	18.0	23.5	15.2	07.6	08.2	07.7	10.7	55	37	80	57	NNE 1	SSW 2	W 3
26	746.4	745.7	743.8	16.7	19.4	17.2	17.8	19.7	14.4	07.1	09.3	09.3	07.9	65	55	54	58	ESE 4	ESE 5	ESE 7
27	745.5	747.7	748.9	16.2	20.6	16.7	17.6	21.0	15.3	10.7	08.2	08.2	07.5	38	45	52	45	NW 2	SSW 3	NW 2
28	748.4	748.6	747.6	15.3	14.8	12.4	13.7	17.0	11.9	08.6	08.6	08.4	09.6	66	67	89	74	ESE 4	S 4	ESE 3
29	749.8	750.3	749.2	10.8	15.3	12.3	12.7	16.2	08.5	04.3	06.9	06.8	06.0	71	52	56	60	- 0	SSW 3	SSW 2
30	747.9	747.9	750.0	10.2	10.2	09.2	09.7	15.2	07.9	04.6	06.5	05.3	03.7	70	57	42	56	NNE 1	NNE 6	NNE 5
MES. VRED.	748.4	748.5	749.5	11.7	15.0	12.6	13.0	16.1	10.0	07.4	06.9	07.4	07.2	66	57	64	62	2.8	3.9	3.3

BR. ST. 91 H_s = 122 m H_b = 128 m h_t = 6.5 m h_r = 1.0 m

Dan	Vidljivost 0–9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	7	04⊙	04⊙	02	03.3	09.1	.	.	F NNE 0-12^04, 21^23-23^30
2	8	00⊙	03⊙	09	04.0	08.3	.	.	⌴ n-10, F N 3^32-3^46 23^04-24
3	7	10●	10●	10	10.0	00.0	00.1	.	F S-E 0-24, ●^0 5^50-26^30 i
4	6	10	10●	10●	10.0	00.0	02.9	.	F-F SSE-ESE 0-14^50 ●^tr-0 4^30-22^20 i
5	6	04	10	04 ℞	06.0	01.7	60.0	.	●^1 1-2^45, 19^45-20, F S 1^34-2^20, 8^55-19^50, ▲^1 5^20-5^40, 19^40-19^45, ℞^1 5^20-5^45
6	8	07	10	10	09.0	03.7	02.4	.	●^0-1 7^25-7^40 11^50-15^45 i, 23^30-24, F 11^45-12^52
7	8	09	07⊙	00	05.3	04.4	02.5	.	●^0 0-4^45, 8^55-9^25, ⌓^tr-2 18^30-24
8	8	00⊙	00⊙	00	00.0	10.2	00.2	.	⌓^2 n, ⌴^1 n-9
9	8	00⊙	00⊙	00	00.0	10.0	.	.	⌓^1 n-9, ⊕ 12-12^45
10	9	02⊙	09⊙	00	03.7	09.5	.	.	
11	8	09	10	10●	09.7	00.0	.	.	●^tr-1 12^20-13^20 i, 16^05-17^40 i, 20^30-24 i; F ESE 17^59-24 i
12	8	10	07⊙	05	07.3	02.6	06.7	.	●^0-1 0-6^40 i, 11^30-11^45, 17-18^45; F ESE 0-1^28
13	8	09	09	10	09.3	05.8	01.2	.	●^tr 5
14	6	10	10●	10	10.0	00.0	.	.	●^0-1 7^20-24 i
15	8	10●	10	10	10.0	00.1	26.8	.	●^0-1 0-12^45
16	8	08	07⊙	00	05.0	06.7	03.4	.	F-F N-NNE 4-24 i
17	8	00⊙	01⊙	00	00.3	10.2	.	.	F-F NNE 0-21^30 i
18	8	09	05⊙	10	08.0	08.9	.	.	
19	6	10	10●	08	09.3	00.9	.	.	●^1-2 11^40-15, ℞^1 NE 13^15-13^30, F-F NNE-N 16^08-24
20	8	02⊙	01⊙	01	01.3	10.8	09.1	.	F-F N 0-7^50
21	9	01⊙	00⊙	00	00.3	10.8	.	.	⌓^0-1 20-24
22	8	01⊙	07⊙	07	05.0	09.5	.	.	⌓^0-1 0-17^30
23	8	10●	10	10	10.0	00.7	00.0	.	●^0 6^40-8^30 F ESE 10^05-18^50 i
24	7	07⊙	01⊙	00	02.7	09.5	00.0	.	F ESE 1^20-13^30
25	8	10●	09	09	09.3	01.2	.	.	F ESE 5^50-24 i, ●^tr 11^25-11^40
26	8	10	10	00	06.7	00.8	00.0	.	F ESE 0-19^30 i
27	7	10	10	10●	10.0	00.0	.	.	●^0-1 11^35-12^45, 15-16^30, 20^50-24; F ESE-E 17^40-24
28	8	10●	10	09	09.7	00.3	07.4	.	●^0-1 0-8^30 i, 11^40-13 i; F ESE-E 0-0^40, 7^05-11^25 i
29	9	02⊙	01⊙	00	01.0	11.1	00.1	.	
30	9	00⊙	00⊙	00	00.0	11.3	.	.	
31	8	08⊙	10	10	09.3	01.6	.	.	F E-ESE 9^55-24, ●^0-1 22^45-24
MES. VRED.		06.2	06.5	05.3	06.0	160.2	122.8		

1	8	10	09	07	08.7	02.9	06.3	.	●^1-tr 0-17^40 i, F ESE 0-6^40
2	8	05⊙	09	09	07.7	04.7	00.1	.	F ESE 19^30-24
3	8	10	09	04	07.7	01.7	00.7	.	●^0 1^45-2^20, 7^30-13^45 i, 18^45-19; ▲^1 9^28-9^32, ▲^1 11^04-11^25 F NNE 15^01-21^06
4	9	08	05⊙	00	04.3	10.3	02.7	.	
5	8	08⊙	10	05	07.7	03.2	.	.	F-F SE 10-19^30 i, ●^0 10^50-13^30 i, 16^45-24 i; ℞^0 s 16^40-20^30
6	8	09	09	05	07.7	08.7	10.8	.	●^0 3^45-6, 10^50-12^30
7	8	10	10	10●	10.0	02.3	00.4	.	F ESE 9^24-20^45 i, ●^1-2 20^30-24
8	6	10●	10●	10●	10.0	00.0	13.8	.	●^0-1 0-24 i, F-F ESE 5^05-20 i
9	8	10	09	00	06.3	03.5	32.6	.	●^tr-0-1 0-5^50, 9^25-11^45 i
10	8	01⊙	07⊙	06	04.7	07.7	00.7	.	⌓^2 n-8
11	9	10	07⊙	10	09.0	04.4	.	.	⌓^1 19-24
12	9	07⊙	03⊙	00	03.3	11.3	.	.	⌓^tr-1 0-7 F N 7^28-20^50 i
13	8	01⊙	10	10	07.0	05.1	.	.	F ESE 18^30-23^55 i, ●^1 22-24
14	8	10●	07⊙	10	09.0	01.7	09.7	.	●^1 0-12^40 i, F NNE 12^45-24
15	8	09	00⊙	01	03.3	09.7	05.2	.	F-F NNE 0-24 i
16	8	07	04⊙	00	03.7	10.6	.	.	F-F NNE-N 0-8^02 i, 11^22-18^54 i
17	8	04⊙	04⊙	03	03.7	11.9	.	.	≡ 18-24, ⌓^0-1 18^30-24
18	8	09⊙	03⊙	00	04.0	11.2	.	.	≡ 0-11^30, ⌓^1-2 0-8^30
19	7	01⊙	05⊙	00	02.0	10.7	.	.	≡ n-11, ⌓^0-1 n-8, 19^30-24
20	8	08⊙	07⊙	07	07.3	09.1	.	.	⌓^0 0-α, F ESE 4^51-24 i
21	8	10	09	09	09.3	04.0	.	.	F-F 0-15^55 i
22	8	09	09⊙	00	06.0	01.6	.	.	⌓^2 19^30-24
23	3	10≡	08≡⊙	00	06.0	07.2	.	.	⌓^2 0-13^30 19-24; ≡^1-2 n-10^45 ≡^1 10^45-13, ≡ 13-14^30
24	8	09⊙	09⊙	00	06.0	08.4	.	.	⌓^1-2 0-12 ≡ n-13^30 ⊕ 12^45-14^45 i
25	8	06⊙	09⊙	00	05.0	08.7	.	.	⌓^0-1 n-10, 19-24; ≡ 5-9, ⊕ 12^30-13^45
26	8	05⊙	08⊙	00	04.3	10.4	.	.	⌓^1 0-17^30 F ESE 9^28-24 i
27	9	09	03⊙	01	04.3	08.0	.	.	F ESE 0-0^52 i
28	8	10	10	10●	10.0	00.1	.	.	●^0-1 20^35-23^50
29	9	02⊙	02⊙	00	01.3	11.9	09.8	.	●^0 2^40-4^30 i, ⌓^0-1 19^30-24
30	8	09	09	02	06.7	05.5	10.1	.	⌓^0 0-0^30, ℞^0 0^45-1, 4^30-4^45, 9^32-10^24; ●^1 0^30-5 i, 10^25-11^40 i, 15^50-16^05, F 12^40-22^55 i
MES. VRED.		07.5	07.1	04.0	06.2	104.5	102.9		

$\varphi = 43^{\circ}\ 31'$ N $\lambda = 16^{\circ}\ 26'$ E Gr. $\Delta G =$ + 1h 06 min. BR. ST. 91

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	751.7	750.8	752.1	09.4	15.6	10.0	11.2	16.1	07.4	03.3	03.4	04.5	03.1	38	34	34	35	NNW 2	W 3	NNE 5
2	751.8	751.2	751.7	08.9	14.8	08.8	10.3	15.9	07.4	04.0	03.2	04.0	03.3	37	32	39	36	NNE 4	SSW 2	NNE 5
3	752.1	751.8	752.8	09.5	14.8	12.1	12.1	15.1	08.0	04.7	03.5	03.8	04.7	40	30	44	38	NNE 4	NNE 5	NNE 5
4	751.7	749.3	747.6	12.6	18.0	15.8	15.6	18.6	10.9	07.0	04.9	06.3	04.1	45	41	31	39	N 4	SSW 4	N 3
5	744.5	743.1	745.6	13.8	16.9	13.9	14.6	18.0	12.5	07.9	04.9	08.1	08.5	42	56	71	56	W 2	SW 3	ESE 2
6	747.7	749.1	749.6	13.2	15.6	13.4	13.9	16.6	12.2	09.0	07.8	09.0	08.0	69	67	69	68	E 3	ESE 5	ESE 4
7	746.4	746.5	747.6	15.6	18.4	17.6	17.3	18.6	11.5	09.1	07.1	07.3	07.0	53	46	46	48	ESE 5	ESE 7	SE 4
8	747.9	749.1	749.4	16.9	18.6	17.0	17.4	20.0	15.4	09.8	08.6	10.2	09.0	59	63	62	61	SSE 4	ESE 5	ESE 4
9	751.5	751.8	750.9	17.0	20.0	17.7	18.1	20.5	15.3	12.6	09.7	10.8	09.9	67	62	65	65	ESE 4	ESE 4	SSE 2
10	747.3	745.4	744.2	19.2	22.0	19.8	20.2	22.5	16.8	12.3	06.9	08.2	08.6	41	42	50	44	ESE 5	ESE 6	ESE 5
11	746.0	746.3	745.3	17.0	20.1	17.2	17.9	20.7	15.4	11.0	10.5	09.7	06.5	72	55	44	57	W 2	SSW 4	NNW 1
12	746.2	746.3	748.7	12.6	17.2	15.2	15.0	18.4	11.6	09.7	09.6	09.1	08.2	88	62	63	71	SSE 1	S 3	ESE 2
13	749.7	750.0	750.7	15.2	20.2	16.2	17.0	21.0	13.7	09.0	09.2	09.7	09.6	71	54	70	65	- 0	SSW 4	NE 1
14	751.6	752.0	751.7	15.5	21.4	17.0	17.7	21.5	13.5	07.9	09.0	11.5	10.0	68	60	69	66	NE 1	S 2	S 2
15	750.5	748.7	746.7	16.8	20.6	18.8	18.8	21.0	14.1	08.4	08.6	09.3	08.8	60	51	54	55	E 3	ESE 5	ESE 5
16	746.6	746.6	745.7	18.4	18.8	16.8	17.7	21.7	16.4	11.7	11.0	11.2	11.1	69	69	77	72	ESE 2	NNE 2	WSW 2
17	744.9	744.1	745.3	17.2	20.7	17.7	18.3	22.1	14.9	08.0	11.7	09.7	10.9	79	53	72	68	S 1	SW 4	ENE 2
18	746.9	749.2	751.9	17.4	19.6	16.8	17.6	20.2	16.3	11.6	07.3	07.0	06.0	49	41	42	44	N 4	N 6	N 6
19	752.5	752.3	751.7	16.6	21.2	16.8	17.8	22.2	15.6	12.8	05.7	05.9	06.3	40	31	44	38	NNE 4	NNE 3	NNE 4
20	750.1	748.3	747.1	17.5	22.5	18.3	19.2	23.8	14.9	11.7	07.8	08.1	07.7	52	40	49	47	NNE 4	S 1	NNE 5
21	745.4	743.9	743.6	19.4	23.4	19.5	20.4	24.7	16.9	14.1	07.4	07.4	09.9	44	34	58	45	N 4	N 3	NW 1
22	742.9	751.8	743.1	17.4	20.4	12.2	15.6	21.7	11.4	08.6	11.3	10.4	08.6	76	58	80	71	E 1	SE 5	N 3
23	749.0	752.6	754.8	13.8	19.3	13.7	15.1	19.4	11.2	09.4	05.1	04.4	05.3	43	26	45	38	NNW 4	NNW 3	NNE 5
24	757.4	757.8	758.4	13.5	17.0	14.2	14.7	18.0	11.5	06.6	04.3	03.7	04.0	37	25	33	32	NNE 4	N 5	N 2
25	757.4	755.1	753.8	14.4	21.2	18.0	17.9	21.5	11.3	07.0	05.4	08.1	06.3	44	43	41	43	NE 1	SSW 4	N 3
26	753.0	751.9	751.8	16.4	21.8	16.6	17.8	22.1	14.0	06.1	06.9	08.7	10.4	49	45	74	56	E 2	SSW 2	NW 2
27	750.9	750.6	750.0	18.0	21.4	16.0	17.8	23.6	15.0	07.6	11.2	10.0	10.5	72	52	77	67	S 2	SW 3	NNW 3
28	749.6	750.1	750.8	13.1	18.4	14.0	14.9	18.7	12.0	09.0	07.4	09.5	08.8	66	60	73	66	NNE 3	SE 2	NE 1
29	750.5	751.0	751.0	15.6	21.6	16.6	17.6	22.0	12.4	06.7	07.3	07.2	08.5	55	37	60	51	NNE 2	SSW 3	SSE 2
30	750.8	750.2	749.7	15.8	21.2	18.0	18.2	21.5	14.4	06.9	08.3	07.1	08.2	61	38	53	51	ENE 3	ESE 4	ESE 4
31	750.2	750.2	751.4	17.0	23.0	18.6	19.3	23.6	16.2	11.2	08.0	10.8	07.1	55	51	44	50	NNW 2	SW 3	N 3
MES. VRED.	749.5	749.6	749.5	15.3	19.5	15.9	16.7	20.4	13.2	08.9	07.5	08.1	07.7	56	47	56	53	2.8	3.7	3.2

1	753.3	753.4	753.7	19.4	22.8	19.5	20.3	24.0	16.6	12.8	06.3	06.3	06.5	38	30	38	35	NNE 3	NE 2	NNE 2
2	753.0	752.5	753.0	19.8	18.2	14.0	16.5	24.4	13.5	11.2	07.2	09.6	08.9	42	61	74	59	NNE 3	NNE 2	NNE 5
3	753.2	752.1	752.0	14.0	18.8	15.6	16.0	19.2	12.6	09.0	04.5	04.8	05.5	38	30	42	37	NNE 5	NNE 4	NNE 4
4	750.9	751.5	752.2	16.4	20.2	16.5	17.4	21.5	13.5	10.3	06.6	07.6	10.4	47	43	74	55	NNE 4	SSW 3	SE 2
5	753.0	753.3	753.0	16.7	21.0	17.0	17.9	22.0	14.4	08.6	10.4	09.5	09.7	73	51	67	64	ESE 2	SSW 3	E 2
6	753.2	752.9	752.1	13.8	17.2	16.5	16.0	18.8	12.9	11.0	10.6	12.1	12.0	89	82	86	86	E 2	E 2	E 3
7	751.0	749.9	748.4	18.2	23.2	21.8	21.2	24.0	16.0	11.7	10.3	10.6	08.1	66	50	41	52	NNE 3	ESE 4	ESE 5
8	748.5	749.1	750.0	21.8	24.1	20.1	21.5	24.5	20.0	17.0	09.9	12.0	13.6	51	53	77	60	ESE 4	ESE 5	ESE 4
9	749.9	750.8	749.7	21.3	23.8	23.0	22.8	25.7	19.4	14.8	10.7	11.1	10.4	56	50	49	52	NE 3	ESE 5	ESE 5
10	749.1	748.6	748.5	23.2	25.3	20.8	22.5	28.0	20.7	16.8	11.4	14.6	14.7	54	60	80	65	SE 3	SSW 3	S 2
11	748.3	748.0	748.2	19.8	26.0	22.2	22.6	27.0	17.9	13.1	15.2	15.3	11.1	88	61	55	68	SSE 2	SW 3	N 3
12	748.4	747.4	747.2	23.2	27.3	23.5	24.4	27.8	21.2	14.9	09.2	10.7	10.2	43	39	47	43	NNE 3	SW 4	NW 3
13	747.5	747.4	747.6	23.0	27.6	24.2	24.8	28.8	20.7	13.5	10.0	11.9	11.2	47	43	50	47	E 1	SSW 3	SW 1
14	748.4	748.8	748.9	21.8	27.1	22.4	23.4	28.3	19.0	12.4	14.3	12.1	10.2	73	45	50	56	E 1	SSW 2	SW 1
15	749.8	750.5	751.2	21.0	27.5	23.6	23.9	28.0	18.3	14.3	12.8	12.2	14.5	69	44	66	60	ENE 1	SSW 3	E 1
16	751.3	751.6	751.5	22.4	29.7	24.8	25.4	29.9	20.3	14.2	16.3	14.3	12.4	80	46	53	60	SSW 2	S 2	NW 2
17	751.1	750.0	749.4	24.4	29.[illegible]	25.4	26.2	31.1	21.9	15.4	13.2	14.6	14.8	57	46	61	55	NE 2	SW 2	NW 2
18	746.7	745.6	745.9	26.8	28.6	22.7	25.2	29.4	22.4	21.0	12.3	13.4	12.4	46	46	60	51	ESE 4	SE 5	NW 3
19	746.4	747.7	748.6	18.9	24.9	20.0	21.0	25.5	16.9	14.8	12.9	13.4	12.6	79	57	72	69	WNW 2	SSW 4	WSW 2
20	748.2	748.8	750.6	17.8	22.0	22.4	21.2	24.0	16.8	14.8	13.0	11.2	09.6	85	56	47	63	NNW 2	NNE 2	NNE 4
21	751.5	752.1	752.8	22.6	28.8	23.0	25.4	29.5	20.5	17.2	08.2	09.8	09.1	40	33	38	37	NNE 4	SSW 3	NNE 3
22	753.6	753.6	752.9	24.8	29.4	25.5	26.3	30.5	22.6	15.0	11.2	11.3	10.6	48	37	43	43	NE 1	SW 3	W 2
23	752.6	752.4	752.1	24.1	29.0	24.2	25.4	29.5	22.2	15.8	12.7	14.7	16.7	57	49	74	60	ENE 1	SSW 3	NNE 1
24	752.5	752.4	752.6	23.8	30.4	25.5	26.3	31.0	20.9	13.9	12.6	12.5	12.2	57	38	50	48	SSE 1	SW 2	ENE 1
25	753.1	752.2	752.7	24.0	29.8	25.4	26.2	30.4	21.6	14.6	12.9	15.9	11.8	58	51	48	52	NE 2	SSW 4	NNE 4
26	753.2	752.1	751.6	25.4	30.0	26.0	26.8	32.0	23.4	15.0	12.1	12.5	15.5	50	39	61	50	NNE 4	SW 3	ENE 2
27	752.1	751.7	751.5	26.0	31.1	27.4	28.0	32.6	23.9	20.7	11.5	13.6	12.3	46	40	45	44	NNE 4	SW 5	- 0
28	751.7	751.3	751.1	25.7	31.2	25.3	26.9	31.6	23.1	17.4	14.7	1[illegible].7	13.3	59	40	55	51	S 1	SSW 1	SW 2
29	750.4	749.3	748.9	24.7	31.0	25.0	26.4	31.3	22.5	16.0	08.6	03.1	11.6	37	09	46	31	- 0	SSW 2	SW 2
30	747.7	746.7	745.6	25.4	27.6	23.4	25.0	29.7	22.4	17.9	12.1	18.5	15.7	50	67	73	63	NE 2	SSW 3	S 3
MES. VRED.	750.6	750.4	750.4	21.7	26.1	22.3	23.1	27.[illegible]	19.[illegible]	14.[illegible]	11.1	11.8	11.6	57	46	57	54	2.4	3.0	2.5

BR. ST. 91 H_s = 122 m H_b = 128 m h_t = 6.5 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	9	00⊙	01⊙	08	03.0	12.8	00.5	.	$F_{NNE}\ 20^{40}-21$
2	9	01⊙	07⊙	00	02.7	07.8	.	.	$F_{NNE}\ 20^{49}-21^{20}$
3	8	00⊙	03⊙	00	01.0	12.6	.	.	$F_{N-NNE}\ 1^{00}-21^{40}i$
4	8	00⊙	02⊙	00	00.7	12.8	.	.	
5	8	09	10	10	09.7	00.1	.	.	
6	7	09	10	10	09.7	05.2	.	.	$\bullet^{0-1}21^{05}-22^{20}$
7	9	10	10	09	09.7	00.2	02.2	.	$F_{E-ESE}\ 2^{54}-24i$, $\bullet^{0-1}3^{40}-4^{20}$
8	7	10	09	01	06.7	06.0	.	.	$F\ 0-2^{32}i$, $9^{28}-19^{22}i$
9	8	06⊙	09⊙	09	07.3	10.3	.	.	
10	8	09⊙	08⊙	01	06.0	08.7	.	.	$F_{ESE}\ 9-23^{40}i$
11	9	09⊙	05⊙	07	07.0	09.6	.	.	$\Delta^{tr}\ 20-24$
12	9	06⊙	07⊙	03	05.3	08.6	06.6	.	$\Delta^{tr}\ 0-2^{20}$ $\bullet^{1}2^{20}-6$
13	8	07⊙	02⊙	00	03.0	12.1	.	.	$\Delta^{1}n-8$, $20-24$
14	8	04	02⊙	00	02.0	12.4	.	.	$\Delta^{1-2}\ 0-9$
15	9	09⊙	06⊙	10	08.3	03.9	.	.	$\Delta\ n-7^{30}$, $\oplus\ 10^{30}-11^{45}$, $\bullet^{tr}12^{32}-12^{45}$
16	8	07⊙	09	07	07.7	05.4	00.0	.	$\bullet^{tr}\ 7^{31}-12^{45}i$
17	8	00⊙	02 ⚲⊙	10 ●⚲	04.0	11.8	01.4	.	$\Delta^{1}n-8^{30}$, $T_N\ 13^{50}-15^{30}$, $18^{50}-22^{30}$, $\bullet^{tr}20^{00}-21^{05}$
18	8	09	05⊙	01	05.0	08.7	00.0	.	$F_N\ 9-22^{30}$
19	8	06	03⊙	01	03.3	10.4	.	.	$F_{NNE}\ 0^{40}-2^{25}i$
20	9	02⊙	09	04	05.0	07.9	.	.	
21	8	05⊙	04⊙	02	03.7	11.3	.	.	$\bullet^{tr}9^{32}-18^{22}$ $20^{40}i$; $F_{ESE}\ 12^{20}-16^{22}$, $21^{40}-24$
22	8	10	09	10●	09.7	02.8	.	.	$F_N\ 0^{L}\ 0^{55}$
23	9	04⊙	08⊙	03	05.0	09.1	00.6	.	
24	8	00⊙	05⊙	00	01.7	12.8	.	.	
25	8	00⊙	00⊙	00	00.0	13.6	.	.	
26	8	06⊙	03⊙	08	05.7	10.8	.	.	$\leftarrow w\ 19^{50}-18^{40}$
27	8	02⊙	06⊙	10●	06.0	11.9	.	.	$\bullet^{0}20^{30}-24$
28	8	10	09	10●	09.7	02.2	00.6	.	$\bullet^{0}0-0^{30}$, $10^{40}-11^{05}$, $18^{18}-21^{40}i$; $T\ 17^{40}-19^{25}$
29	8	00⊙	00⊙	00	00.0	13.6	02.3	.	
30	8	10	09⊙	07	08.7	05.8	.	.	$\oplus\ 11^{30}-14^{30}$
31	8	08	08 ⚲⊙	01	05.7	09.6	.	.	$\Gamma_{NE}\ 13^{40}-14^{30}$, $\bullet^{0}\ 15^{25}-15^{30}$
MES. VRED.		05.4	05.8	04.6	05.2	270.8	14.4		

1	8	07⊙	06⊙	00	05.0	12.1	00.0	.	$\bullet\ 11^{25}-14^{45}i$, $18^{30}-20^{40}$; $\Gamma_{NW}\ 18^{20}-20^{45}$, $F_{N-NNE}\ 22^{40}-23^{42}$
2	8	01⊙	10	10	07.0	06.1	.	.	$F-F_{N-NNE}\ 0^{35}-20i$
3	8	01⊙	03⊙	01	01.7	12.7	07.6	.	
4	9	03⊙	09	00	04.0	07.5	.	.	$\Delta^{1}n-9$
5	8	01⊙	02⊙	03	02.0	11.3	.	.	
6	7	10●	09	09	09.3	00.9	10.5	.	$\bullet^{0-1}0^{30}-12^{40}i$
7	8	02⊙	02⊙	02	02.0	09.1	05.6	.	$F_{ESE}\ 16^{20}-20^{23}i$
8	8	00⊙	01⊙	10	03.7	10.9	.	.	$F_{ESE}\ 9-11^{54}i$
9	8	09	07⊙	02	06.0	07.6	.	.	
10	8	03⊙	00⊙	06	03.0	11.2	.	.	
11	7	10≡	04⊙	00	04.7	11.0	.	.	$\Delta^{1-2}n-8$, $=n-5^{30}$, $8^{30}-12$; $\equiv{}^{1}5-8$, $\equiv 8-8^{45}$
12	8	00⊙	04⊙	01	01.7	12.1	.	.	
13	8	00⊙	01⊙	00	00.3	13.7	.	.	
14	8	00⊙	10	02	04.0	11.8	.	.	$\equiv 5^{30}\ 9 \oplus 13^{45}-14^{45}$
15	8	08	01⊙	00	03.0	11.4	00.4	.	$\bullet^{0}2-2^{30}i$
16	7	02⊙	01⊙	07	03.3	13.2	.	.	$=n-12$, $\Delta^{1}n-8$
17	8	01⊙	02⊙	07	03.3	12.9	.	.	$\equiv n-6$
18	8	06⊙	06⊙	02	04.7	11.8	.	.	$F_{ESE}\ 14^{40}-17^{32}$ $21^{40}-21^{55}$, $\bullet^{1}21^{40}-24^{50}i$, $\Gamma\ 11^{45}-23^{30}$
19	9	05⊙	05⊙	09	06.3	06.4	04.5	.	$\bullet^{0}0-2^{30}$ 16^{40} $17^{45}i$; $F_{NNE}\ 0^{25}-0^{54}$
20	8	10●	09	01	06.7	00.0	04.8	.	$\bullet^{0}4^{05}-13^{05}i$
21	8	00⊙	03⊙	00	01.0	13.6	01.0	.	
22	8	00⊙	01⊙	00	00.3	13.7	.	.	
23	8	00⊙	01⊙	00	00.3	13.8	.	.	
24	7	01⊙	03⊙	00	01.3	13.5	.	.	$\Delta^{0}\ n-7 \equiv 5-12$, $T^{0}_{N}\ 13^{05}-13^{30}$
25	8	00⊙	04 ⚲⊙	01	01.7	11.7	.	.	$\equiv n-9$, $\Gamma\ 14^{42}-14^{54}$, $\nabla^{1}14^{43}-14^{54}$, $\bullet^{0-1}14^{55}-17^{40}$
26	8	01⊙	05⊙	08	04.7	12.7	03.6	.	
27	8	00⊙	01⊙	00	00.3	13.2	.	.	
28	8	00⊙	01⊙	01	00.7	13.4	.	.	$=5-9$
29	8	04⊙	02⊙	07	04.3	13.0	.	.	
30	8	01⊙	08⊙	02	03.7	12.5	.	.	
MES. VRED.		02.9	04.1	03.0	03.3	324.8	30.0		

φ = 43° 31' N λ = 16° 26' E Gr. ΔG = + 1h 06 min. BR. ST. 91

Dan	Vazdušni pritisak p mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost v%				Pravac i jačina vetra D, f (0–12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	743.3	745.5	746.3	21.6	21.2	21.0	21.2	23.7	15.5	18.1	12.5	13.0	12.7	65	69	68	67	N 3	S 2	ESE 1
2	746.6	746.6	746.2	21.0	26.4	22.7	23.2	27.7	18.6	14.0	11.1	12.2	11.4	60	47	55	54	NE 2	SSW 2	W 1
3	746.1	746.2	746.1	22.0	27.7	23.6	24.2	27.9	20.4	15.3	13.6	15.3	16.7	69	55	76	67	ENE 2	S 2	WSW 2
4	745.1	745.6	746.6	23.2	26.4	20.4	22.6	27.0	20.0	17.4	11.7	15.6	08.8	55	61	49	55	E 2	SSW 3	NNE 6
5	748.1	749.5	751.3	15.6	13.4	16.5	16.8	20.5	15.0	12.2	08.7	08.7	10.2	66	55	73	65	NNE 6	NNE 5	N 3
6	750.7	751.3	750.7	19.6	19.7	20.0	19.8	21.0	16.0	12.2	07.9	08.8	10.0	46	51	57	51	NNE 4	N 4	WNW 2
7	748.5	748.1	747.5	22.4	29.4	24.0	24.7	29.2	20.0	16.9	10.3	12.7	11.0	51	44	49	48	NNE 5	SSW 3	NNE 4
8	747.3	747.1	747.3	24.0	29.6	25.4	26.1	30.3	21.7	15.2	12.2	13.4	13.1	54	43	54	50	NNE 2	SSW 2	WNW 2
9	748.6	748.6	748.8	23.8	29.6	26.1	26.4	30.5	21.4	17.3	17.3	14.9	12.9	78	48	51	59	S 1	SW 3	- 0
10	750.5	750.3	751.1	24.2	31.4	28.4	28.1	32.0	22.1	16.3	13.0	15.1	14.0	57	44	48	50	NE 2	SSW 3	NNE 4
11	752.1	751.6	750.5	27.2	31.8	28.8	29.2	32.8	24.5	16.3	13.0	13.6	14.4	48	39	49	45	NNE 3	SW 3	W 1
12	751.1	751.1	751.1	27.4	33.2	28.6	29.4	34.6	25.5	18.2	12.0	13.9	14.2	44	36	48	43	NE 1	SSW 2	NNE 4
13	751.7	751.1	750.2	28.0	33.8	27.2	29.0	33.9	26.1	23.0	12.6	12.3	14.3	44	31	53	43	S 1	SSW 2	ENE 2
14	749.1	748.0	746.9	26.4	31.7	26.4	27.7	32.5	24.4	19.7	11.6	13.1	17.0	45	37	66	49	NE 2	SSW 2	W 2
15	743.3	741.2	739.7	24.8	27.4	25.3	25.7	27.9	23.2	17.3	17.6	16.3	15.0	75	59	62	65	ESE 3	ESE 6	ESE 6
16	739.2	740.7	741.3	21.5	23.0	18.2	20.7	23.7	17.2	18.7	16.5	15.7	08.4	86	66	53	68	SSE 6	S 3	N 4
17	743.7	745.4	747.5	17.4	20.0	18.2	18.5	21.4	16.2	12.3	08.3	06.3	06.5	55	36	41	44	NW 2	NNE 3	NW 2
18	746.9	749.6	749.0	18.8	23.1	19.5	20.2	24.0	16.0	11.7	05.8	06.6	07.0	36	31	41	36	NW 4	WNW 1	W 2
19	748.7	748.7	748.6	19.2	24.6	20.4	21.2	25.2	16.9	08.6	09.6	10.2	11.4	58	44	64	55	SE 1	SSW 3	SSW 1
20	748.4	748.8	746.5	20.6	23.4	21.4	21.7	23.9	18.3	11.8	10.5	13.5	13.2	58	63	69	63	ESE 3	ESE 5	ESE 5
21	751.0	751.7	751.8	21.8	26.2	24.2	24.1	26.5	20.5	18.1	13.9	13.7	09.1	71	54	40	55	ESE 6	ESE 4	ESE 4
22	751.8	751.8	751.7	25.6	31.9	28.4	28.6	32.0	22.9	17.1	09.8	12.6	10.0	40	36	34	37	NE 3	SSE 3	W 2
23	752.1	752.0	751.5	27.0	34.0	29.6	30.0	34.2	24.4	16.5	11.0	10.9	11.6	41	27	37	35	E 1	SSE 2	W 1
24	750.7	749.6	748.3	26.7	32.8	27.4	28.6	33.4	24.5	16.8	12.0	13.8	15.0	46	37	55	46	NE 2	SSW 2	NE 1
25	745.4	743.9	743.8	26.1	31.2	26.0	27.3	32.4	23.1	16.6	13.1	13.2	11.8	52	39	47	46	NE 2	SW 2	N 3
26	745.1	746.7	748.6	23.4	29.8	23.6	25.1	30.1	21.6	19.3	07.8	07.4	07.8	36	24	36	32	NNE 6	NE 3	NNE 3
27	751.1	751.2	751.8	23.2	27.9	26.4	26.0	29.6	21.0	15.0	08.2	09.1	08.4	38	32	33	34	NE 1	SW 4	NNW 3
28	752.7	752.5	751.7	26.1	31.0	26.2	27.4	32.0	23.9	16.6	09.3	11.3	16.1	37	33	63	44	NNE 4	SSW 3	E 2
29	750.8	749.4	750.0	26.4	31.4	25.8	27.4	32.0	24.0	18.1	11.3	13.8	13.7	44	40	55	46	ENE 1	SSE 2	NW 1
30	750.0	750.7	751.4	25.0	32.0	27.4	28.0	32.1	22.8	17.4	14.1	14.0	12.9	59	39	47	48	N 2	SSW 2	E 1
31	752.4	752.6	753.0	25.6	32.2	26.6	27.8	33.0	23.6	18.0	11.8	16.5	13.6	48	46	52	49	NE 2	SSW 2	NNE 1
MES. VRED.	748.5	748.6	748.7	23.4	28.2	24.3	25.0	29.0	21.0	16.2	11.6	12.5	12.0	54	44	52	50	2.7	2.8	2.4

1	752.9	751.6	752.6	25.6	31.0	26.0	27.4	32.5	23.5	18.5	14.4	16.9	10.9	59	48	43	50	SSE 1	SSW 1	SE 2
2	750.9	749.9	749.4	24.4	29.8	25.0	26.0	30.0	22.6	17.1	10.0	17.3	18.3	44	55	77	59	NNE 2	SSW 3	SE 2
3	748.8	748.3	748.0	23.9	28.8	24.8	25.6	30.4	22.4	16.0	11.7	15.1	18.1	52	51	77	60	NNE 2	SSW 2	SW 2
4	748.4	748.3	749.5	24.4	29.8	27.6	27.4	30.5	22.2	17.9	13.5	15.8	11.1	59	50	40	50	NE 1	SW 3	NW 1
5	750.6	751.3	751.7	24.7	30.3	27.8	27.6	31.5	23.1	17.4	12.4	17.3	12.5	53	53	45	50	NNE 2	SW 4	WNW 4
6	752.1	751.6	750.8	26.0	34.4	29.4	29.8	35.1	24.4	17.2	13.6	13.6	13.8	54	33	45	44	- 0	SW 4	WNW 3
7	750.1	749.5	748.6	26.2	33.2	29.2	29.4	33.6	23.8	23.1	15.7	15.1	13.9	62	40	46	49	ENE 2	S 2	- 0
8	747.9	746.8	745.7	27.6	31.7	26.3	28.0	32.4	25.0	19.5	16.0	20.0	19.1	58	57	74	63	W 1	S 2	S 1
9	741.4	751.9	742.9	25.8	30.4	23.5	25.8	31.0	21.9	19.0	13.5	17.4	11.0	54	53	51	53	ESE 6	SSW 3	N 3
10	743.4	746.4	747.3	21.8	22.6	21.2	21.7	24.6	16.2	12.1	13.0	13.0	13.6	66	63	72	67	NNE 2	SE 2	SW 1
11	747.1	748.3	749.1	19.2	26.4	23.6	23.2	27.2	18.6	13.6	12.3	11.7	10.1	74	45	46	55	N 2	NE 2	NNE 2
12	750.6	751.3	751.6	22.2	29.1	24.4	25.0	29.6	20.3	14.6	10.3	11.7	16.6	51	39	73	54	NNE 3	SSW 2	E 1
13	751.9	752.4	752.1	23.4	30.0	25.8	26.2	30.6	21.6	11.4	11.3	12.7	14.8	52	40	59	50	NE 2	S 3	E 1
14	752.3	752.0	752.0	24.0	29.9	27.1	27.0	31.0	22.8	15.2	13.4	17.5	14.8	60	55	55	57	NE 2	SSW 2	W 2
15	752.3	750.5	749.9	25.0	31.0	27.0	27.5	32.0	23.0	19.5	13.6	15.7	15.3	57	46	57	53	NNE 2	SSW 3	WNW 2
16	749.1	748.2	747.3	25.2	31.6	26.8	27.6	32.0	23.8	18.4	16.2	15.0	14.8	67	43	56	55	SSW 1	SSW 3	NNW 2
17	746.3	745.2	744.6	24.2	30.7	27.4	27.4	31.5	23.1	18.2	15.4	14.8	12.0	68	45	44	52	N 3	SSW 3	- 0
18	745.3	745.7	746.0	25.2	31.6	27.0	27.7	32.5	24.0	31.2	11.7	14.0	15.0	49	40	56	48	N 3	SSW 2	N 2
19	746.9	747.8	747.8	24.8	31.4	26.6	27.4	32.2	23.0	19.5	13.6	15.5	14.9	58	45	57	53	NNE 2	S 2	NNW 1
20	747.9	746.8	745.8	25.6	32.8	28.6	28.9	33.4	23.8	18.4	14.3	14.4	11.7	58	39	40	46	ENE 1	SE 3	SE 4
21	744.4	744.7	745.4	26.2	29.0	18.8	23.2	30.5	18.0	17.2	15.4	18.1	15.1	60	60	93	71	SE 6	SE 3	NNW 3
22	745.0	746.1	747.2	22.6	27.6	22.3	23.7	28.0	18.3	17.2	14.1	11.1	10.5	68	40	52	53	WNW 2	W 2	W 2
23	748.1	748.3	748.0	21.2	26.2	22.7	23.2	28.0	20.6	15.3	09.7	11.7	13.7	51	46	66	54	NE 2	SW 3	- 0
24	746.7	745.9	746.8	17.2	19.8	16.6	17.6	22.5	15.6	14.2	12.2	10.7	10.9	83	62	77	74	NE 2	ESE 2	NNE 3
25	748.7	749.9	751.4	17.6	25.0	20.8	21.0	25.4	15.5	12.1	10.2	11.1	08.3	67	47	45	53	WNW 2	SSW 3	N 3
26	752.4	752.9	754.1	19.6	25.4	20.4	21.4	26.2	18.6	14.4	06.6	09.2	09.6	39	38	53	43	NNE 4	SW 2	N 2
27	754.5	753.3	753.1	19.4	26.4	22.2	22.6	26.5	18.0	15.7	09.2	08.4	08.1	54	32	41	43	N 3	N 2	NNE 3
28	751.4	752.2	752.7	19.2	25.2	21.8	22.0	26.2	18.5	17.0	08.9	09.9	11.0	53	41	56	50	NNE 4	SSW 2	E 1
29	752.5	752.9	752.7	21.0	24.4	22.7	22.7	24.9	20.0	17.2	11.1	10.3	11.0	60	45	53	53	E 2	SSE 4	ESE 5
30	750.6	750.3	750.[illegible]	22.0	23.6	21.4	22.2	24.0	20.8	20.2	14.1	16.6	16.5	71	75	86	77	SE 6	ESE 4	ESE 4
31	748.6	748.3	749.1	20.2	20.4	21.4	20.8	22.0	19.2	17.0	14.7	14.3	13.8	83	79	72	78	N 1	E 2	NE 2
MES. VRED.	749.0	749.3	749.1	23.1	28.4	24.4	25.1	29.3	21.0	17.3	12.6	14.1	13.7	59	48	58	55	2.6	2.[illegible]	2.0

SPLIT MARJAN 1970 JUL

BR. ST. 91 H_s = 122 m H_b = 128 m h_t = 6.5 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	8	10	08	01	06.3	04.1	.	.	$F_{ESE}\,0^{40}-0^{50}$, $_{NW}\,7^{30}-8^{19}$; $\bullet^{1}\,17^{40}-11^{30}i$, $T^{0-1}_{NE-S}\,7^{45}\,9^{20}$
2	9	010	010	02	01.3	13.9	40.8	.	$\Delta^{1-2}\,n-8^{30}$; $20-24^{50}$
3	9	030	050	01	03.0	10.1	.	.	$\Delta^{1}\,0-8$
4	8	09	070	08	08.0	07.1	.	.	$F_{NNE}\,19^{50}-24$
5	8	09	08	10●	09.0	00.0	01.8	.	$F_{NNE}\,0-17^{40}i$, $23^{44}-23^{50}$; $\bullet^{0-1}\,2^{40}-3^{20}$, $16^{40}-22^{35}$
6	7	10	10	06	08.7	00.7	03.4	.	$\bullet^{0}\,0^{45}-0^{45}$, $F-F_{N-NNE}\,1^{05}-11i$, $\bullet^{0}\,11^{40}-16^{30}i$
7	8	040	070	00	03.7	12.8	00.4	.	
8	8	000	010	00	00.3	13.4	.	.	
9	7	000	030	07	03.3	13.1	.	.	$=4^{30}-11$
10	8	000	040	00	01.3	13.5	.	.	$=n-12^{30}$, $\Delta^{1}\,n-8$, $T^{0-1}_{N-NNE}\,14^{40}-16^{40}$
11	8	010	010	00	00.7	13.3	.	.	
12	8	000	030	00	01.0	12.6	.	.	$\Delta^{0}\,n-6^{30}$
13	8	000	010	00	00.3	13.5	.	.	
14	8	020	010	02	01.7	13.3	.	.	
15	7	000	000	00	00.0	12.4	.	.	$\Delta^{0}\,n-7^{30}$, $F_{ESE}\,10^{40}-24$
16	8	10●	07	09	08.7	06.2	01.6	.	$F_{ESE-ESE-NNW-NNE}\,0-11^{30}i$, $19^{10}-24$; $\bullet^{1}\,5^{40}-8^{40}$, $20^{45}-20^{49}$, $\Pi^{0}\,6^{02}-10^{40}i$, $\overset{\bullet}{\nabla}{}^{1}\,13^{45}-13^{20}$
17	9	09●	070	07	07.7	08.8	02.0	.	$F_{NNE}\,0-2^{22}\,9^{36}-17^{50}$, $\bullet^{0}\,6^{50}-7^{30}$
18	9	070	09	01	05.7	09.9	00.4	.	$F_{NNW}\,6^{05}-10^{57}$
19	8	020	020	00	01.3	13.5	.	.	
20	8	000	020	01	01.0	12.6	.	.	$F_{ESE}\,9^{10}-24i$
21	8	010	010	00	00.7	12.6	.	.	$F_{ESE}\,0-10^{52}$
22	8	000	000	00	00.0	12.9	.	.	
23	7	000	010	00	00.3	13.0	.	.	
24	8	000	010	00	00.3	12.9	.	.	$=n-9$
25	8	020	070	00	03.0	11.0	.	.	$=n-9^{30}$, $F_{NNE}\,22^{35}-24$
26	8	010	030	01	01.7	13.3	.	.	$F_{NNE}\,0-8^{20}$, $14-24i$
27	9	000	060	00	02.0	13.7	.	.	
28	9	000	020	00	00.7	13.5	.	.	
29	9	000	010	00	00.3	13.4	.	.	
30	8	010	010	08	03.3	12.1	.	.	
31	8	060	040	00	03.3	10.4	.	.	$T^{0}_{N}\,17^{20}-17^{25}$
NES. VRED.		02.6	03.7	02.1	02.8	343.6	50.4		

SPLIT MARJAN 1970 AVGUST

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
1	7	030	07	00	03.3	10.1	.	.	$\Delta^{0-1}\,n-7^{30}$ $T^{0}\,11^{20}-13^{10}i$, $\bullet^{0}pp$
2	8	080	030	00	03.7	07.7	00.0	.	$T^{1}_{N}\,15^{30}$, 15^{30} $\Delta^{1}\,20-24$
3	8	000	03≡	00	01.0	11.7	.	.	$\Delta^{1}\,0-7^{30}=n-9^{30}$ $T\,13^{50}-14^{30}$
4	7	000	010	00	00.3	12.1	.	.	$\Delta^{1-2}\,n-9$, $=n-16^{40}$, $T^{0}_{N}\,11-13^{05}$
5	8	000	060	00	02.0	12.9	.	.	$=n-9$
6	8	000	000	00	00.0	12.0	.	.	$=n-12$
7	6	000	000	03	01.0	12.4	.	.	$=n-15^{30}$
8	7	010	010	00	00.7	11.7	.	.	$=n-9^{30}$ $\Delta^{1}\,20-24$
9	8	09	030	01	04.3	06.1	00.2	.	$\Delta^{1}\,0-4^{30}=n-5$, $F_{ESE}\,6^{04}-9^{30}$ $_{W}\,16^{44}-19^{05}$; $\bullet^{1-2}\,6^{37}-10^{01}i$, $16^{55}-17^{45}$, $\Pi^{1}_{W}\,7^{03}-9$
10	9	09≡	060	01	05.3	05.8	02.4	.	$T^{1}_{N}\,6^{50}-10^{30}$, $\bullet^{1}\,8^{40}-11^{45}$, $\Delta^{0-1}\,19^{30}-24$
11	8	09	08	08	08.3	05.8	06.1	.	$\bullet^{0}\,5^{30}-6^{30}$
12	8	030	030	00	02.0	12.3	.	.	
13	8	000	010	00	00.3	12.5	.	.	$\Delta^{0}\,20^{30}-24$
14	8	000	010	00	00.3	12.5	.	.	$\Delta^{0}\,0-6$
15	8	000	010	00	00.3	12.4	.	.	$=4^{20}-12^{30}$
16	7	040	010	02	02.3	12.1	.	.	$=n-12$
17	6	080	070	03	06.0	11.6	.	.	$=n-15^{30}$, $\Delta^{0}\,n-7^{30}$
18	8	020	020	00	01.3	12.2	.	.	$=n-8$
19	8	020	010	00	01.0	12.0	.	.	$=n-6$
20	8	000	000	00	00.0	12.4	.	.	$F_{SE}\,22^{30}-24$
21	8	070	08	10●≡	08.3	07.6	.	.	$F_{SE}\,0-11^{50}$, $_{ESE}\,19^{50}-20$; $F_{WNW}\,20-20^{32}$, $\bullet^{1-2}\,19^{38}-21^{15}i$, $\overset{\bullet}{\nabla}{}^{1-2}\,19^{50}\,20^{00}$, $\Pi\,19^{40}-20^{30}$
22	8	060	08	00	04.7	10.7	45.7	.	
23	8	020	090	00	03.7	09.9	.	.	
24	8	10●	09	09	09.3	02.5	04.1	.	$\bullet^{0-1}\,n-7^{50}i$, $10^{35}-13^{50}i$; $\Pi\,5^{30}-6^{50}$, $10^{35}-10^{50}$, $F_{ESE}\,9^{52}-10^{50}$
25	8	010	050	00	02.0	11.8	14.5	.	
26	8	000	030	08	01.0	12.1	.	.	
27	8	000	030	00	01.0	10.9	.	.	
28	8	040	050	10	06.3	09.2	.	.	
29	8	09	090	10●	09.3	01.9	.	.	$\bullet^{0-1}\,19^{50}\,n$, $F_{SE}\,21^{30}-24$
30	7	10	09	10●≡	09.7	01.7	00.0	.	$F_{SE}\,0-19^{38}i$, $\bullet^{1}\,10^{20}$, 10^{52}, $17^{23}-21^{40}i$
31	6	09	10●≡	08	09.0	00.8	02.5	.	$\bullet^{0}\,2^{50}-3$, 13^{37}, 15^{30}, $=n-9^{30}$, $T^{1}\,12^{10}-15$
NES. VRED.		03.7	04.3	02.4	03.5	297.4	75.5		

1970 SEPTEMBAR SPLIT MARJAN

φ = 43° 31' N λ = 16° 26' E Gr. ΔG = + 1h 06 min. BR. ST. 91

Dan	Vazdušni pritisak P mm 7	14	21	Temperatura vazduha T C° 7	14	21	Srednji Dnev	Max	Min	Min 5 cm	Napon vodene pare e mm 7	14	21	Relativna vlažnost u% 7	14	21	Srednji Dnev	Pravac i jačina vetra D, f (0—12) 7	14	21
1	747.7	747.5	748.1	23.0	27.1	23.3	24.2	28.4	20.9	18.0	11.0	11.5	11.0	52	43	51	49	NNE 4	S 2	NNE 3
2	749.7	750.4	750.3	22.0	28.0	23.4	24.2	28.2	21.2	18.1	10.1	12.3	13.1	51	43	61	52	NNE 4	SSW 2	E 2
3	751.2	751.9	751.4	21.2	27.0	23.0	23.6	27.6	19.9	16.6	11.3	12.5	14.5	60	47	69	59	NE 2	S 2	E 1
4	751.5	751.5	751.8	21.2	26.0	23.4	23.5	26.8	20.6	16.1	12.4	13.3	12.6	66	53	59	59	NNE 2	SSW 1	ENE 1
5	752.5	752.3	751.6	20.9	27.0	23.4	23.7	27.2	19.9	17.5	08.3	12.5	11.1	45	47	51	48	NNE 2	SSW 2	WSW 1
6	750.5	750.6	750.4	20.2	27.2	22.8	23.2	27.3	18.0	14.5	11.3	13.8	17.1	63	51	82	65	N 2	SW 2	SSW 1
7	751.2	751.4	752.0	21.3	28.4	23.6	24.2	28.4	20.0	16.0	13.2	14.0	16.5	70	48	76	65	NE 2	SSW 2	E 1
8	752.9	752.7	751.8	22.0	28.4	24.0	24.6	28.6	20.4	16.5	10.4	13.3	18.8	52	46	84	61	NE 2	SSW 2	N 2
9	751.9	751.4	751.1	23.0	28.8	25.0	25.4	29.2	21.6	17.1	12.4	12.0	12.7	59	41	54	51	NNE 2	ESE 3	F 1
10	750.9	750.4	750.1	22.4	29.0	25.4	25.6	29.4	20.7	16.5	11.1	11.8	12.7	55	39	52	49	NE 2	SW 2	- 0
11	750.1	749.8	749.3	23.4	30.7	26.8	26.9	31.5	22.1	17.0	09.4	10.6	10.2	44	32	39	38	NNE 3	SSW 2	F 2
12	749.1	748.1	747.1	25.0	30.7	27.4	27.6	30.8	23.2	15.8	07.4	10.0	09.1	31	30	33	31	NNE 3	ESE 4	ESE 2
13	745.4	745.4	747.2	25.6	29.8	24.1	25.9	30.9	24.1	20.3	10.2	13.4	10.1	42	43	45	43	SSE 2	SSW 3	W 2
14	748.2	749.7	749.3	21.8	27.5	23.8	24.2	28.0	20.0	14.2	11.3	12.4	11.7	58	45	53	52	N 2	SSW 3	WNW 2
15	750.7	750.6	750.4	20.7	23.2	23.6	24.0	28.5	20.0	13.9	11.7	12.2	11.2	64	42	51	52	NE 2	S 2	N 1
16	750.5	750.0	749.9	21.8	28.4	24.2	24.6	28.4	20.6	15.0	12.4	12.2	13.0	63	42	57	54	NE 2	SSW 2	NE 1
17	750.0	749.7	751.2	20.1	20.4	18.9	19.6	24.2	18.5	16.0	08.2	07.9	07.4	46	44	45	45	NNE 5	NNE 6	NNE 6
18	750.5	751.3	752.7	20.2	24.4	21.2	21.8	25.2	17.4	13.5	08.5	09.9	09.3	48	43	49	47	NNE 6	NNE 6	NNE 6
19	752.3	752.6	753.0	20.2	27.8	22.4	23.2	28.5	19.4	18.0	08.9	09.4	08.8	50	34	43	42	NNE 6	SSE 2	NNE 5
20	752.9	751.7	751.8	21.2	27.1	22.6	23.4	27.5	20.6	18.8	08.4	09.5	07.4	44	35	36	38	NNE 3	NNE 1	NNE 6
21	751.7	750.9	751.5	20.4	24.3	20.4	21.4	24.6	19.3	15.5	06.9	07.4	07.5	38	32	42	37	NE 2	NNE 6	N 6
22	751.7	751.1	752.5	18.7	25.8	20.4	21.3	26.1	18.0	13.8	09.6	08.2	06.8	60	33	38	44	NW 2	NNE 5	NNE 5
23	753.6	753.2	752.8	17.0	20.0	18.0	18.2	21.5	16.4	16.7	04.7	06.2	06.6	32	35	42	36	NNE 5	NW 2	NNW 2
24	753.2	752.8	752.6	16.0	23.6	18.0	18.9	23.6	14.7	10.0	04.3	05.2	06.7	31	24	43	33	NNE 3	SSW 2	NNW 1
25	753.0	753.0	753.1	14.8	22.3	18.8	18.7	22.5	14.0	12.0	05.3	06.2	05.3	42	31	32	35	NNE 3	SSW 2	NNE 3
26	753.0	752.2	752.5	18.0	24.2	20.3	20.7	25.0	16.0	10.1	04.5	07.5	09.2	29	33	52	38	N 3	SW 3	SW 1
27	754.5	755.7	756.8	18.5	24.4	17.8	19.6	24.8	17.6	12.8	07.4	08.5	06.4	46	37	42	42	NNE 5	S 2	NNE 3
28	757.9	758.2	759.1	13.7	21.8	15.6	16.7	21.8	12.4	09.9	04.1	04.7	04.9	35	24	37	32	NNE 5	NE 4	NNE 5
29	757.7	758.4	758.5	13.4	20.4	16.2	16.6	20.7	12.5	10.9	04.3	04.2	03.1	37	24	23	28	NNE 5	SSW 3	NE 2
30	756.9	755.2	753.4	13.1	20.6	16.4	16.6	21.0	12.4	09.0	03.3	06.7	07.4	29	37	53	40	NNE 2	SSW 2	NE 1
MES. VRED.	751.8	751.6	751.8	20.0	26.0	21.8	22.4	26.5	18.8	15.0	08.7	10.0	10.1	48	39	50	46	3.1	2.7	2.5

1970 OKTOBAR SPLIT MARJAN

1	747.3	743.5	741.8	17.0	16.0	15.2	15.8	18.2	12.9	09.5	09.9	13.1	10.6	68	96	82	82	ESE 6	SE 6	NW 3
2	745.7	746.3	744.9	15.0	19.9	16.5	17.0	20.2	14.3	12.5	05.6	06.5	06.9	44	37	49	43	NNE 4	SW 3	NNE 2
3	741.6	739.9	743.1	16.2	14.8	13.5	14.5	17.6	11.6	12.0	08.4	06.4	04.8	61	50	41	51	ESE 4	NNE 6	NE 3
4	745.9	747.1	749.5	11.6	19.3	16.4	15.9	19.4	11.0	05.8	04.8	05.9	07.8	47	35	56	46	- 0	W 3	N 1
5	752.1	752.2	752.9	13.4	20.0	16.4	16.6	20.5	12.6	07.2	05.6	07.9	10.3	48	45	73	55	NE 2	S 2	SE 2
6	752.7	753.2	753.2	14.4	20.8	17.0	17.3	21.0	14.1	09.7	08.6	08.8	11.0	70	48	76	65	NE 3	SSE 2	E 3
7	752.5	752.4	752.6	15.8	20.6	18.6	18.4	20.7	15.1	11.0	07.9	11.6	13.2	59	64	82	68	NE 2	ESE 5	ESE 4
8	753.8	754.2	754.5	18.0	22.8	18.3	19.4	22.9	17.7	14.3	11.6	13.4	13.9	75	64	88	76	ENE 2	SE 2	NW 2
9	754.9	754.9	755.3	16.6	22.8	19.4	19.6	23.0	16.2	11.5	09.7	10.2	12.2	68	49	72	63	N 3	SSW 2	NW 1
10	756.2	756.9	757.4	17.4	23.3	20.4	20.4	23.5	17.1	11.1	11.3	12.2	12.8	76	57	71	68	- 0	SSW 1	- 0
11	757.8	757.0	756.8	17.4	22.8	19.4	19.8	23.0	16.8	11.4	11.3	14.1	14.8	76	68	87	77	NNE 2	SSW 2	SW 1
12	757.1	756.6	755.9	18.9	22.6	20.4	20.6	23.0	18.6	10.5	10.3	11.7	09.6	63	57	53	58	- 0	S 1	NNE 3
13	755.4	755.6	755.2	18.6	23.8	19.5	20.4	24.3	17.7	15.4	07.3	09.5	08.5	46	43	50	46	NNE 3	SSW 2	ESE 1
14	753.6	752.7	752.1	16.5	21.8	17.8	18.5	22.4	15.9	08.8	08.3	11.3	11.9	59	58	78	65	NE 3	S 2	- 0
15	751.9	751.3	751.9	15.8	20.7	15.8	17.0	21.1	15.4	10.4	08.5	09.0	07.0	63	49	52	55	NNE 2	S 2	NNE 5
16	752.3	752.9	754.5	13.0	15.8	10.8	12.6	16.4	10.6	09.9	05.4	04.9	03.6	48	36	38	41	NNE 5	NNE 6	NNE 6
17	754.0	753.0	753.2	09.6	16.8	11.0	12.1	17.0	09.0	07.7	03.4	05.8	04.1	38	40	42	40	NNE 5	SSW 3	NNE 5
18	751.8	751.5	752.3	10.0	17.3	12.6	13.1	17.5	09.1	07.6	04.0	05.8	04.6	44	39	42	42	NNE 5	NNW 1	NNE 5
19	752.2	750.4	749.3	10.8	17.3	14.0	14.0	17.7	09.0	07.9	04.8	06.7	06.7	50	45	56	50	NNE 2	SSW 2	- 0
20	744.9	741.8	739.7	15.0	19.0	18.2	17.6	19.6	13.0	06.0	09.0	10.0	10.5	71	61	67	66	ESE 5	SSE 6	S 6
21	739.3	743.5	743.7	12.0	15.2	11.2	12.4	18.2	11.2	10.2	08.9	08.4	09.3	84	65	93	81	NW 2	ESE 2	NNW 3
22	746.4	747.1	747.4	11.1	15.1	12.3	12.7	15.4	10.7	09.4	08.4	08.5	06.2	85	66	58	70	NNE 2	SW 1	N 4
23	747.3	747.8	749.8	10.0	13.2	10.0	10.8	13.9	09.7	07.4	05.2	04.8	03.9	57	42	42	47	NNE 4	NNE 3	N 4
24	751.3	753.8	755.9	08.4	10.2	08.4	08.8	10.8	08.0	07.0	04.1	03.6	03.2	49	38	38	42	NNE 7	NNE 6	NNE 7
25	757.5	757.5	757.7	07.3	14.3	12.4	11.6	14.6	06.7	03.8	03.0	05.0	04.0	39	41	37	39	NNE 4	S 2	N 3
26	757.4	756.4	755.7	11.0	17.2	14.0	14.0	17.3	10.4	04.0	05.2	06.7	08.0	53	46	67	55	NE 3	SSW 2	WSW 2
27	755.7	755.9	757.3	12.2	17.4	14.9	14.8	17.5	11.5	05.6	07.9	08.5	08.4	74	57	66	66	W 2	W 2	- 0
28	759.0	759.0	758.8	12.4	18.2	15.0	15.2	18.5	11.8	06.2	06.7	08.1	09.0	62	52	71	62	NNE 2	SSW 2	NW 1
29	758.3	758.6	759.1	12.0	17.8	14.6	14.8	17.8	11.6	05.4	07.4	10.5	10.7	71	69	86	75	NE 3	S 2	WNW 2
30	759.7	759.2	758.9	12.6	18.5	14.8	15.2	19.0	12.2	06.2	08.1	09.6	09.6	74	60	76	70	NE 2	S 3	WNW 1
31	758.3	757.7	758.1	13.1	17.8	15.4	14.9	18.0	12.5	06.2	08.3	10.7	09.3	74	70	76	73	- 0	SSW 3	WNW 2
MES. VRED.	752.4	752.2	752.5	13.6	18.5	15.3	15.7	19.0	12.7	08.8	07.4	08.7	08.6	61	53	63	59	2.9	2.8	2.6

SPLIT MARJAN 1970 SEPTEMBAR

BR. ST. 91 H_s = 122 m H_b = 128 m h_t = 6.5 m h_r = 1.0 m

Dan	Vlažnost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	8	05⊙	07⊙	03	03.3	09.3	15.0	.	
2	7	00⊙	02⊙	00	00.7	10.3	.	.	
3	5	00⊙	02⊙	00	00.7	10.7	.	.	$=^{7^{30}-15}$, $\Delta^{0-1}19^{32}-24$
4	6	06⊙	06⊙	00	04.0	07.6	.	.	$\Delta^{1}0-7$, $=^{5^{30}-15^{30}}$
5	8	01⊙	01⊙	00	00.7	12.3	.	.	
6	7	00⊙	00⊙	00	00.0	10.6	.	.	$\Delta^{2}n-8$, $19^{30}-24$; $=6-12^{30}$, $18-24$
7	6	00⊙	01⊙	00	00.3	10.6	.	.	$\Delta^{1}0-8$, $20^{30}-24$; $=0-24$
8	8	00⊙	00⊙	00	00.0	11.3	.	.	$\Delta^{2}0-7^{30}$ $20-24$; $=0-9$
9	8	00⊙	01⊙	00	00.3	11.0	.	.	$\Delta^{+2}0-6^{30}$
10	8	00⊙	00⊙	00	00.0	11.2	.	.	$=9-10^{30}$
11	8	00⊙	00⊙	01	00.3	11.2	.	.	
12	5	04	04⊙	03	07.0	06.6	.	.	$\infty 5^{30}-8^{30}$, $\bullet^{tr}7^{03}-7^{05}$
13	7	00	02⊙	00	03.3	10.5	00.0	.	
14	7	00⊙	01⊙	00	00.3	11.0	.	.	$=^{5^{30}-9}$
15	8	02⊙	01⊙	00	01.0	10.5	.	.	$\Delta^{0}n-7^{30}$
16	8	00⊙	04⊙	00	01.3	10.6	.	.	$=n-10^{45}$
17	8	00⊙	10●	10	09.3	01.4	.	.	F-FNNE $2^{05}-24$, $\bullet^{tr}13^{35}-14$
18	8	09	09	10	09.3	02.8	00.0	.	FNNE $0-24$, $\bullet^{tr}3^{45}-4$
19	3	03⊙	00⊙	00	01.0	10.3	.	.	FNNE $0-7^{45}$ $20^{40}-21^{28}$
20	8	09	05⊙	00	04.7	07.6	.	.	FNNE $3^{40}-6^{05}$, $15^{30}-24i$
21	3	01⊙	04⊙	00	01.7	10.0	.	.	F-FNNE $0-2^{40}$, $8^{15}-22^{40}i$
22	8	00⊙	04⊙	00	01.3	09.9	.	.	FNNE $11^{20}-24i$
23	8	09	09	00	04.0	01.1	.	.	FNNE $0-7^{30}$ $\bullet^{tr}7^{45}8^{15}$
24	5	00⊙	00⊙	00	00.0	10.6	00.0	.	FNNE $0^{15}-6^{05}$
25	5	00⊙	00⊙	00	00.0	10.6	.	.	FNNE $0-5^{30}i$
26	9	00⊙	01⊙	00	00.3	10.3	.	.	
27	9	09	04⊙	00	04.7	09.3	.	.	FNNE $5^{40}-9^{30}$
28	5	03⊙	01⊙	00	04.3	10.5	.	.	F-FNNE $6^{30}-10^{41}$, $18^{55}-24$
29	5	00⊙	01⊙	00	00.3	10.4	.	.	FNNE $0-9$
30	8	00⊙	00⊙	00	00.0	10.5	.	.	
MES. VRED.		02.8	02.9	01.1	02.3	280.7	15.6		

SPLIT MARJAN 1970 OKTOBAR

Dan	Vlažnost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
1	6	10	10●	07	09.0	00.0	.	.	FESE-SE-N $6^{30}-17^{25}$, $23^{40}-24$; $\bullet^{tr-0-1}10^{25}-20i$, $\Delta^{1}17^{20}-17^{50}$, Γ^{0}w $17^{15}-19$
2	9	01⊙	03⊙	09	04.3	09.9	39.9	.	F-FNNE $0-9^{30}$
3	9	10	02⊙	00	04.0	04.2	.	.	$\bullet^{0-2}7^{04}-11^{45}$, FESE $7^{40}-20i$, Γ^{0}NW $9^{45}-11^{30}$
4	9	01⊙	03⊙	00	02.0	10.6	13.0	.	
5	9	04⊙	04⊙	00	04.0	09.3	.	.	
6	9	08⊙	02⊙	00	03.3	10.2	.	.	
7	8	00⊙	03⊙	01	01.3	10.1	.	.	
8	3	03⊙	01⊙	00	01.3	10.1	.	.	$\Delta^{+2}n-8^{30}$ $19-24$
9	9	00⊙	00⊙	00	00.0	10.0	.	.	$\Delta^{2}0-9$, $19^{30}-24$
10	7	00⊙	00⊙	00	00.0	09.5	.	.	$\Delta^{+2}0-9$, $=5^{30}-15$
11	7	00⊙	00⊙	00	00.0	09.8	.	.	$\Delta^{+2}0-10$, $18^{30}-24$; $=n-9$, $17^{30}-24$
12	8	00≡	00⊙	00	00.0	10.0	.	.	$\Delta^{0}0-9^{30}$, $=0-5$, $\equiv 5-8^{30}$, $\equiv^{1}8^{30}-11^{30}i$
13	5	00⊙	00⊙	00	00.0	09.7	.	.	
14	5	00⊙	01⊙	05	02.0	09.5	.	.	$\Delta^{0-2}n-8$, $20-24$; $=7^{30}-17^{30}$
15	8	08⊙	10⊙	09	09.0	03.5	.	.	$\Delta^{+2}0-7^{30}$, $=n-8$, $\oplus 13-14^{45}$, FNNE $17^{30}-24$
16	8	09	01⊙	00	03.3	06.6	.	.	F-FNNE $0-24$
17	8	00⊙	01⊙	00	00.3	09.9	.	.	F $0-7^{25}i$, $17^{05}-24i$
18	8	00⊙	00⊙	00	00.0	10.0	.	.	FNNE $0-8^{20}$
19	9	00⊙	03⊙	01	02.0	09.9	.	.	$\Delta^{0-1}19^{30}-n$
20	8	09	[illegible]	09	08.7	06.9	.	.	FESE-SSE $5-24i$
21	5	10●	03⊙	10●	09.3	01.0	08.4	.	FSSE $0-6^{25}i$, $\bullet^{0-1}2^{30}-9^{12}i$, $18^{05}-21^{45}i$; Γ^{0} $20^{10}-20^{35}$
22	5	09●	10	09	09.3	01.0	13.5	.	$\bullet^{0-1}5^{20}-7^{20}i$
23	6	09	09	00	05.7	04.7	00.1	.	FNNE $3^{30}-5^{45}i$, $\bullet^{0}5^{10}-5^{12}$, $17^{02}-17^{08}$
24	5	03⊙	03⊙	00	02.0	09.6	00.5	.	FNNE $1^{48}-24$
25	9	00⊙	01⊙	00	00.3	09.9	.	.	FNNE $0-6^{40}$
26	8	03⊙	04⊙	00	02.5	09.2	.	.	
27	5	00⊙	03⊙	00	01.0	08.4	.	.	$\Delta^{1}n-8$
28	8	07⊙	03⊙	00	04.0	08.7	.	.	$=n-11$, $\Delta^{1}19^{30}-24$
29	7	03⊙	07⊙	00	04.0	04.8	.	.	$\Delta^{2}0-8^{30}$ $=12-14^{30}$
30	5	00⊙	07⊙	00	00.0	08.9	.	.	$\Delta^{1}n-8^{30}$ $20-24$; $=n-24$
31	7	00⊙	03⊙	00	00.5	08.2	.	.	$\Delta^{2}0-9$, $18^{30}-24$; $=^{1}0-11^{30}$
MES. VRED.		003.5	03.6	01.9	03.0	244.1	75.4		

φ = 43° 31' N λ = 16° 26' E Gr. ΔG = + 1h 06 min. BR. ST. 91

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	757.6	757.0	756.4	13.5	16.4	15.0	15.0	17.2	12.4	08.3	08.8	08.7	07.4	76	62	58	65	W 1	NW 1	NW 2
2	756.0	755.5	755.3	13.4	18.4	14.7	15.3	18.5	12.2	09.8	08.2	08.4	08.7	71	53	69	64	WNW 2	WSW 2	- 0
3	755.0	753.9	753.6	12.2	17.0	14.1	14.4	17.3	11.8	06.9	08.6	09.9	10.7	80	68	89	79	NNE 2	SSE 1	SSE 1
4	754.3	754.1	754.3	12.6	17.8	15.0	15.1	18.0	12.5	07.3	09.2	11.1	10.5	84	73	82	80	N 2	SSW 1	WSW 1
5	754.4	753.0	751.9	12.6	17.6	15.2	15.2	17.7	12.3	07.3	09.3	10.2	11.6	85	67	90	81	NE 2	S 2	- 0
6	748.9	747.5	750.0	15.1	16.4	12.2	14.0	16.5	10.5	12.0	09.7	09.3	04.0	75	66	38	60	NNE 1	NNW 2	NE 6
7	751.6	751.4	752.1	09.2	15.0	12.4	12.2	15.0	09.1	07.3	03.3	03.7	04.2	38	29	39	35	NNE 4	SW 2	E 2
8	752.1	752.9	754.6	09.2	11.4	12.4	11.4	12.5	08.6	07.4	07.4	08.8	08.6	85	88	79	84	NE 3	NNE 4	NNE 2
9	752.6	750.0	748.9	11.4	14.8	13.0	13.0	15.0	10.6	09.6	08.7	11.3	09.3	86	90	83	86	NNE 2	NNW 1	NE 2
10	746.0	746.3	749.7	12.6	15.2	12.2	13.0	15.6	11.5	10.6	09.2	04.7	03.9	84	36	37	52	NNW 1	NNE 5	NNE 4
11	753.4	754.8	756.1	10.4	14.4	11.7	12.0	14.6	10.2	04.0	04.2	05.9	06.4	45	48	62	52	NNE 4	S 2	NW 2
12	756.2	755.8	755.6	10.6	15.0	12.0	12.4	15.0	09.6	03.4	06.3	07.8	08.4	66	61	80	69	N 1	SSW 2	E 2
13	755.1	754.1	753.3	09.4	14.6	13.4	12.7	15.0	09.2	06.2	06.3	08.0	07.5	71	65	65	67	NE 2	ESE 4	ESE 5
14	749.9	747.9	745.2	15.0	14.7	16.4	15.6	16.4	12.6	10.7	09.7	11.4	11.6	76	91	83	83	ESE 6	ESE 6	SE 6
15	743.0	741.3	739.6	15.0	15.4	11.4	13.3	17.0	11.1	12.5	10.7	09.3	09.2	84	71	91	82	SSE 4	SSE 6	SSW 3
16	738.9	740.5	743.6	08.6	03.6	09.4	09.0	12.0	07.4	06.3	06.3	07.5	04.5	75	90	51	72	NNE 2	NW 2	N 4
17	748.5	750.5	751.8	07.5	12.0	10.5	10.1	12.6	06.8	04.3	04.2	05.2	06.0	54	50	63	56	NNE 3	SSE 1	E 3
18	752.4	752.8	752.9	11.1	13.4	13.4	12.8	14.0	09.6	07.9	06.7	08.0	10.1	68	69	87	75	ENE 2	E 4	ESE 5
19	750.8	750.0	749.3	14.7	17.0	16.2	16.0	17.2	13.2	12.1	11.0	10.7	10.9	88	74	79	80	ESE 5	ESE 5	ESE 6
20	749.7	749.3	750.0	16.0	17.2	16.2	16.4	17.5	15.4	14.5	10.7	11.3	10.8	79	77	78	78	ESE 6	ESE 4	ESE 4
21	749.5	747.6	743.0	15.8	15.4	14.6	15.1	17.0	14.4	13.5	11.3	12.3	11.7	84	94	94	91	ESE 5	E 6	ESE 6
22	742.2	743.4	746.1	12.0	08.8	09.6	10.0	14.6	08.0	06.8	08.4	07.4	05.2	80	88	58	75	SE 5	WNW 5	N 4
23	749.4	750.2	752.2	10.2	11.0	10.0	10.3	11.9	09.1	06.4	04.5	04.7	04.9	48	48	53	50	NNW 3	NNW 3	NNE 5
24	753.1	753.8	754.5	10.6	15.4	12.4	12.7	15.6	09.4	07.2	05.8	06.2	05.8	61	47	54	54	S 2	W 2	ENE 2
25	755.2	756.0	756.7	08.7	14.0	12.0	11.7	14.2	08.6	04.0	05.3	07.2	06.0	62	60	57	60	NNE 3	SSW 1	NNE 1
26	757.2	757.1	757.5	08.8	13.8	12.6	12.0	14.2	08.3	04.6	05.0	06.0	06.8	59	51	62	57	NNE 3	SSW 2	N 2
27	757.0	756.5	756.6	12.6	17.0	13.8	14.3	17.0	10.3	03.2	04.1	06.4	04.3	38	44	36	39	N 2	SSW 1	NE 3
28	756.2	755.3	755.6	11.2	14.2	11.6	12.2	14.6	10.3	04.8	04.2	06.0	05.4	42	49	53	48	NNE 3	SSE 1	NE 1
29	755.0	754.7	755.0	09.2	14.2	12.0	11.8	14.5	08.5	02.6	05.8	06.5	09.5	67	70	90	76	NNE 3	SE 1	E 2
30	754.8	752.5	751.2	12.8	15.0	14.6	14.2	15.2	11.0	07.7	08.9	09.5	09.9	81	74	80	78	ESE 5	ESE 6	ESE 5
MES. VRED.	751.9	751.5	751.8	11.7	14.7	13.0	13.1	15.4	10.5	07.6	07.4	08.2	07.8	70	65	68	68	3.0	2.8	3.0

1	751.9	751.5	751.4	13.4	16.8	11.6	13.1	15.9	11.0	12.2	10.4	10.8	08.9	90	80	86	85	NE 2	E 3	NE 3
2	751.4	751.5	752.4	11.0	17.1	11.4	12.2	15.6	10.3	05.3	07.1	07.2	07.7	72	56	77	68	N 1	SSW 2	WNW 1
3	752.3	751.6	750.6	09.0	12.6	10.4	10.6	12.7	08.3	04.2	06.2	07.7	06.4	72	70	68	70	NNE 3	SW 1	WNW 2
4	751.7	754.6	757.1	09.4	12.4	08.8	09.8	12.5	08.5	03.7	06.6	02.8	02.2	75	26	26	42	SSW 1	SSE 1	NNE 2
5	756.7	756.2	756.4	07.2	11.4	10.6	10.0	11.7	06.9	-00.5	02.9	06.2	06.7	38	62	70	57	NW 2	S 2	N 2
6	757.5	758.7	758.9	09.6	12.0	08.2	09.5	12.2	08.1	06.8	04.2	04.2	03.9	47	40	48	45	NNE 5	NNE 3	NNE 2
7	758.4	757.3	757.4	05.6	11.2	09.2	08.8	11.5	05.3	03.5	03.8	05.8	04.7	56	58	54	56	NNE 3	ESE 2	ENE 2
8	758.4	759.8	761.5	11.0	10.2	08.8	09.7	11.6	08.5	07.7	05.9	07.9	07.5	60	85	89	78	E 4	NNE 4	ENE 3
9	762.4	762.1	761.7	08.8	12.4	11.2	10.9	12.6	08.2	06.5	04.7	05.0	03.6	56	46	36	46	NNE 5	S 2	NNE 4
10	760.2	759.1	759.6	09.1	13.4	12.2	11.7	13.4	08.2	01.2	03.6	04.3	04.9	41	37	46	41	N 2	WNW 1	NNE 3
11	761.1	761.6	762.0	11.8	14.2	11.6	12.3	14.5	08.1	06.5	03.7	04.1	05.3	36	34	52	41	NNE 6	WNW 1	NE 1
12	760.4	760.4	760.3	09.0	12.6	11.2	11.0	13.1	08.5	02.2	03.8	04.7	06.0	44	43	60	49	NE 3	SSE 1	- 0
13	759.6	759.6	759.2	08.2	12.2	09.9	10.0	12.5	07.0	06.0	04.4	06.4	07.1	54	60	78	64	NNE 2	SSE 1	NE 2
14	758.4	757.4	756.3	08.4	12.2	09.9	10.1	12.2	08.0	04.1	05.2	06.8	06.1	63	64	66	64	NNE 3	E 2	NNE 3
15	754.5	753.5	755.4	09.6	11.6	08.1	09.4	11.9	08.1	06.5	06.1	03.8	04.2	68	37	52	52	NNE 4	NNE 5	NNE 7
16	754.1	755.2	756.5	06.5	08.8	06.8	07.2	09.0	05.8	05.2	03.0	02.6	02.2	42	31	30	34	NNE 5	NNE 5	NNE 6
17	757.2	757.6	757.5	05.1	09.0	06.2	06.6	09.4	04.6	02.5	02.7	03.6	03.0	41	42	42	42	NNE 5	S 2	NNE 3
18	756.0	754.8	753.3	05.0	09.0	06.8	06.9	09.2	03.5	00.2	02.9	05.0	04.1	45	58	55	53	N 2	SSW 2	NNE 3
19	756.3	756.3	757.1	05.4	09.5	05.4	06.4	09.6	04.0	00.6	02.9	03.7	03.1	43	42	46	44	NNE 5	ESE 2	NNE 5
20	758.1	757.3	756.8	03.8	09.0	06.5	06.4	09.0	03.4	01.2	02.9	04.2	03.0	47	48	41	45	NNE 4	S 2	- 0
21	753.4	750.5	748.4	04.2	10.0	08.2	07.6	10.0	04.0	01.5	03.5	05.2	03.6	57	57	45	53	NNE 5	WSW 1	NE 3
22	745.5	744.5	742.9	07.6	04.0	05.0	05.4	08.5	03.2	05.6	03.1	04.5	03.2	40	73	49	54	NNE 5	NNE 6	NNE 5
23	737.7	739.2	742.3	04.0	02.3	02.3	02.7	06.0	01.6	00.9	04.1	04.4	04.6	68	82	85	78	NNE 6	NNE 5	SSW 5
24	746.8	748.1	746.7	01.4	04.8	04.0	03.6	05.8	00.8	-02.5	03.7	05.7	04.7	73	88	78	80	NNE 2	NE 2	NNE 5
25	743.3	741.8	743.9	06.8	05.7	05.0	05.6	08.0	00.9	02.2	06.8	06.3	06.2	92	92	94	93	NNE 3	NNE 3	- 0
26	746.3	751.0	751.7	05.0	08.4	04.5	05.6	08.5	03.0	00.5	03.3	05.0	03.8	50	61	60	57	- 0	ESE 2	NNE 4
27	748.9	748.0	744.7	09.0	11.0	12.3	11.2	12.3	04.5	03.0	07.3	08.9	10.0	85	91	93	90	ESE 7	ESE 7	SSE 8
28	741.6	743.8	746.7	14.0	12.2	10.6	11.8	14.4	10.4	12.0	09.8	07.7	06.0	81	72	63	72	SSE 7	SW 3	S 3
29	745.9	742.3	740.3	12.6	13.2	14.0	13.4	14.4	10.4	04.6	06.8	10.4	11.0	62	91	92	82	SE 5	SSE 6	ESE 7
30	736.6	738.1	741.6	14.2	10.6	10.3	11.4	14.5	10.0	13.2	10.8	08.2	04.9	89	86	52	76	ESE 6	W 2	WSW 3
31	740.8	736.3	722.7	10.8	13.0	12.1	12.0	13.4	09.6	04.3	07.3	08.4	09.5	75	75	90	80	ESE 4	ESE 6	SSE 5
MES. VRED.	752.4	751.9	752.4	08.3	10.6	09.3	09.1	11.5	06.6	04.2	05.1	05.8	05.4	60	61	62	61	3.7	2.9	3.3

BR. ST. 91 H_s = 122 m H_b = 128 m h_t = 6.5 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dan		7	7	
1	7	10	10	09	09.7	01.6	.	.	$\triangle^{1}$ 0-9
2	7	09	01⊙	00	03.3	07.5	.	.	$\triangle^{0-1}$ 21-24
3	6	05⊙	08⊙	00	04.3	03.0	.	.	$\triangle^{0-1}$ 0-9, 18^{30}-24; = n-24
4	6	08	08	10	08.7	00.6	.	.	$\triangle^{2}$ 0-8, = 0-n
5	6	03⊙	07⊙	10	06.7	07.4	.	.	$\triangle^{2}$ n-8^{30} 21-24; = n-24
6	7	10	10	07	09.0	00.1	.	.	$\triangle^{0-1}$ 0-9, = 0-12, F-FNNE 16-24
7	9	02⊙	00⊙	09	03.7	08.9	.	.	
8	7	10●	10●	10	10.0	00.0	03.7	.	●$^{0-1}$ 2^{40}-15^{40} i
9	7	10	10	09	09.7	00.7	03.2	.	●$^{0-1}$ n-6^{30} 9^{45}-12^{45} 15^{40}-16^{40}; ℞^{1} NW 10^{17}-11^{30}, 15^{55}-16^{30}
10	8	10	07⊙	00	05.7	06.2	34.5	.	●$^{1-2}$ 2^{20}-8^{50}, ℞^{1} w n-5^{45}, FNNE 12^{30}-23^{32} i
11	9	00⊙	01⊙	00	00.3	09.1	00.2	.	
12	8	00⊙	01	00	00.3	08.8	.	.	$\triangle^{0-1}$ n-8^{30} 19-24
13	8	06	08	09	07.7	05.5	.	.	$\triangle^{1}$ 0-8, FSSE 19^{20}-24 i
14	7	08	10●	10	09.3	03.5	.	.	FESE 0-24, ●^{0} 11-19 i
15	8	06⊙	10●	10●	09.3	00.0	00.7	.	F-FSSE 0-4^{25}, 10^{30}-20^{40}; ●^{0} 13^{55}-24 i
16	7	10	10●	09	09.7	00.0	18.5	.	●$^{0-2}$ 0-3^{30}, 10^{20}-16^{40} i; ▲ 11^{30}-11^{32}
17	8	01⊙	08⊙	03	04.0	08.3	17.7	.	
18	8	10	09	09	09.3	00.2	.	.	●^{0} 7^{45}-9^{30} i, 13^{05}, 16^{50}-20^{30}; FESE 17^{45}-24 i
19	8	07	08⊙	09	08.0	06.4	00.8	.	FESE 0-24 i
20	8	09	08⊙	08	08.3	01.2	.	.	FESE 0-13^{30}
21	8	08	10	10●	09.3	00.5	.	.	FESE 6^{22}-24, ●$^{0-2}$ 12^{40}-16^{30}, 19^{05}-24 i
22	7	09	09●	02	06.7	00.6	23.7	.	FS-W-SSW-WSW 0-1^{50}, 6^{50}-8^{45}, 11^{57}-13^{42} i; ●$^{0-1}$ 0-2, 8^{35}-18^{05} i; ▲^{1} 8^{35}-8^{36}
23	9	07	06⊙	07	06.7	05.1	09.9	.	FNNE 17^{42}-24
24	9	01⊙	00⊙	00	00.3	08.2	.	.	FNNE 0-6^{40}
25	8	01	02⊙	00	01.0	08.3	.	.	
26	8	00	00⊙	00	00.0	08.5	.	.	$\triangle^{0-2}$ 20-24
27	8	01⊙	00⊙	00	00.3	08.6	.	.	$\triangle^{0-2}$ 0-9, = n-12
28	8	08	03	00	03.7	08.2	.	.	
29	8	05	04⊙	00	03.0	07.5	.	.	$\triangle^{2}$ 20-24
30	8	09	10	10	09.7	00.0	.	.	$\triangle^{2}$ 0-7^{30}
MES. VRED.		06.2	06.3	05.3	05.9	139.7	112.9		

1	8	10	09	06●℞	08.3	00.7	01.6	.	●^{0} 3^{50}-6^{35} 19^{23}-21^{46}; ℞^{1} w 19^{42}-n
2	8	02	02⊙	00	01.3	08.0	03.1	.	●^{1} 3^{50}-4^{20}
3	8	03	09	00	04.0	05.7	.	.	= n-9^{50}
4	9	05	01⊙	00	02.0	07.3	.	.	FN-NE 7-17^{29} i
5	8	03	06⊙	10●	06.3	04.7	.	.	●$^{0-2}$ 20^{45}-24
6	9	10	01⊙	00	03.7	05.0	06.7	.	●$^{0-1}$ 0-2^{40}
7	8	06	07⊙	09	07.3	06.2	.	.	
8	8	09	10●	10●	09.7	00.0	.	.	●$^{0-1}$ 10^{45}-24 i, FNNE 23^{10}-24
9	9	03	00●	00	01.0	08.4	03.6	.	FNNE 1^{30}-9^{05} i
10	8	01	02⊙	01	01.3	08.4	.	.	
11	8	03	04⊙	00	02.3	08.3	.	.	FNNE 6-7^{30}
12	8	00	00⊙	00	00.0	07.2	.	.	$\triangle^{1-2}$ 20-24
13	8	00	00⊙	00	00.0	08.2	.	.	$\triangle^{1-2}$ 0-7^{30}
14	8	09	09⊙	09	09.0	03.5	.	.	$\triangle^{0-2}$ 0-8, ⊕ 12^{30}-14^{30}
15	8	09	09	10	09.3	01.3	.	.	FNNE 14^{10}-24
16	8	10	02⊙	00	04.0	04.5	.	.	FNNE 0-24
17	8	01	00⊙	00	00.3	08.2	.	.	FNNE 0-9
18	8	00	08⊙	00	02.7	06.0	.	.	
19	8	02	00⊙	00	00.7	08.2	.	.	
20	8	00	00⊙	00	00.0	08.1	.	.	
21	8	00	01⊙	10	03.7	07.9	.	.	= n-8
22	7	10	09	10	09.7	00.0	.	.	FNNE 6^{33}-24, ●^{0} 10^{02}-13^{40} i; 23^{02}-23^{50}
23	7	10●	10●	09	09.7	01.0	00.5	.	FNNE 0-20, ●^{3} 24-18^{40} i, ℞ 11^{35} ▲$^{1-2}$ 12^{05}-13^{40} i
24	8	10✱	10	10	10.0	01.4	09.2	.	≡ n, ✱$^{1-2}$ 6^{50}-7^{40} ●$^{0-1}$ 12^{05}-12^{20}, 18^{05}-24 i; FS 12^{09}-12^{12}
25	6	10●	10●	10	10.0	00.0	49.4	.	℞^{4} N n, ●$^{1-2}$ 0-18^{45}
26	8	10	01⊙	00	03.7	04.6	31.0	.	
27	7	10●	10●	10●	10.0	00.0	00.9	.	FE-ESE 1^{08}-24, ●$^{0-1}$ 4^{05}-16^{40} i, 19^{40}-24
28	8	10	06⊙	02	06.0	02.7	04.9	.	FSE 0-9^{45} ●$^{0-1}$ n, 7^{45}-12^{10} i; ▲ 9^{50}-10^{25}, ℞^{0} 9^{58}-11^{50} i; ▽ 10^{25}-11^{20}, ▲^{1} 11^{22}-11^{32}
29	7	10	10●	10	10.0	00.0	05.7	.	●^{0} n-a, 13^{30}-20^{30}; FSE-ESE 6^{42}-24
30	7	10	10●	00	06.7	01.3	07.7	.	FESE 0-11^{53} ●$^{0-2}$ 7^{40}-14^{20} i
31	9	10	10	10	10.0	00.0	05.0	.	FSE 8^{30}-16^{50}, ▽$^{1-2}$ 17^{40}-18^{30}, ℞SW 17^{50}, 23^{40}; ●$^{1-2}$ 23^{30}-n
MES. VRED.		06.0	05.4	04.4	05.2	136.8	129.1		

$\varphi = 43^\circ\ 43'$ N $\lambda = 18^\circ\ 16'$ E Gr. $\Delta t =$ + 1h 13 min. BR. ST. 142

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	578.7	575.8	578.8	-01.8	-02.0	-03.0	-02.4	-01.2	-03.0	-	03.9	03.9	03.6	98	98	97	98	SSW 8	S 10	SW 3
2	579.5	580.3	583.0	-04.4	-03.8	-08.0	-06.0	-02.6	-08.0	-	03.2	03.3	02.3	96	96	92	95	- 0	WSW 4	WSW 3
3	584.0	584.1	584.6	-03.0	-03.2	-02.8	-03.0	-01.8	-09.0	-	03.2	03.1	03.2	87	85	86	86	SW 7	SW 9	SW 10
4	586.0	583.8	584.3	-03.2	-03.0	-02.4	-02.8	-02.0	-04.6	-	03.4	03.4	03.8	93	93	98	95	SW 9	SW 11	SSW10
5	583.7	580.0	579.4	-01.8	00.0	00.2	-00.4	00.8	-03.0	-	03.9	04.6	04.7	98	100	100	99	SSW10	SSW12	SSW14
6	581.1	583.4	584.6	00.2	00.1	00.0	00.1	00.6	-00.2	-	04.7	04.6	04.6	100	100	100	100	SSW10	SW 8	SSW 8
7	581.6	584.2	587.5	-01.0	-00.2	-07.2	-03.9	00.4	-08.0	-	04.3	04.5	02.5	100	100	93	98	ESE 6	SSW 6	N 2
8	590.0	591.3	593.9	-12.6	-08.6	-05.0	-07.8	-03.4	-15.4	-	01.5	02.2	03.0	88	92	95	92	NNE 5	SW 3	- 0
9	594.3	595.0	595.7	-01.8	-01.4	00.4	-00.6	00.6	-05.4	-	01.4	02.2	04.7	34	52	100	62	SW 5	SW 4	NW 3
10	596.2	593.8	594.2	01.4	00.6	-01.0	00.0	01.6	-01.2	-	05.1	01.7	02.7	100	36	63	66	- 0	SSW 5	SSW 7
11	592.6	589.9	587.5	-02.0	-01.6	-02.2	-02.0	-00.6	-03.0	-	04.0	04.1	03.8	100	100	98	99	SSW 6	SW 11	SW 13
12	584.9	584.3	584.7	-00.2	00.6	00.0	00.1	00.6	-03.2	-	04.5	04.8	04.6	100	100	100	100	S 10	S 9	S 6
13	583.9	584.3	585.3	-00.8	-00.6	-00.6	-00.6	00.2	-02.2	-	04.3	04.4	04.4	100	100	100	100	S 6	S 7	SW 6
14	585.2	586.2	587.0	-00.8	-01.4	-01.8	-01.4	-00.4	-02.5	-	04.3	04.1	03.9	99	99	98	99	SSW 6	SSW 5	SW 5
15	585.9	585.6	584.3	-02.6	-01.0	-01.0	-01.4	-00.1	-03.4	-	03.7	04.2	04.2	97	99	99	98	SW 8	SSW 9	SSW 9
16	581.5	580.4	581.1	00.0	-00.4	-00.6	-00.4	00.6	-02.4	-	04.6	04.5	04.4	100	100	100	100	SSW12	SW 11	SW 7
17	581.9	582.5	581.6	-07.0	-07.0	-07.0	-07.0	-00.4	-08.8	-	02.5	02.5	02.5	93	93	93	93	NW 3	NNE 7	N 9
18	584.4	583.7	586.9	-09.0	-09.6	-10.2	-09.8	-06.6	-11.2	-	02.1	02.0	01.9	92	91	90	91	N 11	N 12	NNW 8
19	584.3	585.8	586.9	-13.6	-13.0	-16.0	-14.6	-10.0	-17.0	-	01.4	01.5	01.1	88	88	85	87	N 7	N 9	N 7
20	588.3	589.4	590.2	-15.0	-12.0	-10.8	-12.2	-10.6	-17.4	-	01.2	01.6	01.8	86	89	90	88	NE 7	NNE 7	NE 6
21	589.3	589.0	588.9	-09.2	-06.0	-05.2	-06.4	-04.4	-12.0	-	02.1	02.8	03.0	91	94	95	93	N 5	SSE 3	S 2
22	588.7	588.4	589.0	-05.4	-07.8	-04.8	-05.7	-04.0	-09.8	-	02.9	02.4	03.1	95	93	95	94	SSE 3	E 2	SE 2
23	589.3	589.8	590.6	-06.2	-07.2	-04.4	-05.6	-03.6	-09.2	-	02.7	02.5	03.2	94	93	96	94	SSW 1	SW 2	WSW 2
24	590.9	592.2	592.4	-08.2	-09.0	-04.6	-06.6	-03.6	-10.4	-	02.3	02.1	03.1	92	92	96	93	NW 4	NW 3	SW 6
25	590.4	592.0	593.4	-06.0	-04.2	-06.0	-05.6	-03.8	-07.4	-	02.8	03.2	02.8	94	96	94	95	SW 11	SW 7	W 4
26	594.2	595.6	596.4	-05.0	-03.2	-03.4	-03.8	-02.2	-07.0	-	01.7	03.4	03.5	53	93	97	81	NW 4	W 5	WNW 2
27	596.5	595.4	594.0	-02.8	-03.2	-03.0	-03.0	-01.2	-06.0	-	03.5	03.5	03.6	93	97	97	96	WSW 5	SW 7	SW 8
28	592.1	590.6	589.7	-02.2	-01.8	-06.0	-04.0	-01.0	-08.6	-	03.8	03.9	02.8	98	98	94	97	SW 7	SW 3	SW 3
29	588.1	587.9	588.8	-10.2	-11.0	-10.0	-10.3	-06.0	-12.6	-	01.9	01.8	01.9	90	90	91	90	N 8	N 6	N 5
30	586.3	584.5	584.3	-06.0	-05.8	-05.0	-05.4	-04.4	-12.0	-	02.8	02.8	03.0	94	94	95	94	SW 9	SW 8	SW 6
31	583.4	583.6	584.0	-03.8	-04.4	-08.4	-06.2	-03.4	-11.2	-	03.3	03.2	02.2	96	96	92	95	SSW 5	N 3	N 3
MES. VRED.	587.0	586.9	587.5	-04.6	-04.2	-04.5	-04.5	-02.3	-07.6	-	03.1	03.2	03.2	92	92	94	92	6.4	6.7	5.8

1	584.2	583.5	583.5	-14.2	-11.0	-07.0	-09.8	-07.0	-15.2	-	01.3	01.8	02.5	87	90	93	90	N 5	- 0	SW 3
2	584.4	584.0	584.8	-08.2	-04.0	-08.0	-07.0	-03.0	-11.0	-	02.3	03.3	02.3	92	96	92	93	SSW 4	SSW 7	SSW 6
3	583.7	582.6	584.3	-05.0	-06.4	-04.0	-04.8	-03.6	-09.2	-	02.6	02.7	03.3	82	94	96	91	SW 8	SSW 9	SSW 9
4	588.1	586.5	587.0	-04.0	-01.8	-01.0	-02.0	-00.8	-04.8	-	03.3	03.9	04.2	96	98	99	98	SSW 1	SW 7	SSW10
5	584.8	581.8	581.7	-01.4	-01.8	-01.4	-01.5	-00.6	-02.4	-	04.1	03.9	04.1	99	98	99	99	SSW12	SSW13	SSW14
6	584.0	587.5	590.1	-02.0	-01.6	-02.4	-02.1	-01.0	-03.2	-	03.9	04.0	03.8	98	98	98	98	SSW11	SW 9	SW 6
7	589.0	589.5	589.7	-02.4	-03.2	-03.6	-03.2	-01.6	-04.6	-	03.8	03.5	03.4	98	97	97	97	SW 6	WSW 2	SW 3
8	588.0	588.0	588.5	-05.0	-03.0	-04.4	-04.2	-02.6	-06.4	-	03.0	03.6	03.2	95	97	96	96	SW 6	SW 8	SW 9
9	587.7	585.3	583.4	-04.0	-02.0	-02.0	-02.5	-01.4	-05.0	-	03.3	03.9	03.9	96	98	98	97	SW 9	S 11	SSW11
10	581.6	577.6	580.6	-02.0	-01.8	-01.2	-01.6	-01.2	-03.0	-	03.9	03.9	04.2	98	98	99	98	SSW13	SW 13	WSW10
11	582.8	580.9	573.8	-04.2	-04.0	-03.5	-03.8	-01.0	-09.0	-	03.1	03.3	03.4	92	96	97	95	WSW 7	S 7	S 13
12	581.4	585.2	585.1	-13.0	-13.0	-05.0	-09.0	-02.4	-13.6	-	01.5	01.5	02.9	88	88	91	89	N 9	N 2	WSW 7
13	583.8	582.6	583.2	-05.0	-03.8	-03.0	-03.7	-02.0	-05.6	-	02.7	03.3	03.6	87	96	97	93	SSW10	SSW11	W 8
14	583.0	584.6	578.2	-03.2	-03.4	-03.0	-03.2	-02.8	-04.6	-	03.5	03.5	03.6	97	97	97	97	SW 6	S 8	SW 12
15	576.2	576.1	577.2	-03.6	-04.0	-04.6	-04.2	-02.0	-05.4	-	03.4	03.3	03.1	97	96	96	96	S 12	SW 10	SW 8
16	579.4	580.8	580.8	-10.6	-05.0	-12.0	-09.9	-04.0	-12.2	-	01.8	03.0	01.6	90	95	89	91	SW 1	SSW 2	N 2
17	579.6	582.1	587.6	-20.0	-19.0	-18.0	-18.8	-12.0	-20.4	-	00.8	00.9	00.9	82	83	84	83	N 9	N 10	N 4
18	587.0	585.2	582.5	-10.0	-08.0	-07.0	-08.0	-07.0	-18.2	-	01.9	02.3	02.5	91	92	93	92	SW 4	SW 9	SSW10
19	584.0	586.3	587.4	-14.8	-14.4	-14.6	-14.6	-07.0	-15.4	-	01.3	01.3	01.3	86	87	87	87	N 8	N 8	N 10
20	588.2	590.0	589.0	-16.0	-13.0	-07.2	-10.8	-07.0	-16.6	-	01.1	01.5	02.5	85	88	93	89	N 8	N 4	N 5
21	587.9	588.1	588.0	-09.0	-09.8	-09.4	-09.4	-06.8	-10.8	-	02.1	02.0	02.1	92	91	91	91	N 5	NNE 5	W 2
22	587.0	587.6	588.1	-05.8	-05.0	-05.0	-05.2	-03.0	-10.0	-	02.7	03.0	03.0	90	95	95	93	NNE 7	WSW 6	W 6
23	583.4	582.6	581.4	-04.8	-03.4	-06.2	-05.2	-03.0	-07.0	-	03.1	03.5	02.7	95	97	94	95	SW 11	SW 8	NNE 9
24	583.0	583.0	582.8	-10.0	-09.2	-09.6	-09.6	-06.2	-10.8	-	01.9	02.1	02.0	91	91	91	91	NE 7	NE 4	NE 6
25	580.4	581.4	581.4	-12.6	-12.0	-13.0	-12.6	-09.4	-13.4	-	01.5	01.6	01.5	88	89	88	88	NE 9	NNE 7	NNE 7
26	581.3	582.2	582.6	-14.0	-12.6	-12.4	-12.8	-12.0	-14.4	-	01.4	01.5	01.6	87	88	89	88	N 6	NNW 4	NW 3
27	580.2	579.5	580.5	-14.0	-12.6	-14.4	-13.8	-12.0	-14.6	-	01.4	01.5	01.3	87	88	87	87	NNE 6	NNE 4	NNE 5
28	580.7	582.4	584.3	-16.4	-13.2	-14.8	-14.8	-12.6	-16.8	-	01.1	01.5	01.3	85	88	86	86	N 6	N 6	N 5
MES. VRED.	583.8	583.8	583.8	-08.4	-07.2	-07.1	-07.4	-04.8	-10.1	-	02.4	02.7	02.7	91	93	93	92	7.4	6.9	7.2

BR. ST. 142 H_s = 2067 m H_b = 2070.4 m h_t = 3.0 m h_r = 1.5 m

Dan	Vidljivost 0–9	Oblačnost N (0—10) 14	7	14	21	Srednja	Insolacija broj sati	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	0	10*≡	10*≡	10≡	10.0	•	00.0	111		*0-19^30 R_sw 0-0^15 V0-24, ≡ 0-24, F-F_ssw 0-17, ↓→↓ 0-19^15 [*]
2	1	10	10≡	00≡	05.7	•	06.8	113		V0-24, ≡ 0-0^15 ¥^500 0^15-24, ≡≡ 12-21^15 ↓→ 15^15-17, F_wsw 15^30-17, [*]
3	0	00	10≡	10≡	06.7	•	00.3	116		V0-24, ¥^600 0-7^45, F-F_wsw 0^30-24i, ↓→↓ 0^30-24, ≡≡ 7^45-24i, [*]
4	0	10≡	10≡	10≡	10.0	•	•	117		V0-24, F_sw 0-24, ↓→ 0-24, ≡ 0-24 [*]
5	0	10≡	10●	10≡	10.0	•	•	116		V0-10^30, F_ssw 0-24, ≡ 0-24, ↓→ 0-8, ● 11-18^15i, [*]
6	0	10●≡	10≡	10≡	10.0	•	10.2	120		≡ 0-24, F-F_sw 0-24i, ● 4^15-7^30 [*]
7	0	10*≡	10*≡	10*≡	10.0	•	02.6	116		≡ 0-24, F-F_ssw 0-19^05i, ↓ 3^15-5, 11^30-15^05i, * 5-11^30, 15^05-24, ↓→ 5-19^05 V8^40-
8	8	10*≡	00⊙	00	03.3	•	10.7	122		≡ 0-11^50 * 0-8, V0-24, ↓→ 9-10^10 ¥^200-500 11^50-24, [*] [-24, * 19^30-24, [*]
9	2	05	06	00	03.7	•	00.0	125		¥^200-500 0-24, V0-16^20, ↓→ 4^15-10^15 F_sw 7^05-12^15 [*]
10	0	02	00	05	03.7	•	•	120		¥^800-500 0-21^15, F-F_ssw 12^30-24i, ≡ 21^15-24, [*]
11	0	10≡	10≡	10≡	10.0	•	•	113		≡ ²0-24, F-F_ssw 0-24i, V4^30-24, ↓→ 12^05-24 [*]
12	0	10*≡	10●≡	10*≡	10.0	•	00.0	115		V0-12^40, 15^30-24, ≡ 0-24, F-F_s 0-24i, ↓→ 0-9^15, 15^30-16^50 21^40-22^40, * 2^55-3^55 6^30-7^05 15^40-16^40,
13	0	10≡	10≡	10≡	10.0	•	10.0	114		V0-13^40, F-F_ssw 0-14^45, ≡ 0-24, V13^40-24 [*] [20^40-22^30, * 7^05-9, ↓ 9-9^05, ● 9^05-15^40 [*]
14	0	10≡	10≡	10≡	10.0	•	•	112		V0-24, F_s-ssw 0-24, ≡ 0-24, * 16^45-16^45 ↓→ 16^45-24, [*]
15	0	10≡	10≡	10*≡	10.0	•	00.0	112		≡ 0-24, F-F_sw 0-24, V 0-24, ↓→ 0-23^45, * 14^45-23^45, ● 23^45-24, [*]
16	0	10●≡	10*≡	10≡	10.0	•	00.0	111		● 0-10^50, 14^35-15^30 ≡ 0-24, F-F_ssw 0-24i, V 0-3^40-10^55-24, ↓→ 10^50-19^40i, * 10^50-17^40i, ↑ 15^30-
17	0	10*≡	10≡	10≡	10.0	•	10.2	115		V0-24, ≡ 0-24, F-F_sw 0-4^30 8^40-24, * 1^40-8^40 ↓ 1^40-4^30 ↓→ 8^40-24, [*] [15^45, * 17^40-19^40 [*]
18	0	10≡	10≡	10≡	10.0	•	00.3	116		≡ 0-24, V0-24, F-F_N-NNW 0-24, ↓→ ↓ 0-24, ↓ 14^15-18^15 [*]
19	0	10*≡	10≡	10≡	10.0	•	02.4	123		≡ 0-24, F-F_N-NNW 0-24i, ↓→ 0-19^30 V0-24, * 4^50-7
20	1	00≡	00	00	03.0	•	•	123		≡ 0-4^20, 22^15-24, F-F_N-NNE 0-24, V0-24, ≡ 4^20-13^45, ¥^400-500 7^40-22^15, [*]
21	3	04	04⊙	02	03.7	•	•	120		V0-24, ≡ 0-1^40 F_NE 0-2^15 ¥^600-800 1^40-24, [*]
22	6	00	00⊙	00	00.0	•	•	115		V0-24, ¥^600-800 0-24, [*]
23	8	00	05	04	03.0	•	•	114		V0-24, ¥^700-900 0-24, [*]
24	8	00	05⊙	09	04.0	•	•	113		V0-24, ¥^300 0-19^20 ≡ 1^40-4^55 F_sw 20^40-24i, [*]
25	2	10*≡	10≡	00	06.7	•	04.2	115		V0-24, F-F_sw 0-19^40 ≡ 2^45-19^20, * 4^30-7^50, 12^40-14^50, ↓→ 4^30-19^40, ¥^400-800 19^30-24, [*]
26	8	04	04	00	02.7	•	00.7	121		V0-24, ¥^400-600 0-16^10 22^10-24, ≡ 14^40-17^40 ≡ 17^10-20^05 [*]
27	0	10≡	10≡	10≡	10.0	•	•	119		V0-24, ¥^600 0-5^45 ≡ 5^45-6^45 ≡ 6^45-24, ↓ ↓→ 7^30-24, F-F_sw 10^10-24i, [*]
28	0	10≡	10*≡	10*≡	10.0	•	•	115		V0-10^40, ≡ 0-24, ↓→ 0-10^30 F-F_sw 0-13^30 V10^10-24, * 13^40-23^15i, [*]
29	1	04	10≡	00	04.7	•	05.6	129		V0-24, ≡ 0-6^20 8^50-16^55, ↓→ ↓ 0-15^40 F-F_N 1^30-15^40i, ¥^500-800 6^20-8^50 14^50-24, [*]
30	0	09	10≡	10*≡	09.7	•	•	127		V0-24, ¥^600-800 0-8^40 F-F_sw 2^30-24i, ↓→ ↓ 2^00-24 ≡ 8^40-24, * 15^30-21^55, [*]
31	0	10≡	10*≡	10*≡	10.0	•	01.7	12[illegible]		V0-24, F_sw 0-7^05, ≡ 0-24, ↓→ ↓ 0-7^05, * 0^05-4^10, 9^15-24, [*]
MES. VREDN.		07.4	09.2	09.6	07.4	—	01.4			

Dan	Vidljivost 0–9	Oblačnost N (0—10) 14	7	14	21	Srednja	Insolacija broj sati	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	0	10*≡	10*≡	10≡	10.0	00.0	11.2	1[illegible]		≡ 0-24, V0-24, * 0-10^10 13^30-14^45, [*]
2	0	10≡	10≡	00	06.7	03.0	01.6	15[illegible]		≡ 0-24, V0-24, * 0^05-1^30 10^45-10^30, F_ssw 8^30-24i, ↓→ ↓→ 10^45-24, ¥^1000 20^30-24, [*]
3	0	09	10≡	10≡	09.7	00.0	00.1	1[illegible]		V0-24, ↓→ ↓→ 0-24, F-F_ssw 0-24i, ¥^1000 0-8^30 ≡ 8^30-24, [*]
4	0	04	10≡	10≡	09.0	02.4	•	1[illegible]		≡ 0-6^45 9-24i, V V0-24, F-F_S-SW-NW 0-3^45 9^45-24, ↓→ ↓→ 0-3^45 9^15-19^30, ¥^200-600 6^45-
5	0	10≡	10≡	10≡	10.0	00.0	•	14[illegible]		≡ 0-24i, F_ssw 0-24, V 0-24, [*] [9, [*]
6	0	10≡	10*≡	10*≡	10.0	00.0	•	12[illegible]		≡ 0-24, F-F_ssw 0-24i, V 0-24, * 7^15-14^30 19^30-21^30i, ↓→ ↓→ 7^15-24, [*]
7	0	10*≡	10*≡	10≡	10.0	00.0	02.6	147		V0-24, ≡ 0-24, F_sw 0-10^30 ↓→ 0-10^30-18^30-24, * 5^30-19^40i, [*]
8	0	10≡	10≡	10≡	10.0	01.6	03.8	1[illegible]		≡ 0-8^30 12^15-21^15, V 0-24, ↓→ 0-24, F-F_sw 0^15-24, ¥^600-800 8^30-12^15 [*]
9	0	10≡	10≡	10≡	10.0	00.0	•	1[illegible]		V0-24, F_sw 0-24, ↓→ 0-11^30 ≡ 0^15-24i, [*]
10	0	10≡	10≡	10≡	10.0	00.0	00.0	142		V 0-24, F-F_sw-wsw 0-24, ≡ 0-21^30, * 5^30-6, ↓→ 5^30-8^30, [*]
11	0	02	10≡	10*≡	07.3	00.4	•	1[illegible]		V0-24, F-F_w-wsw 0-24i, ¥^1000 0-12^15 ≡ 13^30-24, * 14^45-24i, ↓→ ↓→ 14^45-24 [*]
12	8	10≡	00⊙	03	04.3	06.2	02.6	14[illegible]		V0-24, ≡ 0-13^30 F-F_N-sw 0-11^30 20-24i, ↓→ ↓→ 0-11^30 * 0-14^5 ¥^300 15^45-18 [*]
13	0	10≡	10*≡	10*≡	10.0	00.0	•	1[illegible]		V 0-24, F-F_sw 0-24 ≡ 5^45-24, * 13^30-21^40 ↓→ 13^30-24i, F_S-N 19^30-21^30i, [*]
14	0	09	10≡	10≡	09.7	00.0	00.3	15[illegible]		V 0-24, F-F_sw 0-24, ≡ 0-1^30 13^15-24, ↓→ ↓→ 0-24i, ¥^1000 8-12, * 19^30-24i, F_S-N 22^30
15	0	10≡	10≡	10*≡	10.0	00.0	00.0	1[illegible]		V 0-24, F_S 0-22^30 ≡ 0-24, ↓→ 0-23, * 0-2, 17^30-24i, F_S-N 0-1^30 13^45-22^45, [24, [*]
16	1	10*≡	10≡	10≡	10.0	00.0	00.0	212		V0-24, ≡ 0-24, * 0-17^30 21^30-22^40, ↓→ ↓→ 15^30-17, 22^15-24, F_N 22^30-24, [*] [*]
17	0	10≡	10≡	00	06.7	00.0	03.4	21[illegible]		V0-24, ≡ 0-17^30 F-F_N 0-17, ↓→ ↓→ 0-19^30 [*]
18	1	00	10≡	10≡	06.7	04.8	•	20[illegible]		V 0-24, F-F_sw 7^30-23, ↓→ ↓→ 7^30-23^30 ≡ 12^45-24, * 12^30-15
19	0	10≡	10≡	10≡	10.0	00.0	00.4	21[illegible]		V0-24, ≡ 0-24, * 1^30-4^30 16^45-17^30, ↓→ ↓→ 2-24, F-F_N-NW 2^30-24, [*]
20	8	10≡	05⊙	06	07.0	05.5	01.2	21[illegible]		V 0-24, ≡ 0-8^30, F-F_N 6-21^30i, ↓↓→ 0-12, ¥^1000 8^30-23, ϖ 21^30-22^30, [*] .
21	0	10*≡	10≡	04	01.7	00.5	01.2	21[illegible]		V 0-24, ↓→ 1^30-14^30, * 1^30-17^30, ≡ ≡ 2^30-17^40 F_N 6-14^30 ϖ 20^30-24, [*]
22	8	08	06⊙	10≡	03.0	01.6	00.2	21[illegible]		V 0-24, ϖ 0-1^40, F-F_W-NNW-SW 4^30-24i, ↓→ 4^30-9^30 ≡ 17^15-24i, [*]
23	0	10≡	10*≡	10*≡	10.0	00.0	•	21[illegible]		V 0-24, ≡ 0-24, F-F_SW-NE 0-24, ↓→ 9^15-24, * 9^15-22^40 [*]
24	5	03	09	10≡	07.0	05.0	00.2	2[illegible]		V 0-24, ↓→ 0-13^30 F-F_NE 0-13^05 ≡ ≡ 0-11^05, 16^45-24, [*]
25	0	10≡	10≡	10≡	10.0	01.4	01.4	21[illegible]		V 0-24, ≡ 0-24, F-F_NE 0-24, ↓→ 0-24, * 14^45-6^15i, [*]
26	8	10≡	04⊙	10≡	09.0	03.6	•	2[illegible]		V 0-24, ≡ 0-10^30 16^10-24i, F_N 0-10^30 ↓→ ↓→ 0-10^30 * 7^05-7^15 15^45-17^40, [*]
27	0	10≡	10≡	10*≡	10.0	00.0	00.6	2[illegible]		V 0-24, ≡ 0-24i, ↓→ 2^30 13^30 19^45-24, F_N 2^45-12^45 19^30-24, * 11-15, 19^30-21^45i, [*]
28	0	10≡	10≡	10≡	10.0	00.0	02.8	24[illegible]		V 0-24, ≡ 0-24, ↓→ 0-24, F-F_N-NNE 0-24i, [*]
MES. VREDN.		08.8	09.0	08.8	09.0	02.8	78.[illegible]			

φ = 43° 43' N λ = 18° 16' E Gr. ΔG = + 1h 13 min. BR. ST. 142

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	583.8	584.8	584.0	-17.0	-14.8	-16.0	-16.0	-14.2	-17.2	-	01.0	01.3	01.1	85	86	85	85	NNE 8	NNE 7	NNE 6
2	582.5	582.1	580.6	-17.8	-13.0	-12.8	-14.1	-12.0	-18.0	-	01.0	01.5	01.5	84	88	88	87	NNE 7	NNW 5	WSW 5
3	576.7	574.6	576.6	-10.0	-08.0	-06.2	-07.6	-06.2	-12.8	-	01.9	02.3	02.7	91	92	94	92	SW 10	SW 11	SSW10
4	575.4	575.5	572.0	-05.8	-05.2	-05.2	-05.4	-04.8	-07.0	-	02.8	03.0	03.0	94	95	95	95	SSW11	SSW11	SSW11
5	573.5	576.8	576.3	-05.8	-05.6	-05.4	-05.6	-04.8	-06.4	-	02.6	02.9	02.9	94	95	95	95	SSW11	SSW11	SW 11
6	583.3	583.5	585.4	-05.8	-04.6	-06.0	-05.6	-04.6	-06.8	-	02.8	03.1	02.8	94	96	94	95	SSW 8	S 10	SSW 8
7	584.4	586.8	588.9	-06.0	-06.6	-07.0	-06.6	-05.0	-07.2	-	02.8	02.6	02.5	94	94	93	94	SW 7	SSW 5	- 0
8	589.[illegible]	588.9	589.2	-09.0	-07.4	-06.4	-07.3	-05.0	-09.4	-	02.1	02.4	02.7	92	93	94	93	- 0	WSW 3	WSW 3
9	588.6	589.4	591.0	-06.0	-05.0	-04.0	-04.8	-02.6	-06.8	-	02.8	03.0	03.3	94	95	96	95	SW 3	SW 5	SW 6
10	592.2	594.0	594.6	-04.6	-03.6	-03.0	-03.6	-02.6	-05.6	-	03.1	03.4	03.6	96	97	97	97	SW 2	SW 2	SSE 2
11	593.1	591.3	588.9	-03.6	-02.2	-02.6	-02.8	-02.0	-04.6	-	03.4	03.8	03.7	97	98	97	97	SW 8	SSW 8	SSW 8
12	584.2	584.6	586.3	-03.6	-04.0	-06.0	-04.9	-02.0	-06.4	-	03.4	03.3	02.8	97	96	94	96	SSW 9	SW 7	SW 8
13	589.0	591.0	590.9	-05.8	-06.4	-03.0	-04.6	-03.0	-07.0	-	02.8	02.7	03.6	94	94	97	95	W 6	WNW 2	SE 3
14	587.3	584.5	582.7	-02.0	-00.8	-01.4	-01.4	-00.4	-04.2	-	03.6	04.3	04.1	90	100	99	96	S 9	SSW 3	S 7
15	582.4	582.7	584.7	-01.8	-01.8	-01.6	-01.7	-00.2	-02.6	-	03.9	04.0	04.1	98	100	100	99	SSW 7	SSW 5	- 0
16	585.3	586.2	585.0	-06.0	-07.0	-10.2	-08.4	-01.0	-11.0	-	02.8	02.5	01.9	94	93	90	92	N 5	NE 6	NE 8
17	582.8	585.0	585.8	-11.2	-10.4	-11.8	-11.3	-10.0	-12.0	-	01.8	01.9	01.7	90	90	89	90	N 10	N 8	N 8
18	586.8	585.7	584.0	-12.0	-07.8	-05.0	-07.4	-04.8	-12.9	-	01.6	02.4	02.7	89	93	87	90	N 3	SW 4	SW 8
19	581.0	579.5	579.9	-06.4	-04.8	-08.2	-06.9	-04.2	-09.2	-	02.7	03.1	02.3	94	95	92	94	SW 8	SW 8	NW 9
20	581.2	584.6	587.8	-10.0	-07.8	-11.2	-10.6	-08.2	-12.2	-	01.9	02.0	01.8	91	91	90	91	N 12	N 9	N 9
21	589.7	592.6	593.8	-09.4	-04.8	-05.4	-06.2	-04.8	-12.4	-	02.1	03.1	02.9	91	95	95	94	N 9	N 10	N 6
22	593.7	594.3	594.0	-05.4	-04.0	-02.6	-03.6	-02.4	-06.4	-	02.9	03.3	03.5	95	96	94	95	WSW 5	SW 5	SW 8
23	593.4	593.8	594.4	-03.4	-02.2	-02.4	-02.6	-01.4	-04.2	-	03.5	03.8	03.8	97	98	98	98	SW 8	SSW 7	SW 7
24	593.9	594.2	594.0	-02.0	-00.6	-00.4	-00.8	00.0	-03.2	-	03.9	04.2	04.3	98	96	96	97	SW 9	SW 7	SW 8
25	594.7	593.6	593.8	-00.4	00.6	00.4	00.2	00.8	-01.8	-	04.3	04.8	04.7	96	100	100	99	SW 8	SW 9	SW 8
26	592.6	591.4	588.6	-00.2	00.6	00.4	00.3	01.0	-01.6	-	04.2	04.5	04.4	93	93	93	93	SW 8	SSW 8	SW 9
27	588.0	583.1	583.9	00.4	00.6	00.6	00.6	00.8	-01.0	-	04.7	04.8	04.8	100	100	100	100	SSW 7	SSW13	SSW11
28	581.3	580.4	581.5	-07.0	-03.4	-05.4	-05.3	00.8	-08.0	-	02.5	03.5	02.9	93	97	95	95	N 3	WSW 4	W 4
29	582.4	584.2	586.2	-09.6	-07.6	-10.0	-09.3	-04.0	-11.8	-	02.0	02.4	01.9	91	93	91	92	- 0	W 3	NW 7
30	590.0	591.3	591.9	-10.0	-06.0	-06.6	-07.3	-03.2	-12.8	-	01.9	02.2	02.4	91	74	84	83	NW 7	SW 6	SSW 7
31	589.5	588.3	583.7	-05.8	-03.6	-04.4	-04.6	-03.0	-06.8	-	02.8	03.3	03.2	94	92	96	94	SW 10	SSW10	SSW14
MES. VRED.	586.2	586.4	586.5	-06.5	-05.1	-05.4	-05.6	-03.7	-08.0	-	02.8	03.1	03.0	93	94	94	94	7.0	6.8	7.1

1	584.5	585.0	585.0	-01.6	-00.4	-00.9	-01.0	-00.2	-04.6	-	04.0	04.5	04.2	98	100	98	99	SW 11	SW 8	SW 9
2	585.1	583.9	581.9	-02.0	-01.6	-02.0	-01.9	-00.2	-03.0	-	03.9	04.1	04.0	98	100	100	99	SW 5	SW 9	SW 9
3	579.3	580.2	583.1	-03.4	-03.9	-11.6	-07.6	-01.4	-12.4	-	03.5	03.3	01.7	97	96	89	94	SW 8	SW 7	N 5
4	583.5	585.2	586.1	-12.6	-10.0	-05.6	-08.4	-05.0	-14.0	-	01.5	01.9	02.9	88	91	95	91	N 6	W 2	W 3
5	586.0	584.6	583.1	-03.0	-03.8	-04.6	-04.5	-03.0	-06.8	-	03.0	03.3	03.1	95	96	96	96	WSW 3	SW 9	WSW10
6	584.4	587.0	588.9	-07.2	-04.8	-06.6	-06.3	-03.6	-09.4	-	02.5	03.1	02.6	93	95	94	94	WSW 6	SW 4	SW 3
7	588.8	587.6	586.6	-07.8	-04.0	-02.8	-04.4	-02.8	-08.2	-	02.4	03.3	03.6	93	96	97	95	SSW 3	S 10	S 9
8	583.7	580.5	580.4	-00.6	-01.6	-00.4	-00.8	00.0	-03.8	-	04.2	04.0	04.5	96	98	100	98	S 9	S 12	S 12
9	578.8	579.6	585.2	-00.8	-00.2	-00.8	-00.6	00.0	-01.2	-	04.3	04.5	04.3	100	100	100	100	S 11	S 12	SSW 7
10	586.9	589.5	590.4	-02.0	-01.8	-01.8	-01.8	-00.8	-02.4	-	03.9	03.9	03.9	98	98	98	98	SSW10	SW 7	SW 5
11	590.4	589.9	589.5	-01.8	-01.2	-01.2	-01.4	-00.4	-02.8	-	03.9	04.2	04.2	98	100	100	99	SW 6	SW 7	SW 7
12	588.8	585.7	586.6	-03.6	-05.0	-05.6	-05.0	-00.4	-06.0	-	03.4	03.0	02.9	97	95	95	96	NW 9	N 6	N 6
13	589.7	589.4	589.4	-05.4	-02.2	-02.2	-03.0	-00.6	-06.4	-	02.9	03.8	03.8	95	98	98	97	W 3	W 7	W 9
14	586.0	587.7	585.6	-01.2	-01.4	-04.6	-03.0	-01.0	-05.8	-	04.2	04.1	03.1	100	99	96	98	SW 7	SW 6	N 8
15	587.0	590.0	590.9	-08.6	-08.6	-08.0	-08.3	-04.6	-10.4	-	02.2	02.2	02.3	92	92	92	92	N 10	N 9	NW 9
16	591.3	592.1	593.0	-08.8	-08.0	-08.0	-08.2	-07.8	-09.6	-	02.2	02.3	02.3	92	92	92	92	N 10	N 10	N 7
17	595.5	596.6	596.2	-07.4	-04.6	-02.6	-04.3	-02.0	-08.6	-	02.4	03.1	03.7	93	96	97	95	N 3	N 3	N 5
18	594.0	595.1	594.8	00.2	02.0	03.2	02.2	03.4	-03.0	-	04.7	05.3	04.2	100	100	72	91	N 9	N 8	N 7
19	594.8	595.7	594.1	03.2	05.2	03.6	03.9	05.6	01.8	-	04.2	03.9	04.3	72	58	73	68	N 7	- 0	SW 5
20	592.3	593.6	594.0	03.0	04.3	03.0	03.4	04.9	01.2	-	04.6	05.0	04.3	81	77	75	78	SW 9	SW 7	SSW 7
21	596.1	597.5	599.2	02.4	04.4	02.6	03.0	04.4	01.1	-	03.7	04.5	04.1	68	72	75	72	SSW 8	SSW 6	SSW 8
22	600.2	601.5	602.0	03.6	05.0	05.4	04.8	05.6	01.4	-	04.3	04.7	03.8	73	72	56	67	WSW 6	SW 6	W 3
23	600.6	599.8	599.4	06.6	08.2	06.4	06.9	08.2	03.2	-	03.0	04.0	04.4	41	49	60	50	W 3	WSW 3	WSW 2
24	597.3	597.1	596.6	05.6	04.8	05.6	05.9	07.2	04.8	-	04.3	04.7	04.8	70	63	70	68	SW 4	SW 5	SW 3
25	595.6	594.4	593.2	05.5	07.4	04.4	05.4	08.7	03.6	-	04.3	05.0	05.2	63	64	82	70	- 0	WSW 5	WSW 6
26	589.8	589.4	588.8	03.2	05.0	03.0	03.6	06.0	02.0	-	04.9	05.4	05.5	84	83	97	88	SW 10	SW 10	SW 9
27	588.0	590.8	591.3	02.0	02.8	01.0	01.7	04.8	00.3	-	05.1	05.6	04.8	97	100	97	98	SW 10	SW 8	SW 7
28	591.1	590.7	590.0	-00.2	-00.4	-02.4	-01.4	01.4	-03.4	-	04.5	04.5	03.8	100	100	98	99	SW 6	SW 8	SW 4
29	587.9	590.2	589.2	-02.0	-00.2	-01.2	-01.2	00.4	-04.4	-	03.9	04.5	04.0	98	100	94	97	SW 5	SSW 6	SW 7
30	588.4	588.9	589.8	-02.2	-07.6	-08.6	-06.8	00.2	-09.4	-	03.8	02.4	02.2	98	93	92	94	SW 6	N 7	N 7
MES. VRED.	589.5	590.0	590.1	-01.6	-00.6	-01.4	-01.3	00.9	-03.9	-	03.7	03.9	03.8	89	89	89	88	6.8	6.9	6.6

BR. ST. 142 H_e = 2067 m H_b = 2070.4 m h_t = 3.0 m h_r = 1.5 m

Dan	Vidljivost 0–9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	1	10≡	10≡	10≡	10.0	00.0	•	244	V0-24, ≡ 0-24, F-F NNE 0-24, ↓ ↓ 0-24, * 14^30-17^30 ⊠
2	8	00⊙	05⊙	00	01.7	10.0	00.4	246	V0-24, ≡ 0-6^45 23^30-24; F-F NNE-WSW 0-7^30 18-24, ↓ ↓ 0-18^45 23-24; ⧗^300 6^45 12^45, ⊠
3	0	10≡	10≡	10≡	10.0	00.0	•	242	V0-24, ≡ 0-24, F SW-SSW 0-24, ↓ 0-24, * 7^40-24i, ⟨ 21^45-22^30, ⊠
4	0	10*≡	10≡	10≡	10.0	00.0	02.6	242	V0-24, ≡ 0-24, F SSW 0-24, ↓ ↓ 0-24, * 0-9^45 15^45, 16^30, ⊠
5	0	10*≡	10*≡	10*≡	10.0	00.0	03.6	239	V0-24, ≡ 0-24, F SSW 0-24, ↓ 0-24, * 1^30-21^45 ⊓ S-N 7^45-8^40, ⊠
6	0	10≡	10≡	10≡	10.0	00.0	03.5	265	V0-24, ≡ 0-24, F SW 0-24, ↓ 0-24, ⊠
7	0	10≡	10*≡	00	06.7	00.0	•	265	V0-24, ≡ 0-20^15 F-F SW-SSW 0-18^45 i, ↓ 0-18, * 12^45-17^30 ⧗^300-800 20^45-24, ⊠
8	9	00⊙	00⊙	00	00.0	10.7	01.9	269	V0-24 ⧗^300-800 0-12^40 ⊠
9	9	00⊙	00⊙	00	00.0	11.2	•	267	V0-24, F-F SW 16^45-24i, ⊠
10	9	03⊙	03⊙	00	02.0	10.5	•	264	V0-24, F SW 0-1^40 ⧗^300-800 14^50-24, ⊠
11	9	09	07	10*≡	08.7	00.0	•	260	V0-24, ⧗^300-600 0-16^45 F-F SW-SSW 0^30-24, ≡ 16^45-24 * 19^45-24, ↓ 19^45-24, ⊠
12	0	10*≡	10≡	10≡	10.0	00.0	01.8	264	V0-24, ≡ 0-24, F-F SSW-SW 0-24, ↓ 0-24 * 0-11^05 ⊠
13	8	10≡	06⊙	10	08.7	04.3	00.0	264	V0-24, ≡ 0-8^05, F-F SW 0-7^50 23^40-24, ↓ 0-7^50 ⊠
14	0	10	10*≡	10*≡	10.0	00.0	•	260	V0-24, F-F S 0-24, ⧗^300 4^50 8^45 ≡ 8^45-24, * 10^05-24i, ↓ 10^05-24, ⊠
15	0	10*≡	10≡	10≡	10.0	00.0	08.4	274	V0-24, ≡ 0-22^40 F-F SSW 0-13^40, ↓ 0-13^30 * 0-7^40, 17^40-23; ⧗^300 22^40-24, ⊠
16	0	10≡	10*≡	10≡	10.0	00.0	05.0	293	V0-24, ⧗^300 0-5^45 ≡ 5^40-24, F-F N-NE 9^30-24, ↓ 9^30-24, * 10^40-20^40 i, ⊠
17	0	10≡	10≡	10≡	10.0	00.0	05.0	292	V0-24, ≡ 0-24, F-F N-NE 0-24, ↓ 0-24, ⊠
18	8	05⊙	04⊙	10	06.3	10.2	•	293	V0-24, ≡ 0-4^35, F-F N-SW 0-0^30 12-24; ↓ 0-0^30 ⧗^300-800 4^35-11, ⊠
19	0	10≡	10≡	10≡	10.0	00.0	•	214	V0-24, F-F SW-NW 0-24, ≡ 1^30-24, * 10^40-17^40, ↓ 10^40-24, ⊠
20	0	10≡	10≡	10≡	10.0	00.0	03.1	292	V0-24, ≡ 0-24, F N 0-24, ↓ 0-24, ⊠
21	8	10	01⊙	03	04.7	05.0	•	290	V0-24, ≡ 0-6^05 10^15-12^45, F-F N 0-24, ↓ 0-4^30, ⊠
22	8	07⊙	08⊙	05	06.7	10.4	•	288	V0-24, F-F 0-1^30 8^45-24, ⊠
23	9	10≡	10≡	06	08.7	00.0	•	21[illegible]	V0-24, F-F SW 0-24 ≡ 9^05-16^45 ⊠
24	8	10≡	05⊙	00	05.[illegible]	07.2	•	280	V0-24, F-F 0-24 ⧗^300-800 0^15-6^10 9^45-14^45, ≡ 6^40-9^45i, ⊠
25	8	09*	08⊙	06	07.7	02.0	•	272	V0-24, F SW 0-24, ≡ 3^40-4^45 9^05-9^30, ⧗^300-800 4^45-9^05, ⊠
26	8	06	05	03	06.3	01.2	•	260	V0-12^30, F-F SW 0-24, ≡ 16^40-18^05 ⊠
27	0	10≡	10≡	10≡	10.0	00.0	•	241	F-F SSW 0-24, ≡ 3^05-24, ∾ 14^05-19^15 ⊠
28	0	10*≡	10*≡	10*≡	10.0	00.0	01.7	240	F SW 0-5^30 ≡ 0-24, * 6^30 16^30 20^30-24; △ 16^30-17, ⧗^300-600 17^45-18^30 ⊠
29	9	10≡	05⊙	00	05.0	05.2	04.5	230	V0-24, ≡ 6-12^40 * 9^30-10^30 ⧗^300-500 12^40-18^30 F NW 19^40-24, ↓ ↓ 19^40-24, ⊠
30	9	00⊙	00⊙	00	00.0	11.7	00.5	246	V 0-10^45 F-F NW-SW 0-24, ↓ ↓ 0-8^15, 22^30-24; ⊠
31	8	09	09	10≡	09.3	00.3	•	244	F SW 0-24, ↓ 0-24, ≡ 15^15-24, ⊠
MES. VRED.		08.0	07.3	06.7	07.3	99.9	41.4		

1	0	10*≡	10≡	10≡	10.0	00.0	00.8	246	F SW 0-24, ≡ 0-24, ↓ ↓ 0-24, * 1^40-8^45 V 2^45-24, ⊠
2	3	10≡	10≡	10≡	10.0	00.0	00.9	237	F-F SW 0-24, ≡ 0-24, ↓ 0-24 V 0-24, △ 1^45-1^45 ⊓ S-W 1^40 * 1^45 9^40 15^05-17^40 22^40-24; ⊠
3	0	10≡	10≡	10≡	10.0	00.0	03.0	275	F-F SW 0-24, ≡ 0-24, ↓ 0-24, V 0-16^40 * 0-3^40 24^05-24; V 16^40-24, ⊠
4	8	10≡	02⊙	00	04.0	10.4	01.3	282	F N 0-10^40 ≡ 0-8^30, ↓ ↓ 0-9^30 V 0-24 * 0-2^30 ⊠
5	8	04⊙	08⊙	10≡	07.3	06.7	•	280	V0-24, F-F SW-WSW 10^30-24i, ↓ ↓ 10^30-24, ≡ 20^05-24, ⊠
6	0	10≡	10≡	10≡	10.0	00.0	•	274	F-F WSW 0-9^15 ≡ 0-11^30 18^45-24; ↓ ↓ 0-6^30 V 0-24, * 10^45-13^15, ⊠
7	3	00⊙	10≡	10≡	06.7	•	00.5	270	≡ 0-4^30 11^30-24; V 0-24, F-F SW 9^30-24, ↓ ↓ 10^40-24, * 22^30-24
8	0	10≡	10*≡	10≡	10.0	00.0	01.6	269	≡ 0-24 V 0-24, F S 0-24 ↓ ↓ 0-19^30 * 0-3^40 8-16^45, ∾ 17^30 8, * 8-16^45 ⊓ 15^45, 22^35-24i, ⊠
9	0	10●≡	10≡	02	07.3	00.0	09.0	260	≡ 0-14^30 V 0-24, F-F S-SW 0-24 ⊓ 0-5^30 ● 2^30-9^45, ∾ 11-17, ⊠
10	8	10≡	10	04	08.0	00.3	02.4	256	V 0-24, F-F SW 0-24, ≡ 0^15-9^25, 17^45-20^45; ⊠
11	0	10≡	10*≡	10≡	10.0	00.0	•	255	F SW 0-24, V 0-24, ≡ 4^50-24, * 11^40-14^40, ⊠
12	0	10≡	10≡	10≡	10.0	00.0	00.3	244	F SW 0-23^30 V 0-24, ≡ 0-24 ⊠
13	8	00⊙	09	10≡	06.3	03.6	•	240	V 0-24, ≡ 0-5^15 20^45-24; F-F W 9^30-24, ⊠
14	0	10*≡	10*≡	10*≡	10.0	00.0	01.6	239	F-F WSW-SW 0-24, V 0-24, ≡ 0-24, ∾ 4^45-4^30, ↓ 4^30-24, * 4^30-21^45i, ⊠
15	0	10≡	10≡	10≡	10.0	00.0	08.3	260	V 0-24, ≡ 0-24, F N-NW 0-24, ↓ 0-24, ⊠
16	0	10≡	10*≡	10≡	10.0	00.0	•	254	V 0-24, ≡ 0-24, F-F N 0-23^40, ↓ 0-19^30 * 13^40-14^45 ⊠
17	8	10≡	03⊙	03	05.3	07.8	00.5	255	V 0-24, ≡ 0-9^15 15^05, 16^40, ⧗^300-800 9^45, 20^50, F N 17^45-24i, ⊠
18	8	10≡	06	04	06.7	00.0	•	246	V 0-7^45 F-F N 0-24, ≡ 0^15-11^40, ⊠
19	8	00⊙	05	03	02.7	06.0	•	220	F N 0-10^30 ⊠
20	8	05⊙	07	10	07.3	08.3	•	214	F-F SW 0^05-24, ⊠
21	8	10	08	04	07.3	03.0	•	18[illegible]	F-F SSW 0-24, ⊠
22	8	09	09	00	06.0	00.0	•	172	F SSW-SW 0-18^40, ⧗^300 5^15-11^30, ⊠
23	8	00⊙	04⊙	00	01.3	12.0	•	142	⊠
24	8	05⊙	09	02	05.3	03.2	•	127	F SW 9^30-20^40 ⟨ N 20^40-21^05 ⊠
25	8	01⊙	10	01	04.0	07.9	•	118	⊕ 9^55-11^30, F SW-WSW 12^50-24, ⊠
26	8	01⊙	05	04	03.3	06.8	•	10[illegible]	F-F SW-WSW 0-24, ⊠
27	0	10	10●≡	03	07.7	00.4	•	[illegible]4	F-F SW 0-24, ≡ 8^30-16^30, 19^05-24; ∾ 11^05-13^25 ● 12^30-14^45 ⊠
28	0	00≡	00*≡	00*≡	00.0	00.0	00.0	[illegible]	F-F SW 0-24, ≡ 0-14^45 5^45-24; * 9-24i, ↓ 9^15-24, V 15^30-24, ⊠
29	9	10≡	03⊙	00	04.3	06.8	03.6	8[illegible]	F-F SW-SSW 0-24, V 0-24, ≡ 0-10^15, * 0-5^45 ↓ 0-10^15 ↓ 10^15-11^40 ⊠
30	2	10≡	10*≡	10≡	10.0	00.5	•	[illegible]	V 0-24, F-F N-SW 0-7^30, 13^30-24; ≡ ≡ 1^50-24i, * 6^50-17^30 10^30-20^40, ↓ ↓ 13^40-24, ⊠
MES. VRED.		07.2	07.9	06.0	07.0	[illegible]	39.[illegible]		

φ = 43° 43' N λ = 18° 16' E Gr. ΔG = + 1h 13 min. BR. ST. 142

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	589.3	590.8	591.0	-09.0	-07.4	-08.0	-08.1	-05.6	-09.2	-	02.1	02.1	02.3	92	78	92	87	N 6	NE 3	N 5
2	590.1	590.3	590.3	-09.6	-08.4	-08.4	-08.7	-08.0	-10.0	-	02.0	02.2	02.2	91	92	92	92	N 4	N 2	N 5
3	589.8	590.7	592.3	-08.8	-06.2	-04.8	-06.2	-04.2	-09.8	-	02.2	02.7	03.1	92	94	95	94	N 7	N 8	N 7
4	590.3	590.4	587.7	-04.8	-02.6	-03.0	-03.4	-01.4	-05.8	-	03.1	03.7	03.6	95	97	97	96	N 8	NNE 7	N 10
5	585.1	587.1	588.7	-04.0	-01.2	-00.2	-01.4	01.0	-04.3	-	03.3	04.2	04.5	96	99	100	98	N 11	N 2	SW 4
6	590.3	592.2	592.3	-01.2	00.8	00.0	-00.1	01.0	-02.2	-	04.2	04.9	04.6	100	100	100	100	NE 2	WSW 3	SSW 5
7	590.5	592.8	593.1	-00.4	02.8	02.0	01.6	03.6	-01.0	-	04.0	04.9	04.8	89	87	90	89	SSW 7	SSW 7	SSW 7
8	592.0	592.4	592.7	02.7	04.2	01.8	02.6	05.0	00.6	-	04.9	04.9	04.9	89	79	93	87	SSW 9	SSW 12	SSW 8
9	593.5	595.0	595.8	02.3	05.2	05.0	04.4	05.2	01.0	-	05.4	05.3	03.3	100	80	50	77	SW 9	SW 7	SSW 6
10	593.3	592.1	591.2	05.8	08.0	05.6	06.2	08.8	03.4	-	04.3	04.5	04.0	62	56	59	59	SSW 6	SSW 8	SSW 6
11	589.6	589.7	589.4	03.1	05.8	02.4	03.4	07.0	01.6	-	05.5	05.2	04.2	95	75	78	83	SSW 5	SSW 8	SSW 6
12	587.7	589.2	589.5	-00.8	00.1	-00.6	-00.5	03.6	-01.2	-	04.3	04.6	04.4	99	100	100	100	SSW 3	SW 6	SW 9
13	590.9	592.1	593.2	-00.2	02.2	01.4	01.2	03.4	-01.2	-	04.5	04.3	04.9	100	81	97	93	SW 7	SW 5	WSW 3
14	594.1	594.9	595.2	01.2	05.4	03.4	03.4	06.0	00.0	-	04.7	04.8	05.3	93	72	91	85	- 0	SW 6	SW 6
15	593.1	593.5	592.2	03.0	05.2	02.9	04.0	06.4	01.8	-	05.3	05.3	05.1	94	80	83	86	SSW 6	SW 7	SW 7
16	590.4	591.1	590.8	03.7	05.4	03.4	03.5	05.4	02.2	-	05.2	05.8	05.5	86	100	94	93	WSW 8	SSW 4	SW 3
17	589.9	589.6	588.4	02.0	04.0	00.6	01.8	05.0	00.0	-	05.3	05.0	04.8	100	82	100	94	- 0	W 1	NNW 5
18	587.3	590.7	593.5	00.0	00.0	00.0	00.0	01.2	-00.4	-	04.6	04.6	04.6	100	100	100	100	N 10	NNW 10	N 10
19	593.1	594.8	595.0	-00.8	-00.6	00.2	-00.2	00.2	-01.4	-	04.3	04.4	04.7	100	100	100	100	N 10	N 7	N 6
20	593.9	593.5	592.3	00.6	01.6	01.4	01.2	02.2	-00.2	-	04.8	05.1	05.1	100	100	100	100	N 3	NE 2	NNE 4
21	589.6	588.8	589.3	01.6	01.8	02.0	01.8	02.2	01.0	-	05.1	05.2	05.3	100	100	100	100	N 9	N 6	N 2
22	587.5	586.5	587.2	02.0	03.0	00.8	01.6	04.0	00.2	-	05.3	05.7	04.9	100	100	100	100	SW 7	SW 8	SSW 5
23	586.7	591.3	593.7	-04.2	-03.4	-03.6	-03.7	01.0	-04.2	-	03.2	03.5	03.4	96	97	97	97	NNW 12	N 8	N 6
24	593.2	593.6	594.2	-05.2	-04.7	-03.2	-04.1	-03.2	-05.4	-	03.0	03.1	03.5	95	95	97	96	N 9	N 9	N 10
25	596.0	597.2	596.4	-03.6	-01.0	-01.0	-01.6	-00.6	-05.4	-	03.4	04.2	04.2	97	99	99	98	N 10	N 5	NNW 3
26	595.7	595.4	595.3	-02.4	-00.4	00.2	-00.6	00.4	-03.6	-	03.5	04.1	04.3	90	93	93	92	NNW 1	NNW 2	NNW 3
27	594.8	594.3	593.5	01.2	04.4	02.2	02.5	04.8	-00.4	-	05.0	04.6	05.4	100	74	100	91	- 0	SW 2	S 1
28	592.2	593.5	592.5	-00.2	-00.2	-01.6	-00.9	02.3	-02.2	-	04.5	04.5	04.0	100	100	98	99	SW 2	- 0	N 5
29	592.7	594.4	594.6	-01.2	00.8	01.8	00.8	03.2	-02.6	-	04.2	04.8	04.5	99	98	87	95	N 6	WSW 2	WSW 5
30	594.2	594.8	594.4	03.1	04.9	03.8	03.9	06.2	00.3	-	03.9	05.1	05.3	68	78	88	78	W 3	WSW 6	SW 2
31	594.6	594.5	594.9	02.2	02.2	01.4	01.8	04.2	00.5	-	05.4	05.4	05.1	100	100	100	100	NNW 2	NNE 5	NNE 7
MES. VRED.	591.3	592.2	592.2	-00.7	01.0	00.3	00.2	02.3	-01.9	-	04.2	04.5	04.4	94	90	92	92	5.9	5.4	5.5

1	594.0	595.9	595.2	-00.1	01.2	00.6	00.6	01.6	-00.9	-	04.6	05.0	04.8	100	100	100	100	NNE 9	NNE 5	N 7
2	595.2	595.8	594.7	01.2	01.2	-01.0	00.1	02.0	-02.8	-	05.0	05.0	04.2	100	100	99	100	N 7	N 7	N 7
3	593.0	593.3	595.1	-05.2	-02.8	-02.6	-03.3	-01.0	-06.3	-	03.0	03.6	03.7	95	97	97	96	N 6	NNE 7	NNE 7
4	591.6	593.9	594.7	-01.6	00.0	00.0	-00.4	00.2	-03.4	-	04.0	04.6	04.6	98	100	100	99	N 7	N 4	W 3
5	593.5	595.5	595.5	00.2	02.2	01.8	01.5	03.4	-00.8	-	04.7	05.0	04.2	100	93	80	91	SW 7	WSW 5	SW 5
6	595.3	595.7	596.8	02.8	04.0	04.8	04.1	06.2	00.2	-	05.6	06.1	06.1	100	100	94	98	SSW 5	SSW 5	- 0
7	596.4	597.4	596.7	08.0	12.0	08.0	09.0	12.2	04.0	-	05.4	08.2	06.0	67	78	75	73	SSW 4	SW 2	SW 4
8	594.5	596.8	596.7	08.4	12.2	09.4	09.8	12.6	05.8	-	05.0	08.1	07.3	61	76	83	73	SW 7	SSW 6	SSW 7
9	596.9	597.9	597.6	09.6	09.8	08.6	09.2	12.6	07.0	-	06.8	07.1	06.9	76	79	83	79	SSW 6	S 7	SW 8
10	597.3	596.7	594.7	10.8	14.0	09.0	10.7	14.6	07.0	-	06.9	07.2	06.8	71	60	79	70	SW 6	SSW 7	SSW 6
11	594.5	594.6	594.0	07.6	07.0	06.2	06.8	09.4	06.0	-	07.8	07.5	07.1	100	100	100	100	NW 3	N 4	N 6
12	594.2	594.6	594.2	05.0	05.8	05.6	05.5	07.6	03.2	-	06.5	05.6	06.4	100	81	94	92	N 7	N 6	N 6
13	594.3	594.9	595.2	07.2	10.0	09.0	08.8	10.7	04.2	-	04.9	06.4	06.5	64	70	76	70	NNE 4	N 3	N 4
14	595.0	595.3	595.5	10.4	12.8	08.8	10.2	12.9	06.8	-	05.8	06.7	07.4	61	61	88	70	WSW 5	W 5	WSW 6
15	596.0	597.2	598.1	07.4	10.4	09.0	09.0	11.1	06.0	-	07.3	07.7	06.5	95	81	76	84	WNW 3	NNW 2	NW 3
16	598.1	599.8	598.9	11.0	11.2	09.6	10.4	13.0	08.0	-	08.0	07.7	07.9	82	77	88	82	- 0	W 4	NW 4
17	598.3	598.5	597.8	11.0	14.8	12.6	12.8	14.8	08.7	-	06.5	07.3	07.7	66	57	70	64	W 4	WSW 5	W 4
18	595.7	594.8	594.3	12.0	15.4	09.8	11.8	15.8	09.2	-	08.2	08.1	07.1	78	62	79	73	SW 8	SW 7	SW 7
19	592.3	593.6	594.2	05.0	04.8	05.8	06.6	10.4	03.0	-	06.2	08.0	06.9	94	88	100	94	SW 7	SW 4	SSW 2
20	593.9	594.1	595.5	05.6	05.0	05.6	05.4	06.4	04.0	-	06.8	06.5	06.8	100	100	100	100	N 2	NW 7	NNW 8
21	597.3	598.8	599.9	05.6	07.2	06.6	06.5	08.8	04.0	-	06.8	05.8	06.9	100	76	95	90	NW 7	N 5	N 4
22	598.2	600.5	600.3	08.0	11.4	10.2	10.0	12.0	05.6	-	07.6	07.2	08.9	95	71	95	87	NE 6	NE 3	NW 2
23	600.0	600.0	599.8	11.4	14.0	10.4	11.6	14.2	08.8	-	08.1	07.4	07.9	80	62	84	75	- 0	- 0	W 2
24	599.6	599.8	600.0	11.4	13.8	09.0	10.8	14.8	08.1	-	06.3	07.3	06.9	63	62	80	68	- 0	- 0	W 3
25	599.6	600.0	599.7	10.8	10.0	08.2	09.3	11.8	07.6	-	07.3	07.0	08.2	75	77	100	84	N 2	NNE 4	N 6
26	599.7	600.1	599.7	08.4	10.4	09.6	09.5	11.0	06.2	-	08.3	07.9	09.0	100	84	100	95	N 7	NNW 4	N 4
27	599.6	600.6	599.9	07.8	11.2	10.4	10.0	12.0	06.7	-	07.7	08.2	08.3	97	82	88	89	N 5	N 2	- 0
28	599.4	599.6	599.3	12.0	13.0	11.6	12.0	13.0	09.0	-	07.1	08.8	08.4	68	79	82	76	- 0	SW 2	SW 1
29	598.6	597.9	597.3	11.8	16.2	09.6	11.8	16.4	06.8	-	07.2	08.4	07.2	69	61	81	70	- 0	- 0	- 0
30	595.8	595.6	590.7	10.0	14.4	09.0	10.0	14.8	08.4	-	06.6	09.3	08.2	68	76	95	80	SW 5	SW 6	SW 8
MES. VRED.	596.3	596.9	596.7	07.1	09.2	07.2	07.7	10.2	04.7	-	06.4	07.0	06.8	84	80	89	84	4.6	4.3	4.5

BR. ST. 142 H_s = 2067 m H_b = 2070.4 m h_t = 3.0 m h_r = 1.5 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	8	10	04	10	08.0	-	03.6	98	V0-24, ≡ 0-11^30 16^45 24, F-F_N 0-8^45 19^45 23; + 0-10^30 19-24i; * 16-20, + 19-24,
2	0	10	10	10	10.0	-	01.4	101	V0-24, ≡ 0-4^40 16^45 24; + 0-4, 16^45 24; F_NNW 1^30 24, * 12^30 24i,
3	0	10	10	10	10.0	-	02.8	111	≡ 0-24, V0-24, + + 0-24, F-F_N 0-24, * 0-05
4	8	10	06	10	08.7	-	.	110	≡ 0-11, 20-24, F-F_N 0-24, V0-24, + + 0-24,
5	0	10	10	10	10.0	-	.	106	V0-24, F-F_N 0-11^30, + + 0-11^45, ≡ 0-24, * 12^45 15^45,
6	0	10	10	10	10.0	-	01.2	107	V0-15 ≡ 0-23, * 1^45 7^30 F-F_SSW 20^30 24,
7	8	10	09	10	09.7	-	00.6	104	F-F_SSW 0-24, ≡ 15^45 17^45, ● 15^30-16^30,
8	8	10	09	09	09.3	-	00.3	96	F-F_SSW 0-24,
9	8	10	09	00	06.3	-	.	92	F-F_SSW 0-24, ≡ 0^45 10^00,
10	8	04	07	00	03.7	-	.	86	F-F_SSW 0-24,
11	8	10	05	05	06.7	-	.	84	F-F_SSW 0-5^45, 9^30 23^30, ≡ 7^30 10^30,
12	0	10	10	10	10.0	-	02.2	86	≡ 0^30 24, * 0^30 9^30 13^45 15^45 F-F_SSW 3^45 6^00 12^45 24; + 3^45 6^00 V 7^45 14^30 18^30 24; + [18^30 19^45 + 19^30 24,
13	8	10	04	10	08.0	-	00.6	87	V0-8^30 F-F_SW 0-24, ≡ 0-10^45, 20^30 24^45,
14	8	02	02	00	01.3	-	.	83	F_SW-NW 0-5^45, 13^45 24,
15	8	04	10	04	06.0	-	.	79	F-F_SW-WSW 0-24, ≡ 23^45 24,
16	0	01	10	05	05.3	-	.	76	F-F_SW 0-12^45 ≡ 0-10^45 13^45 16^30, ● 11^30 13^45,
17	8	04	10	10	08.0	-	00.5	73	1^30-6^00 24, 8^00 ≡ 9^45 24, T_SW-N 12^30-15^45 ● 13^30-15^30 * 18^45 19^45,
18	0	10	10	10	10.0	-	10.6	69	≡ 0-24, F-F_N 0^45 24, ● 0^30-6^45 * 6^45 15^45 20-24;
19	0	10	10	10	10.0	-	08.8	72	F-F_N 0-24, ≡ 0-24, * 0-0^30 V4-24, * 4^30-6, 9^45-15^30 + + 4^30 15i,
20	0	10	10	10	10.0	-	06.4	74	F_N 0-3^30, ≡ 0-24, V 0-9,
21	0	10	10	10	10.0	-	02.6	69	≡ 0-24, F_NE-N 0^45-19^30, ● 4^30 6^30 11^45 12^45 16^30 18^30
22	0	10	10	10	10.0	-	03.0	64	≡ 0-24, 600-600 2-6, F_SW 6-21^45 10^30 10^30, ● 11^30-19^45, T_SW-N 11^45 12^45 * 19^45 20^00 * 20^30-24
23	0	10	10	10	10.0	-	15.8	79	* 0-05 13^30 19^30 * 0^30 24, F-F_N 0^45 24i, V 0^45 24,
24	0	10	10	10	10.0	-	03.6	84	≡ 0-24, F-F_N 0-24, V0-24, + 0-24, * 4^30 8^30 11^45 14^30 T 14^30,
25	8	10	08	04	07.3	-	01.5	86	≡ 0-11^45, F-F_N 0-4^30, V0-24, + 0-10^45, 300-500 23^30 24,
26	8	02	05	00	02.3	-	.	83	V0-10^30 300-600 0-10^45 ⊕ 9^45 13^45,
27	8	00	05	10	05.0	-	.	80	● 11^45-15^30 T_N-S 14^45 15^45 ≡ 20^45 24,
28	0	10	10	10	10.0	-	01.1	76	≡ 0-24, 300 3^30-5^30 * 0^30-1^30 * 18^30-22^45 V 18^30 24,
29	8	10	09	02	07.0	-	02.3	81	≡ 0-12^45 V0-11^45 F_N 0-8^45,
30	8	01	09	05	05.0	-	.	76	F_SW-WSW 13^30 15^30,
31	8	10	10	10	10.0	-	.	73	≡ 6-24, ∩ 9^30-10^45, ● 11^30 16^30 21^30 24i; T_N-S 12^30-13^45, F_NNE 16^30 24,
MES. VRED.		08.0	08.4	07.5	08.0	-	68.9		

1	0	10	10	10	10.0	00.0	17.9	68	≡ 0-24, F-F_NNE 0-24, ● 0-[illegible] 24-[illegible] 22-[illegible],
2	0	10	10	10	10.0	00.0	02.7	50	≡ 0-24, F-F_NE 0-24, ● 1^45-4^00 12^30-15^30 + 20^30 22^45 * 20^30 22^45, V 20^30 24,
3	0	10	10	10	10.0	00.0	02.2	48	V0-24, F-F_N 0-24, ≡ 0-24, * 11^30 23^30 + + 16-24,
4	0	10	10	10	09.7	00.0	04.4	56	V0-24, ≡ 0-4^30 21^30 24; F_NNW 0-12^45 + 0-7^45 * 6^30-7^45, 400-600 14^30-21^30,
5	8	10	05	02	05.7	05.2	00.3	48	V 0-7^45, ≡ 0-9^30, 18^30-21^45, F_W-SW 1^45 24,
6	0	10	10	01	07.0	01.7	.	45	F_SW 0-15^30 ≡ 4^45 14^45,
7	8	07	08	02	05.7	05.9	.	40	● + 9^30 F_SW 21^45-24i,
8	8	00	02	00	00.7	10.8	00.0	38	F-F_SW 0-24,
9	8	03	06	04	04.3	03.0	.	35	F-F_SW-WSW 0-24, ● 11^30-13^45,
10	8	04	04	03	03.7	12.6	01.2	28	F-F_SW 0-23,
11	0	10	10	10	10.0	06.0	.	25	≡ 5^45 14^30 18^30 24; ● 10^30 14^45 T_N-S 13^30 14^30 F_N 20^30 24,
12	8	10	05	03	06.0	03.7	01.2	22	≡ 0-11^30 F-F_N 0-24,
13	8	00	08	02	03.3	10.6	.	18	F-F_N 0-4^45 ● 13^30-13^45,
14	8	00	09	04	04.3	08.8	00.3	15	F_W 11^45 24 T_W-E 13^45 16^30 ● 16^30-18^30,
15	8	10	06	03	06.3	02.4	04.5	13	F_WSW 0-4^30 ≡ 7^30-10^30, ● 7^30 8^30 16^30-19^30 T_N 18^30-19^30,
16	8	02	10	03	05.0	05.8	01.5	12	400-1000 0^30-8^45 T_N-S 11^30 14^45, ○ 13^30-15^45,
17	8	03	05	05	04.3	12.3	00.4	11	800 1^45 7^30,
18	8	06	05	09	06.7	10.9	.	09	F-F_SW-WSW 0^45 24 ○ 19^30-23^45 T_W-SSW 19^30-22^30 & 22^30 24,
19	8	10	08	10	09.3	01.8	07.5	08	F-F_S-SW 0-13^30 & d-1^30 T_S-SW 1^30-2^30 ○ 1^30-8^30 19^45-24i; ≡ 18^30-24,
20	0	10	10	10	10.0	00.0	16.6	05	≡ 0-24, ○ 0-13^30, F-F_N 0^45 24,
21	8	10	06	00	05.3	03.7	20.0	04	F-F_NW 0-24, ≡ 0-8^45,
22	8	06	04	00	03.3	10.2	.	03	F_N 0-11^30,
23	8	00	05	05	03.3	09.2	.	03	1000 1^30 7^30 T_E 18^30-20^45 △ 22^30-24,
24	8	01	07	08	05.3	11.1	.	.	600 3-5^45 T_W-E 17-19^30,
25	8	04	10	10	08.0	05.4	.	.	300 3^45-9^45 ○ 11^45-12^30 ≡ 16^30 24,
26	8	10	10	10	10.0	04.5	00.3	.	≡ 0-11^45 15^45 24i; F-F_N 0-13^30,
27	8	10	05	00	05.0	09.7	.	.	≡ 0-8^45 19^30-20^30 F_N 11^45 14, △ 19^30 24,
28	8	01	04	00	01.7	07.9	.	.	△ 0-6^30 19^30 24,
29	8	01	05	03	03.0	06.3	.	.	△ 0-6^30 ● 11^45-19^30 T_NE 12^30-13^45 T_N 13^45-16^45, & 19^45-19^30, < 21^30-22^45
30	8	03	06	00	03.0	11.1	03.0	.	△ 0^45-6^30, 300 3^45-8^30 F-F_SW 13^30-24i
MES. VRED.		06.0	07.1	04.9	06.0	180.6	86.3		

φ = 43° 43' N λ = 18° 16' E Gr. ΔG = + 1h 13 min. BR. ST. 142

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	599.7	598.9	598.3	06.0	09.2	07.4	07.5	09.4	05.0	-	01.6	01.7	00.9	23	19	11	18	- 0	SW 4	WSW 5
2	598.5	598.9	599.1	08.8	09.4	09.4	09.2	10.6	07.2	-	01.0	01.9	01.8	12	22	20	18	NNE 4	NNE 1	W 3
3	598.6	596.7	596.4	08.0	08.9	07.4	07.9	09.4	06.0	-	03.2	02.6	03.4	40	30	44	38	N 2	SSW 7	WSW 7
4	595.7	596.7	598.2	06.8	03.5	03.8	04.5	08.0	01.6	-	01.8	05.0	02.7	24	85	45	51	WNW 4	NNE 5	NE 4
5	597.8	595.4	593.4	06.4	07.2	04.0	05.4	07.3	02.6	-	01.6	03.6	03.6	22	47	59	43	SW 4	SW 8	SW 9
6	592.0	591.2	591.9	01.8	-03.2	-06.8	-03.8	04.0	-07.8	-	05.2	03.5	02.6	100	97	94	97	SSW 3	N 3	N 6
7	591.8	592.5	593.3	-08.0	-06.8	-02.6	-05.0	-02.6	-10.0	-	02.3	02.6	02.7	92	94	71	86	N 6	N 2	- 0
8	591.3	593.3	596.0	-02.2	00.0	00.0	-00.6	01.0	-02.6	-	03.8	04.6	04.6	98	100	100	99	SSW 6	SSW 8	N 1
9	593.8	592.0	590.9	00.4	01.9	01.0	01.0	02.8	-00.1	-	04.7	05.2	04.9	100	100	100	100	SW 7	SW 6	SW 7
10	588.6	588.4	590.4	-00.4	-04.0	-05.6	-03.9	01.4	-05.6	-	04.5	03.3	02.9	100	96	95	97	W 2	N 7	N 6
11	591.9	594.1	594.8	-06.4	-06.6	-05.0	-05.8	-04.8	-07.4	-	02.7	02.6	02.9	94	94	91	93	N 7	N 6	N 6
12	596.3	596.6	596.9	00.3	01.8	02.2	01.6	02.4	-05.2	-	03.4	03.4	02.7	74	64	50	63	N 2	SW 3	SW 3
13	595.7	594.6	593.6	01.1	02.0	00.0	00.8	02.6	00.0	-	01.2	01.2	01.4	23	22	31	25	SW 6	SW 8	SW 8
14	591.3	590.7	588.1	00.0	01.0	02.1	01.3	02.6	-00.8	-	04.6	04.9	05.3	100	100	100	100	SW 11	S 9	S 8
15	586.3	585.4	582.9	00.8	00.0	00.0	00.2	03.2	-01.0	-	04.9	04.6	04.6	100	100	100	100	S 8	SSW 9	SSW11
16	581.8	582.0	584.5	-02.4	-02.8	-07.0	-04.8	00.0	-07.8	-	03.8	03.6	02.5	100	97	93	97	- 0	S 7	N 7
17	587.9	589.7	590.3	-05.7	-05.8	-02.0	-04.6	-01.0	-09.5	-	02.2	02.8	03.6	92	94	90	92	NNE 3	WSW 4	SW 8
18	591.2	592.7	592.7	-03.9	-01.9	-00.7	-01.8	-00.6	-04.0	-	03.3	03.9	04.4	96	98	100	98	SW 9	SW 7	SW 9
19	590.5	589.8	590.4	01.0	01.1	00.8	00.9	01.8	-00.7	-	04.9	05.0	04.9	100	100	100	100	SW 12	SSW13	SW 11
20	590.0	590.9	593.0	01.0	01.6	01.6	01.4	02.0	00.4	-	04.9	05.1	05.1	100	100	100	100	SW 10	SW 9	SW 7
21	591.3	590.0	587.5	02.0	02.6	02.0	02.2	02.8	01.2	-	05.3	05.5	05.3	100	100	100	100	SW 9	SW 11	SW 10
22	584.5	583.7	586.0	-02.0	-02.6	-04.0	-03.2	02.4	-04.0	-	03.9	03.7	03.3	98	97	96	97	SW 8	SW 5	N 2
23	585.6	586.4	589.2	-05.6	-06.4	-06.2	-06.1	-04.0	-06.6	-	02.9	02.7	02.7	95	94	94	94	N 10	N 11	N 10
24	592.6	595.5	596.1	-04.0	-02.6	-02.4	-03.4	-02.0	-06.4	-	03.3	03.7	03.5	96	97	97	97	N 9	N 2	N 4
25	596.2	597.2	597.6	-02.6	-03.0	-03.6	-03.2	-02.0	-04.2	-	03.7	02.9	02.0	97	78	57	77	N 4	N 2	N 3
26	596.2	598.7	598.7	-03.0	-02.3	-02.8	-02.7	-02.0	-03.6	-	02.2	02.4	03.0	59	62	82	68	N 3	NE 7	NE 6
27	599.5	598.9	599.4	-01.8	00.8	02.6	01.0	02.8	-02.8	-	02.2	02.5	02.2	55	52	40	49	NE 7	NNE 4	NNE 4
28	597.9	597.0	596.8	02.4	02.4	01.0	01.7	03.6	00.0	-	02.3	03.2	02.5	43	59	50	51	W 5	W 6	W 5
29	594.9	594.8	594.6	00.1	01.0	01.0	00.8	02.0	-00.8	-	02.6	03.8	04.6	56	76	93	75	WSW 6	SW 7	WSW 7
30	595.0	593.1	592.4	04.0	01.0	00.0	01.2	05.0	00.0	-	04.4	04.9	04.6	72	100	100	91	SW 7	SW 10	SW 11
MES. VRED.	592.8	592.9	593.1	00.0	00.2	-00.1	00.0	02.3	-02.2	-	03.3	03.5	03.4	75	79	77	77	5.8	6.4	6.3

1	594.5	593.6	592.6	01.4	01.0	00.0	00.6	01.8	-00.4	-	05.1	04.9	04.6	100	100	100	100	SW 5	SW 5	SW 2
2	592.2	593.0	593.5	-01.2	-01.4	-03.4	-02.4	00.4	-03.6	-	04.0	03.6	03.5	95	88	97	93	- 0	- 0	NNE 1
3	592.8	591.0	588.3	-04.0	-02.0	-03.4	-03.2	-01.6	-04.4	-	03.3	03.9	03.5	96	98	97	97	N 2	SW 6	W 10
4	589.1	591.1	590.7	-07.0	-10.2	-10.4	-09.5	-02.8	-11.8	-	02.5	01.9	01.9	93	90	90	91	N 10	N 7	N 12
5	592.6	594.5	595.5	-08.9	-04.4	-02.8	-04.7	-02.4	-10.4	-	02.0	02.1	03.6	86	65	97	83	N 10	NNW 6	N 5
6	594.0	595.7	596.0	-07.3	-07.6	-08.0	-07.7	-02.4	-09.4	-	02.5	02.4	02.3	93	93	92	93	NE 10	N 7	ENE 6
7	596.7	596.1	595.9	-07.4	-04.0	-02.8	-04.2	-02.4	-09.8	-	02.4	01.8	01.5	93	52	41	62	W 3	SW 3	WSW 6
8	597.2	598.5	599.6	-04.2	-01.6	-03.6	-03.2	-00.8	-05.0	-	02.7	04.1	03.2	79	100	91	90	SW 7	SW 6	WNW 5
9	599.2	599.1	597.0	-09.2	-07.8	-06.4	-07.4	-03.6	-12.0	-	02.1	02.4	02.3	91	93	80	88	N 8	N 6	N 11
10	595.7	597.2	597.9	-08.0	-06.2	-05.2	-06.2	-04.0	-08.6	-	02.3	02.1	02.6	92	74	82	83	N 11	N 9	NNE 9
11	599.0	600.9	601.9	-04.5	-02.4	-01.5	-02.5	-01.2	-05.8	-	02.1	03.3	03.2	65	86	78	76	N 8	NNE 5	NE 4
12	601.4	601.3	601.3	02.2	03.4	03.8	03.3	03.8	-01.5	-	00.9	01.3	01.4	17	22	23	21	NNE 3	- 0	- 0
13	600.8	598.9	599.2	03.8	03.6	01.8	02.8	04.4	01.4	-	01.4	01.3	01.3	23	22	24	23	- 0	SW 5	- 0
14	597.9	596.8	596.1	00.3	00.9	00.2	00.4	02.8	-01.3	-	02.2	01.4	01.6	47	29	35	37	- 0	W 3	SW 5
15	594.2	593.8	593.8	-04.1	-07.8	-10.0	-08.0	01.4	-10.0	-	02.2	02.4	01.9	65	93	91	83	NNE 3	N 4	N 7
16	593.0	593.3	593.0	-12.0	-11.6	-12.2	-12.0	-09.8	-13.1	-	01.6	01.7	01.6	89	89	89	89	N 9	NE 8	NE 9
17	593.6	594.3	593.3	-12.2	-12.0	-09.8	-11.0	-09.7	-13.2	-	01.6	01.6	02.0	89	89	91	90	NNE 7	N 6	N 7
18	592.7	592.9	593.0	-06.0	-05.0	-08.4	-07.2	-05.2	-10.0	-	01.3	01.5	01.1	46	50	47	48	N 7	NNW 3	NNW 7
19	593.5	593.5	594.3	-09.6	-07.0	-09.0	-08.6	-06.4	-11.0	-	02.0	01.9	01.8	91	70	78	79	NNW 5	W 2	NNE 3
20	595.1	595.1	594.9	-07.0	-03.2	-01.2	-03.2	-01.2	-09.4	-	01.9	01.6	00.2	70	43	04	39	SE 5	SW 3	W 2
21	592.8	590.6	587.9	-02.0	-01.6	-04.0	-02.9	01.0	-04.6	-	00.1	00.3	02.6	03	08	76	29	- 0	WSW 2	SW 5
22	585.5	585.3	584.7	-07.0	-11.0	-12.6	-11.0	-03.8	-13.6	-	02.5	01.7	01.5	93	89	88	90	SW 6	N 5	N 7
23	581.0	579.4	579.5	-12.4	-07.8	-09.8	-09.4	-05.4	-14.9	-	01.6	02.4	02.2	89	93	92	91	SE 4	SSW 7	SW 9
24	583.1	584.9	587.5	-09.0	-06.0	-08.8	-08.2	-05.8	-11.2	-	02.1	02.8	02.2	92	94	92	93	SW 9	SW 7	SW 10
25	584.7	583.0	583.9	-05.0	-04.8	-04.2	-04.6	-03.0	-08.8	-	03.0	03.1	03.2	95	95	96	95	SW 10	SW 9	SW 9
26	584.7	587.7	586.9	-04.8	-05.4	-05.0	-05.0	-04.2	-08.8	-	03.1	02.9	03.0	95	95	95	95	SW 10	SW 9	SW 7
27	589.9	589.2	588.3	-05.6	-03.2	-02.8	-03.6	-02.6	-08.4	-	02.9	03.5	03.6	95	97	97	96	SW 8	SW 9	SW 12
28	583.5	583.1	585.8	-02.0	-01.4	-04.0	-02.8	-00.6	-04.2	-	03.9	04.1	03.3	98	100	96	98	SW 12	SW 11	SSW 8
29	586.9	585.5	582.4	-03.0	-00.6	00.4	-00.8	01.0	-04.0	-	03.6	04.3	04.7	97	100	100	99	SSW10	SSW 9	SW 12
30	578.5	579.3	581.4	00.4	00.4	-03.4	-01.5	01.2	-03.6	-	04.7	04.7	03.5	100	100	97	99	SW 13	SW 12	W 8
31	582.6	580.5	576.7	-04.8	-01.6	-01.8	-02.5	-01.0	-06.2	-	03.1	04.0	03.9	95	98	98	97	WSW 5	SW 9	SW 8
MES. VRED.	591.6	591.6	591.5	-05.2	-04.2	-04.8	-04.7	-02.0	-07.7	-	02.5	02.6	02.5	80	78	79	79	6.6	6.0	6.0

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BR. ST. 142 H_s = 2067 m H_b = 2070.4 m h_t = 3.0 m h_r = 1.5 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednje		7	7	
1	8	10≡	09	10≡	09.7	01.1	.	.	F-F$_{SW}$ 0-13^{20} ≡ 2^{50} 9^{40} 16^{25}-24 ✱^{40} 9^{40}-11^{50} 15^{40}-16^{30}
2	8	00⊙	05⊙	01	02.0	10.4	02.9	.	≡ 0-3^{40} ✱^{500} 3^{40} 10^{50} F^{1}$_{S-SSW}$ 8^{50} 12^{20} 23^{05} 24
3	2	10≡	10	10≡	10.0	09.3	.	.	F$_{SSW}$ 0-6^{40} ≡ ≡ 6^{20}-14^{30} 18^{45}-24 ✱$^{600-500}$ 14^{30}-18^{15}
4	0	10≡	10≡	10≡	10.0	00.0	.	.	≡ 0-24, ● 17^{45}-18 ● 18-18^{45} 22^{45}-24
5	0	10≡	10●≡	10●≡	10.0	00.0	01.7	.	≡ 0-24, ● 0-0^{45} F-F$_{N}$ 0^{45}-24, ● 12^{30}-24
6	0	10≡	10●≡	10≡	10.0	00.0	07.1	.	≡ 0-24, F$_{N}$ 0-24, ● 0-2^{45} 9^{45}-16^{15}
7	0	10≡	10≡	10≡	10.0	00.0	10.9	.	≡ 0-24, F-F$_{N}$ 0-24, ● ● 11^{30}-13^{05} 23^{05}-24
8	8	10≡	04⊙	10≡	08.0	06.6	01.3	.	≡ 0-11^{30} 19^{20}-21^{45}, F$_{N}$ 0-4^{45}, ● 0-0^{50}
9	6	00⊙	05⊙	03	02.7	11.1	.	.	F$_{W}$ 0^{45}, 5^{45} ϟ$_{N}$ 19^{20}-23^{20}
10	2	06	08⊙	10≡	09.7	08.0	00.5	.	● 5^{30} 6^{20}, ≡ 19^{45}-24, F$_{NNE}$ 20^{45}-24
11	5	10≡	04⊙	00	04.7	10.5	.	.	≡ 0-8^{45} F$_{NNE}$ 0-11^{45} ⌓ 19^{30}-24
12	8	10≡	10	10≡	10.0	05.1	.	.	⌓ 0-6^{30}, F$_{N}$ 5^{45}-10^{30} ≡ 6^{30}-10^{45} 16^{45}-24
13	8	10≡	02⊙	00	04.0	11.3	.	.	F$_{N}$ 0-16^{30}, ≡ ≡ 0-7^{45} ⌓ 19^{45}-24
14	5	00⊙	05⊙	03	02.7	12.5	.	.	⌓ 0-7^{30} F$_{SSW}$ 18^{45}-24, ϟ$_{N}$ 20^{45}-23^{45}
15	8	04⊙	05⊙	05	04.7	08.4	.	.	F-F$_{SSW}$ 0-24
16	0	10≡	10●≡	10	10.0	00.0	.	.	F-F$_{SW-SSW}$ 0-16^{45} ≡ 1^{40} 19^{45} 22^{30}-24 ● 7^{05}-16^{10} 22^{45}-23^{30} ✱$^{400-200}$ 19^{45}-22^{30}
17	0	10≡	10≡	10≡	10.0	00.0	22.4	.	≡ 0-24, F-F$_{N}$ 7^{45}-24, ● 11^{45}-13^{10} V^{1}17^{40}-24 ✱ 22^{45}-23^{05}, ✱ 22^{45}-23^{45}, ⊠
18	0	10≡	10≡	10	10.0	00.0	01.6	02	≡ 0-17^{30}, F-F$_{N}$ 0-24 V 0-24 ✱ 17^{02}-8^{40} ✱ 17^{02} 8^{10} ⊠
19	8	06	06	00	04.0	08.5	01.2	01	F$_{SW-N}$ 0-3^{50} 12^{45} 17^{45}, V 0-11^{45}, ⌓ 0^{55}-1^{55} ✱$^{600-500}$ 19^{30}-25, ⌓ 19^{30}-24, ⊠
20	8	02⊙	04⊙	00	02.0	10.0	.	.	⌓ 0-7^{45}, F$_{SW}$ 1^{30}-24
21	8	00⊙	03⊙	00	01.0	14.0	.	.	F-F$_{SW-SSW}$ 0-13^{20}, 21^{30}-24
22	3	00⊙	01⊙	01	00.7	13.7	.	.	F$_{SW}$ 0-4^{30} 15-24
23	8	00⊙	03⊙	00	01.0	13.2	.	.	F$_{SW}$ 0-5^{50}
24	[illegible]	00⊙	03⊙	00	01.0	14.1	.	.	
25	8	00⊙	03⊙	05	02.7	09.3	.	.	F$_{SW}$ 1^{45}-18^{20}, ϟ$_{SW}$ 17^{20}-18^{45}, ● 17^{50}-18^{58}, ✱^{800} 18^{58}-n
26	0	10≡	10≡	10≡	10.0	00.0	03.1	.	● n, 11-12; F$_{N}$ n-n$_{i}$, ≡ n-22^{30}
27	5	05⊙	03⊙	00	02.7	13.9	00.5	.	F$_{NE}$ 15^{40}-h
28	8	00⊙	06	03	03.0	12.0	.	.	F$_{NE}$ n-n$_{i}$
29	9	00⊙	04⊙	00	01.3	14.3	.	.	⌓ n-8^{45} ≡ 19^{10}-20^{05}
30	5	00⊙	04⊙	01	01.7	12.3	.	.	⌓ n-7^{45} ✱^{400} n-9^{20} F$_{NE}$ 6^{45}-18^{45} ≡ ≡ 17^{55}-19^{45}
31	3	03⊙	10	02	05.0	07.1	.	.	⌓ n-7^{20}, ≡ 0^{20}-2^{50} 18^{20}-19^{50}, ✱^{400} n-11^{45}, T$_{N-S}$ 18-19^{40}
MES. VRED.		05.4	06.4	05.0	05.6	232.7	53.2		

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1	1	00⊙	10≡	02	04.0	04.5	.	.	⌓ n-7 ✱$^{400-500}$ n-13^{37} T ϟ$_{S-N}$ 10^{20}-17^{35}, ≡ 13^{37}-15^{50} ▲ 14^{35}-14^{45}, ● 14^{35}-17^{45}
2	8	04⊙	10ϟ	10	08.0	06.2	16.4	.	⌓ n-7^{20} ✱^{600} n-10^{15} ϟ$_{SW}$ 11^{07}-16^{35}, △ 11^{45}-12^{40}, ● 11^{45}-13
3	2	09	08	04	07.0	03.6	19.2	.	⌓ n-7^{20} 19^{45}-24, ✱^{1000} 2^{50}-10^{45}
4	8	04⊙	08⊙	04	05.3	06.3	.	.	⌓ 0-8^{50} ✱^{800} n-8^{45} ≡ 10^{05}-10^{45} ϟ$_{W-S}$ 10^{40}-10^{55}
5	8	00⊙	04⊙	00	01.3	07.4	.	.	⌓ n-7^{35}, ✱$^{500-300}$ n-10^{30}, ≡ 10^{30}-11^{50}
6	5	00⊙	02⊙	00	00.7	12.6	.	.	✱ n-8^{30}
7	8	00⊙	00⊙	00	00.0	12.7	.	.	F$_{W}$ 20^{30}-24, ϟ$_{N}$ 21^{20}-n
8	8	06⊙	05⊙	05	04.7	11.2	.	.	F$_{W,SW}$ 0-n, T$_{NW}$ 18^{07}
9	2	07⊙	03	02ϟ	05.7	04.5	00.2	.	✱^{500} n-8^{45}, F$_{SW}$ n-n, ϟ$_{S-NE}$ 6^{45}-6^{30}, ● 6^{20}-10^{45}, 19^{02}-19^{05}, ▲ 15^{35}-15^{37}, ϟ$_{NE}$ 20^{45}-n
10	0	10≡	10●≡	00	06.7	03.9	00.3	.	F-F$_{S}$ n-n, ✱^{600} n-7^{20}, ≡ 5^{50}-7^{20}, 15^{25}-14^{05}, ● 12^{35}-14^{40}
11	0	08⊙	10≡	10≡	09.3	02.2	00.2	.	≡ 8^{30}-n, ● 8^{35}-16^{25} F-F$_{N}$ 10^{50}-n
12	7	10≡	10●	00	06.7	02.6	04.1	.	≡ ≡ n-10^{55} 14^{35}-n; F$_{N}$ n-17^{30} ● 13^{50}-14^{12}
13	8	05⊙	04⊙	10≡	06.3	08.3	00.0	.	✱^{600} n-7^{45}, 14^{25}-18^{45}, ≡ ≡ 18^{45}-n
14	8	00⊙	02⊙	00	00.7	13.8	.	.	✱$^{1000-600}$ n-8^{30} 20-24, ⌓ 19^{30}-n
15	8	00⊙	02⊙	03	01.7	13.6	.	.	⌓ n-7^{45}, ✱^{800} 0-8
16	8	04⊙	06	03	04.3	08.7	.	.	✱^{500} 9-11^{30}
17	3	02⊙	07	04	04.3	09.1	.	.	✱^{800} n-8^{30} F$_{SW}$ 18-n
18	8	10≡	05⊙	00	05.0	09.4	00.9	.	● n-6^{30}, ≡ n-7, ≡ 7-10^{45}, ✱$^{200-600}$ 10^{45}-n
19	8	00⊙	04⊙	00	01.3	11.7	.	.	✱^{700} n-9, ⌓ n-6^{30}
20	6	05⊙	03⊙	00	02.7	13.2	.	.	✱^{800} n-8^{45}
21	8	03⊙	04⊙	10	05.7	09.2	.	.	✱^{800} n-8^{25} F-F$_{S}$ n-n, ϟ$_{S}$ 20^{25}-n
22	8	10≡	10	01	07.0	00.6	03.7	.	≡ ≡ n-13^{20}, ● n, 10^{12}-14^{35} 18^{26}-19^{03}, ϟ$_{S}$ 10^{22}-11^{15}, F$_{SW}$ 12^{45}-17^{45} ✱$^{800-400}$ 17^{50}-19^{50}
23	8	00⊙	06	00	02.7	10.1	05.9	.	✱$^{200-500}$ n-9, ⌓ n-8^{30}, F$_{SSW}$ 17^{45}-n, [ϟ$_{N}$ 20^{45}-n
24	0	10●≡	10●ϟ	02	07.3	00.8	00.0	.	F-F$_{S}$ n-n, ≡ n-18, ● 6^{30}-15^{40} T 7^{35}-7^{52}, ϟ$_{S-N}$ 13^{20}-14^{05}, ∩ 15^{30}-15^{45}, ϟ$_{SW}$ 20^{30}-n
25	0	10●≡	10≡	10≡	10.0	00.0	12.8	.	≡ n-n, F-F$_{N}$ n-n, ● n-7^{12}, 19^{03}-n
26	3	10≡	07	10≡	09.0	04.9	05.0	.	≡ n-13^{15}, 16^{45}-n; F-F$_{N}$ n-n, ● n-5^{15}
27	9	10≡	05⊙	10≡	09.3	03.7	00.3	.	F-F$_{N}$ n-n, ≡ n-12^{36}, 19^{12}-n
28	8	10≡	03⊙	03	08.7	07.1	.	.	≡ n-9^{40}
29	8	04⊙	08	10≡	07.3	01.7	.	.	F$_{SW}$ 15-n, ≡ 20^{30}-n
30	9	06⊙	10≡	10≡	03.7	00.9	.	.	≡ n, 12^{40}-n; F-F$_{SW}$ n-20, ● 14^{30}-20
31	9	00≡	00≡	00≡	00.0	00.0	21.6	.	≡ n-n, F-F$_{N}$ 8^{30}-n, ● 14^{30}-17^{30}, ϟ$_{N-S}$ 15^{30}-17^{05}
MES. VRED.		05.1	06.5	04.1	05.2	201.1	06.2		

1970 SEPTEMBAR

BJELAŠNICA

φ = 43° 43' N λ = 18° 16' E Gr. ΔG = + 1h 13 min.

BR. ST. 142

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	593.8	594.8	595.0	06.8	07.0	06.2	06.6	07.4	05.6	-	07.4	07.5	07.1	100	100	100	100	N 7	NNE 4	NNE 5
2	595.4	597.1	597.7	06.4	07.1	06.2	06.5	07.8	05.2	-	07.2	07.6	06.9	100	100	97	99	NNE 5	NNE 6	- 0
3	597.4	598.5	590.2	07.6	11.1	09.6	09.5	11.6	05.0	-	05.8	07.8	07.9	74	78	88	80	NW 4	- 0	SW 5
4	597.9	598.0	597.9	08.6	07.9	05.0	06.6	09.6	04.4	-	07.4	08.0	06.5	89	100	100	96	NW 3	NW 3	N 5
5	597.8	596.5	598.1	06.0	09.6	09.8	08.8	10.8	02.4	-	04.9	05.2	05.9	70	58	65	64	NE 5	- 0	NW 5
6	596.8	597.6	598.0	10.6	11.5	09.9	10.5	12.2	07.2	-	04.9	07.9	07.9	51	78	87	72	W 5	N 3	SW 2
7	597.9	598.8	599.2	07.2	07.8	08.1	07.8	10.2	06.2	-	07.6	07.9	05.2	100	100	64	88	N 2	NNE 3	N 5
8	599.4	599.7	600.1	09.6	14.0	10.6	11.2	14.0	06.8	-	05.4	06.1	07.4	60	51	77	63	WSW 5	S 4	WSW 5
9	599.5	599.8	599.3	12.0	15.0	11.6	12.6	15.2	09.0	-	05.0	06.7	06.7	48	52	65	55	SW 5	SW 4	SW 6
10	599.0	599.4	598.9	15.0	17.0	14.0	15.0	18.0	10.0	-	02.9	06.0	02.4	23	47	20	30	N 1	SW 2	SW 5
11	599.1	599.5	599.5	15.2	17.8	13.6	15.0	18.6	12.8	-	03.4	05.3	03.8	26	35	33	31	- 0	SW 5	SW 5
12	598.6	598.2	597.3	13.4	16.4	13.6	14.2	17.0	11.8	-	04.5	06.2	05.2	39	45	45	43	SW 3	SW 4	SW 7
13	595.0	595.2	595.5	12.6	16.8	12.0	13.4	17.0	12.0	-	05.3	06.5	08.0	49	45	76	57	SW 6	SW 6	SW 7
14	596.0	586.7	597.2	07.6	13.0	10.8	10.6	14.0	06.4	-	07.8	09.3	09.0	100	83	93	92	NE 3	S 5	- 0
15	597.3	598.5	598.5	10.4	14.4	11.4	11.9	14.6	09.2	-	07.5	05.1	07.2	79	41	71	64	SW 5	SW 5	SW 4
16	597.8	598.2	597.8	10.2	14.0	10.8	11.4	14.0	09.0	-	08.2	08.3	07.3	88	70	75	78	SW 8	SW 6	SW 5
17	597.5	597.7	597.7	02.6	03.4	01.6	02.3	12.0	00.0	-	05.5	05.8	05.1	100	100	100	100	N 5	N 4	N 6
18	597.7	598.9	599.4	03.6	06.0	05.3	05.0	06.5	00.8	-	05.9	07.0	06.7	100	100	100	100	N 5	ENE 6	NE 3
19	598.8	599.6	599.5	04.4	06.1	05.8	05.5	06.6	03.5	-	06.3	07.1	06.9	100	100	100	100	E 4	ENE 4	NNE 6
20	598.2	598.3	597.1	04.3	05.4	05.0	04.9	06.0	03.2	-	06.2	06.7	06.5	100	100	100	100	NE 6	NNE 5	NE 7
21	595.3	594.9	594.8	02.0	02.4	02.2	02.2	05.0	00.8	-	05.3	05.3	05.4	100	97	100	99	NE 9	NE 8	NE 8
22	593.3	595.5	595.8	03.2	04.0	01.0	02.3	04.7	00.0	-	05.8	06.1	04.9	100	100	100	100	NE 8	NNE 10	N 10
23	596.2	596.6	596.6	-02.2	01.8	03.2	01.5	04.0	-03.0	-	03.4	04.2	02.3	86	80	40	69	N 7	- 0	N 4
24	596.6	596.8	597.1	-01.2	01.8	-00.2	00.0	03.2	-03.0	-	02.8	04.0	04.2	67	77	93	79	NE 5	NE 4	- 0
25	596.1	596.8	597.1	00.0	02.7	02.4	01.9	02.8	-02.8	-	03.0	04.1	01.8	65	73	32	57	NE 2	NNE 2	NE 4
26	596.4	597.0	597.5	02.4	06.0	03.8	04.0	06.6	01.4	-	05.1	06.0	05.1	94	86	85	88	NE 8	NE 5	NE 3
27	597.8	599.5	600.0	00.2	00.2	00.2	00.2	03.8	-01.8	-	04.7	04.7	03.1	100	100	66	89	N 6	N 5	NE 4
28	599.2	600.0	599.9	-03.8	-02.4	-02.8	-03.0	01.4	-05.2	-	03.3	03.8	03.6	96	98	97	97	N 6	NE 6	NE 8
29	599.4	600.0	600.1	-08.4	-01.0	-01.8	-03.2	-00.8	-09.0	-	02.2	01.7	01.1	92	40	27	53	N 7	NE 7	NE 4
30	598.5	597.7	596.2	03.0	05.2	03.0	03.6	06.0	-01.8	-	00.6	01.8	02.9	10	27	51	29	W 2	- 0	SW 3
MES. VRED.	597.3	597.6	597.9	05.6	08.1	06.4	06.6	09.3	03.5	-	05.2	06.0	05.5	77	75	75	76	4.9	4.2	4.7

1970 OKTOBAR

BJELAŠNICA

1	591.2	588.2	586.6	00.0	-00.2	00.4	00.2	03.0	-00.4	-	04.6	04.5	04.7	100	100	100	100	SSW 9	SW 6	W 6
2	586.1	590.0	599.2	-02.2	-01.2	00.0	-00.8	00.4	-02.4	-	03.8	04.2	04.6	98	100	100	99	N 11	N 3	SW 2
3	584.7	584.8	586.2	-00.4	-03.0	-04.0	-02.8	00.0	-04.0	-	04.5	03.6	03.3	100	97	96	98	SW 7	N 7	NNW 5
4	586.6	588.7	590.4	-04.6	-02.8	-02.5	-03.1	-02.2	-05.0	-	03.1	03.6	03.7	96	97	98	97	N 5	N 7	N 10
5	593.1	594.2	595.0	-03.7	-00.5	02.2	00.0	02.4	-04.6	-	03.4	04.4	05.0	96	100	93	96	N 6	W 7	NW 6
6	595.4	596.5	597.2	04.9	05.2	05.2	05.1	06.3	00.6	-	04.3	05.5	04.6	66	83	69	73	W 5	WSW 5	SW 2
7	596.4	596.7	596.6	05.8	07.0	05.0	05.7	07.0	02.6	-	04.1	04.8	06.0	59	64	91	71	SW 6	SW 9	SW 10
8	598.1	598.8	599.6	04.6	08.6	05.4	06.0	08.6	03.0	-	06.4	06.7	05.4	100	80	80	87	SW 5	SW 3	SW 2
9	599.9	600.5	600.9	10.8	09.8	08.6	09.4	10.8	04.2	-	01.8	05.5	05.9	18	61	71	50	E 2	- 0	SSW 1
10	601.1	602.2	602.3	09.8	10.4	09.4	09.8	10.8	08.0	-	01.7	03.8	02.8	19	41	32	31	- 0	N 4	N 4
11	603.2	603.3	603.3	09.8	10.0	08.0	09.0	10.2	07.6	-	01.7	04.0	04.9	19	44	60	41	N 5	N 6	N 5
12	603.1	601.6	601.0	06.4	07.3	04.1	05.5	08.6	02.8	-	03.1	04.5	06.1	43	58	100	67	N 5	N 6	NNE 6
13	600.2	600.3	600.1	03.4	06.4	07.0	06.0	07.0	02.0	-	05.8	05.8	02.8	100	81	37	73	NE 6	ENE 2	- 0
14	598.1	597.6	596.9	05.0	09.0	05.2	06.1	09.4	03.8	-	05.0	05.7	05.7	77	66	86	76	W 4	- 0	- 0
15	595.5	595.3	595.9	01.2	01.0	-00.8	00.2	05.4	-01.1	-	05.0	04.9	04.3	100	100	100	100	NW 1	NNE 2	NNE 4
16	594.8	595.5	596.2	-04.8	-06.4	-07.0	-06.3	-00.8	-07.2	-	03.1	02.7	02.5	95	94	93	94	NNE 6	N 6	N 7
17	595.5	595.4	595.1	-06.8	-03.3	-03.8	-04.6	-03.2	-07.4	-	02.6	03.3	03.3	94	96	96	95	N 6	NNE 4	NNE 3
18	593.8	594.4	594.9	-01.0	00.0	-01.4	-01.0	00.1	-04.8	-	04.2	04.6	04.1	99	100	99	99	NNE 2	NNW 1	N 3
19	594.6	593.0	591.9	-01.0	02.0	01.2	00.8	02.2	-02.8	-	04.2	04.6	02.8	99	87	56	81	- 0	SSW 4	SSW 2
20	587.4	583.3	583.6	00.0	02.6	02.6	02.0	03.4	-00.2	-	04.6	05.5	05.5	100	100	100	100	SSW 7	SSW 12	S 12
21	582.0	584.5	586.8	02.6	02.0	01.4	01.8	03.6	01.2	-	05.5	05.3	05.1	100	100	100	100	S 9	SSW 8	SSW 7
22	589.7	589.8	589.7	01.0	00.6	-03.1	-01.2	02.0	-04.0	-	04.9	04.8	03.5	100	100	97	99	SSW 4	SW 3	NNE 3
23	588.2	588.3	589.0	-06.4	-06.0	-07.1	-06.6	-03.1	-07.6	-	02.7	02.8	02.5	94	94	93	94	NE 5	NE 6	NNE 7
24	590.0	591.0	593.2	-08.2	-08.2	-08.4	-08.3	-06.6	-09.0	-	02.3	02.3	02.2	92	92	92	92	NNE 9	N 8	N 8
25	592.5	595.1	596.2	-09.8	-06.6	-02.4	-05.3	-02.0	-11.2	-	02.0	02.6	03.8	91	94	98	94	N 8	N 8	N 7
26	597.4	598.7	598.0	-00.5	00.0	00.0	-00.1	00.2	-02.4	-	04.4	04.6	03.8	100	100	82	94	N 6	- 0	W 2
27	597.1	597.9	599.0	01.4	02.0	00.6	01.2	02.0	-00.4	-	03.1	04.4	04.8	60	84	100	81	NNE 1	- 0	NNE 2
28	600.3	600.4	599.8	-00.2	03.2	04.0	02.8	04.4	-01.0	-	03.4	04.5	02.6	75	78	42	65	SE 2	SSW 3	SW 6
29	598.2	599.2	599.6	03.0	05.0	03.0	03.5	05.4	01.4	-	02.9	04.0	05.0	51	61	87	66	SW 7	WSW 4	N 7
30	601.6	601.6	600.8	02.2	06.6	06.2	05.3	06.6	01.8	-	05.0	04.7	03.5	93	64	50	69	N 5	WSW 4	SW 7
31	599.5	599.4	599.6	05.1	07.0	02.4	07.2	08.4	04.4	-	02.0	03.0	01.2	31	40	15	29	WSW 7	SW 6	WNW 2
MES. VRED.	594.6	595.0	595.3	00.9	02.2	01.5	01.5	03.6	-01.0	-	03.7	04.4	04.1	80	82	81	81	5.2	4.6	4.8

BJELAŠNICA 1976 SEPTEMBAR

BR. ST. 142 H_s = 2067 m H_b = 2070.4 m h_t = 3.0 m h_r = 1.5 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	0	10 ●≡	10●≡	10≡	10.0	00.0	01.7	•	●n-7^30 ≡ n-n, F-F_NNE n-9^35, ● 13^45-17^55
2	0	10≡	10≡	00	06.7	00.3	02.4	•	● n, 9^40-10^45 ≡≡ n-20^45 F_NNE 6^45-15, ⚡^200 20^45 n
3	3	00⊙	06⊙	07	04.3	03.2	00.0	•	⌒n-8^45 ⚡^440-1000 n-10^30 F 20^45 n
4	0	00	10≡	10≡	09.7	00.0	•	•	⚡^800-1000 10^45-11^33 ≡ 11^30 n, ● 12^55-15^35 i
5	8	00⊙	08⊙	00	02.7	12.5	02.7	•	⚡^1000-800 n-11
6	8	00⊙	07⊙	03	04.3	05.9	•	•	⚡^1000 n-9^40 ≡ 22^30-24
7	0	10≡	10≡	00	06.7	00.3	00.1	•	≡≡ 0-15^30 ⚡^400-600 6^55-24
8	9	00⊙	00⊙	00	00.0	12.6	•	•	⚡^1000 0-11
9	9	00⊙	03⊙	00	01.0	11.5	•	•	F_SW 12^45-n
10	9	00⊙	00⊙	00	00.0	12.0	•	•	
11	9	00⊙	00⊙	00	00.0	12.0	•	•	F_SW 12^45-19^40
12	8	03⊙	00⊙	01	04.0	07.3	•	•	F_SW 0^45-2^30 14^30-24
13	9	03⊙	02⊙	00	01.7	11.7	•	•	F-F_SW 0-24, ≡ 22^30-24
14	8	10≡	04⊙	04	06.0	06.2	00.3	•	F_SW 0-1^30 ≡ 0-10^25 ⌒ 18^30-24
15	8	00⊙	00⊙	00	00.0	11.8	•	•	⌒ 0-17^40 ⚡^1000 5^40-8^50
16	6	00⊙	01⊙	03	02.7	11.4	•	•	F-F_SW 0^40-21^45 G_N 19^30-23^40
17	0	10≡	10≡	10●≡	10.0	00.0	00.2	•	≡ 2^30-24, ● 3^40-4^45 10^45-11^50. F_N 6^40-24 i, ● 17^40-24^40
18	0	10≡	10≡	10●≡	10.0	00.0	00.4	•	F_N 0-18, ≡ 0-24, ● 0^50-2^50 18^45-21^15
19	0	10≡	10≡	10≡	10.0	00.8	00.3	•	≡≡ 0-24 F_E-NE 1-5^45 19^40-24
20	0	10●≡	10≡	10≡	10.0	00.0	01.4	•	≡≡ 0-24, F_NE-N 0-24, ● 4^45-6^25, ● 6^25-7^45
21	8	10≡	08	10≡	09.3	02.9	•	•	F-F_NE 0-24, ≡ 0-11^50, 17^40-24
22	0	10≡	10●≡	10≡	10.0	00.0	•	•	F-F_NE 0-24, ≡ 0-24, ● 7^50-23^45
23	8	08	07	00	05.0	04.2	04.0	•	F-F_N 0-7^45 ≡≡ 0-4^05 V 0^45-8^30 ⚡^1000 4^05-11
24	9	00⊙	03⊙	00	01.0	11.5	•	•	≡≡ 0^35-1^35 ⚡^400 1^25-9, F_NE 6^30-11
25	8	00	00⊙	00	00.0	10.7	•	•	≡ 0-3^45, ⌒ 0^40-8^40 ⚡^1300 3^35-10^30
26	8	08	06⊙	00	04.7	07.4	•	•	F-F_NE 0^45-18^30 ⚡^1000 4^50-8^45
27	0	10≡	10≡	00	06.7	00.0	02.6	02	≡ 0^40-17^45 ● 2^40-4^40 * 4^40-6^40 V 4^40-9^40 F-F_N 7^40-13^45 i, ⚡^300-200 17^45-20^30 ⊠
28	9	10≡	10	10≡	10.0	00.0	•	•	⌒ 4^50-11^40 ≡ 5^45-12^40 17^30-24; F-F_N-NE 6^45-24 i, ⚡^300 12^40-17^30, V 19^40-24
29	8	00⊙	00⊙	00	00.0	10.7	•	•	≡ 0-5^45 V 0-8^40, F-F_N-NE 0-16^40 ⚡^400-600 5^45-8^30
30	9	00⊙	00⊙	00	00.0	11.0	•	•	⚡^1000 4^50-11
MES. VRED.		05.0	05.9	03.6	04.8	192.2	25.7		

BJELAŠNICA 1976 OKTOBAR

1	0	10≡	10≡	10≡	10.0	00.0	•	•	F-F_SW 2-24, ≡ 5^30-8, 12^40-24; * 13^40-15^30 20^45-21^40; ● 15^40-22^40, * 20^40-21^40 ⊠
2	0	10≡	10≡	03	07.7	00.3	12.4	01	≡ 0-14^30 F-F_N-NW 0-12^30 18^30-19^45. V 2-22^40 ⊠
3	0	10*≡	10*R≡	10≡	10.0	00.0	06.0	•	F-F_WSW-SW 0^45-23, ≡ 3^30-24, V 4^30-24, * 6^30-8^30 R_a-N 12^40-14^45 + + 12^30-24 i, ⊠
4	8	10≡	04⊙	10*≡	08.0	03.2	08.2	08	≡ 0-8^30 14^30-24; V 0-24, + 0-6, ⚡^400 8^30-14^30 F-F_N 12^45-24, * 17^30-23^45 i, ⊠
5	8	01⊙	09	06	05.3	06.2	03.6	08	V 0-14^45, ≡ 0-2^55, F-F_N-W 0-7^30, 12^45-24; + + 0-2^45, ⚡^400 5^45-9, ⊠
6	8	00⊙	02⊙	00	00.7	11.1	•	04	F_W 0-12, ⚡^400-800 4^45-10^30 ⊠
7	9	00⊙	00⊙	00	00.0	10.6	•	•	⚡^400-1200 4^45-9^45, F-F_SW 4^30-24, ≡ 23^40-24
8	8	10≡	03⊙	00	04.3	10.0	•	•	≡ 0-7^40 F-F_SW 0-7^30 ⚡^400 7^40-9^45, ⌒ 21^30-24
9	9	00⊙	00⊙	00	00.0	11.2	•	•	⌒ 0-7^30 ⚡^1000 3^30-11^45
10	9	00⊙	00⊙	00	00.0	11.2	•	•	⌒ 0-8, ⚡^400-800 3^30-9^45, F_N 21^30-24
11	9	00⊙	00⊙	00	00.0	10.9	•	•	F_N 0-24, ⚡^800-400 4^30-10^45
12	9	00⊙	00⊙	00≡	00.0	10.8	•	•	F_N 0-24, ⚡^800-200 2^45-10^45, ≡≡ 20^45-24, ⌒ 20^45-24
13	8	10≡	00⊙	00	03.3	09.5	•	•	F 0-8^45 ≡≡ 0-10^45 ⌒ 0-8^30 18^30-24; ⚡^200 10^45-24
14	8	00⊙	02⊙	09	03.7	10.0	•	•	⌒ 0-7^40 ⚡^800-1000 0-11^30 18^30-24
15	0	10≡	10●≡	10●≡	10.0	00.0	•	•	⚡^1000 0-0^45, ≡ 0^45-24, ● 8^30-21^30 i, △ 16^45-17^45, V 19^45-24, * 21^30-24 ⊠
16	0	10≡	10≡	10≡	10.0	00.0	04.6	07	* 0-5^45, ≡ 0-24 V 0-24, F_NNE-N 5^45-24 i, ⊠
17	0	10≡	10≡	10≡	10.0	00.0	•	04	≡ 0-24, V V 0-24, F_N 0-9^45, ⊠
18	0	10≡	10≡	10≡	10.0	00.0	•	12	≡ 0-24, V 0-13^45, ⊠
19	9	00⊙	04⊙	01	01.7	10.7	•	01	≡ 0-5^45 ⚡^400-600 5^45-24 ω 23^30-24, ⊠
20	0	10≡	10≡	10●≡	10.0	00.0	•	•	ω 0-0^40, ⚡^400-600 0-0^40, ≡ 0^40-24, F-F_SSW 0^40-24, ● 14^45-21^40 i
21	0	10≡	10≡	10≡	10.0	00.0	07.6	•	F-F_S 0-24, ≡ 0-24, ● 5^50-14^45 i, 19^40-23^50 i, ∽ 12^30-13^30 * 20^30-20^50 + 23^30-24
22	0	10≡	10*≡	10*≡	10.0	00.0	2.4	•	⌒ 0-1^40 ≡ 0-24, R_S-N 0^45-1^40 F-F_SSW 0-6^40 ● 1^40-4^30 * 17^30-24, V 15^45-24, ⊠
23	0	10*≡	10≡	10≡	10.0	00.0	18.1	•	* 0-7^40 ≡ 0-24, V 0-24, F-F_NE-NNE 8^45-24 + + 8^45-24, ⊠
24	0	10≡	10≡	10≡	10.0	00.0	00.4	•	≡ 0-24, V 0-24, F-F_NNE 0-24, + 0-24, ⊠
25	0	10≡	10≡	10≡	10.0	00.0	•	•	≡ 0-24, F-F_N 0-24, V 0-24, + 0-24, ⊠
26	9	00⊙	00⊙	00	01.7	00.0	•	30	≡ 0-6^40 F-F_N 0-10^45 V 0-13^45, + 0-3^30, ⚡^300-600 6^40-16^30
27	9	03⊙	02⊙	10≡	05.0	03.0	•	22	⚡^800 5-12^45 ≡ 16^40-24 ⊠
28	9	02⊙	04⊙	00	02.0	09.4	•	19	≡ 0-0^30 ⚡^800 0^30-5^45, F_SSW 18^45-24, ⊠
29	9	06⊙	07⊙	02	05.0	07.5	•	15	F-F_SW-N 0-24, ⚡^1000 5-11^30, ⊠
30	9	00⊙	00⊙	00	00.0	09.9	•	12	F-F_N 0-8, 18^30-24; ⊠
31	9	00⊙	00⊙	00	00.0	10.1	•	07	F-F_SW 0-15, ⊠
MES. VRED.		05.5	05.9	03.2	05.4	171.1	31.5		

φ = 43° 43' N λ = 18° 16' E Gr. ΔG = + 1h 13 min. BR. ST. 142

Dan	Vazdušni pritisak P mm 7	14	21	Temperatura vazduha T C° 7	14	21	Sred. Dan	Max	Min	Min 5 cm	Napon vodene pare e mm 7	14	21	Relativna vlažnost u% 7	14	21	Sred. Dan	Pravac i jačina vetra D, I (0—12) 7	14	21
1	599.7	598.9	598.3	06.0	09.2	07.4	07.5	09.4	05.0	-	01.6	01.7	00.9	23	19	11	18	- 0	SW 4	WSW 5
2	598.5	598.9	599.1	08.8	09.4	09.4	09.2	10.6	07.2	-	01.0	01.9	01.8	12	22	20	18	NNE 4	NNE 1	W 3
3	598.6	596.7	596.4	08.0	08.9	07.4	07.9	09.4	06.0	-	03.2	02.6	03.4	40	30	44	38	N 2	SSW 7	WSW 7
4	595.7	596.7	598.2	06.8	03.5	03.8	04.5	08.0	01.6	-	01.8	05.0	02.7	24	85	45	51	WNW 4	NNE 5	NE 4
5	597.8	595.4	593.4	06.4	07.2	04.0	05.4	07.3	02.6	-	01.6	03.6	03.6	22	47	59	43	SW 4	SW 8	SW 9
6	592.0	591.2	591.9	01.8	-03.2	-06.8	-03.8	04.0	-07.8	-	05.2	03.5	02.6	100	97	94	97	SSW 3	N 3	N 6
7	591.8	592.5	593.3	-08.0	-06.8	-02.6	-05.0	-02.6	-10.0	-	02.3	02.6	02.7	92	94	71	86	N 6	N 2	- 0
8	591.3	593.3	596.0	-02.2	00.0	00.0	-00.6	01.0	-02.6	-	03.8	04.6	04.6	98	100	100	99	SSW 6	SSW 8	N 1
9	593.8	592.0	590.9	00.4	01.9	01.0	01.0	02.8	-00.1	-	04.7	05.2	04.9	100	100	100	100	SW 7	SW 6	SW 7
10	588.6	588.4	590.4	-00.4	-04.0	-05.6	-03.9	01.4	-05.6	-	04.5	03.3	02.9	100	96	95	97	W 2	N 7	N 6
11	591.9	594.1	594.8	-06.4	-06.6	-05.0	-05.8	-04.8	-07.4	-	02.7	02.6	02.9	94	94	91	93	N 7	N 6	N 6
12	596.3	596.6	596.9	00.3	01.8	02.2	01.6	02.4	-05.2	-	03.4	03.4	02.7	74	64	50	63	N 2	SW 3	SW 3
13	595.7	594.6	593.6	01.1	02.0	00.0	00.8	02.6	00.0	-	01.2	01.2	01.4	23	22	31	25	SW 6	SW 8	SW 8
14	591.3	590.7	588.1	00.0	01.0	02.1	01.3	02.6	-00.8	-	04.6	04.9	05.3	100	100	100	100	SW 11	S 9	S 8
15	586.3	585.4	582.9	00.9	00.0	00.0	00.2	03.2	-01.0	-	04.9	04.6	04.6	100	100	100	100	S 8	SSW 9	SSW11
16	581.8	582.0	584.5	-02.4	-02.8	-07.0	-04.8	00.0	-07.8	-	03.8	03.6	02.5	100	97	93	97	- 0	S 7	N 7
17	587.9	589.7	590.3	-05.7	-05.8	-02.0	-04.6	-01.0	-09.5	-	02.2	02.8	03.6	92	94	90	92	NNE 3	WSW 4	SW 8
18	591.2	592.7	592.7	-03.0	-01.9	-00.7	-01.8	-00.6	-04.0	-	03.3	03.9	04.4	96	98	100	98	SW 9	SW 7	SW 9
19	590.5	589.8	590.4	01.0	01.1	00.8	00.9	01.8	-00.7	-	04.9	05.0	04.9	100	100	100	100	SW 12	SSW13	SW 11
20	590.0	590.9	593.0	01.0	01.6	01.6	01.4	02.0	00.4	-	04.9	05.1	05.1	100	100	100	100	SW 10	SW 9	SW 7
21	591.3	590.0	587.5	02.0	02.6	02.0	02.2	02.8	01.2	-	05.3	05.5	05.3	100	100	100	100	SW 9	SW 11	SW 10
22	584.5	583.7	586.0	-02.0	-02.6	-04.0	-03.2	02.4	-04.0	-	03.9	03.7	03.3	98	97	96	97	SW 8	SW 5	N 2
23	585.6	586.4	589.2	-05.6	-06.4	-06.2	-06.1	-04.0	-06.6	-	02.9	02.7	02.7	95	94	94	94	N 10	N 11	N 10
24	592.6	595.5	596.1	-04.0	-02.6	-03.4	-03.4	-02.0	-06.4	-	03.3	03.7	03.5	96	97	97	97	N 9	N 2	N 4
25	596.2	597.2	597.6	-02.6	-03.0	-03.6	-03.2	-02.0	-04.2	-	03.7	02.9	02.0	97	78	57	77	N 4	N 2	N 3
26	596.2	598.7	598.7	-03.0	-02.3	-02.8	-02.7	-02.0	-03.6	-	02.2	02.4	03.0	59	62	82	68	N 3	NE 7	NE 6
27	598.5	598.9	599.4	-01.8	00.8	02.6	01.0	02.8	-02.8	-	02.2	02.5	02.2	55	52	40	49	NE 7	NNE 4	NNE 4
28	597.9	597.0	596.0	02.4	02.4	01.0	01.7	03.6	00.0	-	02.3	03.2	02.5	43	59	50	51	W 5	W 6	W 5
29	594.9	594.8	594.6	00.1	01.0	01.0	00.8	02.0	-00.8	-	02.6	03.8	04.6	56	76	93	75	WSW 6	SW 7	WSW 7
30	595.0	593.1	592.4	04.0	01.0	00.0	01.2	05.0	00.0	-	04.4	04.9	04.6	72	100	100	91	SW 7	SW 10	SW 11
MES. VRED.	592.8	592.9	593.1	00.0	00.2	-00.1	00.0	02.3	-02.2	-	03.3	03.5	03.4	75	79	77	77	5.8	6.4	6.3

1	594.5	593.6	592.6	01.4	01.0	00.0	00.6	01.9	-00.4	-	05.1	04.9	04.6	100	100	100	100	SW 5	SW 5	SW 2
2	592.2	593.0	593.5	-01.2	-01.4	-03.4	-02.4	00.4	-03.6	-	04.0	03.6	03.5	95	88	97	93	- 0	- 0	NNE 1
3	592.8	591.0	588.3	-04.0	-02.0	-03.4	-03.2	-01.6	-04.4	-	03.3	03.9	03.5	96	98	97	97	N 2	SW 6	W 10
4	589.1	591.1	590.7	-07.0	-10.2	-10.4	-09.5	-02.8	-11.8	-	02.5	01.9	01.9	93	90	90	91	N 10	N 7	N 12
5	592.6	594.5	595.5	-08.8	-04.4	-02.8	-04.7	-02.4	-10.4	-	02.0	02.1	03.6	86	65	97	83	N 10	NNW 6	N 5
6	594.0	595.7	596.0	-07.3	-07.6	-08.0	-07.7	-02.4	-09.4	-	02.5	02.4	02.3	93	93	92	93	NE 10	N 7	ENE 6
7	596.7	596.1	595.9	-07.4	-04.0	-02.8	-04.2	-02.4	-09.8	-	02.4	01.8	01.5	93	52	41	62	W 3	SW 3	WSW 6
8	597.2	598.5	599.6	-04.2	-01.6	-03.6	-03.2	-00.8	-05.0	-	02.7	04.1	03.2	79	100	91	90	SW 7	SW 6	WNW 5
9	599.2	599.1	597.0	-09.2	-07.8	-06.4	-07.4	-03.6	-12.0	-	02.1	02.4	02.3	91	93	80	88	N 8	N 6	N 11
10	595.7	597.2	597.9	-08.0	-06.2	-05.2	-06.2	-04.0	-08.6	-	02.3	02.1	02.6	92	74	82	83	N 11	N 9	NNE 9
11	599.0	600.9	601.9	-04.5	-02.4	-01.5	-02.5	-01.2	-05.8	-	02.1	03.3	03.2	65	86	78	76	N 8	NNE 5	NE 4
12	601.4	601.3	601.3	02.2	03.4	03.8	03.3	03.8	-01.5	-	00.9	01.3	01.4	17	22	23	21	NNE 3	- 0	- 0
13	600.8	598.9	599.2	03.8	03.6	01.8	02.8	04.4	01.4	-	01.4	01.3	01.3	23	22	24	23	- 0	SW 5	- 0
14	597.9	596.8	596.1	00.3	00.9	00.2	00.4	02.8	-01.3	-	02.2	01.4	01.6	47	29	35	37	- 0	W 3	SW 5
15	594.2	593.8	593.8	-04.1	-07.8	-10.0	-08.0	01.4	-10.0	-	02.2	02.4	01.9	65	93	91	83	NNE 3	N 4	N 7
16	593.0	593.3	593.0	-12.0	-11.6	-12.2	-12.0	-09.8	-13.1	-	01.6	01.7	01.6	89	89	89	89	N 9	NE 8	NE 9
17	593.6	594.3	593.3	-12.2	-12.0	-09.8	-11.0	-09.7	-13.2	-	01.6	01.6	02.0	89	89	91	90	NNE 7	N 6	N 7
18	592.7	592.9	593.0	-06.0	-06.0	-08.4	-07.2	-05.2	-10.0	-	01.3	01.5	01.1	46	50	47	48	N 7	NNW 3	NNW 7
19	593.5	593.5	594.3	-09.6	-07.0	-09.0	-08.6	-06.4	-11.0	-	02.0	01.9	01.8	91	70	76	79	NNW 5	W 2	NNE 3
20	595.1	595.1	594.9	-07.0	-03.2	-01.2	-03.2	-01.2	-09.4	-	01.9	01.6	00.2	70	43	04	39	SE 5	SW 3	W 2
21	592.8	590.6	587.9	-02.0	-01.6	-04.0	-02.9	01.0	-04.6	-	00.1	00.3	02.6	03	08	76	29	- 0	WSW 2	SW 5
22	585.5	585.3	584.7	-07.0	-11.0	-12.6	-11.0	-03.9	-13.6	-	02.5	01.7	01.5	93	89	88	90	SW 6	N 5	N 7
23	581.0	579.4	579.5	-12.4	-07.8	-09.8	-09.4	-05.4	-14.9	-	01.6	02.4	02.2	89	93	92	91	SE 4	SSW 7	SW 9
24	583.1	584.9	587.5	-09.0	-06.0	-08.8	-08.2	-05.8	-11.2	-	02.1	02.8	02.2	92	94	92	93	SW 9	SW 7	SW 10
25	584.7	583.0	583.9	-05.0	-04.8	-04.2	-04.6	-03.0	-08.8	-	03.0	03.1	03.2	95	95	96	95	SW 10	SW 9	SW 9
26	584.7	587.7	589.9	-04.8	-05.4	-05.0	-05.0	-04.2	-08.8	-	03.1	02.9	03.0	95	95	95	95	SW 10	SW 9	SW 7
27	589.9	589.2	588.3	-05.6	-03.2	-02.8	-03.6	-02.6	-08.4	-	02.9	03.5	03.6	95	97	97	96	SW 8	SW 9	SW 12
28	583.5	583.1	585.8	-02.0	-01.4	-04.0	-02.8	-00.6	-04.2	-	03.9	04.1	03.3	98	100	96	98	SW 12	SW 13	SSW 8
29	586.9	585.5	582.4	-03.0	-00.6	00.4	-00.8	01.0	-04.0	-	03.6	04.3	04.7	97	100	100	99	SSW10	SSW 9	SW 12
30	578.5	579.3	581.4	00.4	00.4	-03.4	-01.5	01.2	-03.6	-	04.7	04.7	03.5	100	100	97	99	SW 13	SW 12	W 8
31	582.6	580.5	576.7	-04.8	-01.6	-01.8	-02.5	-01.0	-06.2	-	03.1	04.0	03.9	95	98	98	97	WSW 5	SW 9	SW 8
MES. VRED.	591.6	591.6	591.5	-05.2	-04.2	-04.8	-04.7	-02.0	-07.7	-	02.5	02.6	02.5	80	78	79	79	6.6	6.0	6.0

BR. ST. 142 H_s = 2067 m H_b = 2070.4 m h_t = 3.0 m h_r = 1.5m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	9	00⊙	03⊙	00	01.0	10.1	.	05	F_{sw} 15^{30}-24, ⊠
2	9	09⊙	06⊙	02	05.7	09.6	.	04	⊠
3	9	04	09	00	04.3	05.4	.	03	F_{ssw} 11^{45}-24, ⊠
4	2	00⊙	06	06	04.0	09.0	.	02	F_{sw} 0-5^{45} ⧗$^{600-1000}$ 5^{30}-9^{45} ⊠
5	8	00⊙	07⊙	05	04.0	10.0	.	01	⧗$^{600-500}$ 5^{30}-10^{45}, F-F_{sw} 8^{45}-24, ⊠
6	0	10●≡	10≡	10	10.0	00.0	00.0	.	F-F_{sw-N} 0-3^{45} 14^{30}-24, ≡ 0^{45}-18^{45} ● 6^{45}-8^{45} 11^{45}-13^{30} * 8^{45}-10, 14^{45}-17^{45} + + 14^{30}-24, V14^{45}
7	9	00⊙	01⊙	00	00.3	09.7	03.8	03	F_N 0-10^{30}, V 0-10^{30} + + 0-4^{30}, ≡ 6^{45}-6^{45} * 3^{45}-4^{45} ⧗$^{300-500}$ 6^{45}-14^{30}, ⊠ [-24, ⊠
8	0	10≡	10≡	10≡	10.0	00.0	.	01	F-F_{ssw} 6^{45}-15, ≡ 6^{30}-24, * * 14-17 ⧗^{300} 21^{45}-23, ⊠
9	0	10≡	10●≡	10≡	10.0	00.0	02.0	03	≡ 0-24, ⧗^{600} 16^{30}-4^{30} F_{sw} 2-24, * 10^{30}-11 ● 11-15^{45} * 17^{45}-19^{45}, ⊠
10	0	10*≡	10≡	10≡	10.0	00.0	08.6	02	≡ 0-24, F_{sw} 0-24, * 3^{45}-9^{45}, + 8-17, V 11^{45}-24, ⊠
11	0	10≡	10≡	00	06.7	00.5	02.0	05	≡ 0-15^{30} F-F_N 0-24, V 0-24, ⊠
12	9	00⊙	00⊙	00	00.0	09.6	.	05	V 0-14^{30} F_N 0-4^{45} ⧗$^{1000-1500}$ 5^{45}-12^{45}, ⊠
13	9	00⊙	03⊙	09	04.0	09.9	.	02	F-F_{sw} 0-0^{45}-24, ⧗$^{600-1000}$ 5^{30}-12, ⊠
14	0	10≡	10●≡	10●≡	10.0	00.0	.	01	F_{sw} 0-24, ≡ 4^{30}-24, V V 5-11^{45} ● 11^{45}-16^{30} ● 16^{30}-22^{45} ⊠
15	0	10≡	10●≡	10*≡	10.0	00.0	17.2	.	≡ 0-24, F-F_s 0-24, ● 0^{30}-5^{45}, 13^{30}-19^{45} ● 10^{30}-13^{30} * 19^{45}-20^{45}, * 20^{45}-24, + 20^{30}-24,
16	0	10*≡	10*≡	10≡	10.0	00.0	12.6	15	* 0-17^{30} ≡ 0-24, F-F_{sw} 0-5^{30} 13-24; V 0-24, + 0-5^{30} ⊠ [V 20^{30}-24, ⊠
17	0	00	07⊙	03	03.3	07.4	08.3	27	≡ 0-5^{55} V 0-24, F-F_{N-sw} 0-5, 15^{45}-24; + 0-5, 19^{30}-24, ⧗$^{200-600}$ 5^{55}-13^{45}, ⊠
18	0	10≡	10≡	10≡	10.0	00.0	.	27	V 0-24 F_{sw} 0-24, + 0-14^{45} ≡ 0^{28}-24, ⊠
19	0	10≡	10≡	10≡	10.0	00.0	.	18	≡ 0-24, V 0-2^{45}, F_{sw} 0-24, ⊠
20	0	10≡	10≡	10≡	10.0	00.0	.	10	≡ 0-24, F-F_{sw} 0-24, ⊠
21	0	10≡	10●≡	10●≡	10.0	00.0	01.4	07	≡ 0-24, F-F_{sw} 0-24, ● 2-5, 13^{30}-24; ⊠
22	0	10≡	10*≡	10*≡	10.0	00.0	13.2	03	● 0-3^{30}, F-F_{sw} 0-17, 22^{30}-24, ≡ 0-24, * 3^{30}-4^{30}, 9^{30}-23; + 9-24, F_{ssw-N} 10^{30}-10^{35},
23	0	10≡	10≡	10≡	10.0	00.0	02.3	09	≡ 0-24, F-F_0 0-24, V 0-24, + + 0-24, ⊠ [V 15-24, ⊠
24	0	10≡	10≡	00	06.7	01.3	.	05	≡ 0-14^{45} V 0-24, F-F_N 0-10^{30}, + + 0-11, ⧗$^{300-600}$ 14^{45}-24, ⊠
25	9	00⊙	01⊙	00	00.3	09.0	.	06	V 0-24, ⧗$^{300-600}$ 0-24, ⊠
26	9	00	00⊙	00	00.0	08.3	.	05	V 0-24, ⧗$^{300-1200}$ 0-14^{30} F_{NE} 12^{45}-24, ⊠
27	9	00	00⊙	00	00.0	08.5	.	05	V 0-17^{45} F_{NE} 0-8^{45} ⧗$^{800-1200}$ 5^{30}-24, ⊠
28	9	03	06⊙	00	03.0	03.5	.	04	⧗$^{600-1000}$ 0-24, F_w 13^{45}-24, ⊠
29	9	00	01⊙	00	00.3	09.2	.	03	F-F_{wsw-sw} 0-24, ⧗$^{600-1000}$ 0-20 ≡ 22^{30}-24, ⊠
30	0	08	10≡	10≡	09.3	00.0	.	01	≡ 0-2^{30}, 11^{30}-24, F-F_{sw} 0-24, ⧗^{600} 2^{30}-8, ⊠
MES. VRED.		05.8	07.0	05.5	06.1	124.0	76.4		

1	0	10≡	10≡	10≡	10.0	00.0	01.2	.	F-F_{sw} 0-7^{45} 13^{30}-18, ≡ 0-24, ● 4^{30}-5^{45}, * 15^{30}-16^{45}, * 16^{45}-17^{30} 21^{30}-22^{30}, + 16^{30}-18^{30}, ⊠
2	6	08	04⊙	10≡	07.3	05.8	04.6	05	≡ 0-3^{30} 18^{35}-24; ⧗^{600} 5-18^{35} ⊠
3	0	10≡	10≡	10≡	10.0	00.1	.	05	≡ 0-23^{50}, V 4^{30}-24, F-F_{sw} 9^{45}-24, + + 19^{40}-23^{45} ⊠
4	8	10≡	03⊙	00	04.3	05.5	02.8	11	V 0-24, F-F_{w-N} 0-24, * 3^{10}-5^{45} 8^{45}, 9^{45} + 3^{10}-24, 13^{45} 8^{30} 8^{40} ⊠
5	8	00	08⊙	10*≡	06.0	07.4	02.6	12	V 0-24, F-F_N 0-19^{05}, + 0-8^{50}, ⧗^{1000} 15^{45}-19^{45}, * 18^{30}-24, ≡ 19^{45}-24, ⊠
6	0	10≡	10≡	10≡	10.0	00.0	02.9	16	* 0-2^{45} V 0-24, ≡ 0-21^{45} F-F_{NE} 2^{30}-22^{40}, + 2^{30}-12^{30}, ⧗^{600} 21^{45}-24, ⊠
7	8	00⊙	03⊙	08	03.7	08.0	.	14	V 0-14^{45} ⧗^{800} 0-24, F_{sw} 15^{30}-24, ⊠
8	0	03	10≡	10≡	07.7	01.1	.	10	⧗^{1000} 0-8^{45} F_{sw} 0-17^{30} ≡ 8^{45}-23^{40}, V 14^{30}-24, ⊠
9	8	04	00⊙	08	04.0	07.1	.	07	V 0-24, F-F_N 0-24, ⧗^{800} 0-24, ⊠
10	8	00	02⊙	01	01.0	05.7	.	05	F_N 0-24, V 0-24, ⧗$^{800-400}$ 0-24, ⊠
11	9	00	02⊙	00	00.7	08.2	.	04	V 0-10^{30} F-F_N 0-12^{45}, ⧗$^{600-1000}$ 0-24, ⊠
12	9	00	00⊙	00	00.0	08.2	.	03	⧗$^{600-800}$ 0-24, ⊠
13	9	00	00⊙	00	00.0	08.3	.	02	⧗^{1000} 0-24, ⊠
14	9	00	04⊙	06	03.3	07.1	.	02	⧗^{1000} 0-24, ⊠
15	2	10	10≡	10≡	10.0	03.6	.	02	⧗^{1000} 0-13^{40}, ⊠ 1^{30}-5^{45}, ≡ 11^{40}-11^{50}, 14^{40}-24; V 14^{30}-24, F_N 14^{30}-24, ⊠
16	0	10≡	10≡	10≡	10.0	00.0	00.5	02	V 0-24, ≡ 0-24, F-F_N 0-24, ⊠
17	8	10≡	00⊙	00	03.3	02.0	00.3	02	≡ 0-13^{30} V 0-24, F-F_{NE} 0-24, ⧗$^{600-1000}$ 13^{30}-24, ⊠
18	9	00	04⊙	00	01.3	06.7	.	02	V 0-24, F-F_N 0-9^{45} 15^{30}-21^{30}, ⧗^{1000} 0-24, ⊠
19	9	00	00⊙	00	00.0	08.5	.	01	V 0-24, ⧗^{1000} 0-24, F $_{NNW}$ 6-7^{30} ⊠
20	9	00	00⊙	00	00.0	08.7	.	01	V 0-24, ⧗^{800} 0-24, ⊠
21	9	00	00⊙	00	00.0	09.7	.	01	V 0-10^{30} ⧗^{1000} 0-13^{40} ≡ 23^{40}-24, ⊠
22	0	10≡	10≡	10≡	10.0	00.0	02.6	06	≡ 0-24, F_{sw} 0^{40}-24, * 1^{50}-4^{40} V 3^{30}-24, ⊠
23	0	10*≡	10≡	10≡	10.0	00.0	04.4	20	V 0-24, ≡ 0-24, * 2^{40}-7^{45} 10^{50}-13^{40}, + 11^{45}-24, F-F_0 11^{45}-24, ⊠
24	0	10≡	10≡	10≡	10.0	00.0	03.4	26	V 0-24, ≡ 0-16^{30} 19^{40}-24; F-F_{sw} 0-24, + 0-24, ⊠
25	0	10≡	10*≡	10*≡	10.0	00.0	.	20	V 0-24, F_{sw} 0-24, ≡ 0-24, + 0-24, * 12^{55}-24, ⊠
26	2	10≡	10≡	00	06.7	00.0	07.0	38	≡ 0-15^{40} V 0-24, F-F_{sw} 0-24, * 0-1^{50} + + 0-24, ⊠
27	0	10≡	10≡	10*≡	10.0	00.0	.	36	V 0-24, F-F_{sw-w} 0-24, + + 0-24, ≡ 5^{40}-24, * 15^{45}-24, ⊠
28	2	10*≡	10≡	10≡	10.0	00.0	11.6	00	V 0-24, ≡ 0-24, F-F_{sw} 0-24, + 0-24, * 0-5^{40} * 5^{40}-8^{50} 11^{30}-13^{30} ⊠
29	0	10≡	10≡	10≡	10.0	00.0	01.2	61	V 0-15^{30} ≡ 0-24, F-F_{ssw} 0-24, + 0-13^{30} ∿ 13^{45}-14^{30}, ● 14^{30}-24, ⊠
30	0	10●≡	10≡	08	09.3	00.0	13.0	44	≡ 0-17^{35}, F-F_{ssw} 0-24, ● 0-13^{45}, * 7^{55}-8^{40} ⊠
31	0	10	10≡	10≡	10.0	00.0	06.2	44	F-F_{w-sw} 0-24, V 0-24, * 0-0^{40}-3^{45}, 11^{30}-13^{30}, 21^{45}-24; + + 0^{40}-24, ≡ 0^{40}-4^{30} 9^{45}-24, ⊠
MES. VRED.		06.0	06.1	06.2	06.1	110.7	65.1		

φ = 43° 52' N λ = 18° 26' E Gr. ΔG = + 1h 14 min. BR. ST. 144

Dan	Vazdušni pritisak P mm 7	14	21	Temperatura vazduha T C° 7	14	21	Sred Dies	Max	Min	Min 5 cm	Napon vodene pare e mm 7	14	21	Relativna vlažnost U% 7	14	21	Sred. Dies	Pravac i jačina vetra D, f (0—12) 7	14	21
1	694.0	693.2	693.7	06.2	01.4	00.8	02.3	08.6	-00.2	-	05.4	04.9	04.8	76	97	98	90	S 2	- 0	- 0
2	695.4	697.2	701.8	00.2	-00.6	-01.5	-00.8	00.8	-02.3	-	04.6	04.2	03.8	98	96	93	96	- 0	NW 1	- 0
3	702.8	702.2	703.1	-03.8	01.1	-01.3	-01.3	01.4	-04.9	-	03.2	04.0	03.9	92	81	94	89	E 2	- 0	- 0
4	703.5	701.6	701.0	-00.2	07.0	03.9	03.6	07.0	-02.9	-	04.2	04.7	05.1	93	62	83	79	SSE 1	S 4	- 0
5	697.1	694.9	694.7	09.5	11.8	12.8	11.7	13.1	03.5	-	06.0	06.4	06.5	67	61	59	62	SW 2	S 4	W 2
6	695.8	696.6	699.4	11.3	15.0	02.4	07.8	15.0	01.8	-	05.8	06.2	04.9	57	48	90	65	SE 2	S 3	WNW 1
7	696.9	700.4	706.1	01.0	00.0	-01.0	-00.2	02.5	-01.9	-	04.8	04.3	04.2	97	95	98	97	NNE 1	W 1	WNW 1
8	710.5	711.9	713.3	-02.9	-01.0	-02.8	-02.4	-01.0	-03.6	-	03.4	02.6	02.8	91	60	76	76	- 0	ESE 2	ESE 2
9	712.3	712.2	713.4	-03.8	-00.2	-02.9	-02.4	-00.2	-04.6	-	03.1	03.6	03.4	88	79	91	86	- 0	W 1	NW 1
10	712.3	710.0	709.1	-03.7	02.0	01.3	00.2	02.2	-05.0	-	03.3	03.6	03.9	94	68	78	80	- 0	- 0	ESE 3
11	707.6	706.2	704.6	04.0	09.8	09.3	08.1	10.0	-01.0	-	05.0	05.3	05.0	82	58	57	66	S 1	S 3	S 3
12	698.6	697.8	698.4	09.2	10.0	07.8	08.7	10.2	06.8	-	06.4	07.6	07.1	74	82	90	82	NNW 2	ESE 2	ESE 3
13	697.6	697.6	698.8	06.4	09.8	06.0	07.0	09.9	05.0	-	06.0	07.6	06.2	84	83	89	85	ESE 2	SSW 1	E 1
14	700.4	700.2	702.1	04.6	07.2	05.6	05.8	07.2	03.4	-	06.2	06.4	06.1	97	84	89	90	ESE 1	- 0	- 0
15	701.3	700.2	699.6	03.5	10.8	10.0	08.6	11.5	03.0	-	05.5	06.2	06.4	94	64	70	76	S 1	S 2	E 1
16	697.6	694.8	694.6	10.8	09.6	07.4	08.8	10.8	06.6	-	07.5	06.6	07.5	77	74	97	83	SSE 2	NW 1	- 0
17	697.9	699.3	701.0	00.7	01.7	01.4	01.3	07.4	00.0	-	04.7	04.8	04.9	96	93	97	95	WSW 1	W 1	WNW 1
18	704.6	705.1	706.8	00.2	00.0	-00.8	-00.4	01.4	-01.4	-	04.5	04.4	03.5	96	96	81	91	W 1	WNW 1	WNW 2
19	707.2	707.7	709.9	-04.6	-04.2	-05.6	-05.0	-00.8	-06.4	-	02.9	02.4	02.5	89	71	81	80	WNW 2	W 1	WSW 1
20	711.5	711.1	711.3	-06.4	-04.4	-07.4	-06.4	-04.2	-08.0	-	02.1	02.2	02.2	76	67	83	75	N 1	NW 1	ESE 1
21	709.5	707.7	708.1	-07.9	-03.6	-03.2	-04.5	-03.1	-09.2	-	02.2	02.5	03.0	88	72	83	81	- 0	WSW 1	- 0
22	708.5	708.6	709.2	-04.4	-03.0	-04.0	-03.8	-02.8	-05.2	-	02.6	02.5	02.6	77	68	76	74	ENE 2	- 0	E 2
23	708.6	708.1	709.3	-05.4	-01.0	-04.6	-03.9	-00.9	-06.0	-	02.5	02.7	02.9	82	64	89	78	SE 1	WSW 1	- 0
24	710.0	709.4	710.2	-07.8	01.0	-01.4	-02.4	01.2	-08.4	-	02.2	04.1	03.5	88	83	85	85	- 0	WSW 1	- 0
25	708.2	709.5	710.7	01.0	01.4	00.8	01.0	01.5	-02.1	-	04.3	04.8	04.7	86	95	97	93	SE 2	- 0	- 0
26	711.9	712.5	714.0	-00.3	04.0	00.0	00.9	04.2	-01.0	-	04.2	04.2	04.1	94	69	89	84	ESE 1	- 0	ESE 3
27	713.7	711.4	710.6	00.2	10.1	06.2	05.7	10.4	-01.5	-	03.8	05.1	05.0	82	55	70	69	ESE 3	N 2	WNW 2
28	708.3	707.2	708.2	03.2	03.0	01.0	02.0	06.6	00.0	-	05.0	05.2	04.4	88	92	90	90	WSW 1	WSW 1	ESE 2
29	706.7	707.1	707.6	-00.8	00.6	-01.1	-00.6	01.0	-01.9	-	04.0	04.0	03.3	92	83	79	85	NNE 1	NNW 1	SE 1
30	704.9	702.4	701.1	-06.0	-01.4	00.8	-01.4	01.6	-07.2	-	02.4	03.6	04.2	81	87	86	85	SE 2	- 0	SE 2
31	699.3	699.3	702.1	-00.8	00.0	-02.6	-01.5	01.0	-03.1	-	04.1	04.3	03.5	94	93	94	94	- 0	NW 2	NW 1
MES. VRED.	704.3	704.0	705.0	00.4	03.2	01.2	01.5	04.3	-01.9	-	04.2	04.5	04.4	86	77	85	83	1.2	1.2	1.2

1	704.5	702.6	703.6	-04.6	-03.1	-04.8	-04.3	-02.4	-05.3	-	03.1	03.2	02.8	96	87	87	90	WNW 1	WNW 1	WSW 1
2	704.4	704.1	704.4	-06.0	-02.6	-04.4	-04.4	-02.6	-06.5	-	02.6	03.1	02.9	90	82	87	86	NW 1	WNW 1	- 0
3	702.5	700.0	700.7	-08.5	05.6	03.0	00.8	05.0	-10.0	-	02.3	04.0	04.6	95	59	81	78	ESE 1	WNW 2	- 0
4	702.9	702.9	702.7	02.0	09.4	08.0	06.8	11.1	01.2	-	04.8	05.5	05.7	90	62	71	74	- 0	WNW 1	SSW 1
5	701.3	701.1	700.5	10.2	11.6	11.4	11.2	13.0	07.6	-	05.5	05.2	05.1	59	51	51	54	WNW 3	S 3	SSW 4
6	701.9	703.8	705.7	09.8	09.1	07.2	08.3	11.6	06.7	-	05.7	05.6	05.4	63	64	71	66	WSW 1	S 2	NW 1
7	704.8	705.7	705.7	04.6	04.0	02.8	03.6	07.2	02.2	-	05.4	05.6	05.3	85	91	95	90	- 0	SSE 1	ESE 1
8	704.8	703.9	705.0	-00.4	08.6	05.0	04.6	10.0	-01.0	-	04.2	04.2	03.8	94	50	58	67	- 0	WSW 3	NW 2
9	704.5	704.3	701.5	05.8	12.2	09.6	09.3	13.0	03.0	-	04.3	04.5	05.4	62	42	60	55	NW 2	SSW 4	S 5
10	696.7	695.4	697.9	08.2	10.2	02.6	05.9	12.0	02.4	-	05.4	05.8	05.3	67	62	97	75	S 3	S 2	W 3
11	699.2	695.3	691.1	-00.2	07.0	06.4	04.9	07.2	-01.6	-	03.5	03.1	06.4	78	42	89	70	ESE 1	S 4	W 2
12	701.5	704.1	703.9	-02.2	-02.2	-03.2	-02.7	06.8	-04.0	-	03.7	02.6	02.8	94	68	77	80	W 1	- 0	WSW 2
13	701.2	698.3	700.2	04.2	08.2	02.6	04.4	09.4	-04.6	-	03.3	04.8	05.0	54	58	90	67	S 2	SSW 2	- 0
14	700.4	699.5	694.6	02.3	08.6	08.8	07.1	10.4	00.7	-	03.9	04.4	05.2	73	52	61	62	W 1	ESE 2	SE 7
15	693.9	692.2	695.2	04.2	04.4	-00.8	01.8	09.2	-01.0	-	05.2	05.0	04.0	84	79	92	85	SSW 3	S 2	NW 3
16	699.2	700.5	701.5	-06.1	-05.4	-07.6	-06.7	-00.7	-08.4	-	02.6	02.6	02.2	90	84	83	86	W 1	WNW 1	WSW 1
17	703.1	706.2	709.6	-09.0	-03.2	-10.6	-08.4	-01.6	-11.4	-	02.0	02.2	01.6	86	62	79	76	W 1	W 3	- 0
18	707.4	705.0	701.9	-12.2	-02.4	-01.8	-04.6	00.0	-14.9	-	01.3	02.6	03.5	70	67	87	75	ESE 3	SSE 1	ESE 5
19	706.1	708.3	711.2	-05.0	-01.4	-03.4	-03.3	-01.0	-05.6	-	02.9	03.0	03.2	91	73	89	84	WNW 1	WNW 2	- 0
20	710.3	709.4	706.6	-04.8	00.8	-04.7	-03.4	01.3	-05.2	-	02.4	02.1	02.5	76	43	76	65	ENE 1	- 0	ESE 2
21	706.0	707.4	705.7	-05.4	-00.2	-04.2	-03.5	00.8	-06.9	-	02.6	03.7	02.8	86	82	84	84	ESE 2	W 1	SE 2
22	703.9	703.3	703.7	-06.2	05.2	02.2	00.8	09.0	-07.2	-	02.5	03.2	04.0	87	48	74	70	ESE 1	- 0	- 0
23	699.4	697.8	699.3	04.8	04.3	03.2	02.9	06.0	-00.7	-	04.2	05.6	04.8	66	90	97	84	W 1	- 0	ENE 1
24	700.4	699.5	700.6	-00.6	03.6	-00.6	00.4	05.8	-01.4	-	04.2	03.1	03.4	96	53	78	76	ESE 1	W 1	ESE 2
25	701.1	700.4	700.7	-01.9	02.8	-00.6	-00.1	04.9	-03.0	-	03.4	02.4	02.9	85	44	67	65	- 0	W 2	WNW 2
26	699.9	699.4	700.7	-03.0	03.2	-01.4	-00.6	03.4	-03.8	-	03.0	02.5	03.0	81	43	73	66	W 1	WNW 2	NW 1
27	700.1	698.7	700.5	-04.8	00.1	-03.0	-02.7	01.2	-06.4	-	02.7	03.0	02.3	83	65	62	70	ESE 2	WNW 2	SE 1
28	702.2	703.0	704.8	-05.2	-02.0	-04.2	-03.9	-01.6	-05.8	-	02.8	03.6	02.9	91	90	88	90	W 1	W 1	WNW 1
MES. VRED.	702.3	701.9	702.1	-01.1	03.4	00.6	00.9	[illegible]	-03.2	-	03.6	03.8	03.9	81	64	79	75	1.3	1.0	1.8

SARAJEVO

1970 JANUAR

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H_s = 630 m H_b = 637.0 m h_t = 2.0 m h_r = 1.0 m

Dan	Vlažnost 0—9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena W
	14	7	14	21	Srednja Dnevna		7	7	
1	5	10●	10✱	10✱≡	10.0	00.0	11.4	13	●n-12^55 17^45, 18^40, Fsf 0^42, ≡ 10^30-11^30, 14^30-n; ✱ 11^30-14^30, 18^50-n; = 13^40 14^30, ✱ 14^30-17^45 [✱ 14^45-14^50, ⊠
2	2	10✱≡	10✱≡	10≡	10.0	00.0	33.2	14	✱0-4 n-17^30 ≡ n-n, ⊠
3	2	01	01≡⊙	04≡	02.0	05.6	01.4	11	= n-12^20, ≡ 12^30-n, ⊠
4	7	10≡	07	10	09.0	01.0	00.1	13	✱n-6^30, ≡ n-9^45 = 16^30 n, ⊠
5	7	10	08	06	08.0	00.4	.	07	Fsw 1^49-16^55, ● 16^05-18^30, ⊠
6	7	10	01⊙	10	07.0	03.3	02.6	.	
7	3	10●	10✱	10✱	10.0	00.0	13.3	.	= n-n, ● n-12^20, ✱ 12^30-13^05, ✱ 13^05-n, ⊠
8	6	10	10	09	09.7	00.0	23.2	11	= n-15, ⊠
9	6	08	00	00	02.7	00.0	.	09	= n-n, ⊠
10	3	10≡	02≡⊙	00	04.0	00.0	.	07	≡ n-18^45, = 18^45-n, ⊠
11	7	10	09	03	07.3	01.9	.	03	Fs 20^30-22^30 ⊠
12	7	10●	09●	10●	09.7	00.0	00.2	.	● 6^45-7^30 12^30-n; Fsss 8^50-10^18 i
13	5	09	07	09	08.3	01.4	12.0	.	= 12^30-n
14	4	10≡	10●	09	09.7	00.0	00.1	.	● n, ≡ n-7^30 ≡ 7^30-10^30 = 10^30-16, ● 13^40-14^40 i
15	7	06≡	09	09	08.0	00.8	00.1	.	≡ n-9, = 9-10^30, ● 15^40-18^40 i, Fs 21^45
16	8	09	10●	10●	09.7	00.0	01.2	.	● n-n, Fs 12^44
17	6	10✱	10	10✱	10.0	00.0	15.7	.	= n-n, ✱ 13^30 i, ● 14^30-18^30
18	7	10✱	10✱	10✱	10.0	00.0	02.3	.	✱n-n, ⊠
19	5	10✱	10✱	10✱	10.0	00.0	01.0	01	✱n-n, = n-n, ⊠
20	7	10✱	09	00	06.3	01.5	00.1	01	✱n-8, = n-10^30, 20-n; ⊠
21	5	10	09	10	09.7	00.0	00.0	.	= n-24
22	7	10	10	10	10.0	00.0	.	.	
23	5	10	00⊙	03	04.3	01.9	.	.	= n-n
24	5	00	01⊙	05	02.0	03.5	.	.	≡ n-8^30 V n-10, ≡ 8^30-11
25	3	10✱	10✱	10	10.0	00.0	03.0	03	✱ n-13^30, ● 7^30-8^45, ✱ 13^30-15^30, = 15^30-n, ⊠
26	5	10	06⊙	00	05.3	04.4	06.4	04	= 12-n, ⊠
27	6	09	07⊙	01	05.7	02.6	.	.	= n-n
28	6	10	10●	10✱	10.0	00.0	00.1	.	● n-6^30, 11^30-14^20, ✱ 14^20-14^30, ✱ 14^30-n, ⊠
29	6	10	09	09	09.3	00.0	05.3	03	= n-n, ✱ 8^30-14^30 i, ⊠
30	5	10	08✱	10✱	09.3	00.0	00.1	03	= n-n, ✱ 10^35-n, ⊠
31	4	10	10✱	10✱	10.0	00.0	00.7	02	= n-n, ✱ 8^30-n, ⊠
MES. VRED.		09.1	07.5	07.3	08.0	28.3	134.2		

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1	4	10✱	10✱	10✱	10.0	00.0	18.5	27	✱n-n, ⊠
2	6	10✱	10✱	00	06.7	00.0	03.9	27	✱n-19, = n-n, ⊠
3	7	10	06	10●	08.7	01.1	00.4	25	Fs 2^50, ● 20^20-n, ⊠
4	4	07	08	00	05.0	04.3	00.3	12	= 7^30-13, Fs-ssw 21^35-22^40 i, ⊠
5	7	10	09	05	08.0	03.7	00.1	01	● n, Fs-ssw 1^49-22^41 i, ⊠
6	7	10●	09	10●	09.7	00.9	00.0	.	● 6^30-13^30 i, 20^40 ni
7	6	10	10●	10●	10.0	00.0	01.0	.	● n-ni, = n-8
8	7	06	07	00	04.3	04.6	05.3	.	= n-12 i, ≡ 7^45-8^50
9	7	04	03⊙	05	04.0	08.1	.	.	Fs 14^57-23^54
10	7	06	08	10	08.0	03.3	.	.	Fs 0^40-18^40 i, = 6^30-8^45, ● 13^20-13^40, 18-9^30
11	7	02	10	10	07.3	00.6	01.5	.	⊔6^30 9^45, = 6^30-8^45, ≡ 8^45-9^50, ● 17-20^30, Fnw 22^49
12	6	10✱	05⊙	08	07.7	03.0	08.7	08	✱n-12, = 12^40-n, ⊠
13	7	07	08●	10✱	08.3	01.4	01.1	03	Fs 6^40-10^40, ● 11^40-13^50, 19-20^35, ✱ 20^30-n, ⊠
14	7	06	07	10●	07.7	01.5	13.5	.	= n-9^20, Fs 16^57-24 i, ● 19^40-h
15	6	10●	10●	10✱	10.0	00.1	06.2	.	Fs-sw 0-4^49, ● n-14^30 i, ✱ 9^40-9^40, 14^30-20^30; ✱ 20^40-n, ⊠ 21^40-22, ⊠
16	2	10✱≡	10✱≡	10✱	10.0	00.0	38.2	45	✱n-n, ≡ n-15^30, ⊠ 2-2^40, ⊠
17	6	10✱	03⊙	00	04.3	03.9	05.6	59	✱ n-11^40, = 12^40-n, ⊠
18	6	00	10✱	10✱	06.7	04.5	00.4	55	= n-n, ✱ 6^30-8^30, ✱ 13^40-n, ⊠
19	6	10✱	08	10	09.3	00.1	05.2	51	✱n-12^45 = n-n, ⊠
20	6	10	03⊙	03	05.3	03.3	01.2	30	= n-n, ✱ 8^45-9^20, ⊔ 21-n, ⊠
21	6	10✱	10●	08	09.3	00.7	00.1	27	= n-n, ✱ n-13^30, ● 13^30-14^40, ⊠
22	6	04	06	04	04.7	01.6	01.1	25	= n-n, ⊠
23	6	10	10●	10✱	10.0	00.0	.	19	= n-n, ● 7^30-20^40, ✱ 16^33-17^40, ✱ 18^33-21^05, ⊠
24	6	10	07	00	05.7	04.2	19.0	14	= n-16, ≡ 8^30-10^40, ✱ 15^25-15^45 ⊠
25	6	10≡	06⊙	10	08.7	03.9	00.1	13	≡ n-8^30, = 8^30-16, ✱ 8^35-9^40, ⊠
26	6	07	05⊙	10	07.3	02.1	00.0	12	= n-16, ✱ 7^50-10^40 ⊠
27	6	07✱	07✱	10✱	08.0	04.1	00.0	11	= n-n, ✱ n-9^45, 12^50-14^39, 17^30-ni; ⊠
28	4	10✱	10✱	10✱	10.0	00.0	00.0	10	= n-n, ✱ n-ni, ⊠
MES. VRED.		08.1	07.7	07.2	07.7	61.0	131.4		

1970 MART SARAJEVO

$\varphi = 43^{\circ}\ 52'$ N $\lambda = 18^{\circ}\ 26'$ E Gr. $\Delta t =$ + 1h 14 min. BR. ST. 144

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred. Dnev	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnev	7	14	21
1	705.6	705.5	705.8	-05.8	-03.2	-04.5	-04.5	-01.4	-06.4	-	02.7	03.2	02.5	90	89	75	85	WSW 1	WSW 1	- 0
2	703.7	699.9	697.3	-08.6	01.2	-01.9	-02.8	02.4	-10.3	-	01.8	02.4	02.2	76	47	56	60	NE 1	NW 1	- 0
3	694.5	692.8	693.5	-00.4	03.8	04.4	03.0	05.8	-04.2	-	02.7	03.7	04.4	62	61	69	64	ESE 4	ESE 3	SE 2
4	693.5	690.0	684.4	03.6	09.2	04.6	05.4	10.0	02.1	-	04.7	04.1	05.0	79	47	79	68	ESE 2	SSE 3	ESE 5
5	689.5	692.2	694.4	01.6	04.0	04.2	03.5	05.6	00.0	-	04.1	05.0	04.5	80	82	74	79	WNW 2	S 3	S 3
6	700.0	701.3	702.7	01.2	06.8	03.8	03.9	07.6	00.4	-	04.7	03.6	04.4	93	49	73	72	N 1	SSW 2	SE 2
7	701.6	704.0	707.0	01.4	03.0	-00.3	01.0	06.0	-00.9	-	04.7	04.6	03.8	93	81	85	86	W 2	WNW 1	WNW 1
8	707.0	705.0	705.4	-01.4	07.0	01.0	01.9	07.8	-01.9	-	03.0	02.6	03.4	73	35	69	59	- 0	S 2	E 2
9	704.5	703.1	705.4	-02.8	11.1	03.2	03.7	12.4	-04.0	-	02.8	03.7	04.0	74	37	69	60	E 2	- 0	ESE 2
10	708.8	710.0	711.1	-01.2	10.6	04.5	04.6	11.6	-01.7	-	03.5	04.3	04.8	84	45	77	69	ESE 2	N 1	ESE 1
11	709.0	707.0	705.7	02.8	10.2	07.4	07.0	11.3	02.4	-	04.2	04.1	04.8	75	44	62	60	ESE 3	WNW 1	SW 1
12	700.0	700.7	703.7	05.4	04.0	04.0	04.4	08.8	03.0	-	05.6	05.2	03.6	83	85	59	76	ESE 3	N 2	W 2
13	705.8	706.0	705.9	02.6	10.2	04.6	05.5	11.0	02.1	-	04.0	03.2	03.8	72	34	60	55	WNW 1	SSW 2	ESE 2
14	703.0	699.0	698.0	04.2	03.2	01.2	02.4	05.6	00.7	-	04.5	05.4	04.7	74	94	95	88	S 1	WNW 1	NNW 1
15	697.2	697.4	700.5	01.2	04.6	00.4	01.6	05.0	00.1	-	04.7	05.4	04.0	95	85	96	92	N 1	W 1	WSW 1
16	703.1	704.0	704.8	00.0	01.8	00.3	00.6	01.9	-00.7	-	04.3	04.4	03.8	93	83	81	86	- 0	- 0	- 0
17	703.4	703.9	704.9	-00.8	00.8	-00.2	-00.1	01.8	-01.4	-	03.7	03.2	03.5	85	66	78	76	SSE 1	NW 1	W 1
18	704.2	700.5	700.0	-02.0	08.6	05.2	04.2	10.0	-02.6	-	03.1	02.9	02.5	79	34	38	50	ESE 1	WSW 1	- 0
19	697.0	693.5	698.7	02.4	06.4	00.2	02.3	08.7	-00.4	-	04.9	05.7	04.8	90	78	96	88	- 0	ESE 1	W 1
20	703.2	705.6	708.5	00.2	04.2	-00.5	00.8	04.9	-01.2	-	03.9	02.8	03.1	84	46	70	67	WNW 1	N 2	SSE 1
21	709.0	709.9	709.9	-02.8	08.4	02.8	02.8	10.0	-04.6	-	03.2	03.4	04.2	86	41	75	67	ESE 2	W 2	ESE 2
22	709.4	708.5	709.9	01.0	15.0	08.8	08.4	15.9	00.0	-	04.1	03.5	04.4	83	27	51	54	ESE 4	WSW 2	SSW 1
23	709.6	709.3	709.3	06.1	11.6	08.4	08.6	11.7	03.6	-	04.7	05.4	05.0	66	53	61	60	ESE 1	- 0	WSW 2
24	709.1	708.3	709.2	06.2	17.4	10.0	10.9	17.7	04.6	-	05.8	05.1	05.4	81	34	59	58	E 2	S 4	SSW 1
25	709.2	708.9	707.6	06.2	15.8	14.0	12.5	16.9	03.7	-	05.8	04.8	04.3	81	36	36	51	ESE 2	S 3	S 2
26	707.0	705.3	704.0	13.2	16.6	12.4	13.6	17.4	11.4	-	03.4	04.6	04.8	30	34	45	36	WSW 3	SSW 4	WNW 1
27	701.5	699.4	696.1	12.0	15.0	14.2	13.8	16.6	11.4	-	06.9	06.9	06.4	66	54	53	58	W 2	S 2	WSW 3
28	696.1	696.2	698.7	00.8	00.2	-00.6	00.0	14.2	-01.1	-	04.4	04.3	04.1	90	93	94	92	NW 2	NW 1	NW 1
29	699.7	700.5	704.3	-01.0	03.2	-00.4	00.4	05.0	-01.7	-	04.1	03.3	03.4	96	58	76	77	NW 1	WNW 1	ESE 2
30	708.5	707.7	708.5	-02.6	10.3	05.2	04.5	10.7	-05.1	-	02.8	02.2	03.2	74	24	48	49	ESE 2	WSW 2	- 0
31	707.0	705.7	703.3	03.5	12.2	08.5	08.2	12.4	01.6	-	02.8	03.9	04.2	48	37	51	45	ESE 2	SSW 3	SW 2
MES. VRED.	703.2	702.6	703.2	01.5	07.5	04.0	04.3	09.2	00.0	-	04.0	04.1	04.1	78	55	68	67	1.7	1.7	1.4

1970 APRIL SARAJEVO

1	699.2	699.0	700.3	10.2	10.4	09.2	09.8	14.2	07.4	-	05.7	07.7	06.6	61	81	76	73	SSW 4	WNW 2	WNW 1
2	700.5	697.8	696.2	04.6	11.0	09.4	08.6	12.9	04.0	-	05.4	06.3	05.7	85	64	65	71	ESE 2	WNW 2	N 1
3	693.2	696.9	701.5	05.8	00.6	-00.6	01.3	10.4	-01.2	-	05.6	04.3	04.1	81	89	93	88	WNW 3	WNW 3	W 1
4	701.6	702.2	702.9	-01.8	06.0	01.4	01.8	06.6	-02.2	-	03.4	01.6	02.3	84	23	45	51	ESE 2	WSW 2	WSW 1
5	703.1	700.8	700.0	-01.0	10.4	05.6	05.2	11.0	-02.4	-	02.9	01.6	02.6	67	17	39	41	ESE 3	SSW 3	ESE 2
6	701.2	703.5	706.2	03.8	07.1	04.8	05.1	08.8	01.2	-	04.0	05.3	03.6	66	70	56	64	- 0	ENE 3	S 2
7	706.7	704.7	701.9	04.2	10.4	09.2	08.2	11.4	01.2	-	03.2	03.1	05.0	51	33	58	47	SSE 1	SSW 4	S 2
8	698.3	697.0	695.1	08.0	11.8	12.4	11.2	12.8	05.8	-	06.6	07.0	05.8	82	67	54	68	ESE 2	SSE 2	S 4
9	693.0	696.0	700.2	13.2	14.6	08.5	11.2	15.6	07.9	-	07.4	07.4	04.5	65	59	54	59	SSW 3	S 4	WNW 1
10	704.1	704.0	705.3	09.6	14.6	09.1	10.6	15.2	06.0	-	04.1	03.7	04.6	45	30	53	43	SSW 5	SSW 2	- 0
11	704.4	703.9	703.6	06.0	11.4	09.0	08.8	13.2	04.6	-	05.1	06.6	06.9	73	65	80	73	ESE 2	N 2	- 0
12	704.7	703.6	704.0	03.0	05.0	04.3	04.2	09.2	02.6	-	05.0	03.6	04.9	87	55	79	74	W 1	NW 2	- 0
13	706.2	703.7	705.0	01.8	11.8	09.4	08.1	13.2	-01.0	-	04.4	03.7	03.8	83	36	43	54	ESE 1	W 4	S 3
14	701.0	703.5	705.7	10.4	02.4	01.0	03.7	10.9	00.3	-	07.1	05.1	04.7	75	94	95	88	SSW 2	W 1	- 0
15	710.0	711.2	712.8	00.4	03.8	02.1	02.1	04.7	-00.2	-	04.4	03.7	04.5	93	61	84	79	W 1	N 1	N 1
16	712.3	712.8	714.4	01.4	03.8	03.2	02.9	05.4	00.2	-	04.2	03.7	04.3	83	61	75	73	W 1	N 2	NW 1
17	714.2	713.3	711.9	03.0	12.0	07.0	07.2	13.0	01.8	-	04.8	04.8	05.5	84	46	74	68	- 0	SE 2	ESE 2
18	710.0	708.2	707.8	06.2	19.0	12.7	12.6	19.8	05.1	-	05.9	06.3	06.4	84	38	58	60	- 0	W 2	- 0
19	708.1	707.0	705.6	09.0	22.8	14.8	15.4	23.0	06.8	-	06.7	05.4	05.7	78	26	45	50	ESE 2	- 0	S 1
20	705.2	705.3	707.5	15.9	22.8	17.2	18.3	23.6	10.8	-	05.5	05.6	06.1	40	27	41	36	SSE 2	SW 3	W 1
21	709.2	710.0	713.3	14.2	20.4	11.0	14.2	21.0	10.6	-	04.9	05.6	07.4	41	31	75	49	S 1	S 3	NNW 3
22	715.7	715.1	714.3	07.4	18.6	13.1	13.0	20.0	06.4	-	06.7	08.2	06.8	87	51	60	66	- 0	WSW 1	SSE 1
23	713.7	710.5	710.9	09.5	25.2	16.2	16.8	25.4	06.4	-	06.3	04.4	06.1	70	18	44	44	ESE 2	W 2	SE 1
24	710.1	708.1	707.7	12.2	23.6	15.6	16.8	24.6	08.6	-	06.8	05.2	06.2	64	24	47	45	SE 2	WSW 1	- 0
25	707.9	704.7	704.9	11.6	23.2	14.6	16.0	23.4	09.4	-	08.0	05.9	07.4	78	28	59	55	- 0	W 5	ESE 2
26	703.1	701.8	701.4	11.6	21.8	16.2	16.4	22.5	07.8	-	07.1	04.4	05.9	69	23	43	45	SE 1	SSW 3	SSW 4
27	701.3	703.1	704.2	15.6	17.5	14.0	15.3	19.4	13.3	-	06.3	07.2	07.0	47	48	58	51	W 1	W 2	SW 2
28	705.0	705.0	704.5	09.2	11.8	07.5	09.0	14.0	06.4	-	05.8	08.1	06.8	67	78	87	77	E 1	WSW 1	SW 1
29	703.8	704.6	704.7	07.0	14.2	07.9	09.2	15.0	04.9	-	06.5	02.9	03.3	87	24	42	51	- 0	W 4	WNW 1
30	703.8	705.6	708.1	04.6	01.8	00.7	02.0	13.6	-00.1	-	04.5	05.0	04.7	71	97	96	88	- 0	WNW 3	- 0
MES. VRED.	705.0	704.8	704.4	07.2	13.0	08.9	09.5	15.1	04.4	-	05.5	05.1	05.3	72	49	63	61	1.5	2.4	1.3

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BR. ST. 144 H_s = 630 m H_b = 637.0 m h_t = 2.0 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	6	10✱	06	10✱	07.3	05.0	02.2	14	= n-n, ✱ n-17^45, 20-n; ⊠
2	6	05⊙	05⊙	00	03.3	07.5	01.3	13	= n-n, ⊠
3	6	10	10	10●	10.0	01.1	•	12	= n-n, ✱ 9^05-12^40, ● 12^40-12^50 15^45-ni; ⊠
4	5	07	10	10●	09.0	01.2	00.8	14	= n-n, ● n-7^50 17^20-17^35 20^20-n; F SSE 8^48 16^04-21i; ⊠
5	6	10✱	10●	10	10.0	00.3	06.2	01	= n-n, ✱ n-11^40, Fs 5^40-5^46, 10^31-23^34; ● 11^40-ni, ✱ 12^30-13^40, ⊠
6	6	08	08	08	08.0	07.4	21.1	•	= n-n, Fs 2^49, 16^15; ✱ 7^05-8^10 ● 8^40-8^45 12^40-13^15
7	6	10✱	07✱	10	09.3	01.9	01.7	•	= n-15^50, 18^45-n; ● n-6^20, ✱ 6^20-7^15, 10^40-17^50, ≡ 15^30-18^45
8	6	07	05⊙	00	04.0	09.5	02.6	•	= n-17
9	6	00⊙	00⊙	00	00.0	09.8	•	•	= n-15, ⌣ n-10
10	6	00⊙	00⊙	10	03.3	09.1	•	•	= n-n, ⌣ n-9^30
11	5	10	09	09	09.3	02.3	•	•	= n-n
12	6	10●	10	07	09.0	01.9	00.0	•	= n-n, ● n-9^35, 12^45-13^20, F w-wnw 12^50-12^58, 16^55-17^05 i
13	5	10	06⊙	10	03.7	06.8	00.3	•	= n-n
14	5	10	10●	10●	10.0	00.0	•	•	= n-n, ● 7^40 7^40 10^25-ni
15	5	10	10●	10✱	10.0	00.0	05.6	•	= n-n, ● 11^50-14^10 i, ✱ 19^10-n, ⊠
16	5	10✱	10✱	10	10.0	00.0	12.1	08	= n-n, ✱ n-17^30 △ 20^55-n, ⊠
17	5	10✱	10✱	10	10.0	00.1	02.4	06	= n-n, ✱ n-15^30 i, ⊠
18	6	04⊙	04	10	06.0	09.6	00.1	02	= n-n, ⊠
19	5	10	10	10✱	10.0	00.0	00.1	•	= n-n, ● n-6^20 11^25-12^50, 15^30-17^25; ✱ 17^25-18, ✱ 18-n, ⊠
20	6	10✱	08	00	06.0	03.4	15.8	09	= n-16^30, ✱ n-19^30 i, ⊠
21	5	10	00⊙	00	03.3	03.9	00.1	•	= n-14^20
22	7	04⊙	06⊙	02	04.3	09.0	•	•	= n-12^30 ⌣ n-7^30
23	7	10	10	08	09.3	00.0	•	•	= n-13^30 ● 8^40-11^30 i
24	7	09	06⊙	00	04.7	09.3	00.1	•	= n-12^20
25	7	07	10	07	07.7	02.5	•	•	= n-11, △ n-7^50, ∞ 11-15
26	8	10	10	10	10.0	01.0	•	•	F sw 1^15-23^44 i
27	7	10	10	10	10.0	01.3	•	•	= n-10, Fs 16^02-19^50 i
28	4	10✱	10✱	10✱	10.0	00.0	11.6	•	= n-n, ● n-6^40, ✱ 6^40-ni, ⊠
29	5	10✱	08	00	06.0	02.9	13.2	04	= n-n, ✱ n-10^50 16^30-17i, ⊠
30	5	00⊙	00⊙	00	00.0	11.4	00.4	•	∞ n-11, V n-8^30
31	9	06⊙	08⊙	06	06.7	08.4	•	•	∞ n-9^45, F sw 14^20-23^36 i
MES. VRED.		07.9	07.4	06.7	07.3	121.0	100.6		

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1	7	10	10●	10●	10.0	03.7	•	•	∞ n-8^30, Fs 0^05-1^15 ● 10-n
2	7	10●	09●	07	08.7	02.8	09.7	•	= n-10^30 ● n-19^30, ∞ 10^30-12, F s 15^45
3	4	10●	10✱	09✱	09.7	00.2	08.1	•	● n-7^40, F s-w 1^44-13^02, = 7^30-10, ✱ 7^40-9^45, ✱ 13^05-ni, ⊠
4	7	06⊙	06⊙	00	04.3	09.5	05.8	02	= n-10, ⊠
5	8	06⊙	07⊙	10	07.7	09.0	•	•	⌣ n-8
6	3	08⊙	07⊙	00	05.0	05.6	•	•	● 13-13^25
7	8	00⊙	09	10●	06.3	06.0	00.1	•	Fs 11^50 ● 19^50-ni
8	7	10●	10●	10●	10.0	00.0	04.2	•	= n-11, ● n-12 i, F-Fs-SE 12^22-23^45, 21^29
9	7	10●	10●	01	07.0	04.5	05.3	•	● n-7^40 12^05-17i, Fs 7^58-16^05 i
10	8	04⊙	05⊙	00	03.0	08.8	00.6	•	= 19^30 n
11	7	10	10●	10●	10.0	00.2	•	•	= n-10^30, ● 10^55-14^30, 19^50-ni
12	6	10●	10●	03	07.7	00.0	03.6	•	= n-n, ● n-14^40 i
13	7	00⊙	09	09	05.0	05.8	00.1	•	= n-10^30, ⌣ n-8, Fs 22^59-23^25
14	6	10	10●	10✱	10.0	00.0	00.2	•	= n-n, Fs-w 0^22-10; ● 6^40-14^40, 17^30-19^30; ✱ 12^40-14^20, 19^30-n; ✱ 14^20-17^30, ⊠
15	6	10✱	10✱	10	10.0	00.5	20.[illegible]	[illegible]	= n-n, ✱ n-8^50, ✱ 12^20-n, ⊠
16	6	09✱	09✱	09✱	09.7	00.2	01.3	02	= n-n, ✱ n-n
17	7	10	07⊙	01	05.0	06.7	08.0	00	= n-10^30
18	7	10	07⊙	00	05.7	07.2	•	•	= 8^40-11
19	7	00⊙	06⊙	00	02.0	10.4	•	•	
20	5	03⊙	07⊙	10	06.7	09.9	•	•	Fs 7^40-9^42
21	8	10	09	01	05.7	00.2	•	•	
22	6	10	09	00	06.3	01.5	•	•	= n-15
23	8	00⊙	07⊙	00	02.3	11.1	•	•	= 8^20-10^15
24	8	07⊙	08	04	06.3	03.9	•	•	
25	7	04⊙	09	00	04.3	07.0	•	•	△ n-7^30
26	8	00⊙	06⊙	03	03.0	09.9	•	•	△ n-8
27	7	08	07	04	06.3	03.6	•	•	● 11^20-13^45 i
28	5	10	10●	10●	10.0	00.0	00.0	•	● 9^45-n, = 12^40-n
29	8	04⊙	04⊙	00	02.7	08.8	17.[illegible]	•	
30	6	06⊙	10✱	10✱	08.7	03.0	•	•	= 11^05-16^30, ● 11^25-13^05 i, ✱ ✱ 13^05-ni, ≡ 16^30-n
MES. VREĐ.		06.8	08.2	05.3	06.7	142.0	03.1		

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φ = 43° 52' N λ = 18° 26' E Gr. ΔG = + 1h 14 min. BR. ST. 144

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred. Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	707.9	706.7	709.0	01.0	09.4	02.6	03.9	10.7	-00.1	-	04.7	03.2	04.8	95	36	87	73	- 0	WSW 1	WSW 1
2	708.5	707.9	708.9	01.8	05.0	00.8	02.1	06.7	00.2	-	04.7	03.6	04.5	90	55	93	79	- 0	W 2	- 0
3	709.1	709.5	710.0	01.4	04.0	04.6	03.6	06.4	00.4	-	04.7	05.2	05.6	93	85	88	89	WNW 1	S 1	- 0
4	708.8	705.2	704.0	03.7	14.3	09.2	09.1	14.8	02.0	-	05.4	03.7	04.4	91	30	51	57	- 0	NW 1	- 0
5	701.2	701.3	702.9	06.0	08.4	08.2	07.7	09.5	05.5	-	06.4	06.8	06.5	92	82	80	85	- 0	- 0	SE 1
6	704.9	705.6	705.7	07.4	14.8	10.5	10.8	15.9	05.8	-	07.1	05.7	07.1	92	45	75	71	- 0	WNW 1	ESE 2
7	705.2	705.1	705.9	10.0	19.4	13.5	14.1	20.1	08.2	-	06.8	06.1	06.6	74	36	57	56	ESE 3	ESE 2	ESE 3
8	706.0	706.0	706.4	13.2	19.2	14.9	15.6	20.3	09.3	-	06.7	05.1	05.6	59	30	44	44	SE 1	S 3	SW 2
9	708.1	708.0	707.5	13.6	22.2	15.2	16.6	22.3	09.3	-	07.9	06.4	06.9	67	32	54	51	SE 1	WSW 3	- 0
10	705.2	703.1	701.5	16.0	25.4	19.2	20.0	26.0	11.4	-	07.1	03.6	04.4	52	15	26	31	ESE 4	WSW 2	SW 2
11	701.3	701.2	701.4	17.4	22.2	15.4	17.6	22.3	13.9	-	07.6	07.4	05.4	51	37	41	43	WSW 2	WSW 4	N 1
12	701.7	702.8	704.1	09.2	14.0	10.4	11.0	15.6	08.5	-	07.0	05.9	05.6	81	49	59	63	- 0	SSW 2	- 0
13	704.9	704.4	706.4	12.7	17.9	13.8	14.6	20.6	07.6	-	05.9	05.9	06.4	54	39	54	49	W 1	W 3	W 2
14	708.2	707.4	707.4	09.2	20.4	15.0	14.9	21.3	05.7	-	06.6	06.3	06.9	76	35	54	55	SE 1	WNW 3	N 1
15	707.0	705.6	704.0	10.2	18.2	15.8	15.0	22.3	06.7	-	06.9	06.2	06.8	74	40	50	55	- 0	W 2	- 0
16	702.5	703.8	702.8	15.2	13.0	11.6	12.8	20.3	11.2	-	07.7	09.8	08.1	60	87	79	75	WNW 1	- 0	- 0
17	702.4	700.8	703.0	09.1	19.6	10.8	12.6	19.6	07.5	-	07.7	06.7	08.4	89	39	86	71	- 0	NNW 2	- 0
18	703.7	706.8	709.7	09.9	10.3	09.8	10.0	11.0	08.9	-	08.3	08.6	08.5	90	92	94	92	- 0	W 1	- 0
19	710.7	711.1	710.2	08.4	09.4	08.7	08.8	09.8	07.9	-	07.4	08.0	08.0	90	90	95	92	WNW 1	- 0	- 0
20	707.8	707.3	705.9	09.0	11.2	11.6	10.8	15.8	08.0	-	08.2	09.1	08.7	95	91	85	90	- 0	- 0	- 0
21	704.1	702.7	702.6	10.2	13.2	11.6	11.6	13.3	09.4	-	08.4	09.2	08.9	90	81	86	86	- 0	- 0	- 0
22	700.7	699.9	700.7	09.8	14.4	08.5	10.3	18.0	07.1	-	08.3	09.3	07.8	92	76	94	87	- 0	- 0	WSW 1
23	705.3	708.0	711.4	04.8	11.2	05.7	06.8	11.6	03.0	-	06.1	05.6	06.1	94	56	89	80	- 0	W 2	- 0
24	713.1	713.0	714.3	04.8	08.4	06.1	06.4	08.8	03.6	-	05.9	06.0	06.3	91	73	89	84	W 2	SW 2	- 0
25	714.1	712.4	711.8	06.1	13.3	08.7	09.2	14.8	03.4	-	06.3	05.7	05.8	89	50	68	69	- 0	- 0	E 2
26	711.0	708.6	708.4	06.2	19.4	13.1	13.0	20.1	03.2	-	05.8	05.4	06.6	81	32	58	57	- 0	S 1	N 1
27	708.9	706.5	707.4	08.6	20.6	11.0	12.8	20.9	05.8	-	06.9	06.0	08.0	83	33	82	66	- 0	WNW 2	SW 2
28	707.3	707.2	707.6	08.4	11.6	09.0	09.5	12.2	07.6	-	06.8	08.6	08.3	82	84	96	87	- 0	- 0	W 1
29	707.9	708.0	707.4	09.2	17.7	10.4	11.9	17.8	07.1	-	08.3	06.3	06.6	95	41	70	69	- 0	WNW 1	- 0
30	707.7	707.4	707.0	11.4	18.4	14.2	14.6	19.0	05.6	-	07.4	07.8	09.7	73	49	80	67	SE 1	N 1	ENE 1
31	708.0	708.3	709.9	10.4	15.6	11.2	12.1	17.8	08.4	-	08.8	09.7	09.3	93	73	93	86	- 0	WNW 1	- 0
MES. VRED.	706.6	706.2	706.6	08.8	14.9	10.7	11.3	16.3	06.5	-	06.9	06.5	06.8	82	55	73	70	0.6	1.4	0.7

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1	710.3	710.6	711.2	10.3	12.7	09.9	10.7	15.2	09.0	-	08.6	07.4	07.8	92	67	86	82	- -	- -	- -
2	710.1	709.6	711.2	11.0	17.0	09.2	11.6	17.5	08.8	-	08.7	06.4	08.1	88	44	93	75	- 0	N 1	W 1
3	710.6	709.9	709.5	07.2	09.0	07.2	07.6	09.3	05.6	-	06.2	06.7	06.6	82	78	87	82	NW 1	N 1	- 0
4	707.6	708.2	708.4	07.3	10.2	09.2	09.0	12.4	06.4	-	06.8	08.2	07.6	88	88	87	88	- 0	S 1	- 0
5	708.4	708.5	708.7	10.2	19.6	13.2	14.0	19.7	06.4	-	07.8	05.5	07.1	84	32	62	59	- 0	W 2	- 0
6	708.6	708.9	708.6	10.5	16.8	13.1	13.4	19.0	07.6	-	07.6	08.6	08.9	80	60	79	73	- 0	NNW 1	- 0
7	708.7	708.2	707.1	13.0	24.2	18.8	18.7	25.1	10.2	-	09.5	10.4	11.8	85	46	73	68	- 0	WSW 1	ESE 1
8	706.5	705.8	707.3	16.6	28.4	22.1	22.3	28.4	14.3	-	10.2	09.8	10.0	72	34	50	52	- 0	- 0	S 1
9	708.5	709.5	708.1	18.2	23.0	19.2	19.9	25.0	14.6	-	12.5	12.7	10.4	80	60	62	67	E 1	- 0	- 0
10	708.2	705.8	704.2	16.4	29.6	20.0	21.5	29.6	14.0	-	11.6	07.7	09.9	83	25	56	55	- 0	SSW 2	- 0
11	706.0	706.0	706.3	16.4	22.0	15.7	17.4	25.6	13.8	-	10.8	12.0	11.1	77	61	83	74	- 0	WNW 1	W 1
12	707.0	706.0	705.6	14.8	20.4	16.2	16.9	21.6	12.4	-	11.3	10.1	08.9	90	56	64	70	- 0	NW 1	- 0
13	706.4	705.3	705.0	13.2	25.2	17.4	18.3	25.4	09.0	-	09.0	06.9	09.0	79	29	61	56	ESE 1	W 3	- 0
14	706.3	705.8	706.1	15.0	19.8	14.5	16.0	26.4	11.6	-	10.0	10.9	11.0	78	63	89	77	ESE 1	N 3	ESE 1
15	707.3	707.6	709.2	13.9	23.3	16.4	17.5	24.3	10.6	-	10.5	10.0	12.5	88	47	89	75	- 0	- 0	- 0
16	709.4	708.5	709.3	13.6	26.0	17.0	18.4	26.0	11.4	-	10.4	12.1	12.1	89	48	83	73	- 0	WSW 2	- 0
17	709.2	707.0	706.5	14.9	28.8	23.2	22.5	29.4	12.3	-	11.0	10.4	12.6	87	35	59	60	SW 1	WSW 2	- 0
18	705.4	703.2	704.0	20.8	29.5	23.4	24.3	29.5	15.6	-	12.8	09.4	09.1	69	30	42	47	SE 1	SW 2	SW 1
19	703.5	703.8	705.8	14.1	21.4	15.4	16.6	23.4	12.9	-	09.0	08.9	12.3	75	47	94	72	- 0	- 0	- 0
20	703.9	707.2	708.7	14.6	16.2	15.4	15.4	17.4	14.0	-	11.8	12.2	11.3	95	88	86	90	- 0	- 0	- 0
21	709.3	709.9	711.6	14.8	24.2	16.5	18.0	24.5	11.2	-	10.1	08.2	09.7	80	36	69	62	- 0	NNE 1	- 0
22	712.5	711.9	710.8	14.4	24.8	18.8	19.2	26.5	11.3	-	09.9	12.7	11.6	81	54	71	69	- 0	NW 1	ENE 1
23	710.5	709.1	710.1	15.9	28.4	19.8	21.0	28.6	12.5	-	10.8	08.3	09.3	80	28	54	54	- 0	- 0	- 0
24	710.4	709.4	711.3	15.4	27.5	16.1	18.8	27.9	14.5	-	10.5	09.9	11.8	80	36	86	67	- 0	WNW 1	ESE 1
25	712.0	711.6	711.6	14.4	25.0	17.2	18.4	25.4	12.2	-	10.3	11.1	12.0	84	47	81	71	SE 1	W 2	- 0
26	713.5	712.4	711.1	15.1	24.0	20.0	19.8	25.3	12.9	-	11.1	13.1	13.0	86	58	74	73	- 0	NW 1	- 0
27	711.6	710.2	710.2	16.6	25.4	19.4	20.2	26.4	13.2	-	11.5	10.6	10.9	81	44	64	63	- 0	E 0	E 1
28	710.3	706.9	706.7	16.8	28.2	20.0	21.2	28.4	13.2	-	11.1	10.1	10.8	77	35	62	58	- 0	NE 2	- 0
29	709.5	707.5	708.4	18.2	25.6	15.8	18.8	28.4	14.8	-	11.2	11.1	12.1	71	45	90	69	- 0	S 2	- 0
30	706.6	703.8	703.1	14.2	25.6	21.4	20.9	27.8	12.2	-	11.1	11.5	08.8	92	44	46	61	- 0	NNW 1	S 2
MES. VRED.	708.6	707.9	708.2	14.3	22.8	16.7	17.6	24.0	11.6	-	10.1	09.8	10.3	82	49	73	68	0.2	1.2	0.4

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BR. ST. 144 H_s = 630 m H_b = 637.0 m h_t = 2.0 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	7	08	06⊙	10	09.0	06.1	09.5	00	= n-12^40 • 16^20-19^35
2	6	10	10	10*≡	10.0	00.0	02.8	•	= n-19^50 * 11^15-11^55 19^45 n; ≡ 19^50 n
3	6	10	10•	10	10.0	00.0	03.2	00	= n-n, * 7^25-8^15 * 18^25-8^20, • 8^30 ni
4	7	07≡	04⊙	10	07.0	09.9	00.9	00	≡ n-8^30
5	6	10•	10	10	10.0	00.0	00.2	•	= n-n, • n-13^20 i
6	7	10	08	09	09.0	03.1	01.8	•	= n-14^40
7	8	10	10	10	10.0	00.2	•	•	• 17^50-18^40
8	7	10	10	05	08.3	00.0	09.1	•	
9	8	04⊙	06⊙	04	04.7	10.3	•	•	
10	8	10	07⊙	02	06.3	07.5	00.2	•	• n
11	7	03⊙	06⊙	09	06.0	09.4	•	•	
12	8	10•	09	01	06.7	03.9	01.7	•	• n-7^45
13	9	06⊙	07⊙	09	07.3	06.7	00.1	•	T 16^05-16^20
14	8	04⊙	07⊙	02	04.3	11.0	•	•	• 15^50-16^05 i
15	8	02⊙	10	04	05.3	06.9	00.0	•	
16	7	00⊙	08⊙	03	03.7	07.8	00.0	•	• n, 10^55-13^45 i
17	3	10	08	10	09.3	06.6	01.2	•	= n-10^45 ↯ 14^12-17 i, • 14^30 ni
18	5	10•	10•	10•	10.0	00.0	16.6	•	• n-n, ≡ 8^30-11, = 11-n
19	6	10•	10•	10•	10.0	00.0	07.4	•	• n-n, = n-n
20	6	10	10•	10	10.0	02.3	07.6	•	= n-n, • 12^40-14^40
21	6	10	10	10	10.0	00.0	00.5	•	= n-n, • 7^40-10^15 i
22	7	09	10	10•	09.3	02.0	00.1	•	= n-12, 14^40-n; • 10^55 ni, ⊽ 11^10-11^30, ↯ NW 12^35
23	7	10•	09	08	09.0	03.4	20.9	•	• n-8^20 17^10 19; ≡ n-11^15
24	7	10•	09	04	07.7	01.5	00.2	•	• n-14^50, = n-16^50
25	7	10•	10	02	07.3	03.7	01.5	•	= n-10
26	3	06⊙	08⊙	02	05.3	10.8	•	•	
27	7	00⊙	06⊙	10•	05.3	09.7	•	•	= n-10^50 △ n-8^45, • 15^20, 20^40 n; ↯ NNW 15^38
28	6	10	10•	10•	10.0	00.2	01.6	•	= n-n, • 12^45-n
29	7	10	07⊙	00	05.7	06.0	12.0	•	= n-12^45
30	8	04⊙	10	09	07.7	06.1	•	•	• 11^50-12^20 20^35-20^55
31	7	10	08↯	10	09.3	02.0	01.6	•	↯ ENE-N 16^50, 13^25, • 11^30-14^50, 14^40-n
MES. VRED.		07.8	08.5	07.2	07.8	140.1	102.8		

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1	6	10	10•	10	10.0	01.9	02.9	•	= n-n, • 9^45-14^15
2	6	10	10	10•	10.0	00.5	00.9	•	= n-n, • 15^40-15^20 18^50 n
3	6	10	10•	10	10.0	01.0	00.3	•	= n-n, • 11^40-19^30 i
4	6	10•	10	00	06.7	00.4	04.0	•	= n-n, • n-10^20
5	7	05⊙	06⊙	02	04.3	11.1	01.4	•	= 16-n
6	7	10•	10	02	07.3	03.8	00.0	•	• n-8^40 = 17^30 n
7	7	10	07⊙	04	07.0	03.7	00.2	•	• 10^45-11^20 = 18-n
8	7	03⊙	02⊙	08	04.3	10.3	00.0	•	= n-10^30
9	7	05⊙	07⊙	03	05.0	05.0	•	•	• 11^40-12^10
10	7	08	04⊙	05	05.7	11.4	00.0	•	
11	7	07⊙	08•	03	06.0	09.1	•	•	• 13^40-14^05 19^50-20^35 ↯ NW 13^40, 19^49
12	7	07⊙	10•	07	08.0	06.9	00.2	•	= n-9^20, • 10^55-14^20
13	7	00⊙	04⊙	03	02.3	13.2	02.0	•	
14	7	00⊙	10• ↯	03	04.3	06.4	•	•	= n-10, ↯ NW 13^40 16, ↯ NW 13^20-15, • 13^25-16^20
15	7	10•	04⊙	05	06.3	04.5	12.1	•	= n-11^30, 6^45-9^20, 19^30-20^35, ↯ SE 19^25-20^05
16	7	08⊙	10	06	08.0	07.2	00.7	•	= n-10^30, 18^30-n; ↯ W 15^40-16^35, • 15^20-16^45
17	8	03⊙	05⊙	09	05.7	12.0	00.4	•	= n-10
18	7	04⊙	05⊙	09• ↯	06.0	12.4	00.3	•	• 2^30-2^45 20^45 n; ↯ 20^05-?, ↯ 20^30 n
19	8	10•	07⊙	08	08.3	01.3	12.9	•	• n-9^45, 17^45-17^55
20	6	10•	10•	10	10.0	00.0	03.2	•	= n-n, • 5^45-14^30
21	7	03⊙	03⊙	01	02.3	11.6	14.5	•	= n-10^30, 17^30 n
22	8	01⊙	05•	00	02.0	10.7	•	•	= n-6^30, 17^30 n; △ n-7^30 • 13^30-14^10, T 14^30-15, ↯ 15-15^10
23	8	00⊙	03⊙	09	01.0	12.3	00.0	•	= n-9, 18-n; △ n-7^30 ↯ N 18
24	8	00⊙	04⊙	10•	04.7	11.4	•	•	△ n-8^30 ↯ NE 18^40-20, = 18^30 n • 18^50 n
25	7	03⊙	08↯⊙	03	04.7	07.5	01.4	•	= n-8, ↯ NE-W 9^30-14^55 i, • 11^05-12^40
26	7	10	08⊙	09	09.0	06.0	01.3	•	= n-9^05 ↯ 17^50-18^40, ↯ S 20^40 n
27	8	08⊙	07⊙	00	05.0	08.1	•	•	= n-9^30, ^2 n-9
28	8	00⊙	03⊙	05	02.0	13.2	•	•	= n-6^30 △ n-8^30
29	7	01⊙	09↯	08	06.0	07.7	•	•	= n-9^45, △ n-7^30 T 12^25-13^02, ↯ 13-15^30, 17^55, • 13^55-15^30, ↯ 14^40-14^20
30	7	10≡	04⊙	01	05.0	10.1	11.5	•	≡ n-9, = 9-12
MES. VRED.		05.9	06.8	0..1	05.9	220.7	74.2		

φ = 43° 52' N λ = 18° 26' E Gr. ΔG = + 1h 14 min. BR. ST. 144

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred. Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	702.6	701.9	704.5	17.2	20.2	15.1	16.9	21.6	14.6	-	10.6	12.4	10.7	72	70	83	75	- 0	WNW 1	W 1
2	704.9	702.8	703.2	15.1	25.2	18.8	19.5	25.8	13.6	-	10.7	11.0	11.4	83	46	70	66	SW 1	WNW 1	- 0
3	704.7	705.7	706.2	16.2	17.2	15.8	16.2	18.8	12.2	-	10.4	10.1	10.6	75	69	79	74	S 1	WNW 1	W 1
4	705.3	704.5	707.5	14.2	19.3	11.3	14.0	19.8	10.9	-	10.8	11.4	09.5	89	68	94	84	- 0	WSW 1	NW 1
5	707.5	708.3	708.2	10.2	11.0	11.0	10.8	11.4	09.6	-	08.9	09.5	09.5	95	96	96	96	NW 1	W 1	- 0
6	709.5	710.5	710.8	11.2	11.4	11.4	11.4	11.6	10.5	-	09.3	09.6	09.9	93	95	98	95	- 0	- 0	- 0
7	708.3	708.6	707.8	12.6	15.0	15.4	14.6	16.2	11.0	-	10.7	11.7	12.3	98	92	94	95	- 0	W 1	- 0
8	707.2	705.2	705.6	15.8	24.8	18.5	19.4	29.6	13.8	-	12.1	11.2	12.3	90	48	77	72	SE 1	SE 2	SE 1
9	706.9	705.7	706.2	16.3	28.1	20.8	21.5	28.9	13.3	-	11.4	11.5	15.1	82	40	82	68	- 0	WNW 1	- 0
10	708.7	708.7	711.3	17.4	28.0	20.1	21.4	28.3	16.2	-	12.4	14.5	15.3	83	51	87	74	SSE 2	WNW 1	NNE 2
11	711.7	709.7	710.3	17.4	28.5	20.2	21.6	28.5	15.1	-	12.4	11.1	11.5	87	38	65	62	- 0	WSW 1	E 2
12	711.0	709.9	710.3	17.2	28.2	21.4	22.0	28.4	13.3	-	11.4	12.2	13.1	78	42	68	63	- 0	ENE 2	ESE 2
13	712.6	711.0	710.3	17.6	26.4	19.2	20.6	27.9	14.8	-	12.0	10.1	10.7	80	39	64	61	SE 1	NW 2	SE 2
14	708.1	705.3	704.8	15.4	28.6	22.9	22.4	29.0	13.1	-	10.5	11.7	12.2	80	40	58	59	- 0	WNW 2	- 0
15	701.5	699.7	699.0	18.8	27.6	23.2	23.2	28.6	14.6	-	11.4	09.8	09.5	70	35	44	50	E 1	SW 2	SW 2
16	700.0	700.2	701.1	12.0	11.5	10.3	11.0	23.6	09.8	-	09.8	09.7	09.1	93	95	96	95	NE 1	WSW 1	W 1
17	702.0	703.6	704.9	10.4	10.3	09.4	09.9	11.3	08.7	-	08.6	07.7	07.8	91	82	88	87	W 1	SW 1	- 0
18	705.3	707.7	706.3	08.5	09.7	08.9	09.0	12.2	07.9	-	07.7	07.6	07.4	92	84	86	87	W 1	W 1	- 0
19	705.3	704.2	705.2	10.4	20.2	15.1	15.2	23.0	06.6	-	07.7	06.9	08.5	81	39	66	62	- 0	WNW 1	- 0
20	705.6	705.3	706.1	12.2	24.0	17.9	18.0	24.2	08.3	-	08.1	08.6	07.6	76	38	49	54	- 0	SSW 2	- 0
21	708.1	708.1	708.2	16.8	27.4	20.2	21.2	27.4	13.0	-	09.1	10.2	11.5	63	37	65	55	- 0	W 2	- 0
22	710.1	709.1	709.6	16.0	31.0	21.6	22.6	31.6	13.8	-	10.0	10.5	11.4	73	31	59	54	- 0	W 1	- 0
23	711.1	710.2	710.4	17.4	29.9	21.9	22.8	30.4	14.2	-	10.8	12.6	14.1	72	40	72	61	ESE 2	ESE 1	ESE 1
24	710.5	708.1	707.3	17.2	29.4	22.0	22.4	30.4	14.4	-	11.7	14.8	14.7	79	48	74	67	E 1	WNW 1	- 0
25	704.5	700.9	704.4	18.8	30.6	16.8	20.8	31.8	15.8	-	12.8	12.2	11.6	79	37	81	66	- 0	SW 1	- 0
26	705.1	707.3	707.9	15.4	17.0	13.0	14.6	22.0	12.6	-	10.5	09.0	08.2	80	62	73	72	SW 1	SE 1	ESE 1
27	710.0	709.1	710.5	10.8	23.4	17.2	17.2	24.4	07.6	-	07.3	08.9	09.4	75	41	64	60	- 0	W 2	- 0
28	711.9	710.7	710.5	13.4	26.4	17.6	18.8	26.9	10.5	-	09.1	10.1	10.4	79	39	69	62	- 0	E 2	ESE 1
29	710.5	708.4	708.2	14.6	27.9	20.0	20.6	28.1	12.2	-	09.9	13.1	11.9	80	47	68	65	- 0	W 1	ESE 1
30	709.5	709.4	710.9	16.3	27.1	19.3	20.5	27.6	12.9	-	11.0	09.5	11.4	79	35	68	61	- 0	S 1	SE 1
31	711.4	710.5	711.3	16.1	28.2	19.2	20.7	28.8	13.1	-	11.1	10.7	13.2	81	37	79	66	- 0	W 2	SE 1
MES. VRED.	707.5	706.8	707.4	14.8	23.0	17.3	18.1	24.3	12.2	-	10.3	10.6	11.0	81	54	75	70	0.5	1.3	0.7

1	711.5	710.2	711.5	17.5	20.8	16.6	17.9	26.0	14.3	-	12.2	12.5	11.7	81	68	83	77	ESE 1	ESE 3	NW 1
2	710.1	707.9	708.5	14.6	22.8	17.0	17.8	25.8	13.2	-	10.9	13.4	12.6	88	64	87	80	- 0	- 0	- 0
3	707.3	705.7	706.4	14.8	26.0	17.9	19.2	27.4	13.1	-	11.5	13.0	13.5	91	51	88	77	- 0	WNW 1	- 0
4	706.9	705.8	707.9	16.6	28.7	19.4	21.0	29.0	14.4	-	11.5	12.4	13.6	81	42	81	68	- 0	W 1	- 0
5	709.4	709.1	710.3	16.7	29.1	21.3	22.1	29.4	14.2	-	12.2	09.3	13.8	86	31	73	63	- 0	WNW 1	SE 1
6	710.7	709.6	709.1	17.2	30.8	22.0	23.0	31.2	14.4	-	12.1	05.2	12.6	82	15	64	54	- 0	- 0	- 0
7	709.0	706.9	706.3	18.3	33.0	24.2	24.9	33.2	15.0	-	11.9	13.7	14.2	76	36	63	58	- 0	NNW 1	- 0
8	705.8	703.9	704.1	20.6	29.4	19.9	22.4	31.9	17.1	-	12.3	13.2	14.2	68	43	82	64	ESE 1	WNW 1	- 0
9	702.3	699.6	700.8	18.2	29.4	19.2	21.5	29.6	15.8	-	14.2	10.1	12.9	91	33	77	67	- 0	SSW 2	- 0
10	702.6	703.4	704.1	16.6	20.2	16.2	17.3	24.9	13.2	-	12.5	11.3	10.8	88	63	78	76	- 0	NNW 2	- 0
11	704.1	706.2	707.1	14.2	14.8	14.2	14.4	16.3	10.2	-	08.7	11.7	11.4	72	93	94	86	ESE 1	WSW 1	- 0
12	709.1	710.2	710.3	13.0	18.2	14.7	15.2	21.5	11.4	-	10.7	13.1	11.5	96	84	92	91	- 0	- 0	- 0
13	710.1	709.6	710.4	12.4	25.8	19.2	19.2	26.1	10.2	-	08.9	10.7	11.9	83	43	71	66	SE 1	W 1	E 1
14	710.5	709.4	710.4	14.8	28.0	20.0	20.7	28.3	12.3	-	10.8	12.4	12.5	86	44	71	67	- 0	WNW 1	E 1
15	711.0	708.8	707.9	16.5	30.1	20.4	21.8	30.2	13.0	-	10.2	10.3	10.5	73	32	58	54	ESE 1	WNW 1	SE 1
16	707.4	705.8	705.6	16.4	28.5	21.4	21.9	29.0	12.9	-	10.0	11.4	13.5	72	39	71	61	- 0	W 1	- 0
17	704.1	702.2	702.7	16.6	29.8	23.0	23.1	29.8	14.1	-	12.0	12.6	11.5	85	40	55	60	SW 1	WNW 1	NNW 1
18	706.2	706.1	706.0	15.2	20.0	15.6	16.6	23.0	14.7	-	10.9	10.8	10.9	84	62	82	76	- 0	- 0	SE 1
19	706.2	705.2	706.0	12.6	29.0	20.2	20.5	29.4	10.3	-	10.0	10.3	13.2	91	34	74	66	- 0	NW 1	- 0
20	706.3	705.0	704.8	16.8	31.4	22.4	23.2	31.6	13.7	-	11.1	09.4	13.4	77	27	66	57	- 0	WNW 1	ESE 1
21	703.4	701.8	701.8	18.0	31.0	22.8	23.6	31.6	14.6	-	10.0	07.4	10.5	65	22	50	46	ESE 2	S 2	- 0
22	702.8	702.8	704.1	16.0	22.2	18.0	18.6	24.4	14.3	-	11.8	14.3	11.8	86	71	76	78	- 0	- 0	- 0
23	705.9	704.5	705.0	15.3	24.7	17.8	18.9	25.4	14.1	-	11.6	08.7	09.7	89	37	64	63	- 0	WNW 1	- 0
24	705.4	702.9	702.7	12.8	14.6	14.0	13.8	22.2	11.2	-	08.5	10.9	10.1	77	88	84	83	SE 1	NW 2	NE 1
25	705.5	707.2	708.7	11.5	15.5	12.8	13.2	15.9	11.1	-	09.4	09.3	10.2	92	70	92	85	W 1	W 2	- 0
26	710.2	709.8	711.3	11.9	19.0	13.0	14.2	20.2	10.1	-	09.5	07.0	08.2	91	43	73	69	- 0	WNW 1	- 0
27	711.8	710.7	710.8	11.0	20.6	13.2	14.5	21.0	07.7	-	07.9	07.7	08.1	81	42	71	65	ESE 1	NNW 2	- 0
28	710.7	709.3	709.3	09.9	22.2	14.8	15.4	22.5	06.8	-	07.5	08.1	07.9	82	41	63	62	ESE 1	NNW 1	- 0
29	710.0	710.0	709.8	12.8	24.2	19.5	19.0	25.4	11.0	-	08.0	10.1	09.9	72	45	58	58	ESE 1	WNW 1	- 0
30	708.9	707.9	708.3	15.2	22.4	15.7	17.2	24.0	13.9	-	10.6	09.9	12.6	82	49	94	75	ESE 3	S 1	ESE 1
31	706.8	705.7	707.0	13.8	19.3	15.0	16.3	19.8	12.6	-	11.1	13.4	12.7	94	80	93	89	E 1	- 0	- 0
MES. VRED.	707.5	706.6	707.1	15.1	24.6	18.1	19.0	26.0	12.7	-	10.7	10.8	11.7	83	49	75	69	0.5	1.1	0.3

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BR. ST. 144 H_s = 630 m H_b = 637.0 m h_t = 2.0 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednje		7	7	
1	7	10●	07⊙	10	09.0	04.3	00.5	.	●6^{30} 9^{35}; T 9^{04}; ♀ 9^{10} 9^{25}
2	8	09⊙	02⊙	00	03.7	10.6	03.1	.	
3	7	07⊙	10	10	09.0	00.6	.	.	∞ 7 9^{30}
4	7	10	10	10●	10.0	00.1	.	.	●17^{25} 19^{40}; ● 19^{40} n
5	9	10●	10●	10●≡	10.0	00.0	04.1	.	● n-10; ● 10- n; ≡ 19^{30} n
6	4	10●	10●	10●≡	10.0	00.0	22.4	.	●n-18^{40} i; ● 19- n ≡ 19^{30} n
7	5	10●≡	10	10	10.0	00.0	15.1	.	● n-10^{55}; ≡ n-13^{46}; ● 10^{55}- 11^{30}; = 13^{40} ni
8	8	05⊙	03⊙	00	02.7	12.2	03.1	.	= n-6^{40}
9	8	00⊙	03⊙	01	01.3	12.9	.	.	△ n-7^{40} ↳ 20^{30} n
10	8	09	06⊙	07	07.3	08.9	00.7	.	●n-6^{30}; ↱ n-6^{30}; T 14^{40}; △ 20-n
11	8	00⊙	04⊙	00	01.3	11.3	.	.	△ n-9
12	7	04	05⊙	05	04.7	09.2	.	.	△ n- 8^{20} = n-11^{30}
13	8	00⊙	03⊙	00	01.0	13.0	.	.	△ n-8^{40} ∞ 6^{30}- 8^{30}
14	8	01⊙	05⊙	00	02.0	11.4	.	.	△ n-7^{30} ∞ n- 10; ↳ E 8^{50}
15	8	00⊙	04⊙	00	01.3	12.6	.	.	△ n-7^{45}
16	5	10●	10●	10●	10.0	00.1	00.3	.	● 2-4^{40} 9-16i; ♀ 8^{45}- 10^{55} i; ↱ 9^{55}- 10, 11^{16}; ● 20- 21; = 20-n
17	7	10●	10	10	10.0	00.0	20.[illegible]	.	●6^{40}- 17^{50} i
18	7	10●	10●	09	09.7	00.2	01.4	.	● n
19	8	00⊙	03⊙	00.	01.0	09.8	01.0	.	△ n- 8^{30} = n-9^{30}
20	8	00⊙	04⊙	00	01.3	13.5	.	.	△ n-8^{40}
21	6	02⊙	03⊙	00	01.7	13.6	.	.	△ n-8^{30}
22	8	00⊙	01⊙	02	01.0	13.5	.	.	△ n-8^{30} 20^{40} n
23	8	00⊙	02⊙	00	00.7	13.5	.	.	△ n-8; 20^{45} n
24	8	00⊙	02⊙	00	01.0	13.3	.	.	△ n-8^{15}; 20^{45} n
25	8	00⊙	05⊙	09	04.7	09.4	.	.	△ n-9; ● 17^{58}; ↱ 17^{53}- 18^{10}
26	8	10	10	00	05.7	01.6	00.0	.	△ n-7^{30} 20^{45}-n
27	8	00⊙	03⊙	01	01.3	13.0	.	.	△ n-8^{25}; 20-n
28	3	00⊙	06⊙	00	02.0	10.5	.	.	△ n-8; 20^{30}- n
29	8	00⊙	04⊙	00	01.3	12.8	.	.	△ n-8^{30} 20-n
30	7	00⊙	07	00	02.3	10.7	.	.	△ n-8; 20-n; = n-9^{30}
31	7	01⊙	03⊙	00	01.3	11.6	.	.	△ n-9; 20 -n; = n-9^{30}; T E 17^{48}- 17^{55}
MES. VRED.		04.1	05.7	03.7	04.5	254.8	76.0		

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1	6	00⊙	10↱	05	05.0	05.2	.	.	△ n-10^{30} = n-19^{30} T N 12-13^{35}; ↱ N 13^{35}- 13^{50}; ●▲ 13^{45}- 14; 14-15^{45}
2	7	07	09	10	09.7	05.5	06.7	.	= n-9^{40}; ↱ 10^{15}- 13^{36}; ● 19^{40}- 19^{35};
3	7	10	05⊙	00	03.0	08.9	00.1	.	= n-11^{36}; ● 16^{15}- 16^{40};
4	7	01⊙	06⊙	00	02.3	10.4	00.0	.	△ n-10^{50}; 19^{45}- n; = n-10; T N 14^{55}- 17^{30}
5	7	08⊙	03⊙	00	03.7	11.4	.	.	△ n-9; 20-n; = n-9^{30}
6	8	00⊙	01⊙	00	00.3	12.9	.	.	△ n-9; 19^{45} n; = n-9
7	7	00⊙	00⊙	00	00.0	12.3	.	.	△ n- 8^{30}; 19^{45} n; = n-9
8	7	08⊙	07●	06	07.0	09.6	.	.	△ n-7^{30}; ● 13^{45}- 14^{05}; 19-19^{30}; ↱ NE-S 14^{05}- 14^{10}; 18^{45}- 19; ↳ NE 19-n
9	8	08	06⊙	04	04.0	07.5	03.3	.	= n-9; ● 8^{25}- 8^{35}; T N 15^{20}; ↳ 19^{45}- n
10	8	04⊙	09	01	04.7	06.1	00.0	.	△ n-8^{15}; ♀ 13^{05}- 13^{40}
11	6	06⊙	10	10	03.7	01.3	00.9	.	● 8^{15}- 15^{30} i; = 9-19^{30}
12	6	10≡	09●	00	06.3	03.9	04.7	.	≡ n-11; = 11-14^{45}; ● 12^{30}- 14^{40}
13	8	09	02⊙	07	06.0	10.4	01.7	.	△ 20-n
14	7	00⊙	01⊙	00	00.3	12.4	.	.	△ n-8^{30} 19^{45} n; = n-8^{30}
15	8	00⊙	02⊙	02	01.3	12.8	.	.	△ n-8^{30}; 19^{45} n; = n-8^{30}
16	8	00⊙	02⊙	04	02.0	11.5	.	.	△ n-9; 20-n
17	8	03⊙	04⊙	01	02.7	03.1	.	.	△ n- 8^{45} = n-11
18	7	10●	10	00	06.7	01.8	06.0	.	● n-7^{40} 9^{30}- 10^{40}
19	8	04⊙	02⊙	00	02.0	11.7	00.0	.	△ n-10^{15} 20-n; = n-10
20	3	02⊙	02⊙	00	01.3	12.6	.	.	△ n-9^{30}; 19^{45} n
21	8	01⊙	05⊙	09	05.0	03.8	.	.	△ 20-n; ● 23^{30}- 24
22	7	04⊙	09●	03	05.3	11.2	04.3	.	= n-11; ● 0-1; 11^{30}- 14i
23	8	08⊙	04⊙	04	05.3	09.4	01.4	.	= n-9; △ 20-n
24	6	10	10●↱	06	08.7	01.1	.	.	● 7^{05}- 10; 12^{45}- 14^{15}; = 12^{30}- n; ↱ 12^{59}- 14^{15}; ♀ 13^{30}- 14^{07}
25	6	10●	10	06	08.7	00.2	12.1	.	= n-n; ● 6^{30}- 7^{40}; 15^{30}- 18^{45}; 22-n
26	8	06⊙	07⊙	02	05.0	03.7	03.0	.	= n-10; △ 19^{30} n
27	7	03⊙	06	00	03.3	09.4	.	.	= n-9; △ n-8^{30} 19^{30}- n
28	7	02⊙	03⊙	00	01.7	11.7	.	.	= n-10^{30}; △ n-11; 19^{30} n
29	7	04⊙	08	10	07.3	04.1	.	.	= n-10^{50}
30	7	07	09	10	08.7	01.1	01.1	.	● 1^{40}- 1^{40}; 4^{30}- 6^{20}; 15^{30}- 19
31	6	10	09	10	09.7	00.3	06.[illegible]	.	= 6^{45}- n; ♀ 14^{20}- 14^{30}; ● 14^{50}- 19^{50} i; 23^{40}- 24; ↱ 15^{24}; T 15^{45}-16
MES. VRED.		05.0	05.8	03.3	04.8	239.8	36.7		

φ = 43° 52' N λ = 18° 26' E Gr. ΔG = + 1h 14 min. BR. ST. 144

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	706.1	706.2	706.7	15.3	19.3	15.2	16.2	19.6	14.4	-	12.1	11.4	11.5	93	68	89	83	- 0	WSW 1	- 0
2	708.1	708.7	709.0	14.7	19.5	15.2	16.2	20.8	13.7	-	11.6	12.2	10.4	93	72	80	82	- 0	- 0	ESE 1
3	709.5	708.5	708.7	11.6	25.8	18.6	18.6	25.8	09.3	-	08.9	09.0	11.3	86	36	70	64	ESE 1	WNW 1	- 0
4	708.7	709.7	710.8	14.5	16.5	14.4	15.0	20.4	12.5	-	10.5	12.8	11.5	85	91	94	90	ESE 1	- 0	- 0
5	710.8	709.1	708.8	11.8	24.0	14.9	16.4	24.0	09.0	-	09.0	08.3	09.6	87	37	75	66	ESE 1	W 1	SE 1
6	707.9	707.3	708.7	13.9	24.2	18.6	19.3	26.8	09.6	-	08.7	11.1	11.8	73	43	73	63	- 0	W 1	- 0
7	711.2	710.7	711.8	16.2	22.2	13.8	16.5	22.3	13.7	-	10.9	11.1	09.6	79	55	81	72	SE 1	W 2	SE 1
8	711.1	709.0	709.3	10.7	27.2	18.0	18.5	28.2	08.4	-	08.9	10.0	10.8	92	37	70	66	- 0	WNW 1	- 0
9	709.9	708.3	708.6	14.6	29.8	18.2	20.2	30.2	10.5	-	08.3	08.7	11.3	66	28	72	55	ESE 2	W 2	- 0
10	708.6	707.6	707.8	14.0	30.0	18.1	20.0	30.2	12.1	-	08.1	08.3	11.0	68	26	70	55	SE 2	NW 1	- 0
11	708.4	707.1	707.6	14.0	31.2	19.4	21.0	32.7	11.5	-	07.2	07.4	06.7	60	22	40	41	SE 2	- 0	- 0
12	707.4	706.1	705.6	16.4	28.2	18.8	20.6	28.3	12.6	-	08.2	08.9	09.2	59	31	57	49	ESE 2	ESE 2	- 0
13	704.0	702.6	705.6	17.6	30.4	20.4	22.2	32.1	13.9	-	08.0	07.8	12.3	53	24	68	48	ESE 2	WNW 1	ENE 1
14	708.4	706.5	709.0	15.6	25.8	17.8	19.2	26.4	14.8	-	10.7	11.6	11.4	80	46	75	67	- 0	- 0	SE 1
15	708.7	707.3	708.2	13.0	28.2	18.2	19.4	28.5	10.6	-	10.0	08.7	10.0	89	30	64	61	- 0	WNW 2	ESE 2
16	708.5	706.7	707.5	14.1	28.4	18.0	19.6	28.7	11.3	-	09.2	08.8	10.8	76	30	70	59	SE 1	WSW 1	ESE 2
17	712.2	712.7	713.0	11.6	11.0	09.6	10.4	18.0	09.1	-	08.4	08.0	08.4	82	82	94	86	NNW 1	- 0	NW 1
18	712.3	712.6	713.4	10.0	12.4	12.1	11.6	13.2	09.0	-	08.9	09.7	09.5	96	90	9	92	- 0	- 0	- 0
19	712.5	712.1	712.6	11.6	17.9	15.0	14.9	19.6	10.8	-	09.5	10.6	11.0	93	69	86	83	- 0	W 1	- 0
20	712.3	710.2	710.7	11.4	20.6	13.8	14.9	21.6	10.2	-	09.2	08.9	08.9	91	49	75	72	- 0	ENE 2	- 0
21	710.6	708.9	710.1	08.5	19.5	14.0	14.0	19.8	07.5	-	07.8	06.9	07.9	94	41	66	67	- 0	WNW 1	N 1
22	709.3	710.0	711.9	10.6	16.6	09.8	11.7	17.7	09.1	-	08.4	09.7	06.9	87	68	76	77	- 0	- 0	- 0
23	712.1	710.7	710.9	05.6	14.8	08.6	09.4	16.2	02.9	-	05.6	06.1	06.1	82	49	73	68	SE 2	NNW 1	ESE 2
24	712.8	710.5	711.4	05.0	18.3	08.3	10.0	18.3	01.9	-	05.2	05.0	05.4	80	31	65	59	SE 1	NW 2	E 2
25	712.0	710.1	711.1	04.6	17.1	08.2	09.5	17.9	01.8	-	04.9	05.8	05.7	77	39	70	62	ESE 2	W 2	ESE 1
26	711.0	709.3	710.2	05.6	21.4	13.6	13.6	22.1	03.7	-	05.7	06.7	07.6	83	35	65	61	- 0	WNW 1	ESE 2
27	714.1	714.9	715.5	10.2	15.1	06.8	09.7	16.1	06.2	-	08.4	06.2	05.9	90	48	80	73	- 0	WNW 2	- 0
28	717.1	716.6	718.6	05.2	14.1	08.4	09.0	14.8	02.4	-	05.7	05.2	05.6	86	43	68	66	- 0	ENE 1	- 0
29	718.0	716.0	716.6	03.0	15.7	04.6	07.0	16.0	00.6	-	04.0	02.5	04.3	71	18	68	52	ESE 1	E 2	E 1
30	714.1	710.1	708.6	01.5	18.9	08.3	09.2	19.6	-01.7	-	03.5	04.0	04.7	69	24	57	50	ESE 1	- 0	- 0
MES. VRED.	710.6	709.5	710.3	11.1	21.5	14.0	15.1	22.5	08.7	-	08.2	08.4	08.9	81	45	73	66	0.8	1.0	0.6

1	706.5	702.1	699.7	07.5	12.6	10.2	10.1	18.2	03.1	-	04.8	06.4	08.8	62	58	94	71	- 0	WSW 2	W 1
2	704.4	703.7	701.7	07.6	14.0	07.2	09.0	14.4	06.3	-	07.0	05.9	06.1	90	49	80	73	- 0	W 1	ESE 4
3	698.2	700.1	702.1	09.2	04.3	03.4	05.1	10.1	01.5	-	06.8	05.6	05.5	78	90	94	87	- 0	NW 1	SW 1
4	702.8	703.3	706.7	03.8	12.0	08.0	08.0	12.6	02.9	-	05.5	05.2	06.4	91	50	80	74	- 0	SW 1	- 0
5	709.3	707.6	708.7	03.8	15.7	12.0	10.9	16.7	02.1	-	05.4	05.2	06.5	89	39	61	63	- 0	- 0	- 0
6	708.7	708.8	709.4	06.6	21.0	10.5	12.2	26.5	04.8	-	06.3	06.5	08.0	86	35	84	68	- 0	W 2	- 0
7	709.1	708.3	709.5	07.2	23.2	10.8	13.0	23.6	06.1	-	06.2	06.1	07.1	82	29	73	61	ESE 3	WNW	SE 1
8	710.5	710.4	711.7	07.4	23.4	12.2	13.8	23.6	06.8	-	07.1	08.9	08.8	92	41	82	72	SE 2	- 0	ESE 2
9	712.6	712.4	713.1	08.0	22.2	12.4	13.8	23.2	05.8	-	07.4	09.2	08.0	92	46	74	71	- 0	WSW 1	ESE 1
10	713.7	714.1	715.2	06.6	23.0	12.3	13.6	23.8	06.1	-	06.7	08.5	06.6	92	40	62	65	ESE 1	- 0	ESE 2
11	716.4	715.3	714.0	05.0	22.2	12.1	12.8	23.4	04.7	-	05.2	08.1	05.6	80	41	53	58	SE 1	- 0	ESE 1
12	716.6	714.3	715.5	06.8	21.8	12.6	13.4	21.8	05.1	-	05.5	08.2	08.4	74	42	76	64	SE 2	SW 2	E 1
13	715.2	712.4	712.7	09.0	20.8	10.8	12.8	21.3	07.9	-	07.8	07.6	08.6	90	41	88	73	- 0	WNW 1	ESE 2
14	711.5	709.3	710.0	05.4	17.2	10.6	11.0	18.4	04.4	-	06.3	08.9	07.4	94	60	77	77	- 0	W 1	E 1
15	710.0	710.0	710.9	09.4	10.0	08.3	09.0	11.0	07.8	-	08.0	08.5	06.9	90	93	84	89	- 0	- 0	SE 1
16	712.9	713.6	715.0	03.2	05.2	03.5	03.8	08.4	02.6	-	05.0	03.9	03.8	88	58	65	70	- 0	NE 1	ENE 1
17	714.0	712.4	712.7	02.8	04.8	03.0	03.4	06.0	02.3	-	03.9	04.2	04.3	69	66	75	70	SE 1	SE 3	SE 2
18	710.7	710.5	711.8	02.4	04.8	03.6	03.6	05.4	01.9	-	04.7	05.0	05.0	87	77	85	83	N 1	- 0	NW 1
19	710.2	706.2	705.3	03.4	11.4	05.3	06.4	12.2	02.5	-	05.1	05.6	05.6	88	56	84	76	- 0	- 0	SE 2
20	701.6	698.7	696.7	03.6	16.2	15.0	12.4	17.7	01.0	-	05.4	06.1	06.6	91	44	52	62	SSW 1	SSW 3	S 2
21	695.3	700.4	701.5	15.6	07.4	06.9	08.7	15.1	06.3	-	07.9	07.3	07.1	67	95	95	86	S 2	SSW 1	- 0
22	703.6	705.0	706.0	03.2	03.8	00.9	02.2	07.8	00.3	-	05.4	05.6	04.7	94	94	96	95	- 0	NW 1	- 0
23	705.1	705.5	706.9	00.4	01.8	02.0	01.6	02.3	-00.2	-	04.6	05.0	05.1	96	97	97	97	- 0	- 0	- 0
24	708.7	711.4	713.7	01.4	02.8	01.1	01.6	04.0	00.6	-	04.9	05.1	04.7	97	90	95	94	NNW 1	WNW 2	- 0
25	713.2	713.7	714.7	-00.4	04.8	03.6	02.9	05.4	-01.2	-	04.0	03.9	04.7	89	60	79	76	- 0	WNW 1	- 0
26	714.2	711.6	711.4	02.4	16.4	08.8	09.1	16.8	00.3	-	04.9	06.5	05.8	90	46	68	68	SSE 2	- 0	E 3
27	711.7	711.5	714.4	02.2	14.4	08.1	08.2	14.6	01.2	-	05.0	06.1	06.1	93	50	75	73	SE 1	W 1	SSE 2
28	716.1	714.3	713.7	02.9	16.0	07.5	08.5	17.1	02.0	-	05.2	06.4	06.0	92	47	77	72	- 0	- 0	- 0
29	712.5	712.1	714.7	03.4	18.0	09.3	10.0	21.8	02.4	-	04.9	05.4	06.2	85	35	70	63	- 0	WNW 2	SE 1
30	716.7	714.3	714.1	04.6	19.6	09.0	10.6	20.7	03.6	-	05.8	07.4	06.5	91	44	76	70	SE 2	- 0	- 0
31	712.3	711.0	713.0	04.6	22.0	09.6	11.0	22.2	03.6	-	05.1	04.1	05.0	80	21	60	54	S 1	WNW 3	SE 1
MES. VRED.	709.8	709.2	710.0	05.1	14.0	08.0	09.8	15.7	03.4	-	05.7	06.3	06.3	86	56	78	73	0.7	1.0	1.1

SARAJEVO 1970 SEPTEMBAR

BR. ST. 144 H_s = 630 m H_b = 637.0 m h_t = 2.0 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnevni		7	7	
1	7	09●	09	07	08.3	00.7	10.2	.	●0-3, 15^{12}-15^{30}; = n-11, ●a-7
2	6	10●	07⊙	02	07.0	02.1	01.9	.	= n-n, ● 6^{30}-7, 13^{45}-13^{55}
3	7	00⊙	06⊙	10	05.3	10.4	00.0	.	= n-11, △ n-11, 20^{45}-n
4	5	03⊙	10●	10	07.7	01.7	.	.	= n-n, △ n-9, ● 11^{25}-16
5	7	00⊙	06⊙	00	02.0	11.2	06.5	.	= n-11, △ n-12, 20-n
6	7	00⊙	01⊙	06	02.3	11.2	.	.	△ n-10^{30}
7	8	09⊙	04⊙	00	05.0	05.2	.	.	△ n-9
8	7	00≡⊙	00⊙	00	00.0	10.7	.	.	△ n-10^{30} 19^{45}-n; ≡ n-9^{30}, — 9^{30}-12
9	8	00⊙	02⊙	00	00.7	11.4	.	.	△ n-10, 20-n
10	8	00⊙	00⊙	00	00.0	11.5	.	.	△ n-8^{30}, 20^{30}-n
11	5	00⊙	01⊙	00	00.3	11.5	.	.	= 8^{30}-11^{30}
12	8	03⊙	05⊙	03	03.7	04.7	.	.	
13	8	02⊙	04⊙	00	02.0	10.3	.	.	△ 20-n
14	8	08	02⊙	00	03.3	08.2	.	.	
15	8	00⊙	01⊙	00	00.3	11.2	.	.	△ n-8, = n-8
16	7	00⊙	03⊙	01	01.3	11.1	.	.	△ n-9
17	7	10●	10	10	10.0	00.0	00.0	.	● a-11^{50}, 17^{50}-n; = 16-n
18	5	10●	10	10	10.0	00.0	04.2	.	= n-n, ● 0-1^{30}, 4^{20}-6; ● 6-9
19	5	10	09	09	09.3	01.0	00.2	.	= n-n
20	7	08	07⊙	08	07.7	05.5	.	.	= n-11, △ n-10^{30}
21	7	10	04⊙	10	08.0	05.8	.	.	= n-11, △ n-8
22	6	10	09	07	08.7	02.8	.	.	= n-n, △ n-8, ● 8^{55}-9
23	6	06⊙	06⊙	00	04.0	04.8	00.0	.	= n-15^{30} 18-n; △ n-9, 20^{30}-n
24	7	00⊙	01⊙	00	00.3	10.6	.	.	= n-10^{30}, 17^{30} n; △ n-9
25	6	00⊙	00⊙	00	00.0	10.5	.	.	= n-n, △ n-10, 20^{30}-n
26	7	02≡⊙	07⊙	08	05.7	06.2	.	.	≡ n-10, △ n-9, = 18-n
27	7	06⊙	05⊙	00	03.7	04.1	03.7	.	= n-11, 16-n; ● 1^{35}-5^{40}, 10^{40}-10^{55}; △ 20^{30}-n
28	7	10≡	06⊙	10	08.7	04.0	00.0	.	≡ n-8^{50}, △ h-8
29	8	00⊙	00⊙	00	00.0	10.6	.	.	△ n-8, 19-n
30	6	00⊙	00⊙	00	00.0	10.8	.	.	= n-p, ⊔ n-8
MES. VREDN.			04.2	04.6	03.7	04.2	209.8	26.7	

SARAJEVO 1970 OKTOBAR

1	7	07	10	10●	09.0	02.1	.	.	● 14^{45}-19^{20}; = 16^{30}-n; ▽ 19^{30}-n; ⊔ 20^{00}
2	7	10	07⊙	10	09.0	03.5	17.1	.	● 7^{10}-8^{30};
3	4	10	10●	10	10.0	00.0	03.4	.	● n-14^{40}; = n-n, * 14^{20}-15^{30}
4	7	10	06⊙	10●	08.7	02.4	16.2	.	= n-11^{30} 17-n; ● 17^{20}-n
5	8	02	09	10	07.0	06.2	00.5	.	= n-9, ● 19^{05};
6	7	00⊙	00⊙	00	00.0	10.5	00.0	.	= n-8^{45} 13^{30}-n; △ n-8, 19^{45}-n; ≡ 8^{45}-10
7	7	00⊙	00⊙	00	00.0	10.5	.	.	△ n-8^{40} = 18-n
8	7	02⊙	00⊙	00	00.7	10.5	.	.	△ n-9^{30} ≡ 8^{40}-9, = 9-11^{50}
9	7	00⊙	00⊙	00	00.0	00.7	.	.	△ n-9^{30} = 7^{20}-11^{30}; ≡ 8^{30}-9
10	7	00⊙	00⊙	00	00.0	10.3	.	.	△ n-9^{40}, = n-9^{30}, 18-n
11	7	00⊙	00⊙	00	00.0	10.1	.	.	△ n-9
12	7	00⊙	00⊙	01	00.3	09.8	.	.	⊔ n-7^{40} △ n-8, ⊔ 6-7^{10}; ≡ 7^{10}-12^{30}
13	6	08	04⊙	03	05.0	08.1	.	.	△ n-7^{30}, = n-n
14	6	10	00⊙	09	06.3	07.5	.	.	= n-n, △ n-9
15	6	10●	10●	10	10.0	00.0	00.0	.	△ n-6^{40}, = n-n, ● 6^{40}-9^{20}, 11^{40}-17^{40};
16	6	10	10	09	09.7	00.0	05.4	.	= n-n, ● 8-9^{45}
17	6	10	10	10	10.0	00.0	00.1	.	= n-n
18	6	10	10	10	10.0	00.0	.	.	= n-n, ● 9^{20}-11^{40}
19	6	10	00⊙	00	03.3	04.4	01.0	.	= n-n
20	7	00≡⊙	06⊙	07	04.3	08.7	.	.	⊔ n-8^{40}; ≡ n-8^{30}, = 8^{30}-9, 17-n; ∞ 9-9^{30}
21	6	10●	10●	10●	10.0	00.2	00.2	.	= n-n, ● n-14^{30}; 19^{20}-n
22	5	10●	10	10*	10.0	00.0	00.1	.	= n-n, ● n-12^{40}, 14^{45}-17^{40}; * 12^{40}-13^{45}, 17^{40}-19^{30}; * 19^{30}-n
23	5	10*	10	10	10.0	00.0	01.5	.	* n-13^{20} = n-n, ● 19^{30}-20^{15} [illegible]
24	5	10	10*	10	10.0	00.3	00.2	.	● n-10^{40}; = n-n, △ 6^{20}-6^{50}, 15^{40}-19^{30}
25	6	08	10	10	09.3	03.3	01.0	.	= n-n, ⊔ n-8^{45}
26	8	00⊙	06⊙	00	02.0	07.0	.	.	⊔ n-7^{45}; ≡ 7^{55}-9^{30}
27	6	06⊙	06⊙	06	06.0	06.8	.	.	= n-n, ⊔ a-7^{30}
28	5	04⊙	04⊙	00	02.7	07.6	.	.	= n-16^{40} △ n-9^{30} ≡ 7^{45}-8^{50}
29	6	06	08	02	05.3	05.0	.	.	= n-17^{30} △ n-8^{40}
30	6	00⊙	00⊙	00	00.0	03.1	.	.	≡ n-8^{45} △ n-8^{40}
31	7	00⊙	00⊙	00	00.0	09.5	.	.	△ n-7^{50}
MES. VREDN.			05.5	05.4	05.4	05.4	107.9	119.7	

φ = 43° 52' N λ = 18° 26' E Gr. ΔG = + 1h 14 min. BR. ST. 144

DAN	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	712.2	710.4	710.4	03.0	18.5	07.7	09.2	19.9	02.4	-	04.6	05.4	05.2	81	34	66	60	ESE 1	SSE 1	- 0
2	712.2	710.7	710.7	02.3	18.6	08.3	09.4	18.6	01.5	-	04.4	05.1	05.4	81	32	65	59	SE 2	- 0	ESE 2
3	711.6	708.2	707.9	03.8	16.8	09.8	10.0	17.0	03.0	-	05.3	06.5	04.9	88	45	54	62	- 0	S 1	- 0
4	708.7	710.2	711.5	06.0	18.0	09.1	10.6	20.3	04.6	-	04.9	06.6	06.6	70	42	76	63	SE 1	WNW 1	ESE 2
5	711.0	708.1	706.1	03.2	17.2	14.3	12.2	18.4	02.0	-	05.2	06.5	04.5	91	44	37	57	ESE 1	- 0	NW 1
6	705.3	706.4	709.2	10.4	04.2	03.2	05.2	14.4	02.6	-	06.8	05.4	05.2	72	88	91	84	E 1	ESE 5	- 0
7	709.2	708.1	709.2	-00.4	08.8	01.6	02.9	09.8	-00.8	-	04.1	03.5	04.0	93	41	77	70	- 0	E 2	ESE 1
8	708.8	709.6	712.0	02.0	04.0	04.2	03.6	04.8	00.6	-	04.8	05.6	05.8	90	91	94	92	- 0	NW 1	- 0
9	709.1	706.0	704.7	03.7	07.4	08.3	06.9	08.8	02.4	-	05.7	07.1	07.5	95	92	91	93	E 1	- 0	- 0
10	702.7	705.4	707.6	07.4	06.8	02.4	04.8	09.0	02.3	-	07.1	06.0	05.3	92	81	97	90	NE 1	W 1	ESE 2
11	711.2	712.1	712.4	02.0	06.4	01.2	02.7	07.7	00.4	-	05.1	04.0	03.9	97	55	78	77	- 0	S 1	SE 2
12	712.3	710.2	710.8	-01.5	11.0	04.2	04.5	11.4	-02.4	-	03.7	04.7	04.5	89	48	74	70	- 0	- 0	SE 1
13	710.0	708.7	708.3	00.2	16.0	06.5	07.3	16.1	-00.2	-	03.5	05.1	03.4	75	37	47	53	ESE 2	SSE 1	SSE 2
14	706.4	704.4	702.9	11.4	14.0	11.4	12.0	14.4	05.4	-	05.5	07.0	07.8	55	58	78	64	S 4	SSW 2	W 1
15	699.4	699.3	696.2	13.0	15.2	11.2	12.6	17.2	09.6	-	06.6	05.9	06.7	59	46	67	57	WSW 3	S 3	SSE 3
16	696.1	697.1	701.6	04.4	02.9	00.8	02.2	11.2	00.1	-	05.6	05.4	04.7	90	95	97	94	ESE 2	- 0	- 0
17	705.4	705.7	707.2	01.2	07.2	03.3	03.8	07.8	00.6	-	04.7	04.1	04.1	93	54	71	73	- 0	NW 1	- 0
18	708.4	708.7	709.0	02.0	10.0	08.4	07.2	11.4	01.1	-	04.4	05.4	05.6	84	59	68	70	- 0	SSW 3	WNW 1
19	706.9	706.3	706.3	12.0	15.0	13.2	13.4	17.0	07.4	-	06.9	06.0	06.0	66	47	52	55	SSW 1	SSW 4	S 4
20	705.8	706.5	706.0	13.0	15.5	13.4	13.8	18.0	12.4	-	06.0	06.2	06.4	53	47	56	52	S 4	S 2	SSW 2
21	706.2	704.6	701.6	10.0	15.4	13.2	13.0	16.8	08.4	-	07.7	06.5	07.2	83	50	63	65	E 3	S 3	S 3
22	699.3	699.4	702.4	06.7	08.4	04.4	06.0	13.2	03.8	-	06.5	05.4	05.7	88	66	91	82	- 0	SSW 1	- 0
23	705.8	706.7	709.0	03.0	03.6	03.2	03.2	04.7	02.3	-	05.3	05.4	05.1	94	91	89	91	NE 1	WNW 1	- 0
24	711.2	712.4	712.6	04.0	04.8	03.1	03.8	05.4	02.6	-	05.4	05.5	05.2	88	85	91	88	- 0	- 0	- 0
25	713.3	714.3	714.7	00.2	04.0	03.0	02.6	04.2	-00.5	-	04.5	05.2	05.1	96	85	91	91	E 1	NE 1	- 0
26	714.9	716.4	716.5	-00.1	05.2	00.0	01.3	05.4	-01.5	-	04.1	04.6	04.3	91	69	93	84	- 0	- 0	- 0
27	716.3	715.4	716.1	-02.8	00.0	-00.8	-01.1	00.2	-03.5	-	03.6	04.4	04.1	97	96	94	96	- 0	- 0	- 0
28	714.5	712.3	712.0	-02.1	00.0	-00.5	-00.8	00.2	-02.6	-	03.8	04.1	04.2	96	89	94	93	- 0	- 0	- 0
29	710.6	709.0	709.8	-02.1	05.4	03.8	02.7	07.9	-03.3	-	03.7	04.7	04.5	94	69	75	79	- 0	- 0	- 0
30	708.8	707.6	707.8	05.0	11.8	11.5	10.0	13.0	02.4	-	04.9	05.7	05.3	74	55	52	60	- 0	SW 1	S 1
MES. VRED.	708.4	708.0	708.4	04.0	09.7	06.1	06.5	11.5	02.1	-	05.1	05.4	05.3	84	63	76	74	1.0	1.2	1.0

1	707.9	707.0	707.9	09.0	12.6	08.1	09.4	12.9	07.1	-	08.0	07.5	07.0	93	68	86	82	E 1	- 0	ESE 1
2	707.0	707.3	709.1	04.0	11.4	06.6	07.2	12.2	03.2	-	05.6	06.3	05.8	91	63	80	78	ESE 2	SW 1	ESE 1
3	708.9	707.5	704.1	03.6	11.2	05.7	06.6	12.0	03.0	-	04.7	04.4	04.6	79	44	67	63	ESE 2	SW 1	WNW 1
4	708.8	710.8	712.3	03.6	06.0	00.2	02.5	07.6	-00.7	-	05.4	02.1	02.3	91	30	50	57	- 0	NNW 2	- 0
5	713.0	712.0	712.4	-04.0	04.2	02.4	01.2	05.4	-05.0	-	02.9	03.2	03.4	84	51	62	66	- 0	WNW 1	- 0
6	715.4	715.7	715.0	00.4	02.0	00.6	00.9	02.6	-00.6	-	04.4	04.8	04.5	93	90	93	92	- 0	- 0	- 0
7	714.8	712.3	714.6	-04.6	-01.3	-01.8	-02.4	00.6	-05.2	-	03.0	03.7	03.6	91	90	91	91	E 1	- 0	- 0
8	715.0	716.5	720.1	-03.4	00.2	00.5	-00.6	00.5	-03.9	-	03.3	04.1	04.3	93	88	91	91	- 0	- 0	- 0
9	721.2	720.2	718.7	-00.4	00.2	-00.8	-00.4	00.8	-01.5	-	04.1	04.0	04.0	93	86	92	90	ESE 1	- 0	- 0
10	716.2	718.3	717.1	-02.1	01.4	-01.9	-01.1	02.2	-02.4	-	03.5	03.9	03.5	88	77	87	84	WSW 1	- 0	- 0
11	718.5	719.0	720.2	-01.6	-01.0	-00.6	-01.0	-00.6	-02.8	-	03.8	03.8	04.0	92	89	91	91	WNW 1	- 0	- 0
12	719.3	718.0	717.3	-03.8	-01.8	-02.4	-02.6	-00.6	-04.5	-	03.1	03.6	03.7	88	91	96	92	SE 1	SW 1	- 0
13	716.5	714.7	715.6	-04.2	-02.8	-03.8	-03.6	-02.2	-05.0	-	03.2	03.5	03.3	96	93	96	95	S 1	- 0	- 0
14	715.0	713.3	712.7	-05.1	-03.0	-04.0	-04.0	-01.9	-05.9	-	02.9	03.3	03.3	93	89	96	93	- 0	- 0	- 0
15	712.4	712.8	714.5	-04.8	-04.0	-02.9	-03.6	-02.7	-05.4	-	02.9	03.0	03.4	91	88	91	90	SSW 1	W 1	- 0
16	714.7	714.7	715.6	-02.0	01.2	-01.6	-01.0	01.8	-03.2	-	03.6	02.8	03.0	90	57	75	74	- 0	ESE 1	- 0
17	715.6	715.0	713.5	-02.0	-00.6	-03.0	-02.2	-00.6	-03.7	-	03.3	03.3	02.9	83	74	78	78	NNW 1	WSW 1	- 0
18	711.5	711.0	712.5	-07.8	-00.6	-04.0	-04.1	-00.1	-08.5	-	02.1	03.3	03.0	83	74	88	82	ESE 1	WNW 1	- 0
19	713.4	712.5	714.1	-03.8	-00.4	-01.4	-01.8	00.1	-04.4	-	02.9	03.3	03.3	84	75	81	80	- 0	- 0	- 0
20	714.9	713.2	712.9	-06.0	00.8	-05.2	-03.9	00.8	-06.6	-	02.5	03.3	02.8	85	68	88	80	E 1	- 0	- 0
21	710.2	707.1	705.6	-07.1	-05.3	-06.8	-06.5	-04.9	-08.2	-	02.4	02.9	02.6	91	93	94	93	- 0	SW 1	- 0
22	704.5	704.0	703.9	-05.8	-03.6	-03.8	-04.2	-01.3	-08.2	-	02.8	03.1	03.2	94	88	92	91	- 0	- 0	WNW 1
23	700.0	697.1	698.2	-04.2	-02.3	-04.9	-04.2	-02.5	-05.2	-	03.2	03.3	02.9	96	89	91	92	NW 1	WNW 1	- 0
24	701.5	703.5	704.5	-05.2	-00.2	-01.2	-03.0	-00.2	-06.6	-	02.8	03.6	03.2	91	79	89	86	- 0	- 0	- 0
25	700.1	705.7	701.1	-03.8	-03.0	-05.2	-04.3	-00.1	-05.7	-	03.2	03.4	02.8	92	93	88	91	- 0	NW 1	- 0
26	703.0	705.9	708.3	-06.2	01.0	-04.2	-03.4	02.3	-06.8	-	02.6	02.9	02.8	90	60	84	78	- 0	- 0	SE 2
27	707.0	705.0	704.3	-02.4	07.0	04.6	03.4	07.4	-07.9	-	03.2	05.2	05.5	82	69	87	79	SE 3	SE 1	SE 2
28	699.1	699.1	702.1	07.4	07.0	07.0	07.1	12.0	03.7	-	05.3	06.7	03.9	69	89	51	70	S 2	NNE 1	NW 1
29	702.1	699.8	697.7	08.0	11.4	11.8	10.8	12.0	04.0	-	04.5	04.5	06.8	56	55	65	59	SE 1	S 1	NE 1
30	693.1	692.0	696.9	12.9	13.1	07.4	10.2	14.2	05.8	-	06.0	06.3	04.6	54	56	59	56	S 3	SE 3	NW 1
31	697.6	693.7	689.3	08.3	10.0	11.6	10.4	11.6	05.0	-	04.1	05.3	05.0	50	58	49	52	WNW 2	SW 1	SSE 4
MES. VRED.	709.7	709.2	709.4	-01.1	02.3	00.2	00.4	03.2	-02.8	-	03.7	04.0	03.8	85	75	82	80	0.9	0.0	0.5

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H_s = 630 m H_b = 637.0 m h_t = 2.0 m h_r = 1.0 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj časi	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	7	00⊙	04⊙	00	01.3	09.0	•	•	△ n-8^15, 20^30 n
2	6	07⊙	01⊙	00	02.7	08.2	•	•	△ n-8, = n-pp
3	6	06	09	00	05.0	03.7	•	•	△ n-8^20 = n-n
4	7	00	06⊙	00	02.0	07.6	•	•	△ n-8^40
5	6	00	06⊙	09	05.0	07.8	•	•	△ n-8^50, = n-n
6	6	09	10●	10	09.7	00.0	•	•	= n-n, ● 8^40- 17^50 i
7	7	00	04⊙	01	01.7	08.5	03.0	•	= n-n, ⌣ n-9^15
8	5	10●	10●	10	10.0	00.0	09.6	•	= n-n, ● n-19^40 i
9	3	10●	10≡	04≡	08.0	00.0	03.0	•	= n-8, ● 5^50- 10^30 13^45- 18^40 i
10	6	10●	10	00	06.7	00.1	08.6	•	= n-pp, ● n-12^40
11	6	10	07⊙	00	05.7	01.7	07.[illegible]	•	= n-pp
12	5	00≡	03⊙	00	00.0	06.9	•	•	⌣ n-10^45, ≡ n-8^30, = 8^30- pp
13	5	00	04⊙	08	04.0	08.0	•	•	⌣ n-8^20 = n-pp
14	4	09	07⊙	09	08.3	01.3	•	•	● 16^05 19^15- n, ≤ sw 20^55- n
15	8	10	06●	07●	03.3	04.6	04.[illegible]	•	● 12^40- 14^20 ni, F 20^05
16	3	10●	10●	10≡	10.0	00.0	12.[illegible]	•	● n-9^30 11^45- 16^55, * 8^30- 14^20, = 9^30- 13, * 10-11^40 16^55- n, ≡ 13-n
17	6	08	06⊙	04	07.7	05.2	21.0	•	= n-n
18	7	07	09	03	06.3	01.5	•	•	= n-n
19	5	09	07⊙	07	07.7	03.5	•	•	F 2^55- 3^45, ● 13^20- 15^20
20	3	04	10●	04	06.0	04.4	•	•	
21	8	04	10	09	07.7	03.5	00.5	•	● 15^40- ni, F s 23^40
22	8	04	06⊙	10	06.7	03.4	06.2	•	F w 4^20 ● 9^45- 10^45 17^20 n, * 10^45- 12^20
23	6	10●	10●	10●	10.0	00.0	03.5	•	● n- 16^30 i, = n-n, ● pn, p-ni
24	5	10	10	03	07.7	00.0	02.4	•	= n-n
25	5	06	09	09	06.0	00.0	•	•	= n-n, ⌣ n-8^20
26	5	10	04⊙	00	04.7	02.2	•	•	= n-n, ⌣ n-8^15
27	3	00≡	09≡	10≡	06.3	00.0	•	•	⌣ n-12^50 ≡ n-16, ≡ 16-n
28	5	10	10	10≡	10.0	00.0	•	•	⌣ n-8^20 = n-17^30 = 17^30-n
29	6	10≡	00⊙	00	03.3	03.9	•	•	⌣ n-9^15, ≡ n-10^20, = 10^50-n
30	8	08	10	03	07.0	00.0	•	•	
MES. VREDN.		06.4	07.1	05.2	06.2	36.5	73.7		

1	7	10●	09	10	09.3	00.4	02.[illegible]	•	● n-7^40, 16-17^50, = n-10^20
2	7	04	04⊙	03	03.3	05.3	06.5	•	
3	8	00	04⊙	04	02.7	07.2	•	•	
4	8	08	04⊙	00	04.0	07.2	01.7	•	● n, = n-8^45 * 8^45- 8^40
5	7	02	08	10	06.7	05.6	00.0	00	⌣ n-9^15, = 15^20- n
6	5	10	10	02	07.3	00.0	05.6	02	= n-n, * n, 10^40 12; ● 9^40- 10^05, * 10^05- 10^40, △ 14^20- 16^30, ⊠
7	2	00≡	10≡	10≡	06.7	02.1	00.3	01	≡ a- 13^40, ≡ 9^40- ni, ⊠
8	2	10≡	10≡	10*≡	10.0	00.0	•	01	≡ a-ni, ≡ 7^30- 8, * 13^30- 13^40, ● 13^40- 13^50, △ 13^50- 14^40, * 17^40- n, ⊠
9	6	10	09	10≡	09.7	00.0	01.4	02	≡ n- 20^15, ≡ 20^45- n, ⊠
10	6	10	09	03	07.3	00.0	•	•	= n-n, △ 9^40- 11^20, ⌣ 19^45- n
11	5	10	10	10	10.0	00.0	00.0	•	= n-n
12	5	10	10	10≡	10.0	00.0	•	•	= n-16^30, ≡ 16^30- n
13	3	10≡	10≡	10≡	10.0	00.0	•	•	= n-n
14	3	10≡	10≡	10≡	10.0	00.0	•	•	≡ n-n
15	2	10≡	10≡	10≡	10.0	00.0	•	•	≡ n-n, V n-n, * 14^30- 18^30 i
16	6	10	09	07	08.7	01.8	00.[illegible]	00	= n-n
17	6	10*	10*	02	07.3	00.0	00.0	00	= n-n, * n- 14^40
18	6	00	00⊙	05	02.7	06.0	09.1	00	= n-n
19	6	10	08	10	09.3	00.3	•	•	= n-n
20	6	00	09⊙	00	00.0	05.7	•	•	= n-n, ⌣ n-10^40
21	3	10≡	10≡	10≡	10.0	00.0	•	•	≡ n-n, ⌣ n-n, * 12^30- 13^30
22	3	10*≡	10*≡	10*	10.0	00.0	00.	01	≡ n-15^30, * n-ni ⊠
23	5	10*	10*	10*	10.0	00.0	07.[illegible]	11	* n-n, ≡ n-n, ⊠
24	5	10*	07	08≡	08.3	00.0	09.5	20	* n-16^55 i, = n- 16^30 ≡ 16^30- n, ⊠
25	5	10*	10*	10	10.0	03.0	00.0	19	= n-n, * h-8, 11^05- 19^50 i, ▽ 12^50- 15^25 i, ⊠
26	6	10	04⊙	00	04.7	03.9	10.0	24	= n-20^20 ⊠
27	6	06	09*	10●	08.3	00.6	•	29	= n- 14^30, ● 9^40- 14^45 17^40- ni, ⊠
28	7	10●	10*	09	09.7	01.2	04.6	16	● n-8^40 i, 10^45- 15, ⌣ n- 11, F s 1^30- 4^50 i, ⊠
29	7	08	10*	10●	09.3	00.6	03.5	•	● 10^20- ni, F s 23^35, ⊠
30	6	10	09	02	07.0	00.0	01.7	•	F 0^45- 1^50, 7^40- 9^30, 16^40- 21^40, ● 8^20- 17 i, ∩ 8^45- 8^40
31	8	07	10	10	09.0	00.0	01.7	•	● 14^30- 15
MES. VREDN.		07.9	06.1	07.5	07.4	49.7	09.3		

$\varphi = 44^{\circ}\ 48'$ N $\lambda = 20^{\circ}\ 28'$ E Gr. $\Delta t =$ + 1h 22 min. BR. ST. 174

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred. Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	738.1	737.1	738.3	-00.5	01.8	00.3	00.5	01.9	-02.6	-03.2	03.5	03.8	04.3	78	74	91	81	SE 5	- 0	WNW 1
2	741.1	743.3	746.4	-02.2	-01.2	-01.8	-01.7	00.3	-02.5	-02.6	03.6	03.5	03.1	92	82	76	83	W 1	WNW 2	WNW 2
3	747.4	747.2	747.8	-04.3	04.2	02.5	01.2	04.9	-05.7	-09.8	02.5	03.8	03.8	75	61	68	68	SE 2	S 2	SSE 2
4	748.0	746.6	744.9	02.6	05.0	05.1	04.4	06.6	01.6	-01.8	04.1	04.3	04.4	75	66	66	69	SSE 2	SSE 3	SSE 3
5	740.0	737.8	737.9	06.3	08.3	10.1	08.7	10.2	04.5	-00.9	05.1	06.1	06.6	72	74	71	72	SE 4	SSE 4	SSE 5
6	738.3	742.7	745.4	10.0	03.6	02.0	04.6	12.4	01.9	04.6	06.6	04.8	04.5	68	82	85	78	SSE 4	WNW 3	- 0
7	742.9	744.2	750.4	01.4	00.9	00.0	00.6	02.0	-00.1	00.9	04.7	04.7	04.4	93	97	96	95	ENE 2	W 3	WNW 3
8	755.3	757.7	760.2	-00.6	00.2	-03.2	-01.7	00.5	-03.2	-01.1	03.9	03.4	03.1	89	74	85	83	WNW 3	WNW 3	WNW 1
9	760.1	759.7	760.5	-04.9	-01.2	-02.2	-02.6	-00.5	-06.1	-09.5	02.9	03.0	03.4	91	72	86	83	- 0	NE 1	NE 1
10	759.3	756.0	754.5	-03.0	02.2	00.5	00.0	02.6	-03.8	-07.1	03.3	03.7	03.5	89	69	74	77	ESE 2	SE 4	SE 4
11	752.6	750.1	748.8	00.6	04.1	01.8	02.1	04.6	00.3	-00.8	03.5	03.7	03.3	72	61	63	65	SE 5	SE 4	SE 5
12	745.4	742.7	742.8	02.8	06.2	05.3	04.9	07.2	01.4	00.1	04.1	04.8	05.7	73	68	86	76	SE 4	SE 4	SE 3
13	741.8	741.2	742.4	04.0	10.6	04.9	06.1	11.1	03.1	02.2	04.6	06.5	04.8	76	68	74	73	SE 4	SE 3	SE 3
14	743.4	743.1	744.2	02.5	09.2	07.2	06.5	10.5	01.4	01.6	05.3	06.6	07.0	97	76	92	88	- 0	WNW 1	- 0
15	744.7	743.3	743.6	05.2	14.1	11.4	10.5	15.1	04.0	-00.6	06.1	07.4	07.5	91	61	74	75	SE 2	ESE 2	S 3
16	741.9	739.0	738.0	10.5	12.1	07.5	09.4	12.3	07.5	06.8	06.8	08.2	06.7	71	77	86	78	SE 3	SE 4	W 1
17	740.9	742.6	744.6	02.2	02.6	00.6	01.5	07.5	00.6	01.8	05.2	04.8	03.7	97	87	77	87	WNW 3	WNW 3	WNW 2
18	749.1	751.3	752.0	-03.6	-04.6	-05.0	-04.5	00.6	-05.0	-04.2	02.8	02.4	02.8	78	75	89	81	NW 3	NNW 3	NNW 2
19	754.0	754.7	756.6	-06.2	-04.9	-05.0	-05.3	-04.6	-06.3	-06.8	02.4	02.8	02.8	85	89	89	86	NW 2	WNW 2	NW 2
20	758.3	758.1	758.0	-05.9	-04.4	-04.8	-05.0	-04.2	-07.1	-10.4	02.5	02.5	02.7	83	75	83	80	NW 2	WNW 2	WSW 1
21	756.9	755.8	755.8	-04.8	-02.8	-05.9	-04.8	-02.6	-06.0	-10.5	02.6	02.8	02.5	81	74	88	79	SE 1	SE 1	ESE 2
22	755.6	755.4	755.6	-06.4	-03.3	-03.2	-04.0	-03.0	-09.0	-12.6	02.5	02.8	02.9	89	79	79	82	- 0	N 1	WNW 1
23	755.8	755.8	756.3	-03.4	-01.7	-02.2	-02.4	-01.6	-04.0	-07.2	03.0	03.0	03.2	85	75	81	80	NNE 2	WNW 2	SE 1
24	756.5	756.0	755.5	-02.7	00.0	-03.2	-02.3	00.3	-03.4	-03.2	02.9	03.1	02.9	78	68	81	76	SE 2	ESE 2	SSE 2
25	753.6	754.7	756.4	-01.2	00.4	-00.2	-00.3	00.5	-03.9	-06.4	03.3	04.3	04.4	79	91	96	89	SE 3	SSE 2	W 2
26	757.1	757.5	757.2	-00.4	00.6	01.5	00.8	01.6	-00.8	-01.0	04.4	04.6	04.8	98	97	93	96	SSE 2	S 2	SE 2
27	756.7	754.9	753.0	02.9	07.6	07.2	06.2	08.1	01.1	00.2	04.4	05.0	05.1	78	65	66	70	- 0	SSE 2	SSE 2
28	753.1	753.0	752.5	04.8	03.7	02.7	03.5	07.5	02.5	03.2	05.3	05.6	05.1	83	94	92	90	NNE 2	WSW 2	WNW 2
29	752.1	751.6	752.4	00.0	02.3	-00.2	00.5	02.8	-00.4	-01.4	04.1	03.3	03.9	89	60	85	78	WNW 2	NNW 3	W 2
30	749.8	748.0	746.5	-01.8	04.5	01.2	01.3	05.0	-02.7	-06.8	03.5	03.9	03.4	87	61	68	72	SSE 1	ESE 2	SE 3
31	745.2	746.1	748.5	-00.9	-00.5	-02.0	-01.3	01.2	-02.0	-01.4	03.6	03.5	03.7	85	80	92	86	SE 5	ESE 4	ESE 4
MES. VRED.	749.5	749.3	749.9	00.1	02.6	01.1	01.2	03.9	-01.4	-02.8	04.0	04.3	04.2	83	75	82	80	2.4	2.4	2.2

1970 FEBRUAR BEOGRAD

1	750.1	749.2	749.5	-02.5	-01.6	-03.0	-02.5	-01.3	-03.0	-02.2	03.6	03.9	03.4	96	94	93	94	NNE 2	NE 2	SE 2
2	750.9	751.0	750.5	-04.8	-02.8	-05.3	-04.5	-02.3	-05.3	-04.9	03.0	03.3	02.7	93	88	88	90	SE 2	SSE 2	SE 1
3	744.6	740.7	742.4	-05.4	03.5	03.0	01.0	04.1	-06.5	-11.7	02.7	04.8	05.5	88	82	97	89	SE 2	SSE 3	SE 2
4	747.3	745.8	744.4	01.3	08.6	08.6	06.8	09.1	01.3	-03.4	04.6	04.0	05.3	91	47	63	67	SSE 1	SSE 3	SSE 2
5	743.1	742.4	742.7	08.2	17.2	12.3	12.5	18.3	05.8	-00.1	05.6	06.6	05.9	69	45	55	56	SSE 2	S 2	SSE 2
6	744.4	745.8	748.2	10.8	12.4	11.2	11.4	13.4	08.7	05.0	05.7	07.3	05.6	59	68	56	61	WNW 2	SSE 1	WSW 2
7	750.4	750.2	750.4	00.6	02.4	02.5	02.0	11.2	00.5	00.0	04.6	05.1	05.2	97	94	95	95	NNE 2	NNE 1	SE 2
8	748.1	746.9	747.2	00.6	12.3	07.6	07.0	14.0	00.0	-03.2	04.7	05.6	05.7	98	52	73	74	SE 1	WSW 2	NNW 1
9	746.5	743.8	743.2	03.8	16.8	13.0	12.9	17.2	04.5	-01.7	04.3	05.0	05.2	50	35	47	44	SSW 2	S 3	SW 2
10	739.5	735.6	741.4	11.0	14.3	02.0	07.3	15.9	02.0	05.9	05.3	06.2	04.9	54	50	93	66	S 2	SSW 1	WSW 3
11	742.4	740.7	737.3	01.7	10.9	05.8	06.0	12.1	01.4	-01.6	04.8	03.2	06.0	92	33	86	70	SSE 2	SSW 1	NE 2
12	744.8	748.6	749.2	00.4	02.0	-00.2	00.5	05.8	-00.4	-00.1	04.0	04.2	03.7	86	80	82	83	NW 3	WNW 3	SSE 2
13	745.3	742.1	743.2	02.2	05.6	04.3	04.1	07.6	-01.0	-05.6	03.6	04.2	05.5	68	62	88	73	SE 2	SE 4	N 2
14	746.0	746.2	740.1	03.2	06.4	06.5	05.6	07.3	02.2	00.5	05.6	05.7	05.8	97	80	80	86	NNW 2	SE 3	ESE 4
15	736.9	736.8	739.8	06.0	11.0	01.4	05.0	13.2	01.3	00.2	05.5	05.4	04.7	78	55	93	75	SE 3	W 2	NW 3
16	744.6	747.2	746.9	-04.4	-03.5	-03.5	-03.7	01.4	-04.4	-04.5	03.0	03.2	03.2	92	91	91	91	NW 2	NW 2	NNW 2
17	748.2	751.2	753.6	-05.0	-02.2	-04.2	-03.9	-01.3	-05.1	-05.4	02.8	02.7	02.8	89	68	83	80	WNW 2	NW 2	WNW 3
18	752.5	750.4	750.3	-05.1	02.4	00.8	-00.3	03.3	-05.9	-10.2	02.5	02.8	02.7	80	51	56	62	SSE 2	SE 3	SSE 2
19	752.1	754.6	756.3	-03.0	00.0	-01.4	-01.4	00.8	-03.2	-03.4	03.4	03.9	03.8	91	86	91	89	E 3	WNW 2	W 2
20	756.6	755.7	752.4	-01.9	01.7	-02.1	-01.1	02.7	-02.1	-03.2	03.7	03.5	03.3	92	67	83	81	W 1	W 2	SE 2
21	751.4	752.6	751.0	-03.4	00.0	-01.6	-01.6	01.0	-03.4	-04.4	03.0	03.6	03.5	85	78	85	83	SSE 3	W 2	SSE 2
22	747.5	746.1	745.5	-02.0	04.8	05.4	03.4	05.5	-02.9	-05.4	03.1	03.9	04.1	77	60	61	66	SE 2	SE 2	SSW 2
23	741.4	741.0	742.8	05.6	05.6	04.6	05.1	07.8	04.0	01.8	04.4	06.5	06.0	64	96	94	85	S 1	SSW 2	NW 1
24	744.0	744.0	745.0	01.3	03.9	00.8	01.7	04.7	00.3	-02.8	04.5	04.1	04.3	90	67	88	82	W 1	N 2	NNE 2
25	745.8	745.1	745.0	00.1	02.8	00.6	01.0	02.9	-00.5	-00.8	03.6	03.5	03.8	77	63	79	73	NNW 2	WNW 2	WNW 1
26	743.7	744.2	745.2	-00.6	00.0	-00.3	-00.3	00.8	-01.0	-02.1	04.0	03.8	03.9	91	84	87	87	W 3	WNW 2	W 2
27	745.0	744.8	745.9	-02.4	-01.6	-01.9	-01.9	-00.2	-02.5	-03.8	02.9	03.0	03.2	75	73	81	76	WNW 2	N 1	W 2
28	746.2	747.4	749.7	-01.4	00.2	-01.2	-00.9	00.5	-02.0	-02.2	03.9	03.5	03.4	93	75	81	83	WNW 2	NNW 2	NW 2
MES. VRED.	746.4	746.1	746.4	00.7	04.8	02.3	02.5	06.2	-00.6	-02.5	04.0	04.4	04.4	82	69	80	77	2.0	2.1	2.0

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H_s = 132 m H_b = 131.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vlažnost 0-9		Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednja Dnev			7	7	
1	7	09	10●	10✱	09.7	00.0	00.6	29		F_{SE} 0-^{a20} ● ^{0}11^{45}-18^{30} i, ✱^{0}18^{30}-19^{45} i, ✱^{0}19^{45}-22^{45} i, ⊠
2	6	10	10	10	10.0	00.0	11.5	27		= ^{1}4^{45}-23^{15}, ✱^{0}16^{45}-17^{30}, ⊠
3	7	01	00⊙	10	07.7	07.3	00.0	22		⊠
4	3	09	09	09	09.0	01.5	•	22		F_{SE} 23^{28} ⊠
5	6	10	09	09	09.0	00.0	•	20		● ^{0}11^{30}-12^{30} i, F_{SSE} 4^{20}-20^{45}, ⊠
6	6	10	10	10	10.0	00.0	00.3	07		= ^{0}9-24, ⊠
7	3	10●	10●	10✱	10.0	00.0	00.0	02		= $^{0-2}$0-24 i, ● $^{0-1}$6^{35}-9^{45} 14^{30}-17^{30}, ● ^{0}9^{45}-14^{30} i, = ^{0}13^{45}-14^{30}, ✱ ^{0}17^{30}-19^{30} i, ✱^{0}19^{30}
8	7	10	09⊙	09	09.3	05.0	12.6	01		✱^{0}0-2^{45} = $^{0-1}$0-8^{30} 18^{45}-24 i, ⌣ ^{0}19^{45}-24, ⊠ [-24, ⊠
9	5	04	09⊙	07	06.7	00.2	•	01		⌣ ^{0}0-18^{30} 23^{45}-24 i, = $^{0-2}$0-24, ⊠
10	5	06	09	03	07.7	00.2	•	01		= ^{1}0-19^{45}, ⌣ ^{0}0-9^{45}, F_{SE} 13^{40}-21^{30}, F_{SE} 21^{40}-24, ⊠
11	7	09	06⊙	09	05.0	01.8	•	•		F_{SE} 0-6^{30} 13-13^{30}, F_{SE} 6^{30}-24 i, ● ^{0}11^{45}-12^{05}
12	7	05	10	10●	09.3	00.0	00.1	•		F_{SE} 0-24 i, ● ^{0}11^{45}-12^{45} i, 15^{45}-21^{45}
13	5	03	08	00	03.7	04.5	01.7	•		F_{SE} 0-13^{30}
14	6	10	07⊙	07	08.0	03.7	00.9	•		● ^{0}2^{45}-6^{15} i, 17^{45}-17^{50} = $^{0-1}$5^{30}-24
15	6	01	10⊙	10●	07.0	04.5	00.0	•		= $^{0-1}$0-3^{30}, △ $^{0-1}$2^{45}-5^{15}, ⌣ ^{0}5^{30}-7^{30}, ● ^{0}18^{30}-21^{30} i
16	8	09	10●	10	09.7	00.1	00.5	•		● ^{0}6^{55}-14^{30} 17^{50}-19^{45}, F_{SE} 12^{40}-17^{50} i, = $^{0-2}$22^{45}-23^{15}, = ^{0}23^{15}-24
17	5	10●	10	10	10.0	00.0	01.3	•		= ^{0}0-4^{15} ● ^{0}4^{45}-6^{45}, = ^{2}4^{15}-24, ● $^{0-1}$6^{15}-15^{45} i, $F_{NNW-NNW}$ 8^{20}, 23-23^{49}, ✱^{0}19^{05}
18	6	10✱	10✱	10✱	10.0	00.0	00.4	•		= ^{0}0-24, F_{NNW} 0^{55}-9^{47}, ✱^{0}2^{30}-24 i, ⊠
19	6	10✱	10✱	10	10.0	00.0	04.9	08		✱ ^{0}0-19^{45} i, = ^{0}19^{45}-23, ⊠
20	6	10	09	10	09.7	00.0	00.9	08		= ^{0}3-19^{45}, ✱^{0}8^{45}-13^{45} i, ⊠
21	6	10	10	09	09.7	00.0	00.0	06		= ^{0}6^{30}-18^{45} ⊠
22	5	10	10	10	10.0	00.0	•	04		⌣ ^{0}1^{30}-7 i, = ^{0}5^{30}-7, 9^{45}-18^{30}, = ^{0}7-9^{45}, V ^{0}7-10^{30}, ⊠
23	5	10	10	10	10.0	00.0	•	04		⌣ $^{0-1}$5^{30}-24 i, ✱^{0}9^{05}-9^{30}, ⊠
24	6	10	01⊙	01	04.0	02.9	00.0	04		= ^{0}0-20^{30} ⊠
25	5	10	10	10≡	10.0	00.0	•	04		= ^{0}6^{30}-18^{30}, ✱$^{0-1}$17^{30}-12^{15} i, ✱^{0}12^{15}-13, = ^{0}18^{30}-20, = ^{1}20-24, ⊠
26	5	10	10	09	09.7	00.0	01.2	04		= ^{1}0-1^{15} = $^{1-2}$1^{15}-23 i, = ^{0}18^{15}-20^{15}, ⊠
27	8	10	10	10	10.0	00.0	00.0	01		● ^{0}3^{30}-4^{40}, 22^{40}-24 i, ⊠
28	6	10●	10●	10	10.0	00.0	01.1	•		● ^{0}0-15^{00} = ^{0}15^{30}-19^{30}
29	7	10	08	00	06.0	04.2	04.5	01		✱^{0}3^{45}-4^{30} ✱$^{0-1}$4^{30}-6, = $^{0-1}$6-13^{30}, F_{NNW} 12^{09}, ⌣ ^{0}19^{45}-24, ⊠
30	7	02	00⊙	03	01.7	06.3	•	•		⌣ ^{1}0-10^{15}, F_{SE} 22^{20}-24
31	5	10	10✱	10✱	10.0	00.0	00.3	•		F_{SE} 0-20^{34}, ∿ ^{0}0^{45}-0^{30}, 4^{45}-6^{30}, ✱^{0}13^{15}-24, ⊠
MES. VREDN.		08.3	08.2	07.5	08.0	42.3	46.8			

BEOGRAD

1970 FEBRUAR

1	3	10✱	10✱	10✱	10.0	00.0	07.9	10	✱^{0}0-24, ⊠
2	5	10✱	10✱	06	08.7	00.0	05.6	10	✱^{0}0-16^{15} i, = $^{0-1}$16^{45}-24, ⊠
3	6	02	10	10	07.3	00.0	00.7	10	= ^{0}0-20^{15}, ✱^{0}11^{15}-12^{05}, ● ^{0}14^{15}-24 i, ⊠
4	6	04	03⊙	04	03.7	04.3	16.5	09	● ^{0}0-0^{40}, ⊠
5	8	07	06⊙	07	06.7	04.3	•	02	⊠
6	8	09●	10	07	09.7	00.0	00.0	•	● ^{0}6^{15}-9^{45} i,
7	8	10✱	10	10	10.0	00.0	04.5	03	✱^{0}5^{15}-6^{05}, ✱ ^{1}6^{05}-6^{55}, ✱$^{0-2}$6^{55}-10^{25} i, = $^{1-2}$7^{30}-24, ⊠
8	8	10≡	03⊙	07	06.7	05.1	01.7	•	= $^{0-2}$0-1^{30} 4-10^{15}, = ^{0}12^{30}-9 i, = $^{1-2}$4^{45}-6^{05}, F_{NNE} 19^{50}-21^{15}
9	8	02	02⊙	10	04.7	08.5	•	•	⌣ ^{0}0^{30}-3^{45}
10	8	10	07⊙	10●	09.0	01.6	•	•	● $^{0-1}$7^{45}-9^{15} i, 16^{05}-24 i, F_N 15^{30}-17^{32}, ✱$^{0-1}$17^{35}-18^{05}, ✱^{0}18^{05}-18^{40}
11	5	00	05⊙	10●	05.0	07.1	06.0	•	● ^{0}0-1^{15} 16^{45}-23^{15} i, ⌣ ^{0}4^{30}-8^{30}, F_{NNE} 23^{07}-23^{45}, ✱ 23^{15}-23^{45}, ✱$^{1-2}$23^{45}-24, ⊠
12	6	10	09⊙	09	09.3	03.4	19.2	09	✱$^{1-2}$0-4^{30} = ^{0}9^{45}-15^{15}, ⊠
13	5	10	10	10●	10.0	00.0	00.0	07	△ ^{0}6^{30}-7^{45}, ● ^{0}10^{30}-11^{30} 17^{45}-22^{15}, F_{SE} 13^{50}-18^{50}, ⊠
14	7	10≡	08⊙	03	07.0	01.7	06.3	•	= $^{0-2}$5^{30}-6^{15} 9^{45}-13 i, = $^{0-1}$6^{45}-9^{45}, F_{ESE} 20^{34}-24
15	8	01	10●	10●	07.0	01.9	00.9	•	F_{SE} 0-3^{23}, ● ^{0}2^{30}-4^{45}, 13^{30}-13^{40} i, 16^{30}-21^{30} i
16	5	10✱	10✱	10✱	10.0	00.1	04.0	03	✱^{0}0-21^{30} i, = ^{1}21^{30}-24, ⊠
17	6	10✱	02⊙	00	04.0	04.7	02.1	07	= ^{1}0-21^{45}, ✱^{0}4^{25}-8^{30} i
18	8	02	04⊙	10✱	05.3	00.4	00.0	04	✱^{0}20^{30}-24, ⊠
19	5	10✱	08	10	09.3	00.0	09.5	15	✱$^{0-2}$0-15^{45} i, = ^{0}13^{45}-16^{30}, ⊠
20	6	10	07	00	05.7	03.0	02.4	11	= ^{0}6^{30}-22^{30}, ⊠
21	6	10	10	09	09.3	01.2	•	03	= ^{0}17^{30}-19^{30}, ⊠
22	7	07	05⊙	07●	07.3	00.4	•	07	● ^{0}17^{50}-22^{45} i, ⊠
23	6	03	10	08	08.3	00.0	03.0	01	= ^{0}7^{45}-9^{15}, ● $^{0-1}$9^{45}-16^{15}, ⊠
24	7	05	03⊙	09	07.7	07.3	00.1	•	✱^{0}4^{45}-4^{20}, = ^{0}6^{30}-13^{30} 16^{30}-18^{30}
25	6	10	10	10	10.0	00.0	•	•	= ^{0}4^{30}-24, ✱^{0}9^{15}-10^{45}, ✱^{0}14^{25}-14^{30}
26	5	10	10✱	10	10.0	00.0	00.0	•	= $^{0-1}$0-24, ✱^{0}11^{55}-14^{45} i, 17^{20}-24 i
27	6	10	10✱	10	10.0	00.7	00.4	•	✱^{0}0-2, 8^{45}-9^{45} 12^{45}-15^{45}, = ^{0}0-24
28	6	10	10	10✱	10.0	00.0	00.1	•	= ^{0}0-24, ✱^{0}0^{45}-1, 5^{45}-6, 9^{30} 11^{15}, 14^{45}-24 i
MES. VREDN.		07.6	07.7	07.5	07.6	44.2	46.8		

$\varphi = 44^{\circ}\ 48'$ N $\lambda = 20^{\circ}\ 28'$ E Gr. $\Delta G =$ + 1h 22 min. BR. ST. 174

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	750.2	750.3	750.1	-02.8	-01.7	-02.5	-02.4	-00.5	-02.9	-04.2	03.4	03.2	03.5	91	80	92	88	WNW 2	WNW 2	NW 2
2	748.9	745.7	742.4	-03.6	01.2	-00.8	-01.0	02.6	-04.0	-04.6	03.1	02.6	03.1	89	52	73	71	W 2	SSE 3	SSE 3
3	739.4	738.3	738.9	00.9	06.2	04.4	04.0	07.0	-01.0	-03.0	03.3	03.9	04.0	68	55	64	62	SE 3	SE 5	SSE 5
4	739.4	736.7	730.7	04.1	08.9	05.8	06.2	10.5	04.1	03.2	04.0	04.4	05.0	65	51	72	63	SE 4	SE 6	SE 5
5	733.6	736.5	738.9	07.3	11.6	09.1	09.3	12.4	05.8	04.2	03.8	04.3	05.9	50	42	68	53	S 2	SSE 3	SSW 4
6	745.0	746.0	747.1	04.6	12.0	07.0	07.9	14.1	03.0	-00.8	05.1	03.9	06.3	80	35	84	66	SE 2	ESE 2	SE 2
7	747.0	749.2	753.0	01.8	03.0	00.8	01.6	07.0	00.8	00.6	04.9	04.6	03.2	93	81	66	80	NNW 2	W 3	W 2
8	753.9	752.0	750.9	-02.1	05.6	03.8	02.8	06.4	-02.8	-06.4	03.7	03.8	04.7	94	55	79	76	SSE 2	NE 2	ENE 2
9	749.2	748.4	750.2	03.8	11.2	03.7	05.6	11.4	00.9	-03.1	05.1	05.6	04.5	85	56	76	72	ESE 2	ESE 3	SE 4
10	754.5	756.2	757.5	03.0	08.8	04.5	05.2	09.0	01.9	00.2	04.1	04.4	04.5	72	52	71	65	SE 3	SW 1	SE 3
11	757.4	754.2	751.8	00.9	08.7	04.3	04.6	09.5	00.9	-00.6	03.6	03.8	03.7	74	46	59	60	ESE 3	ESE 3	SE 4
12	746.3	744.5	748.2	02.8	04.6	01.9	02.8	05.7	01.4	01.8	03.7	04.5	04.8	66	71	92	76	SE 5	SE 4	SE 2
13	751.0	752.5	752.5	02.7	07.9	04.4	04.8	09.9	01.8	00.3	04.4	05.2	05.1	79	65	81	75	WSW 2	WNW 2	SE 2
14	749.4	746.5	743.9	04.0	04.6	03.2	03.8	06.2	03.1	00.6	04.6	05.2	05.1	75	82	89	82	ESE 3	ESE 5	ESE 4
15	741.9	742.9	744.5	03.2	03.9	03.8	03.7	04.9	03.2	02.2	05.5	05.5	05.8	95	91	97	94	SE 2	WSW 1	W 3
16	747.6	749.0	749.7	02.8	04.6	03.1	03.4	04.6	02.5	02.2	05.2	04.9	05.1	92	77	89	86	NW 2	NW 2	NNW 2
17	748.5	748.3	748.6	01.2	05.1	03.0	03.1	06.0	01.2	00.4	03.8	03.7	04.2	76	57	74	69	NNE 2	NNW 4	W 2
18	747.8	745.0	742.3	02.6	10.2	06.6	06.5	11.4	01.4	-02.1	04.3	04.5	04.6	78	48	63	63	W 2	SW 2	SE 2
19	741.1	739.4	742.0	05.0	07.1	05.6	05.8	08.6	04.5	03.8	05.9	05.9	06.4	90	78	94	87	SSW 2	ESE 2	WNW 2
20	746.5	749.3	752.3	03.0	08.0	03.8	04.6	09.0	03.0	02.4	04.4	04.0	03.8	78	50	63	64	NW 3	NNW 3	NNW 2
21	753.6	753.4	753.1	01.2	10.6	07.2	06.6	12.7	00.0	-04.6	03.8	04.1	05.0	76	43	65	61	WSW 2	WNW 3	SSW 1
22	752.6	752.2	752.6	06.9	16.6	11.0	11.4	17.6	05.2	-03.1	04.5	04.8	05.4	60	34	55	51	SSE 2	W 2	SSW 2
23	753.4	752.6	752.5	10.0	17.0	13.8	13.6	18.5	07.0	01.8	05.5	05.3	06.6	60	36	56	51	S 2	SSW 2	SSE 2
24	752.4	751.2	750.7	12.0	20.4	14.2	15.2	21.8	11.4	06.4	06.6	06.8	07.3	63	38	60	54	SSE 2	NNW 2	ESE 2
25	752.4	751.2	749.7	12.2	21.6	17.0	17.0	23.5	10.6	04.4	05.4	05.5	07.0	51	28	48	42	SSE 1	WNW 2	S 2
26	748.7	748.2	747.4	15.2	18.2	13.6	15.2	19.4	13.5	08.7	04.6	07.9	09.1	36	50	78	55	S 1	NNE 3	ENE 2
27	744.4	740.9	739.1	10.3	18.5	13.8	14.1	19.2	09.7	06.8	08.5	09.0	09.5	91	56	80	74	SSE 1	WSW 2	NNE 2
28	739.8	741.2	742.4	04.6	03.4	02.2	03.1	13.8	01.8	04.4	05.6	04.9	05.0	88	85	93	89	NNW 3	WNW 2	W 2
29	744.8	745.1	747.7	02.2	08.8	04.2	04.8	09.4	01.5	-00.9	04.8	03.1	03.9	88	37	64	63	WNW 2	W 2	NE 1
30	752.1	751.6	750.6	01.7	12.1	09.0	08.0	13.4	-00.4	-04.9	04.2	02.9	03.2	80	27	38	48	WSW 1	WSW 2	S 2
31	745.0	747.8	745.5	09.7	18.1	13.0	13.4	18.7	06.9	01.2	03.4	03.4	04.3	38	22	38	33	SSW 2	SSE 2	SSW 2
MES. VRED.	747.7	747.3	747.4	04.2	09.6	06.3	06.6	11.1	03.1	00.6	04.6	04.7	05.1	75	54	72	67	2.2	2.6	2.5

1	742.9	740.9	743.8	11.1	17.8	10.4	12.4	19.1	09.6	04.8	05.2	06.4	08.0	52	42	85	60	SSE 2	SSE 3	NNW 2
2	744.3	741.5	739.8	08.8	15.1	11.7	11.8	17.2	08.0	06.6	07.2	07.0	08.0	85	54	78	72	SE 2	SSE 2	WNW 2
3	735.6	740.4	745.1	12.2	04.6	03.4	05.9	12.6	03.2	06.6	07.4	05.2	04.1	70	81	70	74	SSE 2	WNW 4	WNW 2
4	745.9	746.5	747.4	01.6	08.0	05.2	05.0	09.4	00.3	-04.2	03.5	02.1	03.3	69	26	50	48	WSW 1	W 2	NNE 2
5	747.5	746.3	745.6	04.2	13.1	07.6	08.1	14.0	02.5	-03.2	03.1	02.6	02.9	50	23	37	37	SE 2	SSE 3	SE 4
6	745.1	747.6	750.0	06.3	09.6	06.0	07.0	11.8	05.5	03.2	03.5	05.2	05.1	49	58	73	60	SE 3	ESE 2	SSE 1
7	749.7	748.0	746.0	06.4	15.6	12.0	11.5	16.4	04.0	-00.9	04.7	03.8	04.8	65	29	46	47	SSE 2	SSW 2	SSE 2
8	743.4	740.9	738.8	08.6	11.4	13.1	11.6	13.2	08.2	07.4	07.1	08.7	07.8	85	86	69	80	SE 3	SE 4	SSE 4
9	735.5	735.8	742.0	13.4	22.7	13.8	15.9	23.0	12.0	09.8	07.8	08.4	06.9	68	41	58	56	SE 4	S 3	SSW 3
10	746.3	746.7	747.8	10.5	17.6	14.0	14.0	18.0	06.9	01.2	06.5	05.0	06.2	68	33	52	51	SE 1	WNW 1	NE 1
11	747.9	746.8	746.4	10.6	17.5	13.3	13.7	19.0	07.6	02.8	06.6	05.8	06.5	69	39	56	55	- 0	NE 2	NW 2
12	748.3	746.9	746.2	06.2	06.7	07.7	07.1	13.3	06.2	06.2	06.6	06.7	06.7	93	90	85	89	NNW 2	NW 2	W 2
13	748.2	747.4	747.0	06.4	14.6	13.2	11.8	16.7	03.9	00.4	04.5	03.7	05.3	63	30	47	47	WSW 2	SSE 2	- 0
14	746.3	746.5	747.6	09.3	09.0	08.1	08.6	13.2	08.1	08.2	07.5	08.0	07.8	85	92	96	91	SE 2	NW 2	WNW 3
15	753.5	755.0	756.8	03.4	07.1	05.7	05.5	08.6	03.0	02.4	03.9	04.3	04.4	67	56	64	62	NNW 3	NNW 4	NNW 2
16	757.1	756.8	757.6	03.5	09.0	07.4	06.8	09.5	02.3	00.0	04.7	04.4	05.3	80	52	69	67	NNW 3	NNW 3	WNW 2
17	758.2	756.2	754.9	07.1	15.5	10.6	11.0	15.1	05.8	03.4	05.0	05.9	05.8	66	45	61	57	WNW 2	NNW 2	W 1
18	751.6	750.1	749.3	12.4	18.2	16.0	15.6	18.9	10.3	04.3	06.5	08.9	09.7	60	57	71	63	W 1	NW 2	NNE 1
19	750.1	749.6	748.6	12.6	21.4	16.9	17.0	22.2	10.3	06.5	08.9	08.3	09.0	82	43	63	63	- 0	NNE 2	SE 2
20	747.9	747.4	748.2	15.4	26.3	19.3	20.1	27.0	13.4	09.5	08.3	06.8	09.1	64	34	54	51	ESE 3	SSE 2	SE 2
21	751.8	753.3	756.0	18.4	21.8	13.5	16.8	22.2	13.5	10.8	10.0	11.3	07.9	63	58	68	63	- 0	N 2	NW 3
22	760.0	759.4	756.6	10.2	17.1	12.8	13.2	18.3	09.5	06.7	07.2	07.8	08.4	77	54	76	69	NW 2	WNW 2	ENE 1
23	757.0	754.2	752.4	15.4	23.6	17.7	18.6	24.3	10.1	05.3	08.8	07.6	08.8	67	35	58	53	ESE 1	NNW 2	SE 2
24	751.8	750.3	749.6	17.3	25.7	19.0	20.2	26.5	13.5	08.8	09.1	07.4	09.6	61	30	58	50	- 0	WSW 2	N 1
25	751.1	748.4	747.2	14.0	22.2	17.0	17.6	23.2	13.1	11.7	08.9	08.9	09.2	74	44	64	61	WNW 2	NE 2	WNW 2
26	745.4	743.1	742.3	10.1	26.8	21.2	21.8	27.9	11.9	08.2	09.7	08.2	05.4	62	31	29	41	SE 2	SSE 2	SSW 3
27	742.8	747.5	748.8	13.8	17.4	12.7	15.4	21.6	12.6	11.8	06.4	06.9	08.1	39	46	73	53	SSE 3	NNE 3	- 0
28	749.2	748.7	747.8	13.3	16.7	11.7	13.4	19.2	10.3	06.6	07.4	08.2	09.2	65	57	89	70	ESE 2	SSW 2	SSE 2
29	746.4	748.2	748.6	12.1	14.5	08.7	11.0	16.5	08.4	07.0	07.7	06.5	05.8	73	51	68	64	WSW 2	WNW 3	ENE 2
30	748.0	748.8	750.5	09.3	10.0	09.2	09.4	14.7	05.0	02.9	06.6	06.2	04.4	75	68	51	65	SE 2	N 3	NW 3
MES. VRED.	748.3	748.0	748.4	10.6	15.9	12.0	12.6	17.8	08.0	05.2	06.7	06.6	06.8	68	50	64	61	1.9	2.4	2.0

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BR. ST. 174 H_s = 132 m H_b = 131.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	6	10 ✱	10 ✱	10 ✱	10.0	00.0	00.0	1	✱°0-24i, =°0-24, ⊠
2	7	10	01 ⊙	00	02.7	07.6	02.2	.	✱°0-7⁴⁵i, =°0-13¹⁵, ⊠
3	8	10	09	10	09.7	00.0	00.0	.	F SSE 8¹², 12³³, F SE 12⁵⁵ 24
4	7	10	10	04	05.0	01.5	.	.	F ESE-ESE 0-11²⁷, 11¹⁶-24; F SE 1²⁷-11⁴⁶
5	3	04	09	10 ●	07.7	02.5	06.0	.	F SSW 0-23⁵², ●°0⁴⁵-0³⁰, 19³⁰-23⁴⁵
6	5	04 ⊙	04 ⊙	00	02.7	04.8	02.0	.	●¹16³⁰-20⁴⁵i
7	6	10 ●	10	09	09.7	00.2	04.2	.	=°2³⁰-24, ●°3⁴⁵-9¹⁵, ⌣°23-24
8	6	00 ⊙	01 ⊙	00	00.3	08.4	01.1	.	=⁰⁻¹0-15¹⁵, ⌣⁰⁻¹0-8³⁰ 23-24
9	3	08	06 ⊙	00	04.7	06.2	.	.	⌣°0-6¹⁵, F ESE 15³⁵-24
10	5	10	10	09	09.7	00.0	.	.	F SE 0-2¹²⁰
11	7	02	08 ⊙	09	06.3	05.1	.	.	F ESE 0⁴⁰-1⁴⁷ 11⁴⁸-24i
12	7	10	10 ●	10	10.0	00.2	00.0	.	F ESE 0-4, ●⁰⁻¹0³⁰-1¹⁵i, 7¹⁵-8⁴⁵, 13¹⁵-18³⁰i; F ESE 4-15⁵⁵i, △°14⁴⁰-14⁴⁸
13	8	10	06 ⊙	06	07.2	02.8	06.3	.	
14	6	07	10 ●	10 ●	09.0	00.0	.	.	F ESE 9³⁹-23³², ●⁰⁻¹12⁴⁵-24
15	7	10	10	10 ≡	10.0	00.0	00.3	.	●°0-6¹⁵, ●°9¹³⁰-11³⁰, ≡°20³⁰-23³⁰, =¹23³⁰-24
16	6	10 ●	10	10	10.0	00.0	03.2	.	=°0-24, ●⁰⁻¹1³⁰-11, 15¹⁵-16³⁰, ●¹20⁴⁵-21³⁰
17	6	10	09	05	09.0	02.9	00.5	.	=°0-19³⁰i
18	7	06	01 ⊙	06	05.7	06.5	.	.	=°4³⁰-11¹⁵, ⊕¹19¹⁵-23¹⁵
19	6	10 ●	10	10 ●	10.0	00.0	02.2	.	⊕¹0³⁰-1¹⁵, ●°4³⁰-6³⁰ 16¹⁵-24; ●⁺²6³⁰-13¹⁵
20	9	10	07 ⊙	00	05.7	03.9	07.8	.	●¹0-2³⁰, ⊥°2³⁰-11, F NNW 8⁴⁰-9, 13-16⁰³
21	5	06 ⊙	02 ⊙	04	04.0	04.9	.	.	⌣⁰⁻¹0³⁰-7³⁰
22	8	05 ⊙	05 ⊙	00	03.3	09.7	.	.	
23	8	09	09	10	09.3	01.0	.	.	
24	8	10 ●	06	01	05.7	05.9	00.0	.	●°6³⁰-7¹⁵i, △°21³⁰-24
25	8	05 ⊙	09 ⊙	03	05.7	05.7	00.0	.	△°0-7³⁰, 20³⁰-24; ●°17⁵⁰-18
26	8	10	09	09	09.3	01.9	00.0	.	△°0-3³⁰, ●°19⁴⁵-20³⁰
27	7	04	09	09	07.3	00.0	00.1	.	△°1³⁰-8¹⁵, =°5¹⁵-12¹⁵, ●°14¹⁵-17³⁰i, 23¹⁵-24
28	6	10 ●	10 ●	08	09.3	00.0	06.9	.	●°0-8⁴⁰, 12¹⁵-15¹⁵, =°3³⁰-18³⁰, F NW 17⁵⁵-8¹⁵, ✱°8⁴⁰-11¹⁵, 15¹⁵-18³⁰, ●°11¹⁵-12¹⁵i
29	3	03 ⊙	05 ⊙	00	02.7	08.0	04.5	.	△⁰⁻²4³⁰-10⁴⁵, 19³⁰-24
30	8	00 ⊙	00 ⊙	00	00.0	11.0	.	.	△⁰⁻²0-2³⁰, 19³⁰-24; ⌣°2³⁰-7¹⁵
31	8	09	03 ⊙	03	05.0	08.4	.	.	△°0-4
MES. VRED.		07.5	07.2	05.6	06.8	113.9	75.8		

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1	8	09	07 ⊙	10 ●	09.7	02.8	.	.	●°8⁴⁵-10⁴⁵i, 13⁴⁵-24i; F SW-W 14⁵⁹-15¹⁵, ⊕°15-15⁰⁴
2	9	09	08 ⊙	10	09.0	02.9	03.9	.	●°0-1³⁰ 8¹⁴, 12³⁰-13⁴⁵i, 18¹⁸-18³⁰; F SW-SE 17⁵⁹-18³⁰i, ⊕°17⁵⁹-18⁰⁸, ☾°S-W 18³⁰-19¹⁵
3	7	10	10	05	05.7	00.0	01.6	.	F SSE 2³⁹, 17⁰⁸i, ●°8³⁰-13¹⁵i, 17⁵⁰-18⁰⁵
4	8	05 ⊙	06 ⊙	00	03.0	09.2	01.2	.	△⁰⁻¹1³⁰-7, 18⁴⁵-24; F W 13
5	8	01 ⊙	00 ⊙	00	00.3	10.6	.	.	△⁰⁻¹0-4¹⁵, ⌣°4¹⁴⁵-7⁴⁵, F SSE 10³⁰-24i
6	9	10	09	00	06.3	02.8	.	.	F ESE 0-10⁵⁰, ●°10⁵⁵-11¹⁵, △⁰⁻¹19³⁰-24
7	9	09	02 ⊙	10	07.0	07.6	00.0	.	△⁰⁻²0-7³⁰, F ESE 22⁵⁹-24
8	7	10 ●	10 ●	10	10.0	00.0	04.6	.	F ESE 0-9³⁹, ●°0⁴⁵-17⁴⁵i, F SE 9²⁷-21
9	8	10 ●	05 ⊙	08	07.7	06.0	05.6	.	F SSE 1⁰⁶-26³⁰, ●°2⁰⁵-8¹i, F W 14⁵⁰, △⁺²20³⁰-24
10	8	04 ⊙	09	03	05.3	03.6	03.0	.	△⁰⁻²0-8⁴⁵, 20³⁰-24
11	8	06 ⊙	07 ⊙	08	07.0	05.3	.	.	△⁰⁻²0-9³⁰, 22³⁰-24
12	6	10 ●	10 ●	06	09.7	00.0	01.3	.	△°0-2⁴⁵, ●°2⁴⁵-17⁴⁵
13	8	00 ⊙	06 ⊙	09	05.0	06.7	01.6	.	●°19⁴⁵-19⁵¹i, F NW 19¹⁰
14	6	10 ●	10 ●	10 ●	10.0	00.0	0.2	.	●°0³⁰-24i, F NNE 22³⁰-24
15	7	07	10	00	05.7	02.5	20.1	.	●°0-1⁵⁰, F N-NNW 0-2⁵⁸, 15²², F NNW 2⁵⁸-16⁰⁷, △°19³⁰-24
16	7	04 ⊙	09	10	07.7	04.3	.	.	△⁰⁻¹0-7³⁰, F NNW 8⁴⁰-16¹⁵
17	8	01 ⊙	03 ⊙	00	01.3	10.9	.	.	△°19⁴⁵-24
18	7	10	10	10	10.0	01.4	.	.	△°0-6¹⁵, 22³⁰-24; ●°15⁴⁰-15³⁰
19	7	01	00 ⊙	00	00.3	10.2	00.0	.	△°0-7³⁰ 20³⁰-24
20	8	00 ⊙	02 ⊙	06	02.7	10.4	.	.	△°0-7³⁰, F ESE 17³⁸-22⁰⁴i
21	7	05 ⊙	06 ⊙	10	07.0	05.4	.	.	△°0³⁰-8¹⁵, F NNW 15²² 21⁰⁴i, =°15³⁰-17³⁰
22	7	09	03 ⊙	05	04.3	06.7	.	.	△°4³⁰-8¹⁵, 19³⁰-24; =°5³⁰-9³⁰
23	8	00 ⊙	04 ⊙	00	01.3	11.3	.	.	△⁰⁻¹0-8¹⁵, 19³⁰-24
24	7	04 ⊙	07 ⊙	06	05.7	06.6	.	.	△⁰⁻²0-8¹⁵, 20-24
25	8	07 ⊙	04 ⊙	09	05.7	09.8	.	.	△°0-6⁴⁵, ●°18, F S 18²²
26	8	00 ⊙	07 ⊙	02	03.0	09.7	00.0	.	△°1-7⁴⁵ F SSW 12¹⁵
27	8	06	07 ⊙	07	06.7	07.4	.	.	F NNW 8⁴⁴-12⁴⁴, △°20³⁰-24
28	7	09	10 ●	10 ●	09.7	02.5	.	.	△°0-8³⁰ F SSE-S 12⁴⁴-12³⁰ 21⁵⁰ 22⁰², ●⁰⁻¹13⁴⁵-24i
29	8	00 ⊙	02 ⊙	00	01.0	12.1	1[illegible]	.	●⁰⁻¹0-1³⁰i F SSE-WNW 0³⁰-1⁴⁵ 10⁵² 15⁵⁸, △⁰⁻¹20⁴⁵-24
30	8	04 ⊙	10	10	08.0	05.6	.	.	△⁺²0-9¹³⁰, F NNW 10⁵⁹-24i
MES. VRED.		05.7	04.4	05.[illegible]	05.9	180.4	64.[illegible]		

$\varphi = 44^{\circ}\ 48'$ N $\lambda = 20^{\circ}\ 28'$ E Gr. $\Delta G =$ + 1h 22 min. BR. ST. 174

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	751.5	750.7	752.4	05.4	13.6	06.6	08.0	14.3	04.8	03.5	04.9	04.8	05.6	74	41	77	64	W 2	NW 2	WSW 2
2	753.2	752.2	752.8	05.6	10.6	07.9	08.0	11.7	04.0	03.2	05.3	04.1	05.3	78	43	66	62	SW 2	WSW 3	WNW 2
3	753.2	753.0	752.9	05.1	13.0	09.8	09.4	14.8	04.9	04.9	06.2	06.8	07.5	94	61	82	79	WNW 2	W 1	WSW 2
4	751.5	747.3	746.5	08.6	17.2	10.9	11.9	18.0	06.0	03.8	05.5	04.6	06.4	66	31	65	54	WSW 2	NNW 4	NNE 3
5	743.4	744.6	747.2	09.6	11.4	10.1	10.3	11.4	08.9	08.2	08.1	08.3	08.5	90	82	92	88	NW 2	WSW 1	- 0
6	748.7	749.6	749.8	09.4	17.5	13.3	13.4	18.9	07.5	05.3	08.0	07.2	08.7	90	48	76	71	SSE 1	SE 1	ESE 2
7	749.4	749.1	749.6	14.6	20.0	16.2	16.8	21.1	10.7	08.0	08.7	07.4	08.6	70	42	63	58	SE 1	ESE 2	SE 2
8	749.4	749.5	748.4	17.0	22.6	18.6	19.2	24.2	12.6	10.0	09.0	10.9	10.5	62	53	65	60	SE 2	S 2	SSE 3
9	751.0	750.3	748.4	17.0	25.5	19.8	20.5	26.4	12.3	09.5	09.0	09.2	10.2	62	37	59	53	- 0	NE 2	ESE 2
10	748.1	744.8	742.5	17.6	27.2	22.2	22.3	28.1	15.0	13.0	11.1	10.6	11.1	73	39	55	56	WNW 2	SE 3	SSE 3
11	743.0	742.2	743.0	20.4	26.9	17.8	20.7	27.3	16.8	11.1	07.6	08.7	12.2	43	33	80	52	SE 1	WNW 2	NE 2
12	744.2	744.2	745.3	12.1	18.8	13.4	14.4	19.1	11.0	11.0	08.8	07.8	08.4	83	48	73	68	W 4	WSW 2	SSW 2
13	745.6	745.4	747.2	14.2	20.7	15.2	16.3	21.7	13.1	09.6	07.0	07.9	08.9	58	43	69	57	WSW 3	WNW 3	W 2
14	749.7	749.3	749.4	14.1	21.6	15.2	16.5	22.4	11.2	08.5	09.5	07.6	08.9	78	39	69	62	W 2	WNW 3	SW 2
15	749.0	746.1	745.4	18.5	25.6	16.8	19.4	26.1	12.6	08.5	09.0	08.7	10.6	56	35	74	55	SSW 1	WNW 2	SSE 2
16	744.8	743.7	745.2	14.9	21.8	15.4	16.9	23.3	14.5	14.0	10.8	09.2	11.7	85	47	89	74	S 2	WSW 1	SW 2
17	745.3	744.2	744.6	14.0	17.4	14.4	15.0	20.7	10.7	07.9	10.1	08.5	10.3	84	57	84	75	WSW 1	NNW 3	SW 1
18	745.7	747.2	750.7	13.0	18.5	14.3	15.0	18.5	13.0	11.3	10.5	10.5	09.8	93	66	81	80	NNW 2	NNW 3	N 3
19	752.3	752.9	753.0	11.4	14.0	12.6	12.6	14.9	11.4	11.1	09.3	10.7	10.4	92	90	96	93	WNW 2	W 2	SW 1
20	751.8	750.4	749.4	12.5	17.0	13.6	14.2	18.7	11.6	11.4	10.3	10.6	10.4	94	73	89	85	- 0	SE 1	ENE 2
21	747.4	744.6	744.0	13.2	15.6	14.0	14.2	17.4	12.9	11.8	10.9	11.4	10.5	96	86	87	90	NNE 2	WSW 1	- 0
22	742.6	741.4	744.6	14.8	21.6	12.2	15.2	21.7	11.8	09.4	10.2	10.3	10.1	81	53	94	76	- 0	SSE 2	NNW 2
23	745.4	750.3	752.6	09.2	10.5	10.0	09.9	12.4	09.2	09.3	08.3	07.9	06.2	95	83	68	82	WNW 3	NNW 2	WNW 2
24	755.3	755.7	756.0	07.7	10.7	09.4	09.3	11.3	06.0	04.4	06.6	07.3	08.1	83	76	91	83	WNW 2	NW 3	WNW 2
25	757.0	756.0	755.2	10.4	17.5	11.4	12.7	18.5	05.9	04.5	07.4	06.6	07.7	78	44	77	66	WNW 2	NNW 3	NNW 1
26	754.0	752.5	752.1	12.8	19.6	13.2	14.7	20.5	07.7	04.8	07.1	07.0	08.5	64	41	75	60	N 1	ENE 2	ENE 1
27	751.7	750.1	750.4	14.3	21.6	14.6	16.3	22.3	08.4	05.4	08.6	08.8	09.0	71	46	72	63	ESE 1	WNW 2	N 2
28	751.1	751.2	751.1	11.2	13.0	12.6	12.4	14.6	11.0	11.0	09.5	09.5	09.4	95	85	86	89	NW 2	NW 2	N 1
29	751.2	751.0	750.7	11.6	17.9	13.0	13.9	19.0	11.0	11.0	09.7	09.2	09.5	94	59	85	79	WNW 2	SW 1	SE 2
30	749.8	749.5	749.4	14.6	22.8	17.2	18.0	23.4	09.0	06.0	08.9	10.8	10.3	71	52	70	64	ESE 2	NNE 2	SSE 2
31	750.6	750.7	751.6	13.9	19.6	15.3	16.0	20.6	12.5	10.6	10.6	12.0	11.6	89	70	89	83	WNW 1	WNW 2	WSW 2
MES. PRED.	749.2	748.7	749.1	12.5	18.4	13.8	14.6	19.5	10.2	08.4	08.6	08.5	09.2	79	55	77	70	1.7	2.1	1.8

1	753.3	752.0	753.0	13.4	19.3	12.5	14.4	19.3	11.1	09.8	09.3	09.2	10.0	81	55	92	76	WNW 2	NW 2	N 1
2	752.9	751.6	752.5	13.1	18.5	14.0	14.9	20.4	10.0	07.7	08.9	08.7	06.3	79	55	53	62	NW 2	NNW 2	WNW 2
3	753.8	753.6	752.4	09.4	09.4	10.2	09.8	14.0	09.0	08.6	08.1	08.4	08.4	91	95	90	92	WNW 2	W 3	WSW 2
4	749.8	750.6	750.5	10.6	11.8	11.6	11.4	13.8	09.8	10.2	09.1	09.7	09.0	95	93	88	92	WNW 2	NNW 2	S 2
5	750.5	750.4	750.0	11.8	21.6	15.8	16.2	22.3	11.6	11.1	09.7	09.1	10.2	93	47	76	72	SSW 2	WNW 3	SE 2
6	750.8	750.6	750.7	17.7	21.8	16.6	18.2	22.3	11.5	07.8	08.9	08.9	10.9	58	45	77	60	WSW 1	WSW 3	SSE 2
7	750.9	751.6	750.5	17.0	17.0	16.5	16.8	18.2	13.0	09.6	11.5	13.3	12.2	79	91	86	85	SW 1	SE 2	SE 3
8	749.9	749.3	749.7	18.3	27.3	21.4	22.1	27.9	13.8	11.0	11.0	14.8	13.2	70	55	69	65	ESE 2	SE 3	SE 3
9	750.6	750.5	750.5	20.3	27.1	22.5	23.1	28.1	18.0	-	13.3	15.3	16.9	74	57	83	71	SE 3	SSE 1	S 2
10	749.8	747.1	747.1	21.6	29.7	21.3	23.5	30.6	17.1	14.4	13.8	13.8	13.5	71	44	71	62	NNE 2	SSE 3	NW 3
11	747.9	747.9	747.4	19.0	19.6	19.0	19.2	24.6	16.0	13.8	13.0	14.5	14.4	79	85	87	84	W 2	NNW 2	- 0
12	747.5	746.5	746.4	19.1	24.0	19.8	20.7	25.1	17.3	15.8	12.4	13.7	11.9	75	61	69	68	W 2	W 2	W 2
13	746.9	745.8	746.6	19.9	26.4	17.3	20.2	27.1	16.2	13.2	10.6	12.0	13.8	61	47	93	67	SW 1	WSW 3	- 0
14	748.2	747.9	747.4	18.2	24.6	19.6	20.5	25.2	14.6	12.4	12.5	13.5	11.8	80	58	69	69	- 0	ENE 2	SSW 1
15	749.0	750.5	750.9	18.5	25.2	19.8	20.8	26.2	17.0	13.6	12.5	09.9	10.9	78	41	63	61	W 2	N 2	ESE 2
16	751.7	751.3	750.8	21.1	27.6	22.0	23.2	28.0	16.9	13.1	10.0	11.3	10.9	53	41	55	50	SE 2	ESE 2	ESE 2
17	749.9	748.1	747.5	22.1	30.4	23.4	24.8	30.7	17.4	13.6	12.7	13.3	14.7	64	41	68	58	SE 1	WSW 2	- 0
18	747.3	745.8	746.7	19.7	28.0	19.0	21.4	28.6	17.6	17.0	14.8	16.0	14.7	86	56	89	77	ESE 2	E 3	SSW 1
19	746.3	746.0	747.2	18.4	20.9	18.8	19.2	22.7	17.9	17.8	15.0	14.2	14.5	94	76	89	86	SE 2	NNW 3	W 2
20	747.7	747.9	750.3	18.3	24.8	18.6	20.1	25.4	17.8	17.6	14.2	12.8	15.0	90	55	94	80	W 2	NNE 3	WNW 2
21	752.4	752.6	752.9	17.4	26.3	20.1	21.0	27.0	15.2	13.4	12.0	10.7	14.3	80	42	81	68	WNW 2	NNE 3	NNW 1
22	753.4	753.0	752.1	20.6	29.0	23.6	24.2	29.4	16.6	14.2	14.0	13.0	15.7	77	43	72	64	SW 1	NNW 2	WSW 2
23	751.8	751.4	751.5	22.0	28.1	22.0	23.5	30.5	19.6	16.2	15.8	15.9	12.3	79	56	62	66	WSW 2	WNW 2	ENE 3
24	751.3	751.4	751.9	21.9	29.0	22.7	24.1	29.7	17.4	14.2	12.2	15.3	14.6	62	51	71	61	WSW 2	WSW 2	W 1
25	753.0	753.0	753.6	20.0	19.6	19.3	19.6	27.0	19.1	16.8	14.0	15.0	15.1	80	88	90	86	SW 2	- 0	WSW 1
26	754.3	753.4	753.1	20.1	21.9	19.4	20.2	26.6	16.5	14.6	14.3	13.5	14.9	81	69	88	79	WSW 2	W 2	SSE 2
27	753.9	753.7	752.9	18.6	25.7	20.9	21.5	26.9	17.1	15.6	14.3	13.1	14.5	89	53	78	73	W 1	NNW 2	NW 2
28	752.6	751.3	750.9	22.4	28.1	21.9	23.6	29.4	16.5	16.0	15.4	12.2	13.7	76	43	69	63	- 0	ENE 2	ESE 2
29	749.9	748.6	749.9	23.4	29.6	21.5	24.0	30.4	17.5	14.4	12.5	13.4	12.0	59	43	62	55	ESE 2	ESE 2	W 2
30	749.1	746.4	744.7	20.0	28.9	24.2	24.3	29.6	18.2	16.6	14.0	14.6	13.6	80	49	60	63	- 0	SSE 2	SE 2
MES. PRED.	750.5	750.0	750.0	18.[illegible]	24.0	19.2	20.2	26.6	1[illegible]	13.4	12.3	12.6	12.8	77	58	76	70	1.6	2.2	1.7

BR. ST. 174 H_s = 132 m H_b =131.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnevni		7	7	
1	3	00⊙	07⊙	03	04.7	07.4	•	•	F_{WNW} 8^{28} 11^{20} i, ●° 14^{15}
2	4	07⊙	03	09	07.3	07.1	00.2	•	●° 1^{50} 10i 17^{15} 18^{15}i
3	7	10●	08	08	08.7	04.2	02.2	•	⊿° 1^{30} 8^{45}, F_{NNW} 10^{17} 20^{06} ●° 18^{50} 23^{15}
4	9	02⊙	10	10●	7.[illegible]	11.1	00.1	•	═° 4^{30} 24, ●° 9^{30} 15^{45} 15^{45} 16^{45} i, ⊿' 23^{45} 24
5	7	10	10	09	09.3	03.0	00.6	•	
6	8	010⊙	0[illegible]⊙	01	01.7	07.6	01.1	•	⊿°-2 0-2^{30} 19^{30} 24; ═°-2 0-2^{30} 6^{30} 11; ═° 2^{30}- 6^{30}
7	7	10	13	03	09.7	01.1	•	•	⊿' 2 0-7^{45} 21^{30} 24; ●° 7^{05}- 17^{45} i
8	3	07	13	04	07.0	02.3	00.0	•	⊿°-1 0-6^{55} 22^{30} 24; F_{ESE} 5^{12}- 20^{44} i, ●° 6^{55}- 7^{15}, 14^{50}, 14^{15}- 14^{45}
9	8	00⊙	05⊙	05	09.0	11.4	01.[illegible]	•	⊿°-1 0- 7^{30} 24
10	8	10	09⊙	09	07.3	[illegible]	•	•	⊿°-1 0-7^{30}; F_{SE} 9^{58} 23^{02} i
11	2	00⊙	00⊙	10	03.3	02.9	•	•	⊿° 2-7^{30} ⚢' 18^{20} 18^{40} ▽' 18^{25}- 18^{40}
12	6	10●	05⊙	04	06.3	04.0	02.7	•	●°-2 5^{55}- 6^{45} 14^{20} 17^{20} i; F_{WSW} 6^{02}- 6^{48} T 14^{15}- 15^{45} F_{WNW} 14^{53}, ▽°-2 14^{55}- 17^{02} i, ⚢' 16^{45}- 17^{45}
13	8	10	05⊙	09	09.0	06.4	00.3	•	F_{WNW} 9^{08}- 21^{32} i, ●° 17- 17^{35} i, 21^{05}- 22^{30} i, T° 17- 17^{45} [▲° 17^{02}- 17^{03}
14	8	00⊙	00⊙	00	02.3	11.2	00.0	•	F_W 11^{03}- 12^{40} ▽° 14^{45}- 14^{30} i, ⊿°-1 20^{15}- 24
15	9	00⊙	06⊙	07	04.3	09.1	00.[illegible]	•	⊿°-2 0-8^{15} T° 15^{42}- 15^{46}, F_W 15^{44}- 15^{54}, ζ 15^{45}- 16^{15}, ▽°-2 15^{45}- 16^{15}, ⚢° 15^{46}- 16^{45}, ●° 16^{45}- 18^{30} i
16		09	03	06	03.0	04.8	07.0	•	●°-2 0- 5^{30}; 14^{35}- 16^{35} i; ⚢° 14^{45}- 15^{20} F_{WSW} 14^{48}- 15
17	3	09	03	09	09.0	04.5	00.2	•	●° 8^{05}- 9^{15} 14^{20} 18^{42} 18^{50} 21^{45}- 24i; F_{NW} 13^{46}- 13^{58} ▽° 13^{54}- 13^{57}
18	7	10●	09	10●	03.7	00.3	04.9	•	●° 0- 13^{30} i 15^{38}- 24i; ▽°-2 6^{31}- 7^{15} i, 15^{30}- 16^{30} i, ⚢° 6^{46}- 7^{15}, ζ° 6^{51}- 6^{58}, F_{NNW} 12^{34}- 21^{49} F_{NNW} [13^{47}
19	6	10●	10	10●	10.0	00.0	12.3	•	●°-1 0- 10^{45} i, 16^{45}- 23^{30} i
20	7	10●	10	10	10.0	00.8	05.4	•	═° 2^{30}- 14^{30}, ●° 3^{55}- 7^{45} i, 14^{20}- 14^{35} i, 18^{55}- 19^{15}, ▽°-1 14^{32}- 14^{39}, T^3_{SE} 18^{03}
21	7	10●	07	10●	09.0	00.4	02.3	•	═° 3^{45}- 11^{30} ●°-1 4^{45}- 7^{45}, 10^{45} 13^{20} i; 20^{45}- 24 i; ▽° 12^{35}- 12^{40}
22	8	01⊙	08⊙	10●	06.3	04.6	01.7	•	●° 0- 2^{45} 14^{20} 24i; ═° 3^{32}- 4^{30} F_W 14^{08}- 14^{42} T° 14^{19} 14^{28} ζ° 14^{33} 16^{30} ⚢° 14^{38} 16^{45} ▽° 14^{5}
23	7	10●	10●	03	07.7	01.6	24.6	•	●°-1 0- 17^{55} i, F_{NW} 17^{32} 12^{34} i, F_{NW} 8^{30}- 10^{30}, 17^{32}, ζ 17^{45}- 17^{45} T° 17^{15}- 17^{45} [16^{45}
24	7	07⊙	10●	07	08.0	06.5	00.[illegible]	•	═° 4^{30}- 6^{30} F_{NW} 17^{42}- 14^{57} ●° 10^{55}- 18^{45}
25	7	01⊙	08⊙	00	02.0	12.3	02.3	•	F_{NNW} 7^{52}- 14^{11}, ⊿°-2 19^{45}- 24
26	3	00⊙	04⊙	00	01.3	12.6	•	•	⊿°-2 0-8^{30} 20-24
27	3	01⊙	04⊙	10	05.0	11.0	•	•	⊿°-2 0- 8^{30} F_{NNW} 16^{41}- 20^{20} ●°-1 21^{40}- 24
28	7	10●	10●	10●	10.0	00.0	00.1	•	●°-1 0-1^{35} 5-24i; ═° 1^{30}- 12^{15}
29	7	10●	03⊙	03	05.3	04.0	04.0	•	●° 0- 9^{45}; ⊿°-2 19^{15}- 24
30	8	02⊙	03⊙	04	03.0	10.7	00.1	•	⊿°-2 0-8^{45} 19^{30} 24
31	7	10●	07⊙	10	09.0	02.6	01.4	•	⊿°-1 0-5^{45}; T° 5^{40}- 5^{30}, ●°-1 5^{45}- 11, 16^{05}- 17^{15}; ═° 11-11^{45}, ▽°-2 15^{28}- 16^{45} i, ζ 15^{31}- 15^{4}
MES. VRED.		06.3	07.1	06.2	06.5	168.1	102.0		

1	7	10	09	04	07.7	05.2	07.3	•	F_W 7^{32}- 8^{15} 13^{42}, ●° 11^{55}- 13i, ▽° 13^{40}- 16^{20} i, ⚢' 15^{45}- 16^{30} F_{NNW} 15^{53}- 15^{55}
2	7	10●	09●	04	07.7	05.9	04.3	•	●° 1^{5}- 6^{30} ⚢ ▽°-2 6^{31} 6^{46} i, 13^{35}- 13^{50} 23^{08}- 23^{25}, ●°-1 11^{05}- 11^{10} 22^{15}- 23^{45} i; F_{NW} 14^{39} 19^{44} ⚢' [23- 23^{45}
3	6	10●	10●	10●	10.0	00.0	02.1	•	●°-1 2^{45}- 2^{45} 5^{30}- 14^{45} 20^{30}- 24; ═° 14^{45}- 17^{30}
4	6	10	10●	10●	10.0	00.0	11.0	•	●° 0-3, 10^{30}- 21i; ═° 3- 24
5	8	10●	07⊙	00	05.7	03.3	17.0	•	═° 0- 12^{45}, ●°-1 3^{30}- 11i, ⊿' 20^{30}- 24
6	8	06⊙	05⊙	00	03.7	10.5	01.4	•	⊿°-2 0-9^{45} 19^{30} 24
7	7	10	10●	03	07.7	01.0	06.0	•	⊿° 0-6^{55} ▽° 6^{59}- 7^{20} ●°-1 7^{30}- 14^{30}, 18^{20}- 18^{30}
8	3	04⊙	00⊙	05	03.0	11.3	02.0	•	F_{SE} 16^{36}- 17^{05} ●° 22^{45}- 22^{50}
9	8	04⊙	08	10●	07.3	06.5	06.0	•	⊿°-1 0- 7^{30} 14^{25}, 18^{55}- 20^{40} i
10	8	02⊙	05⊙	10	05.7	11.4	00.0	•	⊿°-1 1^{15}- 8^{30}, ●° 8^{50}- 10i, 21^{45}- 22^{45}, F 18^{42}- 20^{50}, ζ $_{NW}$ 19^{30}- 21^{45}
11	3	09	06	04	06.3	07.9	00.6	•	⊿°-1 0- 8^{30} 8, 19^{30}- 24; ●°-1 7^{55}- 9^{15} i, 13- 13^{20}, F_{NNW} 12^{49} ▽' 13^{20}- 13^{30}
12	7	00⊙	01●	02	03.3	09.7	01.7	•	⊿°-1 0- 8^{30} 20- 24; F_{WNW} 10^{45}- 14^{06} i, ▽°-2 12^{42} 13^{45} i, ⚢' 12^{45}- 13^{55} ●° 13^{45}- 13^{50}
13	8	00⊙	02⊙	06●⚢	02.7	09.1	01.2	•	⊿°-1 0- 9^{15} ●° 10- 16^{05}, 17^{45}- 17^{45}, ⚢° 15^{45}- 17^{45} i, 20^{30}- 20^{45}, F_W 15^{52}- 16^{03}, ▽°-2 15^{55}- 17^{05} [20^{25}- 20^{40} i
14	7	06⊙	07⊙	09	07.3	06.3	03.3	•	⊿°-1 1^{30} 9 9^{15} 20^{30}- 24
15	8	07⊙	01⊙	00	02.7	11.7	•	•	⊿°-1 0- 7^{45}, 21^{45} 24
16	8	00⊙	00⊙	04	01.3	12.1	•	•	⊿°-1 0- 7^{45}, 21^{30} 24
17	9	00⊙	06⊙	01	02.3	12.1	•	•	⊿° 0- 6^{45} ζ $_N$ 21^{30} 24, F_{NNE} 22^{06}
18	8	05⊙	04⊙	10●⚢	06.3	08.0	03.6	•	⊿° 0-0^{30} ⚢ 0^{32}- 4^{45} i, 14^{08}- 24i; ▽°-1 0^{35} 15- 16^{09} 17^{08} i, 20^{30}- 23^{05} i; ●°-2 3^{58}- 4^{45} 15^{55}- 18^{45} i; F_{ESE}
19	7	10●	08●	00	08.7	01.7	12.2	•	⚢°-2 5^{45} ●° 10^{45} 15^{45} 6^{55} 13^{30} i, 13^{55}- 16^{40} i, ▽°-1 4^{40}- 23^{4}; T° 13^{50}- 15^{30} [14^{52}- 20^{08}, F_{ESE} 17^{53}
20	7	10	04⊙	05	05.3	06.0	01.	•	═° 4^{30}- 11^{30}, F_{NNE} 13^{08}- 15^{52}, ⚢°-1 15^{30}- 16^{30}, ▽° 15^{30}- 16^{45} i, ●° 15^{40}- 17^{45} i
21	8	04⊙	02⊙	00	02.3	13.2	04.0	•	⊿°-2 19^{30} 24
22	7	00⊙	01⊙	02	01.0	13.3	•	•	⊿°-2 0-8^{45} 19^{45} 24
23	8	00⊙	03⊙	05	02.7	12.1	•	•	⊿°-1 0-8^{30} ζ°-1 19^{30}- 22^{30} F_{ESE} 19^{58}- 22^{30}
24	8	02⊙	00⊙	00	00.7	13.0	•	•	⊿° 2^{30}- 8 20^{45}- 24; ζ° 20^{45}- 24
25	7	04⊙	10●⚢	01	05.0	04.3	00.6	•	ζ 0-2^{45}, ⊿°-1 0-4^{45} 19^{45}- 24; ⚢ 2^{45}- 5^{30} 12^{37} 13^{45}; ▽°-1 4^{55}- 5^{45} 12^{42}- 12^{45}; T° 11^{45}- 12^{39} F_{NNW}
26	8	00⊙	08	10●⚢	06.0	07.7	00.[illegible]	•	⊿°-2 0- 9^{45} F_{WNW} 12^{30} ▽° 12^{42}- 13, 17^{48}- 20^{40} i; T° $_{WNW}$ 12^{50}- 13^{15}, ⚢ [12^{42}- 12^{50}, ●° 12^{45}- 14^{45} i;
27	7	05	04⊙	00	03.0	10.5	07.7	•	⊿°-1 2^{30}- 8^{45} 19^{30}- 24; ═° 4^{45}- 8^{45} [17^{00}- 21
28	7	00⊙	03⊙	00	01.0	12.1	•	•	⊿°-2 0- 9 19^{30} 24
29	8	01⊙	01⊙	06	02.7	03.9	•	•	⊿°-2 0- 9^{45} 22^{30}- 24; F_{WSW} 16^{33}
30	8	04⊙	00⊙	03	02.3	10.1	•	•	⊿°-2 0-8^{45}
MES. VRED.		04.8	05.0	04.4	04.7	247.9	03.3		

φ = 44° 48' N λ = 20° 28' E Gr. ΔG = + 1h 22 min. BR. ST. 170

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
1	751.6	751.9	751.6	11.8	13.4	16.4	14.5	18.6	11.4	10.8	09.8	10.7	10.5	94	93	75	87	W 3	NNW 2	W 2
2	752.4	752.6	752.0	15.2	23.2	19.2	18.7	24.6	13.5	11.7	10.4	11.0	12.9	80	52	83	72	WNW 2	WNW 2	SSW 2
3	754.1	753.3	752.3	19.6	25.1	19.8	21.1	27.5	13.8	10.6	11.8	11.9	12.8	69	50	74	64	- 0	SE 2	SE 2
4	751.6	752.9	752.8	21.3	28.4	21.1	23.0	28.7	14.0	10.4	11.7	12.1	13.6	61	42	73	59	- 0	NE 1	NE 1
5	752.9	751.8	751.3	20.7	28.5	23.0	23.8	29.6	16.0	13.8	12.8	10.2	14.8	70	35	70	58	- 0	ENE 1	SSE 2
6	751.6	750.0	749.8	22.3	28.2	20.9	23.1	28.6	19.0	15.8	13.9	15.4	14.2	69	54	76	66	SSW 2	SSE 3	WNW 1
7	749.6	749.6	748.1	21.5	28.4	23.2	24.1	29.0	17.0	14.4	12.3	13.6	14.7	64	47	69	60	S 1	S 2	SSE 3
8	747.8	749.5	750.6	22.4	24.5	15.4	20.7	30.4	15.4	17.2	14.9	14.7	11.9	74	48	91	71	SSE 2	SSE 2	WNW 2
9	752.7	751.2	750.2	13.9	20.2	16.7	16.9	21.4	13.0	12.6	09.9	08.6	12.2	83	49	86	73	WNW 2	NNE 3	- 0
10	749.2	748.3	748.5	15.4	21.1	18.5	19.4	22.6	14.0	12.2	11.8	10.5	12.9	90	56	81	76	- 0	NNW 2	W 2
11	749.1	748.0	744.9	14.0	15.1	14.9	14.7	18.5	13.5	13.3	11.4	12.1	11.9	95	94	94	94	WNW 2	WNW 2	NW 3
12	747.8	747.8	750.1	13.8	19.7	18.8	15.3	20.0	13.0	12.0	09.7	09.9	10.8	82	59	92	77	WNW 2	NNW 3	WNW 3
13	751.2	750.6	751.2	14.7	19.0	16.8	16.8	20.2	12.9	11.3	09.4	09.2	09.3	75	56	65	65	WNW 3	NNW 3	WNW 2
14	751.4	751.5	754.0	15.9	21.8	14.8	16.8	23.3	13.2	11.8	11.7	09.4	11.2	87	48	89	75	WNW 3	NNW 4	W 2
15	756.4	756.4	757.0	16.2	22.4	16.5	17.9	23.4	12.1	09.7	08.6	07.2	09.1	63	35	65	54	NNW 3	NNW 3	- 0
16	757.4	757.6	757.6	16.0	24.2	17.4	18.8	24.8	09.6	11.8	08.4	08.8	11.6	62	39	78	60	- 0	ENE 1	WSW 1
17	758.3	757.1	755.8	18.2	26.1	18.8	20.5	27.5	12.3	09.0	11.2	10.0	11.7	71	39	72	61	W 1	NNW 2	WSW 1
18	755.2	754.0	753.8	19.3	27.3	21.5	22.5	28.8	13.7	10.4	11.7	11.5	12.8	70	41	67	59	S 1	WNW 2	W 2
19	754.4	754.2	753.9	19.5	27.4	21.6	22.5	28.2	18.4	16.6	15.0	13.8	14.9	88	51	77	72	WNW 2	N 2	- 0
20	753.3	753.0	751.8	19.4	25.9	19.4	21.0	27.6	17.0	12.8	10.6	11.5	12.2	63	46	72	60	WNW 2	NNW 2	- 0
21	751.2	751.6	752.5	19.4	24.3	20.7	21.3	26.1	18.1	14.4	13.2	10.6	11.3	78	46	62	62	WNW 2	N 3	NNW 2
22	753.3	753.0	753.2	16.9	24.5	19.7	20.2	25.7	15.2	12.1	11.4	09.9	10.7	79	43	62	61	- 0	N 2	NNE 2
23	753.3	752.9	753.8	18.1	25.4	20.6	21.2	26.6	14.0	11.0	11.6	12.7	12.9	75	52	71	66	WSW 2	NNE 2	NE 1
24	755.3	754.7	754.7	19.7	27.3	20.7	22.1	28.3	15.4	12.2	13.3	11.6	13.2	77	43	72	64	ESE 2	ESE 2	SE 1
25	755.1	754.6	754.0	21.3	27.8	22.9	23.7	29.2	15.5	11.8	13.1	12.1	14.4	69	43	69	60	ENE 1	NE 2	WSW 1
26	753.6	752.7	752.6	22.1	27.9	22.7	24.3	30.5	18.5	14.4	14.3	12.6	14.6	72	40	71	61	NNW 2	NNW 2	E 1
27	753.1	752.5	752.0	21.1	31.3	23.2	24.7	32.0	17.4	14.0	14.5	13.8	14.8	77	40	70	62	WNW 1	N 2	W 2
28	751.9	751.3	751.4	21.7	29.5	21.3	23.5	31.1	17.7	14.2	15.1	14.7	16.2	78	47	86	70	W 2	NNW 2	SSW 1
29	750.0	749.4	749.9	19.2	26.2	20.4	21.6	26.9	17.9	15.6	15.5	15.7	15.6	95	62	87	81	S 2	SE 2	SE 2
30	749.4	750.2	7[illegible]0.9	21.1	23.2	21.6	21.9	25.4	18.0	17.0	15.1	16.4	15.5	81	77	80	79	SSE 2	ESE 3	SE 3
31	751.[illegible]	752.3	752.0	21.3	25.7	20.6	22.0	25.0	19.2	16.7	12.1	11.8	11.3	64	48	62	58	SE 4	ESE 4	ESE 2
MES. VR.	752.[illegible]	752.0	752.2	18.5	24.9	19.4	20.6	26.2	15.2	13.0	12.1	11.7	12.8	76	51	76	67	1.6	2.2	1.6

1	751.3	751.1	751.6	20.5	27.0	21.3	22.6	28.1	15.5	15.4	11.0	11.3	11.0	60	42	68	53	ESE 3	ESE 4	SE 2
2	751.6	750.9	750.6	21.0	28.8	20.9	22.3	28.9	16.5	12.8	11.7	10.4	14.1	63	35	76	58	ESE 2	SSE 2	NNE 1
3	750.7	749.3	749.4	20.4	29.0	21.8	23.2	29.7	16.2	13.2	13.1	13.4	15.4	73	44	79	65	WSW 2	NNW 2	NW 2
4	750.6	751.4	752.5	21.4	23.7	21.2	21.9	27.0	18.3	14.8	13.9	15.4	15.4	75	70	81	75	SSW 2	N 2	SSE 1
5	753.8	752.2	753.4	19.9	25.7	19.4	20.1	26.3	14.9	11.1	13.1	08.8	10.3	97	35	61	64	NW 1	NW 2	- 0
6	755.5	752.2	752.7	16.2	26.6	20.3	20.6	27.4	11.7	08.5	10.9	09.6	11.8	79	37	66	61	W 2	NNW 2	S [illegible]
7	752.0	752.3	751.9	18.4	28.0	20.8	22.0	29.0	15.1	10.6	10.6	11.4	12.9	67	40	70	59	WSW 2	NNE 1	SSE 2
8	752.3	752.1	752.0	17.7	25.5	18.4	20.0	26.4	15.0	11.0	11.0	14.3	14.4	73	58	91	74	WSW 2	N 2	W [illegible]
9	752.3	750.8	750.3	16.7	22.5	17.3	18.4	22.7	16.3	12.2	12.6	12.8	14.1	88	63	95	82	S 1	WSW 1	ENE 1
10	750.0	750.0	750.7	16.9	21.1	16.7	17.6	24.0	15.1	12.4	13.2	12.8	12.9	92	68	90	83	WNW 1	N 1	SE 2
11	751.8	751.5	751.9	17.5	25.5	18.8	20.2	23.7	13.2	10.0	12.7	11.3	11.7	85	46	72	68	SE 2	SE 2	ENE 2
12	752.0	751.8	752.1	19.7	27.7	22.0	22.6	23.0	15.5	10.7	12.6	15.7	13.9	78	49	70	66	SE 2	SSE 3	SSE 2
13	752.4	752.3	751.8	20.9	30.0	22.1	23.8	30.4	18.3	15.2	12.6	14.6	14.0	69	46	70	62	SSE 2	WSW 2	SSE 1
14	751.0	750.1	748.7	22.0	30.4	24.0	25.1	31.4	19.1	15.3	14.5	15.0	16.5	75	46	74	64	SSE 1	WSW 2	SSE 1
15	745.9	744.5	743.9	25.0	32.6	24.6	26.7	33.0	22.3	17.6	15.2	13.8	16.2	68	38	70	59	SSW 1	W 2	W 2
16	745.3	742.1	742.6	21.5	29.1	20.3	22.8	30.9	18.4	14.4	13.6	13.9	15.5	71	46	87	68	SE 3	ENE 2	N 2
17	744.7	743.4	747.0	18.9	20.1	16.8	18.1	20.3	16.5	17.0	15.7	15.5	13.6	96	88	95	93	WNW 2	NNW 2	SW 1
18	745.8	746.5	748.0	18.8	20.9	18.2	19.0	23.1	16.8	16.9	13.9	13.3	12.9	85	72	82	80	WNW 1	WSW 2	WNW 2
19	749.1	750.3	751.2	16.2	17.5	16.3	16.6	18.5	16.0	15.6	12.0	12.5	12.9	87	82	93	87	WNW 2	W 2	W 3
20	751.5	750.9	750.2	14.9	21.3	17.2	17.6	23.0	14.7	14.9	11.7	12.2	12.5	92	64	85	80	WNW 2	NW 2	SSE 2
21	749.6	74[illegible].7	748.1	18.2	27.5	20.7	21.9	28.6	14.0	10.2	10.9	09.5	13.0	70	35	71	59	SE 2	W 1	SSE 2
22	748.7	747.4	747.1	18.2	27.0	21.2	21.9	27.4	17.0	13.5	15.1	13.9	14.5	83	52	77	71	W 2	N 2	NNE 2
23	745.8	744.9	746.3	18.2	28.8	19.7	21.6	30.2	15.0	11.6	13.6	14.1	14.6	87	47	85	73	- 0	S 1	NNE 2
24	746.9	746.0	746.5	19.5	30.5	22.1	23.5	30.7	16.5	14.2	14.4	14.9	15.4	85	45	77	69	SE 1	SE 3	ESE 2
25	746.6	745.0	745.4	17.5	20.2	19.1	19.0	22.6	16.6	15.2	14.3	15.0	15.8	95	84	95	91	WSW 2	- 0	ESE 2
26	743.2	743.8	746.9	17.9	25.4	17.7	19.7	26.5	17.7	16.3	14.4	12.5	12.0	93	51	79	74	WNW 2	SW 2	NNW 2
27	746.5	743.8	742.7	15.0	22.4	18.4	18.6	23.5	13.4	10.7	11.9	12.4	11.6	93	61	73	76	ENE 2	SE 3	SSE 2
28	741.7	743.1	745.6	15.6	15.4	13.6	14.6	18.4	13.4	13.2	12.2	10.9	10.0	92	83	85	87	WSW 2	WNW 2	W 2
29	748.4	749.4	749.8	13.1	19.3	15.3	15.5	15.6	10.2	07.5	09.7	10.1	11.0	86	64	84	78	S 1	SE 2	SE 2
30	751.1	752.1	753.5	14.2	22.3	18.2	18.2	22.1	11.7	08.6	10.9	13.0	12.[illegible]	90	65	80	78	WSW 1	N 1	NNE 2
31	755.6	754.2	756.4	15.3	25.5	21.1	20.8	26.7	15.0	12.0	12.2	13.[illegible]	11.[illegible]	94	55	62	70	NNW 1	ENE 2	NE 2
MES. VR.	749.4	749.2	749.4	18.1	25.0	19.5	20.6	26.1	15.7	12.9	12.7	12.[illegible]	13.4	82	5[illegible]	76	72	1.7	1.9	1.8

BEOGRAD

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H_s = 132 m H_b = 131.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sat	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednje		7	7	
1	6	00⊙	10	00	03.3	02.9	.	.	=°14^{30}-24; ●°15^{45}-17i; ⌂°19^{30}-24
2	8	09	03●	00	04.0	11.1	00.0	.	⌂$^{0-2}$0-7^{45}, 19^{45}-24; =°0-7^{45}
3	8	10	09	03	07.3	04.6	.	.	⌂$^{+2}$0-7^{45}, 20-24; F$_{NNW}$ 7^{30}-9
4	9	05⊙	07⊙	04	05.3	11.0	.	.	⌂$^{+2}$0-8^{30} F$_{NNW}$ 19^{45}-20^{30}
5	8	10●	10●	10●	10.0	00.0	19.0	.	●$^{0-1}$$4^{30}$-24, F$_{NNW}$ 20^{24}
6	5	10●	10●	10	10.0	00.0	40.7	.	●$^{0-2}$0-14^{30}, ●°14^{30}-18^{30} =$^{+2}$$18^{30}$-24
7	6	10	10●	10●	10.0	00.0	00.7	.	=$^{0-1}$0-16, ⌂$^{0-1}$$17^{00}$-$18^{05}$, 19^{30}-20^{30}i; ●°18^{05}-17^{45}, 19^{45}-22^{30}i; ⊓ 16^{45}-17^{45}, 19^{30}-20^{30}
8	7	10	04●	00	04.7	06.6	07.8	.	=°13^{30}, ⌂$^{+2}$$19^{45}$-24
9	8	04⊙	05⊙	03	04.7	12.2	.	.	⌂$^{0-2}$0-8, ⌂$^{+2}$$20^{30}$-24
10	8	00⊙	06●	00	02.0	08.7	.	.	⌂$^{0-2}$0-8^{45}, 19^{45}-24; T°$_{NW}$ 12^{24}-12^{30}; ⊽°12^{24}-13, 15^{32}-16; ⊓ 15^{45}-16^{45}, F$_{W}$ 15^{50}, ●°16-16^{30}i
11	7	00⊙	03⊙	00	01.0	13.0	02.3	.	⌂$^{+2}$0-8^{45} 19^{45}-24
12	7	00●	06●	00	02.0	10.7	.	.	⌂$^{0-2}$0-8^{30} 20^{30}-24; ⊽°14^{45}, 14^{55}
13	8	00⊙	02⊙	00	00.7	13.1	00.0	.	⌂$^{0-1}$0-8^{40} 20^{45}-24
14	7	00⊙	00⊙	04	01.3	11.7	.	.	⌂^{1}0-8^{45}, ⊽°22^{45}-23^{55}i; T°22^{45}-23^{45} ⊽°22^{45}-23^{45}
15	8	00⊙	01⊙	03	01.3	12.1	00.3	.	F$_{SE-NNW}$ 0-0^{24}, 20^{34}-21^{25}; ⊽°15^{30}-15^{45}, 18^{52}-19; ⊓ 18^{55}-19^{45}
16	7	10	10●	10●	10.0	00.0	00.9	.	⊽°12^{54}-13, 15^{30}-15^{45}; T°$_{W}$ 12^{45}-13^{45} ●$^{0-2}$13-23^{30}i; F$_{WNW}$ 14^{35}-14^{45}
17	7	09	10	10	09.7	00.0	07.5	.	=°0^{30}-8^{30} ●$^{0-1}$$12^{30}$-$12^{35}$i, 23^{45}-24; F$_{W}$ 12^{32}-24i
18	6	10●	10●	10	10.0	00.0	03.2	.	●$^{0-1}$0-14^{45}i; ⊓ 16^{30}-20^{45}i; F$_{W}$ 0-22^{30}i; ●$^{0-1}$$22^{45}$-24
19	9	10	10	02	07.3	03.4	10.4	.	●^{1}0-4^{45}, F$_{W}$ 1^{25}-5^{40}, 9^{43}-13^{29}; ⌂$^{0-2}$$19^{32}$-24
20	8	00⊙	03●	02	01.7	11.8	.	.	⌂$^{0-2}$0-9^{30}, 22-24
21	6	09	00⊙	00	03.0	07.6	00.0	.	⌂$^{0-1}$0-5^{45} 20^{45}-24; ●°5^{45}-6^{40}
22	8	00⊙	00⊙	00	00.0	12.9	.	.	⌂$^{+2}$0-8^{45}, 19^{30}-24
23	8	00⊙	03⊙	00	01.0	12.9	.	.	⌂$^{0-2}$0-8, 19^{45}-24
24	8	10	01●	00	03.7	09.0	.	.	⌂$^{0-2}$0-8^{30}, 20^{45}-24
25	8	00⊙	00●	10●	03.3	11.6	.	.	⌂°0-7^{45}, F$_{SE-W}$ 6-17^{42}, 22; T°17^{45}-17^{30}; ⊽$^{0-2}$$17^{30}$-$18^{59}$; ⊓ 17^{30}-20^{45}; F$_{SE}$ 17^{30}-19^{45} [●$^{0-2}$$18^{45}$-$21^{45}$
26	8	09	07	00	05.3	08.4	35.9	.	F$_{NW}$ 15^{43}-16^{44}; ⌂$^{0-2}$$19^{30}$-24
27	8	02⊙	04●	00	02.0	13.0	.	.	⌂$^{0-2}$0-10 19^{30}-24
28	8	04⊙	05●	00	03.0	09.3	.	.	⌂$^{+2}$0-8^{30} 19^{45}-24
29	8	00⊙	04●	00	01.3	12.9	.	.	⌂$^{+2}$0-8^{30} 20^{30}-24
30	8	00⊙	02⊙	00	00.7	12.1	.	.	⌂$^{+2}$0-9^{45} 20^{45}-24
31	8	00⊙	00⊙	00	00.0	12.4	.	.	⌂$^{0-2}$0-8^{30}, 20^{45}-24
MES. VRED.		04.5	05.0	03.0	04.2	255.0	133.7		

BEOGRAD 1970 AVGUST

1	8	00●	01⊙	00	00.3	10.9	.	.	⌂$^{0-2}$0-8^{45}, 20^{30}-24
2	8	04●	06⊙	08	06.0	07.1	.	.	⌂$^{0-2}$0-8^{45} 20^{45}-24; F$_{NNE}$ 14^{55}-15^{53}; ⊓ 15^{45}-16^{45}
3	7	07	05⊙	00	03.3	07.8	.	.	⌂$^{0-1}$0-10^{30} 20^{45}-24
4	7	00⊙	02●	00	00.7	11.9	.	.	⌂$^{+2}$0-9^{30} 19^{45}-24
5	8	00⊙	03●	00	01.0	12.4	.	.	⌂$^{0-2}$0-10^{20}, 19^{45}-24
6	8	00⊙	02⊙	00	00.7	12.4	.	.	⌂$^{+2}$0-9^{45}, 20^{30}-24
7	8	00⊙	00⊙	00	00.0	11.5	.	.	⌂^{2}0-9^{30}
8	7	07⊙	06⊙	03	05.3	09.4	.	.	F$_{NW}$ 2^{12}-3^{23} ⊽°23^{45}-24
9	8	01⊙	06⊙	07	04.7	10.0	.	.	⊽0-2, 19^{45}-21^{45}i; F$_{SE}$ 9^{44}-20^{49}i; ⊽°19^{45}-19^{45}; T°19^{45}-20^{45}; ⌂°23^{45}-24
10	8	00⊙	09●⊓	03	04.0	07.5	00.0	.	⌂$^{0-2}$0-9^{30}, 20^{45}-24; ⊓ 13^{32}-14^{45}; ⊽°13^{35}-13^{37}
11	7	09	10●	06	09.0	03.5	00.0	.	⌂$^{0-2}$0-8^{40} ●$^{0-2}$$12^{45}$-$13^{45}$; =°$20^{45}$-$21^{45}$
12	8	00⊙	04⊙	00	01.3	11.2	01.4	.	⌂$^{+2}$0-10^{40} 20-24; F$_{NNW}$ 9^{43}-16^{53}
13	8	09	02⊙	00	03.7	09.5	.	.	⌂^{2}0-9^{20} 24-24
14	8	00⊙	02⊙	00	00.7	11.2	.	.	⌂$^{0-2}$0-8^{40} 19^{30}-24
15	8	00⊙	03⊙	00	01.0	11.1	.	.	⌂$^{0-2}$0-8^{40}, 19^{30}-24
16	8	10●	05⊙	02	05.7	04.6	00.6	.	⌂$^{0-1}$0-5^{40} 20^{45}-24; ●$^{0-1}$$5^{40}$-$7^{40}$i
17	8	04●	06⊙	09⊓	06.3	09.9	00.0	.	⌂$^{+2}$0-8^{40} ⊓ $^{0-1}$$20^{00}$-$22^{40}$ F$_{NW}$ 20^{48}-21^{30}; ●^{2}20^{50}-22^{50}
18	8	10●	03⊙	00	04.3	05.5	03.3	.	●°3^{50}-7^{30}i; ⌂$^{0-1}$$19^{30}$-24
19	8	03⊙	00⊙	00	01.0	11.9	00.2	.	⌂$^{+2}$0-9^{40} 19^{45}-24
20	8	03⊙	00⊙	00	01.0	11.3	.	.	⌂$^{0-2}$0-8^{50}, 18^{45}-24
21	8	00⊙	04●	01	01.7	11.5	.	.	⌂$^{0-1}$0-4^{30} F$_{SE}$ 6^{31}-23^{56}
22	8	00	05⊙	09	06.7	09.5	00.1	.	●°3^{45}-4^{40}, 17-17^{45}, 21^{35}-22^{45}i; F$_{WSW}$ 15^{51}; ⊽$^{0-2}$$15^{35}$-$16^{45}$; ⊓ $^{0-2}$$15^{37}$-$16^{45}$; ⊽$^{0-1}$$15^{37}$-$16^{45}$
23	7	10●	04⊙	01	05.0	09.7	08.3	.	●°1^{50}-2^{45} 6^{30} 7; ⌂^{1}18^{45}-24
24	8	03⊙	10●	10	07.7	02.6	.	.	⌂^{1}0-7^{40} ●$^{0-1}$$11^{40}$-$17^{45}$i; F$_{WSW}$ 21^{55}-24
25	7	10●	09⊙	04	07.7	02.2	07.5	.	F$_{WSW}$ 0-16^{32}; ●$^{0-1}$$2^{40}$-$9^{40}$, 17^{45}-20^{45}, 23^{40}-23^{30}; ⊽$^{0-2}$$16^{45}$-$17^{45}$; ⊓ $^{0-1}$$16^{24}$-$17^{30}$; ⊽$16^{24}$-$17^{30}$
26	8	05⊙	05⊙	00	03.3	06.4	14.9	.	=°3^{45}-5^{30} ⌂^{1}18^{45}-24
27	8	00⊙	04⊙	00	01.3	09.7	.	.	⌂^{2}0-9^{45}, 19^{30}-24
28	8	01⊙	02⊙	02	01.7	08.8	.	.	⌂$^{0-2}$0 19^{40} 18^{45}-24
29	7	01⊙	04⊙	05	03.3	05.4	.	.	⌂$^{0-2}$0-8^{45}; =°3^{45}-6^{45}, F$_{SE}$ 6^{42}-9^{48}
30	7	10	10	05	08.3	00.5	.	.	●°11^{35}-12^{30}i;
31	8	09	10	10	09.7	00.7	00.2	.	⌂°0^{30}-3^{30}; ●°7^{35}-8^{45}, 15^{50}-16^{05}, 18^{15}-24i; F$_{ESE}$ 13^{19}-14^{22}
MES. VRED.		04.0	04.4	02.8	03.8	256.8	42.0		

1970 SEPTEMBAR BEOGRAD

φ = 44° 48' N λ = 20° 28' E Gr. ΔG = + 1h 22 min. BR. ST. 174

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7	14	21
1	749.8	749.8	750.0	16.8	20.0	16.9	17.6	20.7	16.5	14.8	13.5	13.0	13.2	94	74	91	86	- 0	NW 2	NE 1
2	750.9	751.1	751.7	17.0	22.4	17.4	18.6	23.1	15.4	12.7	13.1	13.9	12.8	90	68	86	81	NE 1	NW 2	W 1
3	751.9	751.3	750.8	15.4	25.8	18.7	19.6	26.7	13.2	08.8	12.6	10.1	13.0	96	41	80	72	SSE 1	SSE 2	SE 2
4	750.2	752.0	753.0	16.6	18.6	17.8	17.7	22.3	15.0	10.4	12.4	13.7	13.4	87	85	88	87	E 1	WNW 2	W 2
5	753.0	751.2	750.9	13.7	23.8	18.2	18.5	25.4	12.0	07.3	11.1	09.9	11.4	95	45	73	71	WSW 1	W 2	- 0
6	751.4	751.9	752.1	16.6	20.4	15.5	17.0	21.5	15.5	14.0	12.5	10.4	11.6	88	58	88	78	WSW 2	WSW 2	SSE 2
7	754.0	755.1	755.5	15.4	19.2	12.4	14.8	19.6	12.4	13.0	11.5	11.0	10.1	88	66	93	82	N 1	WSW 3	WSW 1
8	754.3	752.2	750.9	14.0	25.5	19.4	19.6	26.2	11.0	06.6	08.8	10.6	11.0	73	43	65	60	ESE 3	SSE 3	ESE 2
9	750.8	750.7	750.4	18.8	29.4	19.9	22.0	29.7	16.0	11.0	12.0	13.5	14.8	74	44	85	68	ESE 2	WSW 2	ESE 2
10	749.8	749.1	748.5	18.4	30.9	22.2	23.4	32.1	16.0	11.7	13.8	14.2	15.3	87	42	76	68	- 0	NNE 1	SE 2
11	749.0	748.3	747.8	19.2	33.0	24.6	25.4	34.0	16.4	11.8	13.4	12.3	14.6	81	33	63	59	SSE 1	SSE 2	SE 2
12	748.2	747.9	746.7	21.2	32.2	23.6	25.2	32.9	18.8	12.1	13.4	11.9	13.3	71	33	61	55	- 0	NNW 2	SE 2
13	745.7	746.8	748.4	21.3	31.6	19.6	23.0	32.0	19.1	12.7	13.0	12.4	13.9	68	35	82	62	SSW 1	SSE 2	NW 3
14	751.0	750.8	750.8	16.4	23.6	18.8	19.4	25.4	15.8	12.0	11.0	11.5	13.6	79	53	84	72	WNW 2	ENE 1	SE 2
15	751.0	750.2	750.3	18.3	28.7	21.6	22.6	28.9	15.5	16.4	13.3	13.8	11.1	84	47	57	63	ESE 2	SSE 2	SE 2
16	749.9	749.3	749.6	20.7	29.8	21.3	23.3	29.9	20.0	13.6	09.7	10.8	11.3	53	34	59	49	SE 3	SE 3	SSE 2
17	754.9	755.5	756.4	14.4	14.8	12.8	13.7	21.3	12.8	-	11.3	10.4	10.7	92	83	97	91	NW 2	W 3	WSW 2
18	756.6	756.8	757.6	13.2	17.2	15.1	15.2	17.4	12.7	-	10.0	11.6	11.6	88	79	90	86	N 2	NNW 2	WSW 2
19	757.1	756.0	755.8	14.8	20.3	16.0	16.8	21.4	14.5	11.6	11.7	12.0	12.7	93	67	93	84	W 1	W 2	- 0
20	755.1	753.6	752.6	13.0	20.8	14.5	15.7	22.2	11.7	07.9	10.9	11.5	09.7	97	62	79	79	WSW 1	W 2	NNE 1
21	752.8	752.2	752.2	14.0	18.1	13.0	14.5	19.1	12.4	09.4	09.0	09.3	09.5	75	60	85	73	NNE 2	NW 2	NW 1
22	751.5	751.8	754.5	11.8	18.9	12.8	14.1	20.4	10.4	07.4	09.4	07.7	08.3	91	47	75	71	SW 1	NNW 3	NW 1
23	755.5	754.5	755.1	08.9	18.0	09.0	11.2	18.5	07.2	03.5	06.8	05.7	06.8	79	37	79	65	W 2	WNW 2	W 1
24	756.0	755.2	755.6	07.0	16.3	08.2	09.9	19.3	04.3	00.5	06.5	05.3	06.9	87	38	85	70	W 1	NNW 2	NNE 1
25	755.5	754.4	754.5	06.6	18.3	08.3	10.4	18.3	03.9	00.4	06.0	05.3	06.8	82	33	82	66	- 0	WNW 1	S 1
26	753.5	753.2	754.4	10.9	15.2	12.4	12.7	16.0	07.7	04.0	06.4	08.0	09.0	65	62	84	70	SW 1	WNW 1	NNE 2
27	758.2	759.3	[illegible]	09.9	16.2	08.2	10.6	17.4	08.2	06.8	08.4	06.2	07.1	92	45	87	75	NNW 1	NNW 2	NW 1
28	761.2	761.5	[illegible]	07.1	15.2	07.8	09.5	16.2	06.1	01.8	06.9	06.0	04.2	91	47	53	64	WNW 1	NW 2	NNE 2
29	763.5	762.1	761.4	01.5	13.5	05.2	06.4	14.1	00.6	-02.5	04.5	04.5	05.0	88	38	76	67	WNW 2	NNW 2	NNW 1
30	758.4	755.1	751.3	03.0	17.1	09.8	09.9	18.5	00.9	-02.6	04.5	04.6	04.8	80	31	53	55	- 0	ESE 2	SSE 2
MES. SRED.	753.4	752.9	753.1	13.9	21.8	15.4	16.6	23.0	12.1	08.5	10.2	10.0	10.6	84	51	78	71	1.3	2.0	1.5

1970 OKTOBAR BEOGRAD

1	747.8	744.7	744.4	10.6	20.0	10.7	13.0	21.1	04.8	00.8	05.0	07.0	08.7	52	40	91	61	SE 2	SSE 2	NNE 4
2	746.3	745.8	744.2	09.9	15.1	10.2	11.4	16.9	09.8	09.0	08.6	07.4	07.4	94	58	79	77	WNW 2	WNW 2	SSE 2
3	742.6	742.3	745.0	09.6	10.5	09.0	09.5	11.6	08.9	06.1	08.7	08.8	08.2	98	93	95	95	- 0	NW 2	WSW 2
4	745.9	746.6	748.5	05.8	14.1	09.2	09.6	15.8	05.2	03.0	06.7	06.3	07.1	97	52	82	77	SW 1	W 2	NW 2
5	751.2	751.5	750.3	09.4	14.6	11.5	11.8	15.8	08.4	07.4	07.0	06.0	07.6	80	48	74	67	WSW 2	WNW 2	SE 1
6	751.0	750.3	751.0	12.3	21.4	13.0	14.9	21.7	11.0	08.3	07.8	08.3	09.0	73	43	80	65	WSW 2	WSW 3	SE 2
7	751.5	751.1	751.6	11.5	24.2	16.0	16.9	25.2	09.6	06.2	08.9	08.3	09.5	88	37	70	65	SE 1	ESE 2	SE 2
8	753.2	753.5	754.2	11.2	23.7	13.9	15.7	24.7	10.4	06.1	09.3	09.2	10.4	93	42	87	74	- 0	NNW 1	NNW 2
9	755.0	756.5	756.4	14.2	24.4	15.4	17.4	24.6	11.3	06.3	09.5	11.2	10.5	78	49	80	69	SE 2	ESE 3	SE 3
10	757.0	757.5	758.5	14.2	24.4	14.5	16.9	24.5	13.5	10.0	09.3	09.8	10.0	77	43	81	67	SE 4	SSE 3	SE 2
11	759.5	758.9	759.1	11.6	23.4	13.4	15.4	24.7	10.2	05.5	08.5	08.2	09.2	83	38	80	67	ESE 2	NE 2	ESE 1
12	759.6	759.0	758.3	10.0	21.5	14.5	15.1	21.9	08.8	05.8	08.5	11.0	10.7	93	57	87	79	NE 1	NNW 2	- 0
13	758.4	757.4	756.3	13.0	20.0	12.2	14.4	20.7	10.6	07.2	10.5	09.2	09.5	93	53	89	78	- 0	NNW 1	NNW 1
14	754.2	753.6	753.6	09.0	13.0	12.2	11.6	13.4	08.2	04.8	08.3	10.0	09.9	96	89	93	93	- 0	WNW 2	WSW 2
15	754.6	755.4	756.9	08.7	11.5	06.8	08.4	12.7	06.8	08.0	07.1	06.4	04.5	84	53	61	66	NNW 2	NNW 3	NNE 2
16	759.4	759.7	761.4	02.3	09.5	04.6	05.2	09.9	02.3	02.6	03.6	04.1	04.9	66	46	77	63	N 2	WNW 1	ESE 3
17	761.5	759.9	759.6	02.8	09.6	05.1	05.6	09.9	02.2	00.2	04.4	04.1	04.5	78	46	69	64	E 2	ESE 3	ESE 3
18	757.5	757.1	757.4	05.0	06.4	05.6	05.6	06.9	04.7	04.4	05.0	05.5	05.7	77	76	83	79	E 2	ESE 2	S 2
19	756.2	751.7	747.6	05.7	13.3	07.2	08.4	14.0	05.2	04.6	05.8	06.4	06.4	85	55	84	75	SE 1	SSE 2	SSE 2
20	743.1	740.1	739.4	06.6	21.5	12.6	13.3	21.9	06.2	03.6	06.2	06.6	08.1	85	34	74	64	ESE 4	S 2	SE 2
21	738.3	744.8	747.2	14.6	07.4	07.0	09.0	16.1	07.0	07.5	08.9	07.3	07.1	71	95	95	87	SSE 3	W 2	- 0
22	748.7	750.4	750.7	06.6	06.9	06.1	06.4	07.0	06.1	05.5	07.0	07.0	06.9	96	93	97	95	NNW 2	NNW 2	WNW 2
23	749.1	748.9	750.7	03.0	08.6	06.5	06.6	07.9	04.9	05.1	06.4	06.7	06.3	98	80	86	88	WSW 2	WNW 2	WNW 2
24	753.6	754.8	757.6	03.2	07.0	05.5	05.3	07.4	03.1	02.1	05.5	06.1	05.6	95	81	83	86	WNW 2	WNW 3	WNW 2
25	758.1	759.2	758.3	00.3	07.9	07.6	05.8	08.7	-00.4	-02.7	04.4	06.4	05.0	93	55	63	70	SSW 2	W 3	SSW 1
26	757.4	755.4	756.4	06.0	17.3	10.1	10.9	17.3	05.3	-02.6	05.3	06.8	07.0	75	46	75	65	SSE 2	SE 2	ESE 3
27	755.1	755.8	758.9	04.5	16.6	11.4	11.0	17.1	04.0	-02.4	06.1	06.9	06.9	97	49	68	71	SSE 1	NW 2	NNE 2
28	761.2	759.4	756.4	06.7	16.2	11.0	11.2	14.3	06.0	-02.6	06.5	05.3	05.8	88	39	59	62	WNW 1	SSE 2	SE 2
29	754.6	754.2	755.0	08.0	16.9	13.4	12.9	17.2	06.5	-02.5	06.5	07.4	07.3	81	51	63	65	SE 2	W 2	NW 2
30	761.1	759.5	757.7	06.9	17.3	13.1	13.1	17.8	07.5	-02.7	06.1	07.0	07.1	71	48	63	71	SSW 1	ESE 2	SE 2
31	754.8	754.0	755.4	07.5	20.7	12.2	13.2	21.1	07.4	-02.5	07.3	07.1	07.8	93	39	73	68	E 1	WNW 2	WSW 2
MES. SRED.	753.5	752.9	753.4	08.7	15.6	10.4	11.1	16.5	07.0	04.5	07.0	07.2	07.6	85	56	79	73	1.6	2.1	1.9

BR. ST. 174 H_s = 132 m H_b = 131.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	7	10	09	10	09.7	09.1	02.2	.	●0-1 0-12^15 i, △0 18^30-24
2	8	09⊙	06⊙	09	06.7	01.9	00.1	.	△0-1 0-8^40, 20^15-24; ●0 12-12^05
3	8	06⊙	03⊙	06	01.0	10.1	00.0	.	△1-2 0-9^20 18^30-24
4	7	07	10●	10	09.0	02.2	.	.	△2 0-9^30, ●0 11^45-15^45 i, 20^50-21^15
5	7	05⊙	04⊙	09	06.0	09.5	00.4	.	
6	7	10	07⊙	10	09.0	01.4	00.4	.	●0 2^30-4^05 i, 6^55-11^45 i, 18^15-21^45 i
7	8	10●	03⊙	01	04.7	02.4	00.0	.	●0-1 2^45-13^10 i, △2 18^45-24
8	5	00⊙	00⊙	00	00.0	11.2	00.4	.	△2 0-8, 21^30-24; F SE 8^19-11^27
9	5	00⊙	04⊙	00	01.3	10.[illegible]	.	.	△0-1 0-8^45 18^45-24
10	8	00⊙	00⊙	00	00.0	10.7	.	.	△0-2 0-8^30, 19^30-24
11	5	00⊙	00⊙	00	00.0	10.7	.	.	△0-2 0-8^40 19-24
12	5	02⊙	02⊙	00	03.3	08.6	.	.	△0-2 0-8^30, 22^45-24
13	5	09	07⊙	10	09.0	05.5	00.1	.	△0 0-1^05, ●0-1 1^05-1^40 6^45-7^15; F N 17^18-19^37
14	7	04⊙	01⊙	00	01.7	05.9	00.1	.	△0-1 20^30-24
15	8	00⊙	00⊙	02	00.7	10.0	.	.	△1 0-9^45
16	8	00⊙	00⊙	00	00.0	09.2	.	.	F SE-W 5^38-10^50 23^43; ☈ 23^30-24
17	7	10	10	10●	10.0	00.0	02.7	.	☈ 0-2^15 F NNE 0^00-1^43, ∇1 1^05-2^05 i, ●0 18^55-21^30, =0 21^30-24
18	7	10	10	10	10.0	00.0	00.3	.	=0 0-10, 14^30-24
19	7	10	08⊙	05	06.7	02.6	.	.	=0-2 0-9^40 22^30-24; △0-2 6^30-8^50 19-24
20	6	04⊙	09⊙	00	04.3	03.7	.	.	△0-2 0-9^30, 19^30-24; =2 0-18^30
21	7	09	09	04	07.3	03.9	.	.	△0-2 0-2, 20^30-24
22	7	04	05⊙	01	03.7	04.9	.	.	△0-1 0-9^30 21^30-24; =1-2 1^30-12^30, F NW 12^05-16^08
23	9	01⊙	03⊙	00	01.3	10.2	.	.	△0-2 0-8^30 19^45-24
24	8	00⊙	06⊙	00	02.0	06.5	.	.	△0-2 0-9, 18^30-24
25	5	00	01⊙	09	00.3	03.2	.	.	△1 0-9, 17^30-24
26	7	10	09	10	09.7	09.0	.	.	△0-1 0-7^30 ●0 16^10-17
27	7	09	02⊙	07	06.0	04.5	00.0	.	△0-1 2^30, 17^30 17^45-24; =0 4^30-12^30
28	8	01⊙	07⊙	00	02.7	06.1	.	.	△0-1 0-8^45 19^30-24
29	7	00⊙	00⊙	00	00.0	09.7	.	.	△0 0-2^30 19^30-24; ⌣0-1 2^30-7^30
30	7	02⊙	01⊙	00	01.0	09.7	.	.	△0-1 0-1^30, 20^15-24; ⌣0-2 1^30-8
MES. VREM.		04.5	04.4	03.9	04.3	139.2	03.2		

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
1	8	08⊙	10	10●	09.3	01.8	.	.	△0-1 0-8, ●0-1 10^55-24, F NNE 20^02-20^28
2	8	10●	07⊙	05	07.3	03.5	10.[illegible]	.	●1 0-6^40, △0-1 20^30-24
3	6	10	10●	10	10.0	00.0	02.2	.	△1 0-2^35, ●0-1 2^55-17^45 i, =0 17^45-18^45
4	8	04	07	09●	06.7	05.4	12.[illegible]	.	=0 1^30-5^15, △0 4^30-8^30, ●0 11^55-18^45-21^15 i; F WNW 14^30-23^18 i, ∇0 15^50-16^00
5	7	10	09	10	09.7	01.9	01.[illegible]	.	F WNW 13^34
6	7	04⊙	00⊙	00	01.3	09.7	00.0	.	●0 2^45, △1-2 18-24
7	8	00⊙	00⊙	00	00.0	10.1	.	.	△1-2 0-10^30 19-24
8	9	00⊙	00⊙	00	00.0	09.7	.	.	△1-2 0-9^45 19-24
9	7	00⊙	00⊙	00	00.0	09.5	.	.	△0-2 0-9^15 19^45-24; F SE [illegible] 24 i
10	7	00⊙	00⊙	00	00.0	09.8	.	.	△0 0-17^45, 17^45-24; F SE 0-1[illegible]
11	7	00⊙	00⊙	00	00.0	09.9	.	.	△0-2 0-9^45 17^45-24
12	7	00⊙	01⊙	00	00.3	06.9	.	.	△0-2 0-9, 17^45-24; =0-1 5^30-7, 16^45-17^15, 22^30-24
13	7	09	01⊙	00	03.3	06.2	.	.	△0-2 0-8^30 18^45-24; =0-1 0-8
14	5	00	10	10	06.7	06.0	.	.	△2 0-7, =0-2 4^45-17, 9^30-24; =2 7-9^30
15	7	10	09	08	09.0	03.3	.	.	=0-1 0-8
16	7	06	00⊙	09	05.0	06.0	.	.	F ESE 20^09-24
17	7	01	04⊙	10	05.0	05.5	.	.	F ESE 0-3^40 7^53-23^24; △0 2^45-5, =0 4^30-6^30, ⌣0 5-7^45
18	7	10	10●	10	10.0	00.0	00.0	.	●0 3^45-4, 9^50-12^30 i; ●0 12^30-19^15 i
19	7	09	05⊙	00	04.7	05.1	00.2	.	△0-1 18^45-24
20	8	00	01⊙	05	02.0	09.[illegible]	.	.	△0-2 0-9^30 19^30-24; F SSE 22^25-23^08
21	7	09	10●	06	05.3	00.1	.	.	△0 0-6^45 F SSE 2^29-9^09 ●0-1 11^45-16^30 i, 23^53-24; =0 19^45-23
22	5	10≡	10●	10●	10.0	00.0	13.0	.	●0-1 0-24 i, ≡0 4^30-7, =2 7-21
23	7	10●	10	09	09.7	01.3	20.3	.	●0 0-17^30, △1 20^30-24
24	6	10●	07⊙	09	08.7	00.2	00.[illegible]	.	△1-2 0-4^05, =0-1 3^45-24, ●0 4^05-4^10 6^30-8^10 18-19 i; F W 13^45-14^00
25	7	00	10	10	06.7	03.1	01.2	.	△2 0-5^30, ⌣0 5^30-9^15
26	8	04	03⊙	00	02.3	03.2	.	.	△0 4^30-9^15 18^30-24
27	8	04	04⊙	06	04.7	03.1	.	.	△1-2 0-5^30 19^15-24; ⌣0 5^30-7^30
28	6	09	04⊙	00	04.3	06.2	.	.	△0-1 0-9^30 20^30-24
29	5	08	09⊙	10	09.0	03.1	.	.	△0 0-8^45
30	7	09	00⊙	00	03.0	07.0	.	.	=1 5^15-9^30 23^15-24
31	7	01	01⊙	00	00.7	0[illegible]	.	.	△1-2 0-9^15, 18^45-24
MES. VREM.		05.3	04.9	05.0	05.1	159.8	06.2		

φ = 44° 48' N λ = 20° 28' E Gr. Δ G = + 1h 22 min. BR. ST. 174

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	756.0	753.5	752.2	07.4	21.6	09.8	12.2	21.6	07.4	03.1	07.3	08.1	08.3	95	42	92	76	SE 2	ESE 1	ENE 2
2	754.9	753.4	752.3	08.0	18.8	12.6	13.0	19.5	07.5	03.1	07.3	07.6	07.7	91	47	70	69	SW 2	SSW 2	SE 1
3	754.0	750.6	748.6	10.4	22.3	14.4	15.4	22.3	09.5	05.4	07.8	07.8	07.5	82	39	61	61	SSW 2	SSE 2	SSE 2
4	751.7	753.9	755.6	10.4	17.0	10.6	12.2	18.1	08.6	04.4	07.5	08.1	07.7	79	56	80	72	WSW 2	WNW 1	SSE 2
5	755.2	751.3	748.2	09.4	10.7	11.7	12.9	18.8	07.5	02.4	04.7	07.4	07.2	53	46	69	56	SE 2	SE 2	- 0
6	750.6	751.3	752.9	09.6	08.4	06.0	07.5	11.9	06.0	02.5	07.4	06.2	06.0	82	75	86	81	NW 2	WSW 2	W 2
7	754.2	754.1	754.5	01.0	09.1	03.4	04.2	09.5	00.7	-02.9	04.6	04.5	04.6	93	52	7	75	SSW 1	WNW 1	SE 2
8	753.3	754.6	757.2	04.2	05.5	05.3	05.1	05.8	02.8	-01.4	04.7	06.3	06.4	76	93	96	88	SE 3	W 1	WNW 1
9	753.3	749.5	747.5	05.3	10.8	09.4	08.7	11.4	04.9	-01.5	06.1	07.5	08.4	91	77	95	88	SSE 2	SE 2	SE 1
10	745.0	748.4	751.0	08.7	09.7	07.6	08.4	11.0	07.4	-01.3	08.1	07.1	07.4	96	79	95	90	NE 2	NW 1	WNW 2
11	754.1	755.4	756.2	03.7	09.0	04.5	05.4	09.7	03.6	00.5	04.9	04.6	04.8	82	54	75	70	WNW 2	WNW 2	SSW 2
12	755.5	754.1	752.8	04.6	16.0	08.4	09.4	16.6	03.3	-01.7	03.9	05.4	05.0	61	40	61	54	SSE 1	SE 2	SE 2
13	753.0	752.0	751.3	04.9	15.7	08.6	09.4	16.2	03.7	-01.4	04.6	06.4	05.1	71	47	61	60	SE 2	NNE 1	SE 2
14	749.1	747.0	745.6	06.0	19.7	14.3	13.6	20.2	04.4	-01.4	04.3	05.4	05.8	61	31	48	47	SE 2	S 3	SSE 3
15	743.2	741.5	740.0	11.2	19.0	13.4	14.2	19.2	11.0	07.9	08.7	08.6	07.3	87	52	63	67	SSE 3	SSE 3	SSE 3
16	739.2	740.4	744.6	10.9	09.0	05.9	07.9	13.4	05.8	08.5	07.9	08.2	06.6	80	95	94	90	SSE 2	W 2	W 2
17	748.2	749.6	750.5	04.2	09.1	05.1	05.9	09.8	04.2	02.2	05.0	04.5	04.7	81	52	72	68	W 2	WNW 2	SSE 2
18	750.5	750.2	750.4	09.0	13.0	13.4	12.2	13.5	05.1	00.0	04.2	05.4	06.6	48	48	57	51	S 2	SSW 2	SSW 2
19	749.1	747.6	747.7	12.9	21.4	14.5	15.8	21.5	12.6	07.8	06.9	07.4	06.6	62	39	53	51	SSE 2	SSW 2	SSE 2
20	748.2	748.3	749.5	11.4	21.9	13.9	15.3	22.3	10.2	04.4	06.8	06.0	09.7	67	31	81	60	SSE 2	WSW 1	SE 2
21	749.7	747.9	745.8	13.0	20.4	15.2	16.0	21.5	12.3	05.6	07.0	07.3	08.6	63	41	66	57	SSE 3	ESE 2	SE 3
22	741.4	742.0	744.8	12.7	15.4	08.5	11.3	16.0	08.5	10.7	08.9	09.3	07.5	81	71	90	81	SSE 4	SE 2	NW 2
23	748.4	748.9	752.6	06.4	06.0	07.7	07.0	08.5	05.3	05.8	05.8	06.8	07.6	81	97	96	91	NW 3	WNW 2	NW 2
24	755.4	756.1	757.4	06.7	07.2	07.6	07.3	07.8	06.0	06.6	07.0	06.7	07.0	94	88	90	91	WNW 2	W 3	W 1
25	758.5	759.2	760.0	06.2	09.5	05.4	06.6	10.0	05.4	03.1	06.3	05.6	06.0	89	62	90	80	- 0	SSE 1	ESE 1
26	761.2	762.1	762.1	01.3	02.7	03.4	02.7	05.4	00.3	-01.8	04.9	05.5	05.6	97	98	95	97	NE 2	WNW 2	W 2
27	761.5	761.0	760.9	03.6	04.4	04.2	04.1	04.6	03.4	03.4	05.0	05.3	05.6	85	85	91	87	WNW 2	W 2	WSW 1
28	759.1	757.3	756.0	03.4	04.9	04.7	04.4	05.0	03.4	03.2	05.2	05.0	05.3	89	77	83	83	WSW 1	- 0	ESE 1
29	753.6	752.2	752.0	04.0	08.8	04.2	05.3	09.7	03.6	03.1	05.3	05.4	05.6	86	64	91	80	- 0	WNW 1	SSE 2
30	750.8	749.9	749.6	09.2	13.1	10.4	10.8	15.2	03.0	-01.0	05.5	07.9	06.7	63	70	71	68	SSE 1	- 0	SE 2
MES. SRED.	751.9	751.4	751.7	07.3	12.9	08.8	09.5	13.9	05.9	02.6	06.1	06.6	06.6	79	62	78	73	1.9	1.7	1.8

1	751.2	751.2	750.7	09.9	12.5	09.2	10.2	13.7	09.2	05.9	07.6	08.5	08.1	83	78	93	85	NW 1	- 0	ESE 2
2	750.4	751.7	753.8	09.4	11.0	07.8	09.0	12.3	07.0	04.1	07.4	07.4	07.1	84	75	90	83	- 0	NNW 2	WNW 1
3	753.8	750.9	746.5	03.0	11.9	08.1	07.8	12.8	02.8	-01.5	05.4	05.1	05.2	95	48	64	69	SSE 1	SSE 2	SSE 2
4	751.5	753.9	756.2	05.0	03.1	02.6	03.3	09.1	02.6	-01.4	04.0	04.8	03.8	61	84	68	71	WNW 3	NW 2	NW 2
5	757.9	757.3	757.2	-01.6	04.7	02.8	02.2	05.5	-01.7	-05.4	03.7	03.1	03.8	90	48	69	69	WSW 1	NW 1	ESE 3
6	759.0	759.8	760.1	02.0	03.3	03.1	02.9	03.6	01.8	01.8	04.7	04.6	04.8	88	80	84	84	WNW 2	NW 2	- 0
7	759.4	757.2	757.7	-00.2	07.6	02.6	03.2	08.2	-00.4	-03.2	04.2	05.0	04.5	92	63	81	79	ESE 2	ESE 3	ESE 2
8	759.1	761.2	763.5	00.2	03.8	03.3	02.6	04.8	00.0	-03.3	04.2	04.9	05.4	91	82	92	88	SE 2	NW 2	W 2
9	764.2	763.1	762.4	01.0	04.9	02.9	02.9	05.1	00.9	-01.2	04.2	04.4	04.7	86	67	83	79	W 2	WNW 2	W 2
10	762.5	761.7	762.8	02.4	04.6	04.0	03.8	05.2	01.9	01.9	04.8	05.2	04.9	89	82	80	84	W 2	W 4	WNW 2
11	764.2	765.0	765.6	01.8	03.8	03.5	03.2	04.8	01.3	-02.8	04.7	05.0	04.7	90	83	80	84	W 2	WNW 2	W 2
12	764.3	762.9	762.9	02.4	03.0	02.3	02.5	03.5	02.3	02.3	04.6	04.7	04.6	84	83	85	84	WNW 1	W 1	NNE 2
13	762.1	761.0	761.4	01.5	01.5	00.8	01.2	02.3	00.8	01.4	04.7	04.7	04.6	92	92	95	93	WNW 1	- 0	WSW 1
14	761.1	760.0	758.8	-00.2	-00.3	-00.8	-00.5	01.0	-01.0	-00.2	04.4	04.0	04.1	96	89	94	93	WNW 2	WNW 1	- 0
15	758.8	759.2	760.0	-00.7	-00.5	-00.2	-00.4	-00.1	-01.0	-00.9	04.0	04.0	04.2	93	91	92	92	W 2	WNW 2	WNW 2
16	760.6	761.2	761.6	00.4	00.1	-00.2	00.0	00.8	-00.3	00.1	04.3	04.4	04.2	91	95	92	93	NW 2	N 2	WNW 2
17	761.0	760.5	759.8	00.1	01.9	00.6	00.8	02.1	-00.8	-00.6	04.4	04.1	04.1	95	79	86	87	W 2	NW 2	WSW 2
18	757.8	757.3	758.2	00.2	00.6	-00.2	00.1	00.9	-00.2	-00.7	03.9	03.3	03.3	84	69	73	75	- 0	WNW 1	WSW 2
19	759.4	759.3	760.6	-00.2	01.4	00.6	00.6	02.6	-00.5	-01.0	03.3	03.3	03.8	73	65	79	72	SW 1	W 2	N 2
20	760.7	759.6	758.3	-00.4	02.2	-01.5	-00.3	02.7	-01.5	-02.8	03.9	03.9	03.6	87	73	87	82	WNW 1	- 0	ESE 2
21	754.8	752.0	750.4	-03.4	03.2	-01.6	-00.8	-03.8	-03.5	-07.4	03.2	04.2	03.7	89	72	91	84	- 0	NNE 1	NNE 1
22	749.8	749.6	749.6	-03.4	-01.6	-01.2	-01.8	-01.2	-04.3	-05.3	03.4	04.0	04.0	97	98	95	97	WNW 1	W 1	W 1
23	746.3	743.2	743.7	-01.8	-00.2	-00.8	-00.9	00.0	-01.9	-01.8	03.9	04.2	04.2	96	93	97	95	NNE 2	NNE 2	SW 1
24	747.5	750.1	751.3	-02.1	-00.2	-02.3	-01.7	00.8	-02.4	-02.5	03.6	03.3	03.3	92	72	86	83	WSW 2	WNW 1	E 2
25	748.2	745.8	747.0	-01.0	02.9	-02.5	-00.8	02.9	-02.5	-02.4	03.8	04.3	03.3	90	77	86	84	ESE 3	ESE 2	WSW 2
26	749.2	752.3	754.4	-03.6	-01.8	-05.8	-04.2	-01.0	-05.8	-01.8	03.3	03.1	02.5	93	76	86	85	WSW 3	WNW 1	SE 2
27	754.0	750.8	750.1	-04.1	02.2	04.7	01.9	05.6	-05.8	-12.2	02.7	04.3	05.2	80	80	81	80	ESE 2	SE 3	NNE 3
28	744.9	742.6	746.2	05.4	09.9	04.6	06.1	10.3	04.0	00.3	04.9	06.6	05.9	74	72	93	80	NE 5	SE 5	SE 2
29	746.7	744.4	740.9	08.3	10.4	11.3	10.3	11.6	03.0	-00.5	04.5	06.8	07.1	55	72	71	66	SE 2	SE 3	SE 4
30	736.9	733.8	739.2	12.4	14.7	07.2	10.4	17.3	07.2	00.0	06.8	07.6	06.7	63	61	88	71	SE 4	SE 2	SSE 2
31	742.5	738.2	733.0	05.1	08.4	04.2	05.0	09.5	03.9	-00.1	05.8	05.3	07.4	88	64	85	79	ESE 2	ESE 2	SE 3
MES. SRED.	754.8	754.1	754.3	01.5	04.2	02.4	02.6	05.2	00.5	-01.2	04.5	04.8	04.7	86	76	85	82	1.8	1.4	1.9

BEOGRAD

1970 NOVEMBAR

BR. ST. 174

H_s = 132 m H_b = 131.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	7	00⊙	00⊙	00	00.0	08.4	•	•	⌓0-2 0-9^30 16^45-24; =0 4^30-12^30
2	7	05	03⊙	09	05.7	07.6	•	•	⌓0-2 0-8^45 18^45-24
3	8	09	09⊙	00	06.0	05.0	•	•	⌓0-1 0-9^45 19^30-24
4	7	05⊙	10	00	05.0	02.8	•	•	⌓0-1 0-8^30 18^45-24
5	8	04⊙	02⊙	10	05.3	06.2	•	•	⌓0-1 0-9^30 18^30-24
6	8	10	10	00	06.7	00.0	•	•	⌓0-1 0-7 20^45-24; =0 6^30-8^30 ●0 7^35-9^45 13^40-13^50; ●0 9^45-10^30 i
7	9	00	00⊙	00	00.0	07.3	00.5	•	⌓1 0-1^30 16^45-21^45; ⌓0 1^30-8^30 =0-1 7^40-9^30;
8	9	10	10●	10●	10.0	00.0	•	•	⌓0 0-4^30 ●0-1 7^55-17^45 i; ●0 17^45-21 i; =1 20^50-24
9	7	02	09	09	06.7	00.6	02.8	•	=0-1 0-8^45 ●0 12^45-13^45 i; 13^45-20 i
10	6	10●	06⊙	10●	08.7	00.5	06.0	•	●0-2 5^40-10^30; 20^45-20^45; =0 10^30-20^45
11	8	06	08	00	04.7	04.9	11.4	•	⌓0 20^30-24
12	3	01	00⊙	00	00.3	08.7	•	•	⌓0 0-8^30 =0 9^45-10^30 ⌓0-1 20^30-24
13	9	00	00⊙	03	01.0	08.0	•	•	⌓1 0-4^30 19^45-24; ⌓1 4^30-8^30 =0 7^30-12^45 Φ0 22^30-24
14	8	07	03⊙	08	06.0	07.0	•	•	⌓0 0-4^30 Φ0 0-2^30 ⌓1 4^30-8^45 FSSE 21^48; ●0 22^45-24
15	8	10●	01⊙	06	05.7	04.7	07.2	•	●0-1 0-8^30; 22^45-24 i; FSSE 2^20-24 i
16	6	10●	10●	10	10.0	00.0	02.1	•	●0-2 0-0^45 2^20-10^45 i; 13^45-19^45; FSSE 0-1^40; ●1 19^45-23^45 i
17	8	01	04⊙	06	03.7	07.5	09.9	•	⌓0 20^45-24
18	3	10	10	10●	10.0	00.0	00.0	•	⌓1 0-5^30 ●0 5^30-6^45 i; FSSW 9; ●0 11^45-12^05; 20^30-20^45 i
19	8	06⊙	04⊙	00	03.3	06.9	00.0	•	⌓0 20-24
20	8	06⊙	03⊙	10	06.3	07.3	•	•	⌓0 0-8^30; ●0 17^45-19^45 i
21	8	02	06⊙	10	06.7	05.5	00.1	•	FESE 19^41-24; ●0 21^45-21^45 i; 23^55
22	9	10●	03⊙	10●	07.7	03.4	01.4	•	FESE-NW 0-6^48 20^55; ●0-1 1^00 5^30-8^45 15^45-24 i; ⌒0 NNE 15^45-16^45
23	6	10	10●	10●	10.0	00.0	08.6	•	●0 0-1^30 i; 9^30-24; FNW-WNW 2^58; 6^48-8^28 i; 14^25-16^26
24	5	10	10	10	10.0	00.0	12.2	•	●0 0-0^20; =0-1 6^20-17^45
25	6	10	06	00	05.3	01.0	•	•	=0 5^30-18^45; ⌓0-1 19^30-24
26	3	10≡	10≡●	10	10.0	00.0	•	•	⌓1 0-0^30; ⌓0-1 0^30-6^30; =0-1 1^30-3^30 11^30-12^45; 16^45-23^30; =0-2 3^30-16^45 i; ●0 7^45-8^45; ⌒0 12^45-14^45 i
27	6	10	10	10	10.0	00.0	00.1	•	=0 6^45-24; ●0 7^45-11^45; 16^30-17^30 i; 19^45-24 i
28	7	10	10	10	10.0	00.0	00.1	•	●0 0-0^30; 0 0-0^30 17^30-11^30 15^30; 18^45
29	6	10	03⊙	00	06.3	06.2	•	•	=0 2^30-16^30 20^30-23^30; ⌓0-1 16^45-19^30 ⌓0-1 19^30-24
30	8	05	10	08	07.7	00.0	•	•	⌓1 0-3^15; ⌓0 20^45-22^45; ●0 22^45-24
MES. VREDN.		06.6	06.1	06.0	06.2	110.1	62.4		

BEOGRAD

1970 DECEMBAR

Dan	Vidljivost 0-9	Oblačnost N (0—10) 14	7	14	21	Srednji Dnev	Insolacija broj sati	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	7	10	05⊙	06	07.0	02.0	00.4	•	●0 0-6^30 i; =0 9^45-11^45 18^30-19^45; ⌓1-2 16^45-24
2	7	05	03⊙	09	05.7	04.2	00.0	•	⌓0-1 0-6^30 6^45 9^30 17^45 19^20; ●0 0^30-0^45 19^20-20^45 i; =0 18^30-20^30
3	7	01	00⊙	00	00.3	07.1	00.1	•	⌓0 0^30-8^45; ⌓0-1 19^30-24
4	7	05	10	00	05.0	02.2	03.0	•	⌓0-1 0^30 20-23^30; ●0 1^30-3^40; FNNW 1^46-14^58; FNW 9^42-11^42; ⌓0 12^40-13^45; ⌓0 23^45-24
5	7	01	00⊙	10	03.7	06.8	00.4	•	⌓0-1 0-9^45
6	6	10	10	10	10.0	00.0	00.0	•	●0 0^45-0^40 15^45-16^45 i; =0 12^30-13^45 16^45-24; ⌓0 20^45-24
7	7	00	03⊙	00	01.0	06.6	00.0	•	=0 0-10^45 ⌓0 0-0^30 18^45-20^30; ⌓0-1 0^30-10^30 20^30-24; FESE 13^35-13^48
8	7	04	10	08	07.3	02.7	•	•	⌓0-1 0-9^30 23^30-24; =0 14^30-17^45; ●0-1 14^30-17^30
9	7	00	07⊙	10	05.7	02.1	00.6	•	⌓0-1 0-8^30
10	7	10	10	10	10.0	00.0	•	•	Fw 11^02-17^40 i
11	7	10	10	10	10.0	00.0	•	•	
12	6	10	10	10	10.0	00.0	•	•	=0 12^30-24
13	6	10	10	10●	10.0	00.0	•	•	=0 0-24; ●0 16^30-24
14	6	10●	10	10●	10.0	00.0	00.2	•	=0 0-16^50; ●0 0^30-3^40 6^30-10^45; 16^30-24 i
15	6	10●	10	10●	10.0	00.0	00.1	•	●0 0-23^30 i; =0 1^30-24
16	5	10	10*	10	10.0	00.0	00.2	•	=0-1 0-24; *0 12^30-14^30
17	6	10	10	10	10.0	00.0	00.6	•	=0 0-24; *0 8^30-11^30
18	6	10	10	10	10.0	00.0	00.2	•	=0 0-21^45; *0 10^45-11^45
19	6	10	10	10	10.0	00.0	00.0	•	=0 5^45-16^30; *0 6^45-10^45 i
20	6	05	06⊙	00	03.7	00.0	00.1	•	=0 7^45-16^30 19^30-24
21	8	01	00⊙	00	00.3	00.3	•	•	⌓2 0-12^45 17^40-23; =2 6^45-22; =2 22-24; V1-2 23-24
22	4	10≡	10	10	10.0	00.0	•	•	=2 0-6^30 V2 0-24; =2 6^30-10^45; =2 10^45-24
23	5	10*	10	10	10.0	00.0	02.1	02	=1-2 0-24; V1 0-2^30 *0 0^45-20^45 i; ⊠
24	6	10*	06	03	03.0	02.6	01.4	04	=1-2 0-24; *0 4^30-10^45 i; ⊠
25	7	08	10	10	09.3	00.0	00.1	02	=1-2 0-3^45 5^30-13^45 17^30-24; =0 3^15-5^30; FESE 4^49-11^01; ●0 14^55-15^40; *0 17^45-17^15; Δ 22^45-23^45; *0 23^45-24; ⊠
26	6	10*	06⊙	00	03.3	03.1	00.2	10	*0-1 0-8^15; =0-1 0-24; ⊠
27	7	09	10	10●	09.7	00.1	00.2	09	=0-2 0-7^45; FESE-SE 5^53 8^50-24 i; ●0-1 14^50-15^45 20^30-24; ⊠
28	7	10	10	04	09.0	00.2	01.5	•	●0-1 0-2^45 13^45-15^45 i; FSE 0-4^35 11^41-18^12 i; FSE 4^45-11^06; ⊠
29	8	10	10	10	10.0	00.0	00.5	•	●0 7^30-9^15 14^45-19^45; 22^45-23^45; FSSW-SE 17^22-17^30 14^45-24
30	8	06	07	00	04.7	02.3	00.7	•	FSE 0-13; ●0 8^45-9^15 16^45-18^45; Fw 16^42-17^40; V0 16^30-16^45; Δ1 17^30-17^40
31	8	09	10	10	09.7	00.0	02.0	•	FESE 13^48-23^57; ●0-1 21^35-24
MES. VREDN.			07.5	07.7	07.2	07.5	47.8	22.6	

1970 JANUAR TITOGRAD

$\varphi = 42^{\circ}\ 26'$ N $\lambda = 19^{\circ}\ 17'$ E Gr. $\Delta G =$ + 1h 17 min. BR. ST. 245

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)					
	7	14	21	7	14	21	Srednja	Max	Min	Min 5 cm	7	14	21	7	14	21	Srednja	7		14		21	
1	746.2	743.2	743.1	11.0	10.8	08.6	09.8	13.4	08.5	07.5	06.5	06.5	07.4	66	67	89	74	SSE	6	SSE	8	SSE	5
2	744.9	746.9	750.8	06.4	08.1	05.6	06.4	09.8	05.6	03.0	07.0	06.6	06.4	97	81	94	91	-	0	-	0	-	0
3	754.0	754.6	755.8	02.9	05.0	04.2	04.1	07.0	02.3	-02.2	05.4	05.9	06.0	95	90	97	94	-	0	-	0	-	0
4	755.2	755.0	754.9	03.4	07.0	06.2	05.7	07.4	03.0	-01.0	05.5	06.5	06.7	94	87	94	92	-	0	-	0	-	0
5	751.7	749.8	748.2	07.0	11.4	12.6	10.9	13.8	06.0	05.0	07.8	08.1	08.1	104	80	74	86	-	0	SSE	4	SSE	5
6	746.9	747.5	749.2	11.4	14.6	11.7	12.4	15.4	10.5	07.0	08.1	09.0	08.0	80	72	78	77	-	0	S	3	-	0
7	745.7	748.7	751.4	11.0	15.0	13.4	13.2	15.6	10.5	08.2	08.0	07.5	08.0	82	59	69	70	-	0	SE	6	SE	4
8	756.0	759.3	761.6	09.2	07.2	06.7	07.4	13.6	06.0	07.7	05.2	05.2	04.8	60	68	66	65	N	6	N	6	N	5
9	762.0	761.2	762.7	03.9	10.6	03.8	05.5	11.4	03.0	-00.4	04.3	06.1	05.6	72	64	94	77	N	4	-	0	-	0
10	762.6	761.6	762.2	01.4	11.0	06.4	06.3	12.0	01.3	-03.0	04.8	06.0	06.8	95	61	94	83	-	0	-	0	-	0
11	760.8	759.0	757.3	06.6	09.6	08.2	08.2	10.0	06.1	03.2	06.9	07.2	07.6	95	81	94	90	-	0	-	0	-	0
12	753.4	750.3	749.4	08.2	12.8	11.2	10.8	13.6	07.6	06.0	07.7	09.5	09.3	95	86	93	91	-	0	SE	5	S	4
13	748.5	747.3	748.0	09.6	13.0	10.4	10.8	14.0	09.2	07.5	08.3	09.3	09.0	93	83	95	90	-	0	NNW	2	-	0
14	750.8	751.4	752.6	09.6	11.6	10.0	10.3	12.0	09.0	05.4	08.5	09.5	08.8	95	93	95	94	-	0	-	0	-	0
15	753.1	751.9	752.7	08.9	11.0	10.2	10.1	11.3	08.6	05.7	08.1	09.4	09.0	95	95	96	95	-	0	-	0	-	0
16	750.4	747.5	745.5	12.2	11.2	11.2	11.4	13.0	08.0	08.5	09.5	09.1	09.1	89	91	91	90	ESE	4	-	0	ESE	4
17	746.1	747.0	749.1	08.0	10.0	09.8	09.4	11.2	08.0	07.0	07.5	08.1	05.0	94	88	55	79	-	0	-	0	NW	5
18	753.6	754.0	755.9	07.8	11.2	06.8	08.2	11.7	04.6	-00.4	05.0	04.3	04.8	62	43	65	57	NW	4	NNW	5	-	0
19	755.9	755.3	757.0	05.4	06.2	03.4	04.6	10.8	03.0	03.0	04.1	03.2	02.6	61	45	44	50	N	6	N	7	N	8
20	759.5	759.2	759.7	00.6	05.2	02.6	02.8	07.0	00.5	-02.0	02.2	02.8	02.5	46	43	45	45	N	6	N	6	N	6
21	758.8	759.1	758.2	00.4	06.0	00.0	01.6	07.0	-01.2	-06.0	03.2	03.8	04.2	67	55	91	71	-	0	S	2	-	0
22	758.1	757.6	758.7	-03.0	06.2	-00.2	00.7	06.8	-03.5	-09.5	03.5	03.9	04.2	95	55	93	81	-	0	S	2	-	0
23	759.7	759.4	760.7	-03.4	07.4	-00.4	00.8	08.8	-03.5	-09.0	03.2	03.5	04.1	89	45	92	75	-	0	S	1	-	0
24	761.2	761.2	762.5	-00.1	08.8	01.2	02.8	09.8	-01.5	-06.5	04.2	04.8	04.7	93	57	93	81	-	0	S	1	-	0
25	762.0	761.5	762.0	02.0	03.5	03.8	03.3	04.8	00.5	-05.0	04.8	05.6	05.7	90	95	95	93	-	0	WNW	2	-	0
26	763.6	764.2	760.4	00.0	10.0	04.8	04.9	11.4	-00.5	-05.0	04.3	04.8	05.0	95	52	77	75	-	0	-	0	N	2
27	766.3	765.3	763.7	02.3	09.2	06.5	06.1	10.4	01.0	-03.6	05.0	05.2	06.7	92	60	92	81	-	0	-	0	-	0
28	760.9	759.1	756.3	06.2	07.8	07.4	07.2	08.8	06.0	04.5	06.7	07.1	07.3	94	90	95	93	N	1	-	0	-	0
29	756.0	755.6	757.9	06.0	10.2	05.2	06.6	11.0	05.0	04.0	05.3	03.8	03.2	75	40	4	54	-	0	N	6	NW	3
30	756.2	753.8	752.3	02.6	06.2	04.6	04.5	07.0	01.0	-04.0	03.5	03.9	05.4	62	55	85	67	N	3	-	0	-	0
31	749.5	748.8	749.5	03.6	05.4	05.6	05.0	06.4	01.5	03.2	05.6	06.3	06.4	94	94	94	94	-	0	-	0	-	0
MES. VRED.	755.1	754.6	755.1	05.2	09.1	06.5	06.8	10.5	04.1	01.2	05.8	06.2	06.2	84	70	83	79	1.3		2.1		1.6	

1970 FEBRUAR TITOGRAD

1	750.4	751.3	752.5	06.0	05.0	02.6	04.0	07.8	02.0	04.5	03.5	05.4	05.2	49	83	94	75	N	6	-	0	-	0
2	755.6	756.0	756.3	01.4	04.8	03.2	03.2	06.0	01.4	-01.0	04.6	05.5	05.3	90	85	92	89	-	0	W	2	-	0
3	756.6	754.3	753.2	00.4	04.5	03.2	02.8	05.0	-00.5	-04.5	04.5	04.6	05.4	95	72	94	87	-	0	-	0	-	0
4	754.5	756.2	755.9	03.3	09.0	07.8	07.0	09.4	-00.4	01.0	05.8	07.1	07.3	100	83	92	92	-	0	-	0	-	0
5	754.4	754.3	754.9	09.0	13.0	12.4	11.7	13.8	07.2	06.0	08.1	09.4	08.0	94	84	74	84	-	0	-	0	SSE	3
6	754.8	756.4	757.0	12.6	14.2	12.8	13.1	15.0	12.0	09.5	09.0	09.2	09.4	83	76	85	81	SE	6	SE	5	SE	4
7	756.6	755.3	755.7	10.6	11.0	10.2	10.5	12.8	09.8	07.4	08.9	08.4	08.7	93	85	93	90	-	0	N	3	-	0
8	755.9	756.1	757.5	08.4	11.8	08.6	09.4	12.4	07.5	04.5	07.8	07.6	08.0	95	74	95	88	-	0	-	0	-	0
9	758.6	757.3	755.9	06.0	11.6	09.5	09.2	12.5	05.0	00.6	06.5	07.5	08.4	93	73	94	87	-	0	W	2	-	0
10	750.8	748.2	747.5	11.4	12.4	10.0	11.0	13.0	09.5	07.0	08.3	08.0	08.5	82	74	93	83	SE	5	SE	4	-	0
11	751.1	748.6	744.8	05.1	11.5	08.2	08.2	12.3	05.0	00.1	05.6	07.1	07.7	84	70	95	83	NNE	2	SSE	4	W	2
12	748.3	752.2	754.7	06.4	08.5	05.2	06.3	11.0	04.5	03.8	03.1	02.8	02.8	43	34	43	40	N	7	N	6	N	4
13	757.0	754.4	751.0	04.0	05.3	06.2	05.4	06.3	03.2	00.0	04.1	05.9	06.7	68	89	94	84	N	2	N	1	NW	1
14	751.9	751.1	747.4	06.4	12.4	13.0	11.2	13.2	03.5	02.2	05.9	08.2	07.9	82	76	71	76	-	0	S	3	SE	6
15	746.9	745.6	746.6	10.3	12.0	08.0	09.6	13.6	07.3	06.7	07.4	06.6	06.0	79	62	75	72	S	3	S	5	SW	5
16	749.0	749.7	748.2	05.0	06.8	04.2	05.0	09.5	03.5	03.0	06.0	05.5	05.6	91	74	91	85	SW	6	SE	6	SE	2
17	750.9	755.5	761.3	-00.6	02.0	-01.0	-00.2	05.0	-01.0	-03.4	02.2	02.2	01.8	51	42	42	45	N	8	N	7	NW	3
18	762.7	760.4	756.7	-04.6	03.6	-01.0	-00.8	08.0	-05.0	-09.2	01.8	02.0	04.1	56	33	9	61	NW	3	-	0	-	0
19	752.8	755.0	756.0	00.7	04.0	01.7	02.0	04.8	-01.3	-01.0	04.6	02.9	02.5	95	48	48	64	NNW	4	N	6	N	6
20	758.9	758.4	758.8	01.6	06.5	02.0	03.0	07.0	00.0	01.4	02.5	03.0	02.8	48	42	52	47	N	6	N	5	N	3
21	757.1	757.9	757.5	01.2	04.0	01.0	01.8	05.5	00.5	00.0	03.7	05.0	04.8	73	82	97	84	-	0	S	1	-	0
22	757.1	757.1	757.1	01.0	06.5	04.8	04.3	07.5	-01.5	-02.0	04.1	04.9	05.2	83	67	80	77	NNW	1	S	2	N	1
23	753.3	750.0	746.1	04.3	05.2	05.8	05.3	06.0	00.0	00.5	05.6	06.3	06.0	90	94	87	90	W	1	W	1	NW	4
24	749.7	749.0	749.0	07.7	11.6	07.0	08.3	11.8	05.8	04.0	03.9	03.8	03.7	49	37	49	45	NNW	5	NNE	4	N	5
25	748.7	748.9	749.9	05.4	09.8	05.0	06.0	09.5	05.0	04.5	02.6	03.1	02.6	39	36	40	38	N	8	N	6	N	6
26	750.1	749.5	750.0	01.8	10.0	03.8	04.8	12.5	01.8	01.4	02.6	03.5	04.1	50	38	69	52	NW	4	SW	2	NNW	3
27	748.1	746.6	747.9	03.9	08.2	04.8	05.4	08.3	03.5	01.6	03.0	02.6	02.7	49	32	42	41	N	7	N	7	N	6
28	750.5	751.4	754.1	01.4	07.0	03.4	03.8	08.2	01.0	00.5	02.6	03.4	03.5	51	45	59	52	NNW	4	SE	3	N	6
MES. VRED.	753.3	753.1	753.0	04.6	08.2	05.8	06.1	09.5	03.2	01.9	04.9	05.4	05.5	73	64	76	71	3.2		3.1		2.6	

BR. ST. 245 H_s = 52 m H_b = 52.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	7	10	10●	10●	10.0	00.0	13.5	.	F 0-20
2	7	10●	10	10	10.0	00.5	40.9	.	● 0-9³⁰ 16⁴⁰-18⁴⁰
3	7	10	10●	09	09.7	00.0	03.5	.	● 10²⁵-14⁴⁵i
4	8	10	10	10●	10.0	00.0	00.3	.	●° 16-24
5	6	10●	10●	10●	10.0	00.0	11.5	.	● 0-24
6	7	10●	10	08	09.3	00.0	35.6	.	●0-8³⁰ 12⁴⁵-12²⁵ 22⁴⁰-24
7	7	10●	10●	10●	10.0	00.0	40.0	.	● 0-24; F 12-15, 21⁴⁵-23; R 22³⁰-23³⁰; ∇ 22³⁰-23³⁰; ζ 23³⁰-24
8	8	10	10	08	09.3	00.0	33.8	.	● 0-0⁴⁵; 9²⁰-10; ζ 0-1³⁰; F 5⁴⁵-7⁴⁵; 12-23; F 7⁴⁵-12
9	8	07	03⊙	00	03.0	06.0	00.0	.	⊙
10	8	09	10	09	09.3	03.0	.	.	△ 18-24
11	8	10	10	10	10.0	00.0	.	.	△ 0-8
12	7	10●	10●	10●	10.0	00.0	03.0	.	● 0⁴⁵-24; F 13⁴⁰-19⁴⁰
13	8	10●	08⊙	10	09.3	00.8	43.7	.	●° 0-13
14	7	10	10●	10	10.0	00.0	00.8	.	● 7³⁰-17⁴⁰
15	7	10	10●	10●	10.0	00.0	01.5	.	● 8⁵⁰-24i
16	7	10●	10●	10●	10.0	00.0	20.2	.	● 0-24; F SSE 15-18⁴⁰; R 16⁴⁰-19
17	8	10●	10●	10	10.0	00.1	42.7	.	● 0-19³⁰i; F NW 17³⁰-24i
18	6	08	07●	10	08.3	05.7	00.0	.	⊙
19	8	10●	09	09	09.0	02.1	00.0	.	● 6³⁵-7³⁰; F 6⁴⁰-8⁵⁰; F 8⁵⁰-24
20	8	00	00⊙	00	00.0	00.1	00.0	.	F 0-24; ⊙
21	8	08	05⊙	00	04.3	06.7	.	.	⊔ 1-9, 18-24; ⊙
22	5	00	00⊙	00	00.0	06.9	.	.	⊔ 0-9³⁰ 19³⁰-24; ⊙
23	9	00	03⊙	04	02.3	06.9	.	.	⊔ 0-9³⁰ 19³⁰-24
24	8	10	02⊙	01	04.3	07.4	.	.	⊔ 0-9³⁰ 20-24
25	7	10●	10●	02	07.3	00.0	00.0	.	⊔ 0-6; 23-24; ⊠ 0-2, ●°⁻⁴ 6-16
26	6	00	09⊙	00	03.0	05.8	17.2	.	⊔ 0-9 ● 12³⁰-14, △ 17-24
27	8	09	10	10●	09.7	00.9	.	.	△ 0-8 ● 20²⁰-24
28	7	10	10●	10●	10.0	00.0	00.8	.	● 0-8⁴⁰i; 13⁴⁵-24i
29	8	10	08⊙	00	06.0	06.3	08.5	.	● 0-1⁴⁵; F 12⁴⁰-19³⁰
30	8	10	10	10	10.0	00.8	.	.	●° 21⁴⁰-24
31	5	10●	10●	10●	10.0	00.0	15.2	.	● 0-24
MES. VRED.		08.4	08.3	07.1	07.9	68.0	333.4		

1	7	10	10	10	10.0	00.0	17.1	.	● 0-3³⁰ 7⁴⁰-20i; F 4-10³⁰; * 8⁴⁰-9
2	7	10	10●	10	10.0	00.1	05.5	.	● 12³⁵-15²⁰
3	8	10	10	10●	10.0	00.0	00.1	.	● 16³⁰-24
4	7	08≡	10	10●	09.3	00.1	07.3	.	● 0-0³⁰ 18⁴⁰-24; ≡ 5-9⁴⁰
5	7	10	10●	10●	10.0	00.2	03.2	.	● 0-24
6	7	10●	10●	10	10.0	00.1	05.2	.	● 0-23i; F SE 0-8³⁰
7	7	10●	10●	10	10.0	00.0	05.0	.	● 6³⁵-14⁴⁰i
8	8	10●	08⊙	03	07.0	02.4	09.5	.	●° 5³⁰-13⁴⁵
9	8	10	07	10	09.0	02.8	00.1	.	● 7³⁰-8⁴⁰ 22³⁰-24
10	7	10●	10●	10●	10.0	00.1	05.2	.	● 0-24i; F SE 4³⁰-6³⁰i; 22³⁵-23; ζ 18³⁵-22³⁰; R 22³⁰-23
11	6	09	10	10●	09.7	02.1	07.5	.	F NW 0-0³⁰ 22⁵⁵-24; ● 14⁴⁵-24
12	8	00	00⊙	00	00.0	10.0	15.5	.	F 0-4⁴⁰i; ● 0⁵⁰-2³⁰; F 4⁴⁰-16i
13	7	10	10●	10●	10.0	00.0	00.2	.	● 10³⁰-22²⁵
14	8	03	10	10	07.7	02.5	17.2	.	●° 0-3; 16-22⁴⁵i; F 18⁴⁰-24; ζ 20³⁰-24
15	7	10	10●	10●R	10.0	00.6	10.3	.	ζ 0-3³⁰; F 0-5; ● 0³⁰-24i; F 8-20⁵⁰i; R 12-23³⁰
16	7	10●	10●	10	10.0	01.3	27.2	.	● 0-22⁴⁰; ζ 0-5; R 0-12i; F 6-17³⁰i; * 22⁴⁰-24
17	8	10	01⊙	00	03.7	05.6	14.9	.	* 0-3³⁰; F 3³⁰-20³⁰; ⊠
18	8	00	10	10*	06.7	06.3	00.0	.	* 17⁴⁰-24; ⊠
19	7	10●	10	00	06.7	00.0	29.6	.	* 0-8³⁰; F 7³⁰-24; ⊠
20	8	00	00⊙	00	00.0	09.0	00.1	.	F 0-11⁴⁰; F 11-15⁴⁰i; ⊠ 22³⁰-24
21	8	10	10	00	06.7	01.5	.	.	⊠ 0-3; * 8³⁰-9³⁰
22	8	08	10	10	09.3	01.6	00.2	.	⊔ 0-7³⁰
23	6	10	10●	10●	10.0	00.0	.	.	●° 7³⁰-21⁵⁰; F 19³⁰-20³⁰
24	8	01	02⊙	03	02.0	09.7	26.2	.	F 0³⁵-6³⁰; F 6³⁰-24
25	6	01	02⊙	00	01.0	09.7	.	.	F N 0-24i; F 1⁵⁰-11⁵⁰
26	8	09	07⊙	03	06.3	09.1	.	.	F 0-1²⁰
27	8	08	09⊙	00	05.7	06.7	.	.	F-F 2³⁰-5³⁰ 23⁴⁰
28	8	00	08⊙	10*	06.0	06.1	.	.	F 19⁵⁰-24; * 20³⁵-24
MES. VRED.		07.4	08.0	05.9	07.4	86.7	207.9		

φ = 42° 26' N λ = 19° 17' E Gr. ΔG = + 1h 17 min. MK. ST. 245

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)					
	7	14	21	7	14	21	Srednji Dnevni	Max	Min	Min 5 cm	7	14	21	7	14	21	Srednji Dnevni	7		14		21	
1	755.4	755.0	754.8	01.6	07.0	03.5	03.9	08.2	01.4	-02.2	02.3	02.8	02.1	45	37	36	39	NW	5	N	5	N	6
2	754.5	751.9	751.2	00.0	07.4	02.1	02.9	07.6	-00.1	-04.0	01.9	02.8	03.8	41	36	71	49	N	5	SSE	3	NE	1
3	749.0	748.2	747.6	01.6	05.4	06.8	05.2	07.0	01.0	-02.0	03.8	05.9	06.0	74	87	81	81	-	0	SE	5	SE	7
4	746.6	743.3	736.0	07.8	07.6	06.2	07.0	09.0	06.0	03.2	05.5	07.3	06.8	70	93	96	86	-	0	NW	1	SW	3
5	743.6	747.9	748.9	07.0	09.8	09.6	09.0	10.2	04.5	03.0	05.5	06.3	07.2	74	70	81	75	S	7	SE	7	SSE	8
6	753.3	755.1	754.7	06.8	10.4	08.2	08.4	11.1	06.0	02.8	06.5	08.3	07.2	88	88	89	88	S	5	W	1	N	1
7	754.4	756.2	757.7	07.2	12.6	05.4	07.6	14.0	05.4	03.6	06.8	04.8	05.4	89	44	80	71	-	0	S	3	-	0
8	757.5	754.8	755.1	05.0	11.5	04.6	06.4	12.0	01.8	02.4	03.8	03.6	05.4	58	35	85	59	NW	5	SW	1	-	0
9	754.9	753.6	756.0	00.0	14.8	07.0	07.2	16.0	-01.6	-02.6	03.8	05.1	05.4	82	40	72	65	-	0	S	1	N	3
10	758.7	758.8	759.6	05.3	14.6	08.4	09.7	18.0	04.5	05.3	04.8	05.9	06.4	72	42	78	64	-	0	S	2	-	0
11	760.3	759.4	758.4	06.2	13.4	09.4	09.6	15.4	05.0	01.0	05.8	06.0	07.7	82	52	87	74	-	0	S	2	-	0
12	753.4	753.9	756.5	09.2	12.4	06.2	08.5	13.3	05.8	08.1	08.3	06.8	05.8	95	63	82	80	SE	5	SE	5	-	0
13	758.7	757.8	756.1	04.0	13.8	09.2	09.0	14.8	03.5	-00.2	05.6	04.9	06.2	92	42	71	68	-	0	SSW	3	-	0
14	751.3	748.4	748.3	08.8	08.4	08.4	08.5	11.3	07.9	07.2	06.5	08.1	07.8	77	97	95	90	-	0	-	0	-	0
15	748.1	748.3	750.5	08.3	12.0	09.0	09.6	13.8	08.3	07.4	07.9	08.4	07.8	96	80	90	89	-	0	ESE	4	SE	2
16	751.2	750.1	749.3	06.4	13.0	08.0	08.8	13.7	06.3	05.4	06.8	05.0	04.1	94	45	51	63	-	0	N	7	N	7
17	748.7	750.3	753.1	07.2	09.8	06.8	07.6	10.0	06.8	05.2	03.8	03.9	03.2	49	42	44	45	N	8	N	8	N	8
18	754.9	753.7	752.8	04.4	11.6	06.2	07.1	12.3	03.1	00.4	03.0	04.1	05.8	47	40	82	56	N	6	S	4	S	3
19	749.9	746.3	745.1	05.0	06.0	06.0	05.8	07.4	04.5	01.8	06.3	06.8	06.6	96	97	94	96	-	0	-	0	W	2
20	748.4	752.7	756.4	08.0	09.6	07.4	08.1	11.1	05.7	05.3	03.8	03.6	03.1	48	40	40	43	NW	8	N	8	N	7
21	759.3	759.2	760.3	07.0	13.1	10.6	10.3	15.3	05.0	02.6	02.4	04.0	03.7	33	35	39	36	N	6	N	6	N	5
22	760.8	761.2	761.6	06.0	15.8	09.6	10.2	16.7	04.6	-00.3	04.4	04.8	06.2	62	36	69	56	NW	3	S	4	-	0
23	762.2	761.8	762.0	09.0	16.2	13.0	12.8	18.0	06.6	03.2	04.7	06.8	07.9	55	49	71	58	N	1	-	0	-	0
24	761.7	760.2	761.1	10.0	19.5	13.8	14.3	20.0	09.2	06.4	06.0	07.0	09.9	65	41	83	63	N	2	SSE	4	W	2
25	762.1	761.1	760.8	10.7	20.6	12.5	14.1	20.9	09.5	05.9	07.0	07.2	07.6	73	39	70	61	N	2	S	4	-	0
26	759.0	756.9	754.9	11.0	19.2	14.8	15.0	22.2	08.8	05.0	06.5	07.4	07.7	66	44	61	57	NNE	3	SSE	2	NNE	2
27	754.0	751.5	748.9	13.8	19.3	15.6	16.1	20.7	10.2	06.4	09.6	09.3	10.3	81	56	78	72	SSE	3	SSW	5	W	1
28	744.8	743.0	745.0	13.8	13.8	13.0	13.4	16.7	12.6	12.7	11.2	11.3	07.8	95	96	70	87	SE	8	SSE	4	N	4
29	748.8	750.2	753.7	09.9	12.5	07.3	09.2	13.2	07.0	06.3	07.7	05.8	06.0	84	53	78	72	E	1	ESE	3	E	3
30	759.1	760.5	761.3	06.4	13.0	07.8	08.8	14.2	05.5	-00.5	03.3	03.9	04.8	45	35	60	47	N	4	N	4	N	2
31	760.8	759.4	757.9	05.4	14.0	12.3	11.0	14.7	04.1	-00.6	04.4	05.4	08.3	65	45	77	62	N	3	SE	5	SE	4
MES. VRED.	754.4	753.9	754.0	06.9	12.6	08.7	09.2	13.8	05.4	03.2	05.5	05.9	06.2	71	55	73	66	2.9		3.6		2.6	

1	753.0	751.7	752.1	11.0	13.0	12.8	12.4	13.6	10.0	09.0	08.3	10.6	10.5	84	95	95	91	SE	6	SE	7	SE	6
2	751.0	750.2	749.3	10.2	15.6	13.0	13.0	16.5	09.9	06.7	08.8	09.8	09.7	94	74	86	85	-	0	SE	5	-	0
3	746.3	748.0	750.9	10.4	12.2	06.8	09.0	13.6	06.5	08.7	08.3	05.7	05.6	88	54	76	73	SE	3	SE	5	-	0
4	752.4	754.5	756.1	03.6	07.4	04.5	05.0	08.6	03.0	03.0	05.0	06.3	05.9	85	82	93	87	-	0	SSE	3	NNW	1
5	756.5	754.1	753.6	03.3	12.0	07.2	07.4	12.7	01.9	-01.2	04.9	04.9	07.2	85	47	95	76	-	0	S	5	SW	3
6	754.8	757.4	758.9	03.3	08.2	05.6	05.7	09.2	01.3	01.0	05.4	05.9	06.3	92	73	93	86	NNW	2	SSE	2	-	0
7	758.9	757.7	755.3	05.0	10.0	07.1	07.3	11.2	03.0	00.0	05.4	05.5	07.3	83	60	96	80	-	0	-	0	-	0
8	752.3	750.9	747.2	08.6	10.4	10.8	10.2	13.3	07.1	07.2	08.2	09.0	09.3	97	95	95	96	N	1	N	2	W	3
9	745.0	748.9	752.3	14.3	17.0	13.6	14.6	17.7	10.8	10.3	11.6	10.7	08.8	95	74	75	81	S	7	SE	5	SE	2
10	756.4	756.4	756.4	10.0	15.0	11.2	11.8	16.8	08.0	03.6	08.1	07.2	07.3	88	56	73	72	-	0	-	0	-	0
11	754.1	753.1	753.0	11.0	17.0	13.5	13.8	17.6	10.0	07.0	07.0	08.3	09.3	71	57	80	69	N	2	SSE	2	NNW	3
12	749.4	748.8	752.2	12.0	10.0	10.6	10.8	13.8	09.0	10.0	09.0	06.9	05.0	86	75	52	71	NW	5	N	7	NW	8
13	757.2	758.0	758.7	07.6	15.6	12.4	12.0	16.0	05.0	00.0	06.0	07.3	08.2	77	55	76	69	-	0	SSE	5	-	0
14	754.5	751.8	752.6	11.2	13.8	10.4	11.4	14.1	09.4	09.0	09.2	10.3	08.6	92	87	91	90	SE	6	SE	6	SE	4
15	755.5	758.3	760.8	09.4	10.4	08.8	09.4	12.4	08.2	06.3	04.2	03.7	03.9	48	39	46	44	N	7	N	8	N	8
16	760.4	760.0	762.5	08.8	09.8	09.8	09.6	12.0	07.2	05.6	03.5	04.1	04.1	41	46	46	44	N	8	N	7	N	7
17	762.7	761.1	761.5	10.6	17.0	13.7	13.8	18.2	08.6	05.7	04.7	04.8	04.9	49	33	42	41	NNE	6	N	5	N	5
18	760.0	757.8	758.0	09.7	17.0	12.4	12.9	18.6	07.7	03.4	06.8	07.5	09.5	75	52	88	72	-	0	SSE	2	-	0
19	758.6	756.5	756.5	10.0	21.4	15.6	15.6	22.8	07.5	03.7	08.3	10.8	11.2	90	56	84	77	-	0	S	4	-	0
20	757.2	757.4	759.4	14.2	24.0	17.6	18.4	24.0	10.5	04.8	08.7	07.8	07.5	72	35	50	52	-	0	S	3	WSW	1
21	760.8	762.4	763.6	13.8	23.4	16.6	17.6	23.8	12.5	06.6	09.9	08.6	10.2	83	40	72	65	-	0	SSE	5	N	1
22	764.7	764.5	764.4	15.0	21.8	15.0	16.7	22.6	13.2	07.0	08.3	11.9	11.7	65	60	92	72	N	3	S	2	-	0
23	763.1	760.8	760.9	14.6	26.0	15.8	18.0	26.4	10.2	05.3	09.0	08.4	11.7	72	33	87	64	-	0	S	3	-	0
24	761.0	758.1	758.3	13.5	25.4	18.6	19.0	26.4	10.8	04.7	09.9	10.2	12.8	85	42	79	69	-	0	S	3	-	0
25	756.9	754.5	754.3	15.0	25.2	18.2	19.2	26.8	11.2	06.0	10.2	09.3	11.7	80	39	75	65	-	0	SE	5	N	2
26	754.6	753.2	753.2	15.4	23.8	17.8	18.7	24.8	12.2	07.4	09.5	10.4	10.7	73	47	70	63	NW	2	S	7	W	1
27	753.1	754.5	756.1	15.3	22.5	16.8	17.8	23.2	13.1	07.7	10.1	08.9	10.0	77	44	69	63	S	3	SW	5	-	0
28	756.7	756.1	754.4	14.4	17.4	16.0	16.0	18.2	12.2	07.0	10.3	13.2	12.8	84	89	94	89	-	0	WSW	2	SW	3
29	756.0	755.8	755.5	13.8	13.0	13.0	14.4	18.6	11.0	08.7	10.7	08.7	07.7	90	56	69	72	SSE	2	SSE	4	NNE	1
30	754.3	753.2	754.8	11.2	14.0	10.5	11.6	16.2	10.3	07.3	08.9	07.8	07.5	90	65	79	78	-	0	SE	4	NW	4
MES. VRED.	755.9	755.5	756.1	10.9	16.5	12.5	13.1	17.6	08.7	05.7	07.9	08.2	08.6	80	59	77	72	2.1		4.1		2.1	

TITOGRAD 1970 MART

BR. ST. 245 H_0 = 52 m H_b = 52.6 m h_0 = 2.0 m h_r = 2.2 m

Dan	Vremenska oznaka	Oblačnost N (0–10) 14	7	14	21	Srednji dnevni	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	8	10	02●	05	05.7	07.8	•	•	F 0-24
2	8	04	01●	00	01.7	09.7	•	•	F 0-10
3	7	10	10●	10●	10.0	00.0	•	•	*°7^00-9^00, ● 9^00-24, F 19-22^00
4	7	10	10●	10●	10.0	00.0	08.0	•	● 0-24, F 22^00-24
5	7	10●	10●	10●R	10.0	00.4	24.0	•	● 0-24, F-F 0-23i, G 13^00-23i, R 16-24^00
6	8	10●	09●	08	09.0	00.9	21.0	•	● 0-3, 6^00-12, 22^00-24; G 18^00-19^00
7	8	10	06●	00	05.3	08.5	15.0	•	● 0-9^00i
8	8	00●	01●	00	00.3	10.7	00.0	•	●
9	8	00●	00●	00	00.0	10.4	•	•	●
10	8	01●	01●	00	00.7	10.4	•	•	●
11	8	06●	10	10●	08.7	06.1	•	•	● 14^00-24i
12	8	10●	07●	00	05.7	04.2	20.5	•	● 0-11^00, F 3^00-15^00
13	8	00●	07●	10	05.7	09.2	09.8	•	
14	7	10	10●	10●	10.0	00.0	•	•	● 7^00-24i
15	7	10●	10●	10	10.0	02.2	48.0	•	● 0-7^00, 13^00-14^00
16	8	10	06●	03	06.3	06.9	07.2	•	● 2^00-4^00, F 12^00-24
17	8	08	01●	00	03.0	10.2	•	•	F 0-24
18	8	06●	04●	03	05.0	09.5	•	•	F N 0-3, F N 3-7
19	8	10●	10●	10●	10.0	00.0	02.8	•	● 1^00-23, F NW 23^00-24
20	8	10	02●	03	05.0	07.6	17.3	•	F NW 0-24
21	8	08●	05●	00	01.7	11.4	•	•	F 0-24
22	8	05●	06●	05	05.3	10.4	•	•	
23	8	10	09	08	09.0	03.4	•	•	
24	8	07	02●	00	03.0	10.3	•	•	△ 20-24
25	8	07●	08	00	05.0	08.6	•	•	△ 0-6
26	8	08	10●	00	06.0	03.3	•	•	F NNE 12-13^00, *°13^00-15^00i
27	8	10	10	10	10.0	01.4	00.6	•	● 21^00-24
28	7	10●	10●	06	08.7	01.4	13.7	•	● 0-15^00, F 2^00-11, F NE 11-13
29	8	10	10	07	09.0	00.2	17.5	•	● 8-12i
30	8	00●	00●	00	00.0	11.5	00.2	•	
31	8	01●	08	10●	06.3	08.8	•	•	● 20^00-24
MES. VRED.			06.9	06.3	04.8	06.0	185.4	205.6	

TITOGRAD 1970 APRIL

Dan	Vremenska oznaka	14	7	14	21	Srednji dnevni	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	7	10●	10●	10●R	10.0	00.0	09.8	•	● 0^00-24, F 4^00-24i, R 13^00-24, G 16-24
2	8	09	09●	10	09.3	03.6	36.0	•	● 0-2, 11^00-12^00, 21^00-24
3	8	10●	09●	00	06.3	03.8	04.0	•	● 0-10^00i, F NE 12^00-16^00
4	8	10●	04●	00	04.7	03.0	05.9	•	△ 20-24
5	8	04●	04●	10●R	06.0	10.2	01.2	•	△ 0-8, R G 19^00-22^00i, ● 19^00-24, F 20-20^00
6	8	10	10	02	07.3	04.2	29.7	•	● 0-12^00 △ 19^00-24
7	8	10	10●	10●	10.0	01.6	10.0	•	△ 0-7^00 ● 0-1 13^00-24
8	7	10●	10●	10●	10.0	00.0	50.5	•	● 0-24, F 10^00-12, R 20^00-22^00, F 23-24
9	7	10●R	10	06	08.7	01.7	50.5	•	● 0-15^00, F 0-7^00, R G 6^00-8
10	8	02●	08●	02	04.0	09.4	02.2	•	
11	8	10	10	10	10.0	00.1	•	•	● 14^00-17i
12	7	10●	10●	06	08.7	00.0	00.7	•	● 6^00-15, F 9-23^00
13	8	00	07●	10●	05.7	11.8	00.2	•	F 16^00-19^00 ● 20^00-24
14	7	10●	10●	10●	10.0	00.0	09.0	•	● 0-22, R 15-18, F 21^00-24
15	8	10	09	07	08.7	06.1	46.6	•	F 0-24
16	8	00●	07●	09	05.3	09.2	•	•	F 0-24
17	8	01●	01●	03	01.7	12.5	•	•	F 4^00-21i
18	8	10	10●	08	09.3	03.4	•	•	△ 20^00-24
19	8	00●	04●	03	02.3	11.2	•	•	△ 0-8, 20^00-24
20	8	02●	04●	09	05.0	12.1	•	•	△ 0-8
21	8	09●	08●	02	06.3	11.4	•	•	
22	8	09	10	09	09.3	00.1	•	•	△ 20-24
23	8	01●	01●	00	00.7	12.3	•	•	△ 0-7^00 20-24
24	8	04●	05●	00	03.0	13.0	•	•	△ 0-7^00 20-24
25	8	05●	06●	00	03.7	12.4	•	•	△ 0-8, F 15^00-18^00
26	8	00●	04●	05	03.0	12.0	•	•	F 12^00-17i
27	8	09●	03●	00	04.0	09.9	•	•	F 7-14^00
28	7	10	10●	10●	10.0	00.0	•	•	● 7^00-24
29	8	07●	05●	10	07.3	11.3	13.0	•	● 0-3
30	8	10●	10	03	07.7	01.9	00.0	•	● 6^00-10, 19^00-19^00
MES. VRED.			06.7	07.3	05.8	06.6	188.3	269.3	

$\varphi = 42^{0}\ 26'$ N $\lambda = 19^{0}\ 17'$ E Gr. $\Delta G =$ + 1h 17 min. BR. ST. 245

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, I (0—12)					
	7	14	21	7	14	21	Srednji Dnev	Max	Min	Min 5 cm	7	14	21	7	14	21	Srednji Dnev	7		14		21	
1	756.6	756.5	757.7	10.0	14.8	11.2	11.8	16.6	09.2	06.4	05.0	05.7	07.8	54	45	79	59	N	6	N	5	-	0
2	757.8	758.2	757.8	09.4	10.0	07.8	08.8	12.0	06.3	05.2	05.4	06.2	05.0	61	68	64	64	NW	3	-	0	NW	3
3	756.0	756.0	757.2	10.0	12.5	11.8	11.5	13.2	06.5	01.0	04.9	04.9	05.4	53	45	52	50	NW	7	NW	7	NW	7
4	756.4	753.9	752.0	13.5	18.0	14.4	15.1	19.4	10.0	04.4	06.4	05.9	05.5	55	38	45	46	N	4	N	6	-	0
5	750.6	751.1	753.6	10.8	12.4	11.2	11.4	15.2	10.2	09.0	08.3	09.4	09.6	85	87	97	90	-	0	S	1	-	0
6	756.4	756.8	757.4	10.5	17.0	13.9	13.8	18.0	10.0	09.0	08.7	08.5	10.5	92	58	88	79	-	0	SSW	1	-	0
7	754.9	754.7	754.9	12.4	20.8	19.0	17.8	22.2	10.8	08.2	09.7	10.7	14.7	90	58	89	79	-	0	-	0	-	0
8	756.2	756.5	757.7	16.0	20.5	16.3	17.3	23.6	13.5	08.0	09.7	09.4	12.4	71	52	89	71	-	0	-	0	-	0
9	759.5	758.4	758.1	14.7	24.6	19.8	19.7	25.2	12.0	07.6	09.9	09.3	11.2	79	40	65	61	-	0	S	4	-	0
10	755.6	753.6	752.6	16.4	26.8	19.0	20.3	28.0	14.0	12.0	11.0	11.7	10.8	79	44	65	63	-	0	-	0	-	0
11	752.0	751.1	751.6	19.0	25.1	19.0	20.5	25.8	14.0	08.8	10.8	12.2	12.8	65	51	78	65	-	0	SE	5	-	0
12	752.6	754.6	755.5	13.4	19.2	14.4	15.4	19.5	12.5	11.0	08.9	08.6	09.7	77	52	79	69	N	1	S	5	-	0
13	756.7	755.4	756.3	14.2	21.8	15.0	16.5	22.4	11.8	08.8	10.4	08.7	08.3	86	45	65	65	-	0	SW	5	N	2
14	758.4	757.6	758.2	15.0	21.5	16.6	17.4	22.0	11.5	07.0	08.4	10.3	10.7	66	54	75	65	N	2	S	3	SW	1
15	758.7	756.5	754.8	15.2	22.8	17.4	18.2	23.8	11.8	06.4	09.8	09.0	09.4	75	43	63	60	N	1	S	4	-	0
16	754.6	752.3	752.4	15.2	22.0	18.0	18.5	24.4	14.0	09.4	11.4	10.2	10.0	88	49	65	67	WNW	2	-	0	SE	2
17	750.8	750.1	750.8	15.2	21.0	16.4	17.2	22.3	13.9	12.2	09.9	11.4	08.6	76	61	61	66	NNE	2	SSE	5	NNW	3
18	751.9	753.0	756.0	14.3	19.6	17.8	17.4	21.5	13.0	10.2	09.7	10.5	08.1	80	61	53	65	-	0	-	0	N	2
19	757.1	757.3	756.8	18.8	20.6	17.2	18.4	21.0	14.4	09.0	08.5	07.7	07.3	52	42	50	48	NNW	3	N	6	N	7
20	755.6	753.1	753.0	18.1	24.0	18.6	19.8	24.3	14.7	10.4	08.0	08.0	12.1	51	36	75	54	N	2	S	3	S	1
21	749.9	748.0	749.4	14.6	21.5	19.0	18.5	21.7	14.2	12.8	10.6	07.5	08.2	85	39	50	58	-	0	NW	7	N	5
22	751.0	751.4	750.5	15.8	17.8	14.8	15.8	19.6	13.5	08.8	10.1	12.2	11.8	75	80	94	83	-	0	SE	6	SE	4
23	753.4	756.9	760.2	09.8	16.6	13.5	13.4	18.3	09.7	09.3	08.2	05.7	06.0	90	40	52	61	WNW	3	N	4	NW	2
24	762.0	761.3	762.6	13.2	16.6	13.3	14.1	17.4	09.8	05.2	05.1	05.9	05.7	45	42	50	46	NW	4	N	5	NW	4
25	762.0	760.0	760.3	14.8	20.5	17.8	17.7	21.8	11.5	06.4	05.9	07.4	06.4	47	41	42	43	N	6	N	6	N	6
26	760.0	757.8	757.6	15.0	22.0	17.0	17.8	22.4	12.8	09.2	07.0	07.9	10.0	55	40	69	55	NNW	2	S	2	-	0
27	757.7	756.1	757.1	16.6	23.0	17.4	18.6	23.3	12.8	07.4	09.3	10.0	12.4	66	47	83	65	-	0	S	3	SE	2
28	756.4	756.1	756.6	15.4	15.8	12.8	14.2	18.0	11.8	10.8	11.8	10.3	10.6	90	77	96	88	-	0	W	2	NW	4
29	756.6	756.3	757.6	14.0	20.0	16.8	16.9	21.8	11.1	10.2	09.4	10.3	12.2	78	59	85	74	-	0	S	5	SE	2
30	758.0	757.1	757.0	15.8	22.0	16.6	17.8	23.0	11.6	07.1	09.7	10.8	11.1	72	54	78	68	NW	2	SE	4	-	0
31	756.3	754.6	756.5	16.8	24.8	19.8	20.3	26.0	12.6	10.0	11.6	11.2	09.6	81	48	55	61	-	0	-	0	N	6
MES. VRED.	755.9	755.2	755.8	14.3	19.9	15.9	16.5	21.1	11.8	08.4	08.8	09.0	09.5	72	51	69	64		1.6		3.4		2.0

1	758.0	757.4	758.4	19.4	22.4	19.0	20.0	23.7	18.0	15.4	09.3	08.0	08.0	55	40	48	48	N	6	N	6	NNW	4
2	758.0	757.2	757.2	17.8	22.8	19.0	19.6	23.8	14.5	08.8	08.7	08.4	07.7	57	40	47	48	NW	3	NW	5	NW	6
3	758.0	756.7	757.2	15.0	19.0	15.8	16.4	20.8	13.0	10.0	07.2	07.0	06.9	56	43	51	50	N	6	N	6	N	7
4	756.9	757.3	758.4	14.0	18.2	16.6	16.4	19.6	10.6	04.0	07.9	08.0	09.2	66	51	65	61	W	2	-	0	-	0
5	759.9	759.3	759.9	16.4	20.7	16.4	17.5	22.0	13.2	07.4	11.2	09.8	10.0	80	54	72	69	-	0	SE	5	-	0
6	760.2	761.2	760.0	14.0	13.6	13.5	13.6	16.8	12.9	07.1	10.9	10.9	11.0	91	94	95	93	NNW	3	NNW	1	-	0
7	758.9	757.2	756.9	16.0	25.3	21.4	21.0	27.3	11.7	08.0	12.2	13.3	13.3	89	55	70	71	-	0	S	3	N	4
8	756.3	756.4	757.0	18.9	28.4	22.5	23.1	28.8	17.0	11.2	12.1	11.6	13.5	74	40	66	60	NW	3	SE	6	N	3
9	757.7	758.0	757.7	21.8	26.6	23.2	23.7	28.2	19.0	14.4	13.9	15.9	16.7	71	61	78	70	NNW	2	NNW	2	-	0
10	756.9	754.3	754.0	21.0	31.0	23.5	24.3	31.6	17.0	13.0	13.0	13.7	13.8	69	40	63	57	-	0	S	3	-	0
11	754.1	753.4	753.3	21.8	28.2	22.0	23.5	28.6	17.8	12.0	13.4	16.6	17.2	69	58	87	71	N	3	S	4	-	0
12	753.4	751.1	752.2	20.2	29.4	25.4	25.1	30.4	17.0	13.0	16.2	09.0	13.6	91	32	56	60	-	0	W	4	-	0
13	753.4	752.3	752.8	22.5	29.0	24.0	24.9	30.0	19.2	13.5	12.1	13.7	12.9	59	46	58	54	NW	3	S	3	-	0
14	755.3	754.4	754.5	21.5	28.6	23.8	24.4	29.7	18.0	13.2	14.5	14.9	17.3	75	51	78	68	-	0	S	4	-	0
15	755.8	755.7	756.9	20.8	29.4	23.0	24.0	30.0	18.0	12.8	14.1	12.5	15.7	76	41	75	64	N	2	S	5	-	0
16	757.9	756.6	757.8	23.0	31.0	26.0	26.5	31.2	19.0	13.0	14.5	15.0	13.0	69	44	51	55	N	3	S	4	N	6
17	757.8	756.1	755.1	22.6	31.8	26.8	27.0	32.8	20.0	17.5	14.5	17.8	15.4	71	50	58	60	N	4	S	4	SE	2
18	754.2	753.0	753.3	24.2	32.9	26.6	27.6	33.4	31.0	16.4	17.4	15.1	14.6	77	40	56	58	-	0	SSE	6	SE	6
19	753.6	753.4	753.9	17.6	27.0	22.5	22.4	27.0	16.8	15.8	13.1	14.0	16.0	87	52	78	72	N	2	S	5	SE	4
20	753.5	753.4	755.7	20.2	22.0	19.2	20.2	25.0	18.6	14.4	15.1	15.4	16.2	85	78	97	87	-	0	SE	5	-	0
21	756.9	756.6	757.9	20.2	29.5	24.4	24.6	29.8	15.0	10.8	12.7	13.1	14.4	71	42	63	59	N	3	SE	4	-	0
22	759.8	757.3	757.0	23.6	30.3	26.0	26.5	31.4	19.5	12.6	10.1	11.3	13.0	46	35	51	44	NW	3	S	3	NE	2
23	758.7	757.5	757.3	24.0	30.8	26.2	26.8	32.2	19.5	13.6	14.6	14.8	18.6	65	44	73	61	-	0	SE	3	-	0
24	758.5	757.9	758.0	23.4	31.2	25.9	26.6	32.0	20.0	15.8	17.5	13.6	19.3	81	40	77	66	-	0	-	0	-	0
25	758.2	757.5	758.0	24.0	31.0	24.5	26.0	31.5	19.8	15.0	15.5	13.7	14.0	69	40	61	57	NNW	2	ESE	4	NNW	3
26	758.7	756.5	756.8	24.8	31.2	27.7	27.8	32.1	22.1	16.7	14.7	15.1	14.5	62	44	52	53	NW	3	SE	5	NE	4
27	758.2	756.9	757.2	26.2	32.2	26.8	28.0	33.0	23.4	20.0	15.2	15.8	17.1	60	44	65	56	N	5	NE	5	-	0
28	758.1	756.3	756.6	25.0	32.0	25.9	27.2	32.8	23.1	20.1	13.3	18.0	17.9	56	50	71	59	NW	3	SE	4	-	0
29	756.9	754.6	755.2	26.0	32.8	24.4	26.9	32.8	21.0	17.8	20.3	20.6	16.1	80	55	70	68	-	0	N	4	NW	5
30	754.9	752.9	751.5	23.4	31.8	25.6	26.6	32.4	20.7	17.6	15.1	15.8	14.7	70	45	60	58	NW	3	S	4	-	0
MES. VRED.	757.0	755.9	756.2	21.0	27.7	22.9	23.6	28.7	18.2	13.4	13.3	13.4	14.0	71	48	66	62		2.1		3.9		1.9

TITOGRAD 1970 MAJ

BR. ST. 245

H_s = 52 m H_b = 52.6 m h_s = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednja Dnev		7	7	
1	8	08⊙	07⊙	00	05.0	11.2	00.0	.	F 0-17i
2	8	10	10	00	06.7	02.2	.	.	F 7^30-22^30i, ● 8-11^30
3	8	03⊙	10	03	05.3	04.1	04.9	.	F 6^30-24i
4	8	02⊙	04⊙	04	07.3	11.9	.	.	F_N 0-19i
5	9	10	10●	10	10.0	00.0	.	.	●° 12-15^30, 21^30-24
6	8	10	10	10●	10.0	01.3	05.5	.	● 0-5, 19-22
7	8	10	10	10	10.0	00.7	00.5	.	F 17^30, 18^40
8	8	10	10	02	07.3	00.0	.	.	△ 19^30-24
9	8	08⊙	08⊙	04	06.7	10.1	.	.	△ 0-8
10	8	01⊙	06⊙	00	02.3	11.2	.	.	F 15^20-17^40
11	8	00⊙	00⊙	06	02.0	10.0	.	.	F 7^40-10^30
12	8	10	09⊙	08	09.0	04.2	02.5	.	● 2^40-4^30, 8^15-12^30; F 3^30-4^30
13	8	02⊙	07	00	03.0	08.8	01.1	.	F 12^40-19^40i
14	9	00⊙	08	00	02.7	11.2	.	.	△ 0-7^30
15	8	03⊙	08	03	04.7	09.6	.	.	
16	8	09●	09⊙	10	09.3	05.4	00.7	.	● 4^20-8^50, 18^40-24i; F 15^30-17^30, ↯ 19-24
17	8	09 ⚡	05⊙	05	06.3	07.1	03.5	.	⚡ 4^30-8, ● 5-8i; F 13^30-18i, ↯ 22-24
18	8	07	10	05	07.3	06.5	00.9	.	↯ 0-3, F 2^30-3^50, 14^55-18i
19	8	01⊙	04⊙	07	04.0	12.9	.	.	F 8^30-24i
20	8	04⊙	09	10	07.7	09.4	.	.	F 17^40-19
21	8	10●	10	10	10.0	01.1	00.0	.	●° 6^30-10^20i, F 13^20-16^30
22	7	10	10	10●	10.0	01.9	00.0	.	▽ 9^15-10, ● 13^15-24i, F 10^55-22^30i
23	8	10●	08	02	06.7	04.5	38.0	.	● 0-7^40, ⚡ 4-5^30
24	8	04⊙	07	10	07.0	08.5	00.8	.	F 13-16^30
25	8	04⊙	02⊙	00	02.0	11.6	.	.	F 4-24
26	8	04⊙	08⊙	04	05.3	13.3	.	.	F 0-3, ⊕ 11^30-12^50, △ 20-24
27	8	04⊙	04⊙	09	05.7	11.5	.	.	F 15-19^30
28	8	10	10	10●	10.0	00.0	.	.	↯ 10-11, ⚡ 10-11, ● 10^20-24
29	8	06	04⊙	02	04.0	08.9	19.5	.	△ 20-24
30	8	04⊙	07⊙	04	05.0	12.1	.	.	△ 0-8
31	9	09⊙	06⊙	10	08.3	08.6	.	.	F 14^40-24i, ● 16-19^15i
MES. VRED.		06.2	07.4	05.4	06.3	218.9	78.6		

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1	8	06	04⊙	08	06.0	10.7	02.0	.	F 0-24; F 8^30-9^30
2	8	08⊙	09⊙	04	07.0	08.5	.	.	F_N 10-24i
3	8	09	09⊙	08	08.7	09.6	00.6	.	F 0-22^30i, ●° 4^30-5^40
4	8	00⊙	09	10	06.3	05.9	.	.	
5	8	08⊙	05⊙	04	05.7	10.1	.	.	
6	7	10●	10●	07	09.0	00.0	00.2	.	●6-14, △ 20-24
7	8	05⊙	06⊙	05	05.3	11.5	00.5	.	△ 0-8
8	9	09⊙	04⊙	05	06.0	10.0	00.5	.	●° 5^30-7^20i, F_55 11^30-14^40
9	8	09	10	01	06.7	03.1	00.0	.	●° 10^15-11
10	8	10	00⊙	00	03.3	10.5	00.0	.	F 15^30-18^30i
11	8	07⊙	06⊙	03	06.0	11.9	.	.	△ 20-24
12	8	03⊙	04⊙	04	03.7	11.7	.	.	△ 0-7^30, F 9^30-11^50
13	8	00⊙	03⊙	03	02.0	13.2	.	.	
14	9	00⊙	08⊙	03	03.7	11.4	.	.	
15	8	09	09	03	07.0	08.3	.	.	
16	9	00⊙	02⊙	04	02.0	10.3	.	.	F 18-24
17	8	00⊙	03⊙	00	01.0	13.6	.	.	F 0-3
18	8	03⊙	03⊙	03	03.0	12.0	.	.	F 11^30-24
19	8	10●⚡	03⊙	04	05.7	09.7	02.3	.	F 0-19i, ⚡ 2^40-8i, ● 3-7^50
20	9	10	09	07	08.7	02.3	01.7	.	● 10^15-11^30, ⚡ 10^30-11^30, F 10^40-11^30i
21	8	02⊙	08⊙	03	04.3	11.9	07.4	.	F 8-11^40
22	8	00	02⊙	00	00.7	14.0	.	.	
23	8	03⊙	04⊙	03	03.3	13.0	.	.	
24	8	00⊙	02⊙	00	00.7	13.3	.	.	
25	8	02⊙	05⊙	00	02.3	09.4	.	.	
26	8	00⊙	04⊙	03	02.3	13.1	.	.	
27	8	01⊙	03⊙	00	01.3	13.8	.	.	
28	8	00⊙	03⊙	10	04.3	12.4	.	.	F 13^15-23^40i, ↯ 16-17, ⚡ 16^15-17^30, ● 16^20-17^20
29	9	08⊙	08⊙	01	05.7	09.9	.	.	
30	8	01⊙	05⊙	00	02.0	13.7	01.5	.	
MES. VRED.		04.4	05.4	03.5	04.4	310.1	25.0		

φ = 42° 26' N λ = 19° 17' E Gr. ΔG = + 1h 17 min. BR. ST. 245

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	751.0	750.9	752.0	24.5	26.0	20.3	22.8	26.8	18.7	17.2	18.6	14.4	15.1	81	57	84	74	SE 6	S 4	- 0
2	752.6	751.8	751.7	20.4	28.4	23.5	24.0	29.4	17.0	13.0	13.1	15.0	15.2	73	52	70	65	N 3	SSE 3	SE 2
3	752.7	751.9	752.2	21.4	29.8	24.8	25.2	30.8	17.8	13.6	14.4	11.9	17.1	75	38	73	62	- 0	SSE 3	- 0
4	752.0	750.9	751.1	24.3	30.0	24.5	25.8	31.6	17.8	14.8	14.4	16.5	16.9	63	52	73	63	N 4	SE 4	- 0
5	751.6	752.7	754.8	22.0	20.8	19.4	20.4	25.6	12.9	14.8	13.9	13.9	10.6	70	76	63	70	NW 2	N 5	N 7
6	754.3	754.2	755.1	21.5	23.2	20.6	21.5	25.0	17.0	15.0	12.0	10.9	10.5	62	51	58	57	N 7	N 7	N 6
7	753.5	751.7	752.8	19.0	26.0	24.6	23.6	28.8	17.8	15.0	15.3	16.8	14.3	93	67	62	74	- 0	N 6	N 6
8	752.3	750.9	752.3	24.6	31.7	27.1	27.6	32.6	20.7	15.8	14.9	17.3	18.9	64	49	70	61	- 0	SE 4	- 0
9	753.9	753.1	754.1	25.4	32.1	26.4	27.6	33.4	22.0	18.2	18.1	18.5	19.9	74	52	77	68	NW 2	S 4	- 0
10	755.8	754.2	757.0	24.8	34.8	23.6	26.7	35.2	22.0	17.0	18.8	17.7	19.4	80	42	89	70	- 0	ESE 3	- 0
11	757.5	755.5	755.9	27.0	34.6	29.4	30.1	35.4	22.5	19.0	16.5	19.0	15.3	62	46	50	53	N 4	E 4	- 0
12	756.3	755.2	756.0	28.2	34.4	30.1	30.7	35.0	25.7	21.6	17.3	17.0	13.9	60	42	44	49	N 4	NE 5	NE 6
13	756.7	755.7	755.5	28.4	34.6	29.6	30.6	35.2	27.2	25.0	17.5	17.1	14.4	60	41	46	49	N 5	N 5	N 4
14	755.6	753.1	753.2	26.6	34.6	27.0	28.8	34.6	24.6	23.0	15.9	18.6	18.2	61	45	68	58	NNW 4	SSE 4	SE 5
15	750.9	748.0	748.1	24.6	32.0	27.6	28.0	32.4	21.4	16.2	16.9	16.4	17.7	73	46	64	61	N 3	SE 4	SE 5
16	748.4	747.4	747.7	25.3	25.3	18.6	22.0	29.4	18.2	20.0	19.8	20.6	15.3	82	85	95	87	SE 3	SE 7	- 0
17	748.7	749.3	751.8	18.4	18.8	18.0	18.3	21.0	16.6	15.8	13.6	14.2	10.1	85	87	65	79	SE 6	NW 4	NW 4
18	752.5	754.4	755.6	17.0	20.4	16.6	17.6	22.4	13.0	10.0	09.0	08.0	07.5	62	45	53	53	WNW 4	NNW 5	- 0
19	754.9	754.7	755.0	15.6	23.2	18.2	18.8	24.2	12.6	08.0	08.7	11.9	13.8	66	56	88	70	NW 3	SE 5	- 0
20	756.5	756.1	755.7	18.8	26.1	21.2	21.8	27.3	14.8	11.7	12.1	13.6	14.8	74	53	78	68	- 0	SE 5	- 0
21	758.1	758.0	758.6	19.8	29.0	23.1	23.8	30.0	16.5	12.1	13.1	13.7	15.7	76	46	74	65	- 0	S 4	- 0
22	758.5	757.4	757.2	23.0	34.2	27.4	28.0	35.2	19.4	14.2	14.8	18.8	19.2	70	47	70	62	N 1	- 0	N 2
23	758.0	756.7	756.8	26.2	35.0	29.0	29.8	36.0	23.0	17.8	18.4	18.8	21.8	72	44	72	63	WNW 2	S 3	- 0
24	756.3	754.0	754.0	26.8	34.7	28.3	29.5	35.4	23.5	18.7	20.8	20.7	21.7	79	50	75	68	- 0	S 4	- 0
25	752.3	749.9	748.8	25.6	33.8	26.0	27.8	34.2	23.8	21.8	19.4	20.3	19.9	79	52	79	70	NW 2	SSE 4	- 0
26	749.8	750.3	753.2	25.2	24.6	22.5	23.7	29.2	20.8	19.2	18.2	14.6	13.5	76	63	66	68	NNW 5	N 6	N 6
27	756.0	755.3	756.5	21.2	30.0	26.6	26.1	30.8	24.0	18.8	11.3	14.5	13.0	60	45	50	52	N 6	N 6	N 5
28	758.0	757.3	757.2	25.0	31.5	27.4	27.8	32.7	21.2	20.0	12.3	16.5	14.6	52	47	53	51	NNW 4	S 3	- 0
29	757.1	756.1	754.9	25.8	32.4	26.4	27.8	33.0	23.5	18.2	15.0	14.5	17.5	60	40	68	56	N 3	S 4	- 0
30	756.2	755.8	756.5	25.6	32.8	29.0	29.1	33.6	23.6	17.6	16.2	17.1	16.3	66	46	54	55	NW 2	S 3	- 0
31	758.5	758.1	757.6	25.4	33.0	28.5	28.8	33.8	24.5	20.8	15.8	17.0	18.0	65	45	62	57	NNW 3	SE 4	SE 2
MES. VRED.	754.4	753.6	754.2	23.5	29.6	24.7	25.6	31.0	20.1	16.9	15.4	16.0	15.8	70	52	68	63	2.8	4.2	1.9

1	758.8	757.0	757.7	25.8	33.5	26.2	27.9	34.0	23.2	23.1	16.3	16.9	14.9	65	44	58	56	NW 1	S 3	NW 3
2	757.0	756.0	756.3	25.0	24.9	22.8	23.9	31.8	21.6	16.2	12.3	14.0	14.6	52	59	70	60	NW 2	NW 4	N 1
3	754.9	752.7	753.1	22.8	31.8	24.8	26.0	31.9	19.0	13.2	11.4	11.2	13.6	55	32	58	48	W 2	S 3	- 0
4	754.4	752.6	754.0	23.4	32.9	26.2	27.2	33.0	21.5	17.0	13.1	13.5	14.3	61	36	56	51	NNW 2	S 3	- 0
5	756.8	755.6	757.5	24.2	33.5	26.2	27.5	34.0	21.5	17.5	13.0	13.7	14.3	57	35	56	49	NNW 3	S 3	N 5
6	757.7	756.1	756.2	24.6	35.4	28.8	29.4	36.0	22.2	16.4	13.2	13.8	14.8	57	32	50	46	- 0	SSE 4	- 0
7	756.6	755.2	754.3	26.1	36.3	28.9	30.0	37.0	23.7	18.3	13.6	12.3	16.6	53	27	55	45	N 3	ENE 3	- 0
8	754.1	752.0	751.1	26.4	35.0	28.6	29.6	36.2	23.7	19.6	14.8	12.7	13.2	57	30	45	44	N 1	S 3	W 2
9	750.6	749.4	749.1	25.4	33.5	28.0	28.7	34.0	23.0	18.5	13.7	14.1	17.0	56	36	60	51	N 2	S 3	SSE 4
10	751.6	752.5	752.5	25.0	26.6	24.0	24.9	29.8	22.2	18.3	12.0	11.0	12.5	50	42	56	49	- 0	NW 2	- 0
11	752.3	752.9	754.3	22.6	24.6	22.4	23.0	28.8	21.0	16.6	13.5	14.0	14.5	66	60	71	66	- 0	W 4	- 0
12	755.9	755.9	757.1	21.6	30.8	25.5	25.8	31.4	19.0	13.0	09.9	09.4	07.8	51	28	32	37	NNW 2	NNE 5	N 5
13	758.6	757.0	757.9	22.5	31.6	25.5	26.3	32.2	19.8	14.6	08.8	11.0	12.0	43	31	49	41	NW 2	SSE 3	- 0
14	758.0	756.8	757.8	23.4	33.3	26.8	27.6	34.0	21.2	14.8	11.9	12.2	17.4	55	32	66	51	N 1	S 4	- 0
15	758.0	756.2	755.2	25.2	35.2	28.4	29.3	35.4	21.1	16.0	13.7	10.9	12.1	57	26	42	42	- 0	SSE 4	- 0
16	755.0	753.3	753.2	24.5	34.2	25.7	27.5	34.3	22.1	17.1	12.5	13.7	14.7	54	34	59	49	N 2	NE 4	NW 3
17	751.5	750.1	750.4	22.8	34.4	27.6	28.1	34.6	21.4	17.0	13.1	13.6	13.4	63	33	48	48	N 3	S 5	- 0
18	751.1	750.0	751.5	24.4	34.0	27.2	28.2	34.4	22.2	17.0	12.3	12.8	16.2	54	32	60	49	NNW 4	SE 4	- 0
19	753.5	752.4	753.2	24.2	34.4	27.4	28.4	35.0	22.6	20.4	13.9	13.0	12.6	61	32	46	46	NNW 4	S 4	- 0
20	753.8	752.3	752.6	24.6	35.6	27.8	29.0	36.0	22.6	17.0	12.8	13.7	15.3	55	31	54	47	NNW 2	ENE 4	- 0
21	752.8	751.4	751.0	24.8	33.2	25.8	27.4	33.6	22.0	16.7	13.6	10.0	15.6	58	26	63	49	N 1	SE 5	- 0
22	751.6	752.0	752.9	24.6	23.0	23.0	24.6	30.4	22.9	18.4	17.2	10.8	15.4	74	38	73	62	SSE 2	SSE 5	- 0
23	754.1	753.2	754.1	21.5	30.5	22.8	24.4	31.0	19.0	14.1	13.7	10.1	09.7	71	31	47	50	N 2	S 4	- 0
24	753.7	752.6	752.2	21.5	24.2	17.2	20.0	24.6	14.0	12.8	11.2	13.9	10.4	58	61	71	63	N 1	SSE 4	NW 2
25	753.3	753.8	755.1	16.6	25.6	22.2	21.6	27.6	14.3	10.6	10.2	08.4	08.1	72	34	41	49	- 0	N 4	NW 3
26	756.9	756.0	756.8	19.6	25.6	21.6	22.1	27.4	17.7	14.8	07.9	08.0	07.2	46	33	37	39	NW 4	N 3	NW 6
27	758.3	757.3	757.4	20.4	26.8	22.4	23.0	27.2	19.0	15.4	07.8	08.5	08.0	43	32	40	38	NNE 4	N 6	NNE 5
28	758.3	757.8	758.4	19.8	27.3	21.5	22.5	28.2	18.4	13.6	08.1	07.3	09.8	47	27	51	42	NNW 4	S 3	NE 2
29	759.5	760.1	760.1	20.3	27.7	21.8	22.9	28.2	18.5	13.3	09.9	10.9	11.0	55	39	56	50	N 2	SSE 3	- 0
30	759.5	758.5	758.4	20.5	24.7	18.4	20.5	26.3	18.1	15.7	12.8	12.9	14.1	71	55	89	72	N 1	SSW 2	W 2
31	754.2	753.4	753.0	17.8	20.6	18.6	18.9	21.6	17.6	17.2	13.3	13.9	13.6	87	76	85	83	- 0	- 0	- 0
MES. VRED.	755.2	754.3	754.6	23.0	30.5	24.6	25.7	31.6	20.5	16.3	12.3	12.0	13.0	58	38	56	51	1.8	3.6	1.4

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BR. ST. 245 H_s = 52 m H_b = 52.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	8	10	09⊙	02	07.0	04.2	.	.	F$_{SE}$ 5^{40}-9^{40}i, ∇ 8^{45}-10^{40}
2	8	00⊙	01⊙	00	00.3	13.9	12.4	.	
3	9	00⊙	01⊙	00	00.3	13.4	.	.	
4	8	06⊙	04⊙	06	05.3	13.3	.	.	
5	8	10	10●	08	09.3	01.1	.	.	F 9, ⊓ 7^{35}-8^{30}, ●° 7^{40}-13^{45}i
6	8	07	05⊙	05	05.7	06.0	01.9	.	F 0-24, ● 2-3^{30}
7	8	10●	02⊙	01	04.3	04.9	01.4	.	● 0^{30}-4^{0}i, F 13^{40}-24
8	6	04⊙	03⊙	04	03.7	12.1	00.0	.	F 0-1, 8^{50}-10^{20}
9	8	00⊙	06	03	03.0	12.3	.	.	
10	8	01⊙	08⊙	00	03.0	11.4	.	.	F 15^{50}-17^{30}, ⊓ 17^{45}-18^{15}, ● 17^{50}-18^{40}
11	8	00⊙	01⊙	00	00.3	13.2	01.4	.	
12	8	00⊙	05⊙	00	01.7	13.6	.	.	
13	8	00⊙	02⊙	00	00.7	13.4	.	.	F 0-10^{30}i
14	8	01⊙	02⊙	02	01.7	13.2	.	.	
15	8	00⊙	02⊙	08	03.3	12.9	.	.	●° 21-22^{30}, ⊓ 21-22, F 21^{40}-22^{30}
16	8	10	10●	10	10.0	04.2	02.6	.	● 1^{50}-24i, F 7^{40}-17^{20}, ⊓ 16^{45}-19^{30}, ⊂ 18^{45}-20
17	9	10	08⊙	09	09.0	02.1	50.0	.	F 0^{50}-10^{40}i, ● 5^{30}-16^{40}i, ⊓ 12-13
18	8	01⊙	08⊙	00	03.0	10.2	07.6	.	
19	8	05⊙	04⊙	04	05.0	11.5	.	.	
20	8	04⊙	03⊙	00	02.3	13.4	.	.	
21	8	00⊙	00⊙	00	00.0	13.6	.	.	
22	8	00⊙	00⊙	00	00.0	13.3	.	.	
23	8	00⊙	01⊙	00	00.3	13.2	.	.	
24	8	00⊙	03⊙	00	01.0	13.4	.	.	
25	8	00⊙	06⊙	00	02.0	12.9	.	.	
26	8	01⊙	04	00	01.7	10.2	.	.	F 11^{30}-24i
27	6	00⊙	00⊙	00	00.0	13.4	.	.	F 0-19
28	8	00⊙	03⊙	00	01.0	13.2	.	.	
29	8	00⊙	03⊙	00	01.0	12.5	.	.	
30	8	00⊙	01⊙	00	00.3	13.3	.	.	
31	8	00⊙	00⊙	09	03.0	12.6	.	.	
MES. VRED.		02.6	03.8	02.3	02.9	343.7	76.9		

TITOGRAD 1970 AVGUST

1	8	06	07⊙	00	04.3	10.3	.	.	⊓ 14-15^{30}, F 15-16
2	8	02⊙	10	02	04.7	06.2	.	.	● 11^{40}-13, ⊓ 13^{20}
3	8	00⊙	07⊙	00	02.3	10.3	05.7	.	
4	8	01⊙	06⊙	00	02.3	09.5	.	.	
5	8	00⊙	05⊙	00	01.0	11.4	.	.	
6	8	00⊙	01⊙	00	00.3	12.5	.	.	
7	8	00⊙	00⊙	00	00.0	12.5	.	.	
8	8	00⊙	07⊙	02	03.0	11.7	.	.	
9	8	04⊙	06⊙	06	05.3	07.5	.	.	F 16^{45}-22^{30}
10	8	07⊙	04⊙	05	05.3	08.1	.	.	F 9^{45}-13
11	8	08⊙	08	00	05.3	05.4	.	.	
12	8	01⊙	06⊙	00	02.3	12.1	.	.	
13	8	00⊙	06⊙	00	02.0	12.7	.	.	
14	8	00⊙	03⊙	00	01.0	12.6	.	.	
15	8	00⊙	02⊙	00	00.7	12.8	.	.	
16	8	00⊙	06⊙	05	03.7	09.7	.	.	
17	8	00⊙	01⊙	07	02.7	12.7	00.0	.	
18	8	04⊙	03⊙	00	02.3	03.4	.	.	⊓ 15^{10}-15^{50}, ●° 15^{20}-15^{30}
19	8	00⊙	01⊙	00	00.3	12.6	00.0	.	
20	8	00⊙	01⊙	00	00.3	12.6	.	.	
21	8	03⊙	02⊙	00	01.7	12.3	.	.	F 12-17^{30}
22	8	06	09	00	05.0	05.3	.	.	F 10^{30}-15
23	8	00⊙	05⊙	00	01.7	12.3	.	.	
24	8	03⊙	10	03	05.3	03.4	.	.	⊓ 10-19, ● 10-16^{40}, ∇ 16^{40}-19, F 18^{35}-18^{40}
25	8	08	08⊙	00	05.3	09.7	53.6	.	
26	8	00⊙	06⊙	00	02.0	11.1	.	.	F 8-24i
27	8	00⊙	04⊙	00	01.3	12.4	.	.	F 0-22
28	8	00⊙	06⊙	00	02.0	12.2	.	.	F 1^{30}-3i
29	9	06⊙	10	10	08.7	05.1	.	.	
30	8	10	10	10●⊓	10.0	01.5	.	.	● 15^{30}-24, F 15^{45}-16^{30}, ⊓ 19^{20}-24
31	8	10	10	00	06.7	00.1	57.0	.	● 0-6^{30}, 13-18^{35}i, ⊓ 0-3^{30}
MES. VRED.		02.5	05.4	01.6	03.2	297.8	116.3		

1970 SEPTEMBAR TITOGRAD

$\varphi = 42^{\circ}\ 26'$ N $\lambda = 19^{\circ}\ 17'$ E Gr. $\Delta G =$ + 1h 17 min. BR. ST. 245

Dan	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)					
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dan	7		14		21	
1	752.2	752.1	753.2	18.6	25.0	22.6	22.2	26.2	17.4	15.4	13.9	10.8	10.6	86	46	52	61	-	0	NNE	6	NNE	6
2	754.5	755.1	756.1	22.2	27.6	21.6	23.2	28.6	17.5	13.4	12.2	12.5	14.6	61	45	75	60	-	0	NNE	4	ENE	2
3	758.2	757.2	758.6	20.0	28.2	21.3	22.7	28.5	18.3	12.3	10.6	12.2	16.1	60	42	85	62	N	3	SSE	2	SSE	1
4	758.5	756.1	756.9	19.7	28.0	23.6	23.7	28.4	18.1	14.2	13.2	12.9	12.1	77	46	55	59	-	0	SSE	3	N	4
5	758.6	756.8	757.2	22.2	29.0	22.4	24.0	29.7	20.4	13.9	09.9	10.0	11.1	49	33	55	46	N	4	S	1	NNE	1
6	757.0	755.9	756.4	20.2	28.9	21.8	23.2	29.4	18.2	12.9	11.5	12.0	14.8	65	40	75	60	N	2	SSE	2	-	0
7	757.2	756.5	758.0	19.6	28.8	23.8	24.0	29.2	17.5	13.2	12.5	13.5	12.4	73	45	56	58	-	0	SE	4	-	0
8	759.2	758.5	758.1	20.2	30.0	22.6	23.8	30.0	17.8	12.0	11.5	12.9	12.3	65	40	60	55	NE	2	NE	1	-	0
9	759.3	757.0	757.0	20.8	30.0	23.6	24.5	30.0	19.0	12.8	12.1	13.2	13.6	65	41	62	56	-	0	ESE	2	N	2
10	756.9	756.0	755.5	21.2	31.2	24.6	25.4	31.7	19.4	13.4	12.7	15.6	12.8	67	46	55	56	-	0	SE	3	N	4
11	756.8	755.1	755.0	21.8	32.4	25.2	26.2	32.8	19.5	12.2	09.9	14.8	12.3	51	41	51	48	N	3	SE	2	N	3
12	755.5	754.1	753.8	22.5	31.5	25.2	26.1	33.2	19.7	12.0	11.2	11.3	13.1	55	33	54	47	N	1	-	0	NNE	1
13	753.1	751.5	752.1	22.2	31.5	23.0	24.9	32.2	20.4	13.4	11.5	13.4	14.2	57	39	67	54	NNE	2	SSE	2	-	0
14	753.3	753.1	753.5	24.0	30.9	24.0	25.7	32.2	20.6	13.3	11.9	15.2	13.8	53	45	62	53	NW	4	SE	3	NE	2
15	756.3	755.3	756.6	22.0	31.0	23.2	24.8	31.6	20.5	14.2	13.5	15.0	14.4	68	44	67	60	NW	4	SE	2	-	0
16	757.0	755.3	754.9	21.0	29.5	22.5	23.9	30.8	19.3	12.0	13.3	11.8	12.4	71	38	60	56	N	2	SSE	2	-	0
17	755.9	755.1	756.4	21.1	28.3	22.7	23.7	28.5	19.3	12.7	13.2	15.3	13.9	70	53	67	63	-	0	N	5	N	4
18	756.6	756.2	756.7	22.1	27.8	24.7	24.8	28.2	20.9	18.0	12.3	14.1	11.3	61	50	48	53	N	4	SE	4	N	6
19	758.3	758.2	758.3	21.7	27.3	21.5	23.0	28.2	21.0	16.8	10.7	14.4	14.5	55	53	75	61	NW	5	SSE	4	-	0
20	758.5	756.1	756.1	22.1	27.0	23.1	23.8	28.2	20.6	14.8	09.5	10.4	09.7	48	39	46	44	N	5	S	3	N	6
21	756.4	755.2	756.6	20.7	24.0	19.4	20.9	25.4	19.1	12.3	08.1	09.1	06.7	44	41	40	42	N	6	N	7	NNW	4
22	755.9	755.9	758.6	19.6	25.0	19.3	20.8	25.6	18.0	13.0	07.9	10.4	06.9	46	44	41	44	N	7	N	7	N	3
23	759.3	759.2	758.2	16.4	21.6	17.2	18.1	22.8	15.2	10.2	06.9	08.2	07.9	49	42	54	48	NNW	3	S	2	-	0
24	759.5	758.2	758.6	15.8	23.0	18.0	18.7	24.2	15.0	07.8	07.0	09.1	06.3	52	43	41	45	N	6	SSE	4	NE	4
25	759.6	757.7	758.5	15.0	21.8	17.0	17.7	22.2	14.6	07.8	06.3	08.1	09.2	49	41	64	51	S	2	SE	3	N	1
26	759.0	757.9	758.2	14.6	24.6	16.8	18.2	25.3	13.5	07.2	07.1	09.2	07.6	57	40	53	50	-	0	SE	5	-	0
27	759.8	762.3	763.3	18.6	21.6	17.6	18.8	22.4	14.2	07.0	08.8	08.1	06.4	55	42	43	47	NW	7	N	7	N	6
28	764.7	762.9	765.6	15.1	20.6	15.4	16.6	21.3	12.6	10.1	06.7	06.0	05.2	52	33	40	42	N	4	N	6	N	7
29	765.8	763.5	764.5	13.9	22.0	15.6	16.8	22.0	12.9	08.8	03.6	04.9	03.5	30	25	26	27	N	5	SSE	3	N	5
30	763.7	761.1	760.5	12.0	21.0	13.6	15.0	21.6	10.6	05.0	04.0	06.0	05.5	38	32	47	39	NNW	3	SSE	4	NNE	2
MES. VRED.	757.9	756.8	757.4	19.6	27.0	21.1	22.2	27.7	17.7	12.1	10.1	11.3	10.8	58	41	56	52		2.8		3.4		2.5

1970 OKTOBAR TITOGRAD

1	759.2	755.2	750.7	11.0	19.6	14.2	14.8	21.0	09.4	01.4	05.7	09.2	09.9	58	54	82	65	N	4	SE	7	SE	7
2	749.2	750.9	751.5	14.5	18.9	15.0	15.8	19.0	14.0	08.3	07.5	05.9	05.9	61	36	46	48	NW	4	N	7	N	5
3	750.7	747.6	747.6	11.8	11.4	13.8	12.7	15.2	10.4	05.7	07.2	09.6	07.8	69	95	66	77	N	2	N	1	N	4
4	750.0	751.5	755.6	13.2	18.6	13.8	14.8	18.7	12.3	06.8	04.9	05.0	06.4	43	31	54	43	N	7	NW	7	-	0
5	759.0	758.3	759.1	12.2	18.7	15.6	15.5	20.4	10.3	04.8	06.2	07.2	09.9	58	44	75	59	-	0	SE	5	-	0
6	759.9	759.6	760.7	11.6	20.8	14.9	15.5	21.0	10.0	05.0	07.7	09.4	10.8	76	51	86	71	-	0	SSE	3	-	0
7	760.1	759.4	760.0	13.0	22.6	15.8	16.8	23.0	11.6	06.0	09.1	09.3	09.8	81	45	73	66	NW	2	SE	2	S	[illegible]
8	760.8	760.4	760.5	14.5	23.8	17.1	18.1	24.6	12.6	07.0	08.3	10.0	10.4	67	45	71	61	N	1	SE	2	N	1
9	761.6	760.5	761.0	13.9	26.3	19.6	19.8	27.3	12.0	06.1	09.5	09.7	09.8	79	38	57	58	-	0	S	1	N	2
10	762.7	762.8	763.3	16.1	26.0	18.4	19.7	26.7	14.6	07.7	09.2	11.3	10.3	67	45	65	59	-	0	SE	3	N	4
11	764.5	763.0	762.8	13.4	24.8	14.4	16.8	25.7	11.4	04.5	08.4	08.6	10.5	73	36	86	65	-	0	S	2	NW	4
12	763.6	761.6	761.3	13.6	25.4	22.6	21.0	25.8	13.0	04.8	04.8	07.3	07.9	41	30	39	37	-	0	SE	2	N	6
13	762.2	761.0	761.1	20.0	24.6	17.8	20.0	25.2	17.6	13.0	08.5	09.3	09.3	48	40	61	50	N	5	SSE	2	-	0
14	760.5	758.7	758.7	15.0	22.9	16.6	17.8	23.2	14.0	07.1	08.9	09.8	12.1	70	47	66	68	N	2	SE	2	-	0
15	758.8	756.9	757.9	12.4	22.6	16.6	17.0	22.8	11.8	06.8	09.1	09.3	09.4	85	45	67	66	-	0	S	3	N	1
16	758.2	759.2	760.9	15.4	14.3	12.4	13.6	17.4	11.7	11.2	07.5	05.9	05.0	57	48	46	50	N	4	N	7	N	7
17	760.5	760.2	760.1	11.3	12.2	11.8	11.8	13.4	10.5	09.7	05.1	07.7	05.3	50	72	51	58	N	7	SE	5	N	5
18	758.2	757.9	758.7	11.6	15.6	14.0	13.8	16.0	10.1	08.0	05.6	07.5	06.1	55	57	51	54	ESE	2	N	2	NNE	4
19	758.7	757.2	756.0	10.8	18.6	12.2	13.4	18.6	08.5	02.0	06.6	07.7	08.6	68	48	80	65	S	2	ESE	2	-	0
20	754.1	752.0	750.5	12.5	15.4	13.3	13.6	15.8	10.6	05.4	08.8	09.4	10.6	80	72	92	81	N	1	-	0	-	0
21	748.4	750.6	751.7	16.2	16.0	14.5	15.3	17.4	12.6	10.4	11.5	11.9	11.5	84	87	93	88	SE	6	E	2	-	0
22	753.3	753.6	752.4	15.2	15.1	14.5	14.8	18.1	14.1	12.3	11.0	11.8	11.4	85	92	92	90	-	0	-	0	S	4
23	752.3	753.7	755.0	10.8	12.8	07.2	09.5	15.0	07.1	08.4	06.3	06.3	05.7	65	57	75	66	N	5	-	0	N	7
24	756.8	759.4	761.9	09.0	11.6	08.8	09.6	12.4	07.9	02.0	04.1	03.6	03.5	47	35	41	41	NNW	5	N	7	N	6
25	763.0	762.3	763.9	08.0	12.4	10.4	10.3	12.6	07.5	04.6	03.0	03.2	03.8	37	30	41	36	N	7	N	6	N	3
26	764.2	762.1	761.5	04.6	17.2	11.4	11.2	18.0	03.4	-01.4	05.2	06.4	07.6	82	43	75	67	-	0	SE	2	-	0
27	762.2	761.9	763.4	07.6	17.8	11.3	12.0	18.3	06.0	00.2	06.3	07.6	08.8	81	50	87	73	-	0	S	2	N	1
28	765.4	765.0	765.1	10.8	19.8	12.8	14.0	20.2	06.2	01.2	06.6	07.8	07.8	68	45	70	61	NW	3	S	2	N	3
29	765.0	764.2	764.9	08.9	18.0	11.3	12.4	18.6	08.5	02.0	06.9	08.5	08.8	80	55	87	74	N	3	SE	1	N	1
30	766.2	764.9	764.6	08.6	20.0	13.0	13.6	21.8	07.6	02.8	07.0	08.4	09.1	84	48	81	71	N	2	-	0	N	2
31	764.6	763.4	763.8	10.6	20.0	12.4	13.8	20.6	08.8	03.0	08.0	08.7	08.8	84	50	81	72	-	0	-	0	-	0
MES. VRED.	759.2	758.5	758.9	12.2	18.8	14.1	14.8	19.8	10.5	05.7	07.2	08.2	08.5	67	51	70	62		2.4		2.8		2.5

TITOGRAD 1970 SEPTEMBAR

BR. ST. 245 H_s = 52 m H_b = 52.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sat	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednji Dnev		7	7	
1	9	03⊙	06	00	03.0	09.8	.	.	F 11^{25}-21
2	8	03⊙	05⊙	00	02.7	11.7	.	.	
3	9	00⊙	02⊙	00	00.7	11.7	.	.	
4	8	00⊙	06⊙	10	02.0	09.2	.	.	⌓ n-8, F 22^{30}-24
5	8	00⊙	04⊙	00	01.3	11.8	.	.	F 0-3
6	8	02⊙	01⊙	00	01.0	11.8	.	.	⌓ 19^{30}-n
7	8	00⊙	06⊙	04	03.3	10.3	.	.	
8	8	00⊙	00⊙	00	00.0	11.7	.	.	
9	8	00⊙	01⊙	00	00.3	11.4	.	.	
10	8	00⊙	00⊙	00	00.0	11.6	.	.	
11	8	00⊙	00⊙	00	00.0	11.5	.	.	
12	8	01⊙	01⊙	02	01.3	11.5	.	.	
13	8	02⊙	01⊙	01	01.3	10.5	.	.	
14	8	03⊙	02⊙	00	01.7	11.0	.	.	
15	8	00⊙	03⊙	03	02.0	10.3	.	.	
16	8	00⊙	00⊙	00	00.0	11.3	.	.	
17	8	04⊙	04⊙	09	05.7	09.7	.	.	F 10-24i, F 15-18^{30}, ⌈ 15^{45}-17, ● 18^{50}-19
18	9	10	09⊙	07	08.7	03.0	00.0	.	F 18-24i
19	8	08	09⊙	04	07.0	05.9	.	.	F 0-24i
20	6	04	08⊙	02	04.7	09.1	.	.	F 0-12, 15-23i, F 1-3^{45}
21	9	01⊙	03⊙	00	01.3	10.1	.	.	F 1^{40}-24, F 6^{30}-15^{30}
22	8	00⊙	06⊙	00	02.0	10.5	.	.	F 0-19i, F 7-15i
23	6	05⊙	10	04	06.3	05.6	.	.	
24	9	00⊙	01⊙	00	00.3	10.2	.	.	F 6^{30}-11, 23-24
25	8	00⊙	01⊙	00	00.3	10.9	.	.	F 0-3^{30}i
26	9	00⊙	06⊙	00	02.0	10.3	.	.	
27	9	10	02⊙	00	04.0	07.1	.	.	F 5^{25}-24i
28	8	01⊙	02⊙	00	01.0	10.3	.	.	F 0-24i
29	9	00⊙	02⊙	00	00.7	10.9	.	.	F 0-9^{20}, 16-24i
30	9	00⊙	00⊙	00	00.0	10.8	.	.	F 0-5^{30}i
MES. VRED.		02.2	03.4	01.5	02.4	301.0	00.0		

TITOGRAD 1970 OKTOBAR

1	8	08⊙	10	10● ⌈	09.3	04.3	.	.	F 13^{10}-23^{50}i, ⌈ 16^{45}-19^{45}, ● 17^{45}-24i, ⌈ 20^{30}-24
2	6	09	02⊙	00	03.7	07.0	71.3	.	● 0-5^{30}, ⌈ 0-1^{45}, F 7^{30}-15, F 15-20
3	6	10	10●	10	10.0	00.0	.	.	● 9^{30}-18^{40}, F 16^{30}-24i, ⌈ 17^{45}-18
4	8	06	09⊙	06	05.7	09.0	24.5	.	F 0-14^{20}
5	8	04⊙	06⊙	10	06.7	08.4	.	.	
6	8	01⊙	01⊙	00	00.7	09.5	.	.	⌓ 0-8, 19-24
7	8	00⊙	01⊙	00	00.3	10.7	.	.	⌓ 0-8, 18^{30}-24
8	8	00⊙	02⊙	00	00.7	10.8	.	.	⌓ 0-7^{30}, 19-24
9	8	00⊙	01⊙	00	00.3	10.8	.	.	⌓ 0-8
10	8	00⊙	00⊙	00	00.0	10.8	.	.	⌓ 19^{30}-24
11	8	00⊙	00⊙	00	00.0	10.7	.	.	⌓ 0-8, 19^{30}-24
12	8	00⊙	00⊙	00	00.0	10.7	.	.	⌓ 0-8, F 20^{35}-24i
13	8	00⊙	00⊙	00	00.0	10.7	.	.	F 1^{35}-17^{20}i
14	8	00⊙	01⊙	00	00.3	10.7	.	.	⌓ 19-24
15	8	07	09⊙	04	06.7	03.5	.	.	⌓ 0-8, 18-24
16	8	10	10	10	10.0	00.3	.	.	F 0-2^{30}, F 9^{40}-24i
17	8	10	10●	10●	10.0	00.0	.	.	F 0-13, 18^{30}-21^{40}i; ● 13^{30}-14^{45}, 18^{45}-22^{40}i
18	8	09	10	09	09.3	00.2	00.2	.	
19	8	07⊙	06⊙	05	06.0	09.8	.	.	
20	8	10	10	10	10.0	00.1	.	.	● 18^{30}-24i
21	8	10●	10●	10● ⌈	10.0	00.0	04.5	.	● 0-2^{40}, 6^{30}-6^{45}, F SE 1^{40}-11^{50}, ⌈ 18^{30}-24, F 23^{40}-24
22	8	10●	10	10●	10.0	00.1	33.0	.	F 0-3, 12-12^{30}, ● 6^{40}-13^{30}i, 17-24
23	8	10●	10	03	07.7	00.9	23.7	.	● 0-7^{20}, 16^{30}-20^{45}i, F 1^{30}-24i, ⌈ 16^{30}-17^{30}
24	8	10	06⊙	00	05.3	07.3	06.6	.	F 7-24i
25	8	02⊙	01⊙	00	01.0	10.4	.	.	F 0-24^{40}i
26	8	01⊙	03⊙	00	01.3	10.2	.	.	⌓ n-8, 19-24
27	8	01⊙	03⊙	00	01.3	10.1	.	.	⌓ 0-8^{30}, 19^{30}-24
28	8	00⊙	02⊙	00	00.7	10.3	.	.	⌓ 0-8^{30}
29	8	03⊙	06⊙	00	03.0	09.5	.	.	⌓ 19^{30}-24
30	8	00⊙	00⊙	00	00.0	10.0	.	.	⌓ 0-8, 18-24
31	8	00⊙	00⊙	00	00.0	10.0	.	.	⌓ 0-8^{30}, 18-24
MES. VRED.		04.4	06.7	03.4	04.2	221.3	169.5		

= 42° 26' N λ = 19° 17' E Gr. ΔG = + 1h 17 min. Br. ST. 245

Dan	Vazdušni pritisak P mm 7	14	21	Temperatura vazduha T C° 7	14	21	Sred Dan	Max	Min	Min 5 cm	Napon vodene pare e mm 7	14	21	Relativna vlažnost U% 7	14	21	Sred Dan	Pravac i jačina vetra 7	14	21
1	763.8	763.4	762.7	10.1	19.5	11.0	12.9	20.4	08.7	02.4	06.8	08.1	08.8	73	48	90	70	N 2	SE 2	- 0
2	762.5	762.0	761.7	12.0	19.5	12.7	14.2	19.8	10.5	05.0	07.1	08.5	09.0	68	50	82	67	N 2	SW 1	NNE 2
3	761.7	760.2	760.8	09.0	18.3	10.4	12.0	19.5	08.2	03.2	07.2	09.3	08.5	84	59	89	77	N 3	SE 4	- 0
4	760.6	759.6	761.0	12.3	18.8	11.4	13.5	19.2	09.5	03.9	08.5	08.3	09.0	79	51	89	73	NW 4	SW 2	- 0
5	761.0	759.1	758.5	07.6	20.8	11.6	12.9	21.8	06.0	00.0	07.0	07.3	08.9	90	40	86	72	- 0	- 0	- 0
6	755.4	754.0	756.9	12.0	12.4	11.6	11.9	13.6	10.2	05.4	09.1	09.7	04.1	87	90	40	72	- 0	- 0	NNE 8
7	758.3	758.5	759.6	10.2	15.0	08.8	10.7	15.8	08.0	06.8	03.5	04.5	05.2	37	36	61	45	N 5	SSE 3	N 1
8	761.4	762.1	761.9	08.5	08.0	08.4	08.3	09.6	07.8	04.2	05.4	07.0	07.3	65	87	89	80	N 1	N 1	- 0
9	761.2	758.2	756.3	09.2	11.2	11.0	10.6	11.6	08.5	07.2	08.1	09.3	09.0	93	93	92	93	- 0	- 0	N 2
10	753.0	752.8	754.4	10.1	11.9	12.3	11.6	13.3	09.0	05.7	08.8	09.4	04.3	95	90	40	75	- 0	- 0	NW 7
11	760.0	760.3	762.3	10.4	13.8	09.4	10.8	13.8	01.0	06.0	03.5	03.7	03.0	37	31	34	34	N 6	N 6	NNE 5
12	763.5	762.4	762.9	01.4	14.4	05.5	06.7	15.8	01.0	-05.0	04.1	03.8	05.2	80	31	76	62	- 0	SE 2	ENE 2
13	763.3	762.0	762.3	04.6	15.2	07.8	08.8	16.4	02.5	-03.0	04.4	04.4	05.1	70	34	65	56	N 2	- 0	N 3
14	761.2	759.1	756.9	07.5	10.4	08.4	08.7	10.9	05.3	00.2	05.1	06.3	07.5	66	67	91	75	N 2	- 0	- 0
15	752.4	751.7	749.0	12.4	15.0	14.2	14.0	15.0	07.6	08.0	09.7	10.6	10.6	90	83	88	87	SE 7	SE 6	SSE 2
16	747.0	748.4	750.0	11.2	11.6	08.4	09.9	12.6	08.0	07.0	08.8	07.7	06.8	89	76	82	82	SE 3	SE 5	NNE 4
17	754.0	756.8	759.3	05.2	12.8	08.0	08.5	13.6	04.5	-01.0	06.0	05.6	06.8	90	51	85	75	- 0	SSE 4	- 0
18	761.5	762.0	761.9	06.8	09.2	09.0	08.5	10.0	05.0	-01.4	06.6	07.0	07.8	89	81	90	87	- 0	- 0	- 0
19	760.6	759.9	758.9	09.6	12.6	10.8	11.0	12.8	08.8	08.4	08.3	09.9	09.1	93	90	94	92	- 0	N 1	- 0
20	758.5	758.1	758.5	11.2	15.8	13.6	13.6	16.8	10.3	06.9	09.7	12.4	11.1	98	92	95	95	- 0	SW 1	- 0
21	759.5	758.1	755.9	12.0	15.5	16.0	14.9	16.4	12.0	10.6	09.9	11.8	11.5	94	89	84	89	- 0	- 0	SE 6
22	751.6	751.4	752.3	13.6	14.4	08.8	11.4	16.4	08.5	09.4	10.1	08.1	08.0	86	66	94	82	SE 2	SE 2	N 2
23	753.1	753.8	755.1	11.2	12.8	11.6	11.8	13.4	07.0	02.6	04.6	04.4	04.7	46	40	46	44	NNW 6	NNW 6	NNW 8
24	757.3	759.3	760.4	12.2	15.4	13.2	13.5	15.6	11.5	09.0	05.4	05.3	05.0	51	40	44	45	N 7	N 8	N 4
25	762.1	762.5	763.4	04.8	14.8	08.0	08.9	15.6	04.0	-01.8	05.3	05.7	06.0	83	45	75	68	- 0	S 2	- 0
26	764.0	763.3	763.5	01.2	14.6	09.2	08.6	15.2	00.8	-04.8	04.7	04.5	03.9	93	36	44	58	- 0	S 4	- 0
27	763.2	762.1	763.3	04.8	15.4	06.6	08.4	16.7	04.0	-01.6	05.3	04.8	06.3	83	36	86	68	SW 2	SSE 2	- 0
28	763.4	762.3	762.2	02.3	15.0	07.3	08.0	16.0	01.8	-03.0	04.8	05.6	06.2	89	44	80	71	- 0	SE 2	N 2
29	762.7	762.4	762.7	06.9	13.5	08.6	09.4	14.4	04.3	-01.9	05.6	07.4	07.2	75	63	86	75	N 2	S 3	N 2
30	762.6	762.5	761.0	07.6	13.0	09.2	09.8	13.2	05.6	02.0	06.7	07.7	07.4	86	69	85	80	- 0	W 1	N 2
MES. VRED.	759.3	758.9	758.8	08.6	14.4	10.1	10.8	15.2	06.7	03.0	06.7	07.3	07.1	79	60	76	72	1.9	2.3	2.1

1	759.9	759.1	759.0	10.0	12.0	11.0	11.0	12.1	08.0	04.4	08.8	09.9	09.3	95	94	94	94	N 1	N 1	- 0
2	757.6	756.8	758.1	10.6	16.8	10.4	12.0	18.8	09.5	07.8	08.2	10.6	08.1	86	74	86	82	S 1	SSE 3	- 0
3	758.8	758.3	757.5	09.4	13.3	09.0	10.2	15.0	08.5	04.8	07.2	07.4	08.0	82	65	93	80	- 0	SE 1	- 0
4	756.7	758.7	762.1	07.6	12.4	07.4	08.7	13.2	05.6	02.6	07.2	02.5	02.3	92	23	30	48	N 1	NE 6	N 5
5	763.4	762.5	763.3	04.8	10.0	04.4	05.9	11.0	02.6	-06.0	02.2	03.1	03.9	34	34	62	43	WNW 5	SE 2	ENE 2
6	764.3	763.8	764.8	04.4	11.4	07.6	07.8	11.5	04.0	00.0	05.7	03.5	03.8	91	35	48	58	- 0	N 6	WNW 4
7	765.8	764.5	765.8	02.0	12.2	03.5	05.3	12.3	01.3	-04.3	04.3	03.5	04.2	80	33	71	61	NE 1	- 0	NE 2
8	767.5	768.2	768.7	03.4	09.4	07.0	06.7	09.6	01.5	-04.0	04.0	04.7	06.2	68	53	83	68	N 2	- 0	- 0
9	768.3	767.6	767.3	09.3	12.7	07.8	09.4	12.8	06.6	04.6	03.5	03.4	03.3	39	31	41	37	N 8	N 7	NW 2
10	766.3	764.7	764.1	09.0	12.0	11.8	11.2	12.8	06.5	-01.0	03.4	03.9	04.1	40	37	40	39	N 8	N 8	NW 6
11	767.2	767.4	768.5	05.8	12.2	05.4	07.2	12.4	-00.4	-00.8	04.2	04.9	04.8	61	46	72	60	- 0	SSE 3	- 0
12	768.0	766.9	767.0	00.0	13.8	04.0	05.4	14.8	-00.3	-05.4	04.3	04.6	05.0	93	39	82	71	- 0	- 0	- 0
13	766.8	765.1	766.3	00.2	13.5	03.7	05.3	14.0	-00.5	-06.7	04.2	03.9	04.9	89	33	82	68	- 0	S 1	NNE 1
14	766.4	764.5	764.0	01.0	12.3	04.6	05.6	13.1	00.3	-06.1	03.8	04.3	04.9	78	40	77	65	N 1	- 0	NNE 1
15	761.7	759.8	759.9	03.4	12.8	09.4	08.0	13.4	03.0	-03.0	04.2	05.6	03.7	73	51	42	55	N 3	- 0	N 8
16	761.0	761.5	762.8	05.8	07.8	05.4	06.1	09.7	05.0	-01.7	02.4	03.2	02.9	35	40	43	39	N 8	N 8	N 8
17	764.6	763.8	764.1	04.4	07.0	04.4	05.0	07.2	-03.2	01.4	02.4	02.8	02.7	38	37	43	39	N 7	N 6	NNW 4
18	763.2	761.4	762.2	-03.0	07.4	00.4	01.3	08.6	-03.2	-09.2	03.1	03.2	03.4	85	42	72	66	- 0	- 0	- 0
19	763.9	764.0	764.7	-02.2	08.3	02.6	02.8	08.4	-03.0	-08.9	03.4	04.0	04.1	86	48	75	70	N 1	SE 1	N 3
20	765.8	764.2	763.5	-02.4	09.1	00.2	01.8	09.2	-03.0	-09.3	03.3	03.6	03.7	86	41	79	69	- 0	SSE 1	- 0
21	760.4	757.4	755.4	-03.0	08.8	00.0	01.4	09.8	-04.0	-10.6	03.1	03.6	03.8	83	42	84	70	- 0	S 2	- 0
22	752.4	751.4	750.4	00.0	05.0	07.2	04.8	07.4	-02.5	-08.7	03.9	05.0	03.9	86	78	81	71	SW 1	SSE 1	N 4
23	747.8	748.1	748.8	03.8	03.2	04.0	03.8	07.2	00.5	02.0	05.4	05.3	05.6	89	92	92	91	- 0	- 0	- 0
24	753.8	755.0	755.9	01.0	10.4	05.0	05.4	11.4	00.4	-04.8	04.5	03.3	04.3	91	35	66	64	- 0	- 0	- 0
25	754.0	751.9	751.6	04.5	05.7	06.2	05.6	09.3	03.7	-03.9	05.1	06.2	06.1	81	90	86	86	NE 2	NW 2	ESE 4
26	755.3	758.3	760.5	04.2	08.8	04.3	05.4	09.4	02.2	01.5	05.7	06.5	05.7	92	77	91	87	- 0	SSW 2	NE 2
27	760.1	759.4	758.1	04.0	04.8	05.6	05.0	06.0	02.5	-03.7	04.5	05.9	06.3	73	91	93	86	NW 1	- 0	SE 2
28	753.5	751.4	756.9	12.7	11.0	06.2	09.0	13.4	05.4	05.2	07.8	08.4	06.2	70	85	88	81	SE 8	SE 7	- 0
29	755.2	753.2	751.2	06.0	10.4	13.4	10.8	15.4	04.0	-01.0	06.0	08.5	08.2	86	89	71	82	- 0	- 0	SE 6
30	746.6	745.7	749.3	14.0	14.8	09.8	12.1	17.0	09.0	10.0	08.6	09.6	06.9	72	76	76	75	SE 8	S 5	SE 4
31	750.2	744.6	742.0	06.8	09.0	12.4	10.2	12.5	05.5	04.2	06.0	07.8	07.9	81	90	73	81	- 0	N 2	SE 8
MES. VRED.	760.2	759.3	759.5	04.4	10.3	06.3	06.8	11.6	02.4	-01.6	04.8	05.2	05.1	75	56	70	67	2.2	2.4	2.4

BR. ST. 245 H_s = 52 m H_b = 52.6 m h_t = 2.0 m h_r = 1.2 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	8	00⊙	00⊙	00	00.0	10.0	.	.	⌓ 0-8, 18^{30}-24
2	8	10	07⊙	00	05.7	06.9	.	.	⌓ 0-8, 19-24
3	8	07	06⊙	00	04.3	07.9	.	.	⌓ 0-7^{30}, 19-24
4	8	10	00⊙	00	03.3	07.1	.	.	⌓ 0-6^{50}, 18-24
5	8	00⊙	02⊙	00	00.7	09.9	.	.	⌓ 0-7, 19-24
6	6	10	10●	10	10.0	00.0	.	.	⌓ 0-7, ● 7^{40}-17^{05}, F 16^{15}-24i
7	8	02	01⊙	00	01.0	09.8	11.7	.	F 0-6^{40}, F 6^{40}-10
8	7	10	10●	10●	10.0	00.0	.	.	● 11-21^{30}
9	7	10●	10●	10	10.0	00.0	08.0	.	● 6^{30}-14^{40}, 21^{40}-23^{30}
10	8	10●	10	04	08.0	00.2	12.5	.	● 2-13^{40}i, F 17^{30}-24
11	8	01	01⊙	00	00.7	09.4	06.7	.	F 0-20^{40}i
12	8	00	00⊙	00	00.0	09.7	.	.	⌣ n-7^{30}, ⌓ 18-24
13	8	00	04⊙	08	04.0	08.9	.	.	⌣ n-7^{30}, ⌒ 22-24
14	8	10	10	10●	10.0	00.2	.	.	⌒ 0-2, ● 15^{30}-24
15	7	10●	10●	10●	10.0	00.2	26.6	.	● 0-24, F 5^{30}-7^{30}, F 12-14^{30}, 20-24i
16	7	10●	10●	09	09.7	01.0	33.6	.	● 0-24i, F 4^{40}-5^{40}, 7^{45}-12^{40}i, ⊓ 21-21^{30}
17	8	04	03⊙	03	03.3	07.7	11.0	.	● 0-1^{45}i
18	8	10	10	10	10.0	00.0	00.2	.	● 22-24
19	8	10	09	08	09.0	00.8	04.0	.	● 0-24i
20	8	09	09●	10●	09.3	01.2	03.6	.	● 0-24i, ⌇ 17-19^{30}
21	8	10●	10●	10●	10.0	00.7	21.7	.	● 0-8^{30}, 13^{30}-24i; F 20^{30}-24i
22	8	10●	10●	10	10.0	02.0	46.5	.	● 0-15^{40}, 21^{50}-22^{50}i; F 0-4^{30}, 10^{30}-13; ⊓ 14^{30}-16
23	8	10	08⊙	03	07.0	05.3	07.4	.	F 4-16, F 20^{40}-24i
24	8	04	03⊙	00	02.3	09.2	.	.	F 0-11, 17-20^{40}, F 11-17
25	8	00	00⊙	00	00.0	09.8	.	.	⌓ 18-24
26	8	00	00⊙	00	00.0	08.6	.	.	⌣ n-7^{30}, ⌓ 18-24
27	8	01	00⊙	00	00.3	08.7	.	.	⌓ 0-8, 18-24
28	8	03	03⊙	02	02.7	08.6	.	.	⌓ 0-8, 18-24
29	8	07	07⊙	02	05.3	04.8	.	.	⌓ 0-8, 18-24
30	7	07	10	05	07.3	00.0	.	.	⌓ 0-7^{30}
MES. VRED.		06.2	05.8	04.5	05.5	147.5	213.5		

1	7	10●	10●	10	10.0	00.0	04.3	.	● 3-17i, 23^{30}-24; = 18^{30}-20
2	8	10	01⊙	02	04.3	07.1	14.2	.	● 0-8^{30}, ∩ 7^{20}-7^{35}, ⊓ 7^{45}-8
3	8	08	09	08	08.3	03.8	05.2	.	● 2-4^{30}, 14-23i
4	8	10	02⊙	00	04.0	07.2	04.0	.	F 10^{30}-14^{30}i
5	8	00	00⊙	00	00.0	08.5	.	.	
6	8	10	06⊙	00	05.3	03.1	02.8	.	● 0^{30}-4^{35}, F 13^{40}-17
7	8	00	00⊙	06	02.0	08.4	.	.	⌣ 20-n, ⌒ 20^{45}-21^{30}
8	8	06	10	10	08.7	01.8	.	.	F 1^{50}-17^{30}i
9	8	02	00⊙	02	01.3	08.5	.	.	F 2^{40}-3^{50}, 16^{30}-24i; F 4-16^{30}i
10	8	02	04	04	03.3	07.2	.	.	
11	8	00	08	00	02.7	08.9	.	.	⌓ 17^{30}-24
12	8	00	00⊙	00	00.0	08.6	.	.	⌣ n-8^{30}, ⌓ 17^{30}-24
13	8	00	00⊙	00	00.0	08.4	.	.	⌣ n-8^{30}, 19-24
14	8	02	08⊙	10	06.7	08.4	.	.	⌣ 0-8, ⌓ 18-23, ⌒ 19-23
15	8	04	04⊙	06	04.7	07.6	.	.	F 18-18^{30}, F 18^{30}-24
16	8	06	09	05	06.7	00.0	.	.	F 0-24
17	8	01	03⊙	00	01.3	08.6	.	.	F 0-20^{35}
18	8	00	00⊙	00	00.0	07.6	.	.	⌣ n-8^{30} 20-24
19	8	00	00⊙	00	00.0	07.5	.	.	⌣ 0-8^{30} 19-24
20	8	00	00⊙	00	00.0	07.7	.	.	⌣ 0-9, 18^{30}-24
21	8	00	03⊙	04	02.3	08.1	.	.	⌣ 0-8^{30} 19-24
22	8	10	10	09	09.7	00.0	.	.	⌣ 0-8^{30}, ● 14^{30}-14^{30} F 13^{30}-13^{30}, 18^{30}-20^{40}
23	7	10●	10●	10●	10.0	00.0	01.2	.	● 5^{45}-23i, * 9-9^{15}
24	8	09	09	10	09.3	02.6	23.9	.	● 7^{15}-24, ⊓ 14-20, F 16^{35}-19^{45}
25	7	10	10●	10●	10.0	00.0	.	.	
26	8	06	08	05	06.3	01.2	34.8	.	● 0-4^{30}, ⌓ 18^{30}-n
27	7	10	10●	10●	10.0	00.0	.	.	● 8^{30}-24
28	7	10●	10●	00	06.7	00.0	19.0	.	● 0-15i, F 6-14^{30}i, ⊓ 9^{20}-13^{30}i
29	7	10	10	10●	10.0	00.0	26.6	.	● $^{0-1}$ 7^{30}-24i, F 17^{45}-24
30	7	10●	10●	00	06.7	00.0	22.2	.	● 0-16^{30}, ⊓ 4^{30}-6, F 6^{45}-7^{35}i, F 7^{30}-10^{20}, 14^{40}-18^{40}
31	7	10●	10●	10●	10.0	00.0	29.9	.	● $^{0-1}$ 0-24, F 18-18^{30}-24i
MES. VRED.		05.4	05.6	04.5	05.2	141.5	188.0		

φ = 41° 57' N λ = 21° 38' E Gr. ΔG = + 1h 27 min. BR. ST. 265

Ден	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	734.3	730.3	729.9	07.0	13.1	09.8	09.9	13.6	06.2	04.0	06.1	06.7	06.5	81	59	72	71	SE 2	SE 5	NE 2
2	729.0	730.6	735.1	04.3	05.0	01.9	03.5	10.1	01.8	01.6	05.9	05.6	04.3	94	81	82	86	- 0	NNE 5	NNE 3
3	738.8	739.3	741.1	00.6	05.6	00.7	01.9	06.6	00.4	00.1	04.0	04.8	04.6	84	70	95	83	NE 3	NNW 1	- 0
4	742.4	741.7	741.5	00.8	03.5	02.6	02.4	04.5	00.2	-02.4	04.5	05.0	05.3	93	85	97	92	- 0	- 0	- 0
5	738.5	736.0	734.7	03.1	09.0	08.4	07.2	09.2	01.6	00.0	05.5	06.9	07.6	95	80	92	89	- 0	NW 1	NNW 2
6	733.9	734.1	735.6	07.8	09.8	08.9	08.8	10.6	07.8	07.5	07.7	08.4	08.2	97	93	96	95	- 0	- 0	- 0
7	733.4	732.8	736.1	10.7	16.6	10.6	12.1	16.7	07.6	06.8	09.1	09.9	08.7	94	70	91	85	SSE 3	SSE 1	- 0
8	741.6	745.3	748.4	04.4	03.4	03.0	03.4	10.7	02.2	04.1	04.8	04.0	03.8	77	68	66	70	NNE 5	NNE 5	NNE 4
9	749.5	748.3	749.1	-01.0	04.6	01.0	01.4	05.4	-01.6	-02.2	03.3	04.0	04.3	77	63	86	75	N 2	- 0	- 0
10	749.2	749.1	749.0	02.2	04.9	04.4	04.0	05.1	00.9	-02.5	04.7	04.9	05.4	87	76	87	83	- 0	- 0	- 0
11	747.3	745.0	744.0	05.0	07.1	05.4	05.7	07.4	04.4	01.0	05.6	05.9	05.8	86	78	86	83	SSE 2	SSE 2	SSE 2
12	741.7	739.4	738.2	05.2	07.0	06.4	06.2	07.5	05.2	05.1	05.9	06.1	06.4	89	81	89	86	SSE 2	SE 1	SW 1
13	736.3	736.1	735.5	07.4	09.8	08.0	08.3	10.2	06.2	06.0	06.9	07.8	07.4	89	86	92	89	S 2	S 3	- 0
14	736.0	735.9	736.0	06.0	11.1	08.6	08.6	11.3	05.4	05.0	06.8	07.9	07.7	97	80	92	90	- 0	NW 2	- 0
15	738.0	737.6	738.4	07.6	12.1	09.2	09.5	12.9	07.4	07.4	07.2	07.5	07.7	92	71	88	84	- 0	- 0	SE 2
16	737.5	735.7	732.5	07.6	11.4	11.8	10.6	12.0	07.6	05.9	07.2	08.3	07.9	92	82	78	83	- 0	SSE 3	SSE 6
17	730.6	729.9	734.3	07.0	08.8	05.0	06.4	12.0	05.0	06.4	06.9	07.4	05.0	92	88	77	86	SW 1	NW 3	NNE 5
18	737.2	738.2	740.3	04.0	04.4	02.0	03.1	05.2	02.0	03.6	04.5	04.5	04.0	73	72	76	74	NNE 3	NNE 4	NE 2
19	741.5	742.3	744.5	-02.6	-02.3	-03.6	-03.0	02.0	-03.7	-02.2	03.1	02.7	02.4	82	70	69	74	NNE 4	NNE 6	NNE 3
20	746.3	746.0	747.1	-04.1	-01.0	-04.2	-03.4	-00.9	-04.8	-04.9	02.4	02.6	02.4	69	62	71	67	NNE 4	NW 2	NNE 4
21	746.3	745.1	744.8	-05.6	-01.1	-04.8	-04.1	-00.4	-06.0	-06.8	02.6	02.7	02.7	86	63	83	77	NNE 3	NE 1	NNE 3
22	744.8	744.7	745.2	-03.8	-02.4	-02.9	-03.0	-02.1	-05.2	-06.5	02.6	02.7	02.9	76	71	78	75	N 2	WNW 1	NNE 4
23	746.1	746.2	747.4	-03.1	-01.9	-02.4	-02.4	-01.9	-03.4	-03.1	02.7	03.0	03.1	73	74	82	76	NNE 3	- 0	NE 1
24	747.2	747.6	748.4	-02.4	00.4	-04.8	-02.9	00.6	-04.8	-03.0	03.2	03.5	03.1	82	73	95	83	N 1	NNE 1	- 0
25	748.0	747.6	747.2	-03.8	00.1	-01.4	-01.6	00.4	-06.6	-10.4	03.3	03.7	04.0	96	81	97	91	- 0	WNW 2	- 0
26	748.8	749.8	751.2	-03.6	01.6	00.6	-00.2	02.0	-03.8	-05.0	03.3	04.4	04.5	92	85	93	90	ENE 2	- 0	- 0
27	751.5	750.6	748.8	00.4	02.4	00.8	01.1	02.6	00.4	00.0	04.5	03.9	04.4	95	71	90	85	- 0	- 0	E 1
28	745.6	743.1	742.5	00.2	01.8	00.4	00.7	02.0	00.2	00.4	04.0	04.3	04.4	86	82	93	87	E 1	NNE 1	- 0
29	741.2	741.7	743.1	03.2	03.3	00.9	02.1	04.3	00.4	-00.2	04.3	04.6	03.8	75	80	78	78	NW 3	N 3	N 3
30	741.6	739.0	739.5	-01.3	03.8	00.0	00.6	05.0	-01.6	-04.0	03.4	03.4	03.9	82	56	86	75	E 1	SSE 2	- 0
31	737.8	736.6	736.2	00.6	01.0	01.2	01.0	01.6	00.0	-02.9	04.5	04.8	04.8	93	97	97	96	- 0	- 0	ENE 0
MES. VRED.	741.4	740.8	741.5	02.0	05.0	02.8	03.2	06.0	01.0	00.3	04.8	05.2	05.1	86	76	86	82	1.6	1.8	1.5

1	736.6	737.1	738.1	02.0	02.0	-00.2	00.9	02.3	-00.2	00.9	04.8	04.3	04.0	90	80	89	86	SW 1	NW 2	NNE 3
2	740.0	740.5	740.2	-00.4	03.4	02.2	01.8	04.0	-00.4	-00.4	03.8	03.9	04.5	85	67	84	79	NNE 2	- 0	- 0
3	738.9	737.2	736.5	-00.2	04.1	02.5	02.2	04.9	-01.4	-04.5	04.2	04.4	05.0	93	72	92	86	- 0	- 0	NE 1
4	738.9	739.6	740.3	01.3	09.2	01.9	03.6	10.8	-00.5	-03.0	04.8	06.0	05.0	95	69	95	86	- 0	NW 1	- 0
5	739.4	738.2	737.6	-00.2	10.8	04.1	04.7	12.4	-02.0	-03.5	04.3	07.1	05.7	96	73	92	87	- 0	W 1	N 2
6	738.5	738.9	740.1	-01.2	13.8	10.8	08.6	15.2	-01.8	-03.0	04.1	07.8	05.4	97	66	56	73	SW 1	SW 1	SSE 1
7	740.0	739.1	740.5	04.0	16.8	07.4	08.9	17.1	02.7	01.0	05.2	06.0	06.7	85	42	87	71	W 1	ENE 2	NNE 4
8	740.4	739.4	740.0	05.0	10.0	04.2	05.8	11.0	03.8	04.0	06.2	07.3	06.0	94	79	97	90	NNE 2	NE 2	NE 1
9	741.6	740.0	739.1	00.8	11.4	06.4	06.2	14.0	00.4	00.2	04.9	07.6	06.2	100	75	86	87	E 1	- 0	SE 1
10	735.3	731.3	729.5	03.9	17.0	15.0	12.7	17.7	03.4	02.1	05.5	05.8	05.4	91	40	42	58	N 2	WSW 3	SW 2
11	734.7	733.6	730.0	05.4	12.2	08.2	08.5	15.6	05.0	03.0	06.0	05.5	05.5	89	52	68	70	NNE 2	SSE 1	SSE 2
12	731.8	737.3	740.5	04.4	06.4	01.2	03.3	11.9	00.7	03.4	04.6	03.1	03.3	74	43	66	61	S 3	NW 3	NNE 3
13	741.6	739.6	737.7	-03.2	06.9	03.9	02.9	09.4	-03.7	-06.4	03.2	03.3	04.4	89	44	73	69	- 0	SSE 2	- 0
14	737.2	737.9	738.8	02.8	08.6	09.4	07.0	09.6	01.7	-00.4	05.1	06.1	06.8	90	73	82	82	- 0	- 0	SE 3
15	731.4	731.2	731.1	11.0	12.8	10.0	11.0	14.0	05.6	05.5	06.3	07.7	06.2	64	69	68	67	SSE 4	NW 3	S 3
16	732.3	734.6	732.7	04.2	09.8	03.2	05.1	11.6	03.2	02.5	05.7	03.9	05.1	92	42	89	74	SSE 2	SW 3	NNE 3
17	734.4	739.1	743.6	-02.1	-01.0	-04.2	-02.9	03.4	-04.2	-02.6	03.0	02.5	02.3	77	58	67	67	N 4	W 5	WNW 2
18	746.0	744.2	743.0	-09.8	01.2	-00.4	-02.4	02.9	-10.0	-13.6	01.9	02.3	03.2	88	46	72	69	E 1	WNW 2	- 0
19	739.7	740.3	743.6	-01.2	00.2	-01.8	-01.2	02.1	-03.2	-04.6	03.5	04.5	03.3	84	96	83	88	- 0	W 2	SW 2
20	744.8	745.1	744.3	-01.2	02.4	-01.4	-00.4	02.6	-02.3	-02.4	03.1	03.2	03.0	74	59	73	69	W 2	WNW 3	N 2
21	742.8	742.1	742.2	-06.4	02.6	-01.6	-01.8	03.5	-06.6	-09.2	02.5	03.5	03.6	89	62	89	80	- 0	SW 1	S 1
22	741.7	740.4	740.1	-05.0	05.4	02.5	01.4	05.7	-05.0	-07.5	02.9	04.6	04.7	91	68	86	82	- 0	SW 1	- 0
23	737.7	735.0	732.5	-01.9	06.5	03.8	03.0	06.9	-07.0	-04.9	03.8	05.0	05.3	96	69	88	84	- 0	W 2	- 0
24	734.3	734.1	734.3	03.8	08.4	02.0	04.0	09.0	01.3	02.5	04.6	03.9	03.8	76	47	72	65	WNW 4	NW 4	NNE 2
25	734.6	734.5	735.5	00.8	03.2	00.2	01.1	04.2	-00.2	-03.6	03.0	03.2	03.2	63	56	68	62	WNW 5	NNE 5	NNE 3
26	735.3	734.6	735.0	-02.0	04.3	01.6	01.9	07.2	-02.2	-05.7	03.5	03.1	04.3	88	44	83	72	ENE 1	NW 2	NE 1
27	733.4	733.3	734.1	00.2	03.4	00.6	01.2	03.7	-01.0	-04.2	03.8	03.7	04.5	82	64	93	80	- 0	W 2	SW 2
28	736.0	735.9	738.2	00.1	04.5	01.9	02.1	05.0	-00.3	-01.1	03.6	03.3	03.1	77	52	60	63	N 2	NNE 4	N 4
MES. VRED.	737.6	737.6	737.7	00.5	07.1	03.3	03.5	08.5	-00.7	-02.0	04.2	04.7	04.6	86	61	78	75	1.4	2.0	1.7

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BR. ST. 265 H_s = 232 m H_b = 233.3 m h_s = 2.0 m h_r = 1.3 m

Dan	Vidljivost 0-9 14	Oblačnost N (0—10) 7	14	21	Srednji Dnev	Insolacija broj sati	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	7	08	10	10	09.3	04.2	•	•	F_{SE} 0-1^{30} 7^{30} 18^{53} i; •° 20^{35}- 24i
2	7	10•	09	09	09.3	00.6	01.8	•	•° 0-3^{40}, 7-7^{40}, 9^{45}, 12^{20}
3	7	08	04⊙	02	04.7	00.9	01.2	•	= 6^{25}- 24
4	6	10	10	07	09.0	00.0	•	•	= 0-24i, •° 0-13^{45}- 4^{40}, 15^{30}- 18^{45} i, 22^{40}- 22^{55}; ≡ 7-8^{30}
5	6	10	10	10	10.0	00.0	00.0	•	
6	4	10•	10	10	10.0	06.0	01.2	•	= 0-22^{30} •° 5^{20} 7^{40} 11^{05}- 13^{20}
7	8	10•	08	03	07.7	01.7	09.1	•	≡ °0-3^{40}, •° 0-12^{40}- 17^{30} i, = 3^{40}- 6^{40}, F_{SSE} 8^{05}- 13^{08}
8	7	10	10	10	10.0	00.0	00.0	•	F_{NNE} 0^{27}- 16^{37} i
9	7	08	08	10	08.7	00.1	•	•	= 6^{40}- 22^{30}
10	6	10	10	10	10.0	00.0	•	•	
11	7	10	10	10	10.0	00.2	•	•	•° 21^{35}- 22
12	7	10	10	10	10.0	00.0	•	•	•° 6^{35}- 11^{55} i, = 8^{30}- 13^{25} 16^{30} 24
13	7	10•	09	10	09.7	00.0	00.0	•	= 0-24i, •° 0^{40}- 1^{30} i, ≡ 6^{55}- 8^{20}
14	6	10	09	10	09.7	00.1	00.4	•	= 0-12^{40}
15	7	10	09	09	09.3	00.9	•	•	
16	7	10	10	09	09.7	00.0	•	•	•° 7^{40}- 9^{40} i, 12^{30} 13^{30} i; F_{SE} 13^{55}- 24i
17	7	10	09•	10	09.7	00.0	16.5	•	•° -1 0^{30}- 5^{20} 13^{22}- 15^{20} i, 18^{40}- 19^{45} i; F_{NE} 15-20^{40}
18	7	10	09	10	09.7	00.1	00.4	•	•° 3^{40}- 3^{45} i, 8^{40}- 11^{40} i; F_{NNW} 14^{52}- 16^{20} i
19	7	10*	10	10	10.0	00.0	00.1	•	F_{NNE} 3^{40}- 23^{45} i, *° 15^{20}- 17^{30}
20	7	10	08	04	07.3	01.9	00.0	•	F_{NNE} 1^{40}- 8^{30} i, 14^{40}- 24i
21	7	09	05⊙	00	06.7	06.6	•	•	= 13^{45}- 18^{40}
22	6	10	10	10	10.0	00.0	•	•	= 13^{40}- 24
23	7	10	10	10	10.0	00.0	•	•	= 0-19^{30} ⌴ 19^{30}- 24
24	6	10	09⊙	00	06.3	00.5	•	•	⌴ °0-9^{40}, = 6^{30}-24, *° -1-2 15^{40}- 15^{45}, 18^{30}- 23i; ⊠
25	6	10	10	10*	10.0	00.0	•	•	
26	5	10	10	10	10.0	00.0	03.2	04	= 0-24, ⊠
27	5	10	10	10	10.0	00.0	•	•	= 0-11^{20}
28	5	10	10	09	09.7	00.0	•	•	= 6^{40}- 24
29	7	10	10	03	07.7	00.0	•	•	= 0-5^{45}, •° 8^{40}- 9^{20}, •° 9^{20}- 13^{15}
30	7	08	06	09	07.7	04.8	00.4	•	*° -1 0-1^{20}, 7^{25}- 15; △ 6^{30}- 7^{25}, * 15-15^{45}, ≡ 15^{40}- 17^{45}, •° 15^{35}- 18^{40}, = 17^{45}-24, ⊠
31	3	10	10*	10	10.0	00.0	00.3	•	
MES. VREDN.		09.7	09.1	08.2	09.0	31.6	44.6		

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1	7	10•	10	10	10.0	00.0	04.0	•	≡ 0-7^{45} i, ≡ 3^{05}- 4^{45}, •° 4^{40}- 4^{45}, • 4^{45}- 8^{35}
2	6	10	10	10	10.0	01.6	00.0	•	*° 7^{02}- 7^{40} i, = 8^{30}- 17^{20}
3	7	10	10	06	08.7	00.1	00.0	•	⌴ 0^{20}- 8^{40}, = 5^{30}- 12^{45} 16^{30}- 24; △ °23-24
4	7	10•	01	00	03.7	04.0	01.6	•	△ °0-3^{30}, = 0-9^{30}, •° 3^{30} 6^{40}
5	6	10≡	03⊙	00	04.3	04.3	•	•	⌴ 0-9^{30}, = 3-6^{30}, 11^{45}- 24; ≡ 6^{30}- 11^{40}, ≡ 11^{40}- 11^{45}, △ °18^{30}- 24
6	5	10≡	06⊙	02	06.0	00.3	•	•	= 0-2^{30} 10^{30} 15, ⌴ °0-8^{30} ≡ 2^{30}- 6^{40}, 9^{30} 10^{30}, ≡ 6^{40}- 9^{30}
7	8	10	09	10•	09.7	02.1	•	•	•° 16^{40}- 23^{50} F_{NNE} 14^{35}- 17^{40}
8	7	10	09	00	06.3	02.0	12.3	•	•° 2^{30}- 5^{45} 10^{30}- 11^{40} i, 14^{30}- 16^{40} i; ≡ °22^{30}- 24
9	6	10≡	01⊙	07	06.0	05.3	01.2	•	≡ °0-6^{30} 10^{30}- 10^{45}, ≡ °6^{30}- 10^{45}, = 10^{45}- 13^{40} 16^{30} 21^{40}
10	8	09	06⊙	04	06.3	03.2	•	•	F_{WSW} 16^{50}- 16^{58}
11	8	09	09⊙	06	05.0	04.8	•	•	$F_{NE-S-SE}$ 2^{45}- 5^{47} 22^{05}- 23
12	8	10•	06⊙	00	05.3	04.7	04.6	•	$F_{S-SE-WNW-NNW}$ 0^{05}- 2^{40}, 11^{40}- 16^{30} i; •° 3^{40}- 7^{40}
13	7	09	03⊙	05	06.0	05.9	00.0	•	⌴ °0^{45}- 10
14	6	09	06	08	07.7	02.0	00.1	•	•° 3^{45}- 3^{25} 5^{30}- 10^{40} i, 18^{35}- 21^{50} i; = 6^{40}- 17^{20} F_{SE} 22^{40}- 24
15	7	05	09	03	05.7	02.0	00.7	•	F_{SE-SSE} 0-7^{37} i, 22^{05}- 22^{07}, •° 7^{40}- 17^{15} i, ∩ 13^{02}- 14^{30} i
16	8	08	08⊙	10•	08.7	06.0	01.0	•	•° 0^{50}- 2^{40} i, 18^{30}- 22^{45} i; $F_{WSW-NNE}$ 10^{15}- 12^{45} 23^{40}- 24
17	7	10*	10	01	07.0	00.1	00.2	•	F_{NNE-W} 0-13^{30} i, *° 5-8^{30}, ⊕ 7^{30}- 10^{40}, ⊠
18	7	00	03⊙	03	04.3	09.1	00.7	-	▽ 19^{40}- 20^{05} ⊠
19	3	08	10*	10*	09.3	00.0	•	•	= 6^{45}- 16^{20}, *° 10^{50}- 24, ⊠
20	7	10	10	00	06.7	00.0	04.0	07	*° 0-6^{45}, ⊠
21	6	08	07	00	05.3	01.7	•	•	⌴ 0-9^{45}, 18^{40}- 24; = 3^{30}- 24, ⊕ 9^{40}- 13^{40}
22	6	04	09	10	07.7	03.3	•	•	⌴ °0-10, = 0-15^{30} ⊕ 2^{40}- 4^{30}
23	7	04	10	10	08.0	02.7	•	•	⌴ 0 3^{30} 9^{30} = 4^{30}- 9^{45}, 20- 24; •° 19^{30}- 19^{45}, 23-24; F_N 23-23^{30}
24	5	10	06⊙	01	05.7	03.5	00.0	•	•° 0-3^{30}, $F_{WNW-NNE-NNW}$ 6-7i, 10^{45}- 16i
25	7	06	06	02	05.3	06.7	•	•	F_{N-NNE} 5-6^{20}, 12^{40}- 19^{45} i
26	7	06	08⊙	04	06.0	06.0	•	•	= 4^{40}- 11^{30}
27	6	10	10	10*	10.0	00.0	•	•	= 4^{30}- 24, *° 9^{30}- 11^{35} 15^{30}- 16^{45} i, 19^{45}- 23^{30} i
28	5	10	09	10	09.7	01.7	00.1	•	= 0-15^{40}, *° 7^{40}- 8^{30}
MES. VREDN.		08.2	07.6	05.2	07.0	34.3	41.7		

φ = 41° 57' N λ = 21° 38' E Gr. ΔG = + 1h 27 min. BR. ST. 265

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	739.8	740.1	740.2	-01.0	02.3	-00.8	-00.1	03.3	-01.1	-01.2	03.5	02.8	02.7	83	51	63	66	NNW 2	NNE 3	NNE 3
2	739.4	737.3	736.1	-02.4	02.8	-03.2	-01.5	03.6	-03.6	-03.0	02.8	02.4	02.8	72	42	77	64	NNW 3	W 1	SE 2
3	735.2	734.1	735.4	-05.2	07.6	02.8	02.0	09.0	-06.2	-09.8	02.8	03.9	03.7	91	50	66	69	ENE 1	SSW 2	SSE 2
4	735.4	732.1	726.1	02.4	06.8	03.8	04.2	09.6	01.8	00.1	04.4	05.8	05.6	81	79	94	85	- 0	SE 3	- 0
5	730.1	734.3	736.0	03.0	14.2	09.5	09.0	15.1	02.2	00.0	04.1	03.7	04.0	72	31	45	49	NE 2	SW 4	SE 4
6	737.5	736.5	738.6	06.6	15.6	10.4	10.8	16.6	06.0	03.4	04.2	04.9	05.7	58	37	60	52	SE 2	S 4	ENE 2
7	738.1	737.9	740.1	03.6	15.0	06.0	07.6	16.5	03.0	00.1	05.1	05.1	04.0	86	40	57	61	ESE 2	WNW 2	NNE 3
8	742.1	740.7	740.4	01.8	08.0	03.8	04.4	08.4	01.4	-02.0	03.9	04.1	04.4	75	51	73	66	NNE 2	NW 2	NNE 2
9	739.2	738.2	740.2	02.0	13.4	07.2	07.4	14.4	00.6	-01.0	04.6	05.3	05.3	87	46	69	67	WSW 1	SW 1	NNE 3
10	743.8	743.8	746.2	-00.4	13.6	06.0	06.3	14.2	-01.4	-04.2	04.2	05.0	04.6	94	43	65	67	ESE 1	N 3	NE 3
11	747.2	745.1	744.2	03.8	11.8	06.4	07.1	12.1	03.8	03.9	04.4	04.9	05.8	73	47	81	67	N 2	S 1	SE 4
12	741.4	739.2	740.2	05.0	07.6	03.2	04.8	08.0	03.2	04.5	05.7	06.1	05.0	87	78	88	84	SE 3	SE 4	SSE 2
13	742.7	742.2	742.3	02.1	14.0	05.5	06.8	14.2	00.1	-02.0	05.1	05.5	04.9	95	46	72	71	- 0	N 1	- 0
14	741.1	737.2	735.2	06.0	08.4	06.0	06.6	09.0	05.2	02.0	06.0	06.6	06.6	86	80	94	87	SSE 1	SSE 4	WSW 1
15	733.5	732.4	733.4	06.0	12.6	09.6	09.4	15.6	05.8	05.6	06.8	09.0	07.0	97	83	78	86	NNE 1	S 1	NNE 3
16	735.9	735.8	736.4	03.7	09.2	05.0	05.7	11.4	02.4	00.2	05.7	05.4	04.3	95	62	66	74	- 0	N 6	N 6
17	733.5	735.7	738.7	04.4	05.6	03.7	04.4	06.9	02.7	02.0	04.3	04.3	03.8	68	63	63	65	NW 5	NNW 4	NW 4
18	739.4	737.6	736.2	02.8	08.4	04.0	04.8	10.2	02.0	01.0	03.8	03.4	03.9	67	41	65	58	- 0	W 2	ESE 2
19	735.0	731.5	731.0	00.9	10.3	07.2	06.4	11.9	-01.4	-04.1	04.5	04.9	06.8	91	52	89	77	- 0	W 1	SE 2
20	733.6	736.9	740.4	04.0	06.0	05.4	05.2	07.5	03.8	03.5	05.4	04.6	03.6	88	65	53	69	S 1	NNW 3	NNW 4
21	743.3	743.6	745.0	02.2	10.2	06.0	06.1	11.5	01.1	-01.6	03.0	03.6	03.8	56	38	55	50	WNW 2	NNW 4	WSW 2
22	746.0	744.5	745.0	-00.8	15.4	06.4	06.8	17.2	-02.8	-05.4	03.8	03.7	04.9	89	28	68	62	- 0	NE 2	- 0
23	746.8	745.5	745.3	02.8	17.2	12.8	11.4	18.8	00.6	-01.6	05.1	05.4	06.0	90	37	54	60	- 0	- 0	SE 3
24	745.9	743.6	743.8	05.9	19.4	13.2	12.9	21.4	04.9	03.5	06.1	06.8	07.6	87	40	67	65	- 0	E 1	SE 1
25	746.1	744.3	743.9	04.3	21.8	17.0	15.0	23.6	02.9	00.0	05.9	05.6	06.5	94	29	45	56	NE 1	E 1	ESE 1
26	744.0	742.0	740.9	07.6	17.0	14.0	13.2	19.4	05.7	04.2	06.8	07.3	07.0	87	50	58	65	- 0	WNW 1	ESE 1
27	738.8	734.4	732.4	07.0	24.0	16.4	16.0	24.4	05.8	03.8	06.7	06.5	07.6	89	29	54	57	NNW 1	SE 5	S 3
28	730.9	728.1	729.3	13.6	17.8	06.0	10.8	20.6	06.0	09.8	09.2	11.7	06.0	79	76	86	80	N 1	S 4	NNE 6
29	734.1	733.9	737.6	04.0	10.4	05.6	06.4	10.4	03.8	04.0	04.6	05.6	04.8	76	59	70	68	NNE 5	NNE 4	N 3
30	743.4	744.1	744.6	02.8	12.3	03.5	05.5	12.7	00.1	-01.5	04.2	02.7	03.7	75	25	62	54	NNE 1	SW 3	SE 1
31	744.8	741.6	740.2	00.0	14.6	10.9	09.1	16.0	-03.4	-06.0	03.8	03.5	04.8	83	28	49	53	- 0	SSE 2	SE 2
MES. VRED.	739.6	738.5	738.9	03.2	12.0	06.9	07.2	13.3	01.8	00.3	04.6	05.2	05.1	82	49	67	66	1.3	2.5	2.4

1	739.0	736.9	736.4	04.2	14.0	12.6	10.8	15.0	03.0	01.2	05.4	06.5	07.0	87	55	64	69	N 1	W 2	SE 3
2	735.8	734.4	733.4	09.0	17.0	12.2	12.6	17.9	08.3	07.5	08.1	07.8	08.1	94	54	76	75	- 0	SE 4	SE 3
3	729.8	728.2	732.8	11.8	17.6	08.2	11.4	18.7	07.0	08.6	08.3	05.2	03.1	80	34	38	51	SSE 2	W 5	W 4
4	735.8	737.5	739.5	03.4	06.9	02.8	04.0	09.1	01.9	-00.5	03.6	04.5	03.7	61	60	66	62	N 5	W 2	- 0
5	740.6	737.7	737.3	-00.8	12.0	06.8	06.2	13.1	-03.7	-05.4	03.8	03.6	03.5	88	34	47	56	ESE 2	N 2	E 3
6	737.4	737.7	741.1	06.2	14.5	06.2	08.3	15.0	05.1	03.5	05.6	02.8	03.0	78	22	42	47	- 0	WNW 5	N 2
7	743.4	740.7	740.1	-00.2	15.2	12.5	10.0	16.1	-03.1	-05.9	03.9	03.3	04.1	85	26	37	49	- 0	SSE 2	SE 4
8	738.9	736.5	736.1	08.8	15.9	12.2	12.3	16.6	07.1	06.4	06.8	07.6	08.3	80	56	78	71	NW 1	SE 4	SSE 2
9	731.3	731.0	735.0	09.6	21.8	16.6	16.2	23.0	09.2	06.6	07.9	09.1	05.0	88	47	35	57	- 0	NW 3	W 4
10	739.2	737.8	739.1	10.4	21.3	13.1	14.5	22.4	05.4	02.4	06.2	05.2	05.4	66	27	48	47	- 0	SSE 2	SE 1
11	739.2	738.0	738.6	09.0	18.2	12.3	13.0	19.4	06.0	04.0	05.9	07.3	09.9	69	47	92	69	- 0	SE 5	SE 2
12	734.7	732.8	736.3	10.9	13.1	05.5	08.8	15.1	05.2	09.0	09.4	07.8	05.7	96	69	84	83	NNW 1	NNW 4	SW 4
13	739.9	740.3	741.3	08.0	16.4	10.2	11.2	17.6	05.5	03.5	05.8	04.9	05.4	72	35	58	55	W 1	NE 2	ENE 1
14	740.1	737.2	736.7	08.5	15.8	12.4	12.3	18.4	06.4	04.7	06.3	07.9	08.2	75	59	76	70	WNW 1	WNW 2	ESE 2
15	738.8	742.4	745.4	08.0	07.2	06.0	06.8	12.6	06.0	05.0	06.6	04.0	03.8	82	52	55	63	SW 1	N 6	N 5
16	745.2	745.1	746.5	05.4	07.6	06.6	06.6	08.1	05.4	04.9	03.8	04.2	04.6	56	54	63	58	N 4	NNW 4	W 2
17	747.2	745.6	745.9	07.1	14.1	08.6	09.6	15.2	05.4	04.0	04.7	06.3	05.9	63	52	71	62	- 0	NW 2	NNE 3
18	743.8	741.3	741.0	04.2	16.8	13.0	11.8	19.0	00.4	-01.0	05.6	07.2	07.7	91	50	69	70	- 0	SW 2	N 2
19	741.3	740.6	740.9	12.6	21.8	11.0	14.1	22.4	10.2	08.0	08.6	09.4	08.0	78	48	82	69	NNE 3	WSW 1	- 0
20	743.3	741.4	743.4	12.8	22.8	15.6	16.7	23.4	09.0	06.9	08.6	08.9	07.9	78	43	59	60	SSE 2	SSE 4	ESE 2
21	746.4	744.6	746.1	10.1	23.6	18.6	17.7	26.0	05.3	04.0	07.6	09.3	08.2	82	43	51	59	- 0	- 0	ESE 3
22	751.2	748.4	748.3	10.8	23.1	15.0	16.0	23.7	06.6	05.5	08.1	08.5	08.8	84	40	69	64	- 0	- 0	- 0
23	748.2	744.9	743.8	10.1	26.3	16.0	17.1	28.0	06.1	04.4	08.3	07.8	08.4	89	30	62	60	SSE 1	NE 1	ENE 1
24	744.8	741.5	741.0	11.1	27.7	14.8	17.1	28.6	05.4	04.0	08.0	05.1	07.7	81	18	61	53	- 0	ENE 1	ESE 1
25	741.7	738.3	738.7	12.5	27.6	18.0	19.0	28.4	07.8	06.0	08.1	08.4	09.0	74	30	58	54	- 0	NNE 2	SSE 2
26	739.6	736.5	736.9	13.6	25.9	15.2	17.5	27.9	07.2	05.9	09.0	07.9	06.8	77	31	53	54	E 2	- 0	ENE 1
27	737.7	736.0	738.5	12.6	29.2	15.4	18.2	29.2	08.2	05.4	07.2	06.0	05.6	66	20	43	43	SSW 1	W 3	- 0
28	741.2	739.9	737.7	12.8	23.9	13.8	16.1	24.4	08.0	05.9	06.7	10.7	09.4	61	48	79	63	- 0	- 0	E 2
29	737.2	736.1	737.2	15.7	23.8	16.2	18.0	24.0	11.3	08.9	08.7	09.3	06.1	65	42	44	50	N 3	NE 3	NE 4
30	738.6	737.7	739.4	11.3	10.2	07.8	09.3	16.3	07.8	09.5	07.5	07.6	06.8	74	81	86	80	N 2	ENE 2	NNE 3
MES. VRED.	740.4	738.9	739.8	09.0	18.4	11.8	12.8	19.8	05.8	04.4	06.8	06.8	06.5	77	44	62	61	1.1	2.5	2.2

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BR. ST. 265 H_s = 232 m H_b = 233.3 m h_t = 2.0 m h_r = 1.3 m

Dan	Vidljivost 0–9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred Dies		7	7	
1	6	10	09	10	09.7	00.5	00.0	•	*°5-8^30 i, = 5^30-18
2	6	10	04⊙	00	04.7	07.0	00.0	•	= 7^45-20, ⌴°20^30-24
3	7	05	02⊙	00	02.3	04.5	•	•	⌴°0-9, = 4^30-13^45 F SSE-SE 14-18^25, 22^40-24 i
4	7	10	10●	10●	10.0	00.0	•	•	F SE 0-3^30 i, 10-12^40, ●¹14^50 23^40 i
5	8	03⊙	02⊙	01	02.0	09.9	10.4	•	≺ E-S-W-NW 0^40-4^40, 19^45-24, F S 8-24 i
6	8	02⊙	08	03	04.3	07.0	•	•	≺ W-NW 0-2, F SE-S-SSE 0-5^10, 8^25-8^35, 16^50-18^30 i
7	8	04	07⊙	00	03.7	04.8	•	•	
8	7	07	10	06	07.7	00.0	•	•	F NNE 0-4^10 ⊕ 12^40-14^30
9	7	10	06⊙	00	05.3	06.9	•	•	= 4^30-9^20
10	7	04	08⊙	00	04.0	09.0	•	•	⌴°2-8, = 6^25-10^30, F N 14^20-19^30
11	7	10	05⊙	10	05.3	03.1	•	•	F SSE 17^25-20^30 ● 21^05-22^05
12	7	10	10	01	07.0	00.0	00.6	•	F SE-SSE 4^55-5^40, 10^30-13^55 i
13	7	09	05⊙	09	07.7	00.3	00.1	•	⌴°0^20-3^30
14	7	10	10●	10●	10.0	00.0	•	•	●0-1 7^02-24, F SSE 10^35-16^30 i
15	7	10●	08⊙	06	08.0	02.9	04.9	•	●0-1 0-0^20, 2^05, 13^05-13^20, = 6^05-11^30, T¹13^37-14^40
16	8	05	10	10	09.3	02.9	00.5	•	F N-NNE 8^50-24
17	7	10	10	10	10.0	00.0	00.2	•	F NNW-N-NW 0-1^20, 6^20-21^35 i
18	7	09	02⊙	01	04.0	08.0	00.0	•	⌴°22^30-24
19	7	10	10	10	10.0	02.2	•	•	⌴ 0-6^20 ⊕ 0^30-14^40 F SE 16^30-17^30 ●¹17-20^30
20	8	10●	10●	10	10.0	00.0	07.4	•	●¹3^45-11^45 i, 13^35-13^50, F-F N-W 8^50-19^02, 13^05-15 i
21	8	02⊙	02⊙	00	01.3	10.6	00.1	•	F NNW 0-5, 8^36-16^36
22	8	00⊙	02⊙	08	03.3	09.1	•	•	⌴¹0-8
23	7	10	07⊙	09	08.7	04.4	•	•	⌴°2^30-7^40 ⊕ 7^20-8^40
24	8	10	03⊙	00	04.3	09.9	•	•	⌓¹0-7^20, 21^30-24
25	8	06⊙	04⊙	02	04.0	09.9	•	•	⌓° 0-8^30
26	7	10	10	05	08.3	00.2	•	•	⌓° 1^40-7^45
27	7	06	03	03	04.0	05.4	•	•	⌓° 0-9, = 7^30-9^20 F SSE 12^25-24
28	7	00	09	03●	04.0	02.8	00.3	•	F SSE-SE-NE 0-1^40 11^30-15^30 i, 17^40-24; ●°3^50-5^20, 7^30-13^40 i, 17^40-18
29	7	09	09	10●	09.3	01.7	01.9	•	F NNE-NE 0-7^30 11^00-24 i
30	8	01⊙	02⊙	00	01.0	11.0	00.6	•	F N 0-0^55, ⌴°21^30-24
31	8	04⊙	09⊙	03	05.3	07.0	•	•	⌴°0-9
MES. VRED.		07.0	06.6	04.8	06.1	151.9	26.5		

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1	7	10	09	05	08.0	01.2	•	•	F SE 16^45-20^40
2	8	10●	06	08●	08.0	05.1	00.5	•	●°5-9^30 i, 20^05-20^45, F SE 9^30-11^00 i, 13^30-17^40 i
3	8	09	09	00	06.0	04.4	00.0	•	●°9^25-9^30 i, F-F W 13^40-19^40
4	7	09	08⊙	00	05.7	03.5	00.0	•	F N 0-9^30 i, ●° 9^30-11 i
5	8	05⊙	04⊙	05	04.7	10.2	00.0	•	⌴¹0-8^30
6	8	09	06⊙	00	05.0	05.5	•	•	F SW-WNW 0^03-1^37, 13^50-16^40, ●°8^30-8^40
7	8	09⊙	05⊙	10	06.0	07.6	00.0	•	⌴¹3^30-7^40 ● 11^45-12^25 ●¹20^40-24
8	7	10	10	10●	10.0	00.5	01.0	•	●°0-2^30 13^45-20^40 i, F SE 15^45-18^15 22^03-24
9	7	04	08	01	04.3	06.4	00.3	•	F SE-W/SW 0-1^40 7^45-12 i, 15^30-21^50 i
10	8	00⊙	04⊙	04	02.7	•	•	•	
11	8	09	10	10●	09.7	02.4	•	•	F SE 12^40-13^40 i, ●° 16^34-22^05
12	7	10	08	10●	09.3	•	05.5	•	●0-1 1^50-4^05 i, 17^45-21^20, F N 10^20-16^56 i
13	8	00⊙	03⊙	04	02.3	10.3	06.0	•	
14	8	09	10	09●	09.3	01.0	•	•	●°11^55-21^30 i
15	7	10	10	10	10.0	00.0	00.4	•	F-F N 8^40-24 i
16	7	10	10	10	10.0	00.0	•	•	F N 0-22^25 i
17	7	09	08	01	06.0	06.7	•	•	F N 12^30-19^35 i
18	7	10	09	09	09.3	03.3	•	•	⌴°2^30-7^20 ●° 8^45-9^10 F NW 11^40-17^40
19	7	09	08	01	06.0	06.5	00.0	•	●0-1 0^45-4^40 i, 13^40-13^45, F NNE 3^33-4^45
20	8	06⊙	02⊙	00	02.7	10.3	•	•	F SE 16^05-19^32 i
21	7	03	08	00	03.7	11.2	•	•	⌴°3^30-8
22	7	08	10	06	09.3	01.9	•	•	⌴¹2^30-8^40 20^45-24
23	8	04⊙	02⊙	00	02.0	11.9	•	•	⌴° 0-8^36 21^20-24
24	8	02⊙	02⊙	00	01.3	12.6	•	•	⌴¹0-6^50, ⌴¹2^30-7^30, ●°17^50-19^05 i, T S 18-19^45 i, T 18^40-18^25, G E 19^45-21^05
25	8	02⊙	02⊙	04	03.7	11.1	•	•	
26	8	04⊙	04⊙	03	03.7	11.0	•	•	⌴¹0-8
27	8	06⊙	04⊙	00	03.3	10.8	•	•	⌴¹2^30-7, 19^40-24; ●° 10^55-12 i, 16^03-16^45, F NNW 11^45-11^40
28	8	04	08	02	04.7	04.7	•	•	⌴° 0-6^45 F NNE-NE 7^03-8^40 13^03-19^40 i
29	8	09	04	10	09.3	00.1	00.2	•	F NNE 0-2^45 i, ●0-1 2^45-19^45 i
30	7	10●	10●	0[illegible]	07.7	00.0	00.1	•	
MES. VRED.		07.0	06.9	04.5	06.1	162.9	16.2		

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φ = 41° 57' N λ = 21° 38' E Gr. ΔG = + 1h 27 min. BR. ST. 265

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	741.4	741.1	742.7	07.0	11.4	06.8	08.0	12.9	06.8	06.6	05.2	04.9	05.1	69	49	68	62	NW 1	NNW 3	NNE 1
2	743.5	740.2	741.8	04.2	14.1	07.0	08.1	14.7	-01.0	-02.8	04.7	04.2	05.9	76	35	79	63	- 0	N 2	NNE 4
3	741.1	740.4	741.3	05.6	07.2	08.6	07.5	09.6	05.1	04.6	05.6	06.2	05.7	82	82	68	77	W 2	W 4	NW 2
4	740.4	736.9	736.2	09.6	14.6	10.4	11.2	14.9	05.1	04.9	05.6	06.4	06.6	63	51	70	61	S 1	NW 3	N 3
5	734.8	735.7	738.3	07.6	11.0	09.2	09.2	11.8	07.0	06.8	07.1	07.4	07.9	91	75	90	85	ENE 1	NE 2	NNE 2
6	740.6	740.9	741.6	07.9	16.7	11.2	11.8	18.2	05.1	04.1	07.7	07.0	08.2	96	49	82	76	- 0	SE 2	- 0
7	741.8	741.2	742.0	08.8	20.0	16.3	15.4	21.4	06.4	05.1	08.1	08.5	10.3	95	48	74	72	- 0	ESE 1	SSW 2
8	742.8	741.5	742.5	12.6	22.4	14.2	15.8	23.4	08.6	07.5	09.7	09.1	11.1	89	45	92	75	SSE 1	SSE 2	ESE 1
9	744.0	742.1	741.6	13.4	25.0	18.0	18.6	26.0	10.4	09.0	10.3	10.8	10.0	89	46	65	67	- 0	SE 3	NE 1
10	741.6	738.2	738.0	15.0	26.9	20.0	20.5	27.0	10.5	09.8	10.2	11.5	08.5	80	43	48	57	- 0	SE 3	SSE 2
11	737.8	734.7	734.4	15.6	27.8	18.6	20.2	28.4	09.8	08.5	10.7	09.9	11.0	80	35	68	61	ENE 1	ESE 5	NNE 2
12	734.4	734.3	737.3	16.4	26.2	16.8	19.0	26.2	11.2	09.4	10.9	06.1	05.6	78	24	39	47	WNW 2	W 5	W 4
13	739.6	738.0	739.1	12.1	23.1	15.4	16.5	23.8	05.3	03.8	06.8	05.2	05.6	65	25	43	44	- 0	WNW 4	WNW 2
14	741.3	740.5	741.0	13.0	21.4	12.8	15.0	23.6	07.8	05.4	07.0	08.0	08.0	63	42	72	59	- 0	NNE 4	E 2
15	741.7	738.9	738.2	12.4	25.4	16.2	17.6	26.9	05.4	03.8	08.2	07.1	08.4	76	29	61	55	- 0	SE 3	- 0
16	738.0	736.1	735.5	16.0	25.6	18.0	19.4	27.3	10.1	07.6	08.8	08.8	10.4	64	36	67	56	ENE 2	S 3	- 0
17	735.6	734.1	734.8	15.2	21.3	16.6	17.4	22.0	14.2	12.0	11.0	08.6	08.7	85	45	61	64	W 1	NNW 2	NNE 5
18	735.2	735.8	739.7	13.8	20.0	15.4	16.2	20.7	10.0	07.4	10.5	09.1	08.3	88	52	64	68	- 0	N 4	WNW 3
19	741.4	742.2	743.0	15.4	18.0	13.8	15.2	18.1	13.4	13.8	07.9	08.5	09.0	60	55	76	64	- 0	N 4	N 2
20	742.0	739.1	738.5	14.4	22.0	15.3	16.8	22.6	10.6	09.3	09.3	09.0	10.1	76	46	77	66	ENE 1	SSE 2	NNE 2
21	735.6	733.4	733.7	12.6	14.6	14.0	13.8	17.4	12.4	12.6	10.2	10.9	10.0	93	88	83	88	WNW 2	WSW 2	- 0
22	735.0	735.0	734.7	14.6	20.2	15.2	16.3	21.8	12.1	11.0	10.7	09.9	10.9	86	56	84	75	SE 1	SE 3	E 3
23	735.8	738.6	743.3	12.6	12.9	11.4	12.0	17.1	10.9	10.3	08.5	06.3	05.5	77	57	55	63	- 0	NNE 4	NW 3
24	745.2	744.6	745.3	12.1	14.6	10.0	11.7	15.6	06.7	04.0	05.1	05.0	06.0	48	40	65	51	WNW 4	NW 5	WNW 4
25	745.8	744.8	745.3	12.5	17.6	11.4	13.2	19.4	09.2	09.4	06.4	05.9	05.8	59	39	58	52	WNW 1	NNW 3	NE 2
26	745.5	742.6	742.3	10.6	20.7	12.0	13.8	21.8	02.9	01.1	06.3	06.4	06.9	66	35	66	56	NW 1	NNW 1	- 0
27	743.2	740.5	740.7	11.6	22.0	13.8	15.3	23.0	05.8	03.6	07.6	07.2	08.2	75	36	69	60	- 0	S 3	S 2
28	741.1	739.9	740.8	14.0	17.8	13.3	14.6	20.8	09.9	09.0	08.8	08.3	10.4	73	55	90	73	- 0	SE 3	S 1
29	740.8	741.6	742.2	12.2	17.7	12.4	13.7	18.7	11.7	11.4	09.9	08.4	08.9	93	55	83	77	- 0	N 3	S 1
30	743.0	741.3	740.5	12.1	21.4	15.9	16.3	22.6	05.6	04.2	09.0	09.9	09.8	85	52	72	70	- 0	SSE 2	- 0
31	741.4	739.0	741.5	15.0	23.8	15.2	17.3	24.6	11.2	09.8	09.7	08.1	10.1	76	37	78	64	- 0	NE 1	SW 2
MES. VRED.	740.4	739.1	739.9	12.1	19.5	13.7	14.8	20.7	08.4	07.2	08.3	07.8	08.3	77	47	70	65	0.7	2.9	1.9

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1	742.3	742.6	743.3	13.4	16.6	12.2	13.6	17.8	11.8	13.0	10.1	08.5	08.3	87	60	78	75	WSW 2	NNW 3	NNE 2
2	742.7	742.4	742.6	15.0	18.0	15.6	16.0	19.2	07.4	05.2	08.1	07.8	07.1	63	50	53	55	SW 1	NNW 4	N 3
3	743.1	742.6	742.6	13.6	13.0	11.2	12.2	15.9	11.2	11.0	06.1	07.4	07.9	52	66	80	66	N 3	NNW 2	NNE 3
4	741.4	740.9	742.6	11.5	18.4	12.8	13.9	19.4	08.7	07.5	07.7	07.4	07.9	76	47	71	65	S 1	NE 2	NNE 3
5	744.1	742.6	742.6	10.7	22.1	13.0	14.7	23.8	04.6	03.3	07.8	06.2	08.4	80	31	75	62	SE 1	ESE 1	NNE 2
6	743.4	742.5	742.8	13.0	21.2	12.8	15.0	21.6	05.4	03.6	07.0	07.1	09.4	63	38	85	62	- 0	- 0	- 0
7	743.8	742.3	741.4	13.4	26.2	18.8	19.3	28.4	06.6	05.0	09.6	09.9	11.2	83	39	69	64	- 0	ENE 2	ESE 2
8	742.5	741.5	742.1	17.8	25.3	20.0	20.8	26.4	11.6	09.8	10.9	12.4	12.9	71	51	74	65	- 0	ESE 2	E 1
9	743.1	742.6	742.5	18.6	28.2	20.8	22.1	28.4	11.9	10.2	12.9	11.6	14.7	80	40	80	67	ENE 1	WSW 2	E 1
10	743.2	740.4	738.7	18.6	30.1	24.2	24.3	31.4	13.6	12.1	13.5	13.1	11.2	84	41	50	58	NNE 1	SE 4	SSE 3
11	738.6	736.3	737.0	20.8	30.4	24.2	24.9	31.2	14.4	11.8	11.8	09.3	12.4	64	28	55	49	- 0	S 3	NW 3
12	738.1	736.5	737.6	21.6	26.4	20.7	22.4	27.5	17.7	15.9	12.8	11.0	10.7	66	43	59	56	- 0	N 5	NNE 2
13	738.9	737.6	737.8	17.2	27.1	18.2	20.2	28.0	12.0	10.0	10.9	10.1	09.9	74	37	63	58	- 0	ENE 1	SSE 1
14	739.6	738.1	738.3	16.6	29.8	23.0	23.1	30.3	10.3	08.5	10.9	09.4	11.7	77	30	55	54	E 1	W 2	NNE 5
15	740.7	739.7	741.8	17.8	28.4	18.4	20.8	29.4	12.3	10.4	10.7	10.3	11.4	70	35	72	59	NE 1	NNE 2	- 0
16	743.3	741.8	742.2	19.0	29.0	24.0	24.0	29.9	12.6	10.6	11.9	11.2	10.2	72	37	46	52	- 0	N 3	- 0
17	742.9	740.7	739.5	19.2	30.7	25.7	25.3	32.2	13.2	13.2	12.0	10.9	13.8	72	33	55	53	- 0	ESE 2	S 3
18	740.7	737.6	736.8	20.6	32.6	25.7	26.2	34.0	14.6	13.0	13.3	12.7	13.1	73	34	53	53	- 0	SSE 2	ESE 1
19	737.1	736.7	737.3	21.2	24.7	20.2	21.6	26.7	15.7	14.0	13.9	13.0	11.8	74	56	67	66	- 0	NE 2	NNE 5
20	738.2	738.2	740.3	17.1	19.9	17.2	17.8	23.4	14.4	12.4	11.5	12.2	13.9	78	70	94	81	SSE 1	NNE 4	- 0
21	742.5	742.1	743.1	17.4	25.4	22.2	21.8	26.4	13.6	11.4	12.4	10.1	11.4	83	41	57	60	- 0	W 3	W 1
22	744.7	742.9	743.5	20.0	28.4	20.2	22.2	30.0	12.2	10.8	11.4	10.0	11.5	65	34	65	55	- 0	SSW 2	NNE 2
23	743.7	742.0	742.2	20.6	30.6	22.8	24.2	30.8	15.3	13.0	12.2	11.9	11.6	67	36	56	53	- 0	W 2	- 0
24	743.6	742.5	743.8	21.0	30.1	18.2	21.9	31.8	15.2	13.4	13.4	10.6	10.4	72	33	66	57	- 0	NW 3	E 1
25	744.5	742.5	743.3	17.0	27.2	24.0	23.0	30.2	11.4	08.6	11.5	09.4	12.3	79	35	55	56	NE 1	NNW 5	NNE 4
26	744.6	742.5	743.0	20.9	28.8	23.4	24.1	29.6	15.3	12.6	11.5	10.7	12.2	62	36	56	51	N 2	NNE 4	NNE 4
27	743.9	742.6	743.4	19.4	28.4	23.0	23.4	28.6	15.0	12.8	13.3	11.5	12.4	79	40	59	59	- 0	N 4	N 4
28	744.3	742.2	741.8	18.6	29.4	23.8	23.9	30.7	12.5	10.2	12.3	09.6	10.3	77	31	47	52	NNW 1	NW 2	NNE 2
29	742.1	739.1	740.3	19.4	31.2	23.4	24.4	32.8	14.3	-	12.2	09.9	10.2	72	29	47	49	- 0	NW 2	NW 3
30	740.6	737.8	737.7	20.6	31.7	22.0	24.1	32.4	14.3	11.6	11.9	10.4	12.3	65	30	62	52	- 0	SE 1	S 2
MES. VRED.	742.1	740.7	741.1	17.7	26.3	20.0	21.0	27.6	12.3	10.5	11.2	10.2	11.1	73	40	63	59	0.6	2.5	2.1

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BR. ST. 265 H_s = 232 m H_b = 233.3 m h_t = 2.0 m h_r = 1.3 m

Dan	Vidljivost 0-9	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednja Dnevna		7	7	
1	8	10	07	02	06.3	01.5	10.0	.	F_{NNW-N} 10^{00} 14^{35} 14^{00} 19i; △°22^{50}-24
2	8	02⊙	10	10	07.3	06.7	.	.	△¹0-3^{45}, ⌣°3^{45}-6^{40}, •°16^{45}-19^{20}i, 21^{55}-24i
3	7	10•	10•	06	08.7	00.0	01.7	.	•$^{0-1}$0-16i
4	7	06	08	10	08.0	01.1	03.1	.	F_{WNW} 11^{00}-21^{00}i, •°21^{50}-24i
5	7	10•	10•	10•	10.0	00.0	02.0	.	•°0-21^{35}i
6	7	10	09	09	09.3	05.0	01.3	.	
7	7	10	09⊙	08	09.0	03.5	.	.	△°1-8^{30}
8	7	04⊙	10	06	06.7	03.6	.	.	△°3-8, •°16^{00}-17^{10}, ℞ 17^{05}, ∩E 17^{00}-17^{35}, ↳SE 19^{30}-21^{05}
9	7	08	09⊙	09	08.7	09.1	01.0	.	△$^{1-2}$0-8^{30}
10	7	06	03⊙	02	03.7	11.5	.	.	△°0^{30}-7^{30}, F_{SE} 15^{00}-19^{05}
11	7	00⊙	00⊙	01	00.3	10.9	.	.	△¹$2^{30}$-7^{30} 23^{40}-24; F_{SE-SSE} 12^{45}-16^{30}i
12	8	09	01⊙	01	03.7	11.0	.	.	△°0-6^{30}, F_{WSW} 10^{00}-18
13	8	02⊙	04⊙	02	02.7	10.7	.	.	F_{WNW} 11^{30}-17^{40}i
14	9	07	07	01	05.0	08.6	.	.	△°21-24
15	8	00⊙	01⊙	01	00.7	11.7	.	.	△¹0-7
16	8	06	07⊙	10	07.7	06.4	.	.	•°14^{05}-14^{40}
17	8	09	09	09•℞	09.0	02.1	00.0	.	•°5^{00}-5^{15} 7^{40}-8^{05}i, 11^{35}-11^{45} 20^{30}-22^{30}i; F_{W-NNE} 14^{30}-14^{53}, 20^{00}-20^{04}, T19^{55}-21^{05}i, ℞20^{00}-21^{05}, ↳S 0-1^{30}, •°8^{30}-10^{30} 16^{20}-17, F_N 12-15^{35}i [∇°20^{00}-21^{05}, ↳21^{15}-24
18	8	08	06⊙	09	07.7	02.7	03.2	.	
19	9	09	09	09	09.0	00.6	00.6	.	$F_{WNW-NNE-N}$ 4^{50}-4^{55} 9-18^{30}
20	8	07	09	10	08.7	06.1	.	.	TE 17^{35}-19^{30}, F_{SSE} 17^{30}-18^{30}, •$^{0-1}$$18^{45}$-24i, ↳NE 19^{30}-20^{30}
21	7	10•	10•	10	10.0	00.2	10.0	.	•$^{0-1-2}$0-8^{30}i, 12^{00}-15^{00}i, 18^{00}-19^{20}i, 21^{30}-22^{20}i
22	8	02⊙	09	02	04.3	07.1	10.1	.	•°0^{20}-1^{20} T$_{SE-NW}$ 10^{50}-12^{20} ∇^{2} 14^{25}-14^{33} △$^{1-2}$ 19^{00}-24
23	8	08	10	06	09.0	01.1	01.0	.	△0-3^{25}, •^{1}3^{25}-5^{00}i, 14^{20}-12^{25} 14^{30}-15^{00}, F-$F_{W-WNW-N}$ 4^{40}-5^{20} 14^{00}-18^{20}i
24	8	04⊙	06⊙	10•	06.7	06.1	00.7	.	F-F-F^{1}6^{35}-24, •°^{1}20-21
25	8	09	09	00	06.0	05.3	00.0	.	F-$F_{NNW-NE-N}$ 8^{00}-10^{30}, 12^{35}-13^{35}i, 16^{00}-18^{30}
26	8	02⊙	01⊙	00	01.0	13.2	.	.	△°0-8
27	8	02⊙	05	04	03.7	09.7	.	.	△¹0-8, F_W 17^{30}-18^{20}, ↳NE 19-19^{30}
28	8	10	09	10	09.7	00.4	.	.	T_{SW-NE} 11^{50}-16^{10}i, F_{SSE} 12^{00}-14i, •$^{0-1}$$14^{55}$-$15^{30}$, 17^{00}-17^{35}, 21-21^{45}, 23^{35}-24
29	7	10	09	00	06.3	04.3	06.4	.	•$^{0-1}$0-3^{15}-13^{35}, △°20^{00}-24
30	7	02⊙	09⊙	09	06.7	06.9	00.0	.	△$^{1-2}$0-9
31	8	09⊙	06	10	08.3	06.2	.	.	△°0-8^{30}, F_N 14^{25}-16^{00}
MES. VRED.		06.5	07.1	06.0	06.5	173.3	57.9		

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1	7	10•	10	02	07.3	00.3	00.0	.	•°3^{45}-8^{20}i, △¹$21^{50}$-24
2	8	03⊙	09	09	07.0	05.9	00.2	.	△¹0-8, F_{WNW} 7^{00}-14^{30}i
3	7	10	10•	10	10.0	00.0	.	.	F_N 3^{30}-4i, •°9^{00}-14^{30}i
4	7	03⊙	05⊙	01	03.0	09.5	01.3	.	•°17^{45}-17^{52}
5	8	02⊙	04	02	02.7	12.7	00.0	.	△°0-8^{40}
6	8	03	10	00	04.3	03.3	.	.	△²0-8^{20} 21-24; •°12^{55}-15^{55}i
7	8	00⊙	01⊙	00	00.3	10.9	00.1	.	△²0-8 21-24
8	8	04⊙	10	05	06.3	04.1	.	.	△¹0-8 22^{30}-24; ∇°8^{40}-8^{45}
9	8	05⊙	09℞	05	06.3	05.9	00.0	.	△°0-8^{40} ℞$_{SW}$ 13^{30}-14^{05}, •°13^{50}-13^{59}
10	8	04⊙	06	00	03.3	07.1	00.0	.	△°0-7, F_{SE-SSE} 12^{30}-22^{30}i
11	8	00⊙	02⊙	06	02.7	11.8	.	.	↳E 22^{20}-23^{30} F_N 18^{05}-19^{55}
12	8	03⊙	07⊙	05	05.3	06.9	.	.	↳S 1^{40}-3^{40}, F_N 8^{30}-17^{50}i
13	7	00⊙	05⊙	01	02.0	10.5	.	.	
14	8	00⊙	04⊙	07	03.7	11.1	.	.	△°0-7^{30} F_{NNE} 20^{00}-23^{30}i
15	8	00⊙	08	03	04.7	09.1	.	.	△²0-8, F_N 15^{50}-16^{55}, •°17-17^{40}
16	7	00⊙	03⊙	06	03.0	03.6	00.0	.	△¹0-8
17	8	00⊙	01⊙	04	01.7	12.3	.	.	△¹$2^{30}$-8
18	8	05⊙	02⊙	02	03.0	11.4	.	.	△²2-7^{30} ∇^{1}14^{45}-15, ℞ 14^{30}-14^{55}
19	8	04	05℞⊙	03	04.0	03.9	00.3	.	△°2-7^{45}, $F_{WNW-NNE}$ 8^{30}-9, 20^{00}-21^{00}, •^{2}10^{50}-13^{00}i, ℞ 10^{00}-13^{30}i, ∩ 16^{00}-17^{25}
20	8	08	10	10	09.3	01.3	03.0	.	△² 0-8^{30}, F_{NNE} 10^{40}-13^{50}i, •°14^{35}-19^{20}i
21	8	01⊙	08	09	06.0	00.6	00.3	.	•^{2}13^{45}-14^{40}i, F_N 14^{05}-14^{08}
22	8	01⊙	04⊙	02	02.3	13.6	00.1	.	△¹$2^{30}$-7^{30}, F_{NNW} 15^{05}-17^{55}, ↳E 20-24
23	8	03⊙	04⊙	02	03.0	11.6	.	.	↳E 0-2
24	7	01⊙	09℞	01	03.7	07.3	.	.	△$^{0-1}$2-6, 21^{30}-24; T 12^{00}-14^{40}i, 17^{55}-18^{40}, ℞ 13^{35}-13^{50}, •^{1}13^{00}-14i, F_{E-N} 14^{05}-14^{35} 16^{00}-17^{40}
25	8	02⊙	06℞	02	03.3	09.8	00.0	.	△¹0-6^{30}, T_{NW} 12^{00}-14^{05}, F_{NNE} 13^{00}-13^{50}i, •°13^{45}-14^{00} [∩$_{SE}$ 18^{00}-18^{30}, ↳N 20-24
26	8	05⊙	06⊙	08	06.3	03.9	00.0	.	
27	7	04⊙	06⊙	01	03.7	07.0	.	.	△°1^{30}-7^{30} F_N 13^{30}-18^{45}i
28	8	00⊙	04⊙	00	01.3	11.9	.	.	△¹2-7
29	7	01⊙	03⊙	09	04.3	11.2	.	.	F_{N-W-NW} 17^{00}-20^{00}, T_S 19^{30}-19^{50}, ↳¹$19^{00}$-23^{30}
30	8	00	03⊙	04	02.3	10.1	.	.	△°0-6^{00}, T_S 12^{45}-16^{30}i
MES. VRED.		02.7	05.8	04.0	04.2	232.5	06.3		

φ = 41° 57' N λ = 21° 38' E Gr. ΔG = + 1h 27 min. BR. ST. 265

Dan	Vazdušni pritisak P mm 7	14	21	Temperatura vazduha T C° 7	14	21	Sred Dan	Max	Min	Min 5 cm	Napon vodene pare e mm 7	14	21	Relativna vlažnost u% 7	14	21	Sred Dan	Pravac i jačina vetra D, f (0—12) 7	14	21
1	737.2	734.0	735.5	20.1	31.2	18.6	22.1	32.0	14.4	12.1	11.9	08.0	13.7	67	23	85	58	- 0	S 5	SW 3
2	737.9	736.4	736.6	19.0	27.6	22.9	23.1	29.6	15.9	14.6	13.5	12.5	14.8	82	45	71	66	- 0	W 2	SSW 1
3	736.9	735.6	736.5	21.1	31.4	22.6	24.4	32.3	16.0	15.3	15.4	12.3	13.2	82	36	64	61	- 0	N 1	NNE 6
4	738.7	736.4	737.0	20.1	29.7	19.4	22.2	31.1	17.6	16.5	12.6	14.3	15.1	71	46	89	69	NW 2	NE 2	S 4
5	737.2	739.1	739.8	20.0	17.8	17.2	18.0	21.4	16.4	17.9	13.3	12.9	09.9	76	84	67	76	N 3	NNE 2	NNW 4
6	739.9	739.9	740.5	16.0	18.8	16.2	16.8	19.0	13.4	12.4	11.2	11.7	11.9	82	72	86	80	NNW 2	N 3	N 2
7	739.4	738.3	736.4	15.8	23.2	19.0	19.2	24.6	14.5	14.2	12.7	14.4	15.3	94	67	93	85	- 0	W 3	NNW 3
8	738.2	737.5	738.9	20.1	26.2	18.2	20.7	27.9	16.9	15.5	14.6	14.8	13.9	83	58	89	77	NW 2	NW 3	- 0
9	740.7	738.8	739.4	19.0	30.0	21.8	23.2	31.6	16.0	14.6	14.1	12.7	15.9	86	40	81	69	- 0	N 2	E 2
10	741.2	741.3	742.7	20.6	23.4	21.8	21.9	27.4	16.6	15.4	14.8	12.8	14.5	81	59	74	71	- 0	WNW 2	NNE 3
11	743.0	741.4	741.8	23.8	30.2	24.6	25.8	30.8	17.8	16.4	15.3	13.4	14.6	69	42	63	58	NNE 1	N 4	S 1
12	742.6	741.4	742.6	23.8	30.9	26.1	26.7	31.2	18.5	17.4	15.0	13.1	12.9	68	39	51	53	NW 1	N 5	N 4
13	743.8	742.2	742.4	24.0	30.4	25.4	26.3	30.9	19.5	17.5	14.9	12.3	12.4	67	38	51	52	NNE 3	N 5	N 4
14	742.6	739.5	738.8	20.6	30.6	23.6	24.6	31.0	16.8	14.6	13.3	14.9	13.3	73	45	61	60	- 0	WNW 2	SE 2
15	736.9	733.3	734.1	20.6	30.2	21.6	23.5	31.4	15.4	13.4	13.3	12.1	13.4	73	38	69	60	- 0	E 2	ENE 2
16	734.4	731.7	731.6	20.3	32.0	23.6	24.9	32.2	16.6	15.2	14.6	13.2	16.1	82	37	73	64	- 0	SE 5	E 2
17	733.6	733.3	739.9	18.4	21.8	15.3	17.7	23.7	13.4	17.0	12.4	10.9	10.0	78	56	76	70	NNE 3	NNE 2	NNE 1
18	737.3	737.3	740.1	15.0	19.0	15.2	16.1	20.9	12.6	11.8	08.8	07.7	07.3	69	47	56	57	NNE 2	WNW 3	WSW 2
19	739.7	738.2	739.0	10.6	22.4	18.8	17.6	24.2	07.6	05.6	07.7	06.5	11.2	80	32	69	60	- 0	SSE 1	- 0
20	741.3	740.2	740.5	14.6	26.1	19.4	19.9	27.6	09.5	07.4	09.2	07.8	10.6	74	31	63	56	- 0	SE 2	SSE 1
21	743.4	742.4	742.6	15.7	29.5	21.9	22.2	31.0	11.6	09.2	10.1	08.0	10.7	76	26	54	52	- 0	ENE 1	ESE 1
22	744.8	743.3	743.0	18.0	32.1	24.9	25.0	33.2	13.3	11.6	12.0	11.5	12.9	77	32	55	55	- 0	WSW 1	ESE 2
23	744.0	741.9	742.3	20.0	33.4	30.4	28.6	34.6	15.8	13.8	13.3	12.6	15.0	76	33	46	52	- 0	WSW 2	ENE 1
24	742.7	740.4	740.9	22.8	32.6	22.6	25.2	33.2	18.3	15.9	16.0	11.7	11.7	77	32	57	55	- 0	NW 3	E 2
25	739.8	735.7	734.4	20.4	31.6	26.6	26.4	32.4	15.3	13.8	13.1	11.6	13.9	73	33	53	53	- 0	SSE 2	NW 2
26	736.5	737.3	740.3	21.6	24.2	21.0	22.0	26.6	17.6	15.1	12.5	12.4	09.0	65	55	48	56	NNE 3	N 5	N 4
27	742.5	742.0	744.2	19.2	25.6	19.7	21.0	26.2	18.6	16.0	09.4	09.4	09.7	56	38	56	50	WNW 2	N 4	NNE 3
28	745.4	743.3	743.7	18.1	27.2	21.8	22.2	28.4	12.0	10.0	09.7	10.0	11.3	62	37	58	52	- 0	W 2	NNE 3
29	743.8	741.7	741.8	19.0	28.2	22.2	22.9	29.1	14.0	11.6	11.9	11.6	10.5	72	40	52	55	- 0	NNE 4	NNE 3
30	743.2	742.2	743.2	19.6	29.4	24.4	24.4	30.9	14.4	11.6	11.6	09.5	11.1	68	31	48	49	- 0	W 1	NNE 2
31	745.0	743.6	743.8	19.2	30.7	23.2	24.1	31.4	15.2	13.0	11.9	10.0	08.8	71	30	41	47	- 0	S 2	NNE 1
MES. VRED.	740.4	739.0	739.8	19.3	27.7	21.6	22.5	29.0	15.2	13.8	12.6	11.5	12.4	74	43	64	60	0.8	2.7	2.2

1	744.8	742.5	742.9	17.6	30.8	24.6	24.4	31.7	15.5	13.2	12.3	10.3	11.0	81	31	47	53	- 0	W 2	NW 1
2	742.7	740.0	741.5	19.4	30.8	19.6	22.4	31.0	15.1	13.0	12.2	11.2	14.7	72	34	86	64	SSE 1	W 2	SSE 1
3	740.8	738.5	739.0	18.0	29.8	23.6	23.8	30.0	15.5	14.0	12.6	12.3	12.1	82	39	55	59	SE 1	SE 3	NW 2
4	740.4	738.8	740.7	18.2	30.6	21.2	22.8	31.4	14.4	11.9	11.3	10.7	08.9	72	32	47	50	- 0	SE 2	ESE 2
5	742.3	741.6	742.1	18.7	32.2	26.2	25.8	32.4	13.4	11.7	11.2	11.6	11.1	69	32	43	48	- 0	WSW 2	WNW 2
6	743.7	741.9	741.8	20.7	32.4	24.8	25.7	33.2	16.6	14.5	12.1	13.0	11.8	66	36	50	51	SSW 1	W 3	- 0
7	742.1	740.4	739.5	20.4	34.1	24.7	26.0	34.6	15.8	13.9	12.6	12.1	14.2	70	30	61	54	- 0	N 5	ESE 2
8	739.7	736.8	737.4	21.0	35.0	22.1	25.0	36.0	15.9	14.2	12.5	10.7	10.9	67	25	54	49	NNE 1	NW 1	SSE 3
9	737.9	735.2	736.0	20.5	32.1	23.8	26.0	33.6	15.7	13.7	11.9	12.5	12.8	67	35	51	51	ENE 1	NNE 2	SSE 2
10	737.0	734.9	736.6	20.8	31.2	21.6	23.8	33.7	16.9	14.9	13.8	14.6	13.7	75	43	71	63	- 0	SSW 5	NNW 2
11	737.0	735.9	738.0	18.0	27.2	20.8	21.7	28.4	13.8	12.0	12.4	10.3	11.8	80	38	64	61	- 0	NW 3	N 4
12	740.8	741.6	743.2	19.6	25.0	20.5	21.4	25.7	16.6	14.0	10.8	10.1	09.3	63	43	51	52	N 1	N 4	NE 2
13	744.9	743.0	743.1	15.4	27.0	20.1	20.6	28.4	09.9	07.0	09.5	08.1	09.5	73	30	54	52	- 0	NW 2	SE 1
14	744.3	742.5	742.7	16.4	28.4	23.2	22.8	30.0	12.5	09.9	10.3	11.2	10.3	73	38	48	53	- 0	NNE 2	E 1
15	744.3	741.9	741.2	17.6	31.4	23.4	24.0	32.5	13.3	11.1	11.2	10.6	10.8	74	31	50	52	- 0	W 3	NNE 3
16	740.7	737.9	738.6	17.4	32.0	23.4	24.0	33.4	13.6	11.0	11.3	11.2	12.5	76	31	58	55	ESE 1	SW 1	E
17	738.1	735.8	734.9	18.8	32.3	24.1	24.8	33.3	15.6	15.6	12.8	11.1	12.4	79	31	55	55	- 0	NE 2	- 0
18	736.8	736.3	738.8	18.4	29.1	22.0	22.9	30.3	16.0	14.0	12.0	14.0	12.0	76	46	61	61	- 0	NNE 5	NNE 3
19	739.8	738.2	738.7	18.1	31.4	25.0	24.9	32.7	15.8	12.9	11.1	12.2	10.7	71	35	45	50	- 0	- 0	SE 1
20	740.2	738.1	738.1	18.8	33.2	28.0	27.0	34.3	14.9	13.5	11.7	11.9	13.4	72	31	47	50	- 0	NW 2	SSE 2
21	738.8	735.5	736.5	21.0	33.8	26.0	26.7	34.6	17.6	16.4	13.5	13.6	13.9	73	34	55	54	- 0	SE 2	E 2
22	737.1	734.6	735.9	20.2	32.4	23.1	24.7	33.4	18.0	15.8	13.5	12.0	08.7	76	33	41	50	- 0	WNW 2	NNW 3
23	738.2	736.9	738.0	17.8	29.8	22.4	23.1	30.7	12.5	10.3	08.8	09.9	11.6	58	31	57	49	- 0	NW 1	NNE 4
24	739.2	736.5	736.5	13.5	29.6	22.8	23.4	30.4	14.4	11.6	11.3	09.1	09.7	71	29	47	49	- 0	NNE 1	- 0
25	736.5	737.6	739.5	17.6	23.6	17.6	19.1	25.4	13.3	12.1	12.8	08.8	08.4	85	40	56	60	NNE 2	N 5	NNE 1
26	741.9	742.0	744.1	17.3	21.6	17.9	18.6	23.2	14.5	11.6	09.1	08.4	09.3	61	44	61	55	- 0	N	NE 5
27	744.4	743.4	744.0	16.9	22.6	17.5	18.6	24.2	11.8	09.8	08.8	08.1	09.0	61	39	60	53	WNW 3	NW 3	N 1
28	744.7	743.0	743.2	12.2	26.2	17.4	18.3	26.8	07.[illegible]	05.2	08.1	07.2	07.8	76	26	52	52	- 0	W 1	- 0
29	745.6	744.5	744.0	16.2	28.2	23.4	22.8	28.9	12.5	10.4	09.0	09.2	11.6	65	32	54	50	- 0	SE 2	SSE 2
30	744.3	741.1	743.0	19.4	26.0	22.0	22.6	27.3	17.7	16.4	12.9	11.5	12.3	76	46	60	61	- 0	S 5	SE 1
31	741.2	739.0	739.2	17.6	21.6	19.6	19.1	22.6	17.2	16.4	14.2	13.3	14.6	94	80	91	88	SSW 1	- 0	SSE 1
MES. VRED.	741.0	739.3	739.8	18.3	29.4	22.4	23.1	30.4	14.6	12.6	11.5	11.1	11.3	73	36	56	55	0.4	2.4	2.1

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BR. ST. 265 H_B = 232 m H_b = 233.3 m h_t = 2.0 m h_r = 1.3 m

Dan	Vidljivost 0–9 14	Oblačnost N (0—10) 7	14	21	Srednji Dnev	Insolacija broj sati	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	8	00⊙	09	10 R	07.0	10.4	•	•	△¹0-6³⁰, F SSE-E 12²⁰-14⁰⁵, 19⁰⁸-20¹⁰, T SW 16³⁵-23ᵢ, R NNE 18²⁰-20³⁵, ●⁰⁻¹19⁰⁸-20⁵⁰, 22²⁰-23ᵢ, [ᶜ SW 19⁰⁸-23³⁰
2	7	03⊙	01⊙	00	01.0	12.6	10.6	•	
3	8	00⊙	04⊙	04	02.7	12.0	•	•	△⁰1-7³⁰, F N 17⁴⁵-22
4	7	02⊙	03⊙	10 ●R	05.0	09.2	•	•	△⁰1³⁰-7, T 15³⁰-24ᵢ, F N-NW 17⁴⁰-19⁵⁸, ●⁰19³⁰-24ᵢ, R 20⁰⁵-21
5	7	10	10●	08	09.3	00.7	01.8	•	T SE 0-11⁴⁰ᵢ, ●⁰⁻¹13³⁵-3⁴⁰, 8⁴⁵-14³⁰ᵢ, R 14⁴⁰-12³⁰, F N 16³⁵-20⁴⁵
6	7	10	10	10	10.0	00.1	13.9	•	●⁰⁻¹5⁴⁰-7⁰⁵ᵢ, 10⁰⁸-11ᵢ, 17³⁰-19⁰⁵ᵢ
7	7	10	07	10●R	09.0	07.1	10.4	•	≺ SE 1⁰⁵-3³⁰, 17⁵⁵-22³⁵, T SE 1⁴⁰-3³⁰ᵢ, 17⁵⁵-22⁴⁰, ●⁰⁻¹⁻²1⁴⁰-4³⁰, R 2-3, ⚡ 18⁴⁵-21⁴⁰
8	7	09	04⊙	03	05.3	05.7	03.4	•	F-F SE-SSE 16⁴⁰-17⁵⁰, ●⁰16³⁰-17³³ᵢ, T NE 17-17⁴⁶
9	8	01⊙	03⊙	03	02.3	11.0	00.1	•	△⁰20⁴⁰-24
10	7	00⊙	01●	02	01.0	06.1	•	•	△¹0-8, T N 11⁴⁵-12³⁰, ●⁰11⁴⁰-14³⁰, R S 12⁴⁰-13³⁰
11	7	04⊙	05⊙	02	03.7	11.6	00.4	•	△⁰⁻¹0-7³⁰ F N 9⁴⁰-18³⁰ᵢ
12	8	02⊙	04⊙	02	02.7	10.1	•	•	F N 9-20⁴⁵ᵢ
13	8	08	02⊙	02	04.0	11.8	•	•	F N 8⁵⁵-21³⁰ᵢ
14	7	01⊙	07 R	03	03.7	08.6	•	•	△⁰2³⁰-6⁴⁰, T SW-N 13³⁰-14⁴⁰ 18⁴⁵-19⁴⁵, F E 17⁵⁸-18³⁶
15	6	00⊙	07 R	06	04.3	09.6	•	•	△ 2-7, T W 12⁴⁵-14⁰⁵, R W-E 14⁰⁵-16⁴⁰, F W-ENE 14⁴⁰-15⁴⁰, ⚡¹14⁴⁰-15⁵⁵
16	8	07⊙	02	06	03.7	07.3	13.2	•	△¹0-8, F SE 13⁴⁵-15, T SW 15-15⁴⁰
17	8	10	03⊙	09	07.3	03.3	00.0	•	F NNE 1⁴⁵-1³⁰, ●⁰⁻¹⁻²5⁴⁰-10⁴⁰ᵢ, 15³⁰-15⁵⁰, R 8⁴⁵-9, 16-16³⁰, T SW 9-10³⁰, 15⁴⁵-16⁴⁵, ⚡¹15³⁰-[16⁴⁵
18	8	02⊙	09	09	06.7	05.6	36.0	•	F N 14⁴⁰-16⁰⁸ᵢ, △⁰ 23³⁰-24
19	8	08	05	09	07.3	07.3	•	•	△⁰⁻¹⁻²0-7³⁰, 20⁴⁰-24
20	8	00⊙	01⊙	00	00.3	13.5	•	•	△⁰⁻¹⁻²0-7, 20³⁰-24
21	8	00⊙	01⊙	00	00.3	18.5	•	•	△⁰⁻¹²0-8, 20³⁰-24
22	8	00⊙	01⊙	00	00.3	13.4	•	•	△⁰⁻¹0-9
23	8	00⊙	01⊙	00	00.3	12.4	•	•	△¹0-8⁴⁰, F N-NNE 17⁴⁴-17⁵⁶ᵢ
24	8	00⊙	04⊙	00	01.3	12.2	•	•	△⁰⁻¹0-10³⁰, 8³⁰-23-24, F N 14⁴⁰-16³⁰, T NE 15⁵⁵-16⁴⁵, ∩ NE 16³⁰-17
25	8	00⊙	01⊙	09	03.3	09.8	•	•	△⁰⁻¹0-7, T S 15²⁰-16³⁵, ≺ S 19-21³⁰
26	8	02⊙	07	08	05.7	07.9	•	•	F-F 0-1⁴⁵, 8³⁵-19³⁰
27	8	05⊙	02⊙	00	02.3	12.3	•	•	F N 3³⁵-22⁴⁵ᵢ
28	8	00⊙	04⊙	00	01.3	12.0	•	•	F W 14⁵⁵-19⁰⁸
29	8	00⊙	03⊙	00	01.0	12.3	•	•	△⁰⁻¹0-8, F NNE 9⁴⁵-18²⁶ᵢ
30	8	01⊙	04⊙	00	01.7	12.2	•	•	△⁰3-7³⁰
31	7	03⊙	04⊙	04	03.7	11.2	•	•	△⁰⁻¹0-7³⁰
MES. VRED.		03.0	04.2	04.2	03.8	296.1	92.2		

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1	8	04	03 ⊙	04	03.7	10.2	•	•	T NW 12²⁵-18²⁰, F N 17-18⁴⁵, ⚡ 18⁴⁰-18³⁰
2	7	01⊙	08 R ⊙	09	06.0	08.4	•	•	△ 0-8³⁰ T NNW 13²⁵-13⁴⁵
3	7	03⊙	04 R ⊙	00	02.3	10.7	00.2	•	△¹2-6⁴⁰
4	8	00⊙	02 ⊙	01	01.0	12.2	•	•	△¹0-6³⁰
5	8	00⊙	03 ⊙	01	01.3	12.4	•	•	
6	7	01	04	00	01.7	12.3	•	•	F N 16⁰⁸-18⁴⁰
7	8	00⊙	01⊙	00	00.3	12.4	•	•	T E 15³⁰-16²⁰, ≺ 16⁴⁵-23¹⁵ᵢ, F-F NNE 16⁵⁵-18²⁰
8	8	02⊙	05⊙	01	02.7	09.2	•	•	T S 13⁴⁰-14⁴⁴, ⚡ 13³⁰-13³⁵
9	8	01⊙	09 ● R	02	04.0	10.2	•	•	△¹2³⁰-6³⁰, F SSE-NNE 14³⁵-19²⁰ᵢ, T W-SSE-NE 12³⁰-16⁴⁵ᵢ, R 15⁴⁵-15³⁰, ●15⁴⁵-15³⁰ᵢ, ⚡ 15⁴⁵-15⁵⁹,
10	8	00⊙	05⊙	02	02.3	11.3	00.0	•	△⁰3-6³⁰ T 11⁰⁵-14³⁰, F NW-N 14⁵⁵-15³⁰, 19⁴⁰-21⁴⁰, ●⁰15⁴⁵-15⁴⁰ᵢ, 21⁴⁰-22⁴⁵ᵢ [≺ 19³⁰-24
11	8	04⊙	08	08	06.7	06.4	00.2	•	F N 14²⁹-16⁴⁷ᵢ
12	8	06	08⊙	01	05.0	05.1	00.2	•	△⁰2³⁰-7⁴⁰ F NE 15³⁰-15⁵⁹
13	8	00⊙	02⊙	00	00.7	12.5	•	•	△⁰1⁴⁵-6²⁰
14	8	00●	01⊙	00	00.3	12.2	•	•	△¹3-7, F NNE 15⁴⁵-19³⁰ᵢ
15	8	00⊙	01⊙	00	00.3	12.5	•	•	
16	8	00⊙	03⊙	00	01.0	10.9	•	•	△⁰3-7, T N 16⁰⁵-19⁴⁰, F N 16⁴⁵-19⁴⁵
17	7	00⊙	03⊙	00	01.0	11.7	•	•	△¹2³⁰-7
18	8	09	02⊙	09	06.7	09.4	•	•	F-F 14⁵⁰-23⁴⁰
19	8	00⊙	02⊙	01	01.0	11.2	•	•	
20	8	01⊙	01⊙	01	01.0	12.1	•	•	
21	7	00⊙	02⊙	00	00.7	11.0	•	•	≺ E 19⁴⁰-21³⁰
22	8	00⊙	06⊙	00	02.0	11.8	•	•	F WNW 15⁵⁵-18⁵³ᵢ
23	8	01⊙	02⊙	00	01.0	11.4	•	•	F N 14⁰⁷-20²²
24	8	02⊙	09	05 R	05.3	08.4	•	•	△⁰3-6³⁰, T W 20⁴⁰-22⁴⁰, ●⁰21¹⁵-22⁵⁰ᵢ, ⚡¹21⁴⁰-22⁴⁰
25	8	03⊙	06	02	03.7	08.4	02.6	•	F-F NNE-NW-N 17⁵⁵-18⁰⁵ᵢ
26	8	06	09	06	07.0	04.0	•	•	F N-NE 9³⁰-21⁴⁰ᵢ
27	8	08	05⊙	09	04.3	07.8	•	•	F N 9⁴⁰-16²⁷ᵢ
28	6	00⊙	06⊙	02	02.7	10.4	•	•	
29	7	07⊙	02⊙	00	03.0	03.6	•	•	F SSE 20⁴⁰-21⁰⁸
30	8	08	08	10●	08.7	01.9	•	•	●¹20²⁵-21¹⁵
31	7	10●	10	10	10.0	00.0	00.2	•	●⁰⁻¹5-10ᵢ
MES. VRED.		02.5	04.5	02.4	03.1	296.2	02.6		

1970 SEPTEMBAR SKOPJE

φ = 41° 57' N λ = 21° 38' E Gr. ΔG = + 1h 27 min. BR. ST. 265

Dan	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost u%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Sred Dan	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dan	7	14	21
1	738.1	738.7	739.7	17.4	19.8	18.2	18.4	21.0	17.1	16.9	13.8	13.3	14.2	92	77	9	87	NNW 2	N 3	- 0
2	740.9	740.7	741.9	16.3	25.1	17.4	19.0	25.7	15.3	14.9	11.9	09.5	11.1	85	40	74	66	NNE 2	N 3	N 1
3	743.5	741.9	742.4	14.2	26.8	18.6	19.6	28.1	10.6	09.4	10.4	09.6	12.3	86	36	77	66	- 0	WSW 1	- 0
4	743.1	740.5	743.5	14.2	28.6	18.8	20.1	29.4	12.3	10.6	11.1	11.4	12.7	92	39	78	70	- 0	NE 2	NE 3
5	743.7	742.2	742.5	17.7	26.2	17.4	19.7	26.4	15.4	13.6	11.4	08.8	10.3	75	35	69	60	NNW 1	WNW 3	SE 1
6	742.5	739.9	740.7	14.2	28.5	21.9	21.6	29.3	10.4	08.6	10.4	10.4	10.8	86	36	55	59	- 0	N 3	N 5
7	743.5	743.3	745.5	18.0	25.3	17.4	19.5	26.2	15.4	13.3	10.4	10.1	07.6	67	42	51	53	NNE 3	NNE 5	NNE 5
8	746.6	744.2	744.5	15.2	26.6	17.4	19.2	28.1	13.1	11.4	08.2	09.7	09.8	63	37	66	55	NE 3	WSW 2	E 1
9	745.3	742.6	742.2	14.2	29.1	18.9	20.3	30.4	10.8	09.0	10.4	10.4	10.1	86	34	61	60	- 0	SW 1	SSE 1
10	743.3	740.7	740.8	13.9	31.6	19.8	21.3	33.0	11.1	08.2	09.8	09.3	09.3	82	27	54	54	- 0	W 2	E 2
11	742.2	740.3	740.3	15.0	33.0	19.2	21.6	34.6	12.3	09.4	10.2	09.8	10.3	80	26	62	56	- 0	WSW 2	ENE 1
12	741.8	739.4	739.0	15.2	32.6	20.0	22.0	34.3	11.7	09.6	10.1	08.6	08.0	78	23	46	49	- 0	WNW 1	- 0
13	739.4	736.6	737.1	16.0	33.2	20.8	22.7	34.1	11.8	09.0	08.8	09.4	09.1	64	25	49	46	- 0	- 0	- 0
14	740.3	739.3	740.8	16.2	29.2	21.6	22.2	29.7	13.9	11.2	10.1	13.3	12.8	73	44	66	61	- 0	NNE 2	NNE 4
15	743.1	740.6	741.0	16.4	30.8	22.0	22.8	31.2	14.6	13.1	12.1	12.5	12.9	86	37	65	63	- 0	SSE 2	- 0
16	742.5	739.9	740.8	17.0	31.8	19.2	21.8	31.9	13.4	11.9	10.5	11.6	10.7	72	33	64	56	- 0	WNW 3	SW 1
17	741.8	741.7	743.2	16.9	26.6	19.6	20.7	27.3	14.6	11.8	09.8	11.9	11.3	68	46	66	60	NNE 1	WNW 4	N 2
18	745.0	743.9	745.0	15.4	25.8	20.2	20.4	26.4	13.9	12.4	10.0	11.6	10.5	76	46	59	60	NNE 3	SW 2	NE 2
19	745.5	744.0	744.3	14.4	26.7	21.3	20.9	26.8	14.0	11.6	10.0	08.6	09.4	82	33	49	55	N 2	WSW 2	N 2
20	744.8	742.4	742.7	18.6	26.2	19.0	20.7	26.6	16.4	14.6	10.2	08.0	09.0	63	31	54	49	NNW 2	NNE 3	NW 4
21	742.4	740.8	742.5	15.4	21.7	16.7	17.6	21.9	12.4	09.4	09.1	07.0	06.9	69	36	48	51	N 4	N 4	NW 2
22	742.2	741.6	743.4	13.2	20.4	16.6	16.7	21.0	10.8	07.9	07.5	07.5	07.3	66	42	51	53	NNW 2	N 3	NW 2
23	745.8	744.6	744.5	11.6	20.1	13.2	14.5	20.8	09.4	05.9	06.2	05.6	06.1	61	32	53	49	N 1	SSW 1	NE 1
24	745.7	744.1	745.0	09.5	20.4	15.4	15.2	21.0	07.4	04.5	06.9	05.8	05.0	77	33	38	49	NE 1	NNE 4	NNE 4
25	745.9	743.7	744.5	10.2	20.0	13.4	14.2	21.0	08.9	07.0	04.9	05.6	04.9	53	32	43	43	NNE 2	NW 2	NNE 4
26	745.5	743.0	743.7	04.6	21.2	17.6	15.2	22.7	03.1	-00.5	05.1	05.7	06.3	80	30	42	51	- 0	SW 3	NNE 4
27	746.7	748.6	749.6	13.6	17.4	11.4	13.4	18.4	11.0	07.1	07.2	07.6	05.1	62	51	51	55	- 0	NW 3	NW 2
28	750.7	749.5	751.8	04.4	17.4	11.2	11.0	17.8	02.4	-01.2	05.2	04.4	04.6	82	30	46	53	- 0	N 5	NW 3
29	752.7	749.8	751.0	06.3	16.2	09.5	10.4	17.6	04.8	00.5	03.9	02.9	03.6	54	21	41	39	NNE 4	NNW 4	NNE 4
30	750.7	746.2	744.9	01.8	17.6	06.4	08.0	19.5	-00.6	-04.7	03.4	02.6	03.1	64	17	43	41	- 0	ESE 2	- 0
MES. VRED.	744.2	742.5	743.3	13.6	25.2	17.3	18.4	26.1	11.2	08.9	09.0	08.8	08.8	74	36	57	56	1.1	2.6	2.0

1970 OKTOBAR SKOPJE

1	744.2	739.2	736.3	02.6	20.0	17.2	14.2	22.2	00.2	-03.5	03.8	06.6	07.9	69	38	54	54	- 0	SSE 4	SE 3
2	734.7	736.0	737.0	12.8	14.0	09.6	11.5	17.2	09.6	12.0	10.5	08.6	07.2	95	72	81	83	WNW 2	N 3	NNE 3
3	735.4	732.5	733.9	03.6	16.1	11.6	10.7	16.6	02.4	00.6	05.8	07.8	09.5	97	57	93	82	- 0	WNW 1	- 0
4	735.5	736.7	739.1	08.8	11.7	07.2	08.7	13.0	07.0	08.2	07.6	07.3	06.8	90	70	89	83	N 1	WSW 2	S 1
5	742.4	741.9	742.3	07.6	17.8	12.4	12.6	18.4	06.5	04.4	06.8	04.9	06.9	87	32	64	61	SSW 1	NNW 3	ESE 2
6	743.0	742.3	743.3	08.8	22.3	12.0	13.8	23.3	08.6	07.0	07.6	08.1	08.9	90	40	84	71	- 0	S 2	SE 2
7	744.5	743.0	743.7	07.2	23.4	13.3	14.3	24.6	05.1	03.0	07.3	08.9	09.2	96	41	80	72	- 0	W 1	- 0
8	745.8	744.4	745.4	07.4	24.5	13.2	14.6	25.6	07.0	05.0	07.5	09.1	09.4	97	40	83	73	- 0	- 0	- 0
9	747.2	746.1	747.0	08.4	24.4	14.6	15.5	25.8	06.8	04.5	07.8	09.2	09.2	95	40	74	70	- 0	N 2	ESE 2
10	749.2	748.4	749.2	11.4	22.8	11.6	14.4	23.6	09.4	06.6	09.4	09.2	07.5	93	44	73	70	- 0	SE 2	- 0
11	751.0	748.7	749.2	06.0	23.0	11.2	12.8	23.7	04.5	01.6	06.4	06.0	06.7	92	28	67	62	- 0	W 2	ESE 1
12	750.0	747.1	-	05.6	24.2	14.4	14.6	24.4	03.4	01.0	06.4	07.1	07.7	94	32	62	63	- 0	WNW 2	NE 1
13	748.0	746.1	746.5	09.8	23.4	16.2	16.4	23.7	08.4	05.8	07.8	08.6	09.4	86	40	68	65	- 0	NE 3	NNE 4
14	745.3	742.9	742.7	06.7	21.6	11.2	12.7	23.0	05.6	02.6	07.0	08.1	07.5	95	42	75	71	- 0	NNW 1	SE 1
15	744.3	742.7	744.1	08.8	19.6	13.6	13.9	19.4	06.4	04.0	07.9	08.4	07.6	92	49	65	69	- 0	NE 2	NNE 4
16	745.0	747.1	749.4	11.0	08.3	05.4	07.5	13.6	05.4	10.5	07.0	07.2	05.9	71	87	87	82	N 3	N 2	NNE 1
17	750.3	749.6	748.7	02.4	03.2	04.2	03.5	05.4	01.5	02.5	04.8	05.4	05.8	89	94	94	92	NNE 1	- 0	- 0
18	746.3	745.6	745.9	05.0	07.6	07.9	07.1	08.1	04.2	04.5	06.2	06.8	06.7	94	87	83	88	- 0	- 0	NNE 2
19	745.5	743.5	742.2	06.4	12.4	06.8	08.1	12.6	06.0	06.5	06.0	07.2	07.0	84	67	95	82	NNE 3	ENE 2	NNE 2
20	739.1	736.2	735.3	08.2	15.6	11.8	11.8	17.3	06.4	04.2	07.9	09.2	09.0	97	69	87	84	ENE 1	- 0	- 0
21	734.8	734.9	735.7	15.2	20.5	18.0	17.9	22.2	10.5	09.2	10.1	09.8	09.1	78	54	59	64	SE 3	SSE 5	SE 5
22	738.1	736.8	738.6	15.2	22.0	13.7	16.2	23.0	13.7	09.5	09.4	09.0	10.2	73	46	86	68	SE 3	SE 5	SSE 2
23	736.3	738.8	740.1	07.6	08.4	07.8	07.9	13.7	06.4	07.2	06.8	06.2	05.5	87	75	70	77	N 4	NNE 4	N 3
24	742.4	744.1	747.1	06.0	08.6	06.6	07.0	09.2	05.3	04.0	05.2	04.9	04.6	74	59	63	65	WNW 2	N 4	NNW 3
25	747.4	746.4	749.0	05.6	09.8	05.0	06.4	10.4	05.0	04.4	04.8	04.1	03.8	71	46	58	58	NNE 3	NNE 5	W 2
26	748.5	746.4	746.4	04.8	15.4	08.2	09.2	16.0	01.6	-00.9	05.2	06.5	06.3	80	50	77	69	- 0	NW 2	NNE 3
27	746.5	745.5	748.2	00.8	17.6	11.2	10.2	18.6	00.6	-01.3	04.7	06.5	06.3	97	43	64	68	- 0	W 2	NNE 3
28	751.5	749.9	750.0	04.1	17.8	06.6	08.8	18.0	03.4	01.1	05.7	05.5	06.1	92	36	84	71	SSE 1	- 0	- 0
29	749.1	746.0	747.9	02.0	17.6	08.4	09.1	18.0	00.6	-00.2	05.1	07.5	07.3	97	50	89	79	- 0	- 0	S 1
30	751.2	750.0	750.1	08.2	18.8	07.2	10.4	19.4	06.4	04.0	07.3	07.6	06.2	90	47	82	73	WNW 1	W 2	- 0
31	748.8	746.3	747.1	01.6	18.7	07.0	08.6	19.5	01.4	-00.7	05.0	07.7	06.7	97	47	89	78	- 0	W 1	- 0
MES. VRED.	744.6	743.4	744.0	07.1	17.1	10.5	11.3	18.4	05.5	04.1	06.8	07.4	07.4	88	52	77	72	0.9	2.1	1.7

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BR. ST. 265 H_s = 232 m H_b = 233.3 m h_t = 2.0 m h_r = 1.3 m

Dan	Vlažnost 6-0	Oblačnost N (0—10)				Insolacija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Srednje		7	7	
1	7	10 ●	10	10	10.0	00.0	12.3	•	T 0^45-2^30 ●^0-1 R 1^40-3^05 6^22-7^12 11^45-14^45 i; = 5^20-13^30, ●° 5^30-6^00
2	8	04 ⊙	04 ⊙	00	02.7	09.2	01.3	•	●° 4^40-4^54, F_N 12^32, △^0-1 21-24
3	8	00 ⊙	01 ⊙	00	00.3	09.5	•	•	△^+2 0-8^40, 20^40-24; = 4^20-7^30
4	7	02 ⊙	04 ⊙	10 ●	05.3	09.2	•	•	△^2 0-7^30 F-F_N 17^46-20^48, ●^0-1 20^44-21^20 i
5	8	04 ⊙	03 ⊙	00	02.3	11.3	03.4	•	F_N 14^30-16^50
6	8	00 ⊙	01 ⊙	00	00.3	10.9	•	•	△^0-1 0^20-8^30 F_N 17^30-24 i
7	8	02 ⊙	04 ⊙	01	02.3	09.6	•	•	F-F 0-1^08, 10^30-21^45 i
8	8	00 ⊙	01 ⊙	00	00.3	11.3	•	•	
9	8	00 ⊙	01 ⊙	00	00.3	11.3	•	•	△^1 0-7
10	8	00 ⊙	01 ⊙	00	00.3	11.2	•	•	△° 0-7
11	8	00 ⊙	01 ⊙	00	00.3	11.1	•	•	△^1 0^30-8
12	8	00 ⊙	01 ⊙	00	00.3	10.8	•	•	△° 0-7^45
13	8	00 ⊙	01 ⊙	00	00.3	10.9	•	•	△° 2-8
14	8	04 ⊙	04 ⊙	00	02.7	09.2	•	•	F_NNE 10^04-13^04 16^40-21 i
15	7	03 ⊙	05 ⊙	06	04.7	07.8	•	•	△° 0-7, = 5^31-7^30, SW 18-23^20
16	7	00 ⊙	03 ⊙	02	01.7	09.0	•	•	
17	7	08	03 ⊙	10	07.0	06.3	•	•	F_N 18-18^40 i
18	7	00 ⊙	09	09	06.0	05.6	•	•	
19	7	02 ⊙	04 ⊙	04	03.3	06.6	•	•	F_NNE-NNW 16^20-21^40 i
20	7	09	04 ⊙	02	05.0	04.3	•	•	F_NNE 13^40-21 i
21	7	02 ⊙	06	10 ●	06.0	05.0	•	•	F-F_N-NNW-NNE 17^12-22^20 i, ●° 20^30-21^40 i
22	7	05 ⊙	09	00	04.7	01.3	00.0	•	F_N 15^50, 21^40-23^30
23	8	01 ⊙	08 ⊙	03	04.0	08.1	•	•	
24	7	03 ⊙	01 ⊙	00	01.3	08.5	•	•	F_N 10-23^30 i
25	7	04 ⊙	00 ⊙	00	01.3	09.2	•	•	
26	7	00 ⊙	00 ⊙	04	01.3	09.5	•	•	F_NNE 19^32-20^50 i
27	7	09	08	00	05.7	02.6	•	•	F_N-NW 6^39-12^08, 14^42-19^40
28	7	01 ⊙	02 ⊙	01	01.3	08.1	•	•	F_N 10
29	8	00 ⊙	01 ⊙	00	00.3	09.7	•	•	F_N 11^40-21 i
30	8	00 ⊙	08 ⊙	00	02.7	10.1	•	•	⌣° 5^45-6
MES. VRED.		02.4	03.6	02.4	02.8	247.2	18.0		

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1	8	04 ⊙	09	05	06.0	06.0	•	•	⌣ 2-6^30 F_SE 20^40-24 i
2	7	10 ●	10	01	07.0	00.0	03.5	•	F_SE-N 0-4^05 11-11^28 13^30-19^45; ● 4^05-13^05 i, △ 23-24
3	7	06 ≡	09	10 ●	08.3	03.6	05.6	•	△ 0-9, ≡ 4^45-8^35 i, ≡ 5^48-7^40, ● 17^32-24, 18-19^20
4	6	10 ●	07 ⊙	08	08.3	01.1	10.2	•	●^0-1 0-2^20 4^32-12^20 i, 15^20-15^40, 18^32-19
5	8	06 ⊙	06 ⊙	10	07.3	05.4	00.2	•	F_NW 10^55-12^25
6	8	04 ⊙	01 ⊙	00	01.7	09.7	•	•	△ 21^30-24
7	8	00 ⊙	02 ⊙	00	00.7	10.9	•	•	△ 0-8^20, 20^32-24
8	8	00 ⊙	01 ⊙	00	00.3	09.8	•	•	△ 0-9
9	8	00 ⊙	01 ⊙	01	00.7	09.6	•	•	△ 2-7^30
10	7	09	03 ⊙	00	03.0	07.6	•	•	△ 0-7
11	7	00 ⊙	00 ⊙	00	00.0	09.4	•	•	△ 7^30-8^30, 21^30-24
12	8	00 ⊙	01 ⊙	00	00.3	09.7	•	•	△ 0-9
13	7	06	04 ⊙	00	03.3	08.0	•	•	△ 20^40-24
14	6	00 ⊙	00 ⊙	00	00.0	09.8	•	•	△ 0-17^40 = 5^40-16^30
15	7	09	06	10	08.3	02.8	•	•	= 3-12^20, △ 3^40-8^30, F_NNE 16^40-20^40, ● 21^40-22^05 i
16	7	10 ●	10 ●	10 ●	10.0	00.0	00.0	•	F_N 2-6^30 i, ● 5^50-24 i
17	5	10 ●	10 ●	10 ●	10.0	00.0	11.5	•	●^0-1 0-7^58 10^32-12^40, *^0-1 7^52-10^30 i, *^0-1 8^42-9^40, = 13^30-24
18	6	10 ●	10	10	10.0	00.0	09.3	•	= 0-24, ●^0-1 0-2^30, 5^40-9^32 i
19	7	10	04 ⊙	05	06.3	02.3	00.0	•	= 0-5^30 14^50-24; △ 20-24
20	7	10	04 ⊙	08	07.3	03.0	•	•	= 0-14^30, △ 0-8^30
21	8	06 ⊙	09	10	08.3	03.7	•	•	F_SE 7^48-17^30 i, 20^48-20^56 i
22	8	07	08	10 ●	08.3	05.9	•	•	F_SE-S 3^48-5^40 i, 8^48-9^45 13^40-14^21 i; ∩ 9^40-9^50, ●^0-1 15^30-24
23	8	10 ●	09	10	09.7	00.0	12.4	•	●^0-1 0-12^30, 23^50-24, F_N 4^30-20^30 i
24	8	09	08 ●	10	09.0	00.6	03.0	•	F_NNE 12^30-19 i, ●° 13^25-14^45 i
25	8	09	03 ⊙	00	04.0	08.5	00.0	•	F_N 7^05-20^40 i
26	8	06	02 ⊙	00	02.7	08.1	•	•	△ 22^30-24
27	7	00 ⊙	01 ⊙	00	00.3	09.6	•	•	△ 0-4^30 ⌣ 4^30-6^30
28	8	01 ⊙	00 ⊙	00	00.3	09.2	•	•	△ 3-5^30
29	6	01 ⊙	09 ⊙	07	05.7	07.2	•	•	△ 0-6, 21^30-24; ⌣ 6-7, ≡ 6-14^30, 23^30-24
30	6	09	02 ⊙	00	03.7	06.7	•	•	△ 0-8, 19^30-24; ≡ 0-14^30
31	7	00 ⊙	00 ⊙	00	00.0	06.8	•	•	△^1 0-8, = 4^30-7^30
MES. VRED.		05.5	04.7	04.4	04.9	174.0	61.0		

1970 NOVEMBAR SKUPJE

φ = 41° 57' N λ = 21° 38' E Gr. ΔG = + 1h 27 min. BR. ST. 265

Mes.	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodene pare e mm			Relativna vlažnost U%				Pravac i jačina vetra D, f (0—12)		
	7	14	21	7	14	21	Srednji Dnev	Max	Min	Min 5 cm	7	14	21	7	14	21	Srednji Dnev	7	14	21
1	748.0	745.4	745.1	00.8	19.9	07.4	08.9	20.9	00.7	-00.5	04.9	06.6	06.6	100	38	86	75	- 0	NNW 1	- 0
2	745.6	744.4	745.4	01.2	19.5	07.1	08.7	20.6	01.0	-00.7	04.7	07.3	06.2	93	43	82	73	- 0	SSW 2	- 0
3	746.4	744.0	743.2	02.0	17.0	06.4	08.0	18.5	01.9	00.2	05.1	06.6	06.3	97	46	88	77	ESE 1	W 1	SE 1
4	743.5	742.6	746.2	-00.4	19.4	11.8	10.6	20.6	-00.6	-02.2	04.3	07.1	06.4	96	42	61	66	- 0	WNW 2	NNE 4
5	747.5	744.3	742.7	02.2	18.9	05.4	08.0	19.4	01.9	-00.7	05.2	07.1	05.6	97	43	83	74	- 0	SSE 1	- 0
6	740.4	738.8	743.3	01.0	13.8	06.6	07.0	16.0	01.0	-01.1	04.8	07.1	05.6	97	60	76	78	- 0	N 5	W 2
7	744.2	743.6	745.4	03.0	12.4	01.4	04.6	12.6	01.3	-01.4	04.7	04.4	04.0	83	41	78	67	NNE 3	W 2	- 0
8	746.4	744.9	746.2	02.1	08.9	08.2	06.8	10.7	-01.4	-03.7	04.7	05.8	06.9	89	67	85	80	- 0	- 0	NW 1
9	745.4	743.1	741.3	07.4	12.4	10.6	10.2	13.0	07.2	05.5	06.9	07.8	08.2	89	72	86	82	ENE 1	- 0	- 0
10	738.4	736.3	740.8	08.8	13.0	08.0	09.4	14.0	08.0	07.4	08.3	09.5	06.4	97	85	80	87	- 0	- 0	NNW 2
11	744.4	744.7	747.5	06.8	11.0	02.6	05.8	11.6	02.2	03.7	05.5	03.2	03.8	74	32	69	58	NNE 3	N 5	- 0
12	748.4	747.4	747.6	-03.8	11.0	00.8	02.2	12.0	-03.8	-06.4	03.2	04.1	04.2	91	42	86	73	- 0	- 0	- 0
13	747.7	745.8	746.0	-03.8	12.2	01.1	02.6	13.5	-04.3	-06.0	03.3	04.5	04.3	96	42	86	75	E 1	NW 1	- 0
14	745.2	742.7	742.3	-02.4	10.0	01.2	02.5	10.5	-03.1	-05.6	03.6	05.0	04.2	94	54	83	77	- 0	- 0	NNE 1
15	738.9	738.0	736.8	00.2	10.7	04.3	04.9	12.0	-02.3	-03.9	04.3	07.0	06.0	93	73	96	87	- 0	WSW 2	N 1
16	733.3	732.7	734.8	09.1	11.9	05.4	08.0	15.4	01.8	00.1	07.6	08.0	05.6	88	77	83	83	S 3	- 0	- 0
17	737.3	741.1	743.2	05.8	09.6	01.4	04.6	10.3	00.0	01.0	05.6	04.7	04.6	81	53	90	75	N 3	S 1	SE 1
18	745.3	744.6	745.3	-03.0	10.8	03.7	03.8	11.6	-03.1	-05.0	03.4	05.4	05.3	93	56	89	79	- 0	- 0	- 0
19	745.4	743.5	743.4	-01.4	14.2	04.2	05.3	14.8	-02.1	-03.0	04.0	06.2	05.6	96	51	91	79	- 0	- 0	- 0
20	743.8	742.5	743.4	-01.0	15.2	04.6	05.8	15.5	-02.0	-02.9	04.3	07.1	05.7	100	54	90	81	- 0	WNW 1	E 1
21	744.2	742.3	741.6	01.9	16.8	07.3	08.3	17.4	00.2	-01.0	05.1	07.4	06.7	97	52	87	79	- 0	S 1	NNE 2
22	736.6	735.3	735.4	11.5	14.6	08.4	10.7	15.6	06.4	05.2	08.4	09.5	05.6	82	76	68	75	SE 4	S 2	ESE 2
23	737.0	737.9	739.8	07.4	08.4	05.4	06.6	09.0	01.1	-01.0	05.3	05.4	05.7	69	66	84	73	N 4	NNE 3	NNE 2
24	743.0	744.6	746.7	07.8	11.4	06.6	08.1	12.0	05.4	04.6	05.5	05.7	05.7	70	57	79	69	N 4	NNW 5	NNE 2
25	747.8	748.7	749.8	08.0	10.2	05.8	07.4	10.9	04.3	05.6	05.0	05.0	05.2	63	54	75	64	N 5	NNW 3	N 2
26	750.2	749.2	749.7	-00.3	11.7	05.4	05.6	12.0	-00.5	-02.6	04.1	04.9	04.5	91	47	67	68	NNE 2	NNW 2	NNE 4
27	749.9	748.7	750.1	-00.2	08.9	02.2	03.3	09.2	-01.4	-04.0	04.0	04.8	04.4	89	56	82	76	NW 2	NNE 4	N 2
28	750.4	749.3	747.4	-02.6	06.0	-02.2	-00.2	06.8	-03.7	-06.5	03.4	04.8	03.4	90	69	88	82	SE 1	NW 1	- 0
29	746.9	745.4	745.8	-02.0	00.9	-00.6	-00.6	01.2	-03.9	-06.0	03.9	04.6	04.4	98	95	100	98	- 0	SW 1	- 0
30	746.0	745.4	744.7	-01.0	01.6	00.3	00.3	02.0	-01.2	-01.1	04.3	04.6	04.7	100	90	100	97	- 0	WNW 1	- 0
MES. VRED.	744.2	743.2	744.0	02.2	12.1	04.7	05.9	13.0	00.4	-01.1	04.9	06.0	05.4	90	58	83	77	1.2	1.6	1.0

1970 DECEMBAR SKUPJE

1	744.1	743.1	743.5	00.5	09.8	06.8	05.7	09.4	00.3	00.3	04.8	06.2	06.6	100	73	8	87	N 1	NNW 2	- 0
2	742.8	742.3	743.3	06.2	09.8	08.4	08.2	09.9	06.2	05.4	06.9	08.4	08.1	97	93	97	96	- 0	N 1	S 1
3	744.3	742.6	741.4	07.0	12.0	02.1	05.8	12.9	02.0	00.0	06.3	05.6	05.1	84	54	95	78	NNW 2	- 0	E 2
4	740.4	742.9	745.1	03.3	05.4	04.0	04.2	08.0	00.6	-00.8	05.5	04.8	03.5	95	72	58	75	- 0	NNE 2	NW 1
5	747.0	747.1	748.8	01.2	06.2	-02.8	00.4	06.9	-03.0	-01.5	03.0	03.0	03.0	60	42	82	61	NNW 2	N 2	- 0
6	748.8	749.5	749.8	-01.7	00.4	00.2	-00.2	00.7	-04.1	-07.1	03.8	04.2	04.5	93	90	96	93	- 0	- 0	- 0
7	750.5	749.8	750.9	00.0	07.3	-00.7	01.5	07.3	-01.3	-00.8	04.4	04.8	04.2	96	63	96	85	- 0	S 1	- 0
8	752.3	751.7	752.4	-04.0	03.6	-00.8	-00.5	03.9	-04.7	-06.9	03.3	04.7	04.2	96	79	96	90	- 0	WSW 2	- 0
9	753.6	752.3	752.3	04.0	09.6	02.0	04.4	09.8	-00.9	-02.4	03.9	02.9	03.6	65	33	68	55	N 2	NNW 4	NNE 1
10	750.9	749.3	750.5	-04.4	06.2	04.5	02.7	08.0	-04.5	-06.8	02.4	04.4	04.0	73	63	64	67	S 1	N 4	- 0
11	753.1	753.0	754.7	04.2	07.0	03.0	04.3	07.6	02.0	00.5	04.9	04.6	04.4	79	61	78	73	- 0	NNE 6	N 3
12	754.3	752.3	752.3	-03.6	08.6	-00.8	00.8	08.8	-04.4	-06.5	03.4	05.1	04.1	96	61	96	84	SE 1	W 1	SE 1
13	752.1	750.4	751.9	-04.0	01.2	-01.8	-01.6	01.9	-05.0	-07.8	03.3	04.7	03.9	96	93	98	96	N 2	- 0	- 0
14	751.1	749.6	749.3	-02.6	-01.4	-02.0	-02.0	-01.0	-02.6	-02.6	03.6	03.9	03.9	96	95	98	96	NW 2	WNW 2	SW 1
15	748.1	747.0	747.9	-02.6	00.2	01.2	00.0	01.3	-02.8	-02.0	03.7	04.5	04.2	97	96	83	92	SW 2	WSW 1	NNE 3
16	748.9	749.3	749.9	00.9	03.3	02.0	02.0	03.6	00.6	00.5	03.7	03.2	02.9	76	55	55	62	N 4	N 4	NNW 3
17	749.8	749.3	749.4	-00.6	01.6	-01.9	-00.7	03.1	-03.9	-06.4	03.0	03.1	03.4	68	60	85	71	NW 3	WNW 2	NNE 2
18	748.4	747.4	748.2	-00.1	03.3	-05.6	-02.0	04.4	-05.6	-06.1	03.5	02.8	02.5	77	48	81	69	NNE 2	SE 1	- 0
19	750.3	749.4	750.9	-08.9	02.2	-04.6	-04.0	02.9	-09.0	-11.1	02.1	02.8	02.8	92	53	87	77	W 1	SW 1	N 1
20	751.8	749.5	749.0	-08.8	04.8	-06.1	-04.0	04.8	-08.9	-11.5	02.2	03.2	02.4	92	50	83	75	ENE 1	- 0	SE 1
21	746.9	743.3	742.2	-09.7	02.0	-05.6	-04.7	03.0	-10.1	-12.1	02.0	03.6	02.6	91	68	86	82	ESE 1	- 0	- 0
22	739.6	738.4	737.9	-03.2	00.2	-00.5	-01.0	00.4	-07.4	-09.4	03.1	04.0	04.3	85	86	98	90	- 0	ENE 1	- 0
23	735.3	733.9	735.5	-00.8	02.2	00.2	00.4	03.4	-01.0	-00.9	04.1	04.3	04.3	96	81	93	90	N 2	- 0	- 0
24	736.1	739.9	742.3	-00.2	03.1	01.2	01.3	03.2	-00.5	-00.8	04.3	04.7	04.7	96	81	93	90	- 0	- 0	NW 2
25	742.1	739.6	738.3	-00.4	02.4	06.8	03.9	07.5	-00.6	-00.2	04.5	04.9	06.4	100	90	87	92	WNW 1	- 0	SE 3
26	738.0	740.2	743.7	01.6	12.7	00.8	04.0	13.6	00.8	-01.0	05.0	05.1	04.2	97	46	86	76	E 2	- 0	- 0
27	746.2	745.5	745.3	-03.8	03.8	01.0	00.5	04.2	-03.8	-06.2	03.1	04.6	04.8	90	76	97	88	- 0	SSW 1	NNE 1
28	741.9	739.1	740.0	02.4	10.9	07.0	06.8	11.4	00.4	-01.4	04.9	07.2	07.1	90	74	95	86	WNW 2	SE 3	- 0
29	741.4	740.2	737.8	06.0	09.6	10.8	09.4	12.0	06.3	05.6	07.1	07.9	07.2	97	88	75	87	NE 1	N 1	E 1
30	734.6	731.3	733.7	09.4	11.8	08.0	09.3	12.5	06.4	05.0	06.9	08.9	08.0	78	85	100	88	SSE 3	SE 5	- 0
31	734.9	731.9	729.7	05.0	12.4	10.4	09.6	13.6	04.2	03.2	06.5	09.4	09.0	100	87	95	94	- 0	SE 5	WNW 2
MES. VRED.	745.8	744.9	745.4	-00.2	05.5	01.5	02.1	06.4	-01.1	-03.0	04.2	04.9	04.6	89	71	87	82	1.2	1.5	1.0

SKOPJE 1970 NOVEMBAR

BR. ST. 265 H_s = 232 m H_b = 233.3 m h_t = 2.0 m h_r = 1.3 m

Dan	Važ. 0-9	Oblačnost N (0—10) 14	7	14	21	Sred Dies	Insolacija broj sat	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	7	00≡	00⊙	00	00.0	08.2	•	•		△0-6,21-24; ⌣6-8, ≡5^30-8^40 = 8^40-13^40
2	7	00≡	05⊙	00	01.7	08.2	•	•		△0-9, = 4^30-9^30 i, ≡ 6^40-7^30
3	7	09	01⊙	00	03.3	•	•	•		△0-9 = 5^30-11^30
4	7	03≡	00⊙	00	01.0	08.3	•	•		△0-2^45 ⌣2^45-7^30 = 3^45-12^20 i, ≡ 6^25-8^30, F NNE 16-18^45
5	7	02	05⊙	02	03.0	08.2	•	•		△1^30-7^30, = 6^40-11^30
6	7	02	10	10	07.3	04.2	•	•		△0^30-5, = 3^30-12^29, ⌣5-8, F N 12^20-20^18 i, ● 18^40-20^40 i
7	8	02	02⊙	00	01.3	07.8	00.0	•		⌣21^30-24
8	6	10	09	10	09.7	00.4	•	•		⌣0-3^30, = 7^05-24, ● 19^05-20^15 22^25-23^45
9	7	10	10	10	10.0	00.2	00.0	•		≡0-3, ● 7-10^20 i, 16-16^30, 22^45-24 i
10	6	10	09●	10	09.7	00.8	00.8	•		● 0-2^30 i, 9^45-18^30 i, = 5^30-16^10, F NNE 16-19^12
11	8	08	04⊙	01	04.3	05.9	02.5	•		F N 8^55-16^10 i
12	8	00	00⊙	00	00.0	07.9	•	•		⌣0-9
13	7	00	00⊙	05	01.7	07.5	•	•		⌣0-8^20 21-24; = 7^20-9^30 ⊕ 20^15-22^10
14	6	08	06	00	04.7	02.5	•	•		⌣0-9^30 20^40 24; = 3-17^30
15	5	09	05⊙	09	07.7	03.2	•	•		⌣0-7^28, = 8^20-16^40 20^30-24; ● 7^28-9^10, △21^10-24
16	7	10●	08●	06	09.0	03.2	00.5	•		△0-2^23, = 0-2^25, F SE-SSE 2^23-3^45, 11^22-12^41; ● 3^40-7^40; 10^05-10^35, 12^45-13^10, 16-16^25 ∩ 13^30-13^40, ↳ SW 17^30-20
17	8	09	08	06	07.7	01.7	02.3	•		
18	7	04	03⊙	02	03.0	07.0	•	•		⌣0-8^50, △20-24
19	7	01	01⊙	00	00.7	07.8	•	•		⌣0-9, = 6^05-12^30, △19^20-24
20	7	10≡	01⊙	00	03.7	05.9	•	•		△0-2, 20^20-24; ⌣2-9, = 3^30-4^15, 9^45-12^25; ≡ 4^15-6^25, ≡ 6^25-9^45, ↳ SW 17^30-19^40
21	7	08⊙	01⊙	04	04.3	07.6	•	•		△0-9^45 19^10-24; = 0^20-11^40 i, ≡ 3^30-5
22	8	09	03⊙	03	05.0	02.6	00.0	•		● 0-9^15 17^45-12^29, F SE 1-2^40 i, 20-9^05 i; ↳ SW 17^30-23^20
23	8	10	10	09	09.7	00.1	00.5	•		F N 5^32-6^52 10^45-13 i, 17^10-18^25 i; ● 7-7^40, 18^30-19^10 i
24	3	10	08	02	06.7	01.4	02.3	•		● 0^30-2^30, F N 7^10-16^10 i
25	8	09*	08	10	09.0	00.4	•	•		F N 5^30-15^56
26	8	00	00⊙	00	00.0	08.5	•	•		⌣4-9
27	7	00	00⊙	00	00.0	08.2	•	•		⌣3^30-9, F N 9^45-19^20 i
28	6	02	06	00	02.7	03.9	•	•		⌣0-8^40 21^30-24; = 6^20-24
29	3	10≡	10≡	10≡	10.0	00.0	•	•		⌣0-12, ≡ 4^30-24
30	5	10≡	10≡	10≡	10.0	00.0	•	•		≡0-24
MES. VRED.			05.8	04.8	04.0	04.9	131.6	08.9		

SKOPJE 1970 DECEMBAR

Dan	Važ. 0-9	Oblačnost N (0—10) 14	7	14	21	Sred Dies	Insolacija broj sat	Padavine R mm 7	Snežni pokrivač h cm 7	Razvoj vremena w
1	4	10≡	09	10●	09.7	00.4	•	•		≡0-10^45, ≡ 6^40-7^40 10^05-12^10, = 12^10-21^45 ● 17^30-24
2	5	10●≡	09	10	09.7	00.0	09.7	•		●°0-12^30 i, = 1^20-6^25 10^35-24; ≡ 6^25-8, ≡ 8-10^35
3	7	09	02⊙	00	03.7	04.5	02.7	•		● 3-4^20, △°18^30-24
4	7	10	09●	05	08.0	01.9	00.1	•		△² 0-5^15 ●°5^15-10^20 i 13^05-13^35 i; = 6^30-8^50, F NNE-N 8^35-9^45 12^45-14, 18-20
5	8	01	00⊙	00	00.3	00.5	00.6	•		F NNW 5-5^05, ⌣°19^30-24
6	4	10	10	09	09.7	00.0	•	•		⌣0-8^30 *°11^05-20^30 = 20^30-24
7	7	09≡	01⊙	00	03.3	05.4	01.9	•		≡0-6^20 9^30-13^40, ⌣ ≡ 6^20-9^30 ⌣20-24
8	6	05	07	08	06.7	02.0	•	•		⌣0-10^05 18^30-24; = 6^30-24
9	8	02	03⊙	01	02.0	08.5	•	•		≡0-3, ⌣0-6^40 F NNW-NNE 10^24-10^45, 13^08-16^40, 22^40-23^40
10	8	03	05	09	05.7	02.1	•	•		⌣3-9^40, F NNW 11^26-15^52 i
11	7	10	04⊙	04	06.0	01.9	•	•		F NNE 11^20-21^05 i
12	6	00	00⊙	00	00.0	05.8	•	•		⌣°1-9^35 20-24; = 4^30-24
13	4	00≡	10	10≡	06.7	00.0	•	•		⌣0-10^40 19^15-24; = 0-6, 10^20-14^30, ≡ 6-8^15 ≡ °8^15-10^20, 14^30-24
14	4	10≡	10*	10*≡	10.0	00.0	•	•		⌣0-9^40, ≡ 0-9^40, 15^30-24; V°2-24, ≡ 11^20-15^50
15	4	10*≡	10	10	10.0	00.0	•	•		≡0-3^15 6^25-11^20, V°0-13^10, = 3^15-6^25, 11^20-24
16	7	10	09	09	09.3	00.0	•	•		≡0-1^30 F NNE 0^34-19^35 i
17	7	04	10	03	05.7	01.2	•	•		F N 16^12-16^55
18	7	10	00⊙	00	03.3	04.8	•	•		⌣°19^30-24
19	6	01	01⊙	02	01.3	04.8	•	•		⌣°0-10^30 21-24; = 4^40-18^40
20	7	00	00⊙	00	00.0	07.6	•	•		⌣0-10^40, 18^30-24; = 6^45-11^30
21	6	00	06⊙	00	02.0	05.8	•	•		⌣0-10^40 19^10-24; = 5^30-17^30 i
22	6	10	10	10*	10.0	00.0	•	•		⌣0-7^30 = 6^20-24, *°7^30-13^20, 15^45-24; ⊠
23	5	10	07	10	09.0	00.4	04.0	01		*°0-6^30, 8^40-9^20, = 0-24 i, ≡ °8^05-9^40, ✱ 19^40-20^40, ⊠
24	3	10≡	10≡	10	10.0	00.0	00.0	03		≡0-3^30 15^30-24; ≡ 5^30-15^30 ⊠
25	5	10≡	10	10	10.0	00.0	•	01		≡0-16^40, ≡ 10^40-11^30, = 11^30-19^40, ● °16^20-17^20 i, 22^20-24 i; ⊠
26	8	08	02⊙	00	03.3	06.6	01.4	•		● 0-7^30, = 6^20-10^30
27	7	01	09	09	06.3	01.4	•	•		⌣0-10, ●°17^30-18^45
28	6	09	09	10	09.3	00.1	00.1	•		≡ 6^30-13^40 i, F SE 10^35-17^40 ●°18-24 i
29	5	10	10	02	07.3	00.7	01.0	•		● 0-2 i, = 2^20-17^20, F SE 17^52
30	7	02	10●	00	04.0	00.0	•	•		F SE-SSE 1^10-2, 4^30-6^31 i, 11^30-15^55, = 7^30-12^20 17^40-23^30 i, ●°1 8^15-22^40 i, ≡ 20^15-20^30
31	7	10≡	10	10	10.0	01.5	02.9	•		≡0-2^20, 6^40-10^40 i, ≡ 2^30-8^30 i, = 10^42-13^24, ● 12^40-16^30 i, F SE 13^52-17^22 i L ≡ 23^20-24
MES. VRED.			06.6	06.5	06.5	06.2	75.9	25.4		

0A217I

B) Mesečni i godišnji pregled

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dlss)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-13) N		NE		E		SE		S		SW		W		NW		C
												f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.	j.		j.	f.	j.	f.
SR SLOVENIJA																												
φ = 46° 20' N λ = 13° 33' E Gr. ΔG = + 54 min.																												
I	-	-02.0	02.1	-00.7	-00.3	02.9	-03.1	09.5	18	-08.7	23	04	01.2	06	02.0	07	02.0	01	01.0	16	01.4	13	01.5	04	01.0	.	.	42
II	-	-02.6	03.9	-00.4	00.1	04.8	-04.1	12.0	23	-15.8	17	16	01.2	12	02.5	05	01.8	.	.	14	01.1	19	01.9	05	02.2	.	.	13
III	-	00.3	05.7	01.6	02.3	06.7	-01.5	13.7	21	-07.4	10	09	01.4	14	02.7	06	01.7	.	.	17	01.4	12	01.8	.	.	.	.	35
IV	-	05.6	10.9	06.3	07.3	12.4	02.5	23.7	19	-05.5	04	09	01.1	11	02.6	06	01.3	.	.	19	01.5	28	02.2	01	01.0	.	.	16
V	-	10.0	15.4	10.5	11.6	16.9	06.1	22.0	20	-01.2	03	12	01.3	11	03.0	09	02.1	.	.	24	01.6	24	02.6	05	01.4	.	.	08
VI	-	15.9	22.4	15.9	17.5	23.8	11.5	28.9	21	04.7	05	07	01.1	06	02.3	12	01.5	01	03.0	12	01.3	24	02.0	11	02.0	.	.	17
VII	-	15.8	23.6	16.3	18.0	24.5	11.9	30.6	24	05.5	19	04	01.8	06	03.0	17	01.9	03	02.3	14	01.2	25	02.2	08	01.5	01	03.0	15
VIII	-	15.9	23.2	16.4	18.0	24.4	12.6	30.8	08	06.7	25	04	01.2	03	02.0	14	01.3	01	02.0	11	01.3	19	02.2	11	01.5	01	02.0	29
IX	-	13.1	21.2	14.0	15.5	22.0	10.4	25.9	11	01.9	30	02	01.5	06	03.2	06	01.0	.	.	09	01.3	29	02.2	10	01.6	.	.	28
X	-	04.9	14.9	07.0	08.5	15.8	03.1	25.1	10	-03.4	18	06	01.7	06	03.3	04	02.2	.	.	18	01.3	23	01.8	14	01.2	01	02.0	21
XI	-	04.0	10.1	05.0	06.0	10.7	02.2	15.0	10	-03.4	26	06	01.5	06	02.3	08	01.5	.	.	11	01.2	25	01.9	03	01.0	.	.	31
XII	-	-02.1	03.6	-00.5	00.1	04.7	-03.3	09.4	02,01	-10.9	26	07	01.0	14	03.1	10	01.3	.	.	15	01.1	13	01.5	04	01.0	.	.	30
GOD.	-	06.6	13.1	07.6	08.7	14.1	04.0	30.8	8 VIII	-15.8	17 II	86	01.3	101	02.7	104	01.6	06	02.2	180	01.3	254	02.0	76	01.5	03	02.3	285
BOVEC — BR. ST. 1																												
φ = 46° 01' N λ = 13° 33' E Gr. ΔG = + 54 min.																												
I	736.0	03.4	05.6	03.7	04.1	06.5	02.1	13.0	28	-02.4	24	.	.	63	02.6	05	01.0	01	02.0	03	01.3	.	.	.	.	.	.	21
II	734.4	01.5	05.6	03.1	03.3	06.6	00.8	12.0	23	-06.1	17	.	.	39	02.3	02	01.0	02	01.0	09	01.1	02	01.0	01	01.0	.	.	29
III	735.4	03.8	08.1	05.3	05.6	08.7	03.0	15.9	22	-01.0	01	02	01.0	48	02.3	.	.	04	01.0	11	01.4	01	02.0	.	.	01	01.0	26
IV	-	08.6	13.5	09.3	10.2	15.0	06.9	22.6	19	00.4	04	03	01.7	40	01.8	01	02.0	.	.	25	02.0	01	01.0	.	.	.	.	20
V	-	12.3	17.4	12.9	13.8	18.8	10.1	23.4	21	04.0	02	01	02.0	34	02.5	03	01.0	02	02.0	23	01.6	01	02.0	01	01.0	03	02.7	25
VI	-	17.9	24.0	19.2	20.1	25.1	15.8	30.0	28,27	10.5	03	01	01.0	42	02.6	04	01.5	23	02.1	06	02.3	10	01.7	01	01.0	03	02.7	.
VII	-	18.6	25.1	20.5	21.2	26.5	15.8	32.8	24	08.8	15	01	01.0	50	02.8	01	02.0	15	02.5	09	01.9	09	01.8	.	.	05	01.8	03
VIII	-	18.4	25.0	20.4	21.1	26.3	17.0	31.4	07	12.5	25	01	01.0	56	02.8	01	01.0	06	01.8	09	01.9	07	02.0	02	01.5	07	01.7	04
IX	-	15.9	23.0	17.9	18.7	23.9	15.2	27.5	11	07.8	30	.	.	54	03.1	.	.	08	01.6	13	02.0	04	01.8	.	.	06	02.7	05
X	-	10.0	17.0	11.9	12.7	17.9	09.1	28.0	12	04.2	25	01	01.0	48	03.0	02	02.0	08	01.6	09	01.3	09	01.7	.	.	03	03.0	13
XI	-	08.3	12.4	09.3	09.8	13.3	07.4	18.0	27	03.8	17	.	.	39	02.9	04	01.8	13	02.3	05	02.2	07	02.1	.	.	03	02.0	19
XII	-	03.7	06.8	03.9	04.6	08.0	02.1	14.0	12	-06.0	26	.	.	61	03.6	02	02.5	09	02.7	05	01.6	07	02.0	.	.	03	01.7	06
GOD.	-	10.2	15.3	11.4	12.1	16.4	08.8	32.8	24 VII	-06.1	17 II	10	01.3	574	02.7	25	01.5	91	02.1	127	01.7	58	01.8	05	01.2	34	02.2	171
VEDRIJAN — BR. ST. 2																												
φ = 46° 30' N λ = 13° 43' E Gr. ΔG = + 54 min.																												
I	683.5	-05.7	00.3	-04.1	-03.4	00.9	-07.3	07.3	28	-14.4	03	.	.	.	.	05	01.6	09	01.8	.	.	03	02.0	05	01.0	.	.	71
II	681.4	-07.4	01.6	-04.1	-03.5	02.4	-09.3	07.4	09	-22.0	17	.	.	01	01.0	04	02.0	09	01.6	01	01.0	06	01.5	08	01.5	.	.	55
III	682.8	-04.5	03.4	-02.0	-01.3	04.1	-05.9	10.4	22,21	-14.2	29	.	.	.	.	07	01.9	07	01.9	.	.	06	01.2	04	02.0	02	01.0	67
IV	685.0	00.1	07.6	01.9	02.6	09.2	-01.8	20.4	25	-13.8	04	01	01.0	04	03.0	04	02.8	06	02.5	02	02.5	02	02.0	08	01.2	.	.	63
V	687.0	05.7	13.3	06.9	08.2	14.6	02.1	19.8	13	-03.7	03	.	.	05	01.8	07	02.6	05	02.0	04	01.5	04	01.5	10	02.0	02	03.0	56
VI	688.9	12.4	20.3	13.7	15.0	21.4	08.3	26.4	28	01.4	05	.	.	02	03.5	07	03.0	04	02.2	.	.	04	02.5	08	01.9	01	01.0	64
VII	688.4	12.0	20.9	13.9	15.2	22.1	08.0	28.9	24	01.0	16,15	.	.	04	01.8	08	01.8	08	01.9	01	01.0	05	01.0	09	01.7	.	.	58
VIII	688.4	12.0	20.6	13.8	15.1	21.6	09.8	29.3	06	03.5	25	.	.	01	02.0	09	01.8	03	01.7	01	02.0	05	01.2	04	01.2	.	.	67
IX	690.7	08.6	18.6	10.5	12.1	19.5	07.0	24.6	11	-00.6	30	.	.	01	01.0	12	02.4	11	02.3	01	03.0	07	01.7	07	01.4	.	.	51
X	689.7	01.6	12.3	03.4	05.2	13.1	00.1	24.5	10	-06.0	24,18	.	.	02	01.5	06	02.5	07	02.1	02	01.5	04	01.5	08	02.8	03	02.0	61
XI	687.3	-00.2	07.6	01.1	02.4	08.7	-01.6	19.5	03	-08.8	17	.	.	01	02.0	07	01.7	05	01.8	02	02.0	06	01.3	02	02.5	01	03.0	66
XII	689.0	-06.6	-00.8	-05.5	-04.6	00.4	-08.0	06.8	01	-18.8	25	.	.	.	.	02	01.5	05	02.0	.	.	01	01.0	05	01.6	.	.	80
GOD.	686.8	02.3	10.5	04.1	05.2	11.5	00.1	29.3	6 VII	-22.0	17 II	01	01.0	21	02.1	78	02.2	79	02.0	14	01.8	53	01.5	78	01.7	09	02.0	759
RATEČE-PLANICA — BR. ST. 3																												
φ = 46° 11' N λ = 13° 44' E Gr. ΔG = + 55 min.																												
I	-	00.2	03.7	01.2	01.6	04.1	-01.9	11.5	28	-07.0	24	.	.	21	03.3	.	.	.	.	.	.	.	.	.	.	05	01.4	67
II	-	-01.5	05.1	01.4	01.6	05.8	-03.7	12.5	23	-14.0	17	.	.	06	03.5	.	.	.	.	.	.	02	02.5	.	.	02	01.0	74
III	-	01.3	07.8	03.6	04.1	08.6	-00.7	16.8	21	-06.5	08	.	.	16	02.4	.	.	01	01.0	01	03.0	.	.	.	.	05	02.0	70
IV	-	05.1	13.6	08.4	08.9	14.7	02.7	25.5	19	-04.0	04	01	01.0	11	02.3	.	.	05	02.8	01	01.0	02	02.5	02	02.5	02	02.0	66
V	-	08.4	17.4	11.8	12.4	18.8	05.5	24.4	21	-08.0	03	.	.	16	01.9	.	.	03	02.0	.	.	01	02.0	.	.	16	02.1	57
VI	-	14.8	23.9	18.1	18.7	25.5	12.2	31.5	27	05.2	05	.	.	12	01.8	.	.	.	.	02	03.0	09	01.8	03	01.7	06	02.0	58
VII	-	14.4	26.4	18.7	19.6	27.4	11.8	34.5	24	05.5	19	.	.	20	02.0	01	02.0	01	01.0	01	01.0	01	01.0	01	01.0	08	01.5	60
VIII	-	15.9	25.6	18.8	19.8	26.7	14.1	34.5	08	09.2	25	.	.	08	01.5	.	.	.	.	.	.	01	02.0	01	02.0	10	01.5	73
IX	-	12.8	23.8	16.1	17.2	24.3	11.2	29.0	11	01.5	30	.	.	22	03.0	02	01.0	02	02.0	.	.	03	01.0	01	01.0	04	01.2	56
X	-	06.1	16.1	09.1	10.1	16.9	04.4	27.0	12,11	-03.5	25	02	02.0	18	03.0	.	.	.	.	.	.	03	02.0	03	01.0	01	01.0	66
XI	-	04.7	11.6	06.4	07.3	11.9	03.0	18.5	10	-03.5	11	.	.	10	01.4	01	01.0	02	01.0	.	.	03	02.3	.	.	01	01.0	73
XII	-	-01.0	04.5	00.6	01.1	05.1	-03.0	12.0	02	-10.0	26	.	.	24	02.3	.	.	01	04.0	.	.	01	04.0	.	.	02	02.0	65
GOD.	-	06.8	15.0	09.5	10.2	15.8	04.6	34.5	8 VIII	-14.0	17 II	03	01.7	184	02.4	04	01.2	15	02.1	05	02.2	26	02.0	11	01.6	62	01.7	785
TOLMIN — BR. ST. 4																												
φ = 46° 17' N λ = 13° 46' E Gr. ΔG = + 55 min.																												
I	-	-03.3	-01.3	-03.3	-02.8	-00.2	-05.7	03.1	16	-15.7	08	01	03.0	08	01.4	04	01.2	04	02.2	04	04.2	19	05.4	14	02.9	29	02.1	10
II	-	-06.4	-04.1	-05.9	-05.6	-02.5	-08.8	02.4	22	-17.0	17	01	01.0	11	01.9	05	01.2	.	.	.	.	07	08.0	15	03.7	40	03.9	05
III	-	-04.9	-02.4	-04.3	-04.0	01.4	-07.0	03.5	24	-15.5	01	01	02.0	08	02.0	12	02.4	07	02.0	10	03.8	13	05.3	07	02.9	28	03.6	07
IV	-	-00.8	01.5	-00.6	-00.1	02.8	03.0	11.5	19	-11.6	04	07	02.0	07	01.7	03	01.0	02	02.0	.	.	16	05.3	24	02.4	27	03.0	04
V	-	03.3	06.1	03.7	04.2	07.4	00.8	12.2	31	-06.1	03	16	01.1	06	02.7	01	01.0	07	01.4	.	.	13	05.6	16	03.7	26	02.7	08
VI	-	10.9	13.8	09.9	11.1	15.5	06.9	21.3	22	00.0	03	06	01.0	07	01.4	01	01.0	02	02.5	.	.	07	03.3	33	02.8	32	02.0	02
VII	-	11.5	14.1	10.6	11.7	15.7	07.2	23.0	23	-01.3	15	09	01.1	09	01.8	06	01.8	07	02.4	04	08.2	13	04.6	20	02.2	15	01.8	10
VIII	-	11.5	14.4	11.1	12.0	16.1	08.6	23.0	06	03.8	18	02	01.5	05	01.6	03	01.0	05	01.2	01	03.0	18	02.8	24	01.6	23	02.0	12
IX	-	08.8	12.0	08.6	09.5	13.5	05.2	17.4	06	-00.6	17	01	01.0	09	01.9	05	01.8	08	01.8	.	.	22	05.1	27	02.2	06	02.0	12
X	-	04.0	07.3	04.0	04.8	09.0	00.7	19.0	11	-07.0	22,18	06	02.5	03	01.3	05	01.2	02	01.0	.	.	31	04.6	24	02.3	17	02.1	05
XI	-	01.8	05.1	02.0	02.7	06.5	-00.3	16.8	01	-06.8	16	04	02.8	03	02.0	.	.	02	01.5	02	07.0	15	05.9	34	02.5	28	02.6	02
XII	-	-04.0	-00.8	-03.9	-03.2	01.1	-06.2	11.5	12	-16.0	25	03	02.7	10	03.2	.	.	04	02.0	.	.	11	05.3	29	02.0	33	02.5	03
GOD.	-	02.7	05.5	02.7	03.4	07.2	00.4	23.0	23 VII 6 VIII	-17.0	17 II	57	01.6	86	02.0	45	01.6	50	01.8	21	05.0	185	05.0	267	02.5	304	02.7	80
DOM NA KOMNI — BR. ST. 5																												

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dim)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dim)	Min	Padavine R mm Σ	Max	Max.	Broj dana s: Tn ≤0,0	Tx ≤0,0	Tn ≤0,0	Tx ≥0,0	Tx ≥0,0	Tn ≥0,0	P(0-12) ≥6	≥8	Nm(0-10) <8,0	>8,0	R mm ≥0,1	≥1,0	≥10,0	●	▽	✱	⚠	≈	▲	▲	T	≡	▦
BOVEC — BR. ST. 1 — SR SLOVENIJA — H_g = 425 m H_b = - m h_g = 2.0 m h_z = 1.5 m																																					
I	7.9	6.9	6.3	7.0	051.1	04.2	96	84	92	90	47	370	100.9	06	.	05	24	.	.	.	.	.	04	17	15	13	09	11	07	.	.	.	.	.	.	07	17
II	7.0	7.1	6.1	6.7	085.8	03.6	87	59	79	75	25	143	075.1	06	01	01	26	.	.	.	.	.	01	10	11	09	02	05	06	.	.	.	.	.	02	01	16
III	7.6	7.8	7.4	7.6	094.1	04.1	84	60	83	76	17	304	095.8	04	.	.	21	.	.	.	.	.	01	17	15	11	09	06	10	.	.	.	.	.	01	05	31
IV	6.7	7.8	6.7	7.1	112.6	05.3	73	57	76	68	23	292	065.8	01	.	.	07	.	.	.	.	.	02	13	19	17	09	17	05	.	02	.	01	.	06	01	10
V	6.3	8.0	7.0	7.1	157.5	07.2	76	57	77	70	23	174	035.3	22	.	.	02	.	.	.	.	.	.	11	18	14	07	18	.	.	.	.	.	.	04	.	.
VI	5.7	7.3	6.1	6.4	181.3	11.6	82	60	85	76	29	149	055.4	29	.	.	.	16	.	.	.	.	02	09	14	11	03	14	.	.	.	.	.	.	11	01	.
VII	5.1	5.4	4.2	4.9	229.3	11.3	78	55	81	71	29	194	073.8	16	.	.	.	16	01	.	.	.	04	06	12	10	06	12	.	.	.	.	01	01	05	.	.
VIII	5.7	6.6	5.4	5.9	177.8	12.6	87	63	90	80	40	180	068.4	22	.	.	.	16	02	.	.	.	01	07	16	14	04	16	.	.	.	.	.	.	05	.	.
IX	5.8	5.0	5.2	5.3	202.1	10.8	87	61	89	79	37	113	081.9	17	.	.	.	02	.	.	.	.	03	05	09	08	01	09	.	.	.	.	.	.	03	03	.
X	4.4	5.3	2.3	4.0	171.8	06.8	91	55	89	78	27	169	149.3	21	.	.	08	01	.	.	.	.	10	03	06	05	01	06	.	.	.	.	01	.	03	02	.
XI	7.2	6.2	6.0	6.5	085.7	05.6	86	63	86	78	25	463	142.6	20	.	.	09	.	.	.	01	.	05	14	09	09	06	09	.	.	.	.	.	.	01	02	.
XII	5.3	5.3	5.1	5.2	069.8	03.9	92	67	86	82	32	301	127.4	30	01	03	26	.	.	.	.	.	08	10	09	07	05	07	06	02	.	.	.	.	.	02	06
GOD.	6.2	6.6	5.6	6.1	1618.9	07.2	84	61	84	76	17	2852	149.3	24 X	02	09	123	51	03	.	01	.	41	122	153	128	62	130	34	02	02	.	03	01	41	24	80
VEDRIJAN — BR. ST. 2 — H_g = 258 m H_b = 255.1 m h_g = 2.0 m h_z = 1.5 m																																					
I	7.2	6.8	6.8	6.9	078.0	04.9	77	71	77	75	41	200	042.0	05	.	.	08	.	.	.	.	.	07	18	14	13	06	14	03	02	.	.	.	.	.	05	01
II	6.6	7.1	5.1	6.3	075.8	04.1	74	62	70	69	31	054	019.0	15	.	.	08	.	.	.	.	.	03	09	08	08	02	06	04	01	.	.	.	.	01	05	02
III	7.7	7.7	7.7	7.7	083.8	05.0	76	64	75	72	13	210	038.0	04	.	.	02	.	.	.	01	.	03	19	15	13	06	09	06	.	.	.	.	.	.	03	-
IV	6.7	6.8	4.6	6.0	-	06.3	71	57	68	66	25	154	030.6	01	.	.	.	.	.	.	.	.	04	07	14	13	07	14	.	.	.	.	.	.	03	02	.
V	5.8	7.2	5.9	6.3	178.0	07.9	71	56	71	66	29	105	034.6	31	.	.	.	.	.	.	01	.	02	09	14	12	03	14	.	.	.	.	.	.	03	04	.
VI	5.0	5.8	5.5	5.4	216.7	12.3	76	60	72	69	33	199	045.9	30	.	.	.	17	02	.	01	01	01	07	14	11	08	14	.	.	.	.	.	.	04	01	.
VII	4.4	4.4	4.8	4.5	303.0	12.1	70	55	63	63	28	091	026.2	01	.	.	.	20	08	05	02	02	03	07	06	06	04	06	.	.	.	.	.	.	02	.	.
VIII	5.3	5.8	5.5	5.5	-	13.6	78	63	75	72	40	161	040.1	31	.	.	.	19	06	03	01	01	.	04	14	13	07	14	.	.	.	.	.	.	03	.	.
IX	5.1	3.6	4.8	4.5	236.3	11.4	73	58	72	68	38	090	044.7	17	.	.	.	15	.	.	.	.	06	02	07	04	03	07	.	.	.	.	.	.	02	01	.
X	4.5	4.2	3.7	4.1	190.8	07.8	72	58	72	67	16	028	023.5	21	.	.	.	04	.	.	02	.	09	04	06	02	01	06	.	.	.	.	.	.	01	03	.
XI	7.5	6.7	5.7	6.7	086.8	06.7	77	66	75	73	34	127	045.0	22	.	.	.	.	.	.	.	.	04	17	08	08	04	08	.	.	.	.	.	.	02	08	.
XII	5.2	5.0	4.1	4.8	118.5	04.5	70	64	68	67	35	215	069.8	30	.	.	06	.	.	.	06	03	09	10	08	08	04	07	01	.	.	.	.	.	.	05	01
GOD.	5.9	5.9	5.4	5.7	-	08.0	73	61	71	68	13	1634	069.8	30 XII	.	.	24	75	16	08	14	07	51	113	128	111	55	119	14	03	.	.	.	.	21	37	-
RATEČE-PLANICA — BR. ST. 3 — H_g = 864 m H_b = 865.1 m h_g = 2.2 m h_z = 1.5 m																																					
I	6.7	5.9	8.0	6.8	-	03.3	92	75	91	86	39	107	037.1	06	12	14	29	.	.	.	.	.	03	16	14	09	03	05	10	.	.	.	.	.	.	06	31
II	7.2	7.0	5.5	6.6	-	02.9	91	60	85	78	33	088	034.7	06	11	07	28	.	.	.	.	.	02	08	14	09	02	03	13	01	.	.	.	.	01	01	28
III	7.8	7.3	6.5	7.2	-	03.4	92	62	88	81	26	206	068.3	04	07	04	27	.	.	.	.	.	.	14	18	14	05	04	15	01	.	.	.	.	.	02	31
IV	7.1	7.9	6.1	7.1	-	04.3	91	54	86	77	20	219	033.9	02	01	.	20	.	.	.	02	01	01	13	17	14	07	10	13	04	.	.	.	.	05	02	30
V	5.3	8.0	5.6	6.3	-	05.7	82	46	80	69	19	088	029.3	22	.	.	06	.	.	.	02	.	01	08	15	12	03	15	.	.	.	.	.	.	05	.	01
VI	5.4	6.2	6.2	5.9	-	09.2	81	51	81	71	33	083	023.7	19	.	.	.	07	.	.	.	.	01	07	15	10	03	15	.	.	.	.	.	.	09	01	.
VII	4.6	5.3	4.8	4.9	-	09.4	84	50	82	72	31	228	115.7	16	.	.	.	12	.	.	.	.	01	04	12	10	06	12	01	01	.	.	01	.	07	.	.
VIII	5.5	6.2	5.1	5.6	-	10.4	92	60	90	81	36	186	036.4	21	.	.	.	08	.	.	.	.	03	06	18	17	07	18	.	.	.	.	.	.	06	01	.
IX	5.0	4.1	4.2	4.4	-	08.5	93	54	92	80	35	078	046.5	17	.	.	01	.	.	.	02	.	03	02	08	06	03	08	.	.	.	.	.	.	03	04	.
X	5.5	5.2	2.4	4.3	-	05.5	94	52	94	80	24	116	088.0	21	.	.	18	.	.	.	01	.	08	04	07	05	02	06	02	01	.	.	.	.	03	04	08
XI	5.6	5.1	5.8	5.5	-	04.6	92	63	92	83	33	150	051.3	15	.	.	19	.	.	.	.	.	06	09	09	08	05	07	02	.	.	.	.	.	01	03	05
XII	5.4	5.0	4.5	5.0	-	02.9	91	73	90	85	35	132	042.3	30	10	15	31	.	.	.	.	.	08	07	11	09	05	01	10	.	.	.	.	.	01	04	24
GOD.	5.9	6.1	5.4	5.8	-	05.8	89	58	87	78	19	1681	115.7	16 VII	41	40	179	27	.	.	07	01	37	98	158	123	51	108	66	08	.	.	01	.	41	28	158
TOLMIN — BR. ST. 4 — H_g = 180 m H_b = - m h_g = 2.0 m h_z = 1.5 m																																					
I	8.9	6.4	7.4	7.6	-	04.5	90	77	87	85	34	319	105.6	06	.	.	24	.	.	.	01	.	02	17	14	13	07	11	05	.	01	.	.	.	.	15	11
II	8.6	6.9	4.9	6.8	-	04.1	92	64	85	80	23	113	052.0	06	.	.	24	.	.	.	01	.	02	10	09	07	03	05	05	.	.	.	.	.	01	15	12
III	8.0	7.7	7.5	7.8	-	05.1	92	68	87	82	26	246	048.4	28	.	.	20	.	.	.	.	.	03	19	16	12	09	14	08	02	.	.	.	.	01	09	13
IV	7.5	7.1	6.4	7.0	-	06.5	91	58	80	77	23	294	061.7	01	.	.	06	01	.	.	.	.	03	12	17	15	09	16	02	01	.	.	.	.	06	05	02
V	7.1	7.5	5.5	6.7	-	08.6	94	62	85	80	27	198	038.6	31	.	.	02	.	.	.	.	.	03	13	21	13	08	21	.	.	.	.	.	.	05	11	.
VI	7.6	6.6	4.9	6.3	-	13.8	95	69	90	85	39	096	034.3	19	.	.	.	17	04	.	01	01	01	09	19	14	02	19	.	.	.	.	.	01	11	12	.
VII	7.5	4.6	3.6	5.2	-	14.0	95	61	87	81	46	150	052.2	16	.	.	.	22	14	.	.	.	04	07	09	07	05	09	.	.	.	.	.	.	05	12	.
VIII	8.9	6.1	4.2	6.4	-	14.8	96	68	91	85	36	161	038.0	18	.	.	.	22	10	.	.	.	02	07	12	11	06	12	.	.	.	.	.	.	05	20	.
IX	7.5	3.9	4.8	5.4	-	12.5	95	66	88	83	48	048	023.8	17	.	.	.	15	.	.	.	.	07	07	08	05	02	08	.	.	.	.	.	.	01	18	.
X	6.7	5.0	2.8	4.8	-	08.0	95	65	89	83	32	090	077.7	21	.	.	07	04	.	.	02	.	09	06	07	05	01	07	.	.	.	.	.	.	01	13	.
XI	8.0	6.7	6.5	7.1	-	06.9	96	73	92	87	38	276	100.1	20	.	.	08	.	.	.	.	.	05	18	11	09	06	11	.	.	.	.	.	.	02	08	.
XII	6.7	4.8	3.6	5.0	-	04.6	92	82	92	89	17	235	071.5	01	01	.	25	.	.	.	01	.	08	10	10	07	05	07	04	.	.	.	.	.	.	14	05
GOD.	7.8	6.1	5.2	6.3	-	08.6	93	67	87	83	17	2226	105.6	6 I	01	.	116	81	28	.	06	01	49	135	153	118	63	140	24	03	01	.	.	01	38	152	43
DOM NA KOMNI — BR. ST. 5 — H_g = 1520 m H_b = - m h_g = 2.0 m h_z = 2.0 m																																					
I	6.6	6.1	6.4	6.4	-	-	-	-	-	-	-	454	164.6	06	04	13	28	.	.	.	05	01	07	15	13	12	08	06	12	04	.	.	.	.	.	05	31
II	5.6	6.3	5.0	5.6	-	-	-	-	-	-	-	207	104.3	06	12	19	28	.	.	.	11	05	04	06	11	11	04	.	11	.	01	.	.	.	02	03	28
III	6.8	7.1	6.6	6.8	-	-	-	-	-	-	-	450	075.2	04	10	20	28	.	.	.	05	03	05	15	17	14	11	04	15	01	.	.	.	.	01	04	31
IV	7.2	7.1	6.6	7.0	-	-	-	-	-	-	-	450	085.2	27	02	08	22	.	.	.	03	02	04	15	17	17	12	04	14	01	01	.	.	.	03	08	30
V	5.5	6.9	6.1	6.2	-	-	-	-	-	-	-	255	057.1	12	.	.	08	.	.	.	04	02	03	13	13	13	07	11	02	.	.	.	.	.	05	06	31
VI	4.5	7.1	5.5	5.7	-	-	-	-	-	-	-	189	076.6	30	.	.	.	.	.	.	.	.	03	08	09	08	04	09	.	.	.	.	.	02	09	01	04
VII	4.2	5.7	4.5	4.8	-	-	-	-	-	-	-	222	054.3	16	.	.	02	.	.	.	04	01	05	05	10	10	06	10	01	.	.	.	01	.	04	03	03
VIII	5.0	7.3	5.3	5.9	-	-	-	-	-	-	-	248	049.9	21	.	.	.	.	.	.	.	.	03	07	18	15	08	18	.	.	.	.	.	.	06	04	.
IX	4.8	4.9	5.5	5.1	-	-	-	-	-	-	-	068	040.2	17	.	.	02	.	.	.	03	02	04	03	08	08	01	08	.	.	.	.	.	.	06	07	01
X	4.5	4.6	3.0	4.1	-	-	-	-	-	-	-	229	203.6	21	.	.	15	.	.	.	06	02	08	03	05	05	01	05	01	.	.	.	.	.	02	07	-
XI	5.7	5.2	5.0	5.3	-	-	-	-	-	-	-	683	214.9	20	.	01	16	.	.	.	08	.	09	12	09	09	07	07	04	.	.	.	.	.	01	02	15
XII	4.9	4.7	4.3	4.6	-	-	-	-	-	-	-	347	137.1	30	08	12	28	.	.	.	02	02	13	09	09	08	07	03	08	.	.	.	.	.	.	01	24
GOD.	5.4	6.1	5.3	5.6	-	-	-	-	-	-	-	3802	214.9	20 XI	36	73	177	.	.	.	51	20	68	111	139	132	76	85	68	06	02	.	01	02	39	51	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dlas)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12): N Č.	N J.	NE Č.	NE J.	E Č.	E J.	SE Č.	SE J.	S Č.	S J.	SW Č.	SW J.	W J.	W Č.	NW J.	NW Č.	C Č.
KREDARICA $\varphi = 46^\circ 23'$ N $\lambda = 13^\circ 51'$ E Gr. Δ G = + 55 min.																												BR. ST. 6
I	554.2	-07.4	-06.9	-07.2	-07.2	-04.2	-09.6	02.9	09	-15.6	08	09	05.3	01	05.0	02	06.0	14	05.9	.	.	.	.	.	.	51	05.6	16
II	551.1	-12.0	-10.9	-11.5	-11.5	-08.6	-14.0	-01.4	04	-22.6	17	10	05.0	08	04.0	09	04.9	02	03.0	02	07.0	.	.	.	.	47	05.8	06
III	553.1	-10.6	-08.7	-09.8	-09.7	-06.7	-12.1	01.6	22	-17.8	07	06	04.8	04	05.0	.	.	16	04.1	05	05.4	01	04.0	.	.	38	05.4	23
IV	556.6	-06.6	-05.2	-06.4	-06.1	-03.5	-08.7	06.7	23	-17.3	04	05	04.6	03	03.3	01	03.0	23	04.7	02	03.0	.	.	01	02.0	31	05.1	24
V	560.2	-03.6	-01.9	-03.1	-02.9	-00.5	-05.2	03.8	26	-13.9	02	06	04.7	07	05.6	.	.	15	03.9	02	04.0	.	.	.	.	33	04.7	30
VI	565.1	03.9	05.8	04.2	04.5	07.2	02.5	13.2	26	-06.3	03	06	03.2	04	02.5	04	01.5	10	03.7	04	02.2	.	.	.	.	32	03.8	30
VII	564.7	04.6	06.2	04.9	05.1	07.9	02.4	14.0	23	-05.0	17	01	04.0	02	03.0	01	03.0	23	03.3	.	.	.	.	.	.	32	05.8	34
VIII	565.0	06.0	07.5	05.8	06.3	09.2	04.0	17.0	07	-01.4	25	03	02.3	03	05.0	.	.	15	04.0	01	04.0	.	.	.	.	22	04.0	49
IX	566.0	03.6	06.0	03.7	04.2	07.2	01.7	12.5	08	-04.8	18	05	04.6	.	.	.	.	02	03.5	.	.	.	.	.	.	39	04.3	44
X	563.2	-00.4	01.4	-00.2	00.1	03.3	-02.9	11.7	13	-14.1	24	06	05.3	03	05.0	.	.	03	05.0	.	.	.	.	.	.	57	05.6	24
XI	560.1	-01.8	-00.7	-02.0	-01.6	01.7	-04.1	10.1	25	-12.7	17	12	06.4	07	04.1	01	04.0	11	05.7	01	04.0	.	.	.	.	34	05.4	24
XII	558.8	-07.7	-06.7	-06.6	-06.9	-03.8	-10.5	06.7	11	-20.6	23	05	06.2	04	03.2	01	04.0	13	05.1	02	05.0	.	.	.	.	36	05.4	32
GOD.	559.8	-02.7	-01.2	-02.4	-02.1	00.8	-04.7	17.0	7 VIII	-22.6	17 II	74	05.0	46	04.2	19	04.0	147	04.4	19	04.3	01	04.0	01	02.0	452	05.2	336
VOJSKO $\varphi = 46^\circ 01'$ N $\lambda = 13^\circ 55'$ E Gr. Δ G = + 56 min.																												BR. ST. 7
I	-	-02.3	-01.1	-02.3	-02.0	00.3	-04.4	06.0	06,05	-10.1	22	.	.	.	.	33	01.6	.	.	.	.	11	01.7	02	01.0	01	02.0	46
II	-	-03.9	-00.8	-03.0	-02.7	00.4	-05.6	04.5	23	-13.0	17	02	02.0	06	01.7	14	01.7	.	.	.	.	18	01.9	01	01.0	01	02.0	42
III	-	-01.8	00.8	-01.1	-00.8	01.7	-03.4	08.9	21	-09.3	01	.	.	.	.	19	01.5	.	.	.	.	15	01.9	03	02.0	.	.	56
IV	-	02.6	06.1	02.9	03.6	07.2	00.4	17.3	19	-05.9	04	.	.	04	02.8	12	01.3	.	.	.	.	22	02.1	01	02.0	.	.	51
V	-	07.2	10.1	06.8	07.7	11.4	04.4	17.0	26	-02.0	02	.	.	05	02.4	09	01.2	.	.	.	.	06	02.0	08	02.4	01	01.0	64
VI	-	14.4	17.5	13.2	14.6	18.4	10.7	22.9	27	02.5	03	03	01.0	04	02.2	07	01.4	.	.	.	.	10	02.4	01	02.0	.	.	65
VII	-	14.3	18.2	13.7	15.0	19.4	10.5	26.5	24	03.3	16	04	01.5	07	02.1	22	02.2	.	.	.	.	11	02.4	01	02.0	.	.	48
VIII	-	14.6	18.4	14.4	15.4	19.5	11.0	25.3	07	05.0	24	01	02.0	.	.	16	01.7	.	.	.	.	09	01.8	05	02.4	.	.	62
IX	-	11.1	15.0	10.9	12.0	16.3	06.4	21.3	11	-01.3	29	.	.	.	.	32	02.2	.	.	.	.	15	02.4	01	01.0	.	.	42
X	-	04.9	09.5	05.7	06.5	10.8	00.8	20.0	10	-06.1	17	05	01.6	15	02.9	13	01.3	.	.	.	.	19	02.2	04	02.0	01	02.0	36
XI	-	03.2	05.8	03.9	04.2	06.8	-00.9	13.3	02	-06.0	17	.	.	.	.	19	01.4	.	.	.	.	14	02.6	03	02.0	05	02.2	49
XII	-	-02.3	-00.2	-01.8	-01.5	01.3	-05.9	08.1	12	-14.5	26	.	.	08	02.8	19	02.0	.	.	.	.	08	02.0	03	03.0	.	.	55
GOD.	-	05.2	08.3	05.3	06.0	09.5	02.0	26.5	24 VII	-14.5	26 XII	15	01.5	49	02.5	215	01.7	.	.	.	.	158	02.1	33	02.1	09	02.0	616
RADOVLJICA $\varphi = 46^\circ 21'$ N $\lambda = 14^\circ 11'$ E Gr. Δ G = + 57 min.																												BR. ST. 8
I	-	-02.0	00.7	-00.9	-00.8	01.6	-04.4	10.0	17	-10.6	03	14	01.3	09	01.7	.	.	08	01.5	05	01.4	01	01.0	.	.	05	01.8	51
II	-	-03.7	02.7	-01.0	-00.8	03.7	-06.5	10.8	06	-19.0	17	10	01.6	04	01.8	.	.	06	01.8	08	01.4	01	02.0	.	.	02	01.0	53
III	-	-01.1	04.5	01.4	01.5	06.0	-02.8	12.9	22	-11.8	08	14	01.4	07	02.1	.	.	02	02.0	11	01.4	02	01.5	.	.	07	01.4	50
IV	-	04.3	10.3	06.2	06.8	12.1	01.8	24.6	19	-05.6	04	05	02.0	11	02.1	.	.	03	01.7	08	01.2	01	01.0	.	.	08	02.0	54
V	-	08.3	15.4	10.5	11.2	17.3	04.6	21.6	20,14	-03.0	01	09	01.8	14	02.4	.	.	01	02.0	09	01.4	03	02.0	.	.	02	02.0	55
VI	-	15.4	22.3	16.5	17.7	23.9	10.7	30.1	17	03.5	05,03	09	01.1	05	02.4	.	.	09	02.6	10	01.6	.	.	.	.	.	.	57
VII	-	15.5	22.6	17.3	18.2	24.6	10.5	30.0	14	05.5	19,15	08	01.4	14	02.6	.	.	05	02.6	07	01.1	.	.	.	.	08	02.8	51
VIII	-	15.4	22.2	17.1	18.0	23.5	11.8	30.9	07	07.0	27,18	02	01.5	02	01.5	.	.	03	03.0	13	02.0	06	01.7	.	.	.	.	67
IX	-	11.0	19.7	13.2	14.3	20.7	08.6	28.3	11	00.1	30	09	01.9	04	02.0	.	.	10	02.6	07	01.9	04	02.0	.	.	02	03.0	54
X	-	04.0	14.0	06.9	08.0	15.1	01.3	24.1	10	-04.6	18,17	12	02.1	09	02.6	.	.	04	02.5	05	02.0	04	01.8	.	.	05	02.0	54
XI	-	03.3	10.0	04.7	05.6	11.0	00.5	17.3	02	-05.0	29,27	13	01.7	05	01.8	.	.	10	02.2	07	01.1	02	01.5	.	.	07	01.7	46
XII	-	-03.3	01.4	-02.0	-01.5	02.2	-05.8	12.3	04	-11.4	26	16	01.4	04	01.5	.	.	07	02.3	03	01.0	.	.	.	.	06	01.7	57
GOD.	-	05.6	12.2	07.5	08.2	13.5	02.5	30.9	7 VIII	-19.0	17 II	121	01.6	88	02.2	.	.	68	02.3	93	01.5	24	01.7	.	.	52	01.9	649
JAVORJE NAD POLJANAMI $\varphi = 46^\circ 10'$ N $\lambda = 14^\circ 11'$ E Gr. Δ G = + 57 min.																												BR. ST. 9
I	-	-01.5	00.2	-00.8	-00.7	01.5	-03.0	09.5	17	-07.3	24	02	02.0	37	02.1	10	01.8	02	02.0	03	02.0	15	02.5	05	02.2	04	02.5	15
II	-	-02.6	01.7	-00.6	-00.5	02.8	-03.9	09.3	23	-11.9	17	07	01.1	32	02.1	04	01.5	01	04.0	05	02.2	26	04.1	.	.	02	01.5	07
III	-	-00.2	03.2	01.3	01.4	04.0	-01.3	09.7	20	-06.6	01	06	02.0	36	02.4	02	02.0	03	02.0	03	03.3	27	03.1	05	01.2	04	02.0	07
IV	-	04.1	08.9	05.5	06.0	10.0	02.6	21.6	19	-04.4	04	10	02.3	25	02.0	09	02.4	06	02.7	06	01.7	20	03.6	03	02.3	06	01.3	05
V	-	08.5	13.5	09.5	10.2	14.5	06.2	18.7	20	-00.2	01	07	01.3	31	02.5	09	02.6	11	02.1	06	02.3	16	04.2	02	02.5	08	01.4	03
VI	-	15.3	19.8	15.7	16.6	20.9	12.8	26.3	22	05.0	03	12	01.5	32	01.8	04	01.8	02	02.0	11	02.6	16	04.2	03	02.7	05	02.2	05
VII	-	15.5	20.8	16.7	17.5	21.7	12.8	27.5	24	05.6	15	20	01.4	38	02.0	08	02.5	05	01.2	04	02.0	15	03.8	01	01.0	02	02.0	.
VIII	-	15.3	21.0	16.6	17.4	21.8	13.6	27.4	08	08.9	18	17	01.6	32	01.8	10	02.0	03	01.7	09	03.3	10	02.5	06	02.3	.	.	06
IX	-	12.0	18.1	13.7	14.4	18.9	10.7	23.9	12	02.4	30	08	01.8	36	02.0	09	02.4	01	03.0	08	02.0	14	04.2	03	02.0	03	01.3	08
X	-	06.1	12.5	07.8	08.6	13.4	05.0	23.2	10	-00.6	25,16	08	02.1	32	02.1	10	01.9	03	01.7	05	02.8	21	04.1	05	02.0	02	01.5	07
XI	-	04.6	08.4	05.8	06.2	09.3	03.4	14.0	02	-01.6	28	07	02.1	20	02.0	07	01.7	01	02.0	16	02.9	22	03.7	06	02.7	07	02.0	04
XII	-	-02.1	01.4	-00.8	-00.6	02.5	-03.5	10.3	02	-11.0	25	04	01.8	23	02.7	10	02.7	.	.	06	01.7	14	02.8	13	02.2	04	02.0	19
GOD.	-	06.2	10.8	07.5	08.0	11.8	04.6	27.5	24 VII	-11.9	17 II	108	01.7	374	02.1	92	02.2	38	02.1	82	02.5	216	03.6	52	02.2	47	01.8	86
GOLNIK $\varphi = 46^\circ 20'$ N $\lambda = 14^\circ 20'$ E Gr. Δ G = + 57 min.																												BR. ST. 10
I	-	-00.9	01.5	00.1	00.2	02.7	-02.2	09.8	17	-06.6	09	05	01.0	09	01.1	08	01.0	15	01.0	04	01.0	15	01.0	17	01.6	20	01.0	.
II	-	-02.3	03.7	00.5	00.6	04.7	-03.2	12.5	23	-14.0	17	11	01.0	10	01.0	08	01.0	09	01.0	02	01.0	15	01.9	19	02.1	10	01.4	.
III	-	-00.1	05.2	02.3	02.4	06.1	-00.9	13.9	22	-07.0	08	15	01.5	15	01.3	08	01.0	10	01.0	08	01.0	17	01.2	08	01.8	12	01.1	.
IV	-	04.8	11.4	07.2	07.6	12.4	03.3	24.4	19	-03.7	04	09	02.0	08	02.1	09	01.4	16	01.1	13	01.3	14	01.4	12	03.3	07	01.3	02
V	-	08.5	16.3	11.0	11.7	17.6	06.7	22.2	14	-00.7	01	06	01.3	04	03.2	09	02.9	12	01.2	14	01.7	19	02.2	16	02.2	13	01.9	.
VI	-	14.5	23.2	17.5	18.2	24.4	13.0	29.3	23	05.7	03	14	02.1	10	02.7	07	01.0	08	02.0	06	01.3	14	01.5	15	01.5	15	01.6	01
VII	-	14.7	23.3	18.3	18.7	24.7	13.1	30.3	24	08.0	19	09	01.9	09	01.9	08	01.9	06	02.0	09	01.9	22	02.7	13	02.9	13	01.4	04
VIII	-	15.3	23.1	18.2	18.7	24.2	13.9	31.0	07	08.3	25	10	01.3	11	01.7	08	01.1	06	01.0	10	01.0	21	01.1	11	01.2	09	01.0	07
IX	-	11.8	20.6	14.8	15.5	21.5	11.0	27.5	11	02.3	30	14	01.8	13	01.7	07	01.1	08	01.0	10	01.0	19	01.5	09	01.2	05	01.0	05
X	-	06.0	15.3	09.7	10.2	16.0	05.0	26.5	10	-00.9	23	11	01.5	11	02.6	11	02.3	13	01.5	03	01.0	16	01.6	11	02.0	13	01.3	04
XI	-	04.9	10.9	06.8	07.4	11.6	03.6	17.9	04	-02.0	28	02	02.0	07	02.4	13	03.0	22	01.5	07	01.1	12	01.2	07	01.6	18	01.3	02
XII	-	-02.5	01.5	-01.7	-01.1	02.0	-03.8	12.7	04	-09.0	26,21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	06.2	13.0	08.7	09.2	14.0	05.0	31.0	7 VIII	-14.0	17 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dim)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dim)	min	Padavine R mm Σ	max	Dan	Broj dana s: Tn ≤ -10,0	Tn ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tx ≥ 30,0	P (0-12) ≥ 6	≥ 8	Nm (0-10) < 8,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	≋	✱	≈	∿	▲	▲	⊤	≡	▥
KREDARICA																																					
BR. ST. 6																																					
H_o = 2514 m H_b = 2519,0 m h_o = 2,0 m h_z = 1,9 m																																					
I	6.0	5.5	4.7	5.4	102.0	02.0	71	72	70	71	59	086	017.6	06	15	28	31	.	.	.	21	11	07	10	13	09	05	.	13	.	.	.	.	.	.	17	31
II	5.5	6.9	5.2	5.9	114.9	01.5	73	73	76	74	16	107	022.3	06	23	28	28	.	.	.	24	09	03	06	16	13	05	.	16	.	.	.	.	.	01	18	28
III	6.3	7.1	5.8	6.4	106.1	01.7	74	76	73	74	03	118	029.8	28	23	29	31	.	.	.	15	05	03	11	21	16	03	.	21	.	.	.	.	.	.	25	31
IV	7.2	7.7	7.3	7.4	097.5	02.2	73	73	81	76	07	110	030.6	10	14	23	28	.	.	.	14	06	02	15	21	17	03	02	21	.	.	.	.	.	04	24	30
V	6.2	7.7	5.7	6.5	143.2	02.9	73	73	81	75	01	067	016.8	31	03	15	31	.	.	.	13	05	01	12	16	11	01	.	16	.	.	.	.	.	04	24	31
VI	5.4	6.9	6.6	6.3	200.7	04.8	74	74	76	75	19	163	057.9	19	.	02	06	.	.	.	07	.	01	08	16	13	05	13	04	.	.	.	02	02	11	14	30
VII	5.0	6.7	6.0	5.9	187.8	05.3	77	82	80	80	32	183	089.4	16	.	03	10	.	.	.	07	07	02	09	13	13	04	09	07	.	.	.	02	.	05	19	14
VIII	5.1	7.9	6.6	6.5	141.8	05.6	74	81	80	78	33	435	100.6	31	.	.	03	.	.	.	03	.	03	11	21	20	09	18	03	.	.	.	02	.	09	18	01
IX	4.6	5.8	4.7	5.0	188.1	04.4	65	67	77	70	02	080	038.4	17	.	01	09	.	.	.	07	02	09	05	08	07	03	08	03	01	.	01	01	.	02	21	03
X	4.1	5.0	3.1	4.1	139.6	02.4	52	58	56	55	12	074	056.9	21	06	07	19	.	.	.	21	10	10	03	08	06	01	01	08	.	.	.	.	.	04	10	17
XI	5.6	5.3	4.0	5.0	111.0	02.2	59	57	61	59	01	201	055.2	15	04	14	23	.	.	.	15	11	06	08	09	07	06	.	09	02	.	.	.	.	01	13	30
XII	5.6	5.7	4.2	5.2	108.3	01.4	62	58	59	59	01	077	032.9	01	16	24	30	.	.	.	18	04	08	10	15	12	01	.	15	.	.	.	.	.	.	17	31
GOD.	5.6	6.5	5.3	5.8	1637.0	03.0	68	70	72	70	01	1701	100.6	31 VIII	104	174	249	.	.	.	165	70	55	108	177	144	46	51	136	03	.	01	07	02	41	220	277
VOJSKO																																					
BR. ST. 7																																					
H_o = 1070 m H_b = - m h_o = 2,0 m h_z = 1,5 m																																					
I	8.8	8.2	7.9	8.3	-	-	-	-	-	-	-	289	094.9	06	03	13	23	.	.	.	.	.	01	20	14	14	05	08	08	.	.	.	.	.	.	21	31
II	7.2	7.4	6.6	7.1	-	-	-	-	-	-	-	133	049.7	06	03	11	26	.	.	.	.	.	01	11	10	09	03	04	08	02	.	01	.	.	02	09	28
III	8.5	7.8	7.9	8.1	-	-	-	-	-	-	-	321	081.2	04	.	14	24	.	.	.	.	.	.	19	19	19	10	05	15	.	.	.	01	.	02	08	31
IV	7.5	6.8	6.6	6.9	-	-	-	-	-	-	-	322	056.8	27	.	01	15	.	.	.	.	.	03	13	20	17	11	12	16	03	05	.	02	.	04	06	30
V	6.6	7.9	5.5	6.7	-	-	-	-	-	-	-	223	051.1	22	.	.	03	.	.	.	.	.	.	07	16	16	06	16	02	02	.	.	03	.	06	04	09
VI	5.3	7.6	6.2	6.4	-	-	-	-	-	-	-	206	082.3	19	.	.	.	.	.	.	.	.	02	09	14	12	06	14	.	.	.	.	03	01	13	04	.
VII	4.9	5.5	4.6	5.0	-	-	-	-	-	-	-	172	043.1	01	.	.	.	01	.	.	.	.	03	05	09	07	05	09	.	.	.	.	01	.	06	04	.
VIII	6.6	6.9	5.5	6.3	-	-	-	-	-	-	-	169	046.9	31	.	.	.	01	.	.	.	.	.	08	15	13	06	15	.	.	.	.	.	.	10	06	.
IX	4.9	4.8	4.8	4.8	-	-	-	-	-	-	-	045	027.6	17	.	.	02	.	.	.	.	.	07	05	07	05	01	07	.	.	.	.	.	.	01	05	.
X	6.4	5.5	3.5	5.2	-	-	-	-	-	-	-	136	090.0	21	.	.	16	.	.	.	.	.	03	02	07	06	04	04	02	.	.	.	.	.	02	09	06
XI	7.5	6.8	6.7	7.0	-	-	-	-	-	-	-	327	092.6	15	.	.	20	.	.	.	.	.	04	17	10	09	06	10	03	.	.	04	.	.	02	08	03
XII	5.9	6.1	5.6	5.9	-	-	-	-	-	-	-	324	128.1	30	07	11	30	.	.	.	.	.	07	12	13	09	06	04	12	.	.	.	.	.	.	05	24
GOD.	6.7	6.8	6.0	6.5	-	-	-	-	-	-	-	2667	128.1	30 XII	13	50	159	02	.	.	.	.	31	128	154	136	69	110	66	07	05	01	14	01	48	89	162
RADOVLJICA																																					
BR. ST. 8																																					
H_o = 495 m H_b = - m h_o = 2,0 m h_z = 1,5 m																																					
I	9.2	8.6	8.7	8.9	-	04.1	91	93	90	91	63	109	032.8	06	03	12	26	.	.	.	.	.	.	24	15	12	04	08	07	.	.	.	.	.	.	07	18
II	6.5	5.1	5.8	5.8	-	03.5	73	75	76	75	06	097	040.5	15	06	05	27	.	.	.	.	.	04	11	12	08	03	03	10	01	.	.	.	.	02	05	-
III	6.9	6.5	6.8	6.8	-	04.0	74	74	78	75	28	150	043.0	05	02	.	23	.	.	.	.	.	04	17	16	10	06	08	11	02	.	01	.	.	.	05	-
IV	6.7	6.1	6.2	6.3	-	06.2	87	73	84	81	36	165	030.0	02	.	.	07	.	.	.	.	.	05	13	18	16	07	14	05	.	03	.	.	.	01	.	-
V	4.4	6.5	4.5	5.1	-	08.5	87	75	86	83	45	083	032.0	22	.	.	02	.	.	.	01	.	06	07	14	12	02	14	.	.	.	.	.	01	03	01	.
VI	3.5	5.7	4.6	4.6	-	11.8	87	61	87	78	15	086	030.0	19	.	.	.	14	01	.	.	.	07	07	14	08	03	13	.	.	.	.	.	.	03	.	.
VII	4.0	4.6	2.9	3.8	-	13.5	88	74	88	84	18	130	043.6	16	.	.	.	19	01	.	.	.	12	04	13	11	05	13	.	.	.	.	.	01	02	.	.
VIII	5.1	6.9	7.2	6.4	-	13.2	93	71	88	83	49	135	034.2	09	.	.	.	11	01	.	.	.	03	11	14	12	06	14	.	.	.	.	.	.	02	02	.
IX	4.8	4.5	6.4	5.2	-	10.5	94	65	90	83	49	036	018.5	17	.	.	.	03	.	.	.	.	07	09	08	05	01	08	.	.	.	.	.	.	.	01	.
X	6.3	3.5	2.2	4.0	-	07.0	90	68	85	81	47	107	071.4	21	.	.	11	.	.	.	.	.	10	04	07	06	03	07	01	01	.	.	.	.	.	03	.
XI	6.1	5.3	6.1	5.9	-	05.9	87	76	83	82	46	167	042.0	16	.	.	11	.	.	.	.	.	07	12	08	08	06	08	01	.	.	.	.	.	.	01	.
XII	6.6	6.5	7.1	6.7	-	03.4	75	79	79	78	41	116	037.5	30	05	12	29	.	.	.	.	.	05	17	08	06	05	03	06	.	.	.	.	.	.	08	05
GOD.	5.8	5.8	5.7	5.8	-	07.6	85	73	84	81	06	1381	071.4	24 X	16	29	136	47	03	.	01	.	70	136	147	114	51	113	41	04	03	01	.	02	13	33	-
JAVORJE NAD POLJANAMI																																					
BR. ST. 9																																					
H_o = 695 m H_b = - m h_o = 2,0 m h_z = 1,5 m																																					
I	9.6	9.6	9.0	9.4	-	04.1	94	90	93	92	34	158	044.5	06	.	15	23	.	.	.	.	.	.	27	17	14	05	10	10	01	.	.	01	.	.	07	18
II	7.2	7.1	5.6	6.6	-	03.5	84	71	78	78	18	094	034.0	15	01	06	25	.	.	.	04	02	03	08	15	11	03	05	11	01	.	.	.	.	01	02	22
III	7.7	8.4	6.7	7.6	-	04.2	84	75	82	81	23	240	045.6	04	.	02	22	.	.	.	04	.	02	16	19	19	11	05	15	.	.	.	.	.	.	08	31
IV	7.7	7.6	6.4	7.2	-	05.2	82	64	75	74	32	237	034.4	22	.	.	06	.	.	.	05	.	01	14	18	18	12	15	08	02	01	.	.	.	04	06	09
V	6.4	6.9	5.0	6.1	-	07.0	82	63	77	74	27	125	049.0	22	.	.	01	.	.	.	07	01	02	09	16	14	02	15	01	.	.	.	.	.	03	03	.
VI	5.0	6.6	5.4	5.7	-	11.1	84	69	79	77	45	110	035.9	19	.	.	.	03	.	.	05	01	05	08	19	11	05	18	01	.	.	.	.	.	13	03	.
VII	4.4	4.9	3.7	4.4	-	11.6	85	66	75	75	38	230	133.2	16	.	.	.	10	.	.	05	.	07	06	12	09	04	12	.	.	.	.	01	.	02	.	.
VIII	5.9	6.3	4.2	5.6	-	12.5	16	27	15	19	51	162	029.2	05	.	.	.	07	.	.	02	.	03	05	14	11	06	14	.	.	.	.	01	.	08	04	.
IX	5.0	5.0	4.7	4.9	-	10.2	88	70	85	81	54	046	018.1	27	.	.	.	.	.	.	03	01	07	04	10	04	02	10	.	.	.	.	.	.	02	02	.
X	6.0	5.0	3.3	4.8	-	06.9	86	67	81	78	39	089	055.9	21	.	.	03	.	.	.	06	01	06	03	09	05	02	09	01	.	.	.	.	.	03	05	01
XI	7.6	6.0	5.8	6.5	-	05.9	85	75	84	81	35	203	050.3	15	.	.	03	.	.	.	04	.	04	14	10	06	06	10	01	01	.	.	.	.	02	04	.
XII	6.3	6.4	5.2	5.9	-	03.8	87	80	83	83	52	106	030.3	30	01	09	23	.	.	.	03	02	07	10	11	08	04	06	08	01	.	.	.	.	.	06	11
GOD.	6.6	6.6	5.4	6.2	-	07.2	79	68	75	74	18	1800	133.2	16 VII	02	32	106	20	.	.	48	08	47	124	170	132	62	129	56	06	01	.	03	.	38	50	92
GOLNIK																																					
BR. ST. 10																																					
H_o = 500 m H_b = - m h_o = 2,0 m h_z = 1,5 m																																					
I	9.5	9.4	9.4	9.4	016.0	04.2	91	83	90	88	35	125	035.2	06	.	11	21	.	.	.	01	.	.	26	12	11	05	08	06	.	.	.	.	01	.	07	18
II	7.3	6.8	7.5	7.2	085.6	03.7	91	59	80	76	28	093	032.7	15	01	02	23	.	.	.	03	.	01	10	14	08	03	06	09	01	.	.	.	.	.	01	21
III	7.5	8.0	8.3	7.9	088.6	04.1	87	63	77	76	09	172	049.2	05	.	.	20	.	.	.	02	.	.	19	18	14	03	10	12	01	.	.	.	.	.	05	23
IV	7.5	7.9	8.4	7.9	103.5	05.2	82	53	66	67	28	170	026.0	02	.	.	03	.	.	.	04	.	.	18	17	15	08	15	05	03	.	.	.	.	01	03	02
V	6.3	7.9	7.8	7.3	168.3	06.8	80	50	70	66	20	135	054.6	22	.	.	02	.	.	.	04	.	.	12	15	14	04	15	.	.	.	.	.	.	02	02	.
VI	4.7	7.1	7.1	6.3	214.6	11.1	85	55	74	72	31	062	029.1	19	.	.	.	15	.	.	03	.	01	09	11	08	01	11	.	.	.	.	.	01	05	01	.
VII	5.1	5.9	6.0	5.7	250.3	11.5	86	56	72	71	30	216	069.1	16	.	.	.	16	02	.	05	01	03	07	12	11	08	12	.	.	.	.	.	.	03	01	.
VIII	6.3	6.8	7.3	6.8	191.3	13.1	93	66	85	81	50	209	056.5	09	.	.	.	13	03	.	01	.	02	12	13	11	07	13	.	.	.	.	.	01	03	03	.
IX	6.7	5.7	6.2	6.2	202.2	10.5	91	62	80	78	46	053	022.7	17	.	.	.	05	.	.	03	.	04	08	10	05	02	10	.	.	.	.	.	.	02	06	.
X	5.5	5.2	5.8	5.5	171.6	07.1	89	55	77	74	29	124	068.0	21	.	.	06	01	.	.	04	.	05	07	10	08	03	10	.	.	.	.	.	.	.	07	.
XI	7.5	6.5	7.1	7.0	091.2	05.8	82	58	78	73	31	123	037.2	16	.	.	04	.	.	.	02	.	02	14	09	08	04	08	.	.	.	.	.	.	01	04	.
XII	6.5	7.0	6.9	6.8	053.6	03.3	83	73	84	80	-	098	023.2	30	.	11	28	.	.	.	02	.	04	12	09	08	04	05	05	.	.	.	.	.	.	04	10
GOD.	6.7	7.0	7.3	7.0	1636.8	07.2	86	61	77	75	-	1580	069.1	16 VII	01	24	107	50	05	.	34	01	22	154	150	121	51	123	37	05	.	.	.	03	17	44	74

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dlen)	Max	Min	Max	Det.	Min	Det.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12): N δ.	N j.	NE δ.	NE j.	E δ.	E j.	SE δ.	SE j.	S δ.	S j.	SW δ.	SW j.	W	W j.	NW δ.	NW j.	C δ.
φ = 46° 13' N λ = 14° 29' E Gr. ΔG = + 58 min. URNIKI-LETALIŠTE BR. ST. 11																												
I	727.8	-02.1	00.2	-01.3	-01.1	01.4	-03.4	08.2	06	-13.8	08	05	01.0	03	01.0	04	01.5	15	01.3	07	01.3	08	01.2	18	01.2	10	01.3	23
II	725.2	-04.0	02.0	-02.0	-01.5	03.4	-06.1	10.9	06	-23.2	17	03	01.0	06	01.5	10	01.4	08	01.1	07	01.0	12	01.5	19	01.4	07	01.1	12
III	726.4	-01.8	04.5	00.5	00.9	05.7	-02.9	13.1	22	-11.6	08	03	01.0	06	01.2	03	01.0	08	01.4	06	01.2	09	01.1	28	01.4	09	01.7	21
IV	728.0	03.9	11.3	05.6	06.6	12.8	01.2	25.5	19	-07.2	04	05	01.8	05	01.2	12	01.7	11	01.4	01	03.0	09	02.0	26	01.5	08	02.5	13
V	729.4	08.3	16.2	09.1	10.7	17.7	04.0	22.4	10	-03.7	03	06	02.0	16	01.2	03	02.0	10	01.4	08	01.1	17	02.0	18	01.7	09	01.8	06
VI	730.7	14.6	22.6	15.7	17.2	24.3	10.0	29.2	22	01.6	03	03	01.3	09	01.4	08	01.8	06	01.8	08	01.5	19	01.7	20	01.2	05	01.4	12
VII	729.9	15.1	23.2	15.6	17.4	24.5	09.9	30.5	23	03.6	05	03	02.0	03	01.3	10	01.7	13	01.7	12	01.3	17	01.8	14	01.4	07	01.1	14
VIII	729.7	14.8	23.2	16.6	17.8	24.6	11.9	31.4	07	05.8	27	03	01.3	06	01.2	14	01.4	08	01.1	08	01.2	09	01.2	21	01.4	03	01.0	21
IX	733.1	10.4	20.3	12.4	13.9	21.3	07.8	27.6	11	-02.1	30	03	01.0	09	01.6	17	01.4	06	01.7	11	01.1	07	01.6	12	01.3	04	01.8	21
X	732.8	03.3	14.6	04.8	06.9	15.4	00.7	25.2	10	-05.5	17	01	01.0	02	02.0	11	01.8	03	02.0	04	01.2	15	01.7	13	01.5	11	01.7	33
XI	730.6	02.6	09.7	03.8	05.0	10.5	00.1	16.3	04	-06.0	27,17	05	01.2	01	02.0	07	01.4	05	01.0	.	.	10	01.8	21	01.4	13	01.8	28
XII	733.3	-04.2	00.4	-03.1	-02.5	01.0	-06.0	11.9	04	-15.4	25	06	01.0	03	01.3	09	01.0	04	01.0	04	01.0	05	01.2	17	01.2	08	01.0	37
GOD.	729.7	05.1	12.4	06.5	07.6	13.6	02.3	31.4	1. VIII	-23.2	17 II	46	01.3	69	01.3	108	01.5	97	01.4	76	01.2	137	01.6	227	01.4	94	01.6	241
φ = 46° 24' N λ = 14° 30' E Gr. ΔG = + 58 min. JEZERSKO BR. ST. 12																												
I	-	-03.1	00.7	-01.9	-01.5	02.2	-05.2	08.2	05	-15.8	08	.	.	11	02.4	04	02.0	05	05.4	.	.	14	03.9	01	03.0	.	.	58
II	-	-05.0	01.0	-02.7	-02.3	02.1	-07.3	08.1	23	-19.5	17	.	.	23	02.6	05	02.8	09	04.0	.	.	10	04.2	.	.	03	02.3	34
III	-	-03.9	02.6	-01.2	-01.0	03.7	-05.8	10.6	22	-15.6	08	.	.	29	02.8	04	05.0	12	04.2	.	.	05	03.2	.	.	01	02.0	42
IV	-	01.2	07.6	02.6	03.5	08.8	-00.5	19.4	23,19	-13.2	04	.	.	26	02.7	03	03.3	10	03.8	.	.	15	03.4	.	.	01	02.0	35
V	-	05.6	12.3	06.8	07.9	13.8	02.7	18.8	25	-04.3	01	.	.	15	02.7	01	03.0	07	03.0	.	.	12	03.1	.	.	04	02.8	54
VI	-	11.3	19.0	12.7	13.9	20.9	08.1	25.9	23	00.2	05	.	.	22	02.2	03	03.0	11	02.5	.	.	14	03.0	01	03.0	.	.	39
VII	-	11.3	19.8	13.5	14.6	21.4	08.4	28.4	24	03.6	19	.	.	18	03.0	02	03.0	21	03.4	.	.	06	03.7	.	.	06	02.5	40
VIII	-	11.3	19.8	13.4	14.4	21.3	09.4	28.6	06	04.4	27	.	.	06	02.2	01	02.0	09	02.7	.	.	13	02.4	02	02.0	01	02.0	61
IX	-	08.3	17.5	10.5	11.7	18.8	06.6	23.6	11	-01.5	30	.	.	20	02.2	01	03.0	05	04.8	.	.	12	03.6	02	02.0	05	01.8	45
X	-	02.3	11.2	03.7	05.2	12.9	00.3	23.9	10	-06.5	18	.	.	15	02.0	02	01.0	09	03.0	.	.	10	03.8	.	.	03	02.0	54
XI	-	01.4	06.9	02.3	03.2	08.3	-00.4	16.7	02	-07.5	17	.	.	11	02.0	01	02.0	18	04.3	.	.	07	04.0	.	.	.	.	53
XII	-	-04.8	-00.8	-04.6	-03.7	00.7	-07.3	07.5	30,01	-16.9	25,24	.	.	12	02.4	07	03.0	13	03.6	.	.	02	02.0	.	.	.	.	59
GOD.	-	03.0	09.8	04.6	05.5	11.2	00.8	28.6	6 VIII	-19.5	17 II	.	.	208	02.5	34	02.9	129	03.6	.	.	120	03.4	06	02.3	24	02.3	574
φ = 46° 04' N λ = 14° 31' E Gr. ΔG = + 58 min. LJUBLJANA-BEŽIGRAD BR. ST. 13																												
I		733.8	-00.6	01.0	00.0	00.1	02.0	-01.5	08.4	28	-06.4	08	07	01.0	19	01.0	12	01.5	19	01.3	02	02.0	06	01.3	04	01.2	04	01.0	20
II		731.2	-01.1	03.4	00.7	00.9	04.7	-02.6	12.0	06	-13.7	17	06	01.2	21	01.0	07	01.6	17	01.2	03	01.3	16	01.8	01	01.0	07	01.1	06
III		732.4	00.5	06.1	03.4	03.3	07.2	00.0	16.0	21	-06.7	08	06	01.2	22	01.3	03	01.7	13	01.3	04	01.8	23	01.9	03	01.3	11	01.3	08
IV		733.5	05.2	12.2	08.3	08.5	13.8	03.8	26.0	19	-03.6	04	08	01.1	20	01.2	03	02.7	09	01.4	07	01.6	17	02.6	03	01.0	14	01.4	09
V		735.4	09.0	17.2	12.0	12.6	18.6	07.0	23.0	10	-00.4	01	06	01.7	25	01.2	06	01.7	11	01.7	01	03.0	28	02.4	02	01.5	05	01.2	09
VI		736.5	15.7	23.7	18.5	19.1	25.1	13.4	30.4	23	06.1	03	07	01.0	16	01.6	10	01.4	10	01.2	08	01.4	25	02.4	02	01.5	03	01.0	09
VII		735.6	15.9	24.5	19.3	19.7	25.6	13.1	32.4	23	08.0	15	08	01.2	24	01.3	10	01.0	21	01.5	01	02.0	18	02.1	01	02.0	04	01.2	06
VIII		735.3	16.1	24.2	19.1	19.6	25.5	14.8	33.2	07	09.9	25	09	01.1	21	01.1	06	01.2	20	01.4	07	01.7	16	01.5	02	01.5	04	01.2	08
IX		738.8	12.1	21.4	15.2	16.0	22.3	11.0	29.0	11	02.2	30	02	01.0	27	01.3	09	01.6	10	01.4	11	01.4	13	01.8	04	02.2	05	01.6	09
X		738.7	05.8	15.3	08.9	09.7	16.3	04.8	26.9	10	-01.7	17	10	01.0	18	01.3	11	01.2	10	01.8	03	01.7	20	02.2	03	01.3	08	01.0	10
XI		736.5	04.7	10.5	07.0	07.3	11.4	03.1	18.0	02	-02.1	17	02	01.0	25	01.8	05	01.0	05	01.2	07	01.1	25	01.8	03	01.3	08	01.1	10
XII		739.3	-02.0	01.0	-00.8	-00.6	01.9	-02.9	13.3	04	-09.4	25	05	01.0	33	01.2	03	01.0	18	01.2	06	01.3	12	01.2	01	01.0	07	01.0	08
GOD.		735.6	06.8	13.4	09.3	09.7	14.5	05.3	33.2	1. VIII	-13.7	17 II	76	01.1	271	01.2	85	01.4	163	01.4	60	01.5	219	02.0	29	01.4	80	01.2	112
φ = 46° 07' N λ = 14° 51' E Gr. Δ G = + 59 min. KLENIK PRI VAČAH BR. ST. 14																												
I	-	-01.2	00.3	-00.4	-00.4	01.6	-02.3	09.5	06	-06.8	09	.	.	05	01.0	04	01.0	15	01.2	38	01.3	08	02.0	13	01.9	01	03.0	09
II	-	-01.4	02.7	00.7	00.7	04.0	-02.9	10.5	06	-14.8	17	02	02.5	.	.	03	01.3	06	01.7	28	01.1	17	01.8	21	03.0	05	03.6	02
III	-	00.7	05.2	02.5	02.7	06.2	-00.6	14.1	21	-06.0	08	01	01.0	.	.	05	01.2	04	01.2	22	01.5	17	02.2	36	01.7	06	01.5	02
IV	-	05.1	10.9	07.5	07.7	12.4	03.5	24.6	19	-04.3	04	01	01.0	05	01.4	07	01.6	15	01.8	09	01.4	27	02.0	25	02.2	01	02.0	.
V	-	09.1	15.1	10.7	11.4	16.8	06.5	21.5	14	-01.7	01	03	01.7	10	02.2	14	01.9	03	02.3	21	01.9	12	02.6	23	03.0	04	02.5	03
VI	-	15.4	21.6	17.2	17.9	23.0	12.8	28.3	23	05.2	03	16	01.8	05	02.2	17	01.7	07	02.0	10	02.5	09	01.9	15	02.2	10	02.8	01
VII	-	16.2	22.5	18.3	18.8	23.6	12.7	30.4	23	06.8	16	12	01.6	05	02.2	31	01.8	08	02.5	11	03.3	10	02.4	06	02.7	08	01.8	02
VIII	-	15.6	22.2	18.0	18.4	23.3	14.0	31.0	07	08.2	25	06	01.7	05	01.6	17	01.4	15	01.7	17	02.1	07	02.4	04	02.0	12	01.7	10
IX	-	11.7	19.9	14.8	15.3	20.7	10.6	26.8	11	-00.1	30	03	01.3	14	01.8	09	01.0	15	01.5	13	01.7	10	03.1	15	02.3	04	01.8	07
X	-	06.5	14.0	09.3	09.8	15.1	05.3	25.5	10	-02.4	19	11	01.7	13	01.4	02	01.5	08	01.2	07	02.6	17	02.0	23	03.0	08	02.2	04
XI	-	05.2	09.8	06.8	07.2	10.9	03.8	17.0	04	-03.2	27	11	01.5	02	01.5	06	01.3	10	01.5	09	02.0	22	02.0	17	02.6	07	02.6	06
XII	-	-02.2	01.3	-00.8	-00.6	02.1	-03.4	12.0	02	-10.2	21	05	01.6	03	01.3	02	03.0	05	03.2	06	01.5	26	01.5	30	01.5	04	01.5	12
GOD.	-	06.7	12.1	08.7	09.1	13.3	05.0	31.0	1. VIII	-14.8	17 II	71	01.7	67	01.7	117	01.6	111	01.7	191	01.7	182	02.1	228	02.3	70	02.2	58
φ = 46° 29' N λ = 15° 07' E Gr. Δ G = + 1h 00 min. ŠMARTNO PRI SLOVENJGRADCU BR. ST. 15																												
I	-	-03.1	-00.1	-02.3	-01.9	01.3	-04.5	10.3	05	-14.9	04	05	01.6	.	.	02	01.0	14	01.6	07	02.1	05	01.2	04	01.0	19	01.6	37
II	-	-04.6	02.6	-00.9	-01.0	03.7	-05.8	10.6	09	-19.5	17	04	02.2	02	01.5	03	01.0	22	01.7	10	01.9	01	02.0	01	02.0	17	02.4	24
III	-	-02.0	05.1	01.3	01.5	06.0	-02.8	13.6	22	-13.6	08	04	02.5	01	03.0	01	02.0	13	02.4	11	02.2	01	01.0	03	01.0	20	02.4	39
IV	-	03.7	10.4	05.4	06.2	11.9	01.8	24.0	19	-10.8	04	05	02.0	.	.	03	03.3	17	02.1	10	02.3	01	04.0	09	01.7	21	02.3	24
V	-	07.8	15.1	09.7	10.6	16.8	04.0	21.6	14	-03.5	01	07	02.0	02	03.0	02	02.0	17	02.1	17	02.6	02	01.0	02	02.0	12	02.3	32
VI	-	14.4	21.9	15.8	17.0	23.3	10.2	29.0	23	02.3	05	06	02.3	.	.	02	01.5	22	01.9	08	01.8	01	04.0	01	01.0	16	01.8	34
VII	-	14.5	22.0	16.2	17.2	23.5	10.5	29.5	24	04.1	06	07	02.7	.	.	01	02.0	21	01.7	16	02.4	.	.	01	01.0	17	01.9	30
VIII	-	14.4	22.4	16.2	17.3	23.5	12.4	30.8	06	07.4	27	03	01.3	.	.	03	02.7	20	01.6	11	02.2	02	02.0	01	02.0	20	02.3	33
IX	-	10.0	19.7	12.8	13.8	20.2	08.4	27.2	11	-01.6	30	01	01.0	.	.	01	01.0	26	01.9	08	02.1	02	02.0	03	01.3	08	02.4	41
X	-	03.6	13.4	04.9	06.7	14.1	01.6	24.1	10	-05.2	18	05	02.0	.	.	01	01.0	22	01.6	05	01.8	03	02.0	01	02.0	12	02.4	44
XI	-	01.8	09.8	03.1	04.4	10.5	-00.3	18.5	03	-05.7	29	02	02.0	01	02.0	01	01.0	12	02.4	12	02.1	.	.	.	.	15	02.0	47
XII	-	-03.8	00.0	-03.5	-02.7	00.8	-05.8	09.3	04	-17.0	25	06	01.7	.	.	01	01.0	07	01.3	02	01.5	01	01.0	03	01.3	30	01.9	43
GOD.	-	04.7	11.9	06.6	07.4	13.0	02.5	30.8	6 VIII	-19.5	17 II	55	02.0	06	02.3	21	01.8	213	01.9	117	02.2	19	01.8	29	01.5	207	02.1	428

Mesec	Oblačnost mm (0-10) 7	14	21	Srred. (Dnevi)	Temperatura Broj dani	Vlažnost vazduha e_m mm	U_m % 7	14	21	Srred. (Dnevi)	Vlažnost	Padavine R mm Σ	Max	Dat.	Broj dana na: TM ≤0,0	TX ≤0,0	TN ≤0,0	TX ≥25,0	TX ≥30,0	TN ≥20,0	F (0-12) ≥6	≥8	Nm (0-10) ≤2,0	≥8,0	R mm ≥0,1	≥1,0	≥10,0	●	▲	≡	▲	▲	▲	▲	▲	▲	▲	▲
BR. ST. 11																																						
I	9.5	9.5	8.8	9.2	010.5	04.1	96	89	94	93	86	104	025.9	06	02	13	26	.	.	.	.	.	.	26	17	14	04	10	09	.	.	.	.	.	.	18	20
II	8.1	7.0	5.9	7.0	081.3	03.8	94	76	90	87	47	075	022.0	15	04	04	27	.	.	.	.	.	01	08	16	11	03	08	12	03	01	.	.	.	03	13	22
III	7.9	8.3	7.4	7.9	078.5	04.3	95	71	92	86	31	172	049.0	04	01	.	25	.	.	.	01	.	.	17	19	17	03	12	15	06	.	.	.	.	01	16	29
IV	7.9	7.0	6.3	7.1	119.8	05.7	91	57	85	78	24	180	021.2	30	.	.	09	01	.	.	06	.	01	12	19	17	09	16	06	02	.	.	.	.	09	06	05
V	6.4	6.8	4.9	6.1	199.7	07.2	86	51	84	74	27	080	023.2	22	.	.	06	.	.	.	08	.	02	06	17	13	02	17	.	.	.	.	.	.	09	09	.
VI	5.5	6.2	5.7	5.8	219.6	11.5	88	58	87	77	37	068	026.3	19	.	.	.	17	.	.	02	.	03	07	14	08	03	14	.	.	.	.	.	01	16	09	.
VII	4.5	5.1	4.2	4.6	269.4	11.7	84	57	88	77	33	202	079.1	16	.	.	.	17	02	.	05	01	06	08	10	08	05	09	.	.	.	.	.	.	08	06	.
VIII	6.3	5.9	5.6	5.9	189.5	12.7	94	63	91	83	42	168	033.8	18	.	.	.	13	02	.	04	.	01	07	16	11	07	16	.	.	.	.	.	01	13	17	.
IX	6.9	5.0	4.8	5.5	187.4	10.2	96	60	93	83	43	042	013.9	14	.	.	01	05	.	.	01	.	04	06	09	04	02	07	.	.	.	.	.	.	06	16	.
X	6.5	4.9	2.4	4.6	158.7	06.5	96	58	92	82	26	074	037.6	21	.	.	17	01	.	.	04	.	05	04	08	05	01	07	01	.	.	.	.	01	04	11	01
XI	8.0	6.7	7.0	7.2	086.7	05.7	92	70	92	84	27	120	038.9	16	.	.	15	.	.	.	02	.	03	17	09	08	05	09	.	.	.	.	.	.	02	08	.
XII	7.9	7.4	7.0	7.4	050.9	03.6	94	87	93	91	29	086	020.0	01	07	15	29	.	.	.	01	.	03	17	17	08	04	07	12	03	.	.	.	.	01	20	10
GOD.	7.1	6.6	5.8	6.5	1652.0	07.2	92	66	90	82	24	1371	079.1	46 VII	14	32	155	54	04	.	34	01	29	135	171	124	48	132	55	14	01	.	.	03	72	149	87
BR. ST. 12																																						
I	7.3	6.8	8.7	7.6	-	03.7	91	78	89	86	31	219	127.9	06	06	11	22	.	.	.	02	01	01	16	15	12	05	08	09	.	.	.	.	.	.	06	17
II	6.3	6.6	6.2	6.4	-	03.0	86	62	78	75	32	107	037.1	06	07	09	27	.	.	.	03	01	03	07	20	12	03	05	16	.	.	.	.	.	.	01	23
III	7.0	7.7	7.3	7.3	-	03.6	89	68	87	81	27	158	030.5	05	09	03	25	.	.	.	04	.	01	14	18	15	06	05	14	01	.	.	.	.	.	03	31
IV	7.5	8.0	7.0	7.5	-	04.7	89	61	86	79	29	225	051.2	27	01	01	15	.	.	.	02	01	04	19	21	17	09	13	12	02	.	.	.	.	03	01	20
V	5.8	7.1	5.6	6.2	-	06.1	86	57	84	76	34	160	044.8	22	.	.	08	.	.	.	.	.	02	09	20	13	06	17	03	.	.	.	.	.	03	.	02
VI	4.8	6.4	5.9	5.7	-	09.8	91	64	89	81	39	087	030.6	19	.	.	.	04	.	.	.	.	03	07	14	10	02	14	.	.	.	.	.	.	10	.	.
VII	4.5	5.7	4.5	4.9	-	10.0	91	61	85	79	39	334	162.8	16	.	.	.	10	.	.	04	.	06	07	15	11	08	15	.	.	.	.	.	01	02	.	.
VIII	5.5	6.2	6.6	6.1	-	10.9	97	70	95	87	41	173	046.5	10	.	.	.	07	.	.	01	.	02	07	17	15	04	17	.	.	.	.	.	.	09	03	.
IX	5.0	5.1	5.4	5.2	-	08.9	95	64	93	84	42	073	032.4	17	.	.	02	.	.	.	01	.	03	04	07	06	03	07	.	.	.	.	.	.	03	04	.
X	4.9	4.4	3.6	4.3	-	06.0	95	67	94	85	30	207	161.7	21	.	.	17	.	.	.	01	.	07	02	10	06	03	08	03	.	.	.	.	.	03	04	-
XI	6.5	5.3	4.5	5.5	-	05.1	92	72	91	85	37	313	098.3	15	.	.	19	.	.	.	04	01	06	08	11	09	06	11	04	04	.	.	.	.	.	02	03
XII	5.2	5.2	4.0	4.8	-	03.2	89	78	91	86	37	134	051.9	30	08	12	30	.	.	.	01	.	11	08	13	08	04	05	11	.	.	.	.	.	.	02	24
GOD.	5.9	6.2	5.8	6.0	-	06.2	90	66	88	82	27	2190	162.8	46 VII	31	36	165	21	.	.	23	04	49	108	181	134	59	125	72	07	.	.	.	01	33	24	-
BR. ST. 13																																						
I	10.0	9.5	9.3	9.6	003.7	04.2	92	84	90	89	71	100	020.5	06	.	09	21	.	.	.	.	.	.	28	18	13	04	13	09	02	.	.	.	.	.	15	18
II	9.0	7.1	6.9	7.7	064.0	04.1	90	71	84	82	46	095	027.1	15	01	02	22	.	.	.	01	.	.	14	17	11	02	09	13	05	.	.	02	.	02	12	20
III	8.9	8.4	7.4	8.2	080.5	04.8	93	70	84	82	25	197	037.4	04	.	.	16	.	.	.	01	.	.	20	19	18	07	14	15	10	01	.	.	.	.	17	22
IV	8.1	7.0	6.0	7.0	135.5	05.9	88	56	72	72	26	239	033.8	03	.	.	04	01	.	.	03	.	.	11	20	19	08	18	06	04	.	.	.	.	06	04	07
V	5.6	6.7	4.7	5.7	218.5	07.4	85	49	73	69	29	091	023.4	22	.	.	01	.	.	.	04	.	03	04	17	13	02	17	01	01	.	.	.	.	10	10	.
VI	6.7	5.8	5.6	6.0	240.9	11.8	87	55	74	72	35	096	036.3	19	.	.	.	17	02	.	02	01	.	07	15	10	03	15	.	.	.	.	.	.	13	07	.
VII	5.0	5.1	3.6	4.6	287.0	12.0	86	52	72	70	32	126	037.1	01	.	.	.	18	05	.	02	.	08	05	09	08	04	09	.	.	.	.	.	.	05	10	.
VIII	8.0	5.8	4.8	6.2	186.1	13.3	93	60	83	79	38	133	027.0	09	.	.	.	16	05	.	01	.	01	08	17	10	05	17	.	.	.	.	.	.	09	14	.
IX	7.5	4.8	4.2	5.5	197.7	10.5	93	53	84	77	38	022	006.8	04	.	.	.	08	.	.	.	.	04	07	06	04	.	06	.	.	.	.	.	.	05	13	.
X	7.2	4.7	2.7	4.9	157.2	07.3	93	58	84	78	29	085	033.7	21	.	.	05	02	.	.	03	.	03	06	08	06	03	07	01	.	.	.	.	.	04	14	01
XI	8.0	6.8	7.2	7.3	074.5	06.4	91	71	85	82	30	103	032.0	16	.	.	08	.	.	.	02	.	01	16	11	08	04	11	.	.	.	.	.	.	01	10	.
XII	9.0	7.9	8.0	8.3	027.9	04.0	94	84	91	90	25	109	024.8	01	.	11	24	.	.	.	.	.	01	20	14	07	05	07	11	02	.	01	.	.	01	19	10
GOD.	7.8	6.6	5.9	6.8	1673.5	07.6	90	63	81	78	25	1396	037.4	4. III	01	22	101	62	12	.	19	01	21	148	171	127	47	143	56	24	01	01	02	.	56	145	78
BR. ST. 14																																						
I	9.7	9.5	9.2	9.5	-	04.3	95	91	93	93	80	083	023.1	06	.	15	21	.	.	.	01	.	.	26	17	13	02	10	08	.	.	.	.	.	.	14	16
II	8.8	7.3	8.4	8.1	-	03.9	89	71	80	80	37	082	020.2	11	01	03	23	.	.	.	.	.	01	17	17	14	02	05	13	.	.	.	.	.	02	05	21
III	8.4	7.5	7.7	7.9	-	04.6	91	71	84	82	22	133	023.2	28	.	.	19	.	.	.	01	.	03	20	19	15	04	07	15	02	.	.	.	.	.	06	20
IV	7.9	7.6	6.2	7.2	-	05.5	86	58	70	71	26	186	036.2	21	.	.	04	.	.	.	.	.	03	16	17	16	09	15	05	01	.	.	.	01	04	06	07
V	6.1	7.5	6.2	6.6	-	07.2	83	59	73	72	31	098	033.0	27	.	.	02	.	.	.	.	.	03	10	16	11	03	15	01	.	.	.	01	08	06	.
VI	5.6	6.2	6.1	6.0	-	11.2	83	62	74	73	35	130	032.1	19	.	.	.	11	.	.	01	.	04	09	16	11	06	16	.	.	.	.	.	.	11	03	.
VII	3.7	4.9	3.3	4.0	-	11.5	84	57	72	71	37	165	087.4	01	.	.	.	15	01	.	.	.	10	07	07	07	03	07	.	.	.	.	.	.	04	02	.
VIII	7.3	5.8	6.6	6.6	-	13.1	93	69	85	82	48	149	031.3	18	.	.	.	11	02	.	.	.	03	11	13	11	06	13	.	.	.	.	.	.	04	11	.
IX	7.0	4.0	5.0	5.4	-	10.2	90	61	80	77	37	039	018.3	04	.	.	01	06	.	.	01	.	06	05	08	05	01	08	.	.	.	.	.	.	01	12	.
X	6.5	4.5	3.8	4.9	-	07.1	89	61	78	76	36	073	035.2	21	.	.	05	01	.	.	.	.	06	06	07	06	02	07	01	.	.	.	.	.	02	10	01
XI	7.6	6.3	6.9	6.9	-	06.2	89	72	81	80	38	096	030.2	22	.	.	05	.	.	.	.	.	03	15	10	07	04	10	.	.	.	.	.	.	01	04	.
XII	8.6	7.1	7.7	7.8	-	04.0	93	81	89	88	29	093	020.7	08	01	12	25	.	.	.	.	.	01	19	13	09	05	05	10	01	.	.	.	.	.	15	10
GOD.	7.3	6.5	6.4	6.7	-	07.4	88	67	79	78	22	1327	087.4	4 VII	02	30	105	44	03	.	04	.	43	161	160	125	47	118	53	04	.	.	.	02	37	94	75
BR. ST. 15																																						
I	9.5	8.0	7.8	8.4	035.1	03.7	94	84	91	90	53	044	019.5	06	04	13	26	.	.	.	.	.	.	21	11	07	01	06	07	02	.	.	.	.	.	09	31
II	7.9	7.6	7.3	7.6	095.6	03.5	95	64	85	82	31	068	023.1	06	05	04	28	.	.	.	.	.	01	13	14	08	02	05	12	01	.	01	.	.	02	06	25
III	8.5	8.6	7.4	8.1	105.9	04.2	94	64	86	81	24	092	022.9	05	01	.	27	.	.	.	.	.	01	19	15	12	03	07	13	03	.	.	.	.	.	09	25
IV	8.4	8.2	6.7	7.8	129.9	05.6	92	58	84	78	20	146	024.1	03	01	.	08	.	.	.	.	.	.	17	21	16	03	19	08	06	.	.	.	.	06	02	06
V	5.7	7.4	5.6	6.3	208.3	06.9	87	53	77	72	29	070	025.1	22	.	.	05	.	.	.	.	.	.	09	14	10	02	14	03	02	.	.	.	02	11	06	01
VI	5.5	6.6	6.9	6.3	225.0	11.0	90	56	82	76	29	044	017.1	19	.	.	.	13	.	.	.	.	02	09	12	07	02	12	.	.	.	.	.	.	12	04	.
VII	4.4	5.9	4.1	4.8	259.1	11.3	89	57	83	76	39	198	078.3	16	.	.	.	14	.	.	.	.	03	04	10	08	05	10	.	.	.	.	.	.	05	06	.
VIII	7.7	6.2	6.0	6.6	193.9	12.5	96	63	93	84	40	146	035.4	09	.	.	.	12	02	.	01	.	.	09	16	10	05	16	.	.	.	.	.	01	14	12	.
IX	7.7	5.2	5.0	6.0	198.2	09.7	95	57	90	81	40	024	011.1	27	.	.	02	04	.	.	.	.	05	10	10	04	01	10	.	.	.	.	.	.	04	14	.
X	8.2	5.1	2.8	5.4	153.1	06.5	96	61	94	84	36	110	069.3	21	.	.	13	.	.	.	01	.	04	06	11	05	03	11	02	02	.	.	.	.	02	16	02
XI	7.8	6.2	5.8	6.6	107.5	05.3	93	62	92	82	34	062	024.8	22	.	.	17	.	.	.	.	.	02	12	10	05	02	10	.	.	.	.	.	.	.	11	.
XII	9.0	5.7	7.7	7.5	062.3	03.5	92	79	93	88	21	035	011.0	28	05	16	29	.	.	.	.	.	02	14	10	08	01	03	08	01	.	.	.	.	.	10	11
GOD.	7.5	6.7	6.1	6.8	1773.9	07.0	92	63	87	81	20	1039	078.3	46 VIII	16	33	155	43	02	.	02	.	20	143	154	108	30	123	53	17	.	01	.	03	56	105	101

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Pm 7	Pm 14	Pm 21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12): N		NE		E		SE		S		SW		W		NW		C
												n.	j.	n.	j.	n.	j.	n.	j.	n.	j.	n.	j.		j.	n.	j.	n.
RADEČE φ = 46° 04' N λ = 15° 11' E Gr. Δ G = + 1h 01 min. BR. ST. 16																												
I	-	-00.8	01.6	-00.1	00.1	02.8	-02.8	09.0	28	-10.3	03	09	03.0	01	02.0	05	02.2	04	02.5	05	02.2	01	02.0	06	02.2	01	02.0	61
II	-	-01.0	04.5	00.9	01.3	05.7	-03.2	12.7	06	-14.2	17	06	03.2	03	04.0	09	02.3	05	02.4	04	02.2	02	04.0	13	03.2	02	06.0	40
III	-	-01.5	07.5	03.6	04.1	08.3	-00.3	16.3	24,21	-07.4	02	08	03.1	03	03.3	08	02.6	04	02.0	03	02.3	04	03.2	19	03.1	06	06.0	38
IV	-	06.0	13.0	07.8	08.6	14.4	04.1	26.6	19	-02.7	04	13	03.8	01	04.0	10	02.7	03	02.7	01	04.0	03	03.7	13	03.2	02	04.0	44
V	-	09.4	17.4	11.1	12.3	18.8	06.4	23.5	14	00.2	04	10	02.6	02	04.5	09	02.3	03	02.3	05	02.2	03	02.7	18	03.1	01	06.0	42
VI	-	16.2	23.7	17.6	18.8	25.0	13.4	30.3	23	05.0	03	10	03.0	01	03.0	13	03.0	05	02.4	05	02.4	.	.	13	03.6	01	02.0	42
VII	-	15.8	24.5	17.6	18.9	25.6	12.7	31.3	23	07.5	19	01	02.0	02	02.0	14	02.9	02	02.5	08	02.5	02	02.0	10	02.5	02	04.5	52
VIII	-	16.5	24.1	18.1	19.2	25.2	14.7	32.8	07	09.5	27	08	03.0	04	02.8	11	02.5	03	02.7	08	03.1	01	04.0	06	02.5	.	.	52
IX	-	12.0	21.7	14.0	15.4	22.2	10.4	29.6	11	01.0	29	01	02.0	02	03.5	13	02.9	04	03.2	04	02.5	05	04.0	14	03.1	.	.	47
X	-	06.2	15.9	08.2	09.6	16.5	04.2	26.5	10	-01.4	17	07	02.7	02	03.5	11	02.8	01	05.0	05	02.2	01	05.0	10	02.8	03	06.7	53
XI	-	05.6	12.4	07.3	08.1	13.3	03.2	19.7	04	-02.1	24,17	06	03.5	03	04.0	08	02.9	01	02.0	12	02.3	04	04.0	11	04.2	03	04.3	42
XII	-	-01.2	03.1	-00.4	00.3	03.9	-03.2	12.5	04	-11.4	25	11	04.5	01	04.0	04	03.2	04	04.2	09	02.6	01	06.0	10	02.7	02	05.0	51
GOD.	-	07.2	14.1	08.8	09.7	15.1	05.0	32.8	7. VIII	-14.2	17. II	90	03.3	25	03.4	115	02.7	39	02.7	69	02.5	27	03.6	143	03.1	23	05.1	564
RADLJE OB DRAVI φ = 46° 37' N λ = 15° 13' E Gr. Δ G = + 1h 01 min. BR. ST. 17																												
I	-	-02.7	01.0	-01.6	-01.2	01.9	-04.8	08.8	05	-13.8	04	.	.	07	01.1	.	.	10	01.0	.	.	14	01.1	.	.	43	01.0	19
II	-	-02.4	04.0	00.1	00.4	04.9	-04.5	11.1	09	-16.6	17	.	.	05	02.2	.	.	10	01.0	.	.	26	01.6	.	.	29	01.2	14
III	-	-00.3	06.6	02.1	02.6	07.4	-01.8	16.9	24	-06.4	01	.	.	03	01.3	.	.	15	01.3	.	.	24	01.3	.	.	32	01.1	19
IV	-	04.4	12.0	06.6	07.4	13.4	02.0	25.1	19	-05.9	04	.	.	07	01.1	.	.	19	01.1	.	.	24	01.4	.	.	28	01.3	12
V	-	08.1	17.0	10.4	11.5	18.2	04.9	23.6	15	-02.1	04	.	.	02	01.5	.	.	19	01.3	.	.	19	01.4	.	.	30	01.2	23
VI	-	14.5	22.9	16.4	17.5	24.6	10.9	31.1	24	04.1	05	.	.	04	01.0	.	.	14	01.1	.	.	22	01.1	.	.	25	01.0	25
VII	-	14.6	23.2	16.9	17.9	24.8	11.7	31.3	24,23	04.9	16	.	.	03	01.0	.	.	07	01.1	.	.	20	01.2	.	.	27	01.3	36
VIII	-	15.0	23.6	17.1	18.2	24.6	13.4	32.5	06	07.1	26	.	.	02	01.0	.	.	05	01.0	.	.	16	01.1	.	.	34	01.1	36
IX	-	11.5	20.8	13.3	14.7	21.6	09.8	28.9	11	01.7	29	.	.	.	.	.	.	04	01.2	.	.	23	01.3	.	.	28	01.1	35
X	-	05.2	14.5	06.6	08.2	15.3	03.6	25.3	10	-02.6	16	.	.	04	01.0	.	.	06	01.5	.	.	20	01.4	.	.	40	01.4	23
XI	-	03.3	11.2	05.1	06.2	11.9	01.6	19.2	03	-03.4	29	.	.	04	02.0	.	.	10	01.0	.	.	22	01.5	.	.	34	01.3	20
XII	-	-03.2	01.4	-02.5	-01.7	02.1	-05.0	11.4	04	-14.8	25	.	.	02	02.5	.	.	23	01.0	.	.	21	01.0	.	.	20	01.2	27
GOD.	-	05.7	13.2	07.5	08.5	14.2	03.5	32.5	6. VIII	-16.6	17. II	.	.	43	01.4	.	.	142	01.1	.	.	251	01.3	.	.	370	01.2	289
CELJE-LEVEC φ = 46° 15' N λ = 15° 14' E Gr. Δ G = + 1h 01 min. BR. ST. 18																												
I	-	-02.3	00.5	-01.2	-01.1	01.8	-04.3	09.2	17	-14.0	03	.	.	19	01.4	01	01.0	10	01.1	.	.	03	01.0	.	.	01	01.0	59
II	-	-02.6	03.5	-00.3	00.1	04.7	-05.1	11.5	06	-20.4	17	.	.	11	01.2	01	01.0	06	01.3	.	.	17	01.8	02	01.0	06	01.3	41
III	-	00.2	06.3	02.2	02.7	07.2	-01.5	15.6	22	-13.4	08	.	.	09	01.2	.	.	08	01.0	.	.	21	01.6	.	.	05	01.2	50
IV	-	05.1	12.2	07.4	08.0	13.9	02.7	26.2	19	-05.1	04	.	.	07	01.6	.	.	03	01.0	.	.	28	01.5	.	.	14	01.4	38
V	-	09.4	16.8	10.9	12.0	18.5	04.7	23.0	14	-03.2	01	.	.	12	01.2	.	.	13	01.0	.	.	26	02.0	02	01.0	09	01.4	31
VI	-	16.2	23.6	17.2	18.5	25.1	11.0	30.6	23	02.6	03	01	01.0	13	01.3	.	.	16	01.5	.	.	25	01.4	.	.	12	01.1	23
VII	-	15.7	23.9	17.3	18.5	25.2	10.8	31.6	24	05.3	07,06	.	.	16	01.2	.	.	11	01.1	.	.	28	01.5	.	.	15	01.3	23
VIII	-	16.1	24.2	17.3	18.7	25.1	12.7	32.6	06	07.1	27	.	.	14	01.2	.	.	12	01.2	.	.	25	01.1	01	01.0	09	01.1	32
IX	-	11.0	20.8	13.5	14.7	21.4	08.7	28.2	11	-00.8	30	.	.	13	01.1	.	.	17	01.2	.	.	16	01.8	.	.	07	01.0	37
X	-	05.1	15.0	06.7	08.4	15.8	02.7	25.1	10	-04.9	19	02	01.0	10	01.1	.	.	09	01.2	.	.	25	01.7	02	01.0	08	01.4	37
XI	-	04.0	11.6	05.3	06.6	12.4	01.7	19.9	03	-05.6	07	01	01.0	07	01.0	01	01.0	07	01.1	.	.	26	01.7	01	01.0	13	01.1	34
XII	-	-03.4	02.1	-02.2	-01.4	03.2	-06.1	12.3	01	-17.1	25	.	.	06	01.2	.	.	06	01.5	01	01.0	18	01.2	01	01.0	11	01.1	50
GOD.	-	06.2	13.4	07.8	08.8	14.5	03.2	32.6	6. VIII	-20.4	17. II	04	01.0	137	01.2	03	01.0	118	01.2	01	01.0	258	01.6	09	01.0	110	01.2	455
SELA PRI PLANINI NAD SEVNICO φ = 46° 06' N λ = 15° 24' E Gr. Δ G = + 1h 02 min. BR. ST. 19																												
I	-	-01.5	00.5	-01.1	-00.8	01.7	-03.5	09.2	05	-09.1	08	.	.	.	.	40	02.9	11	03.3	.	.	18	04.1	04	03.8	.	.	20
II	-	-01.7	02.1	-00.1	00.0	03.5	-03.2	10.1	06	-11.4	17	03	02.7	.	.	28	03.0	03	03.0	.	.	04	03.2	24	04.0	03	03.7	19
III	-	00.5	04.3	02.0	02.2	05.2	-00.7	13.8	25	-06.5	01	.	.	.	.	26	02.8	05	02.6	.	.	01	04.0	34	03.6	01	02.0	26
IV	-	05.1	10.1	06.8	07.2	11.9	03.3	23.4	19	-05.7	04	.	.	01	02.0	25	02.9	06	02.5	03	02.7	09	03.3	28	03.4	01	03.0	17
V	-	09.7	14.2	10.0	11.0	16.3	06.7	20.9	10	00.4	01	.	.	01	02.0	33	02.7	03	02.7	.	.	08	03.6	23	03.5	06	03.0	19
VI	-	16.2	20.9	16.4	17.5	22.4	12.8	27.5	23	05.3	03	01	03.0	01	02.0	26	03.2	04	02.2	01	04.0	01	04.0	31	03.0	03	02.7	22
VII	-	16.4	21.4	16.9	17.9	22.9	12.7	28.6	23	05.9	16	01	02.0	01	02.0	39	02.7	01	02.0	02	03.0	02	03.5	22	03.0	04	02.8	21
VIII	-	16.3	21.6	17.0	17.9	22.5	13.7	30.2	07	09.4	25	01	02.0	.	.	33	02.4	08	02.5	.	.	09	03.1	06	02.5	.	.	36
IX	-	12.2	18.6	13.8	14.6	19.4	10.2	26.2	11	01.8	29	01	02.0	01	03.0	41	02.6	06	02.8	01	01.0	05	03.6	14	03.1	03	03.3	18
X	-	06.9	13.1	08.1	09.1	13.8	04.8	23.5	10	-02.7	17	01	02.0	.	.	39	02.7	03	03.3	.	.	07	04.0	23	03.4	.	.	20
XI	-	05.6	09.9	06.5	07.1	10.9	03.5	17.6	04,02	-01.2	29	01	03.0	.	.	27	02.5	04	03.2	.	.	22	03.6	14	03.9	02	03.0	20
XII	-	-01.6	01.4	-01.0	-00.5	02.6	-03.5	11.5	01	-08.6	25	01	03.0	.	.	42	02.8	05	02.6	.	.	02	03.5	17	03.5	.	.	26
GOD.	-	07.0	11.5	07.9	08.6	12.8	04.7	30.2	7. II	-11.4	17. II	10	02.5	05	02.2	399	02.8	59	02.8	07	02.7	88	03.6	240	03.4	23	03.0	264
MARIBOR-TEZNO φ = 46° 32' N λ = 15° 39' E Gr. Δ G = + 1h 03 min. BR. ST. 20																												
I	735.7	-02.6	00.4	-01.5	-01.3	01.6	-04.0	09.7	15	-14.3	03	03	01.0	03	01.3	01	01.0	19	02.1	05	02.6	01	01.0	01	02.0	03	01.7	57
II	732.7	-02.0	04.1	00.4	00.7	05.2	-03.4	14.7	09	-12.2	17	09	02.0	04	01.2	01	02.0	14	02.1	10	02.4	03	02.7	02	01.0	06	02.5	35
III	734.1	00.5	06.5	02.9	03.2	07.5	-00.7	17.7	24	-09.1	08	01	01.0	06	02.3	02	01.0	05	02.6	10	02.3	05	03.2	03	01.3	27	01.9	34
IV	735.5	06.2	12.5	08.1	08.7	13.8	04.1	25.6	19	-02.4	04	03	03.3	02	02.5	01	01.0	07	02.9	09	04.0	09	02.2	13	02.0	23	02.2	23
V	737.0	10.7	17.1	11.9	12.9	18.5	07.2	23.9	15	-00.7	01	06	03.5	07	02.0	.	.	06	02.2	10	03.5	04	04.0	04	02.2	27	02.0	29
VI	738.2	17.2	22.9	17.7	18.9	24.6	13.6	30.3	23	06.4	05	04	02.0	08	01.4	04	01.8	11	02.0	06	02.7	02	02.5	11	02.2	16	01.8	28
VII	737.5	17.0	23.3	18.4	19.3	24.7	13.5	30.4	14	08.5	16	08	02.6	01	01.0	04	01.8	10	02.5	12	03.1	01	03.0	02	02.0	20	02.5	35
VIII	737.2	16.6	23.3	17.9	18.9	24.5	14.6	32.1	06	10.2	26	01	03.0	02	01.0	03	01.3	11	02.3	04	02.0	.	.	01	03.0	21	02.3	50
IX	740.7	11.9	20.1	13.8	14.9	21.0	10.2	29.7	11	00.4	30	03	02.3	04	01.8	01	01.0	11	02.2	10	03.1	03	01.7	04	01.5	12	01.8	42
X	740.2	06.1	15.0	07.4	09.0	15.7	03.7	24.7	09	-02.9	19	03	02.0	01	02.0	04	01.2	11	01.8	05	04.0	02	01.0	02	02.5	14	01.5	51
XI	737.7	04.6	11.5	05.8	06.9	12.6	02.3	21.2	03	-03.4	27	04	02.0	.	.	.	.	06	01.8	19	02.9	01	02.0	06	02.2	08	03.0	46
XII	741.2	-02.3	02.4	-01.0	-00.5	03.2	-03.8	13.0	02	-09.7	27	02	02.5	01	01.0	.	.	02	01.0	04	03.0	.	.	05	01.6	14	01.4	65
GOD.	737.3	07.0	13.3	08.5	09.3	14.4	04.8	32.1	6. VIII	-14.3	3. I	47	02.4	39	01.7	21	01.4	113	02.2	104	03.0	31	02.5	54	02.0	191	02.0	495

Mesec	Oblačnost N m (0-10) 7	14	21	Povpr. (Dim)	Insolacija trajanje sonč.	Vlažnost zraku e m mm	U m % 7	14	21	Povpr. (Dim)	Min	Padavine R mm Σ	Max	Dan	Broj dana z: Tn ≤ -10,0	Tn ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 10,0	Tx ≥ 20,0	F (0-12) ≥ 6	F (0-12) ≥ 8	Nm (0-10) < 2.0	> 8.0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	⌂	≈	▲	▲	T	■	■
BR. ST. 16																																				
RADEČE																																				
H_a = 230 m H_b = - m h_v = 2.0 m h_r = 1.5 m																																				
I	9.9	8.9	8.9	9.2	-	04.1	91	83	89	88	55	057	018.5	07	01	08	25	.	.	.	01	.	.	24	14	10	02	09	06	.	.	01	.	.	.	11	18
II	7.8	7.4	7.1	7.4	-	04.2	87	69	85	80	37	075	032.9	11	02	01	21	.	.	.	07	.	01	16	12	11	02	03	10	.	01	.	.	.	01	05	13
III	8.2	7.5	5.9	7.2	-	04.8	88	63	81	78	17	138	027.2	05	.	.	16	.	.	.	04	01	04	17	17	14	05	12	09	.	.	.	.	.	.	09	05
IV	7.2	7.3	5.5	6.6	-	06.0	85	54	77	72	22	172	031.3	03	.	.	02	01	.	.	07	.	02	13	20	15	08	18	04	01	.	.	.	.	01	02	01
V	4.9	6.4	4.8	5.4	-	07.6	84	49	81	71	29	101	033.3	22	.	.	.	.	.	.	03	01	06	08	14	10	03	14	.	.	.	.	.	.	07	02	.
VI	4.1	5.3	4.5	4.6	-	12.0	84	56	79	73	34	105	036.5	30	.	.	.	16	02	.	01	.	08	06	10	05	04	10	.	.	.	.	.	.	08	.	.
VII	4.1	4.6	2.6	3.8	-	12.2	87	53	82	74	33	142	040.3	14	.	.	.	20	05	.	02	01	11	04	08	08	06	08	.	.	.	.	.	.	02	.	.
VIII	6.8	6.5	5.2	6.2	-	13.4	89	63	87	80	45	148	030.3	10	.	.	.	16	03	.	.	.	01	10	12	09	07	12	.	.	.	.	.	.	08	07	.
IX	6.4	4.4	4.0	4.9	-	10.5	89	56	88	78	36	021	014.8	27	.	.	.	09	.	.	04	.	09	07	06	03	01	06	.	.	.	.	.	.	.	07	.
X	6.7	4.6	3.3	4.9	-	07.5	91	59	88	80	32	099	054.2	21	.	.	06	02	.	.	04	01	06	03	09	06	03	09	.	.	.	.	.	.	03	09	.
XI	7.5	5.4	6.1	6.3	-	06.6	87	66	84	79	40	085	028.2	22	.	.	06	.	.	.	06	.	03	11	08	08	03	08	.	.	.	.	.	.	01	06	.
XII	8.4	6.1	7.6	7.4	-	04.0	86	75	84	82	30	066	011.5	28	04	06	26	.	.	.	05	02	05	18	14	09	02	08	06	.	.	01	.	.	.	12	10
GOD.	6.8	6.2	5.5	6.2	-	07.7	87	62	83	77	17	1209	054.2	21 X	07	15	102	64	10	.	44	06	56	137	144	108	46	117	35	01	01	02	.	.	31	70	47
BR. ST. 17																																				
RADLJE OB DRAVI																																				
H_a = 365 m H_b = - m h_v = 2.0 m h_r = 1.5 m																																				
I	9.4	7.4	8.2	8.3	-	03.8	92	81	88	87	62	036	014.5	06	04	10	30	.	.	.	.	.	.	21	09	06	01	04	07	02	.	.	.	.	.	07	-
II	8.3	6.1	6.6	7.0	-	03.8	90	65	83	79	42	069	019.8	06	01	03	27	.	.	.	01	.	01	11	14	10	03	04	12	01	.	.	.	.	.	10	16
III	9.0	6.6	7.5	7.7	-	04.5	92	64	85	80	30	126	031.1	05	.	.	24	.	.	.	01	.	02	15	15	12	04	08	12	04	.	.	.	.	.	15	18
IV	8.4	7.2	5.6	7.1	-	06.1	92	59	83	78	28	138	027.0	03	.	.	09	01	.	.	02	.	01	13	20	15	05	17	06	02	.	.	.	.	02	04	04
V	7.3	6.7	5.1	6.4	-	07.9	90	58	83	77	34	091	032.2	22	.	.	04	.	.	.	.	.	.	07	13	07	03	13	.	.	.	.	.	01	05	06	.
VI	6.0	6.0	5.1	5.7	-	11.6	90	58	85	78	31	093	016.1	11	.	.	.	15	05	.	02	.	03	06	16	13	09	16	.	.	.	.	.	01	10	08	.
VII	7.4	5.8	4.8	6.0	-	12.2	90	60	84	78	34	263	087.2	16	.	.	.	16	03	.	03	.	01	05	12	10	07	12	.	.	.	.	.	.	06	11	.
VIII	9.3	5.3	6.4	7.0	-	13.2	95	64	90	83	38	210	074.1	10	.	.	.	13	02	.	01	.	.	11	14	12	07	14	.	.	.	.	.	.	11	16	.
IX	8.5	4.6	4.5	5.9	-	11.1	96	63	92	83	44	037	010.6	02	.	.	.	07	.	.	.	.	01	07	10	06	01	10	.	.	.	.	.	.	03	16	.
X	8.9	4.9	3.9	5.9	-	07.5	98	66	93	86	39	099	059.1	21	.	.	07	01	.	.	01	.	02	08	08	07	03	08	01	01	.	.	.	.	01	20	01
XI	8.3	4.6	5.7	6.2	-	06.2	94	68	92	84	42	058	026.8	22	.	.	11	.	.	.	01	.	02	06	07	07	02	07	.	.	.	.	.	.	.	16	.
XII	8.8	5.2	6.8	6.9	-	03.8	93	85	90	89	57	037	013.5	28	04	12	27	.	.	.	01	.	01	10	08	07	01	01	07	.	.	.	.	.	.	14	11
GOD.	8.3	5.9	5.8	6.7	-	07.6	92	65	87	81	28	1257	087.2	46 VII	09	25	139	53	10	.	13	.	14	120	146	112	42	114	45	10	.	.	.	02	38	143	-
BR. ST. 18																																				
CELJE-LEVIČ																																				
H_a = 244 m H_b = - m h_v = 2.0 m h_r = 1.5 m																																				
I	9.4	8.8	8.9	9.1	009.4	04.0	94	88	93	92	71	043	010.0	06	05	13	24	.	.	.	.	.	.	25	13	08	01	06	08	.	.	.	.	.	.	14	21
II	7.5	7.0	7.4	7.3	070.2	04.1	91	76	91	86	54	073	026.1	11	07	02	26	.	.	.	.	.	01	10	13	08	03	06	10	01	01	.	.	.	.	12	19
III	7.8	8.2	7.6	7.9	084.8	04.9	95	69	91	85	33	132	026.0	05	01	.	25	.	.	.	.	.	.	18	14	14	05	12	09	02	.	.	.	.	.	09	17
IV	8.1	7.8	6.7	7.5	124.5	06.6	92	60	87	80	19	158	028.0	21	.	.	09	01	.	.	.	.	.	15	21	14	05	19	04	02	01	.	.	.	03	01	04
V	5.9	6.7	6.2	6.3	206.2	08.2	88	59	86	77	40	075	021.4	22	.	.	05	.	.	.	.	.	02	07	17	11	03	17	.	.	.	.	.	02	10	02	.
VI	5.4	6.5	6.1	6.0	227.0	12.7	89	59	88	79	28	077	023.3	19	.	.	.	17	04	.	.	.	01	06	14	07	03	14	.	.	.	.	.	01	08	.	.
VII	4.2	5.7	4.5	4.8	242.6	12.9	89	60	88	79	40	130	050.3	01	.	.	.	17	05	.	.	01	03	04	08	07	03	08	.	.	.	.	.	.	03	04	.
VIII	6.8	6.4	6.4	6.5	193.4	13.6	92	65	92	83	41	144	030.9	10	.	.	.	15	03	.	.	.	02	08	12	11	06	12	.	.	.	.	.	01	12	13	.
IX	6.6	4.9	6.1	5.9	186.5	10.7	95	61	94	83	43	049	018.3	05	.	.	01	06	.	.	.	01	03	06	09	07	02	09	.	.	.	.	.	01	05	16	.
X	6.8	5.5	3.9	5.4	145.5	07.1	93	59	90	81	35	077	039.3	21	.	.	11	02	.	.	.	.	02	05	06	06	03	06	01	.	.	.	.	.	02	08	.
XI	7.4	6.0	5.9	6.4	077.3	06.2	90	66	90	82	32	069	025.8	22	.	.	13	.	.	.	.	.	01	10	08	07	03	08	.	.	.	.	.	.	01	06	.
XII	7.5	6.2	7.1	6.9	037.7	03.8	92	77	92	87	12	062	015.7	28	06	09	30	.	.	.	.	.	04	14	12	09	01	06	07	.	.	.	01	.	.	14	10
GOD.	7.0	6.6	6.4	6.7	1605.1	07.9	91	66	90	82	12	1089	050.3	4 VII	19	24	144	58	12	.	.	02	19	128	147	109	38	123	39	05	02	.	01	05	44	99	71
BR. ST. 19																																				
SELA PRI PLANINI NAD SEVNICO																																				
H_a = 550 m H_b = - m h_v = 2.0 m h_r = 1.5 m																																				
I	9.3	8.8	8.8	9.0	-	04.2	96	90	95	94	64	063	011.6	06	.	16	23	.	.	.	.	.	.	25	16	09	01	09	08	.	.	01	.	.	.	09	28
II	8.1	7.7	7.7	7.8	-	04.0	88	77	86	84	50	086	034.5	11	02	08	23	.	.	.	02	.	.	16	17	12	03	04	14	.	01	01	.	.	.	01	23
III	8.0	9.0	7.2	8.1	-	04.4	87	72	85	82	30	154	034.5	05	.	01	23	.	.	.	.	.	01	20	17	15	06	06	13	.	.	01	.	.	.	05	26
IV	8.6	8.1	7.2	7.9	-	05.9	84	66	77	76	36	177	028.8	03	.	.	06	.	.	.	.	.	.	17	17	16	09	14	06	.	.	.	01	.	01	04	08
V	5.8	7.6	5.9	6.4	-	07.4	77	65	80	74	42	078	029.8	22	.	.	.	.	.	.	.	.	01	12	14	10	02	15	01	.	.	.	01	.	09	02	.
VI	5.3	6.7	6.0	6.0	-	11.8	81	68	81	77	46	132	042.0	19	.	.	.	08	.	.	.	.	03	08	12	06	03	12	.	.	.	.	.	.	08	03	.
VII	4.6	6.0	4.9	5.2	-	12.2	82	67	80	77	52	154	045.6	16	.	.	.	16	.	.	01	.	03	04	08	07	05	08	.	.	.	.	.	.	01	.	.
VIII	5.9	7.0	6.3	6.4	-	13.3	90	75	89	85	57	208	064.1	10	.	.	.	09	01	.	.	.	01	11	14	09	06	.	.	.	.	.	.	.	08	03	.
IX	6.0	5.5	4.6	5.4	-	10.4	87	69	84	80	54	055	015.5	27	.	.	.	04	.	.	.	.	04	06	10	08	02	09	01	.	.	.	.	.	02	.	.
X	6.5	5.8	4.5	5.6	-	07.5	88	70	86	81	53	091	052.1	21	.	.	07	.	.	.	.	.	04	05	08	06	03	07	02	.	01	.	.	.	02	04	04
XI	8.3	6.7	6.9	7.3	-	06.1	83	70	82	78	51	084	031.3	22	.	.	06	.	.	.	03	.	.	15	08	07	03	08	.	.	.	.	.	.	.	04	.
XII	7.3	6.4	6.7	6.8	-	03.8	88	80	86	85	47	063	015.8	28	.	08	25	.	.	.	01	.	05	15	11	08	02	06	08	.	.	.	01	.	.	06	11
GOD.	7.0	7.1	6.4	6.8	-	07.6	85	72	84	81	30	1345	064.1	40 VIII	02	33	113	37	01	.	07	.	22	154	154	113	45	98	53	.	02	03	03	.	31	41	100
BR. ST. 20																																				
MARIBOR-TEZNO																																				
H_a = 275 m H_b = 276.8 m h_v = 2.0 m h_r = 1.4 m																																				
I	8.9	8.2	9.1	8.7	026.7	03.8	91	83	89	88	63	043	017.9	06	03	15	26	.	.	.	02	.	01	23	12	07	01	07	08	02	.	.	.	.	.	10	20
II	7.3	7.1	7.8	7.4	072.1	03.7	87	62	82	77	24	047	013.4	15	02	03	23	.	.	.	04	01	01	15	15	08	01	06	12	02	.	.	.	.	.	05	15
III	7.7	8.0	6.8	7.5	090.0	04.5	88	63	81	77	19	122	024.1	05	.	.	18	.	.	.	02	.	.	16	12	11	06	08	08	03	.	.	.	.	.	04	17
IV	8.2	7.8	6.7	7.6	113.8	05.9	81	55	73	70	26	125	027.0	21	.	.	02	01	.	.	08	01	01	16	17	13	05	16	04	02	.	.	.	.	03	02	02
V	6.4	6.6	6.2	6.4	189.9	07.2	73	49	71	64	30	086	035.1	17	.	.	01	.	.	.	09	01	01	10	09	07	02	09	.	.	.	.	.	.	07	.	.
VI	5.1	6.8	6.2	6.0	214.0	11.5	77	55	78	70	29	105	035.8	18	.	.	.	16	01	.	04	01	02	08	14	08	03	14	.	.	.	.	.	01	11	01	.
VII	4.6	5.5	4.4	4.8	253.3	11.8	78	56	75	69	33	122	049.6	16	.	.	.	17	03	.	06	01	04	06	09	09	04	09	.	.	.	.	.	.	06	01	.
VIII	6.9	6.3	6.6	6.6	178.2	13.0	85	62	87	78	36	194	041.5	09	.	.	.	12	02	.	02	.	.	10	14	10	07	14	.	.	.	.	.	.	13	03	.
IX	5.0	4.5	4.4	4.6	170.2	10.0	89	56	87	77	37	022	010.0	07	.	.	.	05	.	.	05	01	09	06	08	05	01	08	.	.	.	.	.	.	01	02	.
X	6.4	4.7	4.0	5.0	143.3	07.0	89	55	90	78	35	100	068.2	21	.	.	05	.	.	.	04	.	08	07	06	05	02	06	02	02	.	.	.	.	02	07	.
XI	6.5	5.8	5.4	5.9	093.1	05.7	85	57	84	75	18	069	034.8	22	.	.	09	.	.	.	03	.	02	06	07	05	02	07	.	.	.	.	.	.	.	06	.
XII	7.2	5.7	5.7	6.2	052.4	03.7	88	72	86	82	27	039	014.8	28	.	08	27	.	.	.	02	.	05	12	10	07	01	05	06	01	.	.	.	.	.	05	10
GOD.	6.7	6.4	6.1	6.4	1597.0	07.3	84	60	81	75	18	1074	068.2	21 X	05	26	111	51	06	.	51	06	34	135	133	95	35	109	40	12	.	.	.	01	43	46	64

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C 7	14	21	Sred. (Dnev)	Max	Min	Max	Dat.	Min	Dat.	Čestina pravca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.		j.	δ.	j.	δ.
PRAGERSKO $\varphi = 46^\circ 24'$ N $\lambda = 15^\circ 39'$ E Gr. $\Delta G =$ + 1h 03 min.																												BR. ST. 21
I	-	-02.4	01.3	-00.8	-00.7	02.3	-03.3	10.6	15	-13.0	08	.	.	22	01.2	05	01.4	02	01.0	.	.	20	02.4	.	.	.	.	44
II	-	-01.6	04.6	01.1	01.3	05.4	-02.8	12.8	23	-17.6	17	.	.	10	02.2	09	01.0	01	01.0	.	.	34	02.9	04	01.0	.	.	26
III	-	00.8	06.8	02.9	03.3	07.6	-00.2	17.2	22	-07.0	08	.	.	20	01.5	05	01.2	01	01.0	01	02.0	31	02.6	02	02.0	.	.	33
IV	-	06.0	13.1	07.7	08.6	14.2	03.8	26.0	19	-03.2	04	02	01.0	13	01.6	04	02.0	03	01.7	.	.	34	02.2	03	01.0	.	.	31
V	-	10.7	16.9	10.6	12.2	18.4	06.1	23.5	14	-01.3	04	01	01.0	13	01.6	03	02.0	03	01.7	.	.	32	02.5	04	01.8	02	02.0	35
VI	-	16.9	23.1	16.3	18.2	24.7	11.7	30.8	28	04.8	04	02	01.0	08	01.4	05	01.6	02	01.5	.	.	21	01.6	04	01.0	01	01.0	47
VII	-	16.9	23.8	17.2	18.8	25.2	12.4	30.8	24	06.7	06	03	01.7	09	01.6	09	01.6	.	.	04	02.0	22	02.0	05	01.0	.	.	41
VIII	-	15.8	23.5	17.3	18.5	24.8	13.4	32.1	06	08.2	27,26	01	01.0	09	01.3	04	01.0	.	.	02	01.5	20	01.4	04	01.0	.	.	53
IX	-	10.9	20.8	13.3	14.6	21.2	09.1	29.0	11	-00.5	29	.	.	11	01.2	02	01.5	03	01.7	.	.	27	01.8	02	01.5	01	01.0	44
X	-	05.7	15.0	07.1	08.7	15.6	03.4	25.2	09	-04.8	17	.	.	08	01.4	01	01.0	02	02.0	01	01.0	40	02.4	06	01.3	01	01.0	34
XI	-	04.5	12.3	06.5	07.4	12.9	02.8	21.5	03	-03.5	27	02	01.5	02	01.5	.	.	03	01.7	.	.	45	02.2	10	01.5	.	.	28
XII	-	-02.2	02.9	-01.2	-00.4	03.6	-04.1	13.4	01	-15.3	25	01	03.0	13	02.0	03	01.0	.	.	01	01.0	30	01.6	02	01.0	01	01.0	42
GOD.	-	06.8	13.7	08.2	09.2	14.7	04.4	32.1	6 VIII	-17.6	17 II	12	01.4	138	01.5	50	01.4	20	01.6	09	01.7	356	02.2	46	01.3	06	01.3	458
MURSKA SOBOTA $\varphi = 46^\circ 40'$ N $\lambda = 16^\circ 08'$ E Gr. $\Delta G =$ + 1h 05 min.																												BR. ST. 22
I	743.3	-03.6	-00.9	-02.4	-02.3	00.4	-05.3	09.3	05	-18.8	04	02	01.0	01	01.0	.	.	05	01.4	01	01.0	01	01.0	.	.	.	.	83
II	740.0	-02.9	02.7	-00.5	-00.3	03.7	-04.5	11.4	09	-14.6	17	02	02.0	02	02.5	01	02.0	07	03.1	05	02.0	.	.	03	02.0	01	01.0	63
III	741.4	00.8	06.6	03.3	03.5	07.7	-00.4	17.5	24	-08.2	08	07	01.9	03	01.7	.	.	02	01.5	04	02.5	12	02.8	03	02.3	01	02.0	61
IV	742.7	06.1	12.9	07.9	08.7	14.4	03.7	25.0	19	-04.1	04	07	01.7	05	01.8	03	01.0	02	02.0	14	02.1	07	02.3	03	01.3	07	01.4	42
V	744.0	09.9	17.2	11.3	12.4	18.4	06.2	26.1	10	-01.8	01	07	02.4	02	01.0	.	.	02	01.5	11	02.7	10	02.9	07	02.0	13	01.5	41
VI	745.1	16.4	22.8	17.1	18.3	24.4	12.5	30.4	23	05.0	03	09	01.6	10	01.6	01	01.0	01	01.0	07	01.7	02	02.5	10	01.1	19	01.8	31
VII	744.4	16.7	23.1	17.9	18.9	24.9	12.9	30.1	14	07.0	20	09	01.9	03	02.0	04	01.8	05	02.2	11	01.6	08	01.6	13	01.7	06	01.3	34
VIII	744.1	16.3	23.6	18.1	19.0	24.6	14.0	31.8	06	09.0	26,19	11	01.3	08	01.4	02	01.0	02	02.0	08	02.4	06	02.7	07	01.9	09	01.3	40
IX	747.8	11.1	20.3	13.8	14.8	21.1	09.3	28.6	11	-01.5	30	04	01.5	06	01.5	07	01.7	03	02.0	12	02.0	01	02.0	08	01.2	05	01.4	44
X	747.4	05.2	14.3	07.3	08.5	15.0	03.3	24.1	09	-04.6	17	03	01.3	05	01.6	04	02.0	06	01.5	11	02.6	04	02.5	02	01.5	12	01.5	46
XI	744.9	04.5	11.3	06.4	07.2	12.0	02.6	20.6	03	-02.2	17	03	03.0	02	01.0	01	01.0	05	01.6	10	01.9	18	02.6	06	01.0	04	01.0	41
XII	748.7	-02.6	01.4	-01.6	-01.1	02.4	-04.5	10.1	04	-18.2	25	09	01.9	05	02.2	.	.	.	.	03	01.7	05	02.8	04	01.2	08	01.1	59
GOD.	744.5	06.5	12.9	08.2	09.0	14.1	04.2	31.8	6 VIII	-18.8	4. I	73	01.8	52	01.6	23	01.6	40	01.9	97	02.1	74	02.5	66	01.5	85	01.5	585
JERUZALEM $\varphi = 46^\circ 28'$ N $\lambda = 16^\circ 12'$ E Gr. $\Delta G =$ + 1h 05 min.																												BR. ST. 23
I	-	-02.4	-00.2	-01.8	-01.6	01.2	-03.6	09.0	05	-08.0	09,03	04	01.0	41	02.0	06	01.2	12	01.8	05	01.4	22	02.3	03	01.0	.	.	.
II	-	-01.2	03.0	00.6	00.7	04.3	-01.9	13.0	23	-10.0	17	04	01.2	30	02.1	01	01.0	06	01.8	02	03.5	34	03.1	05	01.6	02	01.5	.
III	-	01.5	06.1	03.4	03.6	07.0	01.0	17.5	24	-04.5	01	03	01.0	35	02.0	02	02.5	02	02.0	03	01.3	40	02.6	04	01.5	03	01.0	01
IV	-	06.6	12.1	08.1	08.7	13.6	05.4	24.5	19	-02.5	04	05	01.0	28	02.3	07	01.9	03	01.3	04	03.0	29	02.6	10	01.7	04	01.8	.
V	-	10.9	16.8	11.8	12.8	17.8	08.7	23.0	13	02.0	02,01	08	02.1	26	02.3	06	01.5	05	02.4	07	02.4	25	02.7	13	01.8	03	01.7	.
VI	-	17.3	22.4	17.9	18.9	23.8	14.7	29.5	23	07.5	03	05	02.0	38	02.1	03	02.7	06	02.2	03	02.0	22	02.4	06	02.0	07	01.7	.
VII	-	17.3	22.7	18.4	19.2	23.9	14.6	29.5	23,14	08.5	16,15	05	01.4	32	02.3	04	01.8	03	02.7	08	02.6	28	02.2	11	01.9	01	03.0	01
VIII	-	16.8	22.9	18.6	19.2	24.2	15.5	31.5	06	12.0	26,18	.	.	31	02.1	10	01.8	06	02.3	06	01.8	22	02.0	09	01.8	04	01.8	05
IX	-	12.9	19.6	14.5	15.4	20.4	11.6	28.5	11	04.3	29	02	02.5	38	02.3	09	01.7	03	02.0	08	03.2	20	02.2	04	02.0	05	02.6	01
X	-	07.5	13.9	09.0	09.9	14.7	06.0	25.0	10	-00.2	24	02	02.0	19	02.5	08	01.2	07	02.3	13	02.2	37	02.6	04	02.5	03	02.0	.
XI	-	06.2	11.4	07.9	08.3	12.4	04.9	22.0	03	-01.7	27	02	01.0	14	02.1	04	01.8	04	01.8	10	03.1	42	02.4	08	01.9	05	01.6	.
XII	-	-01.4	02.1	-00.6	-00.1	03.1	-02.4	12.0	02,01	-10.5	27	01	02.0	19	02.8	.	.	02	01.0	09	01.3	49	01.7	08	01.5	04	01.8	01
GOD.	-	07.7	12.7	09.0	09.6	13.9	06.2	31.5	6 VIII	-10.5	27 XII	41	01.6	351	02.2	60	01.7	59	02.0	78	02.3	370	02.4	85	01.8	41	01.8	09
VELIKI DOLENCI $\varphi = 46^\circ 51'$ N $\lambda = 16^\circ 17'$ E Gr. $\Delta G =$ + 1h 05 min.																												BR. ST. 24
I	-	-03.7	-00.4	-02.1	-02.1	00.8	-05.2	09.5	05	-13.8	03	11	01.3	18	01.5	04	01.2	11	01.9	11	01.7	22	01.6	04	01.5	12	01.2	.
II	-	-02.5	02.9	00.0	00.1	04.0	-04.3	12.5	09	-14.0	17	09	01.8	18	02.0	06	01.3	09	01.3	09	02.4	22	02.1	08	01.4	03	01.7	.
III	-	00.6	06.4	03.4	03.5	07.4	-01.6	16.5	24	-08.0	08	16	01.6	16	02.1	01	02.0	.	.	08	03.0	31	02.1	11	01.2	09	02.2	01
IV	-	06.5	12.1	08.1	08.7	13.6	03.4	24.0	19	-07.0	04	09	01.9	09	02.3	07	01.3	05	02.8	16	01.9	28	02.2	06	01.7	10	01.8	.
V	-	10.2	16.6	11.3	12.3	17.9	05.8	22.5	14	-05.0	04	13	02.2	09	01.7	06	01.2	02	02.5	13	02.4	25	02.8	12	01.2	13	02.0	.
VI	-	16.6	22.1	17.0	18.2	23.8	12.3	30.0	22	05.2	03	05	02.2	09	02.4	05	01.6	04	02.0	18	01.4	21	02.2	15	01.1	12	02.1	01
VII	-	16.8	22.3	17.4	18.5	23.9	12.6	29.4	23	08.4	16	16	02.1	11	02.4	02	01.0	06	01.3	12	02.0	18	02.3	14	01.7	09	02.2	05
VIII	-	15.8	22.9	18.1	18.7	24.1	13.7	30.5	06	09.0	26,19	07	01.3	20	01.9	03	01.3	02	02.0	20	01.4	22	02.0	09	01.1	07	01.7	03
IX	-	11.2	19.6	14.0	14.7	20.8	09.2	28.0	11	-01.4	30	14	01.4	10	02.2	02	01.0	.	.	14	02.1	20	02.2	19	01.3	11	01.3	.
X	-	05.7	13.9	07.8	08.8	14.8	03.1	23.5	09	-04.0	16	09	01.7	06	03.2	01	01.0	01	01.0	09	02.0	39	01.9	15	01.0	13	02.0	.
XI	-	04.5	11.0	06.7	07.2	11.9	01.9	21.0	03	-03.0	23,17	12	02.1	09	01.7	02	01.0	03	02.3	10	04.1	29	02.4	10	01.2	14	02.1	01
XII	-	-02.2	02.0	-01.1	-00.6	03.1	-04.2	12.5	02	-10.4	26	23	02.0	13	02.7	02	01.0	.	.	05	02.0	27	02.0	13	01.5	09	02.0	01
GOD.	-	06.6	12.6	08.4	09.0	13.8	03.9	30.5	6 VIII	-14.0	17 II	144	01.8	148	02.1	41	01.3	43	01.8	145	02.1	304	02.1	136	01.3	122	01.9	12
TEMNICA $\varphi = 45^\circ 51'$ N $\lambda = 13^\circ 41'$ E Gr. $\Delta G =$ + 55 min.																												BR. ST. 25
I	-	02.7	05.1	03.0	03.4	06.1	01.4	11.0	18	-03.6	23	02	01.0	08	03.1	45	02.5	13	01.5	14	01.4	.	.	02	01.5	01	01.0	08
II	-	01.2	04.4	02.0	02.4	05.3	-00.1	09.7	24	-06.1	17	11	01.0	07	03.0	23	02.2	13	01.3	04	01.5	04	01.5	07	01.9	06	01.3	09
III	-	03.1	06.3	04.2	04.5	07.2	02.1	13.7	21	-02.2	01	10	01.2	14	03.6	35	02.1	08	01.6	07	02.0	08	01.9	04	01.5	03	02.0	04
IV	-	08.1	11.6	08.4	09.1	12.9	05.6	20.1	19	-00.4	04	05	01.4	09	02.4	27	01.9	15	02.2	10	02.9	07	02.7	04	01.5	05	02.0	08
V	-	12.0	15.5	11.9	12.8	16.9	09.0	22.1	20	03.5	02	10	01.6	10	01.8	24	02.0	11	02.1	12	02.3	09	02.9	07	01.7	07	01.7	03
VI	-	18.5	22.3	18.0	19.2	23.4	15.2	28.2	27	08.8	03	07	01.7	05	02.2	27	01.7	07	02.0	13	02.2	12	02.2	02	01.0	05	01.8	12
VII	-	19.7	24.2	19.4	20.6	25.0	16.0	31.2	24	09.3	16	03	01.3	10	03.3	32	02.7	07	02.1	07	02.6	10	02.4	03	02.0	03	02.0	18
VIII	-	19.4	23.8	19.6	20.6	25.1	16.9	31.2	07	12.2	25	08	01.1	16	01.3	26	01.9	07	02.0	01	01.0	19	02.3	04	01.5	02	01.0	10
IX	-	16.0	21.5	16.8	17.8	22.0	14.4	26.0	11	07.4	30	04	01.0	08	03.0	46	02.6	05	01.6	04	01.8	16	02.4	.	.	02	01.5	05
X	-	09.8	14.9	10.7	11.5	15.9	08.5	25.5	12	02.9	25	08	01.1	15	02.9	32	02.3	06	01.7	07	01.6	11	02.0	01	02.0	07	01.7	06
XI	-	08.1	11.0	08.7	09.2	12.1	06.8	16.7	27	03.4	17	03	01.3	10	02.3	16	01.9	19	01.5	15	01.8	11	01.7	04	01.5	04	01.8	08
XII	-	02.8	06.3	03.5	04.0	07.3	01.6	14.4	10	-04.6	26	17	01.2	19	03.6	28	02.4	09	01.4	03	02.0	06	01.3	02	01.5	05	01.6	04
GOD.	-	10.1	13.9	10.5	11.3	14.9	08.1	31.2	24 VII 7 VIII	-06.1	17 II	88	01.2	131	02.7	361	02.2	120	01.7	97	02.0	113	02.2	40	01.6	50	01.7	95

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlen)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dlen)	Min	Padavine R mm Σ	Max	Int.	Broj dana n sa: Tn ≤ -10,0	Tx ≤ -10,0	Tn < 0,0	Tx < 0,0	Tx ≥ 25,0	Tn ≥ 20,0	P(0-12) ≥ 6	Nm(0-10) ≥ 8	< 8,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⁂	≋	≋	≋	▲	▲	⊤	■	■
BR. ST. 21																																						
PRAGERSKO																																						
H_o = 251 m H_b = - m h_b = 2,0 m h_x = 1,5 m																																						
I	9.5	8.2	8.1	8.6	-	03.9	89	84	86	86	63	042	019.0	06	01	13	25	.	.	.	.	.	01	24	09	09	01	04	06	.	.	.	.	.	.	07	15
II	7.6	6.9	7.9	7.3	-	04.0	82	68	79	76	42	057	014.0	14	02	02	20	.	.	.	01	.	02	16	12	11	02	03	10	.	.	.	.	.	.	03	15
III	7.5	7.5	6.3	7.1	-	04.8	87	68	84	79	33	103	018.6	05	.	.	18	.	.	.	01	.	03	16	12	12	02	09	08	03	.	.	.	.	.	04	15
IV	8.0	7.4	5.0	6.8	-	06.6	86	62	80	74	41	132	027.0	21	.	.	05	01	.	.	01	.	04	14	14	15	06	13	04	.	.	.	.	.	.	.	02
V	6.3	6.7	4.8	5.9	-	08.3	82	62	83	76	44	082	041.6	17	.	.	04	.	.	.	02	.	04	11	09	08	02	09	.	.	.	.	.	01	03	.	.
VI	3.9	6.2	3.8	4.7	-	13.0	86	67	89	81	48	081	028.8	19	.	.	.	15	03	.	.	.	09	04	13	13	02	.	.	.	.	.	.	.	07	.	.
VII	3.7	4.7	2.9	3.8	-	13.5	87	67	87	80	50	114	035.5	01	.	.	.	18	04	.	.	.	14	05	08	08	05	08	.	.	.	.	.	.	02	.	.
VIII	5.5	6.1	5.0	5.6	-	14.6	96	79	95	89	54	184	035.0	25	.	.	.	14	03	.	01	01	06	06	13	12	04	13	.	.	.	.	.	.	08	01	.
IX	4.5	3.6	3.7	3.9	-	11.0	94	66	93	84	36	022	007.6	27	.	.	01	08	.	.	.	.	12	06	06	06	.	06	.	.	.	.	.	.	01	.	.
X	6.1	4.1	3.1	4.4	-	07.5	91	66	90	82	54	080	056.3	21	.	.	09	02	.	.	02	.	09	04	06	06	01	06	.	.	.	.	.	.	.	04	.
XI	6.3	5.1	5.1	5.5	-	06.4	90	67	85	81	47	065	022.6	22	.	.	08	.	.	.	01	.	06	09	07	07	02	07	.	.	.	.	.	.	.	05	.
XII	7.1	5.5	6.2	6.3	-	03.8	85	75	85	82	46	033	009.0	28	04	06	28	.	.	.	.	.	06	12	07	06	.	04	03	.	.	.	.	.	.	04	10
GOD.	6.3	6.0	5.2	5.8	-	08.1	87	68	86	81	33	995	056.3	21 X	07	21	118	58	10	.	09	01	76	127	118	113	29	82	31	03	.	.	.	01	21	28	97
BR. ST. 22																																						
MURSKA SOBOTA																																						
H_o = 191 m H_b = 192,9 m h_b = 2,0 m h_x = 1,7 m																																						
I	9.4	9.0	8.6	9.0	018.9	03.5	90	82	86	86	55	029	008.4	06	07	17	26	.	.	.	.	.	.	24	10	07	.	04	06	.	.	.	.	.	.	11	18
II	7.4	7.2	7.6	7.4	056.8	03.7	90	68	82	80	43	032	010.7	14	05	04	25	.	.	.	01	.	02	16	12	07	01	03	09	.	.	.	.	.	.	07	15
III	8.3	8.1	6.0	7.5	081.7	04.6	91	63	81	78	29	085	020.4	05	.	.	19	.	.	.	.	.	.	16	14	12	04	09	08	03	.	.	.	.	.	02	10
IV	8.3	7.6	4.7	6.9	118.7	06.2	86	53	77	72	29	093	024.7	03	.	.	05	01	.	.	.	.	02	12	15	12	02	13	03	.	.	.	.	.	.	01	02
V	6.3	7.2	4.1	5.9	210.8	07.6	84	49	79	70	29	055	017.9	22	.	.	02	01	.	.	01	.	04	09	15	09	02	15	.	.	.	.	.	.	01	01	.
VI	3.5	6.9	4.1	4.9	232.4	11.7	82	54	84	74	34	049	014.9	03	.	.	.	15	02	.	.	.	08	03	15	09	01	15	.	.	.	.	.	.	06	.	.
VII	4.7	5.1	3.7	4.5	251.8	12.2	83	56	85	74	36	121	032.1	16	.	.	.	19	01	.	.	.	11	07	10	09	05	10	.	.	.	.	.	.	05	01	.
VIII	6.3	6.1	4.9	5.8	193.4	13.5	92	61	93	82	40	131	029.2	25	.	.	.	15	01	.	.	.	05	10	14	11	06	14	.	.	.	.	.	01	02	01	.
IX	6.5	4.1	4.9	5.2	181.8	10.4	95	56	91	81	41	030	007.7	07	.	.	02	06	.	.	.	.	06	06	08	07	.	08	.	.	.	.	.	.	.	04	.
X	7.2	5.6	3.1	5.3	126.5	07.0	90	61	91	80	43	064	045.7	21	.	.	08	.	.	.	.	.	05	07	05	05	01	05	01	01	.	.	.	.	.	10	01
XI	7.1	7.0	6.2	6.8	104.9	06.1	91	63	85	80	32	056	020.3	22	.	.	05	.	.	.	.	.	02	10	10	07	03	10	.	.	.	.	.	.	.	04	.
XII	8.3	8.2	6.1	7.5	042.4	03.8	92	78	91	87	22	016	003.4	30	04	07	26	.	.	.	01	.	01	17	10	07	.	05	06	.	.	.	.	.	.	13	10
GOD.	6.9	6.8	5.3	6.4	1620.1	07.5	88	62	85	78	22	761	045.7	21 X	16	28	118	57	04	.	03	.	46	137	138	102	25	111	33	04	.	.	.	01	14	55	56
BR. ST. 23																																						
JERUZALEM																																						
H_o = 345 m H_b = - m h_b = 2,0 m h_x = 1,5 m																																						
I	8.5	8.1	8.1	8.2	034.1	03.8	95	90	93	93	68	038	010.4	06	.	15	27	.	.	.	01	.	02	22	10	08	01	04	07	.	.	.	.	.	.	09	19
II	7.8	6.9	7.1	7.3	072.6	04.0	89	74	82	82	35	063	018.8	11	01	06	18	.	.	.	07	.	01	16	14	11	02	04	11	01	.	.	.	.	01	03	15
III	7.3	7.4	5.8	6.8	-	04.8	88	71	80	80	20	122	020.5	05	.	.	15	.	.	.	05	.	05	15	12	11	05	06	09	.	.	.	.	.	.	03	17
IV	8.1	6.8	5.2	6.7	126.3	06.3	81	62	77	73	35	153	046.0	03	.	.	03	.	.	.	04	.	03	13	15	14	06	13	04	01	.	.	.	.	06	01	05
V	5.2	6.3	4.8	5.4	212.4	08.0	78	60	74	70	44	088	024.4	17	.	.	.	.	.	.	04	.	07	09	10	08	03	10	.	.	.	.	.	01	07	01	.
VI	3.6	6.2	5.3	5.0	239.7	12.4	80	66	78	74	47	052	033.3	19	.	.	.	14	.	.	01	.	10	09	09	06	01	09	.	.	.	.	.	01	10	01	.
VII	4.5	4.5	3.4	4.1	248.2	12.6	81	64	77	74	47	122	032.8	16	.	.	.	16	.	01	04	.	13	07	11	09	05	11	.	.	.	.	.	.	04	01	.
VIII	5.8	5.4	5.1	5.4	196.7	13.8	89	71	84	81	53	121	041.0	25	.	.	.	13	01	01	.	.	09	12	14	12	04	14	.	.	.	.	.	.	08	.	.
IX	5.3	4.1	3.0	4.1	216.3	10.5	88	66	79	77	51	060	020.9	06	.	.	.	04	.	.	01	.	11	06	09	08	02	09	.	.	.	.	.	.	03	.	.
X	6.0	5.7	3.5	5.1	149.1	07.6	84	69	84	79	12	061	037.3	21	.	.	02	01	.	.	02	.	08	08	09	05	02	09	01	01	.	.	.	.	02	04	01
XI	6.9	6.4	5.5	6.3	099.3	06.5	84	70	78	78	46	060	024.8	27	.	.	01	.	.	.	06	.	03	11	10	06	02	10	.	.	.	.	.	.	.	05	.
XII	7.4	7.1	5.3	6.6	063.5	04.1	87	83	88	86	41	045	013.8	28	02	08	23	.	.	.	02	.	05	14	10	07	02	06	06	02	.	.	.	.	.	09	10
GOD.	6.4	6.2	5.2	5.9	-	07.9	85	70	81	78	12	985	046.0	3 IV	03	29	89	48	01	02	37	.	77	142	133	105	35	105	38	05	.	.	.	02	41	37	67
BR. ST. 24																																						
VELIKI DOLENCI																																						
H_o = 308 m H_b = - m h_b = 2,0 m h_x = 1,5 m																																						
I	8.3	7.7	6.8	7.6	-	03.8	97	90	95	94	60	036	013.8	06	05	15	28	.	.	.	.	.	01	15	07	06	02	02	05	.	01	.	.	.	.	11	17
II	7.2	6.4	6.1	6.6	-	03.8	90	68	86	81	41	042	016.0	14	02	03	28	.	.	.	.	.	02	11	10	08	01	04	06	.	.	.	.	.	.	03	16
III	8.1	6.8	5.2	6.7	-	04.7	89	66	83	80	34	139	035.5	13	.	.	23	.	.	.	01	.	02	13	14	13	04	08	09	01	02	.	.	.	.	13	19
IV	7.8	7.4	4.8	6.7	-	06.7	84	64	82	77	44	100	025.8	03	.	.	06	.	.	.	02	.	01	08	15	13	02	01	.	.	.	.	.	.	.	07	02
V	6.1	7.1	4.3	5.8	-	08.3	84	59	82	75	30	082	022.0	27	.	.	02	.	.	.	02	.	02	05	13	10	02	13	.	.	.	.	.	.	.	10	.
VI	4.8	6.8	5.6	5.7	-	12.9	86	67	89	81	48	042	008.7	18	.	.	.	13	01	.	.	.	03	05	15	11	.	15	.	.	.	.	.	.	03	11	.
VII	4.9	6.1	4.5	5.2	-	13.1	87	65	89	80	39	118	033.1	16	.	.	.	14	.	.	01	.	02	07	11	09	06	11	.	.	.	.	.	.	04	05	.
VIII	5.4	6.4	5.6	5.8	-	13.8	93	69	92	85	48	134	054.0	16	.	.	.	12	01	.	.	.	02	07	13	10	04	13	.	.	.	.	.	.	.	14	.
IX	5.4	4.3	3.8	4.5	-	10.6	94	64	89	82	34	021	008.0	02	.	.	02	04	.	.	01	.	06	06	08	06	.	08	.	.	.	.	.	.	.	13	.
X	6.8	5.4	1.9	4.7	-	07.5	94	68	92	84	51	068	054.0	21	.	.	08	.	.	.	02	.	07	05	06	05	01	06	.	.	.	.	.	.	.	10	.
XI	7.8	6.4	4.9	6.4	-	06.0	91	63	82	79	37	077	043.5	22	.	.	10	.	.	.	05	.	01	10	08	07	02	08	.	.	.	.	.	.	.	10	.
XII	7.7	6.7	4.9	6.4	-	04.0	92	80	92	88	35	023	008.1	24	02	07	29	.	.	.	03	.	04	11	12	06	.	06	06	.	01	.	.	.	.	20	10
GOD.	6.7	6.5	4.9	6.0	-	07.9	90	68	87	82	30	882	054.0	21 X	09	25	136	43	02	.	17	.	33	103	132	104	24	95	26	01	04	.	.	.	07	127	64
BR. ST. 25																																						
TEMNICA																																						
H_o = 402 m H_b = - m h_b = 2,0 m h_x = 1,5 m																																						
I	7.1	6.4	6.8	6.7	079.5	04.8	80	74	79	78	40	186	045.0	05	.	.	10	.	.	.	01	.	06	17	15	14	07	14	02	01	.	.	.	.	.	08	01
II	6.6	6.9	6.2	6.6	092.8	04.2	74	70	77	74	21	079	022.5	15	.	.	14	.	.	.	.	.	02	11	12	10	03	10	04	.	.	.	.	.	.	10	10
III	7.1	7.5	7.3	7.3	094.1	04.8	78	69	78	75	20	246	042.9	26	.	.	08	.	.	.	01	.	03	17	16	15	08	13	10	01	.	01	.	.	02	04	14
IV	6.3	6.1	4.9	5.8	161.2	06.1	73	62	72	69	32	179	028.6	22	.	.	01	.	.	.	.	.	04	07	16	15	08	15	03	.	.	.	.	.	05	01	03
V	5.5	7.1	5.1	5.9	209.0	07.5	70	58	71	66	30	128	023.5	31	.	.	.	.	.	.	.	.	02	09	13	12	08	13	.	.	.	.	.	.	07	02	.
VI	4.2	5.2	6.1	5.2	242.8	12.2	73	64	77	72	39	148	040.8	10	.	.	.	11	.	01	.	.	05	06	14	11	05	14	.	.	.	.	.	.	09	01	.
VII	3.3	3.5	3.2	3.3	297.7	11.2	65	52	64	60	32	060	034.3	01	.	.	.	18	02	06	01	.	14	03	04	04	02	04	.	.	.	.	.	.	03	.	.
VIII	3.6	5.5	3.0	4.0	206.0	12.7	73	61	74	69	38	115	033.5	31	.	.	.	15	04	02	.	.	11	03	12	11	03	12	.	.	.	.	.	.	08	.	.
IX	3.5	2.4	3.9	3.3	233.6	10.6	72	56	73	67	38	076	042.4	17	.	.	.	06	.	.	01	.	13	01	06	04	03	06	.	.	.	.	.	.	03	.	.
X	4.5	4.7	3.0	4.1	186.2	07.7	77	63	76	72	33	068	024.5	21	.	.	.	01	.	.	03	.	12	04	07	06	03	07	.	.	.	.	.	.	02	01	.
XI	7.4	6.5	6.3	6.7	088.1	04.8	81	69	80	77	25	131	031.0	20	.	.	.	.	.	.	.	.	06	16	11	09	04	11	.	.	.	.	.	.	02	02	.
XII	4.9	5.3	3.4	4.5	119.9	04.3	72	63	69	68	31	175	056.0	30	.	02	10	.	.	.	04	.	13	09	10	09	04	08	04	01	.	.	.	.	.	04	02
GOD.	5.3	5.6	4.9	5.3	2008.9	07.7	74	63	74	70	20	1591	056.0	30 XII	.	02	43	51	05	09	11	.	91	103	136	120	58	127	23	03	.	01	.	.	41	33	29

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Srednji (Dnevni)	Max	Min	Max	Det.	Min	Det.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												d.	j.	d.	j.	d.	j.	d.	j.	d.	j.	d.	j.		j.	d.	j.	d.
KOPER-SEMEDELA $\varphi = 45^\circ 33'$ N $\lambda = 13^\circ 43'$ E Gr. $\Delta G = +55$ min. BR. ST. 26																												
I	756.6	05.2	07.5	05.5	05.9	08.7	03.1	14.8	12	-03.0	19	.	.	07	03.7	10	03.3	12	02.5	.	.	06	02.8	01	02.0	05	02.0	52
II	755.1	03.9	06.6	04.6	04.9	08.3	02.3	13.8	05	-03.0	17	.	.	07	04.3	11	03.8	11	01.5	01	03.0	05	02.6	05	02.4	15	02.6	29
III	755.9	05.7	09.4	07.0	07.3	10.9	04.5	17.0	24	00.1	02	01	02.0	09	04.3	11	03.8	28	02.2	02	02.5	05	03.6	02	03.5	09	02.8	26
IV	757.4	10.0	13.8	10.5	11.2	15.4	07.7	21.0	25,20	00.7	03	01	02.0	05	04.2	09	03.3	19	02.3	07	02.9	10	04.2	03	03.3	10	02.9	26
V	758.7	13.9	17.9	14.1	15.0	19.2	10.8	22.7	10	04.4	02	.	.	.	.	05	03.4	16	02.3	02	02.5	09	03.0	03	04.0	17	03.1	41
VI	759.2	20.4	24.1	20.2	21.2	25.4	17.2	30.1	28	12.4	05	01	03.0	02	02.5	01	03.0	14	02.1	02	01.5	04	02.2	08	03.1	15	02.7	43
VII	757.9	21.2	25.8	21.1	22.3	27.0	17.0	33.5	30	10.6	16	.	.	07	04.0	08	04.1	11	01.7	03	03.0	02	03.0	02	04.5	21	03.1	39
VIII	757.7	21.2	25.2	21.3	22.2	26.8	18.4	30.6	06	13.5	25	.	.	01	02.0	04	02.5	09	01.7	02	02.0	04	02.8	08	03.2	15	02.5	50
IX	761.0	17.9	23.5	18.9	19.8	24.3	15.9	29.4	12	08.5	30	.	.	07	03.9	12	02.9	19	01.8	02	02.0	03	02.3	05	02.6	15	02.6	27
X	761.7	12.0	17.4	12.9	13.8	18.2	10.0	25.0	13,12	04.7	25	.	.	10	03.8	13	03.5	18	02.6	.	.	06	02.5	03	02.7	15	02.7	28
XI	760.0	10.3	13.6	11.0	11.5	14.7	08.3	18.4	19	04.4	26	.	.	04	03.0	02	03.0	21	02.4	10	02.6	07	02.7	03	02.7	09	02.2	34
XII	762.1	05.0	07.9	05.7	06.1	09.2	02.6	15.0	01	-03.3	26	.	.	11	04.2	13	03.8	09	02.8	04	02.5	06	02.5	04	02.2	09	02.1	37
GOD.	758.6	12.2	16.1	12.7	13.4	17.3	09.8	33.5	30 VII	-03.3	26 XII	03	02.3	70	03.9	99	03.5	187	02.2	35	02.6	47	03.0	47	03.0	155	02.7	432
KUBED $\varphi = 45^\circ 31'$ N $\lambda = 13^\circ 52'$ E Gr. $\Delta G = +55$ min. BR. ST. 27																												
I	-	03.2	07.2	03.6	04.4	08.3	01.1	12.6	12	-05.4	23	09	01.3	02	02.0	05	03.8	05	01.8	51	01.7	10	01.7	10	01.7	01	01.0	.
II	-	01.5	06.3	02.4	03.1	07.5	-00.8	12.0	06	-06.0	17	10	01.7	02	01.0	15	02.9	08	02.4	31	01.8	12	01.6	05	01.0	01	03.0	.
III	-	03.5	08.1	04.6	05.2	09.5	01.3	15.0	21	-04.0	29	13	01.5	01	02.0	16	03.4	08	02.5	40	02.1	05	01.2	09	02.1	01	02.0	.
IV	-	07.8	13.3	08.1	09.3	14.7	04.5	22.0	19	-02.0	04	09	01.9	03	02.7	06	02.3	12	02.3	37	02.1	10	01.4	10	01.4	03	02.3	.
V	-	11.8	17.5	11.1	12.9	18.7	07.4	24.0	20	-00.5	02	13	01.9	03	02.7	11	02.4	04	01.5	45	01.7	12	01.8	02	01.5	03	02.7	.
VI	-	18.8	23.8	17.6	19.5	25.5	14.0	29.7	26	09.4	05	10	02.1	08	02.9	01	03.0	04	01.8	42	01.6	11	01.6	13	01.5	01	01.0	.
VII	-	19.4	25.7	17.6	20.1	26.7	13.8	33.1	13	07.5	18	21	01.8	06	02.5	14	03.9	05	02.4	29	01.5	06	01.7	08	01.6	04	01.2	.
VIII	-	18.4	25.0	17.6	19.7	26.6	14.8	31.8	07	09.0	25	08	01.5	02	04.0	06	02.3	07	02.4	57	01.5	08	01.9	04	01.5	01	01.0	.
IX	-	15.2	23.4	15.4	17.3	24.9	12.5	28.6	11	04.2	30	06	02.2	07	03.1	16	02.8	04	02.2	29	01.2	13	01.5	11	01.8	04	02.2	.
X	-	08.3	16.5	09.4	10.9	18.1	06.1	29.0	06	-00.5	25	06	02.3	06	02.8	23	03.3	07	02.3	31	01.6	11	01.9	07	01.7	02	02.0	.
XI	-	06.7	13.1	08.6	09.2	14.6	04.6	20.0	27	-00.5	26,17	04	01.5	03	02.3	10	02.5	11	02.0	49	01.7	08	01.8	05	02.0	.	.	.
XII	-	01.5	07.5	02.0	03.2	09.1	-01.0	15.0	11	-09.1	26	07	01.6	12	03.5	19	02.6	06	02.8	32	01.8	10	01.7	06	01.8	01	02.0	.
GOD.	-	09.7	15.6	09.8	11.2	17.0	06.5	33.1	13 VII	-09.1	26 XII	116	01.8	55	02.9	142	03.0	81	02.2	473	01.7	116	01.7	90	01.7	22	01.9	.
AJDOVŠČINA $\varphi = 45^\circ 53'$ N $\lambda = 13^\circ 54'$ E Gr. $\Delta G = +54$ min. BR. ST. 28																												
I	749.0	03.3	06.2	03.4	04.1	07.0	01.1	12.2	13	-04.9	24	03	05.0	21	04.5	11	02.6	10	01.9	06	01.7	01	02.0	03	01.7	01	02.0	37
II	747.4	01.0	06.0	02.7	03.1	07.0	-00.9	11.6	24	-08.2	17	03	03.0	13	04.2	09	03.0	04	01.5	02	02.5	09	01.6	04	02.2	02	01.0	38
III	748.2	03.2	08.5	05.0	05.5	09.2	02.0	15.7	21	-04.6	02	03	02.3	26	04.5	07	01.9	03	01.3	03	01.7	01	04.0	06	01.7	03	01.0	41
IV	749.8	07.6	14.0	09.2	10.0	14.9	05.1	22.6	19	-01.9	04	08	03.4	18	03.3	04	01.8	02	01.5	06	02.5	10	02.2	08	01.8	02	01.5	37
V	751.3	11.7	17.7	12.2	13.5	19.0	07.4	23.2	20	-01.2	03	12	02.4	08	02.1	09	02.0	06	01.5	08	02.0	11	01.9	07	02.0	02	02.0	30
VI	752.1	18.1	24.0	17.7	19.4	25.4	13.3	31.2	27	06.9	05	07	01.1	09	01.7	12	01.4	03	01.7	06	01.5	13	01.6	09	01.4	06	01.0	25
VII	750.7	18.8	26.3	19.3	20.9	27.1	14.2	34.6	24	06.4	18	06	01.8	25	03.3	09	02.9	01	01.0	06	02.3	05	01.8	07	01.6	02	02.0	32
VIII	750.6	18.6	26.2	19.9	21.1	27.4	15.3	33.6	07	08.0	25	02	01.0	15	02.5	07	01.3	05	01.4	05	01.4	04	01.8	07	01.7	02	01.0	46
IX	754.0	15.8	23.4	17.1	18.3	24.0	13.6	28.6	12	01.4	30	08	03.1	19	04.3	07	02.0	02	01.5	05	02.0	05	01.8	06	01.7	.	.	38
X	754.3	08.4	17.1	10.8	11.8	17.9	06.4	26.5	11	-02.0	25	05	03.6	20	04.0	03	03.0	02	02.5	04	01.8	02	02.0	05	01.8	.	.	52
XI	752.5	07.9	13.1	09.2	09.8	14.3	05.8	18.5	28,10	-02.0	11	06	03.0	10	02.7	05	02.4	02	01.5	03	02.3	02	01.5	01	01.0	02	01.5	59
XII	754.5	02.6	07.9	02.7	04.0	09.0	-00.7	14.8	10	-07.0	24	06	03.0	22	04.8	02	03.5	02	02.5	05	01.8	03	02.0	01	01.0	01	02.0	51
GOD.	751.2	09.8	15.9	10.8	11.8	16.8	06.9	34.6	24 VII	-08.2	17 II	69	02.7	206	03.7	85	02.2	42	01.7	59	01.9	66	01.9	64	01.7	23	01.3	481
POSTOJNA-ZALOG $\varphi = 45^\circ 46'$ N $\lambda = 14^\circ 12'$ E Gr. $\Delta G = +57$ min. BR. ST. 29																												
I	-	-00.5	01.5	00.1	00.3	02.4	-02.0	10.7	05	-09.4	24	11	03.7	40	04.0	02	05.5	.	.	12	02.9	09	03.1	.	.	.	.	19
II	-	-02.1	02.5	00.0	00.1	03.6	-03.9	09.3	05	-18.2	17	04	03.2	22	03.5	03	02.0	.	.	15	03.5	16	03.0	01	01.0	02	01.0	21
III	-	-01.4	04.0	01.1	01.2	04.7	-02.0	10.6	21	-15.0	08	07	02.4	22	02.4	03	01.7	03	02.0	11	02.7	06	02.3	02	02.0	03	02.0	36
IV	-	03.2	09.8	05.8	06.2	11.4	01.5	21.9	19	-11.6	04	05	03.0	23	02.2	06	02.0	02	01.5	08	02.4	15	02.3	03	02.7	03	01.7	25
V	-	07.1	14.4	09.4	10.1	15.8	04.6	20.5	26	-02.4	03	08	02.4	18	02.5	05	02.4	01	01.0	08	03.1	10	02.6	08	02.2	02	01.5	33
VI	-	13.2	20.7	15.4	16.2	22.4	10.4	27.9	27	02.8	03	07	02.0	16	02.5	02	03.0	05	01.8	09	02.0	09	02.4	09	02.3	01	02.0	32
VII	-	14.1	22.0	16.1	17.1	23.4	10.9	31.0	24	03.3	18	08	01.9	30	02.7	07	03.1	06	02.3	01	02.0	13	02.2	01	03.0	06	01.8	21
VIII	-	14.2	22.0	16.3	17.2	23.2	11.9	29.8	07	05.7	25	.	.	31	02.1	03	02.3	01	02.0	01	03.0	11	01.9	02	01.5	07	01.9	37
IX	-	10.5	19.6	13.4	14.2	20.2	09.7	25.5	11	-01.5	30	13	02.0	27	02.4	03	02.0	02	01.0	08	02.5	08	02.9	04	02.2	04	01.5	21
X	-	04.9	13.7	07.7	08.5	14.3	03.8	23.3	10	-04.6	25	06	02.8	24	02.7	04	02.5	01	04.0	14	02.4	14	02.3	03	02.0	04	01.5	23
XI	-	04.8	09.7	05.8	06.5	10.4	02.8	15.1	04	-05.5	11	07	02.9	18	02.9	03	02.0	01	01.0	23	03.0	18	02.4	01	02.0	04	01.8	15
XII	-	-02.6	02.2	-01.3	-00.7	03.4	-04.6	10.9	01	-13.3	24	06	02.7	40	03.0	07	04.0	01	02.0	08	02.2	07	02.4	02	02.0	.	.	.
GOD.	-	05.4	11.8	07.5	08.1	12.9	03.6	31.0	24 VII	-18.2	17. II	82	02.6	311	02.8	48	02.7	23	01.9	118	02.7	136	02.5	36	02.2	36	01.7	283
ILIRSKA BISTRICA $\varphi = 45^\circ 34'$ N $\lambda = 14^\circ 15'$ E Gr. $\Delta G = +57$ min. BR. ST. 30																												
I	-	00.0	04.5	01.6	01.9	05.8	-01.6	12.1	18	-09.6	23	17	02.9	.	.	01	01.0	01	04.0	25	02.8	.	.	02	01.0	04	03.0	43
II	-	-00.4	04.6	01.4	01.7	05.5	-02.1	11.0	06	-12.0	17	23	03.1	01	02.0	02	02.0	07	03.4	22	02.5	.	.	02	03.0	02	02.5	25
III	-	00.5	06.1	03.0	03.2	06.9	-00.7	13.2	21	-10.0	08	28	03.1	.	.	02	01.5	04	02.5	24	03.2	01	03.0	01	01.0	03	04.0	30
IV	-	04.5	11.9	07.3	07.7	13.0	03.0	21.8	18	-04.9	04	22	03.4	01	04.0	02	01.5	04	02.8	28	03.3	04	03.2	.	.	03	01.7	26
V	-	07.5	15.8	10.7	11.2	17.1	05.6	21.8	20	-01.7	03	16	02.6	02	03.0	05	02.0	05	03.0	21	02.7	03	03.7	04	02.8	03	03.3	34
VI	-	13.4	22.2	16.4	17.1	23.6	11.5	28.5	27,22	03.9	03	12	02.7	01	01.0	01	01.0	05	03.4	13	02.5	05	03.0	02	01.5	03	02.7	48
VII	-	13.7	24.0	17.4	18.1	24.7	11.0	31.1	24	02.0	15	23	03.3	01	01.0	07	02.6	07	03.3	08	02.8	01	03.0	03	02.3	04	03.5	39
VIII	-	13.3	23.5	17.3	17.9	24.8	12.3	31.1	07	06.6	25	17	02.6	01	02.0	02	01.5	06	02.7	14	02.6	02	02.5	01	03.0	.	.	50
IX	-	10.3	21.9	14.2	15.1	22.3	09.5	26.0	11	-03.0	30	18	03.2	03	02.7	04	01.8	07	03.6	15	02.9	03	04.0	03	02.3	03	03.0	34
X	-	05.0	15.9	08.1	09.3	16.4	03.4	26.2	11	-03.9	26	20	03.0	03	03.3	03	01.7	04	03.5	18	02.5	05	03.2	03	01.3	02	02.0	35
XI	-	04.3	11.5	06.4	07.2	12.3	02.6	16.9	04	-04.4	29	18	02.4	02	01.0	01	02.0	01	04.0	28	03.0	06	03.3	01	05.0	03	02.3	30
XII	-	-02.1	05.0	-00.2	00.6	06.3	-03.9	11.9	04	-13.9	26	32	03.2	03	02.7	03	02.0	.	.	11	01.9	.	.	03	02.0	.	.	41
GOD.	-	05.8	13.9	08.6	09.2	14.9	04.2	31.1	24 VII 7. VIII	-13.9	26 XII	246	03.0	18	02.4	33	01.9	51	03.2	227	02.8	30	03.3	25	02.2	30	02.9	435

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dišes)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dišes)	Min	Padavine R mm Σ			Broj dana s: Tn ≤ 10,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	✱	△	▲	▲	⚡	≡	▦
BR. ST. 26 — KOPER-SEMEDELA — H_o = 33 m H_b = 27,7 m h_o = 2,0 m h_b = 1,6 m																																				
I	8.0	7.1	7.2	7.4	056.7	05.7	79	76	80	79	40	097	017.5	05	.	.	05	.	.	.	03	.	04	19	16	12	02	16	.	.	.	.	.	.	08	.
II	6.9	6.9	5.6	6.4	091.1	04.8	72	69	73	71	33	056	013.8	19	.	.	05	.	.	.	09	.	02	08	13	08	02	13	02	01	01	.	.	.	02	.
III	7.0	7.0	6.3	6.8	122.8	05.5	73	66	72	71	36	170	049.2	26	.	.	.	.	.	.	06	.	05	15	14	13	03	14	01	01	.	.	.	.	03	03
IV	6.4	5.9	5.2	5.8	186.5	06.8	72	57	69	66	22	158	046.0	22	.	.	.	.	.	.	07	01	03	07	17	12	05	17	01	.	.	.	.	.	08	.
V	5.1	5.7	4.7	5.2	244.8	08.7	70	58	72	67	38	088	019.9	24	.	.	.	.	.	.	04	.	03	07	15	11	04	15	.	.	.	.	.	.	08	.
VI	4.2	4.7	6.0	5.0	279.6	14.0	75	65	75	72	43	058	013.9	06	.	.	.	18	01	05	03	.	04	05	13	10	02	13	.	.	.	.	.	.	09	.
VII	3.0	3.1	3.2	3.1	331.2	13.0	67	53	67	63	36	056	033.2	01	.	.	.	23	06	07	06	04	16	03	05	05	02	05	.	.	.	.	.	.	03	.
VIII	4.1	4.6	3.2	4.0	257.7	14.6	74	64	76	71	45	145	036.7	30	.	.	.	23	02	10	03	01	12	03	12	11	05	12	.	.	.	.	.	.	11	.
IX	3.1	2.3	2.3	2.6	274.4	12.0	68	59	72	66	35	034	014.7	17	.	.	.	13	.	01	04	.	14	.	05	04	02	05	.	.	.	.	.	.	05	.
X	4.9	4.8	2.3	4.0	189.9	08.3	71	58	71	67	32	026	010.6	21	.	.	.	02	.	.	08	.	10	05	05	04	01	05	.	.	.	.	.	.	04	.
XI	6.7	6.0	5.8	6.2	081.1	07.7	78	69	76	74	40	092	026.7	16	.	.	.	.	.	.	.	02	07	14	09	07	03	09	.	.	.	.	.	.	.	.
XII	5.7	5.7	4.3	5.2	084.8	05.4	77	68	74	73	40	075	029.0	08	.	.	05	.	.	.	06	01	09	08	09	08	02	09	.	.	.	.	01	.	02	03
GOD.	5.4	5.3	4.7	5.1	2196.6	08.9	73	63	73	70	22	1055	049.2	16 IV	.	.	15	79	09	23	59	09	89	94	133	105	33	133	04	02	01	.	01	.	51	16
BR. ST. 27 — KUBED — H_o = 262 m H_b = - m h_o = 2,0 m h_b = 1,5 m																																				
I	7.4	6.7	6.6	6.9	-	-	-	-	-	-	-	128	023.0	05	.	.	12	.	.	.	01	.	06	16	15	13	05	15	.	.	.	.	.	.	07	.
II	6.0	6.5	5.1	5.9	-	-	-	-	-	-	-	062	016.0	15	.	.	17	.	.	.	.	.	03	07	11	10	02	10	03	02	.	.	.	.	01	01
III	6.5	7.3	6.3	6.7	-	-	-	-	-	-	-	200	046.0	04	.	.	11	.	.	.	01	.	05	15	13	13	06	13	05	04	.	.	.	.	02	02
IV	6.7	6.3	4.6	5.9	-	-	-	-	-	-	-	162	038.0	22	.	.	02	.	.	.	.	.	04	07	16	16	06	16	03	02	01	.	.	.	05	.
V	4.9	7.0	5.0	5.6	-	-	-	-	-	-	-	119	045.0	31	.	.	01	.	.	.	.	.	02	08	14	12	02	14	.	.	.	.	.	.	01	.
VI	4.1	6.7	5.0	5.3	-	-	-	-	-	-	-	089	056.6	19	.	.	20	.	.	.	.	.	03	07	12	10	02	12	.	.	.	.	01	.	06	.
VII	2.9	5.1	2.5	3.5	-	-	-	-	-	-	-	085	037.6	01	.	.	.	20	09	01	03	.	11	02	07	07	02	07	.	.	.	.	.	.	02	.
VIII	4.4	6.0	3.4	4.6	-	-	-	-	-	-	-	130	034.0	22	.	.	.	20	05	.	[illegible]	.	06	04	12	11	05	12	.	.	.	.	.	.	06	.
IX	3.1	3.6	2.7	3.1	-	-	-	-	-	-	-	049	021.0	23	.	.	.	21	.	01	02	.	12	02	05	05	02	05	.	.	.	.	.	.	01	01
X	4.3	4.9	2.7	3.9	-	-	-	-	-	-	-	032	014.0	21	.	.	01	05	.	.	03	.	11	03	05	05	01	05	.	.	.	.	.	.	02	.
XI	6.1	6.1	4.8	5.7	-	-	-	-	-	-	-	117	032.0	16	.	.	02	.	.	.	.	.	07	09	08	07	05	08	.	.	.	.	.	.	01	02
XII	5.1	5.1	3.7	4.6	-	-	-	-	-	-	-	092	030.0	30	.	01	19	.	.	.	04	.	12	09	08	08	03	08	.	.	.	.	.	.	01	.
GOD.	5.1	5.9	4.4	5.1	-	-	-	-	-	-	-	1265	056.6	19 VI	.	01	85	66	14	02	14	.	82	89	126	117	41	125	11	08	01	.	01	.	28	13
BR. ST. 28 — AJDOVŠČINA — H_o = 110 m H_b = 114,5 m h_o = 2,0 m h_b = 1,5 m																																				
I	7.5	6.9	7.4	7.2	081.4	04.9	81	70	80	77	39	226	050.2	06	.	.	11	.	.	.	08	06	05	18	16	11	08	15	03	.	.	.	.	.	07	.
II	7.5	8.0	5.8	7.1	082.1	04.4	81	65	79	75	34	094	029.2	15	.	.	16	.	.	.	07	06	02	13	15	10	02	15	04	02	.	.	01	.	.	03
III	7.5	7.8	6.8	7.3	092.2	05.2	83	63	80	75	20	250	042.1	04	.	.	09	.	.	.	12	08	05	16	20	17	08	19	05	.	.	.	.	.	02	.
IV	7.5	6.9	5.3	6.6	141.5	06.4	79	52	73	68	25	186	031.7	03	.	.	01	.	.	.	09	04	02	11	18	15	08	18	01	01	.	.	.	.	04	.
V	5.5	6.9	5.6	6.0	174.3	08.2	78	54	78	70	25	148	033.2	23	.	.	01	.	.	.	04	01	02	10	16	10	06	16	.	.	.	.	.	01	08	.
VI	3.9	5.7	4.3	4.6	211.3	13.2	81	63	84	76	36	103	024.0	15	.	.	.	18	01	.	.	.	04	04	14	13	05	14	.	.	.	.	.	.	07	.
VII	3.6	4.0	2.9	3.5	289.5	13.0	79	52	74	68	36	060	019.6	01	.	.	.	20	11	03	04	05	14	05	06	06	02	06	.	.	.	.	.	.	02	.
VIII	5.0	5.7	3.7	4.8	200.8	14.1	84	60	79	74	43	093	030.4	31	.	.	.	23	09	.	.	.	03	04	12	09	03	12	.	.	.	.	.	.	05	.
IX	4.6	3.2	4.6	4.1	235.1	11.4	78	56	76	70	42	037	019.1	04	.	.	.	15	.	.	04	01	06	.	03	03	02	03	.	.	.	.	.	.	03	.
X	5.9	5.5	5.2	5.5	182.6	08.0	85	59	80	74	24	068	035.6	21	.	.	02	04	.	.	03	.	04	06	07	06	02	07	.	.	.	.	.	.	02	04
XI	7.3	6.2	7.1	6.9	087.0	07.2	85	67	83	78	17	151	040.6	16	.	.	03	.	.	.	.	.	05	18	10	10	05	10	.	.	.	.	.	.	01	08
XII	5.4	5.0	4.8	5.1	104.6	04.8	80	63	84	75	37	130	035.9	01	.	.	16	.	.	.	09	01	08	09	07	07	04	06	02	.	.	.	.	.	01	04
GOD.	5.9	6.0	5.3	5.7	1882.4	08.4	81	60	79	73	17	1546	050.2	6 I	.	.	59	80	21	03	60	32	60	114	144	117	55	141	15	03	.	.	01	01	35	26
BR. ST. 29 — POSTOJNA-ZALOG — H_o = 533 m H_b = 534,1 m h_o = 2,0 m h_b = 1,5 m																																				
I	8.7	7.3	7.2	7.7	066.1	04.4	92	85	90	89	69	153	033.4	06	.	13	22	.	.	.	07	.	01	17	18	13	04	13	08	01	.	.	.	.	.	07
II	7.9	7.8	6.5	7.4	072.8	03.9	89	71	84	81	36	065	017.3	15	03	04	24	.	.	.	03	01	02	13	20	12	02	12	12	.	01	02	01	.	02	06
III	8.2	8.1	6.7	7.6	088.2	04.3	91	73	86	84	27	188	040.4	26	01	01	24	.	.	.	02	.	02	18	20	15	08	06	16	.	03	.	.	.	02	11
IV	7.8	6.9	5.6	6.8	125.7	05.4	87	60	79	75	31	275	042.1	22	01	.	11	.	.	.	.	.	01	14	20	15	12	17	07	03	.	.	01	01	06	04
V	5.9	7.3	5.1	6.1	180.7	07.0	87	57	80	75	36	090	020.1	31	.	.	05	.	.	.	02	.	02	10	17	12	03	16	01	.	.	.	.	.	06	05
VI	5.5	6.8	5.4	5.9	197.2	11.2	92	65	86	81	43	091	032.0	15	.	.	.	09	.	.	.	.	02	07	17	10	03	17	.	.	.	.	.	.	10	06
VII	3.8	4.6	3.1	3.9	280.8	11.3	88	58	83	76	39	203	072.6	16	.	.	.	15	01	.	02	.	16	06	10	09	05	10	.	.	.	.	.	01	03	06
VIII	5.5	6.3	2.4	4.7	197.7	12.2	92	66	89	82	37	122	023.0	31	.	.	.	13	.	.	.	.	07	02	13	11	05	13	.	.	.	.	.	.	08	11
IX	5.3	3.9	4.2	4.5	224.7	09.9	91	61	86	79	46	019	011.6	17	.	.	01	01	.	.	03	.	07	03	07	02	01	06	.	.	.	.	.	.	01	07
X	6.8	5.5	4.3	5.5	160.9	07.0	91	63	88	81	30	062	034.4	21	.	.	05	.	.	.	02	.	06	11	10	05	02	08	01	.	.	.	.	.	02	06
XI	8.1	6.0	6.4	6.8	088.7	06.2	91	71	89	83	33	152	036.3	16	.	.	05	.	.	.	.	.	03	17	12	07	05	12	.	.	.	.	.	.	02	05
XII	6.2	5.3	4.6	5.4	103.9	03.9	91	76	89	85	30	142	048.1	30	04	08	26	.	.	.	03	.	08	11	12	09	05	07	10	03	02	.	.	.	01	02
GOD.	6.6	6.3	5.1	6.0	1787.4	07.2	90	67	85	80	27	1562	072.6	16 VII	09	26	123	38	01	.	24	01	57	129	176	120	55	137	55	07	06	02	02	02	43	76
BR. ST. 30 — ILIRSKA BISTRICA — H_o = 414 m H_b = - m h_o = 2,0 m h_b = 1,5 m																																				
I	7.4	6.2	7.0	6.9	-	04.9	93	79	90	87	34	158	025.7	12	.	.	20	.	.	.	01	.	05	17	17	14	07	13	06	.	.	01	.	.	.	06
II	7.5	7.2	6.4	7.0	-	04.4	89	70	86	82	35	101	031.8	15	02	01	21	.	.	.	.	.	02	12	15	12	03	10	09	02	.	01	.	.	02	06
III	7.9	7.6	6.7	7.4	-	04.8	88	71	86	82	29	226	071.8	04	01	.	17	.	.	.	01	.	04	18	15	13	08	09	12	.	.	.	.	.	02	07
IV	7.0	6.7	5.3	6.3	-	05.9	87	56	79	74	28	234	059.2	06	.	.	06	.	.	.	.	.	03	11	18	14	07	16	03	01	.	.	01	.	04	02
V	5.7	7.5	5.4	6.2	-	07.3	90	54	79	74	31	070	017.2	23	.	.	04	.	.	.	.	.	03	10	16	14	02	16	.	.	.	.	01	.	08	04
VI	6.4	6.6	5.6	6.2	-	11.8	95	61	87	81	35	081	023.8	19	.	.	.	14	.	.	.	.	01	07	17	15	02	17	.	.	.	.	.	02	13	11
VII	4.1	4.9	3.6	4.2	-	11.3	88	53	77	73	35	062	027.8	16	.	.	.	16	03	.	02	.	10	07	05	04	03	05	.	.	.	.	.	01	05	07
VIII	8.4	6.8	4.2	6.5	-	12.6	99	62	88	83	37	157	042.2	31	.	.	.	16	03	.	.	.	.	09	14	12	05	14	.	.	.	.	.	.	13	21
IX	6.3	2.8	3.8	4.3	-	10.1	93	53	85	77	34	020	011.8	04	.	.	02	05	.	.	01	.	07	04	05	03	01	05	.	.	.	.	.	.	03	12
X	7.0	5.0	4.2	5.4	-	07.0	91	55	88	78	29	030	011.7	01	.	.	05	03	.	.	.	.	04	07	07	05	02	07	.	.	.	.	.	01	03	11
XI	7.5	6.0	6.4	6.6	-	06.4	92	66	87	82	33	123	035.7	22	.	.	09	.	.	.	01	.	05	17	12	06	04	12	.	.	.	.	.	.	04	07
XII	5.8	4.7	4.5	5.0	-	04.1	91	67	89	83	23	132	047.7	30	03	02	24	.	.	.	02	01	10	10	12	10	04	08	06	.	.	02	.	.	01	05
GOD.	6.8	6.0	5.3	6.0	-	07.6	91	62	85	79	23	1394	071.8	4 III	06	03	108	54	06	.	08	01	54	129	153	122	48	132	36	03	.	04	02	04	58	99

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Pm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W j.	NW č.	NW j.	C č.
RAKITNA $\varphi = 45^\circ 53'$ N $\lambda = 14^\circ 26'$ E Gr. $\Delta G = +58$ min. BR. ST. 31																											
I	-	-01.9	-00.1	-01.4	-01.2	01.2	-03.9	09.2	05	-16.3	08	08	02.0	13	02.4	17	02.2	16	01.9	10	01.7	12	02.3	06	01.2	07	02.0	04
II	-	-05.0	00.6	-02.1	-02.1	01.8	-07.4	07.0	05	-29.3	17	06	01.7	15	02.5	13	02.1	10	03.0	05	02.4	11	03.1	09	02.1	11	02.8	04
III	-	-02.4	02.4	-01.4	-00.7	03.5	-05.6	10.1	21	-19.7	08	13	01.7	15	02.3	12	01.8	10	02.3	10	01.3	06	01.2	13	02.1	12	02.4	02
IV	-	03.1	08.1	04.2	04.9	09.3	00.7	21.0	19	-12.7	04	09	03.0	10	02.7	05	02.0	16	02.3	08	01.6	12	02.1	14	01.7	14	01.6	02
V	-	08.0	12.7	07.8	09.1	13.9	03.8	18.5	10	-04.2	01	05	03.0	15	02.9	08	02.0	13	02.5	08	01.5	10	02.3	20	01.8	12	02.2	02
VI	-	14.9	19.1	13.6	15.3	20.6	08.8	25.5	22	-00.1	03	10	02.3	10	02.2	08	02.1	06	02.0	07	01.6	03	02.7	20	01.5	22	02.3	04
VII	-	14.6	20.0	14.2	15.8	21.2	08.6	27.4	23	02.3	19	09	02.2	10	02.8	28	02.4	08	02.5	05	02.4	06	02.2	15	01.9	09	01.8	03
VIII	-	13.7	20.2	14.2	15.6	21.4	09.7	27.8	07	03.8	27	08	01.5	11	01.7	10	01.9	08	02.4	02	02.0	07	01.3	14	01.6	29	01.9	04
IX	-	10.4	17.4	11.4	12.7	18.2	07.1	23.6	11	-05.2	30	04	02.2	12	02.2	16	02.6	15	02.8	08	01.4	10	02.3	09	01.3	13	02.7	03
X	-	05.1	11.6	06.3	07.3	12.2	01.9	22.8	10	-06.7	23,19	05	02.0	12	03.2	10	02.9	18	02.2	02	01.5	06	01.7	17	02.8	17	02.6	06
XI	-	03.3	07.8	04.8	05.2	08.7	01.5	14.9	02	-06.7	17	07	01.9	10	02.1	08	01.5	07	01.9	11	02.8	12	02.2	17	02.2	16	02.8	02
XII	-	-04.8	00.7	-04.2	-03.1	01.9	-07.7	09.4	02	-22.2	25	08	01.1	09	01.8	11	02.9	21	01.7	07	01.4	09	01.4	11	01.7	10	01.5	07
GOD.	-	04.9	10.0	05.6	06.6	11.2	01.5	27.8	7.VIII	-29.3	17.II	92	02.0	142	02.4	146	02.3	148	02.3	83	01.8	104	02.1	165	01.9	172	02.2	43
GOMANCE $\varphi = 45^\circ 30'$ N $\lambda = 14^\circ 26'$ E Gr. $\Delta G = +58$ min. BR. ST. 32																											
I	-	-00.5	02.1	-00.3	00.3	03.3	-03.2	07.3	05	-10.2	22	.	.	57	01.7	.	.	03	01.0	02	01.5	31	01.9	.	.	.	.	.
II	-	-02.3	00.5	-01.7	-01.3	01.3	-04.8	05.0	06,04	-13.0	17	01	02.0	56	01.7	.	.	.	.	04	01.0	23	02.0	.	.	.	.	.
III	-	-02.6	01.3	-00.6	-00.6	02.5	-04.5	06.0	26,21	-14.4	08	.	.	60	01.8	.	.	.	.	.	.	32	01.5	.	.	01	02.0	.
IV	-	02.8	06.9	03.0	03.9	08.1	00.1	16.5	23,18	-10.6	04	16	01.4	27	01.5	.	.	.	.	28	01.8	12	02.2	05	01.8	02	01.0	.
V	-	07.7	10.8	07.5	08.4	12.3	03.3	16.8	20	-02.2	01	03	01.0	61	02.0	.	.	.	.	.	.	27	02.2	01	02.0	.	.	01
VI	-	13.9	17.2	13.5	14.5	19.3	08.6	23.5	23	00.3	03	.	.	38	01.8	.	.	.	.	.	.	51	02.2	.	.	.	.	01
VII	-	13.8	18.8	14.0	15.2	20.0	09.1	27.2	30	02.4	24,16	.	.	67	13.2	.	.	.	.	.	.	23	03.7	.	.	03	02.7	.
VIII	-	14.0	19.5	14.0	15.4	20.8	09.9	26.0	07	05.1	25	01	01.0	50	01.9	01	02.0	.	.	03	01.0	33	02.5	.	.	.	.	05
IX	-	11.2	16.3	11.3	12.6	18.4	07.8	21.4	11	-01.2	30	.	.	75	02.5	.	.	.	.	.	.	15	03.0	.	.	.	.	.
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	03.8	07.9	04.7	05.3	09.0	00.3	13.4	04	-05.2	29,17	.	.	40	01.8	.	.	.	.	.	.	49	02.9	.	.	.	.	01
XII	-	-02.6	02.6	-01.5	-00.8	04.6	-04.8	11.9	11	-13.7	26	01	01.0	72	02.0	.	.	.	.	.	.	18	02.0	.	.	.	.	02
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NOVA VAS NA BLOKAH $\varphi = 45^\circ 46'$ N $\lambda = 14^\circ 31'$ E Gr. $\Delta G = +58$ min. BR. ST. 33																											
I	-	-02.0	00.5	-01.3	-01.0	01.8	-03.7	10.0	05	-15.5	08	.	.	13	02.4	28	01.9	.	.	.	.	03	03.7	12	03.2	10	02.5	27
II	-	-05.0	01.7	-02.2	-01.9	02.9	-07.7	08.0	06,04	-30.9	17	01	02.0	11	02.3	13	02.5	01	01.0	01	02.0	06	03.8	16	03.1	10	02.9	25
III	-	-03.5	03.2	-01.0	-00.6	04.2	-05.6	12.2	24	-23.8	08	.	.	25	02.5	04	02.0	.	.	.	.	09	03.2	07	03.0	11	02.5	37
IV	-	02.8	09.0	04.2	05.0	10.5	00.4	22.2	19	-18.0	04	03	02.7	16	01.8	03	01.3	02	02.0	.	.	11	03.2	16	03.1	11	02.6	28
V	-	07.2	12.3	07.7	09.0	14.8	03.0	22.1	14	-04.5	03	03	01.3	20	01.8	01	02.0	01	01.0	.	.	06	03.2	09	02.8	20	02.7	33
VI	-	13.9	19.9	13.8	15.4	21.7	08.8	28.3	27	00.5	03	04	01.2	10	02.0	.	.	.	.	03	02.7	06	02.8	03	02.7	18	02.4	46
VII	-	13.0	21.0	14.3	15.7	22.1	08.5	28.9	24	02.6	06	02	01.5	15	02.0	02	01.5	.	.	02	02.5	02	02.5	04	02.0	24	02.4	42
VIII	-	12.8	21.1	14.3	15.7	22.5	09.8	29.9	07	03.1	25	.	.	10	02.2	03	02.0	.	.	01	02.0	01	02.0	03	02.0	19	02.4	56
IX	-	08.7	18.6	11.1	12.4	19.4	06.6	25.1	11	-06.0	30	02	02.0	22	02.0	01	01.0	02	04.5	.	.	07	01.9	05	02.6	10	02.4	41
X	-	04.0	12.7	05.9	07.1	13.6	01.3	23.0	10	-07.2	23	.	.	23	02.4	02	01.0	01	02.0	01	02.0	04	03.5	05	03.2	25	03.3	32
XI	-	03.5	09.1	04.8	05.5	09.8	01.3	15.8	04	-07.4	11	.	.	19	01.5	01	01.0	.	.	01	04.0	16	03.1	08	03.0	25	02.8	20
XII	-	-05.6	00.6	-04.8	-03.6	01.7	-08.7	10.4	02	-22.5	25	.	.	28	02.6	.	.	01	02.0	.	.	07	03.0	09	02.4	06	02.5	42
GOD.	-	04.2	10.9	05.6	06.6	12.1	01.2	29.9	7.VIII	-30.9	17.II	15	01.7	212	02.2	58	01.9	08	02.4	09	02.6	78	03.1	97	02.9	189	02.7	429
BABNO POLJE $\varphi = 45^\circ 39'$ N $\lambda = 14^\circ 33'$ E Gr. $\Delta G = +58$ min. BR. ST. 34																											
I	-	-03.0	01.0	-01.5	-01.3	02.2	-05.1	09.5	05	-16.6	03	01	02.0	10	02.3	37	02.6	06	02.5	02	03.0	14	02.6	03	02.7	07	02.4	13
II	-	-05.5	01.9	-02.8	-02.3	03.0	-09.4	08.0	23	-31.5	17	06	02.2	05	02.2	26	02.2	.	.	.	.	15	02.9	05	02.6	08	03.0	19
III	-	-04.1	02.8	-01.3	-01.0	04.1	-06.7	10.4	21	-25.0	08	02	02.0	05	02.6	25	02.6	09	02.4	.	.	18	02.4	09	02.4	03	03.0	22
IV	-	01.9	08.6	02.5	03.9	10.0	01.3	21.0	19	-19.0	04	06	02.2	08	02.8	16	02.5	12	02.7	01	02.0	09	02.9	08	03.1	14	03.2	16
V	-	06.8	12.9	06.3	08.1	14.4	01.7	18.4	14	-05.6	03,01	04	02.8	12	03.1	14	03.0	12	02.4	.	.	08	03.5	16	02.8	09	02.6	15
VI	-	13.6	19.9	12.6	14.7	21.4	07.2	26.2	22	-01.0	05	02	02.5	15	02.6	05	02.4	05	02.8	05	03.2	19	02.6	12	02.8	15	02.6	12
VII	-	13.4	20.8	12.9	15.0	21.9	07.1	30.0	23	00.5	06	03	02.7	11	03.0	23	02.7	09	02.4	02	02.5	09	02.4	08	02.5	05	03.4	23
VIII	-	12.8	21.1	13.6	15.3	21.9	08.4	29.5	07	02.7	27	03	02.0	11	02.5	09	02.2	13	02.5	.	.	15	02.5	06	02.3	15	02.7	21
IX	-	08.5	18.5	10.1	11.8	19.4	05.2	24.7	11	-06.8	30	.	.	11	02.4	26	02.7	06	02.2	03	03.3	05	02.4	07	02.7	09	02.9	23
X	-	02.7	13.0	03.9	05.9	13.9	-00.7	24.0	11	-08.5	25	01	05.0	11	02.5	16	03.0	12	02.3	01	03.0	06	03.5	03	03.3	15	04.0	28
XI	-	01.4	09.0	03.5	04.3	09.8	-01.0	17.4	04	-09.0	11	03	04.0	07	02.6	22	02.4	07	02.6	.	.	08	02.5	09	03.0	13	02.8	21
XII	-	-05.7	01.8	-04.4	-03.2	03.0	-08.7	11.2	02	-21.6	25,24	02	04.5	04	03.2	32	03.1	04	02.0	.	.	01	02.0	07	02.1	07	02.9	36
GOD.	-	03.6	10.9	04.6	05.9	12.1	-00.1	30.0	25.VII	-31.5	17.II	33	02.7	110	02.6	251	02.6	95	02.5	14	03.0	127	02.7	93	02.7	120	03.0	249
KOČEVJE $\varphi = 45^\circ 38'$ N $\lambda = 14^\circ 52'$ E Gr. $\Delta G = +59$ min. BR. ST. 35																											
I	-	-00.9	01.7	-00.3	00.1	02.7	-03.0	11.4	05	-13.5	03	04	02.5	49	01.9	.	.	01	02.0	.	.	15	02.7	.	.	14	01.4	10
II	-	-02.5	03.6	-00.7	-00.1	04.8	-05.0	10.6	06	-22.5	17	02	01.5	31	01.9	.	.	01	01.0	.	.	06	02.8	.	.	35	02.2	09
III	-	-00.8	05.4	01.2	01.7	06.3	-02.0	15.0	21	-13.0	08	04	02.2	46	01.8	03	02.7	05	02.8	.	.	09	01.9	.	.	20	01.6	06
IV	-	04.5	11.9	06.8	07.5	12.9	02.4	24.6	19,18	-06.6	04	02	03.0	37	01.8	03	03.3	08	03.6	.	.	05	03.0	.	.	30	02.3	05
V	-	08.4	16.2	10.4	11.3	17.5	04.9	23.5	18	-02.4	03	04	02.5	32	01.6	02	01.5	07	03.4	.	.	04	03.2	.	.	30	01.6	14
VI	-	14.4	22.2	16.2	17.3	23.8	11.2	29.2	22	03.4	03	02	02.0	20	01.5	09	01.8	18	02.2	.	.	.	.	.	.	22	01.6	19
VII	-	14.1	22.7	16.1	17.3	24.1	10.8	31.5	23	04.8	06	.	.	34	01.8	02	01.5	13	02.2	.	.	02	03.5	.	.	22	01.8	20
VIII	-	14.1	23.1	16.7	17.6	24.2	12.7	32.5	07	07.2	27,26	.	.	34	01.9	03	02.7	.	.	.	.	01	01.0	.	.	30	01.9	25
IX	-	10.5	20.9	12.7	14.2	21.6	09.1	28.2	11	-00.6	29	.	.	33	01.6	16	02.2	04	03.2	.	.	03	03.7	.	.	19	02.1	15
X	-	04.5	15.3	06.5	08.2	15.9	02.5	27.2	11	-03.8	25	06	02.7	31	01.7	16	02.3	02	04.0	.	.	.	.	.	.	20	01.6	18
XI	-	03.3	11.1	05.3	06.2	11.6	01.7	19.0	04	-04.6	11	11	01.8	26	01.3	06	02.8	05	04.0	.	.	02	03.5	.	.	25	02.0	15
XII	-	-02.9	01.5	-01.7	-01.2	03.0	-04.5	12.0	01	-16.0	26	03	02.3	33	01.6	29	01.7	01	01.0	.	.	07	01.9	.	.	04	01.8	16
GOD.	-	05.6	13.0	07.4	08.3	14.0	03.4	32.5	7.VIII	-22.5	17.II	38	02.2	406	01.7	89	02.1	65	02.8	.	.	54	02.6	.	.	271	01.9	172

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlim)	Temperatura broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dlim)	Min	Padavine R mm Σ	Max	Dan	Broj dana s: Tm ≤ 0,0	Tx ≤ 0,0	Tm ≤ 0,0	Tx ≥ 0,0	Tx ≥ 0,0	Tm ≥ 0,0	F(0-12) ≥ 6	≥ 8	Nm(0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	✱	✱	✱	▲	▲	⚡	≡	▦
BR. ST. 31 — RAKITNA																																					
I	9.3	9.1	8.7	9.0	-	-	-	-	-	-	-	132	035.8	06	01	13	23	.	.	.	.	.	.	25	18	13	04	11	10	01	.	.	.	.	.	10	15
II	7.1	7.4	5.6	6.7	-	-	-	-	-	-	-	090	020.0	15	08	10	25	.	.	.	03	.	02	09	18	10	03	06	14	01	.	.	01	.	02	06	22
III	7.5	8.1	6.7	7.4	-	-	-	-	-	-	-	259	058.3	04	08	05	25	.	.	.	.	.	01	15	21	18	08	06	17	.	.	.	.	.	01	05	31
IV	7.0	6.5	5.6	6.4	-	-	-	-	-	-	-	278	044.2	06	01	01	11	.	.	.	.	.	03	10	19	16	10	15	09	03	.	.	03	.	08	02	16
V	5.4	6.8	4.7	5.6	-	-	-	-	-	-	-	091	019.0	22	.	.	09	.	.	.	.	.	04	06	15	13	03	14	01	.	.	.	.	.	08	02	01
VI	4.6	6.4	5.2	5.4	-	-	-	-	-	-	-	093	027.7	19	.	.	01	03	.	.	.	.	02	06	12	08	03	12	.	.	.	.	.	.	14	01	.
VII	3.1	5.4	3.1	3.8	-	-	-	-	-	-	-	174	065.6	16	.	.	.	08	.	.	.	.	11	03	09	07	05	09	.	.	.	.	.	.	04	01	.
VIII	5.1	5.9	3.7	4.9	-	-	-	-	-	-	-	206	052.4	31	.	.	.	04	.	.	.	.	07	07	15	12	06	.	.	.	.	.	.	.	12	11	.
IX	3.7	4.5	4.8	4.3	-	-	-	-	-	-	-	019	007.7	27	.	.	03	.	.	.	.	.	09	04	06	04	.	06	.	.	.	.	.	.	04	05	.
X	5.6	5.3	2.8	4.6	-	-	-	-	-	-	-	106	042.4	21	.	.	15	.	.	.	01	.	05	04	05	05	04	05	01	.	.	.	01	.	03	05	02
XI	7.4	6.4	6.4	6.7	-	-	-	-	-	-	-	120	031.3	16	.	.	10	.	.	.	01	.	02	12	10	08	06	10	01	01	.	.	.	.	02	07	.
XII	5.3	5.5	5.1	5.3	-	-	-	-	-	-	-	142	030.8	30	11	11	29	.	.	.	.	.	10	12	14	12	05	06	12	02	.	.	.	.	02	06	24
GOD.	5.9	6.4	5.2	5.8	-	-	-	-	-	-	-	1710	065.6	46 VII	29	40	151	16	.	.	05	.	56	113	162	126	57	100	65	08	.	.	05	.	60	61	111
BR. ST. 32 — GONANCE																																					
I	7.1	6.2	6.5	6.6	-	-	-	-	-	-	-	441	100.2	12	02	04	22	.	.	.	.	.	08	15	16	13	10	12	07	02	.	.	.	.	.	10	15
II	7.3	7.0	8.3	7.6	-	-	-	-	-	-	-	159	028.0	15	04	07	21	.	.	.	02	.	02	18	20	19	06	10	13	03	01	.	01	.	01	06	22
III	6.4	7.3	6.2	6.6	-	-	-	-	-	-	-	378	110.8	04	06	05	25	.	.	.	01	.	05	13	20	18	09	09	16	02	.	.	.	.	03	05	31
IV	7.1	6.3	5.3	6.2	-	-	-	-	-	-	-	362	061.4	14	01	01	14	.	.	.	.	.	08	11	16	15	12	13	10	03	.	.	.	.	03	02	25
V	4.2	7.3	5.3	5.6	-	-	-	-	-	-	-	116	028.3	23	.	.	04	.	.	.	.	.	05	09	17	15	02	17	01	01	.	.	.	.	03	02	.
VI	5.1	6.7	4.9	5.6	-	-	-	-	-	-	-	114	020.2	03	.	.	.	.	.	.	.	.	05	09	15	13	06	15	.	.	.	.	.	.	06	02	.
VII	3.1	5.4	3.7	4.1	-	-	-	-	-	-	-	154	070.2	16	.	.	.	06	.	.	02	.	12	08	10	08	04	10	.	.	.	.	.	.	01	02	.
VIII	4.4	7.2	4.6	5.4	-	-	-	-	-	-	-	249	091.3	31	.	.	.	04	.	.	.	.	08	09	14	14	08	14	.	.	.	.	.	.	06	04	.
IX	4.1	4.2	3.4	3.9	-	-	-	-	-	-	-	041	030.3	17	.	.	01	.	.	.	04	.	09	03	05	03	01	05	.	.	.	.	.	.	.	06	.
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	7.5	6.8	5.9	6.7	-	-	-	-	-	-	-	440	155.3	15	.	.	12	.	.	.	02	01	05	15	10	09	08	09	02	01	.	.	02	.	02	11	.
XII	5.0	5.2	4.2	4.8	-	-	-	-	-	-	-	371	200.1	30	06	06	27	.	.	.	01	.	14	12	14	11	07	07	12	03	.	.	.	.	.	01	10
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 33 — NOVA VAS NA BLOKAH																																					
I	9.6	8.1	8.8	8.8	-	04.3	98	95	99	97	73	088	023.0	06	01	13	23	.	.	.	.	.	.	23	16	12	02	10	08	01	01	.	.	.	.	07	17
II	7.5	7.1	5.6	6.7	-	03.9	90	84	92	88	29	095	027.6	15	08	07	25	.	.	.	01	.	03	09	19	11	05	07	15	03	.	.	.	.	.	07	22
III	7.9	7.9	6.1	7.3	-	04.4	93	86	96	92	43	232	051.2	04	08	01	26	.	.	.	.	.	02	16	21	18	10	04	18	.	.	.	.	.	.	08	31
IV	7.5	7.0	5.3	6.6	-	05.8	93	70	91	85	33	228	035.8	30	01	01	14	.	.	.	01	.	.	11	17	15	09	14	08	01	.	.	.	.	02	05	16
V	4.8	6.5	4.9	5.4	-	07.3	90	69	90	83	12	065	017.4	22	.	.	10	.	.	.	.	.	04	05	15	12	01	14	01	.	.	.	.	.	04	.	.
VI	4.7	6.4	4.8	5.3	-	11.8	92	76	92	87	61	160	053.3	16	.	.	.	06	.	.	.	.	03	05	12	11	05	12	.	.	.	.	.	.	08	.	.
VII	4.0	5.7	2.8	4.2	-	11.8	92	72	89	84	55	141	052.4	16	.	.	.	13	.	.	.	.	07	03	08	07	04	08	.	.	.	.	.	.	02	03	.
VIII	4.3	6.4	3.6	4.8	-	11.9	97	71	93	87	03	166	064.7	31	.	.	.	10	.	.	.	.	06	04	12	11	05	12	.	.	.	.	.	.	08	07	.
IX	4.8	4.4	3.3	4.2	-	09.2	92	64	89	82	45	020	010.8	17	.	.	04	01	.	.	.	.	09	02	06	04	01	06	.	.	.	.	.	.	01	06	.
X	5.9	5.1	1.8	4.3	-	06.6	91	66	89	82	41	083	038.7	21	.	.	14	.	.	.	01	.	05	02	06	06	03	06	01	.	.	.	.	.	01	04	02
XI	7.0	6.1	5.6	6.2	-	05.9	91	72	92	85	36	095	031.7	16	.	.	11	.	.	.	.	.	03	11	11	08	02	11	.	.	.	.	.	.	.	08	.
XII	6.2	5.5	5.0	5.6	-	03.5	92	83	92	89	15	115	020.2	30	13	10	28	.	.	.	.	.	09	10	14	13	04	06	11	.	.	.	.	.	.	07	24
GOD.	6.2	6.4	4.8	5.8	-	07.2	92	75	92	86	03	1488	064.7	34 VIII	31	32	155	30	.	.	03	.	51	101	157	128	51	110	62	05	01	.	.	.	26	62	112
BR. ST. 34 — BABNO POLJE																																					
I	8.6	7.3	7.9	8.0	-	04.1	94	86	94	91	61	160	058.0	06	03	12	24	.	.	.	.	.	02	21	16	14	06	10	07	.	.	.	.	.	.	03	14
II	7.1	6.8	5.2	6.4	-	03.6	88	79	89	85	38	124	031.7	15	10	08	25	.	.	.	.	.	04	10	16	12	05	06	13	.	.	.	.	.	01	02	21
III	7.6	8.4	7.4	7.8	-	04.0	92	79	94	88	38	211	062.1	04	08	01	27	.	.	.	.	.	02	20	20	17	06	06	16	.	.	.	.	.	.	03	31
IV	7.5	7.5	5.4	6.8	-	05.2	91	66	92	83	25	298	058.2	06	01	01	17	.	.	.	.	.	03	12	20	18	10	16	08	.	.	.	01	.	.	02	20
V	5.3	7.4	5.4	6.0	-	06.9	88	66	91	82	39	076	018.1	23	.	.	11	.	.	.	01	.	03	10	16	14	01	15	01	.	.	.	.	.	04	.	.
VI	5.6	7.1	4.6	5.8	-	10.8	91	66	94	83	45	094	021.2	19	.	.	01	07	.	.	.	.	02	08	13	10	03	13	.	.	.	.	.	.	10	.	.
VII	4.0	5.7	3.2	4.3	-	10.9	92	62	93	82	38	137	064.4	16	.	.	.	09	01	.	01	.	11	07	08	07	05	08	.	.	.	.	.	.	03	01	.
VIII	6.0	6.9	4.3	5.7	-	11.4	96	66	96	86	40	193	070.2	31	.	.	.	08	.	.	.	.	04	09	14	12	07	14	.	.	.	.	.	.	11	07	.
IX	5.9	4.2	3.7	4.6	-	08.9	95	61	91	82	38	018	007.5	17	.	.	05	.	.	.	.	.	07	05	08	04	.	08	.	.	.	.	.	.	01	08	.
X	6.6	4.7	2.5	4.6	-	06.1	93	63	93	83	34	116	075.4	21	.	.	17	.	.	.	01	.	05	05	06	05	03	06	01	.	.	.	01	.	03	06	01
XI	8.2	6.1	6.0	6.8	-	05.5	92	71	91	85	41	205	066.1	15	.	.	15	.	.	.	.	.	03	16	11	08	06	11	01	.	.	.	.	.	.	08	01
XII	6.2	5.7	4.4	5.4	-	03.4	92	76	89	86	37	171	068.2	30	12	08	28	.	.	.	.	.	06	10	14	13	04	05	12	.	.	.	.	.	.	04	13
GOD.	6.6	6.5	5.0	6.0	-	06.7	92	70	92	84	25	1803	075.4	31 X	34	30	170	24	01	.	03	.	52	133	162	134	56	118	59	.	.	.	02	.	33	44	101
BR. ST. 35 — KOČEVJE																																					
I	9.8	8.8	9.1	9.2	-	04.5	94	93	95	94	63	069	029.6	07	02	10	23	.	.	.	01	.	.	25	18	10	02	11	08	.	.	.	.	.	.	08	14
II	8.3	6.5	5.8	6.8	-	04.2	89	78	91	86	45	130	033.5	15	07	03	23	.	.	.	02	.	.	10	15	11	06	05	11	.	.	.	.	.	02	10	22
III	8.1	7.8	7.1	7.7	-	04.6	92	73	94	87	37	201	062.6	04	03	.	22	.	.	.	01	.	.	17	21	15	07	08	15	.	.	.	.	.	02	05	26
IV	8.1	6.9	5.5	6.8	-	06.1	90	61	85	79	31	281	037.9	14	.	.	07	.	.	.	04	.	02	12	19	19	09	16	07	03	.	.	.	.	01	03	08
V	5.3	6.4	5.0	5.6	-	07.8	87	59	86	77	39	080	016.1	27	.	.	05	.	.	.	02	.	07	10	18	13	03	17	02	01	.	.	.	.	04	05	.
VI	5.4	6.5	3.8	5.2	-	12.5	94	68	89	83	43	072	016.4	19	.	.	.	12	.	.	.	.	03	04	19	10	02	19	.	.	.	.	.	.	12	06	.
VII	4.9	5.0	3.1	4.3	-	12.6	94	66	89	83	46	176	065.8	16	.	.	.	17	02	.	.	.	09	06	10	09	05	10	.	.	.	.	.	01	04	07	.
VIII	8.8	6.1	3.3	6.1	-	13.0	97	68	91	85	40	237	053.9	31	.	.	.	13	02	.	.	.	03	09	12	11	07	12	.	.	.	.	.	.	11	17	.
IX	7.5	3.8	2.7	4.6	-	10.1	92	61	86	80	45	024	008.1	01	.	.	01	09	.	.	.	.	05	03	06	04	.	06	.	.	.	.	.	.	01	12	.
X	7.4	4.5	2.3	4.7	-	07.2	95	66	88	83	50	094	035.8	21	.	.	07	03	.	.	.	.	04	04	08	06	03	08	01	.	.	.	.	.	03	13	01
XI	8.2	6.2	5.5	6.6	-	06.3	92	74	90	85	48	111	041.3	22	.	.	10	.	.	.	01	.	03	15	12	08	04	12	.	.	.	.	.	.	02	11	.
XII	8.5	6.4	7.4	7.4	-	04.0	92	89	92	91	53	111	022.5	28	05	07	27	.	.	.	.	.	03	17	15	13	05	07	08	.	02	.	.	.	01	13	10
GOD.	7.5	6.2	5.0	6.2	-	07.7	92	71	89	84	31	1586	065.8	46 VII	17	20	125	54	04	.	11	.	39	132	173	129	53	131	52	04	02	.	.	01	43	110	81

H_o = 787 m H_b = - m h_o = 1.8 m h_b = 1.5 m

H_o = 937 m H_b = - m h_o = 2.0 m h_b = 1.5 m

H_o = 722 m H_b = - m h_o = 2.0 m h_b = 1.5 m

H_o = 756 m H_b = - m h_o = 2.0 m h_b = 1.5 m

H_o = 461 m H_b = - m h_o = 2.0 m h_b = 1.5 m

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm: 7	14	21	Srednji dnevni	Max	Min	Apsolutni max	Datum	Apsolutni min	Datum	Učestina pravaca i srednja jačina vetra nD, Fm (0-12): N δ.	N j.	NE δ.	NE j.	E δ.	E j.	SE δ.	SE j.	S δ.	S j.	SW δ.	SW j.	W j.	NW δ.	NW j.	C δ.
NOVO MESTO-GOTNA VAS BR. ST. 36																											
φ = 45° 48' N λ = 15° 11' E Gr. ΔG = + 1h 01 min.																											
I	742.6	-01.7	01.1	-00.7	-00.5	02.3	-02.6	13.9	06	-10.8	03	.	.	44	01.4	13	01.4	18	01.3	08	01.8	03	01.7	01	01.0	03	01.0	03
II	739.8	-02.5	03.6	-00.1	00.2	05.0	-04.2	13.4	09,06	-18.4	17	.	.	33	01.5	04	01.2	26	01.7	06	02.7	10	02.3	02	01.0	02	02.0	01
III	740.9	00.3	06.4	02.6	03.0	07.5	00.6	16.3	24	-08.5	08	02	01.5	29	01.8	07	01.4	24	01.3	08	02.2	14	02.2	01	03.0	07	01.1	01
IV	742.2	05.4	12.7	07.7	08.4	14.2	03.4	25.7	19	-04.5	04	02	02.0	36	01.9	02	02.0	18	01.5	09	02.3	13	02.8	03	01.7	07	01.4	.
V	743.7	09.1	16.9	11.0	12.0	18.3	05.3	23.2	14	-02.4	01	04	01.8	36	01.6	07	01.3	19	01.1	08	02.1	11	02.5	04	02.2	04	01.5	.
VI	744.6	15.9	22.4	16.9	18.0	24.4	11.9	29.8	17	04.4	03	04	02.0	36	01.5	02	03.0	26	01.5	07	01.6	09	02.1	05	01.6	.	.	01
VII	743.8	15.8	23.9	17.6	18.7	25.1	12.1	31.1	23	07.0	06	02	01.0	28	01.4	07	01.1	26	01.3	08	01.5	12	02.4	02	02.0	06	01.0	02
VIII	743.5	15.6	23.9	17.7	18.7	24.8	13.9	32.6	06	08.7	27	05	01.2	44	01.2	04	01.2	22	01.3	06	01.8	05	01.0	02	01.0	04	01.2	01
IX	747.1	11.2	21.3	13.3	14.8	21.8	09.7	29.1	11	-01.2	30	02	01.0	35	01.7	08	01.4	24	01.2	03	01.3	12	02.0	.	.	03	01.3	.
X	747.1	04.7	15.4	07.5	08.8	16.2	03.2	27.4	10	-03.1	17	02	01.5	41	01.5	10	01.4	22	01.2	08	02.0	07	02.0	02	02.5	01	03.0	.
XI	744.8	04.6	11.7	06.3	07.2	12.6	02.8	20.1	14	-03.6	27	01	02.0	23	01.2	03	01.3	30	01.5	12	02.4	11	02.7	03	02.3	03	02.3	04
XII	748.1	-02.4	02.0	-01.6	-00.9	02.6	-03.9	13.4	02	-12.1	27,26	01	01.0	36	01.4	04	01.0	22	01.0	05	01.0	07	01.7	05	01.6	09	01.4	04
GOD.	744.0	06.3	13.4	08.2	09.0	14.6	04.4	32.6	6.VIII	-18.4	17.II	25	01.5	421	01.5	71	01.4	277	01.3	88	02.0	114	02.2	30	01.8	49	01.4	17
ČRNOMELJ BR. ST. 37																											
φ = 45° 34' N λ = 15° 12' E Gr. ΔG = + 1h 01 min.																											
I	-	-01.3	00.9	-00.4	-00.3	02.1	-02.6	10.9	27	-08.4	08	07	01.9	03	01.0	05	01.4	02	01.5	.	.	02	02.0	03	02.0	01	02.0	70
II	-	-00.6	04.5	01.3	01.6	06.0	-02.9	13.8	09	-15.6	17	02	01.0	07	01.7	03	01.7	.	.	06	02.7	12	04.2	02	01.5	.	.	52
III	-	01.3	07.3	04.1	04.2	08.6	00.1	18.3	24	-07.7	08	09	01.7	01	01.0	02	01.5	06	01.5	06	02.0	22	02.1	06	01.8	01	01.0	40
IV	-	06.3	13.7	09.3	09.7	15.2	04.6	27.0	19	-03.3	04	10	01.5	05	02.2	07	01.9	.	.	07	02.3	21	02.5	05	02.0	01	05.0	34
V	-	10.2	17.7	12.4	13.2	19.0	07.0	24.2	14	-02.3	01	06	02.2	09	02.4	10	02.2	02	01.5	07	02.1	18	02.4	09	02.1	01	02.0	31
VI	-	17.2	23.8	18.8	19.7	25.3	13.4	30.5	28,23	05.5	03	02	02.5	05	02.4	02	02.5	05	02.4	11	01.7	06	03.2	05	02.8	03	02.3	51
VII	-	16.6	24.6	19.1	19.9	26.2	13.0	32.5	23	07.8	19	04	01.2	06	02.0	08	01.6	07	02.4	12	02.2	04	05.2	03	01.3	.	.	49
VIII	-	16.4	24.9	19.3	19.9	26.0	14.2	35.1	07	08.3	27	02	01.5	05	02.0	05	01.8	11	01.8	08	01.8	04	03.0	02	01.5	.	.	56
IX	-	11.8	22.0	15.3	16.1	22.7	10.0	31.1	11	-00.8	30	05	02.0	02	02.0	14	01.9	03	01.7	08	02.1	08	02.6	02	02.0	.	.	48
X	-	06.2	16.0	09.8	10.5	16.9	04.6	26.0	09	-02.7	23	02	02.0	10	02.1	08	02.0	05	01.6	03	02.0	09	03.4	05	02.4	.	.	51
XI	-	06.2	12.4	08.1	08.7	13.1	04.2	21.1	04	-03.7	27	05	02.2	09	01.9	04	01.8	.	.	05	02.2	18	03.4	06	02.2	.	.	43
XII	-	-01.7	02.4	-00.1	00.1	03.4	-02.9	16.3	01	-09.3	27	05	02.2	04	02.0	04	01.2	01	02.0	07	01.6	05	03.0	02	01.0	04	01.8	61
GOD.	-	07.4	14.2	09.8	10.3	15.4	05.2	35.1	7.VIII	-15.6	17.II	59	01.8	66	02.0	72	01.8	42	01.9	80	02.0	129	02.9	50	02.0	11	02.2	586
GORNJI LENART BR. ST. 38																											
φ = 45° 56' N λ = 15° 34' E Gr. ΔG = + 1h 02 min.																											
I	-	-01.8	00.7	-01.0	-00.8	01.6	-03.2	07.3	05	-08.6	03	01	01.0	23	01.4	15	01.4	17	01.2	.	.	13	01.2	02	01.0	10	01.1	12
II	-	-01.9	03.6	-00.3	00.3	04.8	-03.8	14.1	09	-14.6	17	01	02.0	17	02.0	10	01.6	04	02.0	04	02.8	20	01.8	14	03.4	05	01.6	09
III	-	01.4	07.7	03.7	04.1	08.6	00.0	18.7	24	-05.3	08	01	04.0	18	01.8	07	01.9	07	01.1	05	01.6	26	02.1	05	01.4	06	01.3	18
IV	-	06.2	13.4	08.0	08.9	14.9	03.8	26.5	19	-03.1	04	.	.	15	01.6	04	01.8	09	01.7	01	02.0	26	01.7	08	02.0	10	01.4	17
V	-	10.0	17.7	11.2	12.5	18.9	06.3	24.1	14	-00.7	01	.	.	11	01.5	05	01.8	06	01.2	02	01.0	31	01.6	10	01.6	10	01.3	18
VI	-	16.8	24.0	17.4	18.9	25.4	13.0	30.4	23	04.6	04	01	01.0	08	02.1	03	01.3	07	01.0	02	01.0	23	01.3	17	01.4	05	01.0	24
VII	-	16.4	24.4	17.7	19.0	25.7	12.5	30.7	14	08.0	06	.	.	17	01.5	06	01.0	11	01.2	01	01.0	22	01.2	07	01.9	10	01.2	19
VIII	-	16.2	24.4	18.2	19.3	25.6	14.4	33.1	07	09.5	27,26	.	.	17	01.3	04	01.5	11	01.4	02	01.0	14	01.4	12	01.3	12	01.1	21
IX	-	11.9	21.5	13.7	15.2	22.1	10.0	30.1	11	-00.4	29	.	.	19	01.3	10	01.4	08	01.6	.	.	15	01.3	08	01.2	04	01.0	26
X	-	05.5	15.5	07.3	08.9	16.2	03.4	25.2	09	-03.5	17	02	01.0	10	01.7	07	01.4	09	01.3	03	02.0	21	02.0	08	01.9	04	01.0	29
XI	-	04.9	11.9	06.6	07.5	12.5	03.0	20.1	14,04	-03.4	17	.	.	06	01.2	04	01.2	09	01.1	.	.	29	02.0	13	02.0	14	01.4	15
XII	-	-02.3	01.8	-01.4	-00.8	03.1	-04.1	13.1	02	-14.6	27	.	.	10	02.2	04	01.0	08	01.2	02	01.5	19	01.3	08	01.2	16	01.2	26
GOD.	-	06.9	13.9	08.4	09.4	15.0	04.6	33.1	7.VIII	-14.6	17.II	06	01.2	171	01.6	79	01.5	106	01.3	22	01.7	259	01.6	112	01.8	106	01.2	234
SR HRVATSKA **KOSTEL** BR. ST. 39																											
φ = 46° 11' N λ = 15° 45' E Gr. Δ G = + 1h 03 min.																											
I	-	-01.5	00.3	-01.2	-00.9	01.1	-03.1	08.6	05	-08.1	03	02	01.0	12	01.0	48	01.1	09	01.0	01	01.0	03	01.0	16	01.0	02	01.0	.
II	-	-01.6	02.9	00.4	00.6	03.8	-03.3	12.1	09	-14.8	17	01	01.0	04	01.0	27	01.1	10	01.0	02	01.0	08	01.1	28	01.0	03	01.0	01
III	-	01.4	06.6	03.1	03.6	07.0	00.1	16.5	22	-05.6	08	.	.	.	.	25	01.2	10	01.0	04	01.2	19	01.0	35	01.0	.	.	.
IV	-	06.3	13.1	07.9	08.8	13.8	04.1	24.0	23,19	-02.9	04	.	.	02	01.0	13	01.2	02	01.0	01	01.0	15	01.0	49	01.1	08	01.0	.
V	-	10.1	16.9	11.0	12.2	17.8	06.6	23.5	14	-01.0	01	.	.	01	02.0	10	01.0	05	01.2	02	01.0	13	01.0	55	01.1	07	01.3	.
VI	-	16.2	23.1	16.5	18.1	23.9	12.6	30.0	17	05.4	03	.	.	02	01.0	25	01.1	04	01.2	05	01.0	10	01.1	34	01.0	09	01.2	01
VII	-	17.0	23.1	17.0	18.5	24.2	13.0	28.8	24,23	08.4	16	.	.	03	01.0	05	01.2	25	01.1	13	01.0	05	01.0	11	01.0	31	01.0	.
VIII	-	16.9	23.3	17.6	18.8	23.7	14.3	30.8	06	09.8	26	01	02.0	03	01.0	16	01.0	12	01.0	04	01.0	16	01.0	39	01.1	02	01.0	.
IX	-	12.0	19.7	13.6	14.7	20.3	09.7	28.2	11	-00.1	30	01	03.0	08	01.0	29	01.1	14	01.1	03	01.0	06	01.0	18	01.1	10	01.6	01
X	-	05.9	13.3	07.4	08.5	13.7	04.0	22.8	09	-02.6	19	01	01.0	02	01.0	27	01.0	23	01.0	04	01.0	15	01.0	21	01.0	.	.	.
XI	-	06.0	10.3	07.0	07.6	11.1	03.8	17.0	14	-01.9	17	.	.	02	01.0	23	01.0	21	01.0	02	01.0	13	01.0	28	01.0	01	01.0	.
XII	-	-01.8	00.9	-00.9	-00.7	01.8	-03.2	10.9	01	-12.3	25	.	.	17	01.0	20	01.1	05	01.0	.	.	05	01.0	30	01.1	16	01.1	.
GOD.	-	07.2	12.8	08.3	09.2	13.5	04.9	30.8	6.VIII	-14.8	17.II	06	01.5	56	01.0	268	01.1	140	01.0	41	01.0	128	01.0	364	01.1	89	01.1	03
VARAŽDIN BR. ST. 40																											
φ = 46° 18' N λ = 16° 21' E Gr. Δ G = + 1h 05 min.																											
I	745.4	-02.5	00.1	-01.5	-01.3	02.0	-04.5	11.1	05	-15.4	03	06	01.3	09	01.3	15	01.5	08	01.5	23	01.7	09	01.2	11	01.0	.	.	12
II	742.3	-01.2	03.8	00.8	01.1	05.1	-02.7	14.4	09	-13.0	20,17	13	01.8	10	01.8	04	01.8	04	01.0	19	01.7	14	01.7	10	01.4	08	01.1	02
III	743.4	02.0	07.1	03.9	04.2	08.3	01.0	18.7	24	-04.0	06	13	01.8	06	01.3	07	01.4	03	01.0	13	01.7	24	01.8	15	01.5	09	01.7	03
IV	744.6	06.6	13.2	09.0	09.4	15.0	04.5	25.4	19	-05.5	04	10	02.6	04	01.2	04	01.2	09	01.4	07	02.0	22	01.8	16	01.2	14	01.6	04
V	746.0	11.0	17.4	12.6	13.4	18.9	07.6	23.9	13	-00.2	01	08	02.0	09	02.6	04	01.2	02	01.5	07	02.0	22	02.2	17	01.6	17	01.7	07
VI	746.9	17.5	23.9	18.2	19.4	25.1	13.7	31.1	22	06.9	03	13	02.2	08	01.5	06	01.7	02	02.0	13	01.5	12	01.3	15	01.1	13	01.5	08
VII	746.3	17.2	23.9	18.6	19.6	25.5	13.4	31.5	23	08.4	27	12	02.4	06	02.2	01	01.0	03	02.0	09	01.6	14	01.6	17	01.2	10	01.5	21
VIII	746.0	16.9	24.1	18.4	19.4	25.5	14.6	32.9	06	09.0	26	07	02.1	10	01.1	04	01.5	10	01.3	15	01.3	08	01.1	09	01.1	07	01.4	23
IX	749.7	12.1	21.1	14.1	15.3	21.9	10.2	30.4	11	-00.6	30	05	02.0	07	01.7	04	01.2	04	01.2	08	01.9	08	01.6	13	01.2	16	01.1	25
X	749.4	06.3	14.7	08.3	09.4	15.6	04.4	24.4	10,09	-03.4	19	11	02.0	03	02.0	03	01.3	05	01.0	15	02.3	20	01.7	10	01.2	06	01.0	20
XI	747.0	05.8	12.6	07.9	08.5	13.6	03.9	20.1	03	-02.0	07	03	03.0	05	01.4	04	01.2	05	01.4	18	02.1	25	02.0	18	01.3	02	01.5	10
XII	750.8	-01.6	02.3	-00.7	-00.1	03.6	-03.7	11.8	06,01	-15.4	25,24	11	02.9	03	02.0	01	02.0	09	01.1	09	01.9	26	01.3	15	01.3	05	01.2	14
GOD.	746.5	07.5	13.7	09.1	09.9	15.0	05.2	32.9		-15.4		112	02.2	80	01.7	57	01.4	64	01.3	156	01.8	204	01.7	166	01.3	107	01.4	149

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlss)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dlss)	min	Padavine R mm Σ	max	mat.	Broj dana s a: Tn ≤ -10,0	Tn ≤ -5,0	Tn ≤ 0,0	Tx ≤ 0,0	Tx ≤ 10,0	Tn ≤ 20,0	F(0-12) ≥ 6	≥ 8	Nm(0-10) < 2.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	≋	✱	≋	≋	▲	▲	T	≡	≡
BR. ST. 36 NOVO MESTO-GOTNA VAS																																					
I	9.6	9.0	9.5	9.4	034.8	04.1	93	85	92	90	64	047	010.3	07	01	13	27	.	.	.	01	.	.	28	15	09	01	10	07	01	.	02	01	.	01	14	20
II	8.3	7.2	7.3	7.6	084.2	03.9	92	67	88	82	35	084	019.2	11	04	03	23	.	.	.	04	.	01	16	17	09	04	07	14	01	01	.	.	.	02	09	23
III	8.2	8.4	7.3	8.0	093.1	04.8	95	70	88	84	27	127	026.6	05	.	.	21	.	.	.	01	.	01	21	18	15	05	13	13	03	01	.	.	.	01	09	19
IV	7.9	7.5	5.9	7.1	127.0	06.2	90	57	80	75	27	152	025.4	29	.	.	05	01	.	.	04	.	.	10	20	15	07	18	06	01	.	.	.	02	05	03	04
V	6.0	6.7	5.5	6.1	207.4	07.8	88	53	84	75	35	066	009.9	23	.	.	04	.	.	.	01	.	01	08	18	13	.	17	01	01	.	.	.	03	10	08	.
VI	5.4	6.7	5.6	5.9	233.9	12.5	88	63	88	80	39	166	088.8	19	.	.	.	14	.	.	01	.	01	07	14	13	04	14	.	.	.	.	.	02	16	07	.
VII	3.9	5.3	3.4	4.2	277.4	12.5	89	56	85	77	37	117	040.2	16	.	.	.	20	03	.	02	.	08	04	08	07	06	08	.	.	.	.	.	01	05	07	.
VIII	7.5	5.9	5.0	6.1	190.4	13.9	97	65	95	86	41	184	033.2	31	.	.	.	15	03	.	01	.	02	09	15	11	06	12	.	.	.	.	.	.	14	18	.
IX	7.0	4.4	3.9	5.1	211.2	10.5	96	57	93	82	42	020	008.0	27	.	.	01	08	.	.	.	.	06	06	09	04	.	06	.	.	.	.	.	.	03	18	.
X	7.0	5.3	3.7	5.3	167.4	07.4	97	59	93	83	40	080	029.0	21	.	.	09	02	.	.	01	.	07	06	08	05	03	08	01	01	.	.	.	.	03	16	01
XI	7.5	6.3	6.9	6.9	096.2	06.5	92	67	91	83	36	059	023.7	22	.	.	07	.	.	.	.	.	01	11	09	06	02	08	.	.	.	.	.	.	01	10	.
XII	8.5	7.2	7.3	7.7	053.0	04.0	95	82	93	90	26	059	016.1	28	04	09	28	.	.	.	.	.	02	19	15	11	01	09	09	01	.	02	01	.	01	12	10
GOD.	7.2	6.7	5.9	6.6	1776.0	07.8	92	65	89	82	26	1161	088.8	19 VI	09	25	129	60	06	.	16	.	30	145	166	118	39	130	51	09	02	04	02	08	64	131	77
BR. ST. 37 ČRNOMELJ																																					
I	9.8	9.4	9.4	9.5	-	04.1	94	86	91	90	61	078	027.5	07	.	10	26	.	.	.	.	.	.	28	21	10	02	13	09	01	02	.	.	.	.	22	29
II	8.0	7.3	7.3	7.5	-	04.3	86	73	86	82	43	126	043.5	15	03	02	21	.	.	.	01	.	01	11	15	11	03	06	12	.	01	03	.	.	02	17	21
III	7.8	7.9	6.9	7.5	-	05.0	91	68	82	81	30	164	024.8	20	.	.	15	.	.	.	01	.	01	16	19	14	07	13	15	04	02	.	.	.	01	12	-
IV	7.5	6.9	6.5	7.0	-	06.3	85	57	72	71	25	172	033.5	14	.	.	01	03	.	.	01	.	.	11	18	13	08	16	05	01	.	.	.	.	01	03	.
V	5.7	6.6	6.4	6.2	-	07.9	82	52	75	70	29	053	018.3	23	.	.	01	.	.	.	01	.	03	12	17	09	02	17	01	.	.	.	.	.	08	03	.
VI	5.0	6.3	5.4	5.5	-	12.5	82	59	76	72	35	065	016.7	08	.	.	.	18	03	.	.	.	02	07	13	09	02	13	.	.	.	.	.	.	15	02	.
VII	3.8	4.8	3.9	4.1	-	12.7	85	56	77	73	34	115	053.5	16	.	.	.	21	05	.	02	.	10	04	09	06	05	09	.	.	.	.	.	01	04	04	.
VIII	5.9	5.5	6.0	5.8	-	13.9	93	60	87	80	10	135	037.0	31	.	.	.	16	04	.	.	.	03	09	12	10	05	12	.	.	.	.	.	.	08	06	.
IX	6.3	4.5	5.9	5.6	-	10.6	92	55	84	77	35	024	007.3	01	.	.	01	12	02	.	.	.	04	06	06	04	.	06	.	.	.	.	.	.	01	11	.
X	7.1	5.2	5.1	5.8	-	07.9	94	61	86	81	47	093	028.3	02	.	.	05	02	.	.	01	.	03	06	09	08	03	09	01	01	.	.	.	.	03	10	.
XI	8.0	6.6	7.3	7.3	-	06.8	86	67	85	80	44	049	017.8	15	.	.	04	.	.	.	01	.	03	12	07	05	02	07	.	.	.	.	.	.	02	08	.
XII	8.4	7.5	8.3	8.1	-	04.2	93	81	90	88	30	079	026.3	30	.	07	26	.	.	.	01	.	02	20	15	14	01	08	09	02	02	.	01	.	02	20	10
GOD.	6.9	6.5	6.5	6.7	-	08.0	88	64	82	78	10	1153	053.5	16 VII	03	19	100	72	14	.	09	.	32	142	161	113	40	129	92	09	07	03	01	01	47	118	-
BR. ST. 38 GORNJI LENART																																					
I	9.9	9.3	9.3	9.5		008.7	04.1	96	88	93	93	75	058	011.3	01	.	11	25	.	.	.	01	.	.	28	13	11	02	08	06	.	.	.	.	.	.	07	18
II	8.5	6.8	7.0	7.4		064.1	04.2	93	73	90	85	41	078	024.1	11	02	02	21	.	.	.	01	01	02	13	11	11	03	03	10	.	.	.	.	.	01	02	-
III	8.0	7.6	5.9	7.2		076.2	05.1	94	67	85	82	26	126	026.0	05	.	.	16	.	.	.	.	.	04	16	15	15	04	11	09	02	.	.	.	.	.	04	05
IV	7.8	7.3	4.7	6.6		121.5	06.6	88	60	84	77	23	131	019.9	03	.	.	04	01	.	.	03	.	01	09	18	13	07	16	04	.	.	.	.	01	01	.	02
V	5.3	5.3	3.6	4.7		185.5	08.0	86	52	82	73	32	062	016.9	22	.	.	02	.	.	.	.	.	06	05	14	13	01	14	.	.	.	.	.	.	03	01	.
VI	4.0	4.8	3.3	4.0		217.2	12.8	86	57	87	77	38	092	046.5	19	.	.	.	17	04	.	.	.	12	06	13	10	03	13	.	.	.	.	.	.	05	.	.
VII	3.3	4.1	2.7	3.4		252.9	13.1	88	58	87	78	32	125	033.6	16	.	.	.	20	04	.	01	.	16	05	08	07	04	08	.	.	.	.	.	01	.	.	.
VIII	6.8	5.1	3.7	5.2		184.9	14.3	96	65	92	85	46	236	042.1	09	.	.	.	16	03	.	.	.	05	07	14	10	08	14	.	.	.	.	.	.	08	09	.
IX	7.3	3.7	2.6	4.5		161.4	11.1	94	60	92	82	44	043	013.2	27	.	.	01	09	01	.	.	.	05	03	08	05	02	08	.	.	.	.	.	.	.	12	.
X	6.5	4.1	2.9	4.5		124.2	07.6	96	63	95	85	41	082	034.6	21	.	.	08	01	.	.	.	.	09	05	08	06	03	08	.	.	.	.	.	.	03	08	.
XI	7.4	6.0	5.7	6.4		073.6	06.7	94	71	91	85	39	078	031.1	15	.	.	06	.	.	.	.	.	04	11	08	08	03	08	.	.	.	.	.	.	.	05	.
XII	7.9	7.1	6.8	7.3		024.3	04.1	94	86	94	91	36	063	019.5	28	04	07	28	.	.	.	01	.	03	17	12	09	01	06	06	.	.	.	.	.	.	13	10
GOD.	6.9	5.9	4.8	5.9		1494.5	08.1	92	66	89	82	23	1174	046.5	19 VI	06	20	111	64	12	.	07	01	67	125	142	118	41	117	35	02	.	.	.	02	21	61	-
BR. ST. 39 KOSTEL																																					
I	9.4	8.9	7.8	8.7	-	04.2	96	90	96	94	66	043	010.6	25	.	14	26	.	.	.	.	.	.	22	12	10	01	06	07	.	.	.	.	.	.	07	19
II	7.2	7.7	6.5	7.2	-	04.6	96	85	97	92	64	064	025.9	11	02	05	21	.	.	.	.	.	02	14	14	09	02	03	12	.	.	.	.	.	.	03	16
III	7.5	7.7	6.8	7.3	-	05.5	93	78	97	90	33	133	021.5	19	.	.	19	.	.	.	.	.	03	15	14	12	07	12	10	07	.	.	.	.	.	01	10
IV	7.6	7.3	5.7	6.8	-	07.9	97	72	96	89	40	126	020.0	03	.	.	04	.	.	.	.	.	04	14	18	15	05	15	04	.	.	.	.	01	04	02	02
V	5.1	6.7	3.3	5.0	-	08.9	87	66	92	81	34	060	016.6	22	.	.	02	.	.	.	.	.	06	06	12	10	01	12	.	.	.	.	.	.	07	01	.
VI	5.6	5.6	3.1	4.8	-	12.9	91	64	88	81	29	106	041.1	19	.	.	.	13	01	.	.	.	08	07	13	10	04	13	.	.	.	.	.	.	08	.	.
VII	3.5	3.9	2.8	3.4	-	12.9	88	62	86	78	42	140	044.9	26	.	.	.	16	.	.	.	.	17	05	07	07	04	07	.	.	.	.	.	01	04	.	.
VIII	7.2	5.8	5.4	6.1	-	14.2	95	67	94	85	52	195	051.6	25	.	.	.	12	02	.	.	.	04	10	16	10	08	16	.	.	.	.	.	.	10	03	.
IX	6.5	4.1	4.5	5.0	-	10.8	94	66	88	82	51	059	023.7	17	.	.	01	04	.	.	.	.	08	07	09	05	03	09	.	.	.	.	.	.	03	07	.
X	4.7	3.3	2.9	3.7	-	07.5	96	68	93	86	51	073	046.2	21	.	.	05	.	.	.	.	.	11	05	07	07	01	07	.	.	.	.	.	.	03	02	.
XI	7.3	6.8	7.1	7.1	-	07.2	97	73	97	89	53	082	033.4	22	.	.	05	.	.	.	.	.	02	14	08	06	03	08	.	.	.	.	.	.	.	02	.
XII	7.5	7.5	6.4	7.1	-	04.2	96	86	96	93	62	047	014.3	28	03	12	24	.	.	.	.	.	04	16	12	09	01	06	08	.	.	.	.	.	.	09	10
GOD.	6.6	6.3	5.2	6.0	-	08.4	93	73	93	86	29	1128	051.6	15 VIII	05	31	107	45	03	.	.	.	69	135	142	110	40	114	41	07	.	.	.	02	39	37	57
BR. ST. 40 VARAŽDIN																																					
I	9.2	8.1	8.1	8.5		034.4	03.7	89	81	87	85	61	049	012.1	01	05	12	25	.	.	.	.	.	01	21	14	09	01	06	10	01	.	.	.	.	.	14	31
II	8.0	7.1	7.5	7.5		074.8	04.0	86	69	80	78	45	066	018.0	11	02	04	19	.	.	.	02	.	01	16	16	10	02	07	12	01	.	.	.	.	01	03	19
III	7.7	8.3	6.8	7.6		100.8	04.8	85	64	81	76	28	106	017.2	05	.	.	12	.	.	.	.	.	01	18	15	13	06	12	09	02	.	.	.	.	.	04	12
IV	7.7	7.8	6.7	7.4		138.9	06.3	82	57	74	71	34	120	025.7	03	.	.	02	01	.	.	03	.	.	12	19	14	03	16	04	.	.	.	.	.	03	.	01
V	5.0	6.7	5.3	5.7		216.6	07.7	77	51	73	67	33	088	030.5	17	.	.	01	.	.	.	07	.	02	08	14	08	03	14	.	.	.	.	.	02	07	03	.
VI	4.6	6.6	6.0	5.7		253.9	12.1	78	55	77	70	39	111	070.0	19	.	.	.	15	02	.	.	.	06	08	11	07	03	11	.	.	.	.	.	.	07	01	.
VII	4.5	4.9	3.9	4.4		262.7	12.4	81	55	78	72	37	086	022.2	17	.	.	.	19	04	.	04	.	10	05	10	10	03	10	.	.	.	.	.	.	03	03	.
VIII	5.5	5.9	4.0	5.2		208.5	13.7	89	62	89	80	44	148	063.1	25	.	.	.	15	03	.	.	.	07	09	14	11	06	14	.	.	.	.	.	.	08	01	.
IX	4.4	4.3	2.8	3.8		209.6	10.2	89	55	85	76	41	049	014.3	07	.	.	02	09	01	01	01	.	11	03	10	08	02	10	.	.	.	.	.	.	03	01	.
X	6.3	5.9	3.7	5.3		145.2	07.2	89	61	86	79	45	058	036.2	21	.	.	05	.	.	.	.	.	06	07	07	05	01	07	01	01	.	.	.	01	01	06	01
XI	7.5	6.4	6.0	6.6		112.4	06.3	86	61	79	75	34	049	017.0	16	.	.	06	.	.	.	03	.	.	08	09	05	02	09	.	.	.	.	.	.	.	07	.
XII	7.8	7.0	6.8	7.2		051.5	04.0	89	79	89	86	29	040	013.9	26	04	04	25	.	.	.	02	.	02	15	11	09	01	07	06	01	.	01	.	.	.	16	10
GOD.	6.5	6.6	5.6	6.2		1809.3	07.7	85	62	81	76	28	970	070.0	19 VI	11	20	95	59	10	01	22	.	47	130	150	109	33	123	42	06	.	01	.	03	33	59	71

Mesec	Vazdušni pritisak Fm mb	Temperatura vazduha °C Fm 7	14	21	Srednji dnevni	Max	Min	Amp.	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-13) N		NE		E		SE		S		SW		W		NW		C
												f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.	j.		j.	f.	j.	f.
φ = 46° 02' N λ = 16° 33' E Gr. ΔG = + 1h 07 min.																												
KRIŽEVCI																												
I	748.0	-02.9	-00.2	-01.6	-01.6	01.2	-04.5	07.2	15	-13.0	08	06	02.0	27	02.5	10	02.2	10	01.9	08	02.1	22	02.0	02	02.0	08	02.0	.
II	744.9	-01.3	02.8	00.7	00.7	04.1	-02.7	13.0	09	-09.0	20	06	03.2	25	03.0	08	02.5	.	.	12	02.2	23	02.8	01	02.0	09	02.0	.
III	745.8	01.5	07.6	04.5	04.5	08.5	00.5	18.1	24	-06.0	02	14	02.5	25	03.2	06	02.7	03	02.0	13	02.4	22	03.2	04	03.8	06	02.3	.
IV	747.1	06.3	13.0	08.9	09.3	14.8	04.0	25.2	19	-03.5	04	16	04.4	13	03.1	01	03.0	02	02.5	09	02.6	20	02.9	09	02.6	20	02.2	.
V	748.4	10.6	17.1	11.9	12.9	18.2	07.0	23.0	08	-01.2	01	20	03.3	13	02.4	01	02.0	06	02.3	11	02.2	21	02.9	09	03.4	12	02.2	.
VI	749.2	17.2	24.0	17.9	19.3	24.9	13.6	30.5	22	08.6	05	16	03.0	22	03.1	04	02.8	03	02.0	13	02.2	15	02.7	03	02.0	14	02.1	.
VII	748.5	17.3	23.6	18.6	19.5	25.2	13.5	30.4	11	08.1	27	30	03.2	14	02.8	01	03.0	06	02.0	11	02.1	17	02.3	01	02.0	13	02.9	.
VIII	748.2	16.8	24.1	18.4	19.4	24.9	14.2	31.0	06	08.5	27	18	02.7	20	02.5	08	01.8	07	02.6	03	01.7	11	02.4	04	02.2	22	02.0	.
IX	752.0	11.6	20.7	13.5	14.8	21.3	09.4	29.5	11	-01.7	30	17	02.9	19	02.5	06	02.3	06	01.7	04	02.2	19	02.6	.	.	19	01.9	.
X	752.0	05.3	14.5	08.2	09.1	15.3	03.3	24.6	11,10	-02.5	25,19	08	02.6	22	02.5	07	02.3	08	02.6	16	02.2	21	02.8	02	03.0	09	02.0	.
XI	749.6	05.3	11.8	07.2	07.9	12.5	03.2	19.5	14	-02.0	27,07	11	02.5	08	02.9	05	02.6	03	02.0	15	02.5	37	03.2	04	03.2	07	01.9	.
XII	753.0	-01.1	01.7	-00.6	-00.2	02.4	-03.2	12.5	02	-13.5	27	10	03.7	18	03.0	05	02.0	04	02.0	09	02.1	31	02.0	05	02.6	11	02.4	.
GOD.	748.9	07.2	13.4	09.0	09.6	14.4	04.9	31.0	6 VIII	-13.5	27 XII	172	03.1	226	02.8	62	02.3	58	02.2	124	02.3	259	02.7	44	02.8	150	02.2	.
φ = 46° 10' N λ = 16° 50' E Gr. ΔG = + 1h 07 min.																												
KOPRIVNICA																												
I	-	-02.7	00.3	-02.0	-01.6	01.7	-05.0	08.2	15	-15.9	03	16	02.1	06	01.7	07	01.6	22	01.9	08	01.9	22	02.2	.	.	09	02.1	03
II	-	-01.0	03.4	00.4	00.8	05.3	-02.7	12.6	09	-10.1	20	22	02.5	08	02.6	02	02.0	07	01.9	05	01.8	36	02.7	.	.	03	03.3	01
III	-	02.4	08.0	04.1	04.6	09.4	01.1	19.2	24	-04.9	02	16	02.7	11	02.4	03	02.3	03	02.0	08	02.2	36	02.7	03	02.0	12	02.2	01
IV	-	07.2	14.0	08.6	09.6	15.7	04.7	26.0	19	-02.8	04	26	02.8	03	02.0	02	02.0	01	02.0	10	02.0	34	02.3	03	03.0	11	02.8	.
V	-	11.4	18.1	11.8	13.3	19.5	07.8	25.0	15	00.6	01	17	02.7	03	02.0	02	03.0	.	.	10	02.1	40	02.7	01	02.0	20	02.6	.
VI	-	18.2	24.9	17.7	19.6	26.2	14.0	32.1	22	07.8	03	13	02.6	02	03.0	04	01.5	03	02.3	10	02.0	30	02.2	02	02.0	26	02.3	.
VII	-	17.6	24.7	18.3	19.7	26.6	13.6	32.0	23	09.4	27	13	03.5	.	.	03	02.0	07	02.0	08	01.8	31	02.2	06	02.2	25	02.8	.
VIII	-	17.5	25.1	18.3	19.8	26.3	14.6	32.0	07,06	09.6	27,19	18	02.2	05	02.2	07	02.0	09	02.0	24	01.8	11	02.1	02	02.0	17	02.6	.
IX	-	12.3	22.0	13.7	15.4	23.1	10.0	30.1	11	-06.2	29	17	02.2	05	02.6	02	01.5	05	01.8	13	01.7	32	02.4	02	02.0	14	02.2	.
X	-	06.8	15.1	08.2	09.6	15.9	04.5	26.0	10	-03.2	17	10	03.1	02	02.0	03	01.3	05	02.0	11	02.5	50	02.9	.	.	12	02.2	.
XI	-	06.0	12.3	08.0	08.5	13.2	03.8	20.0	03	-02.5	07	04	02.8	02	01.0	01	02.0	14	01.9	04	03.8	53	02.9	03	02.0	09	02.2	.
XII	-	-00.9	02.5	-00.2	00.3	03.8	-02.8	15.0	01	-11.7	27	20	03.0	03	02.0	.	.	08	01.9	09	02.3	47	02.4	.	.	06	02.2	.
GOD.	-	07.9	14.2	08.9	10.0	15.6	05.3	32.1	22 VI	-15.9	5 I	192	02.7	50	02.2	36	01.9	84	01.9	120	02.0	422	02.5	22	02.2	164	02.5	05
φ = 45° 14' N λ = 13° 36' E Gr. ΔG = + 54 min.																												
POREČ																												
I	-	04.9	08.5	05.7	06.2	09.5	02.7	14.8	12	-03.4	23	05	01.4	06	01.2	30	01.5	21	02.0	04	02.2	03	02.7	16	02.2	08	01.8	.
II	-	02.8	07.7	03.8	04.5	08.7	-00.2	13.0	05	-05.7	17	05	02.2	09	02.1	28	01.5	18	02.0	01	03.0	08	02.2	13	02.4	02	03.0	.
III	-	05.7	10.0	06.4	07.1	11.0	02.8	16.0	24	-02.0	01	04	02.0	08	01.9	26	01.9	18	02.8	13	02.8	06	02.3	13	02.4	05	02.8	.
IV	-	09.6	14.0	09.4	10.6	14.9	05.5	21.0	19	00.5	06,03	04	02.0	12	02.4	14	01.9	21	02.0	10	03.1	06	02.5	13	02.3	10	02.1	.
V	-	13.7	17.4	12.4	14.0	18.8	08.6	23.0	18	01.0	02	04	02.5	08	01.8	25	01.8	20	02.4	06	02.7	07	02.7	14	02.7	09	02.2	.
VI	-	20.8	24.4	19.1	20.8	25.3	15.3	29.3	21	07.0	03	01	01.0	08	01.2	13	01.3	24	01.9	10	02.7	10	02.8	17	02.4	07	02.0	.
VII	-	21.7	25.4	19.6	21.6	26.4	15.5	30.7	30,15	10.0	16	05	02.0	13	01.8	18	01.9	11	02.1	12	02.2	10	03.0	19	02.7	05	02.8	.
VIII	-	21.3	25.6	20.2	21.8	26.6	16.9	31.0	07,06	12.0	25	03	02.3	10	01.4	23	01.5	17	01.7	06	02.0	10	02.2	18	02.7	06	02.3	.
IX	-	17.0	23.7	17.6	19.0	24.2	13.7	29.2	12,11	05.6	29	05	02.2	10	01.9	29	01.5	15	01.8	03	02.7	08	03.1	16	02.8	04	02.0	.
X	-	10.3	17.6	10.8	12.3	18.3	07.1	23.7	08	-00.8	18,17	06	01.7	08	01.9	31	01.6	15	01.9	06	02.5	08	02.6	18	02.2	01	02.0	.
XI	-	09.3	13.7	09.8	10.6	14.5	06.6	18.0	19	01.5	26,24	01	03.0	08	02.0	31	01.4	25	01.9	05	03.2	06	01.5	12	02.2	02	02.0	.
XII	-	03.9	09.2	04.7	05.7	10.2	01.1	14.3	01	-05.6	26	06	02.2	18	02.2	32	01.5	11	01.9	06	02.3	07	02.6	08	02.1	05	02.6	.
GOD.	-	11.8	16.4	11.6	12.8	17.4	08.0	31.0	6 VIII	-05.7	17 II	49	02.0	118	01.9	300	01.6	216	02.0	82	02.6	89	02.5	177	02.4	64	02.2	.
φ = 45° 05' N λ = 13° 39' E Gr. ΔG = + 55 min.																												
ROVINJ																												
I	-	04.6	09.3	05.4	06.2	10.0	02.9	14.8	12	-03.0	23	26	01.3	12	01.5	02	01.0	29	01.6	04	01.2	07	01.7	01	03.0	03	01.3	09
II	-	02.1	09.1	03.5	04.5	09.8	00.2	13.6	06	-06.5	17	27	01.4	13	01.2	14	01.6	10	01.6	02	02.5	06	02.0	02	01.0	10	01.4	.
III	-	05.4	10.9	06.1	07.1	12.2	02.7	17.0	24	-02.6	01	13	01.4	21	01.9	10	02.1	25	02.1	08	03.0	04	02.0	01	01.0	10	01.8	01
IV	-	09.3	15.0	09.6	10.9	16.1	06.0	21.4	26	-05.0	06	12	01.5	09	01.6	10	01.8	23	01.9	13	02.5	10	01.7	01	02.0	05	02.2	07
V	-	14.0	18.7	12.4	14.4	19.8	09.0	23.4	18	02.7	01	13	01.5	18	01.6	11	01.5	19	01.7	.	.	08	02.1	08	01.8	07	01.0	09
VI	-	19.9	24.9	19.4	20.9	26.2	14.9	30.0	27,26	08.0	02	07	01.4	14	01.7	04	01.5	23	01.5	09	02.0	08	02.0	02	02.0	10	01.4	13
VII	-	21.0	26.4	19.4	21.6	27.5	15.3	31.5	30,12	10.2	18	23	01.6	09	01.3	03	02.0	16	02.1	07	02.6	02	02.0	02	01.5	11	01.9	20
VIII	-	20.4	27.3	20.0	21.9	28.2	16.6	32.9	15	11.8	26	15	01.0	15	01.3	07	01.7	10	01.8	04	03.5	10	01.7	05	02.4	12	02.0	15
IX	-	16.0	24.8	17.3	18.8	25.3	13.8	29.2	11	06.1	29	14	01.4	09	01.2	22	01.3	12	01.9	05	02.2	06	02.5	03	02.3	12	01.8	07
X	-	10.1	18.9	11.6	13.1	19.5	07.4	24.6	08	01.0	18,17	12	01.8	16	01.9	17	02.1	17	02.4	01	05.0	02	02.5	06	02.0	19	01.9	03
XI	-	09.1	14.2	09.8	10.7	-	06.5	-	-	00.9	29	06	02.0	22	01.7	17	01.8	18	02.8	05	03.4	03	01.0	06	02.2	11	01.6	02
XII	-	04.0	09.6	05.1	05.9	-	02.0	-	-	-05.5	26	16	01.7	30	02.0	10	01.8	16	02.8	04	04.5	02	03.0	03	03.7	12	02.5	.
GOD.	-	11.3	17.4	11.6	13.0	-	08.1	-		-06.5	17 II	184	01.5	188	01.6	127	01.7	218	02.0	62	02.7	68	01.9	40	02.1	122	01.8	86
φ = 45° 14' N λ = 13° 56' E Gr. ΔG = + 56 min.																												
PAZIN																												
I	732.4	02.2	07.6	03.7	04.3	08.7	00.5	12.7	18	-07.7	23	.	.	07	01.6	05	02.0	14	02.7	03	02.3	04	01.5	05	01.4	01	02.0	54
II	730.7	00.0	06.6	02.1	02.7	07.7	-02.1	12.5	06	-09.5	17	04	02.0	05	02.4	09	01.8	07	01.9	10	02.0	08	02.2	05	01.8	01	01.0	35
III	731.6	01.9	08.2	04.6	04.8	09.6	00.3	14.6	21	-06.2	08	03	02.3	03	01.7	06	02.3	25	02.6	14	02.6	04	02.2	04	02.8	01	02.0	33
IV	733.5	06.2	13.4	08.3	09.0	14.6	04.1	22.6	19	-03.4	04	01	02.0	08	01.9	04	02.5	16	02.3	13	02.2	09	02.9	05	02.4	02	01.5	32
V	735.2	09.8	17.0	11.2	12.3	19.2	06.4	23.7	20	-01.8	02	02	02.5	06	01.8	10	01.9	13	02.2	10	02.8	11	01.7	03	02.0	02	02.5	36
VI	736.0	16.0	23.9	17.8	18.9	25.5	12.7	30.4	27	05.8	05	03	02.7	06	02.3	07	01.9	08	02.1	04	02.2	10	02.3	09	02.1	.	.	43
VII	735.0	15.9	25.9	18.4	19.7	27.1	12.7	34.2	24	06.4	18	04	02.0	11	02.0	05	02.0	13	02.5	07	02.1	10	01.8	10	01.9	03	03.0	30
VIII	734.9	15.3	25.6	18.2	19.3	27.0	13.6	33.4	06	09.5	27	03	01.3	05	01.4	04	01.8	09	02.2	07	01.3	06	02.2	10	01.8	02	03.0	47
IX	737.9	11.6	23.8	15.0	16.4	24.6	10.3	28.0	12	00.0	30	.	.	06	02.2	06	01.2	14	02.0	02	01.0	05	02.0	08	01.5	02	01.5	47
X	738.0	05.6	17.4	08.5	10.0	18.3	04.0	28.0	12,11	-03.4	25	.	.	05	01.8	05	02.0	07	02.6	06	02.0	08	01.8	03	01.3	06	01.3	53
XI	736.4	05.2	13.0	07.1	08.1	14.0	03.1	19.2	27	-04.0	26	01	02.0	04	01.5	02	01.0	13	02.2	12	02.5	07	02.0	06	01.3	04	01.8	41
XII	737.6	-00.1	08.0	01.3	02.6	09.3	-02.5	16.0	12	-10.8	26	.	.	15	01.8	10	02.2	02	02.0	06	02.2	04	01.5	08	01.1	01	01.0	47
GOD.	734.9	07.5	15.9	09.7	10.7	17.1	05.3	34.2	24 VII	-10.8	16 XII	21	02.1	81	01.9	73	01.9	141	02.3	94	02.2	86	02.0	76	01.8	25	01.9	498

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dias)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dias)	Min	Padavine R mm Σ	Max	Datum	Broj dana s: Tn ≤ 0,0	Tn < 0,0	Tn < 0,0	Tx ≥ 0,0	Tx ≥ 0,0	Tx ≥ 0,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	✱	⊥	⊥	≈	▲	▲	⊓ T	■	■
BR. ST. 41						**KRIŽEVCI**																															
I	9.7	8.9	8.2	8.9	011.9	03.7	92	86	88	88	32	074	016.3	01	04	13	29	.	.	.	01	01	.	24	15	12	02	07	09	01	.	.	.	.	.	12	31
II	7.9	7.5	7.4	7.6	072.2	04.1	89	76	83	83	49	059	017.9	11	.	03	23	.	.	.	05	01	02	16	15	10	02	09	10	04	.	.	.	.	01	04	17
III	7.6	7.9	6.3	7.3	109.1	05.0	90	64	81	78	28	110	019.0	28	.	.	13	.	.	.	05	01	03	15	15	14	04	12	07	04	.	.	.	.	.	08	05
IV	7.8	7.1	5.2	6.7	149.9	06.4	85	57	76	73	29	095	020.7	29	.	.	03	01	.	.	13	04	01	10	13	11	04	12	03	01	.	.	.	01	02	05	.
V	6.1	6.4	5.3	5.9	214.2	08.0	82	55	78	72	35	055	011.6	06	.	.	01	.	.	.	07	02	02	07	12	10	01	12	01	01	.	.	.	.	07	04	.
VI	5.0	5.6	5.2	5.3	290.0	12.5	82	55	84	74	37	072	022.8	19	.	.	.	17	02	.	02	.	04	07	10	09	02	10	.	.	.	.	.	.	12	.	.
VII	4.6	4.5	3.6	4.2	276.5	12.6	81	56	82	73	44	084	028.5	16	.	.	.	19	01	.	05	01	10	04	09	07	03	09	.	.	.	.	.	.	03	01	.
VIII	5.3	5.4	4.8	5.2	219.7	14.0	92	64	90	82	48	122	039.1	25	.	.	.	15	02	.	02	01	06	07	11	09	05	11	.	.	.	.	.	.	12	02	.
IX	5.6	4.3	3.6	4.5	221.1	10.5	92	58	90	80	45	020	009.0	27	.	.	01	07	.	.	01	01	08	07	10	06	.	10	.	.	.	.	.	.	03	02	.
X	7.3	5.3	4.3	5.6	151.8	07.5	94	66	89	83	54	040	017.1	21	.	.	07	.	.	.	02	.	05	06	08	04	02	08	.	.	.	.	.	.	02	15	.
XI	8.2	6.7	6.1	7.0	090.5	06.5	89	69	85	81	43	057	022.0	16	.	.	04	.	.	.	04	.	.	10	10	07	02	10	.	.	.	.	.	.	01	12	.
XII	8.8	8.1	7.9	8.3	-	04.2	93	85	91	90	35	044	013.3	28	04	09	25	.	.	.	02	.	01	23	15	11	01	10	07	.	.	.	.	.	01	17	10
GOD.	7.0	6.5	5.7	6.4	-	07.9	88	65	84	79	28	832	039.1	25 VIII	08	25	106	59	05	.	51	12	42	136	143	110	28	120	37	11	.	.	.	01	44	82	63
BR. ST. 42						**KOPRIVNICA**																															
I	9.1	8.3	8.5	8.6	-	03.6	89	81	87	86	61	082	019.5	01	08	11	27	.	.	.	.	.	01	24	11	11	03	03	08	.	.	.	.	.	.	15	31
II	8.4	7.6	7.4	7.8	-	04.0	86	73	82	80	49	072	015.5	15	01	02	21	.	.	.	.	.	01	16	13	13	03	06	09	.	.	.	.	.	01	02	22
III	7.3	8.1	6.3	7.2	-	05.1	86	65	83	78	33	122	020.8	28	.	.	10	.	.	.	01	.	.	14	16	13	05	12	09	.	.	.	.	.	.	04	10
IV	7.1	7.4	4.7	6.4	-	06.5	81	55	77	71	27	110	024.8	29	.	.	02	01	.	.	02	.	01	10	15	13	04	13	02	.	.	.	.	.	04	01	01
V	6.1	7.2	5.9	6.4	-	08.0	79	51	79	70	29	052	010.8	22	.	.	.	01	.	.	02	.	02	09	12	10	01	12	01	01	.	.	.	.	06	02	.
VI	4.5	6.7	4.6	5.3	-	12.6	78	54	83	72	34	039	007.3	19	.	.	.	21	04	.	.	.	03	05	13	11	.	13	.	.	.	.	.	.	08	.	.
VII	4.4	5.1	3.0	4.2	-	12.7	82	55	82	73	39	118	039.2	01	.	.	.	24	10	.	01	.	09	04	09	08	03	09	.	.	.	.	.	.	03	.	.
VIII	6.1	5.4	4.2	5.2	-	14.0	89	60	88	79	28	083	023.4	25	.	.	.	19	06	.	.	.	06	06	14	10	03	14	.	.	.	.	.	.	07	02	.
IX	5.2	4.2	3.1	4.2	-	10.5	90	56	84	77	39	048	017.2	05	.	.	01	12	01	.	.	.	08	03	10	06	03	10	.	.	.	.	.	.	02	02	.
X	6.9	5.6	3.7	5.4	-	07.5	91	61	87	79	31	030	016.1	21	.	.	06	02	.	.	03	.	06	08	07	04	01	07	.	.	.	.	.	.	01	05	.
XI	8.4	6.9	5.7	7.0	-	06.7	88	69	81	79	39	060	021.0	16	.	.	04	.	.	.	05	.	.	12	08	07	02	08	.	.	.	.	.	.	01	04	.
XII	9.0	7.7	8.2	8.3	-	04.2	90	83	89	87	45	058	015.8	24	03	04	27	.	.	.	01	.	01	20	11	09	02	07	04	.	.	.	.	.	.	11	09
GOD.	6.9	6.7	5.4	6.3	-	08.0	85	63	83	77	27	874	039.2	4 VII	12	17	98	80	21	.	15	.	38	131	139	115	30	114	33	01	.	.	.	.	33	48	73
BR. ST. 43						**POREČ**																															
I	7.6	7.0	7.3	7.3	-	06.4	89	83	88	87	53	106	021.6	05	.	.	08	.	.	.	.	.	04	18	15	12	05	15	.	.	.	.	.	.	.	03	.
II	6.3	6.7	6.4	6.5	-	05.2	82	72	82	78	35	057	020.0	19	.	.	13	.	.	.	.	.	01	09	11	08	02	11	01	01	.	.	.	.	01	05	.
III	7.2	7.0	6.9	7.0	-	06.3	85	73	83	80	45	113	025.8	04	.	.	05	.	.	.	.	.	02	15	13	13	05	13	.	.	.	.	.	.	.	01	.
IV	5.6	5.3	4.6	5.2	-	07.6	83	65	80	76	44	111	041.4	22	.	.	.	.	.	.	.	.	03	04	11	09	03	11	.	.	.	.	.	.	01	.	.
V	4.3	5.8	4.7	4.9	-	09.6	83	67	83	77	46	074	023.0	23	.	.	.	.	.	.	.	.	05	06	15	13	02	15	.	.	.	.	.	.	03	.	.
VI	3.4	4.3	5.3	4.3	-	15.1	82	67	85	78	46	044	019.2	15	.	.	.	18	.	.	.	.	06	04	08	05	02	08	.	.	.	.	.	.	06	.	.
VII	2.2	3.8	3.6	3.2	-	14.5	73	61	80	71	47	031	013.8	16	.	.	.	21	03	.	01	.	11	03	06	04	01	06	.	.	.	.	.	.	.	.	.
VIII	3.9	4.7	3.5	4.0	-	15.5	78	67	85	77	47	162	036.4	22	.	.	.	24	03	02	.	.	10	03	10	10	07	10	.	.	.	.	.	.	06	.	.
IX	3.4	3.3	2.7	3.1	-	13.4	83	69	83	79	43	023	014.2	04	.	.	.	16	.	01	01	.	11	.	04	03	01	04	.	.	.	.	.	.	03	.	.
X	3.9	4.4	3.6	4.0	-	09.7	89	77	88	85	48	023	009.0	21	.	.	02	.	.	.	.	.	10	04	05	05	.	05	.	.	.	.	.	.	01	05	.
XI	6.9	6.3	6.2	6.4	-	08.7	89	83	90	88	57	091	026.3	16	.	.	.	.	.	.	.	.	07	14	09	08	05	09	.	.	.	.	.	.	02	06	.
XII	5.3	5.8	4.3	5.1	-	06.0	87	76	84	82	37	085	029.0	08	.	.	12	.	.	.	.	.	11	12	09	08	02	09	.	.	.	.	.	.	.	03	.
GOD.	5.0	5.4	4.9	5.1	-	09.8	83	71	84	79	35	920	041.4	22 IV	.	.	40	79	06	03	02	.	81	92	116	98	35	116	01	01	.	.	.	.	23	23	.
BR. ST. 44						**ROVINJ**																															
I	7.1	7.2	7.1	7.1	072.9	06.6	89	86	92	89	46	117	023.6	05	.	.	09	.	.	.	.	.	04	18	16	13	06	16	.	.	.	.	.	.	.	02	.
II	5.5	6.0	4.4	5.3	111.6	05.5	90	71	89	83	46	054	020.5	19	.	.	11	.	.	.	.	.	05	05	11	08	02	11	.	.	.	.	.	.	.	.	.
III	7.0	6.9	6.0	6.7	131.0	06.6	87	74	87	83	46	083	017.5	04	.	.	07	.	.	.	.	.	05	13	14	13	04	14	.	.	.	.	01	.	01	.	.
IV	5.5	5.2	5.0	5.2	203.8	08.2	88	67	87	81	37	122	043.6	22	.	.	01	.	.	.	01	.	04	08	14	08	04	14	01	.	.	.	.	.	01	.	.
V	4.4	4.4	4.8	4.5	262.4	09.8	82	66	81	76	46	057	021.5	23	.	.	.	.	.	.	.	.	07	06	09	08	02	09	.	.	.	.	.	.	02	.	.
VI	2.4	3.6	5.2	3.8	294.0	15.3	86	70	82	79	56	042	024.8	15	.	.	.	21	02	.	.	.	11	02	09	04	01	09	.	.	.	.	.	.	05	.	.
VII	2.5	3.3	2.5	2.8	354.0	15.4	78	69	78	75	39	044	019.2	16	.	.	.	24	06	.	.	.	19	03	04	04	02	04	.	.	.	.	.	.	03	.	.
VIII	4.2	4.0	2.3	3.5	288.7	15.3	81	62	83	75	31	124	034.2	24	.	.	.	28	11	.	.	.	12	03	10	10	05	10	.	.	.	.	.	01	07	.	.
IX	2.9	2.0	2.2	2.4	287.6	12.7	83	60	80	74	34	034	025.6	17	.	.	.	20	.	01	.	.	14	.	04	03	01	04	.	.	.	.	.	.	02	.	.
X	3.4	4.1	3.0	3.5	215.0	09.1	85	62	79	75	32	036	014.6	02	.	.	.	.	.	.	.	.	12	03	06	05	01	06	.	.	.	.	.	.	04	02	.
XI	6.8	6.4	6.1	6.4	100.7	08.4	91	71	92	84	49	072	022.0	16	.	-	.	-	-	.	.	.	06	12	10	09	03	10	.	.	.	.	.	.	02	02	.
XII	5.2	5.5	4.3	5.0	108.3	05.7	86	65	83	78	33	053	015.4	30	.	-	10	-	-	.	02	.	11	09	09	08	02	09	.	.	.	.	.	.	.	.	.
GOD.	4.7	4.9	4.4	4.7	2430.0	09.9	85	68	84	79	31	838	043.6	22 IV	.	-	38	-	-	01	03	.	110	82	116	93	33	116	01	.	.	.	01	01	27	06	.
BR. ST. 45						**PAZIN**																															
I	7.3	7.1	7.0	7.1	-	05.6	94	73	90	86	30	158	034.2	07	.	.	12	.	.	.	.	.	05	20	16	13	07	15	01	01	.	.	.	.	.	08	.
II	7.1	7.4	5.5	6.7	-	04.4	88	60	79	76	23	085	026.1	1[illegible]	.	.	19	.	.	.	.	.	02	10	16	13	03	16	02	01	.	.	02	.	03	04	02
III	7.1	7.7	6.9	7.2	-	05.2	89	64	82	78	24	163	037.7	04	.	.	15	.	.	.	.	.	04	16	17	15	05	16	03	02	.	.	01	.	02	05	01
IV	6.4	7.0	5.2	6.2	-	04.3	86	52	79	72	27	146	036.5	04	.	.	05	.	.	.	.	.	02	09	16	13	05	16	02	02	.	02	.	01	06	01	02
V	4.8	7.5	4.6	5.6	-	07.9	86	55	78	73	31	102	034.1	23	.	.	04	.	.	.	.	.	03	07	18	12	02	18	.	.	.	.	.	01	12	01	.
VI	4.1	6.7	5.0	5.3	-	12.8	92	59	84	78	37	110	065.6	25	.	.	.	21	02	.	.	.	03	07	15	09	02	15	.	.	.	.	01	02	14	.	.
VII	2.9	4.3	2.3	3.1	-	12.2	88	49	77	71	36	081	029.7	16	.	.	.	2[illegible]	11	.	.	.	14	02	05	05	04	05	.	.	.	.	.	.	03	.	.
VIII	3.8	6.2	2.7	4.2	-	13.5	96	59	87	81	40	144	041.4	10	.	.	.	2[illegible]	06	.	.	.	07	01	15	11	06	15	.	.	.	.	.	.	12	03	.
IX	3.6	3.5	2.0	3.0	-	10.9	94	50	87	77	30	023	011.1	2[illegible]	.	.	.	18	.	01	.	.	11	01	07	05	01	07	.	.	.	.	.	.	04	06	.
X	4.7	4.8	2.5	4.0	-	07.4	93	52	87	77	35	048	022.6	21	.	.	06	05	.	.	.	.	11	05	05	03	01	05	.	.	.	.	.	01	05	05	.
XI	6.7	6.5	5.5	6.2	-	07.0	94	66	90	83	29	094	029.8	16	.	.	2[illegible]	.	.	.	.	.	07	15	12	08	04	11	.	.	.	.	.	.	04	10	.
XII	5.2	5.5	4.2	5.0	-	04.8	92	63	90	82	34	094	028.1		01	.	2[illegible]	.	.	.	.	.	12	11	10	08	04	09	01	01	.	.	.	.	.	10	.
GOD.	5.3	6.2	4.4	5.3	-	08.2	91	58	84	77	23	1238	065.6	25 VI	01	.	92	86	19	01	.	.	81	104	152	115	44	148	09	07	.	02	04	05	65	53	05

H_o = 155 m H_b = 140,0 m h_s = 2,0 m h_r = 1,0 m

H_o = 149 m H_b = - m h_s = 2,0 m h_r = 1,0 m

H_o = 15 m H_b = - m h_s = 2,0 m h_r = 1,0 m

H_o = 5 m H_b = 16,0 m h_s = 2,0 m h_r = 1,0 m

H_o = 291 m H_b = 293,0 m h_s = 2,0 m h_r = 1,2 m

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nS, Fm (0-12): N b.	N j.	NE b.	NE j.	E b.	E j.	SE b.	SE j.	S b.	S j.	SW b.	SW j.	W j.	NW b.	NW j.	C b.
φ = 45° 20' N λ = 14° 27' E Gr. Δ G = + 58 min.																											
I	749.6	05.2	08.3	05.8	06.3	09.2	03.6	13.4	12	-03.8	22	04	01.0	39	01.7	06	02.3	04	02.2	09	02.0	05	01.2	.	.	07	01.1	19
II	747.9	04.1	07.6	05.1	05.5	08.8	02.6	14.2	06	-02.9	17	05	01.6	42	02.1	04	03.2	04	02.8	14	02.4	07	01.9	01	02.0	02	01.0	05
III	748.9	05.6	08.9	06.7	06.9	10.1	04.0	14.2	21,20	-01.1	02	05	01.4	40	02.4	03	02.3	14	02.4	10	02.5	09	01.2	03	02.0	03	02.3	06
IV	750.5	09.8	13.6	10.6	11.2	14.9	07.7	20.8	25	01.2	04	02	02.0	43	01.6	03	01.3	05	02.2	10	02.3	13	02.1	02	01.0	02	01.5	10
V	751.8	14.1	17.4	13.9	14.9	19.2	10.6	23.2	20	04.0	01	02	02.5	37	01.6	03	01.0	07	01.9	06	01.7	12	01.4	04	01.2	05	01.2	17
VI	752.6	19.8	24.4	20.0	21.1	25.5	16.6	31.1	27	09.4	03	06	01.2	22	01.4	05	01.2	06	01.5	04	01.5	14	01.4	02	01.0	05	01.2	26
VII	751.1	20.9	26.2	21.3	22.4	26.8	17.6	32.4	24,11	10.4	16	11	02.3	35	02.8	04	02.2	06	02.8	08	01.9	13	01.5	03	02.7	02	01.5	11
VIII	750.9	20.7	27.0	21.9	22.9	27.8	18.4	32.7	07	14.0	25	09	01.4	27	01.5	03	01.3	08	01.6	06	01.2	16	01.1	03	01.3	07	01.7	14
IX	754.3	16.8	24.3	18.7	19.6	24.7	15.4	28.8	11	07.0	30	11	02.2	37	02.3	08	02.5	01	03.0	03	01.3	14	01.1	.	.	03	01.0	13
X	754.8	11.4	17.5	12.5	13.5	18.0	09.6	27.5	12	03.0	25	16	01.8	29	02.1	07	02.4	08	02.1	05	01.8	11	01.4	02	01.0	02	01.5	13
XI	753.1	09.9	14.4	10.8	11.5	15.1	08.3	19.2	27	04.3	26,11	11	01.8	28	01.5	05	01.4	10	02.6	13	02.7	10	01.7	02	01.5	.	.	11
XII	754.7	04.9	09.1	05.7	06.3	10.1	03.3	15.4	10	-03.8	26	18	02.3	39	02.6	05	02.0	05	02.2	09	01.8	06	01.3	02	01.0	06	01.2	03
GOD.	751.7	11.9	16.6	12.8	13.5	17.5	09.8	32.7	7 VIII	-03.8	18 I	100	01.9	418	02.0	56	02.0	78	02.2	97	02.1	130	01.4	24	01.5	44	01.4	148
φ = 45° 36' N λ = 14° 38' E Gr. Δ G = + 59 min.																											
I	684.0	00.1	01.8	00.2	00.6	04.1	-02.9	12.2	06	-11.0	24	04	01.5	11	01.2	.	.	45	01.5	11	01.3	18	01.4	.	.	04	01.5	.
II	681.8	-01.2	02.6	-00.1	00.3	04.8	-04.2	10.0	23	-13.6	17	07	01.0	01	01.0	04	01.0	24	01.1	15	01.3	30	02.0	.	.	01	01.0	02
III	683.1	-00.3	03.7	00.9	01.3	05.6	-02.6	13.0	21	-10.0	01	07	01.0	04	01.0	01	01.0	24	01.1	42	01.1	11	01.2	.	.	.	.	04
IV	682.9	03.1	07.6	03.9	04.6	09.9	00.6	21.0	18	-06.0	04	05	01.2	02	01.5	.	.	21	01.3	34	01.6	14	02.3	.	.	06	01.7	06
V	685.2	07.5	12.0	07.5	08.6	14.1	03.7	18.2	20	-04.0	01	08	02.9	03	01.3	05	02.0	25	01.7	14	01.8	24	02.9	.	.	17	01.8	07
VI	689.7	14.3	18.9	14.2	15.4	20.8	10.0	25.2	23	04.5	03	12	01.6	04	01.2	01	01.0	15	01.8	24	02.0	21	02.2	.	.	05	01.6	06
VII	689.0	14.7	19.5	15.2	16.2	22.0	10.3	28.7	23	04.1	16	08	02.2	02	02.0	03	01.0	21	01.6	35	01.7	07	01.7	.	.	04	02.0	13
VIII	689.2	13.4	19.3	14.8	15.6	21.4	10.9	29.6	05	06.2	26,25	06	01.5	01	01.0	.	.	24	01.4	21	01.8	09	01.4	.	.	21	01.7	11
IX	692.8	10.4	16.6	11.6	12.6	18.2	07.7	22.9	12	00.2	30	04	01.8	.	.	.	.	28	01.6	36	01.7	15	01.9	.	.	01	01.0	06
X	690.2	06.7	12.8	07.8	08.8	14.3	03.5	23.5	11	-02.6	25	04	01.0	03	01.7	04	01.2	25	01.6	19	01.7	28	02.0	01	01.0	09	01.8	.
XI	687.7	04.5	08.1	05.6	06.0	09.4	02.4	17.5	04	-03.5	17	05	02.2	01	01.0	03	01.0	26	01.4	04	01.8	34	02.2	03	01.0	12	01.6	02
XII	689.4	-01.6	01.2	-01.1	-00.6	03.0	-04.4	11.7	01	-11.8	26	02	01.5	08	02.1	02	01.5	33	01.5	22	01.6	18	02.2	.	.	01	01.0	07
GOD.	687.1	06.0	10.3	06.7	07.4	12.3	02.9	29.6	5 VIII	-13.6	17 II	72	01.7	40	01.4	23	01.3	311	01.5	277	01.6	229	02.1	04	01.0	76	01.7	63
φ = 45° 10' N λ = 14° 42' E Gr. Δ G = + 59 min.																											
I	758.7	06.1	08.9	06.1	06.8	09.9	04.2	15.0	05	-02.2	23	01	02.0	33	01.8	.	.	10	02.0	18	01.6	.	.	16	01.4	12	01.5	03
II	756.9	04.8	08.5	05.9	06.3	09.4	03.1	13.5	06	-01.0	20	01	01.0	38	02.1	.	.	17	01.9	12	01.9	.	.	12	01.5	04	01.0	.
III	-	06.8	10.1	07.4	07.9	10.8	03.9	15.4	24	-02.0	07	03	01.0	48	02.3	.	.	09	02.2	14	02.7	.	.	14	01.5	04	01.0	01
IV	-	09.7	14.3	10.6	11.3	14.8	07.6	22.0	25	01.3	03	01	01.0	31	01.7	.	.	25	02.4	06	02.7	.	.	15	01.7	11	01.0	01
V	-	14.2	18.2	14.4	15.3	19.3	10.5	25.0	20	03.5	02,01	01	01.0	33	01.6	.	.	18	02.1	06	02.0	.	.	23	01.5	11	01.8	01
VI	-	19.8	25.2	20.4	21.4	26.0	16.7	31.7	28	09.2	03	02	02.0	31	01.4	01	01.0	20	02.0	03	01.0	02	02.0	16	01.2	11	01.2	04
VII	-	20.6	25.8	21.9	22.5	27.7	17.0	33.0	30,12	06.3	04	01	01.0	32	02.9	.	.	25	02.2	01	05.0	.	.	22	01.0	09	01.4	03
VIII	-	21.0	27.0	22.0	23.0	28.1	18.2	32.2	01	13.6	23	03	01.0	39	01.6	.	.	27	02.2	04	01.8	.	.	13	01.3	07	01.0	.
IX	-	18.6	24.7	19.5	20.6	25.7	16.0	32.3	13	06.5	30	02	01.5	53	02.2	.	.	21	02.4	04	02.0	.	.	03	02.0	07	01.1	.
X	-	12.1	17.9	13.4	14.2	19.2	09.4	27.2	12	03.0	25	.	.	36	02.0	.	.	24	01.6	04	02.8	.	.	09	01.1	12	01.4	08
XI	-	10.5	14.7	10.5	11.6	15.7	08.1	18.2	27	04.1	17	01	01.0	20	01.5	.	.	31	02.1	09	03.6	01	02.0	12	01.0	14	01.3	07
XII	-	05.5	09.9	05.4	06.5	10.9	03.1	16.5	04	-01.0	26	01	02.0	36	02.7	.	.	20	01.9	05	01.8	.	.	12	01.5	13	01.5	06
GOD.	-	12.5	17.1	13.1	14.0	18.1	09.8	33.0	18 VII	-02.2	15 I	17	01.3	430	02.0	01	01.0	247	02.1	86	02.2	03	02.0	167	01.3	115	01.3	29
φ = 45° 23' N λ = 14° 53' E Gr. Δ G = + 1h 00 min.																											
I	-	-01.9	00.2	-01.6	-01.3	02.1	-05.4	10.4	05	-19.2	08	03	01.3	02	01.5	22	01.9	10	01.6	12	02.3	15	02.1	10	01.5	12	01.6	07
II	-	-03.5	01.5	-01.7	-01.4	02.9	-07.6	07.8	05	-28.4	17	01	01.0	03	02.0	22	02.0	09	02.0	09	03.1	12	02.7	06	03.2	13	02.1	09
III	-	-02.9	02.6	-00.9	-00.5	04.2	-06.2	10.2	24,21	-21.6	08	04	01.2	02	01.5	27	01.7	12	01.8	10	01.8	11	02.3	09	01.7	09	01.3	09
IV	-	03.4	08.8	04.2	05.1	10.3	-00.5	21.6	19	-11.9	04	01	02.0	06	01.2	12	01.8	18	01.4	15	02.0	20	01.6	05	02.0	10	01.1	03
V	-	07.4	13.2	07.4	08.8	14.3	02.0	19.4	10	-06.5	01	03	01.3	05	01.8	23	01.6	19	01.4	03	01.0	14	01.6	11	01.6	15	01.5	.
VI	-	14.3	20.3	14.0	15.6	21.1	08.1	26.1	28	01.2	01	01	01.0	05	01.4	21	01.5	13	01.5	07	01.9	14	01.6	14	01.5	13	01.5	07
VII	-	13.0	20.2	13.2	14.9	21.6	07.1	29.9	23	01.5	18	.	.	12	01.7	23	01.5	20	01.4	04	01.5	12	02.1	07	01.1	12	01.1	03
VIII	-	12.9	21.0	13.7	15.3	21.9	08.4	28.5	07	02.1	26	02	01.5	09	01.3	23	01.3	10	01.2	11	01.5	06	01.3	12	01.2	18	01.2	07
IX	-	09.1	17.8	10.5	12.0	18.9	05.3	25.2	11	-06.7	30	01	01.0	04	01.8	27	01.9	17	01.8	10	02.1	03	01.3	16	01.5	09	01.3	03
X	-	04.5	11.6	06.1	07.1	13.0	01.2	24.5	10	-07.2	25	.	.	05	02.6	27	01.7	08	01.2	06	01.8	09	02.3	21	01.7	12	01.7	05
XI	-	03.8	08.2	04.5	05.2	09.7	-00.1	17.9	04	-07.4	07	02	01.0	05	01.8	16	01.2	15	01.4	04	02.8	22	02.3	07	02.4	09	02.0	10
XII	-	-04.3	00.6	-03.8	-02.8	02.3	-07.7	10.6	01	-18.0	24	03	01.0	07	01.0	25	01.5	05	01.4	03	01.0	10	01.2	07	01.3	07	01.3	26
GOD.	-	04.6	10.5	05.5	06.5	11.9	00.4	29.9	13 VII	-28.4	17 II	21	01.2	65	01.6	268	01.6	156	01.5	94	02.0	148	01.9	125	01.6	139	01.5	79
φ = 45° 25' N λ = 14° 55' E Gr. Δ G = + 1h 00 min.																											
I	-	-01.2	00.6	-01.2	-00.7	01.8	-03.9	10.8	05	-09.5	24	.	.	45	02.0	08	02.1	02	02.5	01	02.0	23	02.4	14	02.1	.	.	.
II	-	-00.8	02.2	00.0	00.3	03.6	-03.7	09.0	04	-14.6	17	.	.	27	02.3	07	02.6	02	02.0	.	.	30	03.6	15	02.3	03	02.0	.
III	-	00.1	03.6	01.1	01.5	04.8	-02.2	12.4	25	-09.5	08	.	.	32	02.4	10	02.4	03	02.3	.	.	24	02.5	15	02.3	09	01.9	.
IV	-	04.9	09.9	06.0	06.7	11.4	02.3	23.3	19,18	-05.2	04	.	.	20	02.6	07	02.4	02	03.0	.	.	28	02.9	20	02.6	13	02.0	.
V	-	09.3	14.3	09.1	10.5	15.4	05.5	21.3	10	-02.3	01	.	.	31	02.4	05	03.2	04	03.0	.	.	28	02.6	19	02.4	06	02.2	.
VI	-	15.6	21.3	15.9	17.2	22.4	11.7	28.3	28	04.0	03	.	.	29	02.4	04	02.8	01	03.0	.	.	21	02.3	26	02.0	09	02.3	.
VII	-	15.9	21.5	16.2	17.5	22.6	11.6	30.6	23	05.9	16	.	.	29	02.4	09	02.7	03	02.7	.	.	27	02.5	17	02.3	08	02.0	.
VIII	-	15.4	22.1	16.6	17.7	23.2	12.6	30.7	06	07.9	25	.	.	29	02.4	07	02.3	.	.	01	02.0	18	02.3	29	01.9	09	02.3	.
IX	-	12.0	18.8	13.4	14.4	19.9	09.5	26.7	11	-00.8	30	.	.	32	02.6	10	02.7	07	02.4	.	.	13	02.5	19	02.3	09	01.9	.
X	-	06.7	12.7	08.1	08.9	13.6	04.6	26.2	10	-02.6	25	.	.	29	02.5	06	02.7	01	02.0	.	.	34	02.6	18	02.9	05	02.0	.
XI	-	05.8	09.6	06.6	07.2	10.5	03.7	18.2	04	-02.5	17	.	.	20	02.2	07	02.1	01	04.0	01	02.0	34	03.1	26	02.8	01	03.0	.
XII	-	-02.1	01.1	-01.4	-00.9	02.3	-04.2	12.0	01	-10.0	24	01	02.0	36	02.3	09	02.2	03	02.0	01	02.0	16	02.6	19	02.2	08	02.0	.
GOD.	-	06.8	11.5	07.5	08.4	12.6	04.0	30.7	6 VIII	-14.6	17 II	01	02.0	359	02.4	89	02.5	29	02.5	04	02.0	296	02.7	237	02.3	80	02.1	.

RIJEKA — BR. ST. 46

PARG — BR. ST. 47

CRIKVENICA — BR. ST. 48

ZALESINA — BR. ST. 49

SKRAD — BR. ST. 50

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlim)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dlim)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤ 0,0	Tx ≤ 0,0	Tn < 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 3,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	≋	⚠	∽	▲	▲	R T	≡	▦
RIJEKA																																						
BR. ST. 46															H_a = 104 m H_b = 108,1 m h_a = 2,0 m h_b = 1,0 m																								
I	7.5	6.9	6.9	7.1	085.9	05.5	78	67	74	73	33	203	040.6	05	.	.	06	.	.	.	.	.	06	17	17	15	08	17	01	01	.	.	.	.	.	.	.
II	7.3	7.5	7.0	7.3	093.7	04.6	69	58	67	65	26	142	023.8	15	.	.	05	.	.	.	03	.	02	13	16	11	07	16	02	01	.	.	.	01	04	02	.
III	7.8	8.5	7.2	7.8	092.1	05.3	70	62	72	68	16	250	040.0	05	.	.	02	.	.	.	03	.	.	18	15	12	10	15	02	01	01	.	.	.	03	03	.
IV	7.4	6.8	5.9	6.7	159.1	06.5	70	56	67	64	33	248	068.8	14	.	.	.	.	.	.	.	.	03	13	16	14	08	16	01	01	.	.	.	.	08	.	.
V	5.2	7.5	4.2	5.6	204.6	07.7	62	53	66	60	24	049	015.9	23	.	.	.	.	.	.	02	.	04	09	18	12	01	18	.	.	.	.	.	.	04	.	.
VI	5.1	6.2	5.2	5.5	248.0	12.4	71	55	70	65	28	080	014.4	20	.	.	.	20	02	02	.	.	05	08	15	11	03	15	.	.	.	.	.	.	11	.	.
VII	3.3	4.0	2.7	3.3	306.7	11.8	64	46	59	56	32	104	048.3	01	.	.	.	21	11	09	05	.	17	06	08	05	02	08	.	.	.	.	.	.	02	.	.
VIII	4.1	5.9	3.0	4.4	255.0	13.2	70	51	67	63	35	125	055.6	31	.	.	.	24	11	12	.	.	09	08	11	10	04	11	.	.	.	.	.	.	07	.	.
IX	4.0	3.1	2.7	3.2	257.4	10.3	66	46	63	58	32	011	004.9	17	.	.	.	18	.	01	03	01	11	01	06	03	.	06	.	.	.	.	.	.	01	.	.
X	5.4	5.1	3.3	4.6	181.2	07.6	69	52	68	63	29	039	014.8	21	.	.	.	01	.	.	03	.	08	06	05	04	02	05	.	.	.	.	.	.	03	.	.
XI	7.2	6.9	6.0	6.7	088.1	07.3	76	62	72	70	26	193	059.2	22	.	.	.	.	.	.	02	.	04	14	12	08	05	12	.	.	.	.	.	01	03	.	.
XII	5.1	5.9	4.7	5.2	114.9	04.6	65	54	66	62	26	140	040.6	28	.	.	05	.	.	.	04	02	10	11	09	09	04	09	.	.	.	.	.	.	.	.	.
GOD.	5.8	6.2	4.9	5.6	2086.7	08.1	69	55	67	63	16	1584	068.8	44 IV	.	.	18	84	24	24	25	03	79	124	148	114	54	148	06	04	01	.	.	02	46	05	.
PARG																																						
BR. ST. 47															H_a = 863 m H_b = 863,4 m h_a = 2,0 m h_b = 2,0 m																								
I	9.4	8.9	8.5	8.9	013.6	04.8	94	94	94	94	26	204	055.8	06	02	10	22	.	.	.	.	.	.	24	18	14	05	12	08	.	.	.	.	.	.	15	15
II	7.0	7.1	5.9	6.7	060.7	04.2	92	81	89	87	51	174	036.5	06	03	02	24	.	.	.	01	.	02	11	17	15	07	05	15	.	01	.	.	01	03	05	23
III	7.4	7.2	6.9	7.2	078.8	04.7	93	84	91	89	26	262	044.6	04	01	.	24	.	.	.	.	.	03	18	19	19	12	08	14	.	.	.	.	.	02	03	31
IV	7.5	7.2	6.2	6.9	101.6	05.4	90	72	86	83	37	299	042.6	14	.	.	14	.	.	.	.	.	04	14	20	20	10	13	14	01	02	.	.	.	05	07	21
V	5.4	7.0	5.8	6.0	181.7	06.3	78	62	83	74	36	094	024.7	23	.	.	05	.	.	.	.	.	03	07	18	16	01	17	02	01	.	.	.	.	04	02	01
VI	4.7	6.5	4.9	5.4	176.3	10.1	79	65	81	75	40	087	016.1	08	.	.	.	02	.	.	.	.	03	04	15	13	03	15	.	.	.	.	.	01	11	.	.
VII	3.6	5.1	3.2	4.0	260.9	10.3	77	63	77	72	38	150	069.8	16	.	.	.	12	.	.	01	.	10	05	08	07	04	08	.	.	.	.	.	01	06	.	.
VIII	4.4	6.6	5.0	5.4	178.9	10.8	88	69	85	81	34	208	055.8	22	.	.	.	06	.	.	.	.	04	06	15	13	07	15	.	.	.	.	.	.	12	01	.
IX	3.9	4.2	3.2	3.8	202.9	08.5	80	63	84	76	34	022	012.7	17	.	.	.	.	.	.	01	.	10	04	05	04	01	05	.	.	.	.	.	.	01	.	.
X	6.4	5.6	2.8	5.0	169.1	06.7	84	62	81	76	37	099	059.0	21	.	.	07	.	.	.	.	.	04	03	09	05	03	07	03	.	.	.	.	01	03	04	03
XI	8.0	6.6	5.5	6.7	089.3	05.8	87	73	86	82	33	210	049.8	15	.	.	08	.	.	.	01	.	03	13	11	09	06	11	01	.	.	.	.	.	03	05	01
XII	5.3	5.9	5.2	5.5	083.9	03.7	86	74	85	81	29	158	048.1	30	03	09	29	.	.	.	.	.	10	14	15	15	05	06	13	.	.	.	.	.	01	05	24
GOD.	6.1	6.5	5.3	6.0	1597.7	06.8	85	71	85	80	26	1967	069.8	46 VII	09	21	133	20	.	.	04	.	56	123	170	150	64	122	70	02	03	.	.	04	51	47	119
CRIKVENICA																																						
BR. ST. 48															H_a = 2 m H_b = - m h_a = 2,0 m h_b = 1,5 m																								
I	7.5	6.8	7.4	7.3	-	05.9	77	74	75	75	41	131	027.3	06	.	.	02	.	.	.	.	.	05	19	14	14	04	13	.	.	.	.	.	.	.	.	.
II	7.1	7.6	7.8	7.5	-	05.3	76	67	70	71	34	113	029.9	15	.	.	04	.	.	.	.	.	03	16	14	13	03	14	.	.	.	.	.	.	03	.	.
III	6.9	7.3	7.2	7.1	-	05.7	70	66	71	69	35	152	036.1	05	.	.	04	.	.	.	01	.	02	15	12	11	07	12	.	.	.	.	.	.	04	.	.
IV	6.5	5.9	6.4	6.3	-	07.4	75	65	73	71	38	137	026.1	09	.	.	.	.	.	.	.	.	05	14	15	13	05	15	.	.	.	.	.	.	04	.	.
V	4.8	6.7	5.7	5.7	-	08.5	68	57	69	65	21	066	018.2	23	.	.	.	01	.	.	.	.	06	10	12	10	02	12	01	01	.	.	.	.	02	.	.
VI	4.8	5.5	5.1	5.1	-	14.5	79	65	76	73	34	111	022.3	15	.	.	.	19	05	03	.	.	07	06	14	13	03	14	.	.	.	.	.	.	10	.	.
VII	3.5	3.2	3.5	3.4	-	13.9	75	57	66	66	33	059	040.5	16	.	.	.	24	10	05	01	.	17	07	05	05	02	05	.	.	.	.	.	.	03	.	.
VIII	3.7	5.0	5.0	4.6	-	15.6	76	66	75	72	52	068	021.0	31	.	.	.	26	10	06	.	.	11	06	12	10	02	12	.	.	.	.	.	.	09	.	.
IX	3.4	2.1	2.8	2.8	-	12.6	70	61	67	66	28	002	002.3	13	.	.	.	18	03	03	01	.	12	01	01	01	.	01	.	.	.	.	.	.	.	.	.
X	4.6	5.1	4.8	4.8	-	08.2	67	57	69	64	31	066	045.2	02	.	.	.	03	.	.	.	.	10	08	05	05	02	05	.	.	.	.	.	.	02	.	.
XI	7.4	6.9	6.4	6.9	-	08.1	79	72	78	76	30	127	043.2	22	.	.	.	.	.	.	.	.	06	16	10	10	04	10	.	.	.	.	.	.	.	01	.
XII	5.1	5.8	4.7	5.2	-	05.3	72	59	75	68	28	107	047.7	28	.	.	03	.	.	.	02	.	12	10	09	08	03	09	.	.	.	.	.	.	03	.	.
GOD.	5.4	5.7	5.6	5.6	-	09.2	73	63	72	69	21	1139	047.7	28 XII	.	.	13	91	28	17	05	.	96	128	123	113	37	122	01	01	.	.	.	.	40	01	.
ZALESINA																																						
BR. ST. 49															H_a = 750 m H_b = - m h_a = 2,0 m h_b = 2,0 m																								
I	9.3	9.5	9.1	9.3	-	04.0	87	86	86	86	67	219	049.0	06	06	11	23	.	.	.	.	.	.	27	18	17	07	13	08	01	.	.	.	.	.	13	20
II	7.7	7.5	7.2	7.5	-	03.8	81	83	84	83	35	234	035.8	11	08	08	24	.	.	.	.	.	01	13	22	16	09	11	14	.	03	.	.	.	03	04	23
III	7.8	8.5	7.5	7.9	-	04.0	88	79	88	85	27	294	051.2	04	09	03	25	.	.	.	.	.	.	20	24	17	11	13	18	04	.	.	.	.	01	05	31
IV	7.7	6.8	6.5	7.0	-	05.3	88	68	81	79	26	346	042.5	22	01	.	19	.	.	.	.	.	01	12	22	18	10	18	13	04	.	.	.	.	03	05	17
V	5.5	7.0	6.0	6.2	-	06.6	80	62	81	75	36	110	032.8	23	.	.	10	.	.	.	.	.	03	10	18	14	03	16	04	.	02	.	.	.	01	04	.
VI	5.5	6.7	4.8	5.7	-	10.3	84	60	81	75	40	092	027.1	30	.	.	.	04	.	.	.	.	04	07	15	09	04	15	.	.	.	.	.	.	07	.	.
VII	4.7	4.9	2.9	4.2	-	10.1	87	61	83	77	42	200	098.2	16	.	.	.	10	.	.	.	.	13	06	09	06	05	09	.	.	.	.	.	.	04	.	.
VIII	5.1	5.9	4.5	5.2	-	11.2	93	67	90	83	32	175	060.5	31	.	.	.	07	.	.	.	.	07	08	13	11	06	13	.	.	.	.	.	.	08	01	.
IX	5.1	3.7	3.8	4.2	-	08.7	86	66	84	79	40	031	010.3	01	.	.	06	01	.	.	.	.	09	04	09	05	02	09	.	.	.	.	.	.	02	04	.
X	6.5	6.0	3.4	5.3	-	06.2	88	68	84	80	22	138	056.4	21	.	.	15	.	.	.	.	.	05	07	10	08	04	09	03	.	.	.	.	.	02	06	02
XI	7.9	7.1	5.6	6.9	-	05.8	87	75	88	83	50	268	153.6	15	.	.	14	.	.	.	.	.	02	15	15	11	04	15	05	03	01	.	.	.	.	06	02
XII	6.2	6.5	5.6	6.1	-	03.5	86	81	88	85	57	206	042.3	30	08	12	29	.	.	.	.	.	10	16	15	13	07	06	12	01	01	.	.	.	.	03	16
GOD.	6.6	6.7	5.6	6.3	-	06.6	86	71	84	80	22	2313	153.6	45 XI	32	34	165	22	.	.	.	.	55	145	190	145	72	147	77	13	07	.	.	.	31	51	111
SKRAD																																						
BR. ST. 50															H_a = 668 m H_b = - m h_a = 2,0 m h_b = 2,0 m																								
I	9.3	9.3	9.9	9.5	-	04.3	93	88	94	92	61	126	022.3	06	.	14	23	.	.	.	01	.	.	26	22	14	06	15	11	04	.	.	.	.	.	17	13
II	7.6	7.5	6.9	7.3	-	04.1	85	77	86	83	42	157	036.0	15	04	06	23	.	.	.	03	.	.	12	20	13	05	10	14	02	01	.	.	.	03	06	22
III	7.3	8.5	7.3	7.7	-	04.6	90	83	89	88	51	229	043.9	04	.	01	24	.	.	.	.	.	01	18	21	18	10	06	17	01	.	.	.	.	01	14	31
IV	7.2	6.9	6.3	6.8	-	05.6	84	66	79	76	28	299	047.8	14	.	.	09	.	.	.	.	.	01	13	20	17	09	17	08	03	.	.	.	.	05	10	08
V	5.0	6.6	4.7	5.4	-	07.0	77	58	79	72	34	080	023.4	23	.	.	04	.	.	.	.	.	03	09	16	11	02	15	02	01	.	.	.	.	02	02	.
VI	5.6	6.2	5.0	5.6	-	11.2	82	62	80	75	38	078	028.2	30	.	.	.	11	.	.	.	.	04	07	16	10	03	16	.	.	.	.	.	.	10	01	.
VII	3.7	5.2	2.3	3.7	-	11.2	78	63	79	73	35	160	088.8	16	.	.	.	14	01	.	.	.	14	03	08	07	05	08	.	.	.	.	.	.	02	01	.
VIII	5.5	5.9	4.3	5.2	-	12.2	89	66	85	80	38	190	055.0	09	.	.	.	11	02	.	.	.	04	07	12	11	05	12	.	.	.	.	.	01	08	09	.
IX	4.9	4.3	3.9	4.4	-	09.5	86	61	81	76	36	026	010.6	07	.	.	01	04	.	.	.	.	06	04	08	05	01	08	.	.	.	.	.	.	01	03	.
X	6.4	5.8	3.2	5.1	-	07.2	89	66	87	81	38	130	043.3	21	.	.	07	01	.	.	02	.	04	05	09	07	04	09	03	01	01	.	.	01	04	10	02
XI	7.0	7.0	6.4	6.8	-	06.2	84	72	83	80	40	174	107.8	15	.	.	06	.	.	.	.	.	04	14	12	10	03	12	.	.	.	.	.	.	02	09	.
XII	6.7	6.7	7.2	6.9	-	03.9	88	83	90	87	26	146	033.7	28	01	11	28	.	.	.	01	.	04	14	15	15	04	09	11	04	.	.	.	.	02	18	15
GOD.	6.4	6.7	5.6	6.2	-	07.2	85	70	84	80	26	1795	107.8	45 XI	05	32	125	41	03	.	07	.	45	132	179	138	57	137	66	16	02	.	.	02	40	100	91

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Tdes)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12): N		NE		E		SE		S		SW		W		NW		C
												δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.		j.	δ.	j.	δ.
OGULIN — φ = 45° 16' N λ = 15° 14' E Gr. ΔG = + 1h 01 min. — BR. ST. 51																												
I	731.5	-01.0	01.6	-00.2	00.0	02.9	-02.7	14.7	06	-11.0	03	01	01.0	27	01.3	12	01.0	12	01.1	02	01.0	12	02.0	07	02.0	04	01.0	16
II	728.8	-00.4	03.4	01.2	01.3	05.7	-03.0	13.8	05	-17.0	17	03	01.0	13	01.4	09	01.4	10	01.3	05	01.8	16	04.4	10	03.4	03	01.0	15
III	730.0	00.9	06.2	02.9	03.2	07.3	-00.4	17.3	24	-10.0	08	06	01.8	11	01.3	05	01.2	08	01.4	04	01.2	25	02.2	15	01.3	11	01.4	08
IV	731.5	06.6	12.4	08.6	09.0	13.9	04.8	26.1	19	-02.3	04	05	02.0	09	02.0	09	01.6	07	01.3	03	01.7	24	02.4	15	01.7	15	01.5	03
V	733.0	09.7	16.2	11.6	12.2	17.6	07.0	22.3	10	-01.7	01	01	02.0	20	01.7	08	02.0	08	01.4	07	01.1	21	02.4	16	01.8	06	01.2	06
VI	734.1	16.5	23.0	17.8	18.8	24.7	13.0	30.3	28	04.8	04	.	.	10	01.8	13	01.5	08	01.6	03	01.3	10	02.8	20	01.7	14	01.4	12
VII	733.4	15.8	23.8	18.0	18.9	25.3	12.2	31.3	23,14	07.1	06	04	02.2	14	01.9	10	01.8	09	01.2	02	02.0	16	02.5	16	01.2	15	01.1	07
VIII	733.1	15.9	24.1	18.3	19.2	25.2	13.8	33.6	06	08.7	27,26	01	01.0	14	01.4	08	01.5	06	01.2	05	01.4	05	01.8	27	01.2	15	01.3	12
IX	736.6	11.4	21.1	14.5	15.4	21.8	10.0	29.7	11	-02.2	30	02	01.5	10	01.4	13	01.9	11	01.2	.	.	14	02.2	20	02.0	08	01.5	12
X	736.4	07.1	15.2	09.9	10.5	16.2	05.8	26.8	10,09	-02.4	25	01	01.0	21	01.4	06	01.7	09	01.4	01	02.0	23	02.5	17	01.7	06	01.2	09
XI	734.0	06.9	12.0	08.4	08.9	12.9	04.7	21.5	02	-03.2	27	05	03.2	12	01.3	07	01.6	06	01.3	05	01.8	20	02.7	13	02.3	11	02.0	11
XII	736.9	-01.7	02.3	-00.1	00.1	03.5	-03.0	15.4	01	-11.8	27	05	01.2	17	01.5	06	01.0	08	01.0	06	01.0	10	02.5	19	01.4	04	01.0	18
GOD.	733.3	07.3	13.4	09.2	09.8	14.8	05.2	33.6	6 VIII	-17.0	47 II	34	01.8	178	01.5	106	01.5	102	01.3	43	01.4	196	02.6	195	01.7	112	01.4	129
KARLOVAC — φ = 45° 30' N λ = 15° 33' E Gr. ΔG = + 1h 02 min. — BR. ST. 52																												
I	750.6	-01.1	01.1	-00.4	-00.2	02.5	-02.2	12.4	05	-06.5	03,02	08	01.5	29	01.7	03	02.0	01	01.0	.	.	19	01.5	02	01.0	.	.	31
II	747.8	-01.2	04.1	01.0	01.2	06.0	-02.7	14.3	09	-11.0	20,17	07	01.3	20	01.7	02	01.5	01	01.0	.	.	15	02.3	03	01.3	08	01.2	28
III	748.6	01.8	08.0	04.9	04.9	09.3	00.9	20.2	24	-06.4	02	02	03.5	28	01.9	.	.	02	01.5	01	03.0	15	02.4	03	01.3	08	01.9	34
IV	749.8	06.6	14.5	10.4	10.5	16.4	05.5	28.0	19	-01.6	04	03	02.7	19	01.9	06	02.0	01	02.0	01	03.0	18	02.6	01	03.0	12	02.8	29
V	751.3	09.6	18.0	13.4	13.6	19.8	07.6	25.0	14	00.0	01	04	02.2	23	01.9	04	02.2	01	02.0	02	02.0	16	02.3	01	02.0	03	02.3	39
VI	751.9	16.9	25.3	20.0	20.5	26.5	14.4	33.0	28	06.7	04	05	01.4	18	01.9	04	03.0	02	01.0	03	01.3	18	01.7	01	01.0	04	01.5	35
VII	751.2	16.5	25.7	20.8	20.9	27.3	14.3	33.0	23	09.5	16	07	01.1	25	02.1	05	02.4	01	01.0	.	.	16	02.2	01	02.0	12	01.2	26
VIII	750.8	16.6	25.5	20.6	20.8	26.7	15.7	35.1	06	10.5	27	06	01.7	23	01.7	03	01.7	.	.	04	01.5	09	01.9	.	.	10	01.3	38
IX	754.6	11.8	22.4	15.7	16.4	23.2	11.2	31.7	11	00.4	30	03	01.3	23	01.6	02	02.5	03	01.3	01	03.0	14	02.0	01	01.0	02	01.5	41
X	754.7	06.0	15.9	09.9	10.4	16.7	05.1	26.4	09	-01.1	25	04	01.5	32	01.6	01	01.0	06	01.7	.	.	12	03.2	.	.	01	01.0	37
XI	752.6	06.0	12.5	08.2	08.7	13.4	04.5	21.0	03	-01.8	27	03	01.3	14	01.1	.	.	02	02.0	02	02.0	28	02.4	02	01.0	05	01.4	34
XII	756.1	-00.9	02.3	00.0	00.3	03.6	-02.2	16.0	02	-10.1	27	02	01.5	43	01.7	01	02.0	.	.	.	.	04	01.5	02	01.0	03	01.3	38
GOD.	751.7	07.4	14.6	10.4	10.7	16.0	06.0	35.1	6 VIII	-11.0	47,10 VIII	54	01.6	297	01.7	31	02.2	20	01.5	14	01.9	184	02.2	17	01.3	68	01.7	410
SLUNJ — φ = 45° 07' N λ = 15° 35' E Gr. ΔG = + 1h 02 min. — BR. ST. 53																												
I	-	-00.8	02.2	00.0	00.3	03.9	-03.0	15.0	28	-13.0	04,03	19	02.0	19	02.0	07	02.0	14	02.1	08	02.0	17	02.1	04	02.0	05	02.0	.
II	-	00.7	03.6	01.2	01.7	05.8	-02.1	14.0	09,05	-12.0	20,17	04	02.0	23	02.0	02	02.0	15	02.1	10	02.3	26	02.1	.	.	03	02.0	01
III	-	02.4	06.5	02.8	03.6	08.7	-00.2	18.0	24	-07.5	02,01	15	02.0	13	02.0	02	02.0	26	02.1	07	02.0	16	02.1	01	02.0	13	02.0	.
IV	-	07.5	13.0	08.5	09.4	15.5	04.1	26.5	19	00.0	06,03	12	02.0	10	02.1	01	02.0	19	02.1	03	02.3	27	02.3	03	02.0	.	.	15
V	-	11.3	16.3	11.5	12.7	18.2	07.0	23.0	10	-01.0	01	08	02.0	15	01.9	02	01.0	06	02.2	03	01.7	15	02.3	08	02.8	11	01.8	25
VI	-	16.7	23.8	17.9	19.1	25.3	13.4	31.2	28	06.5	04	03	01.7	03	01.7	11	01.4	17	01.4	02	01.0	06	01.2	04	02.2	15	01.5	29
VII	-	16.1	24.2	18.4	19.3	25.6	13.2	31.7	23	08.5	16	03	02.0	09	01.7	14	01.4	17	01.6	.	.	06	02.8	02	02.0	06	01.3	36
VIII	-	16.6	24.9	18.7	19.7	25.9	14.5	34.5	07	09.0	26	02	01.0	09	01.2	01	02.0	13	01.4	03	01.7	06	01.5	02	01.5	11	01.7	46
IX	-	11.6	21.4	14.3	15.4	22.4	10.3	32.4	11	-01.2	30	02	01.0	11	01.3	08	01.1	25	01.1	.	.	04	01.2	03	01.7	03	01.7	34
X	-	07.1	14.9	09.3	10.1	16.1	05.3	27.3	10	-01.8	20,19	03	01.0	09	01.6	04	01.5	27	01.6	01	03.0	06	01.8	04	02.0	04	01.5	35
XI	-	06.6	11.9	08.4	08.9	12.9	05.0	20.2	03	-02.6	27	04	01.0	03	01.0	03	01.0	37	01.7	08	02.4	04	01.5	09	02.2	01	01.0	21
XII	-	-01.1	02.4	-00.1	00.3	03.3	-02.4	16.0	01	-10.6	27	08	01.6	06	01.3	11	01.1	27	01.3	07	01.4	10	01.2	08	01.8	07	01.3	09
GOD.	-	07.9	13.8	09.2	10.0	15.3	05.4	34.5	7 VIII	-13.0	5,4 I	83	01.8	130	01.8	66	01.4	243	01.7	52	02.0	143	02.0	48	02.1	79	01.7	251
BISTRAC — φ = 45° 49' N λ = 15° 42' E Gr. ΔG = + 1h 03 min. — BR. ST. 54																												
I	-	-01.7	00.6	-01.1	-00.8	01.8	-03.5	10.5	05	-12.5	[illegible]	08	01.9	10	02.0	13	01.8	19	02.1	20	01.8	10	02.1	08	01.6	05	02.2	.
II	-	-02.1	03.3	00.3	00.4	04.6	-03.8	14.0	09,06	-15.0	[illegible]	04	01.8	08	02.0	06	02.0	11	01.9	23	01.9	17	02.0	12	01.8	03	02.0	.
III	-	01.6	07.9	04.3	04.5	08.8	00.3	19.4	24	-06.7	[illegible]	07	02.1	18	02.2	05	02.2	04	02.5	20	01.9	13	02.0	16	01.9	10	02.0	.
IV	-	06.4	13.8	08.5	09.3	15.2	04.4	26.6	19	-02.5	04	14	02.1	19	02.2	05	01.4	06	02.2	12	01.8	05	02.0	20	02.2	09	02.0	.
V	-	11.0	17.8	12.4	13.4	19.0	06.9	23.5	14	-00.8	01	13	02.1	24	02.0	09	01.9	03	02.0	07	02.0	08	02.2	18	01.9	11	02.1	.
VI	-	17.3	24.3	18.1	19.5	25.9	13.0	31.2	28	06.0	04	08	02.0	18	02.2	10	01.9	20	02.0	11	02.1	10	02.0	07	02.1	06	02.3	.
VII	-	16.9	24.7	18.6	19.7	26.5	13.0	32.4	23,22	08.8	06	05	01.4	26	01.8	11	02.0	14	01.9	14	02.1	03	02.0	15	01.9	05	01.8	.
VIII	-	16.8	24.3	18.8	19.6	25.6	-	32.8	06	-	-	12	02.2	20	01.8	12	01.9	10	01.9	13	01.7	04	01.8	13	01.8	09	01.6	.
IX	-	11.8	20.5	14.8	15.5	21.4	09.4	29.0	10	00.0	30	06	02.2	21	01.9	13	01.6	03	01.7	19	02.2	08	02.2	15	02.0	05	02.4	.
X	-	06.3	14.7	09.3	09.9	15.8	03.8	24.0	10	-02.4	19	06	01.7	13	02.1	11	01.6	11	02.1	25	01.9	07	02.1	15	01.8	05	02.6	.
XI	-	06.0	11.5	07.4	08.1	13.0	03.0	19.6	04	-02.5	27	04	01.8	12	01.8	11	01.5	09	01.8	37	01.7	07	01.9	06	02.0	04	01.8	.
XII	-	-01.1	01.6	-00.1	00.1	02.7	-03.0	12.2	01	-10.0	25	23	01.7	07	01.9	14	01.6	06	01.5	17	01.5	11	01.7	11	01.4	04	01.5	.
GOD.	-	07.4	13.8	09.3	09.9	15.0	-	32.8	6.VIII	-		110	01.9	196	02.0	120	01.8	116	02.0	218	01.9	103	02.0	156	01.9	76	02.0	.
SLJEME — φ = 45° 54' N λ = 15° 57' E Gr. ΔG = + 1h 04 min. — BR. ST. 55																												
I	672.1	-03.0	-02.1	-03.0	-03.1	-01.4	-04.8	07.6	06	-10.6	23	09	01.7	07	03.4	05	03.0	11	02.4	21	03.7	21	03.6	04	03.0	09	01.9	06
II	668.6	-04.0	-02.2	-03.2	-03.1	-00.6	-05.4	06.4	06	-13.2	16	11	02.9	11	03.4	04	02.8	06	02.8	13	03.2	20	03.4	06	03.5	10	03.1	03
III	670.1	-01.9	-00.7	-00.8	-00.7	01.6	-02.8	10.2	24	-09.1	02	11	03.1	15	03.6	.	.	10	03.2	19	03.2	17	03.4	07	02.4	11	02.5	03
IV	672.5	02.6	06.1	04.1	04.2	08.1	01.4	18.9	19	-05.7	04	16	03.5	12	04.1	.	.	07	02.9	18	02.7	18	03.0	08	02.6	07	02.7	04
V	674.7	06.1	10.2	07.3	07.7	11.8	04.8	17.9	10	-02.6	02,01	17	03.4	07	02.4	03	03.0	06	02.8	16	02.4	12	02.7	06	03.0	22	02.8	04
VI	677.2	13.0	16.7	14.2	14.5	18.0	11.6	23.8	23	02.8	03	17	03.0	12	03.2	01	03.0	04	03.0	16	02.4	14	02.5	02	02.0	18	02.8	06
VII	676.6	13.1	16.7	14.1	14.5	18.5	11.4	24.8	23	03.5	16	12	04.6	13	03.3	03	01.7	11	02.2	21	02.3	14	02.7	04	03.5	10	03.5	05
VIII	676.4	13.7	16.8	14.4	14.9	18.0	12.4	24.0	06	07.6	25	22	03.5	05	03.0	02	02.0	14	02.4	23	02.5	08	02.2	03	02.0	07	02.7	09
IX	679.1	10.2	13.9	11.1	11.6	15.2	08.8	23.0	11	00.9	29	13	03.2	17	03.2	03	02.0	11	02.5	14	02.2	11	03.1	07	02.9	08	03.4	06
X	677.5	05.0	08.4	06.1	06.4	09.8	03.7	20.5	10	-03.6	24	20	03.5	11	03.2	01	02.0	03	02.3	29	02.5	12	03.0	02	03.0	13	03.8	02
XI	675.0	03.8	06.4	04.2	04.7	07.9	02.2	17.6	02	-01.4	28,08	08	03.8	05	03.2	.	.	06	02.8	24	03.5	11	04.9	09	03.4	20	04.0	07
XII	676.1	-01.9	-00.5	-01.8	-01.5	01.8	-03.6	09.2	01	-10.2	26,25	12	05.1	15	04.5	.	.	11	03.3	18	03.1	07	03.0	07	03.1	12	02.8	11
GOD.	674.7	04.7	07.5	05.6	05.8	09.1	03.3	24.8	23 VII	-13.2	46 II	168	03.5	130	03.5	22	02.5	100	02.7	232	02.8	165	03.2	65	02.9	147	03.1	66

Mesec	Oblačnost Nm (0-10) 7	14	21	Srednji (0-10)	Insolacija broj sati	Vlažnost vazduha e m	Um % 7	14	21	Srednji (0-10)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤ -10,0	Tn ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	P (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 6,0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	*	⁂	♨	≈	△	▲	R T	≡	▥
OGULIN																																					
BR. ST. 51																																					
H_o = 325 m H_b = 325,2 m h_v = 2,0 m h_r = 1,5 m																																					
I	9.5	9.2	9.1	9.3	-	04.2	90	83	88	87	57	144	035.2	06	03	12	21	.	.	.	02	01	.	26	20	14	05	14	10	02	.	01	01	.	01	13	29
II	7.8	7.6	7.5	7.6	-	04.1	83	71	81	78	46	196	049.9	15	04	02	22	.	.	.	08	07	01	15	16	14	07	11	10	05	03	.	03	.	04	06	22
III	7.4	7.8	6.2	7.1	-	04.6	86	68	83	79	31	206	032.2	07	01	.	14	.	.	.	01	.	03	17	21	16	10	14	17	09	01	.	02	.	03	04	25
IV	8.1	7.3	5.6	7.0	-	05.9	80	56	72	69	23	192	025.4	14	.	.	01	02	.	.	04	.	02	12	18	17	08	17	05	04	.	.	01	.	05	.	03
V	6.3	7.0	5.5	6.3	-	07.3	79	53	74	69	35	072	029.2	23	.	.	03	.	.	.	.	.	03	11	15	07	03	14	02	01	.	.	.	.	05	01	.
VI	4.8	6.7	5.7	5.7	-	11.9	82	59	78	73	39	087	032.1	19	.	.	.	17	01	.	.	.	07	09	14	07	03	14	.	.	.	.	.	.	12	.	.
VII	3.9	5.1	3.2	4.1	-	11.9	84	55	77	72	34	117	059.7	16	.	.	.	19	04	.	04	.	10	05	10	06	04	10	.	.	.	.	.	.	05	.	.
VIII	5.3	5.8	4.5	5.2	-	13.1	90	61	85	79	34	137	041.3	31	.	.	.	15	04	.	.	.	06	09	12	09	05	12	.	.	.	.	.	.	08	02	.
IX	5.0	4.6	3.8	4.5	-	10.1	89	56	82	76	37	027	018.2	01	.	.	02	10	.	.	03	.	10	05	08	04	01	08	.	.	.	.	.	.	01	02	.
X	6.0	6.0	3.8	5.3	-	07.4	88	59	81	76	32	116	043.0	02	.	.	02	02	.	.	02	.	07	08	09	07	04	09	02	02	.	.	.	.	02	04	.
XI	7.3	7.4	6.3	7.0	-	06.4	82	63	79	75	41	048	022.3	22	.	.	05	.	.	.	09	.	02	13	10	07	01	10	.	.	.	.	.	.	01	02	.
XII	7.8	7.4	7.7	7.6	-	04.0	91	76	85	84	23	128	030.6	28	02	11	24	.	.	.	01	.	03	20	14	14	05	07	09	01	01	.	02	.	02	08	10
GOD.	6.6	6.8	5.7	6.4	-	07.6	85	63	80	76	23	1470	059.7	46	VII	10	25	94	65	09	.	34	08	54	150	167	122	56	140	55	24	05	01	09	.	49	42	89
KARLOVAC																																					
BR. ST. 52																																					
H_o = 112 m H_b = 122,6 m h_v = 2,0 m h_r = 1,0 m																																					
I	10.0	9.5	8.8	9.4	009.9	04.1	88	85	88	87	73	112	025.2	01	.	10	23	.	.	.	.	.	.	27	16	14	03	10	08	01	.	.	.	.	.	14	31
II	8.5	7.0	7.7	7.8	080.3	04.2	89	73	84	82	50	135	027.6	11	02	03	21	.	.	.	.	.	02	15	16	14	06	11	10	03	.	.	.	.	02	07	-
III	7.6	8.2	5.6	7.1	097.8	05.2	90	69	80	80	35	149	025.5	12	.	.	10	.	.	.	.	.	03	14	19	15	07	16	11	06	.	.	.	.	01	04	-
IV	8.0	7.4	4.5	6.6	162.1	06.9	88	59	73	73	25	165	027.0	14	.	.	01	04	.	.	.	.	01	09	17	13	06	17	02	02	.	.	.	.	.	01	.
V	6.2	7.2	5.3	6.2	217.3	08.4	88	57	75	73	36	058	020.5	23	.	.	.	01	.	.	.	.	03	08	12	09	02	12	02	01	.	.	.	.	05	01	.
VI	4.4	6.8	5.0	5.4	254.6	13.4	89	56	78	74	35	069	017.6	15	.	.	.	18	06	.	.	.	04	09	14	11	03	14	.	.	.	.	.	.	10	01	.
VII	3.8	5.1	3.7	4.2	305.6	13.5	89	55	76	73	39	108	038.0	16	.	.	.	23	13	01	.	.	10	06	10	08	03	10	.	.	.	.	.	01	04	01	.
VIII	5.6	5.5	5.2	5.4	226.8	14.8	94	64	85	81	43	173	044.4	09	.	.	.	18	09	.	.	.	06	09	14	11	05	14	.	.	.	.	.	.	06	05	.
IX	5.5	4.5	2.7	4.2	227.2	11.1	92	56	86	78	39	015	007.2	01	.	.	.	12	03	.	.	.	09	04	07	04	.	07	.	.	.	.	.	.	01	08	.
X	7.7	5.9	2.9	5.5	154.1	07.8	92	62	86	80	43	110	043.0	02	.	.	02	03	.	.	.	.	05	07	08	07	05	08	.	.	.	.	.	.	02	08	.
XI	8.1	7.5	6.2	7.3	080.9	06.9	89	69	85	81	40	033	011.6	22	.	.	02	.	.	.	.	.	01	14	08	06	02	08	.	.	.	.	.	.	.	09	.
XII	8.8	8.5	8.0	8.4	037.0	04.3	92	85	90	89	36	093	021.9	28	01	07	24	.	.	.	.	.	01	23	15	13	03	08	08	.	.	01	.	.	.	13	10
GOD.	7.0	6.9	5.5	6.5	1853.6	08.4	90	65	82	79	25	1220	044.4	9	VIII	03	20	83	79	31	01	.	.	45	145	156	125	45	135	41	13	.	01	.	01	31	72	-
SLUNJ																																					
BR. ST. 53																																					
H_o = 258 m H_b = - m h_v = 2.0 m h_r = 2.0 m																																					
I	9.9	9.3	9.3	9.5	-	04.3	91	84	87	87	31	108	036.5	01	03	12	22	.	.	.	.	.	.	28	12	10	03	06	08	.	.	.	.	.	.	05	12
II	7.9	7.6	7.0	7.5	-	04.4	83	77	80	80	18	139	026.3	15	03	03	18	.	.	.	.	.	02	15	13	13	05	08	10	.	.	.	.	.	.	.	18
III	6.6	8.0	5.8	6.8	-	04.7	79	70	80	76	19	140	028.0	12	.	.	14	.	.	.	.	.	05	14	11	11	06	08	08	01	.	.	.	.	.	.	12
IV	6.2	5.8	4.8	5.6	-	06.6	74	68	72	71	30	137	028.4	14	.	.	.	02	.	.	.	.	06	09	10	10	06	09	02	.	.	.	.	.	.	.	01
V	5.3	5.7	4.9	5.3	-	08.2	79	60	78	72	37	063	031.0	23	.	.	01	.	.	.	.	.	07	07	10	08	02	10	.	.	.	.	.	.	.	01	.
VI	5.6	5.8	5.3	5.6	-	12.8	84	62	81	76	31	168	047.4	10	.	.	.	18	01	.	.	.	05	07	11	10	05	11	.	.	.	.	01	.	12	04	.
VII	4.2	4.5	2.9	3.8	-	12.4	87	55	78	74	34	128	037.0	16	.	.	.	19	06	.	.	.	13	04	08	07	04	08	.	.	.	.	.	.	05	04	.
VIII	7.2	6.2	6.7	6.7	-	13.6	91	61	86	79	27	137	040.2	10	.	.	.	17	05	.	01	.	05	14	11	09	04	11	.	.	.	.	.	.	06	14	.
IX	5.9	4.4	3.9	4.8	-	10.1	89	56	82	76	28	012	004.4	01	.	.	01	11	03	01	.	.	09	08	06	03	.	06	.	.	.	.	.	.	01	16	.
X	6.6	5.2	3.8	5.2	-	07.4	90	61	84	78	39	087	031.3	02	.	.	03	02	.	.	.	.	09	10	09	07	03	09	02	01	.	.	.	.	01	13	.
XI	6.7	6.8	5.1	6.2	-	06.4	84	65	78	76	32	039	012.1	22	.	.	04	.	.	.	.	.	04	10	09	06	01	09	.	.	.	.	.	.	01	12	.
XII	8.0	7.4	7.5	7.6	-	04.1	91	78	88	86	31	104	025.3	28	02	10	23	.	.	.	.	.	03	19	13	12	03	07	07	.	01	.	.	.	02	16	10
GOD.	6.7	6.4	5.6	6.2	-	07.9	85	66	81	77	18	1262	047.4	40	VI	08	25	86	69	15	01	01	.	68	145	123	106	42	102	37	02	01	.	01	.	28	85	53
BISTRAC																																					
BR. ST. 54																																					
H_o = 160 m H_b = - m h_v = 2.0 m h_r = 1.0 m																																					
I	9.5	8.6	8.5	8.9	-	04.0	86	90	89	88	49	064	012.0	01	02	11	25	.	.	.	.	.	.	23	12	12	03	07	07	01	.	.	.	.	.	01	31
II	7.9	6.9	6.6	7.2	-	04.4	85	88	88	87	28	072	027.0	12	03	04	24	.	.	.	.	.	03	12	08	08	02	02	07	.	.	.	.	.	.	01	21
III	7.3	8.1	6.4	7.3	-	05.6	92	79	89	86	31	124	022.2	05	.	.	14	.	.	.	.	.	03	16	13	13	04	11	07	04	.	.	.	.	01	03	06
IV	7.7	6.8	5.4	6.6	-	07.5	92	67	88	82	39	158	028.2	14	.	.	01	02	.	.	.	.	.	09	16	16	06	14	04	02	.	.	.	.	01	03	01
V	5.1	6.6	5.9	5.9	-	08.9	87	61	80	76	31	062	018.0	22	.	.	01	.	.	.	.	.	02	09	09	09	02	09	.	.	.	.	.	.	03	.	.
VI	4.5	5.8	5.7	5.3	-	13.5	83	66	79	76	34	063	033.0	19	.	.	.	19	05	.	.	.	05	06	09	09	02	09	.	.	.	.	.	.	02	.	.
VII	4.6	4.7	4.2	4.5	-	14.3	87	71	82	80	30	111	045.2	16	.	.	.	22	10	.	.	.	07	07	07	07	03	07	.	.	.	.	.	.	.	.	.
VIII	5.4	5.8	6.4	5.9	-	15.4	90	78	91	86	57	260	060.7	09	-	.	-	15	04	-	.	.	06	09	10	10	08	10	.	.	.	.	.	.	04	04	.
IX	6.2	3.8	2.8	4.3	-	11.1	91	67	85	81	49	047	021.2	02	.	.	.	06	.	.	.	.	07	04	05	05	03	05	.	.	.	.	.	.	.	05	.
X	5.3	5.1	3.2	4.5	-	07.7	90	67	85	81	37	098	029.4	03	.	.	07	.	.	.	.	.	10	07	07	07	03	07	.	.	.	.	.	.	.	05	.
XI	7.7	7.0	5.6	6.8	-	06.7	85	73	83	80	24	070	026.0	22	.	.	03	.	.	.	.	.	01	12	07	07	03	07	.	.	.	.	.	.	.	04	.
XII	8.1	8.5	8.3	8.3	-	04.2	88	86	88	88	65	063	031.5	28	01	08	24	.	.	.	.	.	.	19	11	08	01	04	08	.	.	.	.	.	.	08	10
GOD.	6.6	6.5	5.8	6.3	-	08.6	88	74	85	82	24	1192	060.7	9	VIII	-	23	-	64	19	-	.	.	44	133	114	111	40	92	33	07	.	.	.	.	11	34	69
SLJEME																																					
BR. ST. 55																																					
H_o = 1007 m H_b = 1015.7 m h_v = 2.0 m h_r = 1.8 m																																					
I	8.8	9.1	8.4	8.8	023.6	03.8	94	94	94	94	81	086	023.7	01	05	18	23	.	.	.	06	.	.	23	19	11	03	08	12	01	.	.	.	.	.	27	31
II	7.4	7.8	7.1	7.4	060.6	03.3	89	88	87	88	50	137	055.1	11	03	15	24	.	.	.	06	.	02	17	19	14	03	06	16	.	.	.	.	.	01	18	28
III	7.2	7.9	6.5	7.2	084.5	03.8	88	81	89	86	35	164	022.1	12	.	16	24	.	.	.	05	.	02	13	21	17	08	05	18	01	.	.	.	.	01	20	31
IV	7.7	6.9	5.4	6.7	128.9	04.7	80	71	77	76	35	184	030.1	29	.	01	14	.	.	.	05	.	02	11	19	16	07	14	12	01	04	01	02	.	02	13	20
V	5.5	7.3	5.0	6.0	191.8	05.9	77	65	78	74	45	089	020.6	22	.	.	03	.	.	.	04	.	03	08	17	10	04	14	04	01	.	.	.	01	06	10	03
VI	4.2	5.9	5.6	5.2	224.9	09.7	81	74	77	77	44	112	038.2	19	.	.	.	.	.	.	04	.	04	06	13	07	04	13	.	.	.	.	.	.	11	09	.
VII	4.4	5.8	3.5	4.5	255.5	09.8	79	73	79	77	52	144	053.6	16	.	.	.	.	.	.	05	.	06	07	08	08	04	08	.	.	.	.	.	.	03	06	.
VIII	4.4	5.8	5.0	5.1	195.2	11.0	89	81	87	86	55	221	039.2	25	.	.	.	.	.	.	05	.	05	08	17	14	08	16	.	.	.	.	.	01	10	12	.
IX	4.4	4.5	2.7	3.8	157.0	08.2	78	74	79	77	48	049	021.8	17	.	.	.	.	.	.	03	.	07	03	12	07	02	12	.	.	.	.	.	.	02	07	.
X	4.9	5.4	3.0	4.4	125.3	06.0	83	74	81	79	45	089	024.6	03	.	.	09	.	.	.	04	02	09	06	09	07	04	06	04	.	02	.	.	.	02	11	04
XI	6.7	6.8	5.3	6.3	090.7	05.2	85	74	83	80	28	083	026.0	16	.	.	11	.	.	.	12	01	04	09	09	08	03	09	04	02	.	.	.	.	01	15	01
XII	6.2	6.1	4.9	5.7	083.9	03.3	81	78	80	80	31	074	015.9	28	02	11	24	.	.	.	09	04	08	11	13	12	02	06	12	.	.	.	01	.	.	21	10
GOD.	6.0	6.6	5.2	5.9	1621.9	06.2	83	77	82	81	28	1432	055.1	44	II	10	61	134	.	.	.	68	07	52	122	176	131	52	117	82	06	06	01	03	02	39	169	128

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Otles)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Pm (0-12): N Č	N J.	NE Č	NE J.	E Č	E J.	SE Č	SE J.	S Č	S J.	SW Č	SW J.	W	W J.	NW Č	NW J.	C Č
STUBIČKA GORA — φ = 45° 56' N λ = 15° 59' E Gr. Δ G = + 1h 04 min. — BR. ST. 56																												
I	-	-01.2	-00.3	-01.2	-01.0	01.4	-03.4	10.4	06,05	-09.1	24	06	01.5	25	02.0	08	01.9	13	03.0	12	04.0	12	03.6	.	.	17	01.3	.
II	-	-01.3	01.1	-00.3	-00.2	02.7	-03.1	09.4	06	-10.8	17	04	01.5	23	03.0	03	01.3	16	03.2	02	02.0	21	04.2	06	03.5	08	02.4	01
III	-	00.9	03.5	01.6	01.9	04.6	-00.6	13.4	24	-06.7	02	06	01.5	23	02.9	01	01.0	19	03.7	08	03.5	19	03.5	04	02.5	13	03.0	.
IV	-	05.8	09.0	06.7	07.0	11.0	03.5	22.4	19	-03.5	04	07	03.0	17	02.9	05	01.8	15	03.1	03	03.3	27	03.4	07	02.4	09	02.3	.
V	-	09.4	13.1	09.9	10.6	15.0	07.1	19.1	14,10	-00.6	01	07	02.1	23	02.6	06	01.7	09	02.3	02	02.0	23	03.1	07	02.6	16	02.6	.
VI	-	16.5	19.9	16.3	17.2	21.4	13.7	26.2	23	05.8	03	05	03.0	15	02.5	07	02.4	13	02.7	.	.	20	02.6	19	02.8	08	01.8	03
VII	-	16.4	20.0	16.8	17.5	21.9	13.8	27.4	24	05.8	16	08	02.2	22	03.1	12	02.0	20	02.8	03	03.0	08	03.6	09	02.8	11	02.5	.
VIII	-	16.7	20.4	17.1	17.8	21.5	14.6	28.2	06	09.8	24	01	01.0	10	02.6	08	01.8	23	02.8	05	02.2	26	02.8	08	02.0	11	02.5	01
IX	-	13.4	17.2	13.7	14.5	18.3	11.1	25.8	11	03.2	29	05	02.6	20	03.4	18	01.8	16	03.3	01	02.0	09	03.2	13	02.0	07	03.1	01
X	-	07.6	11.6	08.5	09.0	12.7	05.8	23.5	09	-01.2	16	06	01.5	18	03.9	05	01.8	13	02.8	03	02.3	26	03.8	10	03.2	09	03.4	03
XI[1]	-	06.2	08.6	06.7	07.1	09.8	04.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-00.9	01.1	-00.6	-00.2	02.9	-02.6	11.6	01	-08.0	25	11	01.5	22	03.3	04	01.0	13	02.5	06	02.0	16	03.1	08	01.2	11	01.7	02
GOD.	-	07.5	10.4	07.9	08.4	11.9	05.4	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ZAGREB-GRIČ — φ = 45° 49' N λ = 15° 59' E Gr. Δ G = + 1h 04 min. — BR. ST. 57																												
I	746.4	-00.7	01.0	00.2	00.2	02.2	-01.6	10.9	06	-05.4	08,03	04	01.5	21	01.4	19	01.1	16	01.6	08	01.2	13	01.2	08	01.4	04	01.8	.
II	743.3	00.5	04.1	02.2	02.2	05.1	-00.7	14.0	09	-05.7	20,17	05	01.2	19	01.9	11	01.7	04	01.5	07	01.6	11	02.3	20	02.0	07	02.1	.
III	744.3	03.2	07.8	05.5	05.5	08.8	02.6	18.3	24	-04.2	02	04	02.5	23	02.2	09	01.8	03	01.7	07	01.3	08	02.6	26	02.0	13	01.7	.
IV	745.6	08.2	13.7	10.3	10.7	15.4	06.9	25.8	19	-00.1	04	07	01.9	19	01.8	05	01.8	06	01.3	06	01.7	12	02.0	23	02.0	12	01.9	.
V	747.0	11.6	17.4	13.7	14.1	18.8	09.9	23.8	14	01.6	01	13	02.2	17	01.9	08	01.5	04	01.5	08	02.0	09	02.2	16	02.2	16	01.9	02
VI	747.8	18.4	24.3	20.1	20.7	25.2	16.1	30.5	28,23	08.7	03	11	01.5	17	01.8	14	01.9	09	01.7	05	02.0	08	02.0	15	02.0	11	01.6	.
VII	747.1	18.1	24.2	20.5	20.9	25.8	15.9	30.5	14	09.6	16	12	02.0	21	01.8	12	01.5	04	02.0	12	01.7	05	02.2	13	01.8	14	01.4	.
VIII	746.8	18.1	24.1	20.5	20.8	25.0	16.9	32.0	07,06	13.3	27,26	15	01.7	24	01.4	11	01.5	05	02.0	10	01.5	04	02.0	10	01.6	13	01.8	01
IX	750.6	13.8	20.8	16.6	16.9	21.3	13.2	29.6	11	03.8	30	18	01.4	29	01.6	12	01.4	07	01.7	07	02.1	07	02.0	08	01.6	02	02.0	.
X	750.5	07.9	14.3	10.7	10.9	14.8	07.3	22.9	09,08	00.9	19	11	01.4	20	01.6	09	01.4	07	01.3	12	01.5	11	02.2	17	02.2	05	02.4	01
XI	748.2	07.6	11.9	09.2	09.5	12.6	06.6	19.9	04	-00.1	27	07	01.6	12	01.4	12	01.2	04	01.5	07	02.1	17	02.2	25	02.2	06	02.2	.
XII	751.6	00.6	02.6	01.1	01.3	03.4	-00.5	13.1	01	-04.8	27	05	02.8	23	01.6	07	01.0	07	01.3	12	01.2	09	01.6	23	01.5	07	01.3	.
GOD.	747.4	08.9	13.8	10.9	11.1	14.9	07.7	32.0	6,7 VIII	-05.7	17. II	112	01.7	245	01.7	129	01.5	76	01.6	101	01.6	114	02.0	204	01.9	110	01.8	04
TOPUSKO — φ = 45° 18' N λ = 15° 59' E Gr. Δ G = + 1h 04 min. — BR. ST. 58																												
I	-	-01.4	01.4	-01.3	-00.6	02.1	-04.1	11.6	05	-11.0	03,02	09	01.3	09	01.1	13	01.6	11	01.5	.	.	15	01.3	16	01.2	07	01.4	13
II	-	-01.1	04.6	00.4	00.9	05.8	-04.4	15.2	09	-16.4	20	06	01.5	06	01.7	07	02.1	12	01.2	02	01.5	20	01.5	13	01.6	08	01.4	10
III	-	01.8	08.4	04.3	04.7	09.4	-00.4	20.3	24	-07.6	08	09	01.2	07	01.7	02	01.5	08	01.4	07	01.7	22	02.1	12	01.3	16	01.6	10
IV	-	06.9	14.4	08.8	09.7	16.0	03.3	27.0	19	-02.0	05	05	02.2	03	01.7	08	02.1	13	01.7	04	01.5	24	01.9	16	01.7	12	01.9	05
V	-	10.3	17.8	11.2	12.6	18.9	05.7	25.0	14	-01.6	02,01	09	01.4	08	02.0	09	01.9	10	01.5	04	01.0	15	01.7	16	01.9	14	01.6	06
VI	-	17.2	25.1	17.5	19.3	25.7	12.1	31.2	28	04.0	04	04	01.0	09	01.7	05	01.8	12	01.5	04	01.2	14	01.4	11	01.6	22	01.4	09
VII	-	16.8	25.5	17.6	19.4	26.1	12.1	32.5	23	08.0	06	07	01.4	13	01.8	12	01.7	17	01.5	08	01.9	09	01.9	09	01.0	05	01.2	13
VIII	-	16.8	25.5	18.3	19.7	26.0	13.5	35.2	07	07.8	27	11	01.7	07	01.6	10	01.6	10	01.3	04	01.2	08	01.4	09	01.1	11	01.2	23
IX	-	11.9	21.9	13.6	15.3	23.0	08.5	32.6	11	-01.6	28	01	01.0	12	01.3	09	01.7	08	01.8	04	01.5	08	01.2	10	01.4	12	01.8	26
X	-	06.9	15.6	08.6	09.9	16.6	03.7	26.4	08	-03.6	25	13	01.5	07	02.6	09	01.8	11	01.5	08	02.1	12	01.5	06	02.0	11	01.5	16
XI	-	05.9	13.2	07.3	08.4	14.0	02.6	22.0	03	-02.6	27	05	01.2	12	01.1	03	01.3	04	01.2	05	01.6	30	01.5	12	01.2	09	01.1	10
XII	-	-01.2	03.3	-00.5	00.3	04.0	-03.9	19.0	01	-15.2	27	17	01.4	09	01.2	08	01.2	11	01.4	05	01.2	18	01.0	10	01.1	08	01.0	07
GOD.	-	07.6	14.7	08.8	10.0	15.6	04.1	35.2	7.VIII	-16.4	20 II	96	01.4	102	01.6	95	01.7	127	01.5	55	01.6	195	01.6	140	01.4	135	01.5	150
ZAGREB-MAKSIMIR — φ = 45° 49' N λ = 16° 02' E Gr. Δ G = + 1h 04 min. — BR. ST. 59																												
I	749.7	-01.8	00.4	-01.2	-00.9	01.5	-03.4	10.2	05	-11.2	03	09	01.2	16	01.8	16	01.6	09	01.0	11	01.1	07	01.6	01	02.0	.	.	24
II	746.6	-01.2	03.7	00.9	01.1	05.1	-03.0	14.7	09	-11.0	20	08	01.4	20	01.9	07	02.0	04	01.0	09	01.7	10	02.7	06	02.8	.	.	20
III	747.5	02.0	08.1	04.6	04.8	09.2	00.6	18.6	24	-08.8	02	21	01.7	18	02.7	03	01.7	.	.	05	01.8	20	02.2	11	01.8	.	.	15
IV	748.7	07.1	13.8	08.5	09.5	15.4	04.2	25.2	18	-02.8	04	21	01.9	13	02.5	06	01.8	01	02.0	03	02.0	16	02.4	12	01.8	03	01.3	15
V	750.1	11.2	17.2	12.0	13.1	18.6	07.6	23.6	14	-01.2	01	19	01.6	15	02.7	05	01.4	05	02.2	05	01.4	16	02.2	13	02.2	02	01.5	13
VI	750.8	18.0	24.4	18.0	19.6	25.4	13.8	30.7	23	06.5	03	23	01.7	16	02.1	03	01.7	06	01.8	08	01.4	13	02.2	06	02.2	01	01.0	14
VII	750.1	18.0	24.2	18.3	19.7	25.9	13.5	30.8	23	09.2	06,02	30	01.6	14	02.8	09	01.7	07	01.6	07	01.7	10	01.9	05	01.8	07	01.5	09
VIII	749.8	17.6	24.6	18.9	20.0	25.7	14.9	32.8	06	09.8	26	32	01.5	12	02.2	07	01.9	08	01.1	02	01.5	05	02.2	05	01.8	04	02.0	18
IX	753.7	12.2	21.5	14.4	15.6	22.4	10.5	31.0	11	-00.6	30	32	01.5	10	02.0	07	01.9	04	01.8	08	01.8	09	01.8	03	02.0	.	.	17
X	753.6	06.5	14.7	09.0	09.8	15.6	04.3	25.0	10	-02.8	19	23	01.6	14	02.1	03	02.0	03	01.0	11	01.4	16	02.4	09	02.2	01	04.0	13
XI	751.4	05.7	12.0	07.7	08.3	13.0	03.8	20.4	04	-03.0	27	15	01.3	15	01.3	03	02.3	03	01.3	08	01.6	23	02.3	11	02.6	.	.	12
XII	754.9	-00.8	02.3	-00.2	00.3	03.3	-02.7	12.8	01	-11.6	27	17	02.1	15	02.3	05	01.2	06	01.0	14	01.5	17	01.5	04	02.2	02	01.5	13
GOD.	750.6	07.9	13.9	09.2	10.1	15.1	05.3	32.8	6 VIII	-11.6	17 XII	250	01.6	178	02.2	74	01.7	56	01.4	91	01.5	162	02.1	86	02.1	15	01.7	183
BOŽJAKOVINA — φ = 45° 49' λ = 16° 17' E Gr. Δ G = + 1h 05 min. — BR. ST. 60																												
I	-	-02.2	00.3	-01.4	-01.2	01.5	-04.0	09.9	05	-13.2	03	19	01.7	17	02.0	09	01.0	01	01.0	14	01.4	10	01.6	05	02.2	15	01.1	03
II	-	-01.0	03.4	00.6	00.9	04.6	-03.0	13.6	09	-10.1	20	13	03.0	11	01.7	07	01.4	08	01.5	08	01.2	17	02.2	09	03.4	11	01.8	.
III	-	02.6	08.3	05.0	05.2	09.1	01.0	18.5	24	-07.0	02	24	03.0	13	03.2	02	01.5	03	01.3	10	02.2	12	02.9	13	02.8	16	01.9	.
IV	-	07.6	14.1	09.5	10.1	15.5	04.7	25.6	19	-02.1	04	21	03.5	07	02.4	02	01.5	05	01.6	05	02.0	20	02.2	11	02.8	19	01.6	.
V	-	12.1	17.5	12.5	13.6	18.7	07.3	23.2	14,10	00.1	01	15	03.2	13	01.6	03	01.0	06	01.5	04	01.5	20	02.6	16	02.6	15	01.6	01
VI	-	18.7	24.6	18.4	20.0	25.5	13.7	31.0	22	06.9	03	24	02.2	13	01.8	03	01.0	03	01.7	05	01.0	21	02.1	09	02.2	12	01.3	.
VII	-	18.6	24.3	19.1	20.3	25.9	13.4	31.0	23	09.0	27	22	03.0	10	01.8	05	01.6	06	01.8	03	01.7	14	02.4	12	02.1	20	01.6	01
VIII	-	18.3	24.7	19.7	20.6	25.7	14.6	32.4	07	09.1	26	17	01.8	19	01.8	02	01.5	09	01.6	07	02.1	06	01.8	08	01.6	25	01.5	.
IX	-	13.1	21.5	14.9	16.1	22.1	10.3	30.3	11	00.5	30	22	01.9	13	02.2	03	01.0	07	01.3	07	01.6	11	02.1	09	02.3	16	01.2	02
X	-	06.6	15.0	08.6	09.7	15.7	04.1	25.4	10	-01.7	19	12	02.2	08	02.0	07	01.4	05	01.2	05	01.4	26	02.0	13	02.1	15	01.3	02
XI	-	05.7	12.1	07.6	08.2	12.9	03.6	19.4	14	-01.7	17	16	01.7	10	01.2	03	01.0	05	01.0	05	02.2	30	02.1	11	02.3	10	01.3	.
XII	-	-00.8	02.0	-00.3	00.1	02.9	-03.0	11.8	02	-14.7	27	22	02.5	08	01.6	11	01.2	01	01.0	08	01.5	23	01.6	11	01.4	09	01.0	.
GOD.	-	08.3	14.0	09.5	10.3	15.0	05.2	32.4	7.VIII	-14.7	17. XII	227	02.5	142	02.0	57	01.2	59	01.4	81	01.6	210	02.1	127	02.3	183	01.5	09

1) NEDOSTAJE JEDAN DAN OSMATRANJA

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlas)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dlas)	min	Padavine R mm Σ	max	min	Broj dana n sa: Tn ≤ -20,0	Tn ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F(0-12) ≥ 6	F(0-12) ≥ 8	Nm(0-10) ≤ 8,0	≥ 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	▷	✱	✱	△	≈	▲	▲	⊤	≡	≡
BR. ST. 56						**STUBIČKA GORA**																																
H_o = 620 m H_b = - m h_o = 2,0 m h_r = 2,0 m																																						
I	9.5	8.9	7.6	8.7	-	03.9	86	87	84	86	27	075	013.1	06	.	16	22	.	.	.	03	01	.	22	12	12	01	05	08	01	.	.	.	.	.	20	12
II	7.2	7.5	7.7	7.5	-	03.8	85	78	79	80	41	079	025.1	11	02	08	23	.	.	.	06	.	02	17	19	14	02	05	15	.	.	.	.	.	01	06	24
III	7.3	8.4	6.1	7.3	-	04.5	86	79	86	84	28	146	020.2	12	.	03	22	.	.	.	03	.	03	16	17	17	08	03	14	.	01	.	.	.	01	09	26
IV	7.8	7.4	5.2	6.8	-	09.5	75	68	73	72	23	173	036.0	29	.	.	06	.	.	.	03	.	02	11	14	12	07	10	07	01	01	.	.	.	01	11	08
V	5.3	6.5	5.5	5.8	-	06.9	73	65	74	70	41	076	026.6	22	.	.	01	.	.	.	03	.	03	08	11	09	03	10	01	.	.	.	.	.	04	04	.
VI	4.8	5.5	5.1	5.2	-	10.7	74	65	73	71	40	093	037.9	19	.	.	.	05	.	.	01	.	08	06	09	06	03	09	.	.	.	.	.	.	04	03	.
VII	4.1	4.9	3.2	4.1	-	12.0	81	74	80	78	52	106	036.4	16	.	.	.	12	.	.	01	.	13	05	07	07	04	07	.	.	.	.	01	.	04	04	.
VIII	5.8	6.7	5.3	5.9	-	13.2	87	80	85	84	64	188	056.1	25	.	.	.	07	.	.	.	.	04	09	12	124	07	12	.	.	.	.	.	.	07	06	.
IX	5.1	4.2	2.9	4.0	-	09.9	79	73	79	77	38	036	014.8	17	.	.	.	01	.	.	02	.	10	05	09	05	02	09	.	.	.	.	.	.	02	.	.
X	5.4	5.1	2.9	4.4	-	07.2	85	75	81	80	56	074	024.8	21	.	.	02	.	.	.	07	.	11	05	06	06	03	05	02	.	.	.	.	.	.	04	01
XI[1]	7.0	7.1	5.8	6.6	-	06.3	85	78	82	82	-	085	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	7.2	7.6	5.5	6.7	-	03.9	85	82	84	84	58	071	022.3	28	.	11	22	.	.	.	05	01	05	14	13	11	02	07	07	01	.	.	.	.	.	13	10
GOD.	6.4	6.6	5.2	6.1	-	07.3	81	75	80	79	-	1202	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 57						**ZAGREB-GRIČ**																																
H_o = 157 m H_b = 162,5 m h_o = 6,0 m h_r = 2,0 m																																						
I	9.6	9.2	8.6	9.2	010.4	-	-	-	-	-	-	080	020.2	01	.	12	20	.	.	.	01	.	.	26	15	11	02	09	07	01	01	01	.	.	.	14	19
II	6.5	7.6	6.7	6.9	073.4	-	-	-	-	-	-	071	026.2	11	.	04	16	.	.	.	04	.	04	13	17	08	03	11	13	03	.	.	.	.	01	08	15
III	7.3	8.1	6.5	7.3	096.6	-	-	-	-	-	-	106	025.2	12	.	.	04	.	.	.	02	.	03	18	18	14	04	10	16	04	.	.	.	.	.	06	04
IV	8.1	7.6	5.2	7.0	144.0	-	-	-	-	-	-	139	029.0	14	.	.	01	01	.	.	06	.	.	11	18	12	09	17	04	02	.	.	.	01	01	03	.
V	6.2	7.0	5.0	6.1	199.6	-	-	-	-	-	-	068	018.9	22	.	.	.	.	.	.	06	.	03	09	15	10	03	15	.	.	.	.	.	01	06	.	.
VI	5.0	6.1	5.8	5.6	235.1	-	-	-	-	-	-	077	025.8	19	.	.	.	17	02	01	02	.	04	08	10	05	03	10	.	.	.	.	.	.	08	.	.
VII	4.5	4.9	3.3	4.2	283.9	-	-	-	-	-	-	100	035.4	01	.	.	.	20	04	03	07	.	10	06	08	05	03	08	.	.	.	.	.	.	05	.	.
VIII	4.9	6.0	5.7	5.6	228.7	-	-	-	-	-	-	175	055.9	09	.	.	.	15	03	03	01	.	04	09	11	09	06	11	.	.	.	.	.	01	08	.	.
IX	4.9	3.8	3.7	4.1	202.2	-	-	-	-	-	-	038	016.9	17	.	.	.	06	.	.	.	.	09	04	10	04	01	10	.	.	.	.	.	01	.	01	.
X	5.7	5.8	3.6	5.0	141.8	-	-	-	-	-	-	076	029.3	03	.	.	.	.	.	.	04	.	07	07	09	06	03	09	.	.	.	.	.	.	01	09	.
XI	8.1	7.2	7.0	7.4	083.1	-	-	-	-	-	-	049	019.2	22	.	.	01	.	.	.	06	.	.	13	09	08	02	09	.	.	.	.	.	.	01	10	.
XII	7.9	8.1	7.4	7.8	040.3	-	-	-	-	-	-	051	021.8	28	.	07	19	.	.	.	04	.	01	17	14	10	01	08	08	.	02	.	.	.	.	14	10
GOD.	6.6	6.8	5.7	6.4	1739.1	-	-	-	-	-	-	1030	055.9	9 VIII	.	23	61	59	09	07	43	.	45	141	154	102	36	131	50	10	03	01	.	04	31	65	48
BR. ST. 58						**TOPUSKO**																																
H_o = 129 m H_b = - m h_o = 2,0 m h_r = 1,0 m																																						
I	9.8	9.2	9.1	9.3	-	04.4	94	95	96	95	74	069	016.3	07	03	12	31	.	.	.	.	.	.	28	14	10	02	08	07	.	.	.	.	.	.	17	31
II	8.5	7.6	7.2	7.8	-	04.9	89	89	94	91	68	141	028.5	11	05	02	23	.	.	.	.	.	02	16	12	12	05	07	08	.	.	.	.	.	01	10	21
III	7.2	7.8	6.7	7.3	-	06.2	96	86	96	93	64	133	024.2	12	.	.	19	.	.	.	01	.	02	16	15	10	06	13	07	02	.	.	.	.	02	08	07
IV	7.5	7.8	4.9	6.7	-	08.8	96	83	94	91	51	152	036.2	29	.	.	07	03	.	.	01	.	.	07	14	12	05	14	03	.	.	.	.	.	01	02	01
V	7.0	7.0	6.0	6.7	-	10.8	97	86	96	93	62	046	018.5	23	.	.	03	01	.	.	.	.	.	11	11	08	02	11	.	.	.	.	.	.	03	10	.
VI	5.2	6.5	5.4	5.7	-	16.6	98	85	96	93	73	109	048.6	30	.	.	.	19	04	.	.	.	03	05	13	11	03	13	.	.	.	.	.	04	08	03	.
VII	5.4	5.5	3.3	4.7	-	16.7	96	84	96	92	60	178	073.0	26	.	.	.	21	07	.	01	.	09	04	09	07	05	09	.	.	.	.	.	01	05	08	.
VIII	6.9	5.6	3.9	5.5	-	17.0	98	86	97	94	72	190	063.7	10	.	.	.	16	04	.	.	.	02	07	11	09	05	11	.	.	.	.	.	01	06	20	.
IX	7.2	4.3	3.2	4.9	-	13.4	98	89	97	95	66	014	007.6	01	.	.	01	11	04	.	.	.	06	03	05	03	.	05	.	.	.	.	.	.	.	17	.
X	6.5	4.7	4.9	5.3	-	09.6	98	95	97	97	56	056	023.5	02	.	.	06	02	.	.	.	.	03	07	06	05	02	06	.	.	.	.	.	.	.	22	.
XI	7.8	7.0	5.6	6.8	-	08.4	97	91	95	94	72	038	010.5	16	.	.	09	.	.	.	.	.	01	11	09	08	01	09	.	.	.	.	.	.	01	11	.
XII	9.5	8.5	7.6	8.5	-	04.7	96	92	96	95	71	085	017.2	24	02	05	29	.	.	.	.	.	01	21	12	11	03	06	07	.	.	.	.	.	.	13	10
GOD.	7.4	6.8	5.6	6.6	-	10.1	96	88	95	93	51	1211	073.0	26 VII	10	19	128	73	19	.	03	.	29	136	131	106	39	112	32	02	.	.	.	06	27	141	70
BR. ST. 59						**ZAGREB-MAKSIMIR**																																
H_o = 123 m H_b = 127,6 m h_o = 2,0 m h_r = 2,0 m																																						
I	9.8	9.2	9.2	9.4	011.1	03.9	91	86	90	89	65	079	016.9	01	01	11	27	.	.	.	.	.	.	27	14	11	02	08	07	01	.	.	01	.	.	16	21
II	7.8	7.4	6.9	7.4	076.5	04.2	90	72	83	82	46	072	027.5	11	01	03	23	.	.	.	01	.	02	13	15	10	03	11	10	02	01	01	.	.	01	10	17
III	7.3	8.0	6.4	7.2	104.4	05.0	87	61	81	76	20	101	022.0	12	.	.	13	.	.	.	01	.	03	16	18	15	03	14	10	02	.	.	.	.	.	04	04
IV	7.9	7.3	5.1	6.8	150.3	06.4	81	54	79	71	24	138	029.8	29	.	.	03	03	.	.	03	.	.	09	16	11	05	16	04	04	.	.	.	.	01	04	.
V	6.2	7.2	5.3	6.2	188.0	07.9	79	53	78	70	35	061	011.9	22	.	.	02	.	.	.	02	.	02	08	13	09	03	13	.	.	.	.	.	.	07	.	.
VI	4.8	6.1	5.6	5.5	224.9	12.5	79	55	80	71	38	070	030.1	19	.	.	.	17	02	.	01	.	05	06	10	05	02	10	.	.	.	.	.	.	08	01	.
VII	4.4	5.2	3.2	4.3	269.0	12.4	77	54	81	70	37	092	036.4	16	.	.	.	20	06	.	02	.	07	05	09	06	03	09	.	.	.	.	.	01	05	.	.
VIII	4.9	5.5	5.7	5.4	228.4	13.8	87	60	86	78	40	168	048.5	09	.	.	.	16	03	.	01	01	03	08	10	09	06	10	.	.	.	.	.	01	09	.	.
IX	5.3	4.3	3.2	4.3	203.2	10.4	90	53	85	76	35	031	010.6	17	.	.	01	10	02	.	.	.	08	05	08	04	01	08	.	.	.	.	.	01	02	06	.
X	6.7	5.6	4.2	5.5	137.4	07.5	91	62	87	80	43	076	029.3	03	.	.	06	01	.	.	01	.	07	08	09	06	03	09	.	.	.	.	.	.	02	11	.
XI	8.1	7.2	6.5	7.3	085.3	06.7	91	67	86	81	37	049	017.7	22	.	.	02	.	.	.	03	.	.	11	10	08	02	10	.	.	.	.	.	.	01	09	.
XII	8.5	8.5	7.4	8.1	038.3	04.3	94	81	91	89	27	044	019.1	28	02	08	23	.	.	.	03	.	02	21	11	09	01	07	06	.	.	01	.	.	.	11	10
GOD.	6.8	6.8	5.7	6.4	1716.8	07.9	86	63	83	77	20	981	048.5	9 VIII	04	22	100	67	13	.	18	01	39	137	143	103	34	125	37	09	01	02	01	03	36	72	52
BR. ST. 60						**BOŽJAKOVINA**																																
H_o = 110 m H_b = - m h_o = 2,0 m h_r = 1,2 m																																						
I	9.9	9.2	8.7	9.3	-	03.9	91	88	89	89	65	092	016.6	01	02	12	28	.	.	.	.	.	.	27	19	13	05	11	09	.	.	.	.	.	.	12	25
II	8.5	7.2	7.1	7.6	-	04.0	86	72	83	80	43	088	024.5	11	01	04	22	.	.	.	02	.	01	18	17	13	03	10	10	01	.	.	.	.	02	06	07
III	7.2	7.8	6.9	7.3	-	05.0	86	63	76	75	20	103	022.3	12	.	.	11	.	.	.	04	.	.	15	19	13	03	15	10	.	.	.	.	.	.	04	02
IV	8.1	7.0	5.9	7.0	-	06.6	80	55	75	70	26	156	040.6	29	.	.	02	02	.	.	02	.	01	09	15	10	06	15	03	03	.	.	.	02	01	02	.
V	6.1	6.5	5.6	6.1	-	08.3	78	56	78	71	34	061	013.7	22	.	.	.	.	.	.	01	.	01	06	15	13	02	15	.	.	.	.	01	01	02	.
VI	5.2	5.9	5.9	5.7	-	13.0	78	56	83	73	37	094	034.4	19	.	.	.	17	03	.	.	.	02	07	11	08	03	11	.	.	.	.	01	.	02	.	.
VII	4.7	4.8	4.2	4.6	-	13.1	77	46	82	72	39	094	036.0	16	.	.	.	19	05	.	04	.	08	03	08	07	04	08	.	.	.	.	.	.	02	02	.
VIII	6.0	5.5	5.7	5.7	-	14.8	89	64	88	80	46	243	055.2	11	.	.	.	16	03	.	.	.	03	09	14	13	07	14	.	.	.	.	.	03	06	05	.
IX	6.1	4.3	3.3	4.6	-	11.0	88	57	86	77	41	040	015.3	27	.	.	.	09	01	.	.	.	08	06	05	05	02	04	.	.	.	.	.	.	.	06	.
X	7.6	6.1	3.5	5.7	-	07.6	91	65	88	81	41	078	034.6	03	.	.	08	01	.	.	01	.	04	10	08	07	03	08	.	.	.	.	.	.	02	14	.
XI	8.4	7.2	6.4	7.3	-	06.7	89	70	85	81	41	054	020.1	16	.	.	02	.	.	.	01	.	.	13	09	07	02	09	.	.	.	.	.	.	.	10	.
XII	8.9	8.2	7.7	8.3	-	04.3	91	86	91	89	35	059	016.6	28	03	09	26	.	.	.	.	.	02	22	14	13	01	07	07	.	.	.	.	.	.	14	10
GOD.	7.2	6.6	5.9	6.6	-	08.2	85	65	83	78	20	1162	055.2	44 VIII	06	25	95	64	12	.	15	.	30	145	154	122	41	127	39	04	.	.	01	06	16	77	44

1) NEDOSTAJE JEDAN DAN OSMATRANJA

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (dnev.)	Tmx	Tmn	Tax	Tat.	Tin	Tat.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
SISAK $\varphi = 45^\circ$ 30' N $\lambda = 16^\circ$ 22' E Gr. Δ G = + 1h 06 min. BR. ST. 61																												
I	751.2	-01.5	00.7	-00.4	-00.4	02.0	-03.6	12.8	05	-09.4	08,01	12	01.8	13	01.7	10	01.7	15	01.7	06	01.2	05	01.0	07	01.3	04	01.2	21
II	748.2	00.0	03.4	01.5	01.6	05.0	-02.9	14.9	09	-13.7	20	11	02.0	15	02.3	09	01.8	14	01.7	06	02.0	13	01.5	10	02.0	04	02.0	02
III	749.1	03.1	09.0	05.9	06.0	10.1	01.4	20.7	24	-04.9	01	14	02.4	11	02.3	12	01.6	07	01.6	14	01.6	14	02.2	10	02.0	04	01.0	07
IV	750.3	07.9	14.8	10.8	11.0	16.2	05.3	26.0	23	-00.9	04	21	02.5	12	02.3	09	01.2	02	01.5	01	02.0	10	02.5	10	02.0	06	01.3	19
V	751.7	11.9	18.1	13.0	14.0	19.1	07.9	24.2	16,14	00.2	01	09	02.8	10	02.6	05	02.0	06	01.5	.	.	25	02.0	17	02.0	12	02.2	09
VI	752.4	18.3	25.3	19.4	20.6	26.0	13.9	31.2	23	06.9	04	12	01.9	11	02.3	08	01.9	05	01.2	07	01.7	15	01.9	15	01.9	13	01.9	04
VII	751.7	18.0	25.0	19.8	20.7	26.1	13.9	31.9	15	09.7	16	14	02.1	12	02.3	14	01.9	11	01.5	02	02.5	11	02.0	15	01.8	06	01.5	08
VIII	751.3	17.6	25.3	19.9	20.7	26.4	14.9	33.6	07	10.4	26	16	02.0	10	02.0	20	01.6	04	01.5	05	01.4	08	01.6	15	01.7	09	01.3	06
IX	755.2	12.1	21.9	14.5	15.7	22.8	10.1	31.9	11	-00.7	30	11	02.1	09	02.0	10	01.5	05	01.2	07	01.1	20	01.2	11	01.5	13	01.2	04
X	755.0	06.3	15.4	09.3	10.1	16.4	04.3	26.1	09	-02.2	19	11	01.8	17	02.1	08	01.4	12	01.4	07	02.0	13	01.8	12	01.8	09	01.4	04
XI	752.8	06.4	13.1	08.4	09.1	13.8	04.1	20.7	03	-02.4	27	05	01.6	11	01.2	05	01.2	11	01.4	06	02.2	26	01.7	11	01.5	10	01.2	05
XII	756.2	-00.3	02.8	00.3	00.7	03.8	-02.6	16.0	01	-14.6	26	13	02.0	10	02.2	04	01.2	08	01.1	05	01.4	13	01.5	12	01.1	11	01.0	.
GOD.	752.1	08.3	14.6	10.2	10.8	15.6	05.6	33.6	7 VII	-14.6	16 XII	149	02.1	141	02.1	114	01.6	100	01.5	66	01.7	173	01.8	145	01.7	101	01.5	89
ČAZMA $\varphi = 45^\circ$ 45' N $\lambda = 16^\circ$ 37' E Gr. Δ G = + 1h 06 min. BR. ST. 62																												
I	-	-02.2	00.8	-01.3	-01.0	01.9	-04.5	10.4	06	-12.0	03	16	01.6	17	01.8	15	01.6	01	02.0	22	01.4	09	01.8	06	01.0	07	01.4	.
II	-	-00.4	03.4	00.4	01.0	04.6	-03.4	14.6	09	-12.0	20,02	10	02.1	13	02.8	16	02.0	02	01.0	24	01.8	10	02.4	06	02.0	03	01.0	.
III	-	03.4	08.8	04.6	05.4	09.5	01.1	19.4	24	-03.8	08	22	02.3	06	02.7	20	02.1	01	01.0	20	02.1	12	02.2	07	02.1	05	02.0	.
IV	-	07.6	14.4	09.0	10.0	15.7	04.3	26.0	19	-02.4	05	25	02.6	01	03.0	07	02.0	04	01.0	15	01.9	22	02.5	05	03.2	11	02.2	.
V	-	11.9	18.0	11.2	13.1	18.9	07.1	24.6	14	-00.4	04,01	14	02.6	09	02.3	10	01.6	05	01.0	12	01.5	21	02.3	09	02.6	13	01.7	.
VI	-	18.2	25.1	17.4	19.6	25.8	13.1	30.8	23	05.8	04,03	18	02.1	12	01.8	09	01.2	09	01.6	16	01.8	14	01.9	06	02.5	06	02.0	.
VII	-	18.5	24.5	17.8	19.7	25.9	13.3	31.0	23	08.6	27	17	02.0	12	02.2	19	01.5	06	01.7	16	01.5	11	02.5	05	01.6	06	01.3	01
VIII	-	17.9	25.1	18.2	19.8	25.7	14.2	32.6	07	08.2	26	16	01.6	13	01.9	21	01.4	08	01.8	11	01.3	08	01.6	05	01.4	11	01.8	.
IX	-	12.7	21.8	13.3	15.3	22.1	09.2	31.0	11	-01.4	30	20	02.1	18	01.7	17	01.2	01	02.0	12	01.6	10	01.9	02	01.5	08	01.6	02
X	-	06.8	15.7	08.1	09.7	16.1	03.8	26.6	11	-03.4	17	11	02.1	11	01.7	07	01.6	10	01.2	15	01.3	27	01.7	04	02.0	06	01.2	02
XI	-	06.5	12.6	07.4	08.5	13.2	03.5	20.4	03	-02.2	27,17	10	01.1	06	01.7	12	01.5	02	02.0	13	02.2	35	02.1	04	01.0	08	01.4	.
XII	-	-00.7	02.5	-00.4	00.2	03.4	-03.4	16.4	01	-14.4	26	19	01.8	12	02.0	08	01.2	07	01.0	09	01.7	23	01.0	09	01.2	06	01.7	.
GOD.	-	08.4	14.4	08.8	10.1	15.2	04.9	32.6	7 VIII	-14.4	16 XII	198	02.1	130	02.0	161	01.6	56	01.4	185	01.7	202	02.0	68	01.9	90	01.7	05
BJELOVAR $\varphi = 45^\circ$ 54' N $\lambda = 16^\circ$ 51' E Gr. Δ G = + 1h 07 min. BR. ST. 63																												
I	748.1	-02.7	01.2	-01.4	-01.1	01.8	-04.8	10.7	05	-12.0	09	08	01.4	33	01.2	13	01.0	05	01.0	04	01.0	21	01.0	04	01.0	05	01.0	.
II	745.0	-01.0	03.6	00.5	00.9	04.7	-03.4	14.7	09	-12.2	20	06	01.3	18	01.9	03	01.0	12	01.2	04	01.0	21	01.6	08	01.1	12	01.2	.
III	746.0	02.2	08.6	04.9	05.1	09.1	00.4	19.6	24	-04.9	02	06	02.2	22	01.9	13	01.8	12	01.1	05	01.2	23	02.2	06	01.5	06	01.3	.
IV	747.2	06.6	14.4	09.4	10.0	15.6	03.7	26.0	19	-03.2	04	11	02.5	16	01.4	05	01.0	15	01.2	03	01.0	21	02.0	05	01.2	14	01.6	.
V	748.6	11.1	18.2	12.4	13.5	18.8	06.8	23.8	10	-01.5	01	13	02.3	14	01.1	01	01.0	07	01.0	12	01.6	20	02.0	10	01.3	16	01.4	.
VI	749.4	17.3	25.3	18.5	19.9	25.7	12.5	31.4	22	06.2	03	11	01.9	18	01.7	11	01.1	16	01.0	07	01.0	10	01.5	10	01.6	07	01.4	.
VII	748.7	17.8	24.8	18.8	20.0	26.0	12.8	31.4	24	08.4	27	11	01.9	25	01.6	14	01.1	09	01.0	09	01.2	11	02.2	08	01.1	06	01.5	.
VIII	748.5	17.5	25.9	19.2	20.5	26.3	14.1	33.0	06	07.8	27	10	01.6	32	01.1	09	01.2	17	01.1	03	02.3	12	01.5	.	.	10	01.8	.
IX	752.2	11.9	22.0	14.1	15.5	22.4	09.4	30.0	11	-01.0	30	11	01.6	33	01.3	15	01.0	09	01.2	04	01.5	10	01.8	02	01.5	06	01.3	.
X	752.2	05.9	15.5	08.6	09.6	15.8	03.2	26.1	10	-03.5	25	13	02.2	16	01.3	11	01.2	23	01.1	14	01.1	11	02.1	01	01.0	04	01.0	.
XI	749.9	05.8	12.9	07.7	08.5	13.5	03.0	20.2	03	-02.7	17	04	02.5	14	01.2	05	01.0	16	01.2	06	01.3	36	01.6	06	01.5	03	01.3	.
XII	753.2	-00.9	02.6	-00.3	00.2	03.2	-03.5	16.3	01	-13.3	27	04	01.8	24	01.6	01	01.0	20	01.0	07	01.0	21	01.0	08	01.0	08	01.0	.
GOD.	749.1	07.6	14.6	09.4	10.2	15.2	04.5	33.0	6 VIII	-13.3	17 XII	108	02.0	265	01.4	101	01.2	161	01.1	78	01.2	217	01.7	68	01.3	97	01.4	.
NOVSKA $\varphi = 45^\circ$ 21' N $\lambda = 16^\circ$ 59' E Gr. Δ G = + 1h 06 min. BR. ST. 64																												
I	-	-01.4	00.6	-00.7	00.6	02.2	-03.3	13.5	05	-11.7	03	23	03.0	11	02.8	07	01.7	23	02.9	13	02.0	03	02.7	03	02.3	05	01.6	05
II	-	-00.1	03.4	01.5	01.6	05.2	-01.8	15.3	09	-09.1	20	26	03.5	02	03.0	02	02.5	21	03.1	10	02.8	03	03.3	07	02.6	06	02.7	07
III	-	02.8	08.3	05.2	05.4	09.4	01.6	20.3	24	-05.7	08	24	03.4	07	02.3	12	02.6	17	03.4	13	02.7	04	03.2	08	02.9	03	03.0	05
IV	-	07.7	14.2	10.0	10.5	15.8	05.6	26.5	19	-01.7	04	19	03.6	03	04.7	08	02.1	11	02.9	09	02.2	12	03.3	08	03.0	07	03.0	13
V	-	11.4	17.2	12.4	13.3	18.5	08.5	24.3	14,10	00.1	01	22	03.2	04	02.2	14	02.1	07	03.0	10	02.3	06	02.5	16	03.2	07	02.7	07
VI	-	17.4	24.8	18.5	19.8	25.6	14.0	30.8	23	05.1	03	22	02.6	03	02.7	13	02.0	08	02.9	09	02.6	05	02.2	15	02.7	03	02.7	12
VII	-	17.4	24.5	18.6	19.8	25.6	14.0	31.7	23	09.6	16	24	03.1	12	02.2	15	02.1	02	02.5	16	01.8	05	03.4	07	02.3	02	03.0	10
VIII	-	17.1	25.2	19.1	20.1	26.1	15.1	33.0	07	09.9	26	24	02.4	12	02.1	13	02.2	08	02.5	11	02.3	01	02.0	09	02.1	04	02.0	11
IX	-	12.2	21.8	14.3	15.7	22.5	10.6	31.5	11	00.1	30	22	02.6	12	01.6	13	01.9	04	01.8	08	02.4	.	.	06	02.0	05	01.4	20
X	-	06.3	14.9	09.4	10.0	15.8	05.3	25.2	10	-01.4	25	17	02.2	07	01.7	09	02.0	08	02.9	09	02.2	04	02.0	08	03.1	03	02.0	28
XI	-	06.5	12.6	08.8	09.2	13.6	05.1	21.1	03	-01.1	07	17	02.5	06	02.3	03	02.0	16	02.8	22	02.5	06	02.5	03	01.7	03	02.7	14
XII	-	-00.3	02.5	00.3	00.7	03.3	-01.7	15.7	01	-09.2	27	17	03.1	07	01.7	10	01.8	04	03.0	17	02.1	05	01.6	15	01.5	02	02.5	16
GOD.	-	08.1	14.2	09.8	10.6	15.3	06.1	33.0	7 VIII	-11.7	3 I	257	03.0	86	02.2	119	02.1	129	02.9	147	02.3	54	02.7	105	02.5	50	02.4	148
LIPIK $\varphi = 45^\circ$ 25' N $\lambda = 17^\circ$ 10' E Gr. Δ G = + 1h 09 min. BR. ST. 65																												
I	-	-01.5	01.3	-01.2	-00.6	03.1	-04.1	13.0	05	-15.4	03	10	02.0	10	02.2	11	01.5	07	01.9	08	02.5	10	02.1	14	02.0	23	02.2	.
II	-	00.1	04.0	00.5	01.3	05.6	-03.1	15.0	09	-13.0	20	21	02.3	09	03.0	11	01.8	04	02.0	06	02.5	13	02.6	11	02.5	09	02.3	.
III	-	02.2	09.0	04.5	05.0	10.2	00.5	20.9	24	-10.5	08	10	02.1	08	02.2	14	02.1	13	02.6	08	02.2	16	02.9	06	02.7	18	02.3	.
IV	-	07.2	14.8	09.0	10.0	16.2	04.3	26.3	19	-03.4	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	11.4	17.4	11.7	13.0	18.8	07.3	25.0	10	-01.0	02,01	10	02.7	11	02.2	10	01.7	11	02.5	04	02.8	07	03.3	15	03.2	25	03.0	.
VI	-	17.4	25.1	17.7	19.5	26.0	13.0	30.7	23	04.2	03	12	03.1	06	02.8	16	01.6	07	01.9	05	03.0	11	01.9	15	02.5	18	02.7	.
VII	-	17.2	24.6	17.9	19.4	26.0	12.9	31.8	22	09.3	27	09	02.9	16	02.6	10	01.6	07	02.0	08	02.2	10	02.4	14	02.5	19	02.4	.
VIII	-	16.8	25.4	18.1	19.6	26.2	14.0	32.9	07	08.2	26	08	03.2	09	02.1	13	01.5	06	01.2	10	02.0	12	02.3	12	02.5	23	02.4	.
IX	-	11.3	21.9	13.3	14.9	22.7	09.2	31.7	11	-00.7	30	10	03.1	07	02.4	19	01.7	11	02.1	05	02.2	06	02.3	13	02.5	19	02.5	.
X	-	05.2	15.3	07.9	09.0	16.0	03.4	26.4	10	-02.7	25	06	02.7	08	02.5	20	01.6	07	02.3	08	02.9	14	02.3	12	03.0	18	02.6	.
XI	-	05.4	12.9	07.5	08.3	13.9	03.4	20.7	19	-03.7	07	10	02.6	08	02.1	11	02.0	06	02.3	14	02.9	20	02.4	08	02.4	13	02.6	.
XII	-	-00.8	03.2	-00.3	00.5	04.2	-02.9	18.0	01	-14.3	27	15	02.3	03	01.7	11	01.8	10	01.9	09	01.7	18	02.0	10	02.0	17	01.9	.
GOD.	-	07.7	14.6	08.9	10.0	15.7	04.8	32.9	7 VIII	-15.4	3 I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (bles)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (bles)	Min	Padavine R mm Σ	Max	Broj dana n sa: Tn ≤ -20,0	Tn ≤ -10,0	Tn ≤ 0,0	Tn ≥ 25,0	Tn ≥ 30,0	Tn ≥ 20,0	F(0-12) ≥ 6	F(0-12) ≥ 8	Nm(0-10) < 2.0	Nm(0-10) > 8.0	R mm ≥ 0.1	R mm ≥ 1.0	R mm ≥ 10.0	●	⚹	⚹	△	∽	▲	▲	T	■	■
SISAK																																					
BR. ST. 61																																					
H_a = 98 m H_b = 105,9 m h_t = 2.0 m h_v = 1.5 m																																					
I	9.9	9.2	8.9	9.3	018.8	04.0	91	85	88	88	67	100	023.3	01	.	12	25	.	.	.	01	.	.	28	18	12	03	08	14	01	.	.	.	.	.	09	31
II	9.4	8.4	7.5	8.4	066.7	04.3	87	75	81	81	46	092	023.0	11	01	03	21	.	.	.	02	01	.	18	17	12	03	10	11	03	.	.	.	.	01	06	21
III	7.4	8.3	6.9	7.5	098.1	05.4	87	64	80	77	32	092	013.8	15	.	.	11	.	.	.	01	01	03	18	19	12	04	16	09	01	.	.	.	.	.	02	03
IV	7.8	8.4	4.9	7.0	139.8	06.9	84	53	71	69	32	116	029.6	29	.	.	01	04	.	.	06	.	01	11	16	11	04	16	03	02	.	.	.	.	.	.	.
V	6.1	7.2	5.5	6.3	231.2	07.7	78	45	72	65	25	058	011.8	23	.	.	.	.	.	.	02	01	03	09	14	11	01	14	.	.	.	.	.	.	06	02	.
VI	5.4	6.1	5.9	5.8	248.3	13.3	82	53	82	72	34	074	035.5	30	.	.	.	19	05	.	01	.	05	10	13	08	02	13	.	.	.	.	.	01	09	01	.
VII	4.7	5.1	4.1	4.6	299.4	13.6	84	55	81	74	34	112	029.5	01	.	.	.	20	07	.	02	01	09	05	10	07	04	10	.	.	.	.	.	.	06	07	.
VIII	5.6	5.3	5.4	5.4	247.7	14.6	93	59	88	80	39	145	035.7	11	.	.	.	17	04	.	03	02	05	10	11	08	05	11	.	.	.	.	.	01	10	15	.
IX	6.9	4.0	2.1	4.3	218.5	10.8	94	52	89	79	27	039	013.7	01	.	.	01	11	03	.	.	.	07	03	07	07	02	07	.	.	.	.	.	.	01	15	.
X	8.0	6.2	3.9	6.1	143.2	07.3	93	55	84	77	30	086	033.3	02	.	.	05	03	.	.	01	.	03	10	10	07	03	09	.	.	.	.	.	.	03	13	.
XI	8.6	8.2	6.0	7.6	095.2	06.3	86	58	78	74	29	043	012.2	22	.	.	03	.	.	.	01	.	.	15	10	06	02	10	.	.	.	.	.	.	.	07	.
XII	9.5	7.8	7.1	8.1	046.1	04.1	89	78	85	84	24	039	009.3	28	03	07	22	.	.	.	01	.	01	20	14	09	.	09	08	01	.	.	.	.	.	09	10
GOD.	7.4	7.0	5.7	6.7	1853.0	08.2	87	61	81	76	24	996	035.7	44 VIII	04	22	89	74	19	.	21	06	37	157	159	110	33	133	45	08	.	.	.	02	36	86	65
ČAZMA																																					
BR. ST. 62																																					
H_a = 144 m H_b = - m h_t = 2.0 m h_v = 1.2 m																																					
I	9.7	8.7	8.5	9.0	-	03.9	91	85	89	88	62	112	021.9	01	02	11	29	.	.	.	.	.	.	25	17	14	04	07	10	.	.	.	.	.	.	07	31
II	7.4	7.5	7.4	7.5	-	04.2	87	76	85	83	51	107	027.6	11	03	04	20	.	.	.	.	.	03	15	19	12	04	09	12	01	.	.	.	.	01	05	18
III	7.0	7.7	6.5	7.1	-	05.3	84	66	84	78	30	104	016.9	12	.	.	10	.	.	.	.	.	02	16	18	16	03	12	11	02	.	.	.	.	.	01	03
IV	6.5	7.3	4.8	6.2	-	06.9	83	59	78	73	32	159	035.2	29	.	.	04	02	.	.	.	.	02	11	16	12	05	16	03	02	.	.	.	.	03	.	.
V	5.4	6.7	6.4	6.2	-	08.3	80	54	83	72	35	058	012.4	23	.	.	03	.	.	.	.	.	01	07	15	12	02	14	02	01	.	.	.	.	06	.	.
VI	4.9	6.3	5.2	5.5	-	13.0	82	55	86	74	29	086	024.3	30	.	.	.	17	04	.	.	.	05	08	12	10	03	12	.	.	.	.	.	.	12	.	.
VII	3.9	4.7	3.4	4.0	-	13.3	81	57	88	75	40	102	036.5	01	.	.	.	22	05	.	.	.	09	05	10	06	04	10	.	.	.	.	.	.	03	.	.
VIII	5.0	5.2	5.0	5.1	-	14.4	90	63	91	81	47	237	053.1	11	.	.	.	16	03	.	.	.	07	09	14	12	07	14	.	.	.	.	.	.	09	.	.
IX	4.5	4.0	3.4	4.0	-	10.8	89	57	91	79	43	020	012.7	27	.	.	01	09	02	.	.	.	11	05	09	03	01	09	.	.	.	.	.	.	01	03	.
X	5.8	5.0	3.6	4.8	-	07.7	92	63	89	81	46	052	019.6	03	.	.	07	04	.	.	.	.	09	07	10	04	03	10	.	.	.	.	.	.	02	08	.
XI	7.5	6.1	6.1	6.6	-	06.7	88	67	85	80	40	051	021.3	16	.	.	06	.	.	.	01	.	02	10	11	07	02	10	.	.	.	.	.	.	01	04	.
XII	8.8	7.3	7.8	8.0	-	04.3	92	84	92	89	36	066	011.6	28	03	06	25	.	.	.	01	.	01	21	15	11	02	10	06	.	.	.	.	.	.	11	10
GOD.	6.4	6.4	5.7	6.2	-	08.2	86	65	86	79	29	1154	053.1	44 VIII	08	21	105	70	14	.	02	.	52	139	166	119	40	133	44	06	.	.	.	.	38	39	62
BJELOVAR																																					
BR. ST. 63																																					
H_a = 141 m H_b = 142.4 m h_t = 2.0 m h_v = 1.0 m																																					
I	9.7	8.6	8.8	9.1	-	04.0	95	86	92	91	69	090	017.8	01	04	13	28	.	.	.	01	.	.	25	15	14	03	07	10	02	.	.	.	.	.	12	31
II	8.1	7.1	7.1	7.4	-	04.5	93	80	91	88	52	084	026.0	11	01	03	23	.	.	.	.	.	02	17	19	14	02	10	13	03	.	.	.	.	01	06	18
III	6.5	7.8	6.9	7.1	-	05.1	90	61	80	77	30	080	015.5	12	.	.	15	.	.	.	.	.	02	15	17	15	02	16	09	07	.	.	.	.	.	02	02
IV	6.6	7.0	4.9	6.2	-	06.6	89	55	74	72	29	123	026.0	29	.	.	06	01	.	.	01	.	02	09	16	12	05	16	03	03	.	.	.	01	04	01	.
V	4.8	6.2	5.3	5.4	-	08.2	83	51	77	71	32	054	011.4	22	.	.	03	.	.	.	01	.	03	07	14	10	02	14	01	01	.	.	.	.	03	.	.
VI	4.6	5.2	4.0	4.6	-	12.8	84	53	81	73	35	054	016.5	19	.	.	.	21	03	.	.	.	06	06	13	11	02	13	.	.	.	.	.	01	08	01	.
VII	4.1	4.3	2.8	3.7	-	12.9	81	55	82	73	40	078	021.8	01	.	.	.	20	07	.	02	.	11	05	09	08	04	09	.	.	.	.	.	.	03	.	.
VIII	5.4	5.0	4.7	5.0	-	14.2	90	57	87	78	37	176	061.6	11	.	.	.	21	06	.	.	.	05	06	10	09	06	10	.	.	.	.	.	.	06	01	.
IX	4.4	3.5	2.6	3.5	-	10.5	91	52	88	77	40	018	005.0	18	.	.	01	10	01	.	.	.	11	03	10	06	.	10	.	.	.	.	.	.	01	02	.
X	6.5	4.9	3.5	5.0	-	07.4	92	59	87	79	44	046	017.5	03	.	.	06	02	.	.	.	.	08	07	06	05	03	06	.	.	.	.	.	.	01	09	.
XI	7.9	5.9	6.0	6.6	-	06.5	88	63	82	78	39	041	011.9	22	.	.	05	.	.	.	.	.	02	08	10	06	02	10	.	.	.	.	.	.	01	07	.
XII	9.1	7.7	8.0	8.3	-	04.3	92	82	92	89	34	049	008.0	24	04	07	28	.	.	.	.	.	01	21	13	09	.	08	07	01	.	.	01	.	01	14	10
GOD.	6.5	6.1	5.4	6.0	-	08.1	89	62	84	78	29	893	061.6	44 VIII	09	23	115	75	17	.	05	.	53	129	152	119	31	129	43	17	.	.	01	02	29	55	61
NOVSKA																																					
BR. ST. 64																																					
H_a = 136 m H_b = 134.7 m h_t = 2.0 m h_v = 1.0 m																																					
I	9.9	8.1	7.6	8.5	-	03.9	89	82	85	86	58	108	032.9	17	02	13	26	.	.	.	01	.	.	21	13	12	03	08	08	.	.	.	.	01	.	05	26
II	7.8	8.4	6.2	7.4	-	04.2	86	74	83	81	48	112	032.5	12	.	04	18	.	.	.	03	.	02	14	15	13	05	09	09	.	.	.	.	.	01	04	19
III	7.8	8.2	6.9	7.7	-	05.1	85	63	79	76	33	105	019.1	07	.	.	09	.	.	.	.	.	03	17	16	14	04	12	08	03	.	.	.	.	.	03	05
IV	7.3	8.3	4.6	6.7	-	06.6	82	55	71	69	31	092	023.3	14	.	.	02	02	.	.	02	.	.	08	14	13	04	14	01	.	.	.	.	.	01	.	.
V	7.4	8.3	5.1	6.9	-	08.3	83	58	77	72	40	054	015.1	23	.	.	.	.	.	.	.	.	03	13	12	08	01	12	03	.	.	.	.	.	02	02	.
VI	6.1	6.6	5.5	6.1	-	12.9	86	56	80	74	36	090	036.0	19	.	.	.	19	03	.	.	.	03	08	12	09	03	11	.	.	.	.	.	.	09	01	.
VII	4.9	5.3	3.3	4.5	-	13.0	83	57	83	74	41	092	025.0	17	.	.	.	20	07	.	01	.	09	08	11	09	03	11	.	.	.	.	.	.	04	01	.
VIII	5.7	5.1	3.5	4.8	-	14.0	90	59	86	78	47	167	054.3	11	.	.	.	17	03	.	.	.	10	08	12	07	05	12	.	.	.	.	.	.	09	03	.
IX	5.1	4.0	2.4	3.9	-	10.7	92	56	86	78	40	032	012.0	27	.	.	.	09	03	.	.	.	11	04	07	06	02	07	.	.	.	.	.	.	01	01	.
X	6.0	6.2	3.3	5.1	-	07.6	94	65	86	82	40	050	027.9	02	.	.	03	02	.	.	.	.	08	07	09	06	01	09	.	.	.	.	.	.	.	06	.
XI	7.7	7.5	4.8	6.7	-	06.7	87	64	80	77	41	050	013.3	22	.	.	03	.	.	.	01	.	01	10	12	09	01	12	.	.	.	.	.	.	.	03	.
XII	8.2	7.7	5.9	7.3	-	04.4	92	84	89	89	39	057	009.5	25	.	08	22	.	.	.	01	.	02	16	14	10	.	09	07	.	.	.	.	.	.	.	08	10
GOD.	7.0	7.0	4.9	6.3	-	08.1	87	64	82	78	31	1009	054.3	44 VIII	02	25	83	69	16	.	09	.	52	134	147	116	32	126	36	03	.	.	.	01	27	37	56
LIPIK																																					
BR. ST. 65																																					
H_a = 154 m H_b = - m h_t = 2.0 m h_v = 1.2 m																																					
I	9.5	8.5	8.3	8.8	-	04.0	90	82	89	87	61	110	032.5	17	05	09	27	.	.	.	.	.	.	19	14	11	03	07	09	.	.	.	.	.	.	07	29
II	8.0	8.1	8.2	8.1	-	04.2	86	73	84	81	46	111	029.9	12	03	04	20	.	.	.	01	.	01	20	16	15	04	08	10	.	.	.	.	.	01	06	15
III	7.2	8.1	6.8	7.3	-	05.1	86	61	82	76	31	092	015.9	07	01	.	12	.	.	.	01	.	03	16	15	14	03	13	07	02	.	.	.	.	.	01	05
IV	7.1	7.6	5.0	6.5	-	-	-	-	-	-	-	094	025.8	14	.	.	05	04	.	.	05	.	02	08	14	13	03	14	03	02	.	.	.	01	02	01	.
V	7.3	8.0	6.8	7.4	-	08.5	83	59	81	74	41	045	016.6	23	.	.	02	01	.	.	01	.	02	15	14	09	01	14	01	.	01	.	.	01	04	01	.
VI	6.3	6.7	5.4	6.1	-	13.1	84	57	84	75	36	071	036.4	19	.	.	.	20	04	.	02	.	03	10	12	08	01	12	.	.	.	.	.	01	10	.	.
VII	4.3	5.5	4.3	4.7	-	13.1	85	57	87	76	32	077	017.8	17	.	.	.	21	07	.	02	.	10	08	11	07	05	11	.	.	.	.	.	01	03	.	.
VIII	4.6	5.2	4.5	4.8	-	14.1	94	59	92	82	40	152	036.8	16	.	.	.	18	06	.	.	.	09	07	11	08	05	11	.	.	.	.	.	.	08	01	.
IX	6.1	4.3	3.2	4.5	-	10.4	95	54	90	80	34	047	028.1	17	.	.	02	08	03	.	01	01	08	04	05	04	02	05	.	.	.	.	.	.	02	04	.
X	6.3	5.6	3.7	5.2	-	07.4	96	63	91	83	32	052	026.1	02	.	.	05	02	.	.	.	.	08	08	07	05	01	07	.	.	.	.	.	.	.	09	.
XI	7.4	6.5	6.2	6.7	-	06.5	90	63	85	79	35	055	013.2	22	.	.	04	.	.	.	01	.	02	10	11	09	02	11	.	.	.	.	.	.	.	04	.
XII	8.6	7.7	7.7	8.0	-	04.3	94	80	91	88	42	054	008.9	26	03	04	25	.	.	.	01	.	01	19	14	10	.	09	06	.	.	.	.	.	.	13	10
GOD.	6.9	6.8	5.8	6.5	-	-	-	-	-	-	-	960	036.8	46 VIII	12	17	102	74	20	.	15	01	49	144	144	113	30	122	36	04	01	.	.	04	30	47	59

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		j.	č.	j.	č.
φ = 45° 36' N λ = 17° 14' E Gr. ΔG = + 1h 09 min.																												DARUVAR BR. ST. 66
I	746.9	-01.0	01.6	-00.7	-00.2	03.5	-03.5	14.0	15	-14.2	03	06	01.0	16	01.5	01	01.0	04	01.2	02	01.0	08	01.1	04	01.0	06	01.0	46
II	743.9	00.2	04.1	01.2	01.7	05.5	-01.9	15.0	09	-10.0	20	05	02.0	16	01.4	01	02.0	05	01.4	08	01.5	09	01.4	03	01.7	04	01.0	33
III	744.7	02.7	08.8	05.1	05.4	09.8	01.5	20.4	24	-08.7	08	07	01.0	13	01.1	04	01.2	06	02.0	03	01.7	12	02.0	05	01.6	.	.	43
IV	745.9	07.4	14.8	09.8	10.4	16.0	05.1	26.8	19	-02.0	04	09	01.9	09	01.8	03	01.0	05	01.4	04	01.2	13	01.7	08	01.8	03	01.7	36
V	747.3	11.7	17.9	12.6	13.7	19.2	08.3	26.2	10	00.0	02	10	01.6	06	01.3	01	01.0	02	01.0	11	01.4	05	01.8	12	01.7	06	01.8	40
VI	748.0	18.1	25.5	18.8	20.3	26.4	13.7	31.6	28	04.0	03	04	01.5	06	01.0	02	01.0	02	01.0	02	01.0	08	01.4	08	01.4	07	01.4	51
VII	747.4	18.2	24.5	18.7	20.0	26.0	13.7	32.9	23	09.9	27	09	01.4	13	01.5	.	.	02	01.0	03	01.0	06	01.5	03	01.0	11	01.2	46
VIII	747.0	17.4	25.6	18.9	20.2	26.6	14.7	33.0	07	08.8	26	07	01.0	06	01.0	.	.	01	01.0	02	01.0	07	01.0	04	01.0	05	01.0	61
IX	750.9	12.2	22.4	14.3	15.8	23.0	10.2	31.5	12	-00.4	30	08	01.4	04	01.0	01	01.0	.	.	03	01.0	02	01.5	07	01.7	02	01.0	63
X	750.9	06.6	15.3	09.1	10.1	16.2	04.9	27.4	09	-02.2	17	04	01.2	05	01.6	04	01.2	01	01.0	05	02.0	11	01.7	07	01.6	05	01.2	51
XI	748.7	06.6	12.9	08.4	09.1	13.7	05.0	20.4	03	-02.3	07	03	01.3	05	01.2	02	01.0	04	01.5	10	02.1	11	02.4	09	01.6	04	01.0	42
XII	752.0	-00.4	03.3	00.2	00.9	04.1	-01.9	17.4	01	-13.0	27	03	01.3	05	01.4	03	01.3	05	01.2	06	01.3	08	01.4	06	01.2	06	01.0	51
GOD.	747.8	08.3	14.7	09.7	10.6	15.8	05.8	33.0	7 VIII	-14.2	3 I	75	01.4	104	01.4	22	01.2	37	01.4	59	01.5	100	01.6	76	01.5	59	01.2	563
φ = 45° 20' N λ = 17° 41' E Gr. ΔG = + 1h 11 min.																												SLAVONSKA POŽEGA BR. ST. 67
I	-	-02.6	00.9	-01.5	-01.2	02.0	-04.6	08.0	05	-18.1	03	12	01.2	15	01.0	11	01.3	04	01.2	02	01.0	08	01.1	16	01.2	25	01.1	.
II	-	-01.3	04.0	00.5	00.9	05.8	-03.4	15.2	09	-11.9	03	15	01.5	09	01.0	05	01.4	01	01.0	02	01.0	16	01.9	19	01.1	17	01.4	.
III	-	01.7	08.9	05.1	05.2	-	00.5	-	-	-08.0	02	18	01.7	03	01.3	12	01.7	03	02.0	07	02.1	23	01.7	01	01.0	26	01.0	.
IV	-	06.9	15.6	09.4	10.3	16.4	04.5	26.4	24	-02.7	05	20	02.2	04	01.2	05	01.6	04	01.5	02	02.0	18	01.8	24	01.5	13	01.4	.
V	-	11.7	17.8	12.0	13.4	19.4	07.7	25.5	10	-00.8	01	17	02.4	09	01.4	03	01.7	.	.	04	02.5	17	01.5	24	01.5	19	01.1	.
VI	-	17.7	25.5	17.6	19.6	26.3	12.8	30.8	23	05.9	03	10	01.5	09	02.2	11	01.5	02	01.0	.	.	20	01.7	18	01.0	20	01.7	.
VII	-	17.5	25.4	18.1	19.8	26.4	13.1	32.5	23	08.2	20	10	02.1	10	02.0	.	.	06	02.0	07	01.1	12	01.7	28	01.2	20	01.4	.
VIII	-	17.4	26.2	18.3	20.0	26.9	14.2	34.6	07	08.9	28	04	01.5	16	01.4	05	01.2	05	01.2	04	01.0	14	01.1	27	01.3	18	01.4	.
IX	-	11.7	22.8	13.3	15.2	23.3	09.7	32.6	11	-00.9	30	11	01.6	11	01.8	05	01.0	05	01.4	02	01.5	20	01.1	23	01.1	13	01.1	.
X	-	04.7	16.0	08.2	09.3	16.6	03.4	25.6	10	-02.4	19	03	01.7	11	01.1	06	02.0	07	01.1	01	02.0	20	01.3	23	01.3	22	01.2	.
XI	-	04.5	12.9	06.5	07.6	13.6	02.7	22.6	03	-02.1	07	11	01.4	10	01.5	06	01.2	04	01.2	07	02.1	17	01.5	15	01.3	20	01.3	.
XII	-	-00.8	03.4	-00.2	00.6	04.2	-03.0	15.4	01	-16.1	27	12	01.3	10	01.3	04	01.2	07	01.1	04	01.2	15	01.3	22	01.2	19	01.3	.
GOD.	-	07.4	15.0	08.9	10.1	-	04.8	-		-18.1	3 I	143	01.7	117	01.4	73	01.5	48	01.4	42	01.6	200	01.5	240	01.3	232	01.3	.
φ = 45° 44' N λ = 17° 38' E Gr. ΔG = + 1h 11 min.																												PODRAVSKA SLATINA BR. ST. 68
I	-	-02.6	00.3	-01.6	-01.4	02.1	-04.7	14.6	05	-15.2	03	08	02.1	16	02.5	16	02.4	04	02.5	17	02.4	13	02.2	13	02.7	06	02.8	.
II	-	-00.9	02.6	00.3	00.6	04.6	-02.9	15.4	09	-09.4	20	06	02.5	05	02.0	14	02.6	03	01.7	18	02.5	14	02.4	17	02.5	07	02.0	.
III	-	02.6	08.1	05.1	05.2	09.7	01.1	19.4	24	-09.6	02	01	03.0	10	02.4	11	02.5	07	02.4	23	02.2	17	02.1	18	02.4	06	02.2	.
IV	-	07.8	15.1	09.8	10.6	16.5	04.9	25.8	26	-02.0	05	04	02.5	05	02.2	11	02.4	09	02.0	20	02.2	15	02.3	18	02.3	08	02.2	.
V	-	12.1	18.0	12.7	13.6	19.7	09.1	24.8	10,08	00.6	03	02	02.5	05	02.0	16	02.1	04	02.5	22	02.2	15	02.1	22	02.7	04	02.2	.
VI	-	17.9	25.3	17.9	19.8	26.1	14.1	31.6	23,22	07.0	03	08	02.5	07	02.6	10	02.0	03	01.7	22	02.1	21	02.2	16	02.9	03	02.7	.
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	12.8	22.0	13.8	15.6	22.9	10.1	32.5	11	01.3	30	16	01.6	05	01.6	07	01.3	05	01.0	01	01.0	06	01.2	24	01.2	15	01.3	11
X	-	07.2	15.3	09.3	10.3	17.1	04.6	26.2	09,08	-01.4	19	04	01.5	04	01.2	12	01.4	07	01.6	03	02.0	16	01.4	24	01.5	19	01.7	04
XI	-	06.0	12.7	07.9	08.6	-	03.5	-	-	-03.0	27,09	06	01.5	01	01.0	09	01.4	09	01.0	04	01.0	17	01.3	11	01.3	19	01.5	14
XII	-	-00.6	03.0	00.2	00.7	-	-	-	-	-	-	10	01.8	07	01.1	06	01.2	07	01.1	03	01.0	16	01.2	20	01.2	20	01.3	04
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 45° 10' N λ = 18° 01' E Gr. ΔG = + 1h 12 min.																												SLAVONSKI BROD BR. ST. 69
I	753.4	-02.4	00.3	-01.4	-01.2	02.0	-04.3	08.0	27	-15.3	03	10	01.6	23	02.0	13	01.8	03	01.0	03	01.3	16	01.5	08	01.9	06	01.7	11
II	750.3	-00.8	03.4	00.2	00.7	05.5	-03.4	15.2	09	-12.6	03	08	02.6	13	01.8	02	03.5	06	01.5	02	02.0	27	02.1	15	02.0	07	01.7	04
III	751.1	02.2	09.1	05.3	05.5	10.5	00.5	22.2	24	-07.0	02	06	02.5	24	02.4	06	02.7	.	.	08	01.6	26	02.3	11	02.0	06	02.2	06
IV	752.1	07.3	14.9	09.8	10.5	16.9	04.4	28.0	20	-03.6	05	13	03.8	12	01.9	11	01.7	01	03.0	05	01.8	22	02.9	08	02.5	10	02.5	08
V	753.3	11.0	17.4	12.2	13.2	19.6	07.4	27.0	10	-01.7	02	09	02.7	06	02.5	03	01.7	02	02.0	07	01.7	26	02.0	20	02.2	13	03.0	07
VI	754.0	17.0	24.6	18.3	19.6	26.2	12.5	31.4	23	04.7	03	08	01.9	12	02.2	08	01.6	04	02.0	09	01.8	23	02.0	11	02.0	07	02.4	08
VII	753.3	17.2	24.6	18.9	19.9	26.4	13.2	32.6	15	08.6	27	05	01.6	13	01.3	04	02.2	07	01.9	09	02.6	27	02.0	07	01.9	10	02.2	11
VIII	753.0	17.1	25.6	19.3	20.3	27.1	13.8	34.7	07	08.0	28	02	02.0	18	01.6	13	01.8	05	02.0	02	02.0	12	01.8	17	02.1	04	01.5	20
IX	756.9	11.5	22.0	14.3	15.5	23.6	09.1	33.7	11	-03.1	30	15	02.0	11	01.3	07	01.7	02	01.5	04	01.0	14	01.6	13	01.3	05	01.8	19
X	757.2	04.9	15.4	08.6	09.4	16.6	03.0	25.0	08	-03.3	19	06	01.8	23	01.5	06	01.5	02	02.0	05	01.2	13	01.3	21	02.1	05	01.6	12
XI	755.3	04.4	12.4	06.9	07.6	13.5	02.5	22.5	19	-03.3	13	06	02.5	18	01.7	08	01.8	08	01.1	06	01.3	19	01.8	10	01.9	04	01.5	11
XII	758.5	-01.2	02.4	-00.4	00.1	03.7	-03.7	15.5	01	-15.7	26	01	03.0	13	01.8	10	01.3	06	01.3	04	01.0	12	01.6	30	01.8	09	01.8	08
GOD.	754.0	07.4	14.3	09.3	10.1	16.0	04.6	34.7	7 VIII	-15.7	26 XII	89	02.4	186	01.8	91	01.8	46	01.6	64	01.7	237	02.0	171	02.0	86	02.1	125
φ = 45° 46' N λ = 18° 10' E Gr. ΔG = + 1h 13 min.																												DONJI MIHOLJAC BR. ST. 70
I	-	-03.0	00.5	-01.9	-01.6	01.4	-04.7	08.0	27	-14.9	03	01	02.0	09	01.8	24	02.2	16	02.2	02	01.5	05	01.6	17	01.8	19	02.7	.
II	-	-01.1	03.2	00.6	00.8	04.6	-03.0	14.0	09,06	-09.8	03	07	02.3	06	02.3	09	02.1	18	02.2	02	01.5	07	02.0	15	02.4	20	02.8	.
III	-	02.6	08.9	05.2	05.5	09.9	01.1	20.5	24	-08.8	02	05	03.0	08	03.5	12	03.0	15	02.7	08	02.8	10	02.8	13	02.4	22	02.6	.
IV	-	07.8	15.5	09.7	10.7	16.7	05.3	27.6	20	-02.2	04	12	03.2	01	05.0	11	02.2	17	02.6	09	01.8	13	02.4	07	02.0	20	02.7	.
V	-	12.1	18.3	12.8	14.0	19.7	08.4	25.8	10	00.5	03	07	03.0	03	02.7	06	02.3	15	02.2	02	02.0	05	03.6	26	02.4	29	03.0	.
VI	-	18.6	26.5	18.7	20.6	27.2	14.5	32.3	23	07.6	03	06	02.8	05	02.4	09	02.2	14	01.8	05	01.8	06	02.0	19	02.4	26	02.6	.
VII	-	18.4	25.7	18.9	20.5	27.2	14.3	33.2	24,23	09.4	20	08	02.9	08	01.8	07	01.7	10	01.6	09	01.9	05	02.2	17	02.1	29	02.7	.
VIII	-	18.1	26.3	19.1	20.6	27.1	15.2	34.8	07	10.5	19	08	01.6	09	02.2	17	01.8	15	02.1	07	01.6	03	01.0	12	02.0	22	02.5	.
IX	-	12.7	22.5	14.7	16.2	23.4	10.7	32.6	11	-00.2	30	11	01.9	03	02.3	10	02.0	13	02.0	11	01.9	04	01.8	14	02.1	24	02.2	.
X	-	06.1	16.0	09.0	10.0	16.8	04.5	25.7	09	-02.2	19	06	02.8	05	02.2	16	02.0	12	02.2	08	02.1	11	01.7	14	02.4	21	02.3	.
XI	-	04.9	12.6	07.5	08.1	13.5	03.4	21.5	03	-01.1	07	02	02.0	01	02.0	14	02.1	23	02.3	09	02.7	10	02.1	20	02.2	11	03.1	.
XII	-	-00.3	02.6	00.3	00.7	03.5	-02.0	13.7	01	-12.5	27	05	02.4	04	03.0	19	02.2	10	02.3	03	01.7	06	02.3	22	02.5	24	02.5	.
GOD.	-	08.1	14.9	09.6	10.5	15.9	05.6	34.8	7 VIII	-14.9	3 I	78	02.6	62	02.4	154	02.2	178	02.2	75	02.0	85	02.2	196	02.3	267	02.6	.

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e mm	U % 7	14	21	Sred. (Dies)	min	Padavine R mm Σ	max	dan	Broj dana n a: Tn ≤ -10,0	Tx ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	F (0-12) ≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	♨	♨	≈	▲	▲	⚡	≡	▦
BR. ST. 66							**DARUVAR**																														
																																					H_o = 161 m H_b = 162.2 m h_p = 2.0 m h_z = 2.0 m
I	8.9	7.9	7.7	8.2	026.4	03.9	86	76	84	82	59	098	023.1	17	05	10	23	.	.	.	.	.	.	19	17	11	03	11	11	01	.	.	02	.	.	04	27
II	7.2	7.9	6.5	7.2	062.5	04.1	82	71	80	78	45	108	023.0	12	01	03	19	.	.	.	.	.	.	11	18	13	03	10	11	03	.	.	.	.	01	.	17
III	6.5	7.6	6.7	7.0	109.3	05.0	83	59	79	74	29	086	012.4	28	.	.	09	.	.	.	.	.	01	13	17	14	01	13	08	01	.	.	.	.	.	.	04
IV	6.4	7.1	4.4	6.0	163.0	06.6	83	52	73	69	30	093	032.2	14	.	.	03	02	.	.	.	.	01	05	14	11	02	14	02	.	.	.	.	.	02	02	.
V	5.6	6.9	5.2	5.9	180.4	08.6	82	57	79	73	35	043	013.0	23	.	.	.	01	.	.	.	.	02	07	14	08	01	14	.	.	.	.	.	.	03	01	.
VI	4.1	5.5	4.0	4.5	240.3	13.0	82	53	81	72	34	079	030.1	30	.	.	.	21	05	.	.	.	07	04	12	07	02	12	.	.	.	.	.	.	11	01	.
VII	3.8	4.7	3.0	3.8	266.4	14.4	87	64	90	80	49	121	020.8	16	.	.	.	20	07	.	.	.	13	07	12	08	06	12	.	.	.	.	.	.	04	.	.
VIII	4.7	4.4	3.1	4.1	264.4	14.0	90	59	86	78	41	223	065.8	10	.	.	.	20	05	.	.	01	11	05	11	11	05	11	.	.	.	.	.	.	08	.	.
IX	4.8	3.3	2.8	3.6	222.4	11.2	95	56	91	81	43	030	015.5	27	.	.	01	09	03	.	.	.	12	03	09	06	01	09	.	.	.	.	.	.	01	02	.
X	5.7	5.3	3.0	4.7	147.9	07.5	92	61	83	79	39	057	024.3	02	.	.	03	02	.	.	.	.	07	06	09	05	02	09	.	.	.	.	.	.	01	06	.
XI	7.2	6.3	5.5	6.3	099.2	06.5	84	62	81	75	35	038	010.6	22	.	.	03	.	.	.	.	.	02	11	11	08	01	11	.	.	.	.	.	.	01	02	.
XII	7.6	7.5	5.8	7.0	047.2	04.4	92	79	90	87	38	064	014.3	24	02	04	21	.	.	.	.	.	03	13	12	09	02	07	06	.	.	.	.	.	.	10	10
GOD.	6.0	6.2	4.8	5.7	1829.4	08.3	86	62	83	77	29	1040	065.8	40 VIII	08	17	82	75	20	.	.	01	59	104	156	111	29	133	38	05	.	.	02	.	32	28	58
BR. ST. 67							**SLAVONSKA POŽEGA**																														
																																					H_o = 152 m H_b = - m h_p = 2.0 m h_z = 1.0 m
I	8.7	8.2	8.0	8.3	-	03.8	87	84	87	86	43	124	032.8	17	03	09	27	.	.	.	.	.	01	21	17	13	04	11	08	.	.	.	.	.	.	12	31
II	7.9	8.1	6.1	7.4	-	04.3	89	76	88	84	46	099	017.2	12	02	04	24	.	.	.	.	.	01	15	16	15	04	09	10	.	.	.	.	.	.	09	13
III	6.9	7.4	5.5	6.6	-	05.4	90	67	85	81	40	094	019.6	07	.	-	11	-	-	.	.	.	01	10	17	12	03	12	08	01	.	.	.	.	01	03	01
IV	6.0	6.9	4.1	5.7	-	07.2	85	56	81	74	29	065	015.8	14	.	.	04	05	.	.	02	.	.	05	12	08	02	12	.	.	.	.	.	.	01	01	.
V	5.7	7.0	5.2	6.0	-	09.3	86	63	86	79	42	054	011.2	28	.	.	02	01	.	.	.	.	01	06	14	11	01	14	.	.	.	.	.	01	02	01	.
VI	5.0	6.4	4.9	5.4	-	13.4	86	58	84	76	41	082	042.2	19	.	.	.	21	01	.	.	.	01	01	17	09	02	17	.	.	.	.	.	01	14	.	.
VII	4.0	5.5	4.4	4.6	-	13.9	87	61	85	78	46	060	017.2	26	.	.	.	21	11	.	.	.	06	07	11	10	02	11	.	.	.	.	.	01	04	01	.
VIII	4.4	4.9	3.9	4.4	-	14.9	91	65	91	82	48	118	034.2	18	.	.	.	23	07	.	.	.	07	02	13	08	05	13	.	.	.	.	.	01	11	02	.
IX	5.5	4.4	3.3	4.4	-	11.2	92	62	91	81	13	054	030.6	17	.	.	01	12	05	.	.	.	08	04	10	05	02	10	.	.	.	.	.	01	01	01	.
X	5.4	5.2	3.7	4.8	-	07.8	94	69	92	85	48	038	019.0	02	.	.	06	03	.	.	01	.	09	05	08	06	01	08	.	.	.	.	.	.	.	02	.
XI	7.1	6.2	5.9	6.4	-	06.9	94	71	93	86	48	045	014.6	22	.	.	04	.	.	.	.	.	01	09	12	10	01	12	.	.	.	.	.	.	.	06	.
XII	7.1	7.1	6.7	7.0	-	04.4	93	84	91	89	43	042	011.1	25	01	05	25	.	.	.	.	.	01	12	13	11	01	08	06	.	.	.	.	.	.	08	09
GOD.	6.1	6.4	5.1	5.9	-	08.5	89	68	87	81	13	875	042.2	49 VI	06	-	104	-	-	.	03	.	37	97	160	118	28	137	32	01	.	.	.	05	34	46	54
BR. ST. 68							**PODBAVSKA SLATINA**																														
																																					H_o = 120 m H_b = - m h_p = 2.0 m h_z = 1.0 m
I	9.8	8.2	8.4	8.8	-	03.6	85	83	84	84	63	115	028.5	17	04	11	28	.	.	.	.	.	01	24	14	10	05	07	09	02	.	.	.	.	.	04	07
II	9.0	9.2	7.8	8.6	-	04.2	85	84	83	84	28	116	025.0	11	.	05	22	.	.	.	.	.	.	20	18	16	02	07	11	.	.	.	.	.	.	01	03
III	6.6	6.5	7.4	6.9	-	05.7	83	79	82	81	56	109	020.2	15	.	.	12	.	.	.	.	.	05	15	14	12	04	11	04	.	.	.	.	.	.	.	.
IV	4.9	5.1	3.8	4.6	-	08.2	82	80	79	80	57	064	013.1	14	.	.	03	04	.	.	.	.	09	07	10	10	02	10	01	.	.	.	.	.	.	.	.
V	6.8	5.4	5.6	5.9	-	09.2	79	68	78	73	47	-	-	-	.	.	.	.	.	.	.	.	05	10	06	06	03	-	-	-	-	-	-	-	-	-	-
VI	3.5	5.3	4.9	4.6	-	11.4	69	55	67	64	35	050	022.2	19	.	.	.	21	04	.	.	.	09	06	09	09	01	09	.	.	.	.	.	.	.	.	.
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	4.9	3.4	3.2	3.8	-	11.0	87	60	87	78	38	030	012.6	06	.	.	.	.	04	.	.	.	10	03	08	05	01	08	.	.	.	.	.	.	02	01	.
X	5.6	4.6	4.4	4.8	-	07.7	87	64	86	79	39	056	022.4	03	.	.	01	02	.	.	.	.	08	10	06	05	02	06	.	.	.	.	.	.	.	06	.
XI	7.1	6.2	4.3	5.8	-	06.6	86	67	82	78	31	026	007.5	22	.	-	05	-	-	.	.	.	04	09	09	08	.	09	.	.	.	.	.	.	.	04	.
XII	8.6	7.5	6.6	7.6	-	-	-	-	-	-	-	060	012.0	26	-	-	-	-	-	.	.	.	01	18	12	11	02	07	06	.	.	.	.	.	.	09	10
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 69							**SLAVONSKI BROD**																														
																																					H_o = 88 m H_b = 90. m h_p = 2.1 m h_z = 1.2 m
I	9.7	8.8	8.9	9.2	018.9	03.9	93	85	90	89	70	096	024.8	17	05	09	28	.	.	.	01	.	.	25	16	10	03	11	10	.	.	02	.	.	.	15	31
II	8.1	8.5	7.4	8.0	073.7	04.2	91	74	86	84	51	089	014.8	11	02	02	25	.	.	.	05	01	01	16	20	14	02	10	14	04	.	.	.	.	.	11	17
III	7.9	8.1	8.1	8.0	110.3	05.2	87	62	81	77	28	074	019.1	28	.	.	15	.	.	.	04	01	01	22	17	11	02	13	10	04	.	.	.	.	01	03	03
IV	7.7	8.4	5.6	7.2	163.1	06.9	89	53	76	73	29	062	019.7	29	.	.	04	05	.	.	12	03	.	11	14	11	02	14	.	.	.	.	.	.	.	01	.
V	7.3	8.0	7.5	7.6	176.8	08.5	86	57	80	74	33	052	010.9	28	.	.	03	01	.	.	06	01	01	17	14	10	01	14	.	.	.	.	.	.	03	06	.
VI	6.1	6.5	6.1	6.2	238.7	13.1	87	57	82	75	38	143	052.4	19	.	.	.	22	03	.	08	01	02	09	15	12	05	15	.	.	.	.	.	01	12	07	.
VII	4.7	5.6	4.0	4.8	272.9	12.8	84	55	82	74	40	043	016.1	17	.	.	.	21	11	.	06	03	07	08	11	06	01	11	.	.	.	.	.	.	02	06	.
VIII	5.1	5.4	4.5	5.0	266.5	13.6	91	54	84	76	39	076	029.7	22	.	.	.	23	08	.	02	01	07	08	11	09	02	11	.	.	.	.	.	.	08	14	.
IX	6.3	4.9	4.2	5.1	194.6	10.3	94	50	88	77	23	047	028.8	17	.	.	02	11	05	.	01	.	07	06	10	04	02	10	.	.	.	.	.	.	01	20	.
X	7.4	5.4	4.8	5.8	149.1	07.2	96	59	86	80	40	047	023.3	02	.	.	06	01	.	.	02	.	06	11	07	06	02	07	.	.	.	.	.	.	.	21	.
XI	7.5	6.8	7.3	7.2	104.2	06.4	92	66	84	81	36	047	008.7	07	.	.	07	.	.	.	03	01	02	13	13	11	.	13	.	.	.	.	.	.	.	14	.
XII	9.0	7.5	7.4	8.0	036.2	04.3	93	84	91	89	42	038	007.3	23	02	04	28	.	.	.	01	.	01	18	15	11	.	10	06	.	.	02	.	.	01	24	10
GOD.	7.2	7.0	6.3	6.8	1805.0	08.0	90	63	84	79	23	814	052.4	49 VI	09	15	118	84	27	.	51	12	35	164	163	115	22	139	40	08	.	04	.	01	28	142	61
BR. ST. 70							**DONJI MIHOLJAC**																														
																																					H_o = 97 m H_b = - m h_p = 2.0 m h_z = 1.5 m
I	8.5	7.5	7.5	7.9	-	03.8	85	83	94	88	49	097	031.2	17	04	10	26	.	.	.	.	.	01	17	16	10	03	09	10	03	.	.	.	.	.	02	31
II	8.0	7.6	8.0	7.9	-	04.4	90	82	93	89	47	095	021.0	11	.	04	21	.	.	.	.	.	01	19	22	15	03	10	16	.	.	.	.	.	01	02	28
III	7.5	7.5	6.9	7.3	-	05.4	84	68	85	79	32	095	016.2	15	.	.	10	.	.	.	02	.	01	14	17	12	04	14	06	02	.	.	.	.	01	01	06
IV	5.5	7.0	4.6	5.7	-	07.0	85	53	78	72	30	064	011.4	29	.	.	02	04	.	.	.	.	03	06	16	12	01	16	01	01	.	.	.	02	02	.	.
V	6.5	7.3	5.3	6.3	-	08.7	81	57	78	72	33	043	007.8	14	.	.	.	01	.	.	.	.	03	12	15	10	.	15	.	.	.	.	.	.	03	01	.
VI	3.2	4.9	4.6	4.2	-	12.9	79	49	80	69	31	100	031.4	30	.	.	.	23	07	.	.	.	09	03	13	08	03	13	.	.	.	.	.	.	08	01	.
VII	3.6	4.5	3.7	4.0	-	13.3	81	54	84	73	35	055	012.7	18	.	.	.	22	11	.	.	.	14	07	13	08	03	13	.	.	.	.	.	.	05	.	.
VIII	4.5	3.4	3.8	3.9	-	14.0	86	57	84	76	41	140	068.5	22	.	.	.	22	07	01	.	.	12	06	13	09	04	13	.	.	.	.	.	01	08	01	.
IX	4.9	3.7	2.7	3.8	-	10.7	89	52	84	75	30	014	004.2	06	.	.	01	13	04	.	.	.	11	07	12	04	.	12	.	.	.	.	.	.	01	01	.
X	5.4	5.0	3.6	4.7	-	07.3	93	56	86	78	15	042	014.8	02	.	.	03	07	.	.	.	.	10	06	10	05	02	08	.	.	.	.	.	.	.	06	.
XI	7.0	6.0	5.0	6.0	-	06.4	89	66	82	79	35	028	007.3	22	.	.	03	.	.	.	.	.	03	10	17	08	.	15	.	.	.	.	.	.	.	04	.
XII	9.0	7.6	7.1	7.9	-	04.5	92	84	92	89	53	067	017.0	24	01	05	25	.	.	.	.	.	01	17	18	12	02	11	08	02	.	.	.	.	.	08	10
GOD.	6.1	6.0	5.2	5.8	-	08.2	86	63	85	78	1[illegible]	840	068.5	22 VIII	05	19	59	88	30	01	02	.	69	124	182	113	25	149	41	08	.	.	.	03	29	27	75

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm: 7	14	21	Tmin	Tmax	T	Tmax	Tmin	Tmin	N		NE		E		SE		S		SW		W		NW		C
											f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.	j.		j.	f.	j.	f.
DJAKOVO $\varphi = 45^\circ 17'$ N $\lambda = 18^\circ 25'$ E Gr. $\Delta G =$ + 1h 14 min.																											BR. ST. 71
I	-	-03.0	00.3	-02.0	-01.7	01.5	-05.9	08.0	05	-15.5	03	17	01.2	18	01.2	06	01.3	07	01.0	01	01.0	11	01.1	03	01.0	30	01.8	.
II	-	-00.6	03.1	00.3	00.8	04.3	-03.2	14.2	09	-14.0	03	12	02.1	03	01.3	.	.	16	01.5	05	01.4	16	01.6	04	01.5	28	02.7	.
III	-	02.8	08.8	05.3	05.5	09.7	00.8	21.0	24	-09.8	02	06	02.3	05	02.4	04	02.2	11	02.0	12	01.2	15	01.7	04	01.8	36	01.7	.
IV	-	08.2	15.0	10.0	10.8	16.4	05.1	27.0	20	-04.5	05	18	02.2	03	02.0	.	.	11	01.7	07	01.4	17	01.8	04	01.5	30	02.0	.
V	-	12.1	17.6	12.6	13.7	18.5	08.3	24.5	10	-00.2	02,01	22	02.1	07	01.7	01	02.0	04	02.5	03	01.3	20	02.2	03	01.0	33	02.2	.
VI	-	18.3	25.0	18.2	19.9	25.8	13.7	30.5	23	08.0	03	08	01.9	01	01.0	02	02.0	19	01.6	08	01.6	18	01.5	02	01.0	32	01.8	.
VII	-	18.5	25.1	18.5	20.1	26.1	13.7	32.6	15	10.0	27	17	02.1	06	01.5	.	.	08	01.8	07	01.3	08	01.8	01	01.0	46	01.5	.
VIII	-	17.9	26.0	18.9	20.5	26.7	14.3	34.2	07	09.8	19	15	01.7	05	01.2	02	01.0	15	01.7	18	01.2	11	01.2	04	01.2	23	01.6	.
IX	-	13.3	21.3	14.5	15.9	22.2	10.2	32.5	11	-01.0	30	18	01.7	03	02.0	01	01.0	10	01.2	07	01.1	14	01.3	01	01.0	36	01.7	.
X	-	06.2	15.5	09.0	09.9	16.2	02.8	24.8	09	-04.0	24	11	01.6	06	01.0	01	02.0	12	01.7	08	01.5	14	01.4	02	01.0	39	01.4	.
XI	-	04.7	12.2	07.7	08.1	13.0	03.2	21.2	03	-01.2	07	07	01.6	01	01.0	.	.	16	01.6	05	01.0	16	01.4	.	.	45	01.4	.
XII	-	-00.6	02.7	00.1	00.6	03.4	-02.8	15.6	01	-18.0	27	08	01.1	05	01.4	.	.	09	01.2	08	01.1	37	01.2	01	01.0	25	01.4	.
GOD.	-	08.2	14.4	09.4	10.3	15.3	05.0	34.2	7 VIII	-18.0	17 XII	159	01.8	63	01.4	17	01.6	138	01.6	89	01.3	197	01.5	29	01.3	403	01.7	.
BRESTOVAC-BELJE $\varphi = 45^\circ 42'$ N $\lambda = 18^\circ 44'$ E Gr. $\Delta G =$ + 1h 15 min.																											BR. ST. 72
I	753.7	-03.5	00.2	-02.6	-02.1	00.9	-05.7	05.7	05	-15.3	09	09	02.0	21	01.7	16	01.7	03	01.3	15	01.5	06	01.7	13	01.5	10	02.4	.
II	750.7	-01.4	02.8	00.2	00.5	03.9	-02.5	14.7	09	-10.5	03	10	02.8	13	01.8	02	01.5	06	02.5	19	01.6	11	02.1	06	02.2	17	02.1	.
III	751.8	02.0	08.8	04.8	05.1	09.6	00.9	20.4	24	-11.6	02	14	02.6	10	02.1	07	02.1	10	02.1	12	02.2	19	02.1	09	01.7	12	02.2	.
IV	752.5	07.8	15.0	10.1	10.7	16.4	05.2	26.7	20	-02.0	05,04	16	03.2	09	02.0	04	02.2	09	02.6	15	01.8	12	02.6	14	01.9	11	01.9	.
V	753.4	12.3	18.1	12.8	14.0	19.4	08.5	25.6	15	00.3	01	14	02.9	05	01.4	04	01.8	06	01.8	07	01.6	04	02.5	28	02.2	25	02.4	.
VI	754.4	18.6	25.4	18.7	20.4	26.1	14.2	31.5	23	09.1	03	12	02.4	08	01.8	07	01.6	09	01.8	05	02.4	08	01.8	17	02.0	24	02.3	.
VII	753.6	18.6	25.3	18.9	20.4	26.4	14.3	32.6	23	10.3	27	17	02.9	07	02.0	05	01.0	06	02.3	11	01.5	09	01.9	19	01.9	19	02.8	.
VIII	753.7	17.9	25.6	19.0	20.4	26.3	14.9	33.0	07	10.0	26	10	01.8	14	01.7	12	01.4	06	01.8	10	01.7	10	01.3	12	01.5	19	02.3	.
IX	757.2	12.4	21.5	14.1	15.5	22.4	10.0	33.0	11	-01.1	30	19	02.0	08	01.6	06	01.2	06	01.8	08	01.2	07	01.9	21	01.5	14	01.7	.
X	757.3	05.8	15.6	08.9	09.8	16.2	04.4	24.9	07	-01.8	19	06	01.7	15	01.7	08	01.2	07	02.1	15	01.4	11	01.5	19	02.0	12	02.6	.
XI	755.5	04.7	12.1	06.9	07.6	13.0	03.3	21.0	03	-01.4	09	05	02.6	05	01.2	07	01.4	05	01.6	23	01.9	24	01.9	07	01.6	14	01.9	.
XII	758.3	-00.6	02.8	-00.1	00.5	03.5	-02.7	14.0	01	-15.4	27	06	02.3	12	02.0	03	02.0	04	01.8	14	01.6	09	01.6	27	01.8	18	02.1	.
GOD.	754.3	07.9	14.4	09.3	10.2	15.3	05.4	33.0	7 VIII	-15.4	17 XII	138	02.5	127	01.8	81	01.6	77	02.0	154	01.7	130	01.9	192	01.8	195	02.2	.
OSIJEK $\varphi = 45^\circ 32'$ N $\lambda = 18^\circ 44'$ E Gr. $\Delta G =$ + 1h 15 min.																											BR. ST. 73
I	753.5	-03.1	00.4	-02.4	-01.9	01.6	-05.2	05.6	28	-15.9	03	18	01.4	11	01.2	05	01.2	19	01.3	10	01.0	03	01.0	19	01.3	06	02.0	.
II	750.4	-01.3	03.1	-00.2	00.4	04.0	-02.7	14.6	09	-11.6	03	10	02.2	08	01.6	07	02.0	11	01.4	19	01.5	01	02.0	10	01.9	18	02.0	.
III	751.4	01.9	09.2	05.1	05.4	10.1	01.2	21.2	24	-10.2	02	08	01.9	08	02.1	07	01.7	14	02.4	12	01.8	12	01.8	17	01.6	15	01.9	.
IV	752.1	07.3	15.4	10.2	10.8	16.9	05.3	28.0	20	-02.3	05	16	02.2	02	01.5	07	01.9	13	01.8	12	01.5	08	01.5	19	01.9	13	02.5	.
V	753.3	11.5	18.4	13.3	14.2	19.9	08.5	27.2	15	00.2	01	16	02.1	06	01.3	01	01.0	11	01.4	03	01.3	11	01.5	26	01.5	19	01.8	.
VI	754.0	17.8	25.4	19.3	20.4	26.6	14.3	31.8	23	07.8	03	21	01.4	08	01.8	03	01.0	09	01.0	05	01.4	06	01.0	20	01.4	18	01.7	.
VII	753.3	17.8	25.6	19.4	20.6	26.8	14.5	33.6	23	09.9	20	22	01.5	06	01.2	06	01.0	10	01.0	10	01.0	02	01.0	13	01.5	24	01.7	.
VIII	753.2	17.5	26.0	19.5	20.6	27.0	15.5	34.3	07	10.1	28	16	01.4	16	01.1	11	01.1	09	01.0	11	01.2	04	01.2	10	01.3	16	01.3	.
IX	757.0	11.9	22.0	14.6	15.8	23.0	10.5	33.3	11	-00.7	30	14	01.3	15	01.1	02	01.5	10	01.0	09	01.3	10	01.0	11	01.2	19	01.4	.
X	757.3	05.5	16.0	09.3	10.0	16.8	04.4	26.0	09	-01.8	19	14	01.5	13	01.2	06	01.5	13	01.2	10	01.0	04	01.2	17	01.5	16	01.2	.
XI	755.4	04.4	12.5	06.8	07.6	13.5	03.0	22.3	03	-01.2	09	05	01.0	06	01.3	01	01.0	07	01.7	30	01.5	15	01.5	15	01.5	11	01.9	.
XII	758.4	00.4	02.7	00.2	00.7	03.7	-02.4	14.6	01	-15.6	27	07	01.4	12	01.2	01	01.0	10	01.1	07	01.3	14	01.1	27	01.4	15	01.7	.
GOD.	754.1	07.6	14.7	09.6	10.4	15.8	05.6	34.3	7 VIII	-15.9	3 I	167	01.6	111	01.3	57	01.4	136	01.4	138	01.4	90	01.3	204	01.5	192	01.7	.
ILOK $\varphi = 45^\circ 14'$ N $\lambda = 19^\circ 23'$ E Gr. $\Delta G =$ + 1h 18 min.																											BR. ST. 74
I	-	-00.5	01.7	-00.6	00.0	03.1	-03.1	12.5	15	-11.6	10	04	01.5	15	01.5	04	02.0	30	02.3	09	02.0	07	01.6	14	02.6	07	02.6	03
II	-	00.1	03.7	01.6	01.8	05.3	-01.5	15.6	09	-07.4	17	04	02.5	08	01.8	06	01.5	19	02.1	06	02.2	12	02.5	15	02.6	14	01.9	.
III	-	03.1	08.7	04.7	05.3	09.7	01.9	21.2	25	-10.6	02	02	03.0	06	02.5	07	02.6	21	03.1	08	02.5	12	01.9	19	02.5	16	02.3	02
IV	-	09.1	14.5	10.0	10.9	16.3	06.9	26.2	20	00.4	04	08	02.8	14	01.8	01	02.0	11	03.3	06	02.8	12	02.3	16	02.6	17	02.4	05
V	-	12.0	17.8	12.2	13.5	19.4	09.3	27.8	10	01.5	02	06	02.5	05	01.4	03	02.3	03	02.7	04	02.5	11	02.0	24	02.4	34	02.4	03
VI	-	18.2	24.5	17.7	19.5	25.6	14.7	30.5	29	08.0	03	06	02.0	11	02.1	09	01.8	07	01.7	.	.	09	02.3	28	02.4	14	02.3	06
VII	-	18.5	24.4	17.6	19.5	25.8	14.8	31.9	24	10.0	27	02	01.5	09	01.9	01	03.0	13	02.4	03	02.3	13	02.0	12	02.4	26	02.0	14
VIII	-	18.2	25.3	18.0	19.9	26.2	15.0	32.5	07	10.0	28,19	01	02.0	10	02.0	03	01.3	25	01.7	.	.	10	01.8	16	01.9	14	01.9	14
IX	-	13.3	20.6	13.9	15.4	22.1	11.0	32.2	11	-02.6	29	04	02.2	02	01.5	02	02.0	09	01.8	04	01.2	17	01.7	11	02.4	19	01.8	22
X	-	07.9	14.7	09.5	10.4	15.8	06.0	24.5	09	-00.5	19	03	01.7	12	01.8	06	02.0	13	01.8	06	01.5	12	02.1	22	02.1	07	01.7	12
XI	-	06.7	11.7	07.8	08.5	13.0	05.1	21.2	03	-01.2	26,07	03	02.0	07	01.7	.	.	15	02.6	04	03.2	21	01.9	30	01.9	07	01.4	03
XII	-	00.5	03.0	01.0	01.4	04.1	-01.3	14.6	30	-11.2	27	06	02.2	06	02.0	03	02.0	12	02.2	03	01.0	08	02.4	23	02.1	30	01.6	02
GOD.	-	08.9	14.2	09.4	10.5	15.5	06.6	32.5	7 VIII	-11.6	10 I	49	02.2	105	01.8	45	02.0	178	02.3	53	02.2	144	02.0	230	02.3	205	02.0	86
PULA $\varphi = 44^\circ 52'$ N $\lambda = 13^\circ 51'$ E Gr. $\Delta G =$ + 55 min.																											BR. ST. 75
I	-	05.5	08.4	06.3	06.6	09.7	04.3	13.8	06	-03.0	23	12	01.2	.	.	29	02.0	15	02.2	07	02.1	02	01.5	03	02.0	07	02.0	18
II	-	04.1	08.4	04.7	05.5	09.6	01.6	14.0	09,04	-03.6	17	10	01.3	09	02.0	19	02.2	05	01.6	12	01.8	04	03.0	07	01.7	11	02.0	07
III	-	05.8	09.7	06.8	07.2	10.8	04.1	15.4	24	-02.4	02	04	01.2	13	02.1	21	02.3	16	02.4	14	02.0	03	02.0	04	02.2	05	01.6	13
IV	-	09.9	13.7	10.2	11.0	14.7	07.2	20.4	25	01.6	16	06	01.5	06	01.8	14	02.6	13	02.2	12	02.2	16	02.0	03	02.0	08	02.5	12
V	-	14.4	17.4	13.7	14.8	18.8	10.2	23.2	21	02.0	02	11	01.3	19	01.9	16	02.2	13	02.2	08	02.1	06	02.3	05	02.2	08	01.8	07
VI	-	21.1	24.6	20.1	21.5	25.7	16.7	31.0	28	08.4	05	05	01.0	06	01.5	18	01.6	12	01.7	06	02.0	07	01.9	08	01.8	12	02.1	16
VII	-	22.0	26.0	21.1	22.5	27.2	17.5	33.4	13	10.8	19,18	09	01.6	06	01.8	18	02.7	11	01.7	05	02.0	05	02.0	10	02.0	11	02.2	18
VIII	-	21.6	26.1	21.5	22.6	27.0	18.2	31.6	07	14.0	27	04	01.2	02	01.0	13	01.8	18	01.7	03	02.3	06	01.8	07	02.1	08	02.1	32
IX	-	18.0	24.1	18.2	19.6	24.8	15.8	30.0	12	07.0	30	07	01.3	08	02.0	34	01.9	18	01.8	04	02.2	04	01.5	05	01.8	04	03.0	06
X	-	11.7	17.6	11.8	13.2	18.4	09.3	24.8	13	01.3	25	04	01.0	10	02.4	28	02.1	09	02.1	03	01.7	03	01.3	11	01.8	07	01.9	18
XI	-	09.8	14.4	10.4	11.2	15.1	07.6	18.0	14	02.4	26	07	01.3	01	01.0	14	01.6	10	02.4	12	02.3	03	01.7	10	01.5	04	01.8	29
XII	-	04.9	09.4	05.9	06.6	10.3	03.4	14.8	01	-01.8	24	06	01.0	18	01.6	23	02.9	04	02.5	01	01.0	06	03.5	09	01.9	07	01.6	19
GOD.	-	12.4	16.6	12.6	13.5	17.7	09.7	33.4	13 VII	-03.6	17 II	85	01.3	98	01.9	247	02.2	144	02.0	87	02.1	65	02.1	82	01.9	92	02.0	195

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha °m mm	Um % 7	14	21	Sred. (Dies)	min	Padavine R mm Σ			Broj dana sa: Tn ≤ 10,0	Tn ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F(0-12) ≥ 6	≥ 8	Nm(0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	⁂	⁂	⁂	▲	▲	T	≡	▦
BR. ST. 71						**DJAKOVO**																															**H_o = 98 m H_b = - m h_v = 2.0 m h_r = 1.0 m**
I	8.2	7.7	7.8	7.9	-	03.0	65	74	68	69	26	070	020.9	17	08	10	29	.	.	.	.	.	.	16	16	08	04	10	08	.	.	.	.	.	.	07	31
II	8.1	7.3	7.5	7.7	-	03.7	68	73	71	71	33	059	014.9	12	03	05	25	.	.	.	.	.	01	16	19	10	02	08	14	.	.	.	.	.	.	04	20
III	7.3	7.4	7.4	7.4	-	05.2	77	71	71	73	46	080	021.5	28	.	02	09	.	.	.	.	.	.	12	16	11	03	12	06	.	.	.	.	.	01	02	02
IV	6.1	6.4	5.6	6.1	-	07.4	72	72	69	71	43	098	016.5	14	.	.	04	03	.	.	.	.	.	05	17	07	02	17	01	.	.	.	.	.	01	.	.
V	6.6	6.8	6.2	6.5	-	08.8	72	72	66	70	52	060	013.3	28	.	.	02	.	.	.	01	.	.	05	15	10	03	15	.	.	.	.	.	.	04	.	.
VI	5.6	5.2	5.3	5.4	-	14.1	80	70	78	76	50	106	049.4	19	.	.	.	19	01	.	05	.	.	03	12	10	03	12	.	.	.	.	.	.	05	02	.
VII	5.3	5.3	5.3	5.3	-	15.2	86	75	81	80	51	049	014.0	17	.	.	.	21	09	.	01	.	01	07	10	09	02	10	.	.	.	.	.	01	.	02	.
VIII	4.7	4.6	4.1	4.5	-	14.5	81	70	77	76	22	116	060.0	22	.	.	.	20	07	.	.	.	01	03	09	07	03	09	.	.	.	.	.	02	03	07	.
IX	5.6	4.5	4.9	5.0	-	11.0	72	75	73	74	38	041	015.3	17	.	.	01	09	02	.	01	.	01	03	10	08	01	10	.	.	.	.	.	.	.	05	.
X	5.7	5.9	4.9	5.5	-	07.7	83	77	75	78	55	094	020.2	02	.	.	09	.	.	.	.	.	01	05	09	06	02	09	.	.	.	.	.	.	.	08	.
XI	7.0	6.1	6.3	6.5	-	07.0	87	83	76	82	50	034	008.5	22	.	.	01	.	.	.	.	.	.	08	12	10	.	12	.	.	.	.	.	.	.	07	.
XII	8.5	7.6	6.7	7.6	-	04.0	78	80	77	78	07	040	009.8	24	03	08	24	.	.	.	.	.	.	14	14	09	.	10	04	.	.	.	.	.	.	12	10
GOD.	6.6	6.2	6.0	6.3	-	08.5	76	74	73	74	07	767	049.4	49 VI	14	25	104	72	19	.	08	.	05	97	159	105	25	134	33	.	.	.	.	03	14	56	63
BR. ST. 72						**BRESTOVAC-BELJE**																															**H_o = 91 m H_b = 92.0 m h_v = 2.0 m h_r = 1.0 m**
I	9.3	7.4	7.0	7.9	034.4	03.8	93	88	94	92	72	073	023.2	17	09	13	27	.	.	.	.	.	01	17	14	08	03	08	07	.	.	.	.	.	.	23	31
II	8.8	7.6	8.0	8.1	063.7	04.4	95	83	93	90	56	073	015.6	11	01	05	21	.	.	.	.	.	.	18	23	14	02	11	17	01	.	.	.	.	.	13	20
III	8.2	8.4	7.4	8.0	102.1	05.6	91	69	88	83	29	084	014.8	13	01	01	10	.	.	.	02	.	.	18	18	13	04	14	06	.	.	.	.	.	.	08	05
IV	6.9	8.0	5.5	6.8	147.5	07.4	88	58	79	75	36	060	013.2	09	.	.	02	03	.	.	.	.	.	09	12	09	01	12	01	.	.	.	01	.	01	01	.
V	6.5	7.7	6.9	7.0	151.0	09.1	83	59	81	75	39	043	009.4	18	.	.	.	07	.	.	.	.	.	13	13	08	.	13	.	.	.	.	.	.	03	01	.
VI	5.0	5.7	6.7	5.8	234.1	13.4	82	55	81	73	38	055	015.1	19	.	.	.	22	03	.	01	.	03	05	13	08	01	13	.	.	.	.	.	.	12	03	.
VII	4.3	5.5	5.6	5.1	241.2	13.0	80	53	81	71	32	056	019.5	26	.	.	.	21	09	.	02	.	07	07	11	09	02	11	.	.	.	.	01	.	04	01	.
VIII	4.9	5.3	4.2	4.8	252.1	14.0	89	56	87	77	38	088	024.8	22	.	.	.	19	06	.	.	.	04	04	09	08	04	09	.	.	.	.	.	.	11	03	.
IX	5.4	4.9	3.2	4.5	187.3	10.8	92	56	88	79	36	034	014.6	17	.	.	02	09	03	.	.	01	07	05	12	07	01	12	.	.	.	.	.	.	02	06	.
X	6.1	5.9	4.4	5.5	124.4	07.4	93	59	85	79	41	040	013.2	02	.	.	04	.	.	.	.	.	07	10	08	05	02	08	.	.	.	.	01	.	.	11	.
XI	8.2	7.4	6.1	7.3	088.5	06.4	91	68	85	81	42	024	007.4	16	.	.	03	.	.	.	.	.	01	13	12	05	.	12	.	.	.	.	.	.	.	10	.
XII	8.8	8.1	7.2	8.1	040.9	04.5	93	85	92	90	49	044	009.4	24	04	05	22	.	.	.	.	.	01	16	14	09	.	09	06	.	01	.	.	.	.	25	10
GOD.	6.9	6.8	6.0	6.6	1667.2	08.3	89	65	86	80	29	674	024.8	28 VIII	15	24	91	76	21	.	09	01	31	135	159	103	20	132	37	01	01	.	03	.	33	105	66
BR. ST. 73						**OSIJEK**																															**H_o = 89 m H_b = 91.8 m h_v = 2.0 m h_r = 1.5 m**
I	8.4	8.1	6.8	7.8	030.6	03.9	96	90	94	93	75	083	035.6	17	06	10	26	.	.	.	.	.	01	18	14	07	03	10	07	.	.	.	.	.	.	04	31
II	7.2	7.3	6.6	7.1	059.0	04.5	97	85	94	92	64	085	018.0	12	02	06	21	.	.	.	.	.	03	13	22	15	02	10	16	01	.	.	.	.	.	02	19
III	7.2	7.5	6.5	7.1	111.8	05.9	96	76	87	86	44	056	013.5	15	01	.	10	.	.	.	.	.	04	16	17	11	01	14	04	.	.	.	.	01	01	01	03
IV	6.0	7.2	4.3	5.8	163.2	07.9	96	63	82	80	40	060	013.5	09	.	.	02	05	.	.	.	.	02	06	13	07	02	13	.	.	.	.	.	.	01	.	.
V	6.2	7.8	6.1	6.7	152.5	09.9	94	63	84	81	37	066	033.1	21	.	.	.	03	.	.	.	.	01	11	14	10	01	14	.	.	.	.	.	01	02	.	.
VI	5.0	4.6	3.6	4.4	231.8	14.7	93	62	86	80	43	069	020.2	19	.	.	.	22	06	.	.	.	09	03	13	08	02	13	.	.	.	.	.	.	09	.	.
VII	4.2	4.9	3.9	4.3	245.3	14.7	93	60	88	80	40	056	009.9	26	.	.	.	21	12	.	01	.	12	08	12	08	.	12	.	.	.	.	.	.	03	.	.
VIII	4.2	4.8	3.9	4.3	250.5	15.6	97	67	90	84	49	084	019.7	22	.	.	.	23	07	.	01	.	08	05	12	09	04	12	.	.	.	.	.	.	07	.	.
IX	5.2	4.6	2.8	4.2	197.4	11.8	99	63	93	85	40	038	014.6	17	.	.	01	11	03	.	.	.	09	05	08	06	01	08	.	.	.	.	.	.	01	01	.
X	5.4	5.4	4.0	4.9	146.8	08.0	99	65	91	85	42	049	018.7	02	.	.	04	05	.	.	.	.	09	10	09	07	02	09	.	.	.	.	.	.	.	03	.
XI	6.8	7.0	6.1	6.6	097.2	07.2	98	76	94	90	48	030	007.9	22	.	.	04	.	.	.	.	.	02	10	11	08	.	11	.	.	.	.	.	.	.	03	.
XII	8.0	7.8	7.0	7.6	035.1	04.7	97	87	98	94	46	045	014.9	24	03	05	20	.	.	.	.	.	02	18	13	08	01	08	06	.	.	.	.	.	.	05	10
GOD.	6.2	6.4	5.1	5.9	1721.2	09.1	96	71	90	85	37	721	035.6	49 I	18	21	88	90	28	.	02	.	62	123	158	104	19	134	33	01	.	.	.	02	24	19	63
BR. ST. 74						**ILOK**																															**H_o = 133 m H_b = - m h_v = 2.0m h_r = 1.0 m**
I	9.0	8.9	8.1	8.7	-	04.2	89	79	91	87	56	051	015.0	08	03	07	21	.	.	.	.	.	.	21	15	09	01	08	09	02	.	.	.	.	.	01	18
II	7.9	8.9	8.2	8.3	-	04.5	88	74	92	84	37	079	008.8	16	.	04	19	.	.	.	.	.	.	17	22	11	.	09	17	.	01	.	.	.	.	01	13
III	8.5	8.0	7.6	8.1	-	05.3	83	65	87	78	33	075	019.1	15	01	.	08	.	.	.	01	02	02	19	16	12	02	13	05	.	.	.	.	.	.	01	02
IV	6.9	8.0	4.2	6.4	-	07.2	80	56	81	72	29	078	024.2	09	.	.	.	04	.	.	.	.	.	03	07	13	08	03	13	01	.	.	.	.	01	02	.	.
V	8.1	8.8	7.7	8.2	-	09.0	84	57	88	76	35	093	032.0	23	.	.	.	02	.	.	.	.	.	17	15	13	03	15	.	.	.	.	.	.	03	.	.
VI	5.7	6.4	5.5	5.8	-	13.4	83	58	88	77	44	086	021.0	19	.	.	.	20	04	.	01	.	04	09	17	12	04	17	.	.	.	.	.	.	11	01	.
VII	4.1	5.4	3.9	4.5	-	13.5	82	64	85	77	44	102	023.7	06	.	.	.	21	09	.	.	.	10	08	12	10	09	12	.	.	.	.	.	.	01	.	.
VIII	5.5	4.9	3.6	4.7	-	13.8	86	58	88	78	41	055	011.8	25	.	.	.	19	05	.	.	.	07	04	11	09	01	11	.	.	.	.	.	.	07	.	.
IX	5.7	6.3	3.2	5.1	-	10.8	91	60	86	79	34	019	013.2	17	.	.	01	11	03	.	01	.	07	06	09	04	01	09	.	.	.	.	.	.	01	07	.
X	5.4	5.3	4.1	4.9	-	07.9	90	64	91	82	39	061	032.1	02	.	.	01	.	.	.	.	.	09	10	06	06	02	06	.	.	.	.	.	.	.	03	.
XI	7.2	7.6	6.1	7.0	-	06.9	87	70	89	82	32	040	010.6	17	.	.	02	.	.	.	.	.	01	11	13	10	01	13	.	.	.	.	.	.	.	03	.
XII	8.4	8.2	6.6	7.7	-	04.8	93	87	95	92	57	039	010.0	24	04	06	19	.	.	.	01	.	01	17	16	08	01	11	07	01	.	.	.	.	01	11	06
GOD.	6.9	7.2	5.7	6.6	-	08.4	86	66	88	80	29	778	032.1	2. X	08	17	71	77	21	.	04	02	44	146	165	112	24	137	39	03	01	.	.	01	26	23	39
BR. ST. 75						**PULA**																															**H_o = 30 m H_b = 32.0 m h_v = 2.0 m h_r = 1.0 m**
I	7.9	7.1	7.4	7.5	065.7	06.6	91	82	90	87	47	126	021.6	01	.	.	04	.	.	.	.	.	03	19	13	13	06	13	.	.	.	.	.	.	.	06	.
II	6.0	5.9	4.8	5.6	101.7	05.7	84	72	83	80	44	068	031.0	19	.	.	07	.	.	.	02	02	04	07	11	08	03	11	01	01	.	.	.	.	01	.	.
III	6.0	7.2	6.2	6.5	114.9	06.6	89	76	87	84	48	087	010.2	04	.	.	04	.	.	.	02	.	05	12	14	14	01	14	01	01	.	.	.	.	01	01	.
IV	5.9	4.8	5.0	5.3	183.6	07.5	81	62	82	75	41	088	024.2	03	.	.	.	.	.	.	01	.	04	08	13	09	04	13	01	01	.	.	.	.	02	.	.
V	4.0	5.1	4.1	4.4	238.6	09.1	72	62	80	71	31	046	016.0	08	.	.	.	.	.	.	.	.	08	06	15	09	02	15	.	.	.	.	.	.	01	01	.
VI	3.4	4.0	3.6	3.7	273.2	13.7	72	57	81	70	34	035	018.7	15	.	.	.	19	04	03	01	.	12	02	10	04	01	10	.	.	.	.	.	.	07	.	.
VII	1.7	2.7	2.0	2.2	340.5	13.0	62	51	73	62	31	047	021.0	04	.	.	.	24	07	09	03	01	20	01	04	04	02	04	.	.	.	.	.	.	02	.	.
VIII	3.0	3.3	1.5	2.6	285.4	14.6	73	58	78	70	43	135	037.5	30	.	.	.	24	02	05	.	.	17	01	09	08	04	09	.	.	.	.	.	.	09	.	.
IX	3.0	1.6	1.0	1.9	260.8	12.2	73	53	79	68	32	012	004.0	23	.	.	.	19	01	03	02	01	17	05	05	05	.	05	.	.	.	.	.	.	03	.	.
X	3.5	3.0	2.8	3.1	202.6	08.8	76	61	80	73	34	046	017.4	22	.	.	.	.	.	.	.	.	13	01	06	05	02	06	.	.	.	.	.	01	04	01	.
XI	5.4	6.1	5.2	5.6	089.9	08.3	85	73	83	80	36	060	028.1	16	.	.	.	.	.	.	.	.	08	09	08	06	01	08	.	.	.	.	.	.	03	03	.
XII	4.5	5.1	4.1	4.6	099.1	05.8	82	69	79	77	46	099	025.4	20	.	.	03	.	.	.	04	02	12	07	08	08	04	08	.	.	.	.	.	.	.	03	.
GOD.	4.5	4.7	4.0	4.4	2250.0	09.3	78	64	81	74	31	849	037.5	30 VIII	.	.	18	86	14	20	15	06	123	78	116	93	30	116	03	03	.	.	.	01	33	15	.

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm: 7	14	21	Sred. (Dim)	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	Učestina pravaca i srednja jačina vetra nE, Fm (0-12): N		NE		E		SE		S		SW		W		NW		C
												δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.		j.	δ.	j.	δ.
φ = 44° 58' N λ = 14° 24' E Gr. Δ G = + 58 min.																												CRES BR. ST. 76
I	-	06.3	09.1	06.4	07.0	10.0	03.4	15.4	06	-03.1	23	18	02.2	31	03.2	02	02.0	19	02.8	01	02.0	09	01.4	07	01.4	06	01.0	.
II	-	04.5	08.9	05.7	06.2	10.0	01.5	15.4	07	-03.2	17	05	01.4	23	03.1	07	02.7	19	03.3	09	02.0	10	02.2	08	01.6	03	01.0	.
III	-	06.0	10.0	07.2	07.6	11.4	03.1	16.5	24	-03.5	02	15	01.6	26	03.3	05	02.4	17	03.7	10	02.4	07	02.3	06	01.7	07	02.0	.
IV	-	10.1	14.5	10.4	11.4	16.0	06.3	22.1	25	-00.8	04	18	02.2	14	02.7	05	01.6	16	02.9	06	02.2	13	02.5	13	01.8	05	01.4	.
V	-	14.8	18.8	14.2	15.5	20.6	09.3	24.8	20	01.3	01	20	02.6	24	02.6	04	02.5	10	02.7	09	01.8	10	02.1	05	02.4	11	01.7	.
VI	-	21.0	25.5	20.5	21.9	27.2	15.9	32.2	26	08.8	05	11	01.6	21	02.4	07	02.0	08	02.4	11	01.3	07	01.9	10	02.0	15	02.0	.
VII	-	21.8	27.4	21.4	23.0	28.5	16.4	34.6	13	08.9	18	12	02.2	32	03.3	05	02.8	11	03.3	04	01.2	05	01.4	09	02.2	15	01.7	.
VIII	-	21.5	27.9	22.0	23.3	29.0	17.3	33.6	06	12.2	25	08	01.6	22	02.5	04	01.8	11	02.6	07	01.3	07	01.9	12	02.4	22	02.0	.
IX	-	17.9	25.4	19.4	20.5	26.3	14.8	30.4	12	05.4	30	04	01.8	43	03.4	02	03.5	06	02.2	02	01.0	05	01.6	13	02.3	15	01.6	.
X	-	11.6	18.3	12.6	13.8	19.3	08.4	27.4	12	01.4	25	12	01.8	30	03.7	.	.	14	02.4	04	02.0	04	01.8	08	02.0	21	01.3	.
XI	-	10.0	15.0	11.1	11.8	15.7	07.0	19.8	27	00.4	17	23	01.7	16	02.6	02	01.5	19	03.5	12	01.6	06	01.7	01	01.0	11	01.3	.
XII	-	05.3	10.0	06.9	07.3	11.2	03.1	16.4	10	-01.8	21,18	13	02.3	43	03.2	05	01.6	05	04.6	01	04.0	08	02.0	05	01.6	13	01.3	.
GOD.	-	12.6	17.6	13.2	14.1	18.8	08.9	34.6	15 VII	-03.5	1 III	159	02.0	325	03.1	48	02.2	155	03.0	76	01.8	91	02.0	97	02.0	144	01.6	.
φ = 44° 32' N λ = 14° 28' E Gr. Δ G = + 58 min.																												MALI LOŠINJ BR. ST. 77
I	754.2	07.8	09.1	08.3	08.4	10.1	06.4	15.5	05	01.4	22	23	03.7	16	03.7	04	02.0	19	03.5	05	02.4	04	02.2	08	02.0	04	02.5	10
II	752.6	06.7	08.9	07.4	07.6	10.1	04.9	14.7	09,06	-00.8	17	10	04.8	18	04.7	05	02.8	14	03.5	14	03.1	10	03.7	02	03.5	08	02.5	03
III	753.5	07.7	10.0	08.1	08.5	11.1	06.0	15.6	24	01.9	07	18	03.2	13	04.3	07	02.4	22	02.8	22	03.6	03	05.0	03	02.3	03	02.3	02
IV	755.3	11.0	13.9	11.3	11.8	15.1	09.0	21.7	25	04.1	03	08	03.9	18	03.8	.	.	07	04.0	26	03.5	11	03.3	13	02.5	04	03.2	03
V	756.5	14.5	18.2	15.0	15.7	19.6	12.4	23.3	21	07.0	01	16	02.9	24	03.9	02	02.0	06	03.5	12	03.8	08	02.9	13	03.2	05	02.6	07
VI	757.2	20.7	25.0	21.0	21.9	26.0	18.3	31.0	27	13.3	03	08	02.0	19	02.5	07	02.0	.	.	16	02.8	12	02.8	20	02.6	01	01.0	07
VII	755.6	21.7	26.1	22.5	23.2	27.4	19.4	32.7	12	13.2	16	18	02.7	26	03.5	02	02.0	03	03.0	10	03.7	10	02.8	13	02.5	02	01.5	09
VIII	755.7	22.3	26.5	23.0	23.7	27.7	20.4	32.5	07	14.9	24	08	02.1	18	01.8	05	01.4	09	02.4	07	03.3	12	02.3	17	02.6	10	02.5	07
IX	758.8	19.4	24.0	20.4	21.0	24.8	18.2	29.5	12	12.4	30	17	02.9	16	02.8	08	02.5	05	02.2	17	02.7	03	03.0	07	03.1	08	02.0	09
X	759.4	14.2	18.0	14.8	15.5	18.8	12.8	25.0	13	05.3	24	12	03.2	15	03.1	04	02.0	15	02.5	11	03.5	07	02.6	13	02.2	02	02.0	14
XI	758.1	12.4	14.9	13.3	13.5	15.8	11.3	18.5	03,02	06.0	16	15	02.9	18	02.4	03	01.7	20	03.2	13	03.2	06	02.7	05	03.6	06	02.5	04
XII	759.3	08.4	10.2	08.8	09.1	11.4	06.9	15.1	09	00.8	23	18	02.8	19	04.1	07	04.0	12	04.4	01	03.0	09	04.4	03	01.7	11	02.5	13
GOD.	756.4	13.9	17.1	14.5	15.0	18.2	12.2	32.7	12 VII	-00.8	17 II	171	03.1	220	03.4	54	02.4	132	03.2	154	03.3	95	03.1	117	02.6	64	02.4	88
φ = 44° 45' N λ = 14° 46' E Gr. Δ G = + 59 min.																												RAB BR. ST. 78
I	756.8	07.8	10.3	07.8	08.4	11.1	05.6	15.0	05	-00.6	23	20	02.4	07	01.3	04	01.8	32	04.3	06	01.5	06	02.0	02	01.0	12	01.8	04
II	755.4	06.2	09.2	07.1	07.4	10.4	04.3	14.4	06	-02.5	17	09	04.1	15	03.1	09	03.1	31	05.5	06	03.5	03	01.7	.	.	06	03.0	05
III	756.3	07.0	10.4	07.8	08.3	11.4	04.9	15.1	24	-00.1	02	15	02.7	17	01.8	07	02.4	32	05.1	04	05.5	03	01.3	04	02.2	07	02.9	04
IV	758.0	10.6	14.2	11.5	12.0	15.3	08.5	20.3	18	02.8	04	14	03.3	06	03.3	02	02.5	34	04.0	06	04.7	08	02.6	01	02.0	07	03.1	12
V	759.2	14.7	18.8	15.2	16.0	19.8	11.8	25.2	21	05.3	01	26	03.4	09	03.2	.	.	22	02.8	12	02.8	05	01.8	02	03.5	05	02.6	12
VI	760.0	20.5	24.8	21.2	21.9	26.0	17.5	31.5	26	12.3	05	13	03.2	05	02.4	01	02.0	14	02.3	09	02.1	16	01.7	02	02.5	08	02.1	22
VII	758.2	21.4	26.6	22.8	23.4	27.8	18.6	34.3	12	12.0	16	09	03.3	16	03.2	03	02.3	13	03.8	05	03.2	13	02.4	03	02.0	07	02.6	24
VIII	758.3	21.8	26.8	22.9	23.6	28.0	19.4	31.6	06	14.7	24	10	01.9	02	01.0	03	01.7	10	03.4	13	02.7	10	01.5	04	01.5	01	01.0	40
IX	761.4	19.0	25.1	20.5	21.3	25.7	17.0	29.7	12	10.2	30	09	02.0	12	02.8	07	03.7	11	02.5	11	02.5	11	02.0	02	02.5	03	02.0	24
X	762.0	13.4	18.6	14.6	15.3	19.3	11.6	25.6	12	06.0	17	16	02.4	09	02.6	13	02.3	19	04.7	07	02.9	09	01.1	03	01.7	09	02.0	08
XI	760.7	11.6	15.3	12.8	13.1	16.0	10.2	18.3	04	06.3	17	12	02.4	09	01.9	07	01.6	34	05.4	04	02.5	07	01.7	02	01.0	04	01.2	11
XII	762.0	07.4	10.9	07.9	08.5	12.1	05.5	16.0	30	-01.2	24	15	01.7	25	02.5	10	03.5	18	04.7	02	02.5	07	03.1	02	02.0	06	02.0	08
GOD.	759.0	13.4	17.6	14.3	14.9	18.6	11.2	34.3	12 VII	-02.5	17 II	168	02.7	132	02.6	66	02.6	270	04.3	85	02.9	98	01.9	27	02.0	75	02.3	174
φ = 44° 59' N λ = 14° 54' E Gr. Δ G = + 1h 00 min.																												SENJ BR. ST. 79
I	756.3	06.3	07.5	06.4	06.7	09.4	04.3	17.0	05	-02.5	22	08	01.4	21	06.5	31	04.9	15	02.0	07	02.3	02	02.5	04	01.8	05	01.6	.
II	754.7	05.9	08.3	06.4	06.7	09.8	03.8	15.3	05	-04.4	17	02	02.5	19	04.7	22	04.3	12	02.9	11	03.2	07	03.0	05	01.4	06	01.5	.
III	755.6	06.5	09.5	07.6	07.8	10.8	05.0	17.3	24	00.5	02,01	06	02.2	17	05.0	29	03.9	17	02.1	10	03.1	07	03.0	02	01.5	04	01.8	01
IV	757.3	10.4	14.2	11.8	12.1	15.8	08.7	22.3	19	02.2	04	06	02.2	13	04.2	22	03.1	14	01.7	10	02.7	11	02.4	03	03.0	04	02.8	07
V	758.5	14.5	18.4	14.8	15.6	20.0	11.9	24.8	21	05.4	03	09	01.6	21	03.9	26	03.3	11	02.0	07	02.4	06	01.5	04	01.8	09	01.6	.
VI	759.1	20.6	25.1	21.3	22.1	26.3	18.3	31.6	27	10.8	03	08	01.8	09	03.3	22	02.8	18	01.8	06	01.5	05	01.4	05	01.2	13	01.4	04
VII	757.5	21.2	26.5	22.2	23.0	27.6	19.0	33.3	13	10.5	16	03	02.0	23	05.1	31	04.5	12	02.2	08	02.4	02	01.0	04	01.2	03	01.3	07
VIII	757.5	22.1	27.2	23.5	24.1	28.3	20.6	33.0	06	15.4	24	06	01.7	11	04.6	27	02.9	17	01.6	08	01.4	06	01.5	01	01.0	07	01.3	10
IX	760.8	18.3	24.0	19.9	20.5	24.8	17.3	31.4	12	10.5	29	02	01.5	21	06.1	36	04.3	11	02.0	04	01.5	04	01.2	02	01.5	05	01.0	05
X	761.4	12.3	17.2	14.0	14.4	18.6	11.1	26.6	12	05.4	24	04	01.5	18	06.3	28	04.8	17	02.2	09	02.6	02	01.5	.	.	05	01.4	10
XI	759.8	11.8	14.8	12.7	13.0	15.7	10.6	20.9	14	07.5	17	03	01.3	13	05.5	26	03.7	14	03.1	12	04.0	07	03.0	02	03.0	04	01.5	09
XII	761.5	06.4	08.9	07.0	07.4	10.6	04.5	17.3	30	-03.0	23	06	02.3	21	06.5	37	04.8	11	02.5	02	03.5	08	02.8	03	02.7	01	03.0	04
GOD.	758.3	13.0	16.8	14.0	14.4	18.1	11.3	33.3	15 VII	-04.4	17 II	63	01.8	207	05.3	337	04.0	169	02.1	94	02.7	67	02.3	35	01.8	66	01.5	57
φ = 44° 49' N λ = 14° 59' E Gr. Δ G = + 1h 00 min.																												ZAVIŽAN BR. ST. 80
I	623.6	-02.3	-01.6	-02.6	-02.3	00.2	-04.8	04.8	05	-11.6	08	.	.	.	.	31	02.1	14	02.6	07	02.7	11	03.2	15	02.2	13	01.7	02
II	621.1	-06.4	-04.1	-06.0	-05.7	-02.9	-08.1	02.2	05	-17.3	17	01	01.0	02	01.0	33	03.4	01	01.0	01	02.0	17	03.5	23	02.5	04	02.0	02
III	622.4	-04.8	-02.5	-03.8	-03.8	-01.0	-06.1	06.0	26,24	-12.8	01	03	01.0	.	.	29	03.2	03	03.7	09	03.0	23	02.7	16	03.2	08	01.9	02
IV	625.9	00.4	02.0	00.6	00.9	03.7	-01.4	13.4	19	-10.0	04	.	.	.	.	24	02.5	04	01.8	15	02.5	19	02.8	23	02.3	03	01.3	02
V	628.2	02.3	05.9	03.2	03.7	07.4	01.2	13.2	10	-06.6	01	.	.	.	.	47	02.6	10	03.2	04	02.2	08	02.9	20	02.6	01	02.0	03
VI	631.8	09.9	13.5	10.4	11.0	14.6	08.4	20.3	27	-01.9	03	01	01.0	.	.	26	03.2	07	02.9	06	02.7	03	02.7	36	02.7	07	02.4	04
VII	631.0	10.2	14.4	11.0	11.6	15.7	08.4	23.3	23	00.2	16	01	02.0	.	.	51	04.0	01	02.0	03	03.3	08	03.5	20	02.4	04	02.2	05
VIII	631.4	11.4	14.9	12.2	12.7	16.1	10.4	22.6	08	05.0	25,24	.	.	.	.	27	02.8	06	03.3	08	03.2	10	03.0	26	02.8	11	02.4	05
IX	633.0	08.2	12.2	09.0	09.6	13.4	06.9	20.0	11	-01.1	29	.	.	.	.	46	04.4	01	02.0	03	04.7	13	03.2	20	03.1	06	02.5	01
X	630.9	03.0	06.3	03.9	04.3	07.8	01.5	20.3	11	-06.8	24	.	.	.	.	37	04.5	02	02.5	09	04.2	04	03.5	31	03.3	08	03.4	02
XI	628.8	02.2	04.0	02.5	02.8	05.5	00.4	16.4	02	-06.1	17	.	.	.	.	21	03.7	04	03.8	10	05.4	12	05.0	31	04.1	08	03.1	04
XII	627.9	-03.2	-01.2	-03.0	-02.6	00.6	-05.1	09.6	11	-13.7	24	.	.	.	.	38	04.5	08	03.4	07	02.7	06	04.0	17	03.8	10	02.5	07
GOD.	628.0	02.6	05.3	03.1	03.5	06.8	01.0	23.3	15 VII	-17.3	17 II	06	01.2	02	01.0	410	03.5	61	02.9	82	03.3	134	03.3	278	03.0	83	02.4	39

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ			Broj dana n sa: Tn ≤ -10,0	Tn ≤ -5,0	Tn ≤ 0,0	Tx ≤ 0,0	Tx ≤ 25,0	Tn ≤ 20,0	F(0-12) ≥ 6	≥ 8	Nm(0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	⁂	⚠	≈	▲	▲	⊤	■	■
BR. ST. 76						CRES																						H_v = 10 m H_b = - m h_v = 2,0 m h_z = 1,0 m										
I	7.6	6.5	7.0	7.1	-	06.1	80	69	82	77	27	147	034.1	06	.	.	03	.	.	.	.	.	06	20	15	13	05	15	.	.	.	.	.	.	02	.
II	6.9	6.2	6.1	6.4	-	05.2	78	60	74	70	31	106	038.6	19	.	.	07	.	.	.	01	.	03	08	14	11	03	14	01	.	.	.	.	01	04	01	01
III	6.8	6.9	6.5	6.7	-	05.9	80	64	76	73	25	168	034.5	03	.	.	09	.	.	.	.	.	03	14	15	15	06	15	.	.	.	.	.	.	02	.	.
IV	7.0	5.8	5.7	6.1	-	07.2	77	58	76	70	27	102	022.6	06	.	.	01	.	.	.	.	.	02	10	15	13	05	15	.	.	.	.	.	.	03	.	.
V	4.5	4.7	5.4	4.9	-	08.5	68	52	72	64	28	052	022.5	23	.	.	.	.	.	.	.	.	07	07	10	08	02	10	.	.	.	.	.	.	03	.	.
VI	4.1	4.7	5.2	4.6	-	13.2	72	55	71	66	34	041	014.2	10	.	.	.	23	08	03	.	.	06	04	09	07	01	09	.	.	.	.	.	.	10	.	.
VII	2.6	2.8	3.3	2.9	-	12.5	65	45	65	58	09	091	041.3	16	.	.	.	25	11	05	.	.	15	05	07	05	03	07	.	.	.	.	.	.	04	.	.
VIII	3.3	3.8	3.4	3.5	-	14.3	76	50	73	66	36	048	021.7	10	.	.	.	29	14	04	.	.	14	04	09	07	01	09	.	.	.	.	.	.	08	.	.
IX	3.1	1.8	1.6	2.1	-	11.4	71	46	66	61	26	009	005.2	23	.	.	.	21	01	01	.	.	17	.	06	03	.	06	.	.	.	.	.	.	03	.	.
X	4.3	4.5	2.6	3.8	-	08.7	80	56	77	71	29	078	031.5	02	.	.	.	03	.	.	.	.	11	04	06	04	03	06	.	.	.	.	.	.	04	03	.
XI	6.4	6.1	5.7	6.1	-	07.9	84	64	78	75	21	067	030.8	22	.	.	.	.	.	.	01	.	06	12	10	08	01	10	.	.	.	.	.	.	04	.	.
XII	5.8	4.6	4.9	5.1	-	05.5	79	60	71	70	30	106	038.4	28	.	.	05	.	.	.	02	.	09	10	08	08	04	08	.	.	.	.	.	.	.	.	.
GOD.	5.2	4.9	4.8	4.9	-	08.9	75	56	73	68	09	1015	041.3	46 VII	.	.	25	101	34	13	04	.	99	98	124	102	34	124	01	.	.	.	.	01	44	06	01
BR. ST. 77						MALI LOŠINJ																						H_v = 53 m H_b = 51,7 m h_v = 2,0 m h_z = 1,0 m										
I	8.0	6.8	6.9	7.3	086.6	06.7	81	76	80	79	51	111	025.1	25	.	.	.	.	.	.	03	.	03	17	17	14	03	17	.	.	.	.	.	.	01	05	.
II	6.6	6.1	5.4	6.0	113.5	05.6	72	64	70	69	37	095	022.1	19	.	.	02	.	.	.	12	02	04	08	12	09	04	12	01	.	.	.	01	01	03	.	.
III	6.5	6.7	5.5	6.3	147.8	06.2	74	66	76	72	34	114	023.7	05	.	.	.	.	.	.	05	.	05	11	16	12	04	16	01	01	.	.	02	.	01	.	.
IV	6.5	6.6	4.7	5.9	201.2	07.3	74	60	72	69	38	046	009.6	29	.	.	.	.	.	.	05	01	01	09	12	07	.	12	.	.	.	.	02	.	05	02	.
V	5.0	5.0	4.7	4.9	278.2	08.7	68	55	69	64	37	015	006.8	23	.	.	.	.	.	.	03	.	05	07	07	05	.	.	.	.	.	.	.	.	04	.	.
VI	4.0	4.1	4.2	4.1	322.3	13.5	74	55	75	68	37	025	011.2	10	.	.	.	19	03	11	03	.	11	04	07	05	01	07	.	.	.	.	.	.	05	.	.
VII	2.4	2.9	2.2	2.5	383.4	13.2	69	50	66	61	28	065	020.1	02	.	.	.	22	10	15	05	.	16	01	05	05	04	05	.	.	.	.	.	.	03	.	.
VIII	4.3	3.5	2.9	3.5	308.4	15.2	78	58	70	69	35	138	060.2	24	.	.	.	26	07	21	.	.	15	02	07	05	03	07	.	.	.	.	.	01	07	.	.
IX	3.3	2.2	1.1	2.2	282.7	12.9	75	55	71	67	35	025	016.5	17	.	.	.	18	.	09	02	.	18	.	05	02	01	05	.	.	.	.	.	.	02	.	.
X	4.0	4.6	2.8	3.8	232.5	09.5	74	61	72	69	32	065	036.2	02	.	.	.	01	.	.	05	.	11	04	08	04	02	07	.	.	.	.	01	.	04	01	.
XI	6.5	6.3	4.5	5.7	120.4	08.7	79	69	75	74	38	076	026.9	16	.	.	.	.	.	.	04	.	04	06	12	12	02	12	.	.	.	.	01	01	03	.	.
XII	5.9	6.0	4.5	5.5	113.6	06.4	76	68	73	72	40	089	023.6	28	.	.	.	.	.	.	09	.	10	10	13	12	02	13	02	02	.	.	.	.	.	.	.
GOD.	5.2	5.1	4.1	4.8	2590.6	09.5	74	61	72	69	28	864	060.2	24 VIII	.	.	02	86	20	56	56	03	103	79	121	92	26	113	04	03	.	.	07	03	38	08	.
BR. ST. 78						RAB																						H_v = 24 m H_b = 19,9 m h_v = 2,0 m h_z = 1,2 m										
I	7.5	6.7	6.1	6.8	088.1	06.4	77	68	78	74	28	098	013.6	06	.	.	01	.	.	.	09	05	05	15	18	14	04	18	.	.	.	.	.	.	.	.	.
II	6.6	6.6	6.1	6.5	109.4	05.3	69	59	65	64	24	103	035.5	12	.	.	02	.	.	.	16	10	02	08	12	10	03	12	.	.	.	01	02	.	04	.	.
III	6.4	7.0	6.1	6.5	138.9	05.6	70	60	70	67	29	162	051.5	05	.	.	01	.	.	.	13	10	04	12	15	12	05	15	02	01	01	.	01	.	05	.	.
IV	6.9	6.4	4.6	6.0	193.7	07.3	76	58	69	68	30	098	044.3	09	.	.	.	.	.	.	13	07	03	09	14	10	02	14	.	.	.	.	01	.	06	.	.
V	4.9	5.2	4.5	4.9	257.7	-	-	-	-	-	-	040	009.9	09	.	.	.	01	.	.	07	02	07	06	11	07	.	11	.	.	.	.	.	.	05	.	.
VI	4.2	4.1	3.6	4.0	282.4	13.4	73	59	68	67	35	030	008.3	10	.	.	.	21	04	06	06	02	10	04	09	07	.	09	.	.	.	.	.	.	09	.	.
VII	2.7	3.3	2.7	2.9	356.8	12.6	66	48	59	58	33	084	062.8	16	.	.	.	22	10	10	05	03	15	03	08	05	02	08	.	.	.	.	.	.	04	.	.
VIII	4.0	3.9	2.4	3.4	292.5	14.5	74	57	66	66	38	043	012.7	09	.	.	.	27	10	13	02	.	12	02	08	07	02	08	.	.	.	.	.	.	07	.	.
IX	3.8	2.3	1.6	2.6	272.1	11.4	66	49	62	59	27	016	013.2	17	.	.	.	19	.	05	04	02	14	.	04	02	01	04	.	.	.	.	.	.	02	.	.
X	4.3	4.6	2.2	3.7	228.7	08.8	70	56	68	65	27	057	027.9	02	.	.	.	02	.	.	07	04	13	02	03	03	03	03	.	.	.	.	.	01	04	.	.
XI	6.2	6.2	4.4	5.6	117.6	08.2	78	65	72	72	34	086	031.1	22	.	.	.	.	.	.	10	09	06	08	13	12	02	13	.	.	.	.	.	01	05	01	.
XII	5.5	6.3	4.1	5.3	110.6	05.8	72	62	68	67	36	084	031.1	28	.	.	01	.	.	.	10	09	11	10	09	08	03	09	.	.	.	.	01	.	01	.	.
GOD.	5.2	5.2	4.0	4.8	2448.5	-	-	-	-	-	-	901	062.8	46 VII	.	.	05	92	24	34	102	63	102	79	124	97	27	124	02	01	01	01	05	02	52	01	.
BR. ST. 79						SENJ																						H_v = 26 m H_b = 29,9 m h_v = 2,0 m h_z = 1,0 m										
I	7.8	7.0	6.6	7.1	075.3	05.5	71	69	68	69	46	146	031.0	07	.	.	05	.	.	.	14	08	05	17	19	15	06	19	01	01	.	.	.	.	01	.	.
II	7.4	7.2	7.1	7.2	090.9	04.9	66	59	64	63	29	145	033.7	19	.	.	06	.	.	.	14	03	02	12	12	11	04	02	.	.	.	.	01	.	04	.	.
III	6.8	7.4	6.3	6.8	121.8	05.3	66	60	65	63	28	168	040.4	28	.	.	.	.	.	.	10	04	02	12	15	14	07	15	01	01	.	.	01	.	04	.	.
IV	6.9	7.0	5.2	6.4	166.2	06.6	68	55	61	61	27	139	029.1	09	.	.	.	.	.	.	06	.	03	09	17	15	06	17	01	01	.	.	.	.	06	.	.
V	5.3	6.3	5.3	5.6	217.0	07.6	59	48	61	56	30	083	032.7	23	.	.	.	.	.	.	06	.	04	09	13	08	02	13	.	.	.	.	.	.	04	.	.
VI	4.9	5.6	4.5	5.0	268.2	12.5	68	53	65	62	37	056	021.6	15	.	.	.	21	04	09	07	.	05	06	09	07	02	09	.	.	.	.	.	.	08	.	.
VII	3.2	3.6	3.3	3.4	322.0	12.0	62	47	59	56	34	154	082.0	16	.	.	.	22	12	16	13	02	15	04	07	06	03	07	.	.	.	.	.	.	03	.	.
VIII	3.8	4.6	3.4	3.9	261.0	13.6	66	51	63	60	34	078	021.1	25	.	.	.	28	13	16	03	.	11	04	09	07	03	08	.	.	.	.	.	.	08	.	.
IX	3.8	2.5	2.0	2.8	267.0	10.5	64	48	58	57	32	040	026.8	13	.	.	.	16	01	04	15	04	14	.	05	02	02	05	.	.	.	.	.	.	02	.	.
X	4.4	5.2	3.5	4.4	196.0	07.8	65	54	64	61	31	074	028.3	02	.	.	.	02	.	.	15	05	10	03	07	07	02	07	.	.	.	.	.	01	04	.	.
XI	7.1	6.6	6.0	6.6	106.2	07.4	68	59	67	65	31	045	025.5	22	.	.	.	.	.	.	09	.	04	13	10	06	01	10	.	.	.	.	.	.	05	.	.
XII	5.5	6.1	4.8	5.4	101.8	04.7	62	57	58	59	17	110	044.3	28	.	.	04	.	.	.	19	08	10	09	12	09	04	09	03	.	.	.	01	.	01	.	-
GOD.	5.6	5.8	4.8	5.4	2193.4	08.2	65	55	62	61	17	1238	082.0	46 VII	.	.	15	89	30	45	131	34	85	98	135	107	42	121	06	03	.	.	03	01	48	.	-
BR. ST. 80						ZAVIŽAN																						H_v = 1594 m H_b = 1596,9 m h_v = 2,0 m h_z = 2,0 m										
I	7.8	7.0	6.6	7.1	070.9	03.4	86	83	83	84	27	186	037.4	07	01	16	27	.	.	.	.	.	04	16	18	18	06	12	10	.	01	01	.	.	.	21	31
II	7.9	8.4	8.7	8.3	054.3	03.1	97	96	97	96	76	200	035.8	16	12	19	27	.	.	.	02	.	.	18	20	18	07	02	18	.	04	.	01	.	03	23	28
III	6.8	7.8	6.6	7.1	097.7	03.2	90	85	87	87	24	261	039.1	15	05	20	26	.	.	.	03	.	04	15	18	16	09	04	15	.	02	.	.	.	04	21	31
IV	8.4	7.2	5.7	7.1	132.0	04.2	86	81	82	83	36	150	026.4	09	01	09	21	.	.	.	.	.	02	11	16	15	06	08	11	01	04	.	.	.	05	19	30
V	6.9	6.3	6.0	6.4	201.6	04.5	82	67	78	76	34	109	043.7	23	.	01	09	.	.	.	01	.	03	09	12	09	04	09	04	.	.	.	.	.	01	19	24
VI	5.7	6.1	4.1	5.3	223.6	07.6	82	71	76	76	38	105	032.0	19	.	.	01	.	.	.	.	.	06	07	12	09	04	12	.	.	.	.	.	.	04	13	.
VII	4.0	4.8	4.3	4.3	289.7	07.8	80	68	78	75	36	155	054.1	17	.	.	.	.	.	.	06	01	09	05	07	05	05	07	01	.	.	.	.	.	03	12	.
VIII	5.2	5.7	3.6	4.8	231.4	08.8	85	76	80	80	39	116	031.6	09	.	.	.	.	.	.	01	.	07	07	11	09	05	11	.	.	.	.	.	.	05	08	.
IX	5.8	4.1	3.7	4.6	228.5	06.9	82	70	73	75	14	032	017.1	17	.	.	01	.	.	.	05	02	08	04	11	06	01	11	.	.	.	.	01	02	12	.
X	5.5	5.2	4.4	5.1	176.5	04.4	79	68	72	73	16	140	054.9	21	.	05	12	.	.	.	07	.	08	00	06	05	03	04	04	.	.	.	02	01	03	18	08
XI	7.3	6.3	5.1	6.2	114.8	04.2	76	74	78	76	14	120	047.4	22	.	03	12	.	.	.	07	02	03	08	13	11	02	11	04	01	02	.	01	.	03	21	12
XII	6.3	6.4	6.0	6.2	092.6	02.9	80	76	77	78	09	175	045.8	28	05	09	25	.	.	.	08	03	08	15	15	14	06	04	14	.	01	.	.	.	.	19	27
GOD.	6.5	6.3	5.4	6.0	1913.6	05.1	83	76	80	79	09	1749	054.9	24 X	24	82	161	.	.	.	40	08	62	123	159	135	58	95	81	02	14	01	04	02	33	206	191

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dsim)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra sD, Fm (0-12) N s.	j.	NE s.	j.	E s.	j.	SE s.	j.	S s.	j.	SW s.	j.	W	j.	NW s.	j.	C s.
φ = 44° 27' N λ = 15° 04' E Gr. ΔG = + 1h 00 min.												PAG																BR. ST. 81
I	-	07.2	09.7	07.8	08.1	11.1	04.9	15.5	06	-02.5	23	20	02.4	08	03.1	02	01.5	28	02.4	16	03.1	.	.	.	.	19	01.6	.
II	-	05.8	08.8	06.6	06.9	10.2	03.4	15.2	06	-02.5	17	18	02.9	14	03.4	02	01.5	25	02.5	14	02.6	02	01.5	01	02.0	08	02.4	.
III	-	06.9	10.5	08.3	08.5	12.0	04.7	17.5	24	-01.6	02	17	03.4	10	03.9	08	01.8	22	02.7	18	02.7	03	02.3	03	01.7	12	02.2	.
IV	-	11.0	15.0	12.2	12.6	16.5	08.7	23.5	24	03.7	04	14	03.0	05	03.4	07	01.9	25	02.4	14	02.5	06	01.5	01	01.0	18	02.2	.
V	-	15.7	19.3	16.0	16.8	20.6	12.5	25.6	21	05.7	01	26	02.7	14	03.1	06	01.8	15	02.3	11	02.9	04	02.2	10	02.3	07	01.9	.
VI	-	21.1	25.9	21.9	22.7	27.2	18.4	34.1	26	11.1	05	22	02.3	04	02.8	06	01.3	13	02.2	10	02.3	02	02.5	10	01.9	23	02.0	.
VII	-	22.7	27.2	23.1	24.0	28.5	19.3	34.5	29	13.5	16	35	02.6	17	03.4	03	02.0	10	02.3	06	02.8	04	02.0	.	.	18	01.8	.
VIII	-	22.7	27.9	23.8	24.5	28.9	20.2	38.2	07	15.8	24	22	01.9	01	02.0	09	01.3	16	01.7	05	02.2	10	02.0	09	02.1	21	02.0	.
IX	-	19.6	25.1	21.1	21.7	26.5	17.5	35.5	12	08.5	30	20	03.1	17	03.2	07	01.6	10	02.1	06	02.2	06	01.5	05	01.8	19	01.6	.
X	-	13.1	18.1	14.3	14.9	18.7	10.8	26.5	06	05.0	26	19	02.9	10	04.0	10	01.1	18	02.0	09	02.6	.	.	03	01.3	24	01.7	.
XI	-	11.0	15.4	12.6	12.9	16.2	09.0	19.6	25	04.0	26,17	17	02.2	02	03.0	08	01.4	29	02.3	15	03.0	02	01.5	04	02.0	13	02.2	.
XII	-	07.3	10.6	07.5	08.2	11.4	04.4	15.5	11,04	-02.5	23	21	03.1	16	03.6	04	01.5	17	02.2	09	03.2	02	01.5	04	01.8	20	02.0	.
GOD.	-	13.7	17.8	14.6	15.2	19.0	11.2	38.2	7 VIII	-02.5	25 I, 28 II	251	02.7	118	03.4	72	01.5	228	02.3	133	02.7	41	01.8	50	01.9	202	01.9	.
φ = 44° 08' N λ = 15° 13' E Gr. ΔG = + 1h 01 min.												ZADAR																BR. ST. 82
I	758.9	06.7	10.4	07.6	08.1	11.3	05.1	16.6	06	-00.5	23,22	06	02.8	03	01.3	11	01.5	41	02.6	01	02.0	.	.	03	02.0	10	02.3	18
II	757.8	05.2	09.5	06.3	06.8	10.2	03.5	15.5	06	-02.2	17	14	02.6	05	02.2	17	01.7	27	02.8	04	03.2	.	.	03	02.3	05	02.2	09
III	758.4	06.6	10.6	08.2	08.4	11.6	04.7	15.7	26	-01.0	01	09	01.9	07	01.9	07	01.4	38	02.8	07	02.3	01	01.0	01	04.0	14	03.1	09
IV	760.6	11.0	14.4	11.7	12.2	15.5	08.7	22.0	25	03.0	05	09	02.9	01	04.0	05	01.6	26	02.8	07	01.7	.	.	03	03.0	17	02.5	27
V	761.1	15.2	18.5	15.3	16.0	19.7	11.6	24.5	20	04.0	01	06	03.2	06	02.5	01	03.0	24	02.9	04	02.8	01	02.0	.	.	26	02.7	29
VI	761.5	20.7	24.6	20.6	21.6	25.8	17.2	30.6	28	11.4	04,03	02	01.0	01	01.0	01	01.0	20	02.0	06	01.5	03	01.3	03	02.0	25	02.4	29
VII	759.8	21.8	26.2	22.1	23.0	27.3	18.5	34.2	12	14.1	19	06	02.2	05	02.0	.	.	18	02.3	05	01.8	01	01.0	04	01.5	28	02.3	26
VIII	760.0	22.3	26.7	22.8	23.7	27.4	19.8	33.8	07	15.6	27	03	02.0	.	.	04	01.2	10	02.2	02	02.0	02	02.5	03	03.0	30	02.4	30
IX	762.8	18.4	24.7	20.0	20.8	25.3	16.2	28.9	12	09.5	29	05	02.8	06	03.3	04	02.2	16	01.7	02	01.5	.	.	03	02.0	20	02.4	34
X	763.7	12.3	18.3	13.4	14.4	19.1	10.6	23.6	13	04.6	25	05	01.4	13	01.6	03	01.3	13	02.7	.	.	.	.	.	.	17	01.8	42
XI	762.7	10.6	15.6	12.4	12.8	16.5	09.3	19.2	04	05.2	17	02	03.0	05	01.0	17	01.5	27	03.1	03	02.7	.	.	01	01.0	17	02.4	18
XII	763.4	06.6	11.2	07.7	08.3	12.3	05.2	17.6	01	-01.7	24	08	01.5	03	03.0	24	01.8	16	03.0	01	01.0	.	.	04	03.0	07	02.4	30
GOD.	760.9	13.1	17.6	14.0	14.7	18.5	10.9	34.2	41 VII	-02.2	17 II	75	02.3	55	02.0	94	01.6	276	02.6	42	02.1	08	01.6	28	02.4	216	02.4	301
φ = 44° 48' N λ = 15° 19' E Gr. ΔG = + 1h 01 min.												LIČKO LEŠĆE																BR. ST. 83
I	-	00.6	02.8	01.4	01.5	04.2	-01.7	13.5	06	-08.6	24	13	01.8	03	01.3	01	01.0	07	02.1	19	02.5	04	01.0	01	01.0	27	01.4	18
II	-	-00.2	04.0	00.7	01.3	05.3	-03.4	12.2	05	-16.1	20	08	02.2	02	01.5	01	01.0	16	01.9	14	02.7	05	03.4	04	01.5	22	01.5	12
III	-	00.7	05.8	02.3	02.8	07.0	-01.7	16.6	24	-11.1	09	09	02.1	05	01.6	05	01.4	09	02.3	17	02.7	03	02.0	02	01.5	23	01.5	20
IV	-	07.1	12.6	07.3	08.6	13.9	03.8	25.2	19	-03.1	04	12	02.2	06	02.0	.	.	11	01.9	19	02.7	06	03.0	07	01.1	20	01.6	09
V	-	09.8	16.3	09.7	11.4	17.5	04.5	23.6	10	-02.9	01	20	01.9	09	01.7	03	01.0	04	02.2	07	03.3	06	02.0	02	01.0	26	01.3	16
VI	-	15.2	23.2	14.6	16.9	24.4	10.1	29.3	17	02.4	05	15	01.5	10	01.0	02	01.0	06	01.3	02	03.0	04	01.0	04	01.0	12	01.3	3
VII	-	15.4	24.1	14.4	17.1	24.8	09.9	32.3	24	03.7	18	11	01.7	09	01.8	02	01.5	06	02.2	05	03.2	03	01.0	01	01.0	27	01.4	29
VIII	-	15.0	24.9	15.2	17.6	25.5	11.2	33.5	07	06.6	27	12	01.8	01	02.0	.	.	04	01.0	02	01.0	07	01.7	04	01.2	20	01.3	43
IX	-	10.8	21.9	12.4	14.4	22.6	07.6	30.4	11	-04.2	30	16	01.4	04	02.0	.	.	06	01.8	06	02.5	04	01.5	01	01.0	23	01.4	31
X	-	05.6	14.8	06.4	08.3	15.9	02.2	25.0	11	-06.2	25	15	01.2	03	01.3	02	01.5	07	01.4	05	03.0	06	01.3	03	01.3	27	01.3	25
XI	-	04.5	11.3	05.8	06.8	11.9	01.4	18.8	04	-03.9	17	02	01.0	02	02.0	01	01.0	09	01.9	19	03.7	07	02.6	04	01.0	25	01.1	21
XII	-	-02.7	02.7	-01.3	-00.7	03.9	-05.2	16.2	01	-15.6	26	05	01.8	07	01.6	01	01.0	04	01.8	08	02.2	05	02.4	07	01.6	27	01.8	29
GOD.	-	06.8	13.7	07.4	08.8	14.7	03.2	33.5	7 VIII	-16.1	20 II	138	01.7	61	01.6	18	01.2	89	01.9	123	02.8	60	02.0	40	01.2	279	01.4	267
φ = 44° 33' N λ = 15° 22' E Gr. ΔG = + 1h 02 min.												GOSPIĆ																BR. ST. 84
I	709.5	-00.3	02.0	00.2	00.5	03.6	-02.6	11.0	05	-10.0	24	18	01.9	08	01.6	01	01.0	10	02.2	14	01.6	.	.	06	01.2	03	01.0	15
II	707.4	-01.1	03.2	00.0	00.5	04.6	-03.9	10.7	05	-18.1	20	12	02.4	14	02.5	01	01.0	09	02.0	09	02.2	10	02.9	09	02.7	04	01.5	16
III	708.5	-01.8	04.6	01.3	01.4	06.0	-03.4	15.2	26	-13.0	09	16	01.8	05	02.2	02	01.5	09	02.4	10	02.1	04	02.8	05	03.2	05	01.2	37
IV	710.4	05.5	11.2	07.0	07.7	12.8	02.9	23.0	19,18	-04.3	04	07	02.3	12	02.6	04	02.0	05	01.6	14	02.1	07	02.9	12	02.7	03	01.0	26
V	712.1	08.1	14.8	09.8	10.6	16.2	04.4	21.7	10	-03.9	01	08	02.2	16	02.5	05	02.6	07	01.6	11	01.8	07	02.3	06	02.2	02	01.0	31
VI	713.6	13.8	22.6	16.1	17.2	23.6	09.6	28.6	28	00.7	05	06	01.7	12	01.8	04	01.8	02	01.5	04	01.5	06	02.5	10	02.6	03	02.0	41
VII	712.7	14.4	23.1	16.3	17.5	23.9	09.9	31.5	23	03.7	19	14	02.1	09	02.3	07	02.3	02	01.5	05	02.4	06	01.7	10	01.9	06	01.7	34
VIII	712.5	13.3	24.1	16.5	17.6	24.9	10.7	31.6	07	04.9	27	07	01.6	09	02.0	02	01.0	02	02.0	03	01.3	09	02.0	07	02.0	05	01.2	49
IX	715.6	08.8	20.8	12.5	13.7	21.3	07.0	28.6	12	-05.6	30	17	01.9	10	02.4	02	02.0	02	02.0	03	01.7	07	02.1	06	02.2	03	01.7	40
X	715.2	03.4	14.5	06.8	07.8	15.5	01.4	26.0	11,10	-06.3	25	14	02.4	11	02.5	.	.	04	02.2	09	02.0	08	02.0	06	01.7	01	02.0	40
XI	713.3	03.7	10.3	06.0	06.5	11.4	01.3	18.4	04	-05.1	17	06	02.0	05	02.0	01	01.0	04	01.8	17	02.5	11	02.4	08	02.4	01	02.0	37
XII	714.5	-02.9	03.2	-01.3	-00.6	04.3	-05.4	13.0	01	-14.4	26,24	06	02.2	10	02.4	03	01.7	07	02.1	03	02.7	04	02.5	03	03.3	07	01.7	50
GOD.	712.1	05.4	12.9	07.6	08.4	14.0	02.7	31.6	7 VIII	-18.1	20 II	131	02.0	121	02.3	32	01.9	63	02.0	102	02.0	79	02.4	88	02.3	43	01.5	436
φ = 44° 51' N λ = 15° 36' E Gr. ΔG = + 1h 02 min.												PLITVIČKI LJESKOVAC																BR. ST. 85
I	-	-01.8	00.9	-01.2	-00.9	03.0	-04.3	12.2	28	-12.0	24	07	01.3	34	01.8	01	02.0	02	01.5	02	02.0	35	02.1	01	01.0	11	01.6	.
II	-	-01.4	01.8	-01.0	-00.4	04.0	-04.6	11.4	05	-15.1	20	06	01.8	30	02.4	01	03.0	01	02.0	01	02.0	35	02.7	.	.	10	01.4	.
III	-	-01.5	04.0	00.4	00.8	05.7	-03.9	14.4	24	-15.0	02	02	01.5	31	02.0	01	01.0	02	01.0	02	01.0	47	02.0	.	.	08	01.4	.
IV	-	04.8	11.4	06.1	07.1	12.6	01.6	24.0	19	-07.0	04	03	01.0	20	02.0	.	.	01	02.0	07	01.0	55	01.7	.	.	04	01.6	.
V	-	08.0	14.3	08.4	09.8	15.2	03.6	22.5	10	-03.0	01	04	01.0	17	01.9	.	.	01	02.0	03	01.0	64	01.4	.	.	04	01.5	.
VI	-	13.8	21.5	13.7	15.7	22.3	09.1	27.4	16	03.2	05	03	01.0	14	01.2	.	.	08	01.0	12	01.0	50	01.1	01	01.0	02	01.5	.
VII	-	13.4	22.7	14.5	16.3	23.2	09.6	29.5	23,22	04.9	20	02	01.5	17	01.9	.	.	15	01.1	14	01.0	38	01.2	01	01.0	06	01.2	.
VIII	-	12.8	22.8	14.7	16.3	23.5	10.2	31.5	07	05.0	28	02	01.0	06	01.7	01	01.0	12	01.1	14	01.2	45	01.2	01	02.0	10	01.0	02
IX	-	09.1	19.6	11.1	12.7	20.1	06.7	29.8	11	-02.5	30	02	01.5	17	01.4	02	01.0	07	01.1	07	01.3	46	01.2	01	01.0	08	02.0	.
X	-	04.8	12.6	06.9	07.8	14.4	02.4	26.0	09	-02.5	24	06	02.0	20	02.0	.	.	06	01.0	03	02.0	51	01.5	01	01.0	06	01.3	.
XI	-	04.3	10.7	05.6	06.5	11.8	01.5	18.0	04	-04.0	17	06	02.2	16	01.7	01	01.0	08	01.8	01	02.0	56	02.1	01	01.0	01	01.0	.
XII	-	-03.0	02.1	-01.9	-01.2	03.5	-04.9	13.1	01	-12.0	24	17	01.6	38	01.8	01	02.0	03	01.7	01	01.0	23	02.1	.	.	10	01.3	.
GOD.	-	05.3	12.0	06.4	07.5	13.3	02.2	31.5	7 VIII	-15.1	20 I	60	01.6	260	01.9	08	01.5	66	01.2	67	01.2	545	01.6	07	01.1	80	01.4	02

Mesec	Oblačnost Nm (0-10) 7	14	21	Srednja	Tlak zraka	Vlažnost zraka e_m mm	Um % 7	14	21	Srednja	Srednja	Padavine R mm Σ	I	I	Broj dana s: 7h ≤ 10,0	7h < 0,0	7h ≤ 0,0	7h ≥ 25,0	7h ≥ 30,0	7h ≥ 30,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 8,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	≈	△	∽	▲	▲	T	≡	▥
BR. ST. 81						**PAG**																															H_o = 1 m H_v = - m h_v = 2.0 m h_v = 1.0 m
I	7.8	6.7	6.6	7.0		071.3	06.2	78	67	76	74	38	155	029.6	01	.	.	04	.	.	.	.	.	06	17	17	14	05	17	.	.	.	.	.	.	.	.	.
II	7.4	6.5	6.6	6.8		102.8	05.2	71	60	69	67	26	114	035.8	12	.	.	04	.	.	.	01	.	.	12	11	09	04	11	.	.	.	.	.	.	04	01	.
III	6.3	6.4	5.8	6.2		126.7	05.8	71	61	72	68	35	177	048.1	05	.	.	02	.	.	.	02	01	08	14	14	13	06	14	01	01	.	.	01	.	04	.	.
IV	6.4	6.0	5.9	6.0		171.3	07.4	76	55	69	66	23	081	018.9	01	.	.	.	.	.	.	01	.	03	08	16	13	04	16	.	.	.	.	01	01	03	01	.
V	5.1	5.5	5.4	5.3		242.3	08.1	59	48	61	56	29	042	023.5	23	.	.	.	02	.	.	01	.	03	07	10	07	01	10	.	.	.	.	.	.	06	.	.
VI	4.3	3.8	3.8	4.0		276.2	13.1	70	51	67	63	26	029	013.0	19	.	.	.	23	06	09	.	.	09	03	08	06	01	08	.	.	.	.	.	.	10	01	.
VII	2.8	3.0	2.9	2.9		326.1	12.9	61	46	62	56	34	050	025.2	01	.	.	.	25	13	14	02	.	16	02	03	03	02	03	.	.	.	.	.	.	01	.	.
VIII	3.7	3.1	2.4	3.1		283.8	14.9	74	50	68	64	28	062	020.1	31	.	.	.	29	14	18	.	.	15	03	07	04	04	07	.	.	.	.	.	.	05	.	.
IX	3.3	1.7	0.9	1.9		273.9	11.7	66	48	63	59	28	019	015.0	17	.	.	.	20	03	07	02	.	.	.	03	03	01	03	.	.	.	.	.	.	01	.	.
X	4.1	3.7	3.3	3.7		204.9	09.1	72	60	74	69	39	053	028.6	02	.	.	.	01	.	.	01	.	11	03	05	05	02	05	.	.	.	.	.	.	02	02	.
XI	6.6	6.2	5.4	6.1		096.6	08.4	81	66	76	75	36	087	016.6	10	.	.	.	.	.	.	01	.	07	12	10	09	04	10	.	.	.	.	.	.	01	.	.
XII	5.5	5.5	4.9	5.3		083.0	05.9	72	64	73	69	39	096	032.6	28	.	.	03	.	.	.	04	01	10	11	10	08	03	08	02	.	.	.	.	.	02	.	01
GOD.	5.2	4.8	4.4	4.9		2258.9	09.1	70	56	69	65	23	965	048.1	5 III	.	.	13	100	36	48	15	02	88	92	114	94	37	112	03	01	.	.	02	01	39	05	01
BR. ST. 82						**ZADAR**																															H_o = 5 m H_v = 3.7 m h_v = 2.0 m h_v = 1.0 m
I	7.2	6.1	5.2	6.2		095.3	07.0	85	77	83	82	47	119	026.7	25	.	.	02	.	.	.	.	.	08	12	16	12	05	16	.	.	.	.	.	.	.	.	.
II	7.1	6.3	4.9	6.1		106.7	-	-	-	-	-	-	074	015.2	15	.	.	05	.	.	.	01	.	04	08	10	09	02	10	02	.	.	.	.	01	03	.	01
III	5.8	6.3	6.3	6.1		146.6	06.8	82	75	83	80	42	154	059.3	12	.	.	02	.	.	.	01	.	08	13	15	11	04	15	01	.	.	.	.	01	04	.	.
IV	7.2	6.0	4.9	6.0		165.2	08.8	85	73	82	80	40	090	011.0	29	.	.	.	.	.	.	01	.	02	07	16	08	01	16	.	.	.	.	.	02	04	.	.
V	4.7	4.3	4.8	4.6		283.1	10.4	77	68	79	75	41	043	017.5	09	.	.	.	.	.	.	.	.	06	06	12	06	02	12	.	.	.	.	.	.	02	.	.
VI	2.9	3.1	3.4	3.1		305.1	14.9	80	65	80	75	46	027	008.0	20	.	.	.	18	02	04	01	.	11	03	09	06	.	09	.	.	.	.	.	.	01	.	.
VII	2.4	2.2	2.0	2.2		-	14.8	74	59	73	69	32	067	035.5	01	.	.	.	24	05	09	.	.	20	02	05	04	03	05	.	.	.	.	.	.	.	.	.
VIII	3.4	2.9	2.1	2.8		296.2	16.9	81	66	80	76	48	097	061.4	09	.	.	.	25	03	19	.	.	17	03	07	06	03	07	.	.	.	.	.	.	04	.	.
IX	1.7	1.7	0.7	1.4		283.4	13.3	74	62	73	70	30	011	004.6	23	.	.	.	19	.	02	.	.	20	.	03	03	.	03	.	.	.	.	.	.	01	.	.
X	3.5	3.3	1.8	3.0		-	09.3	76	62	77	72	33	151	093.0	02	.	.	.	.	.	.	.	.	14	02	06	06	03	06	.	.	.	.	.	.	02	02	.
XI	5.3	5.4	4.3	5.0		124.5	08.4	80	67	77	75	30	053	016.5	10	.	.	.	.	.	.	02	.	07	08	11	11	01	11	.	.	.	.	.	.	02	01	.
XII	5.7	4.6	4.7	5.0		121.1	05.9	75	60	73	69	30	054	016.9	28	.	.	02	.	.	.	.	.	10	10	11	09	02	10	01	.	.	.	.	01	.	.	01
GOD.	4.7	4.4	3.8	4.3		-	-	-	-	-	-	-	900	093.0	1 X	.	.	11	86	10	34	06	.	127	74	121	91	26	120	04	.	.	.	.	05	23	03	02
BR. ST. 83						**LIČKO LEŠCE**																															H_o = 463 m H_v = - m h_v = 2.0 m h_v = 2.0 m
I	8.6	7.3	7.1	7.7		-	04.4	84	78	81	81	82	127	024.3	01	.	08	20	.	.	.	.	.	16	18	15	04	15	07	.	.	03	.	.	.	02	12	
II	8.4	6.8	7.2	7.5		-	04.0	75	69	76	73	43	152	040.2	15	04	04	21	.	.	.	01	.	.	14	16	13	05	11	10	04	01	.	.	.	03	07	18
III	7.9	7.3	6.1	6.7		-	04.4	80	67	79	75	32	214	042.0	12	02	.	23	.	.	.	01	.	01	09	18	12	08	10	16	05	.	.	.	.	04	07	20
IV	6.6	6.2	5.4	6.1		-	05.7	73	52	75	67	26	110	027.1	09	.	.	04	01	.	.	02	.	02	07	20	14	04	19	05	02	.	01	.	.	03	01	02
V	5.1	5.7	4.7	5.2		-	07.0	75	52	75	67	36	047	026.1	23	.	.	05	.	.	.	.	.	04	04	10	08	01	09	01	.	.	.	.	.	01	04	.
VI	5.5	6.0	3.9	5.1		-	11.2	84	56	66	75	52	111	048.8	20	.	.	.	17	.	.	.	.	03	06	13	08	03	13	.	.	.	.	.	.	13	12	.
VII	5.9	4.6	2.6	4.4		-	11.0	81	53	64	73	38	071	024.2	16	.	.	.	19	03	.	.	.	08	03	06	06	03	06	.	.	.	.	01	.	04	13	.
VIII	7.9	4.6	3.4	5.3		-	12.0	90	55	68	78	33	073	016.4	08	.	.	.	17	04	.	.	.	03	04	08	08	04	08	.	.	.	.	.	.	05	19	.
IX	7.6	3.2	2.6	4.5		-	08.9	83	50	70	70	27	016	012.6	17	.	.	06	11	03	.	.	.	06	02	05	02	01	05	.	.	.	.	.	.	01	14	.
X	7.4	4.6	4.1	5.3		-	06.6	86	59	81	76	36	096	018.3	02	.	.	08	01	.	.	.	.	04	07	08	06	02	07	03	01	.	.	.	.	03	14	01
XI	8.5	6.7	5.8	7.0		-	04.2	86	71	82	80	47	044	020.0	22	.	.	12	.	.	.	02	.	01	11	12	07	03	12	.	.	.	.	.	.	02	15	.
XII	7.3	6.3	6.3	6.6		-	03.7	83	74	81	79	28	112	030.6	28	04	08	25	.	.	.	.	.	05	13	14	12	04	09	07	.	.	02	.	.	02	12	09
GOD.	7.2	5.8	4.8	6.0		-	07.1	81	61	80	74	36	1165	048.8	20 VI	10	20	124	44	10	.	04	.	37	96	148	111	42	124	49	12	01	04	01	.	41	120	62
BR. ST. 84						**GOSPIĆ**																															H_o = 564 m H_v = 564.2 m h_v = 2.0 m h_v = 2.0 m
I	9.1	8.3	7.6	8.4		040.5	04.4	90	83	90	88	48	190	036.8	01	01	10	21	.	.	.	.	.	01	22	17	13	08	15	04	.	.	01	.	.	.	11	14
II	8.0	7.9	6.8	7.6		064.1	04.1	84	73	85	81	47	171	038.2	18	03	05	22	.	.	.	01	.	01	15	16	12	07	12	06	01	01	.	.	.	05	05	15
III	7.8	7.8	5.9	7.2		083.5	04.3	90	71	87	83	42	323	038.9	04	04	.	25	.	.	.	.	.	02	14	17	12	07	09	13	04	.	.	.	.	05	06	28
IV	8.0	8.2	5.0	7.1		136.2	05.8	83	59	76	73	29	116	024.8	09	.	.	07	.	.	.	01	.	01	12	18	15	04	17	04	.	.	.	.	.	04	.	02
V	5.8	7.7	5.2	6.2		208.7	06.9	83	55	76	71	38	078	033.3	23	.	.	04	.	.	.	.	.	03	09	12	08	03	11	02	01	.	.	.	.	.	.	.
VI	5.0	6.4	4.0	5.1		245.9	11.0	88	54	82	75	39	078	030.8	19	.	.	.	14	.	.	01	.	04	05	12	06	03	12	.	.	.	.	.	.	08	03	.
VII	4.5	5.4	3.5	4.4		289.6	11.0	86	51	81	73	29	152	049.9	14	.	.	.	18	02	.	02	.	10	06	07	05	05	07	.	.	.	.	.	.	04	03	.
VIII	6.1	5.6	2.2	4.6		242.7	11.8	96	53	90	80	28	093	026.4	09	.	.	.	17	03	.	01	.	07	04	08	08	05	08	.	.	.	.	.	.	08	10	.
IX	4.3	4.3	1.9	3.5		217.7	09.1	93	50	87	77	28	017	010.5	17	.	.	05	07	.	.	.	.	09	02	04	03	01	04	.	.	.	.	.	.	01	10	.
X	6.1	5.2	3.4	4.9		175.8	06.3	92	54	89	78	33	069	016.9	02	.	.	10	02	.	.	.	.	06	06	07	05	04	06	01	.	.	.	.	.	03	12	.
XI	8.3	7.3	5.4	7.0		080.1	05.9	91	65	86	81	31	111	027.7	22	.	.	13	.	.	.	01	.	03	13	11	09	04	11	.	.	.	.	.	01	04	08	.
XII	6.2	6.2	5.2	5.9		068.9	03.9	92	72	88	84	22	155	048.1	28	06	08	26	.	.	.	01	.	08	15	14	13	03	08	08	.	.	02	.	.	03	09	09
GOD.	6.6	6.7	4.7	6.0		1853.7	07.0	89	61	84	78	22	1453	069.9	46 VII	14	23	135	58	05	.	08	.	55	123	143	109	54	120	38	06	01	03	.	01	45	77	68
BR. ST. 85						**PLITVIČKI LJESKOVAC**																															H_o = 650 m H_v = - m h_v = 2.0 m h_v = 2.0 m
I	8.9	7.9	7.0	7.9		-	04.1	88	86	90	88	66	120	032.4	17	02	09	25	.	.	.	.	.	01	16	11	11	05	05	08	.	.	.	.	.	.	07	31
II	7.4	7.3	5.8	6.8		-	03.8	83	74	85	81	29	159	055.4	16	04	07	25	.	.	.	.	.	01	09	13	13	03	06	07	.	.	.	.	.	.	01	21
III	7.7	7.8	6.2	7.2		-	03.8	79	68	80	76	15	154	048.6	12	04	02	24	.	.	.	.	.	01	16	14	14	04	05	14	03	.	.	.	.	01	.	31
IV	6.8	5.1	4.9	5.6		-	05.4	81	59	77	73	19	123	024.4	30	.	.	07	.	.	.	.	.	01	07	13	13	05	10	05	01	.	.	.	.	.	02	07
V	5.6	3.7	4.0	4.4		-	06.1	78	47	79	68	26	185	126.5	23	.	.	05	.	.	.	.	.	04	05	09	08	03	08	02	.	.	.	.	.	.	.	.
VI	4.5	4.0	3.6	4.0		-	09.9	84	51	83	73	26	160	045.4	20	.	.	.	11	.	.	.	.	07	02	11	10	05	11	.	.	.	.	.	.	06	.	.
VII	3.5	2.8	2.7	3.0		-	10.0	87	52	79	73	20	150	044.5	17	.	.	.	16	.	.	.	.	15	04	07	07	05	07	.	.	.	.	.	.	.	01	.
VIII	4.4	2.7	3.5	3.5		-	11.6	92	66	89	82	25	074	020.4	09	.	.	.	11	02	.	.	.	09	03	07	07	04	07	.	.	.	.	.	.	.	04	.
IX	5.3	3.1	2.2	3.5		-	09.8	92	56	92	80	27	017	097.0	01	.	.	04	09	.	.	.	.	09	03	04	03	.	04	.	.	.	.	.	.	.	05	01
X	5.6	4.7	4.5	4.9		-	07.0	89	75	93	86	11	097	040.0	21	.	.	07	02	.	.	.	.	10	08	08	06	03	06	04	02	.	.	.	.	.	02	.
XI	6.6	6.0	3.6	5.4		-	06.1	92	66	89	82	35	071	019.8	23	.	.	08	.	.	.	.	.	04	07	13	10	03	13	02	02	.	.	.	.	.	.	09
XII	7.8	5.7	4.3	6.0		-	03.8	88	80	86	85	40	042	018.4	06	02	09	29	.	.	.	01	.	05	10	11	08	01	07	06	01	.	.	.	.	.	.	.
GOD.	6.2	5.1	4.4	5.2		-	06.7	86	65	85	78	11	1352	126.5	25 V	12	27	134	49	02	.	01	.	67	90	121	110	41	89	46	09	.	.	.	.	08	22	100

Mesec	Vazdušni pritisak Pa 760	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm (Sm+i+2Sm)/4	Tmi	Tmin	Tmax	Amt.	Amin	Amt.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12): N		NE		E		SE		S		SW		W		NW		C
												δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.	δ.	j.		j.	δ.	j.	δ.
GRAČAC — φ = 44° 18' N λ = 15° 51' E Gr. Δ G = + 1h 03 min. — BR. ST. 86																												
I	-	00.8	02.9	01.4	01.6	04.5	-01.5	11.0	06	-08.6	24	18	01.4	02	03.5	09	01.1	10	02.4	11	03.0	01	02.0	13	01.4	12	01.4	11
II	-	00.1	03.0	00.5	01.0	04.4	-02.5	11.4	09	-10.5	18	29	02.1	04	01.2	02	01.0	11	02.5	16	02.7	04	03.2	07	01.7	04	01.6	07
III	-	00.0	05.3	02.6	02.6	06.9	-01.5	16.0	26	-15.3	08	18	02.4	03	02.0	06	01.3	14	02.7	07	03.4	09	01.8	15	01.7	05	01.8	16
IV	-	06.0	11.4	08.1	08.4	12.9	03.9	22.4	23,18	-05.4	04	24	02.0	03	01.0	10	01.2	09	02.2	21	02.4	08	02.2	04	01.2	04	01.2	07
V	-	08.9	14.6	11.1	11.4	16.5	05.9	21.6	26,10	-01.5	01	28	01.7	04	01.8	08	01.0	06	02.2	09	02.8	09	01.6	14	01.5	06	01.3	09
VI	-	14.4	22.6	16.9	17.7	23.8	10.9	29.0	28	02.4	05	17	01.6	04	01.2	06	01.0	03	01.3	07	01.6	12	01.3	13	01.3	08	01.0	20
VII	-	14.6	23.4	17.9	18.4	24.8	11.6	32.0	23	05.2	19	34	01.5	03	01.3	01	01.0	04	02.2	06	02.2	04	01.0	11	01.5	14	01.3	16
VIII	-	14.4	24.6	18.0	18.7	25.6	12.2	32.0	07	06.2	28	13	01.2	04	01.2	.	.	03	01.3	10	01.5	13	01.2	16	01.1	03	01.0	31
IX	-	10.3	21.3	14.7	15.3	22.4	08.9	29.5	12	-03.3	30	27	01.8	05	01.4	01	01.0	01	01.0	08	01.4	09	01.4	10	01.2	11	01.3	18
X	-	05.1	14.8	08.7	09.3	15.8	03.7	26.2	11	-02.6	26	32	02.0	01	01.0	02	01.0	08	02.0	09	02.0	04	01.2	08	01.2	09	01.6	20
XI	-	04.5	10.2	06.9	07.2	11.5	03.0	17.5	04	-03.8	29	19	01.3	02	01.0	02	01.0	15	02.1	12	02.4	10	01.7	12	01.4	03	01.0	19
XII	-	-01.6	03.7	00.0	00.5	05.1	-04.0	13.0	01	-15.2	26	19	02.3	01	02.0	02	01.0	08	01.1	05	02.6	14	02.2	18	01.4	03	01.3	23
GOD.	-	06.5	13.2	08.9	09.3	14.5	04.2	32.0	7 VIII	-15.3	8 III	278	01.8	36	01.5	49	01.1	92	02.1	121	02.4	97	01.7	141	01.4	82	01.3	199
KNIN — φ = 44° 02' N λ = 16° 12' E Gr. Δ G = + 1h 05 min. — BR. ST. 87																												
I	737.6	03.9	07.8	04.8	05.3	09.2	01.9	17.4	06	-05.9	24	29	03.0	03	01.3	02	01.0	07	02.7	10	01.9	03	03.0	.	.	06	02.2	33
II	735.8	02.7	07.4	03.6	04.3	08.3	00.8	15.6	05	-05.4	17	37	03.4	03	03.3	02	02.0	04	01.2	14	02.6	06	03.2	02	02.5	02	01.6	14
III	737.0	03.7	09.9	06.4	06.6	11.3	02.3	20.6	26	-04.3	08	33	03.0	04	03.5	10	02.5	02	03.5	11	02.1	13	03.0	04	01.0	04	02.2	12
IV	738.6	08.7	15.5	10.8	11.5	16.7	06.5	25.0	19	-00.3	04	23	03.3	03	01.7	01	04.0	01	03.0	13	02.8	15	02.3	09	01.9	05	02.7	20
V	739.6	12.2	19.6	13.7	14.8	20.8	09.5	26.3	10	04.0	03	42	02.9	02	02.5	02	02.0	.	.	15	02.1	04	03.0	08	02.2	05	02.2	15
VI	740.8	17.3	26.8	20.2	21.2	27.8	14.8	32.6	28	08.3	05	13	02.8	06	03.0	.	.	.	.	08	02.4	09	02.6	15	02.1	04	01.2	35
VII	739.1	18.5	28.1	21.4	22.4	29.4	15.8	36.8	24	08.5	19	23	03.5	01	04.0	07	01.7	.	.	06	02.0	01	02.0	09	02.3	14	03.6	37
VIII	739.6	17.4	27.6	20.6	21.6	28.7	15.6	35.2	07	11.4	28,27	14	01.9	03	01.3	03	01.7	02	02.0	04	01.5	07	01.7	08	01.6	02	02.5	50
IX	742.4	14.2	26.3	17.8	19.0	26.7	13.0	32.9	12	01.0	30	44	03.4	.	.	.	.	01	02.0	05	01.6	02	03.0	05	01.6	02	01.0	31
X	742.9	07.3	19.0	11.1	12.1	19.5	06.0	28.4	12	00.0	26	29	03.8	01	04.0	01	04.0	.	.	06	02.3	05	01.8	09	01.8	05	03.0	37
XI	741.8	06.7	14.2	09.6	10.0	15.3	05.4	19.0	03	-01.3	29	12	02.8	04	01.2	04	01.5	02	03.0	13	02.7	06	02.0	03	01.7	09	02.1	37
XII	742.6	02.8	09.1	04.2	05.1	10.3	00.1	15.4	11	-07.3	21	36	03.4	02	03.5	03	02.3	02	01.5	07	02.7	03	03.3	05	01.2	01	01.0	34
GOD.	739.8	09.6	17.6	12.0	12.8	18.7	07.6	36.8	14 VII	-07.3	14 XII	335	03.2	32	02.5	35	02.1	21	02.3	112	02.3	74	02.5	77	01.9	59	02.4	350
ŠIBENIK — φ = 43° 44' N λ = 15° 54' E Gr. Δ G = + 1h 04 min. — BR. ST. 88																												
I	751.9	07.1	10.2	07.6	08.1	11.2	05.0	18.3	06	-01.0	22	19	03.9	17	04.1	06	02.8	28	03.8	01	01.0	.	.	01	01.0	.	.	21
II	750.5	05.5	09.3	06.2	06.8	10.2	03.5	16.6	05	-03.8	17	21	04.6	13	05.4	07	02.3	21	04.0	03	01.3	02	02.0	02	02.0	01	01.0	14
III	751.1	06.8	11.2	08.6	08.8	12.4	05.2	20.6	26	-00.5	02	15	04.6	17	04.6	02	01.0	26	04.4	03	04.7	05	03.4	08	01.2	.	.	17
IV	753.0	11.5	15.1	12.1	12.7	16.6	08.9	24.9	25	01.7	04,03	10	04.7	07	06.0	06	02.0	24	04.2	05	01.6	03	02.0	07	01.4	05	03.0	23
V	753.9	15.2	19.6	15.4	16.4	20.7	12.3	25.6	10	05.2	01	23	04.6	09	04.3	03	04.3	14	04.2	07	04.0	07	01.9	10	02.8	03	03.0	17
VI	754.9	20.9	25.5	21.6	22.4	26.8	17.9	32.0	26	11.8	03	14	03.6	04	02.0	07	01.7	07	01.7	06	02.2	07	02.4	12	02.1	04	02.8	29
VII	752.9	23.0	27.4	23.5	24.3	29.0	19.9	35.3	23	13.0	16	23	04.4	08	05.1	.	.	11	03.5	06	02.5	03	03.7	17	01.9	06	01.5	19
VIII	753.4	22.2	27.6	23.5	24.2	28.7	19.8	34.6	07	14.8	24	17	02.8	05	04.0	07	02.0	08	03.8	03	01.0	06	02.3	15	01.7	06	02.3	26
IX	756.1	19.0	25.5	20.6	21.4	26.5	17.2	32.3	12	10.0	30	24	03.6	14	04.0	.	.	.	.	02	01.5	10	01.7	10	01.6	04	02.2	26
X	757.0	12.4	18.8	14.2	14.9	19.5	11.0	25.2	13	04.9	25	17	04.8	17	04.5	01	01.0	13	04.0	01	03.0	07	02.0	08	01.2	03	02.0	26
XI	756.1	11.2	15.6	12.5	12.9	16.6	09.5	19.4	02	04.8	17	15	02.9	10	02.6	05	01.6	24	04.0	02	05.5	03	01.0	05	02.2	03	01.0	23
XII	756.9	06.7	10.9	08.0	08.4	12.0	04.9	15.6	30,01	-01.8	26	25	03.6	16	04.4	04	03.0	15	04.9	.	.	03	02.7	02	02.0	02	01.0	26
GOD.	754.0	13.5	18.1	14.5	15.1	19.2	11.3	35.3	13 VII	-03.8	17. II	223	04.0	137	04.4	48	02.2	191	04.0	39	02.6	56	02.2	97	01.8	37	02.1	267
KOMIŽA — φ = 43° 03' N λ = 16° 05' E Gr. Δ G = + 1h 04 min. — BR. ST. 89																												
I	-	09.7	12.1	10.0	10.4	13.0	07.6	18.3	06	01.8	23	26	02.8	07	03.3	13	02.5	21	03.5	13	02.5	02	02.0	05	02.2	05	02.0	01
II	-	08.3	10.9	08.6	09.1	12.1	05.8	17.6	06	-00.8	17	21	03.0	11	02.9	12	02.1	14	03.2	10	03.1	04	05.0	03	01.7	09	02.6	.
III	-	09.1	12.1	10.1	10.3	13.0	07.4	16.7	27	01.8	01	10	03.4	15	03.1	10	03.4	22	04.2	12	03.8	06	03.7	05	01.8	12	02.2	01
IV	-	13.4	15.6	13.0	13.8	16.9	10.1	24.1	25	03.4	03	06	03.3	10	03.3	10	03.7	18	03.1	09	02.3	07	01.9	15	02.4	09	02.8	06
V	-	16.2	19.0	16.0	16.8	20.0	12.9	23.5	27	06.6	01	18	02.7	09	02.4	09	03.2	19	03.5	04	02.0	03	01.7	08	03.0	18	02.8	05
VI	-	22.4	25.1	21.5	22.6	26.2	17.7	31.5	29	11.0	04	14	02.2	04	02.5	09	03.3	13	03.2	03	01.7	06	01.5	14	01.6	14	02.1	13
VII	-	23.9	26.6	23.1	24.2	27.9	19.3	32.5	25	15.8	18	17	02.9	05	03.0	05	03.6	12	02.9	05	01.8	09	01.7	16	01.9	12	02.0	12
VIII	-	24.5	27.5	23.6	24.8	28.8	20.7	33.9	07	16.0	28	11	02.8	02	03.0	07	02.6	07	03.0	03	02.3	07	01.6	22	01.6	17	02.0	17
IX	-	21.9	25.8	21.4	22.6	26.4	17.6	32.1	11	10.8	29	21	02.6	11	03.6	06	01.3	09	02.6	05	01.4	05	01.6	13	01.6	10	02.2	10
X	-	14.9	19.3	15.6	16.3	20.0	12.5	25.3	13	08.2	25	14	02.9	08	02.6	12	01.9	11	02.6	04	04.2	03	01.7	10	01.7	20	02.4	11
XI	-	13.4	16.5	13.6	14.3	17.4	10.8	20.0	20	04.4	17	13	02.2	09	03.7	08	02.0	19	03.0	06	02.2	08	02.5	05	02.6	12	02.1	10
XII	-	10.0	12.9	10.2	10.8	13.8	07.4	18.2	01	01.8	20	16	02.4	19	02.7	15	02.3	14	03.4	04	03.0	03	03.7	07	02.4	11	01.8	04
GOD.	-	15.6	18.6	15.6	16.3	19.6	12.5	33.9	7 VIII	-00.8	47 II	187	02.7	110	03.0	116	02.6	179	03.3	78	02.7	63	02.3	123	02.0	149	02.3	90
KAŠTEL STARI — φ = 43° 33' N λ = 16° 21' E Gr. Δ G = + 1h 05 min. — BR. ST. 90																												
I	-	07.6	11.3	08.1	08.8	12.1	05.0	17.6	06	-01.0	24	02	03.5	16	02.4	11	02.5	24	02.3	.	.	02	01.0	01	01.0	17	02.2	20
II	-	05.4	10.0	06.6	07.2	11.1	03.1	17.2	06	-03.5	18	05	02.8	26	03.2	13	02.4	12	03.2	01	05.0	06	01.7	.	.	13	02.1	08
III	-	07.2	11.9	08.8	09.2	13.3	05.0	18.2	26	-00.4	02	01	01.0	20	03.2	14	01.6	25	03.1	05	02.0	04	02.0	.	.	11	02.1	13
IV	-	11.5	16.0	11.8	12.8	17.1	07.8	24.0	25	02.0	04	03	03.0	12	02.9	14	02.2	22	02.6	.	.	08	01.4	02	02.5	05	02.4	24
V	-	15.6	20.7	15.5	16.8	21.5	11.1	26.1	31	05.0	01	01	03.0	23	03.3	10	02.1	16	02.5	02	01.0	11	02.2	.	.	13	03.1	17
VI	-	21.4	26.7	21.2	22.6	27.8	16.6	32.7	27	11.3	05,03	.	.	13	02.6	04	01.8	12	02.1	01	02.0	18	01.7	01	01.0	10	01.9	31
VII	-	23.2	28.6	23.1	24.5	29.5	18.0	35.0	23	13.0	19	.	.	24	02.7	02	01.0	15	02.1	01	02.0	24	01.9	.	.	10	02.7	17
VIII	-	22.7	29.0	23.1	24.4	29.7	18.3	36.6	06	14.5	26	.	.	20	01.8	02	01.5	19	01.7	01	02.0	13	02.3	.	.	09	02.4	29
IX	-	18.7	26.6	20.0	21.3	27.1	15.6	31.9	12	06.5	30	01	03.0	20	03.2	.	.	12	01.2	01	02.0	13	01.5	.	.	08	02.1	35
X	-	12.0	19.7	13.8	14.8	20.4	09.6	25.2	13	05.0	26,25	01	03.0	24	03.5	04	02.0	14	02.5	.	.	08	01.5	03	01.0	04	03.0	35
XI	-	10.5	15.9	11.9	12.6	16.8	08.0	19.5	02	02.5	27	01	02.0	09	02.7	08	02.0	19	02.6	.	.	03	01.3	.	.	18	02.3	32
XII	-	07.3	12.2	08.0	08.9	12.9	04.0	17.6	11	-01.0	18	01	02.0	22	03.1	12	02.3	12	02.6	.	.	08	01.4	01	01.0	10	02.1	27
GOD.	-	13.6	19.0	14.3	15.3	19.9	10.2	36.6	6 VIII	-03.5	48 II	16	02.8	229	02.9	94	02.1	202	02.4	12	02.1	118	01.8	08	01.4	128	02.3	288

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dles)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dles)	min	Padavine R mm Σ	max	Dnev.	Broj dana sa: Tn ≤0,0	Tn ≤-5,0	Tn ≤-10,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) <8,0	>8,0	R mm ≥0,1	≥1,0	≥10,0	●	*	≈	△	▲	R T	■	▦
GRAČAC																																				
BR. ST. 86																																				
H_a = 560 m H_b = - m h_a = 2,0 m h_b = 2,0 m																																				
I	9.3	8.3	8.5	8.7	-	04.8	89	86	88	88	65	404	107.5	01	.	07	19	.	.	.	02	.	.	23	15	14	09	14	04	02	.	01	.	.	.	02	-
II	8.9	7.9	8.4	8.4	-	04.2	82	77	79	80	48	267	065.7	12	01	07	21	.	.	.	03	.	.	20	15	13	08	13	04	01	.	.	.	.	03	01	14
III	7.8	7.8	6.3	7.3	-	04.5	87	71	80	79	34	327	086.1	04	03	01	19	.	.	.	01	.	02	17	13	13	08	08	11	02	01	.	.	.	05	02	22
IV	7.8	7.6	7.2	7.5	-	06.3	83	65	75	74	38	301	107.5	09	.	.	04	.	.	.	01	.	.	16	18	15	07	17	03	01	.	.	.	.	03	.	02
V	5.6	6.8	6.1	6.2	-	07.1	81	61	69	71	33	100	048.0	23	.	.	06	.	.	.	01	.	04	08	16	11	02	15	02	01	.	.	.	.	03	.	.
VI	4.8	6.0	4.8	5.2	-	11.0	88	55	75	72	38	062	021.4	10	.	.	.	14	.	.	.	.	04	06	11	06	03	11	.	.	.	.	.	.	05	02	.
VII	4.0	5.1	4.2	4.4	-	11.1	84	54	73	70	35	124	047.0	05	.	.	.	17	05	.	.	.	09	06	07	07	04	07	.	.	.	.	.	.	01	03	.
VIII	5.9	5.2	3.3	4.8	-	11.8	92	53	78	74	37	118	031.8	25	.	.	.	18	03	.	.	.	06	05	12	09	04	12	.	.	.	.	.	.	04	07	.
IX	4.7	3.3	1.8	3.3	-	09.5	89	56	73	73	32	012	010.0	18	.	.	01	12	.	.	.	.	13	02	04	02	01	04	.	.	.	.	.	.	01	04	.
X	6.8	4.2	3.2	4.7	-	07.1	89	63	83	79	29	098	040.7	02	.	.	06	02	.	.	01	.	06	04	05	05	03	05	.	.	.	.	.	.	01	07	.
XI	7.8	6.8	6.3	7.0	-	06.6	91	78	84	84	46	164	078.7	22	.	.	06	.	.	.	02	01	02	13	10	09	04	10	.	.	.	.	.	.	02	05	.
XII	6.8	6.0	5.6	6.1	-	04.2	85	76	84	82	27	310	144.7	28	05	05	25	.	.	.	01	01	08	15	14	13	07	10	04	.	.	.	.	.	03	02	07
GOD.	6.7	6.2	5.5	6.1	-	07.4	86	66	78	77	27	2287	144.7	26 XII	09	20	104	63	08	.	12	02	54	135	140	117	60	126	28	07	01	01	.	.	31	35	-
KNIN																																				
BR. ST. 87																																				
H_a = 234 m H_b = 242.8 m h_a = 2,0 m h_b = 1,0 m																																				
I	7.2	7.0	5.6	6.6	-	05.3	80	69	77	75	32	238	055.2	01	.	.	11	.	.	.	01	.	05	14	17	14	08	17	01	01	.	.	.	.	.	.	.
II	7.1	6.5	5.5	6.3	-	04.5	73	58	73	68	31	103	020.6	15	.	01	13	.	.	.	04	.	02	12	13	13	06	13	03	02	.	.	.	01	02	02	-
III	6.3	6.8	5.8	6.3	-	05.1	78	58	71	68	21	200	058.5	05	.	.	09	.	.	.	03	.	03	14	11	11	08	11	04	02	.	.	.	02	07	.	02
IV	7.3	7.6	4.5	6.5	-	06.8	80	50	70	67	20	099	029.7	09	.	.	01	01	.	.	03	.	01	13	15	13	02	15	01	01	.	.	.	02	02	01	.
V	5.4	6.3	4.2	5.3	-	08.1	76	47	68	64	27	063	025.9	12	.	.	.	01	.	.	.	.	04	07	09	06	03	09	.	.	.	.	.	.	01	.	.
VI	3.4	5.8	3.3	4.2	-	12.4	83	47	70	67	30	031	005.6	25	.	.	.	23	09	01	.	.	07	02	12	08	.	12	.	.	.	.	.	.	08	.	.
VII	3.2	5.1	2.7	3.7	-	12.6	78	45	66	63	29	040	020.4	01	.	.	.	23	17	02	03	.	12	03	05	04	01	05	.	.	.	.	.	01	02	.	.
VIII	3.5	5.3	3.0	3.9	-	13.7	91	49	78	73	32	194	033.5	01	.	.	.	27	14	.	.	.	11	06	10	09	06	10	.	.	.	.	.	.	09	.	.
IX	3.3	2.4	0.7	2.1	-	10.4	80	40	69	63	25	004	003.2	01	.	.	.	21	03	.	02	.	17	.	02	01	.	02	.	.	.	.	.	.	01	.	.
X	3.3	3.8	2.2	3.1	-	07.5	85	47	81	71	27	050	016.4	02	.	.	.	05	.	.	02	.	13	04	05	05	03	05	.	.	.	.	.	.	02	05	.
XI	5.5	5.9	5.4	5.6	-	07.2	89	63	82	78	28	102	040.2	22	.	.	01	.	.	.	.	.	09	12	12	08	03	12	.	.	.	.	.	.	03	05	.
XII	5.8	5.6	4.4	5.3	-	04.9	82	59	79	73	22	136	026.6	25	.	.	16	.	.	.	05	.	10	12	12	12	07	10	03	.	.	.	.	.	.	02	04
GOD.	5.1	5.7	3.9	4.9	-	08.2	81	52	73	69	20	1220	058.5	5 III	.	01	51	101	43	03	23	.	94	99	123	104	47	121	12	06	.	.	.	06	32	15	-
ŠIBENIK																																				
BR. ST. 88																																				
H_a = 77 m H_b = 75.2 m h_a = 2,0 m h_b = 1,0 m																																				
I	7.1	6.3	4.9	6.1	106.9	05.9	71	62	70	68	28	136	035.1	14	.	.	03	.	.	.	14	03	02	11	16	12	05	16	.	.	.	.	.	.	03	01	.
II	6.6	6.2	5.3	6.0	129.6	04.6	62	52	60	58	24	059	011.7	12	.	.	05	.	.	.	17	04	05	09	12	09	02	12	02	01	.	.	01	01	02	.	02
III	6.2	6.3	5.6	6.0	171.3	05.2	65	52	60	59	17	127	055.2	05	.	.	03	.	.	.	17	07	06	14	13	08	04	13	.	.	.	.	01	.	03	.	.
IV	6.4	7.9	5.3	6.5	206.2	06.9	67	53	63	61	28	078	018.4	14	.	.	.	.	.	.	15	04	01	08	11	09	04	11	01	01	.	.	01	02	02	02	.
V	4.5	5.2	5.0	4.9	289.2	07.5	57	43	57	52	24	016	008.5	28	.	.	.	02	.	.	17	04	08	04	05	03	.	05	.	.	.	.	.	.	03	.	.
VI	4.0	4.8	4.7	4.5	317.1	11.9	63	49	62	58	24	050	013.5	03	.	.	.	22	04	08	08	.	05	04	12	10	02	11	.	.	.	.	.	.	06	01	.
VII	3.1	4.4	2.7	3.4	348.0	11.5	54	41	53	49	24	021	012.1	01	.	.	.	24	16	18	14	05	12	03	06	03	01	06	.	.	.	.	.	.	03	.	.
VIII	3.9	3.9	3.3	3.7	294.6	13.3	67	48	60	59	25	082	028.0	22	.	.	.	27	12	17	11	02	10	05	07	06	04	07	.	.	.	.	.	01	06	01	.
IX	2.8	2.7	1.3	2.3	291.2	10.0	55	41	56	51	24	004	003.2	01	.	.	.	21	02	05	08	02	14	02	02	01	.	02	.	.	.	.	.	.	01	.	.
X	3.7	3.6	2.4	3.3	250.2	08.3	68	51	69	63	26	048	018.9	02	.	.	.	01	.	.	12	02	13	04	05	05	02	05	.	.	.	.	.	.	03	02	.
XI	5.9	5.4	5.4	5.6	146.6	07.6	71	59	69	66	21	114	041.1	10	.	.	.	.	.	.	13	02	06	09	10	07	03	10	.	.	.	.	01	01	06	04	.
XII	5.9	5.3	4.3	5.2	133.3	05.2	66	55	62	61	22	076	019.9	25	.	.	05	.	.	.	16	02	09	08	14	12	02	13	03	.	.	01	.	.	04	01	03
GOD.	5.0	5.2	4.2	4.8	2684.2	08.2	63	50	61	58	17	811	055.2	5 III	.	.	16	97	34	48	162	37	91	81	113	85	29	111	06	02	.	01	04	05	42	12	05
KOMIŽA																																				
BR. ST. 89																																				
H_a = 6 m H_b = - m h_a = 2,0 m h_b = 1,0 m																																				
I	6.5	5.9	4.8	5.7	-	07.4	78	69	79	75	40	129	034.5	17	.	.	.	.	.	.	01	.	05	06	14	14	05	14	.	.	.	.	.	.	01	.	.
II	5.1	5.5	3.7	4.8	-	05.7	65	58	66	63	30	020	007.2	19	.	.	01	.	.	.	03	.	06	04	06	06	.	06	.	.	.	.	.	.	01	.	.
III	5.8	5.7	5.1	5.5	-	06.5	68	60	70	66	25	066	029.1	05	.	.	.	.	.	.	07	.	08	10	12	11	01	12	.	.	.	.	.	.	02	.	.
IV	5.1	4.8	3.7	4.6	-	07.7	67	58	66	64	28	031	010.9	09	.	.	.	.	.	.	04	.	07	04	07	05	01	07	.	.	.	.	.	.	02	.	.
V	4.4	3.1	3.9	3.8	-	09.0	64	54	66	61	29	017	007.2	07	.	.	.	.	.	.	01	.	08	03	03	03	.	03	.	.	.	.	.	.	.	.	.
VI	2.4	2.2	2.2	2.3	-	12.5	62	54	62	59	35	006	003.2	19	.	.	.	19	07	06	01	.	15	01	03	02	.	03	.	.	.	.	.	.	01	.	.
VII	2.4	1.5	1.8	1.9	-	13.6	62	53	62	59	33	014	011.2	02	.	.	.	25	10	10	.	.	21	.	02	02	01	02	.	.	.	.	.	.	01	.	.
VIII	2.5	1.8	1.9	2.1	-	14.7	63	55	66	61	40	028	012.2	22	.	.	.	28	14	17	.	.	16	01	04	04	01	04	.	.	.	.	.	.	02	.	.
IX	2.0	1.4	0.9	1.4	-	11.7	59	48	58	55	27	013	012.6	18	.	.	.	22	03	06	01	.	23	01	01	01	01	01	.	.	.	.	.	.	01	.	.
X	3.3	2.8	1.5	2.6	-	09.9	73	61	72	69	36	041	019.0	22	.	.	.	01	.	.	.	.	16	02	05	05	02	05	.	.	.	.	.	.	01	.	.
XI	4.5	5.2	3.7	4.5	-	08.9	75	65	74	71	39	067	042.1	17	.	.	.	.	.	.	02	.	11	05	06	06	02	06	.	.	.	.	.	.	01	.	.
XII	5.6	5.5	4.5	5.2	-	07.0	75	64	71	70	36	098	033.2	23	.	.	.	.	.	.	01	.	07	06	12	12	02	12	.	.	.	.	.	.	02	.	.
GOD.	4.1	3.8	3.1	3.7	-	09.6	67	58	67	64	25	530	042.1	17 XI	.	.	01	95	29	39	21	.	143	43	75	71	16	75	.	.	.	.	.	.	15	.	.
KAŠTEL STARI																																				
BR. ST. 90																																				
H_a = 24 m H_b = - m h_a = 2,0 m h_b = 1,0 m																																				
I	6.5	7.0	6.2	6.6	086.1	06.3	74	64	76	71	30	204	041.2	17	.	.	03	.	.	.	.	.	05	14	15	14	08	15	.	.	.	.	.	.	01	.	.
II	6.2	7.0	5.2	6.2	114.9	04.9	64	52	64	60	25	076	021.1	15	.	.	04	.	.	.	.	.	04	07	10	09	02	09	02	.	.	.	.	.	01	05	.
III	6.1	6.1	6.0	6.1	155.0	05.6	67	58	64	63	20	193	097.2	05	.	.	01	.	.	.	02	.	07	15	11	10	05	11	.	.	.	.	.	.	01	04	.
IV	7.0	6.5	5.1	6.2	177.1	07.3	71	54	67	64	26	168	062.2	09	.	.	.	.	.	.	.	.	02	10	11	11	07	11	.	.	.	.	.	.	02	02	.
V	5.3	5.5	4.9	5.2	251.9	07.8	60	42	58	53	25	019	006.2	12	.	.	.	01	.	.	.	.	06	06	06	05	.	06	.	.	.	.	.	.	04	.	.
VI	3.2	4.1	4.0	3.8	310.9	12.0	64	46	62	58	28	059	022.6	20	.	.	.	25	11	03	.	.	07	02	08	06	02	08	.	.	.	.	.	.	06	.	.
VII	2.8	3.3	2.3	2.8	336.2	12.2	59	41	56	52	26	037	016.5	02	.	.	.	26	19	06	01	.	19	03	06	05	02	06	.	.	.	.	.	.	02	.	.
VIII	3.6	4.0	2.4	3.3	296.1	13.3	67	46	60	58	29	233	144.5	31	.	.	.	28	19	06	.	.	14	05	05	05	04	05	.	.	.	.	.	.	06	.	.
IX	2.4	3.0	1.0	2.1	271.1	10.6	66	40	58	54	21	.	.	.	.	.	.	23	04	02	01	.	19	02	.	.	.	.	.	.	.	.	.	.	01	02	.
X	3.2	3.1	2.4	2.8	215.2	08.5	76	50	70	65	31	116	070.0	02	.	.	.	02	.	.	01	.	16	03	04	04	03	04	.	.	.	.	.	.	02	03	.
XI	5.8	5.6	5.6	5.7	125.9	07.9	78	67	72	71	29	108	030.4	22	.	.	.	.	.	.	.	.	08	12	10	08	04	10	.	.	.	.	.	.	03	02	.
XII	5.3	5.0	4.9	5.1	131.4	05.5	68	55	65	63	20	175	052.1	25	.	.	03	.	.	.	03	.	09	10	13	13	07	13	01	.	.	.	.	.	06	.	.
GOD.	4.8	5.0	4.2	4.7	2471.8	08.5	67	50	64	61	20	1388	144.5	31 VIII	.	.	11	107	53	17	08	.	116	89	99	90	44	98	03	.	.	.	.	02	42	09	.

[illegible]	[illegible]	Temperatura vazduha °C										Učestina pravaca i srednja jačina vetra nD, Fm (0-12)																							
		Tm										N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	f.	F.	f.	F.	f.	F.	f.	F.	f.	F.	f.	F.	f.	F.	f.	F.	f.	
SPLIT-MARJAN — φ = 43° 31' N λ = 16° 26' E Gr; Δ G = + 1h 06 min. — BR. ST. 91																																			
I	747.5	07.9	10.2	08.7	08.9	11.3	06.3	16.2	06	01.5	23	19	03.6	24	02.9	19	03.9	17	04.1	01	02.0	02	01.5	03	02.3	07	02.3	01	
II	749.9	05.6	09.0	06.8	07.0	10.1	04.4	16.0	10,06	-02.4	17	24	04.2	21	03.7	14	03.4	12	04.2	06	04.3	02	03.5	03	01.7	02	02.5	.	
III	746.7	07.5	10.8	09.0	09.1	11.9	06.7	16.0	26	-00.6	02	18	03.4	16	03.5	16	04.9	19	04.8	10	02.4	04	02.0	.	.	08	02.5	02	
IV	748.6	11.7	15.0	12.6	13.0	16.1	10.0	23.5	25	03.4	03	12	03.8	12	03.6	21	03.6	16	04.0	10	03.0	10	02.4	02	02.0	05	02.4	02	
V	749.5	15.3	19.5	15.9	16.7	20.4	13.2	24.7	21	07.4	02,01	25	03.5	12	03.1	13	03.9	15	03.6	11	02.5	08	03.1	04	02.2	04	02.2	01	
VI	750.5	21.7	26.1	22.3	23.1	27.3	19.3	32.6	27	12.6	03	11	03.4	18	02.6	15	02.5	07	04.0	12	02.4	19	02.4	02	02.0	04	02.5	02	
VII	748.6	23.4	28.2	24.3	25.1	29.0	21.0	34.6	12	15.0	05	14	03.7	20	02.6	12	02.6	06	04.2	15	02.3	11	02.5	09	01.6	05	02.2	01	
VIII	749.2	23.1	28.4	24.4	25.1	29.3	21.0	35.1	06	15.5	25	19	02.3	13	02.3	08	01.9	12	03.6	13	02.2	13	02.5	07	01.9	04	02.5	04	
IX	751.7	20.0	26.0	21.8	22.4	26.5	18.8	31.5	11	17.4	30,28	23	03.7	27	03.3	08	01.8	01	03.0	13	02.0	11	02.1	03	01.7	03	01.7	01	
X	752.4	13.6	18.5	15.3	15.7	19.0	12.7	24.3	13	06.7	25	19	03.7	21	03.5	05	03.4	07	03.9	14	02.4	08	02.0	04	02.2	07	01.7	08	
XI	751.7	11.7	14.7	13.0	13.1	15.4	10.5	18.5	02	06.8	17	16	02.9	18	02.7	14	04.4	15	04.1	09	02.0	03	01.7	05	01.6	08	02.1	02	
XII	752.2	08.3	10.6	08.8	09.1	11.5	06.6	15.9	01	00.8	24	22	03.8	27	03.6	09	04.0	09	04.4	11	02.8	04	01.8	04	02.2	03	01.7	04	
GOD.	749.5	14.2	18.1	15.2	15.7	19.0	12.5	35.1	6 VIII	-02.4	47 II	222	03.5	229	03.1	154	03.5	136	04.1	125	02.5	95	02.4	46	01.9	60	02.2	28	
HVAR — φ = 43° 10' N λ = 16° 27' E Gr. Δ G = + 1h 06 min. — BR. ST. 92																																			
I	756.5	09.3	12.1	09.8	10.3	13.0	06.9	17.1	06	01.2	20	21	01.8	07	01.4	29	02.7	14	03.9	01	02.0	02	02.0	01	02.0	10	01.9	08	
II	755.1	07.4	11.1	08.2	08.7	12.2	05.1	17.6	06	-02.3	17	21	01.9	16	01.9	21	03.0	12	03.4	03	05.0	02	03.0	01	02.0	05	02.6	03	
III	756.0	08.8	12.4	10.0	10.3	13.5	07.0	17.2	26	-00.4	02	17	01.9	11	02.5	16	03.8	21	03.5	05	04.2	05	03.8	.	.	12	02.7	06	
IV	757.8	12.7	15.5	12.8	13.4	16.6	10.3	21.6	25	04.3	04	07	02.2	06	02.2	15	03.3	27	02.7	03	01.7	.	.	07	02.3	11	02.9	07	
V	758.6	16.2	19.6	16.2	17.0	20.8	13.2	25.0	20	08.0	03,01	17	02.1	06	03.0	15	03.2	19	02.8	01	02.0	03	01.3	12	02.5	15	03.0	05	
VI	759.4	22.0	25.1	21.4	22.5	26.5	19.0	31.4	27	13.3	03	06	01.7	06	02.5	09	02.9	17	02.5	06	01.3	04	01.0	10	01.9	18	02.1	14	
VII	757.4	23.6	27.0	23.1	24.2	28.5	20.6	34.6	12	16.1	01	09	02.2	06	02.5	07	03.4	13	02.8	04	02.0	02	01.0	14	01.9	23	01.8	15	
VIII	757.8	24.0	27.8	23.8	24.9	29.0	21.3	32.6	08	17.0	10	12	01.9	01	02.0	05	03.2	16	02.0	04	01.2	03	01.0	13	02.5	22	01.9	17	
IX	760.6	21.5	26.5	21.6	22.8	27.7	18.8	31.8	12	12.0	30	12	01.5	19	02.1	08	01.5	09	01.9	04	01.0	06	01.2	12	02.2	08	01.5	12	
X	761.5	15.0	20.0	15.8	16.6	20.8	13.0	26.0	13	07.4	25	18	01.6	19	02.1	08	02.6	09	03.6	05	01.8	01	02.0	06	02.3	16	02.2	11	
XI	760.8	13.1	16.7	13.9	14.4	17.9	11.6	20.7	05	05.3	17	20	01.7	09	01.9	16	03.2	14	03.9	02	05.0	02	03.5	07	01.7	14	02.0	06	
XII	761.5	09.9	13.1	10.4	11.0	14.1	07.9	18.2	11	03.3	20	17	01.4	18	02.6	17	02.8	10	04.7	02	01.0	06	03.3	04	03.0	15	02.0	04	
GOD.	758.6	15.3	18.9	15.6	16.3	20.0	12.9	34.6	12 VII	-02.3	47 II	177	01.8	124	02.2	166	03.0	181	03.1	40	02.3	36	02.2	87	02.2	169	02.2	108	
SINJ — φ = 43° 42' N λ = 16° 41' E Gr. Δ G = + 1h 07 min. — BR. ST. 93																																			
I	-	04.2	07.9	04.8	05.4	09.3	01.7	16.0	06	-05.8	24	12	03.2	12	03.4	.	.	11	02.4	10	02.3	02	01.5	01	01.0	.	.	45	
II	-	02.2	06.3	03.2	03.7	07.7	00.2	15.4	06	-07.7	18	18	03.0	17	03.4	01	05.0	08	03.5	08	04.0	.	.	02	02.5	.	.	30	
III	-	04.2	09.3	05.7	06.3	10.9	02.4	19.4	26	-04.1	08	15	03.0	13	02.9	02	02.5	13	03.1	15	02.6	03	02.7	02	01.0	02	02.5	28	
IV	-	08.7	14.5	10.1	10.9	16.1	06.5	25.4	23	-00.6	05	10	03.2	06	04.2	.	.	15	02.7	15	02.6	05	03.0	01	02.0	02	02.5	36	
V	-	11.7	18.2	12.9	13.9	19.7	09.5	24.6	10	05.1	02	22	02.6	13	03.2	.	.	08	03.1	10	02.5	06	03.2	01	02.0	.	.	33	
VI	-	17.4	25.8	19.1	20.3	27.3	14.2	31.9	27	09.6	05	08	01.8	03	03.3	.	.	01	05.0	03	02.7	16	02.4	07	02.1	01	03.0	51	
VII	-	18.8	27.2	21.1	22.1	28.8	14.9	36.6	24	07.9	19	18	02.4	11	02.7	01	01.0	04	02.2	05	02.2	07	02.6	01	03.0	04	03.2	42	
VIII	-	18.0	27.3	20.8	21.7	28.9	15.1	36.9	07	10.4	28	07	01.4	03	02.3	.	.	04	02.2	04	01.8	10	02.4	07	02.0	03	02.0	55	
IX	-	14.2	25.7	17.0	18.5	26.6	11.6	32.4	12	01.4	30	14	03.2	19	02.8	01	02.0	05	01.4	03	01.3	07	01.7	.	.	01	02.0	40	
X	-	07.6	18.3	11.1	12.0	19.6	05.5	30.7	11	00.3	26	10	03.6	13	03.2	.	.	05	02.0	03	02.7	06	01.8	02	01.0	03	01.7	51	
XI	-	06.1	13.6	08.7	09.3	15.0	04.3	19.6	06	-02.6	26	10	02.5	06	03.3	.	.	09	02.9	04	03.8	03	02.0	.	.	05	02.6	53	
XII	-	02.7	08.4	03.7	04.6	09.9	00.0	16.2	11	-07.1	21	14	02.9	13	02.8	01	03.0	03	03.3	06	03.2	03	02.3	.	.	05	01.4	48	
GOD.	-	09.6	16.9	11.5	12.4	18.3	07.2	36.9	7 VIII	-07.7	48 II	158	02.8	129	03.1	06	02.7	86	02.7	86	02.7	68	02.4	24	01.9	26	02.3	512	
MAKARSKA — φ = 43° 18' N λ = 17° 01' E Gr. Δ G = + 1h 08 min. — BR. ST. 94																																			
I	-	08.3	11.5	08.9	09.4	12.8	06.3	18.1	06	00.1	23	07	03.4	11	02.1	15	02.1	26	02.5	14	02.6	02	01.0	03	02.3	01	02.0	14	
II	-	06.9	10.3	08.3	08.5	11.9	04.1	16.8	10	-00.4	17	18	04.9	14	02.5	09	01.3	22	02.7	13	02.5	06	02.5	01	04.0	01	03.0	.	
III	-	08.8	12.0	09.5	10.0	13.5	05.8	19.6	26	-00.6	07	15	05.4	08	02.4	05	01.0	21	02.8	18	02.3	08	02.0	01	02.0	07	02.1	10	
IV	-	13.0	15.4	12.8	13.5	17.3	09.2	23.8	26	04.4	15	11	04.8	14	03.4	02	01.0	22	02.5	07	02.0	17	01.9	02	01.5	05	02.4	10	
V	-	16.6	19.6	16.4	17.3	21.4	12.1	26.4	10	01.6	03	14	04.9	11	03.0	03	01.0	28	02.6	04	01.5	10	02.1	.	.	14	02.6	09	
VI	-	21.4	25.5	21.3	22.4	27.0	17.7	33.2	30	11.4	01	02	07.0	09	02.8	02	01.0	14	01.9	18	01.6	19	01.7	03	01.3	06	02.8	17	
VII	-	22.9	26.9	23.0	23.9	28.9	18.9	33.2	14	13.4	19	12	04.8	05	02.6	05	01.0	25	01.3	08	01.5	16	01.6	10	01.3	05	02.0	07	
VIII	-	23.3	27.7	23.8	24.6	28.9	19.5	33.4	20	15.3	25	05	03.2	09	01.8	06	01.5	16	02.4	09	02.2	12	01.7	14	01.6	08	01.8	14	
IX	-	20.6	26.2	20.8	22.1	27.5	16.6	33.4	12	09.3	30	03	06.0	11	02.9	10	01.5	23	01.6	07	01.6	11	01.6	03	02.0	10	02.6	12	
X	-	13.1	18.7	14.4	15.1	19.8	10.9	24.2	08	06.8	01	06	05.3	15	02.4	22	01.1	12	01.7	12	02.2	03	01.7	10	01.2	08	02.8	05	
XI	-	11.5	15.7	12.0	12.8	16.9	09.1	-	-	05.5	29,12	05	07.4	25	02.3	05	01.2	26	02.2	09	02.4	06	02.2	07	01.9	06	02.7	01	
XII	-	08.5	12.4	09.1	09.8	-	06.0	-	-	01.2	18	.	.	19	02.6	02	04.0	47	01.8	02	02.5	13	01.8	01	02.0	09	02.2	.	
GOD.	-	14.6	18.5	15.0	15.8	-	11.4	-		-00.6	7 III	98	05.0	151	02.6	86	01.4	282	02.2	121	02.1	123	01.8	55	01.6	80	02.4	99	
OPUZEN — φ = 43° 01' N λ = 17° 34' E Gr. Δ G = + 1h 10 min. — BR. ST. 95																																			
I	-	07.3	10.1	08.1	08.4	10.9	04.6	18.4	06	-01.6	26	02	02.0	16	02.4	07	02.3	57	02.1	09	02.6	02	03.0	.	.	.	.	.	
II	-	05.2	09.4	06.8	07.1	10.7	03.1	17.6	06	-05.2	18	23	03.8	09	03.1	08	02.8	41	02.5	03	02.3	.	.	.	.	.	.	.	
III	-	07.3	12.4	09.7	09.8	13.7	04.2	18.8	24	-02.9	01	03	04.0	10	03.4	03	02.3	44	03.2	09	03.8	09	03.0	14	02.8	01	03.0	.	
IV	-	11.8	16.3	12.8	13.5	17.6	08.1	25.0	25	01.9	06	04	04.5	06	03.3	07	02.7	34	03.1	08	03.6	07	02.4	22	02.6	02	03.0	.	
V	-	15.8	20.3	15.5	16.8	21.3	11.0	26.3	10	06.3	04	01	04.0	13	03.2	06	04.0	28	02.5	05	03.4	09	02.6	21	02.9	10	03.5	.	
VI	-	20.9	26.1	20.8	22.1	27.4	15.3	34.0	27	09.7	04	05	03.8	.	.	02	02.0	36	02.3	08	02.9	08	02.5	31	02.5	.	.	.	
VII	-	22.6	28.2	22.7	24.1	29.7	16.5	35.1	12	10.6	19	07	03.0	11	02.8	02	02.5	30	02.4	06	02.8	07	02.6	25	02.2	05	02.6	.	
VIII	-	21.8	28.5	22.6	23.9	29.8	16.8	35.8	07	11.6	25	.	.	02	03.0	02	02.5	40	02.4	02	02.5	07	02.4	38	02.3	02	02.0	.	
IX	-	18.8	27.1	19.6	21.3	28.1	14.8	33.8	11	08.8	26	06	03.2	19	03.0	07	02.3	23	02.3	03	02.0	03	02.0	29	02.3	.	.	.	
X	-	13.3	19.3	15.4	15.8	20.0	09.7	25.6	11	06.8	29	.	.	23	02.7	07	02.3	50	02.3	.	.	07	02.6	01	02.0	05	02.8	.	
XI	-	09.1	15.7	11.1	11.8	16.9	05.9	22.4	05	02.0	13	03	03.7	06	02.0	06	02.2	61	02.2	04	03.0	05	02.2	02	02.0	03	03.7	.	
XII	-	06.0	11.7	07.6	08.2	12.5	03.0	16.8	28	-01.5	21	03	02.3	13	02.3	07	02.0	62	02.2	04	02.0	02	03.0	01	03.0	01	03.0	.	
GOD.	-	13.3	18.8	14.4	15.2	19.9	09.4	35.8	7 VIII	-05.2	48 II	57	03.6	128	02.8	64	02.4	506	02.4	61	03.0	66	02.6	184	02.5	29	03.1	.	

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dišm)	Insolacija broj sati	Vlažnost vazduha p_m mm	U_m % 7	14	21	Sred. (Dišm)	min	Padavine R mm Σ	max	max.	Broj dana s: Tn ≤ -10,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F(0-12) ≥ 6	≥ 8	Nm(0-10) < 8,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	✱	△	≈	▲	▲	R T	■	■
SPLIT-MARJAN BR. ST. 91																																						
I	7.6	6.8	5.7	6.7	097.2	06.2	70	67	70	69	33	167	025.0	16	.	.	.	.	.	.	15	01	05	14	15	13	08	15	.	.	.	.	.	.	.	01	.
II	6.1	6.9	4.3	5.7	127.4	04.8	60	55	60	59	27	049	011.3	24	.	.	03	.	.	.	16	07	04	08	11	09	01	10	03	01	.	.	.	01	04	.	.
III	6.2	6.5	5.3	6.0	160.2	05.5	62	60	61	61	17	123	060.0	05	.	.	01	.	.	.	19	05	07	13	13	10	02	13	.	.	.	.	.	01	04	.	.
IV	7.5	7.1	4.0	6.2	194.5	07.2	66	57	64	62	26	103	032.6	09	.	.	.	.	.	.	16	05	01	07	13	09	04	13	.	.	.	.	01	01	02	01	.
V	5.4	5.8	4.6	5.3	270.8	07.8	56	47	56	53	25	014	006.6	12	.	.	.	.	.	.	10	.	05	07	07	04	.	07	.	.	.	.	.	.	04	.	.
VI	2.9	4.1	3.0	3.3	324.8	11.5	57	47	57	54	09	038	010.5	06	.	.	.	21	08	17	06	01	10	01	08	07	01	08	.	.	.	.	.	.	08	01	.
VII	2.8	3.7	2.1	2.9	343.6	12.0	54	44	52	50	24	050	040.8	02	.	.	.	25	16	22	12	01	17	03	07	05	01	07	.	.	.	.	.	.	04	.	.
VIII	3.7	4.3	2.4	3.5	297.4	13.3	59	49	58	55	33	076	045.7	22	.	.	.	26	18	21	04	01	13	06	07	06	02	07	.	.	.	.	.	.	10	.	.
IX	2.8	2.9	1.1	2.3	280.7	09.6	48	39	50	46	23	015	015.0	01	.	.	.	21	03	14	12	03	20	02	01	01	01	01	.	.	.	.	.	.	.	.	.
X	3.5	3.6	1.9	3.0	244.1	08.2	61	53	63	59	35	075	039.9	02	.	.	.	.	.	.	12	02	13	05	06	04	03	06	.	.	.	.	.	.	03	01	.
XI	6.2	6.3	5.3	5.9	139.7	07.8	70	65	68	68	29	113	034.5	10	.	.	.	.	.	.	13	03	06	12	10	07	04	10	.	.	.	.	.	02	04	.	.
XII	6.0	5.4	4.4	5.2	136.8	05.5	60	61	62	61	26	129	049.4	25	.	.	.	.	.	.	15	.	08	11	13	11	02	12	01	.	.	.	01	02	06	01	.
GOD.	5.1	5.3	3.7	4.7	2617.2	08.3	60	53	60	58	09	952	060.0	5 III	.	.	04	93	45	74	152	29	109	89	111	86	29	109	04	01	.	.	02	07	49	05	.
HVAR BR. ST. 92																																						
I	7.1	6.3	5.4	6.2	097.4	07.2	76	68	76	73	30	141	020.3	02	.	.	.	.	.	.	01	.	04	10	16	13	06	16	.	.	.	.	.	.	.	.	.
II	6.3	5.6	4.6	5.5	132.0	05.5	64	55	64	61	27	058	031.5	19	.	.	02	.	.	.	04	.	06	09	09	07	01	09	01	01	.	.	.	.	03	.	.
III	6.5	6.3	6.0	6.3	162.0	06.2	68	60	64	64	23	098	041.9	05	.	.	01	.	.	.	05	01	06	14	14	11	03	14	.	.	.	.	01	01	02	.	.
IV	6.0	6.1	4.2	5.4	217.6	07.9	70	61	69	66	26	064	015.3	06	.	.	.	.	.	.	02	.	02	04	12	10	03	12	.	.	.	.	01	.	03	03	.
V	5.1	3.9	4.5	4.5	297.9	08.7	61	52	62	59	28	016	005.1	28	.	.	.	01	.	.	.	.	07	04	05	04	.	05	.	.	.	.	.	.	02	.	.
VI	2.4	2.8	3.0	2.7	338.6	13.1	63	58	67	63	29	016	005.9	03	.	.	.	21	05	15	.	.	13	01	04	03	.	04	.	.	.	.	.	.	02	01	.
VII	2.7	1.9	2.0	2.2	369.6	14.1	63	55	63	60	28	022	020.0	02	.	.	.	28	11	22	.	.	19	01	03	02	01	03	.	.	.	.	.	.	01	.	.
VIII	3.3	2.3	2.0	2.5	326.0	15.4	66	58	68	64	27	021	008.0	24	.	.	.	29	15	23	.	.	18	02	05	04	.	05	.	.	.	.	.	.	06	.	.
IX	2.5	1.9	1.3	1.9	288.8	11.5	52	47	60	53	21	017	009.0	01	.	.	.	26	05	10	.	.	21	02	02	02	.	02	.	.	.	.	.	.	01	.	.
X	3.2	2.5	2.5	2.7	247.3	09.6	69	55	71	65	30	042	021.3	22	.	.	.	02	.	.	01	.	17	04	06	04	02	06	.	.	.	.	.	.	03	01	.
XI	5.6	5.4	4.2	5.0	140.2	08.7	75	62	71	69	35	058	021.2	16	.	.	.	.	.	.	06	.	06	07	09	06	03	09	.	.	.	.	.	.	02	.	.
XII	5.8	5.1	5.0	5.3	132.3	06.4	68	56	64	63	17	114	056.2	25	.	.	.	.	.	.	04	.	09	11	12	10	02	12	.	.	.	.	.	.	03	.	.
GOD.	4.7	4.2	3.7	4.2	2749.7	09.5	66	57	66	63	17	667	056.2	15 XII	.	.	03	107	36	70	23	01	128	69	97	76	21	97	01	01	.	.	02	01	28	05	.
SINJ BR. ST. 93																																						
I	7.0	6.8	6.1	6.7	083.3	05.6	80	72	82	79	69	245	053.8	17	.	.	13	.	.	.	01	.	05	14	16	15	07	16	.	.	.	.	.	.	.	03	.
II	5.7	6.6	5.8	6.0	109.6	04.4	72	63	73	69	31	134	033.4	16	.	.	14	.	.	.	01	.	04	10	12	10	06	10	03	.	.	.	.	.	03	02	08
III	5.4	5.9	5.5	5.6	144.6	05.3	79	63	74	70	20	173	044.5	05	.	.	09	.	.	.	02	.	09	11	12	10	08	12	02	.	.	.	.	.	03	.	.
IV	5.3	6.7	4.8	5.6	176.1	07.1	81	59	76	72	32	170	052.1	09	.	.	01	02	.	.	02	01	05	08	14	12	07	12	03	.	.	.	.	.	.	.	.
V	4.6	5.8	3.7	4.7	255.1	08.4	79	54	74	69	34	044	016.5	28	.	.	.	.	.	.	.	.	05	02	09	07	02	09	.	.	.	.	.	.	02	.	.
VI	2.9	4.6	3.6	3.7	293.5	12.9	84	52	79	72	33	038	007.2	26	.	.	.	23	08	.	.	.	08	01	11	11	.	11	.	.	.	.	.	.	06	.	.
VII	2.7	3.8	1.3	2.6	330.4	12.7	81	47	64	64	29	043	014.6	02	.	.	.	23	16	.	.	.	19	03	05	05	02	05	.	.	.	.	.	.	02	.	.
VIII	3.1	4.6	2.2	3.3	275.8	13.9	88	55	74	72	31	104	028.5	11	.	.	.	23	16	01	01	.	12	03	09	06	04	09	.	.	.	.	.	.	06	.	.
IX	2.0	2.8	0.8	1.8	277.8	10.6	80	45	69	65	29	003	002.6	01	.	.	.	20	05	.	01	.	20	01	02	01	.	02	.	.	.	.	.	.	.	07	.
X	3.3	3.3	2.2	2.9	218.6	08.1	89	59	79	76	38	129	079.0	02	.	.	.	05	01	.	01	.	15	04	06	04	04	06	.	.	.	.	.	.	02	10	.
XI	4.8	5.1	5.2	5.0	117.6	07.4	91	72	84	82	39	114	029.7	22	.	.	04	.	.	.	01	.	10	09	11	09	04	11	.	.	.	.	.	.	02	10	.
XII	5.1	4.6	4.5	4.7	113.8	05.4	86	73	84	81	40	189	045.4	26	.	.	16	.	.	.	01	.	11	10	13	12	05	11	04	02	.	.	.	01	04	01	05
GOD.	4.3	5.0	3.8	4.4	2396.2	08.5	82	59	76	72	20	1386	079.0	2 X	.	.	57	96	46	01	11	01	123	76	120	102	49	114	12	02	.	.	.	01	30	33	13
MAKARSKA BR. ST. 94																																						
I	5.9	5.8	6.3	6.0	-	07.5	87	75	83	82	36	214	036.2	17	.	.	.	.	.	.	02	.	03	10	16	14	10	16	.	.	.	.	.	.	.	.	.
II	5.0	4.4	4.6	4.7	-	05.9	74	63	70	69	27	089	031.4	16	.	.	01	.	.	.	05	02	05	03	10	10	03	10	01	.	.	.	.	01	01	.	.
III	5.4	5.0	4.9	5.1	-	06.1	73	57	62	64	29	237	103.5	05	.	.	01	.	.	.	04	02	10	11	11	11	06	11	.	.	.	.	.	03	02	.	.
IV	5.5	5.1	4.0	4.9	-	08.0	69	61	71	67	31	130	038.2	09	.	.	.	.	.	.	03	01	06	05	13	12	03	13	.	.	.	.	.	.	.	02	.
V	4.0	5.1	4.8	4.6	-	08.4	59	49	61	56	29	030	024.5	23	.	.	.	04	.	.	05	02	06	05	04	04	01	04	.	.	.	.	.	.	01	.	.
VI	2.8	3.4	1.9	2.7	-	13.1	70	52	67	63	29	048	019.1	06	.	.	.	23	05	05	02	.	13	01	04	04	02	04	.	.	.	.	.	.	.	01	.
VII	2.0	2.3	1.0	1.8	-	13.6	66	51	63	60	32	044	026.1	17	.	.	.	27	13	09	03	.	24	02	05	05	01	05	.	.	.	.	.	.	.	.	.
VIII	3.1	3.1	2.4	2.9	-	15.0	72	53	67	64	31	056	027.5	25	.	.	.	29	11	15	02	.	17	05	05	04	02	05	.	.	.	.	.	.	03	.	.
IX	2.2	2.3	1.2	1.9	-	11.4	66	44	60	57	17	007	004.0	01	.	.	.	24	06	04	06	01	19	.	02	02	.	02	.	.	.	.	.	.	01	.	.
X	2.6	3.6	2.1	2.8	-	09.6	83	60	78	74	34	132	071.0	02	.	.	.	.	.	.	02	02	19	05	05	05	03	05	.	.	.	.	.	01	01	01	.
XI	5.3	4.6	4.1	4.7	-	08.4	80	65	77	74	25	086	022.0	22	.	.	.	.	.	.	04	01	09	10	09	09	03	09	.	.	.	.	.	01	02	.	.
XII	6.4	5.0	4.6	5.3	-	06.3	73	60	71	68	19	178	054.1	26	.	.	.	.	.	.	01	.	09	11	13	11	05	13	.	.	.	.	.	01	03	.	.
GOD.	4.2	4.1	3.5	4.0	-	09.4	72	57	69	66	17	1251	103.5	5 III	.	.	02	.	.	33	39	11	140	68	97	91	39	97	01	.	.	.	.	07	14	04	.
OPUZEN BR. ST. 95																																						
I	7.5	7.9	8.5	8.0	-	06.8	80	74	82	79	41	283	039.7	13	.	.	03	.	.	.	.	.	.	19	18	15	11	18	.	.	.	.	.	.	.	.	.
II	6.6	5.8	6.6	6.3	-	05.4	73	62	73	69	17	096	023.6	01	.	.	04	.	.	.	03	.	03	09	11	09	04	11	01	.	01	.	.	.	05	.	.
III	6.4	5.7	6.4	6.2	-	06.2	72	62	69	68	28	182	054.8	05	.	.	03	.	.	.	06	.	09	15	13	12	06	13	.	.	.	.	.	.	01	.	.
IV	5.9	5.6	6.2	5.9	-	08.2	79	60	71	70	25	121	043.8	08	.	.	.	01	.	.	04	01	03	08	09	08	03	09	.	.	.	.	.	.	01	03	.
V	5.1	4.5	4.9	4.8	-	09.6	72	58	62	64	29	028	010.0	12	.	.	.	02	.	.	01	.	06	06	05	05	01	05	.	.	.	.	.	.	03	.	.
VI	2.4	2.7	2.4	2.5	-	12.4	70	52	61	61	26	042	025.4	07	.	.	.	23	07	01	.	.	11	01	05	02	02	05	.	.	.	.	.	.	02	01	.
VII	2.5	2.5	2.6	2.5	-	14.1	69	51	65	62	31	061	023.6	06	.	.	.	25	16	02	.	.	19	04	05	05	03	05	.	.	.	.	.	.	01	.	.
VIII	2.4	2.4	2.6	2.5	-	14.6	74	52	66	64	12	079	025.8	25	.	.	.	29	18	.	.	.	20	04	05	05	03	05	.	.	.	.	.	.	04	.	.
IX	1.2	1.2	1.2	1.2	-	12.1	72	48	67	62	34	002	001.8	01	.	.	.	25	11	.	.	.	24	.	01	01	.	01	.	.	.	.	.	.	01	.	.
X	2.8	2.8	2.9	2.8	-	08.8	72	58	65	65	37	041	017.6	23	.	.	.	01	.	.	.	.	15	04	03	03	02	03	.	.	.	.	.	.	02	02	.
XI	4.7	4.7	4.6	4.6	-	07.8	83	65	74	74	33	146	037.6	22	.	.	.	.	.	.	.	.	11	07	08	08	05	08	.	.	.	.	.	01	01	06	02	.
XII	5.0	4.1	4.5	4.5	-	05.8	80	59	67	69	30	189	040.0	28	.	.	06	.	.	.	.	.	12	09	11	11	07	11	.	.	.	.	.	.	02	.	.
GOD.	4.4	4.2	4.4	4.3	-	09.3	74	58	68	67	12	1270	054.8	5 III	.	.	16	106	52	03	14	01	133	86	94	84	47	94	01	.	01	.	01	01	28	08	.

H_s = 122 m H_b = 128.0 m h_s = 6.5 m h_r = 1.0 m

H_s = 20 m H_b = 25.4 m h_s = 2.0 m h_r = 1.2 m

H_s = 298 m H_b = 298.6 m h_s = 2.0 m h_r = 1.5 m

H_s = 6 m H_b = - m h_s = 2.0 m h_r = 1.0 m

H_s = 2 m H_b = - m h_s = 2.0 m h_r = 1.0 m

Mjesec	Vazdušni pritisak Fm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12): N n.	N j.	NE n.	NE j.	E n.	E j.	SE n.	SE j.	S n.	S j.	SW n.	SW j.	W n.	W j.	NW n.	NW j.	C n.
PALAGRUŽA $\varphi = 42^\circ 24'$ N $\lambda = 16^\circ 16'$ E Gr. $\Delta G =$ + 1h 05 min. BR. ST. 96																												
I	749.7	10.4	11.2	10.6	10.7	12.6	09.2	17.5	06	05.6	03	06	05.2	05	02.0	.	.	35	04.9	06	02.5	05	02.6	03	03.0	31	03.6	02
II	748.4	09.0	10.6	09.4	09.6	11.2	08.3	15.8	06	01.2	17	12	05.0	04	03.5	03	02.0	22	04.5	02	03.5	15	04.7	02	04.5	24	04.8	.
III	749.3	09.6	11.6	10.4	10.6	12.7	08.7	16.0	28	03.4	02	06	05.3	02	04.0	08	03.4	23	04.6	03	04.3	11	05.0	09	03.7	31	03.7	.
IV	751.2	12.4	15.0	12.7	13.2	15.8	11.2	20.3	27	04.8	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	752.0	15.4	18.0	15.2	16.0	18.6	13.9	21.5	16	09.8	03	03	05.0	02	03.0	04	03.8	19	04.7	01	01.0	07	02.9	07	02.7	48	04.0	02
VI	753.3	20.8	23.9	20.8	21.5	24.6	19.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	751.3	22.4	25.1	21.9	22.8	26.6	20.6	30.0	15	16.0	17	05	02.8	01	01.0	02	02.5	12	03.4	04	02.0	02	05.0	20	02.4	41	03.4	.
VIII	751.8	23.9	27.0	24.0	24.7	28.3	22.7	32.5	08,07	17.6	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	754.4	21.4	24.3	21.6	22.2	25.5	20.7	28.2	12	16.0	29	02	02.0	18	03.3	02	03.5	17	02.9	02	01.5	01	04.0	09	02.2	28	03.4	11
X	755.1	16.0	18.0	16.4	16.7	19.4	15.3	22.8	08	10.0	25	02	03.0	10	04.1	.	.	20	03.6	01	06.0	05	02.2	14	02.2	36	03.6	05
XI	754.3	13.8	15.4	14.3	14.4	16.6	13.1	18.6	09	07.2	16	04	04.8	02	04.5	02	03.0	30	03.8	03	03.0	05	03.4	12	03.4	26	03.7	06
XII	754.8	10.9	12.0	11.5	11.4	13.4	10.3	17.5	30	06.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	752.1	15.5	17.7	15.7	16.2	18.8	14.4	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VELA LUKA $\varphi = 42^\circ 58'$ N $\lambda = 16^\circ 43'$ E Gr. $\Delta G =$ + 1h 07 min. BR. ST. 97																												
I	-	07.7	11.7	08.2	09.0	12.7	05.2	18.0	06	-01.6	24,21	06	02.8	10	01.5	26	01.1	34	03.0	03	03.0	02	02.5	01	01.0	11	02.3	.
II	-	06.4	11.2	07.6	08.2	12.2	03.3	18.8	06	-04.2	18	20	02.8	04	01.0	15	01.3	28	02.5	02	04.5	02	04.0	01	03.0	12	02.8	.
III	-	07.9	12.4	09.3	09.7	13.3	05.3	17.3	24	-01.5	08	13	02.3	02	02.5	20	01.1	34	03.9	04	03.0	04	03.8	06	02.5	10	02.9	.
IV	-	12.3	15.9	12.0	13.0	17.1	08.6	23.7	25	01.8	05	13	02.8	01	02.0	15	01.1	36	03.1	03	02.3	01	01.0	06	02.7	15	02.5	.
V	-	15.9	19.6	15.6	16.7	20.6	11.6	24.8	21	03.8	01	15	02.5	01	01.0	10	01.5	28	03.3	02	01.5	.	.	07	03.0	21	02.9	09
VI	-	22.1	25.7	21.2	22.5	26.9	16.4	31.6	27	08.2	04	05	01.4	02	02.0	10	01.4	21	02.7	03	01.7	.	.	23	02.5	12	01.9	14
VII	-	23.7	27.4	22.9	24.2	28.9	18.1	33.5	14,12	14.1	17	12	02.8	03	02.3	16	01.1	20	03.0	02	01.5	.	.	22	02.5	06	01.7	12
VIII	-	23.0	27.9	23.3	24.4	29.0	19.3	35.0	07	14.0	28	05	02.2	01	01.0	20	01.0	15	03.0	04	01.5	01	01.0	20	02.6	16	02.5	11
IX	-	19.6	26.3	20.5	21.7	27.4	15.6	33.8	11	07.2	30	09	01.9	03	02.0	32	01.2	14	01.7	03	02.0	01	02.0	17	02.6	07	02.6	04
X	-	13.4	19.2	14.9	15.6	20.5	10.2	27.0	10	04.6	24	09	02.7	06	02.3	26	01.1	22	02.7	.	.	.	.	07	02.9	20	02.7	03
XI	-	10.9	16.3	11.6	12.6	17.6	07.6	19.4	04,03	03.2	27,26	03	03.0	02	02.0	22	01.0	31	03.0	.	.	04	02.5	06	02.2	16	02.2	06
XII	-	07.0	12.8	08.5	09.2	13.8	04.1	17.2	11,01	-01.8	20,18	04	01.2	04	01.5	21	01.1	35	01.9	06	02.2	03	02.7	05	02.4	15	01.9	.
GOD.	-	14.2	18.9	14.6	15.6	20.0	10.4	35.0	7 VIII	-04.2	18 II	114	02.5	39	01.8	233	01.1	318	02.9	32	02.3	18	02.8	121	02.6	161	02.5	59
LASTOVO $\varphi = 42^\circ 46'$ N $\lambda = 16^\circ 54'$ E Gr. $\Delta G =$ + 1h 08 min. BR. ST. 98																												
I	741.8	09.1	10.0	09.3	09.4	11.3	07.6	17.0	06	02.3	20	06	02.5	11	02.0	08	01.6	35	04.0	07	03.7	04	03.8	01	05.0	17	01.7	04
II	740.4	07.3	09.3	07.8	08.1	10.6	05.7	15.8	06	-01.7	17	12	02.2	11	03.0	06	02.3	19	03.0	10	03.0	07	02.6	01	03.0	11	02.9	07
III	741.3	08.3	10.5	08.9	09.2	11.8	06.6	15.2	28	00.3	02	06	02.5	07	02.6	07	02.3	33	04.2	07	03.9	07	03.1	01	03.0	18	02.6	07
IV	743.3	11.3	14.1	11.7	12.2	15.5	09.5	20.5	25	03.7	03	04	02.5	05	02.6	.	.	34	03.1	08	03.1	03	03.3	03	02.3	23	02.8	10
V	744.0	14.6	17.8	14.7	15.4	18.7	12.3	22.3	22	04.5	03	09	02.4	04	03.0	05	02.4	28	03.1	01	03.0	01	02.0	.	.	34	02.6	11
VI	745.3	21.0	24.1	20.4	21.5	25.4	18.4	30.0	29	12.5	06	.	.	04	02.5	10	02.2	20	02.2	03	01.3	01	01.0	.	.	36	01.8	16
VII	743.4	23.2	26.0	22.5	23.5	27.6	20.0	32.0	12	13.8	16	04	03.2	08	02.1	02	01.0	21	02.9	03	02.3	01	01.0	03	01.3	37	02.0	14
VIII	743.8	23.0	26.6	23.3	24.1	28.0	20.9	33.3	07	16.6	24	05	02.4	04	01.2	01	01.0	19	02.4	.	.	02	01.0	01	01.0	47	02.0	14
IX	746.4	20.6	24.3	20.8	21.6	25.2	19.1	31.4	11	14.0	29	02	02.0	21	02.5	04	01.8	19	01.5	01	01.0	01	01.0	.	.	31	01.6	11
X	746.9	14.9	17.3	15.5	15.8	18.4	13.8	23.2	13	07.5	25	08	02.5	08	03.0	06	02.8	19	02.5	03	02.7	03	02.3	01	02.0	37	01.9	08
XI	746.2	13.0	14.6	13.2	13.5	15.7	11.6	19.5	09	06.3	16	06	03.7	10	02.6	01	01.0	29	02.9	06	04.0	02	02.5	01	03.0	29	01.8	06
XII	746.7	09.7	11.0	10.2	10.3	12.0	08.4	16.0	30,01	03.5	23	10	01.6	14	03.6	05	01.4	23	03.7	03	03.7	07	03.7	03	03.3	23	02.0	05
GOD.	744.1	14.7	17.1	14.9	15.4	18.4	12.8	33.3	7 VIII	-01.7	17 II	72	02.4	107	02.6	55	02.0	299	03.1	52	03.2	39	02.8	15	02.5	343	02.1	113
KORČULA $\varphi = 42^\circ 57'$ N $\lambda = 17^\circ 08'$ E Gr. $\Delta G =$ + 1h 12 min. BR. ST. 99																												
I	-	09.7	11.6	09.9	10.2	12.4	07.5	16.8	08	02.4	21,20	02	01.5	05	01.8	26	02.5	22	02.1	10	01.8	19	01.8	04	02.0	05	02.0	.
II	-	07.8	10.4	08.2	08.6	11.2	05.4	16.4	10,06	-01.8	18	07	03.0	09	03.3	16	03.1	19	02.4	07	02.0	07	02.0	05	02.0	14	01.9	.
III	-	09.1	11.8	09.7	10.1	12.9	06.8	16.2	14	-01.8	02	07	02.7	07	02.3	29	03.2	16	02.9	04	02.0	12	02.0	12	02.1	06	02.0	.
IV	-	12.7	15.2	12.5	13.2	16.2	10.0	21.0	27	03.6	04	03	03.3	03	03.0	26	03.2	29	02.9	02	01.0	04	02.0	12	02.5	11	02.3	.
V	-	16.4	19.6	15.9	16.9	20.6	13.2	26.2	21	07.4	03	04	02.5	05	03.2	29	02.8	21	02.4	.	.	05	02.4	16	02.7	13	02.3	.
VI	-	22.4	25.4	21.5	22.7	26.3	18.6	31.8	27	12.2	04	03	02.7	07	03.7	23	02.5	15	01.9	04	01.5	10	01.9	19	02.1	09	01.9	.
VII	-	24.1	27.3	23.1	24.4	28.6	20.0	34.8	13	14.0	16	05	02.6	04	02.2	26	02.5	08	01.8	02	01.5	06	01.8	35	01.8	07	01.9	.
VIII	-	24.7	27.8	23.8	25.0	29.1	21.1	33.3	06	17.0	24	06	01.2	03	01.3	19	02.1	06	02.0	06	01.5	08	01.6	34	01.5	11	01.5	.
IX	-	22.0	26.1	21.4	22.7	27.0	18.5	31.0	12	12.2	30	02	01.0	09	03.2	32	02.3	16	01.2	04	01.0	02	01.0	21	01.6	04	01.5	.
X	-	15.4	19.2	15.9	16.6	20.1	13.1	25.0	13	07.0	25	02	01.5	05	02.4	30	02.5	06	01.7	08	01.1	06	01.3	31	01.7	05	01.4	.
XI	-	13.1	16.3	13.5	14.1	17.1	11.1	19.6	04	06.4	17	04	02.8	.	.	24	02.6	21	01.7	06	02.2	04	01.5	28	01.5	03	01.3	.
XII	-	09.7	12.3	10.3	10.7	13.5	07.8	17.4	02	04.0	24	.	.	02	01.5	32	03.1	09	02.3	08	02.0	17	01.9	20	01.8	05	02.2	.
GOD.	-	15.6	18.6	15.5	16.3	19.6	12.8	34.8	15 VIII	-01.8	18 II	45	02.4	59	02.5	312	02.7	188	02.2	61	01.7	100	01.8	237	01.8	93	01.9	.
OREBIĆ $\varphi = 42^\circ 58'$ N $\lambda = 17^\circ 10'$ E Gr. $\Delta G =$ + 1h 09 min. BR. ST. 100																												
I	-	09.3	11.9	09.5	10.0	12.6	07.0	17.0	06	00.6	21	19	02.0	17	02.1	11	02.3	26	03.2	.	.	05	02.6	05	02.6	08	01.6	02
II	-	07.2	10.7	07.7	08.3	11.8	04.4	17.5	06	-01.5	18	23	02.2	21	02.7	03	03.0	21	03.2	01	05.0	.	.	06	03.2	09	01.7	.
III	-	09.5	12.2	09.2	10.0	13.2	06.6	16.6	24	00.5	08	13	02.1	22	02.2	07	03.4	26	03.1	.	.	08	03.4	06	03.2	10	01.9	01
IV	-	13.3	15.2	12.0	13.1	16.3	09.3	21.3	18	02.8	05	13	01.7	15	02.7	09	02.8	23	02.7	03	01.7	11	02.6	06	03.2	04	02.0	06
V	-	16.3	19.5	15.6	16.8	20.3	12.8	24.3	21	05.1	01	16	02.2	20	02.5	09	02.7	20	02.2	01	01.0	10	03.3	15	02.9	02	01.5	.
VI	-	22.4	24.7	20.5	22.0	25.9	17.3	31.0	27,26	10.6	05,04	15	01.6	16	02.4	06	01.7	25	02.2	03	01.3	09	02.8	07	02.4	06	01.2	03
VII	-	24.3	27.2	21.9	23.8	28.3	19.3	35.2	12	14.7	19	12	02.2	17	02.8	06	02.7	24	02.2	02	02.5	08	03.0	14	02.3	07	01.7	03
VIII	-	24.4	27.7	23.0	24.5	28.7	19.7	33.1	06	16.4	25	13	01.2	12	02.4	04	02.8	23	02.2	02	01.0	11	02.6	16	02.2	08	01.8	04
IX	-	20.9	26.0	20.0	21.7	26.9	17.1	29.6	12,11	09.0	30	15	01.4	31	03.0	01	02.0	16	02.1	03	01.7	05	02.2	06	02.8	07	01.3	06
X	-	14.8	19.4	14.6	15.8	20.2	11.7	25.7	13	06.9	25	15	02.1	26	03.1	04	01.8	18	02.8	02	03.0	05	03.0	12	02.3	07	01.6	04
XI	-	12.8	16.6	12.6	13.6	17.5	10.3	19.5	05,02	06.0	26,12	27	01.9	13	02.5	03	02.7	23	02.8	05	02.8	05	02.8	07	02.9	07	01.6	.
XII	-	08.9	13.1	09.4	10.2	13.8	06.4	17.5	02	01.2	18	19	01.6	28	03.4	03	02.7	15	03.5	03	02.0	07	03.1	10	02.5	06	02.0	02
GOD.	-	15.3	18.7	14.7	15.8	19.6	11.8	35.2	18 VII	-01.7	18 II	200	01.9	238	02.7	66	02.6	260	02.7	25	02.1	84	02.9	110	02.6	81	01.7	31

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Mjes.)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Mjes.)	Min	Padavine R mm Σ	Max	Broj dana n sa: Tn ≤ 10.0	Tn ≤ 0.0	Tn ≤ 0.0	Tx ≥ 25.0	Tx ≥ 30.0	Tn ≥ 20.0	F (0-12) ≥ 6	≥ 8	Nm (0-10) ≤ 8.0	≥ 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	✱	✱	△	≈	▲	▲	⊤	≡	▦
BR. ST. 96 — PALAGRUŽA — H_a = 98 m H_b = 81.9 m h_v = 2.0 m h_r = 1.5 m																																					
I	7.3	6.8	3.9	6.0	105.1	07.7	77	78	80	78	51	016	005.4	05	.	.	.	.	.	.	11	01	03	04	05	04	.	05	.	.	.	.	.	.	.	.	.
II	6.7	6.8	5.5	6.3	136.4	06.4	68	67	73	69	39	000	000.1	20	.	.	.	.	.	.	13	07	.	03	01	.	.	01	.	.	.	.	.	.	.	.	.
III	6.5	6.1	4.7	5.8	-	07.0	73	69	72	72	36	007	002.5	15	.	.	.	.	.	.	13	03	06	11	05	03	.	05	.	.	.	.	.	.	.	.	.
IV	5.5	6.3	3.7	5.2	221.2	08.5	74	67	78	73	-	008	003.5	08	.	.	.	.	.	.	11	02	-	-	03	03	.	03	.	.	.	.	.	.	.	.	.
V	5.4	3.9	3.4	4.3	269.0	10.2	75	64	81	73	40	009	004.0	17	.	.	.	.	.	.	12	02	09	03	06	03	.	06	.	.	.	.	.	.	01	01	.
VI	2.9	2.5	2.6	2.7	323.1	14.9	80	67	80	75	-	003	002.0	20	-	-	-	-	-	-	03	.	-	-	02	02	.	02	.	.	.	.	.	.	05	.	.
VII	2.3	1.8	1.4	1.8	350.5	15.6	76	64	79	73	18	000	000.4	17	.	.	.	25	01	21	05	.	19	.	01	.	.	01	.	.	.	.	.	.	02	02	.
VIII	2.2	1.6	1.5	1.8	-	17.2	77	64	77	73	46	009	009.0	31	.	.	.	28	09	28	01	.	-	-	02	01	.	02	.	.	.	.	.	.	01	.	.
IX	2.1	1.5	1.3	1.6	275.6	14.7	75	62	76	71	38	001	000.5	01	.	.	.	21	.	21	04	.	22	02	03	.	.	03	.	.	.	.	.	.	.	.	.
X	4.2	4.0	3.7	3.9	222.7	11.0	77	71	79	76	46	001	000.3	02	.	.	.	.	.	.	08	.	11	04	03	.	.	03	.	.	.	.	.	.	02	.	.
XI	4.6	4.3	3.9	4.2	161.2	09.5	77	74	77	76	47	022	013.7	17	.	.	.	.	.	.	09	03	08	04	04	03	01	04	.	.	.	.	.	01	01	.	.
XII	6.8	7.0	4.0	6.1	106.0	07.5	75	71	72	73	38	034	007.5	23	.	.	.	.	.	.	11	01	-	-	08	08	.	08	.	.	.	.	.	.	03	.	.
GOD.	4.7	4.4	3.3	4.1	-	10.8	75	68	77	73	-	110	013.7	44 XI	-	-	-	-	-	-	99	19	-	-	43	27	01	43	.	.	.	.	.	01	01	15	03	.
BR. ST. 97 — VELA LUKA — H_a = 30 m H_b = - m h_v = 2.0 m h_r = 1.0 m																																					
I	8.4	7.3	7.0	7.6	-	07.1	85	69	82	79	34	164	026.4	07	.	.	04	.	.	.	.	.	04	16	15	15	06	15	.	.	.	.	.	.	01	.	.
II	7.8	6.7	5.7	6.7	-	05.4	69	51	70	63	25	062	025.3	19	.	.	05	.	.	.	.	.	03	13	10	07	02	10	.	.	.	.	.	.	02	.	.
III	6.3	5.9	5.6	5.9	-	06.1	73	56	67	65	22	110	046.3	05	.	.	04	.	.	.	07	01	07	12	13	11	03	13	.	.	.	.	.	.	02	.	.
IV	6.5	6.4	5.2	6.0	-	07.6	73	53	70	65	28	082	015.3	06	.	.	.	.	.	.	02	.	03	09	11	08	03	11	.	.	.	.	.	.	04	.	.
V	5.4	4.2	5.1	4.9	-	08.3	61	47	63	57	24	010	003.7	07	.	.	.	.	.	.	01	.	09	09	04	03	.	04	.	.	.	.	.	.	01	.	.
VI	2.5	3.0	3.1	2.8	-	12.2	62	48	65	58	33	010	005.6	06	.	.	.	23	06	01	01	.	13	02	04	02	.	04	.	.	.	.	.	.	01	.	.
VII	2.8	2.5	2.1	2.5	-	12.9	59	47	62	56	23	017	008.7	02	.	.	.	27	12	06	01	.	16	01	03	03	.	03	.	.	.	.	.	.	02	.	.
VIII	3.4	2.8	2.2	2.8	-	14.6	71	50	68	63	28	037	017.8	24	.	.	.	29	13	11	.	.	16	02	04	03	02	04	.	.	.	.	.	.	05	.	.
IX	2.3	2.2	1.6	2.0	-	11.1	64	42	62	56	16	039	031.8	18	.	.	.	23	07	02	.	.	19	02	02	02	01	02	.	.	.	.	.	.	01	.	.
X	3.5	3.6	3.1	3.4	-	09.2	74	56	74	68	31	048	015.2	23	.	.	.	03	.	.	.	.	15	05	06	06	03	06	.	.	.	.	.	.	02	04	.
XI	6.2	6.0	5.2	5.8	-	08.2	79	60	80	73	23	036	009.3	15	.	.	.	.	.	.	02	.	07	10	09	06	.	09	.	.	.	.	.	.	01	03	.
XII	5.5	5.2	5.4	5.4	-	05.9	77	52	69	66	15	073	020.5	25	.	.	06	.	.	.	.	.	09	11	10	09	02	10	.	.	.	.	.	.	02	.	.
GOD.	5.0	4.6	4.3	4.6	-	09.0	70	52	69	64	15	688	046.3	5 III	.	.	19	105	38	20	14	01	121	92	91	75	22	91	.	.	.	.	.	.	24	07	.
BR. ST. 98 — LASTOVO — H_a = 186 m H_b = 186.7 m h_v = 2.0 m h_r = 1.0 m																																					
I	7.7	7.0	5.7	6.8	089.1	07.3	82	78	80	80	42	115	028.7	07	.	.	.	.	.	.	06	.	02	11	15	11	03	15	.	.	.	.	01	.	01	.	.
II	6.3	5.8	4.5	5.5	126.8	05.6	68	63	68	66	39	035	012.9	01	.	.	01	.	.	.	05	.	03	06	08	06	01	08	.	.	.	.	01	01	04	.	.
III	6.2	5.8	5.2	5.7	165.6	06.2	70	66	69	68	28	086	037.0	05	.	.	.	.	.	.	05	01	08	11	10	07	02	10	.	.	.	.	.	.	02	.	.
IV	4.8	5.0	3.9	4.6	223.4	07.9	77	64	73	72	36	055	020.7	06	.	.	.	.	.	.	05	.	06	04	09	08	02	09	02	.	.	.	.	.	05	02	.
V	5.4	3.4	3.9	4.2	301.5	09.0	71	60	70	67	35	014	005.0	12	.	.	.	.	.	.	04	01	10	06	05	04	.	05	.	.	.	.	.	.	03	.	.
VI	2.1	2.1	2.6	2.3	343.6	12.9	68	58	71	66	33	010	003.8	06	.	.	.	18	01	14	.	.	18	.	06	03	.	06	.	.	.	.	.	.	03	.	.
VII	3.2	2.1	1.5	2.3	359.6	13.7	65	56	66	62	26	026	015.1	17	.	.	.	26	09	17	.	.	17	01	04	03	01	04	.	.	.	.	.	.	01	.	.
VIII	2.9	2.0	1.7	2.2	326.1	15.0	75	57	68	66	37	007	003.0	31	.	.	.	28	07	22	.	.	18	02	05	03	.	05	.	.	.	.	.	.	05	.	.
IX	2.1	1.9	1.5	1.8	293.8	12.2	63	54	67	61	26	048	031.8	18	.	.	.	17	01	18	.	.	21	02	03	02	02	03	.	.	.	.	.	.	01	.	.
X	3.1	3.1	2.7	3.0	231.2	10.0	74	67	75	72	39	030	011.3	23	.	.	.	01	.	.	03	.	17	03	07	04	01	05	.	.	.	.	.	.	04	.	.
XI	4.7	5.1	3.8	4.5	147.8	08.8	75	71	77	74	39	028	011.4	17	.	.	.	.	.	.	06	.	08	07	07	04	01	07	.	.	.	.	01	.	03	.	.
XII	5.3	5.0	4.2	4.8	123.4	06.6	72	66	69	69	33	069	024.5	23	.	.	.	.	.	.	09	.	08	07	13	09	02	13	.	.	.	.	01	.	04	.	.
GOD.	4.5	4.0	3.4	4.0	2731.9	09.6	71	63	71	68	26	523	037.0	5 III	.	.	01	90	18	71	43	02	136	60	92	64	15	90	02	.	.	.	04	01	36	02	.
BR. ST. 99 — KORČULA — H_a = 20 m H_b = - m h_v = 2.0 m h_r = 1.0 m																																					
I	7.9	6.8	6.7	7.2	-	07.3	78	69	77	75	38	249	067.6	31	.	.	.	.	.	.	.	.	01	15	21	16	10	21	01	.	.	.	.	.	01	.	.
II	7.0	5.9	5.1	6.0	-	05.8	66	62	69	66	28	108	033.8	24	.	.	01	.	.	.	.	.	02	07	10	08	03	10	02	01	.	.	.	.	03	.	.
III	6.2	6.2	5.9	6.1	-	06.4	70	63	69	67	28	147	068.8	05	.	.	01	.	.	.	02	.	06	14	14	13	04	14	.	.	.	.	02	.	03	.	.
IV	6.0	5.9	4.0	5.3	-	08.4	76	63	76	72	33	101	033.2	08	.	.	.	.	.	.	.	.	02	07	12	09	03	12	.	.	01	.	.	.	04	03	.
V	5.5	5.1	4.3	4.9	-	09.0	64	52	67	61	27	018	005.2	23	.	.	.	03	.	.	.	.	06	08	07	05	.	07	.	.	.	.	.	.	01	.	.
VI	2.3	3.3	2.6	2.7	-	13.2	63	54	67	62	28	011	005.4	06	.	.	.	22	03	12	.	.	13	02	04	03	.	04	.	.	.	.	.	.	01	.	.
VII	3.5	2.6	1.9	2.7	-	14.0	63	52	64	60	32	038	020.7	17	.	.	.	26	12	21	.	.	16	01	05	03	02	05	.	.	.	.	.	.	02	.	.
VIII	3.1	2.5	1.4	2.3	-	15.3	65	57	66	63	31	027	012.0	25	.	.	.	30	11	23	.	.	18	02	05	05	01	05	.	.	.	.	01	.	05	.	.
IX	1.6	2.0	1.0	1.5	-	11.7	55	46	62	54	19	014	013.5	18	.	.	.	24	02	09	02	.	19	.	01	01	01	01	.	.	.	.	.	.	01	.	.
X	3.0	3.7	2.3	3.0	-	09.8	71	59	73	68	38	065	028.4	02	.	.	.	01	.	.	.	.	15	04	05	05	02	05	.	.	01	.	.	.	03	.	.
XI	5.9	5.0	3.9	4.9	-	09.0	76	64	77	73	29	084	020.4	10	.	.	.	.	.	.	01	.	09	10	09	07	04	09	.	.	01	.	.	.	05	.	.
XII	5.1	4.9	4.0	4.7	-	06.6	72	60	70	67	25	090	015.4	28	.	.	.	.	.	.	02	.	08	08	11	10	05	11	.	.	.	.	.	02	02	.	.
GOD.	4.8	4.5	3.6	4.3	-	09.7	68	58	69	65	19	952	068.8	5 III	.	.	02	106	28	65	07	.	115	78	104	85	35	104	03	01	03	.	03	02	31	03	.
BR. ST. 100 — OREBIĆ — H_a = 6 m H_b = - m h_v = 2.0 m h_r = 1.0 m																																					
I	7.9	6.8	7.2	7.3	-	07.4	78	73	77	76	37	240	032.5	07	.	.	.	.	.	.	.	.	01	16	20	16	10	20	.	.	.	.	.	.	01	01	.
II	7.1	5.8	6.1	6.3	-	05.8	67	61	69	66	30	165	044.1	01	.	.	02	.	.	.	01	.	01	10	11	09	05	11	01	.	01	.	01	01	01	.	.
III	6.0	5.8	5.5	5.8	-	06.4	66	64	68	66	23	170	086.2	05	.	.	.	.	.	.	01	.	08	11	15	12	03	15	.	.	.	.	.	.	01	.	.
IV	5.3	5.5	5.1	5.3	-	08.3	71	65	75	70	36	096	034.6	08	.	.	.	.	.	.	.	.	07	06	10	08	03	10	.	.	.	.	.	.	03	01	.
V	5.2	4.3	4.7	4.8	-	08.9	61	56	63	60	31	016	004.6	12	.	.	.	.	.	.	.	.	10	06	09	05	.	09	.	.	.	.	.	.	01	.	.
VI	2.0	2.7	2.7	2.5	-	12.7	59	59	68	62	30	046	032.1	19	.	.	.	20	02	04	.	.	16	01	04	03	01	04	.	.	.	.	.	.	01	03	.
VII	3.3	2.8	1.6	2.6	-	13.4	57	53	66	59	30	036	017.9	17	.	.	.	27	13	13	.	.	18	01	04	03	02	04	.	.	.	.	.	.	02	.	.
VIII	3.0	2.5	1.8	2.4	-	14.7	62	58	66	62	30	036	019.4	22	.	.	.	30	11	14	.	.	18	02	05	04	01	05	.	.	.	.	.	.	05	.	.
IX	1.4	1.8	1.0	1.4	-	11.0	56	45	60	54	12	006	006.1	18	.	.	.	24	.	03	.	.	23	01	01	01	.	01	.	.	.	.	.	.	01	.	.
X	3.2	3.8	3.3	3.4	-	09.1	68	56	72	65	33	069	031.5	02	.	.	.	01	.	.	01	.	14	03	07	06	02	07	.	.	.	.	.	.	03	.	.
XI	6.0	5.0	5.2	5.4	-	08.6	74	63	76	71	27	096	039.7	10	.	.	.	.	.	.	.	.	08	11	07	07	03	07	.	.	.	.	01	01	02	.	.
XII	5.2	4.8	5.2	5.0	-	06.4	68	61	67	65	20	144	053.9	26	.	.	.	.	.	.	01	.	07	09	11	09	05	11	.	.	.	.	02	.	03	.	.
GOD.	4.6	4.3	4.1	4.4	-	09.4	65	59	68	64	17	1120	086.2	5 III	.	.	02	102	26	54	04	.	131	77	104	83	35	104	01	.	01	.	04	03	26	02	.

Mjesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												d.	j.	d.	j.	d.	j.	d.	j.	d.	j.	d.	j.		j.	d.	j.	d.
φ = 42° 50' N λ = 17° 42' E Gr. Δ G = + 1h 11 min.																												STON BR. ST. 101
I	-	08.2	10.9	08.7	09.1	12.4	05.7	16.2	06	-00.6	22	16	01.4	06	01.5	01	01.0	28	02.9	07	02.3	.	.	04	01.5	16	01.6	15
II	-	05.8	10.0	07.6	07.7	11.6	03.1	15.6	10	-05.0	18	03	01.0	18	01.6	01	05.0	20	03.5	07	04.1	.	.	.	.	22	02.0	13
III	-	08.5	12.2	09.0	09.7	13.6	04.9	18.2	26	-01.2	02	04	02.0	11	02.4	.	.	26	03.5	16	02.8	05	02.0	.	.	18	01.6	13
IV	-	11.5	15.4	11.9	12.7	16.7	07.4	21.5	18	-01.5	05	03	02.0	09	02.0	03	01.7	34	02.8	07	03.6	.	.	04	01.5	09	02.3	21
V	-	15.4	19.8	15.2	16.4	20.8	11.2	25.5	10	07.2	15	04	02.5	05	02.6	01	02.0	17	02.5	13	01.4	04	01.2	02	02.0	19	02.0	28
VI	-	21.2	25.3	20.2	21.8	26.6	15.9	32.4	26	08.4	05	06	02.0	15	01.4	01	01.0	14	02.1	08	02.0	01	02.0	.	.	15	01.4	30
VII	-	23.2	27.5	22.3	23.8	28.9	18.1	35.0	11	11.5	19	01	02.0	08	01.4	.	.	15	02.5	10	01.6	01	02.0	02	01.0	29	02.2	27
VIII	-	22.9	28.1	22.6	24.0	29.3	18.3	35.2	06	13.6	25	03	01.0	08	01.1	01	01.0	17	02.5	08	01.5	04	01.5	.	.	17	01.5	35
IX	-	18.8	26.0	18.5	20.5	27.2	15.1	30.8	14	06.5	30	06	01.3	10	01.7	.	.	11	01.5	03	01.3	02	01.5	03	01.3	23	02.2	32
X	-	12.0	18.9	12.9	14.2	20.3	09.2	25.5	13	03.7	26	08	02.1	05	01.6	.	.	10	02.3	12	01.5	.	.	01	02.0	21	02.0	36
XI	-	10.5	16.0	11.0	12.1	17.0	07.2	19.6	03	00.6	12	07	01.3	12	01.5	.	.	21	02.8	06	02.5	.	.	01	01.0	17	01.9	26
XII	-	07.6	12.1	07.8	08.9	13.5	03.8	17.6	02	-02.2	18	07	01.1	14	01.4	.	.	16	03.6	06	02.3	04	01.5	02	01.0	20	01.8	24
GOD.	-	13.8	18.5	14.0	15.1	19.8	10.0	35.2	6 VIII	-05.0	18 II	68	01.6	121	01.6	08	01.9	229	02.8	103	02.2	21	01.6	19	01.4	226	01.9	300
φ = 42° 39' N λ = 18° 06' E Gr. Δ G = + 1h 12 min.																												DUBROVNIK BR. ST. 102
I	-	09.5	11.6	10.1	10.3	12.4	08.1	16.0	06	03.2	20	14	01.9	09	02.8	10	02.8	26	03.3	08	04.0	.	.	01	03.0	05	01.6	20
II	-	07.5	10.5	08.9	09.0	11.8	05.8	16.0	10,05	-01.0	18	16	02.9	05	03.0	03	02.7	10	03.9	15	04.4	02	04.0	01	01.0	05	03.0	27
III	-	09.7	12.5	10.3	10.7	13.5	07.6	18.0	26,14	01.0	02	15	03.1	10	02.8	07	01.6	12	03.1	22	02.9	05	02.8	03	01.3	04	02.2	15
IV	-	12.8	15.2	13.1	13.6	16.2	10.4	20.5	21	05.0	06,03	09	02.6	04	03.0	04	02.2	28	02.8	15	02.5	04	01.2	03	01.3	06	03.0	17
V	-	16.1	18.9	16.4	16.9	19.9	13.4	24.0	21,10	08.0	03	09	02.2	03	03.7	01	02.0	18	01.6	14	01.4	03	01.3	.	.	15	01.9	30
VI	-	22.1	24.2	21.4	22.3	25.5	18.4	30.2	26	12.0	06	05	02.2	08	02.4	.	.	13	01.5	05	01.2	03	01.0	02	01.0	01	02.0	51
VII	-	24.3	26.0	23.8	24.5	28.1	20.9	33.0	14,13	16.0	17	05	03.4	14	03.2	04	01.0	13	02.4	03	01.7	01	01.0	04	01.8	05	03.0	44
VIII	-	24.1	27.0	24.1	24.8	28.0	21.4	30.5	20	15.2	24	01	02.0	01	01.0	.	.	22	02.9	02	02.5	11	01.5	06	02.8	07	01.9	43
IX	-	21.3	25.4	21.4	22.4	26.0	19.1	29.0	18	13.5	30,29	18	03.0	14	04.5	03	01.0	02	02.5	07	01.0	08	01.1	05	02.2	01	04.0	40
X	-	15.2	19.4	16.2	16.7	20.2	13.6	24.0	10,09	07.5	25	18	03.2	12	03.0	.	.	10	03.6	07	02.1	02	01.0	04	02.0	04	01.0	36
XI	-	13.2	16.0	13.5	14.1	17.0	11.5	19.5	15	08.0	16	08	02.1	06	03.8	09	03.1	21	03.0	08	01.5	09	03.0	04	01.5	05	01.8	20
XII	-	09.8	13.1	10.5	11.0	13.9	08.6	17.1	02	04.0	18	07	04.3	30	04.3	.	.	19	04.3	03	04.3	13	03.4	03	03.0	14	02.7	04
GOD.	-	15.5	18.3	15.8	16.4	19.4	13.2	33.0	4,5 VIII	-01.0	18 II	117	02.6	116	03.5	41	02.3	194	02.9	109	02.6	61	02.2	36	02.0	72	02.3	349
SR BOSNA I HERCEGOVINA																												BOSANSKI NOVI BR. ST. 103
φ = 45° 03' N λ = 16° 23' E Gr. Δ G = + 1h 06 min.																												
I	-	-01.3	01.3	-00.6	-00.3	02.2	-03.0	14.0	05	-09.2	21	07	01.4	11	02.0	03	01.3	02	01.5	06	02.2	.	.	01	02.0	08	02.1	51
II	-	-00.3	05.1	01.1	01.8	06.2	-02.5	15.5	09	-10.6	20	07	02.4	16	02.2	07	01.6	04	01.8	11	03.1	03	04.0	.	.	01	01.0	33
III	-	01.3	08.7	04.5	04.8	09.7	00.5	20.5	24	-07.2	08	05	01.6	06	01.7	03	01.0	01	02.0	18	02.7	12	01.8	04	01.8	06	02.7	58
IV	-	06.5	14.9	09.8	10.3	16.3	04.5	26.5	19	-02.2	04	11	01.4	04	01.8	06	02.0	01	01.0	15	02.5	15	02.2	03	01.3	05	02.6	30
V	-	09.3	18.2	12.2	13.0	19.4	07.4	25.0	15,14	-01.0	01	04	02.2	04	01.2	03	01.0	08	01.2	15	01.7	07	01.3	02	01.0	06	02.0	44
VI	-	15.4	25.3	17.8	19.1	26.2	13.3	32.0	17	06.0	05	.	.	.	.	.	.	09	01.3	05	01.4	02	02.0	01	02.0	01	01.0	72
VII	-	15.5	25.3	17.5	18.9	26.1	13.7	31.5	22	08.8	20	06	02.0	02	01.5	.	.	04	01.0	02	01.0	05	02.0	03	01.0	02	01.0	69
VIII	-	16.5	26.1	18.7	20.0	26.7	-	35.0	07	-	-	04	01.5	16	02.0	04	02.0	06	01.5	01	01.0	12	01.6	01	05.0	02	01.5	47
IX	-	11.5	22.8	13.2	15.2	23.1	-	33.0	11	-	-	01	03.0	20	02.0	01	02.0	04	01.8	02	01.0	07	01.4	.	.	03	01.7	52
X	-	05.8	15.8	08.4	09.6	16.5	-	28.0	08	-	-	04	01.8	16	01.3	06	02.0	01	03.0	01	06.0	04	02.0	03	02.0	05	01.6	53
XI	-	05.3	13.5	07.5	08.5	14.0	-	22.0	04,03	-	-	02	02.0	05	01.2	02	01.0	05	01.2	05	02.0	14	02.2	02	01.5	.	.	55
XII	-	-01.1	03.0	00.0	00.5	03.7	-	16.5	01	-	-	05	01.0	07	01.3	04	01.2	03	01.0	02	01.0	04	01.0	.	.	02	02.0	66
GOD.	-	07.0	15.0	09.2	10.1	15.8	-	35.0	4 VIII	-		56	01.7	107	01.8	39	01.6	48	01.4	83	02.3	85	01.9	20	01.7	41	01.9	614
φ = 45° 11' N λ = 16° 49' E Gr. Δ G = + 1h 07 min.																												BOSANSKA DUBICA BR. ST. 104
I	752.3	-01.5	00.9	-01.0	-00.6	02.0	-03.8	12.5	05	-12.8	21	07	01.6	11	01.2	37	01.5	03	01.0	01	02.0	02	02.0	02	02.0	02	01.5	28
II	-	-00.6	03.4	00.9	01.2	05.6	-03.6	14.9	09	-15.5	20	12	02.1	04	01.2	25	01.4	08	01.4	05	01.6	07	02.7	05	01.8	03	02.3	15
III	-	01.9	08.7	04.6	04.9	09.6	00.1	21.5	24	-10.0	08	06	01.8	06	01.3	25	01.6	07	01.4	08	02.0	09	02.6	07	01.9	03	01.3	27
IV	-	07.6	15.1	09.7	10.6	16.3	04.5	26.5	19	-01.9	05	23	02.0	15	01.7	09	01.8	06	01.7	06	01.8	06	02.3	06	02.8	10	02.7	09
V	-	12.1	17.9	12.1	13.6	19.0	07.4	25.0	14	-02.4	01	39	01.3	29	01.2	.	.	.	.	.	.	.	.	.	.	20	01.4	05
VI	-	18.6	25.1	17.9	19.9	25.7	13.0	31.3	23	05.4	03	13	01.1	16	01.1	27	01.1	03	01.3	07	01.9	05	01.6	03	01.3	12	01.8	04
VII	-	18.2	24.9	18.2	19.9	25.9	13.3	32.0	15	08.4	27	07	01.3	24	01.2	32	01.2	04	02.0	03	01.0	08	01.9	02	01.5	12	01.8	01
VIII	-	17.9	25.8	19.2	20.5	26.5	14.7	33.8	07	08.6	27	04	01.0	24	01.4	28	01.2	18	01.4	02	01.0	07	01.7	02	01.5	08	01.8	.
IX	-	12.2	21.8	13.5	15.2	22.8	09.3	34.0	11	00.0	30	03	01.0	34	01.5	33	01.0	04	02.0	.	.	03	01.7	.	.	13	01.8	.
X	-	05.6	14.9	08.4	09.3	16.5	03.3	26.5	08	-01.2	25	.	.	39	01.3	36	01.0	01	02.0	01	01.0	08	01.9	.	.	08	02.0	.
XI	-	05.8	12.6	08.0	08.6	14.1	03.2	22.0	03	-03.2	12	01	02.0	26	01.5	27	01.0	16	01.8	02	01.5	12	01.9	.	.	06	02.0	.
XII	-	00.0	03.2	-00.2	00.7	05.3	-02.9	18.5	01	-10.8	27	08	01.2	28	01.8	34	01.0	08	01.9	.	.	04	02.0	01	01.0	08	01.9	02
GOD.	-	08.2	14.5	09.3	10.3	15.8	04.9	34.0	4,5 IX	-15.5	10 II	123	01.5	256	01.4	313	01.2	78	01.6	35	01.7	71	02.1	28	01.9	105	01.8	86
φ = 45° 00' N λ = 17° 55' E Gr. Δ G = + 1h 12 min.																												DERVENTA BR. ST. 105
I	-	-02.4	00.9	-01.7	-01.2	01.6	-04.7	08.0	05	-14.6	21	.	.	02	01.0	.	.	.	.	.	.	.	.	01	04.0	.	.	90
II	-	-01.2	04.4	-00.3	00.7	05.4	-03.7	15.2	09	-13.0	05	.	.	04	01.0	04	01.5	.	.	.	.	02	01.0	02	02.0	01	01.0	71
III	-	02.4	09.6	05.1	05.6	10.6	00.4	22.8	24	-10.0	02	01	02.0	06	01.3	06	02.5	.	.	01	02.0	01	03.0	09	01.2	01	01.0	68
IV	-	07.8	16.0	10.1	11.0	17.0	04.9	28.6	20	-02.8	05	01	01.0	02	01.0	04	01.2	.	.	.	.	03	01.0	13	01.3	04	02.0	63
V	-	11.8	18.4	12.7	13.9	19.8	08.0	26.8	10	-00.6	01	01	02.0	01	01.0	02	01.0	01	01.0	.	.	02	02.0	13	01.2	04	01.2	69
VI	-	18.0	25.5	18.4	20.1	26.0	13.4	30.6	23	05.4	03	01	01.0	01	01.0	02	01.0	02	01.0	.	.	.	.	09	01.1	01	01.0	74
VII	-	18.2	25.3	18.8	20.3	26.2	13.8	33.2	15	09.8	20	.	.	02	01.0	.	.	03	01.0	.	.	01	01.0	05	01.0	02	01.5	80
VIII	-	18.1	26.3	19.1	20.7	26.9	14.7	34.6	07	10.0	28,26	.	.	01	01.0	03	01.0	.	.	01	01.0	.	.	07	01.1	02	01.0	79
IX	-	12.6	22.5	14.1	15.8	22.9	10.0	33.6	11	-01.0	30	.	.	02	01.0	04	01.5	.	.	.	.	.	.	.	.	01	01.0	83
X	-	05.9	16.2	08.9	10.0	17.0	03.8	25.6	09	-01.6	20	.	.	05	01.0	01	01.0	01	01.0	.	.	.	.	03	01.3	02	01.0	81
XI	-	04.7	13.0	07.0	08.0	14.0	03.0	21.0	19	-01.8	07	.	.	.	.	02	02.0	01	02.0	.	.	.	.	04	01.2	02	01.5	81
XII	-	-01.3	03.1	-00.6	00.1	03.7	-03.6	17.4	01	-14.4	27	.	.	01	01.0	05	01.8	.	.	.	.	.	.	05	01.0	.	.	82
GOD.	-	07.9	15.1	09.3	10.4	15.9	05.0	34.6	4 VIII	-14.6	14 I	04	01.5	27	01.1	33	01.6	08	01.1	02	01.5	09	01.4	71	01.2	20	01.3	921

Mesec	Oblačnost Nm (0-10) 7	14	21	Srednji (Dnevni)	Insolacija broj sati	Vlažnost vazduha e mm	Um % 7	14	21	Srednji (Dnevni)	Min	Padavine R mm Σ	I	II	Broj dana n sa: Tn ≤ -20,0	Tn ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 10,0	Tn ≥ 20,0	F(0-12) ≥ 6	F(0-12) ≥ 8	Nm(0-10) < 8.0	Nm(0-10) > 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	✱	≡	△	∽	▲	▲	T	≡	▦
BR. ST. 101						STON																																
I	7.8	7.6	7.1	7.5	-	07.1	80	73	78	77	27	262	039.4	02	.	.	02	.	.	.	02	.	02	16	20	18	12	20	.	.	.	.	01	.	03	.	.
II	6.6	6.2	6.0	6.3	-	05.5	70	60	68	66	26	103	045.6	01	.	.	08	.	.	.	05	.	04	11	10	09	03	09	01	.	.	.	.	.	04	.	.
III	6.7	5.9	5.8	6.1	-	06.0	68	56	70	64	26	181	068.4	05	.	.	05	.	.	.	06	01	07	15	12	12	06	12	.	.	.	.	.	02	03	.	.
IV	5.9	5.7	4.4	5.4	-	08.0	78	61	73	70	31	161	055.6	08	.	.	01	.	.	.	02	01	05	07	09	08	05	09	.	.	.	.	.	.	04	02	.
V	5.5	4.6	3.8	4.6	-	08.7	66	50	67	61	27	043	016.2	23	.	.	.	01	.	.	.	.	09	05	06	06	01	06	.	.	.	.	.	.	02	.	.
VI	2.5	3.3	2.1	2.7	-	12.7	65	55	71	63	30	029	009.8	06	.	.	.	21	04	02	.	.	15	01	05	04	.	05	.	.	.	.	.	.	02	.	.
VII	2.8	2.5	1.3	2.2	-	12.8	59	48	64	57	26	024	014.4	17	.	.	.	24	16	12	.	.	22	03	05	04	01	05	.	.	.	.	.	.	03	.	.
VIII	3.2	2.5	1.2	2.3	-	14.6	71	53	69	64	29	096	041.6	31	.	.	.	29	14	07	.	.	22	03	04	04	03	04	.	.	.	.	.	.	07	.	.
IX	1.9	2.0	1.2	1.7	-	10.8	62	44	67	58	16	.	.	.	.	.	.	24	02	09	.	.	21	.	.	.	.	.	.	.	.	.	.	.	01	.	.
X	3.2	3.9	2.3	3.1	-	08.9	78	58	77	71	35	102	074.8	02	.	.	.	03	.	.	.	.	18	03	05	05	02	05	.	.	.	.	.	.	02	02	.
XI	5.2	5.1	4.1	4.8	-	08.2	80	65	80	75	30	112	049.6	10	.	.	.	.	.	.	01	.	10	08	10	09	04	10	.	.	.	.	.	.	05	01	.
XII	5.2	4.1	4.1	4.5	-	06.0	72	59	71	68	30	160	048.2	28	.	.	05	.	.	.	02	01	11	08	09	09	04	09	.	.	.	.	.	02	04	.	.
GOD.	4.7	4.4	3.6	4.3	-	09.1	70	56	71	66	16	1273	074.8	8 X	.	.	21	102	36	26	18	03	146	80	95	88	41	94	01	.	.	.	01	04	40	05	.
BR. ST. 102						DUBROVNIK																																
I	8.5	7.7	7.5	7.9	074.6	07.2	75	71	75	73	30	217	037.3	17	.	.	.	.	.	.	03	.	01	17	17	17	09	17	.	.	.	.	.	.	01	.	.
II	7.8	6.8	6.1	6.9	117.0	06.0	64	64	69	66	31	070	022.4	01	.	.	01	.	.	.	06	.	01	15	14	09	01	14	.	.	.	.	.	.	.	.	.
III	7.0	5.1	5.0	5.7	165.2	06.5	62	65	69	65	33	182	043.1	05	.	.	.	.	.	.	05	.	08	11	14	13	05	14	.	.	.	.	.	.	01	.	.
IV	6.2	5.8	5.6	5.9	194.7	08.1	69	65	70	68	32	186	067.7	08	.	.	.	.	.	.	02	.	04	09	13	12	05	13	.	.	.	.	.	.	01	.	.
V	4.6	5.0	4.4	4.7	269.5	09.6	65	65	66	66	26	056	025.1	23	.	.	.	.	.	.	.	.	10	06	09	07	03	09	.	.	.	.	.	.	.	.	.
VI	3.1	3.8	2.4	3.1	329.8	13.9	65	66	70	67	16	021	008.4	19	.	.	.	22	02	11	.	.	14	01	05	03	.	05	.	.	.	.	.	.	.	.	.
VII	3.0	3.1	1.6	2.6	337.2	12.6	53	51	60	55	28	032	019.5	06	.	.	.	27	13	20	02	.	17	03	06	03	02	06	.	.	.	.	.	.	.	.	.
VIII	3.1	3.8	1.5	2.8	323.7	16.5	67	67	73	69	35	064	026.5	25	.	.	.	30	04	24	.	.	15	03	05	05	02	05	.	.	.	.	.	.	02	.	.
IX	1.9	2.7	0.9	1.8	-	12.4	54	59	63	58	28	.	.	.	.	.	.	23	.	17	.	.	17	01	.	.	.	.	.	.	.	.	.	.	.	.	.
X	3.6	4.3	2.0	3.3	224.5	09.4	62	62	67	64	26	111	056.7	02	.	.	.	.	.	.	02	.	16	05	05	05	03	05	.	.	.	.	.	.	.	.	.
XI	6.2	5.8	4.4	5.5	152.5	08.7	70	67	74	70	28	075	016.6	15	.	.	.	.	.	.	04	.	08	11	10	09	03	10	.	.	.	.	.	.	.	.	.
XII	5.6	5.3	3.7	4.9	142.9	06.5	65	61	65	64	31	150	056.1	28	.	.	.	.	.	.	11	.	09	07	11	08	04	11	.	.	.	.	.	.	.	.	.
GOD.	5.0	4.9	3.8	4.6	-	09.8	64	63	68	65	16	1164	067.7	8 IV	.	.	01	102	19	72	35	.	120	89	109	91	37	109	.	.	.	.	.	.	05	.	.
BR. ST. 103						BOSANSKI NOVI																																SR BOSNA I HERCEGOVINA
I	9.0	9.3	7.8	8.7	-	03.4	79	67	75	74	49	128	038.2	17	.	10	28	.	.	.	.	.	.	22	14	13	04	09	06	.	.	.	.	.	.	10	31
II	8.1	7.2	5.9	7.1	-	03.8	70	62	74	69	31	087	015.6	11	.	01	19	.	.	.	02	01	02	12	12	12	03	07	07	.	.	.	.	.	.	08	18
III	8.4	7.3	4.8	6.8	-	04.4	74	57	71	67	24	116	022.6	28	.	.	12	.	.	.	03	.	02	11	15	10	05	13	07	01	.	.	.	.	01	08	08
IV	7.9	7.7	4.4	6.6	-	06.6	75	56	73	68	26	068	014.8	29	.	.	04	06	.	.	01	.	.	09	15	09	02	15	01	01	.	.	.	.	.	04	.
V	8.2	7.2	4.2	6.5	-	07.6	80	48	77	68	14	054	020.6	23	.	.	01	02	.	.	.	.	.	07	12	09	02	12	01	01	.	.	.	.	02	06	.
VI	6.5	6.6	4.8	6.0	-	11.6	81	48	79	69	21	170	048.2	19	.	.	.	22	04	.	.	.	02	10	11	09	05	11	.	.	.	.	.	.	07	09	.
VII	6.3	4.3	3.5	4.7	-	11.0	82	45	78	68	17	146	046.2	01	.	.	.	21	09	.	.	.	08	06	09	08	04	09	.	.	.	.	.	.	01	09	.
VIII	2.4	4.1	3.5	3.3	-	13.9	93	54	91	79	36	136	055.8	11	-	.	-	19	09	-	.	.	15	04	11	11	03	11	.	.	.	.	.	.	07	15	.
IX	8.5	3.8	2.6	5.0	-	10.6	97	51	94	81	35	022	006.8	17	-	.	-	12	04	-	.	.	03	04	07	05	.	07	.	.	.	.	.	.	01	17	.
X	5.3	5.2	4.7	5.1	-	07.5	95	60	92	82	33	072	023.6	02	-	.	-	03	.	-	01	.	09	09	10	07	03	10	.	.	.	.	.	.	.	20	.
XI	8.8	6.4	5.9	7.0	-	06.8	91	65	87	81	36	049	011.5	22	-	.	-	.	.	-	01	.	.	13	09	09	02	09	.	.	.	.	.	.	01	12	.
XII	9.3	8.1	7.9	8.4	-	04.3	93	81	91	88	40	073	012.6	26	-	07	-	.	.	-	.	.	.	23	11	10	04	05	08	02	.	.	.	.	.	26	10
GOD.	7.4	6.4	5.0	6.3	-	07.6	84	57	81	74	14	1121	055.8	44 VIII	-	18	-	85	26	-	08	01	41	130	136	112	37	118	30	05	.	.	.	.	20	144	67
BR. ST. 104						BOSANSKA DUBICA																																
I	9.8	8.5	8.8	9.0	-	04.0	93	84	91	90	62	112	034.0	17	03	11	27	.	.	.	.	.	.	26	15	12	03	10	07	.	.	.	.	.	.	08	30
II	7.8	7.9	5.7	7.1	-	04.1	87	71	87	82	41	117	030.1	12	03	04	23	.	.	.	01	.	01	12	19	13	04	11	11	01	.	.	.	.	.	02	15
III	6.8	7.7	6.5	7.0	-	05.0	86	61	82	77	25	115	026.3	07	01	.	15	.	.	.	.	.	02	16	16	11	04	12	09	01	.	.	.	.	01	02	-
IV	5.9	6.1	6.2	6.1	-	06.6	81	53	76	69	29	075	014.0	29	.	.	06	04	.	.	.	.	.	05	16	14	03	16	01	01	.	.	.	.	.	.	.
V	5.5	4.8	7.8	6.0	-	08.7	79	57	85	74	35	057	017.8	23	.	.	02	01	.	.	.	.	.	02	14	11	02	14	.	.	.	.	.	.	.	.	.
VI	3.8	4.0	8.7	5.5	-	13.7	82	58	88	76	17	111	060.6	19	.	.	.	21	03	.	.	.	.	01	12	07	03	12	.	.	.	.	.	01	08	01	.
VII	4.1	4.0	7.9	5.3	-	13.9	82	60	91	77	41	153	036.9	10	.	.	.	20	06	.	.	.	.	.	09	08	06	09	.	.	.	.	.	.	03	03	.
VIII	5.1	4.4	5.8	5.1	-	15.2	91	66	89	82	42	077	026.9	11	.	.	.	22	04	.	.	.	02	06	10	08	03	.	.	.	.	.	.	.	03	02	.
IX	5.5	4.2	3.4	4.4	-	11.2	93	63	93	83	33	026	008.1	17	.	.	.	11	03	.	.	.	03	.	04	04	.	04	.	.	.	.	.	.	.	06	.
X	6.6	6.1	5.1	5.9	-	08.0	95	72	93	87	34	070	030.0	02	.	.	06	02	.	.	.	.	.	06	07	07	02	07	.	.	.	.	.	.	.	04	.
XI	6.7	6.0	7.2	6.6	-	07.0	90	70	88	82	13	054	012.6	22	.	.	03	.	.	.	.	.	.	05	10	10	01	10	.	.	.	.	.	.	.	02	.
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	03	01	26	.	.	.	.	.	-	-	-	-	-	-	-	-	.	.	.	.	.	02	.
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	10	16	108	81	16	.	01	.	-	-	-	-	-	-	-	-	.	.	.	01	15	-	-
BR. ST. 105						DERVENTA																																
I	9.5	7.6	8.2	8.4	-	03.9	94	86	93	91	68	115	034.7	17	05	10	26	.	.	.	.	.	.	20	14	12	03	09	10	01	.	01	.	01	.	07	-
II	7.5	7.2	6.3	7.2	-	04.5	94	82	93	90	53	131	017.6	12	03	03	21	.	.	.	.	.	02	14	18	16	06	09	13	03	.	.	.	.	.	01	24
III	7.0	6.8	6.9	6.9	-	05.7	92	67	88	82	32	114	032.4	28	01	.	11	.	.	.	.	.	03	15	16	15	04	12	08	01	.	.	.	.	.	02	06
IV	5.8	6.7	5.3	5.9	-	07.5	87	56	85	76	27	076	017.3	29	.	.	04	05	.	.	01	.	02	08	14	13	02	14	.	.	.	.	.	.	.	.	.
V	5.3	6.9	7.6	6.6	-	09.4	86	61	87	78	31	093	019.0	28	.	.	01	05	.	.	01	.	01	08	16	14	02	16	.	.	.	.	.	.	01	01	.
VI	5.5	5.1	4.6	5.1	-	14.1	86	59	90	78	39	181	033.9	18	.	.	.	21	02	.	03	.	05	04	14	12	06	14	.	.	.	.	.	.	01	06	01	.
VII	3.6	4.5	4.2	4.1	-	13.9	86	58	89	78	37	051	021.4	17	.	.	.	21	10	.	.	.	14	09	10	08	01	10	.	.	.	.	.	.	.	.	.
VIII	4.7	3.7	4.1	4.2	-	14.7	90	59	90	80	43	074	017.6	23	.	.	.	22	08	.	.	.	10	05	10	09	03	10	.	.	.	.	.	.	03	04	.
IX	5.8	4.1	4.4	4.8	-	11.5	92	60	94	82	42	102	037.4	17	.	.	01	11	03	.	.	.	07	06	05	05	03	05	.	.	.	.	.	.	01	05	.
X	6.1	4.8	3.8	4.9	-	08.1	95	68	93	85	38	069	031.0	02	.	.	03	02	.	.	.	.	08	08	08	07	02	08	.	.	.	.	.	.	.	08	.
XI	6.2	5.6	6.1	5.9	-	07.2	95	73	93	87	49	052	008.4	09	.	.	05	.	.	.	.	.	05	11	12	11	.	12	.	.	.	.	.	.	.	01	.
XII	7.7	7.8	6.9	7.5	-	04.4	94	82	93	90	47	060	014.2	23	03	05	26	.	.	.	.	.	04	17	13	11	02	07	06	.	.	.	.	.	.	13	10
GOD.	6.2	5.9	5.7	6.0	-	08.7	90	67	90	83	27	1118	037.4	43 IX	12	18	98	87	23	.	05	.	61	125	150	133	34	126	37	05	.	01	.	02	11	43	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dim)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dim)	min	Padavine R mm Σ	Max	Dat.	Broj dana s: Tn ≤ -10,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	✱	△	∽	▲	▲	R T	≡	▦
BIHAĆ — φ = 44° 49' N λ = 15° 53' E Gr. Δ G = + 1h 04 min. — BR. ST. 106																																					
I	738.5	01.1	02.6	01.6	01.8	04.9	-01.5	15.6	05	-11.0	03	05	01.2	03	01.7	07	01.7	11	03.6	16	02.8	10	02.1	07	01.9	18	01.6	16
II	735.8	01.7	04.9	02.1	02.7	07.2	-01.9	15.8	09	-13.6	20	03	01.3	03	01.0	04	02.2	08	03.5	09	04.0	24	02.7	17	02.9	08	02.2	08
III	736.8	02.0	07.9	04.6	04.8	09.0	00.2	19.8	24	-10.6	08	05	01.6	.	.	08	04.0	20	03.0	13	02.7	16	02.7	12	01.5	06	01.8	13
IV	738.3	07.9	14.2	10.4	10.7	16.2	05.2	27.4	23	-03.4	04	02	02.0	02	03.0	06	02.8	12	02.8	16	03.1	22	02.6	15	02.8	12	02.0	03
V	739.8	10.5	17.3	12.4	13.1	18.8	07.5	26.8	10	-02.4	01	04	02.0	04	01.8	05	02.0	18	02.0	13	02.3	13	02.6	09	01.7	19	01.9	08
VI	740.6	16.9	24.6	18.4	19.6	25.9	13.1	31.8	17	06.9	05,03	09	01.4	01	01.0	06	02.0	12	01.8	13	01.5	11	01.7	11	01.8	13	01.3	14
VII	739.9	16.6	24.4	19.1	19.8	26.0	12.7	33.0	23	08.1	19	08	01.8	08	01.6	08	02.0	16	02.2	11	02.3	10	01.1	10	01.3	16	01.8	06
VIII	739.6	16.3	25.9	18.9	20.0	26.6	13.8	36.4	07	07.6	27	09	01.8	03	01.7	09	01.2	06	02.3	13	01.4	08	01.5	14	01.4	12	01.3	19
IX	743.2	12.2	22.3	15.6	16.4	23.2	10.4	33.2	11	-02.4	30	02	01.5	04	01.2	06	02.0	07	02.1	08	02.4	13	02.5	12	02.0	14	01.6	24
X	743.1	07.7	15.9	10.5	11.2	17.1	05.5	28.4	10	-03.9	25	04	01.2	04	02.0	05	01.0	06	03.0	19	02.3	19	02.5	11	01.5	05	01.4	20
XI	741.1	07.2	13.0	09.7	09.9	14.3	05.0	22.2	03	-01.6	17	.	.	01	03.0	10	01.6	12	03.2	16	03.9	19	02.8	14	02.0	07	01.3	11
XII	743.9	-00.4	03.2	00.5	00.9	04.4	-02.6	17.8	01	-12.6	27	03	01.3	01	01.0	05	01.2	11	01.6	09	02.2	22	01.9	19	01.5	11	01.1	12
GOD.	740.0	08.3	14.7	10.3	10.9	16.1	05.6	36.4	7. VIII	-13.6	20 II	54	01.6	34	01.7	79	01.9	139	02.6	156	02.6	187	02.3	151	01.9	141	01.6	154
BOSANSKA KRUPA — φ = 44° 53' N λ = 16° 10' E Gr. Δ G = + 1h 05 min. — BR. ST. 107																												
I	-	-00.2	01.9	00.0	00.4	03.6	-03.1	15.0	05	-11.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	00.5	04.6	01.7	02.1	06.9	-03.4	15.8	09	-15.2	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	01.2	08.6	04.0	04.4	10.0	-01.2	20.8	24	-16.4	08	02	01.0	09	02.7	01	02.0	10	02.4	09	01.6	12	01.9	.	.	03	02.3	47
IV	-	07.1	14.7	09.1	10.0	16.4	04.3	27.6	23,19	-03.0	04	04	01.8	07	02.0	.	.	16	02.6	01	02.0	12	03.0	01	01.0	08	02.1	41
V	-	10.0	18.2	11.0	12.5	19.5	06.3	25.6	14	-07.0	02,01	02	01.5	10	02.3	.	.	12	01.8	04	02.8	13	02.0	.	.	03	01.0	49
VI	-	15.1	25.0	17.0	18.5	26.5	12.3	32.0	17	04.8	05	04	01.8	11	02.4	.	.	11	01.5	01	01.0	05	01.6	.	.	04	01.2	54
VII	-	15.4	25.1	17.9	19.1	26.5	12.3	-	-	-	-	04	01.8	12	02.3	.	.	04	01.8	07	03.0	06	01.5	.	.	05	02.4	55
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
DRVAR — φ = 44° 23' N λ = 16° 24' E Gr. Δ G = + 1h 06 min. — BR. ST. 108																												
I	717.0	-00.2	03.4	01.0	01.3	04.8	-02.0	13.0	06	-10.4	09	10	03.9	03	03.3	.	.	04	03.8	09	04.3	02	02.0	01	03.0	11	03.1	53
II	714.9	-00.7	04.0	00.6	01.1	05.4	-03.0	13.2	05	-14.8	20	10	04.1	07	04.1	01	02.0	02	04.5	16	03.4	06	05.2	.	.	08	03.1	34
III	716.0	-00.4	06.5	02.6	02.8	08.1	-01.7	18.2	26	-13.9	08	09	04.8	04	02.5	01	04.0	02	04.5	10	04.0	09	03.2	01	04.0	04	02.2	53
IV	717.7	06.1	12.8	08.1	08.8	14.6	03.7	24.6	23	-04.0	04	09	04.3	03	05.0	02	02.5	01	02.0	11	03.6	09	03.9	03	03.7	05	03.0	47
V	719.2	09.1	15.7	10.7	11.5	17.5	05.5	25.2	10	-02.6	01	06	03.3	15	04.1	01	06.0	06	03.5	09	04.7	06	03.2	02	03.5	04	03.2	44
VI	720.6	14.4	23.8	16.9	18.0	25.1	10.9	30.6	28	03.8	05	02	03.5	08	03.4	.	.	.	.	04	02.8	09	03.4	02	02.0	06	02.8	59
VII	719.6	14.4	24.5	17.2	18.4	25.4	11.4	33.1	23	06.2	19	10	03.6	03	05.3	03	02.7	.	.	02	02.5	05	04.2	06	02.5	14	03.6	50
VIII	719.5	14.4	25.2	17.3	18.5	26.5	12.1	34.6	07	05.8	28,27	05	03.2	04	02.8	.	.	.	.	02	03.0	04	02.8	01	03.0	09	03.4	68
IX	722.6	09.3	22.4	12.9	14.4	23.2	07.3	31.2	12	-03.8	30	07	04.4	03	02.7	03	03.7	02	02.0	03	04.0	04	02.8	02	03.5	08	03.2	58
X	722.4	03.6	16.0	07.7	08.8	17.3	02.0	28.0	11,10	-04.6	25	13	03.5	03	04.3	.	.	02	03.0	05	03.6	03	02.3	.	.	05	03.0	62
XI	720.8	03.6	11.6	06.0	06.8	13.1	01.6	21.0	03	-04.4	29	03	05.3	.	.	.	.	06	03.8	06	03.2	11	03.6	01	05.0	02	02.5	61
XII	721.9	-02.0	03.9	-00.7	00.1	05.4	-04.4	13.0	30,01	-12.6	27	07	04.7	01	03.0	.	.	03	04.0	08	04.0	01	02.0	05	02.8	05	03.2	63
GOD.	719.4	06.0	14.2	08.4	09.2	15.5	03.6	34.6	7. VIII	-14.8	20 II	91	04.0	54	03.8	11	03.3	28	03.6	85	03.7	69	03.5	24	03.0	81	03.1	652
DRINIĆ — φ = 44° 31' N λ = 16° 28' E Gr. Δ G = + 1h 06 min. — BR. ST. 109																												
I	-	-00.9	01.4	-00.1	00.1	03.6	-04.1	11.0	05	-12.4	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-01.3	02.2	00.0	00.3	04.5	-03.9	10.5	05	-13.2	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-01.0	04.3	00.4	01.1	06.3	-02.9	16.0	26	-10.0	29,01	03	02.3	03	02.7	12	02.8	22	01.5	14	02.5	04	02.5	07	01.7	.	.	28
IV	-	04.8	10.3	05.9	06.7	12.0	02.0	23.0	23	-07.0	05,04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	08.1	13.3	09.1	09.9	15.0	04.9	25.0	10	-03.0	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	15.0	21.1	14.7	16.4	22.6	10.4	27.8	28	03.0	05	.	.	16	01.8	13	01.3	12	01.4	03	01.7	05	02.2	06	02.3	02	02.0	33
VII	-	15.3	21.6	15.1	16.8	22.4	10.5	30.0	23	05.0	19	.	.	11	02.1	06	01.3	08	02.1	02	02.0	06	02.6	01	01.0	.	.	57
VIII	-	15.8	23.2	16.0	17.7	23.8	11.3	32.0	07	09.2	27	01	01.0	07	01.3	16	01.3	20	01.3	04	01.2	01	02.0	01	02.0	03	01.3	40
IX	-	10.8	19.4	12.1	13.6	20.1	08.4	29.0	12	-02.0	30	01	01.0	13	01.5	14	01.4	11	01.5	05	02.4	03	03.0	02	02.0	.	.	41
X	-	04.5	13.2	07.3	08.1	14.3	02.4	24.8	09	-05.6	25	.	.	03	02.3	11	01.9	25	02.1	11	02.0	11	02.3	.	.	.	.	32
XI	-	-	-	-	-	-	-	-	-	-	-	02	03.0	03	02.3	10	01.7	13	02.2	12	02.8	10	02.7	04	02.8	01	04.0	35
XII	-	-01.9	03.0	00.4	00.5	04.5	-03.8	12.0	01	-12.4	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SANSKI MOST — φ = 44° 46' N λ = 16° 42' E Gr. Δ G = + 1h 07 min. — BR. ST. 110																												
I	-	-00.8	01.5	-00.2	00.1	03.3	-03.0	14.0	06	-10.0	03	05	01.8	01	02.0	.	.	05	03.2	04	02.5	02	01.5	08	01.5	19	01.8	49
II	-	00.3	05.4	01.1	02.0	07.5	-03.2	16.1	09	-15.5	20	09	03.1	.	.	02	03.0	04	03.8	06	03.5	09	03.4	05	01.8	22	02.3	27
III	-	01.8	08.6	04.5	04.9	10.2	00.0	21.5	24	-09.8	08	05	02.8	03	02.0	01	01.0	14	03.4	05	03.4	04	03.5	07	01.7	06	02.3	46
IV	-	07.4	14.9	09.5	10.3	16.8	04.2	28.5	19	-03.7	04	08	04.0	03	02.7	01	01.0	08	03.2	10	04.0	08	03.5	05	01.4	14	02.0	33
V	-	10.3	17.7	11.8	12.9	19.1	06.9	25.2	16	-02.3	01	08	02.8	03	02.3	02	02.0	03	03.3	10	02.0	09	02.4	02	03.5	09	02.6	47
VI	-	16.1	24.7	17.3	18.9	26.0	12.3	31.7	17	05.1	05	07	02.4	03	02.3	.	.	03	01.7	01	03.0	01	02.0	04	02.0	13	01.9	58
VII	-	16.2	25.0	17.6	19.1	25.8	12.5	32.5	23	08.1	19	10	02.9	08	02.4	03	01.7	03	02.3	.	.	06	02.8	03	01.7	09	02.1	51
VIII	-	16.2	26.0	18.1	19.6	26.8	13.9	33.5	07	07.6	27	08	02.0	04	02.2	01	01.0	.	.	.	.	01	03.0	08	02.0	06	02.2	65
IX	-	11.0	22.8	13.1	15.0	23.6	09.0	33.6	11	-01.7	30	08	02.6	07	02.0	02	02.0	01	02.0	01	01.0	.	.	03	01.3	11	01.9	57
X	-	05.1	16.1	07.8	09.2	17.2	03.1	26.6	10,08	-03.5	25	04	02.8	05	01.8	01	02.0	03	03.3	06	03.2	03	02.3	08	01.4	11	02.2	52
XI	-	05.3	13.4	07.3	08.3	14.5	03.2	21.9	03	-02.3	12	05	01.6	01	02.0	.	.	06	04.5	07	02.7	10	02.5	03	01.6	07	02.4	49
XII	-	-01.1	03.2	-00.1	00.5	04.5	-03.3	18.4	01	-16.4	27	04	02.2	01	01.0	.	.	03	01.7	05	02.0	05	02.6	05	01.4	13	01.8	57
GOD.	-	07.3	14.9	09.0	10.1	16.3	04.6	33.6	11 IX	-16.4	27 XII	81	02.7	39	02.2	13	01.9	55	03.2	55	02.9	58	02.8	63	01.7	140	02.1	591

Mesec	Oblačnost Nm (0-10) 7	14	21	Srednji (Dnevni)	Insolacija (broj sati)	Vlažnost vazduha e_m mm	U_m % 7	14	21	Srednji (Dnevni)	Min	Padavine R mm Σ		
BIHAĆ														
BR. ST. 106														
I	9.6	9.4	8.8	9.2	013.1	04.3	84	77	79	81	44	136	039.0	01
II	8.6	8.3	7.7	8.2	065.1	04.0	77	68	74	73	28	136	026.8	12
III	7.3	8.5	7.7	7.8	096.3	04.7	82	63	75	73	23	172	032.0	28
IV	8.1	8.5	6.8	7.8	131.2	05.8	76	50	61	63	25	125	026.5	29
V	6.9	7.9	6.5	7.1	182.5	07.3	80	49	68	66	32	102	053.9	23
VI	5.4	7.3	5.0	5.9	230.9	11.8	80	52	75	69	32	097	032.7	20
VII	4.7	6.5	4.6	5.3	260.9	11.6	84	51	72	69	28	169	064.2	05
VIII	6.6	6.2	3.5	5.4	209.9	13.1	90	54	83	76	25	146	031.7	23
IX	6.8	5.8	4.1	5.6	183.7	09.6	86	51	75	71	25	018	005.6	17
X	6.6	6.5	3.9	5.7	141.4	07.1	85	56	76	72	28	101	028.4	04
XI	7.6	7.7	6.1	7.1	095.9	06.4	82	60	73	72	31	058	019.0	22
XII	9.0	8.2	8.0	8.4	048.5	04.2	89	76	86	83	29	136	024.4	28
GOD.	7.3	7.6	6.1	7.0	1659.4	07.5	83	58	74	72	23	1396	064.2	5 VII

Broj dana sa:

Mesec	Tn ≤ -20,0	Tx ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	≡	≡	≈	▲	▲	⚠ T	■	■
BR. ST. 106																							
I	.	.	.	.	.	.	10	03	.	26	15	12	04	10	07	.	.	.	.	.	.	08	15
II	.	.	.	.	.	.	16	08	01	19	17	16	05	11	11	01	.	.	.	.	03	09	15
III	.	.	.	.	.	.	15	05	02	16	17	13	07	11	13	06	.	.	.	.	02	08	15
IV	.	.	03	03	.	.	19	06	.	14	15	12	04	14	05	.	.	.	.	.	03	.	03
V	.	.	03	01	.	.	15	.	02	13	13	08	03	13	01	.	.	.	.	.	03	05	.
VI	.	.	.	20	03	.	08	.	02	09	17	11	03	17	.	.	.	.	.	.	14	08	.
VII	.	.	.	20	09	.	07	01	06	09	09	07	05	09	.	.	.	.	.	.	04	01	.
VIII	.	.	.	19	07	.	05	.	04	08	13	10	05	13	.	.	.	.	.	.	04	07	.
IX	.	.	01	11	04	03	06	.	04	06	05	04	.	05	.	.	.	.	.	.	.	12	.
X	.	.	03	03	.	.	12	.	06	09	11	08	04	11	01	.	.	.	.	.	01	12	01
XI	.	.	05	.	.	.	17	04	03	12	12	11	01	12	.	.	.	.	.	.	02	09	.
XII	02	23	.	.	.	.	08	03	01	21	14	13	07	07	09	.	.	.	.	.	03	11	10
GOD.	04	37	69	77	23	03	138	30	31	162	158	125	48	133	47	07	.	.	.	.	39	85	59

Mesec	Oblačnost 7	14	21	Srednji (Dnevni)	Insolacija (broj sati)	Vlažnost vazduha e_m mm	U_m % 7	14	21	Srednji (Dnevni)	Min	Padavine R mm Σ		
BOSANSKA KRUPA														
BR. ST. 107														
I	9.7	9.6	9.4	9.6	-	04.2	88	83	83	85	07	139	042.5	17
II	8.9	6.8	6.9	7.5	-	04.5	81	78	81	80	19	113	032.0	12
III	6.7	7.3	7.4	7.1	-	05.2	82	74	79	78	43	150	038.5	07
IV	6.3	6.8	5.2	6.1	-	07.0	80	65	76	74	39	093	016.0	29
V	6.9	6.1	5.7	6.2	-	08.2	80	62	75	72	40	079	031.1	23
VI	4.1	5.4	4.2	4.6	-	11.3	79	54	73	69	37	203	073.2	20
VII	3.7	3.6	2.6	3.3	-	12.1	82	59	76	72	-	180	054.3	05
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Tn ≤ -20,0	Tx ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	≡	≡	≈	▲	▲	⚠ T	■	■
BR. ST. 107																							
I	.	.	.	.	.	.	.	.	.	28	14	12	05	09	08	.	.	.	.	.	.	06	27
II	.	.	.	.	.	.	02	.	01	16	15	14	03	09	08	.	.	.	.	.	.	03	-
III	.	.	.	.	.	.	02	.	03	17	12	12	05	.	.	.	.	.	.	.	.	01	05
IV	.	.	03	04	.	.	.	.	02	11	14	13	04	14	01	.	.	.	.	.	.	02	.
V	.	.	03	02	.	.	.	.	03	10	10	09	03	09	02	.	.	.	.	.	.	04	.
VI	.	.	.	20	06	.	.	.	08	06	10	09	04	.	.	.	.	.	.	.	03	01	.
VII	.	.	.	.	.	.	01	.	16	04	08	08	05	08	.	.	.	.	.	01	.	03	.
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost 7	14	21	Srednji (Dnevni)	Insolacija (broj sati)	Vlažnost vazduha e_m mm	U_m % 7	14	21	Srednji (Dnevni)	Min	Padavine R mm Σ		
DRVAR														
BR. ST. 108														
I	8.8	8.3	6.4	7.8	031.8	04.5	92	78	89	86	57	163	075.6	01
II	8.6	7.8	7.0	7.8	063.6	04.1	86	69	81	79	45	126	033.0	15
III	6.6	7.3	6.2	6.7	108.0	04.6	87	67	82	79	40	150	030.2	28
IV	7.1	7.6	4.6	6.4	153.6	06.1	85	57	74	72	31	107	022.8	09
V	5.7	7.7	5.0	6.1	191.6	07.1	81	55	72	70	32	079	031.7	23
VI	4.8	7.0	2.5	4.8	238.9	11.3	88	54	78	73	35	060	027.4	20
VII	3.2	5.6	3.2	4.0	266.1	12.0	91	53	85	76	34	092	031.8	17
VIII	4.3	6.3	3.0	4.5	229.9	12.3	94	54	84	78	30	094	027.8	11
IX	5.0	4.9	1.8	3.9	208.0	09.8	96	51	87	78	31	004	002.4	01
X	7.7	4.4	3.0	5.0	151.0	06.4	91	51	81	75	33	069	028.2	04
XI	7.6	6.0	5.2	6.3	096.0	05.8	88	61	83	77	29	092	043.8	22
XII	7.1	5.6	4.6	5.8	082.1	03.9	86	70	86	81	35	130	033.4	28
GOD.	6.4	6.5	4.4	5.8	1820.6	07.3	88	60	81	77	29	1166	075.6	04 I

Mesec	Tn ≤ -20,0	Tx ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	≡	≡	≈	▲	▲	⚠ T	■	■
BR. ST. 108																							
I	.	.	.	.	.	.	03	02	01	15	13	11	04	11	04	01	.	.	.	.	.	05	12
II	.	.	.	.	.	.	12	09	.	15	13	12	06	11	05	01	.	01	.	01	04	04	15
III	.	.	.	.	.	.	06	04	04	14	10	10	06	10	08	04	01	.	.	.	02	.	15
IV	.	.	05	.	.	.	07	01	.	10	17	14	03	16	02	01	.	.	.	.	02	.	.
V	.	.	04	01	.	.	08	03	03	07	12	09	02	12	02	.	.	.	.	.	04	01	.
VI	.	.	.	20	02	.	01	01	04	04	11	08	02	11	.	.	.	.	.	.	10	01	.
VII	.	.	.	19	07	.	07	03	12	07	06	05	04	06	.	.	.	.	.	.	03	01	.
VIII	.	.	.	21	06	.	.	01	07	06	10	08	04	10	.	.	.	.	.	.	07	04	.
IX	.	.	05	12	02	.	03	.	11	02	02	02	.	02	.	.	.	.	.	.	.	07	.
X	.	.	11	03	.	.	04	02	04	03	07	05	03	07	01	.	.	.	.	.	01	12	.
XI	.	.	12	.	.	.	04	03	04	12	08	07	03	08	.	.	.	.	.	.	01	08	.
XII	03	05	27	.	.	.	05	.	06	11	13	09	04	08	06	.	.	.	.	.	01	06	07
GOD.	09	16	123	76	17	.	60	29	56	106	122	100	41	112	28	07	01	01	.	01	35	49	49

Mesec	Oblačnost 7	14	21	Srednji (Dnevni)	Insolacija (broj sati)	Vlažnost vazduha e_m mm	U_m % 7	14	21	Srednji (Dnevni)	Min	Padavine R mm Σ		
DRINIĆ														
BR. ST. 109														
I	8.8	8.0	7.7	8.2	-	04.2	81	82	86	83	-	145	037.0	17
II	8.6	7.5	7.4	7.8	-	04.3	82	83	86	84	-	172	033.5	19
III	6.7	6.8	6.8	6.8	-	04.1	76	80	77	78	40	138	037.0	28
IV	5.3	6.2	4.4	5.3	-	06.1	78	79	75	77	32	141	036.0	09
V	5.6	6.1	6.1	5.9	-	06.9	73	71	72	72	34	128	041.0	23
VI	4.8	5.6	4.1	4.8	-	11.8	81	75	82	79	47	098	030.0	20
VII	3.9	3.8	3.8	3.8	-	12.4	78	77	86	80	52	098	040.0	17
VIII	4.0	4.6	3.4	4.0	-	12.1	79	67	80	76	36	076	021.0	25
IX	5.1	3.7	2.8	3.9	-	09.1	76	66	76	73	40	010	003.8	01
X	4.9	3.7	3.2	3.9	-	06.2	70	68	75	71	39	082	025.0	02
XI	6.0	5.0	5.0	5.3	-	-	-	-	-	-	-	086	025.7	22
XII	6.6	5.7	4.7	5.7	-	03.8	68	74	78	73	29	211	070.0	22
GOD.	5.9	5.6	5.0	5.4	-	-	-	-	-	-	-	1385	070.0	22 XI

Mesec	Tn ≤ -20,0	Tx ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	≡	≡	≈	▲	▲	⚠ T	■	■
BR. ST. 109																							
I	.	.	.	.	.	.	.	.	.	14	15	15	05	10	08	.	.	.	.	01	.	26	31
II	.	.	.	.	.	.	03	01	.	14	14	13	08	07	10	01	.	.	.	02	01	13	23
III	.	.	.	.	.	.	01	.	03	17	15	14	04	03	13	.	.	.	.	.	.	17	28
IV	.	.	.	.	.	.	.	.	07	05	12	12	06	10	06	.	.	.	.	.	.	08	01
V	.	.	03	01	.	.	.	.	05	08	12	11	06	10	02	.	.	.	.	.	-	09	01
VI	.	.	.	10	.	.	.	.	07	03	10	10	04	10	.	.	.	.	.	.	02	02	.
VII	.	.	.	15	01	.	.	.	13	06	05	05	04	05	.	.	.	.	.	.	-	06	.
VIII	.	.	.	15	02	.	.	.	11	04	06	06	03	06	.	.	.	.	.	.	-	05	.
IX	.	.	01	09	.	.	.	.	10	05	03	03	.	03	.	.	.	.	.	.	-	07	.
X	.	.	06	.	.	.	.	.	13	07	07	06	04	07	.	.	.	.	.	.	-	11	.
XI	.	.	-	-	-	-	01	.	08	06	10	10	03	10	.	.	.	.	.	.	-	14	.
XII	02	06	25	.	.	.	.	.	08	12	12	12	05	07	07	02	.	.	.	.	.	06	10
GOD.	-	-	-	-	-	-	05	01	85	101	121	117	52	86	47	03	.	.	.	03	-	124	94

Mesec	Oblačnost 7	14	21	Srednji (Dnevni)	Insolacija (broj sati)	Vlažnost vazduha e_m mm	U_m % 7	14	21	Srednji (Dnevni)	Min	Padavine R mm Σ		
SANSKI MOST														
BR. ST. 110														
I	9.4	8.5	7.8	8.6	022.2	04.1	91	80	87	86	58	115	041.5	17
II	8.8	7.5	6.4	7.6	067.5	04.2	85	66	84	78	37	100	026.1	12
III	7.3	7.8	6.8	7.3	099.9	05.0	89	62	83	78	25	123	030.0	28
IV	7.1	8.0	4.4	6.5	141.8	06.5	84	52	74	70	24	066	012.7	09
V	7.4	7.5	5.4	6.8	177.2	08.3	86	54	83	75	28	087	034.8	23
VI	4.9	5.8	3.8	4.9	233.9	13.2	89	58	90	79	34	106	029.0	03
VII	4.7	5.4	3.8	4.6	255.5	13.4	89	59	91	80	36	120	034.7	17
VIII	7.0	5.5	3.3	5.3	225.8	14.3	95	60	93	83	45	098	021.5	11
IX	8.0	4.4	2.6	5.0	187.3	10.4	96	52	90	79	29	020	007.2	01
X	8.7	5.3	3.6	5.9	143.8	07.3	95	60	91	82	32	079	032.5	02
XI	7.7	6.6	5.4	6.6	097.9	06.4	90	60	86	79	37	049	008.9	22
XII	9.0	7.5	7.2	7.9	045.1	04.2	93	79	89	87	37	087	020.0	23
GOD.	7.5	6.6	5.0	6.4	1697.9	08.1	90	61	86	79	24	1050	041.9	17 I

Mesec	Tn ≤ -20,0	Tx ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	≡	≡	≈	▲	▲	⚠ T	■	■
BR. ST. 110																							
I	.	.	.	.	.	.	02	01	01	21	14	11	03	08	07	.	.	.	.	.	.	12	31
II	.	.	.	.	.	.	06	02	.	12	17	14	03	08	12	01	.	.	.	.	.	05	16
III	.	.	.	.	.	.	02	01	02	15	15	11	04	10	10	02	.	.	.	.	01	04	07
IV	.	.	04	04	.	.	09	02	.	09	12	09	03	12	01	.	.	.	.	.	.	.	01
V	.	.	03	03	.	.	05	.	02	09	14	11	03	14	01	01	.	.	.	.	02	04	.
VI	.	.	.	21	03	.	02	01	06	04	16	09	05	16	.	.	.	.	.	01	14	01	.
VII	.	.	.	21	08	.	03	02	08	09	11	08	05	11	.	.	.	.	.	.	02	06	.
VIII	.	.	.	20	08	.	.	.	04	06	13	12	04	13	.	.	.	.	.	.	06	12	.
IX	.	.	01	13	04	.	01	.	02	02	05	04	.	05	.	.	.	.	.	.	.	17	.
X	.	.	06	05	.	.	01	01	02	09	11	06	03	11	.	.	.	.	.	.	01	16	.
XI	.	.	04	.	.	.	02	02	03	09	12	11	.	12	.	.	.	.	.	.	01	10	.
XII	03	09	27	.	.	.	01	.	01	18	12	11	04	06	07	.	.	.	.	.	.	09	10
GOD.	10	21	101	87	23	.	34	12	31	123	152	117	37	126	38	04	.	.	.	01	27	96	65

Mjesec	Visina postaje 2m iznad	Temperatura vazduha °C Tm 7	14	21	Sred. (Dlas)	Max	Min	Max	Datum	Min	Datum	Costina pravca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												n.	j.	n.	j.	n.	j.	n.	j.	n.	j.	n.	j.		j.	n.	j.	n.
PRIJEDOR BR. ST. 111																												
φ = 44° 59' N λ = 16° 44' E Gr. Δ G = + 1h 07 min.																												
I	-	-01.6	00.9	-02.1	-01.2	-	-04.4	-	-	-14.9	03	08	02.1	.	.	.	.	.	.	03	03.0	01	01.0	.	.	.	.	81
II	-	-01.2	04.2	00.1	00.8	-	-03.2	-	-	-02.5	-	11	01.7	.	.	.	.	.	.	.	.	.	.	03	02.0	.	.	70
III	-	02.0	07.9	04.3	04.6	-	00.3	-	-	-05.9	08	24	01.5	.	.	.	.	.	.	02	02.5	.	.	01	02.0	.	.	66
IV	-	07.8	15.0	10.5	11.0	-	05.3	-	-	-02.7	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	11.4	18.3	12.5	13.7	-	07.3	-	-	00.2	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	17.6	25.3	18.3	19.9	-	12.6	-	-	05.5	03	19	01.7	07	01.0	08	01.6	06	01.8	05	01.6	02	01.5	.	.	15	01.2	28
VII	-	16.5	25.6	18.8	19.9	-	13.2	-	-	09.0	20,02	13	01.5	09	01.6	14	01.5	04	01.2	04	01.8	07	01.6	02	01.0	17	01.6	23
VIII	-	16.7	26.3	19.2	20.4	-	14.6	-	-	08.5	27	12	01.5	08	01.6	10	01.3	13	01.1	04	01.2	02	01.0	05	01.4	20	01.4	19
IX	-	12.0	23.0	13.9	15.7	-	-	-	-	-	-	20	01.4	09	01.2	02	01.0	08	01.4	05	01.2	10	01.0	01	01.0	11	01.4	24
X	-	05.8	15.1	08.7	09.6	-	-	-	-	-	-	12	01.3	08	01.4	06	01.2	06	01.5	05	01.4	02	01.5	06	01.3	10	01.1	38
XI	-	04.5	11.0	06.2	07.0	-	-	-	-	-	-	07	01.3	06	01.0	10	01.1	15	01.7	04	01.2	02	01.0	02	01.5	09	01.2	35
XII	-	-01.2	02.8	-00.5	00.2	-	-03.4	-	-	-	-	29	01.2	03	01.3	06	01.0	06	01.0	04	01.0	08	01.2	10	01.1	04	01.2	23
GOD.	-	07.5	14.6	09.2	10.1	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
MLINIŠTE BR. ST. 112																												
φ = 44° 16' N λ = 16° 51' E Gr. Δ G = + 1h 07 min.																												
I	-	-01.7	-00.6	-01.9	-01.5	01.2	-05.0	07.6	05	-13.2	21	.	.	07	02.1	.	.	27	03.1	.	.	18	02.9	.	.	10	02.0	31
II	-	-03.9	-01.8	-03.4	-03.1	00.2	-06.5	07.0	05	-16.8	18	.	.	01	02.0	.	.	10	03.6	.	.	34	02.9	.	.	22	02.0	17
III	-	-01.4	01.2	-00.7	-00.4	03.3	-04.0	12.2	26	-13.8	02	.	.	03	02.7	01	03.0	25	03.0	.	.	25	03.0	.	.	16	02.1	23
IV	-	03.3	07.3	03.7	04.5	08.9	00.0	19.6	24,23	-08.4	04	.	.	02	01.5	.	.	40	02.8	.	.	14	03.5	.	.	18	02.4	16
V	-	06.8	10.3	06.3	07.4	11.6	02.7	20.0	10	-06.2	02	.	.	15	01.1	.	.	18	03.1	.	.	15	02.5	.	.	26	02.3	19
VI	-	13.9	18.3	13.3	14.7	19.6	09.6	25.1	28	00.8	03	.	.	15	02.1	.	.	17	02.6	.	.	18	02.1	.	.	18	02.2	22
VII	-	14.2	19.0	14.0	15.3	20.2	09.3	26.4	22	04.0	19	.	.	12	01.8	.	.	20	02.2	.	.	16	01.7	.	.	25	02.1	20
VIII	-	15.5	19.8	14.5	16.1	20.7	10.8	30.1	07	06.4	27	.	.	13	01.7	.	.	21	01.7	.	.	30	01.7	.	.	15	02.4	14
IX	-	11.9	16.2	10.9	12.5	17.3	08.0	26.8	11	00.0	30	.	.	06	01.7	.	.	11	02.2	.	.	19	02.4	.	.	30	02.1	24
X	-	05.2	09.6	05.7	06.5	10.8	03.0	21.6	10	-05.0	25	.	.	10	01.6	.	.	13	02.8	.	.	23	03.1	.	.	20	02.0	27
XI	-	03.7	05.6	03.5	04.1	07.1	-	19.4	03	-	-	.	.	02	03.0	.	.	23	02.3	.	.	25	02.9	.	.	01	02.0	39
XII	-	-01.6	00.0	-01.7	-01.2	02.2	-	10.0	30	-	-	.	.	02	02.5	.	.	18	02.5	.	.	13	02.6	.	.	15	02.3	45
GOD.	-	05.5	08.7	05.4	06.2	10.3	-	30.1	7.VIII	-		.	.	88	01.8	01	03.0	243	02.7	.	.	250	02.6	.	.	216	02.2	297
GLAMOČ BR. ST. 113																												
φ = 44° 03' N λ = 16° 52' E Gr. Δ G = + 1h 07 min.																												
I	-	-01.4	01.8	-00.7	-00.2	04.0	-04.8	10.9	13	-15.8	23	42	02.2	07	02.4	04	02.0	12	02.8	11	02.5	.	.	08	01.9	.	.	09
II	-	-03.7	-00.3	-02.7	-02.3	02.2	-07.3	08.3	06	-18.4	18	30	02.6	12	03.2	03	02.3	16	02.9	10	03.6	01	04.0	02	02.0	04	02.2	04
III	-	-02.6	01.9	-00.7	-00.5	04.0	-06.0	13.3	26	-21.6	09	36	02.1	03	04.3	05	03.8	07	03.4	22	02.9	01	01.0	01	03.0	06	03.3	12
IV	-	04.2	09.7	05.5	06.2	11.2	00.8	21.6	23	-10.0	04	29	02.4	01	03.0	01	02.0	12	02.5	09	02.7	03	03.7	03	03.3	05	03.4	27
V	-	06.9	12.4	08.1	08.9	14.0	04.0	20.3	10	-02.6	03	41	02.7	10	02.1	02	01.0	01	01.0	11	02.0	01	01.0	07	02.7	03	01.7	17
VI	-	13.6	20.2	14.7	15.8	21.5	08.8	27.4	28	02.8	05,04	33	02.0	10	01.9	.	.	02	02.0	07	01.7	01	02.0	05	01.0	.	.	32
VII	-	13.9	21.4	15.0	16.4	22.9	08.7	30.4	23	01.8	19	23	02.2	04	01.8	01	01.0	.	.	06	01.5	02	02.0	.	.	.	.	57
VIII	-	13.5	21.7	15.3	16.5	22.7	09.6	30.8	07	04.3	25	33	02.2	08	02.1	02	02.0	04	01.8	09	01.4	01	02.0	02	01.5	02	01.5	32
IX	-	10.2	18.6	12.2	13.3	20.1	06.3	28.2	12,11	-03.6	30	43	01.9	05	01.4	04	02.2	04	01.2	04	01.2	01	02.0	10	02.0	08	01.8	11
X	-	05.0	12.4	06.5	07.6	14.0	00.5	25.6	11	-05.0	24	49	02.1	05	02.6	02	01.5	04	03.5	05	04.0	01	02.0	14	01.9	.	.	13
XI	-	02.2	06.9	05.1	04.8	09.0	-00.5	19.0	03	-04.0	18,12	54	02.2	.	.	02	01.0	09	03.9	06	04.8	01	02.0	02	01.5	.	.	16
XII	-	-03.6	01.2	01.2	00.0	04.4	-04.9	09.5	01	-10.6	26	56	01.7	10	02.1	.	.	02	02.5	09	02.3	05	02.4	.	.	06	01.8	03
GOD.	-	04.8	10.7	06.6	07.2	12.5	01.3	30.8	7.VIII	-21.6	9.II	471	02.2	75	02.3	26	02.2	75	02.8	109	02.6	18	02.4	54	02.0	34	02.3	233
BANJA LUKA BR. ST. 114																												
φ = 44° 47' N λ = 17° 13' E Gr. Δ G = + 1h 09 min.																												
I	747.2	-01.3	01.6	-00.6	-00.3	02.8	-03.5	15.2	05	-11.6	03	21	01.1	07	01.1	02	01.0	03	01.0	07	02.1	01	01.0	16	01.2	14	01.3	22
II	744.2	00.2	05.5	01.0	01.9	07.0	-03.2	15.4	09	-12.8	03	22	01.5	05	02.0	03	01.0	03	01.0	07	03.3	08	02.9	15	01.5	12	01.5	09
III	745.1	01.8	08.9	05.0	05.2	10.3	00.1	20.4	24	-10.8	08	12	01.4	05	02.2	05	01.2	10	01.6	06	01.7	10	02.5	11	01.9	09	01.8	25
IV	746.3	07.6	15.5	10.0	10.8	16.8	04.6	27.3	19	-02.4	05	17	01.9	07	01.3	06	01.7	04	01.2	10	01.2	11	02.5	12	01.9	10	02.0	13
V	747.7	11.4	17.6	12.5	13.5	19.3	07.5	26.4	10	-01.4	01	16	01.8	04	02.0	10	01.2	07	01.0	06	01.2	12	02.3	06	01.7	13	02.2	19
VI	748.5	17.5	25.0	18.2	19.7	26.0	13.0	31.6	23	05.2	05	11	01.6	11	01.5	12	01.5	07	01.0	07	01.3	07	01.9	05	01.6	09	01.7	21
VII	747.7	17.4	24.9	18.6	19.9	26.1	13.3	33.0	23	08.8	27	09	01.4	10	01.7	09	01.7	13	01.1	01	01.0	08	02.2	06	01.3	10	01.6	27
VIII	747.4	17.1	26.1	19.1	20.3	26.8	14.6	34.6	07	08.8	27	16	01.3	14	01.5	06	01.2	12	01.2	02	01.5	04	01.5	05	01.6	03	01.3	31
IX	751.2	11.6	23.0	14.0	15.6	23.5	09.6	35.1	11	-01.4	30	08	01.2	14	01.4	09	01.6	04	01.0	01	01.0	02	01.0	02	01.5	11	01.3	39
X	751.3	05.6	15.9	08.4	09.6	16.9	03.5	26.8	07	-03.2	25	11	01.3	17	01.4	05	01.4	09	01.0	03	01.3	04	02.0	09	01.0	05	01.0	30
XI	749.3	05.8	13.5	07.4	08.5	14.4	03.5	21.4	03	-01.9	07	14	01.2	07	01.9	06	01.2	09	01.2	02	01.0	15	02.7	06	01.2	09	01.3	22
XII	752.4	-01.5	03.4	-00.4	00.3	04.2	-03.3	17.6	01	-14.2	27	19	01.4	09	01.2	07	01.1	07	01.1	05	01.4	02	02.0	10	01.5	06	01.2	28
GOD.	748.2	07.8	15.1	09.4	10.4	16.2	05.0	35.1	4.IX	-14.2	1.I, XII	176	01.4	110	01.5	80	01.4	88	01.1	57	01.7	84	02.3	103	01.5	111	01.6	286
JAJCE BR. ST. 115																												
φ = 44° 21' N λ = 17° 16' E Gr. Δ G = + 1h 09 min.																												
I	-	-00.4	02.6	00.5	00.8	03.9	-03.5	13.2	05	-12.2	08	.	.	.	.	01	04.0	02	03.5	03	04.7	03	02.7	08	03.0	03	03.7	73
II	-	-00.4	04.4	00.3	01.2	05.4	-04.3	15.0	05	-13.6	18	03	04.7	01	04.0	.	.	01	05.0	05	05.0	06	04.5	03	03.0	03	03.3	62
III	-	00.9	07.2	03.8	03.9	09.3	-00.8	21.2	26	-12.0	02	01	03.0	01	04.0	01	05.0	02	03.0	02	04.5	12	03.3	03	02.3	13	03.5	58
IV	-	07.1	13.9	09.1	09.8	16.0	04.3	26.5	23	-02.2	04	.	.	07	03.3	02	02.5	01	04.0	.	.	10	03.7	08	04.6	01	03.0	61
V	-	09.9	16.3	11.1	12.1	18.4	05.7	28.0	10	-01.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	14.7	23.8	17.4	18.3	25.3	11.5	32.8	18,17	05.0	03	.	.	.	.	01	05.0	01	01.0	.	.	20	03.4	04	03.5	06	03.5	58
VII	-	15.1	24.3	17.2	18.5	25.4	12.2	33.0	23,22	07.5	20,19	01	03.0	02	02.5	02	01.0	.	.	03	02.3	18	02.6	10	03.1	03	02.7	54
VIII	-	15.7	25.8	18.0	19.3	26.7	13.6	34.6	07	09.4	27	03	03.0	02	03.5	03	01.0	01	05.0	06	01.2	15	01.6	09	02.6	01	03.0	53
IX	-	11.3	22.1	13.1	14.9	22.8	08.9	33.0	11	-02.0	29	01	03.0	04	03.5	01	01.0	.	.	.	.	10	02.2	13	02.3	02	05.5	59
X	-	05.8	15.3	08.4	09.5	16.7	04.5	26.9	10	00.6	17	02	01.5	01	03.0	01	02.0	03	01.7	07	02.4	11	02.2	14	02.2	02	02.0	52
XI	-	05.7	11.9	07.6	08.2	13.4	-	20.0	05	-	-	05	01.8	.	.	03	01.0	03	01.3	12	02.0	03	02.7	06	01.2	01	01.0	57
XII	-	00.6	03.7	01.5	01.8	05.0	-	14.2	30	-	-	01	02.0	.	.	01	01.0	.	.	.	.	01	02.0	04	02.0	.	.	86
GOD.	-	07.2	14.3	09.0	09.9	15.7	-	34.6	7.VIII	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlas)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dlas)	Min	Padavine R mm Σ	Max	Max.	Broj dana n sati Tn ≤ 0,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F(0-12) ≥ 6	≥ 8	Nm(0-10) < 2.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	✱	≡	≡	≈	▲	▲	T	≡	≡
BR. ST. 111						PRIJEDOR																	H_o = 135 m H_b = - m h_o = 2.0 m h_b = 1.0 m														
I	10.0	8.9	9.9	9.6	-	04.2	97	93	97	95	63	130	052.0	17	02	-	27	-	-	.	.	.	27	14	11	05	09	07	.	.	.	.	.	.	08	26
II	9.1	6.6	8.6	8.1	-	04.8	96	89	94	93	56	143	048.5	12	02	-	22	-	-	.	.	.	01	15	14	14	05	07	11	01	.	.	.	.	.	10	17
III	7.2	6.3	7.8	7.1	-	05.3	92	73	85	83	24	143	039.5	07	.	-	14	-	-	.	.	.	04	18	12	11	05	09	10	04	.	.	.	.	.	01	05
IV	6.6	5.7	5.6	6.0	-	07.2	81	58	81	74	20	070	012.8	09	.	-	02	-	-	.	02	.	06	10	15	13	02	15	01	.	.	.	.	.	01	01	.
V	5.4	5.5	4.4	5.1	-	09.7	85	70	84	80	31	059	015.0	06	.	-	.	-	-	.	.	.	04	05	15	10	02	14	01	01	.	.	.	01	02	02	.
VI	4.5	4.3	2.5	3.8	-	15.4	85	77	90	84	35	145	044.4	19	.	-	.	-	-	.	.	.	10	04	11	11	04	11	.	.	.	.	.	01	07	.	.
VII	4.0	3.7	3.7	3.8	-	14.8	89	68	88	82	37	110	029.1	17	.	-	.	-	-	.	.	.	16	08	13	11	04	13	.	.	.	.	.	.	01	06	.
VIII	5.7	4.4	3.6	4.6	-	15.4	91	68	91	84	34	078	023.5	11	.	-	.	-	-	.	.	.	09	06	11	10	03	11	.	.	.	.	.	.	03	08	.
IX	7.2	3.6	3.4	4.7	-	12.4	95	73	94	87	45	024	008.6	17	-	-	-	-	-	-	.	.	04	03	06	06	.	06	.	.	.	.	.	.	02	15	.
X	5.2	5.1	3.6	4.6	-	08.8	96	85	92	91	69	059	024.5	02	-	-	-	-	-	-	.	.	12	10	09	07	02	09	.	.	.	.	.	.	.	17	.
XI	8.5	6.2	5.7	6.8	-	06.5	89	76	86	84	48	063	020.0	23	-	-	-	-	-	-	.	.	02	13	11	11	02	11	.	.	.	.	.	.	.	14	.
XII	8.9	7.6	8.1	8.2	-	04.6	96	88	95	93	-	069	028.0	23	-	-	-	-	-	-	.	.	01	20	10	10	01	04	07	.	.	01	.	.	.	10	10
GOD.	6.9	5.7	5.6	6.0	-	09.1	91	76	89	85	-	1093	052.0	44	1	-	-	-	-	-	02	.	69	139	141	125	35	119	37	06	.	01	.	02	16	92	98
BR. ST. 112						NLINIŠTE																	H_o = 1130 m H_b = - m h_o = 2.0 m h_b = 1.0 m														
I	8.9	8.9	7.7	8.5	-	04.1	96	94	95	95	80	211	075.2	01	08	11	24	.	.	.	05	.	.	20	11	11	05	07	07	.	.	.	.	.	.	08	31
II	8.7	8.1	8.0	8.3	-	03.7	96	97	96	96	75	221	032.6	15	09	11	23	.	.	.	02	.	.	17	14	14	09	04	13	.	.	.	.	.	.	03	28
III	7.5	7.6	7.2	7.4	-	-	-	-	-	-	-	193	043.4	28	03	06	25	.	.	.	03	.	04	16	11	11	07	02	11	.	.	.	.	.	.	08	31
IV	7.0	8.1	6.6	7.2	-	-	-	-	-	-	-	158	073.2	09	.	01	13	.	.	.	01	.	.	12	10	10	04	06	05	.	.	.	.	.	.	03	20
V	7.4	7.5	7.3	7.4	-	06.6	81	79	81	80	49	145	042.2	28	.	.	07	.	.	.	02	.	01	14	13	11	04	10	05	.	.	.	.	.	.	03	05
VI	5.4	6.7	6.5	6.2	-	10.2	80	71	82	78	46	057	030.4	20	.	.	.	02	.	.	.	.	01	06	13	09	01	13	.	.	.	.	.	.	02	02	.
VII	5.2	6.2	5.7	5.7	-	-	-	-	-	-	-	066	023.4	17	.	.	.	05	.	.	.	.	04	09	09	07	02	09	.	.	.	.	.	.	.	14	.
VIII	5.4	6.1	5.3	5.6	-	10.0	72	66	73	70	49	079	020.5	25	.	.	.	05	01	.	.	.	02	05	13	10	03	13	.	.	.	.	.	.	01	02	.
IX	6.0	5.5	4.8	5.4	-	08.0	72	65	76	71	30	046	017.1	01	.	.	.	03	.	.	.	.	05	06	09	07	02	08	.	.	.	.	.	.	.	13	.
X	5.4	5.8	5.7	5.6	-	05.6	75	71	74	74	42	091	028.0	02	.	.	11	.	.	.	02	05	10	07	07	04	05	04	.	.	.	.	.	.	.	11	07
XI	6.7	7.0	6.8	6.8	-	04.7	77	73	75	75	36	151	060.4	22	-	.	-	.	.	-	01	.	01	13	11	11	02	08	05	.	.	.	.	.	.	04	05
XII	7.1	6.8	7.3	7.1	-	-	-	-	-	-	-	204	054.2	28	-	09	-	.	.	-	02	.	02	17	10	09	09	05	08	.	.	.	.	.	.	09	26
GOD.	6.7	7.0	6.6	6.8	-	-	-	-	-	-	-	1622	075.2	4	1	-	38	-	15	01	-	18	05	30	142	131	114	53	89	54	.	.	.	.	.	03	80	158
BR. ST. 113						GLAMOČ																	H_o = 1031 m H_b = - m h_o = 2.0 m h_b = 1.0 m														
I	8.1	7.1	6.4	7.2	-	03.9	82	82	81	82	-	244	040.0	02	08	05	23	.	.	.	04	.	03	15	16	16	08	15	04	.	.	.	.	.	.	01	21
II	8.5	7.4	6.6	7.5	-	03.4	83	83	83	83	35	162	040.4	16	10	10	24	.	.	.	03	02	01	12	17	15	06	10	10	02	.	.	.	.	.	.	19
III	6.6	6.6	6.4	6.5	-	03.9	78	82	80	80	02	156	027.0	04	06	04	27	.	.	.	03	01	05	15	14	12	09	06	12	03	.	.	.	.	.	.	29
IV	6.2	7.1	5.0	6.1	-	06.0	82	75	83	80	41	157	042.0	09	01	.	11	.	.	.	03	.	02	08	16	16	06	14	05	02	.	.	.	.	.	.	07
V	6.6	7.0	5.8	6.5	-	07.4	83	78	83	82	42	113	048.0	23	.	.	04	.	.	.	.	.	02	11	12	10	03	10	03	.	.	.	.	.	.	.	02
VI	3.4	6.8	4.2	4.8	-	11.4	83	74	83	80	42	056	015.0	17	.	.	.	08	.	.	.	.	05	03	10	10	01	10	.	.	.	.	.	.	.	.	.
VII	3.9	5.1	3.6	4.2	-	11.8	82	76	81	80	46	044	014.6	17	.	.	.	15	01	.	.	.	13	07	06	06	01	06	.	.	.	.	.	.	01	01	.
VIII	4.5	5.9	3.3	4.6	-	12.0	83	78	79	80	53	124	035.0	10	.	.	.	11	01	.	.	.	07	07	12	11	05	12	.	.	.	.	.	.	02	.	.
IX	4.7	4.1	2.4	3.7	-	08.3	74	61	71	69	32	002	001.0	01	.	.	05	05	.	.	01	.	11	04	02	01	.	02	.	.	.	.	.	.	.	.	.
X	7.4	4.6	4.5	5.5	-	04.8	66	53	55	58	26	097	027.5	21	.	.	12	01	.	.	01	.	06	09	09	08	04	06	05	.	.	.	.	.	.	07	04
XI	8.0	5.8	4.4	6.1	-	04.3	64	63	70	66	20	167	051.8	22	.	.	17	.	.	.	05	.	02	10	09	09	06	09	02	01	.	.	.	.	01	03	.
XII	9.8	7.9	6.7	8.2	-	-	-	-	-	-	-	177	035.5	25	01	04	30	.	.	.	.	.	.	16	14	14	08	08	11	05	.	.	.	.	.	01	11
GOD.	6.5	6.3	4.9	5.9	-	-	-	-	-	-	-	1499	051.8	44	XI	26	23	193	40	02	.	20	03	57	117	137	128	57	108	52	13	.	.	.	.	04	13	93
BR. ST. 114						BANJA LUKA																	H_o = 153 m H_b = 156.2 m h_o = 2.0 m h_b = 1.0 m														
I	9.6	8.1	7.7	8.5	026.8	04.0	92	82	90	88	56	132	045.8	17	01	10	26	.	.	.	01	.	.	20	18	14	03	10	09	.	.	01	.	.	.	12	31
II	8.4	7.8	5.9	7.4	063.5	04.1	86	62	82	77	32	136	029.1	12	03	04	20	.	.	.	05	.	01	12	19	12	05	10	11	01	.	.	.	.	01	04	21
III	7.0	7.8	7.2	7.3	108.9	05.0	89	61	78	76	26	138	034.3	28	01	.	15	.	.	.	02	.	03	16	17	14	05	12	10	01	.	.	.	.	01	02	08
IV	6.3	8.0	5.0	6.4	147.4	06.7	85	52	72	70	24	067	011.6	14	.	.	05	05	.	.	08	.	.	08	10	10	04	10	.	.	.	.	.	.	02	01	.
V	6.7	7.3	6.0	6.6	172.2	08.2	81	55	78	71	28	093	017.8	23	.	.	02	03	.	.	03	.	02	10	18	12	03	18	.	.	.	.	.	.	05	.	.
VI	5.0	6.1	4.6	5.2	221.0	12.8	85	53	82	73	33	086	031.9	20	.	.	.	20	03	.	03	.	05	05	13	09	03	13	.	.	.	.	.	.	13	.	.
VII	4.3	5.1	4.3	4.5	261.4	13.0	84	55	85	74	35	083	025.9	17	.	.	.	21	09	.	02	.	10	09	11	08	03	11	.	.	.	.	.	01	02	03	.
VIII	5.6	5.1	3.5	4.7	220.3	14.4	93	57	90	80	40	092	017.7	18	.	.	.	20	08	.	01	.	07	05	14	13	03	14	.	.	.	.	.	.	08	06	.
IX	5.1	4.3	2.6	4.0	207.3	10.5	93	50	91	78	23	025	008.8	18	.	.	01	11	05	.	.	.	10	02	05	04	.	05	.	.	.	.	.	.	01	06	.
X	5.5	5.5	3.9	5.0	149.9	07.4	93	60	91	81	27	079	033.3	02	.	.	03	05	.	.	.	.	09	08	09	08	03	09	.	.	.	.	.	.	.	06	.
XI	6.3	7.1	5.9	6.4	096.5	06.4	88	60	87	78	26	053	009.8	22	.	.	03	.	.	.	04	.	05	12	11	10	.	11	.	.	.	.	.	.	.	05	.
XII	7.8	7.1	6.6	7.2	045.6	04.3	94	79	91	88	33	080	029.0	23	02	05	28	.	.	.	.	.	04	18	14	10	03	09	05	.	.	01	.	.	.	06	10
GOD.	6.5	6.6	5.3	6.1	1720.8	08.1	88	60	84	77	23	1064	045.8	44	1	07	19	103	85	25	.	29	.	56	125	159	124	35	132	35	02	.	02	.	01	33	51	70
BR. ST. 115						JAJCE																	H_o = 430 m H_b = - m h_o = 2.0 m h_b = 1.0 m														
I	9.6	7.3	7.9	8.3	-	04.8	96	91	97	94	31	130	042.3	17	02	08	23	.	.	.	.	01	.	17	16	11	03	13	08	02	.	.	.	.	.	15	20
II	8.9	6.4	6.8	7.4	061.3	04.6	90	78	92	87	49	127	019.4	12	05	07	23	.	.	.	04	02	.	12	12	10	06	06	09	01	.	.	.	.	02	14	18
III	10.0	7.2	6.8	8.0	077.3	05.3	93	76	85	85	46	110	020.6	20	01	01	18	.	.	.	01	01	.	19	15	08	06	13	08	05	.	.	.	.	.	22	08
IV	9.6	6.6	7.0	7.7	-	07.2	90	64	80	78	33	112	038.6	09	.	.	05	03	.	.	05	04	.	11	16	10	03	16	02	02	.	.	.	.	01	22	.
V	8.6	6.7	6.5	7.3	134.9	08.9	91	70	87	83	35	129	048.4	28	.	.	02	01	.	.	03	03	.	13	13	11	02	13	02	02	.	.	.	.	02	17	.
VI	7.4	5.5	5.8	6.2	200.2	13.7	95	69	91	85	44	080	033.8	20	.	.	.	20	04	.	03	01	.	06	15	11	02	15	.	.	.	.	.	.	05	17	.
VII	7.0	4.5	4.5	5.4	240.3	13.5	93	66	92	83	40	075	020.2	17	.	.	.	20	07	.	01	01	04	09	10	10	03	10	.	.	.	.	.	.	03	14	.
VIII	8.7	4.8	5.0	6.2	-	13.9	92	63	88	81	20	-	-	-	.	.	.	21	07	.	.	.	02	11	-	-	-	-	.	.	.	.	.	.	01	04	.
IX	-	-	-	-	163.7	10.8	89	66	89	81	37	012	007.4	01	.	.	01	11	04	.	01	.	-	-	05	03	.	05	.	.	.	.	.	.	.	12	.
X	9.3	6.8	6.7	7.6	107.1	07.5	82	74	81	79	39	099	026.9	02	.	.	.	03	.	.	.	.	.	17	09	08	04	09	02	02	.	.	.	.	.	24	.
XI	9.4	6.5	8.1	8.0	097.1	07.0	83	79	83	82	49	078	020.0	16	-	.	-	.	.	-	.	.	.	13	11	11	02	11	.	.	.	.	.	.	.	22	.
XII	9.6	7.8	9.8	9.1	039.3	04.3	82	79	81	81	38	104	032.7	25	-	.	-	.	.	-	.	.	.	26	11	11	05	06	05	.	.	.	.	.	.	20	-
GOD.	-	-	-	-	-	08.5	89	72	87	83	20	-	-		-	16	-	79	22	-	18	13	-	-	-	-	-	-	-	14	.	-	.	.	14	203	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dies)	M̄ax	M̄in	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
KUPRES — φ = 44° 00' N λ = 17° 17' E Gr. ΔG = + 1h 09 min. — BR. ST. 116																												
I	-	-03.4	-00.1	-02.3	-02.0	01.7	-06.2	06.5	16	-17.0	09	19	02.0	03	01.0	02	01.0	.	.	42	02.1	.	.	06	01.2	08	01.1	13
II	-	-04.7	-01.2	-04.4	-03.7	00.2	-08.6	07.0	06	-21.6	18	40	02.3	.	.	.	.	.	.	37	03.2	02	01.0	.	.	04	01.0	01
III	-	-04.3	01.3	-02.3	-01.9	02.4	-06.6	09.5	26	-24.0	08	31	02.1	02	01.0	.	.	02	01.0	48	02.4	02	02.0	02	01.0	02	01.0	04
IV	-	03.4	07.8	03.6	04.6	09.5	00.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	06.3	10.3	06.2	07.2	11.7	03.0	18.5	10	-04.6	01	32	02.3	12	01.9	02	01.0	08	02.1	23	02.3	10	02.1	01	01.0	04	01.5	01
VI	-	12.8	17.9	11.9	13.6	19.5	07.2	25.0	28	01.6	05	18	01.8	35	01.9	05	01.4	03	01.3	12	01.9	07	02.4	02	01.5	04	02.2	04
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	08.7	17.8	10.1	11.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	02.1	10.5	02.9	04.6	11.8	-00.5	22.6	11	-05.4	-	29	02.8	09	05.2	.	.	.	.	20	03.6	05	04.0	03	02.0	03	03.3	24
XI	-	00.4	07.5	02.7	03.3	08.7	-01.5	19.2	02	-08.4	17	26	02.1	.	.	.	.	.	.	37	04.7	03	05.3	.	.	.	.	24
XII	-	-05.0	01.4	-03.2	-02.5	02.7	-06.3	11.0	13	-15.0	07	36	03.2	04	06.0	.	.	.	.	17	04.6	04	04.2	02	02.0	.	.	30
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
KOTOR VAROŠ — φ = 44° 38' N λ = 17° 23' E Gr. ΔG = + 1h10 min. — BR. ST. 117																												
I	-	-01.0	01.8	-00.2	00.1	03.2	-03.8	15.4	05	-15.6	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	00.6	05.5	01.4	02.2	06.9	-04.3	16.8	05	-14.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	01.8	08.6	04.6	04.9	09.8	-00.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	07.4	15.1	10.1	10.7	16.6	04.2	27.4	23	-02.5	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	10.0	17.9	12.1	13.0	19.0	05.9	25.2	09	-02.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	15.6	24.4	16.9	18.4	25.4	11.7	31.2	28	04.1	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	16.4	24.7	17.7	19.1	25.5	12.1	32.7	24	08.5	19,02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	17.0	25.6	18.5	19.9	26.7	13.4	34.0	07	07.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	11.2	22.3	14.1	15.5	23.2	08.4	34.6	11	-02.5	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	09.3	16.5	09.1	11.0	17.3	03.4	26.4	07	-01.0	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	05.4	14.1	08.3	09.0	15.0	02.6	23.2	03	-04.0	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-02.0	03.2	-00.2	00.2	04.2	-04.6	18.0	01	-17.5	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	07.6	15.0	09.4	10.3	16.1	04.0	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BUGOJNO — φ = 44° 04' N λ = 17° 28' E Gr. ΔG = + 1h 10 min. — BR. ST. 118																												
I	710.3	09.0	03.1	01.1	01.4	04.7	-02.0	14.7	06	-09.4	09	14	03.1	01	03.0	01	02.0	04	02.8	11	03.0	02	01.5	02	02.0	10	02.3	48
II	708.1	-01.5	03.7	-00.3	00.4	04.7	-04.5	13.2	06	-18.5	18	10	03.6	01	03.0	.	.	04	05.0	19	03.4	05	03.2	04	03.8	16	02.8	25
III	709.2	00.5	06.7	03.2	03.4	08.0	-01.1	17.2	26	-11.8	02	06	03.5	.	.	.	.	04	03.8	21	03.1	10	03.3	05	01.8	17	02.4	30
IV	711.0	06.0	12.8	08.4	08.9	14.5	03.1	25.6	23	-04.4	05	04	03.8	01	03.0	.	.	06	03.5	09	03.2	22	02.8	05	02.4	14	02.6	29
V	712.3	08.4	15.2	10.2	11.0	16.9	04.9	25.4	10	-02.4	01	06	03.0	.	.	01	03.0	01	06.0	10	03.6	07	02.0	03	03.7	22	02.5	43
VI	714.1	13.0	22.5	15.7	16.7	24.1	09.6	30.0	28	04.4	05	06	02.7	.	.	.	.	03	03.0	04	03.2	05	02.4	03	03.0	08	02.5	61
VII	713.2	13.8	23.2	16.4	17.4	24.0	10.4	31.0	23,22	04.9	27	07	02.7	01	05.0	03	02.7	.	.	04	03.5	07	02.1	02	02.5	22	02.6	47
VIII	713.1	13.1	24.7	16.5	17.7	25.7	11.1	33.4	07	04.4	27	03	02.3	01	02.0	02	02.5	01	01.0	05	02.3	05	02.4	06	02.3	16	01.8	56
IX	716.2	08.6	21.9	12.1	13.7	22.6	06.4	32.6	11	-05.7	30	08	03.1	03	03.3	01	04.0	.	.	03	03.3	06	04.2	03	02.0	15	02.6	51
X	715.7	03.8	14.2	07.0	08.0	15.7	01.9	26.3	10	-03.0	25	11	02.7	01	05.0	01	04.0	02	03.5	08	03.9	02	03.5	02	01.0	20	02.2	40
XI	714.2	03.1	10.6	05.5	06.2	12.0	01.1	21.2	03	-05.8	12	01	05.0	01	06.0	.	.	03	03.3	17	03.6	09	03.1	04	01.8	10	02.2	45
XII	715.3	-03.0	02.9	-01.0	-00.5	04.1	-05.1	12.0	30,01	-17.4	27	06	02.7	01	02.0	.	.	02	04.0	06	03.5	05	02.0	03	01.7	12	02.4	58
GOD.	712.7	05.5	13.5	07.9	08.7	14.8	03.0	33.4	7 VIII	-16.5	48 II	82	03.1	11	03.5	09	02.9	30	03.6	115	03.3	85	02.8	42	02.4	182	02.4	537
TRAVNIK — φ = 44° 14' N λ = 17° 41' E Gr. ΔG = + 1h 11 min. — BR. ST. 119																												
I	-	-02.0	01.6	-01.0	-00.6	02.2	-03.6	14.4	05	-10.6	21,09	.	.	.	.	07	01.1	07	01.0	.	.	.	.	05	01.2	02	01.0	7
II	-	-02.4	03.5	-00.7	-00.1	04.4	-04.0	14.0	06	-15.6	18	.	.	02	01.0	13	01.2	01	02.0	01	01.0	.	.	10	01.1	22	01.5	35
III	-	00.6	08.2	03.3	03.8	09.1	-00.8	19.2	24	-11.6	02	.	.	.	.	28	01.2	05	01.6	.	.	.	.	06	01.3	13	01.4	41
IV	-	07.0	14.6	08.2	09.5	15.2	03.9	26.6	23	-03.4	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	10.1	17.1	10.5	12.1	17.9	06.1	27.0	10	00.4	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	15.1	23.8	15.5	17.5	24.2	11.0	30.4	17	05.4	05,03	.	.	.	.	26	01.3	12	01.2	06	01.2	.	.	12	01.2	02	01.0	32
VII	-	15.5	23.2	15.8	17.5	23.9	11.6	30.6	23	06.4	19	01	01.0	.	.	10	01.1	27	01.4	03	01.3	.	.	09	01.1	08	01.4	35
VIII	-	14.9	24.6	16.2	18.0	25.0	12.5	31.4	07	07.4	28	.	.	02	01.5	11	01.2	10	01.6	01	01.0	03	01.0	09	01.6	.	.	57
IX	-	10.9	21.8	14.7	15.5	24.2	08.0	36.1	15	-03.0	30	01	03.0	03	01.7	06	01.5	32	01.8	08	02.0	05	01.4	02	01.0	01	02.0	32
X	-	04.3	13.0	07.0	07.8	14.6	02.4	22.6	11	-02.4	25	01	02.0	04	02.8	01	02.0	58	01.9	12	01.8	01	01.0	.	.	04	02.5	12
XI	-	04.0	09.4	06.0	06.3	11.1	01.5	17.4	19	-03.2	12	05	01.6	04	02.5	03	02.3	48	01.9	09	02.0	02	02.0	.	.	05	01.2	14
XII	-	-02.3	00.6	-01.0	-00.9	01.9	-03.8	13.6	30	-13.2	24	03	01.3	09	02.1	01	02.0	40	01.6	03	01.7	09	02.2	01	02.0	08	01.6	19
GOD.	-	06.3	13.4	07.9	08.9	14.5	03.7	36.1	15 IX	-15.6	48 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
PRNJAVOR — φ = 44° 52' N λ = 17° 42' E Gr. ΔG = + 1h 11 min. — BR. ST. 120																												
I	-	-02.5	00.9	-01.5	-01.2	02.1	-04.6	16.0	06,05	-16.0	03	12	01.9	15	01.7	16	01.8	03	02.0	05	01.4	23	01.8	10	01.8	08	01.9	.
II	-	-01.2	04.9	00.3	01.1	05.7	-03.7	15.0	09	-14.6	18	01	02.0	11	02.2	09	01.7	03	01.7	13	02.0	32	01.8	10	01.7	05	02.0	.
III	-	01.6	08.7	04.1	04.6	09.3	-00.1	21.0	24	-11.2	08,02	04	01.5	13	02.3	10	01.4	08	02.6	18	01.5	33	01.9	.	.	07	01.9	.
IV	-	06.6	15.1	08.6	09.7	16.2	04.2	27.5	20	-02.6	05	04	01.2	17	01.6	06	02.5	03	02.0	11	01.6	40	02.1	02	01.5	06	02.0	01
V	-	11.9	17.8	11.7	13.2	19.3	07.6	26.0	10	00.0	01	05	02.0	12	01.6	02	01.5	05	01.6	13	01.2	47	01.8	07	01.9	02	01.5	.
VI	-	17.2	25.3	18.1	19.6	26.0	13.4	31.0	23,17	06.6	03	03	01.3	13	01.3	.	.	06	01.2	18	01.1	29	01.6	04	01.5	04	01.5	13
VII	-	17.7	24.5	18.1	19.6	25.4	13.4	32.4	23	08.6	27	02	01.0	11	01.3	01	01.0	06	01.0	11	01.2	32	01.5	04	01.0	01	01.0	25
VIII	-	17.0	26.0	18.2	19.9	26.6	14.3	33.5	07	10.0	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	11.7	22.0	13.7	15.3	22.7	09.0	32.5	11	00.8	30,25	06	01.2	16	01.1	10	01.1	05	01.2	12	01.1	13	01.2	04	01.5	05	01.2	19
X	-	05.2	15.5	08.5	09.4	16.3	02.9	25.0	09,08	-02.4	20	14	01.3	07	01.6	04	01.0	07	01.3	14	01.1	31	01.5	02	01.0	02	01.0	12
XI	-	03.0	12.9	06.9	07.4	13.7	01.8	21.5	03	-02.6	13	09	01.2	08	01.2	07	01.0	14	01.1	16	01.1	22	01.5	02	02.0	01	01.0	11
XII	-	-01.8	02.9	-00.5	00.1	03.9	-03.5	16.5	01	-15.4	27	05	01.0	12	01.1	07	01.6	12	01.0	20	01.2	27	01.3	02	01.0	03	01.0	05
GOD.	-	07.2	14.7	08.8	09.9	15.6	04.6	33.5	7 VIII	-16.0	3. I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dias)	Insolacija broj sati	Vlažnost vazduha e mm	Um 7	14	21	Sred. (Dias)	Min	Padavine R mm Σ	Max	Max.	Broj dana s: Tn ≤-20,0	Tn ≤-10,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) <2,0	>8,0	R mm ≥0,1	≥1,0	≥10,0	●	⚹	⚹	⚹	≈	▲	▲	⊤	≡	▦
KUPRES																																					
BR. ST. 116																																					
H_o = 1190 m H_b = - m h_o = 2,0 m h_b = 1,0 m																																					
I	8.8	7.1	7.4	7.9	-	-	-	-	-	-	-	203	049.7	01	10	08	26	.	.	.	.	.	01	16	18	16	07	12	09	.	.	.	.	.	.	06	27
II	8.1	7.2	7.5	7.6	-	03.4	92	89	91	91	61	154	026.6	14	10	12	25	.	.	.	04	.	.	13	15	14	07	07	13	.	.	.	.	.	.	03	28
III	6.8	6.5	6.2	6.5	-	03.7	89	84	90	88	56	088	021.2	07	09	08	26	.	.	.	02	.	06	13	14	13	04	06	13	02	.	.	.	.	.	.	05	31
IV	6.2	6.9	5.3	6.1	-	05.1	84	68	84	79	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	7.4	7.8	5.7	7.0	-	07.5	93	92	95	93	65	079	029.0	23	.	.	05	.	.	.	01	.	03	12	14	10	02	09	06	.	.	.	.	.	.	.	01
VI	4.3	6.6	4.1	5.0	-	10.0	85	72	90	82	52	083	024.5	20	.	.	.	01	.	.	.	.	03	04	13	10	03	13	.	.	.	.	.	.	02	.	.
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	009	004.7	01	-	-	-	-	-	-	-	-	-	-	03	02	.	03	.	.	.	.	.	.	.	11	.
X	5.6	5.0	5.6	5.4	-	05.5	89	68	87	82	39	132	043.2	02	.	.	17	.	.	.	08	03	08	10	09	09	04	08	03	01	.	.	.	.	01	01	03
XI	6.4	6.6	6.1	6.4	-	05.0	89	72	87	83	46	146	043.2	16	.	.	20	.	.	.	12	06	06	16	11	11	05	09	04	.	.	.	.	.	.	.	05
XII	4.9	5.6	5.9	5.5	-	03.1	72	75	78	75	11	190	052.4	26	06	07	28	.	.	.	09	03	09	13	14	14	08	07	08	.	.	.	.	.	.	.	24
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
KOTOR VAROŠ																																					
BR. ST. 117																																					
H_o = 266 m H_b = - m h_o = 2,0 m h_b = 1,0 m																																					
I	8.9	8.9	9.7	9.2	-	04.2	85	88	87	87	65	098	032.1	17	03	09	23	.	.	.	.	.	-	-	15	12	03	06	10	.	.	.	.	.	.	01	30
II	9.0	8.8	9.2	9.0	-	04.8	90	79	85	85	40	135	023.9	19	06	04	22	.	.	.	02	.	.	20	18	18	06	08	12	.	.	.	.	.	.	.	18
III	7.3	7.6	7.3	7.4	-	05.5	88	71	84	81	-	111	017.2	15	-	-	-	-	-	-	-	-	01	18	16	15	05	12	10	04	.	.	.	.	.	.	07
IV	6.6	7.0	8.0	7.2	-	07.4	81	60	83	75	30	099	030.1	15	.	.	05	05	.	.	-	-	.	14	12	12	03	12	.	.	.	.	.	.	.	.	.
V	7.9	8.7	8.9	8.5	-	09.2	84	68	86	79	41	-	-	-	.	.	04	02	.	.	.	.	.	23	22	21	08	22	.	.	.	.	.	.	.	-	.
VI	5.9	6.3	5.0	5.8	-	12.7	85	63	84	77	33	119	030.2	10	.	.	.	18	05	.	-	-	.	07	13	06	05	13	.	.	.	.	.	.	.	-	.
VII	5.6	6.5	5.3	5.8	-	13.4	83	65	85	78	45	080	017.0	05	.	.	.	19	06	.	-	-	01	09	14	13	04	14	.	.	.	.	.	.	.	-	.
VIII	6.4	6.1	5.5	6.0	-	15.2	85	77	86	83	64	119	027.0	10	.	.	.	20	08	.	-	-	02	08	11	11	06	11	.	.	.	.	.	.	.	-	.
IX	5.3	5.7	4.2	5.1	-	10.7	84	65	84	78	42	067	025.2	01	.	.	02	12	04	.	.	.	04	08	07	07	03	07	.	.	.	.	.	.	.	01	.
X	6.0	6.0	7.6	6.5	-	08.5	81	74	81	79	48	108	040.2	02	.	.	02	05	.	.	.	.	.	09	07	07	04	07	.	.	.	.	.	.	.	-	.
XI	7.0	6.8	5.4	6.4	-	07.2	85	70	84	79	44	101	020.3	17	.	.	09	.	.	.	01	.	.	11	11	11	04	11	.	.	.	.	.	.	.	.	.
XII	6.3	6.9	5.5	6.2	-	04.1	85	83	84	84	50	061	011.0	26	04	09	26	.	.	.	.	.	01	13	11	11	01	06	05	.	.	.	.	.	.	.	-
GOD.	6.8	7.1	6.8	6.9	-	08.6	84	71	84	80	-	-	-		-	-	-	-	-	-	-	-	-	-	157	144	52	129	37	04	.	.	.	.	-	-	-
BUGOJNO																																					
BR. ST. 118																																					
H_o = 562 m H_b = 566,2 m h_o = 2,0 m h_b = 1,0 m																																					
I	9.6	8.8	8.4	8.9		036.8	04.4	91	76	87	85	47	125	034.8	17	.	09	19	.	.	.	10	.	.	25	17	10	04	14	08	05	.	.	.	.	.	.	04	11
II	9.1	8.1	7.2	8.1		070.0	03.8	88	64	85	79	37	087	020.6	16	05	06	23	.	.	.	19	02	.	17	15	12	03	09	08	.	.	.	.	.	.	04	05	18
III	7.7	7.3	6.6	7.2		111.0	04.4	86	63	78	76	28	087	019.2	28	01	01	17	.	.	.	17	01	02	16	16	12	04	11	13	05	.	.	.	.	.	.	01	12
IV	6.7	8.1	5.7	6.8		140.8	05.7	81	53	71	68	23	080	031.9	09	.	.	06	01	.	.	21	01	.	10	16	10	02	15	03	02	.	.	.	.	.	01	02	.
V	7.2	7.6	5.6	6.8		147.2	06.8	82	54	75	70	26	063	026.4	23	.	.	04	01	.	.	20	.	.	12	14	06	02	13	02	01	.	.	.	.	.	03	06	.
VI	6.4	6.7	4.8	6.0		206.4	10.7	91	54	82	76	31	102	029.6	15	.	.	.	18	01	.	10	.	04	05	15	09	04	15	.	.	.	.	.	01	10	11	.
VII	6.3	5.6	3.9	5.3		233.6	11.1	90	55	80	75	36	071	030.4	17	.	.	.	19	04	.	08	01	06	10	11	09	02	11	.	.	.	.	.	.	06	11	.
VIII	8.8	5.7	3.1	5.9		195.9	11.7	97	52	87	79	31	054	012.9	10	.	.	.	18	04	.	09	.	02	06	12	09	03	12	.	.	.	.	.	.	07	19	.
IX	8.3	4.6	2.0	5.0		180.5	08.7	95	45	85	75	16	008	004.5	01	.	.	04	12	05	.	07	.	04	03	05	03	.	03	.	.	.	.	.	.	.	17	.
X	7.4	5.5	4.9	5.9		146.7	06.2	91	56	87	78	16	100	036.2	02	.	.	06	02	.	.	10	02	06	12	12	06	03	09	01	01	.	.	.	.	02	17	.
XI	7.7	6.5	5.4	6.6		092.9	05.6	89	64	83	79	33	061	017.6	16	.	.	15	.	.	.	13	.	01	11	12	12	03	12	.	.	.	.	.	.	01	11	.
XII	8.1	5.8	5.6	6.5		077.3	03.9	90	73	87	83	35	123	037.3	26	04	05	25	.	.	.	06	.	04	11	13	12	03	09	06	.	.	.	.	.	01	12	10
GOD.	7.8	6.7	5.3	6.6		1639.1	06.9	89	59	82	76	16	961	037.3	26 XII	10	21	119	71	14	.	150	07	29	138	158	110	33	133	41	14	.	.	.	01	35	116	51
TRAVNIK																																					
BR. ST. 119																																					
H_o = 581 m H_b = - m h_o = 2,0 m h_b = 1,0 m																																					
I	8.8	8.4	7.1	8.1	-	04.2	94	87	94	92	55	107	032.1	17	03	11	23	.	.	.	.	.	02	20	11	10	04	07	05	.	.	.	.	.	.	04	31
II	8.3	6.9	7.0	7.4	-	04.0	91	75	88	85	37	154	025.1	16	03	09	21	.	.	.	.	.	04	17	16	15	08	09	09	.	.	.	.	.	.	02	19
III	7.0	6.0	5.7	6.2	-	04.9	87	67	83	79	40	069	020.0	28	01	01	17	.	.	.	.	.	07	14	15	13	01	11	10	02	.	.	.	.	.	.	.	09
IV	5.4	6.6	5.1	5.7	-	06.8	77	63	82	74	27	082	027.1	09	.	.	05	02	.	.	.	.	-	-	13	11	02	13	.	.	.	.	.	.	.	.	.
V	5.8	6.4	4.6	5.6	-	07.4	76	57	74	69	29	080	023.0	28	.	.	.	02	.	.	.	.	09	11	15	11	02	15	.	.	.	.	.	.	.	.	.
VI	4.9	3.0	4.0	4.0	-	11.0	81	58	72	70	36	090	024.7	20	.	.	.	16	01	.	.	.	12	07	16	10	03	16	.	.	.	.	.	.	.	04	.
VII	3.8	3.5	3.1	3.5	-	11.0	82	58	76	72	34	076	034.8	17	.	.	.	19	02	.	.	.	16	08	09	09	01	09	.	.	.	.	.	.	.	.	.
VIII	5.1	3.9	2.9	4.0	-	12.8	90	66	85	80	31	081	021.0	02	.	.	.	17	04	.	.	.	11	06	14	11	04	14	.	.	.	.	.	.	02	10	.
IX	4.8	3.7	2.7	3.7	-	10.6	91	57	84	77	34	010	004.0	18	.	.	02	14	02	.	.	.	11	04	06	03	.	06	.	.	.	.	.	.	.	06	.
X	3.9	4.4	4.1	4.2	-	06.5	90	64	87	80	21	113	034.5	02	.	.	04	.	.	.	.	.	11	07	09	08	03	09	02	02	.	.	.	.	02	06	.
XI	7.1	6.4	6.0	6.5	-	05.4	79	70	76	75	11	057	014.2	16	.	.	10	.	.	.	.	.	04	10	11	09	02	11	.	.	.	.	.	.	.	10	.
XII	7.8	8.0	8.2	8.0	-	03.7	83	82	85	83	58	071	020.0	26	02	16	26	.	.	.	.	.	02	20	13	10	02	06	08	.	.	.	.	.	.	13	11
GOD.	6.1	5.6	5.0	5.6	-	07.4	85	67	82	78	11	990	034.8	47 VII	09	40	119	70	09	.	.	.	-	-	148	120	32	126	34	04	.	.	.	.	04	55	70
PRNJAVOR																																					
BR. ST. 120																																					
H_o = 150 m H_b = - m h_o = 2,0 m h_b = 1,0 m																																					
I	9.9	8.6	8.5	9.0	-	03.5	78	77	88	81	-	116	032.5	17	03	11	26	.	.	.	.	.	.	23	14	12	03	10	.	01	.	.	.	.	.	21	31
II	8.6	7.9	6.6	7.7	-	03.8	81	64	78	75	31	153	025.0	12	03	03	22	.	.	.	.	.	01	14	17	16	06	08	10	.	.	.	.	.	.	09	25
III	8.0	8.3	7.3	7.9	-	04.8	82	63	77	74	33	125	034.2	28	02	.	13	.	.	.	01	.	01	18	17	16	05	13	09	03	.	.	.	.	01	05	05
IV	7.6	8.4	6.2	7.4	-	06.3	82	54	72	69	22	084	013.0	29	.	.	06	05	.	.	.	.	.	13	15	13	05	15	.	.	.	.	.	.	02	.	.
V	7.0	8.1	6.8	7.3	-	08.3	77	56	79	71	35	120	025.2	28	.	.	.	03	.	.	.	.	01	14	17	14	05	17	01	01	.	.	02	.	05	.	.
VI	5.9	6.0	5.5	5.8	-	12.6	77	54	86	72	35	112	030.0	20	.	.	.	22	03	.	.	.	01	08	13	11	04	13	.	.	.	.	01	.	12	01	.
VII	4.6	5.5	4.5	4.9	-	13.2	79	61	85	75	32	070	023.0	17	.	.	.	20	08	.	01	.	07	09	09	09	02	08	.	.	.	.	01	.	04	.	.
VIII	5.3	4.8	3.6	4.6	-	13.8	83	61	88	77	41	083	016.0	18	.	.	.	20	06	.	.	.	07	05	10	09	05	10	.	.	.	.	.	.	08	01	.
IX	6.2	5.0	3.0	4.8	-	10.4	82	61	88	77	38	056	025.5	01	.	.	.	10	03	.	.	.	06	04	06	06	02	06	.	.	.	.	.	.	01	14	.
X	6.7	5.5	4.2	5.5	-	07.3	88	64	87	80	38	098	033.0	02	.	.	05	02	.	.	.	.	07	11	08	07	04	08	.	.	.	.	.	.	.	12	.
XI	8.0	7.0	6.6	7.2	-	06.2	91	65	83	80	34	058	009.6	09	.	.	04	.	.	.	.	.	01	16	13	13	.	13	.	.	.	.	.	.	01	07	.
XII	9.2	7.7	6.6	7.8	-	04.1	89	79	92	86	45	061	019.0	23	02	05	27	.	.	.	.	.	.	15	12	10	02	07	06	.	.	.	.	.	.	01	14	10
GOD.	7.2	6.9	5.8	6.7	-	07.9	82	63	83	76	-	1136	034.2	28 III	10	19	103	82	20	.	02	.	32	150	151	136	43	128	26	05	.	.	04	.	35	84	71

[illegible]	[illegible]	Temperatura vazduha °C										Učestalost pravaca i srednja jačina vetra nD, Fm (0-12)																				
		Tm										N		NE		E		SE		S		SW		W		NW		C
		7	14	21	[illegible]							f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.
TESLIC — φ = 44° 36' N λ = 17° 52' E Gr. Δ G = + 1h 11 min. — BR. ST. 121																																
I	-	-01.4	01.5	-00.7	-00.3	02.8	-03.4	15.8	05	-16.0	03	28	01.6	.	.	01	01.0	02	02.0	09	02.3	.	.	.	.	.	.	53
II	-	-01.1	03.9	00.1	00.8	05.3	-03.5	18.0	05	-12.6	18.03	27	01.9	02	02.0	.	.	06	02.7	07	03.1	.	.	02	03.0	01	02.0	39
III	-	01.6	08.5	04.0	04.5	09.6	00.2	19.6	27	-13.0	02	37	01.8	08	02.0	.	.	01	02.0	02	03.0	.	.	.	.	.	.	45
IV	-	06.1	14.8	08.5	09.5	16.1	04.4	27.2	20	-02.0	04	24	01.9	06	02.2	02	02.0	02	04.0	01	04.0	04	03.0	02	02.0	01	04.0	48
V	-	08.5	16.9	11.2	12.0	18.0	06.7	27.0	10	-01.0	01	22	01.5	02	03.0	.	.	.	.	01	01.0	01	04.0	02	02.0	05	02.8	60
VI	-	15.0	24.2	16.8	18.2	25.4	13.1	30.0	28	05.8	03	13	01.3	02	01.0	01	01.0	01	04.0	.	.	.	.	02	03.0	.	.	71
VII	-	15.8	23.8	16.9	18.3	24.8	14.1	31.2	24	09.6	17	21	01.3	07	01.7	.	.	.	.	.	.	.	.	01	02.0	.	.	64
VIII	-	15.7	25.3	17.3	18.9	26.1	14.2	31.0	07	07.8	27	13	01.2	08	01.8	02	01.5	.	.	01	02.0	05	02.2	05	01.4	.	.	59
IX	-	10.3	20.1	13.4	14.3	21.1	09.1	33.0	11	00.6	27,24	16	01.4	04	01.5	.	.	.	.	.	.	.	.	05	01.8	.	.	65
X	-	04.6	14.1	08.0	08.7	15.4	03.0	26.2	11,09	-02.0	27,25	27	01.4	04	02.0	.	.	.	.	02	05.0	01	02.0	03	01.7	.	.	56
XI	-	03.1	12.4	06.8	07.3	13.5	01.8	20.6	04,02	-02.6	12	18	01.5	02	02.0	.	.	02	02.0	07	02.9	.	.	02	01.5	.	.	59
XII	-	-01.9	04.8	02.0	01.7	05.9	-03.2	20.6	30	-14.6	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	06.4	14.2	08.7	09.5	15.3	04.7	33.0	11 IX	-16.0	1 I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ZENICA — φ = 44° 13' N λ = 17° 54' E Gr. Δ G = + 1h 12 min. — BR. ST. 122																																
I		729.7	-00.5	02.1	00.1	00.4	02.9	-02.2	12.9	05	-08.7	09	14	02.2	03	01.7	.	.	01	01.0	07	01.3	06	02.0	01	03.0	01	03.0	60
II		727.1	-00.8	05.0	00.6	01.4	06.1	-03.1	16.1	05	-13.6	18	09	02.9	04	01.8	01	01.0	02	02.0	16	01.9	18	02.3	02	03.0	01	01.0	51
III		727.9	01.7	09.0	05.1	05.2	10.5	00.3	20.5	24	-08.6	02	17	02.5	01	02.0	01	02.0	05	02.6	10	02.8	16	02.0	01	02.0	01	02.0	41
IV		729.5	07.2	14.7	09.8	10.4	16.5	04.5	27.8	23	-03.2	05	13	02.9	03	01.7	02	01.5	04	01.2	06	02.5	16	02.5	03	03.3	.	.	4
V		730.8	10.2	17.4	11.8	12.8	18.6	06.9	29.3	10	-00.3	02	12	03.8	05	02.0	04	01.8	06	01.8	06	02.3	18	02.2	01	01.0	03	03.0	38
VI		732.1	15.6	24.4	17.7	18.8	26.2	12.2	31.8	17	05.7	05	11	02.4	02	02.0	04	01.5	02	02.0	10	01.3	04	02.2	01	05.0	.	.	56
VII		731.2	16.0	24.6	18.0	19.2	25.7	12.7	33.8	22	07.7	20	21	02.8	04	02.2	02	01.0	.	.	04	01.2	12	01.9	02	04.0	01	02.0	47
VIII		731.0	16.0	26.2	18.4	19.8	27.2	13.8	34.4	07	09.0	28	10	03.2	03	02.7	03	02.0	04	01.5	05	01.4	10	01.3	.	.	02	04.5	56
IX		734.5	11.2	22.4	14.0	15.4	23.4	09.0	32.8	11	-01.5	30	13	02.5	07	02.1	04	01.5	03	01.0	05	01.4	13	01.5	.	.	.	.	42
X		734.4	05.3	15.1	08.6	09.4	16.3	03.7	25.4	10	-00.9	25	14	02.4	11	02.1	02	01.5	02	01.5	02	03.0	07	01.9	01	02.0	.	.	54
XI		732.9	03.5	11.1	05.5	06.4	12.1	01.9	19.9	04	-03.0	12	06	01.8	.	.	.	.	03	01.7	10	01.9	12	01.7	02	01.5	.	.	57
XII		735.0	-00.9	02.9	00.1	00.5	03.5	-03.0	16.2	30	-12.8	27	02	03.5	01	02.0	.	.	01	01.0	10	01.5	19	01.6	02	02.0	.	.	[illegible]
GOD.		731.3	07.0	14.6	09.1	10.0	15.8	04.7	34.4	7 VIII	-13.6	18 I	142	02.7	44	02.0	23	01.6	33	01.7	91	01.8	151	01.9	16	02.7	09	02.9	500
DOBOJ — φ = 44° 44' N λ = 18° 06' E Gr. Δ G = + 1h 12 min. — BR. ST. 123																																
I	-	-01.7	01.5	-00.6	-00.4	02.5	-03.3	14.6	05	-13.6	03	.	.	07	01.0	10	01.9	08	01.4	04	01.0	05	01.0	02	01.5	08	01.2	49
II	-	-01.1	05.5	00.1	01.1	06.4	-03.0	16.4	05	-13.2	03	03	01.0	.	.	06	02.5	06	01.8	03	02.3	06	02.0	13	01.8	08	01.2	34
III	-	02.9	09.7	05.2	05.7	10.7	01.2	21.6	24	-12.2	02	01	01.0	02	01.5	16	01.8	04	02.2	09	01.2	16	01.7	04	02.0	10	01.5	51
IV	-	08.4	15.3	10.3	11.1	16.9	05.8	27.8	20	-01.7	05	.	.	02	01.5	05	01.6	04	01.5	09	01.7	14	02.4	09	01.9	11	02.1	36
V	-	11.2	18.2	12.2	13.5	19.2	08.3	28.8	10	-00.3	01	01	03.0	03	01.0	06	03.2	06	02.0	02	01.0	12	01.5	09	02.0	09	02.3	43
VI	-	17.2	24.8	18.2	19.6	26.1	13.4	31.7	23	05.8	03	.	.	03	02.0	02	01.5	06	01.3	11	01.2	05	01.2	08	01.8	01	03.0	54
VII	-	17.3	24.9	18.5	19.8	25.8	14.1	33.0	15	09.8	20	03	02.0	06	01.8	03	02.0	04	02.2	05	01.0	16	01.4	09	01.4	05	02.0	42
VIII	-	16.9	26.2	18.9	20.3	27.1	14.9	35.0	07	09.2	27	.	.	01	02.0	05	01.8	06	02.0	04	01.2	03	01.7	10	01.7	05	02.4	50
IX	-	12.4	22.9	14.0	15.8	23.4	10.7	34.8	11	00.2	30	04	02.2	02	01.5	05	01.8	08	01.8	01	01.0	04	01.2	06	01.5	03	02.0	57
X	-	06.0	16.3	08.5	09.8	16.9	04.6	26.0	10,09	-01.8	25,17	.	.	04	01.8	01	01.0	08	01.8	02	02.5	03	01.0	07	01.7	02	02.0	66
XI	-	04.9	13.1	07.0	08.0	13.7	03.6	21.2	19,03	-01.2	13	.	.	.	.	06	02.0	16	01.9	04	02.0	13	01.5	05	02.4	.	.	46
XII	-	-01.3	03.4	-00.1	00.5	03.8	-03.0	15.7	01	-13.8	27	.	.	.	.	02	01.0	06	02.0	03	01.0	09	01.0	07	01.1	03	01.7	6[illegible]
GOD.	-	07.8	15.2	09.4	10.4	16.0	05.6	35.0	7 VIII	-13.8	27 XII	12	01.8	30	01.5	67	02.0	82	01.8	57	01.4	106	01.6	89	01.7	65	01.8	507
MODRICA — φ = 44° 59' N λ = 18° 17' E Gr. Δ G = + 1h 13 min. — BR. ST. 124																																
I	-	-02.3	00.9	-01.5	-01.1	01.8	-04.2	10.0	05	-12.8	21	14	02.1	01	02.0	07	02.3	02	02.0	02	01.5	02	02.0	23	02.2	.	.	4[illegible]
II	-	-00.9	03.7	-00.1	00.6	05.4	-03.2	16.4	09	-11.6	17	22	02.6	02	02.0	06	01.8	.	.	01	01.0	01	02.0	27	02.8	.	.	2[illegible]
III	-	02.9	09.3	04.7	05.4	10.6	00.8	20.8	24	-11.6	02	24	02.4	06	02.0	15	02.4	.	.	02	01.0	03	04.0	36	02.6	.	.	57
IV	-	07.5	14.8	09.8	10.5	16.2	04.5	28.4	20	00.4	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	10.8	18.4	12.4	13.5	19.4	07.0	27.4	09	01.8	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	17.5	26.0	19.2	20.5	26.6	12.5	32.0	23	07.2	03	10	02.1	06	02.0	10	02.0	.	.	.	.	05	02.6	36	02.3	03	02.7	20
VII	-	18.3	25.1	18.8	20.2	26.1	13.8	32.4	15	06.8	16	06	02.0	04	02.2	06	02.3	.	.	04	01.5	.	.	34	02.0	14	02.6	25
VIII	-	17.5	25.8	18.1	19.9	26.5	14.7	34.8	07	10.5	28	03	02.3	06	02.5	06	02.8	03	01.7	.	.	25	02.6	02	02.5	48	03.1	.
IX	-	13.0	21.9	13.8	15.6	22.8	09.4	32.0	11	-01.0	30	05	02.0	05	02.6	06	02.0	03	02.7	.	.	.	.	.	.	68	02.4	67
X	-	06.1	15.3	09.0	09.8	16.0	04.3	25.0	09,08	-02.0	20	04	01.5	.	.	08	02.2	02	02.5	.	.	.	.	01	02.0	68	02.4	10
XI	-	05.3	12.6	07.0	08.0	13.7	03.5	21.5	19	00.0	13	03	03.3	01	02.0	03	01.7	02	01.5	07	02.4	01	02.0	06	03.3	31	02.8	36
XII	-	-00.7	03.2	00.9	01.1	03.9	-	15.6	01	-	-	06	01.5	03	01.7	05	02.4	.	.	04	03.2	02	02.0	44	03.1	09	02.6	20
GOD.	-	07.9	14.8	09.3	10.3	15.8	-	34.8	7 VIII	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
MAOČA — φ = 44° 19' N λ = 18° 26' E Gr. Δ G = + 1h 14 min. — BR. ST. 125																																
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	10.7	16.1	10.6	12.0	17.7	07.0	28.5	10	00.4	01	01	01.0	04	02.0	19	01.7	06	01.7	.	.	03	01.3	04	01.0	18	01.3	38
VI	-	16.4	23.3	16.0	17.9	24.7	12.3	31.0	18	06.2	03	.	.	03	02.0	18	01.7	01	03.0	.	.	01	01.0	03	01.3	11	01.6	53
VII	-	16.9	23.3	16.1	18.1	24.4	12.7	34.0	24	08.2	19	01	01.0	.	.	18	01.5	.	.	.	.	.	.	03	01.0	16	01.3	55
VIII	-	16.7	25.0	16.7	18.8	25.8	13.3	33.5	07	07.8	29	02	01.5	.	.	22	01.6	01	01.0	.	.	01	01.0	01	01.0	20	01.4	46
IX	-	12.5	20.9	12.6	14.6	22.3	09.6	33.5	12,11	-00.4	30,29	01	01.0	02	01.0	24	01.8	.	.	.	.	.	.	03	01.3	17	01.5	43
X	-	06.6	14.1	07.6	09.0	15.7	04.3	24.0	10,09	-02.4	17	02	01.0	03	05.0	25	01.6	.	.	.	.	.	.	02	01.0	15	01.1	46
XI	-	05.4	11.4	06.3	07.4	12.8	02.5	20.5	03	-03.2	27	.	.	02	01.0	46	01.7	05	04.4	.	.	01	01.0	.	.	09	01.0	27
XII	-	-00.9	02.9	-00.1	00.5	04.3	-03.4	16.0	30	-10.8	26	01	01.0	02	01.0	23	01.2	04	02.0	04	01.5	03	01.0	02	01.0	26	01.0	28
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha °m mm	Um % 7	14	21	Sred. (Dies)	min	Padavine R mm Σ	Max	Broj dana n sa: Tn ≤ -20,0	Tn ≤ -10,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 8,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⚹	⚹	△	∽	▲	▲	⊤	≡	▦
TESLIĆ																																					
BR. ST. 121																																					
H_o = 210 m H_b = - m h_v = 2,0 m h_r = 1,0 m																																					
I	8.5	8.9	9.4	8.9	-	04.4	94	92	95	94	67	114	040.4	17	02	10	22	.	.	.	.	.	24	13	12	03	08	07	.	.	.	.	.	.	03	31
II	7.8	7.8	6.2	7.3	-	04.7	93	87	94	91	52	164	028.0	24	05	05	22	.	.	.	02	.	01	14	18	16	07	08	12	01	.	.	.	.	.	01	25
III	7.9	7.2	5.8	7.0	-	05.5	93	74	90	85	33	101	026.2	28	01	01	12	.	.	.	.	.	03	15	14	14	03	10	10	03	.	.	.	.	.	05	12
IV	6.8	7.9	7.0	7.2	-	07.7	93	66	92	84	43	108	048.2	15	.	.	02	05	.	.	.	.	01	12	13	12	03	13	01	.	.	.	.	.	.	.	.
V	6.9	7.4	4.9	6.4	-	09.0	95	66	93	85	33	135	028.6	23	.	.	01	02	.	.	.	.	01	11	16	15	05	16	01	01	.	.	.	.	.	.	.
VI	4.8	5.8	3.8	4.8	-	12.4	93	54	89	79	25	137	042.6	19	.	.	.	19	01	.	.	.	07	06	17	14	05	17	.	.	.	.	.	.	04	.	.
VII	4.1	5.4	3.5	4.3	-	13.1	94	62	94	83	35	136	036.4	26	.	.	.	20	06	.	.	.	11	08	13	12	04	13	.	.	.	.	.	.	01	02	.
VIII	4.2	4.4	1.9	3.5	-	12.8	94	51	92	79	32	108	026.8	24	.	.	.	21	07	.	.	.	12	04	10	10	04	10	.	.	.	.	.	.	06	06	.
IX	4.8	4.7	2.6	4.0	-	10.4	94	59	94	82	36	043	018.4	18	.	.	.	11	03	.	.	.	11	06	06	05	01	06	.	.	.	.	.	.	01	10	.
X	4.8	5.8	4.3	5.0	-	07.0	95	61	94	83	30	112	040.2	02	.	.	06	03	.	.	01	.	13	11	09	08	04	09	.	.	.	.	.	.	.	07	.
XI	6.0	7.0	6.4	6.5	-	06.4	94	64	94	84	28	102	024.6	17	.	.	08	.	.	.	.	.	07	13	12	12	04	12	.	.	.	.	.	.	.	04	.
XII	7.5	7.6	7.4	7.5	-	04.8	91	85	93	89	47	054	018.4	23	03	05	25	.	.	.	.	.	04	21	08	08	02	03	05	.	.	.	.	.	.	11	10
GOD.	6.2	6.7	5.3	6.0	-	08.2	93	68	92	84	25	1314	048.2	15 IV	11	21	98	81	17	.	03	.	71	145	149	138	45	125	36	05	.	.	.	.	12	49	78
ZENICA																																					
BR. ST. 122																																					
H_o = 344 m H_b = 348,0 m h_v = 2,0 m h_r = 1,0 m																																					
I	9.7	8.3	7.6	8.5	019.5	04.2	91	77	88	86	61	115	032.6	02	.	05	22	.	.	.	01	.	.	21	17	12	03	10	10	02	.	.	.	.	.	09	20
II	8.9	6.5	6.0	7.2	075.0	03.9	87	61	80	76	28	110	022.5	16	02	05	20	.	.	.	08	03	.	10	20	12	06	10	12	02	.	.	.	.	01	01	16
III	8.0	7.4	6.3	7.2	103.2	04.6	84	55	72	70	23	071	018.8	06	.	01	14	.	.	.	08	01	02	17	16	11	02	12	07	02	.	.	.	.	.	01	03
IV	6.3	8.4	5.9	6.9	133.5	05.9	77	46	66	63	22	055	025.0	15	.	.	04	03	.	.	13	01	.	11	14	09	01	14	02	.	.	.	.	.	01	.	.
V	6.5	7.9	5.4	6.6	127.0	07.3	79	49	73	67	20	100	047.2	23	.	.	01	02	.	.	08	01	03	12	17	09	02	17	01	.	.	.	.	.	04	.	.
VI	5.7	6.0	3.3	5.0	185.6	11.6	84	51	77	71	33	064	020.0	19	.	.	.	22	05	.	12	02	05	04	15	08	02	15	.	.	.	.	.	.	11	04	.
VII	5.0	4.8	3.3	4.4	236.9	11.8	82	52	78	71	33	044	018.4	17	.	.	.	20	07	.	04	.	13	09	09	08	01	09	.	.	.	.	.	.	04	06	.
VIII	7.2	4.9	3.0	5.0	204.4	12.8	90	50	84	75	29	045	012.7	22	.	.	.	20	10	.	06	02	04	04	13	09	01	13	.	.	.	.	.	.	05	07	.
IX	7.2	4.2	2.3	4.6	172.2	09.6	90	47	81	72	25	013	004.0	05	.	.	01	12	05	.	.	.	06	03	05	05	.	05	.	.	.	.	.	.	.	10	.
X	7.5	5.0	4.8	5.8	119.3	06.9	91	57	83	77	27	083	028.6	02	.	.	03	03	.	.	02	.	06	12	10	08	03	10	.	.	.	.	.	.	02	13	.
XI	6.8	6.1	6.0	6.3	082.9	05.7	90	62	86	79	37	058	011.3	16	.	.	05	.	.	.	01	.	02	08	12	10	01	12	.	.	.	.	.	.	.	05	.
XII	8.6	7.7	7.4	7.9	009.3	04.2	90	77	85	84	31	048	012.0	26	03	09	25	.	.	.	.	.	01	19	14	09	01	10	06	01	.	.	.	.	.	02	08
GOD.	7.3	6.4	5.1	6.3	1468.8	07.4	86	57	79	74	20	806	047.2	15 V	05	20	95	82	27	.	63	10	42	130	162	110	23	137	38	07	.	.	.	.	28	58	47
DOBOJ																																					
BR. ST. 123																																					
H_o = 146 m H_b = - m h_v = 2,0 m h_r = 1,0 m																																					
I	9.1	8.3	7.5	8.3	025.9	04.2	98	85	93	92	52	134	035.0	02	03	09	24	.	.	.	.	.	.	21	16	12	03	10	10	02	.	.	.	.	.	10	31
II	8.5	7.7	6.3	7.5	070.5	04.3	95	70	91	85	33	129	018.5	12	04	06	22	.	.	.	02	.	.	11	19	14	06	09	13	03	.	.	.	.	.	06	22
III	8.6	7.4	7.2	7.7	107.8	05.4	89	63	82	78	34	097	027.2	28	01	.	09	.	.	.	.	.	.	17	18	15	03	14	09	04	.	.	.	.	.	05	07
IV	6.2	7.8	4.6	6.2	142.3	07.2	85	55	78	73	24	084	031.6	15	.	.	03	05	.	.	01	.	01	08	13	11	03	13	.	.	.	.	.	.	01	02	.
V	6.0	7.4	5.8	6.4	138.0	08.9	88	58	84	77	30	113	029.6	23	.	.	01	04	.	.	02	.	01	05	17	13	03	17	01	.	.	.	.	.	04	08	.
VI	5.0	5.7	4.0	4.9	234.0	13.4	89	57	86	77	37	130	048.1	19	.	.	.	21	03	.	02	01	06	04	16	13	04	16	.	.	.	.	.	01	09	.	.
VII	4.1	5.4	3.6	4.4	248.1	13.4	88	58	87	77	35	086	024.0	17	.	.	.	20	09	.	01	.	10	09	11	09	04	11	.	.	.	.	.	01	01	04	.
VIII	5.7	4.7	2.9	4.5	216.0	14.5	95	58	90	81	36	087	027.0	23	.	.	.	21	07	.	.	.	06	02	12	09	03	12	.	.	.	.	.	.	04	15	.
IX	6.4	4.2	2.8	4.5	192.6	10.9	95	53	91	80	24	049	015.0	17	.	.	.	12	06	.	.	.	06	04	06	05	02	06	.	.	.	.	.	.	01	15	.
X	6.5	5.5	4.3	5.4	144.0	07.8	97	62	93	84	39	083	030.5	02	.	.	02	05	.	.	.	.	06	09	10	08	03	10	.	.	.	.	.	.	.	17	.
XI	6.8	6.6	5.3	6.2	091.9	06.8	94	68	89	84	39	076	013.9	24	.	.	02	.	.	.	.	.	03	09	13	11	02	13	.	.	.	.	.	.	.	08	.
XII	8.5	7.5	6.9	7.6	038.5	04.5	96	84	93	91	38	056	015.5	23	03	05	26	.	.	.	.	.	02	17	14	09	01	09	05	.	.	.	.	.	.	12	10
GOD.	6.8	6.5	5.1	6.1	1649.6	08.4	92	64	88	81	24	1124	048.1	49 VI	11	20	89	88	25	.	08	01	41	116	165	129	37	140	38	09	.	.	.	02	20	102	70
MODRIČA																																					
BR. ST. 124																																					
H_o = 115 m H_b = - m h_v = 2,0 m h_r = 1,0 m																																					
I	9.7	8.4	8.0	8.7	-	03.9	90	89	90	90	77	119	033.5	17	03	08	25	.	.	.	.	.	.	22	17	13	02	08	09	.	01	.	.	.	.	12	28
II	8.5	7.0	6.6	7.4	-	-	-	-	-	-	-	136	017.4	12	03	05	20	.	.	.	01	.	.	14	20	17	07	08	16	.	.	.	.	.	.	06	21
III	6.6	5.5	6.0	6.1	-	05.7	90	69	91	83	28	106	031.2	28	01	01	08	.	.	.	04	01	02	09	17	14	03	13	07	01	.	01	.	.	.	04	05
IV	5.9	5.9	5.9	5.9	-	07.3	82	64	80	76	33	113	027.4	09	.	.	.	04	.	.	06	01	03	08	17	14	04	17	.	.	.	.	.	.	02	04	.
V	6.6	6.5	5.9	6.3	-	08.7	78	64	76	73	34	085	026.0	23	.	.	.	07	.	.	04	02	02	09	18	16	02	18	.	.	.	.	.	.	06	.	.
VI	5.5	5.4	5.1	5.3	-	12.3	74	54	71	67	41	144	030.4	11	.	.	.	24	05	.	04	01	02	06	17	12	05	17	.	.	.	.	.	01	10	.	.
VII	4.2	3.8	4.0	4.0	-	12.9	81	56	79	72	32	097	019.4	17	.	.	.	20	12	.	03	.	12	06	13	10	05	12	.	.	.	.	.	01	02	.	.
VIII	5.1	4.3	2.8	4.1	-	14.4	82	72	81	78	46	-	-	-	.	.	.	22	07	.	01	01	09	05	-	-	-	-	-	.	.	.	.	-	-	.	03	.
IX	6.1	2.5	3.1	3.9	-	11.0	80	69	78	76	52	028	007.0	17	.	.	01	10	03	.	01	.	09	04	06	06	.	06	.	.	.	.	.	.	02	05	.
X	-	-	-	-	-	07.3	81	70	77	76	46	066	022.0	02	.	.	01	02	.	.	01	.	-	-	07	07	02	07	.	.	.	.	.	.	.	11	.
XI	5.3	5.3	6.3	5.6	-	06.6	83	73	80	79	55	049	007.7	11	.	.	.	.	.	.	02	.	06	10	12	12	.	12	.	.	.	.	.	.	.	09	.
XII	7.0	6.8	7.5	7.1	-	-	-	-	-	-	-	-	-	-	-	03	-	.	.	-	04	01	03	16	-	-	-	-	-	.	.	.	.	.	.	15	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		-	17	-	89	27	-	31	07	-	-	-	-	-	-	-	-	01	01	-	-	22	69	-
MAOČA																																					
BR. ST. 125																																					
H_o = 335 m H_b = - m h_v = 2,0 m h_r = 1,0 m																																					
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	6.3	7.3	5.8	6.5	-	08.8	87	68	91	82	40	192	052.8	19	.	.	.	01	.	.	.	.	01	11	21	16	05	21	.	.	.	.	.	.	03	06	.
VI	4.4	5.4	4.0	4.6	-	13.1	86	67	93	82	46	105	022.7	20	.	.	.	20	01	.	.	.	09	06	18	11	04	18	.	.	.	.	.	.	03	03	.
VII	4.1	5.0	3.7	4.3	-	13.5	85	71	94	83	41	150	050.1	06	.	.	.	19	05	.	.	.	12	09	12	09	05	12	.	.	.	.	.	.	01	06	.
VIII	3.9	5.3	3.1	4.1	-	14.7	89	72	97	86	57	090	029.0	09	.	.	.	21	05	.	.	.	09	03	12	11	03	12	.	.	.	.	.	.	05	02	.
IX	4.6	4.2	3.1	4.0	-	11.2	90	70	94	84	40	047	011.5	18	.	.	02	11	06	.	.	.	12	04	08	06	02	08	.	.	.	.	.	.	.	08	.
X	4.4	5.4	4.7	4.8	-	07.9	89	78	96	87	56	122	031.4	04	.	.	01	.	.	.	02	.	11	09	09	09	04	09	.	.	.	.	.	.	.	12	.
XI	5.3	5.1	5.4	5.3	-	06.6	87	76	89	84	30	115	030.7	74	.	.	04	.	.	.	03	.	05	08	12	11	06	12	.	.	.	.	.	.	.	09	.
XII	6.5	6.4	5.3	6.1	-	04.2	85	77	86	83	30	055	010.6	26	02	06	28	.	.	.	.	.	04	10	12	11	02	07	06	.	.	.	.	.	.	01	.
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Cestina pravaca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												d.	j.	d.	j.	d.	j.	d.	j.	d.	j.	d.	j.		j.	d.	j.	d.
TUZLA φ = 44° 33' N λ = 18° 42' E Gr. Δ G = + 1h 15 min.																												BR. ST. 126
I	733.7	-01.3	02.3	-00.3	00.1	03.8	-03.4	16.4	05	-10.6	09	01	02.0	11	01.3	02	01.5	02	01.5	.	.	02	01.0	06	01.2	01	02.0	65
II	730.9	-00.7	05.0	00.2	01.2	06.2	-03.4	16.6	05	-13.6	18	.	.	07	01.9	.	.	05	01.6	01	01.0	02	01.5	11	02.1	06	01.3	52
III	731.9	02.4	09.2	05.0	05.4	10.5	00.8	21.2	24	-09.0	02	02	01.0	06	01.5	04	02.0	06	02.5	03	02.0	03	01.7	08	01.4	10	01.5	51
IV	733.2	07.6	14.4	10.0	10.5	16.7	04.8	27.3	20	-03.2	05	01	01.0	06	01.2	01	02.0	05	01.2	.	.	02	01.5	12	02.2	14	01.8	49
V	734.5	10.2	16.5	11.5	12.4	18.2	07.4	29.5	10	-00.8	01	.	.	02	02.0	.	.	02	01.5	.	.	05	01.2	13	01.9	08	01.5	63
VI	735.7	15.8	23.8	17.1	18.5	25.2	12.3	30.2	17	06.0	03	.	.	04	01.5	.	.	02	01.0	04	01.8	03	01.3	10	01.4	03	02.0	64
VII	734.9	16.5	23.7	17.3	18.7	24.7	13.3	33.0	25	08.4	19	01	01.0	06	01.0	01	01.0	02	01.0	.	.	.	.	07	01.7	08	01.4	68
VIII	734.8	16.3	24.9	17.9	19.3	26.1	13.8	33.2	07	07.9	27	.	.	07	01.1	.	.	03	01.0	.	.	.	.	09	01.7	07	01.3	67
IX	738.3	11.5	21.0	13.0	14.7	22.3	09.5	33.4	11	-01.4	30	01	01.0	19	01.3	02	01.5	04	01.2	.	.	.	.	02	01.0	07	01.4	55
X	738.1	05.6	14.9	08.3	09.3	16.2	04.2	26.4	10	-01.6	25	02	01.0	15	01.5	02	02.0	01	01.0	.	.	.	.	06	01.5	06	01.5	61
XI	736.5	04.7	12.1	06.6	07.5	13.4	02.8	22.6	03	-02.2	26	.	.	20	01.5	01	01.0	04	01.2	01	01.0	03	02.3	08	01.4	06	01.3	47
XII	738.6	-00.9	03.3	00.1	00.6	04.3	-02.6	17.4	30	-12.0	27	01	01.0	09	01.6	.	.	02	01.0	.	.	.	.	07	01.6	06	01.2	68
GOD.	735.1	07.3	14.3	08.9	09.8	15.6	05.0	33.4	4 IX	-13.6	18 II	09	01.1	112	01.4	13	01.7	38	01.4	09	01.7	20	01.5	99	01.7	82	01.5	710
BRČKO φ = 44° 53' N λ = 18° 49' E Gr. Δ G = + 1h 15 min.																												BR. ST. 127
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	12.8	18.0	15.2	15.3	-	10.5	-	-	02.5	01	04	01.2	04	01.0	06	01.0	03	01.3	01	02.0	05	01.6	08	01.0	43	01.2	19
VI	-	18.3	25.0	20.4	21.0	-	-	-	-	-	-	07	01.0	12	01.1	03	01.0	06	01.0	02	01.0	03	01.0	02	01.0	41	01.2	14
VII	-	18.5	24.7	19.8	20.7	25.1	-	32.2	15	-	-	14	01.0	03	01.0	12	01.0	02	01.0	.	.	02	01.0	09	01.1	29	01.1	22
VIII	-	18.5	25.9	20.0	21.1	26.1	15.6	31.8	07	11.2	19	12	01.0	08	01.0	08	01.0	05	01.0	.	.	01	01.0	11	01.1	24	01.2	24
IX	-	15.1	22.4	16.6	17.6	22.9	-	32.2	12,11	-	-	23	01.0	11	01.0	05	01.0	03	01.0	.	.	01	01.0	15	01.1	22	01.1	10
X	-	07.4	15.6	10.1	10.8	16.4	06.3	24.6	09,08	01.4	27	12	01.0	14	01.0	10	01.1	03	01.0	.	.	04	01.0	12	01.0	30	01.0	08
XI	-	05.7	12.4	08.6	08.8	13.9	04.5	22.0	03	-00.4	13,12	05	01.0	11	01.0	12	01.0	14	01.0	04	01.5	13	01.4	03	01.0	21	01.2	07
XII	-	00.2	03.6	01.5	01.7	04.1	-01.2	15.4	01	-07.4	27	21	01.0	05	01.0	10	01.0	14	01.1	01	01.0	05	01.0	11	01.4	24	01.3	02
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VLASENICA φ = 44° 12' N λ = 18° 57' E Gr. Δ G = + 1h 16 min.																												BR. ST. 128
I	-	00.1	02.0	00.4	00.7	04.2	-02.9	12.8	14	-09.4	20	20	01.1	12	01.7	19	01.4	11	02.8	03	06.3	02	02.0	09	01.0	08	01.6	09
II	-	00.2	02.9	00.4	01.0	04.5	-03.6	13.4	05	-10.8	16	21	01.3	08	01.6	17	01.3	18	03.4	04	05.5	.	.	02	01.0	10	01.0	04
III	-	02.5	07.0	04.0	04.4	08.5	00.3	19.8	25	-08.6	02	25	01.2	09	01.8	13	01.4	20	02.9	.	.	06	02.7	01	01.0	14	01.6	05
IV	-	08.8	12.6	08.6	09.6	14.5	04.8	25.0	20	-02.8	04	10	01.3	09	02.0	05	02.0	10	03.1	.	.	12	03.0	16	01.9	24	02.0	04
V	-	10.5	14.5	10.6	11.5	16.0	07.0	28.0	10	-00.2	01	05	01.8	04	02.0	10	01.3	13	02.8	.	.	12	02.9	15	01.4	30	01.9	04
VI	-	16.9	20.9	16.1	17.5	22.1	12.7	28.8	22	05.4	03	01	02.0	04	01.2	13	01.6	03	02.0	02	04.0	04	02.8	28	01.3	24	01.9	11
VII	-	17.2	21.5	16.7	18.0	22.9	13.1	30.0	23	07.8	18	.	.	02	02.0	25	01.5	11	02.4	01	01.0	12	02.3	26	01.3	07	01.7	08
VIII	-	17.6	22.7	17.4	18.8	-	13.9	-	-	09.2	27	01	01.0	08	01.0	22	01.6	15	02.1	.	.	19	02.1	17	01.2	05	01.2	06
IX	-	13.7	18.7	14.0	15.1	20.1	10.3	29.8	11	00.4	29	03	01.0	09	01.2	15	01.5	03	01.7	.	.	06	02.0	20	01.0	28	01.2	06
X	-	08.0	12.6	08.8	09.5	14.3	05.1	23.6	10	-00.2	17	13	01.3	16	01.1	13	01.4	07	02.7	.	.	03	03.0	13	01.1	26	01.2	02
XI	-	06.0	10.0	06.8	07.4	11.8	03.5	19.0	01	-03.4	27	05	01.2	08	01.2	15	01.6	17	05.4	02	03.0	04	02.5	17	01.1	16	01.6	06
XII	-	00.1	02.5	00.8	01.1	03.7	-02.2	14.4	30	-07.4	18	33	01.0	08	01.5	10	01.0	09	03.8	.	.	08	02.4	12	01.0	09	01.7	04
GOD.	-	08.5	12.3	08.7	09.6	-	05.2	-		-10.8	16 II	137	01.2	97	01.5	177	01.5	137	03.1	12	04.7	88	02.5	176	01.2	201	01.6	69
BIJELJINA φ = 44° 46' N λ = 19° 16' E Gr. Δ G = + 1h 17 min.																												BR. ST. 129
I	-	-01.4	00.9	-01.2	-00.7	02.0	-03.3	08.2	05	-11.8	09	.	.	02	01.0	08	01.0	.	.	03	01.0	01	01.0	08	01.2	03	01.3	68
II	-	-01.0	04.7	00.7	01.3	06.2	-02.7	16.6	10	-12.2	03	.	.	05	01.0	06	01.2	.	.	02	01.0	02	01.0	04	01.0	07	01.6	58
III	-	02.8	09.8	04.9	05.6	10.9	00.9	21.6	24	-09.4	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	08.6	15.6	09.7	10.9	17.1	05.4	27.5	20	-01.8	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	12.5	18.3	12.8	14.1	19.4	07.6	28.6	10	02.8	02	21	01.2	.	.	08	01.2	01	01.0	06	01.2	07	01.1	25	01.3	16	01.6	09
VI	-	17.9	24.9	17.9	19.6	26.0	14.5	30.8	23,18	08.0	03	04	01.0	01	01.0	12	01.0	05	01.0	04	01.0	04	01.0	21	01.3	06	01.3	33
VII	-	18.2	24.8	18.8	20.2	25.9	14.5	33.2	15	10.4	18	02	01.0	01	01.0	10	01.0	07	01.0	04	01.0	02	01.0	18	01.1	16	01.2	33
VIII	-	18.4	26.3	19.0	20.7	27.1	15.2	33.4	08,07	10.0	27	02	01.0	02	01.0	04	01.0	03	01.0	03	01.0	.	.	15	01.1	08	01.0	56
IX	-	13.6	22.4	14.3	16.1	23.2	10.5	34.2	11	-01.7	29	02	01.0	.	.	08	01.0	01	01.0	01	01.0	01	01.0	11	01.0	11	01.0	55
X	-	06.7	16.0	09.0	10.2	17.1	04.9	25.8	07	-00.8	25	03	01.0	.	.	07	01.1	02	01.0	05	01.0	.	.	20	01.1	07	01.0	49
XI	-	05.6	12.3	06.9	07.9	13.5	03.3	22.9	03	-00.8	07	.	.	.	.	03	01.0	01	01.0	04	01.0	05	01.2	08	01.0	02	01.0	67
XII	-	00.1	03.7	01.0	01.5	04.8	-01.9	15.5	01	-15.6	27	01	01.0	.	.	04	01.0	02	01.0	02	01.0	02	01.0	13	01.0	07	01.1	62
GOD.	-	08.5	15.0	09.5	10.6	16.1	05.7	34.2	4 IX	-15.6	17 XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SREBRENICA φ = 44° 07' N λ = 19° 18' E Gr. Δ G = + 1h 17 min.																												BR. ST. 130
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	11.8	18.6	14.1	14.7	21.7	08.5	32.0	11	-01.0	30	.	.	.	.	06	01.8	51	01.8	15	01.9	10	02.0	02	02.0	03	02.0	03
X	-	06.1	11.0	07.1	07.8	-	-	-	-	-	-	.	.	.	.	01	01.0	68	02.0	24	02.0	.	.	.	.	.	.	.
XI	-	05.1	09.4	06.1	06.7	10.8	-	18.0	21,03	-	-	.	.	.	.	20	01.8	55	01.9	12	01.9	03	01.7	.	.	.	.	.
XII	-	-00.8	02.0	00.0	00.3	03.2	-02.9	16.0	30	-08.0	18	01	01.0	.	.	07	01.3	46	01.6	17	01.8	22	01.4	.	.	.	.	.
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dles)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dles)	Min	Padavine R mm Σ	Max	Max.	Broj dana n sa: Tn ≤-20,0	Tx ≤0,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) ≤3,0	≥8,0	R mm ≥0,1	≥1,0	≥10,0	●	●	≡	≡	≡	▲	▲	T	≡	≡
TUZLA BR. ST. 126 — H_o = 305 m H_b = 306.5 m h_o = 2.0 m h_r = 1.0 m																																					
I	8.9	8.1	7.4	8.1	034.5	04.0	93	77	89	86	43	112	040.9	02	02	07	22	.	.	.	.	.	01	21	17	11	03	13	11	02	.	02	.	.	.	14	31
II	9.0	7.9	6.1	7.7	069.7	04.0	89	61	87	79	28	120	022.2	12	03	06	21	.	.	.	02	.	.	14	16	11	04	09	12	02	01	.	.	.	.	07	19
III	7.5	7.2	6.4	7.0	124.4	04.7	82	57	76	72	25	091	024.7	28	.	01	13	.	.	.	.	.	03	17	18	13	03	13	09	.	.	.	.	.	.	01	06
IV	5.9	8.4	5.3	6.5	143.2	06.2	78	51	66	65	20	090	039.1	15	.	.	05	04	.	.	01	.	.	09	15	11	03	15	01	.	.	.	.	.	01	01	.
V	7.5	8.0	6.5	7.3	132.0	08.0	87	58	80	75	32	126	030.3	18	.	.	01	04	.	.	.	.	.	12	23	11	05	22	01	.	.	.	.	.	09	07	.
VI	5.4	5.8	4.1	5.1	214.4	12.4	89	56	85	77	33	177	051.9	19	.	.	.	20	02	.	01	.	07	06	16	10	05	16	.	.	.	.	.	03	11	05	.
VII	4.0	5.6	3.9	4.5	253.7	12.5	86	58	84	77	36	150	032.2	06	.	.	.	20	07	.	.	.	10	09	10	08	06	10	.	.	.	.	.	01	01	04	.
VIII	4.9	5.4	2.9	4.4	240.5	13.2	92	55	90	79	38	097	052.7	23	.	.	.	19	06	.	.	.	07	02	11	08	03	11	.	.	.	.	.	.	13	09	.
IX	5.0	4.7	3.0	4.2	196.8	09.9	92	52	90	78	26	054	018.4	17	.	.	02	10	04	.	.	.	10	04	09	06	02	09	.	.	.	.	.	01	01	07	.
X	5.5	5.4	5.3	5.4	155.1	07.0	93	58	89	80	35	096	028.9	22	.	.	02	.	.	.	.	.	09	12	12	08	04	12	.	.	.	.	.	.	.	07	.
XI	7.2	6.9	5.9	6.7	099.5	06.0	88	62	85	79	21	074	013.7	17	.	.	04	.	.	.	.	.	03	12	15	10	04	15	.	.	.	.	.	.	.	08	.
XII	7.6	6.9	6.8	7.1	057.6	04.2	90	77	87	85	38	047	011.2	29	02	05	25	.	.	.	.	.	03	15	12	08	01	06	07	01	01	.	.	.	.	08	09
GOD.	6.5	6.7	5.3	6.2	1721.4	07.7	88	60	84	77	20	1234	052.7	11 VII	07	19	95	77	19	.	04	.	53	133	174	115	43	151	41	05	02	02	.	05	36	78	65
BRČKO BR. ST. 127 — H_o = 96 m H_b = - m h_o = 2.0 m h_r = 1.0 m																																					
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	6.3	6.2	5.6	6.0	-	09.5	79	64	73	72	18	113	051.2	23	.	-	.	-	-	.	03	01	02	08	15	12	02	15	.	.	.	.	.	.	05	-	.
VI	4.9	5.3	3.3	4.5	-	14.3	83	66	76	75	43	102	022.5	19	-	-	-	-	-	-	02	02	05	02	14	10	03	14	.	.	.	.	.	.	09	01	.
VII	3.6	4.4	3.6	3.9	-	15.1	86	69	87	80	42	120	026.4	06	-	.	-	19	08	-	.	.	11	05	09	09	06	09	.	.	.	.	.	.	01	-	.
VIII	3.8	3.2	2.4	3.1	-	15.9	88	71	88	83	54	115	026.0	03	.	.	.	20	04	03	.	.	10	01	11	09	05	11	.	.	.	.	.	.	06	04	.
IX	5.5	4.5	4.1	4.7	-	12.7	87	69	86	81	47	034	017.6	17	-	.	-	11	03	-	.	.	05	02	07	05	01	07	.	.	.	.	.	.	-	-	.
X	5.1	5.5	5.7	5.4	-	08.6	93	72	92	86	36	037	018.5	22	.	.	.	.	.	.	-	-	09	08	07	06	01	07	.	.	.	.	.	.	-	-	.
XI	6.8	6.4	6.9	6.7	-	07.5	89	78	91	86	43	058	010.2	11	.	.	03	.	.	.	.	.	02	12	12	10	01	11	.	.	.	.	.	.	.	05	.
XII	8.0	6.8	6.1	7.0	-	04.7	89	85	91	89	53	053	020.4	23	.	04	21	.	.	.	.	.	03	14	12	08	02	07	05	.	.	.	.	.	.	-	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VLASENICA BR. ST. 128 — H_o = 680 m H_b = - m h_o = 2.0 m h_r = 1.0 m																																					
I	8.1	7.9	6.2	7.4	-	04.2	82	83	84	83	48	086	021.4	02	.	08	21	.	.	.	01	03	01	15	14	13	04	05	11	.	.	01	.	.	.	07	25
II	8.0	7.6	6.4	7.3	-	04.1	84	76	82	81	52	168	038.2	24	01	09	21	.	.	.	03	03	.	12	18	17	06	07	15	01	.	.	.	.	.	02	21
III	6.6	6.5	4.8	6.0	-	04.7	81	66	77	75	35	105	035.0	28	.	01	16	.	.	.	01	.	05	10	15	11	03	06	13	02	.	.	.	.	.	03	14
IV	6.1	7.1	4.4	5.8	-	06.2	67	61	72	67	25	115	034.9	15	.	.	05	01	.	.	01	01	01	08	14	12	03	11	05	.	.	.	.	.	04	.	-
V	6.9	8.0	7.2	7.4	-	08.3	77	74	84	78	38	176	040.6	23	.	.	01	01	.	.	03	.	01	15	19	17	06	18	03	01	.	.	.	01	06	.	.
VI	4.7	5.9	4.6	5.1	-	12.2	78	73	83	78	48	165	032.8	30	.	.	.	06	.	.	01	01	05	07	19	18	06	19	.	.	.	.	.	02	12	.	.
VII	4.3	5.1	3.5	4.2	-	13.0	82	73	86	80	49	125	041.2	06	.	.	.	14	01	.	02	.	12	09	11	11	03	11	.	.	.	.	.	.	03	02	.
VIII	4.7	5.1	4.0	4.6	-	13.4	85	72	84	80	40	071	028.5	09	.	-	.	-	-	.	.	.	07	04	11	10	02	11	.	.	.	.	.	.	09	03	.
IX	4.6	4.4	3.2	4.1	-	10.9	81	75	82	80	46	053	020.5	01	.	.	.	05	.	.	.	.	12	04	09	06	02	09	.	.	.	.	.	.	.	03	.
X	4.9	5.1	4.8	5.0	-	08.1	86	82	86	85	52	141	031.2	02	.	.	01	.	.	.	01	.	13	12	11	10	04	10	02	01	.	.	.	.	02	04	.
XI	5.3	5.4	4.5	5.1	-	06.5	83	76	85	81	47	107	018.4	17	.	.	05	.	.	.	06	05	03	05	12	11	05	12	01	.	.	.	.	.	.	04	.
XII	5.8	6.1	5.6	5.8	-	04.2	83	79	83	81	35	043	010.2	29	.	11	21	.	.	.	02	02	05	11	12	10	01	06	06	.	.	.	.	.	.	08	09
GOD.	5.8	6.2	4.9	5.6	-	08.0	80	74	82	79	25	1355	041.2	6 VII	01	-	91	-	-	.	21	15	65	112	165	146	45	125	56	05	.	01	.	03	36	36	-
BIJELJINA BR. ST. 129 — H_o = 90 m H_b = - m h_o = 2.0 m h_r = 1.0 m																																					
I	8.9	7.9	7.8	8.2	-	04.1	91	89	91	90	68	067	033.6	02	03	09	24	.	.	.	.	.	.	19	12	08	02	08	09	.	.	.	.	.	.	03	31
II	7.9	6.6	7.8	7.4	048.3	04.5	87	79	88	85	57	086	020.4	12	02	02	22	.	.	.	.	.	.	11	16	13	02	07	10	.	.	.	.	.	.	05	21
III	6.5	6.2	6.8	6.5	-	05.5	87	70	81	79	43	083	023.2	28	.	01	07	.	.	.	.	.	01	10	17	12	02	13	05	.	.	.	.	.	.	02	03
IV	6.3	6.0	6.4	6.2	107.6	07.6	80	68	76	75	48	066	020.2	15	.	.	02	05	.	.	.	.	.	07	13	08	02	13	.	.	.	.	.	.	.	.	.
V	6.8	6.1	7.5	6.8	-	09.6	81	69	78	76	46	104	042.8	23	.	.	.	03	.	.	.	.	01	10	17	14	02	16	.	.	.	.	.	.	02	.	.
VI	4.5	5.0	4.8	4.7	206.7	14.0	85	66	85	79	43	100	020.0	30	.	.	.	20	05	.	.	.	03	02	15	12	04	15	.	.	.	.	.	01	12	01	.
VII	4.5	4.5	4.7	4.6	-	14.2	84	68	83	78	51	084	034.2	06	.	.	.	20	09	.	01	.	08	08	09	08	02	09	.	.	.	.	.	.	02	01	.
VIII	4.0	3.4	4.0	3.8	205.9	14.9	88	64	85	79	47	064	042.5	18	.	.	.	22	08	.	02	.	08	02	08	05	01	08	.	.	.	.	.	.	04	01	.
IX	5.1	3.9	4.5	4.5	164.7	11.8	89	68	87	81	37	015	007.0	01	.	.	02	10	04	.	.	.	09	04	08	05	.	08	.	.	.	.	.	.	.	08	.
X	4.8	4.9	4.8	4.9	132.5	08.1	90	72	86	83	53	066	020.4	02	.	.	02	04	.	.	.	.	06	08	08	06	03	08	.	.	.	.	.	.	.	05	.
XI	6.1	6.2	6.2	6.1	083.0	07.1	90	80	87	86	55	060	013.4	17	.	.	01	.	.	.	.	.	03	11	13	11	01	13	.	.	.	.	.	.	.	04	.
XII	7.6	6.9	7.4	7.3	-	04.6	88	84	86	86	36	045	009.8	24	02	03	19	.	.	.	.	.	01	14	12	09	.	09	03	.	.	.	.	.	.	11	08
GOD.	6.1	5.6	6.1	5.9	-	08.8	86	73	84	81	36	840	042.8	15 V	07	15	79	84	26	.	03	.	40	106	148	111	21	127	27	.	.	.	.	01	20	41	63
SREBRENICA BR. ST. 130 — H_o = 550 m H_b = - m h_o = 2.0 m h_r = 1.0 m																																					
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	4.3	3.9	3.2	3.8	-	09.7	84	69	79	77	21	042	010.0	18	.	.	01	08	06	.	.	.	11	04	08	08	01	08	.	.	.	.	.	.	.	12	.
X	4.4	4.3	4.3	4.3	-	06.9	89	78	87	85	42	107	021.0	04	-	-	-	-	-	-	.	.	15	11	10	08	05	09	03	02	.	.	.	.	.	.	.
XI	6.7	6.0	5.9	6.2	-	06.0	87	74	84	81	44	099	020.0	11	-	.	-	.	.	-	.	.	08	13	09	09	04	09	.	.	.	.	.	.	.	.	.
XII	6.7	6.5	6.3	6.5	-	04.3	92	84	90	88	38	038	007.0	04	.	12	24	.	.	.	.	.	04	14	12	11	.	04	08	.	.	.	.	.	.	04	07
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Vazdušni pritisak Pa mm	Temperatura vazduha °C: 7	14	21	Sred. (dnevna)	Max	Min	Amp	Dat.	Min	Dat.	Čestina pravca i srednja jačina vetra nD, Fm (0-12): N		NE		E		SE		S		SW		W		NW		C
												č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		j.	č.	j.	č.
LIVNO $\varphi = 43^\circ 50'$ N $\lambda = 17^\circ 01'$ E Gr. ΔG = + 1h 08 min. BR. ST. 131																												
I	695.8	00.4	03.6	01.5	01.7	05.4	-01.6	12.6	06	-10.3	09	06	01.8	.	.	10	02.0	14	02.1	03	01.7	05	01.6	13	02.1	07	02.0	35
II	693.8	-01.7	02.5	-00.7	-00.1	04.1	-04.1	10.4	10	-16.3	18	18	03.4	.	.	08	02.4	14	02.2	08	02.6	03	02.7	01	02.0	08	02.0	24
III	695.0	-00.3	05.1	01.9	02.2	06.6	-02.1	15.4	26	-14.4	08	13	03.7	06	02.3	15	02.3	16	02.2	03	02.7	03	02.0	04	02.8	08	01.9	22
IV	697.2	06.3	10.9	07.2	07.9	12.8	03.2	22.6	23	-04.8	05	05	03.2	08	01.9	19	02.4	15	02.6	01	01.0	07	01.9	06	02.0	15	02.7	14
V	698.4	09.7	14.3	10.0	11.0	15.9	05.3	21.6	10	-00.7	04	13	02.9	02	02.0	14	02.6	13	02.7	04	03.0	05	02.4	10	01.9	18	02.7	14
VI	700.5	15.3	22.0	15.8	17.2	23.5	09.7	28.4	28	04.9	05	08	02.4	06	01.5	07	01.7	16	02.1	01	02.0	14	02.1	04	01.8	09	02.2	25
VII	699.3	15.5	23.4	17.2	18.3	24.7	10.6	32.3	24	02.7	19	14	02.6	06	02.0	06	02.5	07	02.3	04	01.8	12	01.9	13	01.5	03	02.0	28
VIII	699.5	14.7	23.9	16.6	17.9	25.1	10.8	32.4	07	05.3	28	05	02.4	04	01.8	07	01.4	11	01.7	05	01.8	15	02.1	10	01.8	02	01.5	34
IX	702.0	09.8	21.5	12.2	13.9	22.4	06.5	29.1	11	-04.3	30	15	02.6	04	01.0	04	01.2	08	02.0	03	02.0	11	02.0	02	02.5	07	01.9	36
X	701.5	03.1	14.7	06.7	07.8	15.9	01.3	25.7	11	-05.2	18	11	02.6	04	01.5	05	02.4	11	01.7	05	02.0	08	01.6	06	02.2	05	01.6	38
XI	700.2	02.3	10.4	04.7	05.6	11.9	00.6	19.1	03	-05.3	26	05	02.6	08	02.0	21	02.1	08	02.4	03	01.0	09	01.6	04	02.2	03	02.7	29
XII	700.5	-01.1	05.1	-00.2	00.9	06.3	-04.0	11.2	02	-15.0	27	06	02.5	06	01.5	11	02.7	03	02.3	03	02.7	05	02.2	05	02.4	06	02.8	46
GOD.	698.6	06.2	13.1	07.7	08.7	14.6	03.0	32.4	7 VIII	-16.3	48 II	119	02.8	54	01.8	127	02.2	136	02.2	43	02.1	97	02.0	78	02.0	91	02.3	350
RAKITNO $\varphi = 43^\circ 33'$ N $\lambda = 17^\circ 27'$ E Gr. ΔG = + 1h 10 min. BR. ST. 132																												
I	-	01.4	04.7	01.7	02.4	05.5	-	09.2	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-02.2	02.4	-00.7	-00.3	03.6	-	10.6	05	-	-	34	04.7	05	02.8	03	01.3	07	03.4	10	01.9	.	.	05	01.4	.	.	29
III	-	00.3	05.4	01.8	02.3	05.9	-	13.2	26	-	-	11	04.5	06	04.3	04	01.0	28	02.4	05	01.6	.	.	05	02.2	.	.	34
IV	-	06.2	10.9	06.5	07.5	11.8	-	21.2	24,23	-	-	18	03.8	04	02.5	07	02.4	02	01.5	28	02.7	.	.	03	02.3	.	.	28
V	-	09.0	14.1	08.9	10.2	14.6	-	19.6	10	-	-	37	03.5	03	02.7	01	04.0	21	02.4	03	02.0	.	.	01	02.0	01	05.0	26
VI	-	15.8	21.0	14.4	16.4	21.7	-	28.0	28	-	-	21	03.0	16	02.1	08	01.1	08	02.0	03	02.0	.	.	02	01.0	.	.	32
VII	-	16.9	22.7	16.1	17.9	23.3	11.5	31.2	24	03.5	19	44	02.8	10	04.2	.	.	02	03.5	05	01.4	.	.	05	02.8	.	.	27
VIII	-	17.1	24.1	16.5	18.6	24.5	11.8	31.2	07	09.0	27,25	19	02.4	03	01.3	.	.	05	02.2	06	03.0	.	.	12	02.0	02	01.5	46
IX	-	12.5	20.7	12.8	14.7	21.0	08.6	26.4	12	-01.5	30	40	04.0	06	04.0	03	03.3	02	03.0	.	.	.	.	.	.	.	.	39
X	-	06.3	15.5	07.4	09.1	15.8	02.6	24.4	14,12	-01.8	29,25	32	03.7	04	02.2	.	.	04	03.8	08	02.5	.	.	02	01.0	01	02.0	42
XI	-	03.6	10.5	05.3	06.1	11.0	01.0	18.4	03	-04.5	13	20	03.2	06	02.7	02	01.5	06	02.0	20	02.5	.	.	04	01.5	.	.	32
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
LISTICA $\varphi = 43^\circ 23'$ N $\lambda = 17^\circ 36'$ E Gr. ΔG = + 1h 10 min. BR. ST. 133																												
I	-	03.8	08.2	05.0	05.5	09.3	00.9	16.0	06	-06.8	23	03	03.0	.	.	.	.	.	.	13	01.5	.	.	.	.	.	.	77
II	-	01.9	06.6	03.4	03.8	08.4	-01.0	13.5	10,06	-11.4	18	12	03.8	.	.	.	.	.	.	12	02.7	.	.	.	.	.	.	65
III	-	04.0	10.2	06.6	06.8	11.4	01.3	19.0	26	-06.8	02	14	04.4	.	.	.	.	.	.	09	02.6	.	.	.	.	.	.	67
IV	-	09.6	15.0	10.9	11.6	16.2	05.6	25.4	24	-03.4	05	10	03.3	.	.	.	.	.	.	13	02.7	.	.	.	.	.	.	67
V	-	13.1	18.2	13.4	14.5	19.7	07.9	24.0	10	01.8	03	21	02.4	.	.	.	.	.	.	13	02.0	.	.	.	.	.	.	59
VI	-	18.6	24.9	18.6	20.2	26.0	12.7	31.0	27	05.4	04	08	02.6	.	.	.	.	.	.	07	02.1	.	.	.	.	.	.	7
VII	-	20.7	27.2	21.3	22.6	28.5	14.3	35.0	24	07.0	19	12	02.5	.	.	.	.	.	.	12	02.8	.	.	.	.	.	.	67
VIII	-	19.6	28.4	21.2	22.6	29.4	14.4	36.0	07	09.4	28	04	02.2	.	.	.	.	.	.	10	02.1	.	.	.	.	.	.	79
IX	-	15.1	25.6	17.4	18.9	26.2	10.4	31.8	11	00.6	30	21	03.0	.	.	.	.	.	.	06	01.8	.	.	.	.	.	.	61
X	-	07.9	18.8	10.9	12.1	19.6	05.0	27.0	11	-00.8	24	08	02.0	.	.	.	.	.	.	12	02.0	.	.	.	.	.	.	73
XI	-	05.9	14.1	08.3	09.1	14.9	03.0	20.4	05	-02.6	12	10	02.0	.	.	.	.	.	.	03	01.7	.	.	.	.	.	.	77
XII	-	01.1	09.5	03.7	04.5	10.5	-01.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	10.1	17.2	11.7	12.7	18.3	06.1	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
PROZOR $\varphi = 43^\circ 50'$ N $\lambda = 17^\circ 37'$ E Gr. ΔG = + 1h 10 min. BR. ST. 134																												
I	-	00.0	02.9	00.8	01.1	04.2	-03.6	10.2	16,15	-07.2	07	12	01.3	02	01.0	05	01.0	07	01.6	02	01.0	01	02.0	22	01.4	20	01.3	27
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	06.4	11.4	07.2	08.1	13.2	03.3	23.8	23	-04.8	05	15	02.3	.	.	.	.	06	03.2	05	02.8	.	.	10	02.8	.	.	54
V	-	08.9	13.5	09.0	10.1	15.4	-	22.2	10	-	-	19	02.1	.	.	03	02.3	05	03.0	09	02.1	.	.	10	02.2	.	.	47
VI	-	14.6	20.9	14.5	16.1	22.7	10.1	28.2	28	05.4	05,03	11	01.6	.	.	.	.	02	02.0	02	02.0	.	.	08	02.2	.	.	67
VII	-	14.7	23.0	15.3	17.1	24.1	11.3	31.8	23	05.4	19	17	02.2	.	.	.	.	12	03.3	02	03.5	.	.	13	02.5	.	.	49
VIII	-	14.2	24.3	15.7	17.5	25.6	-	32.4	07	-	-	12	02.2	.	.	.	.	05	02.4	.	.	.	.	15	02.5	.	.	61
IX	-	09.9	21.6	12.7	14.2	22.5	08.1	29.6	11	-03.2	30	08	02.2	.	.	.	.	15	02.9	.	.	.	.	16	02.4	.	.	51
X	-	03.8	13.5	06.7	07.7	15.5	02.5	25.6	11	-01.8	25	10	02.0	.	.	.	.	14	02.9	.	.	.	.	17	02.1	.	.	52
XI	-	02.8	10.3	04.4	05.5	11.7	00.6	18.4	05	-03.6	13	04	01.8	.	.	.	.	14	03.1	.	.	.	.	11	02.5	.	.	61
XII	-	-01.4	04.7	00.2	01.0	05.7	-03.6	11.2	01	-10.4	27,24	05	02.6	.	.	01	02.0	11	02.5	.	.	.	.	09	02.1	.	.	67
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ČAPLJINA $\varphi = 43^\circ 07'$ N $\lambda = 17^\circ 43'$ E Gr. ΔG = + 1h 11 min. BR. ST. 135																												
I	-	06.2	10.1	07.4	07.8	11.3	03.8	16.1	06	-02.0	23	10	03.0	01	01.0	.	.	.	.	22	03.7	.	.	.	.	01	01.0	59
II	-	03.8	09.3	06.1	06.3	10.5	-	17.0	06	-	-	21	02.3	.	.	02	01.0	.	.	20	03.4	.	.	.	.	.	.	41
III	-	06.7	12.6	08.0	08.8	14.4	03.4	19.5	24	-03.4	02	14	02.9	.	.	02	02.0	03	05.0	18	03.4	02	02.5	02	02.5	.	.	52
IV	-	10.8	16.5	11.0	12.3	18.0	06.3	25.5	24	00.0	05	15	02.7	01	01.0	01	02.0	02	02.0	24	03.2	.	.	04	02.5	01	01.0	42
V	-	15.5	20.9	14.3	16.2	21.9	09.1	26.8	10	02.2	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	21.2	27.1	20.0	22.1	28.3	13.7	33.0	18	05.0	06	07	02.3	.	.	01	05.0	01	05.0	04	03.0	02	01.0	11	02.0	.	.	64
VII	-	22.5	28.5	21.2	23.4	30.0	14.9	36.0	29,13	08.4	20	16	02.2	.	.	.	.	02	03.0	02	04.0	.	.	13	01.8	01	02.0	59
VIII	-	21.5	28.9	21.0	23.1	30.3	15.2	36.0	08	09.6	27	03	02.0	01	01.0	01	02.0	01	04.0	08	02.5	.	.	08	01.9	.	.	71
IX	-	16.3	27.5	18.8	19.3	28.3	10.9	34.0	13	00.2	30	23	02.1	01	01.0	.	.	.	.	.	.	01	01.0	11	01.6	.	.	54
X	-	09.0	19.6	10.4	12.3	20.7	04.9	26.6	10	00.0	26	13	02.5	01	03.0	.	.	.	.	06	04.3	.	.	09	01.7	.	.	64
XI	-	06.7	15.3	08.2	09.6	16.4	03.7	-	-	-	-	08	01.9	.	.	.	.	.	.	08	04.4	.	.	02	02.0	.	.	72
XII	-	03.2	11.0	05.6	06.4	11.7	01.1	17.1	30	-08.0	21,20	12	02.4	.	.	.	.	01	02.0	10	05.0	.	.	01	01.0	.	.	69
GOD.	-	12.0	18.9	12.5	14.0	20.2	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dim)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dim)	Min	Padavine R mm Σ	Max	Int.	Broj dana n sa: Tn ≤ -20,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) ≤ 8,0	≥ 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	●	▲	▲	▲	▲	▲	▲	▲
LIVNO BR. ST. 131																																					
I	8.1	7.6	7.1	7.6	070.1	04.3	86	70	81	79	29	235	057.6	01	01	01	19	.	.	.	10	.	05	21	16	16	06	15	04	01	.	.	.	.	.	05	10
II	7.8	7.0	5.9	6.9	100.0	03.4	79	59	78	72	28	141	040.0	16	02	26	23	.	.	.	16	09	02	14	16	14	04	12	06	01	.	.	.	.	04	01	08
III	7.0	7.0	5.7	6.6	138.8	04.1	83	66	76	75	27	122	019.2	04	03	01	19	.	.	.	16	06	05	16	14	11	07	11	11	06	01	.	.	.	01	.	10
IV	7.2	8.2	6.1	7.2	162.4	05.5	78	56	71	68	25	134	046.6	09	.	.	06	.	.	.	17	04	.	12	15	12	05	13	02	.	.	.	.	.	01	.	01
V	6.4	7.8	5.5	6.6	206.0	06.4	71	53	68	64	29	046	020.8	28	.	.	02	.	.	.	21	04	04	10	10	05	02	10	01	.	.	.	.	.	05	.	.
VI	4.2	6.5	4.3	5.0	285.9	10.1	77	51	76	68	31	039	007.5	20	.	.	.	13	.	.	10	.	04	04	14	09	.	14	.	.	.	.	.	.	07	.	.
VII	3.4	4.9	2.7	3.7	307.8	10.1	76	47	70	64	23	038	013.3	17	.	.	.	18	04	.	08	.	12	06	06	04	01	06	.	.	.	.	.	.	05	.	.
VIII	4.4	6.1	2.5	4.3	266.2	10.6	85	46	80	70	25	107	032.0	10	.	.	.	17	04	.	08	.	08	04	10	08	05	10	.	.	.	.	.	.	06	01	.
IX	3.7	3.3	1.5	2.8	262.8	08.2	85	42	78	68	18	002	001.3	01	.	.	06	09	.	.	05	02	11	02	03	01	.	03	.	.	.	.	.	.	.	.	.
X	3.9	4.3	2.6	3.6	-	05.6	87	47	81	72	25	102	035.8	02	.	.	13	02	.	.	10	01	13	06	08	06	04	08	.	.	.	.	.	.	02	02	.
XI	6.6	6.1	4.8	5.8	145.3	05.6	91	63	86	80	32	125	030.1	16	.	.	15	.	.	.	12	02	07	12	13	10	05	13	.	.	.	.	.	.	.	04	.
XII	5.2	5.4	4.3	5.0	140.5	03.8	82	61	81	75	27	193	046.0	26	03	01	25	.	.	.	11	04	11	11	13	13	06	11	05	01	.	.	01	.	02	.	07
GOD.	5.7	6.2	4.4	5.4	-	06.5	81	55	77	71	18	1284	057.6	41	09	29	128	59	08	.	144	32	82	118	138	109	45	126	29	09	01	.	01	.	33	13	36

H_a = 724 m H_b = 727,9 m h_a = 2,0 m h_r = 1,0 m

RAKITNO BR. ST. 132																																					
I	6.9	6.1	6.3	6.5	-	-	-	-	-	-	-	548	112.5	01	-	.	-	.	.	-	01	.	-	-	15	15	10	12	04	01	.	.	.	.	.	.	.
II	7.0	6.6	6.5	6.7	-	-	-	-	-	-	-	-	-	-	-	03	-	.	.	-	09	05	04	13	-	-	-	-	-	-	-	.	.	.	-	-	-
III	6.3	5.1	5.6	5.6	-	-	-	-	-	-	-	287	065.8	04	-	01	-	.	.	-	04	01	08	12	12	12	08	11	07	01	.	.	01	.	.	01	.
IV	5.9	4.7	5.3	5.3	-	-	-	-	-	-	-	382	153.4	09	-	.	-	.	.	-	03	.	06	09	13	13	10	12	04	03	.	.	.	.	.	01	.
V	4.7	4.8	4.1	4.5	-	07.3	77	69	78	75	-	078	042.5	23	-	.	-	.	.	-	04	02	07	03	08	08	02	08	01	.	.	.	.	.	.	-	.
VI	2.7	4.4	2.2	3.1	-	10.8	74	67	78	73	-	128	055.0	19	-	.	-	08	.	-	02	.	13	01	13	13	02	13	.	.	.	.	.	.	.	.	.
VII	2.4	2.3	1.8	2.2	-	11.3	73	63	77	71	45	131	060.0	17	.	.	.	15	02	.	06	.	21	01	05	05	03	05	.	.	.	.	.	.	-	-	.
VIII	2.0	2.5	1.1	1.9	-	12.1	76	63	77	72	50	168	041.6	31	.	.	.	16	01	.	.	.	22	.	10	10	05	10	.	.	.	.	.	.	-	-	.
IX	1.3	0.9	0.6	1.0	-	10.4	81	70	81	77	56	006	005.7	01	.	.	01	08	.	.	04	01	24	.	01	01	.	01	.	.	.	.	.	.	.	.	.
X	2.7	2.7	2.1	2.5	-	07.2	82	69	83	78	51	155	046.6	02	.	.	05	.	.	.	04	02	21	04	05	05	04	05	.	.	.	.	.	.	.	02	.
XI	5.5	4.9	4.6	5.0	-	06.2	88	78	83	83	59	232	072.6	22	.	.	10	.	.	.	01	.	10	12	11	11	06	11	.	.	.	.	.	.	.	04	.
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

H_a = 915 m H_b = - m h_a = 2,0 m h_r = 1,0 m

LIŠTICA BR. ST. 133																																					
I	8.4	7.2	7.3	7.6	-	06.0	85	80	84	83	50	360	060.2	31	.	.	14	.	.	.	.	.	02	16	17	17	11	17	.	.	.	.	.	.	.	01	.
II	7.6	6.8	5.8	6.7	-	05.0	79	75	80	78	48	219	063.5	16	01	.	17	.	.	.	05	02	03	13	13	12	06	10	05	.	.	01	.	01	02	-
III	6.7	5.7	4.9	5.8	-	05.6	76	67	75	73	44	363	068.0	06	.	.	12	.	.	.	05	03	07	12	16	15	10	15	04	02	.	.	.	.	.	.	02
IV	5.7	6.4	4.3	5.4	-	07.8	78	66	74	73	49	223	081.4	09	.	.	01	01	.	.	03	.	05	08	13	13	04	11	02	.	.	.	.	.	.	.	.
V	4.6	6.0	3.2	4.6	-	09.2	74	67	73	71	51	087	058.6	23	.	.	.	.	.	.	.	.	07	04	06	06	02	06	.	.	.	.	.	.	.	.	.
VI	3.4	4.5	2.6	3.5	-	13.3	74	64	78	72	43	068	015.5	19	.	.	.	22	03	.	01	.	11	03	09	09	02	09	.	.	.	.	.	.	01	.	.
VII	2.8	3.0	1.5	2.4	-	13.8	71	59	68	66	38	040	025.5	17	.	.	.	24	14	01	.	.	19	01	04	04	01	04	.	.	.	.	.	.	.	.	.
VIII	2.5	3.6	1.4	2.5	-	14.2	75	57	74	68	29	102	055.0	31	.	.	.	24	18	.	.	.	16	02	06	05	03	06	.	.	.	.	.	.	03	01	.
IX	1.6	1.6	0.5	1.2	-	11.4	71	56	72	66	41	005	004.5	05	.	.	.	19	05	.	05	.	22	.	02	01	.	02	.	.	.	.	.	.	.	.	.
X	2.7	2.4	1.9	2.3	-	08.3	80	65	76	74	46	102	052.0	02	.	.	02	05	.	.	.	.	18	03	05	05	03	05	.	.	.	.	.	.	.	.	.
XI	5.4	5.0	4.2	4.9	-	07.3	85	72	80	79	54	268	071.0	15	.	.	06	.	.	.	.	.	11	11	11	11	08	11	.	.	.	.	.	.	.	06	.
XII	4.4	4.0	3.7	4.1	-	05.1	75	70	77	74	-	276	086.5	27	-	-	-	-	-	-	04	02	.	.	12	12	07	11	03	.	.	.	.	.	.	.	01
GOD.	4.6	4.7	3.4	4.2	-	08.9	76	66	75	73	-	2113	086.5	17 XII	-	-	-	-	-	-	23	07	121	73	114	110	57	107	14	02	.	.	01	.	05	10	-

H_a = 320 m H_b = - m h_a = 2,0 m h_r = 1,0 m

PROZOR BR. ST. 134																																					
I	6.3	6.8	6.8	6.6	-	04.2	81	80	86	82	47	202	056.2	01	.	.	28	.	.	.	.	.	04	16	17	15	06	14	06	.	.	.	.	.	.	02	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	5.9	6.3	5.1	5.8	-	05.2	72	51	70	64	18	086	023.3	15	.	.	06	.	.	.	.	.	04	08	15	14	03	12	05	01	.	.	.	.	.	.	03
V	5.3	5.7	5.1	5.4	-	06.3	73	55	75	68	23	080	026.0	23	-	.	-	.	.	-	.	.	08	10	15	14	03	13	03	01	.	.	.	.	01	.	.
VI	3.9	3.6	3.7	3.7	-	10.0	79	55	81	72	35	027	011.0	17	.	.	.	13	.	.	.	.	11	04	09	06	01	08	.	.	.	.	.	01	03	01	.
VII	3.8	2.7	2.7	3.1	-	10.8	84	53	83	73	30	029	020.0	17	.	.	.	18	02	.	.	.	19	06	04	03	01	03	.	.	.	.	.	.	.	.	.
VIII	3.9	3.9	1.8	3.2	-	11.3	89	53	86	76	15	054	013.5	02	-	.	-	18	04	-	.	.	14	03	10	09	02	09	.	.	.	.	.	.	05	.	.
IX	4.4	2.2	1.0	2.5	-	09.1	87	49	83	73	27	022	015.0	01	.	.	02	11	.	.	.	.	15	02	02	02	01	02	.	.	.	.	.	.	.	.	.
X	3.8	4.0	3.0	3.6	-	06.7	90	68	88	82	40	092	037.0	04	.	.	03	01	.	.	.	.	15	09	06	05	03	06	.	.	.	.	.	.	.	.	.
XI	6.1	4.3	3.1	4.5	-	06.0	92	73	89	85	49	086	018.0	10	.	.	15	.	.	.	.	.	11	07	11	11	04	11	01	01	.	.	.	.	.	.	.
XII	6.4	5.4	4.7	5.5	-	-	-	-	-	-	-	175	039.6	28	02	02	23	.	.	.	.	.	08	10	14	14	06	09	06	.	.	.	.	.	01	01	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

H_a = 800 m H_b = - m h_a = 2,0 m h_r = 1,0 m

ČAPLJINA BR. ST. 135																																					
I	8.2	7.4	6.7	7.4	-	-	-	-	-	-	-	258	029.0	15	.	.	03	.	.	.	-	-	02	18	18	18	10	18	.	.	-	-	-	-	-	-	-
II	7.1	6.1	5.1	6.1	-	05.8	82	70	81	78	33	095	026.5	01	-	.	-	.	.	-	02	01	03	10	12	10	03	11	03	.	.	.	.	.	.	.	-
III	6.2	5.1	4.8	5.4	-	06.3	78	65	73	72	33	184	040.0	15	.	.	04	.	.	.	02	.	09	12	13	12	06	13	.	.	.	.	.	.	.	.	.
IV	5.5	5.7	4.2	5.1	-	08.1	79	62	75	72	28	126	040.5	08	.	.	.	01	.	.	01	01	06	09	12	10	04	12	.	.	.	.	.	.	.	01	.
V	4.7	4.8	4.0	4.5	-	09.3	71	54	69	65	26	022	008.2	23	.	.	.	05	.	.	.	.	04	02	05	04	.	05	.	.	.	.	.	.	01	.	.
VI	2.4	3.4	2.6	2.8	-	13.3	72	48	76	65	22	054	029.5	19	.	.	.	25	12	.	.	.	16	02	03	03	02	03	.	.	.	.	.	.	.	.	.
VII	2.6	2.4	1.2	2.1	-	14.1	69	50	74	64	10	071	037.0	06	.	.	.	26	18	.	.	.	22	01	04	04	02	04	.	.	.	.	.	.	.	.	.
VIII	2.6	3.2	1.5	2.5	-	15.5	78	56	80	71	23	117	033.1	25	.	.	.	30	19	.	.	.	19	02	05	04	04	05	.	.	.	.	.	.	01	.	.
IX	1.8	2.1	0.6	1.5	-	12.2	79	49	79	69	27	004	004.0	01	.	.	.	25	11	.	.	.	20	.	01	01	.	01	.	.	.	.	.	.	.	.	.
X	2.5	3.1	2.1	2.6	-	08.2	84	55	82	73	35	078	035.0	22	.	.	.	06	.	.	01	.	17	03	05	04	02	05	.	.	.	.	.	.	.	10	.
XI	5.9	4.6	3.7	4.7	-	07.4	83	69	84	79	-	168	049.0	15	-	-	-	-	-	-	01	.	09	08	08	08	06	08	.	.	.	.	.	.	01	09	.
XII	5.1	4.6	4.1	4.6	-	05.8	86	65	77	76	22	157	046.0	28	.	.	11	.	.	.	03	.	10	09	08	08	05	08	.	.	.	.	.	.	.	02	.
GOD.	4.6	4.4	3.4	4.1	-	-	-	-	-	-	-	1334	049.0	45 XI	-	-	-	-	-	-	-	-	137	76	94	86	44	93	03	.	-	-	-	-	-	-	-

H_a = 10 m H_b = - m h_a = 2,0 m h_r = 1,0 m

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dnev)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12) N d.	N j.	NE d.	NE j.	E d.	E j.	SE d.	SE j.	S d.	S j.	SW d.	SW j.	W j.	NW d.	NW j.	C d.
JABLANICA — φ = 43° 40' N λ = 17° 46' E Gr. Δ G = + 1h 11 min. — BR. ST. 136																											
I	-	03.5	06.8	04.6	04.9	08.0	-	16.0	12	-	-	10	02.4	.	.	12	03.0	.	.	15	03.0	.	.	12	02.7	01	03.0	43
II	-	01.3	05.9	02.8	03.2	07.0	-	-	-	-	-	13	02.5	01	04.0	08	02.9	.	.	11	03.5	.	.	10	02.8	.	.	41
III	-	04.0	10.6	06.8	07.0	11.4	02.7	20.0	26	-05.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	09.1	16.5	11.2	12.0	17.9	07.5	28.4	23	-00.2	05	16	02.9	.	.	08	03.8	.	.	15	03.7	.	.	09	02.9	.	.	42
V	-	11.9	19.1	14.4	15.0	20.1	10.4	27.0	11	05.2	03	19	02.6	.	.	07	03.1	.	.	11	03.0	.	.	03	02.7	.	.	53
VI	-	17.1	25.4	19.4	20.4	26.9	15.2	32.2	28	10.0	04	08	02.1	.	.	06	03.8	.	.	13	02.6	.	.	04	02.8	.	.	59
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	17.6	27.6	20.9	21.7	28.6	16.2	34.0	07,06	11.0	28	07	02.3	01	02.0	03	02.7	.	.	07	03.1	.	.	10	02.4	.	.	65
IX	-	13.4	25.2	17.9	18.6	25.9	12.3	32.2	14,13	01.6	30	05	02.0	.	.	07	03.4	.	.	01	03.0	.	.	09	02.6	.	.	68
X	-	07.5	17.5	11.2	11.8	18.2	06.6	27.0	12	02.0	26,25	11	02.0	.	.	03	02.3	.	.	09	03.6	.	.	20	02.4	.	.	50
XI	-	05.3	12.4	08.2	08.5	13.9	04.3	19.2	05,01	-01.0	12	12	02.4	01	02.0	07	02.3	.	.	12	03.8	.	.	09	02.2	.	.	49
XII	-	01.2	06.8	03.4	03.7	07.4	00.0	15.2	29	-07.4	20	07	02.4	.	.	06	03.0	.	.	08	03.9	.	.	12	02.7	.	.	60
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
DOMANOVICI — φ = 43° 09' N λ = 17° 47' E Gr. Δ G = + 1h 11 min. — BR. ST. 137																											
I	-	05.9	09.4	06.4	07.0	10.0	03.0	17.5	06	-02.2	23	42	02.1	.	.	.	.	02	01.0	20	03.4	02	01.5	.	.	02	01.5	25
II	-	03.5	08.2	04.7	05.3	09.4	01.1	16.5	06	-08.0	18	45	02.4	02	02.0	.	.	02	03.5	19	03.9	.	.	.	.	.	.	16
III	-	06.0	11.5	07.5	08.2	12.5	03.5	18.8	25,24	-05.0	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	10.6	15.6	11.0	12.0	17.0	07.0	24.5	24	01.4	06,05	24	02.9	.	.	.	.	01	03.0	33	03.2	01	03.0	.	.	01	02.0	30
V	-	14.7	19.5	13.9	15.5	20.4	09.5	25.2	10	02.8	03	33	02.4	.	.	.	.	02	02.5	26	02.7	.	.	.	.	.	.	32
VI	-	20.4	26.4	19.1	21.3	26.9	14.7	32.2	27	06.4	04	29	02.1	.	.	.	.	.	.	24	02.4	.	.	.	.	.	.	37
VII	-	22.1	28.3	21.2	23.2	29.1	16.3	35.0	24	09.2	19	36	02.2	.	.	.	.	.	.	25	02.4	.	.	.	.	.	.	32
VIII	-	21.9	28.7	21.5	23.4	29.7	16.7	35.5	07	11.8	27	30	01.9	.	.	.	.	.	.	25	03.4	.	.	.	.	.	.	38
IX	-	17.4	26.3	18.0	19.9	26.8	13.4	33.0	11	04.0	30	40	02.0	.	.	.	.	.	.	15	02.1	.	.	.	.	01	02.0	34
X	-	10.9	18.6	12.0	13.4	19.4	07.8	26.0	12,09	02.6	25	39	02.6	.	.	.	.	01	01.0	26	02.5	.	.	.	.	.	.	27
XI	-	07.8	14.9	09.4	10.4	15.8	05.0	19.0	05	00.2	12	23	02.2	.	.	.	.	.	.	27	02.6	.	.	.	.	01	02.0	39
XII	-	04.6	10.7	05.9	06.8	11.3	02.3	16.0	30,29	-03.8	18	32	02.5	.	.	.	.	.	.	23	03.4	.	.	.	.	.	.	38
GOD.	-	12.2	18.2	12.6	13.9	19.0	08.4	35.5	7.VIII	-08.0	48 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
MOSTAR — φ = 43° 21' N λ = 17° 48' E Gr. Δ G = + 1h 11 min. — BR. ST. 138																											
I	750.0	05.8	08.8	06.5	06.9	09.6	04.3	18.2	06	-00.6	23	24	04.0	01	04.0	02	01.5	10	02.2	06	02.7	05	01.2	12	02.8	22	04.0	11
II	748.3	03.3	07.6	05.4	05.4	09.1	02.1	15.3	09	-07.0	18	23	04.2	22	04.0	04	04.8	10	03.0	04	02.8	02	03.5	02	03.0	06	01.2	11
III	749.1	05.7	11.7	07.9	08.3	13.0	04.2	21.2	26	-01.3	02	10	02.5	23	04.7	07	04.1	06	02.5	10	03.2	10	02.7	07	01.9	09	01.7	11
IV	750.7	10.6	17.3	12.2	13.1	18.5	08.2	28.6	24	00.4	05	08	04.2	08	03.8	05	03.6	19	02.9	07	02.6	13	02.3	03	02.3	02	04.5	25
V	751.2	14.4	20.6	15.2	16.3	21.8	11.1	28.1	10	06.1	01	30	03.6	17	03.3	.	.	02	01.5	08	02.9	08	02.0	03	02.7	07	03.1	18
VI	752.2	19.9	27.6	20.9	22.3	28.7	16.2	33.7	28	09.8	04	28	02.7	15	03.0	02	01.0	03	01.7	05	03.0	03	02.3	09	02.0	07	02.4	18
VII	750.3	22.1	29.6	23.3	24.6	30.7	18.5	37.2	24	11.0	19	29	03.9	24	03.5	05	02.0	05	02.2	05	03.2	02	02.5	03	03.3	03	04.0	17
VIII	750.7	20.9	29.5	22.9	24.1	30.8	18.1	36.8	08	13.0	25	20	02.4	16	02.8	01	04.0	05	02.0	07	02.4	07	02.1	06	02.0	08	01.8	23
IX	753.7	18.0	27.5	20.1	21.4	28.3	15.9	34.2	11	08.1	30	28	03.7	30	03.6	03	02.3	04	01.8	01	01.0	04	01.8	02	02.0	03	02.3	15
X	754.5	10.8	19.5	12.9	14.0	20.5	09.4	28.9	12,10	04.8	27	33	03.2	17	03.8	02	01.0	03	02.0	03	02.7	.	.	03	01.3	14	02.8	18
XI	754.1	08.1	14.8	09.9	10.7	15.9	06.8	20.0	27,05	01.0	13	20	03.3	15	03.5	05	02.0	.	.	08	02.9	01	01.0	04	01.5	05	03.4	32
XII	754.8	05.2	10.1	06.1	06.9	10.9	03.8	16.8	30	-00.6	18	21	03.2	29	03.8	02	02.5	.	.	06	04.2	06	03.7	01	01.0	15	02.6	13
GOD.	751.6	12.1	18.7	13.6	14.5	19.8	09.9	37.2	14.VIII	-07.0	48 II	274	03.4	217	03.7	38	02.9	67	02.5	70	02.9	61	02.3	55	02.2	101	02.8	212
POTOCI-BIJELO POLJE — φ = 43° 24' N λ = 17° 53' E Gr. Δ G = + 1h 12 min. — BR. ST. 139																											
I	-	05.1	08.7	05.9	06.4	09.8	03.2	18.0	06	-01.2	03	47	03.4	.	.	02	02.5	.	.	12	04.3	.	.	01	02.0	.	.	31
II	-	03.1	07.6	05.1	05.2	09.0	01.1	17.0	09	-09.6	18	54	03.0	.	.	05	03.4	.	.	13	04.1	.	.	02	02.0	.	.	10
III	-	05.5	11.9	07.8	08.2	13.1	02.9	20.4	26	-04.6	02	43	03.3	.	.	07	03.4	.	.	21	03.8	.	.	.	.	.	.	27
IV	-	11.0	16.9	12.4	13.2	18.3	07.1	28.0	24,23	-01.2	05	50	03.1	.	.	05	02.6	.	.	20	03.5	.	.	01	05.0	.	.	14
V	-	14.2	20.1	14.9	16.0	21.1	09.8	27.4	10	04.2	03	49	02.9	.	.	08	02.4	.	.	20	03.2	.	.	02	03.5	.	.	14
VI	-	20.1	27.2	20.3	22.0	28.2	15.1	34.0	14	09.0	04	33	03.0	.	.	05	02.6	.	.	16	02.8	.	.	03	01.7	.	.	33
VII	-	22.5	29.3	22.6	24.3	30.3	17.0	36.8	23	09.0	-	55	03.0	.	.	08	03.1	.	.	15	02.9	.	.	02	03.5	.	.	13
VIII	-	21.7	29.4	22.7	24.1	30.8	16.6	37.4	07	12.0	25	41	02.7	.	.	09	02.2	.	.	22	03.0	.	.	03	02.0	.	.	18
IX	-	17.9	27.2	18.4	20.5	27.7	13.7	34.0	11	07.0	30	55	03.4	.	.	04	02.2	.	.	10	02.7	.	.	.	.	.	.	19
X	-	09.8	19.0	11.0	12.7	19.9	07.3	28.6	12	02.0	31,29	43	03.3	.	.	09	02.2	.	.	20	02.3	01	06.0	02	02.0	.	.	18
XI	-	07.4	14.5	09.0	10.0	15.6	04.8	19.8	05	-01.8	13	47	03.1	.	.	10	01.8	.	.	17	03.1	.	.	02	01.5	.	.	14
XII	-	04.9	09.9	05.9	06.7	11.2	02.5	17.0	30,28	-03.0	18	42	03.1	.	.	05	01.4	.	.	15	03.7	.	.	03	04.0	.	.	28
GOD.	-	11.9	18.5	13.0	14.1	19.6	08.4	37.4	7.VIII	-09.6	48 II	559	03.1	.	.	77	02.5	.	.	201	03.3	01	06.0	21	02.6	.	.	234
IVAN SEDLO — φ = 43° 46' N λ = 18° 02' E Gr. Δ G = + 1h 12 min. — BR. ST. 140																											
I	-	-01.3	00.1	-00.9	-00.7	02.0	-03.1	09.4	12	-12.5	21	.	.	.	.	23	01.7	10	01.8	.	.	03	02.0	30	04.1	08	05.9	19
II	-	-03.3	-00.4	-02.0	-01.9	01.1	-04.9	08.0	06	-15.6	18	.	.	.	.	11	01.9	20	02.0	.	.	.	.	30	05.5	09	06.0	14
III	-	-00.9	03.4	01.1	01.2	04.6	-02.2	13.4	26	-13.6	02	.	.	.	.	10	01.9	14	02.6	.	.	04	01.8	41	05.0	07	06.7	17
IV	-	05.3	09.2	05.9	06.6	11.0	02.6	22.0	23	-07.2	04	.	.	.	.	09	02.4	10	03.1	.	.	07	03.1	48	04.4	05	04.2	11
V	-	07.2	11.4	07.8	08.6	12.9	04.9	21.4	10	-02.2	01	.	.	.	.	14	02.4	30	02.3	.	.	02	02.0	26	04.4	09	05.1	12
VI	-	14.0	19.6	13.6	15.2	20.6	10.4	25.6	29,23	03.0	03	.	.	.	.	11	01.9	18	02.2	02	01.5	01	02.0	30	03.1	07	05.0	21
VII	-	14.1	19.5	14.7	15.7	20.5	10.9	27.4	25,22	05.6	19	.	.	.	.	16	01.8	29	02.3	.	.	02	02.0	19	03.3	03	07.7	24
VIII	-	15.1	21.0	15.3	16.7	21.8	11.9	28.8	07	06.6	28	.	.	.	.	17	01.9	07	02.1	02	01.5	03	02.0	26	03.3	.	.	38
IX	-	09.9	17.4	12.1	12.9	18.2	08.3	27.0	11	-02.0	30	.	.	.	.	18	02.0	32	02.1	02	02.5	09	02.2	17	02.8	.	.	12
X	-	04.2	10.5	06.4	06.9	11.7	02.8	21.0	10	-03.0	25	.	.	.	.	15	02.2	29	02.1	.	.	05	01.6	26	04.7	04	06.5	14
XI	-	03.0	06.9	04.4	04.7	08.2	01.3	16.0	02	-04.0	28,17	.	.	.	.	10	02.0	19	01.9	.	.	07	01.9	40	05.3	07	06.3	07
XII	-	-02.1	00.6	-01.2	-01.0	02.0	-03.7	10.0	01	-09.0	22	.	.	.	.	18	01.7	21	02.2	.	.	04	04.2	26	04.1	06	06.2	18
GOD.	-	05.4	09.9	06.4	07.1	11.2	03.3	28.8	7.VIII	-15.6	48 II	.	.	.	.	172	02.0	239	02.2	06	01.8	47	02.3	359	04.3	65	05.9	207

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Brt.	Broj dana s: Tn ≤ -30,0	Tx ≤ -20,0	Tn ≤ 0,0	Tx ≤ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⁎	≡	≈	≈	▲	▲	RT	≡	≡
BR. ST. 136 — JABLANICA																																					
I	9.8	8.8	9.0	9.2	-	-	-	-	-	-	-	368	092.2	01	-	.	-	.	.	-	.	.	.	28	17	16	10	16	02	01	.	.	.	.	.	02	-
II	9.2	8.3	9.6	9.1	-	04.8	81	72	88	80	21	221	040.6	16	.	.	.	.	.	.	.	.	.	21	13	13	07	12	03	.	.	.	.	.	.	.	-
III	7.9	7.0	8.5	7.8	-	05.8	81	65	80	75	26	296	046.2	06	.	.	04	.	.	.	.	.	02	21	13	13	10	13	.	.	.	.	.	.	.	.	.
IV	6.8	6.8	8.7	7.5	-	07.4	77	54	77	70	28	348	122.2	09	.	.	01	07	.	.	04	02	01	15	12	12	08	12	.	.	.	.	.	.	.	.	.
V	7.3	7.6	8.8	7.9	-	09.3	77	55	84	72	35	047	026.7	23	.	.	.	05	.	.	.	.	01	18	11	08	01	11	.	.	.	.	.	.	.	01	.
VI	4.3	5.9	7.3	5.8	-	13.2	81	54	85	73	31	106	043.4	30	.	.	.	22	11	02	01	.	05	07	12	10	03	12	.	.	.	.	.	.	.	.	.
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	4.5	5.0	6.0	5.2	-	14.5	88	57	78	74	38	050	020.2	25	.	.	.	25	15	01	.	.	09	09	10	06	02	10	.	.	.	.	.	.	01	.	.
IX	4.7	4.6	5.9	5.1	-	12.1	90	54	77	73	21	001	001.1	05	.	.	.	17	08	.	01	.	10	10	01	01	.	01	.	.	.	.	.	.	.	.	.
X	8.1	4.6	5.1	5.9	-	07.9	90	58	77	75	34	145	051.6	22	.	.	.	06	.	.	01	01	05	13	07	05	04	07	.	.	.	.	.	.	.	04	.
XI	7.7	5.6	6.1	6.4	-	06.7	90	65	83	79	36	288	158.3	15	.	.	01	.	.	.	02	.	06	16	13	12	05	13	.	.	.	.	.	.	02	10	.
XII	6.4	5.0	5.5	5.6	-	04.9	84	68	86	80	45	337	083.6	28	.	01	16	.	.	.	03	01	10	14	14	12	09	11	05	.	.	.	.	.	01	04	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 137 — DOMANOVIĆI																																					
I	6.8	6.7	7.0	6.8	-	06.1	80	68	80	76	08	192	021.0	07	.	.	07	.	.	.	02	.	03	12	17	17	10	17	.	.	.	.	.	.	.	.	.
II	6.1	5.5	5.0	5.6	-	05.0	74	61	78	71	30	085	019.0	24	.	.	11	.	.	.	02	.	04	08	12	11	02	10	05	.	.	.	.	.	.	.	03
III	5.9	5.5	5.1	5.5	-	05.8	76	59	76	70	27	187	037.5	15	.	.	07	.	.	.	-	-	08	11	14	14	07	14	.	.	.	.	.	.	02	.	.
IV	5.1	5.8	4.4	5.1	-	07.7	78	56	79	71	30	147	041.2	08	.	.	.	.	.	.	02	01	06	06	11	11	05	11	.	.	.	.	.	01	01	.	.
V	4.0	4.5	3.4	4.0	-	08.6	69	50	69	63	31	030	021.2	23	.	.	.	01	.	.	.	.	08	03	04	03	01	04	.	.	.	.	.	.	01	.	.
VI	2.4	3.9	2.4	2.9	-	12.4	69	48	74	64	33	029	015.5	19	.	.	.	22	08	.	01	.	12	.	04	04	01	04	.	.	.	.	.	.	03	.	.
VII	2.3	3.0	1.2	2.2	-	13.5	67	49	71	63	31	046	023.1	17	.	.	.	26	16	04	01	.	22	01	04	04	02	04	.	.	.	.	.	.	.	.	.
VIII	2.0	3.0	1.6	2.2	-	13.6	71	45	73	63	26	077	033.2	25	.	.	.	26	18	01	.	.	19	.	04	04	03	04	.	.	.	.	.	.	.	.	.
IX	1.3	1.7	0.3	1.1	-	10.5	71	38	67	58	13	006	006.0	01	.	.	.	21	07	.	01	.	23	.	01	01	.	01	.	.	.	.	.	.	.	.	.
X	2.0	2.3	1.4	1.9	-	08.4	78	55	79	71	34	104	041.3	02	.	.	.	05	.	.	02	.	22	02	05	05	03	05	.	.	.	.	.	.	.	.	.
XI	4.3	3.8	3.1	3.7	-	07.7	86	65	85	79	38	128	046.0	15	.	.	.	.	.	.	01	.	14	05	09	09	05	09	.	.	.	.	.	.	01	.	.
XII	4.0	3.9	3.5	3.8	-	05.6	81	60	78	73	24	116	032.5	26	.	.	07	.	.	.	05	.	.	.	10	09	04	09	02	.	.	.	.	.	.	.	.
GOD.	3.8	4.1	3.2	3.7	-	08.7	75	54	75	68	08	1147	046.0	15 XI	.	.	32	101	49	05	-	-	141	48	95	92	43	92	07	.	.	.	.	01	08	.	03
BR. ST. 138 — MOSTAR																																					
I	7.5	7.8	7.0	7.5	067.4	05.7	75	69	70	71	34	395	064.4	17	.	.	03	.	.	.	15	04	03	15	19	18	13	19	01	01	.	.	.	.	01	02	.
II	7.4	7.1	6.3	7.0	094.6	04.6	70	61	64	65	29	208	030.6	16	.	.	07	.	.	.	18	09	03	13	17	16	08	13	08	01	.	.	.	02	05	01	07
III	7.3	6.9	5.6	6.6	137.5	05.2	66	58	60	61	31	275	045.6	04	.	.	02	.	.	.	20	06	05	16	16	13	08	15	03	02	.	.	.	.	04	.	01
IV	6.3	7.9	5.7	6.7	164.4	07.1	72	54	59	62	34	209	054.0	08	.	.	.	05	.	.	15	05	.	09	15	14	05	15	.	.	.	.	01	.	06	.	.
V	5.6	7.2	4.7	5.8	212.7	08.1	66	49	55	57	33	031	013.6	23	.	.	.	05	.	.	17	03	02	06	10	07	01	10	.	.	.	.	.	.	04	.	.
VI	3.9	5.9	3.5	4.5	277.6	12.4	71	49	61	60	36	069	023.8	19	.	.	.	23	16	01	12	02	05	04	12	08	02	12	.	.	.	.	.	.	07	.	.
VII	3.3	4.5	1.6	3.1	307.9	12.3	63	44	53	53	27	030	016.8	17	.	.	.	27	19	11	17	02	14	02	06	05	01	06	.	.	.	.	.	.	05	.	.
VIII	3.3	5.3	2.0	3.5	-	13.2	73	46	59	59	28	092	024.6	31	.	.	.	29	18	07	11	02	10	01	09	06	04	09	.	.	.	.	.	04	09	.	.
IX	2.3	3.4	1.3	2.3	267.6	10.1	63	41	51	51	29	004	002.4	05	.	.	.	23	12	01	14	01	15	02	04	01	.	04	.	.	.	.	.	.	01	.	.
X	3.3	3.9	2.3	3.2	225.0	07.8	73	52	65	63	31	113	042.0	02	.	.	.	07	.	.	18	03	15	04	05	05	03	05	.	.	.	.	.	01	.	04	.
XI	6.0	5.9	4.3	5.4	142.6	06.9	77	62	71	70	32	204	050.6	22	.	.	.	.	.	.	14	02	07	10	12	10	07	12	.	.	.	.	.	.	01	06	01
XII	5.4	4.9	4.9	5.1	135.5	05.2	71	60	67	66	38	203	051.7	30	.	.	03	.	.	.	17	05	11	10	15	11	06	14	02	.	.	.	.	.	.	05	.	03
GOD.	5.1	5.9	4.1	5.1	-	08.2	70	53	61	61	27	1833	064.4	17 I	.	.	15	119	65	20	188	44	90	92	140	114	58	134	14	04	.	.	02	07	57	04	11
BR. ST. 139 — POTOCI-BIJELO POLJE																																					
I	6.6	6.3	5.9	6.3	-	06.4	86	81	87	85	52	378	063.0	08	.	.	09	.	.	.	06	.	07	13	18	18	12	18	.	.	.	.	.	.	.	.	.
II	6.4	6.2	6.1	6.2	-	06.0	89	84	87	87	55	223	047.0	07	.	01	10	.	.	.	-	-	05	10	16	16	08	13	05	.	-	-	-	-	-	-	-
III	6.6	5.7	4.9	5.7	-	07.3	88	80	88	86	55	284	066.0	15	.	.	05	.	.	.	09	.	08	14	14	14	08	13	03	02	.	.	.	.	.	.	.
IV	5.5	6.3	4.3	5.4	-	09.4	84	73	81	80	44	245	063.0	08	.	.	01	06	.	.	07	.	09	09	13	12	05	13	.	.	.	.	.	.	-	.	.
V	4.5	5.4	3.8	4.5	-	10.9	80	73	78	77	50	038	019.0	23	.	.	.	03	.	.	05	.	08	05	06	06	01	06	.	.	.	.	.	.	-	.	.
VI	3.2	3.9	2.8	3.3	-	15.9	81	68	81	77	42	055	026.0	19	.	.	.	23	15	.	-	-	12	01	06	06	01	06	.	.	.	.	.	.	-	.	.
VII	1.4	1.9	1.1	1.5	-	15.9	70	60	74	68	32	059	045.5	17	.	.	.	27	18	08	03	.	24	01	06	05	01	06	.	.	.	.	.	.	-	.	.
VIII	1.5	2.1	1.1	1.6	-	16.9	79	63	77	73	36	107	033.0	31	.	.	.	28	19	.	01	.	22	01	09	08	05	09	.	.	.	.	.	.	-	.	.
IX	0.6	1.0	0.4	0.7	-	13.6	76	60	78	71	27	.	.	.	.	.	.	23	09	.	02	.	27	.	.	.	.	.	.	.	.	.	.	.	-	-	.
X	1.5	2.1	1.8	1.8	-	09.2	81	67	88	78	36	097	038.0	02	.	.	.	06	.	.	03	.	23	02	05	05	04	05	.	.	.	.	.	.	-	-	.
XI	4.8	4.0	3.8	4.2	-	07.9	89	75	87	84	39	162	041.0	22	.	.	01	.	.	.	08	.	12	08	09	08	07	09	.	.	.	.	.	.	.	.	.
XII	3.6	3.4	3.4	3.5	-	06.2	84	74	83	80	29	193	067.0	26	.	.	09	.	.	.	07	.	15	07	13	12	06	12	03	.	.	.	.	.	-	-	03
GOD.	3.8	4.0	3.3	3.7	-	10.5	82	71	82	78	27	1841	067.0	26 XII	.	01	35	116	61	08	-	-	172	71	115	110	58	110	11	02	-	-	-	-	-	-	-
BR. ST. 140 — IVAN SEDLO																																					
I	9.3	9.3	8.9	9.2	011.4	04.3	95	93	94	94	72	268	052.7	17	02	14	23	.	.	.	14	08	.	27	20	19	08	13	11	01	.	.	.	.	01	16	31
II	9.1	8.4	7.7	8.4	043.4	03.6	88	81	88	86	58	194	061.7	16	04	12	23	.	.	.	16	12	.	17	24	15	06	10	18	02	.	.	.	.	04	09	22
III	8.4	7.6	6.9	7.6	113.9	04.0	87	72	80	80	31	192	042.9	06	01	04	25	.	.	.	20	10	02	18	22	15	08	06	21	03	.	.	.	.	01	09	31
IV	7.0	8.6	6.9	7.5	126.7	05.3	80	64	75	73	26	261	085.0	09	.	.	12	.	.	.	20	10	.	12	16	12	07	12	06	01	.	.	.	.	02	04	09
V	8.4	8.4	7.1	8.0	146.6	06.6	85	69	82	79	33	097	033.0	23	.	.	04	.	.	.	12	08	.	15	22	17	02	18	05	.	.	.	.	.	04	05	04
VI	6.0	7.0	5.8	6.3	225.4	10.2	84	62	83	76	42	068	019.6	19	.	.	.	04	.	.	09	03	.	07	16	11	02	16	.	.	.	.	.	.	11	08	.
VII	5.5	5.7	4.0	5.1	246.4	10.6	87	65	83	78	43	128	041.7	17	.	.	.	06	.	.	09	01	10	09	12	09	04	12	.	.	.	.	.	.	04	11	.
VIII	5.4	6.2	4.6	5.4	218.4	11.0	86	61	83	77	35	072	018.6	25	.	.	.	08	.	.	06	01	03	06	14	08	03	14	.	.	.	.	.	.	09	07	.
IX	5.6	5.1	3.7	4.8	177.0	08.4	89	58	78	75	26	018	004.5	17	.	.	01	03	.	.	02	.	08	08	10	05	.	10	.	.	.	.	.	.	.	15	.
X	5.5	5.5	5.2	5.4	143.7	06.1	93	67	86	82	36	135	050.6	22	.	.	08	.	.	.	13	05	08	13	09	09	05	07	04	01	.	.	.	.	02	13	04
XI	7.0	7.1	5.9	6.7	076.0	05.4	90	75	84	83	46	164	031.8	15	.	.	12	.	.	.	22	11	02	14	15	12	05	15	04	01	.	.	.	.	03	14	02
XII	7.6	7.1	6.8	7.2	045.8	03.8	89	81	86	85	39	204	059.1	28	.	11	24	.	.	.	12	06	03	17	19	18	07	08	12	.	.	.	.	.	01	12	26
GOD.	7.1	7.2	6.1	6.8	1574.7	06.6	87	70	83	80	26	1801	085.0	9 IV	07	41	132	21	.	.	155	75	36	163	199	150	57	141	81	09	.	.	.	.	42	123	129

Legend: Tn ≤ -30,0 — Tx ≤ -20,0 — Tn ≤ 0,0 — Tx ≥ 25,0 — Tx ≥ 30,0 — Tn ≥ 20,0 — F (0-12) ≥ 6 — ≥ 8 — Nm (0-10) < 2,0 — > 8,0 — R mm ≥ 0,1 — ≥ 1,0 — ≥ 10,0 — RT

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dnev.)	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	Čestina pravaca i srednja jačina vetra nD, Fm (0-12) N č.	j.	NE č.	j.	E č.	j.	SE č.	j.	S č.	j.	SW č.	j.	W	j.	NW č.	j.	C č.
φ = 43° 06' N λ = 18° 11' E Gr. ΔG = + 1h 13 min.																												**BERKOVIĆI** BR. ST. 141
I	-	03.3	06.5	04.6	04.8	07.5	01.1	13.6	06	-06.0	23,20	21	02.8	14	01.8	17	02.4	.	.	15	01.3	14	02.1	.	.	.	.	12
II	-	00.8	04.4	02.1	02.4	05.4	-01.3	12.4	09,06	-11.2	18	36	02.9	15	01.9	17	01.9	.	.	12	01.7	01	02.0	.	.	.	.	03
III	-	03.8	08.8	05.6	05.9	09.6	01.1	17.8	25	-06.0	02	24	02.7	12	01.8	37	02.0	.	.	09	02.0	04	02.2	.	.	.	.	07
IV	-	08.8	13.2	10.1	10.5	14.6	05.1	24.0	24	-01.6	05	21	02.5	11	01.8	19	02.1	.	.	25	01.6	09	02.2	.	.	.	.	05
V	-	11.5	16.2	12.9	13.4	17.4	07.7	24.4	10	02.4	01	26	02.5	12	01.7	12	01.4	.	.	15	01.3	15	02.3	.	.	.	.	13
VI	-	17.3	23.7	18.0	19.2	24.5	12.2	29.0	17	06.4	04	16	02.0	05	01.6	03	01.3	.	.	22	01.2	17	02.0	.	.	.	.	27
VII	-	19.3	25.8	19.8	21.2	26.5	13.5	33.0	24	06.2	20	25	02.5	04	01.2	03	01.0	.	.	17	01.2	11	01.7	.	.	.	.	33
VIII	-	18.6	26.3	20.2	21.3	27.5	13.7	33.8	07	09.8	28	12	01.9	06	01.3	07	01.4	.	.	16	01.3	09	01.8	.	.	.	.	43
IX	-	15.0	23.6	17.5	18.4	24.2	11.3	30.4	11	02.4	30	44	02.2	.	.	.	.	.	.	11	01.3	03	02.0	.	.	.	.	32
X	-	08.8	16.1	11.2	11.8	17.0	05.4	25.8	11	00.2	25	34	02.6	03	01.3	02	02.5	.	.	18	01.2	05	02.2	.	.	.	.	31
XI	-	06.0	12.0	08.4	08.7	13.1	02.6	18.0	05	-02.4	13	19	02.4	11	02.0	32	01.7	.	.	09	01.3	02	02.0	.	.	.	.	17
XII	-	02.3	07.1	04.5	04.6	07.8	-00.2	13.2	30	-06.2	21,18	24	02.9	07	02.3	11	01.8	.	.	25	01.5	08	02.1	.	.	.	.	18
GOD.	-	09.6	15.3	11.2	11.8	16.3	06.0	33.8	7.VIII	-11.2	48 II	302	02.5	100	01.8	160	01.9	.	.	194	01.4	98	02.1	.	.	.	.	241
φ = 43° 43' N λ = 18° 16' E Gr. ΔG = + 1h 13 min.																												**BJELAŠNICA** BR. ST. 142
I	587.1	-04.6	-04.2	-04.5	-04.5	-02.3	-07.6	01.6	10	-17.4	20	16	06.7	03	06.7	02	04.0	01	02.0	17	07.5	42	06.9	04	03.2	05	03.4	03
II	583.8	-08.4	-07.2	-07.1	-07.4	-04.8	-10.1	-00.6	05	-20.4	17	24	05.9	07	07.1	.	.	.	.	13	09.8	34	07.7	04	05.0	01	03.0	01
III	586.4	-06.5	-05.1	-05.4	-05.7	-03.7	-08.0	01.0	26	-18.0	02	16	07.4	03	07.0	.	.	01	03.0	15	08.5	45	07.4	06	03.7	03	07.7	04
IV	789.9	-01.6	-00.7	-01.4	-01.3	00.9	-03.9	08.7	25	-14.0	04	19	07.0	.	.	.	.	.	.	10	10.2	47	06.5	10	05.0	02	09.0	02
V	591.0	-00.7	01.0	00.3	00.2	02.3	-01.9	08.8	10	-10.0	02	37	06.4	05	03.6	.	.	.	.	09	06.6	31	05.6	04	03.2	03	06.0	04
VI	596.6	07.1	09.3	07.2	07.7	10.2	04.7	16.4	29	-06.3	03	28	05.2	04	05.8	.	.	.	.	04	07.5	26	05.2	09	03.8	08	04.0	11
VII	596.1	08.4	10.5	08.5	09.0	12.0	05.7	19.2	22	-02.0	18	35	06.0	14	04.5	02	03.5	01	02.0	10	05.0	22	05.1	03	04.3	.	.	06
VIII	596.6	09.3	11.6	09.7	10.1	12.6	07.3	20.2	07	00.4	26	27	05.4	08	03.2	02	02.0	01	01.0	13	06.1	20	04.8	06	03.8	03	03.0	13
IX	597.6	05.6	08.1	06.4	06.6	09.3	03.5	18.6	11	-09.0	29	22	05.1	26	05.5	02	04.5	.	.	02	04.5	24	04.9	02	03.5	04	03.8	08
X	595.0	00.9	02.2	01.5	01.5	03.6	-01.0	10.8	10,09	-11.2	25	34	05.7	10	04.3	01	02.0	01	02.0	06	08.2	24	05.2	07	04.6	02	03.5	08
XI	592.9	00.0	00.2	-00.1	00.0	02.3	-02.2	10.6	02	-10.0	07	28	04.8	06	05.3	.	.	.	.	07	07.7	39	07.7	07	04.9	.	.	03
XII	591.5	-05.2	-04.2	-04.8	-04.7	-02.0	-07.7	04.4	13	-14.8	23	29	06.7	07	07.0	.	.	02	04.5	01	08.0	38	07.8	07	04.7	01	04.0	08
GOD.	608.7	00.4	01.8	00.9	01.0	03.4	-01.8	20.2	7.VIII	-20.4	43 II	315	05.9	93	05.2	09	03.3	07	02.7	107	07.7	392	06.5	69	04.3	32	04.6	71
φ = 43° 50' N λ = 18° 21' E Gr. ΔG = + 1h 13 min.																												**SARAJEVO-AERODROM** BR. ST. 143
I	715.4	-00.2	02.5	00.5	00.8	04.4	-02.1	15.0	06	-08.6	21	05	02.2	01	02.0	01	02.0	07	03.3	07	02.4	01	02.0	02	02.0	13	02.2	56
II	713.3	-02.7	03.5	-00.6	-00.1	05.1	-05.1	13.6	09	-22.6	18	02	02.0	.	.	03	01.7	03	02.3	11	04.5	.	.	04	02.2	23	02.1	38
III	714.3	01.2	08.0	03.9	04.3	09.6	-00.2	18.6	26	-09.9	02	03	02.0	02	02.0	01	02.0	09	03.0	15	03.9	02	02.0	01	02.0	25	02.2	35
IV	716.1	06.3	13.2	08.8	09.3	15.5	03.7	26.2	23	-03.8	05	02	03.5	.	.	03	02.0	06	03.5	15	03.7	.	.	06	02.2	24	02.6	34
V	717.4	08.5	15.3	10.6	11.2	17.1	06.1	26.4	10	00.6	02	02	03.5	.	.	04	02.0	02	02.0	08	03.1	03	03.3	06	02.2	23	02.3	45
VI	719.1	13.4	22.6	15.9	17.0	24.3	11.0	30.1	18	06.0	05	02	02.0	03	02.3	02	01.5	06	02.0	03	03.0	02	02.5	04	03.0	14	02.6	54
VII	718.1	14.0	23.1	16.5	17.5	24.6	11.4	32.0	25	06.0	27	04	02.0	01	02.0	04	02.5	01	02.0	01	04.0	01	03.0	03	02.7	25	02.0	53
VIII	718.1	13.8	24.8	16.9	18.1	26.2	11.7	34.0	07	05.7	28	03	02.3	.	.	.	.	.	.	02	04.0	.	.	02	03.5	24	02.1	62
IX	721.2	09.4	21.5	12.8	14.1	22.6	07.5	33.2	11	-04.0	30	04	03.0	.	.	.	.	01	02.0	04	01.8	.	.	03	02.3	17	02.0	61
X	720.9	03.6	14.1	07.1	08.0	15.6	02.3	23.7	11	-01.5	01	.	.	.	.	05	01.6	02	02.0	04	05.2	.	.	05	01.6	19	02.0	58
XI	719.6	02.3	09.3	04.0	04.9	10.8	00.4	19.6	01	-04.4	13	.	.	.	.	02	02.0	01	02.0	10	02.9	01	01.0	04	02.0	04	02.0	68
XII	720.9	-01.4	02.0	-00.7	-00.2	03.2	-03.5	16.0	30	-15.4	27	03	02.0	.	.	03	01.7	05	02.6	07	02.9	02	02.5	.	.	07	02.0	66
GOD.	717.9	05.7	13.3	08.0	08.7	14.9	03.6	34.0	7.VIII	-22.6	48 II	30	02.4	07	02.1	28	01.9	43	02.7	87	03.5	12	02.5	40	02.3	218	02.2	630
φ = 43° 52' N λ = 18° 26' E Gr. ΔG = + 1h 14 min.																												**SARAJEVO** BR. ST. 144
I	704.4	00.4	03.2	01.2	01.5	04.3	-01.9	15.0	06	-09.2	21	04	01.5	01	01.0	11	01.8	13	01.9	11	02.3	04	01.2	13	01.2	11	01.2	25
II	702.1	-01.1	03.4	00.6	00.9	05.3	-03.2	13.0	09,05	-14.9	18	01	02.0	.	.	09	01.7	09	02.3	12	02.8	03	02.3	25	01.4	11	01.7	14
III	703.0	01.5	07.5	04.0	04.3	09.2	00.0	17.7	24	-10.3	02	05	01.4	01	01.0	13	02.2	12	02.2	14	02.3	09	01.9	17	01.4	11	01.2	11
IV	705.1	07.2	13.0	08.9	09.5	15.1	04.4	25.4	23	-02.4	05	06	01.7	.	.	07	02.1	11	01.7	16	02.6	10	02.2	20	02.0	05	01.8	15
V	706.5	08.8	14.9	10.7	11.3	16.3	06.5	26.0	10	-00.1	01	05	01.2	.	.	05	02.2	07	01.6	04	01.8	07	02.0	18	01.7	04	01.5	43
VI	708.3	14.3	22.8	16.7	17.6	24.0	11.6	29.6	10	05.6	03	05	01.4	01	02.0	06	01.0	04	01.0	05	01.6	04	01.5	08	01.6	06	01.0	48
VII	707.2	14.8	23.0	17.3	18.1	24.3	12.2	31.8	25	06.6	19	01	02.0	01	01.0	08	01.6	13	01.2	02	01.0	08	01.4	19	01.2	07	01.1	.
VIII	707.0	15.1	24.6	18.1	19.0	26.0	12.7	33.2	07	06.8	28	02	01.5	01	01.0	09	01.4	11	01.1	03	01.7	01	01.0	11	01.1	11	01.2	44
IX	710.1	11.1	21.5	14.0	15.1	22.5	08.7	32.7	11	-01.7	30	02	01.0	01	01.0	13	01.6	17	01.4	.	.	01	01.0	11	01.4	07	01.3	39
X	709.6	05.1	14.0	08.1	08.8	15.7	03.4	26.5	06	-01.2	25	02	01.0	01	01.0	08	01.8	19	01.7	05	01.6	05	01.4	09	01.4	06	01.3	38
XI	708.3	04.0	09.7	06.1	06.5	11.5	02.1	20.3	04	-03.5	27	.	.	03	01.0	10	01.9	10	01.6	16	02.5	03	02.0	05	01.4	04	01.0	39
XII	709.4	-01.1	02.3	00.2	00.4	03.2	-02.8	14.2	30	-08.5	18	01	01.0	01	01.0	06	01.2	12	01.8	05	02.0	06	01.0	06	01.0	09	01.2	47
GOD.	706.8	06.7	13.3	08.8	09.4	14.8	04.5	33.2	7.VIII	-14.9	48 II	34	01.4	11	01.1	105	01.7	138	01.6	93	02.3	61	01.7	162	01.4	92	01.3	362
φ = 43° 31' N λ = 18° 27' E Gr. ΔG = + 1h 14 min.																												**KALINOVNIK** BR. ST. 145
I	668.2	-00.4	01.8	00.2	00.4	02.7	-02.0	08.9	12	-12.0	30	06	02.7	08	02.9	17	02.4	04	01.2	05	01.0	18	03.6	18	02.2	05	01.4	12
II	666.1	-02.2	00.0	-01.7	-01.4	01.5	-04.6	07.2	05	-21.1	18	07	03.0	15	02.8	09	02.2	02	01.0	05	02.8	22	04.3	16	02.5	03	01.3	05
III	666.9	-00.2	03.5	00.9	01.3	04.5	-01.9	12.5	26	-10.9	08	11	02.8	08	02.6	09	02.1	03	01.3	06	04.7	25	03.1	18	02.4	03	02.7	10
IV	669.2	05.5	09.2	05.5	06.4	10.5	02.8	21.9	23	-03.2	04	07	03.4	06	02.7	04	01.8	01	01.0	02	03.0	30	03.8	22	02.2	03	01.0	16
V	670.3	07.4	11.1	07.7	08.5	12.1	04.7	20.7	10	00.0	01	16	03.0	07	01.9	17	01.9	04	01.2	03	01.0	18	03.2	14	02.1	.	.	14
VI	672.9	13.6	18.8	13.4	14.8	20.0	09.7	25.4	18	03.7	04	12	02.6	08	02.4	10	02.1	05	01.2	02	01.0	16	03.1	16	02.0	05	01.2	16
VII	671.7	15.0	19.7	14.8	16.1	20.8	11.1	28.1	23	06.4	19	14	02.9	09	02.2	23	02.4	08	01.8	01	01.0	17	03.3	06	02.2	03	02.0	12
VIII	672.1	14.8	21.0	15.3	16.6	22.4	10.4	31.6	07	06.6	28	16	02.1	05	02.4	08	02.0	05	01.0	03	03.7	12	03.3	12	02.1	05	01.0	27
IX	674.3	10.1	17.6	11.4	12.6	18.6	07.3	29.1	13	-03.4	30	14	02.8	14	02.9	24	02.5	01	01.0	.	.	09	02.4	07	02.3	.	.	21
X	673.4	05.3	11.2	06.4	07.3	12.3	03.4	21.3	10	00.0	24,17	04	02.5	08	02.6	29	02.3	04	01.0	02	01.0	15	03.7	14	02.4	01	02.0	16
XI	672.3	03.8	08.5	05.4	05.8	09.8	02.0	18.9	03	-02.2	12	03	03.3	06	02.3	17	02.3	04	01.2	02	01.0	18	04.0	26	02.7	.	.	14
XII	671.8	-00.3	03.7	00.9	01.3	04.7	-01.9	10.3	01	-09.4	07	02	02.0	17	03.2	19	02.2	06	01.0	05	02.8	21	03.4	12	01.9	.	.	11
GOD.	670.8	06.0	10.5	06.7	07.5	11.7	03.4	31.6	7.VIII	-21.1	48 II	112	02.8	111	02.7	186	02.3	47	01.2	36	02.5	221	03.5	181	02.3	28	01.5	173

Mjesec	Oblačnost Nm (0-10) 7	14	21	Srednji (Dlim)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Srednji (Dlim)	Min	Padavine R mm Σ	Max	Broj dana s sa: Tn ≤ -10,0	Tx ≤ -10,0	Tn ≤ 0,0	Tx ≤ 0,0	Tx ≥ 25,0	Tn ≤ -20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 8,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⚹	⚹	△	≈	▲	▲	⚠	■	■
BR. ST. 141																																					
I	7.5	4.9	7.2	7.2	-	05.7	88	80	84	84	44	217	041.2	02	.	.	12	.	.	.	.	.	04	17	13	13	09	13	01	.	.	.	.	.	.	.	01
II	7.6	4.5	7.1	7.0	-	04.8	85	80	85	83	49	135	024.2	14	01	03	17	.	.	.	02	.	02	13	13	13	06	10	04	.	.	.	.	.	.	.	00
III	5.5	5.1	5.2	5.2	-	05.6	82	73	81	78	45	209	042.4	05	.	.	14	.	.	.	01	.	09	11	13	13	07	13	02	.	.	.	.	.	.	.	01
IV	5.3	5.7	5.3	5.4	-	07.5	78	71	78	76	50	185	048.4	29	.	.	04	.	.	.	.	.	05	09	12	12	07	11	03	.	.	.	.	.	.	.	02
V	4.4	3.7	3.9	4.7	-	08.0	69	63	69	67	38	033	015.4	23	.	.	.	.	.	.	.	.	06	04	05	05	01	05	.	.	.	.	.	.	.	.	.
VI	3.1	3.8	3.4	3.4	-	11.5	70	59	71	67	43	082	055.4	19	.	.	.	20	.	.	.	.	11	01	05	05	02	05	.	.	.	.	.	.	.	.	.
VII	2.5	3.1	2.1	2.6	-	11.5	68	51	64	61	25	072	062.6	17	.	.	.	21	11	.	.	.	20	02	03	03	01	03	.	.	.	.	.	.	.	.	.
VIII	2.5	4.0	2.3	2.9	-	12.4	72	55	70	66	26	079	043.6	25	.	.	.	21	13	.	.	.	18	02	04	04	02	04	.	.	.	.	.	.	.	.	.
IX	1.9	2.2	1.3	1.8	-	09.8	65	52	61	60	34	036	036.4	01	.	.	.	14	02	.	.	.	19	01	01	01	01	01	.	.	.	.	.	.	.	.	.
X	2.5	3.2	2.7	2.8	-	07.0	70	59	66	65	42	130	033.6	02	.	.	.	01	.	.	.	.	18	04	06	06	05	05	.	.	.	.	.	.	.	.	.
XI	4.7	4.4	3.4	4.2	-	06.2	77	67	72	72	41	127	056.8	16	.	.	03	.	.	.	.	.	10	07	07	07	03	07	.	.	.	.	.	.	.	.	.
XII	5.0	4.3	4.3	4.5	-	04.8	78	69	70	72	39	189	046.4	28	.	.	17	.	.	.	01	.	11	09	12	12	07	10	02	.	.	.	.	.	.	.	04
GOD.	4.4	4.6	4.0	4.3	-	07.9	75	64	72	70	25	1494	062.6	43 VII	01	03	67	77	26	.	04	.	133	80	96	96	51	89	12	.	.	.	.	.	.	.	10
BR. ST. 142																																					
I	7.4	8.3	6.6	7.4	-	03.2	96	95	98	96	28	081	010.7	08	09	23	31	.	.	.	27	20	01	18	16	12	04	06	15	04	01	.	.	.	01	28	31
II	8.8	9.0	8.9	8.9	032.8	02.6	99	100	100	100	86	078	028.6	16	15	20	20	.	.	.	24	21	.	18	18	14	02	.	18	.	.	.	.	.	03	28	28
III	8.0	7.3	6.7	7.3	094.9	03.0	93	94	94	94	74	041	008.4	15	10	26	31	.	.	.	23	28	04	18	13	11	.	01	13	.	.	01	.	.	01	26	31
IV	7.2	7.9	6.0	7.0	085.7	03.8	89	89	89	89	41	039	009.0	03	03	15	21	.	.	.	26	22	02	11	13	08	.	03	12	01	.	04	.	.	03	22	30
V	8.0	8.4	7.5	8.0	-	04.4	94	90	93	92	50	069	015.8	23	01	06	19	.	.	.	27	20	01	17	19	15	02	09	14	04	.	03	01	.	05	26	31
VI	6.0	7.1	4.9	6.0	180.6	06.7	84	80	89	84	57	086	020.0	21	.	01	05	.	.	.	24	14	02	08	16	12	03	14	03	.	.	.	01	.	00	19	23
VII	5.4	6.4	5.0	5.4	232.7	07.2	83	79	88	83	30	053	022.4	17	.	01	03	.	.	.	26	10	06	12	11	09	02	10	02	.	01	.	.	.	02	19	22
VIII	5.1	6.5	4.1	5.2	201.1	07.6	80	81	85	82	38	080	021.6	31	.	.	.	.	.	.	17	09	07	04	13	08	04	12	.	.	.	.	01	02	00	17	.
IX	5.0	5.9	3.6	4.8	192.2	05.6	77	75	75	76	10	026	009.6	01	.	01	07	.	.	.	21	10	10	09	12	06	.	10	01	.	.	.	.	.	.	19	01
X	5.5	5.5	5.2	5.4	171.1	04.1	80	82	81	81	15	082	000.0	22	01	06	16	.	.	.	24	17	10	12	08	07	03	05	07	02	.	01	.	.	02	23	17
XI	5.8	7.0	5.5	6.1	124.0	03.4	75	79	77	77	11	076	018.2	22	01	08	20	.	.	.	26	18	07	14	10	10	03	07	08	02	.	.	.	.	01	19	28
XII	6.0	6.1	6.2	6.1	110.7	02.5	80	78	79	79	03	065	013.0	30	11	22	30	.	.	.	23	20	08	14	15	13	02	06	11	04	.	01	.	.	01	21	30
GOD.	6.5	7.1	5.8	6.5	-	04.5	85	85	87	86	03	784	028.6	46 I	51	137	213	.	.	.	288	209	58	157	164	125	25	83	104	17	02	10	03	02	35	269	252
BR. ST. 143																																					
I	9.1	8.2	7.7	8.3	025.0	04.4	93	81	88	87	55	136	034.8	02	.	06	22	.	.	.	.	.	01	19	16	10	06	11	11	01	.	.	.	.	.	10	15
II	9.4	7.6	7.2	8.1	072.5	03.9	92	71	85	83	48	126	036.4	16	05	07	22	.	.	.	07	01	.	15	17	13	05	09	12	.	01	.	.	.	03	09	19
III	7.7	7.3	6.8	7.3	123.6	04.7	87	63	77	76	39	112	026.3	06	.	01	15	.	.	.	02	.	03	17	14	12	05	10	12	.	.	.	.	.	.	.	05
IV	6.7	7.9	5.6	6.7	151.7	06.2	84	60	70	71	27	076	025.2	15	.	.	06	01	.	.	05	.	01	09	10	08	03	10	03	01	.	.	.	.	.	.	.
V	7.3	8.3	6.8	7.4	147.5	07.4	88	59	79	75	32	078	027.8	23	.	.	.	01	.	.	02	.	.	12	17	12	01	17	01	.	.	.	.	.	02	02	.
VI	6.0	6.3	5.6	6.0	218.1	11.1	91	56	85	77	28	097	023.0	15	.	.	.	19	02	.	.	.	01	07	16	13	04	16	.	.	.	.	.	.	10	08	.
VII	4.8	5.5	3.8	4.7	241.6	11.3	91	56	82	76	33	067	019.8	17	.	.	.	19	04	.	.	.	12	09	10	09	03	10	.	.	.	.	.	.	04	04	.
VIII	4.7	5.6	2.8	5.0	212.9	10.9	93	47	77	72	22	039	011.0	25	.	.	.	19	07	.	.	.	04	04	10	08	01	10	.	.	.	.	.	.	07	15	.
IX	5.9	4.8	3.6	4.7	-	08.5	91	47	74	71	16	017	006.8	01	.	.	03	11	04	.	.	.	08	05	06	05	.	06	.	.	.	.	.	.	.	10	.
X	7.9	5.1	5.1	6.0	134.2	06.0	91	56	81	76	18	128	041.0	22	.	.	06	.	.	.	03	.	06	12	09	08	04	09	02	01	.	.	.	.	.	03	15	01
XI	7.4	6.6	5.7	6.5	091.4	05.3	91	65	89	82	24	080	022.8	17	.	01	10	.	.	.	02	.	01	10	12	11	02	12	.	.	.	.	.	.	.	11	.
XII	8.3	7.5	8.3	8.0	-	04.1	90	79	90	86	36	088	022.8	26	02	11	24	.	.	.	03	03	01	21	16	14	03	07	10	.	.	.	.	.	.	13	10
GOD.	7.3	6.7	5.8	6.6	-	07.0	90	61	81	77	16	1044	041.0	12. X	07	26	116	70	17	.	24	04	38	140	153	123	37	127	51	03	01	.	.	.	29	97	48
BR. ST. 144																																					
I	9.1	7.5	7.3	8.0	028.3	04.3	88	75	84	82	44	134	033.9	02	.	07	22	.	.	.	05	.	.	19	22	14	06	15	13	06	.	.	.	.	.	00	16
II	8.1	7.7	7.2	7.7	061.0	03.6	84	61	78	74	35	131	038.2	16	03	06	21	.	.	.	03	.	.	12	21	15	04	12	14	03	.	.	.	.	02	05	20
III	7.9	7.4	6.7	7.3	121.0	04.1	79	55	68	67	24	101	021.3	06	01	01	16	.	.	.	07	.	02	17	19	12	05	11	15	02	.	.	.	.	.	01	10
IV	8.8	8.2	5.0	6.7	142.9	05.3	72	49	63	61	17	085	028.3	15	.	.	06	01	.	.	07	01	.	10	13	09	02	13	03	03	.	.	.	.	.	01	02
V	7.8	8.5	7.2	7.8	140.1	06.8	82	55	73	70	15	103	029.8	23	.	.	01	01	.	.	.	.	.	15	22	15	03	21	03	02	.	.	.	.	05	03	.
VI	5.9	6.8	5.1	5.9	220.7	10.0	82	49	73	68	25	074	014.5	21	.	.	.	19	.	.	.	.	01	06	18	11	04	18	.	.	.	.	.	.	11	01	.
VII	4.1	5.4	3.7	4.5	254.8	10.7	81	54	75	70	31	076	023.4	06	.	.	.	16	04	.	.	.	13	09	11	08	03	11	.	.	.	.	.	.	05	03	.
VIII	5.0	5.8	3.5	4.8	239.8	11.0	83	49	75	69	15	047	012.1	25	.	.	.	19	06	.	.	.	06	06	12	10	01	12	.	.	.	.	.	01	07	01	.
IX	4.2	4.6	3.7	4.2	209.8	08.5	81	45	73	66	18	027	010.2	01	.	.	01	11	04	.	.	.	10	06	06	05	01	06	.	.	.	.	.	.	.	03	.
X	5.6	5.4	5.4	5.4	187.9	06.1	86	56	78	73	21	115	034.1	22	.	.	02	01	.	.	.	.	09	13	11	08	04	11	04	02	.	.	.	.	01	06	01
XI	6.4	7.1	5.2	6.2	096.5	05.3	84	63	76	74	32	074	021.0	17	.	.	08	.	.	.	04	.	03	07	12	10	02	12	02	02	.	.	.	.	.	06	.
XII	7.9	8.1	7.5	7.8	049.7	03.9	85	75	82	81	30	068	019.0	26	.	12	24	.	.	.	03	.	01	19	16	12	01	09	09	02	.	.	.	.	.	10	12
GOD.	6.6	6.9	5.6	6.4	1732.5	06.6	82	57	74	71	13	1035	038.2	46 II	04	26	101	70	14	.	29	01	45	139	183	129	36	151	63	22	.	.	.	01	31	48	61
BR. ST. 145																																					
I	9.0	8.5	8.7	8.8	-	04.2	89	83	85	86	00	193	034.4	01	01	09	20	.	.	.	03	.	.	23	21	13	08	13	11	.	.	.	.	.	.	05	18
II	8.5	7.9	7.6	8.0	-	03.7	88	83	84	85	65	122	022.5	16	05	10	18	.	.	.	08	02	.	17	20	13	04	11	15	.	.	.	.	.	06	05	21
III	7.8	6.6	6.4	6.9	-	04.3	87	77	83	83	40	108	019.4	28	03	03	17	.	.	.	05	02	03	15	18	11	05	08	16	.	.	.	.	.	01	04	27
IV	8.0	7.7	6.4	6.8	-	05.5	80	66	80	75	28	165	044.1	09	.	.	07	.	.	.	03	02	01	12	15	11	04	13	05	.	01	.	.	.	01	.	03
V	7.8	8.1	6.4	7.4	-	06.5	84	66	83	78	31	067	017.2	29	.	.	.	.	.	.	01	.	.	14	22	10	02	19	04	.	.	.	.	.	04	01	.
VI	5.8	6.5	4.7	5.4	-	09.7	84	59	85	76	34	039	014.9	19	.	.	.	04	.	.	.	.	03	07	17	07	01	17	.	.	.	.	.	.	12	01	.
VII	4.5	5.8	3.5	4.3	-	09.9	79	56	80	72	32	056	036.1	17	.	.	.	07	.	.	01	.	10	06	09	04	01	09	.	.	.	.	.	.	06	.	.
VIII	4.8	6.0	3.0	4.3	-	09.3	78	48	74	67	22	050	018.4	25	.	.	.	12	01	.	01	01	07	03	13	08	02	13	.	.	.	.	.	.	07	01	.
IX	4.6	4.7	2.5	3.9	-	07.4	80	48	75	68	13	015	006.9	05	.	.	01	07	.	.	.	.	10	04	05	02	.	05	.	.	.	.	.	.	01	03	.
X	5.8	5.1	4.9	5.1	-	05.7	84	59	81	75	14	122	040.1	22	.	.	.	.	.	.	04	01	10	11	08	07	04	07	02	.	.	.	.	.	03	07	02
XI	5.9	5.9	4.6	5.4	-	05.0	83	62	74	73	21	125	029.2	14	.	.	04	.	.	.	05	.	05	10	12	10	04	12	04	02	.	.	.	.	02	03	00
XII	6.0	5.9	5.2	5.8	-	04.0	88	67	81	78	23	114	028.9	30	.	05	22	.	.	.	04	03	05	09	15	10	06	07	09	.	.	.	.	.	.	.	.
GOD.	6.3	6.5	5.3	6.0	-	06.3	83	64	80	76	13	1176	044.1	9 IV	04	27	89	30	01	.	35	11	54	131	175	108	39	134	66	02	01	.	.	.	46	26	70

Mesec	Vremenski prizemak za III	Temperatura vazduha °C: 7	14	21	Srednji dnevni	III	IV	V	VI	VII	VIII	Učestina pravca i srednja jačina vetra m/s, Pa (0-13): N		NE		E		SE		S		SW		W		NW		C
												U.	S.	U.	S.	U.	S.	U.	S.	U.	S.	U.	S.		S.	U.	S.	U.
BAČKO																												
φ = 43° 10' N λ = 18° 33' E Gr. Δ G = + 1h 14 min.																												Br. St. 146
I	-	-00.4	02.8	00.3	00.7	04.0	-02.4	09.0	16,06	-09.8	23	.	.	25	03.3	01	02.0	22	03.2	.	.	02	04.5	.	.	09	02.3	34
II	-	-02.9	01.0	-01.1	-01.0	02.5	-04.4	08.5	07	-17.2	18	.	.	35	03.6	.	.	25	03.0	01	03.0	09	04.6	.	.	01	03.0	13
III	-	-00.9	04.2	00.6	01.1	05.2	-03.7	11.5	25,24	-12.0	09	01	02.0	26	03.6	01	02.0	27	03.5	01	02.0	11	04.3	.	.	03	03.0	21
IV	-	05.3	10.3	05.3	06.6	11.6	-	22.0	24,23	-	-	.	.	25	03.1	.	.	33	03.6	01	03.0	11	04.1	.	.	05	03.4	19
V	-	08.5	12.4	08.3	09.4	16.3	-	21.5	10	-	-	.	.	30	03.1	.	.	23	02.8	01	03.0	10	03.0	.	.	21	03.0	06
VI	-	14.4	20.2	14.3	15.8	21.5	06.4	27.0	28	00.4	04,03	.	.	36	02.5	01	02.0	18	02.6	.	.	05	02.6	.	.	09	02.4	21
VII	-	15.8	22.2	16.2	17.6	23.3	10.7	29.0	24	03.0	19	01	02.0	30	02.8	04	02.0	12	02.9	01	02.0	10	03.1	01	02.0	09	02.9	05
VIII	-	14.6	22.5	15.9	17.2	24.3	10.0	30.5	07	04.0	24	.	.	38	02.3	09	02.1	15	02.8	.	.	10	03.0	.	.	12	02.6	06
IX	-	10.6	20.8	12.6	14.2	21.7	07.3	29.5	12,11	-04.2	30	.	.	49	02.9	.	.	04	02.7	01	02.0	03	03.0	.	.	13	02.7	18
X	-	03.8	13.5	04.2	07.4	14.5	01.7	24.0	10	-02.8	29	.	.	35	03.5	.	.	15	02.7	02	02.5	07	02.6	01	02.0	14	02.7	19
XI	-	02.0	09.6	04.3	05.0	10.7	00.1	19.0	03	-05.4	13	01	02.0	24	02.9	.	.	34	02.6	.	.	04	02.5	.	.	09	02.3	18
XII	-	-01.2	04.8	00.4	01.1	05.7	-03.2	14.0	29	-11.0	21	.	.	40	03.1	.	.	26	02.8	.	.	05	03.6	.	.	08	03.0	14
GOD.	-	05.8	12.0	04.9	07.9	13.3	-	30.5	7 VII	-		03	02.0	413	03.0	16	02.1	294	03.0	06	02.8	87	03.5	02	02.0	113	02.7	193
ČENERING																												
φ = 43° 14' N λ = 18° 36' E Gr. Δ G = + 1h 14 min.																												Br. St. 147
I	647.2	-01.8	-00.2	-01.8	-01.4	01.2	-04.1	07.0	07	-12.4	20	14	02.1	00	01.9	03	02.3	09	03.0	07	03.9	33	03.2	04	02.0	05	03.0	10
II	644.9	-04.5	-02.1	-03.2	-03.2	-00.4	-06.1	04.8	05	-17.6	18	12	02.3	07	03.0	04	03.8	06	03.2	09	04.7	30	04.9	05	02.4	03	04.3	08
III	646.6	-02.3	01.0	-00.9	-00.8	02.7	-03.9	10.8	25	-13.0	02,01	09	02.4	03	02.0	00	03.4	06	04.3	07	04.0	37	03.1	06	02.2	04	02.0	13
IV	650.5	03.3	06.6	03.2	04.1	08.0	00.6	19.2	23	-07.3	04	05	02.4	05	03.0	03	03.7	04	03.6	18	04.7	31	03.9	08	01.8	05	03.0	09
V	650.6	05.3	08.9	06.0	06.6	10.5	03.1	18.4	10	-03.8	03,01	20	02.3	06	02.0	10	02.5	03	02.0	02	02.5	27	03.4	11	02.6	07	02.7	07
VI	653.7	12.5	16.7	12.5	13.5	18.1	09.2	23.2	23	01.4	03	07	02.9	07	03.3	08	02.5	04	03.5	05	03.6	27	02.7	08	02.4	05	02.4	19
VII	652.8	13.2	17.7	13.6	14.5	19.1	10.1	24.0	24	03.5	19	14	03.3	12	02.4	11	02.5	02	02.5	.	.	24	03.3	09	02.3	04	03.0	17
VIII	653.2	14.5	19.2	13.9	15.4	20.3	10.7	27.8	07	05.6	28	14	02.0	07	02.3	04	04.5	01	02.0	.	.	20	03.6	14	02.2	05	01.4	23
IX	654.9	09.9	16.2	10.4	11.7	17.4	07.4	26.0	11	-02.2	30	28	02.9	11	03.0	10	02.8	.	.	01	02.0	00	03.8	03	02.7	07	02.9	22
X	653.6	04.0	09.6	05.1	05.9	10.6	02.3	19.4	10	-05.0	25	20	02.4	00	03.8	04	02.0	01	03.0	05	03.8	16	03.4	13	01.8	08	02.5	18
XI	652.3	02.4	05.9	03.2	03.7	07.4	00.5	17.2	03	-03.4	17,12	20	02.4	03	02.7	03	03.3	.	.	02	03.8	17	03.9	00	02.5	03	02.0	14
XII	651.6	-02.2	01.3	-01.1	-00.8	02.5	-03.6	10.0	13	-09.6	19	20	02.8	00	02.0	04	03.0	06	03.3	04	03.2	26	04.1	10	02.6	06	03.7	09
GOD.	651.0	04.5	08.4	05.1	05.8	09.8	02.2	27.0	7 VII	-17.6	46 I	183	02.4	05	02.6	72	02.9	44	03.6	60	04.3	316	03.6	99	02.3	42	02.7	174
SOKOLAC																												
φ = 43° 27' N λ = 18° 49' E Gr. Δ G = + 1h 15 min.																												Br. St. 148
I	-	-02.6	00.0	-02.5	-01.9	01.4	-05.0	10.0	06	-15.7	30	13	01.6	.	.	.	.	.	.	26	01.0	01	01.0	.	.	13	02.2	40
II	-	-05.7	00.0	-03.4	-03.1	01.5	-07.9	09.8	09	-24.1	18	17	01.8	01	02.0	.	.	04	01.8	18	02.7	04	01.2	.	.	15	02.1	25
III	-	-02.2	04.8	-00.2	00.5	06.2	-04.5	15.6	24	-16.0	02	14	01.9	.	.	.	.	03	01.0	25	02.6	01	03.0	04	01.0	07	02.1	42
IV	-	04.2	10.9	05.5	06.5	12.6	01.3	23.3	23	-07.2	05	16	01.9	.	.	01	01.0	03	03.0	20	02.6	03	01.7	01	01.0	12	02.9	34
V	-	07.1	12.4	07.8	08.8	13.7	03.9	24.0	10	-02.2	02	35	01.0	.	.	.	.	.	.	06	02.2	04	02.5	.	.	22	02.4	26
VI	-	12.4	19.0	13.2	14.7	21.4	08.5	27.0	18	03.8	03	08	01.8	01	01.0	.	.	.	.	12	01.8	05	02.0	.	.	10	02.3	54
VII	-	12.6	20.5	13.8	14.8	21.5	06.1	28.3	22	03.9	20	15	01.9	01	02.0	.	.	.	.	01	03.0	01	03.0	.	.	15	02.6	60
VIII	-	11.9	21.8	14.0	15.4	23.0	08.2	30.8	07	02.2	28	08	02.0	01	01.0	01	01.0	.	.	06	02.2	07	01.7	.	.	08	02.1	62
IX	-	07.2	18.4	09.5	11.1	19.4	04.4	30.0	11	-07.6	30	17	01.7	01	01.0	.	.	.	.	07	01.7	.	.	.	.	10	02.8	55
X	-	00.7	11.5	03.8	04.9	12.5	-00.9	-	-	-06.1	20	12	02.0	.	.	02	01.0	01	01.0	05	02.6	03	02.3	02	01.5	14	02.6	54
XI	-	-00.4	07.6	01.8	02.7	08.9	-02.1	17.4	02	-07.2	29	14	02.0	01	01.0	.	.	.	.	10	01.7	03	01.7	.	.	12	02.2	50
XII	-	-04.4	01.2	-03.3	-02.5	02.1	-06.7	11.1	30	-18.5	27	13	01.8	.	.	.	.	.	.	16	02.6	.	.	.	.	08	02.6	56
GOD.	-	03.4	10.7	04.9	06.0	12.0	00.6	-		-26.1	48 I	102	01.7	06	01.3	04	01.0	11	01.8	152	02.3	32	01.9	04	01.2	144	02.4	556
GORAŽDE																												
φ = 43° 40' N λ = 18° 59' E Gr. Δ G = + 1h 16 min.																												Br. St. 149
I	-	00.3	03.8	01.8	01.5	04.4	-02.0	15.4	12	-07.0	23,22	.	.	23	01.2	.	.	09	00.9	.	.	01	02.0	.	.	02	01.0	58
II	-	-00.6	03.6	01.3	01.9	06.6	-02.7	16.2	06	-15.0	18	.	.	24	01.4	.	.	11	01.4	.	.	.	.	.	.	.	.	49
III	-	02.3	10.5	04.0	05.2	11.7	-00.5	20.0	24	-05.5	08	.	.	30	01.3	.	.	12	01.2	.	.	02	02.5	.	.	02	02.0	47
IV	-	07.1	15.7	09.3	10.4	17.0	03.2	27.0	23	-04.3	05	.	.	21	01.6	.	.	09	01.8	.	.	06	01.5	.	.	03	01.0	51
V	-	09.3	17.6	11.1	12.3	18.5	06.2	28.0	10	00.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	14.9	24.6	16.4	18.1	25.6	11.6	32.0	18	05.5	03	.	.	28	01.4	.	.	19	01.5	.	.	01	01.0	.	.	02	01.5	48
VII	-	15.0	25.2	17.0	18.5	26.3	12.4	32.4	23,22	07.0	20,19	.	.	22	01.4	.	.	14	01.5	.	.	02	01.5	.	.	02	02.0	53
VIII	-	15.1	26.3	17.1	18.9	27.6	12.6	33.4	07	08.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	11.1	22.3	13.2	14.9	23.2	09.3	31.4	13	-02.0	30	.	.	21	01.3	.	.	08	01.2	.	.	01	01.0	.	.	03	01.3	57
X	-	06.0	15.0	07.5	09.0	15.7	03.7	24.6	08,07	-01.0	01	.	.	15	01.3	.	.	14	01.4	.	.	03	02.3	.	.	02	01.5	59
XI	-	03.3	10.6	04.8	05.9	11.3	00.9	20.0	03	-02.0	12	.	.	28	01.3	.	.	05	01.2	.	.	.	.	.	.	03	02.0	54
XII	-	-00.6	03.0	00.8	01.0	03.7	-02.9	10.0	28	-07.5	18	.	.	19	01.2	.	.	09	01.4	.	.	02	01.5	.	.	14	01.4	53
GOD.	-	06.9	15.0	08.6	09.8	16.0	04.3	33.4	7 VII	-15.0	45 I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
LJUBINJE																												
φ = 42° 58' N λ = 18° 06' E Gr. Δ G = + 1h 27 min.																												Br. St. 150
I	-	02.5	07.7	04.3	04.9	06.4	01.8	15.0	06	-05.4	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	00.7	05.2	02.0	02.5	05.0	-01.3	09.2	07	-08.5	17	24	02.0	04	01.0	.	.	07	01.7	23	02.0	05	01.0	.	.	02	01.5	19
III	-	04.2	09.9	05.3	06.1	11.2	01.7	17.5	26,25	-05.[illegible]	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	08.3	14.7	09.3	10.4	15.9	04.8	25.5	24	-03.[illegible]	05	06	03.0	.	.	.	.	02	02.0	33	02.5	03	01.7	.	.	15	02.1	29
V	-	12.1	17.0	11.5	13.3	18.8	06.4	29.0	10	00.4	03	06	01.0	01	01.0	.	.	02	01.0	34	02.1	04	01.5	.	.	26	01.9	30
VI	-	18.4	24.7	17.4	19.5	25.9	11.3	30.2	17	04.2	04	05	02.2	02	01.5	.	.	06	01.3	24	01.8	09	01.8	.	.	10	02.2	34
VII	-	19.4	26.8	18.8	20.9	27.9	12.1	33.6	24	06.0	19	07	02.3	01	02.0	.	.	03	01.7	15	02.2	04	02.3	03	01.7	16	01.6	42
VIII	-	17.6	27.0	17.2	20.0	28.4	-	35.0	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	11.6	24.7	11.2	14.6	25.6	-	31.0	12	-	-	14	01.9	09	01.4	02	01.0	01	01.0	07	01.3	15	01.4	.	.	08	01.7	39
X	-	05.5	17.0	07.4	09.5	18.4	03.4	25.4	10	-01.0	27	13	02.0	01	01.0	.	.	06	02.0	11	02.3	01	02.0	.	.	16	01.8	50
XI	-	02.6	13.4	05.6	07.1	14.3	02.0	20.5	05	-09.0	13	08	02.1	04	01.2	.	.	.	.	20	02.2	.	.	.	.	18	04.7	42
XII	-	00.3	08.3	02.4	03.4	09.0	-	14.5	30	-	-	10	02.4	01	01.0	.	.	01	02.0	24	02.6	02	01.0	.	.	08	02.0	42
GOD.	-	08.8	16.4	09.4	11.0	17.3	-	35.0	7 VII	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dnev.)	Temperatura kod tal	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dnev.)	min	Padavine R mm Σ	Ξ	max	Broj dana sa: Tn ≤0,0	Tn <0,0	Tn <0,0	Tx ≥0,0	Tx ≥0,0	Tn ≥0,0	P(0-12) ≥1	≥1	Nm(0-10) <8,0	>8,0	R mm ≥0,1	≥1,0	≥10,0	●	≡	✱	≈	∿	▲	▲	⊤	■	▦
BR. ST. 146																																						
I	8.2	8.2	6.9	7.8	-	04.5	92	87	90	89	-	372	095.4	13	.	02	20	.	.	.	04	.	02	18	19	18	12	13	08	01	.	.	.	.	.	02	18
II	7.8	7.2	7.1	7.4	-	03.9	89	87	89	88	67	220	056.6	14	04	07	19	.	.	.	06	01	.	11	18	17	07	14	10	04	.	.	.	.	03	01	20
III	7.0	6.4	5.7	6.4	-	04.3	87	77	85	83	39	240	056.4	28	03	03	26	.	.	.	08	02	02	12	15	13	09	10	09	04	.	.	.	.	.	.	29
IV	6.6	7.1	5.5	6.4	-	05.1	76	59	75	70	26	308	074.4	09	-	.	-	.	.	-	05	01	01	07	15	14	07	13	06	04	.	.	.	.	02	.	04
V	6.4	7.4	5.0	6.3	-	06.0	69	56	73	66	29	085	022.7	29	-	.	-	.	.	-	02	.	.	05	15	11	03	14	01	.	.	.	.	.	.	.	.
VI	4.6	6.4	3.7	4.9	-	09.0	71	53	72	65	34	050	014.7	19	.	.	.	06	.	.	.	.	.	03	12	09	01	12	.	.	.	.	.	.	01	.	.
VII	3.0	5.0	3.3	3.8	-	09.6	71	47	72	63	30	055	041.3	17	.	.	.	16	.	.	01	01	10	04	07	05	01	07	.	.	.	.	.	.	.	.	.
VIII	3.0	6.9	2.8	4.2	-	09.8	78	50	72	67	26	049	019.8	25	.	.	.	17	01	.	01	.	05	03	06	04	02	06	.	.	.	.	.	01	01	02	.
IX	3.0	3.9	1.4	2.7	-	07.1	70	37	66	58	12	002	001.3	01	.	.	01	09	.	.	.	.	12	01	02	01	.	02	.	.	.	.	.	.	.	01	.
X	4.5	5.0	2.9	4.2	-	05.4	80	51	78	70	12	167	054.8	22	.	.	05	.	.	.	03	.	09	05	05	05	04	05	.	.	.	.	.	.	02	07	.
XI	6.0	5.1	4.6	5.2	-	05.0	83	61	79	75	24	183	058.0	22	.	.	17	.	.	.	01	.	10	13	11	10	04	11	01	.	.	.	.	.	01	01	.
XII	5.7	5.0	4.7	5.1	-	03.9	80	66	82	76	25	202	041.2	31	02	01	24	.	.	.	01	.	08	10	12	12	06	08	05	01	.	.	.	.	01	.	09
GOD.	5.5	6.1	4.5	5.4	-	06.1	78	60	77	72	-	1933	074.4	9	IV	-	13	-	48	01	-	32	05	59	92	137	121	56	115	40	14	.	.	.	01	11	14	80
BR. ST. 147																																						
I	8.5	8.5	8.3	8.4	-	04.1	96	92	97	95	50	414	071.2	01	05	11	22	.	.	.	06	01	.	22	21	16	10	12	14	03	.	.	.	.	01	05	31
II	8.3	7.7	7.0	7.7	-	03.5	97	90	93	93	58	208	032.0	14	06	13	23	.	.	.	11	06	02	18	22	19	10	10	18	04	02	.	.	.	03	02	28
III	7.3	6.8	6.1	6.7	-	03.6	86	74	83	81	34	243	060.1	28	02	06	26	.	.	.	07	03	04	14	20	15	10	09	19	03	.	.	.	.	.	02	31
IV	7.1	7.7	5.9	6.9	-	04.6	80	65	79	74	32	366	101.0	09	.	04	12	.	.	.	11	03	03	11	17	12	08	10	10	01	01	.	.	.	03	.	21
V	7.3	8.3	6.3	7.3	-	05.8	84	71	81	79	39	115	024.8	23	.	.	05	.	.	.	07	02	.	13	22	17	03	17	08	.	.	.	.	.	03	02	05
VI	4.4	6.0	3.5	4.7	-	08.8	79	64	81	74	35	065	014.0	19	.	.	.	.	.	.	03	01	05	04	12	09	02	12	.	.	.	.	.	.	.	.	.
VII	4.0	5.3	4.1	4.4	-	09.4	82	64	81	75	40	096	053.0	17	.	.	.	03	.	.	05	01	12	07	10	09	02	10	.	.	.	.	.	.	05	04	.
VIII	3.3	5.9	2.5	3.9	-	09.5	77	58	80	72	35	046	020.0	25	.	.	.	03	.	.	05	01	09	04	09	06	03	09	.	.	.	.	.	.	05	01	.
IX	4.0	3.9	2.2	3.4	-	06.7	73	48	71	64	19	004	002.0	05	.	.	01	04	.	.	03	.	13	02	03	02	.	03	.	.	.	.	.	.	01	04	.
X	6.1	4.9	4.9	5.3	-	05.2	82	60	83	75	25	170	070.8	22	.	02	09	.	.	.	04	02	10	11	07	06	04	06	03	01	01	.	.	.	05	07	05
XI	6.9	7.2	5.5	6.5	-	04.5	79	70	77	76	23	196	052.8	16	.	.	14	.	.	.	07	02	05	14	12	10	06	09	06	02	.	.	.	.	02	02	08
XII	6.1	5.0	5.7	5.6	-	03.4	79	71	79	76	24	198	041.2	29	.	08	23	.	.	.	08	04	06	11	13	12	06	07	08	01	.	.	.	.	02	03	16
GOD.	6.1	6.4	5.2	5.9	-	05.8	82	68	82	77	19	2121	101.0	9	IV	13	44	135	10	.	.	77	26	69	131	168	133	64	110	86	15	04	.	.	.	28	32	145
BR. ST. 148																																						
I	9.5	8.3	8.1	8.6	027.3	03.9	93	89	92	92	66	066	018.9	03	04	13	25	.	.	.	.	.	.	21	17	12	02	09	13	.	.	.	.	.	.	08	30
II	9.4	8.5	7.2	8.4	-	03.5	89	83	88	86	64	054	012.4	16	11	10	26	.	.	.	02	.	.	17	22	14	01	07	18	01	.	.	.	.	.	06	23
III	7.9	5.4	5.7	6.3	129.1	04.1	90	72	89	83	44	082	017.3	28	05	05	27	.	.	.	01	.	03	13	19	11	04	06	17	02	.	.	.	.	.	02	20
IV	6.9	6.5	5.6	6.3	-	05.9	92	64	85	80	38	078	023.1	15	.	.	11	.	.	.	.	.	03	10	13	10	02	10	07	02	.	.	.	.	.	01	05
V	7.2	8.6	7.9	7.9	-	07.4	93	75	90	86	37	099	024.7	23	.	.	04	.	.	.	.	.	01	17	22	16	03	20	04	.	.	.	.	.	.	02	03
VI	5.1	7.3	5.3	5.9	186.6	10.5	93	67	88	82	42	083	030.0	30	.	.	.	10	.	.	.	.	03	07	19	11	02	19	.	.	.	.	.	.	.	05	04
VII	4.3	5.5	3.6	4.4	265.2	10.0	91	59	86	79	37	085	023.6	17	.	.	.	09	.	.	01	.	14	09	09	09	04	09	.	.	.	.	.	.	01	06	.
VIII	5.7	6.3	3.4	5.1	218.7	10.6	96	58	89	81	36	060	011.7	23	.	.	.	12	01	.	.	.	05	05	15	11	03	15	.	.	.	.	.	01	03	14	.
IX	5.7	4.6	2.7	4.3	206.7	08.1	95	56	88	79	35	021	008.2	03	.	.	07	07	01	.	.	.	08	05	06	03	.	06	.	.	.	.	.	.	.	13	.
X	5.5	5.2	4.7	5.1	-	05.3	94	61	90	82	24	089	025.3	22	.	.	18	.	.	.	.	.	10	12	08	08	04	07	02	.	.	.	.	.	.	11	04
XI	7.0	6.4	5.7	6.4	-	04.5	91	63	88	81	32	082	014.6	17	.	.	23	.	.	.	.	.	03	11	11	11	02	10	06	03	.	.	.	.	.	05	05
XII	6.9	6.0	5.6	6.2	098.9	03.3	85	72	84	80	43	019	005.4	24	09	08	25	.	.	.	01	01	06	12	11	07	.	02	09	.	.	.	.	.	.	07	15
GOD.	6.8	6.6	5.5	6.2	-	06.4	91	68	88	82	24	818	030.0	30	VI	29	36	166	38	02	.	05	01	56	139	172	123	27	120	76	08	.	.	.	01	04	80	109
BR. ST. 149																																						
I	9.0	8.3	8.2	8.5	-	-	-	-	-	-	-	130	048.0	13	.	03	20	.	.	.	.	.	01	23	12	12	04	08	06	.	.	.	.	.	.	09	19
II	8.6	7.9	8.4	8.3	-	-	-	-	-	-	-	108	026.5	16	02	01	20	.	.	.	.	.	01	18	14	11	03	08	07	.	.	.	.	.	.	11	10
III	5.4	6.2	5.3	5.6	-	06.0	92	77	89	86	46	093	024.0	06	.	.	14	.	.	.	.	.	08	12	10	09	05	10	03	.	.	.	.	.	.	14	02
IV	4.9	5.8	5.8	5.5	-	08.2	92	75	80	82	48	090	030.4	29	.	.	05	05	.	.	.	.	07	09	10	09	03	10	.	.	.	.	.	.	.	13	.
V	5.6	7.3	7.3	6.7	-	09.4	93	73	87	85	35	079	015.6	18	.	.	.	02	.	.	.	.	01	12	13	12	02	13	.	.	.	.	.	.	01	.	.
VI	3.6	5.4	4.7	4.6	-	13.4	92	70	86	83	43	075	017.8	19	.	.	.	22	04	.	.	.	08	07	14	09	03	14	.	.	.	.	.	.	03	18	.
VII	6.9	4.4	3.2	4.8	-	13.7	93	67	88	83	36	037	020.2	06	.	.	.	22	08	.	.	.	06	06	07	06	01	06	.	.	.	.	.	.	02	15	.
VIII	9.7	5.5	4.7	6.7	-	13.8	94	64	90	83	42	057	010.2	04	.	.	.	23	09	.	.	.	.	11	10	09	01	10	.	.	.	.	.	01	03	24	.
IX	9.4	3.5	2.3	5.1	-	11.7	95	72	93	87	46	024	012.6	01	.	.	01	12	06	.	.	.	.	05	06	04	01	06	.	.	.	.	.	.	.	24	.
X	3.2	4.9	3.6	3.9	-	07.8	93	75	89	86	17	093	030.2	22	.	.	02	.	.	.	.	.	13	05	07	07	03	07	01	.	.	.	.	.	01	19	01
XI	3.7	6.1	5.1	5.0	-	06.3	94	79	90	87	41	080	018.6	16	.	.	11	.	.	.	.	.	09	09	10	10	04	10	.	.	.	.	.	.	.	18	.
XII	6.0	6.1	6.3	6.1	-	04.7	94	92	91	92	69	050	010.2	22	.	02	26	.	.	.	.	.	09	13	11	11	01	09	04	01	.	.	.	.	.	13	08
GOD.	6.3	6.0	5.4	5.9	-	-	-	-	-	-	-	916	048.0	16	I	02	06	99	86	27	.	.	.	63	130	124	109	31	111	21	01	.	.	.	01	10	178	8
BR. ST. 150																																						
I	7.5	7.5	6.6	7.2	-	05.7	86	75	89	83	48	518	104.2	01	.	.	13	.	.	.	.	.	03	17	18	17	11	18	01	.	.	.	.	.	03	01	.
II	7.2	6.1	5.6	6.3	-	04.8	90	82	88	86	54	172	041.0	17	.	.	21	.	.	.	01	.	04	10	17	16	07	12	07	.	.	.	01	.	03	01	-
III	6.1	5.9	5.4	5.8	-	05.1	79	58	77	72	26	247	062.2	04	.	.	11	.	.	.	.	.	08	14	14	13	09	13	02	.	.	.	.	01	03	01	01
IV	5.9	6.2	4.2	5.4	-	06.3	74	53	69	65	28	276	064.8	08	.	.	03	07	.	.	.	.	05	07	12	12	09	12	03	03	.	.	.	.	02	.	.
V	5.2	5.6	3.3	4.7	-	07.3	69	48	68	62	26	059	023.2	23	.	.	.	01	.	.	.	.	04	04	10	07	02	10	.	.	.	.	.	.	04	.	.
VI	3.3	4.2	2.9	3.5	-	10.6	68	48	64	60	25	046	018.4	07	.	.	.	22	02	.	.	.	13	04	07	06	02	07	.	.	.	.	.	.	01	.	.
VII	2.8	3.4	0.9	2.4	-	11.6	70	43	71	61	26	059	043.0	17	.	.	.	23	14	.	.	.	19	01	06	04	02	06	.	.	.	.	.	.	01	.	.
VIII	-	-	-	-	-	11.5	76	42	75	64	23	082	034.0	25	-	.	-	22	17	-	.	.	-	-	05	05	03	05	.	.	.	.	.	.	-	-	.
IX	1.4	1.7	0.9	1.3	-	09.0	69	54	71	64	37	000	000.0	18	-	.	-	18	04	-	.	.	24	.	.	.	.	.	.	.	.	.	.	.	.	.	.
X	2.7	3.4	2.3	2.8	-	06.7	80	55	78	71	31	134	064.2	02	.	.	01	03	.	.	.	.	19	03	08	05	04	05	.	.	.	.	.	.	02	06	.
XI	5.3	5.1	3.8	4.7	-	06.2	86	64	86	79	35	252	078.8	15	.	.	11	.	.	.	.	.	10	09	14	10	06	11	.	.	.	.	.	.	04	04	.
XII	5.5	4.6	3.7	4.6	-	04.9	89	62	88	79	38	341	075.4	28	-	.	-	.	.	-	.	.	12	09	14	11	08	11	02	.	.	.	.	.	04	04	01
GOD.	-	-	-	-	-	07.5	78	57	77	70	23	2186	104.2	4	I	-	.	-	91	37	-	01	.	-	-	125	106	63	110	15	03	.	.	01	01	-	-	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dles)	Max	Min	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12) N č.	j.	NE č.	j.	E č.	j.	SE č.	j.	S č.	j.	SW č.	j.	W	j.	NW č.	j.	C č.
BILEĆA φ = 42° 53' N λ = 18° 27' E Gr. ΔG = + 1h 14 min.																												BR. ST. 151
I	-	03.1	07.2	04.1	04.6	08.3	01.2	15.0	06	-06.6	26	19	02.2	07	01.4	06	01.2	32	01.5	19	01.7	03	02.3	.	.	.	.	07
II	-	01.8	06.4	03.6	03.8	07.6	-00.9	13.2	14	-11.6	18	22	03.0	18	01.4	03	01.0	18	01.9	15	02.8	05	04.4	.	.	.	.	03
III	-	03.8	10.3	05.6	06.3	11.1	01.9	19.0	25	-05.8	01	20	03.1	11	01.2	02	01.0	25	02.3	13	02.8	10	03.6	.	.	03	01.3	09
IV	-	08.7	15.1	10.2	11.0	15.9	06.4	25.8	25,24	-02.2	05	21	02.7	05	01.4	05	01.0	22	01.7	18	02.6	08	02.4	.	.	02	02.0	09
V	-	11.6	17.5	12.3	13.4	18.4	08.1	25.4	10	01.6	03	28	02.6	07	01.7	05	01.0	23	01.1	10	01.5	11	01.7	02	01.5	.	.	07
VI	-	17.1	24.7	18.4	19.7	25.6	13.2	31.6	18	05.6	04	17	01.6	07	01.3	06	01.0	25	01.1	16	01.2	12	01.3	.	.	.	.	07
VII	-	19.1	27.5	20.7	22.0	28.4	14.6	35.6	23	08.8	19	23	02.0	09	02.1	02	02.0	21	01.1	13	01.3	10	01.9	.	.	01	01.0	14
VIII	-	17.9	26.9	20.6	21.5	28.3	14.7	34.4	07	10.4	26	21	01.5	05	01.0	03	01.0	24	01.2	03	01.3	09	01.2	01	01.0	03	01.7	24
IX	-	14.1	25.7	16.7	18.3	26.1	11.1	33.0	16	03.0	30	26	02.0	07	01.6	03	01.0	15	01.0	07	01.3	07	01.6	01	01.0	01	02.0	23
X	-	07.6	18.3	10.6	11.8	18.7	05.2	27.0	12	-00.2	26	26	02.4	02	01.5	03	01.0	23	01.3	13	01.5	05	01.6	01	01.0	.	.	20
XI	-	05.9	13.6	08.2	08.9	14.3	03.4	20.6	05	-01.4	12	12	02.6	05	01.4	03	01.0	30	01.4	20	01.6	02	02.5	.	.	.	.	18
XII	-	02.4	08.7	03.8	04.7	09.5	00.3	15.6	02	-05.8	21	29	02.4	02	01.0	03	02.0	32	01.2	14	02.8	02	03.5	.	.	.	.	11
GOD.	-	09.4	16.8	11.2	12.2	17.7	06.6	35.6	23.VII	-11.6	18.II	264	02.3	85	01.4	44	01.1	290	01.5	161	01.9	84	02.1	05	01.2	10	01.6	152
LASTVA φ = 42° 43' N λ = 18° 29' E Gr. ΔG = + 1h 14 min.																												BR. ST. 152
I	-	04.2	08.5	05.8	06.1	09.2	02.5	15.0	06	-04.2	23,22	01	02.0	09	02.2	05	02.2	38	01.3	02	01.5	01	01.0	03	02.3	09	02.6	25
II	-	02.2	06.9	03.5	04.1	08.1	00.1	14.0	07	-10.0	18	01	01.0	06	01.5	02	01.0	07	01.6	.	.	.	.	01	03.0	29	02.3	38
III	-	04.1	11.5	05.0	06.4	12.1	01.9	20.0	25	-06.4	02	01	01.0	10	02.3	02	01.5	13	02.0	.	.	.	.	01	01.0	32	02.1	34
IV	-	08.5	16.1	08.8	10.5	16.8	05.1	25.4	24	-01.4	05	.	.	13	01.5	04	01.0	13	02.5	.	.	.	.	01	02.0	34	03.1	25
V	-	10.7	18.9	11.5	13.1	19.5	07.4	28.0	10	-00.2	03	.	.	11	01.7	01	01.0	05	01.4	.	.	01	04.0	01	01.0	33	02.4	41
VI	-	17.6	25.3	17.3	19.4	25.9	12.0	30.6	18	04.4	04	.	.	04	01.2	02	02.5	04	02.2	.	.	.	.	03	01.0	34	02.1	43
VII	-	18.8	27.4	20.0	21.6	28.3	13.5	33.6	23	07.4	18	.	.	02	01.0	03	01.3	11	01.5	.	.	01	01.0	.	.	29	02.2	47
VIII	-	18.3	27.8	19.4	21.2	28.8	13.4	34.2	07	09.2	27	.	.	03	01.0	06	01.5	07	01.9	.	.	.	.	01	02.0	32	02.2	44
IX	-	12.9	25.8	16.1	17.7	26.1	09.9	32.4	13	02.0	30	.	.	05	01.0	03	01.3	14	01.7	.	.	.	.	.	.	31	02.1	37
X	-	08.3	17.4	10.3	11.6	18.0	05.8	24.2	10	-00.2	25	.	.	08	01.6	03	01.3	07	01.6	.	.	.	.	.	.	29	02.1	46
XI	-	05.0	13.0	06.4	07.7	13.6	03.4	17.6	05	-00.6	13,12	01	02.0	06	01.2	07	01.3	09	01.3	.	.	01	02.0	05	01.2	22	02.1	39
XII	-	01.5	08.2	02.9	03.8	08.6	-00.2	15.8	30	-07.4	21	.	.	16	01.6	08	02.2	16	01.9	.	.	.	.	.	.	21	03.0	32
GOD.	-	09.3	17.2	10.6	11.9	17.9	06.2	34.2	7.VIII	-10.0	18.II	04	01.5	93	01.6	46	01.6	144	01.7	02	01.5	04	02.0	16	01.6	335	02.3	451
SR SRBIJA **PALIĆ** φ = 46° 06' N λ = 19° 46' E Gr. ΔG = + 1h 18 min.																												BR. ST. 153
I	751.8	-02.8	-00.2	-02.0	-01.7	00.7	-04.5	07.1	06	-16.3	03	03	02.0	04	01.2	06	01.3	05	01.0	11	01.9	11	02.2	09	-32.9	.	153.2	-24
II	748.4	-01.1	01.7	-00.3	00.0	02.8	-03.0	07.5	15	-11.9	03	08	02.1	06	02.2	01	03.0	07	02.0	05	01.6	21	02.0	19	01.9	12	02.1	05
III	749.7	02.3	07.6	04.7	04.8	08.7	01.2	18.0	25	-10.2	02	08	02.6	05	02.6	08	02.8	16	02.6	14	02.9	15	02.4	10	02.0	13	02.5	04
IV	750.4	08.2	14.4	10.1	10.7	15.9	06.0	25.1	20	-01.2	05	13	03.2	05	02.4	06	02.7	13	02.3	11	02.4	13	03.1	13	02.6	15	01.9	01
V	751.2	12.2	17.7	13.2	14.1	19.1	09.2	24.1	10	01.8	03	15	03.0	04	02.0	04	01.2	09	01.8	06	01.8	16	02.1	11	02.6	22	02.3	06
VI	752.3	18.5	24.4	19.1	20.3	25.4	14.6	31.0	22	08.7	03	13	02.4	11	01.7	07	01.3	08	01.9	05	01.6	04	02.5	14	02.1	24	02.3	04
VII	751.3	18.4	24.7	18.8	20.2	25.9	14.8	32.0	23	11.0	19	15	02.3	06	01.7	04	01.2	07	02.0	04	02.0	12	01.8	15	02.2	24	02.2	06
VIII	751.6	17.9	24.6	18.6	20.0	25.9	14.9	32.3	07	09.2	14	11	01.5	13	01.8	12	01.8	11	01.7	06	02.7	05	02.2	14	01.5	14	02.2	07
IX	755.2	12.8	20.5	14.4	15.5	21.5	10.6	29.8	11	-00.4	30	16	02.0	05	01.8	04	01.5	05	01.8	04	01.5	11	02.4	15	02.1	21	01.7	09
X	755.4	06.2	14.8	08.6	09.5	15.6	04.8	24.6	11	-01.3	16	08	01.8	05	01.2	06	01.5	06	01.8	12	01.7	20	02.0	16	02.2	12	02.3	08
XI	753.6	05.2	11.5	07.0	07.7	12.2	03.7	18.0	04,02	-01.0	09	09	02.1	04	01.5	03	01.0	06	01.7	14	01.9	28	02.2	10	02.5	12	02.4	04
XII	756.6	-00.1	03.0	00.6	01.1	03.9	-02.2	13.8	01	-16.1	27	14	01.7	11	02.5	03	02.0	05	02.4	09	02.2	15	02.0	17	01.6	13	02.1	06
GOD.	752.3	08.1	13.7	09.4	10.2	14.8	05.8	32.3	7.VIII	-16.3	3. I	133	02.3	79	01.9	64	01.6	98	02.0	101	02.1	171	02.2	163	-27.9	182	02.2	-84
SOMBOR φ = 45° 45' N λ = 19° 06' E Gr. ΔG = + 1h 16 min.																												BR. ST 154
I	-	-03.2	00.0	-02.8	-02.2	01.2	-05.6	06.0	15	-17.0	03	07	03.3	06	02.5	06	02.7	16	02.2	08	01.6	02	01.5	06	02.3	11	03.0	31
II	-	-01.4	02.4	00.3	00.4	03.7	-02.7	14.0	09	-10.6	03	13	02.9	02	04.0	05	03.0	05	02.0	11	02.1	12	02.2	02	01.5	14	02.6	17
III	-	02.4	08.4	05.0	05.2	09.5	01.2	20.6	25	-09.8	02	13	03.2	03	02.7	09	03.1	14	03.6	06	02.5	06	03.5	13	02.5	07	03.4	22
IV	-	08.1	14.7	10.2	10.8	16.3	05.6	26.1	20	-02.1	05	22	03.1	02	02.5	03	03.0	08	02.8	08	02.0	06	02.8	13	02.8	05	02.8	23
V	-	11.9	17.5	13.0	13.9	19.1	08.6	26.6	10	00.9	03	16	03.2	03	01.7	02	02.0	09	02.4	.	.	05	02.0	14	02.6	19	03.0	25
VI	-	18.2	24.7	18.9	20.2	25.9	14.0	30.6	23	08.6	03	13	02.2	01	05.0	04	01.8	08	01.8	.	.	03	02.0	17	02.4	13	02.7	31
VII	-	18.4	24.7	18.9	20.2	26.4	14.0	32.0	11	10.0	27	15	03.0	05	02.6	.	.	06	01.8	02	02.0	04	02.0	10	02.1	17	02.8	34
VIII	-	17.6	25.1	18.6	20.0	26.2	14.6	33.1	07	09.8	28	03	02.3	04	01.5	04	01.5	10	01.6	03	01.3	03	01.0	06	01.7	09	02.4	51
IX	-	11.9	20.9	13.9	15.1	22.0	09.5	31.0	11	-02.2	30	13	03.0	04	02.0	02	02.5	01	02.0	04	01.5	09	01.9	04	02.0	09	01.8	44
X	-	05.7	15.3	08.7	09.6	16.1	04.1	25.2	09	-02.0	19	03	02.0	04	01.8	02	02.0	07	01.4	07	01.9	05	01.8	09	02.0	12	02.7	44
XI	-	05.1	12.1	07.2	07.9	12.9	03.5	21.1	03	-01.6	07	07	02.9	02	02.0	.	.	03	02.0	12	01.9	15	02.2	11	02.1	05	03.2	35
XII	-	-00.3	02.8	00.0	00.6	03.7	-02.9	13.4	01	-19.2	27	07	03.1	02	03.0	05	02.6	04	03.0	09	02.0	02	02.0	18	02.3	06	03.2	40
GOD.	-	07.9	14.0	09.3	10.1	15.2	05.3	33.1	7.VIII	-19.2	17.XII	132	02.9	38	02.4	42	02.6	91	02.3	70	01.9	72	02.2	123	02.3	127	02.8	397
SID φ = 45° 07' N λ = 19° 15' E Gr. ΔG = + 1h 17 min.																												BR. ST. 155
I	-	-01.3	01.3	-00.5	-00.2	02.4	-03.8	10.0	16,15	-13.5	09	04	02.8	02	02.5	10	02.2	45	03.2	02	02.5	.	.	03	01.7	23	03.0	04
II	-	-01.0	03.5	00.4	00.8	04.6	-03.0	16.5	09	-10.5	18	06	02.0	01	03.0	04	03.2	43	02.6	02	01.5	.	.	.	.	27	02.7	01
III	-	02.8	09.2	05.4	05.7	10.3	00.9	22.0	25	-08.5	02	03	02.3	.	.	02	02.5	34	03.4	02	02.5	01	05.0	10	01.9	27	02.7	14
IV	-	08.6	15.5	10.3	11.1	16.8	05.9	27.0	20	-02.0	04	13	02.7	.	.	05	02.4	32	03.0	.	.	.	.	04	01.8	32	03.0	04
V	-	11.6	18.3	13.1	14.0	19.8	08.4	29.0	10	00.5	02	04	02.0	.	.	02	04.0	20	02.8	03	02.7	.	.	02	02.0	56	02.6	06
VI	-	17.7	25.4	18.9	20.2	26.4	13.7	31.5	17	07.0	03	.	.	.	.	09	01.9	20	02.6	02	01.5	03	01.3	08	01.5	38	02.7	10
VII	-	18.1	25.2	19.3	20.5	26.3	13.9	33.0	23	09.5	27,18	01	02.0	.	.	11	01.7	13	01.9	05	01.6	01	01.0	02	01.5	40	02.6	20
VIII	-	17.9	26.1	19.5	20.7	26.9	14.4	33.0	07	09.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	13.1	22.2	15.2	16.4	23.3	10.1	34.0	11	-02.0	29	06	01.8	.	.	07	02.0	17	02.4	07	02.1	01	04.0	02	01.5	23	02.4	27
X	-	06.5	15.7	09.4	10.3	16.5	04.5	25.5	11	-02.0	25	08	01.5	01	01.0	15	02.0	22	02.1	.	.	.	.	10	01.8	30	02.1	07
XI	-	05.1	12.2	07.3	08.0	13.3	03.2	21.5	19,03	-02.5	14	06	02.2	03	02.3	16	02.2	17	02.4	08	01.9	08	02.5	10	02.4	22	03.0	.
XII	-	00.0	03.6	00.8	01.3	04.1	-02.0	15.5	01	-11.5	27	12	02.2	06	02.2	06	02.2	24	02.3	01	02.0	01	02.0	20	02.2	23	02.3	.
GOD.	-	08.3	14.8	09.9	10.7	15.9	05.5	34.0	4.IX	-13.5	9. I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Tn ≤ -10.0	Tx ≤ 0.0	Tn < 0.0	Tx ≥ 25.0	Tx ≥ 30.0	Tn ≥ 20.0	F (0-12) ≥ 6	Nm (0-10) ≥ 8	R mm < 2,0	> 8,0	≥ 0,1	≥ 1,0	≥ 10.0	●	*	⁂	≈	▲	▲	⊤	≡	▦
BILEĆA BR. ST. 151																																				
I	8.8	8.9	8.2	8.6	-	05.8	87	84	88	86	62	308	046.8	01	.	12	.	.	.	.	.	.	.	23	21	20	09	21	01	.	.	.	.	01	03	01
II	7.7	8.6	7.9	8.1	-	05.4	84	81	86	84	51	188	040.7	14	01	01	18	.	.	.	04	.	02	17	17	15	06	13	05	.	.	.	.	06	01	11
III	6.9	6.8	6.5	6.8	-	05.6	77	69	77	75	49	274	052.6	06	.	.	09	.	.	.	03	.	05	17	13	13	09	12	03	.	.	.	.	06	.	02
IV	6.7	6.7	5.1	6.2	-	07.3	78	63	74	72	41	251	071.8	09	.	.	01	02	.	.	02	.	05	11	13	11	07	13	01	.	.	.	.	02	.	.
V	6.5	7.3	5.0	6.3	-	08.6	79	61	76	72	42	074	018.3	29	.	.	.	01	.	.	.	.	01	08	10	07	04	10	.	.	.	.	.	05	.	.
VI	3.7	6.2	3.8	4.6	-	11.4	76	50	70	65	39	055	014.9	19	.	.	.	21	04	.	.	.	06	06	07	06	03	07	.	.	.	.	.	06	.	.
VII	2.8	4.1	2.8	3.2	-	12.3	70	50	66	62	39	046	031.6	17	.	.	.	24	16	.	.	.	17	06	06	04	01	06	.	.	.	.	.	04	.	.
VIII	2.8	5.5	1.8	3.4	-	12.5	76	52	70	66	40	132	044.2	25	.	.	.	22	14	.	.	.	13	03	07	06	05	07	.	.	.	.	.	07	.	.
IX	2.4	3.5	0.8	2.2	-	11.7	86	51	82	73	42	817	015.2	18	.	.	.	18	06	.	.	.	18	.	02	02	01	02	.	.	.	.	.	01	.	.
X	4.3	4.9	3.8	4.4	-	-	-	-	-	-	-	133	048.1	02	.	.	01	05	.	.	.	.	15	11	06	05	04	06	.	.	.	.	.	05	.	.
XI	6.4	5.8	4.8	5.7	-	07.1	88	68	88	81	43	222	050.6	10	.	.	02	.	.	.	.	.	07	11	13	11	07	13	.	.	.	.	.	08	.	.
XII	5.5	4.5	4.7	4.9	-	05.1	80	66	82	76	44	194	052.4	28	.	.	17	.	.	.	05	.	10	10	12	11	07	12	02	.	.	.	.	06	.	01
GOD.	5.4	6.1	4.6	5.4	-	-	-	-	-	-	-	1894	071.8	9 IV	01	13	48	94	40	.	14	.	99	123	127	111	65	122	12	.	.	.	.	57	04	15

H_e = 476 m H_b = - m h_t = 2.0 m h_r = 1.0 m

LASTVA BR. ST. 152																																				
I	7.3	7.6	7.6	7.5	-	05.9	88	70	86	81	42	351	083.6	02	.	.	09	.	.	.	04	.	03	17	19	16	10	19	02	01	.	.	.	.	02	09	.
II	6.5	7.0	7.4	7.0	-	05.2	88	70	87	82	40	184	036.9	15	01	.	14	.	.	.	02	.	04	14	22	16	08	16	08	02	.	.	03	.	03	03	09
III	5.7	5.3	5.2	5.4	-	05.6	86	57	81	74	32	226	063.4	06	.	.	11	.	.	.	04	.	08	09	17	12	07	16	01	.	.	.	.	.	02	.	01
IV	4.8	5.1	4.8	4.9	-	06.6	82	46	78	68	26	230	070.2	09	.	.	01	01	.	.	06	02	05	06	12	11	06	12	01	.	.	.	01	.	.	01	01
V	4.0	6.1	3.8	4.6	-	08.1	81	50	80	70	28	058	027.2	23	.	.	01	01	.	.	.	.	06	05	09	08	02	09	.	.	.	.	.	.	06	.	.
VI	2.5	3.9	1.7	2.7	-	11.6	75	50	77	67	31	037	009.5	19	.	.	.	21	04	.	.	.	14	.	07	06	.	07	.	.	.	.	.	.	02	.	.
VII	1.9	3.2	1.5	2.2	-	12.8	75	46	79	67	27	063	026.8	17	.	.	.	25	14	.	03	.	21	03	08	04	03	08	.	.	.	.	.	.	03	.	.
VIII	1.7	4.2	1.8	2.6	-	12.5	77	44	78	66	29	042	017.2	25	.	.	.	25	15	.	.	.	17	01	08	05	02	08	.	.	.	.	.	.	04	01	.
IX	1.2	2.3	1.3	1.6	-	09.7	77	38	76	64	22	014	013.5	01	.	.	.	20	04	.	.	.	22	.	02	01	01	02	.	.	.	.	.	.	01	02	.
X	3.4	3.9	2.3	3.2	-	07.5	83	51	83	73	39	164	070.2	02	.	.	01	.	.	.	.	.	15	03	06	05	05	06	.	.	.	.	.	.	02	04	.
XI	4.1	3.6	3.0	3.6	-	06.6	91	65	90	82	40	200	051.2	15	.	.	04	.	.	.	01	.	13	05	10	10	05	10	.	.	.	.	.	.	05	06	.
XII	4.8	3.9	3.7	4.1	-	05.0	88	62	90	80	39	204	062.5	28	.	.	15	.	.	.	03	01	13	07	11	09	05	11	.	.	.	.	.	.	04	02	.
GOD.	4.0	4.7	3.7	4.1	-	08.1	82	54	82	72	22	1773	083.6	2.1	01	.	56	93	37	.	23	03	141	70	131	103	54	124	12	03	.	.	04	.	34	28	11

H_e = 295 m H_b = - m h_t = 2.0 m h_r = 1.0 m

PALIĆ BR. ST. 153																																				
I	8.5	8.0	7.5	8.0	034.5	03.7	90	84	89	88	66	072	029.1	17	03	13	26	.	.	.	02	.	01	18	12	06	03	09	08	02	.	.	.	.	.	12	29
II	8.4	8.4	7.7	8.2	059.4	04.0	88	81	88	86	55	060	014.1	14	02	05	24	.	.	.	02	.	.	16	21	12	02	09	16	02	.	.	.	.	.	09	09
III	7.8	8.0	6.4	7.4	097.3	05.2	87	68	83	79	37	063	010.9	15	01	01	11	.	.	.	06	01	01	17	17	13	01	13	06	.	.	.	01	.	.	02	06
IV	6.0	7.6	4.6	6.1	165.0	06.9	81	54	73	70	32	040	009.6	09	.	.	02	02	.	.	10	01	.	06	13	11	.	13	.	.	.	.	.	01	03	.	.
V	6.2	8.0	5.4	6.5	157.8	08.6	80	56	77	71	29	046	008.3	23	.	.	.	.	.	.	06	.	01	09	15	10	.	15	.	.	.	.	.	.	07	01	.
VI	3.9	6.2	5.0	5.0	256.1	12.4	76	52	76	68	35	081	025.6	30	.	.	.	20	02	.	02	.	03	06	14	07	03	14	.	.	.	.	.	.	11	.	.
VII	4.1	5.1	4.1	4.4	283.3	12.9	79	55	81	72	38	090	028.3	09	.	.	.	20	06	.	04	.	08	05	11	09	04	11	.	.	.	.	.	01	03	.	.
VIII	4.5	5.3	3.5	4.4	256.4	13.3	84	57	85	75	40	135	045.3	25	.	.	.	16	05	.	03	.	08	04	09	08	04	09	.	.	.	.	.	01	11	01	.
IX	5.3	4.9	3.1	4.4	219.6	10.2	86	56	81	74	39	046	031.2	17	.	.	01	08	.	.	.	.	07	04	10	05	01	10	.	.	.	.	.	.	03	02	.
X	5.3	5.4	3.4	4.7	155.6	07.0	90	57	84	77	43	022	008.2	02	.	.	04	.	.	.	.	.	10	07	08	03	.	08	.	.	.	.	.	.	.	04	.
XI	7.4	7.3	6.3	7.0	101.1	06.2	89	64	84	79	31	016	005.0	22	.	.	03	.	.	.	.	.	03	13	08	04	.	08	.	.	.	.	.	.	.	04	.
XII	7.6	8.2	7.8	7.9	045.1	04.5	91	82	91	88	49	042	007.3	24	04	02	24	.	.	.	02	.	02	18	15	12	.	11	05	.	.	.	.	.	.	14	07
GOD.	6.2	6.9	5.4	6.2	1831.2	07.9	85	63	82	77	29	713	045.3	15 VIII	10	21	95	66	13	.	37	02	44	123	153	100	18	130	35	04	.	.	01	03	38	49	51

SR SRBIJA

H_e = 102 m H_b = 104.9 m h_t = 2.0 m h_r = 1.4 m

SOMBOR BR. ST. 154																																				
I	8.5	8.2	6.4	7.7	037.9	03.7	91	84	90	88	68	079	025.8	17	07	11	27	.	.	.	02	01	02	18	15	08	03	12	06	02	.	01	.	.	.	09	31
II	8.3	7.4	7.4	7.7	071.6	04.1	91	79	88	86	51	064	-	-	01	05	22	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	7.5	8.3	6.6	7.5	110.6	05.3	88	65	84	79	32	061	013.8	15	.	01	10	.	.	.	11	04	01	14	18	12	02	13	07	.	.	.	.	.	.	01	05
IV	6.4	7.7	5.3	6.5	175.1	07.0	85	54	73	71	30	056	012.6	09	.	.	02	02	.	.	13	03	.	09	13	09	01	13	.	.	.	.	.	02	02	.	.
V	6.5	8.4	5.9	6.9	162.5	08.6	84	55	78	72	32	038	008.0	18	.	.	.	02	.	.	09	02	01	13	12	09	.	12	.	.	.	.	.	.	03	04	.
VI	4.9	6.0	5.2	5.4	273.0	12.7	81	51	79	70	32	038	013.2	19	.	.	.	21	02	.	07	01	03	05	16	08	01	16	.	.	.	.	.	.	08	03	.
VII	4.1	5.2	4.0	4.5	281.9	13.0	82	53	83	73	35	049	013.7	26	.	.	.	20	11	.	06	04	10	07	12	06	02	12	.	.	.	.	.	.	06	.	.
VIII	4.4	4.8	3.2	4.1	271.6	13.9	90	57	89	78	38	158	061.0	25	.	.	.	19	06	.	09	01	07	04	12	09	05	12	.	.	.	.	.	01	10	03	.
IX	5.4	5.4	2.6	4.5	218.1	10.5	94	55	86	78	30	018	007.1	17	.	.	02	09	01	.	05	.	06	03	09	03	.	09	.	.	.	.	.	.	03	02	.
X	5.7	5.9	3.6	5.1	150.4	07.0	94	54	86	78	32	038	012.5	02	.	.	07	02	.	.	04	.	07	09	07	04	02	07	.	.	.	.	.	.	01	04	.
XI	7.4	7.3	6.2	7.0	102.2	06.5	91	66	85	81	35	027	007.0	22	.	.	04	.	.	.	06	.	12	13	13	07	.	13	.	.	.	.	.	.	.	05	.
XII	8.4	8.4	6.5	7.8	049.3	04.4	91	82	92	88	51	032	009.0	24	04	06	23	.	.	.	03	01	01	17	11	07	.	06	06	.	.	.	01	.	.	09	09
GOD.	6.5	6.9	5.2	6.2	1904.2	08.1	88	62	84	78	30	658	-			12	23	97	75	20	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

H_e = 89 m H_b = - m h_t = 2.0 m h_r = 1.0 m

VIŠ BR. ST. 155																																				
I	9.3	7.5	8.3	8.4	-	04.2	92	86	90	89	60	-	-	-	03	09	26	.	.	.	02	.	.	21	-	-	-	-	-	-	-	-	-	-	-	-
II	8.1	7.7	7.2	7.7	-	04.3	92	78	90	87	42	096	017.7	12	01	06	23	.	.	.	.	.	01	14	19	16	02	09	12	.	.	.	.	.	.	-	-
III	7.6	5.7	6.1	6.5	-	-	-	-	-	-	-	078	017.0	15	.	01	10	.	.	.	03	.	01	14	15	13	03	13	03	.	.	.	.	.	.	-	-
IV	6.1	6.6	4.3	5.7	-	07.9	90	63	83	79	19	057	020.0	15	.	.	02	05	.	.	02	.	02	08	12	07	02	12	.	.	.	.	.	.	.	.	.
V	6.4	7.4	6.5	6.8	-	-	-	-	-	-	-	066	023.0	23	.	.	.	04	.	.	-	-	.	11	14	11	01	14	.	.	.	.	.	.	-	.	.
VI	4.0	4.3	7.3	5.2	-	13.6	83	59	83	75	44	062	014.7	19	.	.	.	21	05	.	02	.	03	05	15	11	02	15	.	.	.	.	.	.	-	.	.
VII	3.4	4.3	3.9	3.9	-	14.6	88	64	86	79	42	075	018.0	17	.	.	.	21	12	.	-	-	10	07	10	10	03	10	.	.	.	.	.	.	-	.	.
VIII	-	-	-	-	-	-	-	-	-	-	-	051	012.7	25	.	.	.	22	08	.	02	01	-	-	10	09	02	10	.	.	.	.	.	.	.	.	.
IX	5.2	2.9	6.0	4.7	-	12.0	93	68	85	82	28	042	020.5	17	.	.	02	09	01	.	.	.	05	06	06	06	02	06	.	.	.	.	.	.	.	.	.
X	4.9	5.0	4.5	4.8	-	-	-	-	-	-	-	052	020.6	02	.	.	01	02	.	.	.	.	09	09	07	06	02	07	.	.	.	.	.	.	.	01	.
XI	6.8	7.0	6.8	6.9	-	-	-	-	-	-	-	041	009.0	17	.	.	04	.	.	.	.	.	01	13	12	10	.	12	.	.	.	.	.	.	.	-	.
XII	7.8	7.5	8.6	8.0	-	04.7	93	83	90	88	67	038	008.8	23	01	06	22	.	.	.	.	.	.	20	13	09	.	10	03	.	.	.	.	.	.	07	07
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		05	22	90	84	26	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

H_e = 105 m H_b = - m h_t = 2.0 m h_r = 1.2 m

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C 7	14	21	Sred. (Dlas)	Max	Min	Max	Dat.	Min	Dat.	Cestina pravca i srednja jačina vetra m/s, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		j.	č.	j.	č.
BAČKI PETROVAC φ = 45° 22' N λ = 19° 34' E Gr. Δ G = + 1h 17 min.																												BR. ST. 156
I	-	-01.8	01.2	-01.5	-00.9	02.4	-04.9	10.3	15	-13.4	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-00.2	04.2	00.5	01.2	05.0	-02.9	16.5	09	-12.5	03	06	01.5	07	01.3	04	01.2	10	01.3	09	01.3	14	01.6	05	01.2	14	01.6	15
III	-	03.4	09.6	05.3	05.9	10.5	01.5	22.3	25	-08.5	02	06	01.2	06	01.2	09	01.9	20	02.0	08	01.8	12	01.8	06	01.0	17	01.6	09
IV	-	08.9	15.8	10.3	11.3	17.3	05.7	27.4	20	-01.3	04	08	01.5	06	01.8	06	01.5	11	01.5	06	02.0	11	01.6	14	01.8	18	01.7	10
V	-	12.5	18.8	12.9	14.3	20.3	08.9	28.2	10	01.4	02	05	01.2	02	01.5	08	01.0	08	01.0	02	01.0	08	01.6	22	01.7	24	01.7	14
VI	-	16.4	25.9	18.3	20.2	26.6	13.9	31.5	23	08.5	03	02	02.0	07	01.3	04	01.5	06	01.2	05	01.4	02	01.0	11	01.6	18	01.6	33
VII	-	18.6	25.8	18.7	20.5	26.9	14.2	33.1	24,22	10.0	27	03	01.0	04	01.2	05	01.2	03	01.0	06	01.3	06	01.3	11	01.6	17	01.6	38
VIII	-	18.0	26.5	18.6	20.4	27.4	14.4	33.9	07	09.8	19	02	02.0	05	01.6	16	01.2	03	01.7	04	01.2	04	01.0	11	01.4	09	01.6	39
IX	-	12.8	22.5	13.6	15.6	23.4	09.9	33.2	11	-02.1	29	08	01.4	04	01.2	04	01.0	03	01.0	03	01.0	10	01.2	06	01.3	08	01.2	44
X	-	06.5	16.1	08.7	10.0	16.9	04.4	26.0	09	-01.9	16	03	01.0	05	01.2	08	01.1	10	01.4	05	01.4	06	01.5	12	01.6	16	01.4	28
XI	-	05.8	13.0	07.3	08.3	13.8	03.7	22.1	03	-01.0	14,07	08	01.2	04	01.2	06	01.0	13	01.2	16	01.6	11	01.6	06	01.2	10	01.5	16
XII	-	00.3	03.3	00.9	01.4	04.2	-02.4	15.2	01	-15.2	27	02	01.0	14	01.2	09	01.3	11	01.5	02	01.0	10	01.3	19	01.6	18	01.4	06
GOD.	-	08.6	15.2	09.5	10.7	16.2	05.5	33.9	7.VIII	-15.2	27.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BAČKA TOPOLA φ = 45° 49' N λ = 19° 39' E Gr. Δ G = + 1h 18 min.																												BR. ST 157
I	-	-02.7	00.2	-01.8	-01.5	01.0	-04.5	06.1	06	-16.1	20	01	03.0	11	01.7	01	01.0	37	01.0	.	.	13	01.3	.	.	22	02.1	08
II	-	-01.2	02.8	00.3	00.5	03.7	-02.6	14.2	09	-09.8	03,02	.	.	04	01.8	.	.	19	01.7	.	.	29	01.3	01	01.0	24	02.2	07
III	-	02.5	08.5	04.9	05.2	09.6	01.3	21.0	25	-08.8	02	.	.	09	01.8	.	.	27	02.4	01	03.0	33	01.5	.	.	20	01.9	03
IV	-	08.2	15.1	10.4	11.0	16.6	05.8	26.5	20	-01.5	05	.	.	05	02.2	01	02.0	20	01.9	01	01.0	27	01.5	05	01.4	27	02.4	04
V	-	12.2	18.5	13.3	14.3	19.7	08.8	27.4	10	00.8	03	.	.	04	02.8	.	.	16	01.4	.	.	21	01.6	01	04.0	41	07.0	16
VI	-	18.4	25.2	18.9	20.3	26.0	14.2	31.6	23	08.4	04	01	01.0	04	01.0	.	.	17	01.1	.	.	20	01.4	02	01.0	33	02.0	13
VII	-	18.8	25.7	19.2	20.7	26.9	14.3	33.2	24,23	10.2	27	01	01.0	05	01.0	.	.	12	01.2	01	01.0	20	01.4	02	02.0	33	01.5	19
VIII	-	18.0	25.9	18.9	20.4	26.7	14.9	33.7	07	09.6	28	.	.	08	01.2	.	.	26	01.2	.	.	14	01.1	01	01.0	19	01.5	25
IX	-	12.7	21.2	13.9	15.4	22.3	10.2	32.0	11	-01.4	30	01	03.0	06	01.7	.	.	09	01.4	01	01.0	19	01.2	04	01.2	24	01.4	26
X	-	6.0	15.4	08.9	09.8	16.1	04.6	25.0	09	-02.4	16	01	02.0	01	01.0	.	.	19	01.4	02	02.0	29	01.2	02	03.0	25	01.6	14
XI	-	05.0	12.2	07.3	08.0	12.8	03.7	21.5	03	-01.5	07	.	.	.	.	.	.	27	01.3	02	01.0	35	01.2	.	.	17	02.1	09
XII	-	-00.4	03.0	00.6	01.0	04.8	-02.2	-	-	-15.1	27	.	.	11	01.9	.	.	16	01.9	03	01.3	20	01.1	03	01.0	19	02.1	13
GOD.	-	08.1	14.5	09.6	10.4	15.5	05.7	-		-15.1	27.XII	05	02.0	68	01.7	02	01.5	245	01.6	11	01.4	200	01.3	21	01.6	304	01.9	151
VRBAS φ = 45° 34' N λ = 19° 39' E Gr. Δ G = + 1h 18 min.																												BR. ST. 158
I	-	-02.9	00.2	-02.4	-01.9	01.0	-05.3	05.9	16	-15.2	03	02	04.5	03	02.3	13	03.0	32	03.2	.	.	07	01.4	12	02.4	18	03.6	06
II	-	-01.3	03.1	00.1	00.5	04.0	-02.9	14.8	09	-15.6	03	07	02.7	05	02.6	07	03.1	18	02.4	03	01.7	17	02.0	05	02.2	21	03.5	01
III	-	02.1	08.8	04.4	04.9	09.8	01.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	08.3	15.2	09.8	10.7	16.7	05.0	27.1	20	-02.7	04	11	04.2	03	03.7	05	02.2	18	02.9	06	02.0	19	02.2	13	03.5	15	3.1	-
V	-	12.1	18.5	13.2	14.3	19.8	08.2	27.5	10	01.2	01	18	04.2	05	02.4	04	02.2	02	03.0	10	02.3	06	02.4	10	03.6	26	03.1	10
VI	-	18.2	25.1	18.8	20.2	26.0	14.2	31.5	23	08.3	06	14	03.4	06	02.5	07	02.3	08	02.4	04	01.8	06	02.0	15	02.7	10	03.2	20
VII	-	18.4	25.3	18.6	20.2	26.3	14.1	32.7	24	08.8	27	15	02.6	03	02.0	03	02.0	08	01.9	07	01.7	04	01.8	15	02.5	12	03.2	26
VIII	-	17.7	25.9	18.2	20.0	26.6	14.0	33.2	07	08.8	27	09	02.2	05	02.2	09	01.9	08	02.2	09	01.8	.	.	12	02.2	10	02.6	31
IX	-	12.4	21.7	13.5	15.3	22.8	09.4	32.5	11	-02.5	30	21	02.2	02	02.5	05	02.0	02	01.0	07	01.9	01	02.8	07	01.4	07	02.4	38
X	-	05.6	15.7	08.3	09.4	16.5	03.9	25.6	07	-02.5	19,16	02	02.5	03	01.7	07	02.1	09	02.4	07	02.0	04	03.0	16	02.2	19	02.9	26
XI	-	04.4	12.6	06.4	07.4	13.4	02.7	22.3	03	-02.8	07	05	01.8	.	.	04	02.2	15	01.9	08	02.1	06	02.2	10	02.0	11	02.9	31
XII	-	-00.7	02.8	00.0	00.5	03.9	-02.7	14.0	01	-16.0	27	06	02.7	06	02.7	09	02.6	05	02.8	07	02.3	06	01.2	15	02.3	14	02.1	25
GOD.	-	07.9	14.6	09.1	10.1	15.6	05.1	-				-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
NOVI SAD-RIMSKI ŠANČEVI φ = 45° 20' N λ = 19° 51' E Gr. Δ G = + 1h 18 min.																												BR. ST. 159
I	752.9	-02.0	00.5	-01.2	-01.0	02.0	-04.2	10.8	15	-17.5	22	02	03.0	02	02.0	08	01.8	40	03.1	02	01.5	01	02.0	13	02.5	19	02.7	06
II	749.7	-00.6	03.7	00.5	01.0	04.7	-02.6	14.0	09	-14.2	03	04	01.8	04	02.8	01	02.0	21	02.6	02	01.5	09	02.9	17	02.2	19	02.9	07
III	751.0	02.8	09.0	05.2	05.6	10.1	01.9	21.5	25	-07.1	02	12	02.5	.	.	06	01.7	30	03.5	04	02.5	07	02.6	20	02.6	13	02.9	01
IV	751.8	08.4	15.1	10.4	11.1	17.1	06.1	27.0	26	-00.7	05	11	03.5	02	02.0	05	02.4	21	02.9	04	02.5	03	02.7	22	02.5	16	02.9	06
V	752.4	12.0	18.2	13.7	14.4	19.6	09.7	27.0	10	02.5	02	09	03.3	.	.	04	01.8	13	02.2	05	01.8	05	01.2	17	02.5	33	02.8	07
VI	753.5	18.1	24.6	19.2	20.3	25.6	14.6	31.0	23	09.6	03	12	02.3	01	02.0	04	02.2	18	01.8	02	01.0	02	01.0	23	02.1	12	02.8	16
VII	752.5	18.2	24.8	19.5	20.5	26.3	15.0	32.6	24	11.4	18	09	01.8	.	.	01	02.0	17	01.6	01	02.0	04	01.8	20	01.8	24	02.2	16
VIII	752.9	17.6	25.8	19.3	20.5	26.7	15.1	32.6	07	10.2	19	05	01.4	01	02.0	08	01.5	25	01.7	03	01.0	02	01.5	12	01.8	16	02.2	21
IX	756.4	12.3	21.9	14.6	15.8	23.1	10.8	33.5	11	-01.6	30	09	01.9	.	.	03	01.3	18	01.7	02	01.5	02	02.5	30	01.7	16	02.0	18
X	756.6	06.3	15.6	09.4	10.2	16.6	05.3	25.6	09	-01.8	16	05	02.4	02	01.5	23	02.3	03	02.0	02	01.5	24	02.2	18	02.2	14	02.2	14
XI	754.8	05.4	12.6	07.4	08.2	13.5	04.1	22.0	03	-01.0	14,07	02	02.0	03	02.3	05	01.4	28	02.1	04	01.5	09	02.1	18	02.2	11	02.7	10
XII	758.0	00.2	03.0	00.7	01.2	04.2	-01.9	14.5	01	-15.2	27	02	01.5	06	02.2	05	02.0	17	02.8	01	02.0	04	02.0	34	02.1	12	02.1	12
GOD.	753.5	08.2	14.6	09.9	10.6	15.8	06.2	33.5	4.IX	-15.2	27.XII	02	02.4	21	02.2	52	01.8	271	02.5	23	01.8	51	02.1	250	02.2	209	02.5	126
NOVI SAD-PETROVARADIN φ = 45° 15' N λ = 19° 52' E Gr. Δ G = + 1h 18 min.																												BR. ST. 160
I	749.5	-00.4	01.6	00.3	00.5	03.2	-02.5	13.0	15	-09.0	10	03	02.7	04	01.2	26	02.7	10	03.3	03	02.0	14	02.0	24	02.2	07	02.7	02
II	746.2	00.6	04.0	02.0	02.2	05.4	-00.9	16.5	05	-07.3	17	02	01.5	04	02.0	09	02.2	12	02.1	02	02.0	21	02.7	17	02.7	15	01.9	02
III	747.5	03.9	08.7	05.9	06.1	09.9	03.0	21.4	25	-05.1	02	05	01.6	04	01.8	17	02.9	08	03.9	07	03.1	24	02.5	12	02.7	14	02.4	02
IV	748.3	09.7	14.6	11.5	11.8	16.6	07.8	26.5	20	01.6	04	06	02.3	07	01.8	07	02.4	10	03.1	07	02.9	24	02.3	11	03.0	15	02.6	03
V	749.2	12.3	18.0	14.5	14.8	19.3	10.4	26.4	10	03.3	03	03	03.3	02	01.0	08	01.9	03	01.3	07	02.4	23	02.3	27	02.6	15	02.1	05
VI	750.2	18.4	24.1	19.9	20.6	25.2	16.1	30.3	17	09.2	03	04	02.0	04	01.5	14	01.6	07	01.9	04	01.5	29	02.4	11	02.6	08	02.1	09
VII	749.3	18.7	24.2	20.5	21.0	25.4	16.3	31.9	23	11.0	18	02	01.5	.	.	12	01.6	18	01.9	09	01.6	26	02.1	17	02.6	12	02.2	05
VIII	749.4	18.5	25.4	20.4	21.2	26.2	16.9	32.5	07	12.8	27	05	01.2	06	01.3	21	02.1	08	02.0	08	01.5	22	01.9	19	02.3	06	02.5	02
IX	753.3	14.1	21.5	16.6	17.2	22.6	12.9	33.1	11	01.7	29	09	01.3	.	.	10	02.2	04	02.8	09	01.7	32	01.7	15	01.7	08	02.9	03
X	753.4	08.7	14.9	11.5	11.7	16.0	07.3	24.5	07	00.4	16	06	01.3	03	02.3	15	02.1	09	02.0	06	01.7	27	02.2	16	02.7	07	01.3	04
XI	751.6	08.3	12.5	09.6	10.0	13.3	06.6	21.5	03	-00.8	26	03	01.3	03	01.0	09	02.0	07	02.4	09	02.6	30	02.1	09	02.2	13	02.1	07
XII	754.5	01.4	03.3	02.0	02.2	04.6	-00.4	16.2	30	-1[illegible].2	25	04	01.0	08	02.0	12	02.6	06	02.2	05	02.6	27	02.2	21	02.3	05	02.4	05
GOD.	750.2	09.5	14.4	11.2	11.6	15.6	07.8	33.1	4.IX	-1[illegible].2	25.XII	52	01.7	45	01.6	160	02.2	94	02.5	76	02.1	299	02.2	195	02.5	125	02.2	49

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	U m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤ -10.0	Tx ≤ 0.0	Tn < 0.0	Tx ≥ 25.0	Tx ≥ 30.0	Tn ≥ 20.0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	*	●	△	∿	▲	▲	⊤	≡	▦
BR. ST. 156 — BAČKI PETROVAC — H_s = 85 m H_b = - m h_t = 2.0 m h_r = 1.5 m																																						
I	7.5	7.4	6.1	7.0	043.4	03.9	88	83	88	86	61	045	-	-	05	10	29	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	7.3	7.3	6.8	7.1	057.6	04.4	88	77	88	84	54	090	017.4	12	01	05	24		.	.	.	.	02	11	19	15	01	11	11	.	.	.	.	.	.	12	20
III	7.0	7.3	6.7	7.0	121.1	05.6	85	68	83	79	41	057	013.4	15	.	01	10	.	.	.	01	.	03	15	17	08	02	14	07	03	.	.	.	.	.	11	02
IV	5.7	6.6	4.0	5.4	168.0	07.9	85	62	81	76	26	066	026.4	09	.	.	02	04	.	.	.	.	02	06	12	07	02	12	.	.	.	.	.	.	03	01	.
V	6.1	7.6	5.0	6.2	153.4	09.2	83	58	82	74	33	055	019.2	23	.	.	.	04	.	.	.	.	02	08	14	08	02	14	.	.	.	.	.	.	05	02	.
VI	4.2	5.0	4.0	4.4	261.2	13.9	84	58	86	76	45	058	011.8	19	.	.	.	22	27	.	.	.	07	03	17	10	02	17	.	.	.	.	.	.	10	01	.
VII	3.9	4.9	3.5	4.1	-	14.3	84	61	87	77	44	063	013.6	06	.	.	.	22	12	.	01	.	10	05	10	10	02	10	.	.	.	.	.	.	05	03	.
VIII	3.8	4.0	3.3	3.7	265.9	14.4	88	59	89	79	41	078	031.4	25	.	.	.	21	11	.	.	.	08	02	09	07	02	09	.	.	.	.	.	.	09	04	.
IX	4.5	4.8	3.2	4.1	194.7	11.4	93	60	90	81	42	021	008.6	17	.	.	02	12	05	.	.	.	07	04	07	04	.	07	.	.	.	.	.	.	02	06	.
X	4.3	5.0	4.0	4.4	157.5	07.6	92	60	89	80	39	057	023.4	02	.	.	03	05	.	.	.	.	10	07	07	06	03	07	.	.	.	.	.	.	.	04	.
XI	6.7	6.3	5.3	6.1	100.5	07.0	90	71	88	83	42	031	011.0	17	.	.	02	.	.	.	.	.	02	10	13	06	01	13	.	.	.	.	.	.	.	05	.
XII	7.4	7.8	6.9	7.4	043.4	04.6	91	84	90	88	64	041	009.7	24	03	05	23	.	.	.	01	.	01	16	18	10	.	12	06	.	.	.	.	.	.	14	07
GOD.	5.7	6.2	4.9	5.6	-	08.7	87	66	86	80	26	662	-		09	21	95	90	55	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 157 — BAČKA TOPOLA — H_s = 100 m H_b = - m h_t = 2.0 m h_r = 1.0 m																																						
I	8.6	7.8	6.3	7.6	-	03.8	91	86	89	89	57	066	018.0	08	04	11	27	.	.	.	01	01	02	18	17	08	04	10	09	01	.	.	01	.	.	12	31
II	8.6	7.6	7.4	7.9	-	04.4	90	87	90	89	67	070	015.0	14	.	07	24	.	.	.	01	01	.	15	21	13	02	12	13	02	.	.	.	.	.	04	07
III	7.7	7.3	6.3	7.1	-	05.3	85	67	85	79	35	056	011.8	15	.	01	10	.	.	.	03	01	.	13	14	11	01	11	04	.	.	.	.	.	.	01	02
IV	5.3	6.7	4.2	5.4	-	07.2	83	57	74	72	30	049	013.0	09	.	.	02	02	.	.	01	.	02	03	13	10	01	13	.	.	.	.	.	.	02	.	.
V	5.6	7.8	6.2	6.5	-	09.0	82	58	79	73	38	056	014.6	18	.	.	.	02	.	.	.	.	01	09	15	11	02	15	.	.	.	.	.	.	04	02	.
VI	4.5	5.1	5.1	4.9	-	13.4	81	56	82	73	36	067	018.5	11	.	.	.	02	.	.	02	01	04	06	18	11	02	18	.	.	.	.	.	.	06	01	.
VII	4.0	4.9	4.1	4.3	-	13.7	80	57	83	73	40	046	013.4	17	.	.	.	21	13	.	01	01	09	06	10	08	02	10	.	.	.	.	.	01	01	.	.
VIII	4.2	4.9	3.8	4.3	-	14.1	87	57	88	77	41	134	046.7	25	.	.	20	07	.	.	.	.	07	03	11	10	05	11	.	.	.	.	.	.	06	01	.
IX	5.9	5.3	3.0	4.7	-	10.8	90	59	88	79	34	041	020.5	17	.	.	01	09	03	.	.	.	06	04	09	04	01	09	.	.	.	.	.	.	01	02	.
X	5.0	5.1	3.8	4.7	-	07.2	91	58	84	78	37	036	014.5	02	.	.	04	01	.	.	.	.	10	07	09	05	01	09	.	.	.	.	.	.	.	04	.
XI	7.1	6.6	4.8	6.2	-	06.4	88	66	82	79	38	022	005.7	17	.	.	02	.	.	.	.	.	05	11	09	05	.	09	.	.	.	.	.	.	.	04	.
XII	8.4	7.6	6.9	7.6	-	04.5	92	81	90	87	56	041	009.0	24	03	-	23	-	-	.	01	01	01	16	15	11	.	11	05	01	.	.	.	.	01	08	08
GOD.	6.2	6.4	5.2	5.9	-	08.3	86	65	84	79	30	684	046.7	25 VIII	07	-	113	-	-	.	10	06	47	111	161	107	21	138	31	04	.	.	01	01	21	39	48
BR. ST. 158 — VRBAS — H_s = 87 m H_b = - m h_t = 2.0 m h_r = 1.0 m																																						
I	8.9	8.1	6.7	7.9	046.2	03.8	93	85	92	90	72	044	012.7	08	07	10	27	.	.	.	10	01	02	18	13	07	01	09	07	01	.	.	.	.	.	06	27
II	8.8	8.1	7.1	8.0	065.3	04.4	94	81	92	89	53	070	012.3	12	02	06	22	.	.	.	10	.	01	18	22	11	02	11	15	.	.	.	.	.	.	04	12
III	8.0	8.4	6.7	7.7	115.8	05.5	92	68	90	83	-	047	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	6.6	7.8	5.4	6.6	164.2	07.4	87	59	86	75	36	062	022.4	09	.	.	02	03	.	.	12	01	01	09	10	08	03	10	.	.	.	.	.	.	03	.	.
V	6.1	7.9	5.7	6.6	161.6	09.4	86	60	82	76	36	058	022.7	23	.	.	.	03	.	.	07	.	01	08	13	09	01	13	.	.	.	.	.	.	05	01	.
VI	4.6	5.3	4.6	4.8	277.0	13.6	85	56	85	76	30	086	018.7	11	.	.	.	21	04	.	06	02	05	04	16	11	02	16	.	.	.	.	.	.	11	.	.
VII	3.7	4.7	3.4	3.9	287.2	14.0	85	60	86	77	43	058	018.2	06	.	.	.	22	09	.	02	02	14	07	09	08	02	09	.	.	.	.	.	.	02	.	.
VIII	3.5	4.6	3.5	3.9	272.8	14.3	90	60	90	80	44	104	048.1	25	.	.	.	18	05	.	01	01	10	01	10	09	04	10	.	.	.	.	.	.	06	.	.
IX	5.0	4.9	2.4	4.1	209.3	11.1	94	60	90	81	42	025	008.6	17	.	.	02	09	04	.	.	.	07	05	09	04	.	09	.	.	.	.	.	.	04	.	.
X	5.1	5.5	3.5	4.7	163.4	07.4	95	61	90	82	41	052	022.5	02	.	.	05	03	.	.	.	.	11	09	08	05	01	08	.	.	.	.	.	.	.	04	.
XI	7.0	7.0	5.5	6.5	102.1	06.7	94	69	91	85	37	033	009.7	17	.	.	08	.	.	.	02	.	02	12	12	08	.	12	.	.	.	.	.	.	.	03	.
XII	8.0	7.8	7.3	7.7	043.7	04.6	95	87	94	92	61	036	008.5	24	04	05	23	.	.	.	04	02	02	17	12	09	.	07	05	.	.	.	.	.		07	07
GOD.	6.3	6.7	5.2	6.0	1929.6	08.5	90	67	88	82	-	675	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 159 — NOVI SAD-RIMSKI ŠANČEVI — H_s = 84 m H_b = - m h_t = 2.0 m h_r = 1.0 m																																						
I	8.8	8.3	7.5	8.2	044.5	03.9	91	85	91	89	70	037	012.9	08	05	12	26	.	.	.	01	.	.	18	13	08	02	08	08	03	.	.	.	.	.	06	26
II	8.0	8.4	7.1	7.8	067.2	04.4	90	78	90	86	45	085	015.7	12	02	05	22	.	.	.	01	01	.	15	21	13	02	13	14	.	.	.	.	.	.	04	15
III	7.9	7.9	5.5	7.1	116.9	05.3	86	64	83	78	28	053	013.4	15	.	01	07	.	.	.	06	01	02	13	15	10	02	12	05	.	01	.	.	.	.	.	02
IV	6.4	7.5	4.9	6.3	163.6	07.2	86	55	76	72	24	050	020.0	09	.	.	02	03	.	.	04	.	02	09	11	06	02	11	.	.	.	.	.	.	02	.	.
V	6.1	8.2	6.6	7.0	163.2	08.8	84	55	77	72	30	070	029.1	23	.	.	.	04	.	.	06	.	01	14	17	14	01	15	.	.	.	.	.	.	03	01	.
VI	4.2	5.4	5.0	4.9	263.3	13.5	85	56	84	75	38	107	022.8	20	.	.	.	20	04	.	.	.	05	04	18	12	04	18	.	.	.	.	.	01	08	.	.
VII	3.8	4.8	4.2	4.3	276.0	13.7	86	57	84	76	42	091	021.7	06	.	.	.	22	09	.	01	.	11	06	11	09	04	11	.	.	.	.	.	.	03	.	.
VIII	4.0	4.9	3.4	4.1	259.8	14.0	91	55	87	78	39	053	015.7	25	.	.	.	19	07	.	03	.	08	03	08	06	03	08	.	.	.	.	.	.	05	.	.
IX	4.9	5.5	2.0	4.2	203.7	10.5	94	50	86	77	28	021	008.6	17	.	.	02	11	05	.	.	.	07	03	08	05	.	08	.	.	.	.	.	.	03	.	.
X	5.4	5.2	4.3	5.0	171.7	07.4	94	57	85	79	32	061	026.2	02	.	.	02	04	.	.	.	.	10	08	09	07	02	09	.	.	.	.	.	01	.	02	.
XI	7.7	6.9	6.4	7.0	100.3	06.5	90	64	87	80	30	036	017.1	17	.	.	04	.	.	.	.	.	04	14	12	08	01	12	.	.	.	.	.	01	01	02	.
XII	8.0	7.9	7.0	7.6	046.7	04.6	92	84	92	90	53	033	007.3	29	04	05	21	.	.	.	02	.	01	16	12	10	.	08	04	.	.	.	.	.	.	07	06
GOD.	6.3	6.7	5.3	6.1	1876.9	08.3	89	63	85	79	24	697	029.1	25 V	11	23	86	83	25	.	24	02	51	123	155	108	23	133	31	03	01	.	.	03	25	22	49
BR. ST. 160 — NOVI SAD-PETROVARADIN — H_s = 132 m H_b = 129.4 m h_t = 2.0 m h_r = 1.2 m																																						
I	8.5	8.3	7.3	8.0	047.9	04.0	83	78	83	81	55	050	020.1	08	.	10	22	.	.	.	23	09	.	17	14	08	02	09	08	.	01	.	.	.	.	05	19
II	8.1	7.8	6.6	7.5	072.2	04.2	82	73	80	79	45	097	016.6	12	.	06	20	.	.	.	02	01	.	13	18	13	02	09	14	01	.	.	.	.	.	02	16
III	7.6	7.9	5.4	7.0	122.9	05.0	77	60	74	70	30	052	013.8	15	.	01	05	.	.	.	20	07	02	15	15	13	02	12	05	01	.	.	.	.	.	.	03
IV	6.2	6.7	4.8	5.9	168.0	07.0	75	58	68	67	29	053	016.6	15	.	.	.	03	.	.	20	07	03	07	10	08	02	10	.	.	.	.	.	.	03	01	.
V	6.2	7.7	6.3	6.7	173.0	09.3	83	63	76	74	37	086	045.2	23	.	.	.	08	.	.	15	05	03	12	19	11	01	19	.	.	.	.	.	.	01	01	.
VI	4.2	4.9	4.2	4.4	270.9	13.6	81	62	78	74	49	101	024.1	20	.	.	.	19	01	01	16	04	07	04	14	11	05	14	.	.	.	.	.	.	07	.	.
VII	4.1	4.7	3.6	4.2	276.1	13.1	80	61	73	71	38	081	020.8	06	.	.	.	20	06	02	11	02	12	06	11	08	03	11	.	.	.	.	.	.	03	.	.
VIII	3.8	4.4	2.4	3.5	273.7	13.5	83	57	75	72	42	044	011.8	25	.	.	.	20	04	04	13	04	09	03	11	07	01	11	.	.	.	.	.	.	07	.	.
IX	4.7	5.1	1.8	3.9	212.7	10.1	81	52	70	68	26	021	008.4	01	.	.	.	08	04	.	09	01	08	04	07	04	.	07	.	.	.	.	.	.	01	01	.
X	4.9	4.9	4.8	4.9	172.7	07.1	79	58	70	69	36	056	026.1	02	.	.	.	.	.	.	15	02	09	09	08	08	02	08	.	.	.	.	.	.	.	01	.
XI	7.1	5.8	5.8	6.2	112.1	06.1	73	61	70	68	32	032	014.8	17	.	.	01	.	.	.	12	02	04	11	11	06	01	11	.	.	.	.	.	.	01	01	.
XII	7.9	7.2	6.5	7.2	094.2	04.5	83	78	84	82	47	027	008.0	24	01	04	17	.	.	.	14	04	.	16	12	05	.	08	04	.	.	.	.	.	.	05	05
GOD.	6.1	6.3	5.0	5.8	1956.4	08.1	80	63	75	72	26	700	045.2	23 V	01	21	65	73	15	07	170	48	57	117	150	102	21	129	31	02	01	.	.	.	23	17	43

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C
GLADNOŠ — φ = 45° 08' N λ = 20° 00' E Gr. Δ G = + 1h 20 min. — BR. ST. 161																												
I	-	-02.0	00.8	-01.2	-00.9	01.8	-04.0	09.9	15	-09.8	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	-01.1	02.8	00.4	00.6	03.9	-02.9	14.8	05	-09.5	18	03	01.7	01	02.0	02	02.0	03	01.7	06	01.8	15	02.1	•	•	28	02.8	26
III	-	02.3	08.6	04.6	05.0	09.8	01.0	22.1	25	-07.7	02	03	02.0	05	03.0	03	02.7	13	02.8	08	02.4	08	01.8	04	03.0	27	02.7	22
IV	-	09.2	14.8	09.8	10.9	16.5	06.3	26.5	20	-02.0	04	02	02.0	03	02.3	•	•	11	02.5	05	02.2	09	02.1	03	02.7	36	03.1	21
V	-	12.2	17.7	12.7	13.8	18.9	09.4	27.5	10	02.0	02	02	02.0	03	01.7	•	•	09	01.8	04	02.0	12	02.1	02	02.0	38	03.1	23
VI	-	18.1	23.4	18.0	19.4	24.7	14.8	30.4	23	08.0	03	04	02.0	08	02.1	04	02.0	06	01.8	•	•	10	01.8	01	02.0	32	02.6	25
VII	-	18.6	23.7	18.4	19.8	25.3	15.3	31.7	22	10.2	18	03	02.0	07	01.7	04	02.0	03	02.0	02	02.0	04	02.0	06	01.8	41	02.7	23
VIII	-	18.0	25.0	18.7	20.1	26.2	15.6	33.0	06	11.5	28	08	01.6	13	01.7	04	01.8	07	01.6	03	01.7	03	01.7	03	02.3	25	02.4	27
IX	-	13.3	20.9	14.5	15.8	22.2	11.6	33.2	12	01.0	29	01	02.0	02	01.5	•	•	08	01.8	02	02.0	09	01.9	03	02.0	41	02.2	24
X	-	07.0	14.7	09.1	09.9	15.3	05.8	24.1	09	-01.0	16	04	01.8	02	02.0	04	02.2	15	01.7	•	•	08	01.8	01	02.0	29	02.6	30
XI	-	05.6	11.8	07.0	07.8	12.5	04.0	20.6	03	-01.6	26	03	01.7	02	02.0	•	•	10	01.7	07	01.7	07	01.9	06	01.8	16	02.8	29
XII	-	00.3	03.1	00.7	01.2	03.9	-01.5	13.0	01	-09.5	27	02	02.5	09	01.7	•	•	06	02.3	02	02.0	04	01.8	•	•	28	02.6	42
GOD.	-	08.5	13.9	09.4	10.3	15.1	06.3	33.2	18.IX	-09.8	22.I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
BEČEJ — φ = 45° 37' N λ = 20° 04' E Gr. Δ G = + 1h 20 min. — BR. ST. 162																												
I	-	-02.2	01.0	-01.4	-01.0	02.1	-04.6	10.7	15	-15.9	03	04	01.8	04	01.5	09	02.1	22	02.1	14	02.4	06	01.5	18	02.6	11	02.4	05
II	-	-00.6	03.7	00.8	01.2	04.5	-02.1	16.7	09	-09.6	18	07	02.4	05	01.8	01	01.0	19	02.7	14	02.3	07	02.4	11	02.9	17	02.6	03
III	-	02.4	09.2	05.1	05.5	10.0	01.1	22.3	25	-10.1	02	09	02.6	04	02.0	05	03.4	19	03.1	16	02.6	13	02.6	14	02.9	11	03.3	02
IV	-	08.7	15.5	10.3	11.2	16.8	05.2	26.7	26	-02.4	04	07	04.1	01	01.0	06	02.2	19	02.9	18	02.1	11	02.4	17	02.6	11	03.7	•
V	-	12.5	19.1	13.5	14.6	20.2	08.5	27.7	10	01.0	02	09	03.4	03	02.0	02	02.5	15	02.0	13	01.7	12	02.7	18	02.9	21	02.9	•
VI	-	18.3	25.2	19.1	20.4	26.0	14.2	32.1	23	08.4	04	11	02.3	05	01.6	07	02.4	11	02.0	06	02.3	07	02.4	16	02.6	22	02.5	05
VII	-	18.5	25.0	19.4	20.6	26.3	14.6	32.3	15	09.4	27	08	01.8	06	01.3	08	01.6	12	01.8	07	02.0	12	02.0	10	02.3	24	01.9	06
VIII	-	17.7	25.7	18.9	20.3	26.4	14.7	32.9	07	08.3	27	05	01.8	10	01.1	13	01.9	15	01.8	05	01.6	06	01.8	16	01.6	12	01.9	11
IX	-	12.5	21.5	14.2	15.6	22.4	10.2	32.7	11	-01.9	30	11	01.6	05	01.6	02	02.0	11	01.8	12	01.8	12	01.6	13	01.6	15	01.8	09
X	-	06.0	15.4	08.9	09.8	16.1	04.6	24.8	09,08	-02.2	19	08	01.2	01	01.0	05	02.2	20	01.9	12	01.7	07	01.9	17	02.1	16	02.1	07
XI	-	05.0	12.4	07.2	08.0	13.1	03.8	21.8	03	-02.1	07	03	02.0	03	01.3	03	01.3	21	02.0	17	02.1	15	02.0	10	02.0	11	02.5	07
XII	-	-00.4	03.0	00.5	00.9	03.9	-02.4	12.1	30	-16.2	27	09	02.1	04	02.2	07	02.0	14	02.3	08	02.0	16	01.6	22	01.9	05	01.6	08
GOD.	-	08.2	14.7	09.7	10.6	15.6	05.6	32.9	7.VIII	-16.2	27.XII	91	02.3	51	01.5	68	02.1	198	02.2	142	02.1	124	02.1	182	02.3	176	02.4	63
SENTA — φ = 45° 56' N λ = 20° 05' E Gr. Δ G = + 1h 20 min. — BR. ST. 163																												
I	-	-02.0	00.7	-01.0	-00.8	01.6	-03.2	09.0	15	-13.1	03	04	01.8	10	01.9	05	02.2	26	03.1	05	02.2	14	02.1	16	02.4	11	02.2	02
II	-	-00.3	03.3	00.5	01.0	04.2	-01.6	14.0	09	-09.7	03	07	02.1	01	02.0	02	02.0	10	01.9	19	02.4	11	02.1	12	02.1	18	02.3	04
III	-	02.8	08.7	05.4	05.6	09.6	02.0	20.2	25	-08.3	02	03	02.0	10	02.2	02	02.0	13	03.4	16	02.4	17	01.9	13	01.7	17	02.6	02
IV	-	08.7	15.4	10.7	11.4	16.8	06.5	27.0	24	-00.7	04	05	01.8	07	01.9	•	•	21	02.5	12	02.2	12	01.8	09	03.0	22	02.8	02
V	-	12.8	19.2	13.6	14.8	20.1	09.6	26.5	10	02.0	01	09	01.6	01	01.0	02	01.5	06	01.7	10	01.4	20	01.8	12	02.0	27	02.4	06
VI	-	18.8	25.3	19.0	20.5	26.0	14.9	32.6	23	09.1	04	05	01.4	12	02.1	03	02.0	06	01.8	07	02.0	12	01.7	14	02.0	22	01.9	09
VII	-	19.4	26.3	19.6	21.2	27.2	15.2	33.3	24	10.8	27	03	01.7	03	01.7	03	01.3	09	01.3	08	01.8	18	01.8	10	01.9	31	02.3	08
VIII	-	18.9	26.2	19.0	20.8	27.2	15.3	33.4	07	09.6	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	13.1	22.0	14.7	16.1	22.9	10.8	33.5	12	-00.8	30	03	01.0	03	01.3	01	01.0	02	01.5	10	01.3	10	01.3	20	01.4	23	01.6	18
X	-	06.5	15.6	09.6	10.3	16.3	05.0	26.0	08	-02.8	16	02	01.5	04	01.5	02	02.0	12	01.1	10	01.4	22	01.4	16	02.4	17	01.8	08
XI	-	05.4	12.3	07.5	08.1	12.9	04.2	20.4	03	-00.8	07	03	02.0	02	01.0	06	02.3	17	01.8	14	01.6	18	01.6	08	02.0	17	01.9	05
XII	-	00.2	03.3	00.9	01.3	04.1	-01.7	11.7	30	-13.9	27	07	01.4	04	01.8	02	02.5	16	01.9	09	01.8	18	01.8	15	01.7	14	02.0	08
GOD.	-	08.7	14.9	10.0	10.9	15.7	06.4	33.5	12.IX	-13.9	27.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ZRENJANIN — φ = 45° 22' N λ = 20° 25' E Gr. Δ G = + 1h 22 min. — BR. ST. 164																												
I	-	-01.6	01.0	-00.8	-00.5	02.0	-03.5	12.0	15	-13.2	20	04	01.5	06	01.7	07	02.1	33	03.6	08	02.8	04	02.0	23	02.7	08	02.6	
II	-	-00.4	02.8	00.9	01.1	03.9	-01.6	14.5	09	-10.5	03	10	02.1	04	02.0	03	03.7	25	03.0	13	02.8	07	02.9	09	02.8	13	02.6	
III	-	03.1	08.7	05.7	05.8	09.5	02.0	20.3	25	-07.6	02	09	02.4	05	03.0	06	03.2	25	03.7	13	02.8	12	02.4	10	03.2	12	03.7	01
IV	-	08.9	14.7	11.3	11.5	16.3	06.8	25.4	26	-00.[illegible]	04	07	03.6	07	02.4	04	02.0	22	03.2	11	02.8	07	03.1	18	02.8	14	03.6	-
V	-	12.3	18.0	13.7	14.4	19.2	09.9	26.7	10	02.7	02	12	03.7	05	02.6	01	02.0	14	02.3	08	02.5	15	02.3	17	03.1	21	03.2	-
VI	-	18.3	24.2	19.4	20.3	25.1	15.2	30.7	23	09.6	03,02	10	02.5	04	02.5	09	02.1	15	01.9	08	02.1	09	02.2	18	02.6	15	02.9	02
VII	-	18.5	24.6	19.5	20.5	26.0	15.5	32.1	24	10.8	27	11	02.3	07	01.9	03	01.7	13	02.2	13	02.2	06	02.3	17	03.0	21	02.6	02
VIII	-	18.1	25.5	19.0	20.4	26.5	15.1	32.0	07	09.0	27	05	02.2	06	02.0	10	01.8	25	02.0	06	02.2	04	01.8	18	02.2	14	02.7	05
IX	-	12.7	21.6	14.2	15.7	22.7	10.0	33.5	12	-03.0	29	12	02.4	03	01.7	04	01.5	19	02.2	08	02.4	06	01.5	16	01.8	19	02.2	03
X	-	06.6	15.2	09.1	10.0	16.9	05.4	24.7	08	-02.3	16	08	02.1	01	01.0	03	01.7	29	02.5	10	02.1	08	01.9	17	02.4	16	02.4	01
XI	-	05.4	12.1	07.2	08.0	12.6	03.8	21.0	03	-03.7	07	04	02.5	01	02.0	05	02.4	31	02.5	15	02.7	06	01.5	14	02.6	12	02.8	02
XII	-	-00.1	03.1	00.7	01.1	04.0	-02.1	11.8	30	-13.7	24	03	02.0	05	01.8	07	02.1	21	02.8	05	01.8	09	02.0	30	02.1	13	02.4	-
GOD.	-	08.5	14.3	10.0	10.7	15.3	06.4	33.5	12.IX	-13.7	24.XII	95	02.5	54	02.1	62	02.2	272	02.7	118	02.5	93	02.2	207	02.6	178	02.8	16
KIKINDA — φ = 45° 51' N λ = 20° 28' E Gr. Δ G = + 1h 21 min. — BR. ST. 165																												
I	-	-01.8	00.9	-00.8	-00.6	02.1	-03.5	12.0	15	-12.7	03	05	01.8	09	01.6	09	01.8	22	02.8	13	03.4	07	01.4	11	02.3	13	02.6	04
II	-	-00.5	03.1	00.6	01.0	04.1	-01.9	14.8	09	-10.6	03	10	01.9	04	02.0	02	02.0	10	02.5	24	02.4	06	02.8	08	02.0	17	02.2	03
III	-	02.6	08.5	05.1	05.3	09.5	01.6	21.2	25	-09.4	02	06	02.8	10	01.7	04	02.0	11	03.1	23	02.9	19	02.2	04	02.8	14	02.5	02
IV	-	08.5	14.9	10.6	11.1	16.3	05.8	26.0	26	-01.1	04	11	03.3	02	02.0	07	01.7	21	02.7	12	03.1	11	02.3	07	03.4	16	02.8	03
V	-	12.4	18.5	13.6	14.5	19.6	09.4	26.8	10	01.8	01	20	03.1	05	01.4	04	02.2	08	02.4	13	01.7	05	01.4	17	02.6	17	02.9	04
VI	-	18.2	23.9	19.1	20.1	25.5	14.6	32.0	19	08.8	03	10	02.2	07	01.6	11	02.1	11	02.3	05	03.2	10	01.8	09	01.9	22	02.3	05
VII	-	18.8	25.3	19.4	20.7	26.2	15.0	32.0	24	10.5	18	13	02.2	08	01.2	03	01.7	11	01.9	11	01.9	05	01.8	15	02.7	21	02.6	06
VIII	-	17.9	25.4	19.1	20.4	26.3	15.0	32.6	07	10.3	27,14	02	01.0	15	01.3	07	01.3	17	02.0	06	01.8	09	01.4	06	02.5	17	02.3	14
IX	-	12.3	21.1	14.4	15.6	22.2	10.5	32.2	12	-01.4	29	16	02.1	04	02.2	02	01.5	12	01.8	11	01.9	09	01.8	12	01.7	15	02.1	09
X	-	06.2	15.1	09.2	09.9	16.0	04.9	25.0	09	-01.6	16	08	01.4	03	01.3	01	02.0	17	02.0	16	02.3	13	01.8	06	01.7	23	02.3	06
XI	-	05.3	11.9	07.2	07.9	12.5	03.7	20.8	03	-01.6	07	04	01.5	02	01.0	02	01.5	22	02.2	25	02.4	07	02.0	07	02.4	18	02.4	03
XII	-	-00.1	03.0	01.1	01.3	04.0	-01.6	11.2	02	-13.0	27,25	04	02.8	07	02.1	03	02.0	14	02.6	15	02.1	14	01.6	07	01.4	19	02.2	10
GOD.	-	08.3	14.3	09.9	10.6	15.4	06.1	32.6	7.VIII	-13.0	25,27 XII	109	02.4	76	01.6	55	01.8	176	02.4	174	02.4	115	01.9	109	02.3	212	02.4	69

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha p_m mm	U_m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤-20.0	Tx ≤0.0	Tn ≤0.0	Tx ≥25.0	Tx ≥30.0	Tn ≥20.0	F (0-12) ≥6	≥8	Nm (0-10) ≤2.0	≥8.0	R mm ≥0.1	≥1.0	≥10.0	●	✱	✱	⌂	≈	▲	▲	⚡	≡	▦
GLADNOS																																					
BR. ST. 161																																					
H_o = 185 m H_b = - m h_o = 2.0 m h_b = 1.2 m																																					
I	8.9	8.1	8.1	8.4	-	85.9	89	85	91	88	69	050	-	-	.	11	27	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	8.6	7.9	7.5	8.0	-	84.1	87	79	86	85	87	105	032.5	12	.	06	24	.	.	.	05	.	.	16	18	16	04	10	14	.	.	.	.	.	.	11	22
III	8.3	8.2	9.5	7.3	-	85.4	87	69	84	80	50	062	016.0	28	.	01	13	.	.	.	05	.	01	16	14	11	02	12	04	01	.	.	.	.	.	06	01
IV	6.3	7.0	5.5	6.2	-	07.2	78	59	76	71	26	064	021.7	15	.	.	02	03	.	.	04	.	01	09	11	09	02	11	.	.	.	.	.	01	03	.	.
V	6.7	7.8	7.1	7.2	-	08.9	80	62	80	74	36	094	020.1	18	.	.	.	03	.	.	02	.	.	12	18	12	04	18	.	.	.	.	.	.	05	02	.
VI	4.8	5.2	7.2	5.7	-	13.2	82	65	84	77	50	093	033.9	11	.	.	.	19	02	.	.	.	04	05	14	11	03	14	.	.	.	.	.	.	10	01	.
VII	4.2	5.4	4.7	4.8	-	13.5	80	65	83	76	45	093	028.5	17	.	.	.	19	07	03	01	.	08	08	10	06	04	10	.	.	.	.	.	.	05	01	.
VIII	4.5	5.0	3.3	4.3	-	13.4	83	59	80	74	47	029	009.7	25	.	.	.	20	06	02	.	.	08	02	11	04	.	11	.	.	.	.	.	.	07	.	.
IX	5.1	5.3	2.8	4.4	-	10.2	82	57	79	73	38	024	011.2	17	.	.	.	09	04	.	.	.	07	06	09	03	01	09	.	.	.	.	.	.	02	01	.
X	5.4	5.6	5.4	5.5	-	07.2	88	61	82	77	42	051	020.9	02	.	.	02	.	.	.	.	.	08	12	08	07	01	08	.	.	.	.	.	.	01	01	.
XI	7.6	6.6	6.0	6.7	-	06.4	86	68	85	80	42	038	015.8	17	.	.	03	.	.	.	.	.	04	12	11	08	01	11	.	.	.	.	.	.	01	05	.
XII	8.1	7.6	7.3	7.7	-	04.5	91	83	90	88	59	024	005.5	26	.	04	19	.	.	.	02	.	01	17	11	08	.	08	04	.	.	.	.	.	.	14	04
GOD.	6.5	6.6	5.9	6.4	-	08.2	84	67	83	78	87	734	-		.	22	90	73	19	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BEČEJ																																					
BR. ST. 162																																					
H_o = 75 m H_b = - m h_o = 2.0 m h_b = 1.0 m																																					
I	8.7	7.9	5.6	7.4	-	03.8	88	80	86	85	63	044	015.4	08	05	10	25	.	.	.	02	.	01	15	15	08	01	10	08	02	.	01	.	.	.	08	23
II	8.8	7.6	6.7	7.7	-	04.3	88	76	88	84	49	076	011.8	14	.	05	23	.	.	.	01	.	.	14	18	13	03	10	13	.	.	.	.	.	.	04	10
III	7.8	7.8	5.3	7.0	-	05.3	88	63	83	78	28	057	015.9	15	01	01	12	.	.	.	04	.	01	14	18	10	01	14	04	01	.	.	01	.	.	02	01
IV	5.7	7.1	4.9	5.9	-	07.4	85	58	76	73	30	061	027.3	09	.	.	04	03	.	.	02	.	.	07	13	08	02	13	.	.	.	.	.	.	02	.	.
V	6.4	8.1	5.2	6.6	-	09.6	86	59	83	76	33	066	024.2	23	.	.	.	04	.	.	03	.	01	08	18	12	01	18	.	.	.	.	.	.	04	02	.
VI	4.5	6.1	4.8	5.1	-	14.2	85	60	87	77	44	074	018.3	18	.	.	.	19	04	.	02	.	03	03	13	10	03	13	.	.	.	.	.	01	10	.	.
VII	4.1	5.8	4.1	4.7	274.2	14.3	86	62	85	78	46	075	024.7	06	.	.	.	21	09	.	01	01	08	05	11	07	02	11	.	.	.	.	.	.	03	.	.
VIII	4.6	5.2	5.2	5.0	268.1	14.7	91	60	93	81	46	115	037.4	25	.	.	.	19	05	.	.	.	02	06	11	10	04	11	.	.	.	.	.	.	07	01	.
IX	4.9	5.5	2.7	4.3	204.9	11.1	92	61	88	80	31	046	025.8	17	.	.	02	09	03	.	.	.	08	04	10	05	02	10	.	.	.	.	.	.	03	.	.
X	5.7	5.8	4.3	5.2	169.3	07.3	93	58	88	80	39	036	013.1	02	.	.	04	.	.	.	.	.	09	10	09	05	01	09	.	.	.	.	.	.	.	03	.
XI	7.7	6.9	5.7	6.8	104.0	06.5	92	64	88	81	32	035	012.8	17	.	.	02	.	.	.	.	.	04	11	12	09	01	12	.	.	.	.	.	.	01	02	.
XII	8.0	7.9	7.7	7.9	-	04.5	93	83	90	89	55	044	010.5	24	04	03	20	.	.	.	01	.	01	19	17	10	01	10	07	.	.	.	.	.	.	08	04
GOD.	6.4	6.8	5.2	6.1	-	08.6	88	65	86	80	28	729	037.6	15 VIII	10	19	92	75	21	.	16	01	38	116	165	107	22	143	32	03	.	01	01	01	30	30	40
SENTA																																					
BR. ST. 163																																					
H_o = 80 m H_b = - m h_o = 2.0 m h_b = 1.0 m																																					
I	8.3	7.8	7.1	7.7	-	04.8	90	88	89	89	60	040	016.8	08	02	10	23	.	.	.	.	.	02	17	16	07	01	10	08	.	.	01	.	.	.	14	23
II	7.6	7.8	6.4	7.9	-	04.4	90	80	90	87	61	072	017.5	11	.	04	19	.	.	.	.	.	01	16	20	12	03	10	12	.	.	01	.	.	.	10	-
III	8.1	8.2	6.2	7.5	-	05.6	90	71	84	81	45	058	011.3	15	.	01	09	.	.	.	01	01	.	17	17	12	02	15	04	01	.	.	.	.	.	05	01
IV	5.4	7.0	4.7	5.7	-	07.9	86	64	78	76	38	035	016.5	09	.	.	01	03	.	.	01	01	03	06	13	08	01	12	01	.	.	.	.	.	.	02	.	.
V	6.6	7.8	6.2	6.9	-	09.9	86	63	83	77	28	048	009.8	28	.	.	.	05	.	.	.	.	01	10	16	10	.	16	.	.	.	.	.	.	06	03	.
VI	4.5	5.8	5.6	5.3	-	13.7	82	58	83	74	31	101	018.6	19	.	.	.	21	06	.	01	01	04	05	16	10	04	16	.	.	.	.	.	.	11	01	.
VII	4.1	4.7	3.7	4.2	-	14.2	82	58	81	74	42	048	017.7	17	.	.	.	22	13	.	02	02	12	05	07	06	03	07	.	.	.	.	.	.	01	.	.
VIII	3.8	5.0	3.5	4.1	-	14.7	85	63	85	78	17	130	058.5	10	.	.	.	.	.	.	.	.	09	03	11	08	04	11	.	.	.	.	.	.	11	01	.
IX	4.4	4.3	2.7	3.8	-	12.0	90	70	86	82	53	031	017.3	17	.	.	01	09	03	.	.	.	10	04	07	05	01	07	.	.	.	.	.	.	01	05	.
X	5.5	5.3	4.9	5.2	-	08.5	93	75	89	86	57	030	015.0	02	.	.	03	04	.	.	.	.	09	08	09	04	01	09	.	.	.	.	.	.	.	05	.
XI	7.3	6.9	6.4	6.9	-	06.8	92	71	86	83	33	033	012.6	17	.	.	01	.	.	.	.	.	03	13	10	07	01	10	.	.	.	.	.	.	.	10	07
XII	8.2	8.0	7.0	7.7	-	04.7	92	85	93	90	53	044	008.0	24	04	.	23	.	.	.	.	.	02	18	16	11	.	12	05	.	.	.	.	.	.	.	.
GOD.	6.2	6.6	5.5	6.1	-	08.9	88	70	85	81	17	670	058.5	10 VIII	06	15	80	64	22	.	05	05	56	122	158	100	21	135	30	01	.	02	.	.	33	37	-
ZRENJANIN																																					
BR. ST. 164																																					
H_o = 82 m H_b = - m h_o = 2.0 m h_b = 1.0 m																																					
I	7.9	7.8	7.3	7.7	049.2	03.9	86	81	86	84	55	040	015.8	02	02	12	24	.	.	.	11	04	.	15	13	06	02	09	06	.	.	01	.	.	.	04	20
II	8.6	8.5	7.5	8.2	055.1	04.3	88	79	86	84	57	084	016.7	12	01	04	18	.	.	.	12	03	.	17	19	15	03	10	14	01	.	.	.	.	.	03	12
III	8.1	8.0	5.1	7.1	113.7	05.4	86	65	80	77	45	047	011.7	15	.	01	08	.	.	.	17	04	02	14	15	10	01	13	05	03	.	.	.	.	.	01	01
IV	6.4	7.3	5.0	6.2	170.6	07.7	84	62	75	74	36	048	012.0	02	.	.	01	02	.	.	19	06	02	10	13	09	02	13	.	.	.	.	.	.	03	.	.
V	6.0	8.0	5.7	6.6	184.5	09.9	86	65	85	79	42	071	016.9	23	.	.	.	02	.	.	17	01	02	09	14	11	02	14	.	.	.	.	.	.	07	01	.
VI	3.9	4.9	4.6	4.5	257.0	14.4	85	64	89	79	50	140	058.7	11	.	.	.	20	01	.	09	03	05	02	15	12	04	15	.	.	.	.	.	01	12	01	.
VII	4.2	5.4	3.6	4.4	284.0	14.5	86	64	86	79	50	078	031.4	06	.	.	.	21	07	.	10	02	01	08	08	07	02	08	.	.	.	.	.	.	05	.	.
VIII	3.9	5.2	2.2	3.8	272.4	14.3	87	59	86	78	46	036	014.0	25	.	.	.	19	05	.	08	02	09	03	10	09	01	10	.	.	.	.	.	.	08	.	.
IX	5.1	5.6	2.1	4.3	202.7	10.5	91	55	84	76	26	027	012.4	17	.	.	02	09	04	.	07	.	08	04	07	04	01	07	.	.	.	.	.	.	01	01	.
X	5.7	5.4	4.5	5.2	168.4	07.4	92	60	86	79	44	040	010.5	02	.	.	03	.	.	.	04	.	08	09	08	07	01	08	.	.	.	.	.	01	01	05	.
XI	7.5	7.0	5.5	6.7	103.6	06.5	89	67	85	80	41	041	016.2	17	.	.	02	.	.	.	06	.	04	12	11	08	01	11	.	.	.	.	.	.	01	01	.
XII	7.6	8.1	7.2	7.6	039.8	04.5	92	83	90	88	55	027	007.3	24	04	02	23	.	.	.	04	03	01	16	17	08	.	12	08	02	.	.	.	.	.	08	06
GOD.	6.2	6.8	5.0	6.0	1881.0	08.6	87	67	84	79	26	679	058.7	4 VI	07	19	81	73	17	.	124	28	42	119	150	106	20	130	33	06	.	01	.	02	38	25	39
KIKINDA																																					
BR. ST. 165																																					
H_o = 81 m H_b = - m h_o = 2.0 m h_b = 1.0 m																																					
I	8.6	7.9	7.0	7.9	040.2	03.9	87	80	87	85	60	041	013.9	08	04	09	24	.	.	.	01	.	01	17	14	06	01	09	06	01	.	.	.	.	.	05	21
II	8.1	8.1	6.8	7.7	060.9	04.2	86	75	85	82	49	069	013.1	11	01	05	20	.	.	.	02	01	.	14	17	10	03	11	10	01	.	.	.	.	.	05	07
III	7.7	8.0	5.5	7.1	102.0	05.2	85	64	81	77	34	058	009.8	15	.	01	11	.	.	.	03	02	02	15	17	11	.	15	03	01	.	.	.	.	.	02	01
IV	5.6	7.1	4.9	5.9	176.0	07.0	81	54	72	69	24	059	021.8	09	.	.	02	02	.	.	03	02	02	08	13	09	02	13	.	.	.	.	.	.	02	.	.
V	5.9	7.8	5.9	6.5	174.5	08.9	81	54	77	71	31	066	012.1	24	.	.	.	02	.	.	03	01	03	09	15	12	01	15	.	.	.	.	.	.	05	01	.
VI	4.1	5.2	4.9	4.8	275.0	12.7	80	56	79	72	35	102	028.9	24	.	.	.	21	03	.	02	01	05	05	14	12	04	14	.	.	.	.	.	01	10	01	.
VII	3.8	5.3	3.1	4.1	288.9	13.0	80	54	78	71	39	052	017.2	06	.	.	.	21	09	.	03	.	11	05	10	06	02	10	.	.	.	.	.	.	05	.	.
VIII	3.8	4.6	3.7	4.0	271.8	13.5	85	54	84	74	40	141	047.8	03	.	.	.	19	05	.	01	03	08	03	11	09	04	11	.	.	.	.	.	01	11	.	.
IX	4.4	5.3	2.5	4.1	210.4	10.1	88	54	79	74	31	023	007.4	18	.	.	02	09	03	.	.	.	09	03	07	04	.	07	.	.	.	.	.	.	01	.	.
X	4.8	5.3	4.5	4.9	164.6	06.9	89	55	81	75	37	026	008.8	02	.	.	03	01	.	.	.	.	10	06	08	05	.	08	.	.	.	.	.	.	01	.	02	.
XI	6.8	6.7	5.0	6.2	105.8	06.3	88	64	82	78	29	033	015.0	17	.	.	01	.	.	.	02	.	03	09	06	01	09	.	.	.	.	.	.	.	.	01	03	.
XII	8.5	8.0	7.4	8.0	039.9	04.5	91	81	89	87	53	049	011.9	26	02	.	21	.	.	.	01	.	.	19	15	10	01	10	06	.	.	.	.	.	.	08	07
GOD.	6.0	6.4	5.1	5.9	1912.0	08.0	85	62	81	76	24	719	047.8	5 VIII	07	15	84	75	20	.	21	10	54	115	150	100	19	132	27	03	.	.	.	03	35	27	36

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dles)	Max	Min	Max	Dat.	Min	Dat.	Cestina pravaca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
φ = 45° 27' N λ = 20° 51' E Gr. ΔG = + 1h 22 min. — JAŠA TOMIĆ — BR. ST. 166																												
I	-	-01.0	02.0	-00.4	00.1	02.8	-02.4	13.2	15	-12.5	20	05	01.4	06	01.0	02	01.0	40	02.6	04	01.0	02	01.5	09	02.3	17	02.1	[illegible]
II	-	-00.2	03.6	01.2	01.5	04.5	-01.4	15.0	09	-12.5	03	02	01.0	08	01.1	04	01.2	19	01.8	12	01.8	05	01.4	02	01.5	25	01.8	[illegible]
III	-	03.1	09.3	05.5	05.8	10.1	02.1	21.4	25	-06.5	2	07	01.7	02	01.0	01	01.0	27	03.6	10	01.5	07	07.0	12	02.0	17	02.7	10
IV	-	09.1	15.8	11.1	11.8	17.0	06.8	27.5	26	0[illegible].0	04	12	01.8	04	01.0	02	01.0	23	02.7	10	02.3	07	01.7	04	03.0	19	02.4	[illegible]
V	-	12.7	19.3	13.6	14.8	19.9	10.0	27.5	10	02.4	03	16	02.0	03	01.3	03	01.3	15	01.8	03	01.3	07	01.7	06	02.5	23	03.[illegible]	17
VI	-	18.5	24.8	18.8	20.2	25.7	15.0	31.5	23,22	06.8	03	09	01.8	09	01.1	03	01.3	09	01.4	08	02.0	08	01.9	05	01.6	2[illegible]	02.[illegible]	[illegible]
VII	-	19.4	25.9	19.8	21.2	27.0	15.7	32.7	24,23	11.0	19,18	05	01.8	03	01.0	02	01.0	18	01.9	02	02.5	07	02.1	10	02.1	29	02.[illegible]	17
VIII	-	18.6	26.6	19.4	21.0	27.4	15.5	33.6	07	10.[illegible]	27	02	01.0	09	01.1	05	01.0	18	01.8	10	01.9	06	02.0	02	01.5	19	02.[illegible]	22
IX	-	12.8	22.4	14.7	16.2	23.3	10.9	34.4	12	-01.[illegible]	30,29	07	01.9	01	02.0	.	.	20	01.7	05	01.2	06	01.3	09	01.6	29	01.7	13
X	-	06.6	15.3	09.2	10.1	16.1	05.2	25.0	08	-02.[illegible]	16	08	01.4	01	01.0	02	01.0	26	01.9	03	01.0	10	01.6	07	01.7	22	01.7	14
XI	-	05.6	12.3	07.3	08.1	12.6	04.3	20.5	03	-01.[illegible]	07	07	01.1	05	01.2	02	01.0	26	02.2	14	01.3	06	01.8	07	01.4	11	02.5	12
XII	-	00.2	03.2	01.3	01.5	04.0	-01.2	11.5	30	-13.3	27	02	01.0	05	01.0	06	01.2	17	02.9	06	01.3	03	01.7	18	01.3	22	01.3	14
GOD.	-	08.8	15.0	10.1	11.0	15.9	06.7	34.4	18 IX	-13.3	27 XII	82	01.7	55	01.1	32	01.1	258	02.3	87	01.6	74	01.8	91	01.8	253	02.1	163
φ = 45° 09' N λ = 21° 19' E Gr. ΔG = + 1h 25 min. — VRŠAC — BR. ST. 167																												
I	753.9	00.5	03.0	01.2	01.5	04.4	-02.3	14.6	15	-12.8	22	04	01.2	02	01.5	04	04.5	33	05.0	10	02.9	02	01.5	22	02.1	04	03.0	12
II	750.5	01.2	04.1	02.5	02.6	05.8	-00.7	16.2	09	-08.7	18	06	01.8	03	01.7	02	03.5	20	03.6	22	03.1	02	02.0	08	01.8	14	02.8	07
III	751.9	04.0	09.0	06.1	06.3	10.5	01.9	22.2	25	-01.7	02	05	02.4	05	01.8	05	03.4	32	04.1	19	02.8	04	02.5	07	01.9	08	02.8	08
IV	752.3	10.1	15.6	11.4	12.1	17.4	06.4	26.6	26,24	-0[illegible].7	04	11	02.6	05	01.6	01	06.0	23	04.0	14	02.8	06	01.8	05	02.4	18	02.3	[illegible]
V	752.8	12.6	18.1	13.6	14.5	19.4	09.4	27.4	10	04.1	04	15	02.3	11	01.9	01	04.0	18	02.4	11	02.4	05	01.8	07	02.1	15	02.9	10
VI	753.9	18.0	23.6	18.9	19.9	25.1	14.4	30.7	29	08.4	03	06	01.7	12	01.8	04	02.5	16	03.1	16	02.1	04	01.5	04	01.8	12	02.2	16
VII	753.0	18.6	25.1	19.6	20.7	26.4	14.8	31.8	24,23	10.2	18	12	01.7	03	02.0	05	02.4	13	02.7	11	02.4	09	01.4	11	01.8	08	01.9	21
VIII	753.2	18.0	25.3	19.3	20.4	26.8	14.4	32.3	07	07.3	19	11	01.5	13	01.7	07	01.1	20	03.5	08	01.4	02	01.0	06	02.0	09	02.1	17
IX	757.0	12.5	21.5	14.4	15.7	22.7	09.7	33.0	12	-04.2	30	10	01.9	12	01.7	02	01.5	14	02.4	15	01.7	03	01.7	06	01.7	08	02.6	20
X	757.3	07.6	15.0	09.3	10.3	16.1	04.5	25.6	07	-01.6	25	08	02.2	07	01.7	03	01.0	19	03.0	16	02.2	10	01.6	08	02.5	10	02.[illegible]	12
XI	755.9	06.6	12.2	07.6	08.5	13.2	02.7	20.4	03	-04.2	26	04	01.2	07	01.4	06	01.0	22	03.5	25	03.1	05	01.6	07	02.1	07	02.3	07
XII	758.6	00.6	03.7	01.8	02.0	05.1	-01.8	14.0	30	-15.8	27	07	02.1	07	01.6	07	04.3	14	03.8	10	02.5	04	01.2	10	01.6	20	01.8	14
GOD.	754.2	09.2	14.7	10.5	11.2	16.1	06.1	33.0	18 IX	-15.8	27 XII	99	02.0	87	01.7	47	02.6	244	03.6	177	02.5	56	01.6	101	02.0	133	02.4	[illegible]
φ = 44° 33' N λ = 19° 14' E Gr. ΔG = + 1h 17 min. — LOZNICA — BR. ST. 168																												
I	750.4	-01.0	01.9	-00.2	00.1	03.2	-02.7	10.8	27	-09.7	03	.	.	01	01.0	02	01.5	.	.	.	.	03	01.7	06	02.3	05	03.0	76
II	747.2	00.0	05.4	01.5	02.1	06.7	-02.2	17.8	05	-10.5	18	07	02.0	01	01.0	02	02.0	01	01.0	01	02.0	16	02.7	03	01.7	13	02.2	45
III	748.2	03.7	09.9	06.0	06.4	11.0	02.3	22.7	24	-03.7	02	01	02.0	04	02.0	03	02.3	06	02.2	01	03.0	13	02.2	10	01.9	09	02.8	46
IV	749.1	08.9	15.7	10.8	11.6	17.5	06.2	28.8	20	-0[illegible]	05	11	02.3	02	01.0	02	01.5	.	.	04	01.5	12	02.1	04	02.5	10	02.8	45
V	750.2	11.9	17.7	13.3	14.0	19.3	09.4	29.1	10	02.8	01	02	02.0	04	01.5	02	02.0	.	.	.	.	12	02.2	06	02.0	15	02.9	[illegible]
VI	751.1	17.5	24.8	18.5	19.8	26.0	14.3	31.8	23	08.4	03	05	02.2	06	02.3	04	01.5	.	.	02	01.5	13	01.8	03	02.3	08	02.6	49
VII	750.3	17.6	24.8	18.6	19.9	26.0	14.6	34.3	25	10.4	27	07	01.7	03	01.7	05	02.0	.	.	.	.	09	01.9	08	02.9	09	02.6	[illegible]
VIII	750.2	17.6	25.8	18.7	20.2	26.8	14.7	33.4	07	09.6	27	08	01.8	09	01.4	03	01.0	.	.	01	02.0	06	01.8	05	01.8	01	03.0	61
IX	754.0	12.8	22.1	13.9	15.6	23.2	10.4	33.7	11	-01.2	29	07	01.6	02	01.5	03	01.7	.	.	.	.	04	01.8	02	02.5	03	02.[illegible]	69
X	754.2	06.5	16.4	08.9	10.2	17.3	05.0	26.2	10	-00.8	17	06	02.0	02	02.0	03	02.0	.	.	01	02.0	05	01.6	02	02.5	05	02.2	69
XI	752.4	06.0	13.1	07.6	08.6	14.0	04.1	20.0	30	-10.2	27	02	02.0	01	01.0	.	.	01	02.0	06	02.3	16	02.3	04	02.8	04	02.8	56
XII	755.3	01.0	04.4	01.5	02.1	05.5	-00.8	22.0	03	-06.8	26	02	02.5	01	01.0	01	01.0	.	.	01	02.0	08	03.0	04	02.0	06	02.3	70
GOD.	751.0	08.5	15.2	09.9	10.9	16.4	06.3	34.3	25 VIII	-10.5	18 II	53	02.0	35	01.6	30	01.7	08	02.0	17	02.0	117	02.2	57	02.2	88	02.6	640
φ = 44° 11' N λ = 19° 23' E Gr. ΔG = + 1h 18 min. — LJUBOVIJA — BR. ST. 169																												
I	-	-00.5	03.2	00.2	00.8	04.8	-02.1	14.2	15	-07.8	04	07	01.1	.	.	08	01.0	01	01.0	.	.	.	.	20	01.2	11	01.3	46
II	-	-00.6	05.3	01.2	01.8	06.9	-02.4	-	-	-	-	01	02.0	01	01.0	06	01.2	06	02.3	.	.	09	01.8	25	01.4	19	1.2	17
III	-	02.6	10.6	05.2	05.9	12.1	01.2	22.4	24	-03.7	09	04	01.0	02	01.0	17	01.8	05	02.0	02	01.0	01	03.0	17	01.2	12	01.1	33
IV	-	07.3	16.5	09.9	10.9	18.0	05.5	28.0	20	-02.0	05	02	01.0	02	01.0	08	01.6	02	01.0	02	04.0	07	01.0	24	01.2	11	01.3	[illegible]
V	-	10.0	17.6	11.7	12.8	18.8	08.5	29.6	1[illegible]	02.7	01	1[illegible]	01.0	01	01.0	02	01.0	02	01.0	02	01.0	05	01.0	32	01.3	10	1.0	29
VI	-	15.0	23.9	16.9	18.2	25.5	13.3	31.0	18	06.9	03	11	01.0	02	02.0	05	01.0	02	02.0	01	01.0	01	01.0	21	01.1	07	01.1	40
VII	-	15.6	24.4	17.4	18.7	25.9	13.8	32.8	25	08.6	20	10	01.0	03	01.0	.	.	04	01.0	01	01.0	02	01.0	26	01.2	07	01.1	4[illegible]
VIII	-	15.9	25.9	18.1	19.5	27.0	14.5	34.0	07	10.6	28	13	01.1	01	01.0	03	01.3	01	01.0	02	01.0	05	01.0	10	01.1	23	01.1	35
X	-	11.6	22.5	13.1	15.0	23.5	10.1	33.9	11	-0[illegible].5	29	14	01.0	01	02.0	.	.	01	01.0	01	01.0	01	01.0	17	01.2	13	01.0	42
X	-	06.1	16.1	08.0	09.6	16.9	04.8	26.6	10	-01.[illegible]	25	26	01.2	.	.	03	01.0	.	.	.	.	.	.	14	01.0	11	01.1	39
XI	-	04.1	12.6	05.9	07.1	13.6	02.2	-	-	-	-	14	01.0	01	01.0	02	01.0	04	02.8	01	03.0	02	01.0	13	01.1	07	01.0	46
XII	-	00.0	04.4	00.7	01.5	05.3	-01.7	19.2	30	-12.3	27	10	01.4	01	01.0	.	.	.	.	03	01.0	03	07.7	22	01.0	12	01.0	42
GOD.	-	07.3	15.2	09.0	10.2	16.5	05.6	-				122	01.1	15	01.2	54	01.4	28	01.8	15	01.5	31	01.5	241	01.2	143	01.1	446
φ = 44° 58' N λ = 19° 38' E Gr. ΔG = + 1h 18 min. — SREMSKA MITROVICA — BR. ST. 170																												
I	-	-01.6	01.1	-00.5	-00.4	02.0	-03.4	07.3	16	-13.5	09	.	.	09	01.6	42	02.2	02	01.0	.	.	01	01.0	24	02.2	11	02.7	[illegible]
II	-	-01.0	03.2	00.5	00.8	04.4	-02.5	16.8	09	-1[illegible].2	18	03	02.3	09	02.0	28	01.9	06	01.7	03	01.3	06	01.7	13	02.5	16	02.8	.
III	-	03.0	09.7	05.7	06.0	10.9	01.9	22.2	25	-0[illegible].9	02	03	01.0	06	01.5	27	02.6	08	02.4	04	01.5	07	01.4	24	02.0	14	03.0	.
IV	-	09.0	15.6	10.9	11.6	17.3	06.5	26.8	26,24	-0[illegible].7	04	09	01.2	07	01.9	20	02.0	08	01.9	02	03.0	05	01.4	18	02.5	21	03.1	
V	-	11.9	18.6	13.4	14.3	20.1	09.3	27.5	10	03.2	02,01	03	03.0	01	02.0	10	01.6	08	02.0	.	.	10	01.9	30	02.3	30	02.9	[illegible]
VI	-	18.1	24.9	18.8	20.2	26.2	14.5	31.2	23	08.5	03	04	02.2	09	01.9	12	01.7	07	02.0	03	01.7	13	01.6	22	01.7	19	02.6	[illegible]
VII	-	18.2	25.0	18.5	20.1	26.2	14.6	32.4	25	09.[illegible]	20	06	02.0	05	01.4	13	01.6	10	01.5	07	02.0	12	01.7	14	02.5	26	02.6	[illegible]
VIII	-	17.7	26.3	18.6	20.3	27.1	14.6	32.7	07	10.0	28,19	03	01.3	07	01.3	18	01.7	13	01.6	.	.	07	01.4	14	02.1	20	02.5	11
IX	-	12.2	22.0	13.8	15.4	23.2	10.3	32.3	11	-0[illegible]	30	03	01.3	15	01.5	04	01.5	08	01.1	02	02.0	08	01.2	21	01.8	22	01.9	[illegible]
X	-	05.9	16.2	09.0	10.0	16.9	04.7	26.2	09	-01.5	25	04	02.0	10	01.3	16	01.9	13	01.3	01	02.0	06	01.2	19	01.7	22	02.2	[illegible]
XI	-	04.8	12.9	06.7	07.8	13.6	03.2	22.4	03	-01.4	14,13	03	01.3	07	01.3	18	01.6	11	01.5	02	01.0	11	01.5	17	01.8	17	02.2	[illegible]
XII	-	00.3	04.0	00.9	01.5	04.9	-01.8	15.1	01	-1[illegible]	27	01	01.0	09	01.6	23	01.8	04	01.8	.	.	01	01.0	35	01.9	18	02.5	[illegible]
GOD.	-	08.2	15.0	09.7	10.6	16.1	06.0	32.7	1 VIII	-1[illegible].5	9 I	42	02.3	94	01.6	231	01.9	98	01.7	19	01.7	87	01.5	251	02.1	236	02.6	37

Mesec	Oblačnost mm (0-10) 7	14	21	Sred. (Dnev.)	Insolacija (ure) mesec	Vlažnost zraka e_m mm	U_m % 7	14	21	Sred. (Dnev.)	Min	Padavine R mm Σ	Max	Dnev.	Broj dana s: Tn ≤ 30.0	Tx ≤ 0.0	Tn < 0.0	Tx ≤ 25.0	Tx ≤ 10.0	Tn ≤ 0.0	F (0-12) ≥ 6	F ≥ 8	Sm (0-10) < 2.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	●	⊥	⊥	≈	▲	▲	RT	≡	▦
BR. ST. 166 — JASA TONEC																																					
I	9.4	8.4	8.5	8.7	-	84.1	85	81	87	84	41	042	014.1	08	02	07	23	.	.	.	04	02	01	24	11	05	02	08	05	.	.	.	.	.	.	02	15
II	9.1	9.3	8.8	9.1	-	84.5	88	79	87	85	57	085	015.1	12	02	04	16	.	.	.	.	01	.	21	18	14	04	10	12	02	.	.	.	.	.	.	02	04
III	8.7	8.5	7.4	8.2	-	85.5	84	68	82	77	35	047	018.2	15	.	01	08	.	.	.	04	02	01	20	15	11	01	13	05	.	.	.	.	.	.	.	02
IV	5.8	7.5	7.5	6.9	-	07.9	84	61	79	74	36	078	013.1	15	.	.	.	03	.	.	03	01	01	13	11	10	04	11	.	.	.	.	.	01	03	.	.
V	6.0	7.0	7.9	7.3	-	10.9	88	71	91	83	52	128	022.5	21	.	.	.	05	.	.	04	01	03	15	17	15	06	17	.	.	.	.	.	01	09	01	.
VI	4.6	6.3	7.0	6.0	-	15.2	86	71	91	83	48	119	026.2	11	.	.	.	21	04	.	01	01	04	09	15	13	05	15	.	.	.	.	.	.	12	01	.
VII	4.6	6.7	3.9	5.1	-	15.1	84	63	87	78	41	091	027.4	06	.	.	.	21	11	01	01	01	04	08	09	07	04	09	.	.	.	.	.	.	05	.	.
VIII	4.6	6.1	4.8	5.2	-	15.3	87	65	90	80	37	096	013.4	08	.	.	.	22	08	01	.	.	06	09	08	08	01	08	.	.	.	.	.	.	10	01	.
IX	4.8	5.0	3.7	4.5	-	11.0	89	57	82	76	36	038	014.5	02	.	.	02	09	04	.	.	.	09	05	08	04	01	08	.	.	.	.	.	.	04	02	.
X	5.1	5.6	6.1	5.6	-	07.9	91	67	91	83	48	044	014.2	02	.	.	02	01	.	.	.	.	07	11	08	07	01	08	.	.	.	.	.	.	02	04	.
XI	7.1	6.3	6.6	6.7	-	07.3	93	77	92	87	56	025	005.5	24	.	.	01	.	.	.	01	.	04	11	09	08	.	09	.	.	.	.	.	.	01	04	.
XII	7.5	8.7	8.9	8.4	-	04.8	92	88	93	91	79	057	008.8	26	01	.	19	.	.	.	01	01	01	22	17	11	.	13	06	01	.	.	.	.	.	05	01
GOD.	6.4	7.2	6.8	6.8	-	09.1	87	70	87	81	35	764	027.4	6.VII	05	12	71	82	27	02	19	10	41	168	146	113	29	129	26	03	.	.	.	02	46	24	26
BR. ST. 167 — VRSAC																																					
I	7.3	8.4	6.9	7.5	-	043.8	84.0	80	72	77	74	28	032	013.5	08	02	08	19	.	.	.	18	10	01	14	11	09	01	06	07	01	.	.	.	.	.	05	11
II	8.8	8.5	7.5	8.3	-	052.8	84.4	82	72	82	79	48	089	020.7	12	.	03	18	.	.	.	19	06	.	18	20	14	02	11	16	03	.	.	.	.	.	04	13
III	8.0	7.8	6.5	7.4	-	111.3	09.1	79	81	75	71	29	062	014.4	15	.	01	11	.	.	.	20	11	01	15	15	12	02	13	06	03	.	.	.	.	.	.	02
IV	5.5	7.0	6.7	6.4	-	177.9	07.1	74	54	72	67	27	070	019.1	15	.	.	01	03	.	.	16	06	02	10	14	12	03	14	.	.	.	.	.	01	04	01	.
V	7.1	7.3	7.0	7.1	-	171.7	09.2	82	58	82	74	34	144	024.2	23	.	.	.	03	.	.	17	04	02	14	19	14	06	19	.	.	.	.	.	.	12	.	.
VI	4.5	6.0	5.8	5.4	-	252.4	13.3	83	63	82	76	40	114	022.1	19	.	.	.	19	02	02	09	04	01	03	16	14	05	16	.	.	.	.	.	.	13	03	.
VII	4.3	5.5	4.3	4.7	-	261.9	13.8	83	59	82	75	33	119	035.4	17	.	.	.	22	09	01	08	02	08	07	10	08	06	10	.	.	.	.	.	.	08	01	.
VIII	4.3	5.1	4.0	4.5	-	171.8	13.5	84	57	82	75	44	050	014.8	03	.	.	.	20	06	02	14	06	05	03	13	07	01	13	.	.	.	.	.	01	10	02	.
IX	4.6	5.4	3.0	4.3	-	187.1	10.5	88	54	82	76	35	026	007.4	01	.	.	04	09	04	03	09	02	10	05	09	06	.	09	.	.	.	.	.	.	03	04	.
X	5.6	6.1	4.6	5.4	-	198.6	07.3	85	61	84	77	36	061	016.0	02	.	.	04	02	.	.	12	03	07	09	10	06	05	10	.	.	.	.	.	.	01	03	.
XI	7.8	6.5	6.1	6.8	-	101.5	06.2	81	64	81	75	32	052	020.6	25	.	.	11	.	.	.	16	03	03	12	12	07	02	12	.	.	.	.	.	.	.	04	.
XII	7.8	8.7	6.9	7.8	-	033.7	04.6	88	79	87	85	48	028	006.3	26	01	01	20	.	.	.	10	06	01	17	17	08	.	12	06	.	.	.	.	.	.	10	06
GOD.	6.3	6.9	5.8	6.3	1704.6	08.2	82	63	80	75	27	855	035.4	11.VII	03	13	88	78	21	00	168	65	41	127	166	117	31	145	35	07	.	.	.	02	51	39	33
BR. ST. 168 — LOZNICA																																					
I	9.1	8.1	6.9	8.1	-	031.2	04.0	88	78	86	84	57	051	019.8	02	.	07	22	.	.	.	03	.	02	22	15	07	02	13	08	03	.	01	.	.	.	05	24
II	8.4	8.0	7.2	7.9	-	065.7	04.1	83	65	82	77	30	091	020.8	12	01	04	18	.	.	.	04	02	.	15	15	13	04	08	10	01	.	.	.	.	.	02	18
III	7.2	7.4	6.1	6.9	-	124.4	05.0	77	57	75	70	26	083	020.7	20	.	01	07	.	.	.	07	01	03	14	15	13	03	12	05	02	.	.	.	.	.	.	03
IV	6.9	7.6	5.2	6.5	-	194.0	06.8	79	51	78	67	21	073	023.8	15	.	.	02	04	.	.	11	.	02	12	14	09	03	16	.	.	.	.	.	.	01	.	.
V	7.6	7.8	6.5	7.3	-	164.5	08.6	80	58	77	71	33	111	018.3	23	.	.	.	03	.	.	08	.	01	13	18	13	05	18	.	.	.	.	.	.	08	.	.
VI	5.6	5.9	4.7	5.4	-	251.0	13.0	81	57	82	73	34	105	044.8	19	.	.	.	21	04	.	02	01	04	07	17	13	03	17	01	.	.	.	.	.	01	14	02	.
VII	4.7	5.1	4.0	4.6	-	273.2	13.2	85	57	84	75	37	102	046.7	06	.	.	.	20	09	.	04	01	10	08	10	07	03	10	.	.	.	.	.	.	02	01	.
VIII	5.3	4.8	3.1	4.4	-	297.0	14.2	90	58	89	79	38	091	019.6	03	.	.	.	20	07	01	02	.	05	04	09	08	04	09	.	.	.	.	.	.	09	03	.
IX	5.1	5.1	3.3	4.5	-	284.4	18.4	91	52	89	77	-	018	005.3	18	02	11	05	.	.	.	02	01	07	07	13	05	.	13	.	.	.	.	.	.	.	06	.
X	5.7	5.5	5.0	5.4	-	182.4	07.2	91	54	87	77	32	093	025.1	02	.	.	02	05	.	.	02	01	10	13	09	08	04	09	.	.	.	.	.	.	.	01	.
XI	7.9	6.9	6.1	7.0	-	107.6	06.3	85	60	83	76	24	075	020.3	17	01	04	16	.	.	.	02	.	02	13	12	10	04	12	.	.	.	.	.	.	.	04	.
XII	7.6	7.5	7.1	7.4	-	061.0	04.4	85	72	84	80	35	038	012.0	24	.	.	02	.	.	.	04	01	03	17	11	07	01	07	04	.	.	.	.	.	.	04	07
GOD.	6.8	6.6	5.4	6.3	1860.6	08.1	84	59	82	75	-	931	046.7	6.VII	04	27	74	73	20	01	56	08	49	145	160	113	36	144	28	06	.	01	.	01	34	28	49
BR. ST. 169 — LJUBOVIJA																																					
I	9.0	8.1	6.9	8.0	-	04.5	90	83	92	88	59	065	014.5	02	.	05	22	.	.	.	.	.	01	18	18	10	03	13	10	01	.	.	.	.	01	05	23
II	8.3	7.3	6.8	7.4	-	04.4	87	70	89	82	-	111	018.2	24	-	-	-	-	-	-	02	.	.	14	19	11	05	09	13	.	.	.	.	.	.	03	19
III	7.3	6.4	5.0	6.2	-	05.9	91	69	88	83	36	081	020.5	28	.	.	09	.	.	.	.	.	03	09	19	13	02	14	07	.	.	.	.	.	.	03	04
IV	7.1	7.1	4.8	6.3	-	08.4	92	70	87	83	46	072	032.5	15	.	.	03	07	.	.	03	.	01	12	20	11	02	20	01	01	.	.	.	.	01	05	.
V	8.4	7.5	6.6	7.5	-	-	-	-	-	-	-	149	024.5	23	.	.	.	04	.	.	.	.	.	16	27	19	05	25	01	01	.	.	.	.	07	06	.
VI	7.9	5.8	4.8	6.2	-	14.7	96	78	95	90	38	137	023.9	21	.	.	.	19	05	.	02	.	.	07	24	16	06	20	.	.	.	.	.	01	14	11	.
VII	9.1	5.9	4.2	6.4	-	-	-	-	-	-	-	141	040.4	06	.	.	.	20	08	.	.	.	.	09	18	09	04	14	.	.	.	.	.	.	05	16	.
VIII	9.0	4.8	4.1	6.0	-	18.0	97	67	96	87	40	044	016.3	23	.	.	.	20	08	.	.	.	01	07	11	08	01	11	.	.	.	.	.	.	09	21	.
IX	9.0	4.7	2.7	5.4	-	-	-	-	-	-	-	036	016.5	18	.	.	01	11	06	.	.	.	02	06	11	06	01	11	.	.	.	.	.	.	02	19	.
X	9.2	5.6	4.6	6.5	-	-	-	-	-	-	-	104	032.5	23	.	.	01	04	.	.	.	.	02	12	14	09	04	10	02	.	.	.	.	.	16	.	.
XI	8.6	6.5	4.8	6.6	-	-	-	-	-	-	-	080	015.2	17	-	-	-	-	-	-	.	.	01	09	12	08	04	12	.	.	.	.	.	.	.	10	.
XII	9.4	7.4	6.7	7.8	-	04.6	92	78	91	87	39	030	005.0	04	01	01	22	.	.	.	02	.	.	23	18	10	.	11	07	.	.	.	.	.	.	08	07
GOD.	8.5	6.4	5.2	6.7	-	-	-	-	-	-	-	1050	040.4	6.VII	-	-	-	-	-	-	09	.	11	139	211	130	37	178	41	03	.	.	.	01	35	107	93
BR. ST. 170 — SREMSKA MITROVICA																																					
I	8.9	8.1	8.3	8.4	-	04.0	91	81	89	87	64	072	030.8	02	02	09	24	.	.	.	02	.	.	19	16	09	02	14	09	.	.	02	02	.	.	08	25
II	7.5	7.9	7.2	7.5	-	04.3	91	78	89	86	43	094	013.5	12	01	04	25	.	.	.	03	01	01	14	18	14	02	09	13	01	.	.	.	.	.	06	17
III	7.2	7.6	5.2	6.7	-	05.3	86	59	81	75	30	060	014.4	15	.	01	06	.	.	.	08	01	03	13	13	09	02	10	05	01	.	.	.	.	.	01	02
IV	6.1	7.2	4.7	6.0	-	07.1	88	53	74	69	30	059	016.9	15	.	.	02	04	.	.	07	01	01	07	13	09	02	13	.	.	.	.	.	.	03	.	.
V	6.8	7.5	5.7	6.7	-	09.2	85	57	80	74	36	097	020.8	23	.	.	.	04	.	.	08	01	01	11	18	14	04	18	.	.	.	.	.	01	06	02	.
VI	3.9	5.3	5.2	4.8	-	13.4	85	57	82	75	39	114	039.0	11	.	.	.	22	05	.	02	01	06	03	18	11	02	18	.	.	.	.	.	01	14	.	.
VII	4.1	4.8	3.3	4.0	-	13.8	86	56	88	78	41	079	026.3	06	.	.	.	20	11	.	06	01	13	06	13	09	02	13	.	.	.	.	.	.	04	01	.
VIII	3.8	4.1	3.3	3.7	-	14.2	89	56	89	78	42	039	016.8	18	.	.	.	21	09	.	04	.	09	02	13	09	01	13	.	.	.	.	.	01	.	08	01	.
IX	3.1	4.7	3.0	4.2	-	18.9	94	55	89	80	30	034	011.6	18	.	.	02	11	05	.	.	.	07	04	10	06	01	10	.	.	.	.	.	.	01	03	.
X	4.5	5.3	4.2	4.6	-	07.3	94	56	87	79	35	054	018.2	02	.	.	01	05	.	.	.	.	10	08	08	06	02	08	.	.	.	.	.	.	.	04	.
XI	6.8	6.5	5.8	6.4	-	06.5	92	64	89	82	34	042	018.1	17	.	.	06	.	.	.	01	.	04	11	13	08	01	13	.	.	.	.	.	.	.	03	.
XII	8.0	7.8	6.9	7.3	-	04.6	92	78	92	87	45	025	008.7	24	02	03	20	.	.	.	02	.	01	17	14	07	.	10	04	.	.	.	.	.	.	07	07
GOD.	6.1	6.8	5.2	5.9	-	08.4	88	62	85	79	30	771	035.0	4.VI	05	17	84	87	30	.	43	06	56	115	167	111	21	149	33	02	.	02	04	01	36	36	51

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dias)	Max	Min	Max	Dat.	Min	Dat.	Cestina pravaca i srednja jačina vetra ND, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
SABAC																												
φ = 44° 46' N λ = 19° 41' E Gr. Δ G = + 1h 19 min.																												BR. ST 171
I	-	-01.0	01.7	-00.2	00.1	02.9	-03.1	11.0	15	-13.0	09	02	01.0	01	02.0	09	01.8	25	02.0	06	01.0	08	01.5	13	02.0	06	02.8	23
II	-	-00.6	04.8	01.1	01.6	06.0	-02.1	-	-	-	-	01	03.0	03	01.7	02	01.5	22	01.8	08	01.0	05	01.0	16	02.1	09	02.8	20
III	-	03.2	09.9	06.0	06.3	11.1	01.9	22.9	25	-05.4	02	09	02.8	02	01.5	10	02.5	19	02.8	05	01.2	09	02.0	14	01.9	04	02.0	21
IV	-	09.1	15.7	11.2	11.8	17.4	06.6	27.5	26	-00.5	04	10	02.5	01	01.0	02	02.0	11	02.7	04	01.8	14	01.9	12	01.4	13	03.8	23
V	-	11.5	18.3	13.4	14.1	19.7	09.2	28.0	10	02.0	02	06	02.0	02	02.5	05	01.4	08	02.4	03	01.0	14	01.9	12	01.6	25	03.0	18
VI	-	17.7	24.8	18.2	19.7	26.0	14.3	31.4	23,17	07.5	03	05	01.8	04	01.5	02	02.0	03	02.3	04	02.0	21	01.8	11	01.6	14	02.0	26
VII	-	17.8	24.8	18.8	20.1	25.7	14.4	33.3	25	1 .5	27,18	04	01.5	06	02.0	02	01.0	05	01.2	03	01.7	04	01.2	12	02.5	11	02.4	46
VIII	-	17.6	26.3	19.1	20.5	26.9	14.7	33.0	07	10.0	28	02	01.0	03	01.3	05	01.2	03	01.7	02	01.5	04	02.0	11	01.3	13	02.3	50
IX	-	11.7	22.1	14.6	15.7	23.0	10.1	36.0	11	-01.7	30	08	01.5	09	01.6	05	02.2	01	02.0	.	.	03	01.7	09	01.0	13	02.4	42
X	-	05.9	15.7	09.3	10.0	16.6	04.7	25.6	09	-01.7	25	09	01.1	05	01.4	06	01.8	04	02.0	.	.	08	01.9	09	01.7	10	01.9	42
XI	-	05.0	12.6	07.4	08.1	13.6	03.6	-	-	-	-	09	01.8	05	01.4	06	01.8	08	01.6	01	01.0	08	02.4	02	01.0	15	02.1	36
XII	-	00.5	03.9	01.5	01.9	05.0	-01.4	17.5	30	-12.2	27	01	01.0	08	02.2	09	01.6	07	02.3	02	01.0	02	03.0	20	01.2	21	01.5	23
GOD.	-	08.2	15.0	10.0	10.8	16.2	06.1	-		-		66	01.9	49	01.7	63	01.8	116	02.1	38	01.4	100	01.9	139	01.7	154	02.4	370
VLADIMIRCI																												
φ = 44° 37' N λ = 19° 47' E Gr. Δ G = + 1h 14 min.																												BR. ST. 172
I	-	-00.7	02.2	00.1	00.4	03.2	-01.9	12.6	15	-08.0	03	01	01.0	.	.	05	02.2	05	03.6	.	.	04	02.8	22	03.1	02	01.0	54
II	-	-00.4	05.0	01.4	01.8	06.0	-01.6	-	-	-	-	.	.	.	.	04	01.0	03	02.7	03	01.3	08	02.4	23	02.5	11	02.9	37
III	-	03.2	09.8	05.8	06.2	10.8	02.3	22.5	25	-03.4	08	03	01.3	01	01.0	19	01.8	04	02.5	03	01.0	06	03.0	29	01.9	08	03.1	20
IV	-	08.7	15.7	11.0	11.6	17.2	06.8	28.5	26	-00.4	04	.	.	01	03.0	07	01.6	04	01.8	.	.	04	01.8	27	02.1	12	03.4	35
V	-	11.5	17.6	13.5	14.0	19.1	09.9	27.0	10	04.0	02,01	01	01.0	.	.	02	01.5	.	.	.	.	02	02.5	36	02.1	07	02.6	45
VI	-	17.8	24.2	19.2	20.1	25.4	14.7	31.0	23	08.4	03	02	02.5	.	.	.	.	.	.	.	.	.	.	24	01.5	06	02.3	58
VII	-	17.6	24.2	19.3	20.1	25.5	14.8	32.0	25,15	10.8	27,18	.	.	.	.	.	.	.	.	01	01.0	02	01.5	20	02.3	04	02.8	66
VIII	-	17.9	26.1	19.4	20.7	27.0	15.3	33.0	07,06	10.0	28,27	.	.	.	.	.	.	.	.	.	.	.	.	13	02.1	03	02.3	77
IX	-	12.5	22.1	15.0	16.1	23.1	10.8	34.8	13	-01.6	29	.	.	01	02.0	.	.	.	.	.	.	.	.	21	01.6	03	02.0	65
X	-	06.9	15.7	09.7	10.5	16.4	05.8	26.0	09	00.4	25	01	01.0	.	.	03	02.0	.	.	.	.	.	.	31	01.8	02	01.0	56
XI	-	06.0	12.4	07.8	08.5	13.3	04.7	-	-	-	-	01	01.0	.	.	02	02.0	01	02.0	01	01.0	.	.	22	01.7	03	03.7	60
XII	-	00.7	04.0	01.8	02.1	05.0	-00.2	19.2	30	-09.0	27	.	.	.	.	05	01.6	05	02.6	.	.	.	.	24	02.0	16	03.4	43
GOD.	-	08.5	14.9	10.3	11.0	16.0	06.8	-		-		09	01.4	03	02.0	47	01.7	22	02.6	08	01.1	26	02.3	292	02.0	77	02.9	611
VALJEVO																												
φ 44° 17' N λ = 19° 55' E Gr. Δ G = + 1h 18 min.																												BR. ST. 173
I	745.4	-00.6	03.0	00.2	00.7	04.8	-02.4	15.6	15	-08.8	03	01	01.0	.	.	03	02.0	01	03.0	01	03.0	01	02.0	11	02.1	05	02.6	70
II	742.4	-01.2	05.2	00.9	01.5	06.6	-03.2	16.9	10,05	-12.4	18	01	02.0	.	.	01	02.0	01	02.0	01	05.0	04	03.5	09	02.0	05	02.6	62
III	743.4	02.9	10.0	05.4	06.0	11.4	01.1	23.0	25	-03.8	09,02	01	03.0	02	01.0	08	02.9	02	02.5	05	02.6	04	03.2	07	01.9	09	02.4	55
IV	744.3	08.9	16.1	10.6	11.5	17.7	05.8	27.7	20	-03.6	05	05	03.4	05	01.4	02	02.5	.	.	.	.	06	03.0	06	02.3	09	02.7	57
V	745.3	11.5	16.7	12.7	13.4	18.6	08.8	28.4	10	02.4	02	05	01.6	02	01.5	05	01.2	03	01.0	.	.	.	.	13	01.8	08	02.6	57
VI	746.4	17.5	23.8	18.0	19.3	25.3	13.7	32.2	17	08.0	06,03	02	01.5	04	01.8	06	01.8	.	.	.	.	02	01.5	06	01.8	02	02.0	68
VII	745.5	18.0	24.3	18.7	19.9	25.8	14.3	33.8	25	08.2	20	04	01.8	03	01.3	08	01.5	01	01.0	.	.	01	02.0	14	02.1	03	02.0	59
VIII	745.4	17.6	25.8	19.2	20.5	26.7	14.5	33.2	07	10.4	29,19	04	01.2	03	01.7	06	01.5	01	01.0	.	.	.	.	05	02.2	05	02.2	69
IX	749.2	12.6	21.7	14.5	15.8	23.0	09.9	33.3	11	-02.2	30	07	01.9	02	01.5	05	01.4	01	01.0	.	.	.	.	05	02.0	01	01.0	69
X	749.3	06.1	15.7	08.7	09.8	16.4	04.2	25.3	11	-01.3	20	02	01.0	01	02.0	05	01.4	.	.	.	.	03	03.0	08	02.0	03	02.7	71
XI	747.7	05.0	13.0	07.0	08.0	14.1	02.9	22.7	03	-02.6	12	01	01.0	.	.	.	.	01	03.0	04	01.7	02	02.5	05	02.2	04	01.8	69
XII	750.2	00.4	05.0	01.4	02.1	05.9	-01.5	20.1	30	-11.8	27	03	01.7	.	.	02	01.5	01	04.0	03	03.3	.	.	09	01.6	07	02.6	68
GOD.	746.2	08.2	15.0	09.8	10.7	16.4	05.7	33.8	15.VII	-12.4	48.II	36	01.9	22	01.5	51	01.8	12	01.9	16	02.6	23	03.1	98	02.0	63	02.4	774
BEOGRAD																												
φ = 44° 48' N λ = 20° 28' E Gr. Δ G = + 1h 22 min.																												BR. ST. 174
I	749.6	00.1	02.6	01.1	01.2	03.9	-01.4	15.1	15	-09.0	22	03	02.0	03	01.3	04	02.5	37	03.1	09	02.6	.	.	16	02.0	16	02.1	07
II	746.3	00.7	04.8	02.3	02.5	06.3	-00.6	18.3	05	-06.5	03	08	01.6	03	02.0	01	03.0	24	02.2	13	02.8	04	02.0	16	02.1	15	02.1	.
III	747.4	04.2	09.6	06.3	06.6	11.1	03.1	23.5	25	-04.0	02	04	02.5	05	02.0	05	03.2	30	02.9	12	02.4	08	01.9	18	02.0	11	02.4	.
IV	748.2	10.6	15.9	12.0	12.6	17.8	08.0	27.9	26	00.3	04	09	02.4	06	01.7	02	02.0	24	02.4	10	02.3	03	02.3	12	01.9	10	02.3	06
V	749.0	12.5	18.4	13.8	14.6	19.5	10.3	28.1	10	04.0	02	09	02.3	05	02.0	03	01.3	15	01.8	05	02.8	12	01.8	21	02.0	10	02.2	05
VI	750.2	18.5	24.0	19.2	20.2	25.6	15.6	30.7	17	09.0	03	07	02.1	02	02.5	06	02.7	18	02.0	05	02.8	11	01.6	22	02.0	12	02.0	07
VII	749.3	19.0	24.6	19.7	20.8	26.1	15.9	32.2	25,23	11.0	18	12	01.9	03	01.3	09	02.0	13	02.2	08	01.6	02	01.0	24	02.1	16	02.0	06
VIII	749.3	18.9	25.8	20.1	21.2	27.0	16.4	33.0	07	10.7	27	05	01.6	02	02.0	14	01.9	30	02.2	03	02.0	06	01.2	11	01.9	15	01.9	07
IX	753.1	13.9	21.8	15.4	16.6	23.0	12.1	34.0	11	0.6	29	10	01.6	04	01.2	04	01.8	18	02.0	05	02.0	06	01.7	20	01.6	16	01.8	07
X	753.3	08.2	15.6	10.4	11.1	16.5	07.0	25.2	07	-00.6	25	07	01.9	03	02.3	08	02.4	26	02.0	07	02.1	05	01.8	15	02.1	16	01.9	06
XI	751.7	07.3	12.9	08.8	09.5	13.9	05.9	23.3	03	00.3	26	01	01.0	02	02.0	03	01.3	30	01.9	14	02.4	06	01.7	18	01.8	11	01.7	05
XII	754.4	01.5	04.2	02.4	02.6	05.2	00.5	17.3	30	-05.8	27,26	05	01.8	04	02.8	06	02.2	20	02.6	01	02.0	05	01.6	25	01.8	10	01.6	08
GOD.	750.2	09.6	15.0	11.0	11.6	16.3	07.7	34.0	11.IX	-09.0	11.I	80	01.9	42	01.9	65	02.2	285	02.3	92	02.2	68	01.7	218	01.9	182	02.0	64
GORNJI MILANOVAC																												
φ = 44° 02' N λ = 20° 29' E Gr. Δ G = + 1h 22 min.																												BR. ST 175
I	-	-02.2	02.2	-01.1	-00.5	03.6	-04.3	15.0	16	-13.2	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-02.2	03.9	-00.3	00.3	05.7	-04.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	01.1	10.2	04.0	04.8	11.1	-00.7	22.4	25	-07.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	06.6	16.8	09.0	10.4	18.3	03.4	27.2	26,20	-05.6	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	09.2	16.4	10.5	11.6	17.9	06.5	28.8	11	01.2	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	14.5	23.7	15.4	17.2	24.8	11.4	31.2	17	04.5	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	15.4	24.4	16.6	18.2	25.3	12.3	32.2	25	06.8	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	15.3	25.0	16.5	18.3	26.2	12.1	32.7	07	07.4	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	10.4	21.7	11.9	14.0	22.4	07.8	32.9	11	-05.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	05.3	15.2	06.7	08.5	16.2	02.7	25.0	08	-03.0	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	02.5	12.2	04.6	06.0	13.6	00.4	23.9	01	-05.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-00.7	04.4	00.2	01.0	05.6	-03.0	19.4	30	-11.6	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	06.3	14.7	07.8	09.2	15.9	03.7	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana s: Tn ≤ -20.0	Tx ≤ 0.0	Tn < 0.0	Tx < 25.0	Tx ≥ 30.0	Tn ≥ 20.0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 3.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	✱	✱	♨	∽	▲	▲	R T	≡	▥
BR. ST. 171						**SABAC**																															
																																					H_s = 80 m H_b = - m h_1 = 2.0 m h_2 = 1.0 m
I	9.2	8.1	7.9	8.4	-	04.1	89	84	88	87	57	051	013.9	08	02	07	22	.	.	.	.	.	01	22	14	12	02	12	08	04	.	.	.	.	.	07	24
II	7.7	7.1	7.8	7.5	-	04.4	88	73	87	82	-	093	021.6	12	-	-	-	-	-	-	.	.	02	13	18	11	03	09	10	.	.	.	.	.	05	16
III	6.3	7.0	5.9	6.4	-	05.3	83	61	78	74	31	061	017.3	15	.	.	08	.	.	.	02	01	04	13	15	09	02	13	06	04	.	.	.	.	.	01	02
IV	5.5	6.6	6.2	6.1	-	07.5	79	58	75	70	30	061	016.8	15	.	.	01	03	.	.	07	02	04	10	14	09	02	14	.	.	.	.	.	.	01	.	.
V	6.8	7.1	6.8	6.9	-	09.4	87	61	83	77	41	125	024.9	23	.	.	.	04	.	.	06	01	01	12	19	15	05	19	.	.	.	.	.	.	05	.	.
VI	4.4	4.9	5.9	5.1	-	13.7	86	61	86	77	44	071	020.0	19	.	.	.	22	04	.	03	01	04	05	20	12	02	20	.	.	.	.	.	.	07	.	.
VII	4.0	4.7	3.5	4.1	-	14.0	87	62	86	78	44	093	030.1	06	.	.	.	19	09	.	01	01	12	07	07	07	03	07	.	.	.	.	.	.	-	.	.
VIII	2.6	3.8	2.8	3.1	-	14.7	91	60	89	80	48	039	020.6	18	.	.	.	23	07	.	01	01	14	03	10	06	01	10	.	.	.	.	.	.	06	02	.
IX	4.5	4.2	3.1	3.9	-	11.0	93	58	88	80	34	026	004.9	01	.	.	02	11	06	.	02	01	12	05	11	08	.	11	.	.	.	.	.	.	01	04	.
X	4.8	4.8	4.8	5.2	-	07.5	91	62	86	80	36	065	020.5	02	.	.	01	03	.	.	.	.	08	10	09	06	03	09	.	.	.	.	.	.	.	04	.
XI	6.3	5.9	6.7	6.3	-	06.5	89	65	84	80	-	051	014.0	17	-	-	-	-	-	-	01	.	05	13	14	08	02	14	.	.	.	.	.	.	.	03	.
XII	7.5	7.8	7.0	7.5	-	04.6	90	79	88	86	54	025	006.5	24	01	04	21	.	.	.	02	01	02	18	14	08	.	11	03	.	.	.	.	.	.	06	06
GOD.	5.8	6.0	5.8	5.9	-	08.6	87	65	84	79	-	757	030.1	6.VII	-	-	-	-	-	-	25	09	69	131	165	111	25	149	27	08	.	.	.	.	-	32	48
BR. ST. 172						**VLADIMIRCI**																															
																																					H_s = 120 m H_b = - m h_1 = 2.0 m h_2 = 1.0 m
I	8.7	7.4	8.2	8.1	-	04.3	91	86	90	89	65	-	-	-	.	08	21	.	.	.	01	.	.	20	-	-	-	-	-	-	.	.	.	.	.	06	-
II	7.4	6.1	6.6	6.7	-	04.5	90	76	85	84	-	102	021.6	12	-	-	-	-	-	-	.	.	.	10	15	11	04	06	10	.	.	.	.	.	02	10
III	6.6	5.3	5.9	5.9	-	05.3	80	63	79	74	31	076	017.5	15	.	01	06	.	.	.	.	.	07	12	13	13	03	11	01	.	.	.	.	.	.	.	01
IV	-	-	-	-	-	07.2	77	56	75	69	32	058	017.0	15	.	.	01	04	.	.	01	.	-	-	12	09	02	12	.	.	.	.	.	.	.	.	.
V	6.4	6.2	6.5	6.4	-	09.4	84	66	83	78	41	139	022.2	19	.	.	.	04	.	.	.	.	05	13	18	17	06	18	.	.	.	.	.	.	02	.	.
VI	-	-	-	-	-	13.4	81	62	81	75	45	098	027.2	19	.	.	.	21	03	.	.	.	-	-	13	11	04	13	.	.	.	.	.	.	-	.	.
VII	-	-	-	-	-	13.7	84	63	85	77	35	111	049.5	06	.	.	.	19	09	.	.	.	-	-	08	08	03	08	.	.	.	.	.	.	-	.	.
VIII	-	-	-	-	-	13.7	82	57	82	74	35	041	012.2	10	.	.	.	20	08	01	.	.	-	-	06	06	02	06	.	.	.	.	.	.	01	.	.
IX	4.3	3.1	2.4	3.2	-	10.6	87	56	83	75	28	024	007.0	17	.	.	02	10	05	.	.	.	15	05	09	07	.	09	.	.	.	.	.	.	.	.	.
X	4.7	4.6	3.7	4.4	-	07.6	87	64	83	78	43	088	031.0	23	.	.	.	03	.	.	.	.	10	07	08	07	04	08	.	.	.	.	.	.	.	01	.
XI	5.7	5.1	5.4	5.4	-	06.4	83	65	82	77	-	044	013.0	11	-	-	-	-	-	-	.	.	09	11	10	08	01	10	.	.	.	.	.	.	.	05	.
XII	7.1	6.5	6.2	6.6	-	04.6	88	79	87	85	46	019	004.2	23	.	03	17	.	.	.	02	01	03	11	10	07	.	06	04	.	.	.	.	.	.	12	04
GOD.	-	-	-	-	-	08.4	84	66	82	77	-	-	-		-	-	-	-	-	-	04	01	-	-	-	-	-	-	-	-	.	.	.	.	-	26	-
BR. ST. 173						**VALJEVO**																															
																																					H_s = 174 m H_b = 176.1 m h_1 = 2.0 m h_2 = 1.3 m
I	8.9	8.4	7.3	8.2		039.2	04.2	88	75	87	84	50	055	014.6	02	.	06	22	.	.	.	01	.	02	20	20	08	02	16	09	03	.	01	.	.	.	03	16
II	8.1	8.0	7.1	7.7		066.1	04.1	87	67	85	80	34	096	017.0	19	02	03	21	.	.	.	03	.	.	15	16	12	06	09	11	02	.	.	.	.	.	04	17
III	8.3	7.1	5.5	7.0		125.3	05.0	82	56	78	72	26	088	025.0	28	.	01	12	.	.	.	04	01	01	13	15	12	02	13	06	04	.	.	.	.	01	01	02
IV	6.8	7.2	5.5	6.5		162.2	06.7	78	48	73	66	22	081	024.2	15	.	.	03	03	.	.	05	.	.	10	14	10	03	14	.	.	.	.	.	.	01	.	.
V	7.1	8.1	6.6	7.3		158.9	08.6	81	60	82	74	34	185	030.8	19	.	.	.	04	.	.	02	.	01	14	21	19	05	21	.	.	.	.	.	01	08	01	.
VI	5.0	6.0	5.0	5.4		229.3	13.0	82	60	86	76	38	147	026.0	15	.	.	.	18	03	.	05	01	03	04	18	15	05	18	.	.	.	.	03	11	01	.
VII	4.5	5.0	4.0	4.5		254.0	13.2	82	56	87	75	34	096	035.0	06	.	.	.	19	08	.	01	.	10	08	09	09	04	09	.	.	.	.	.	.	05	.	.
VIII	3.3	5.0	3.0	3.8		263.6	13.9	87	55	88	77	35	076	035.4	09	.	.	.	21	08	01	01	.	11	05	09	09	02	09	.	.	.	.	.	.	07	01	.
IX	5.0	5.5	3.6	4.7		198.2	10.4	90	50	88	76	26	032	006.7	01	.	.	01	12	05	.	.	.	08	06	11	09	.	11	.	.	.	.	.	.	02	02	.
X	5.6	5.7	5.2	5.5		159.7	07.0	90	55	89	78	20	090	028.1	23	.	.	01	02	.	.	01	.	09	12	11	09	04	11	.	.	.	.	.	.	.	01	.
XI	6.8	7.0	5.1	6.3		111.4	06.0	89	58	84	77	28	052	014.0	11	.	.	06	.	.	.	.	.	04	09	10	07	02	10	.	.	.	.	.	.	.	04	.
XII	7.7	7.3	7.5	7.5		074.8	04.4	88	68	87	81	37	012	003.2	04	01	02	18	.	.	.	04	.	03	20	07	05	.	03	04	.	.	.	.	.	.	02	05
GOD.	6.4	6.7	5.4	6.2		1842.7	08.0	85	59	84	76	20	1010	035.4	9.VIII	03	12	84	79	24	01	27	02	52	136	161	124	35	144	30	09	.	01	.	04	35	20	40
BR. ST. 174						**BEOGRAD**																															
																																					H_s = 132 m H_b = 131.6 m h_1 = 2.0 m h_2 = 1.2 m
I	8.3	8.2	7.5	8.0		042.3	04.2	83	75	82	80	60	047	015.6	08	.	06	19	.	.	.	12	03	01	20	18	08	02	16	09	04	.	01	.	.	.	06	21
II	7.6	7.7	7.5	7.6		064.2	04.3	83	69	80	77	33	097	019.9	12	.	04	16	.	.	.	05	.	00	13	17	13	02	08	16	03	02	.	.	.	.	02	16
III	7.5	7.2	5.6	6.8		113.9	04.8	75	54	72	67	22	076	033.8	15	.	01	05	.	.	.	10	03	02	12	14	11	01	12	03	01	.	.	01	.	.	01	02
IV	5.7	6.4	5.6	5.9		180.4	06.7	68	50	64	61	23	064	020.1	15	.	.	.	.	.	.	18	04	.	.	10	10	02	10	.	.	.	.	.	.	02	.	.
V	6.3	7.1	6.2	6.5		168.1	08.8	79	55	77	70	31	103	024.6	23	.	.	.	.	.	.	16	04	02	10	20	17	02	20	.	.	.	.	.	01	10	01	.
VI	4.8	5.0	4.4	4.7		247.9	12.6	77	58	76	70	41	088	019.5	19	.	.	.	21	04	.	14	02	04	03	17	15	03	17	.	.	.	.	.	.	07	02	.
VII	4.5	5.0	3.0	4.2		255.0	13.2	78	58	78	71	40	134	040.7	06	.	.	.	21	10	01	11	01	10	06	11	09	04	11	.	.	.	.	.	.	06	.	.
VIII	4.0	4.5	2.8	3.8		256.8	13.3	79	54	78	70	39	042	014.9	26	.	.	.	19	08	01	11	01	13	03	09	05	01	09	.	.	.	.	.	.	06	.	.
IX	4.5	4.4	3.9	4.3		186.2	10.3	84	51	78	71	31	007	002.7	17	.	.	.	11	04	01	05	.	12	06	10	02	.	10	.	.	.	.	.	.	02	.	.
X	5.3	4.9	5.0	5.1		159.8	07.3	85	56	79	73	34	067	020.3	23	.	.	.	01	.	.	10	.	08	10	09	07	04	09	.	.	.	.	.	.	.	02	.
XI	6.6	6.1	6.0	6.2		110.1	06.4	79	62	78	73	31	062	012.2	24	.	.	.	.	.	.	07	.	04	09	13	09	02	13	.	.	.	.	.	.	.	01	.
XII	7.5	7.7	7.3	7.5		047.8	04.7	86	76	85	82	48	023	008.2	26	.	03	16	.	.	.	09	03	03	17	20	06	.	13	09	01	.	.	01	.	.	03	05
GOD.	6.0	6.2	5.4	5.9		1832.5	08.0	79	59	77	72	22	810	040.7	6.VII	.	14	56	73	26	03	128	21	59	109	168	112	23	148	37	09	02	01	02	01	33	18	44
BR. ST. 175						**GORNJI MILANOVAC**																															
																																					H_s = 330 m H_b = - m h_1 = 2.0 m h_2 = 1.0 m
I	7.4	6.1	6.6	6.7		-	-	-	-	-	-	66	061	013.4	17	04	07	25	.	.	.	.	.	01	14	15	11	02	08	09	.	.	.	.	.	.	02	19
II	7.0	7.0	6.1	6.7		-	-	-	-	-	-	-	082	012.5	24	-	-	-	-	-	-	.	.	03	13	16	15	02	06	11	01	.	.	.	.	.	04	16
III	-	-	-	-		-	-	-	-	-	-	-	070	016.8	28	.	01	15	.	.	.	.	.	-	-	14	10	03	12	03	.	.	.	.	.	.	.	03
IV	-	-	-	-		-	-	-	-	-	-	26	069	020.7	15	.	.	05	05	.	.	.	.	-	-	12	09	03	12	01	.	.	.	.	.	.	02	.
V	-	-	-	-		-	-	-	-	-	-	34	159	024.5	23	.	.	.	02	.	.	.	.	-	-	23	22	06	23	02	02	.	.	.	.	-	03	.
VI	-	-	-	-		-	-	-	-	-	-	45	107	019.0	15	.	.	.	20	03	.	01	.	-	-	19	14	05	19	.	.	.	.	.	.	04	.	.
VII	-	-	-	-		-	-	-	-	-	-	38	060	017.7	06	.	.	.	20	06	.	01	.	-	-	10	10	02	10	.	.	.	.	.	.	02	04	.
VIII	-	-	-	-		-	-	-	-	-	-	39	136	057.9	03	.	.	.	20	06	.	.	.	-	-	12	11	04	12	.	.	.	.	.	01	-	.	.
IX	-	-	-	-		-	-	-	-	-	-	31	014	003.8	21	.	.	03	11	05	.	.	.	-	-	10	07	.	10	.	.	.	.	.	.	.	01	.
X	-	-	-	-		-	-	-	-	-	-	33	094	035.4	23	.	.	05	01	.	.	.	.	-	-	12	10	04	12	02	02	.	.	.	.	.	04	01
XI	-	-	-	-		-	-	-	-	-	-	-	067	013.0	24	.	.	14	.	.	.	.	.	-	-	10	10	03	10	.	.	.	.	.	.	.	07	.
XII	-	-	-	-		-	-	-	-	-	-	-	029	006.0	04	03	05	26	.	.	.	.	.	-	-	15	10	.	08	08	.	.	.	.	.	.	05	06
GOD.	-	-	-	-		-	-	-	-	-	-	-	948	057.9	3.VIII	-	-	-	-	-	-	02	.	-	-	168	139	34	142	36	05	.	.	.	01	-	32	45

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dias)	Max	Min	Max	Dat.	Min	Dat.	Učestalost pravca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W j.	NW č.	NW j.	C č.
RUDNIK φ = 44° 08' N λ = 20° 31' E Gr. Δ G = + 1h 21 min.																											BR. ST 176
I	-	-00.4	01.1	-00.3	00.0	03.0	-	14.4	12	-	-	15	01.7	04	02.0	04	02.2	09	02.6	09	02.9	26	02.5	13	01.7	13	1.8
II	-	-01.3	01.4	-00.6	-00.2	03.7	-	-	-	-	-	26	01.9	03	02.0	.	.	04	02.2	07	02.6	26	02.7	09	01.8	09	02.1
III	-	01.2	05.6	03.3	03.4	07.3	-	18.6	24	-	-	21	01.9	03	02.0	02	02.5	15	04.0	05	01.6	19	02.5	25	01.5	03	02.0
IV	-	07.6	12.7	08.2	09.2	14.8	-	25.1	24	-	-	11	02.0	.	.	03	01.7	16	02.2	05	01.2	20	01.9	27	01.7	08	02.1
V	-	08.9	13.1	10.1	10.5	14.8	-	26.3	11	-	-	16	01.6	02	01.5	01	05.0	05	01.8	09	01.4	12	01.8	32	01.4	16	01.8
VI	-	15.7	19.9	16.3	17.0	22.1	12.4	28.3	18,17	04.0	03	03	01.3	01	01.0	02	01.5	05	01.8	09	01.3	20	01.4	42	01.4	08	01.6
VII	-	15.7	19.4	16.4	17.0	22.0	13.0	28.4	25	06.2	20,19	19	01.3	03	02.0	02	01.5	01	02.0	09	01.4	12	01.4	36	01.2	11	01.3
VIII	-	17.1	21.6	17.6	18.4	23.6	14.4	29.5	07	09.4	25	04	01.2	07	01.9	.	.	03	01.3	14	01.1	14	01.6	37	01.3	12	01.8
IX	-	12.2	17.5	14.0	14.4	19.9	10.4	29.8	12	-04.5	30	21	01.5	11	01.8	06	01.3	01	03.0	22	01.6	08	01.5	12	01.3	09	01.7
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	05.7	08.6	06.8	07.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-00.4	01.9	00.6	00.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-				-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BUKOVIČKA BANJA φ = 44° 18' N λ = 20° 33' E Gr. Δ G = + 1h 22 min.																											BR. ST. 177
I	-	-00.5	02.9	00.4	00.8	04.8	-03.5	15.2	15	-11.2	03	02	02.0	06	02.2	11	02.4	24	02.2	11	02.3	05	03.0	12	04.4	22	03.5
II	-	00.0	04.9	01.2	01.8	06.5	-03.4	-	-	-	-	05	02.8	02	01.5	10	01.8	13	02.2	05	02.6	11	04.1	12	04.3	23	03.4
III	-	03.2	09.2	04.7	05.4	10.8	00.5	24.5	25	-07.0	08	09	01.7	06	02.7	07	02.7	12	02.8	07	02.4	06	02.5	14	04.1	32	03.3
IV	-	10.0	15.7	10.0	11.4	18.0	04.9	28.0	26	-02.5	05	11	02.4	03	01.3	08	02.0	12	01.9	09	02.7	10	02.6	07	04.1	27	04.0
V	-	11.4	17.1	11.9	13.1	18.6	07.7	29.1	10	02.0	02	06	01.7	09	01.9	06	01.5	04	01.5	01	02.0	02	02.0	29	03.5	36	03.7
VI	-	17.8	23.5	17.2	18.9	25.2	12.8	31.2	10	07.0	04	05	02.8	09	02.3	09	01.6	10	01.8	04	01.8	05	03.4	23	03.3	25	03.3
VII	-	18.4	23.9	17.9	19.5	25.7	13.5	33.7	25	08.9	19	06	02.0	07	01.9	08	01.8	08	01.9	01	02.0	09	02.4	19	03.8	35	03.2
VIII	-	17.4	25.1	17.6	19.4	26.6	13.0	33.3	07	08.8	14	06	01.7	07	01.7	12	01.5	17	01.6	04	01.8	01	04.0	17	03.0	22	03.1
IX	-	13.0	21.4	13.1	15.1	22.7	08.8	34.2	11	-03.5	30	10	02.3	05	02.4	09	01.9	10	01.4	04	01.2	.	.	16	03.2	35	03.0
X	-	08.8	15.0	08.4	09.7	16.2	03.9	25.4	07	-01.1	17	07	01.9	11	02.0	13	01.6	05	02.2	08	01.9	06	01.7	14	03.7	28	03.2
XI	-	06.2	12.9	06.9	08.2	14.1	02.7	-	-	-	-	08	02.0	03	01.0	10	01.5	11	01.9	07	02.0	11	03.0	19	03.1	18	03.6
XII	-	00.5	04.2	01.6	02.0	05.5	-02.1	19.6	30	-11.8	27	07	02.3	06	01.8	09	02.0	15	01.9	08	01.9	.	.	19	03.4	28	03.5
GOD.	-	08.7	14.6	09.2	10.4	16.2	04.9	-		-		82	02.1	74	02.0	112	01.8	141	02.0	69	02.1	66	02.9	201	03.6	331	03.4
PANČEVO φ = 44° 53' N λ = 20° 40' E Gr. Δ G = + 1h 22 min.																											BR. ST. 178
I	-	-01.3	01.7	-00.2	00.0	03.0	-02.9	13.6	15	-12.5	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-00.5	03.9	01.1	01.4	05.5	-02.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	09.4	16.0	11.1	11.9	17.8	06.8	27.0	26	-01.7	05	04	03.2	02	02.0	04	02.8	15	02.9	07	02.4	02	02.5	13	02.2	19	02.4
V	-	12.9	18.3	13.6	14.6	19.8	10.0	27.4	10	05.0	02	07	02.9	.	.	01	02.0	04	02.0	07	01.6	04	01.8	23	02.3	21	02.7
VI	-	18.4	24.1	19.0	20.1	25.6	15.2	31.0	17	09.6	03	02	03.0	01	02.0	07	02.4	09	02.1	04	02.2	01	03.0	18	02.3	12	03.1
VII	-	18.6	24.7	19.4	20.5	26.0	15.4	32.4	24	10.2	21,20	05	02.2	01	03.0	01	02.0	10	02.1	03	02.0	.	.	20	02.7	13	02.8
VIII	-	17.8	25.5	19.1	20.4	26.7	15.1	32.2	07	10.2	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	12.6	21.7	15.0	16.1	22.7	11.0	33.1	12	01.0	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	06.7	15.4	09.2	10.1	16.2	05.7	26.4	11	00.5	27	05	02.0	01	02.0	13	02.3	16	02.2	03	01.0	.	.	21	02.9	10	02.5
XI	-	-	-	-	-	-	-	-	-	-	-	03	02.3	.	.	10	02.3	26	02.3	03	02.7	.	.	16	02.5	10	02.7
XII	-	00.5	03.3	01.4	01.6	04.2	-01.3	12.8	01	-10.8	26	14	02.4	02	02.5	07	03.4	12	03.2	01	02.0	.	.	11	03.2	05	03.0
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SMEDEREVO φ = 44° 39' N λ = 20° 54' E Gr. Δ G = + 1h 24 min.																											BR. ST. 179
I	-	00.1	02.7	00.5	00.9	04.1	-02.3	14.0	15	-11.0	22,21	16	01.4	.	.	12	02.6	08	02.8	20	02.4	.	.	.	.	.	.
II	-	00.9	04.8	02.2	02.5	06.1	-01.1	-	-	-	-	16	01.6	.	.	.	.	06	02.8	23	02.2	.	.	.	.	.	.
III	-	03.5	09.7	05.6	06.1	11.2	02.0	23.5	25	-04.0	08	19	01.7	.	.	13	02.8	07	02.7	19	01.9	.	.	.	.	.	.
IV	-	09.4	16.3	11.0	11.9	17.9	07.1	28.0	26	-00.5	04	15	01.9	.	.	02	02.5	09	02.7	25	01.8	.	.	.	.	.	.
V	-	12.3	18.3	12.9	14.1	19.3	10.0	28.2	10	04.0	02	21	02.0	.	.	.	.	01	03.0	14	01.7	.	.	.	.	.	.
VI	-	17.9	24.1	18.2	19.6	25.2	14.5	31.0	17	09.5	03	18	01.8	.	.	.	.	02	02.0	13	01.8	.	.	.	.	.	.
VII	-	18.6	24.4	18.8	20.1	25.7	15.1	32.0	25	10.0	20	24	01.8	01	01.0	01	02.0	07	02.1	03	01.3	.	.	.	.	.	.
VIII	-	18.4	25.7	18.9	20.5	26.9	15.1	32.8	07	10.5	27	12	01.8	01	01.0	.	.	06	02.0	04	01.2	.	.	.	.	.	.
IX	-	13.0	22.0	14.5	16.0	23.0	10.6	33.0	11	-02.8	29	15	01.7	.	.	.	.	06	02.2	02	02.0	.	.	.	.	.	.
X	-	08.0	15.6	09.6	10.7	16.2	06.1	25.0	09	-01.5	25	18	01.4	.	.	03	02.7	07	02.6	06	02.2	.	.	.	.	.	.
XI	-	06.3	12.8	07.7	08.6	13.3	03.7	-	-	-	-	18	01.6	.	.	.	.	06	02.5	12	02.2	.	.	.	.	.	.
XII	-	01.3	04.4	02.1	02.5	05.1	-00.7	18.0	30	-10.0	27	16	01.6	.	.	.	.	03	02.0	09	02.0	.	.	.	.	.	.
GOD.	-	09.1	15.1	10.2	11.1	16.2	06.7	-		-		208	01.7	02	01.0	31	02.7	68	02.5	150	02.0	.	.	.	.	.	636
KRAGUJEVAC φ = 44° 02' N λ = 20° 56' E Gr. Δ G = + 1h 24 min.																											BR. ST 180
I	-	-00.1	03.0	01.2	01.3	04.5	-01.8	15.6	15	-11.5	22	09	01.6	02	01.0	.	.	12	02.2	08	02.9	15	01.9	04	01.0	12	02.4
II	-	-00.5	04.4	01.4	01.7	06.3	-02.2	16.2	10	-12.1	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	03.2	10.0	05.6	06.1	11.3	01.7	24.0	25	-03.4	02	08	01.8	06	01.7	.	.	13	02.5	11	02.1	14	01.8	02	01.0	07	02.3
IV	-	09.6	16.3	10.8	11.9	18.2	06.1	27.6	26	-02.8	05	10	01.8	02	01.0	01	02.0	05	02.8	13	01.8	06	01.5	03	01.3	14	02.6
V	-	12.0	17.3	12.7	13.7	18.6	08.9	29.5	11	02.7	03	05	02.0	.	.	.	.	02	04.0	06	01.5	09	01.9	10	02.2	17	02.5
VI	-	17.5	23.9	17.6	19.1	24.7	13.9	30.4	17	08.5	06	04	02.0	.	.	.	.	01	02.0	03	02.0	14	01.6	02	01.5	08	02.4
VII	-	18.2	24.7	18.6	20.0	25.6	14.4	31.6	24,22	09.6	20	11	02.1	01	02.0	.	.	04	02.2	04	01.8	10	02.0	04	02.0	05	02.6
VIII	-	17.6	25.5	18.5	20.0	26.6	13.8	32.0	07	09.0	27	07	01.9	.	.	01	02.0	04	02.2	07	02.5	05	02.2	02	01.0	08	02.4
IX	-	12.6	21.8	13.9	15.6	22.6	10.3	33.6	12	-02.0	29	06	01.7	01	02.0	.	.	03	01.0	04	01.2	03	01.3	.	.	09	02.0
X	-	07.2	15.4	09.2	10.2	16.5	05.5	25.2	08	-00.8	25	09	01.8	02	01.5	.	.	.	.	07	01.6	07	01.3	01	01.0	11	02.6
XI	-	05.5	12.6	07.0	08.0	13.8	03.6	22.0	01	-02.4	29	05	01.4	02	01.0	.	.	05	02.4	07	01.4	17	01.5	01	02.0	10	02.0
XII	-	00.8	05.1	02.0	02.5	06.2	-01.0	20.8	30	-06.4	27,26	04	01.2	04	01.0	.	.	02	04.0	08	01.9	13	01.6	.	.	18	02.3
GOD.	-	08.6	15.0	09.9	10.8	16.2	06.1	33.6	12.IX	-12.1	3. II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlas)	Insolacija broj sati	Vlažnost vazduha p_m mm	Um % 7	14	21	Sred. (Dlas)	Min	Padavine R mm Σ	Max	Dat.	Broj dana n a: Tn ≤0,0	Tx ≤0,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) ≤2,0	≥8,0	R mm ≥0,1	≥1,0	≥10,0	●	☀	☁	≈	▲	▲	R T	≡	▦
BR. ST. 176						RUDNIK																														
																																				H_s = 700 m H_b = - m h_b = 2,0 m h_r = 1,0 m
I	8.3	7.8	6.9	7.7	-	-	-	-	-	-	-	065	011.6	02	-	11	-	.	.	-	.	.	02	16	16	13	01	09	10	01	.	.	.	.	10	24
II	7.5	7.0	7.3	7.3	-	-	-	-	-	-	-	119	014.2	19	-	-	-	-	-	-	.	.	.	12	19	16	07	05	14	.	.	.	.	.	15	22
III	7.3	7.0	6.0	6.8	-	-	-	-	-	-	-	103	023.6	28	-	03	-	.	.	-	02	01	.	13	15	12	03	11	10	05	.	.	.	.	07	10
IV	6.3	5.8	5.4	5.8	-	06.3	74	64	74	71	21	091	031.2	15	-	.	-	01	.	-	.	.	01	09	13	12	03	11	04	01	.	.	.	.	05	-
V	7.0	6.7	6.2	6.6	-	-	-	-	-	-	-	213	034.2	19	-	.	-	02	.	-	.	.	.	11	23	22	07	20	04	.	.	.	.	.	13	03
VI	5.3	5.4	4.7	5.1	-	-	-	-	-	-	-	110	032.0	18	.	.	.	12	.	.	.	.	.	05	17	17	03	17	.	.	.	.	.	01	-	05	.
VII	4.9	5.8	4.6	5.1	-	-	-	-	-	-	-	095	029.4	06	.	.	.	08	.	03	.	.	02	07	12	11	03	12	.	.	.	.	.	.	-	09	.
VIII	4.0	5.1	3.8	4.3	-	-	-	-	-	-	-	098	036.4	09	.	.	.	14	.	01	.	.	03	02	12	11	02	12	.	.	.	.	.	.	03	05	.
IX	5.5	5.2	4.1	4.9	-	10.1	85	72	80	79	41	021	004.6	19	.	.	02	07	.	.	.	.	04	06	09	08	.	09	.	.	.	.	.	.	.	05	.
X	6.1	6.3	6.1	6.1	-	-	-	-	-	-	-	110	025.8	23	-	-	-	-	-	-	.	.	-	-	14	13	04	13	03	.	.	.	.	.	.	12	03
XI	6.4	5.9	5.1	5.8	-	-	-	-	-	-	-	064	021.2	24	-	-	-	-	-	-	.	.	.	08	12	10	01	12	02	02	.	.	.	.	.	12	-
XII	7.5	8.2	7.5	7.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	01	16	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	6.3	6.4	5.6	6.1	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 177						BUKOVIČKA BANJA																														
																																				H_s = 265 m H_b = - m h_b = 2,0 m h_r = 1,5 m
I	9.5	8.4	7.9	8.6	-	-	-	-	-	-	-	038	007.2	02	03	06	24	.	.	.	04	.	.	23	16	09	.	12	09	02	.	.	.	.	.	-	-
II	8.5	8.2	7.8	8.2	-	-	-	-	-	-	-	093	018.6	19	-	-	-	-	-	-	07	.	.	17	19	11	05	10	11	01	.	.	.	.	.	-	-
III	8.3	7.6	6.1	7.3	-	-	-	-	-	-	-	086	018.5	16	.	01	15	.	.	.	04	.	01	13	16	09	04	11	09	01	01	.	.	.	.	-	03
IV	7.3	7.5	5.6	6.8	-	06.3	67	48	70	62	18	062	016.2	15	.	.	03	04	.	.	05	.	03	14	12	10	03	12	.	.	.	.	.	.	01	-	.
V	7.4	7.7	7.3	7.5	-	08.6	83	60	84	76	30	177	035.2	23	.	.	.	04	.	.	06	01	.	14	23	21	04	23	.	.	.	.	.	01	07	-	.
VI	5.8	6.3	5.9	6.0	-	12.3	78	60	83	73	38	157	030.2	01	.	.	.	20	03	.	02	02	02	09	16	12	06	16	.	.	.	.	.	.	09	-	.
VII	4.4	6.0	4.6	5.0	-	13.1	79	61	87	76	30	062	014.0	06	.	.	.	20	08	.	05	01	07	07	12	09	02	12	.	.	.	.	.	.	05	-	.
VIII	4.3	5.8	3.9	4.7	-	13.2	86	55	89	77	36	073	036.5	03	.	.	.	20	08	.	02	.	07	04	12	09	01	12	.	.	.	.	.	01	06	-	.
IX	5.3	5.4	4.2	5.0	-	09.8	84	52	87	74	21	014	002.9	06	.	.	02	10	06	.	02	.	07	08	09	05	.	09	.	.	.	.	.	.	02	-	.
X	6.3	5.8	5.3	5.8	-	07.1	89	60	86	78	30	065	016.0	23	.	.	02	03	.	.	.	.	08	14	09	07	04	09	01	.	.	.	.	.	.	-	.
XI	7.7	6.7	5.3	6.6	-	06.1	84	60	82	75	-	056	016.9	23	-	-	-	-	-	-	02	.	02	12	13	08	02	13	.	.	.	.	.	.	.	-	.
XII	8.6	7.7	7.9	8.1	-	-	-	-	-	-	-	018	006.0	26	02	04	20	.	.	.	02	.	02	21	16	04	.	10	07	.	.	.	.	.	.	-	05
GOD.	7.0	6.9	6.0	6.6	-	-	-	-	-	-	-	901	036.5	3.VIII	-	-	-	-	-	-	41	04	39	156	173	114	31	149	37	04	01	.	.	02	30	-	-
BR. ST. 178						PANČEVO																														
																																				H_s = 80 m H_b = - m h_b = 2,0 m h_r = 1,0 m
I	8.6	8.4	7.6	8.2	-	-	-	-	-	-	61	034	017.3	08	01	05	22	.	.	.	.	.	.	20	13	05	01	09	04	.	.	.	.	.	.	04	10
II	7.2	6.7	6.4	6.7	-	04.7	94	85	91	90	-	102	023.3	04	-	-	-	-	-	-	.	.	04	12	15	13	02	09	13	04	.	.	.	.	02	02	12
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	6.0	6.2	5.1	5.8	-	08.3	87	64	81	77	32	073	018.8	15	.	.	01	04	.	.	.	.	03	10	12	11	02	12	.	.	.	.	.	.	01	.	.
V	6.3	6.7	5.8	6.3	-	10.0	86	64	86	79	18	099	023.6	13	.	.	.	05	.	.	.	.	01	08	16	11	02	16	.	.	.	.	.	.	09	02	.
VI	4.6	5.2	5.1	5.0	-	13.9	84	63	85	77	31	116	027.4	19	.	.	.	19	04	.	.	.	05	05	18	15	04	18	.	.	.	.	.	.	11	.	.
VII	4.8	5.3	3.4	4.4	-	14.5	86	63	88	79	39	066	023.8	06	.	.	.	20	06	.	.	.	07	06	09	07	03	09	.	.	.	.	.	.	05	02	.
VIII	3.9	4.0	3.1	3.7	-	14.4	88	61	88	79	45	077	034.4	03	.	.	.	19	07	01	.	.	-	-	12	05	03	12	.	.	.	.	.	.	07	02	.
IX	4.5	4.0	2.4	3.6	-	11.6	92	64	89	82	36	022	015.4	17	.	.	.	11	04	.	.	.	12	05	07	02	01	07	.	.	.	.	.	.	01	07	.
X	6.4	5.3	4.9	5.5	-	07.8	92	64	89	82	42	066	018.6	23	.	.	.	01	.	.	.	.	08	11	08	07	03	08	.	.	.	.	.	.	.	02	.
XI	6.8	5.9	5.2	6.0	-	-	-	-	-	-	-	056	015.7	23	-	-	-	-	-	-	.	.	03	10	13	09	02	13	.	.	.	.	.	.	.	04	.
XII	7.5	8.1	7.5	7.7	-	05.2	98	95	98	97	83	022	003.9	26	02	03	19	.	.	.	.	.	02	18	11	10	.	09	04	.	.	.	.	.	.	06	05
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 179						SMEDEREVO																														
																																				H_s = 90 m H_b = - m h_b = 2,0 m h_r = 1,0 m
I	9.2	7.8	7.4	8.1	-	-	-	-	-	-	-	038	013.0	02	03	06	19	.	.	.	.	.	01	19	12	07	01	09	04	01	.	.	.	.	.	03	13
II	7.2	7.0	6.2	6.8	-	-	-	-	-	-	-	109	020.5	04	-	-	-	-	-	-	.	.	.	11	14	14	05	08	07	01	.	.	.	.	.	.	12
III	7.2	6.4	3.8	5.8	-	-	-	-	-	-	-	057	012.0	15	.	.	08	.	.	.	.	.	03	06	12	10	02	09	03	.	.	.	.	.	02	-
IV	-	-	-	-	-	-	-	-	-	-	-	074	020.6	15	.	.	01	03	.	.	.	.	-	-	10	10	02	10	.	.	.	.	01	.	02	.	.
V	5.9	6.2	5.5	5.9	-	-	-	-	-	-	-	110	025.4	23	.	.	.	04	.	.	01	.	03	07	18	16	02	18	.	.	.	.	.	.	05	.	.
VI	-	-	-	-	-	-	-	-	-	-	-	082	017.0	05	.	.	.	19	03	.	.	.	-	-	13	11	02	13	.	.	.	.	.	.	-	.	.
VII	4.6	4.9	2.9	4.1	-	-	-	-	-	-	-	107	027.2	26	.	.	.	20	08	.	02	.	11	06	12	10	04	12	.	.	.	.	01	.	05	01	.
VIII	3.4	4.2	2.6	3.4	-	-	-	-	-	-	-	030	013.5	18	.	.	.	19	10	01	.	.	13	03	10	07	01	10	.	.	.	.	.	.	05	02	.
IX	4.8	4.0	2.0	3.6	-	-	-	-	-	-	-	014	009.2	01	.	.	02	10	06	.	.	.	12	03	07	03	.	07	.	.	.	.	.	.	01	03	.
X	5.7	4.9	4.5	5.0	-	-	-	-	-	-	-	068	019.0	23	.	.	01	01	.	.	.	.	08	07	08	08	02	08	.	.	.	.	.	.	.	03	.
XI	6.4	5.4	5.1	5.6	-	-	-	-	-	-	-	066	020.0	23	-	-	-	-	-	-	.	.	06	12	09	09	02	09	.	.	.	.	.	.	01	04	.
XII	8.1	7.6	7.5	7.8	-	-	-	-	-	-	-	019	004.0	28	01	01	17	.	.	.	.	.	02	19	14	10	.	08	06	.	.	.	.	.	.	10	05
GOD.	-	-	-	-	-	-	-	-	-	-	-	774	027.2	26.VII	-	-	-	-	-	-	03	.	-	-	139	115	23	121	20	02	.	.	02	.	-	28	-
BR. ST. 180						KRAGUJEVAC																														
																																				H_s = 190 m H_b = - m h_b = 2,0 m h_r = 1,4 m
I	8.3	8.1	7.4	7.9		037.2	04.1	81	72	80	78	52	040	015.0	02	01	06	20	.	.	.	.	.	.	17	14	08	01	09	08	.	.	.	.	.	.	13
II	7.7	7.5	7.3	7.5		075.1	04.1	83	66	81	77	37	062	010.3	24	02	04	16	.	.	.	03	.	01	12	15	13	01	07	08	.	.	.	.	.	.	13
III	7.5	7.3	4.8	6.5		124.1	04.7	79	53	71	68	25	086	031.6	20	.	.	09	.	.	.	01	.	01	14	13	07	04	10	06	.	.	.	.	.	.	03
IV	6.3	6.6	4.6	5.8		178.9	04.7	74	49	69	64	23	056	015.2	13	.	.	02	04	.	.	02	.	03	09	11	10	02	11	.	.	.	.	.	.	01	.	.
V	7.1	7.5	6.5	7.0		162.1	08.5	78	59	78	72	36	170	033.8	23	.	.	.	04	.	.	.	.	02	15	20	17	05	20	.	.	.	.	.	.	09	.	.
VI	5.5	5.8	4.5	5.3		233.5	12.7	81	58	85	75	41	176	036.6	18	.	.	.	20	01	.	01	.	04	06	19	14	06	19	.	.	.	.	.	01	11	.	.
VII	4.3	5.5	4.4	4.7		253.9	13.2	81	56	85	74	39	106	023.6	08	.	.	.	19	05	.	01	.	11	07	10	09	06	10	.	.	.	.	.	.	06	.	.
VIII	2.7	5.3	3.0	3.7		261.9	13.7	86	57	89	77	34	069	016.8	03	.	.	.	20	07	.	01	.	10	04	12	08	03	12	.	.	.	.	.	.	09	.	.
IX	5.0	4.7	4.0	4.6		186.3	10.5	91	53	89	78	24	025	007.4	17	.	.	02	11	05	.	.	.	11	07	08	04	.	08	.	.	.	.	.	.	01	.	.
X	5.5	5.5	4.5	5.2		154.3	07.2	88	58	85	77	33	062	022.4	23	.	.	01	01	.	.	.	.	08	10	13	10	02	13	.	.	.	.	.	.	.	.	.
XI	6.1	6.1	4.6	5.6		115.6	06.1	84	60	81	75	29	036	010.7	11	.	.	04	.	.	.	.	.	06	11	09	06	01	09	.	.	.	.	.	.	.	.	.
XII	7.5	7.5	7.3	7.4		060.4	04.5	88	70	85	81	39	013	005.1	26	.	03	19	.	.	.	.	.	04	18	08	04	.	04	04	.	.	.	.	.	.	01	05
GOD.	6.1	6.4	5.2	5.9		1843.3	08.0	82	59	81	74	23	901	036.6	18 VI	03	13	73	79	18	.	04	.	61	130	152	110	31	132	26	.	.	.	.	01	37	01	34

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dlas)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12) N b.	j.	NE b.	j.	E b.	j.	SE b.	j.	S b.	j.	SW b.	j.	W	j.	NW b.	j.	C
φ = 44° 22' N λ = 20° 58' E Gr. Δ G = + 1h 22 min.																												SMEDEREVSKA PALANKA BR. ST. 181
I	750.5	-00.3	02.7	00.6	00.9	04.0	-02.4	14.7	15	-14.0	22	05	01.4	02	02.0	18	03.0	29	02.5	03	02.3	02	02.5	14	02.8	10	03.2	10
II	747.2	00.0	04.6	01.8	02.1	06.0	-01.8	16.5	10	-09.9	18	07	02.0	01	03.0	12	02.5	20	02.2	08	02.5	02	04.0	12	03.0	20	02.5	02
III	748.4	02.9	09.5	05.9	06.1	11.1	01.4	23.4	25	-00.7	02	05	02.4	.	.	17	02.7	23	02.2	08	02.1	02	03.5	17	02.4	19	02.3	02
IV	748.9	09.1	16.1	10.9	11.7	17.8	06.0	27.4	26	-00.7	04	07	02.4	03	01.7	10	02.2	22	02.5	06	03.0	03	02.0	18	02.8	20	02.6	01
V	749.6	11.7	17.7	12.9	13.8	18.7	09.0	28.8	11	03.4	26	13	02.2	02	03.0	10	01.6	14	01.9	07	01.1	02	03.0	28	02.3	17	03.2	.
VI	750.7	17.4	23.9	18.5	19.6	24.8	13.8	30.3	17	08.3	02	06	01.7	02	02.0	11	01.9	20	01.8	05	01.4	04	02.2	25	02.0	14	02.0	03
VII	749.7	17.8	24.3	19.6	20.3	25.7	14.5	31.5	25,22	10.0	20	10	02.0	01	02.0	11	01.5	18	01.7	01	01.0	02	01.5	26	02.4	18	02.3	06
VIII	749.9	17.1	25.2	19.4	20.3	26.4	14.1	32.0	07	09.0	19	10	01.5	03	02.7	19	01.6	15	01.8	04	02.0	03	01.3	11	02.8	13	02.0	15
IX	753.6	12.0	21.3	14.3	15.5	22.5	09.8	32.9	12	-03.0	30	14	01.6	01	01.0	05	01.6	14	01.6	04	01.5	01	01.0	18	01.9	18	02.1	15
X	754.0	06.5	15.2	09.0	09.9	16.2	04.7	24.8	09	-00.6	25	07	01.7	05	01.4	09	01.8	20	02.0	03	02.7	.	.	19	02.3	21	02.1	09
XI	752.5	05.3	12.4	07.5	08.2	13.2	03.4	21.4	20	-02.6	08	08	01.6	01	01.0	12	02.0	24	01.9	04	02.0	04	01.0	16	02.1	12	02.2	09
XII	755.2	01.1	04.5	02.1	02.4	05.4	-01.2	19.8	30	-15.3	27	07	01.9	07	01.0	06	02.0	19	02.6	01	01.0	04	01.0	22	02.1	21	02.4	06
GOD.	750.8	08.4	14.8	10.2	10.9	16.0	05.9	32.9	12 IX	-15.3	27 XII	99	01.9	28	01.7	140	02.1	238	02.1	54	02.0	29	02.0	226	02.4	203	02.4	78
φ = 44° 56' N λ = 21° 05' E Gr. Δ G = + 1h 24 min.																												FLAMUNDA BR. ST. 182
I	-	-01.8	02.0	-01.1	-00.5	03.7	-04.7	14.0	15	-19.4	22	03	01.0	.	.	.	.	25	03.9	18	02.3	.	.	09	02.3	07	02.6	31
II	-	-00.7	04.1	00.5	01.1	05.4	-03.3	17.4	09	-16.4	18	09	02.1	01	02.0	.	.	06	02.5	21	02.4	04	03.5	02	02.0	06	02.3	35
III	-	01.6	09.0	04.2	04.6	10.4	-00.6	22.4	25	-09.4	08	05	02.6	.	.	01	03.0	19	04.5	16	02.6	02	02.5	04	02.2	04	02.8	42
IV	-	08.8	15.7	09.0	10.6	17.4	03.4	27.2	26	-05.6	05	19	02.4	.	.	.	.	05	03.2	23	02.9	02	03.0	01	02.0	05	01.4	35
V	-	12.1	18.1	11.3	13.2	19.3	06.7	28.8	11	-01.2	03	19	02.6	01	02.0	01	01.0	04	02.2	14	02.1	01	02.0	05	02.8	08	03.1	40
VI	-	17.6	23.6	16.6	18.6	24.8	11.6	30.4	24	04.0	06	05	02.2	.	.	01	03.0	12	02.7	05	02.2	01	03.0	06	02.2	07	02.1	53
VII	-	18.0	24.4	16.6	18.9	25.5	11.8	31.8	23	05.4	27	05	02.4	.	.	03	01.7	01	02.0	05	02.2	01	02.0	07	02.9	08	02.8	63
VIII	-	16.9	24.8	16.1	18.5	26.0	10.9	32.0	07	03.0	14	03	01.7	03	02.0	01	01.0	04	02.2	10	02.9	.	.	06	02.2	02	03.0	64
IX	-	11.0	21.1	11.4	13.7	22.2	07.0	32.6	12	-09.2	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	05.6	14.8	06.8	08.5	15.6	02.0	24.4	08	-04.2	27	10	02.0	.	.	05	02.4	07	02.6	11	02.0	01	02.0	06	02.7	08	02.5	45
XI	-	04.2	12.1	05.0	06.6	12.7	00.9	20.2	20,03	-07.4	26	07	02.0	.	.	.	.	01	03.0	32	02.4	.	.	.	.	08	02.6	42
XII	-	-00.4	03.1	00.4	00.9	04.1	-02.8	12.6	02	-17.2	26	17	01.5	.	.	.	.	07	03.4	10	03.7	.	.	09	01.6	14	01.9	36
GOD.	-	07.7	14.4	08.1	09.6	15.6	03.6	32.6	12 IX	-19.4	22.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 44° 56' N λ = 21° 08' E Gr. Δ G = + 1h 24 min.																												ŠUŠARA BR. ST. 183
I	-	-01.5	01.5	-00.7	-00.4	02.8	-03.7	13.5	15	-15.5	22	01	01.0	02	01.5	.	.	43	03.5	01	04.0	.	.	.	.	21	02.0	25
II	-	-00.7	03.3	00.4	00.9	04.7	-02.8	15.5	09	-12.0	18	01	03.0	.	.	.	.	29	02.4	.	.	01	04.0	01	02.0	24	02.2	28
III	-	02.5	08.5	04.8	05.1	09.6	00.7	22.4	25	-05.5	08	01	02.0	.	.	.	.	46	03.0	01	01.0	01	01.0	03	01.7	24	02.3	17
IV	-	08.6	15.2	09.1	10.5	16.8	05.2	27.2	24	-02.6	04	06	03.7	.	.	.	.	39	02.8	.	.	.	.	.	.	28	02.3	17
V	-	11.9	18.1	12.6	13.8	19.4	08.5	29.2	11	01.8	01	.	.	.	.	.	.	32	02.3	.	.	01	01.0	03	01.3	44	02.7	13
VI	-	17.6	23.5	18.1	19.3	24.9	13.4	31.0	17	07.8	03	03	01.0	02	02.5	.	.	31	02.5	.	.	03	01.7	01	02.0	29	02.5	21
VII	-	17.9	24.5	18.9	20.0	25.8	13.8	32.0	23	09.5	27,19	.	.	.	.	.	.	25	02.6	.	.	.	.	.	.	46	02.0	22
VIII	-	17.3	25.1	18.1	19.6	26.2	13.2	32.5	07	06.4	14	02	01.0	01	02.0	.	.	31	02.8	.	.	01	04.0	01	01.0	23	02.2	34
IX	-	12.0	21.0	13.6	15.1	22.2	09.0	32.6	12	-04.5	29	.	.	.	.	.	.	26	02.2	.	.	01	01.0	.	.	30	02.2	33
X	-	06.8	14.6	08.5	09.6	15.6	04.7	25.4	08	-03.0	25	01	01.0	01	02.0	.	.	37	02.1	.	.	.	.	.	.	27	02.2	27
XI	-	05.0	11.4	06.7	07.4	12.2	02.8	21.0	03	-03.4	08	05	01.2	.	.	.	.	33	02.0	01	03.0	01	02.0	01	01.0	17	02.4	32
XII	-	-00.5	02.7	00.6	00.9	03.7	-02.2	12.0	02	-13.2	27	.	.	.	.	.	.	19	03.1	02	02.0	.	.	.	.	32	01.6	40
GOD.	-	08.1	14.1	09.2	10.2	15.3	05.2	32.6	12 IX	-15.5	22 I	20	02.0	06	02.0	.	.	391	02.6	05	02.4	09	02.0	10	01.5	345	02.2	309
φ = 44° 54' N λ = 21° 25' E Gr. Δ G = + 1h 25 min.																												BELA CRKVA BR. ST. 184
I	-	-00.3	03.0	00.6	01.0	04.5	-02.9	15.3	15	-12.5	22	.	.	.	.	15	03.3	22	02.7	03	02.3	04	02.2	07	01.7	19	02.3	23
II	-	00.6	04.5	02.4	02.5	06.2	-01.2	16.0	09	-08.9	18	.	.	.	.	06	03.2	10	02.1	04	02.0	08	01.8	23	01.8	16	02.6	17
III	-	04.1	09.3	05.9	06.3	10.7	01.6	22.7	25	-04.5	02	.	.	01	04.0	07	04.3	17	03.4	05	03.0	23	01.8	08	01.9	18	01.9	14
IV	-	09.8	16.3	11.2	12.1	17.7	06.1	27.2	26	-00.7	04	01	01.0	.	.	.	.	13	02.8	12	02.6	12	01.9	06	02.7	32	02.7	14
V	-	12.7	18.2	13.3	14.4	19.5	09.1	29.3	11	04.0	26	.	.	01	02.0	.	.	06	02.2	.	.	12	02.1	16	02.3	34	02.1	24
VI	-	18.1	24.1	18.9	20.0	25.3	13.9	30.7	29	07.7	02	01	01.0	04	02.2	03	01.7	07	02.7	.	.	06	01.8	14	02.0	19	01.9	36
VII	-	19.1	25.0	19.3	20.7	26.5	14.3	32.3	23	09.9	20	02	02.0	.	.	01	03.0	06	02.7	01	03.0	07	01.7	19	02.2	24	01.8	33
VIII	-	18.5	26.0	18.8	20.5	26.7	14.1	32.0	07,06	08.6	14	.	.	.	.	05	02.0	13	02.2	02	02.0	02	02.5	14	02.0	18	01.7	39
IX	-	12.3	21.8	14.0	15.5	22.6	09.7	32.3	12	-02.7	30	01	02.0	01	01.0	05	02.2	.	.	04	01.5	06	02.0	09	01.7	27	02.0	37
X	-	07.7	15.2	09.7	10.6	16.3	04.8	25.1	08	-01.5	25	.	.	01	01.0	01	03.0	07	03.4	01	03.0	04	02.5	16	01.8	14	02.0	49
XI	-	05.6	12.1	06.8	07.8	12.9	02.9	20.9	03	-02.1	26	.	.	.	.	01	01.0	10	02.3	01	02.0	10	01.7	02	02.0	23	02.1	43
XII	-	00.5	03.8	01.9	02.0	05.1	-01.4	13.7	30	-15.2	27	02	01.5	.	.	02	02.5	11	04.4	.	.	01	02.0	05	01.4	29	01.8	43
GOD.	-	09.1	14.9	10.2	11.1	16.2	05.9	32.3	12 IX	-15.2	27 XII	07	01.6	08	02.1	46	03.0	122	02.8	33	02.5	95	01.9	139	02.0	273	02.1	372
φ = 44° 23' N λ = 21° 25' E Gr. Δ G = + 1h 26 min.																												PETROVAC BR. ST. 185
I	-	-00.4	02.8	00.1	00.7	04.6	-03.1	16.4	06	-13.8	22	01	01.0	21	02.2	23	02.9	02	03.5	01	01.0	01	01.0	23	01.6	02	01.0	19
II	-	00.2	04.9	02.0	02.3	06.5	-01.9	16.5	09	-14.0	18	01	02.0	10	01.5	18	02.1	07	02.1	.	.	02	02.0	20	02.4	01	01.0	25
III	-	04.6	09.2	05.5	06.2	10.6	01.6	23.0	25	-03.5	02	.	.	06	02.0	34	02.5	12	01.9	05	01.4	01	01.0	14	01.9	04	01.0	17
IV	-	10.2	16.3	10.8	12.0	18.0	05.7	27.0	26	-01.8	04	02	02.0	04	01.5	25	02.0	09	02.9	01	01.0	02	01.5	20	02.3	03	01.3	24
V	-	12.4	17.9	12.5	13.8	19.2	08.7	29.5	11	02.0	04	01	03.0	.	.	15	01.4	05	01.2	06	02.2	05	01.2	26	02.4	01	01.0	34
VI	-	18.1	24.0	18.0	19.5	25.2	14.0	31.0	10	06.5	02	01	02.0	01	01.0	15	01.3	11	01.3	06	01.7	03	01.0	13	01.7	02	01.5	38
VII	-	18.5	24.5	18.5	20.0	25.8	14.2	31.2	25	09.4	28	.	.	02	01.5	14	01.3	10	01.5	02	02.5	04	02.2	26	01.5	01	02.0	34
VIII	-	17.6	25.5	18.4	20.0	26.6	13.5	32.4	07	09.0	27	01	01.0	03	01.0	31	01.5	05	01.2	03	01.3	01	01.0	22	01.7	01	01.0	26
IX	-	12.3	21.4	13.5	15.2	22.6	09.3	32.5	12	-02.2	29	.	.	02	01.0	20	01.7	06	01.0	03	01.7	04	01.2	21	01.7	02	01.5	32
X	-	08.3	14.9	08.4	10.0	16.0	04.8	25.0	08	-00.6	25	06	01.8	02	02.5	29	01.5	02	01.5	04	01.8	.	.	24	01.9	.	.	26
XI	-	06.3	12.4	06.7	08.0	-	03.3	-	-	-02.4	26	01	01.0	04	01.0	29	01.3	10	02.0	01	01.0	.	.	20	01.4	01	01.0	24
XII	-	00.9	04.1	01.8	02.2	05.4	-01.2	18.5	30	-12.5	27	01	01.0	02	01.5	20	02.2	02	01.5	02	01.0	.	.	29	01.4	04	01.5	33
GOD.	-	09.1	14.8	09.7	10.8	-	05.7	-		-14.0	18.II	15	01.7	57	01.8	273	01.8	81	01.8	34	01.7	23	01.4	258	01.8	22	01.3	332

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dias)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dias)	Min	Padavine R mm Σ	Max	Dat.	Tn ≤ -10.0	Tx < 0.0	Tn < 0.0	Tx ≥ 25.0	Tx ≥ 30.0	Tn ≥ 20.0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	✱	⁂	△	∽	▲	▲	⊤	≡	▦
BR. ST. 181 — SMEDEREVSKA PALANKA — H_s = 120 m H_b = 118.2 m h_t = 2.0 m h_r = 1.2 m																																					
I	8.8	8.2	7.2	8.1	045.0	04.3	86	77	85	83	51	044	012.2	08	02	06	21	.	.	.	13	.	.	19	17	10	01	12	09	01	.	01	.	.	.	01	17
II	8.0	8.0	7.2	7.7	080.8	04.3	85	70	82	79	40	070	014.4	04	.	03	18	.	.	.	13	03	02	16	19	12	02	10	11	.	.	.	.	.	.	02	15
III	7.8	7.5	6.2	7.2	117.2	04.8	82	58	72	71	24	066	013.9	16	.	01	09	.	.	.	12	01	01	15	13	10	03	10	06	02	.	.	.	.	.	.	02
IV	6.3	6.4	5.6	6.1	180.0	07.0	78	52	72	68	25	065	016.3	13	.	.	01	03	.	.	18	04	03	13	13	12	03	13	.	.	.	.	01	.	02	04	.
V	7.4	7.5	6.1	7.0	178.4	09.1	87	60	84	77	34	129	031.9	23	.	.	.	04	.	.	16	03	02	13	20	18	03	20	.	.	.	.	.	.	09	06	.
VI	5.2	5.4	4.3	4.9	258.3	12.9	86	60	79	75	40	082	016.3	05	.	.	.	21	01	.	14	01	04	03	18	11	02	18	.	.	.	.	.	.	12	03	.
VII	4.3	4.9	3.9	4.4	252.8	13.5	86	60	82	76	41	107	021.6	17	.	.	.	19	07	.	13	02	08	07	12	10	04	12	.	.	.	.	.	.	07	02	.
VIII	3.5	5.0	3.5	4.0	273.2	13.5	88	58	83	76	41	046	008.9	23	.	.	.	19	06	01	09	02	13	05	12	08	.	12	.	.	.	.	.	.	10	08	.
IX	4.5	5.1	3.6	4.4	191.7	10.4	91	55	85	77	34	025	007.0	18	.	.	02	10	05	.	04	.	10	07	08	04	.	08	.	.	.	.	.	.	03	06	.
X	6.1	5.5	4.3	5.3	159.2	07.2	90	60	87	79	32	067	026.6	23	.	.	02	.	.	.	05	.	09	10	09	07	02	09	.	.	.	.	.	.	.	05	.
XI	7.2	6.8	5.6	6.5	123.4	06.4	88	65	82	78	28	051	011.2	24	.	.	07	.	.	.	04	.	02	11	11	09	02	11	.	.	.	.	.	.	02	06	.
XII	8.1	7.9	7.3	7.8	058.3	04.8	89	78	87	85	57	019	005.4	26	02	02	16	.	.	.	05	.	02	19	16	05	.	12	06	02	.	.	.	.	.	04	05
GOD.	6.4	6.5	5.4	6.1	1918.3	08.2	86	62	81	77	24	771	031.9	23.V	04	12	76	76	19	01	126	16	56	138	168	116	22	147	32	05	.	01	01	.	45	47	39
BR. ST. 182 — FLAMUNDA — H_s = 160 m H_b = - m h_t = 2.0 m h_r = 1.5 m																																					
I	8.9	8.1	6.9	8.0	-	04.0	85	80	87	84	45	040	013.4	08	06	07	24	.	.	.	04	.	01	19	11	06	01	07	04	.	.	.	.	.	.	01	19
II	8.7	7.8	7.3	7.9	054.3	04.4	90	77	89	86	32	127	027.1	12	03	03	21	.	.	.	.	.	.	14	17	15	05	08	10	.	.	.	.	.	.	03	18
III	7.9	6.6	6.4	7.0	-	05.3	88	69	84	80	40	099	013.7	15	.	01	14	.	.	.	04	.	03	14	14	12	01	10	05	.	.	.	.	.	.	02	03
IV	5.5	6.3	5.3	5.7	157.1	07.4	83	60	82	75	28	098	030.2	15	.	.	06	03	.	.	.	.	07	09	11	10	04	11	.	.	.	.	.	.	.	01	.
V	6.0	6.8	6.0	6.3	143.6	08.8	84	57	87	76	34	157	038.7	23	.	.	03	04	.	.	.	.	04	10	15	14	06	15	.	.	.	.	01	.	04	.	.
VI	5.0	5.7	5.1	5.3	210.8	13.0	85	62	89	78	42	135	023.2	01	.	.	.	18	04	.	.	.	03	04	18	14	06	18	.	.	.	.	.	.	04	.	.
VII	3.9	4.8	3.7	4.1	223.8	13.7	88	63	92	81	48	162	049.2	17	.	.	.	20	07	.	.	.	12	08	10	10	06	10	.	.	.	.	.	02	04	.	.
VIII	4.3	4.6	3.1	4.0	224.6	13.3	90	61	91	81	44	114	060.4	03	.	.	.	19	06	.	.	.	07	02	11	10	02	11	.	.	.	.	.	01	06	.	.
IX	4.8	4.1	2.0	3.7	179.0	-	-	-	-	-	33	044	020.6	01	.	.	06	09	04	.	.	.	12	03	06	05	02	06	.	.	.	.	.	.	.	03	.
X	6.5	6.0	3.9	5.4	128.3	07.5	91	72	92	85	34	084	022.1	23	.	.	05	.	.	.	.	.	07	10	08	07	04	08	.	.	.	.	.	.	.	03	.
XI	7.5	6.4	5.2	6.4	109.5	06.6	93	74	91	86	35	070	020.2	23	.	.	15	.	.	.	.	.	05	12	09	08	02	09	.	.	.	.	.	.	.	06	.
XII	8.7	8.7	7.8	8.4	028.3	04.7	95	91	94	93	64	-	-	-	03	04	21	.	.	.	02	.	01	21	-	-	-	-	-	-	.	.	.	.	.	06	-
GOD.	6.5	6.3	5.2	6.0	-	-	-	-	-	-	28	-	-		12	15	115	73	21	.	10	.	62	126	-	-	-	-	-	-	.	.	01	03	18	25	-
BR. ST. 183 — SUŠARA — H_s = 180 m H_b = - m h_t = 2.0 m h_r = 1.4 m																																					
I	8.6	7.9	6.6	7.7	-	04.1	91	83	90	88	44	032	011.5	08	04	08	22	.	.	.	04	.	01	15	11	07	01	06	05	.	.	.	.	.	.	05	16
II	7.8	7.9	7.2	7.6	-	04.4	89	80	91	86	45	099	021.5	12	01	05	19	.	.	.	.	.	.	14	16	13	04	08	10	.	01	.	.	.	01	07	18
III	7.4	7.2	6.4	7.0	-	05.2	86	67	85	79	20	060	017.4	15	.	01	11	.	.	.	05	.	01	12	14	12	01	09	05	.	01	.	.	.	.	02	03
IV	5.5	6.3	5.7	5.8	-	07.6	85	62	83	76	39	079	019.2	15	.	.	02	02	.	.	03	.	04	09	11	11	04	11	.	.	.	.	.	.	01	01	.
V	6.5	6.6	6.4	6.5	-	09.2	86	60	85	77	31	105	025.6	23	.	.	.	04	.	.	02	.	03	10	17	15	04	17	.	.	.	.	.	.	09	01	.
VI	3.9	5.7	5.1	4.9	-	13.0	84	63	83	77	39	083	015.6	05	.	.	.	20	04	.	01	.	03	03	16	14	03	16	.	.	.	.	.	.	08	01	.
VII	4.5	5.0	3.8	4.4	-	13.9	87	63	85	78	45	121	023.0	17	.	.	.	21	09	.	02	.	09	06	10	09	06	10	.	.	.	.	.	01	04	03	.
VIII	4.2	5.3	2.8	4.1	-	13.8	89	61	88	79	38	055	011.6	18	.	.	.	19	07	.	01	.	08	02	11	10	02	11	.	.	.	.	.	.	06	.	.
IX	4.4	4.6	2.0	3.7	-	10.6	90	58	87	78	31	038	021.0	01	.	.	05	08	05	.	.	.	10	03	06	06	01	06	.	.	.	.	.	.	01	03	.
X	5.8	5.4	3.9	5.0	-	07.3	89	63	89	80	35	060	017.8	23	.	.	03	02	.	.	.	.	08	06	07	07	02	07	.	.	.	.	.	.	.	03	.
XI	7.4	6.0	4.6	6.0	-	06.4	89	71	87	82	40	058	017.0	23	.	.	05	.	.	.	.	.	05	13	10	09	01	10	.	.	.	.	.	.	.	09	.
XII	8.8	8.5	7.4	8.2	-	04.6	94	86	93	91	63	027	006.1	26	03	02	20	.	.	.	01	.	01	20	15	11	.	08	07	.	.	.	.	.	01	15	05
GOD.	6.2	6.4	5.2	5.9	-	08.3	88	68	87	80	20	817	025.6	25 V	08	16	87	76	25	.	19	.	53	113	144	124	29	119	27	.	02	.	.	01	31	50	42
BR. ST. 184 — BELA CRKVA — H_s = 90 m H_b = - m h_t = 2.0 m h_r = 1.5 m																																					
I	8.3	8.2	7.3	7.9	-	04.2	85	78	85	83	37	037	010.7	08	03	08	23	.	.	.	01	.	.	17	13	08	01	07	07	.	.	.	.	.	.	01	09
II	8.3	8.3	8.3	8.3	-	04.8	90	78	87	85	44	103	023.5	12	.	02	17	.	.	.	02	.	.	17	20	15	03	12	10	.	.	.	.	.	.	01	07
III	7.0	7.3	6.2	6.8	-	05.2	83	64	74	74	28	056	009.4	15	.	01	10	.	.	.	02	01	.	10	17	12	.	14	06	03	.	.	.	.	.	.	02
IV	6.5	6.6	6.0	6.4	-	06.8	69	54	65	63	30	065	012.2	13	.	.	01	03	.	.	03	01	01	09	14	11	02	14	.	.	.	.	.	.	04	01	.
V	6.7	7.0	6.6	6.8	-	09.0	80	60	76	72	36	145	025.6	24	.	.	.	03	.	.	01	01	02	10	23	17	06	23	.	.	.	.	.	01	08	01	.
VI	4.8	5.8	5.1	5.2	-	12.8	79	62	74	72	39	110	019.9	01	.	.	.	21	05	.	.	.	02	04	20	15	04	20	.	.	.	.	01	.	12	01	.
VII	5.0	5.4	4.5	5.0	-	13.1	77	60	74	70	45	144	035.2	17	.	.	.	22	11	.	01	01	02	06	12	10	06	12	.	.	.	.	.	01	06	.	.
VIII	4.5	4.9	3.9	4.5	-	13.0	79	55	75	70	40	078	026.7	11	.	.	.	19	08	.	.	.	06	02	12	10	02	12	.	.	.	.	.	01	07	02	.
IX	5.1	5.2	2.9	4.4	-	09.9	82	58	73	71	31	026	016.2	01	.	.	02	08	04	.	.	.	06	03	06	04	01	06	.	.	.	.	.	.	01	01	.
X	5.3	5.1	4.3	4.9	-	07.0	83	57	77	72	28	058	016.8	23	.	.	01	.	.	.	.	.	09	05	08	08	02	08	.	.	.	.	01	.	01	01	.
XI	6.6	6.2	5.4	6.1	-	06.0	84	64	77	75	32	056	018.1	23	.	.	07	.	.	.	.	.	04	11	12	10	02	12	.	.	.	.	.	.	01	02	.
XII	8.0	8.3	6.4	7.5	-	-	-	-	-	-	-	044	011.0	27	01	01	19	.	.	.	03	01	03	16	15	11	01	12	06	01	.	.	.	.	.	06	06
GOD.	6.3	6.5	5.6	6.2	-	-	-	-	-	-	-	922	035.2	17.VII	04	12	80	76	28	.	13	05	35	110	172	131	30	152	29	04	.	.	02	03	40	17	24
BR. ST. 185 — PETROVAC — H_s = 120 m H_b = - m h_t = 2.0 m h_r = 1.2 m																																					
I	8.1	7.6	7.5	7.7	-	-	-	-	-	-	-	042	010.5	02	02	06	20	.	.	.	01	.	02	19	13	10	01	09	06	.	.	.	.	.	.	04	-
II	7.3	8.5	8.4	8.1	-	-	-	-	-	-	-	077	024.0	04	02	03	17	.	.	.	01	01	01	17	20	14	01	11	12	.	.	.	.	.	.	02	11
III	7.1	7.6	6.6	7.1	-	-	-	-	-	-	-	066	014.5	16	.	01	09	.	.	.	01	.	01	13	16	13	03	13	07	02	.	.	.	.	.	04	03
IV	5.9	6.1	5.6	5.9	-	07.7	79	56	80	72	26	073	019.0	13	.	.	01	05	.	.	01	.	05	11	12	12	02	12	.	.	.	.	.	.	02	02	.
V	7.0	7.5	6.5	7.0	-	09.8	88	65	91	81	36	170	024.5	23	.	.	.	05	.	.	.	.	03	15	23	19	05	23	.	.	.	.	.	02	07	.	.
VI	5.2	5.4	4.1	4.9	-	13.7	84	64	88	79	47	129	028.0	20	.	.	.	20	04	.	01	.	05	04	17	15	06	17	.	.	.	.	.	.	07	01	.
VII	4.3	5.5	4.1	4.6	-	-	-	-	-	-	-	134	031.3	15	.	.	.	20	08	.	01	.	09	07	10	10	07	10	.	.	.	.	.	.	05	.	.
VIII	4.1	5.1	3.5	4.2	-	14.0	89	61	87	79	46	040	009.8	26	.	.	.	19	08	.	01	.	12	04	12	09	.	12	.	.	.	.	.	01	07	.	.
IX	4.7	5.1	3.6	4.5	-	11.3	94	65	92	84	36	024	014.0	01	.	.	02	11	05	.	.	.	11	09	09	03	01	09	.	.	.	.	.	.	02	03	.
X	6.3	5.7	5.2	5.7	-	07.7	89	65	90	81	41	064	019.6	23	.	.	01	01	.	.	.	.	08	14	08	08	02	09	.	.	.	.	.	.	.	02	.
XI	6.3	6.3	6.1	6.2	-	-	-	-	-	-	-	058	017.3	24	.	-	.	-	-	.	.	.	03	12	12	09	01	11	.	.	.	.	.	.	.	06	.
XII	8.8	8.6	7.4	8.3	-	-	-	-	-	-	-	028	006.3	26	02	01	18	.	.	.	02	.	02	23	16	10	.	11	06	01	.	.	.	.	.	10	05
GOD.	6.3	6.6	5.7	6.2	-	-	-	-	-	-	-	905	031.3	16 VII	06	-	68	-	-	.	09	01	62	148	168	132	29	146	31	03	.	.	.	03	30	34	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dlan)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12) N č.	j.	NE č.	j.	E č.	j.	SE č.	j.	S č.	j.	SW č.	j.	W j.	č.	j.	NW č.	j.	C č.
VELIKO GRADIŠTE																													
φ = 44° 46' N λ = 21° 31' E Gr. Δ G = + 1h 26 min.																													BR. ST. 186
I	755.0	-01.0	02.3	-00.1	00.3	03.3	-03.0	12.2	15	-12.2	21	.	.	.	.	21	03.6	19	03.9	.	.	.	.	06	01.2	13	01.8	34
II	751.4	-00.4	04.2	01.5	01.7	05.5	-01.6	16.7	09	-09.4	18	.	.	01	01.0	13	02.5	14	02.3	01	01.0	.	.	05	01.6	13	02.4	37
III	752.6	03.4	09.4	05.6	06.0	10.8	01.8	23.3	25	-02.8	02	.	.	.	.	16	04.4	16	04.3	.	.	03	01.3	05	01.6	16	01.7	37
IV	752.9	08.9	16.4	10.9	11.8	17.9	06.0	26.6	26	-01.6	05	.	.	.	.	14	02.9	12	03.3	02	01.5	.	.	03	01.7	23	02.1	36
V	753.3	12.2	18.3	13.4	14.3	19.5	09.2	29.6	11	03.9	26	01	01.0	.	.	04	02.8	08	01.6	.	.	.	.	03	02.0	31	02.3	46
VI	754.6	17.3	24.4	18.4	19.6	25.2	14.0	31.0	29	08.0	02	01	01.0	.	.	08	02.4	08	02.5	.	.	01	01.0	09	01.6	17	01.6	46
VII	753.5	17.9	25.3	19.2	20.4	26.2	15.1	31.8	24	10.5	19	02	01.5	.	.	06	02.0	04	02.5	.	.	.	.	09	01.3	24	01.8	48
VIII	753.8	17.6	25.6	18.6	20.1	26.4	14.8	32.2	07	09.1	14	02	01.5	01	03.0	11	02.3	10	02.2	.	.	.	.	08	01.5	09	01.6	52
IX	757.5	12.7	22.1	14.5	16.0	23.0	10.5	32.3	12	-02.1	30	01	02.0	.	.	05	02.2	05	02.4	.	.	03	01.3	07	01.7	16	01.8	53
X	758.0	07.0	15.0	09.0	10.0	16.0	05.6	24.6	14,07	-00.3	25	.	.	.	.	12	02.6	12	02.3	.	.	.	.	02	02.5	16	01.8	51
XI	756.6	04.6	12.1	06.4	07.4	12.7	02.9	20.0	01	-01.5	12	.	.	.	.	14	01.6	12	01.5	.	.	01	01.0	03	01.7	17	01.5	43
XII	759.4	00.6	03.8	01.8	02.0	04.9	-01.0	14.1	02	-12.0	27	01	01.0	.	.	10	03.4	10	03.2	.	.	.	.	14	01.4	22	01.5	36
GOD.	754.9	08.4	14.9	09.9	10.8	16.0	06.2	32.3	12 IX	-12.2	21 I	08	01.4	02	02.0	134	02.9	130	02.8	03	01.3	08	01.2	74	01.5	217	01.9	519
ŽAGUBICA																													
φ = 44° 12' N λ = 21° 47' E Gr. Δ G = + 1h 27 min.																													BR. ST. 187
I	-	-02.7	00.9	-01.7	-01.3	02.3	-04.5	14.0	15	-15.0	22	.	.	.	.	27	03.5	.	.	01	02.0	.	.	07	02.3	10	02.4	48
II	-	-02.4	03.4	00.4	00.5	05.2	-03.4	15.6	05	-15.3	03	.	.	.	.	12	02.8	.	.	.	.	02	03.0	11	02.0	14	02.4	45
III	-	01.6	07.6	04.2	04.4	09.3	-00.1	22.9	25	-05.0	03,02	.	.	02	01.0	23	02.9	.	.	05	04.4	02	02.0	20	01.6	09	01.9	32
IV	-	06.5	15.3	09.9	10.4	17.2	04.2	27.0	24	-05.5	05	01	01.0	.	.	14	02.9	05	02.0	06	03.2	01	02.0	13	02.2	12	01.9	38
V	-	10.2	16.8	12.1	12.8	18.5	07.8	30.0	11	02.0	26	01	02.0	.	.	07	02.9	.	.	01	02.0	.	.	26	02.2	19	02.1	39
VI	-	14.9	22.9	17.3	18.1	24.0	11.9	29.8	18	04.7	02	.	.	02	02.0	24	02.0	02	02.5	.	.	02	02.5	21	02.2	02	02.0	37
VII	-	19.0	23.9	17.9	18.7	25.4	13.0	32.0	15	06.1	20	01	02.0	04	01.8	19	02.2	03	03.3	02	02.0	02	01.5	34	02.7	04	02.5	24
VIII	-	14.8	24.4	17.4	18.5	25.3	12.4	31.8	08	05.8	14	01	02.0	02	03.0	18	02.7	04	02.8	.	.	02	01.0	20	02.6	04	02.0	42
IX	-	09.5	20.9	12.6	13.9	21.6	07.8	32.2	12	-04.0	30	.	.	.	.	11	02.0	.	.	.	.	02	01.0	18	02.3	08	02.2	51
X	-	04.9	13.9	07.2	08.3	15.0	03.2	24.8	08	-02.0	01	01	01.0	03	01.7	10	02.5	05	02.4	02	02.5	01	03.0	26	02.0	06	01.7	39
XI	-	02.5	11.8	04.9	06.0	12.7	01.2	21.0	01	-04.2	26	02	01.0	03	02.7	05	02.0	.	.	02	02.0	01	01.0	15	01.9	06	01.7	56
XII	-	-00.5	03.3	00.5	00.9	04.1	-02.0	18.0	30	-12.8	27	.	.	04	03.0	05	03.2	05	02.8	.	.	03	01.3	26	01.7	08	02.2	42
GOD.	-	06.2	13.8	08.6	09.3	15.0	04.3	32.2	12 IX	-15.3	3 II	07	01.4	20	02.2	175	02.7	24	02.6	19	03.1	18	01.8	237	02.2	102	02.1	493
DEBELI LUG																													
φ = 44° 22' N λ = 21° 55' E Gr. Δ G = + 1h 26 min.																													BR. ST. 188
I	-	-03.4	-00.6	-02.3	-02.1	00.5	-04.7	06.5	15	-12.8	03	02	02.5	.	.	05	02.0	34	03.3	04	02.8	01	02.0	.	.	19	04.1	28
II	-	-02.3	02.5	-00.4	-00.1	03.8	-03.7	14.4	10	-14.6	03	03	03.0	01	02.0	05	03.6	21	03.0	.	.	06	02.5	.	.	21	03.1	27
III	-	01.1	07.3	03.0	03.6	08.4	-00.7	21.8	26,25	-09.0	03	02	03.0	.	.	08	03.2	26	03.3	02	02.5	01	02.0	05	02.8	19	03.5	30
IV	-	06.2	14.7	09.0	09.7	16.2	04.0	26.4	24	-04.6	05	03	02.7	.	.	09	02.4	22	03.0	04	02.0	.	.	.	.	27	03.7	25
V	-	09.8	16.1	11.0	12.0	17.9	07.5	28.2	11	02.0	26,02	02	04.0	.	.	12	02.5	23	02.5	01	03.0	01	03.0	.	.	25	03.9	29
VI	-	14.9	22.6	16.3	17.5	23.5	11.9	29.0	29,17	05.6	06	04	02.2	03	02.0	06	01.8	15	02.5	05	02.2	.	.	.	.	18	03.4	39
VII	-	15.6	23.3	17.1	18.3	24.5	13.1	30.4	24	07.2	20	04	03.0	03	03.0	08	02.2	16	02.9	01	01.0	01	03.0	.	.	28	03.6	32
VIII	-	14.9	23.5	16.7	18.0	24.3	12.8	30.0	07	06.8	14	01	03.0	01	02.0	04	02.5	25	03.0	.	.	.	.	01	03.0	18	03.0	43
IX	-	10.0	20.2	13.0	14.0	20.8	08.7	31.2	12	-02.8	30	02	01.0	.	.	02	03.0	10	02.9	01	02.0	.	.	01	02.0	23	02.9	51
X	-	05.0	12.5	06.9	07.8	13.3	03.7	22.8	11	-00.8	29	01	02.0	.	.	08	02.4	20	03.4	01	02.0	01	02.0	02	02.0	23	03.4	37
XI	-	02.6	10.3	04.1	05.3	11.0	00.7	19.8	03,01	-02.8	12	02	03.0	01	02.0	.	.	20	03.0	.	.	.	.	.	.	25	02.7	42
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BOR																													
φ = 44° 05' N λ = 22° 06' E Gr. Δ G = + 1h 28 min.																													BR. ST 189
I	-	-03.1	-00.7	-02.3	-02.1	00.5	-04.4	11.2	15	-09.7	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-00.8	03.1	00.3	00.7	04.7	-02.5	14.5	10,15	-11.9	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	02.6	07.6	04.2	04.7	08.9	01.0	22.4	25	-04.7	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	06.2	15.2	10.5	11.1	16.9	06.3	28.0	24	-02.5	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	12.0	17.2	12.3	13.5	18.4	08.9	28.5	11	03.9	03,01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	17.7	22.7	17.8	19.0	24.1	14.1	29.9	17	08.7	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	19.1	24.2	18.6	20.1	25.7	14.8	31.5	23	08.7	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	18.4	24.2	18.4	19.9	25.3	14.5	31.5	08	10.5	28,14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	14.8	21.5	14.2	16.2	22.6	10.6	32.5	12	-02.8	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	07.4	12.8	08.0	09.1	14.2	-	25.9	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	05.2	11.0	06.2	07.1	12.2	03.6	23.3	01	-01.3	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	00.2	02.8	00.4	00.9	04.2	-01.5	13.5	01	-07.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	08.5	13.5	09.0	10.0	14.8	-	32.5	12 IX	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
TEKIJA																													
φ = 44° 41' N λ = 22° 25' E Gr. Δ G = + 1h 29 min.																													BR. ST. 190
I	-	-02.2	01.2	-01.2	-00.8	02.0	-03.5	06.8	28	-09.4	04,03	.	.	03	02.0	.	.	04	02.2	.	.	04	01.8	.	.	20	04.4	62
II	-	-00.8	04.0	00.7	01.2	04.9	-02.0	11.8	14	-08.2	18	01	01.0	06	01.8	.	.	01	03.0	.	.	02	02.5	.	.	20	03.2	54
III	-	03.3	10.0	05.3	06.0	10.9	01.4	24.4	25	-04.2	03	.	.	11	02.2	.	.	06	02.3	.	.	01	02.0	.	.	25	03.8	50
IV	-	09.1	16.4	11.1	11.9	17.6	06.0	25.8	24	-03.8	05	.	.	15	03.1	.	.	01	02.0	.	.	01	03.0	.	.	22	03.4	51
V	-	12.9	18.8	13.9	14.9	20.2	09.7	27.8	11	03.4	02	01	02.0	10	03.7	.	.	02	01.5	.	.	03	02.7	03	02.0	25	04.3	49
VI	-	17.7	24.4	18.7	19.9	25.2	13.7	30.4	23	09.2	06,03	.	.	11	02.5	.	.	03	01.7	01	01.0	01	02.0	01	02.0	26	03.7	47
VII	-	18.9	25.8	20.1	21.2	27.0	15.8	31.8	23	10.2	20	.	.	08	02.5	.	.	06	02.5	02	01.0	01	02.0	04	01.5	27	03.7	45
VIII	-	17.9	25.7	18.7	20.2	26.3	14.7	32.8	06	09.8	14	01	01.0	08	02.4	.	.	04	02.0	.	.	04	01.5	02	01.5	16	04.2	50
IX	-	13.2	22.7	15.9	16.9	23.2	10.7	29.4	13	00.0	30	.	.	12	02.6	.	.	01	04.0	.	.	.	.	.	.	25	03.4	52
X	-	07.1	14.9	08.9	09.9	15.6	05.3	24.4	07	00.0	25	.	.	04	02.5	.	.	01	02.0	04	01.2	07	03.0	02	01.5	23	03.0	52
XI	-	04.0	10.9	05.6	06.5	11.4	01.9	21.6	01	-02.4	13	02	01.0	.	.	.	.	.	.	06	01.5	04	04.5	01	02.0	16	04.0	61
XII	-	-00.1	04.2	01.2	01.6	04.8	-01.4	13.8	01	-07.2	27	01	02.0	.	.	.	.	02	03.0	02	01.0	04	03.8	07	03.0	23	03.6	54
GOD.	-	08.4	14.9	09.9	10.8	15.8	06.0	32.8	6 VII	-09.4	3,4 I	06	01.3	88	02.6	.	.	31	02.3	15	01.3	32	02.8	20	02.2	268	03.7	635

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤ -30,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-13) ≥ 6	F (0-13) ≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	*	∴	≡	∿	▲	▲	⊤	≡	▦
VELIKO GRADIŠTE																																					
BR. ST. 186															H_s = 79 m H_b = 80,3 m H_t = 2,0 m h_r = 1,2 m																								
I	8.4	8.6	7.0	8.0	-	03.8	84	73	80	79	47	029	006.6	08	02	07	22	.	.	.	13	03	01	19	13	08	.	00	08	.	.	.	02	.	.	.	17
II	8.7	9.1	8.3	8.7	-	04.2	88	70	84	80	43	094	017.6	04	.	02	20	.	.	.	06	03	.	20	22	16	03	12	17	05	01	.	.	.	.	02	12
III	7.4	8.1	6.1	7.2	-	05.0	82	58	75	72	26	055	015.0	16	.	.	08	.	.	.	10	07	01	13	19	11	01	15	04	.	.	.	01	01	.	.	03
IV	7.0	6.8	5.7	6.5	-	07.3	82	52	74	69	26	088	017.4	15	.	.	02	05	.	.	06	03	04	14	14	11	03	14	.	.	.	.	.	.	05	01	.
V	7.1	7.8	6.3	7.1	-	09.6	88	63	83	78	32	144	024.2	23	.	.	.	04	.	.	06	.	02	16	21	18	09	21	.	.	.	.	.	.	09	01	.
VI	5.4	5.6	5.3	5.5	-	13.4	88	61	83	77	42	091	019.0	05	.	.	.	21	02	.	03	01	04	06	19	17	02	19	.	.	.	.	.	01	11	01	.
VII	4.5	4.9	3.8	4.4	-	14.2	90	61	84	79	34	142	040.5	08	.	.	.	21	06	.	02	01	11	06	13	09	06	13	.	.	.	.	.	.	07	.	.
VIII	5.2	5.0	2.7	4.3	-	13.8	89	57	86	78	41	080	022.1	11	.	.	.	18	05	02	06	01	10	05	13	08	03	13	.	.	.	.	.	01	08	01	.
IX	5.5	4.3	2.5	4.1	-	11.0	92	55	85	77	30	027	016.7	01	.	.	02	10	04	.	02	.	08	04	07	05	01	07	.	.	.	.	.	.	03	04	.
X	6.4	5.6	4.3	5.4	-	07.5	92	62	87	81	34	057	014.9	23	.	.	01	.	.	.	05	.	08	11	11	08	03	11	.	.	.	.	.	.	.	06	.
XI	7.1	7.0	4.9	6.4	-	06.3	91	66	86	81	33	060	014.1	17	.	.	06	.	.	.	02	.	03	11	14	09	02	14	.	.	.	.	.	01	02	03	.
XII	8.2	8.2	6.5	7.6	-	04.7	90	81	87	86	55	038	007.9	26	01	01	19		.	.	07	03	02	17	18	13	.	16	07	02	.	.	.	.	.	06	05
GOD.	6.7	6.8	5.3	6.3	-	08.4	88	63	82	78	26	905	040.5	8.VII	03	10	80	79	17	02	68	22	54	142	184	133	29	163	36	07	01	.	03	04	45	25	37
ZAGUBICA																																					
BR. ST. 187															H_s = 314 m H_b = - m h_t = 2,0 m h_r = 1,5 m																								
I	9.4	8.5	8.6	8.8		037.3	03.5	85	74	81	80	46	020	003.3	02	03	09	25	.	.	.	.	02	.	22	15	05	.	08	10	01	.	.	.	.	.	03	20
II	8.9	8.9	9.4	9.1		069.8	03.9	88	71	79	80	37	062	024.7	04	03	06	21	.	.	.	.	.	.	22	23	12	01	09	17	01	.	.	.	.	.	03	18
III	8.9	8.5	8.3	8.6		111.7	04.8	88	68	76	77	18	059	019.7	05	.	01	14	.	.	.	01	01	.	22	18	11	01	11	08	.	.	.	.	.	01	.	05
IV	8.2	7.4	6.8	7.5		161.5	07.0	89	58	73	74	28	068	019.3	13	.	.	04	04	.	.	.	.	.	13	14	10	03	14	02	02	.	.	.	.	.	02	.
V	8.7	8.5	7.4	8.2		144.2	08.9	90	67	80	79	32	102	011.5	25	.	.	.	03	01	.	.	.	01	19	19	17	04	19	.	.	.	.	.	.	03	01	.
VI	5.7	6.6	4.4	5.6		-	11.5	85	59	77	74	35	080	020.3	19	.	.	.	17	.	.	01	.	03	07	14	11	02	14	.	.	.	.	.	.	05	.	.
VII	5.0	5.8	4.0	4.9		245.7	12.2	88	59	80	76	34	116	022.5	05	.	.	.	20	04	.	.	.	08	07	15	10	05	13	.	.	.	.	.	.	05	09	.
VIII	5.5	5.7	3.0	4.8		246.2	11.5	83	54	79	72	26	040	012.4	23	.	.	.	17	02	.	.	.	09	04	11	09	01	11	.	.	.	.	.	.	02	07	.
IX	5.5	5.7	3.0	4.7		190.7	08 7	87	47	78	71	22	024	019.6	01	.	.	05	09	04	.	.	.	09	07	06	03	01	06	.	.	.	.	.	.	01	13	.
X	6.3	5.8	4.8	5.7		137.5	06.0	84	55	80	73	18	037	013.0	23	.	.	05	.	.	.	.	.	08	11	12	09	01	12	.	.	.	.	.	.	.	09	.
XI	8.1	6.6	5.4	6.7		098.4	05.2	85	55	80	73	17	044	016.9	24	.	.	10	.	.	.	.	.	01	12	11	06	01	09	.	.	.	.	.	01	01	08	.
XII	8.8	8.5	7.5	8.3		033.0	04.0	84	71	82	79	33	023	004.6	04	02	04	20	.	.	.	.	.	02	19	15	07	.	11	05	01	.	.	.	.	01	03	03
GOD.	7.4	7.2	6.0	6.9		-	07.3	86	61	78	75	17	675	024.7	4.II	08	20	104	70	11	.	02	03	41	165	173	110	20	137	42	05	.	.	.	01	19	58	46
DEBELI LUG																																					
BR. ST. 188															H_s = 290 m H_b = - m h_t = 2,0 m h_r = 1,5 m																								
I	9.4	8.3	8.5	8.7	-	-	-	-	-	-	-	-	044	012.7	02	02	14	26	.	.	.	05	.	.	23	15	09	02	09	07	01	.	.	.	.	.	07	31
II	8.6	7.9	7.7	8.1	-	-	-	-	-	-	-	-	106	022.2	04	02	07	24	.	.	.	.	.	01	17	19	18	02	08	13	.	.	.	.	.	.	03	28
III	7.9	7.8	6.1	7.3	-	05.1	91	73	88	84	32	091	021.0	15	.	01	15	.	.	.	01	.	02	15	20	12	04	15	09	04	.	.	.	.	01	.	10
IV	7.7	6.6	4.8	6.4	-	07.2	88	63	83	78	36	081	019.2	09	.	.	05	03	.	.	04	.	02	11	12	10	02	12	02	02	.	.	.	01	.	-	.
V	8.4	8.1	7.2	7.9	-	08.9	91	68	92	84	27	136	022.4	25	.	.	.	02	.	.	04	01	01	17	21	19	05	21	.	.	.	.	.	.	.	07	.
VI	5.6	6.0	5.5	5.7	-	12.9	92	68	92	84	50	084	027.8	27	.	.	.	15	.	.	.	02	03	07	13	11	03	13	.	.	.	.	.	.	.	02	.
VII	4.8	6.2	4.9	5.3	-	13.2	92	66	89	83	30	232	055.8	08	.	.	.	19	01	.	04	.	06	07	12	11	08	12	.	.	.	.	.	.	04	11	.
VIII	6.6	5.4	2.6	4.9	-	13.0	93	65	91	83	44	030	006.8	26	.	.	.	17	01	.	03	.	07	06	12	09	.	12	.	.	.	.	.	.	02	08	.
IX	6.1	5.5	2.9	4.8	-	10.5	94	64	92	83	45	040	021.8	01	.	.	03	07	02	.	.	.	08	06	06	04	01	06	.	.	.	.	.	.	02	11	.
X	7.8	6.2	6.1	6.7	-	06.6	90	64	92	82	38	048	011.6	04	.	.	03	.	.	.	04	.	03	16	13	09	01	13	03	.	.	.	.	.	.	12	.
XI	8.2	6.3	4.3	6.3	-	-	-	-	-	-	-	-	059	020.3	24	.	.	13	.	.	.	02	.	04	12	11	07	02	11	.	.	.	.	.	.	.	06	.
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BOR																																					
BR. ST. 189															H_s = 180 m H_b = - m h_t = 2,0 m h_r = 1,5 m																								
I	8.7	7.9	6.8	7.8	-	-	-	-	-	-	16	028	011.0	02	27	.	.	.	.	.	.	.	03	19	11	08	01	08	04	.	.	01	.	.	.	08	18
II	7.9	7.2	8.5	7.8	-	-	-	-	-	-	-	-	069	012.6	04	01	06	19	.	.	.	.	01	14	19	12	03	08	13	.	01	.	.	.	.	03	12
III	7.9	7.1	6.2	7.0	-	-	-	-	-	-	17	086	024.2	15	.	01	12	.	.	.	.	.	04	17	16	08	04	10	10	02	01	.	.	.	.	03	05
IV	5.9	6.6	4.8	5.8	-	-	-	-	-	-	24	068	021.4	09	.	.	03	03	.	.	.	.	06	12	14	09	02	14	04	02	.	.	.	.	01	02	.
V	6.7	7.6	5.1	6.5	-	-	-	-	-	-	24	101	011.2	25	.	.	.	02	.	.	.	.	05	10	20	17	02	20	.	.	.	.	.	.	09	.	.
VI	4.6	4.9	3.2	4.3	-	-	-	-	-	-	40	068	026.6	19	.	.	.	18	.	01	.	.	07	04	10	08	02	10	.	.	.	.	.	01	08	.	.
VII	4.3	5.5	3.5	4.4	-	-	-	-	-	-	35	134	038.6	08	.	.	.	20	03	01	.	.	06	06	14	09	05	14	.	.	.	.	.	.	07	01	.
VIII	3.4	3.7	2.3	3.1	-	-	-	-	-	-	33	058	021.2	17	.	.	.	18	02	.	.	.	14	03	07	06	02	07	.	.	.	.	.	.	05	.	.
IX	2.8	3.3	1.7	2.6	-	-	-	-	-	-	27	023	014.8	01	.	.	01	10	04	.	.	.	17	02	03	03	01	03	.	.	.	.	.	.	.	.	.
X	6.0	6.0	5.0	5.7	-	-	-	-	-	-	25	050	012.2	18	-	.	-	01	.	-	.	.	09	12	14	09	02	13	03	.	.	.	.	.	.	07	01
XI	6.3	5.8	4.1	5.4	-	-	-	-	-	-	21	029	015.2	24	.	.	03	.	.	.	.	.	07	09	08	07	01	08	02	02	.	.	.	.	.	04	.
XII	6.9	6.5	5.6	6.3	-	-	-	-	-	-	24	030	008.5	23	.	01	22	.	.	.	.	.	07	15	10	08	.	06	08	02	.	.	.	.		06	08
GOD.	6.0	6.0	4.7	5.6	-	-	-	-	-	-	-	744	038.6	8.VII	-	08	-	72	09	-	.	.	86	123	146	104	25	121	44	08	02	01	.	01	30	34	44
TEKIJA																																					
BR. ST. 190															H_s = 50 m H_b = - m h_t = 2,0 m h_r = 1,2 m																								
I	9.5	8.7	8.8	9.0	-	-	-	-	-	-	-	-	055	018.6	17	.	08	28	.	.	.	02	01	.	25	06	06	03	04	02	.	.	.	.	.	.	25	17
II	9.8	8.0	8.7	8.9	-	-	-	-	-	-	-	-	090	027.0	12	.	02	21	.	.	.	03	.	.	20	18	16	02	08	11	01	.	.	.	12	.	12	21
III	8.9	7.7	6.5	7.7	-	-	-	-	-	-	-	-	074	024.0	15	.	.	.	.	.	.	03	.	.	17	13	10	03	12	02	01	.	.	.	.	.	09	01
IV	7.0	6.3	5.7	6.3	-	08.0	85	58	83	75	33	110	040.2	09	.	.	01	04	.	.	01	.	03	13	11	10	04	11	.	.	.	.	.	.	.	.	.
V	8.5	7.3	7.2	7.6	-	10.3	85	67	86	79	44	065	014.4	29	.	.	.	02	.	.	02	02	01	15	17	15	01	17	.	.	.	.	.	.	03	02	.
VI	6.7	6.1	6.6	6.5	-	14.1	86	65	87	79	47	049	008.4	10	.	.	.	19	02	.	02	01	02	07	12	12	.	12	.	.	.	.	.	.	03	.	.
VII	7.0	5.5	5.6	6.0	-	-	-	-	-	-	-	-	225	052.2	05	.	.	.	23	05	.	03	01	04	09	12	12	08	12	.	.	.	.	.	.	08	.	.
VIII	6.3	5.3	4.1	5.2	-	-	-	-	-	-	-	-	057	020.8	03	.	.	.	19	03	.	02	01	06	07	09	08	02	09	.	.	.	.	.	.	02	01	.
IX	6.3	5.2	4.4	5.3	-	11.6	89	59	84	77	34	006	004.8	01	.	.	.	13	.	.	02	.	04	07	03	01	.	03	.	.	.	.	.	.	.	13	.
X	8.9	6.0	5.5	6.8	-	-	-	-	-	-	-	-	032	010.4	02	.	.	.	.	.	02	.	.	13	08	07	01	08	.	.	.	.	.	.	.	16	.
XI	8.4	6.7	4.6	6.6	-	-	-	-	-	-	-	-	045	017.2	24	.	.	06	.	.	01	.	02	11	08	07	02	08	.	.	.	.	.	.	.	19	.
XII	8.9	7.0	6.5	7.5	-	-	-	-	-	-	-	-	069	023.2	24	.	.	17	.	.	.	02	.	02	17	08	08	02	06	03	.	.	.	.	.	.	14	08
GOD.	8.0	6.6	6.2	7.0	-	-	-	-	-	-	-	-	877	052.2	5.VII	.	10	73	80	10	.	25	06	24	161	125	112	28	110	18	02	.	.	.	12	16	111	47

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dias)	Max	Min	Max	Det.	Min	Det.	Učestina pravaca i srednja jačina vetra nD, Pm (0-12): N		NE		E		SE		S		SW		W		NW		C
												č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		j.	č.	j.	č.
NEGOTIN — φ = 44° 14' N λ = 22° 33' E Gr. ΔG = + 1h 29 min. — BR. ST 191																												
I	759.2	-02.2	00.1	-01.7	-01.4	01.1	-04.1	06.5	28	-11.6	04	.	.	02	02.0	15	01.6	14	01.4	08	01.0	10	01.6	23	03.3	12	04.6	08
II	754.9	-01.4	03.2	00.7	00.8	04.8	-02.9	17.7	10	-18.5	03	09	01.3	09	01.4	04	01.8	11	01.0	01	02.0	06	02.5	21	03.6	21	03.2	02
III	756.3	03.2	09.6	05.4	05.9	11.0	01.2	24.4	25	-05.7	03	09	01.4	09	01.6	21	02.0	05	02.0	01	02.0	06	02.2	14	04.0	25	02.9	03
IV	756.0	09.7	16.7	11.8	12.5	18.2	07.0	27.3	27	-04.0	05	17	01.8	08	01.5	12	01.4	03	02.0	02	02.5	03	02.0	19	03.6	18	03.9	08
V	756.0	13.5	19.1	14.1	15.2	20.6	10.2	29.6	11	04.1	02	07	01.3	08	01.2	08	01.6	02	02.5	04	01.2	05	01.8	26	03.0	25	03.0	08
VI	757.5	18.9	25.2	19.6	20.8	26.4	15.1	31.5	24	07.2	07,06	11	01.6	07	01.6	05	01.8	11	01.2	01	01.0	10	01.2	18	03.2	22	02.8	05
VII	756.2	19.7	26.0	20.4	21.6	27.6	16.4	33.0	23	09.6	20	09	01.4	01	01.0	18	01.1	08	01.4	.	.	03	02.3	22	03.0	26	02.7	06
VIII	756.8	18.7	26.2	19.3	20.9	27.2	14.9	32.0	07	09.1	14	16	01.5	17	01.4	11	01.3	02	01.5	02	01.0	01	01.0	15	02.9	21	02.3	08
IX	760.1	13.5	24.0	15.4	17.1	24.7	11.0	32.6	12	-01.5	30	07	01.9	09	01.3	07	01.4	09	01.7	02	01.0	01	01.0	23	02.8	24	02.8	08
X	761.2	06.5	14.9	08.6	09.7	16.0	04.5	26.2	07	-01.8	26	06	01.5	06	01.2	12	01.7	14	01.4	03	01.0	01	04.0	22	03.1	18	03.3	11
XI	759.9	05.1	11.8	05.6	07.0	12.7	01.9	25.6	01	-03.0	14,13	14	01.1	12	01.2	05	01.0	07	01.4	03	01.3	06	01.5	22	02.8	14	03.4	07
XII	762.5	01.1	04.3	02.1	02.4	05.2	-00.9	15.4	01	-08.4	22	13	01.6	05	01.4	07	01.3	06	01.2	.	.	01	03.0	27	03.5	27	03.7	07
GOD.	758.0	08.9	15.1	10.1	11.0	16.3	06.2	33.0	28.VII	-18.5	3.II	118	01.5	93	01.4	125	01.5	92	01.4	27	01.2	53	01.8	252	03.2	253	03.1	81
MITROVAC-TARA — φ = 43° 55' N λ = 19° 26' E Gr. ΔG = + 1h 18 min. — BR. ST. 192																												
I	-	-03.6	-00.8	-03.8	-03.0	01.2	-06.2	09.5	12,05	-14.0	09	.	.	40	03.0	.	.	.	.	.	.	33	03.2	.	.	.	.	20
II	-	-04.6	-01.2	-03.5	-03.2	-	-	-	-	-	-	32	02.4	22	02.4	03	02.0	11	02.3	15	02.1	01	03.0	.	.	.	.	.
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	02.7	09.1	02.9	04.4	10.9	-00.5	20.8	23	-07.0	05	42	01.8	01	01.0	.	.	01	02.0	42	01.8	.	.	.	.	.	.	04
V	-	05.1	10.1	05.8	06.7	11.3	02.8	22.0	10	-03.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	11.9	17.5	11.2	13.0	18.8	07.8	25.5	18,10	02.5	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	12.3	18.0	13.1	14.1	19.2	08.6	27.0	25	03.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	11.6	18.8	12.3	13.8	19.9	08.5	28.0	07	05.0	28,13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	07.5	16.0	08.3	10.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	02.6	08.7	03.3	04.4	09.8	00.6	18.5	10,09	-05.0	25,01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-04.5	00.8	-02.6	-02.2	02.0	-06.0	09.5	30	-12.5	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ZLATIBOR — φ = 43° 44' N λ = 19° 43' E Gr. ΔG = + 1h 17 min. — BR. ST. 193																												
I	670.1	-02.1	00.1	-01.7	-01.3	02.1	-04.2	11.6	06	-11.6	20	37	01.8	01	02.0	02	02.0	.	.	31	03.5	06	04.3	05	03.4	09	01.7	02
II	667.5	-03.8	00.0	-02.6	-02.2	01.7	-05.6	10.2	06	-15.4	18	27	01.6	.	.	01	02.0	.	.	41	04.1	07	02.9	01	01.0	07	01.7	.
III	669.3	-00.9	04.0	01.0	01.3	05.9	-02.2	16.4	27	-10.3	02	20	02.0	06	01.5	07	02.4	01	04.0	40	04.0	13	03.0	03	01.7	03	01.0	.
IV	671.4	05.4	10.2	05.6	06.7	12.4	02.7	22.0	23	-05.6	04	25	02.0	.	.	05	01.8	03	02.7	45	03.7	08	02.5	03	01.7	01	01.0	.
V	672.9	07.1	10.9	07.9	08.5	12.3	05.1	22.6	10	-02.7	01	32	02.0	07	01.9	03	01.7	03	01.0	17	02.5	15	03.3	07	02.6	06	01.7	03
VI	675.6	13.7	17.9	14.2	15.0	20.0	10.6	26.4	18,17	03.2	04	27	01.8	04	02.0	02	01.5	02	02.5	18	02.4	20	02.4	11	02.3	06	01.5	.
VII	674.7	14.3	18.5	14.9	15.6	20.0	11.5	27.5	25	05.4	18	31	01.9	14	01.8	11	01.5	03	02.0	05	02.8	15	02.7	13	02.5	.	.	01
VIII	674.8	14.9	19.7	16.1	16.7	21.2	12.1	28.6	07	06.6	28	19	02.1	10	01.8	08	01.9	04	01.5	21	02.6	23	02.3	07	02.1	01	02.0	.
IX	677.3	10.3	16.0	12.1	12.6	17.4	08.7	28.4	11	-01.9	30	25	01.7	14	01.9	08	01.8	03	02.3	13	02.9	18	02.4	06	01.3	03	01.7	.
X	676.0	04.6	09.7	06.5	06.8	11.2	02.9	19.5	07	-04.5	25	22	01.8	16	01.8	04	02.5	05	02.2	16	03.6	25	02.8	04	02.2	01	01.0	.
XI	674.5	03.2	08.3	04.5	05.1	09.7	01.3	18.2	01	-05.0	29	14	01.7	05	02.0	02	01.0	02	02.0	31	03.9	30	03.4	03	02.7	.	.	03
XII	774.7	-02.2	01.5	-00.9	-00.6	02.8	-03.5	11.2	30	-09.2	14	18	01.8	06	01.7	.	.	05	02.4	22	03.9	29	02.7	06	02.0	02	02.0	05
GOD.	681.6	05.4	09.7	06.5	07.0	11.4	03.3	28.6	7.VIII	-15.4	18.II	297	01.8	83	01.8	53	01.8	31	02.1	300	03.5	209	02.8	69	02.3	39	01.6	14
KOKIN BROD — φ = 43° 31' N λ = 19° 50' E Gr. ΔG = + 1h 19 min. — BR. ST. 194																												
I	-	-00.8	03.4	-00.2	00.6	04.9	-03.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-03.5	01.9	-01.2	-01.0	03.6	-06.0	11.2	06	-18.7	03	15	01.7	06	02.5	06	01.8	07	02.6	05	03.6	19	02.8	14	02.3	12	01.8	.
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	05.8	12.0	06.6	07.7	14.1	02.2	23.4	23	-05.5	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	09.1	14.4	10.5	11.4	16.1	05.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	15.1	20.8	15.8	16.9	22.6	10.6	29.6	22	04.3	19	11	02.1	20	02.2	07	01.9	13	01.5	05	02.0	14	02.3	08	02.2	13	01.6	02
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	10.6	19.4	12.5	13.6	21.4	07.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	04.3	12.6	06.7	07.6	13.8	02.6	23.0	10	-03.0	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-01.7	03.8	-01.0	00.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
TITOVO UŽICE — φ = 43° 52' N λ = 19° 51' E Gr. ΔG = + 1h 21 min. — BR. ST. 195																												
I	-	-01.8	02.3	-00.7	-00.2	03.4	-02.7	11.0	14	-06.5	30,20	.	.	.	.	.	.	01	02.0	.	.	04	01.5	.	.	26	01.3	62
II	-	-01.5	04.9	00.5	01.1	06.2	-02.6	15.2	05	-11.5	18	.	.	01	02.0	.	.	01	02.0	.	.	08	01.5	.	.	26	01.5	48
III	-	01.9	09.4	04.4	05.0	10.8	00.9	22.5	24	-05.2	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	07.3	15.8	09.4	10.4	17.9	04.5	27.8	24	-03.2	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	09.7	16.3	11.1	12.0	17.4	07.9	28.5	10	02.0	03,02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	15.4	23.3	16.3	17.8	24.8	12.6	32.0	18	07.5	05,03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	16.3	23.8	17.2	18.6	25.0	13.3	31.8	25	07.4	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	15.6	25.3	17.9	19.1	26.5	13.9	33.0	08	08.2	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	10.7	21.5	13.2	14.7	22.5	09.9	32.0	12	-01.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	05.0	15.2	07.4	08.7	16.1	04.1	25.2	07	-00.6	25	.	.	02	02.0	.	.	01	02.0	.	.	05	01.2	02	01.5	.	.	83
XI	-	03.4	12.3	05.4	06.6	13.2	02.1	20.5	21,01	-03.0	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-01.3	03.4	00.4	00.7	04.0	-02.1	17.2	30	-08.4	27	.	.	01	01.0	.	.	.	.	.	.	03	01.7	01	01.0	15	01.3	73
GOD.	-	06.7	14.5	08.5	09.5	15.6	05.2	33.0	8.VIII	-11.5	18.II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlim)	Insolacija broj sati	Vlažnost vazduha P_m mm	U_m % 7	14	21	Sred. (Dlim)	Min	Padavine R mm Σ	Max	Dan.	Broj dana sa: Tn ≤ -10,0	Tx ≤ 0,0	Tn < 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	P (0-12) ≥ 6	≥ 8	Nm (0-10) ≤ 2,0	≥ 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	✱	≈	▲	▲	R T	≡	▦
NEGOTIN																																				
BR. ST. 191																																				
H_a = 42 m H_b = 44,5 m h_a = 2,0 m h_b = 1,2 m																																				
I	8.3	8.5	7.8	8.2	037.3	03.5	86	79	86	84	49	023	008.0	02	02	13	29	.	.	.	10	04	03	22	07	04	.	05	04	.	.	01	.	.	.	08	27
II	8.3	7.8	6.3	7.4	073.6	04.0	87	72	83	81	46	056	012.6	12	01	05	21	.	.	.	14	07	01	15	19	13	01	08	12	.	.	01	.	.	.	06	17
III	7.5	7.5	5.5	6.8	121.0	05.1	84	59	77	73	28	074	029.7	15	.	.	10	.	.	.	17	04	02	14	14	10	02	13	05	04	.	.	.	.	.	.	01
IV	6.2	6.4	6.2	6.3	182.2	07.5	79	54	72	68	29	079	023.6	09	.	.	03	05	.	.	17	04	03	13	15	11	03	15	.	.	.	.	.	.	02	.	.
V	6.6	7.2	5.6	6.5	183.2	09.4	80	56	78	72	36	070	017.0	18	.	.	.	05	.	.	11	04	04	09	18	16	01	18	.	.	.	.	.	01	08	.	.
VI	4.8	5.8	5.0	5.2	256.0	12.5	76	52	73	67	35	031	018.1	20	.	.	.	22	08	01	09	.	04	04	10	04	01	10	.	.	.	.	.	.	08	.	.
VII	4.0	4.9	3.1	4.0	266.9	14.6	82	59	81	74	35	192	067.0	05	.	.	.	23	11	02	15	03	12	06	10	10	06	10	.	.	.	.	.	.	13	.	.
VIII	4.3	4.6	2.4	3.8	276.2	13.5	83	54	80	72	40	021	014.3	25	.	.	.	24	04	01	07	03	10	02	10	04	01	10	.	.	.	.	.	.	08	.	.
IX	2.8	3.9	0.9	2.6	242.8	10.0	82	43	75	67	31	008	006.0	01	.	.	01	14	04	.	10	.	13	01	05	02	.	05	.	.	.	.	.	.	03	.	.
X	6.6	5.6	3.9	5.4	140.9	07.0	89	60	83	77	29	052	017.2	18	.	.	04	01	.	.	13	01	06	11	08	08	01	08	02	01	.	.	.	.	.	04	01
XI	7.2	6.6	3.6	5.8	117.8	05.9	84	64	85	78	32	029	006.6	10	.	.	09	01	.	.	08	03	05	10	08	04	.	08	.	.	.	.	.	.	.	01	.
XII	6.4	6.7	6.1	6.4	075.1	04.3	83	72	82	79	41	033	010.2	23	.	.	20	.	.	.	13	04	06	15	10	06	01	08	04	.	.	.	.	.	.	08	08
GOD.	6.1	6.3	4.7	5.7	1973.0	08.1	82	60	79	74	28	668	067.0	5.VII	03	18	97	95	27	04	144	37	69	122	134	94	17	118	27	05	.	02	.	01	42	27	54
MITROVAC-TARA																																				
BR. ST. 192																																				
H_a = 1080 m H_b = - m h_a = 2,0 m h_b = 1,5 m																																				
I	9.0	8.0	5.9	7.6	032.8	03.6	91	89	91	90	63	076	017.2	02	09	13	29	.	.	.	.	.	01	17	16	12	03	06	14	.	.	.	.	.	.	15	31
II	-	-	-	-	-	-	-	-	-	-	-	136	024.3	24	-	-	-	-	-	-	.	.	-	-	19	18	05	02	18	.	.	.	.	.	03	21	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	198.3	-	-	-	-	-	-	080	035.2	29	.	01	14	.	.	.	.	.	-	-	14	13	02	09	06	01	.	.	.	.	01	02	-
V	-	-	-	-	115.4	-	-	-	-	-	-	164	022.0	18	.	01	06	.	.	.	.	.	-	-	23	22	07	19	06	02	.	.	.	.	04	03	-
VI	-	-	-	-	-	-	-	-	-	-	-	151	030.0	21	.	.	.	02	.	.	-	-	-	-	21	19	08	21	.	.	-	-	-	-	-	-	.
VII	5.0	5.0	7.6	5.9	223.6	-	-	-	-	-	35	138	039.0	06	.	.	.	04	.	.	.	.	02	07	11	09	05	11	.	.	.	.	.	.	-	02	.
VIII	5.4	5.4	9.1	6.6	202.4	-	-	-	-	-	40	069	021.0	09	.	.	.	05	.	.	.	01	.	08	09	09	03	09	.	.	.	.	.	.	01	05	.
IX	5.8	4.8	6.9	5.8	159.6	-	-	-	-	-	-	019	006.0	05	-	-	-	-	-	-	.	.	04	10	06	06	.	06	.	.	.	.	.	.	.	04	.
X	6.5	5.5	8.5	6.8	133.6	-	-	-	-	-	-	110	026.0	23	.	05	14	.	.	.	.	.	.	11	12	12	04	10	05	01	.	.	.	.	.	09	-
XI	-	-	-	-	070.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	8.0	6.8	9.9	8.3	072.0	-	-	-	-	-	-	-	-	-	05	07	28	.	.	.	-	-	.	17	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ZLATIBOR																																				
BR. ST. 193																																				
H_a = 1029 m H_b = 1028,6 m h_a = 2,0 m h_b = 2,0 m																																				
I	8.6	8.1	7.3	8.0	047.7	03.9	90	87	91	89	62	071	021.4	26	04	10	22	.	.	.	17	03	01	20	13	10	01	05	11	.	.	.	.	.	.	16	27
II	8.6	8.3	6.0	7.6	073.7	03.4	87	77	86	83	48	124	022.2	24	04	11	24	.	.	.	19	11	.	12	21	16	04	06	20	.	.	.	.	.	.	07	24
III	8.5	7.2	5.6	7.1	121.3	03.9	85	69	80	78	37	084	014.7	20	01	05	24	.	.	.	18	07	01	14	17	13	03	06	15	01	.	.	01	.	.	13	23
IV	6.5	7.4	5.1	6.3	169.8	05.4	76	62	77	72	26	083	026.9	29	.	01	12	.	.	.	19	03	01	10	12	09	02	09	06	01	.	.	.	.	01	10	.
V	7.9	8.1	6.6	7.5	135.0	06.5	85	70	83	79	30	148	019.8	29	.	.	03	.	.	.	10	01	01	14	21	18	06	17	06	.	.	.	.	02	06	16	04
VI	5.4	7.2	4.8	5.8	221.6	09.6	80	65	78	74	34	093	015.3	05	.	.	.	05	.	.	08	02	01	05	18	12	03	18	.	.	.	.	.	.	10	06	.
VII	4.4	6.4	4.2	5.0	253.2	10.5	82	70	82	78	39	094	024.7	17	.	.	.	04	.	.	09	02	04	07	12	09	04	12	.	.	.	.	.	.	05	12	.
VIII	3.9	6.4	2.9	4.4	234.5	10.5	80	65	77	74	30	076	034.2	23	.	.	.	07	.	.	11	.	06	04	11	08	02	11	.	.	.	.	.	.	07	04	.
IX	5.2	5.9	3.7	4.9	200.1	08.9	83	63	75	74	27	046	018.3	01	.	.	02	05	.	.	01	.	09	09	12	07	01	12	.	.	.	.	.	.	.	07	.
X	5.9	5.3	5.2	5.4	158.5	05.8	87	69	81	79	33	106	035.9	23	.	02	08	.	.	.	11	03	08	12	09	08	04	07	05	01	.	.	.	.	.	12	05
XI	6.2	6.0	4.2	5.5	137.4	04.8	82	64	76	74	29	086	019.9	11	.	.	15	.	.	.	16	03	04	08	10	09	04	09	06	01	.	01	.	.	.	12	05
XII	5.6	5.7	5.8	5.7	097.1	03.6	85	75	84	81	51	031	009.0	29	.	07	24	.	.	.	11	03	05	10	13	06	.	07	09	01	.	.	.	01	01	06	09
GOD.	6.4	6.8	5.1	6.1	1849.9	06.4	83	69	80	77	26	1042	035.9	15.X	09	36	134	21	.	.	150	38	41	125	169	125	34	119	78	05	.	01	01	03	30	121	99
KOKIN BROD																																				
BR. ST. 194																																				
H_a = 570 m H_b = - m h_a = 2,0 m h_b = 1,5 m																																				
I	8.0	7.6	7.7	7.8	-	-	-	-	-	-	-	076	020.5	17	-	-	-	-	-	-	01	.	-	-	12	09	03	08	07	02	.	.	.	.	.	.	-
II	7.8	8.6	6.0	7.5	-	-	-	-	-	-	-	109	021.0	15	06	10	21	.	.	.	02	.	-	10	20	15	04	10	16	05	.	.	.	.	.	.	-
III	-	-	-	-	-	-	-	-	-	-	-	094	028.0	06	-	-	-	-	-	-	02	.	-	-	15	11	03	07	13	05	.	.	.	.	.	.	-
IV	-	-	-	-	-	-	-	-	-	-	-	083	031.0	29	.	.	09	.	.	.	01	.	-	-	13	08	03	09	07	02	.	.	.	.	.	.	-
V	7.1	7.4	7.1	7.2	-	07.3	83	62	79	74	-	100	016.0	19	-	-	-	-	-	-	.	.	-	-	14	14	04	14	.	.	.	.	.	.	-	.
VI	-	-	-	-	-	-	-	-	-	-	-	094	025.9	30	-	-	-	-	-	-	.	.	-	-	16	15	02	16	.	.	.	.	.	.	-	01	.
VII	4.1	6.7	4.5	5.1	-	11.1	84	63	83	77	41	068	021.8	17	.	.	.	11	.	.	.	.	06	07	10	10	02	10	.	.	.	.	.	.	03	01	.
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	5.1	4.3	3.8	4.4	-	-	-	-	-	-	-	021	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	5.6	4.8	5.0	5.1	-	-	-	-	-	-	-	105	032.5	23	.	.	05	.	.	.	.	.	10	10	11	10	03	09	06	04	.	.	.	.	.	.	-
XI	-	-	-	-	-	-	-	-	-	-	-	098	032.2	16	-	-	-	-	-	-	.	.	-	-	10	10	04	10	04	03	.	.	.	.	.	04	.
XII	6.3	5.7	5.1	5.7	-	-	-	-	-	-	-	042	019.5	29	-	-	-	-	-	-	.	.	07	12	13	07	01	07	07	01	.	.	.	.	.	-	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
TITOVO UZICE																																				
BR. ST. 195																																				
H_a = 440 m H_b = - m h_a = 2,0 m h_b = 1,2 m																																				
I	8.5	7.1	8.3	8.0	-	04.1	91	89	92	88	46	060	014.4	24	.	05	23	.	.	.	.	.	02	18	15	10	02	09	09	03	.	.	.	.	.	11	29
II	7.3	7.4	7.3	7.3	-	04.4	92	71	91	85	45	106	018.5	01	02	03	20	.	.	.	.	.	.	11	17	15	03	10	09	01	.	.	.	.	.	03	19
III	7.7	5.8	4.6	6.0	-	-	-	-	-	-	30	094	018.8	28	.	.	08	.	.	.	.	.	05	12	20	12	04	15	10	05	.	.	.	.	.	01	03
IV	5.5	6.0	5.4	5.6	-	-	-	-	-	-	27	060	023.0	29	.	.	03	06	.	.	.	.	03	08	10	07	02	10	02	02	.	.	.	.	01	01	.
V	6.5	6.7	6.4	6.5	-	-	-	-	-	-	39	128	022.0	19	.	.	.	04	.	.	.	.	03	13	23	21	05	23	.	.	.	.	.	.	04	.	.
VI	4.1	4.8	5.8	4.2	-	-	-	-	-	-	48	146	040.2	30	.	.	.	18	04	.	01	.	07	02	21	15	06	21	.	.	.	.	.	.	08	.	.
VII	3.2	4.3	3.4	3.6	-	-	-	-	-	-	51	099	030.1	02	.	.	.	19	03	.	.	.	15	06	12	10	03	12	.	.	.	.	.	.	05	.	.
VIII	2.7	3.9	2.4	3.0	-	-	-	-	-	-	37	075	050.0	23	.	.	.	20	08	.	.	.	14	02	09	07	01	09	.	.	.	.	.	01	03	.	.
IX	4.5	4.0	3.8	4.1	-	-	-	-	-	-	48	029	010.0	01	.	.	02	13	05	.	.	.	12	06	08	05	01	08	.	.	.	.	.	.	.	.	.
X	5.3	4.7	4.6	4.8	-	-	-	-	-	-	-	095	031.0	23	.	.	01	01	.	.	.	.	11	11	12	08	03	12	02	02	.	.	.	.	.	04	01
XI	5.4	4.7	3.6	4.6	-	-	-	-	-	-	40	056	016.0	11	.	.	04	.	.	.	.	.	10	07	11	10	01	11	.	.	.	.	.	.	.	03	.
XII	6.8	6.3	7.3	6.8	-	04.4	93	81	91	88	47	018	005.6	26	.	09	22	.	.	.	.	.	03	14	11	07	.	08	04	.	.	.	.	.	.	05	06
GOD.	5.6	5.5	5.1	5.4	-	-	-	-	-	-	-	964	050.0	13.VII	02	17	83	81	22	.	01	.	85	110	169	127	31	148	36	13	.	.	.	01	21	28	58

Mesec	Vazdušni pritisak Pm mm	[redacted] °C										Čestina pravaca i srednja jačina vetra nO, Fm (0-12)																	
		Tm										N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dies)	Min	Min	Max	Dat.	Min	Dat.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		j.	č.	j.	č.
SJENICA φ = 43° 16' N λ = 20° 01' E Gr. Δ G = + 1h 20 min. BR. ST. 196																													
I	672.3	-03.7	-00.3	-02.6	-02.3	01.3	-06.1	10.2	07	-20.6	30	17	02.0	06	01.7	03	02.0	14	02.1	08	02.1	10	02.9	01	04.0	06	02.0	28
II	669.5	-04.5	00.2	-02.7	-02.4	02.3	-07.3	10.3	05	-23.6	18	18	01.7	02	02.0	04	01.2	06	02.3	02	01.5	20	03.6	06	03.8	10	01.9	16
III	671.3	-01.6	04.0	00.4	00.8	05.4	-03.4	15.3	27	-14.9	02	12	02.5	03	02.3	03	02.0	16	02.4	14	02.4	18	02.9	03	02.7	04	02.2	20
IV	673.4	04.0	10.6	05.6	06.5	11.9	01.0	21.6	23	-08.1	13	14	02.1	02	01.0	03	02.0	05	01.8	12	02.7	18	03.7	08	02.9	10	02.3	18
V	674.5	06.5	11.6	07.7	08.4	13.1	04.0	22.3	10	-02.4	26	17	02.5	05	02.2	06	01.7	06	01.5	07	01.6	11	02.7	05	03.4	25	02.4	11
VI	677.2	11.3	18.4	12.8	13.8	20.2	07.6	25.2	17	01.6	05	18	02.1	13	02.2	04	01.0	03	01.3	09	01.6	08	02.9	07	01.7	09	02.3	19
VII	676.3	12.6	19.8	13.8	15.0	21.3	08.8	28.3	22	03.6	28	15	02.5	10	02.4	03	02.0	06	01.5	04	01.2	10	03.0	06	02.3	14	02.0	25
VIII	676.6	11.0	21.0	13.9	15.0	22.7	08.1	29.7	07	01.4	28	14	02.4	03	02.3	07	01.4	08	01.8	09	01.4	09	02.2	02	04.0	14	02.4	27
IX	678.9	06.4	18.2	09.2	10.8	19.1	04.0	29.1	11	-09.3	30	18	02.1	09	02.6	08	01.1	03	01.0	03	01.0	02	03.0	03	02.0	17	02.1	27
X	677.9	02.5	11.3	04.6	05.8	12.5	00.3	21.1	10,09	-04.8	25	21	01.7	05	02.8	06	01.5	12	01.5	05	02.0	07	02.3	10	02.3	13	02.3	14
XI	676.5	00.4	09.2	03.0	03.9	10.5	-01.4	20.0	03,01	-06.6	12	11	01.9	08	01.6	05	01.0	07	01.4	06	01.8	18	02.5	06	02.8	09	01.9	20
XII	676.7	-03.6	02.3	-02.1	-01.4	03.4	-05.5	10.4	30	-13.5	21	16	02.2	05	01.6	05	01.4	15	02.1	05	02.6	11	02.8	02	03.5	09	02.4	25
GOD.	675.1	03.4	10.5	05.3	06.2	12.0	00.8	29.7	44.IX	-23.6	18.II	191	02.1	71	02.1	57	01.4	101	01.9	84	02.0	142	03.0	59	02.7	140	02.2	250
UZIČKA POŽEGA φ = 43° 51' N λ = 20° 02' E Gr. Δ G = + 1h 20 min. BR. ST. 197																													
I	733.0	-03.1	00.5	-01.6	-01.4	02.2	-04.5	08.3	14	-16.8	09	06	01.7	09	01.3	07	01.6	03	01.0	02	01.0	02	02.0	09	02.1	36	01.6	19
II	729.9	-02.2	03.0	-00.1	00.2	05.3	-03.9	14.9	10	-16.6	18	06	02.0	08	01.5	05	01.8	04	01.8	01	01.0	06	02.8	15	02.1	27	01.7	12
III	731.0	01.7	09.7	04.8	05.3	11.2	00.2	22.4	27,24	-05.2	02	04	01.8	12	01.9	12	02.8	07	02.6	01	03.0	09	03.3	11	02.3	24	01.8	13
IV	732.0	06.4	16.3	10.3	10.8	18.0	04.2	27.7	24	-04.6	05	07	02.3	06	01.5	09	02.3	05	03.0	02	04.0	09	03.2	14	02.9	29	02.1	09
V	733.1	09.3	16.5	12.0	12.4	18.0	07.5	28.2	11,10	0[illegible].8	03	07	02.4	10	01.9	09	02.2	05	02.0	03	02.0	02	03.5	14	02.4	22	02.0	21
VI	734.6	14.3	23.1	17.2	17.9	24.8	12.5	31.8	18	06.0	06	06	02.0	19	02.2	05	02.8	03	02.7	02	02.0	01	03.0	07	01.9	15	01.7	32
VII	733.6	14.7	24.3	17.9	18.7	25.5	13.5	31.8	25	06.8	19	08	01.9	11	01.5	11	02.5	01	03.0	.	.	08	01.8	10	02.5	26	01.6	18
VIII	733.5	15.0	25.4	17.9	19.1	27.0	13.5	34.2	08	09.2	13	03	01.0	09	01.6	15	02.0	09	02.4	02	01.0	02	01.5	08	01.6	24	01.8	21
IX	737.1	11.0	21.2	13.0	14.6	22.8	09.8	32.6	11	-02.4	30	03	02.3	03	01.3	05	01.6	11	02.1	02	02.0	03	02.0	08	01.6	24	01.3	31
X	737.1	05.2	15.4	07.5	08.9	16.5	03.6	25.9	07	-01.8	25	05	02.2	09	01.6	07	02.0	04	01.2	01	02.0	02	03.0	22	01.4	13	01.6	30
XI	735.7	02.6	11.1	04.9	05.8	12.5	01.1	21.0	01	-09.4	13,12	03	01.3	10	01.5	08	01.6	03	02.0	01	02.0	10	02.1	11	01.7	24	01.7	20
XII	737.7	-01.1	02.4	00.4	00.5	03.5	-02.5	18.3	30	-11.2	27	08	01.8	06	01.5	01	01.0	08	01.6	02	02.0	06	02.3	12	01.6	28	01.5	22
GOD.	734.0	06.2	14.1	08.7	09.4	15.6	04.6	34.2	8.VIII	-16.6	18.II	66	02.0	112	01.7	94	02.1	63	02.1	19	02.0	60	02.6	141	02.0	292	01.7	248
IVANJICA φ = 43° 35' N λ = 20° 14' E Gr. Δ G = + 1h 21 min. BR. ST. 198																													
I	-	-01.5	03.4	-00.2	00.4	04.7	-03.7	16.8	06	-10.2	24	25	01.7	01	01.0	13	01.7	08	02.5	01	08.0	01	01.0	05	03.2	10	02.0	29
II	-	-01.4	05.0	00.6	01.2	06.6	-03.5	16.5	06	-13.8	18	18	01.8	04	01.2	17	01.5	04	02.2	01	05.0	02	01.0	06	02.2	14	02.3	18
III	-	02.3	09.4	04.2	05.0	10.8	00.2	21.8	25	-05.3	21	18	01.4	08	01.5	26	01.9	04	03.5	01	05.0	02	01.5	02	01.0	13	02.1	19
IV	-	06.8	16.0	08.9	10.1	17.6	04.2	26.7	23	-02.4	05	19	01.8	03	01.3	27	01.9	06	02.3	03	04.3	01	02.0	02	02.5	09	02.8	20
V	-	10.0	16.1	10.4	11.7	17.4	07.4	28.6	10	0[illegible].6	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	14.5	23.0	15.4	17.1	25.1	11.1	32.5	18	06.5	02	09	01.2	05	01.8	24	01.4	05	02.2	03	03.0	01	03.0	02	02.0	04	02.2	37
VII	-	14.6	23.7	16.6	17.9	25.2	12.7	32.6	25	07.6	19	16	02.1	08	01.5	24	02.0	04	02.2	03	02.3	.	.	.	.	08	02.0	30
VIII	-	14.3	25.9	16.6	18.3	26.8	12.6	33.6	07	07.0	28	05	01.8	16	01.6	20	01.8	06	02.8	03	01.7	01	02.0	03	01.3	02	01.5	37
IX	-	10.4	21.6	12.0	14.0	22.5	08.8	34.7	11	-02.0	30,29	11	02.0	06	01.2	22	01.9	03	02.0	04	01.8	03	01.3	04	01.5	03	02.3	34
X	-	05.3	15.0	07.1	08.6	16.1	03.6	25.8	07	-01.1	25	19	01.7	05	01.6	29	02.1	02	04.0	.	.	.	.	01	01.0	06	02.0	31
XI	-	03.1	11.7	04.9	06.2	13.0	00.9	20.8	03	-04.0	29	10	01.7	11	01.5	23	01.7	05	02.2	02	02.0	.	.	01	02.0	03	01.7	35
XII	-	-00.8	03.6	00.5	01.0	05.2	-02.9	17.7	30	-10.5	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	06.5	14.5	08.1	09.3	15.9	04.3	34.7	44.IX	-13.8	18.II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BELE VODE-GOLIJA φ = 43° 25' N λ = 20° 17' E Gr. Δ G = + 1h 21 min. BR. ST. 199																													
I	-	-03.2	-00.1	-03.3	-02.4	01.9	-05.9	09.0	06	-17.0	19	12	01.4	01	01.0	13	01.5	02	01.5	19	01.8	04	01.5	25	01.4	05	01.2	12
II	-	-05.4	-01.8	-04.3	-03.9	00.1	-07.3	07.0	10,05	-15.9	18	09	01.3	.	.	14	01.7	01	01.0	15	01.6	04	02.0	34	01.7	06	01.3	11
III	-	-02.5	02.2	-01.1	-00.6	03.9	-04.6	14.0	25	-14.0	02	07	01.4	03	01.0	18	01.7	04	01.2	22	01.9	04	01.5	24	01.2	07	01.6	04
IV	-	03.3	07.7	02.6	04.1	09.3	-00.5	19.0	23	-09.5	04	09	01.1	.	.	10	01.3	05	01.2	20	01.9	04	01.5	27	01.4	07	01.4	08
V	-	04.7	08.1	04.6	05.5	09.8	01.8	20.3	10	-06.0	02	15	01.3	02	01.0	11	01.2	01	01.0	18	01.4	.	.	30	01.5	11	01.2	05
VI	-	11.4	15.5	10.6	12.0	17.1	07.1	24.0	10	-01.5	07	05	01.2	01	01.0	09	01.1	01	01.0	13	01.2	06	02.0	26	01.3	18	01.2	11
VII	-	12.7	16.3	11.8	13.1	18.1	08.8	25.0	22	03.0	18	16	01.2	03	01.3	11	01.1	.	.	18	01.4	01	01.0	33	01.4	04	01.0	07
VIII	-	13.7	17.9	12.3	14.1	19.4	09.5	26.0	07	05.0	28	25	01.2	01	01.0	09	01.0	.	.	17	01.3	01	01.0	18	01.2	06	01.5	16
IX	-	08.8	14.5	08.6	10.1	16.2	05.5	28.0	13	-05.0	29	22	01.0	07	01.1	11	01.0	01	01.0	09	01.6	.	.	12	01.0	16	01.3	12
X	-	03.4	08.4	03.2	04.6	09.7	00.4	19.0	09	-07.0	25	17	01.0	04	01.0	13	01.2	01	01.0	20	01.2	02	01.0	20	01.2	08	01.2	08
XI	-	01.5	07.0	02.4	03.3	09.1	-01.3	19.0	01	-06.4	12	11	01.3	03	01.0	08	01.2	01	02.0	24	01.5	03	01.7	14	01.2	11	01.6	15
XII	-	-03.1	01.4	-02.5	-01.7	03.3	-05.5	10.0	13	-12.5	16	14	01.1	01	01.0	20	01.2	.	.	22	01.5	01	02.0	17	01.3	02	01.5	16
GOD.	-	03.8	08.1	03.7	04.8	09.8	00.7	28.0	49.IX	-17.0	49. I	162	01.2	26	01.1	147	01.3	17	01.2	217	01.5	30	01.6	280	01.4	101	01.3	115
ČAČAK φ = 43° 54' N λ = 20° 21' E Gr. Δ G = + 1h 21 min. BR. ST. 200																													
I	-	-01.3	01.8	-00.8	-00.3	02.9	-04.4	13.5	16	-10.0	03	01	02.0	02	01.0	01	01.0	01	03.0	.	.	01	02.0	04	01.8	06	01.3	77
II	-	-01.0	03.7	00.0	00.7	05.0	-04.1	16.0	09	-13.0	18	03	01.0	.	.	.	.	.	.	03	01.7	03	01.0	10	02.1	02	01.5	63
III	-	02.5	09.6	04.8	05.5	11.0	00.1	22.0	27	-06.1	03	03	01.0	04	01.2	13	02.5	01	03.0	04	01.8	08	01.2	07	01.6	04	02.0	49
IV	-	08.3	16.4	10.3	11.3	18.3	04.5	28.0	24	-04.7	05	02	02.0	02	01.5	09	01.8	.	.	06	01.7	08	03.5	02	02.0	07	01.6	54
V	-	11.4	16.8	11.6	12.9	18.4	07.4	28.9	11	01.5	02	04	01.5	.	.	03	02.3	.	.	.	.	10	01.8	10	02.1	04	01.8	62
VI	-	17.4	23.7	16.2	18.4	25.0	12.2	30.5	17	06.7	06	01	01.0	02	01.5	02	01.8	01	01.0	02	01.0	13	01.2	01	01.0	06	01.0	62
VII	-	17.8	24.6	17.3	19.2	25.8	13.1	32.0	23	07.6	20	04	01.2	03	01.7	03	01.3	01	01.0	.	.	02	01.0	06	03.0	04	01.0	70
VIII	-	18.9	25.8	17.3	19.8	26.7	13.0	32.8	08	07.8	28	02	01.0	02	02.0	06	01.2	02	01.0	.	.	03	01.3	04	01.5	03	01.3	71
IX	-	12.3	21.4	13.5	15.2	22.7	09.3	-	-	-	-	01	02.0	02	01.0	03	01.3	.	.	.	.	02	01.5	01	02.0	04	01.2	77
X	-	06.5	15.2	08.6	09.7	16.4	04.0	25.2	11	-01.5	25	.	.	02	01.5	02	01.5	.	.	.	.	09	01.6	06	02.3	01	01.0	73
XI	-	04.3	11.6	05.5	06.7	13.0	01.6	20.4	21	-02.6	12	.	.	.	.	01	02.0	01	01.0	.	.	03	01.7	01	02.0	.	.	84
XII	-	00.2	04.3	01.2	01.7	05.1	-02.1	19.2	30	-08.3	21	02	01.0	04	01.8	01	01.0	.	.	02	01.5	04	02.2	05	02.4	01	01.0	74
GOD.	-	08.1	14.6	08.8	10.1	15.9	04.6	-		-		23	01.3	23	01.5	44	01.8	07	01.6	17	01.6	66	01.7	57	02.1	42	01.4	816

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e mm	Um % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana n sa: Tn ≤0,0	Tx ≤0,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) ≤2,0	≤8,0	R mm ≥0,1	≥1,0	≥10,0	●	⚲	✱	✱	≈	▲	▲	⊤	≡	≡
SJENICA																																					
BR. ST. 196																																					
H_s = 1015 m H_b = 1016,2 m h_s = 2,0 m h_v = 1,5 m																																					
I	8.1	8.7	8.3	8.4	034.9	03.7	90	83	90	88	67	091	023.3	02	09	14	25	.	.	.	02	01	01	22	13	09	05	06	10	.	.	01	.	.	.	19	24
II	7.8	8.3	6.3	7.5	094.5	03.3	84	71	83	79	47	080	017.3	16	08	11	22	.	.	.	15	08	.	10	18	11	02	08	15	02	.	.	.	.	.	05	21
III	8.5	6.8	5.4	6.9	136.1	03.8	84	66	78	76	37	057	023.0	06	04	04	23	.	.	.	14	03	01	14	18	06	02	08	15	01	.	.	02	.	.	03	18
IV	6.8	7.8	5.2	6.6	175.4	05.0	80	54	74	70	28	078	026.0	15	.	.	11	.	.	.	18	05	01	10	13	06	04	12	04	03	.	01	.	.	.	01	04
V	7.6	8.0	5.4	7.0	154.5	06.2	84	63	79	75	35	073	012.7	23	.	.	04	.	.	.	12	01	02	11	22	16	02	18	07	02	.	01	.	.	04	02	02
VI	5.3	7.0	4.0	5.4	214.5	09.1	87	60	82	76	35	094	015.3	21	.	.	.	03	.	.	09	01	03	06	18	09	02	16	.	.	.	.	.	.	11	13	.
VII	4.8	5.6	3.7	4.7	267.8	09.9	88	59	85	77	30	052	018.4	17	.	.	.	06	.	.	08	01	10	07	12	06	02	09	.	.	.	.	.	.	07	11	.
VIII	5.6	6.0	2.0	4.5	229.4	09.5	93	51	84	76	31	048	022.5	03	.	.	.	11	.	.	10	.	04	02	09	06	02	08	.	.	.	.	.	01	09	19	.
IX	5.6	4.5	2.1	4.1	220.1	07.3	94	48	83	75	16	025	008.9	01	.	.	06	08	.	.	03	.	08	03	11	06	.	08	.	.	.	.	.	.	03	14	.
X	5.9	5.3	5.5	5.6	159.9	05.4	90	60	88	79	24	089	033.6	23	.	.	15	.	.	.	08	.	08	11	15	08	05	09	05	.	.	.	.	.	.	11	09
XI	6.2	5.8	3.9	5.3	147.2	04.6	90	60	80	76	25	059	022.1	16	.	.	18	.	.	.	09	01	07	07	11	09	01	10	05	.	.	01	.	02	04	02
XII	6.2	6.0	5.4	5.8	107.8	03.5	86	70	85	80	36	034	013.4	29	07	07	24	.	.	.	08	01	06	09	10	06	01	06	06	.	.	01	.	.	03	09
GOD.	6.5	6.6	4.8	6.0	1942.1	05.9	87	62	82	77	16	740	033.6	23.X	28	36	148	28	.	.	116	22	51	112	170	98	28	118	67	08	.	03	04	01	34	96	81
UŽIČKA POŽEGA																																					
BR. ST. 197																																					
H_s = 311 m H_b = 312,1 m h_s = 2,0 m h_v = 1,5 m																																					
I	9.4	7.8	8.0	8.4	021.4	03.7	91	79	90	87	55	057	009.2	26	03	07	28	.	.	.	.	.	.	20	17	09	.	09	10	02	.	.	.	.	.	14	31
II	8.6	7.6	6.5	7.6	050.6	03.9	90	68	87	82	36	095	015.8	24	02	04	23	.	.	.	02	02	.	14	19	16	03	09	11	.	.	.	.	.	01	09	19
III	8.9	7.0	5.8	7.3	112.2	04.7	87	54	78	73	23	092	016.3	20	.	.	12	.	.	.	05	02	01	15	18	09	05	12	09	01	.	.	01	.	.	02	02
IV	7.7	6.9	5.8	6.8	144.5	06.2	86	45	69	66	20	054	017.2	29	.	.	04	05	.	.	02	02	.	12	08	04	03	08	02	.	.	.	.	.	.	04	.
V	8.7	7.9	6.7	7.8	116.7	08.2	90	59	82	77	30	144	026.0	19	.	.	.	04	.	.	01	01	.	13	24	18	04	23	01	01	.	.	.	.	09	06	.
VI	8.0	6.0	4.7	6.2	180.4	12.1	93	59	84	79	33	124	019.6	27	.	.	.	19	04	.	04	01	.	11	20	14	07	19	.	.	.	.	.	.	14	16	.
VII	9.1	5.2	4.1	6.1	209.7	12.7	95	57	86	79	37	108	049.4	02	.	.	.	20	05	.	.	.	01	08	12	08	03	11	.	.	.	.	.	.	05	23	.
VIII	8.4	5.5	3.6	5.8	182.2	13.2	96	56	90	80	35	076	033.3	23	.	.	.	20	08	.	02	02	01	04	09	07	02	09	.	.	.	.	.	01	08	21	.
IX	9.6	5.2	3.5	6.1	143.3	10.5	97	56	92	82	25	041	026.8	01	.	.	02	12	05	.	.	.	01	08	20	04	01	13	.	.	.	.	.	.	01	20	.
X	9.2	5.2	4.9	6.4	113.2	06.9	96	56	89	81	33	096	034.6	23	.	.	02	02	.	.	.	.	01	13	23	08	03	12	02	01	.	.	.	.	.	14	01
XI	8.7	6.1	4.9	6.6	084.6	05.7	95	64	89	82	39	043	011.2	11	.	.	10	.	.	.	.	.	01	10	18	08	01	12	.	.	.	.	.	.	.	13	.
XII	8.9	7.7	8.3	8.3	031.6	04.2	94	80	90	86	35	019	005.4	26	01	10	25	.	.	.	.	.	.	20	13	07	.	08	04	.	.	.	.	.	.	15	08
GOD.	8.8	6.5	5.6	7.0	1390.4	07.7	92	61	85	79	20	949	049.4	2.VII	06	21	106	82	22	.	16	10	06	148	201	112	32	145	39	05	.	.	01	01	38	157	61
IVANJICA																																					
BR. ST. 198																																					
H_s = 465 m H_b = - m h_s = 2,0 m h_v = 1,5 m																																					
I	7.7	7.4	7.6	7.6	-	-	-	-	-	-	-	080	023.4	02	01	06	24	.	.	.	01	01	01	18	17	12	03	08	11	01	.	.	.	.	.	06	-
II	7.8	7.6	6.9	7.4	-	04.4	88	77	87	84	42	120	016.0	24	04	04	19	.	.	.	.	.	.	12	21	18	04	12	10	.	.	.	.	.	.	05	15
III	7.7	6.3	6.2	6.7	-	04.9	84	61	81	75	32	107	034.4	20	.	.	15	.	.	.	02	01	03	11	16	08	04	13	07	03	.	.	.	.	.	06	03
IV	6.1	7.1	5.5	6.2	-	06.5	80	50	80	70	23	069	024.0	15	.	.	04	05	.	.	04	01	03	11	11	06	03	10	04	01	.	.	.	.	01	01	-
V	6.9	7.6	6.3	7.0	-	08.2	85	64	87	79	31	191	049.3	19	.	.	.	04	.	.	.	.	-	-	24	19	08	24	.	.	.	.	.	.	05	04	.
VI	5.4	6.3	4.3	5.4	-	-	-	-	-	-	-	104	027.4	27	.	.	.	18	04	.	.	.	05	09	15	14	04	15	.	.	.	.	.	.	06	01	.
VII	4.1	5.8	4.4	4.7	-	12.6	90	63	90	81	40	118	031.1	07	.	.	.	20	06	.	.	.	09	08	11	11	04	11	.	.	.	.	.	.	02	07	.
VIII	3.9	4.6	3.6	4.1	-	12.7	91	56	91	79	29	029	007.9	09	.	.	.	21	08	.	.	.	10	03	10	07	.	10	.	.	.	.	.	01	05	02	.
IX	5.5	5.0	3.3	4.6	-	10.0	92	58	91	80	23	026	007.4	05	.	.	02	12	05	.	.	.	10	07	12	05	.	12	.	.	.	.	.	.	02	10	.
X	6.1	4.7	5.3	5.4	-	06.9	93	61	91	82	30	116	034.2	23	.	.	02	01	.	.	.	.	07	10	11	10	05	10	02	.	.	.	.	.	.	08	02
XI	6.4	5.2	4.3	5.3	-	05.8	91	62	88	80	44	089	028.0	24	.	.	10	.	.	.	.	.	05	07	12	08	03	11	.	.	.	.	.	.	01	04	.
XII	7.1	6.4	7.2	6.9	-	-	-	-	-	-	-	027	007.4	02	01	07	23	.	.	.	02	02	04	14	11	06	.	06	07	01	.	.	.	.	.	05	07
GOD.	6.2	6.2	5.4	5.9	-	-	-	-	-	-	-	1076	049.3	19.V	06	17	99	81	23	.	09	05	-	-	171	124	38	142	41	06	.	.	.	01	22	61	-
BELE VODE-GOLIJA																																					
BR. ST. 199																																					
H_s = 1500 m H_b = - m h_s = 2,0 m h_v = 1,2 m																																					
I	6.1	7.0	5.8	6.3	060.0	03.7	92	83	91	89	48	104	027.0	02	08	10	24	.	.	.	.	.	03	13	13	11	03	04	11	02	.	.	.	.	.	03	31
II	7.9	7.7	7.3	7.6	058.9	-	-	-	-	-	-	137	024.0	24	13	12	25	.	.	.	.	.	.	14	22	19	03	.	22	.	.	.	.	.	.	.	20
III	7.7	6.3	4.6	6.3	101.0	03.5	85	71	82	79	36	070	015.0	29	04	07	26	.	.	.	.	.	04	11	16	14	03	04	14	.	.	.	.	.	.	08	31
IV	5.6	6.5	5.8	6.0	162.6	-	-	-	-	-	-	104	026.5	15	.	03	13	.	.	.	.	.	04	08	12	09	04	07	07	.	.	.	.	.	.	04	13
V	7.5	7.3	6.0	6.9	123.3	05.5	84	71	89	81	37	253	075.2	19	.	02	10	.	.	.	.	.	.	13	21	19	08	14	09	01	.	.	.	01	-	10	08
VI	5.8	5.7	4.0	5.2	191.1	08.3	81	64	85	77	37	112	026.3	01	.	.	01	.	.	.	.	.	05	06	17	17	03	17	.	.	.	.	.	.	03	07	.
VII	3.9	5.7	3.5	4.4	232.7	09.3	81	71	89	80	46	104	026.4	07	.	.	.	01	.	.	.	.	11	08	11	11	04	11	.	.	.	.	.	.	-	10	.
VIII	4.0	4.9	4.1	4.3	210.6	-	-	-	-	-	-	054	015.0	03	.	.	.	03	.	.	.	.	08	06	08	07	03	08	.	.	.	.	.	.	03	06	.
IX	5.1	4.7	3.8	4.5	165.3	07.6	87	65	86	79	22	026	010.0	05	.	.	06	06	.	.	.	.	09	07	08	08	01	08	.	.	.	.	.	.	.	08	.
X	5.6	5.0	5.4	5.3	149.7	-	-	-	-	-	-	134	030.6	23	.	06	17	.	.	.	.	.	09	10	11	10	05	06	08	.	.	.	.	.	.	09	08
XI	5.2	4.7	2.8	4.2	-	04.5	84	67	82	78	26	101	024.0	24	.	01	18	.	.	.	.	.	09	05	10	10	03	04	07	.	.	.	.	.	.	06	11
XII	6.9	5.4	4.9	5.8	-	-	-	-	-	-	-	056	019.0	04	06	06	28	.	.	.	.	.	05	08	10	10	01	03	08	01	.	.	.	.	.	07	20
GOD.	5.9	5.9	4.8	5.6	-	-	-	-	-	-	-	1255	075.2	19.V	31	47	168	10	.	.	.	.	67	109	159	145	41	86	86	04	.	.	.	01	-	77	150
ČAČAK																																					
BR. ST. 200																																					
H_s = 240 m H_b = - m h_s = 2,0 m h_v = 1,0 m																																					
I	7.6	7.8	6.7	7.4	-	04.0	86	82	85	85	56	064	014.6	17	01	08	26	.	.	.	.	.	03	18	17	08	02	11	08	02	.	.	.	.	.	07	18
II	7.0	7.4	6.5	7.0	-	-	-	-	-	-	-	094	017.3	01	03	05	24	.	.	.	.	.	02	10	16	14	04	11	08	02	.	.	.	.	.	05	16
III	7.9	6.9	5.0	6.6	-	05.0	81	60	78	73	28	073	019.0	20	.	.	15	.	.	.	.	.	02	15	14	08	04	12	05	03	.	.	.	.	.	.	-
IV	6.0	6.4	5.3	5.9	-	06.8	79	52	71	67	30	060	020.1	15	.	.	03	05	.	.	01	.	07	11	10	05	03	10	01	01	.	.	.	.	02	01	.
V	7.3	7.4	5.1	6.6	-	08.6	80	64	84	76	29	153	023.5	19	.	.	.	04	.	.	.	.	02	12	23	21	06	23	.	.	.	.	01	.	04	03	.
VI	4.7	6.1	3.4	4.7	-	12.7	79	63	88	77	42	140	033.4	24	.	.	.	20	03	.	.	.	04	06	20	17	04	20	.	.	.	.	.	01	10	01	.
VII	4.3	5.1	3.6	4.3	-	13.3	83	62	87	77	46	081	019.3	17	.	.	.	20	06	.	.	.	09	06	11	10	04	11	.	.	.	.	.	.	05	01	.
VIII	3.9	5.2	2.0	3.7	-	13.8	82	59	89	77	37	049	021.1	23	.	.	.	20	07	.	.	.	12	04	08	06	02	08	.	.	.	.	.	.	08	03	.
IX	4.9	5.1	1.8	3.9	-	10.8	92	59	89	80	-	024	016.6	01	-	-	-	-	-	-	.	.	13	05	09	04	01	09	.	.	.	.	.	.	02	03	.
X	5.6	4.9	5.4	5.3	-	07.3	90	60	87	79	32	098	036.2	23	.	.	01	01	.	.	.	.	09	10	12	07	03	12	.	.	.	.	.	.	.	05	.
XI	6.4	6.0	4.1	5.5	-	06.2	90	67	89	82	44	051	010.2	11	.	.	10	.	.	.	.	.	04	09	13	11	01	13	.	.	.	.	.	.	.	-	.
XII	7.4	7.7	7.5	7.5	-	04.5	86	76	88	83	40	013	002.9	26	.	03	25	.	.	.	.	.	03	18	09	06	.	08	03	01	.	.	.	.	.	03	05
GOD.	6.1	6.3	4.7	5.7	-	-	-	-	-	-	-	900	036.2	23.X	-	-	-	-	-	-	01	.	70	124	162	117	34	148	25	09	.	.	01	01	31	-	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dies)	M̄ax	M̄in	Max	Dat.	Min	Dat.	Cestina pravaca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
φ = 43° 08' N λ = 20° 31' E Gr. ΔG = + 1h 21 min. NOVI PAZAR BR. ST 201																												
I	-	-02.2	02.4	-00.7	-00.3	03.9	-03.8	13.5	16	-14.5	30	04	01.2	05	01.8	.	.	02	03.0	.	.	04	01.5	01	01.0	01	02.0	76
II	-	-02.8	04.1	-00.4	00.1	05.8	-04.2	14.5	10	-16.7	18	01	01.0	02	01.0	.	.	.	.	02	01.0	08	01.9	01	01.0	02	02.0	68
III	-	01.3	09.3	03.8	04.6	10.9	-00.5	21.0	25,24	-07.0	03	.	.	09	01.7	.	.	04	02.5	.	.	08	03.6	08	01.4	03	03.3	61
IV	-	06.9	15.7	08.2	09.8	16.7	03.0	26.8	24	-06.5	05	01	02.0	04	02.0	.	.	11	03.5	01	01.0	11	05.0	.	.	10	02.0	52
V	-	09.5	16.3	09.9	11.4	17.8	05.3	27.0	11,10	-02.2	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	14.5	23.1	15.0	16.9	24.5	09.4	31.5	18	04.0	05	01	01.0	14	01.5	.	.	02	02.5	.	.	06	01.7	01	02.0	08	01.2	58
VII	-	16.3	24.2	16.3	18.3	25.5	10.2	32.0	22	03.5	19	.	.	15	01.5	.	.	01	07.0	.	.	05	02.8	.	.	06	01.5	66
VIII	-	15.2	25.7	16.4	18.4	26.9	11.1	33.5	07	04.5	28	.	.	17	01.7	.	.	03	01.0	.	.	04	03.2	01	01.0	06	01.2	62
IX	-	10.6	21.9	11.8	14.0	22.6	07.2	32.6	11	-04.8	30	.	.	27	01.5	.	.	.	.	.	.	.	.	.	.	07	01.6	56
X	-	05.1	15.5	07.8	09.0	16.3	02.9	24.6	09	-03.0	01	.	.	07	02.1	.	.	06	02.8	.	.	05	02.8	.	.	13	01.6	62
XI	-	01.5	10.5	03.7	04.9	11.3	00.0	21.0	03	-05.0	12	.	.	04	01.2	.	.	02	01.5	.	.	04	02.5	01	01.0	03	02.3	76
XII	-	-02.0	05.4	00.2	01.0	06.1	-03.6	15.0	30	-10.6	21	.	.	03	01.7	.	.	04	03.5	.	.	08	02.1	01	01.0	09	01.7	68
GOD.	-	06.2	14.5	07.7	09.0	15.7	03.1	33.5	7.VIII	-16.2	18 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 43° 44' N λ = 20° 41' E Gr. ΔG = + 1h 23 min. KRALJEVO BR. ST. 202																												
I	741.8	-00.5	02.9	01.2	01.2	04.1	-01.9	13.6	16	-08.0	03	.	.	.	.	32	03.9	.	.	.	.	.	.	05	02.2	03	02.0	52
II	738.5	-00.8	04.8	01.7	01.8	06.7	-02.4	18.3	10	-11.1	03	.	.	.	.	11	02.5	.	.	.	.	03	02.7	15	02.3	03	02.0	52
III	739.7	03.1	10.3	06.4	06.5	11.7	01.9	24.0	25	-03.7	02	02	02.0	03	02.0	24	04.5	02	03.5	06	02.2	01	02.0	02	02.0	04	02.0	49
IV	740.4	09.3	16.9	11.6	12.3	18.7	06.2	28.7	26	-01.7	05	03	02.0	02	02.0	17	02.8	04	03.8	04	02.8	02	02.5	11	01.9	04	02.0	43
V	741.2	11.1	17.1	12.7	13.4	18.9	08.5	29.8	11	00.2	03	03	03.0	.	.	08	02.6	04	02.5	01	02.0	07	02.1	14	02.0	07	02.4	49
VI	742.6	16.5	23.7	18.0	19.0	25.2	13.5	31.7	17	08.0	06	05	02.2	03	02.3	11	03.1	01	03.0	01	01.0	02	02.0	17	02.0	03	02.0	47
VII	741.6	17.5	24.5	19.2	20.1	25.8	14.2	32.2	23	08.4	20	05	02.2	01	02.0	14	02.3	.	.	03	02.7	.	.	20	02.2	04	02.8	46
VIII	741.6	16.9	26.0	19.6	20.5	27.0	14.0	33.1	07	07.9	28	03	02.0	.	.	18	02.7	02	01.5	.	.	02	02.0	17	02.1	08	02.5	43
IX	745.3	12.0	21.9	15.0	16.0	23.1	10.1	33.0	12	-01.8	30	02	02.0	03	01.7	09	02.6	02	01.5	.	.	.	.	08	02.2	06	02.2	60
X	745.7	06.1	15.5	09.5	10.2	16.7	04.6	25.3	08	-00.4	20,01	.	.	01	03.0	14	02.6	01	04.0	.	.	.	.	11	02.4	02	02.0	64
XI	744.2	04.3	12.4	07.0	07.7	13.5	02.6	22.3	20	-04.0	29	01	02.0	.	.	15	02.3	01	04.0	02	01.5	01	02.0	11	01.7	05	02.0	54
XII	746.3	00.6	05.1	02.4	02.6	06.0	-00.6	21.9	30	-07.2	21	01	02.0	01	02.0	14	03.9	.	.	01	06.0	02	02.0	13	02.4	02	02.0	59
GOD.	743.4	08.0	15.1	10.4	10.9	16.4	05.9	33.1	7.VIII	-11.1	3. II	25	02.2	14	02.1	187	03.2	17	02.9	18	02.5	20	02.2	144	02.1	51	02.2	618
φ = 43° 37' N λ = 20° 54' E Gr. ΔG = + 1h 22 min. VRNJAČKA BANJA BR. ST. 203																												
I	-	-01.4	02.9	00.1	00.4	04.0	-02.8	14.2	16	-09.0	24	15	01.7	16	01.9	07	02.6	02	02.0	22	01.4	01	02.0	02	01.0	17	01.9	11
II	-	-01.1	04.8	01.0	01.4	06.3	-02.4	17.5	10	-12.3	18	11	02.2	06	02.2	02	02.0	03	02.3	15	02.3	05	03.0	.	.	20	02.3	23
III	-	02.4	09.9	05.1	05.6	11.2	01.4	22.9	25	-05.0	03	17	01.9	13	02.0	12	02.7	04	02.5	16	02.0	01	05.0	01	03.0	15	02.3	14
IV	-	08.6	16.5	10.3	11.4	18.5	05.8	28.0	26	-02.8	05	16	01.7	10	02.3	02	02.5	03	02.3	24	01.9	01	02.0	02	03.0	16	02.6	16
V	-	11.3	16.5	11.6	12.7	18.2	08.2	29.8	11	00.6	03	17	01.8	07	02.1	01	02.0	02	02.0	13	02.2	.	.	01	03.0	20	02.4	32
VI	-	16.8	23.2	16.6	18.3	24.8	12.9	31.0	18	08.0	07,03	22	01.5	10	01.5	01	03.0	01	02.0	13	01.5	.	.	01	01.0	11	01.7	31
VII	-	17.5	24.5	18.2	19.6	25.6	13.9	31.9	15	08.5	20	29	01.7	05	01.4	.	.	01	01.0	14	01.8	.	.	02	02.5	18	01.8	24
VIII	-	17.0	25.5	18.0	19.7	26.5	14.0	32.0	08,07	09.3	28	24	01.6	09	02.0	02	01.5	02	02.0	17	01.8	.	.	01	01.0	11	02.1	27
IX	-	12.1	21.5	13.7	15.3	22.4	10.3	33.0	12	-01.4	30	20	01.6	08	02.0	04	02.2	04	03.0	15	01.7	01	01.0	04	02.2	08	02.2	26
X	-	05.8	15.1	08.2	09.3	16.0	04.6	23.7	08	00.0	25	04	01.8	38	01.9	03	02.0	.	.	10	01.5	.	.	.	.	07	02.0	31
XI	-	04.0	12.2	05.5	06.8	13.1	02.4	21.7	20	-04.2	29	14	01.6	13	01.6	06	02.0	04	01.2	19	01.5	01	03.0	12	01.7	07	01.7	14
XII	-	00.2	04.9	01.7	02.1	05.8	-00.9	20.4	30	-07.3	21	31	01.6	10	02.0	03	01.7	01	01.0	10	02.0	.	.	01	01.0	18	02.4	19
GOD.	-	07.8	14.8	09.2	10.2	16.0	05.6	33.0	18 IX	-12.3	18 II	220	01.7	144	01.9	43	02.3	27	02.1	188	01.8	10	02.8	27	01.9	168	02.2	268
φ = 43° 27' N λ = 21° 04' E Gr. ΔG = + 1h 21 min. ALEKSANDROVAC BR. ST. 204																												
I	-	-00.7	03.0	00.2	00.7	04.4	-03.1	13.4	15	-07.9	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-00.5	04.8	01.7	01.9	06.8	-02.5	16.0	09	-11.7	18	13	01.7	01	02.0	.	.	03	02.0	03	01.7	06	01.2	09	01.4	43	01.6	06
III	-	03.8	09.7	05.2	06.0	11.0	01.3	22.7	24	-04.8	03	09	01.3	02	01.0	01	01.0	02	02.0	06	03.2	11	01.8	15	01.3	40	01.7	07
IV	-	10.3	16.5	10.5	12.0	18.0	05.7	27.1	21	-02.8	06	05	01.8	02	01.0	01	01.0	02	02.5	05	02.0	10	01.7	14	01.8	46	01.8	05
V	-	12.3	16.7	11.9	13.2	17.9	08.2	29.1	11	00.3	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	17.6	22.8	16.9	18.5	24.6	-	30.6	10	-	-	17	01.3	01	01.0	09	01.3	.	.	05	02.2	01	01.0	34	01.3	22	01.2	01
VII	-	19.1	24.6	19.2	20.5	25.5	-	30.8	23	-	-	12	01.3	.	.	02	01.0	.	.	12	01.4	02	01.0	26	01.4	38	01.3	01
VIII	-	18.7	25.6	18.6	20.4	26.7	-	32.3	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	08.6	14.9	08.9	10.3	16.0	05.8	24.4	31	0 .5	28,25	18	01.2	14	01.6	07	01.4	.	.	02	01.0	05	02.2	14	01.2	19	01.2	14
XI	-	05.8	12.1	06.6	07.8	13.5	02.6	21.4	01	-01.7	29	25	01.0	.	.	.	.	.	.	26	01.3	02	01.0	08	01.2	25	01.1	04
XII	-	00.8	04.8	01.7	02.3	05.9	-00.8	16.4	30	-06.5	21	10	01.4	.	.	03	01.0	02	03.5	18	01.6	01	01.0	19	01.3	39	01.3	81
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 43° 52' N λ = 21° 06' E Gr. ΔG = + 1h 24 min. REKOVAC BR. ST 205																												
I	-	-00.4	03.1	00.7	01.0	04.4	-02.0	13.6	15	-09.7	22	.	.	.	.	.	.	04	01.8	14	01.6	.	.	02	01.5	15	02.0	58
II	-	-00.7	04.8	01.0	01.6	06.4	-02.5	17.0	10	-14.0	18	04	01.2	.	.	.	.	.	.	11	02.3	.	.	.	.	17	03.1	52
III	-	02.4	09.8	04.9	05.5	11.1	00.8	23.5	25	-05.5	01	.	.	01	01.0	02	02.0	05	02.4	13	02.1	.	.	.	.	14	02.8	58
IV	-	09.1	16.5	10.3	11.6	18.4	05.4	28.4	24	-01.4	07	02	01.5	.	.	.	.	08	03.4	07	01.4	01	01.0	02	02.5	21	02.8	49
V	-	12.0	17.0	11.9	13.2	18.8	08.3	30.2	11	01.7	03	02	02.0	.	.	01	01.0	.	.	05	01.4	.	.	05	03.6	21	02.9	59
VI	-	17.5	23.8	16.9	18.8	24.8	12.3	30.4	17	06.4	07,06	.	.	.	.	02	01.0	04	01.2	05	01.2	01	01.0	03	01.3	08	01.5	67
VII	-	17.9	24.7	18.0	19.7	25.7	13.5	32.0	24	07.2	20	01	01.0	01	01.0	01	01.0	.	.	04	01.2	01	02.0	06	01.8	18	01.5	61
VIII	-	17.6	25.8	17.7	19.7	26.8	12.8	33.0	08	08.0	28,13	01	01.0	.	.	01	01.0	02	01.0	04	01.2	01	02.0	05	02.6	10	01.3	69
IX	-	12.2	21.7	13.4	15.2	22.8	09.3	33.7	12	-03.2	30	02	01.5	01	01.0	02	01.0	.	.	02	01.5	.	.	01	02.0	16	02.3	66
X	-	05.8	15.2	08.2	09.3	16.3	04.3	25.0	08	-00.5	25	01	03.0	01	01.0	.	.	01	04.0	02	01.5	.	.	07	01.9	11	02.3	70
XI	-	04.0	12.5	05.7	07.0	13.5	01.8	21.4	01	-03.5	12	.	.	.	.	.	.	04	01.0	08	01.4	01	01.0	02	01.5	09	02.6	66
XII	-	00.5	04.7	01.8	02.2	05.7	-01.3	19.0	30	-07.8	21	02	02.0	.	.	01	02.0	04	01.5	01	01.0	.	.	02	02.5	14	02.1	69
GOD.	-	08.2	15.0	09.2	10.4	16.2	05.2	33.7	12 IX	-14.0	18 II	15	01.6	04	01.0	10	01.3	32	02.1	76	01.7	05	01.4	35	02.2	174	02.3	744

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dzm)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dzm)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤ -10,0	Tx ≤ 0,0	Tn < 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	P (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	✱	♨	≈	▲	▲	R T	≡	▦
NOVI PAZAR BR. ST. 201																																					
H_a = 545 m H_b = - m h_a = 2,0 m h_b = 1,5 m																																					
I	8.8	7.1	7.7	7.9	-	04.0	87	83	88	86	40	098	023.4	02	01	06	24	.	.	.	.	.	.	17	13	11	03	06	09	.	.	.	.	.	.	06	-
II	7.6	5.6	6.7	6.7	-	03.7	83	70	81	78	29	091	021.0	16	04	02	23	.	.	.	.	.	.	07	14	15	04	10	10	.	.	.	.	.	.	03	10
III	-	-	-	-	-	04.5	82	57	73	70	30	047	014.8	29	.	.	14	.	.	.	01	01	-	-	13	08	01	08	10	05	.	.	.	.	.	-	.
IV	6.8	5.1	6.1	5.3	-	06.2	78	48	76	68	28	074	030.4	15	.	.	03	05	.	.	05	04	04	07	09	07	02	08	03	.	.	.	.	.	.	.	.
V	5.8	6.9	7.9	6.8	-	08.0	85	62	86	78	33	092	018.6	23	.	.	02	04	.	.	.	.	-	-	19	18	02	19	02	02	.	.	.	.	02	02	.
VI	4.8	5.0	6.0	5.3	-	11.9	88	63	88	80	35	060	014.4	25	.	.	.	18	02	.	.	.	05	07	13	10	02	13	.	.	.	.	.	.	-	02	.
VII	2.6	2.7	5.1	3.5	-	11.9	81	56	85	74	34	071	022.4	07	.	.	.	22	05	.	01	.	13	06	09	06	02	09	.	.	.	.	.	.	02	.	.
VIII	2.2	2.4	3.3	2.6	-	12.3	88	55	87	77	37	052	029.9	09	.	.	.	22	09	.	01	.	16	02	05	04	01	05	.	.	.	.	.	.	.	01	.
IX	4.0	2.3	3.4	3.2	-	10.2	89	62	89	80	43	024	011.4	02	.	.	04	13	03	.	.	.	13	03	05	04	01	05	.	.	.	.	.	.	.	05	.
X	5.2	4.4	4.8	5.1	-	07.5	95	67	91	84	40	072	023.5	23	.	.	05	.	.	.	.	.	08	09	12	08	04	12	02	.	.	.	.	.	.	03	.
XI	6.9	4.6	5.8	5.8	-	05.4	94	63	89	82	33	041	011.0	16	.	.	13	.	.	.	.	.	05	09	10	06	02	10	.	.	.	.	.	.	.	06	.
XII	7.4	4.7	7.2	6.4	-	04.0	85	66	86	79	35	021	009.2	29	01	01	27	.	.	.	.	.	02	11	08	04	.	06	02	.	.	.	.	.	.	06	.
GOD.	-	-	-	-	-	07.5	86	62	84	78	28	743	030.4	15.IV	06	09	115	84	19	.	08	05	-	-	132	101	24	111	38	07	.	.	.	.	-	-	-
KRALJEVO BR. ST. 202																																					
H_a = 219 m H_b = 220,9 m h_a = 2,0 m h_b = 1,4 m																																					
I	8.8	8.5	7.5	8.3		025.3	04.3	88	78	85	84	61	059	018.8	02	.	07	21	.	.	.	06	.	01	21	18	10	01	10	11	.	.	.	.	.	01	07	14
II	8.6	8.8	7.5	8.3		072.5	04.2	88	67	82	79	31	082	016.5	24	02	04	21	.	.	.	03	01	.	17	20	15	01	10	14	.	.	.	.	.	05	11
III	8.6	8.0	5.3	7.3		129.2	04.7	81	54	68	68	24	084	024.0	20	.	.	07	.	.	.	09	01	01	13	15	09	04	11	06	01	.	.	.	01	.	.	04
IV	6.7	7.7	5.3	6.4		166.9	06.6	75	47	64	62	22	069	024.3	15	.	.	02	05	.	.	06	01	03	14	11	06	02	11	02	.	.	.	.	.	01	02	.
V	7.8	8.1	6.1	7.3		151.4	08.8	84	61	81	76	35	194	025.7	19	.	.	.	05	.	.	01	.	02	15	22	18	08	22	02	.	.	.	.	01	07	01	01
VI	5.9	6.5	4.5	5.4		208.3	12.7	87	60	82	76	39	099	035.0	21	.	.	.	20	04	.	03	.	04	06	18	13	02	18	.	.	.	.	.	01	13	06	.
VII	4.2	5.7	4.6	4.9		244.6	13.4	87	60	81	76	39	145	031.1	11	.	.	.	21	06	.	02	01	12	09	12	11	06	12	.	.	.	.	.	.	07	04	.
VIII	4.3	4.6	4.0	4.3		252.2	13.5	90	55	81	75	34	039	012.1	25	.	.	.	20	06	.	02	01	11	07	09	06	02	09	.	.	.	.	.	.	09	07	.
IX	5.7	5.1	3.9	4.9		177.6	10.2	93	52	79	75	26	019	010.4	05	.	.	02	12	05	.	.	.	09	08	09	03	01	09	.	.	.	.	.	.	02	07	.
X	6.2	5.1	5.2	5.5		148.9	07.2	92	58	83	78	25	086	028.7	23	.	.	02	01	.	.	.	.	08	11	12	12	02	12	02	.	.	.	.	.	.	10	01
XI	7.4	6.4	4.3	6.1		109.3	06.0	90	60	81	77	39	063	025.7	24	.	.	08	.	.	.	.	.	04	09	10	07	02	10	.	.	.	.	.	.	.	06	.
XII	8.3	7.2	7.5	7.7		056.3	04.6	88	72	84	81	39	016	004.0	04	.	04	20	.	.	.	03	.	02	19	13	07	.	08	05	.	.	.	.	.	.	09	05
GOD.	6.9	6.8	5.5	6.4		1742.5	08.0	87	60	79	75	22	955	035.0	21.VI	02	15	83	84	21	.	35	05	57	149	169	117	31	142	42	01	.	.	.	03	40	64	34
VRNJAČKA BANJA BR. ST. 203																																					
H_a = 235 m H_b = - m h_a = 2,0 m h_b = 1,5 m																																					
I	7.8	8.1	7.2	7.7		042.4	04.2	89	78	88	85	65	044	007.1	02	.	06	23	.	.	.	.	.	03	20	15	11	.	09	08	.	.	.	.	.	01	02	19
II	7.7	8.2	6.1	7.3		075.5	04.3	89	69	86	82	37	076	010.4	01	02	04	19	.	.	.	02	01	01	12	15	12	02	09	08	.	.	.	.	.	.	02	13
III	8.0	7.0	5.5	6.8		127.4	05.1	86	61	78	75	35	076	022.5	20	.	.	09	.	.	.	01	01	03	14	16	13	02	13	05	01	.	.	.	.	01	.	03
IV	6.1	6.8	5.1	6.0		178.3	07.1	80	53	74	69	21	076	025.4	15	.	.	03	06	.	.	.	01	03	10	12	08	02	11	03	01	.	.	.	.	03	.	.
V	7.1	7.7	5.5	6.8		158.9	08.9	86	67	85	79	34	180	030.2	19	.	.	.	04	.	.	.	.	02	11	21	19	07	21	02	01	.	.	.	01	08	.	01
VI	5.9	5.7	4.2	5.3		223.6	12.9	85	66	87	79	46	061	013.0	31	.	.	.	20	04	.	.	.	05	05	18	13	01	18	.	.	.	.	.	.	10	.	.
VII	3.7	5.5	4.2	4.5		250.6	13.7	86	64	84	78	45	101	021.5	07	.	.	.	19	05	.	.	.	12	09	12	10	05	12	.	.	.	.	.	.	08	.	.
VIII	3.6	4.8	4.2	4.2		264.4	13.6	88	60	86	78	46	052	027.0	03	.	.	.	20	07	.	03	.	10	06	10	06	01	10	.	.	.	.	.	.	05	02	.
IX	4.2	4.6	3.3	4.0		190.1	10.7	92	59	86	79	38	022	010.4	05	.	.	02	10	04	.	.	.	15	06	07	04	01	07	.	.	.	.	.	.	01	.
X	5.2	4.8	4.9	5.0		150.7	07.4	94	64	90	83	41	085	020.0	23	.	.	.	.	.	.	.	.	11	09	12	11	02	12	02	01	.	.	01	.	.	03	01
XI	5.9	6.2	4.4	5.5		120.5	06.2	93	64	89	82	37	048	018.8	24	.	.	08	.	.	.	01	.	06	09	10	07	02	10	.	.	.	.	.	.	03	.
XII	7.4	7.5	7.1	7.3		062.0	04.6	91	75	88	85	47	021	004.4	04	.	04	21	.	.	.	02	.	03	17	15	08	.	11	07	.	.	.	.	.	.	05	06
GOD.	6.0	6.4	5.1	5.9		1846.4	08.2	88	65	85	79	21	842	030.2	19.V	02	14	85	79	20	.	09	03	74	128	143	122	25	143	35	04	.	.	01	01	36	18	43
ALEKSANDROVAC BR. ST. 204																																					
H_a = 360 m H_b = - m h_a = 2,0 m h_b = 1,5 m																																					
I	8.0	7.9	7.8	7.9	-	04.7	92	88	92	91	75	054	-	-	.	07	24	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	8.6	8.2	7.1	7.9	-	04.8	89	81	90	87	51	091	017.3	24	.	01	02	18	.	.	.	01	.	01	16	16	12	02	08	10	.	.	.	.	.	.	04	11
III	8.2	6.6	6.4	7.0	-	05.7	81	68	85	78	32	059	022.0	20	.	.	10	.	.	.	03	.	02	12	11	09	02	08	06	01	.	.	.	.	.	01	.
IV	6.3	7.0	6.4	6.6	-	07.7	75	55	82	71	31	062	016.8	15	.	.	03	05	.	.	02	.	.	11	09	09	03	06	03	.	.	.	.	.	.	.	.
V	6.3	6.8	5.8	6.3	-	09.6	81	73	90	82	43	155	032.0	24	.	.	.	05	.	.	.	.	.	03	10	19	18	06	19	01	01	.	.	.	01	.	.
VI	5.0	4.4	4.0	4.5	-	-	-	-	-	-	-	041	007.2	03	-	.	-	.	.	.	-	.	.	04	05	11	09	.	11	.	.	.	.	.	.	.	.
VII	3.6	4.4	3.6	3.9	-	-	-	-	-	-	-	068	015.2	08	-	.	-	.	.	.	-	.	01	13	05	10	07	04	10	.	.	.	.	.	.	.	.
VIII	2.6	4.2	4.0	3.6	-	-	-	-	-	-	-	037	012.6	03	-	.	-	.	.	.	-	.	.	12	02	06	05	02	06	.	.	.	.	.	.	.	.
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	4.7	4.2	4.9	4.6	-	-	-	-	-	-	-	077	021.5	23	.	.	.	.	.	.	.	.	.	13	12	11	11	02	11	03	03	.	.	.	.	.	.
XI	4.2	5.0	4.0	4.4	-	-	-	-	-	-	-	029	008.4	24	.	.	04	.	.	.	.	.	.	11	06	08	07	.	08	.	.	.	.	.	.	.	.
XII	7.3	7.5	7.0	7.2	-	-	-	-	-	-	-	010	003.5	26	.	04	21	.	.	.	.	.	.	04	17	05	04	.	03	02	.	.	.	.	.	.	.	03
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
REKOVAC BR. ST. 205																																					
H_a = 230 m H_b = - m h_a = 2,0 m h_b = 1,2 m																																					
I	8.4	8.2	8.2	8.2	-	04.5	89	81	89	86	65	041	014.0	02	.	05	21	.	.	.	.	.	.	19	11	10	01	08	04	.	.	.	.	.	.	01	13
II	8.2	7.2	7.1	7.5	-	04.4	89	72	88	83	46	085	013.2	04	01	03	18	.	.	.	02	.	01	14	16	13	02	08	09	01	.	.	.	.	.	03	12
III	6.8	6.6	5.5	6.3	-	-	-	-	-	-	-	074	027.4	20	.	.	11	.	.	.	03	.	02	10	11	09	02	09	04	01	.	.	.	.	.	01	02
IV	5.8	5.9	5.3	5.7	-	07.8	81	60	81	74	32	062	019.2	13	.	.	03	04	.	.	04	.	04	08	10	08	02	10	.	.	.	.	.	.	.	.	.
V	6.4	7.2	6.7	6.8	-	10.0	87	75	92	85	47	163	032.5	19	.	.	.	04	01	.	02	.	03	15	20	17	06	20	.	.	.	.	.	.	.	01	.
VI	4.9	5.3	5.0	5.1	-	-	-	-	-	-	-	120	-	-	.	.	.	21	02	.	.	.	04	06	-	-	-	-	-	.	.	.	.	.	04	03	.
VII	4.1	4.6	4.6	4.4	-	-	-	-	-	-	-	096	021.4	08	.	.	.	20	05	.	.	01	09	07	11	09	04	11	.	.	.	.	.	.	02	.	.
VIII	2.5	4.2	2.9	3.2	-	-	-	-	-	-	-	066	019.0	25	.	.	.	21	09	.	01	.	12	01	08	07	03	08	.	.	.	.	.	.	01	02	.
IX	4.0	4.5	3.7	4.1	-	11.1	91	62	92	81	38	027	018.3	01	.	.	02	11	05	.	.	.	13	05	05	05	01	05	.	.	.	.	.	.	.	05	.
X	4.9	5.5	4.2	4.9	-	-	-	-	-	-	-	072	019.2	23	.	.	01	01	.	.	.	.	10	07	12	12	02	12	.	.	.	.	.	.	.	.	.
XI	6.0	5.7	4.7	5.5	-	06.6	98	69	92	85	38	037	010.9	24	.	.	08	.	.	.	.	.	05	09	10	07	02	10	.	.	.	.	.	.	.	01	.
XII	7.5	7.4	6.0	7.0	-	-	-	-	-	-	-	028	007.0	26	.	01	23	.	.	.	.	.	03	11	08	06	.	05	03	.	.	.	.	.	.	07	05
GOD.	5.8	6.0	5.3	5.7	-	-	-	-	-	-	-	871	-		01	09	87	84	22	.	12	01	46	112	-	-	-	-	-	-	.	.	.	.	-	20	32

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dies)	M̄ax	M̄in	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Pm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
φ = 43° 59' N λ = 21° 14' E Gr. Δ G = + 1h 25 min.																												
I	-	-00.7	02.9	00.4	00.7	04.5	-03.2	16.0	15	-13.5	22	.	.	.	.	.	.	01	04.0	.	.	05	01.8	.	.	19	02.7	68
II	-	-00.7	04.9	01.7	01.9	07.0	-	18.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	02.8	09.7	05.3	05.8	11.7	-	25.0	25	-	-	.	.	.	.	.	.	05	03.4	.	.	12	03.9	.	.	11	02.3	65
IV	-	08.4	16.4	10.8	11.6	18.8	05.0	28.1	24	-02.0	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	16.0	24.4	17.7	19.0	26.0	-	32.0	18,17	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	16.7	25.9	18.9	20.1	26.7	13.7	33.0	25	07.5	20	.	.	.	.	.	.	.	.	.	.	01	03.0	.	.	08	02.0	84
VIII	-	16.2	26.9	19.8	20.7	27.7	12.6	33.6	08	06.5	28	.	.	.	.	.	.	.	.	.	.	.	.	.	.	15	01.7	78
IX	-	11.2	22.1	15.6	16.2	23.4	08.2	33.1	12	-04.1	30	.	.	.	.	.	.	.	.	.	.	.	.	.	.	14	02.0	76
X	-	06.3	15.5	09.1	10.0	16.6	03.3	26.0	08	-02.1	27	.	.	.	.	.	.	.	.	.	.	06	01.5	.	.	11	01.9	76
XI	-	04.3	12.7	07.2	07.8	13.8	01.2	22.0	01	-04.9	26	.	.	.	.	.	.	04	02.2	.	.	.	.	01	01.0	09	02.2	76
XII	-	00.8	04.6	02.4	02.6	05.8	-02.1	20.0	30	-1[illegible].8	27	.	.	.	.	.	.	05	03.0	.	.	.	.	.	.	06	01.5	82
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

SVETOZAREVO — BR. ST. 206

Mesec	Vazdušni pritisak Pm mm	7	14	21	Sred. (Dies)	M̄ax	M̄in	Max	Dat.	Min	Dat.	N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
φ = 43° 08' N λ = 21° 16' E Gr. Δ G = + 1h 25 min.																												
I	-	-00.1	03.3	00.4	01.0	04.5	-01.9	13.0	15	-07.4	30	11	01.7	13	01.5	02	01.0	11	02.1	19	01.9	09	01.4	.	.	03	01.0	25
II	-	-00.5	05.3	01.6	02.0	06.7	-02.4	16.9	06	-17.5	18	19	02.1	05	01.6	02	02.0	05	02.8	20	03.2	16	02.5	01	01.0	03	01.3	13
III	-	02.8	09.8	05.5	05.9	11.2	01.3	22.6	25	-06.0	02	16	01.9	09	01.8	.	.	06	02.3	24	02.5	19	02.9	02	01.5	07	01.4	10
IV	-	07.9	16.5	10.3	11.3	17.6	05.5	27.0	24	-04.1	05	13	02.3	08	01.6	01	01.0	05	02.4	27	03.1	22	02.5	01	02.0	02	02.0	11
V	-	10.4	16.7	11.4	12.5	18.2	07.4	28.5	11	-00.3	02	10	02.0	14	01.4	01	02.0	04	02.0	12	02.3	22	01.6	01	01.0	10	01.9	19
VI	-	14.9	23.4	16.5	17.8	24.6	11.5	30.8	18	04.7	04,03	03	01.3	18	01.7	04	01.5	08	01.8	09	02.0	18	01.8	.	.	02	02.5	28
VII	-	16.8	24.8	17.7	19.2	26.0	13.1	31.8	25	07.5	19	09	02.4	20	01.7	01	02.0	05	02.0	06	01.8	25	01.8	.	.	08	02.0	19
VIII	-	15.7	25.7	17.0	18.9	27.0	12.8	33.9	08	07.2	28	06	02.2	12	01.7	06	01.5	02	02.5	06	02.2	33	01.6	.	.	03	01.3	25
IX	-	10.7	21.8	12.8	14.5	22.6	08.9	33.1	12	-01.8	30	10	01.6	16	01.8	.	.	.	.	02	01.0	37	01.3	.	.	06	01.2	19
X	-	05.6	15.2	07.8	09.1	16.2	04.4	24.6	08	00.4	27	15	01.5	10	01.4	.	.	03	01.7	06	01.7	31	01.4	.	.	03	01.0	25
XI	-	03.9	12.2	06.4	07.2	13.4	02.3	22.9	01	-04.0	12	14	01.4	03	02.3	.	.	05	02.2	22	02.1	24	01.7	.	.	04	02.0	18
XII	-	-00.2	04.8	01.2	01.8	05.6	-01.7	15.7	30	-08.6	21	23	01.3	07	01.4	01	02.0	04	02.2	17	01.5	10	01.4	.	.	03	01.3	28
GOD.	-	07.3	15.0	09.0	10.1	16.1	05.1	33.9	8.VIII	-17.5	18 II	149	01.8	135	01.6	18	01.6	58	02.2	170	02.3	266	01.8	05	01.4	54	01.6	240

KURSUMLIJA — BR. ST. 207

Mesec	Vazdušni pritisak Pm mm	7	14	21	Sred. (Dies)	M̄ax	M̄in	Max	Dat.	Min	Dat.	N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
φ = 43° 34' N λ = 21° 21' E Gr. Δ G = + 1h 25 min.																												
I	-	-00.8	03.3	00.9	01.1	04.8	-02.3	14.4	16	-11.0	03	11	01.5	12	01.6	17	02.0	10	01.8	08	01.4	07	01.6	.	.	10	02.1	18
II	-	-00.6	05.1	01.9	02.0	06.8	-02.2	16.4	10	-13.8	18,03	10	02.1	09	01.6	09	01.6	07	01.7	23	01.8	08	01.9	.	.	15	02.4	03
III	-	03.1	10.1	05.9	06.3	11.5	01.4	24.0	25	-03.5	02	06	02.0	15	02.5	07	02.0	09	02.6	16	02.0	08	02.2	02	01.5	15	02.5	15
IV	-	08.9	16.9	11.5	12.2	18.7	06.2	28.3	24	-01.6	05	08	02.4	04	02.8	08	01.8	11	02.2	23	01.9	13	02.2	01	03.0	17	02.4	05
V	-	11.0	17.0	12.8	13.4	19.0	08.5	30.2	11	00.4	03	08	01.8	03	01.3	05	01.2	09	01.2	15	01.4	06	02.5	11	02.7	25	02.4	11
VI	-	16.6	23.9	18.3	19.3	25.1	13.3	32.0	18	07.4	06	09	01.6	09	01.7	08	01.4	07	01.7	13	01.3	17	01.6	03	02.0	13	01.8	11
VII	-	17.3	25.0	19.2	20.2	26.2	14.4	32.9	25	09.0	20	10	02.4	05	02.0	05	01.4	07	02.0	19	01.6	08	01.5	09	02.2	14	02.0	16
VIII	-	16.4	25.6	19.0	20.0	26.9	13.6	33.6	08	08.3	28	10	02.0	12	01.6	06	01.5	11	01.5	23	01.5	05	01.6	07	01.9	07	02.3	12
IX	-	11.7	21.7	14.3	15.5	22.8	09.8	32.6	12	-03.0	30	10	02.1	09	01.6	06	01.5	09	01.8	22	01.5	06	01.3	10	02.0	13	02.4	05
X	-	05.8	15.2	08.9	09.7	16.7	04.1	24.7	08	-01.0	01	07	01.6	12	01.3	09	01.8	12	01.5	18	01.4	06	01.3	10	01.6	12	01.9	07
XI	-	03.5	12.0	06.1	07.0	13.7	01.8	23.4	01	-04.1	29	07	02.1	10	01.5	10	01.6	12	01.8	22	01.5	06	02.0	04	02.2	09	02.1	12
XII	-	00.7	04.8	02.1	02.4	06.4	-00.8	19.0	30	-08.1	21	15	01.8	06	01.5	08	02.4	07	02.4	14	01.3	08	01.5	08	02.1	11	02.0	16
GOD.	-	07.8	15.0	10.1	10.8	16.6	05.6	33.6	8.VIII	-13.8	3,18 II	111	01.9	106	01.8	98	01.7	111	01.8	216	01.6	98	01.8	65	02.1	161	02.2	129

KRUŠEVAC — BR. ST. 208

Mesec	Vazdušni pritisak Pm mm	7	14	21	Sred. (Dies)	M̄ax	M̄in	Max	Dat.	Min	Dat.	N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
φ = 43° 56' N λ = 21° 23' E Gr. Δ G = + 1h 25 min.																												
I	750.8	-00.7	03.0	00.4	00.8	04.2	-02.5	15.6	15,06	-14.0	22	07	02.1	.	.	03	04.0	32	02.9	06	02.8	.	.	01	01.0	11	02.3	33
II	747.4	-00.3	05.4	02.0	02.3	07.9	-01.5	-	-	-12.7	18	05	02.2	.	.	03	03.0	05	03.2	17	02.1	01	02.0	02	02.5	12	02.8	39
III	748.6	03.2	09.9	05.8	06.1	11.2	01.2	24.2	25	-03.6	30	04	02.5	01	01.0	11	03.3	18	03.2	13	02.3	.	.	02	01.0	10	02.7	34
IV	749.0	08.9	16.8	11.2	12.1	18.5	05.8	28.0	26	-02.6	05	04	02.2	02	01.5	04	03.5	13	03.2	12	02.6	.	.	09	01.8	13	02.8	33
V	749.6	11.6	17.7	12.8	13.7	19.1	08.8	30.5	11	02.0	04	03	01.7	.	.	01	01.0	07	02.4	09	02.2	01	02.0	12	02.7	16	02.7	44
VI	750.9	17.2	23.7	17.9	19.2	25.0	13.7	30.9	17	06.4	02	03	02.7	03	02.0	01	03.0	08	01.9	10	01.7	.	.	06	02.2	07	02.3	52
VII	749.7	17.7	24.8	18.8	20.1	25.9	14.1	32.2	22	10.2	04	03	02.7	.	.	05	01.8	03	02.7	05	01.8	.	.	09	02.6	16	02.2	57
VIII	749.9	17.0	25.8	18.6	20.0	26.9	13.5	33.6	08	07.9	28	06	02.3	.	.	06	02.3	06	02.0	07	02.4	01	02.0	06	02.3	07	02.4	54
IX	753.6	12.0	21.8	13.6	15.2	22.8	09.2	34.4	12	-03.0	30	05	02.8	.	.	02	02.0	03	02.3	04	02.0	.	.	08	02.2	10	02.1	58
X	754.1	06.6	15.2	08.4	09.7	16.2	04.8	25.4	08	00.0	27	01	02.0	.	.	03	02.7	06	02.3	03	01.7	.	.	05	02.4	11	02.1	64
XI	752.7	04.7	12.7	06.5	07.6	13.3	02.8	21.7	01	-02.9	26	02	02.0	.	.	05	02.6	11	02.5	09	01.9	.	.	08	02.1	06	02.5	49
XII	755.2	01.0	04.4	01.8	02.2	05.2	-00.9	19.5	30	-09.6	27	01	02.0	.	.	07	04.7	05	03.0	05	02.0	.	.	04	02.8	15	02.5	56
GOD.	751.0	08.2	15.1	09.8	10.8	16.4	05.8	-		-14.0	22 I	44	02.3	06	01.7	51	03.1	117	02.8	100	02.2	03	02.0	72	02.3	134	02.5	568

ĆUPRIJA — BR. ST. 209

Mesec	Vazdušni pritisak Pm mm	7	14	21	Sred. (Dies)	M̄ax	M̄in	Max	Dat.	Min	Dat.	N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
φ = 43° 14' N λ = 21° 36' E Gr. Δ G = + 1h 26 min.																												
I	-	00.4	03.7	01.3	01.7	05.2	-01.4	14.4	15	-08.0	25	01	03.0	05	01.8	.	.	13	03.1	01	05.0	02	02.0	06	02.0	.	.	65
II	-	00.2	05.2	02.7	02.7	07.2	-01.4	17.0	06	-14.4	18	09	01.3	03	02.3	.	.	10	01.9	.	.	10	03.2	07	03.3	02	02.0	43
III	-	03.3	10.4	06.0	06.4	12.0	01.6	23.5	25	-04.5	03	03	02.3	08	02.0	03	02.3	12	02.3	03	03.0	19	02.9	03	01.3	04	03.0	38
IV	-	08.4	17.1	11.1	11.9	18.5	05.6	28.1	24	-03.5	05	03	02.7	.	.	03	01.3	06	02.8	02	04.5	17	03.2	13	02.8	07	02.1	39
V	-	10.7	17.5	12.1	13.1	19.3	07.8	29.9	11	-00.2	02	06	03.2	.	.	.	.	04	02.5	.	.	15	02.1	07	03.0	10	03.2	51
VI	-	15.7	24.1	17.7	18.8	25.4	12.5	31.9	18	06.0	06	05	02.0	02	01.5	01	01.0	03	02.3	02	02.5	01	02.0	09	02.1	02	01.5	65
VII	-	17.0	25.6	18.5	19.9	26.8	13.9	32.4	23	08.4	20	02	05.5	01	02.0	.	.	04	02.0	01	02.0	03	02.3	07	01.9	11	02.2	64
VIII	-	16.1	26.5	17.9	19.6	27.8	13.2	33.5	08,07	08.0	28	01	02.0	04	01.8	01	02.0	05	02.0	.	.	03	02.3	06	02.7	03	02.3	70
IX	-	11.3	22.6	13.3	15.1	23.4	09.0	33.0	12	-02.5	30	02	02.5	.	.	.	.	02	01.5	.	.	01	03.0	05	01.8	08	02.2	72
X	-	05.4	15.5	08.3	09.3	16.8	04.0	25.5	08	-01.5	01	05	02.2	.	.	.	.	05	01.8	03	03.7	.	.	07	02.4	01	03.0	72
XI	-	03.2	12.2	05.7	06.7	13.2	01.6	20.1	01	-03.3	12	02	03.5	01	02.0	02	01.5	04	02.8	01	04.0	08	02.8	02	02.5	03	03.3	67
XII	-	00.8	04.6	01.9	02.3	06.0	-01.1	17.7	30	-08.6	21	.	.	01	02.0	01	02.0	05	02.2	04	04.0	01	02.0	05	02.8	07	03.0	69
GOD.	-	07.7	15.4	09.7	10.6	16.8	05.4	33.5	7 8.VIII	-14.4	18 II	39	02.4	25	01.9	11	01.7	73	02.4	17	03.6	80	02.8	77	02.5	58	02.6	715

PROKUPLJE — BR. ST. 210

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤-10.0	Tx ≤0.0	Tn ≤0.0	Tx ≥25.0	Tx ≥30.0	Tn ≥20.0	F (0-12) ≥6	≥8	Nm (0-10) ≤2.0	≥8.0	R mm ≥0.1	≥1.0	≥10.0	●	✱	✱	△	◜	▲	▲	⊓	≡	▦
SVETOZAREVO																																					
BR. ST. 206																																					
H_B = 115 m H_b = - m h_s = 2.0 m h_p = 1.0 m																																					
I	8.5	7.6	6.4	7.5	-	-	-	-	-	-	-	-	-	-	02	06	23	.	.	.	.	.	.	16	-	-	-	-	-	-	-	-	-	-	01	.
II	7.5	6.3	6.3	6.7	-	-	-	-	-	-	-	-	-	-	-	02	-	.	.	-	.	.	.	10	-	-	-	-	-	-	-	.	.	.	01	10
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	.	-	01	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	075	-	-	.	.	03	06	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	128	032.0	19	-	.	-	23	09	-	.	.	-	-	14	11	05	14	.	.	.	.	.	01	.	04	.
VII	3.3	4.5	4.0	3.9	-	-	-	-	-	-	-	102	023.0	02	.	.	.	21	13	.	.	.	15	07	10	08	04	10	.	.	.	.	.	.	02	06	.
VIII	3.4	3.5	2.3	3.1	-	-	-	-	-	-	-	041	012.0	23	.	.	.	24	13	.	.	.	15	03	08	07	01	08	.	.	.	.	.	.	01	06	.
IX	6.7	5.2	2.7	4.9	-	-	-	-	-	-	-	021	012.0	01	.	.	03	12	06	.	.	.	06	07	02	02	01	02	.	.	.	.	.	.	01	09	.
X	6.0	4.8	4.2	5.0	-	-	-	-	-	-	-	071	035.0	23	.	.	03	04	.	.	.	.	09	09	07	07	03	07	.	.	.	.	.	.	.	07	.
XI	-	-	-	-	-	-	-	-	-	-	-	044	011.6	24	.	.	09	.	.	.	.	.	-	-	10	06	01	10	.	.	.	.	.	.	.	09	.
XII	7.7	7.7	6.8	7.4	-	-	-	-	-	-	-	023	-	-	01	01	22	.	.	.	.	.	06	20	-	-	-	-	-	-	-	-	-	-	02	03
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
KURSUMLIJA																																					
BR. ST. 207																																					
H_B = 380 m H_b = - m h_s = 2.0 m h_p = 1.2 m																																					
I	8.6	8.2	7.7	8.2	028.4	04.4	86	77	85	83	55	051	011.3	17	.	06	21	.	.	.	.	.	.	21	14	09	01	07	11	.	.	.	.	.	.	.	17
II	7.5	6.8	6.1	6.8	061.8	04.0	81	61	76	73	38	086	016.4	24	03	03	19	.	.	.	04	.	01	08	14	13	03	08	08	.	01	.	.	.	.	01	12
III	7.4	6.2	5.4	6.3	103.3	04.5	77	53	70	67	25	054	022.4	29	.	.	11	.	.	.	03	02	04	14	13	08	02	11	02	.	.	.	.	.	.	01	01
IV	6.4	6.2	5.3	6.0	141.4	06.2	77	44	68	63	26	050	013.3	12	.	.	04	05	.	.	05	01	03	11	10	08	02	10	01	.	01	.	.	.	02	01	.
V	6.6	7.4	5.7	6.6	106.3	08.0	83	57	81	73	30	136	018.3	21	.	.	01	02	.	.	.	.	02	11	20	18	06	20	02	02	.	.	.	.	06	01	01
VI	5.3	5.6	3.7	4.9	161.4	11.4	85	55	83	74	31	050	012.0	15	.	.	.	18	02	.	.	.	04	03	13	08	02	13	.	.	.	.	.	01	08	.	.
VII	3.2	4.4	4.1	3.9	231.6	12.2	83	53	82	73	30	050	015.1	05	.	.	.	22	07	.	.	.	12	06	09	05	02	09	.	.	.	.	.	.	11	.	.
VIII	3.0	4.5	2.7	3.4	238.6	11.9	85	49	86	73	30	057	024.6	09	.	.	.	21	08	.	.	.	12	03	07	06	03	07	.	.	.	.	.	01	07	.	.
IX	4.3	3.6	1.7	3.2	205.4	09.6	91	51	85	76	27	068	041.5	01	.	.	02	10	04	.	.	.	13	03	05	04	02	05	.	.	.	.	.	.	02	.	.
X	5.5	4.4	4.7	4.9	150.9	06.7	91	57	86	78	29	079	029.8	23	.	.	.	.	.	.	.	.	10	08	11	09	02	11	01	01	.	.	.	.	.	02	.
XI	5.4	5.3	3.9	4.9	109.9	05.7	86	58	81	75	25	035	010.8	24	.	.	10	.	.	.	.	.	07	05	09	07	01	09	.	.	.	.	.	.	.	01	.
XII	7.5	6.5	6.8	6.9	052.0	04.3	87	69	86	81	37	032	012.7	31	.	05	21	.	.	.	.	.	03	14	10	06	01	08	02	.	.	.	.	.	.	01	04
GOD.	5.9	5.8	4.8	5.5	1591.2	07.4	84	57	80	74	23	748	041.5	4. IX	03	14	89	78	21	.	12	03	71	107	135	101	27	118	27	03	02	.	.	02	36	08	35
KRUŠEVAC																																					
BR. ST. 208																																					
H_B = 166 m H_b = - m h_s = 2.0 m h_p = 1.2 m																																					
I	8.5	8.2	6.9	7.8	028.9	04.5	92	80	90	87	57	045	010.6	02	01	05	21	.	.	.	.	.	02	20	17	11	01	11	10	01	.	.	.	.	.	02	14
II	8.3	8.1	7.0	7.8	058.8	04.4	91	69	85	82	29	070	009.9	24	03	03	18	.	.	.	02	.	.	15	19	14	.	11	09	.	.	.	.	.	.	01	12
III	8.2	7.1	5.6	7.0	133.2	05.3	90	55	81	75	23	076	022.7	20	.	.	10	.	.	.	01	.	01	13	14	09	03	13	04	01	.	01	.	.	.	.	.
IV	6.8	6.7	5.5	6.3	148.6	07.3	83	50	74	69	25	071	015.2	13	.	.	02	05	.	.	02	.	02	10	14	08	04	14	01	01	.	01	.	.	02	01	.
V	7.4	7.9	6.0	7.1	149.2	09.5	91	66	90	82	34	179	026.1	23	.	.	.	04	01	.	.	.	01	15	21	18	07	21	02	02	.	.	.	.	06	02	.
VI	5.8	6.2	5.0	5.7	205.8	13.2	89	61	85	78	40	101	027.8	01	.	.	.	21	04	.	03	.	03	05	15	12	04	15	.	.	.	.	.	.	09	01	.
VII	4.0	5.5	4.4	4.6	241.3	13.4	88	57	84	76	33	097	016.4	05	.	.	.	21	08	.	01	.	11	06	11	10	03	11	.	.	.	.	.	.	07	03	.
VIII	3.5	5.2	3.1	3.9	241.6	13.1	91	51	85	76	33	094	024.1	23	.	.	.	21	09	.	.	.	12	04	10	08	05	10	.	.	.	.	.	02	07	.	.
IX	4.9	4.9	3.2	4.3	178.7	10.2	93	51	85	76	33	015	008.8	01	.	.	02	11	05	.	.	.	12	06	06	02	.	06	.	.	.	.	.	.	01	02	.
X	5.8	5.7	5.2	5.6	138.5	07.2	94	61	88	81	30	069	015.0	23	.	.	03	.	.	.	.	.	08	14	13	11	03	13	.	.	.	.	.	.	.	07	.
XI	6.1	6.7	4.6	5.8	093.5	06.1	92	64	87	81	39	054	017.0	24	.	.	10	.	.	.	.	.	03	08	10	06	03	10	.	.	.	.	.	.	.	04	.
XII	8.0	7.8	7.3	7.7	042.7	04.8	91	78	89	86	44	021	005.3	23	.	02	18	.	.	.	01	.	01	17	13	05	.	09	06	.	.	.	.	.	.	04	05
GOD.	6.4	6.7	5.3	6.1	1660.8	08.2	90	61	85	79	23	892	027.8	4. VI	04	10	84	83	27	.	10	.	56	133	163	114	33	144	32	05	.	02	.	02	32	27	31
ĆUPRIJA																																					
BR. ST. 209																																					
H_B = 123 m H_b = 124.4 m h_s = 2.0 m h_p = 1.5 m																																					
I	8.5	8.1	7.0	7.9	038.4	04.0	83	72	82	79	49	040	012.2	02	03	05	22	.	.	.	01	.	01	17	16	09	01	10	10	.	.	.	.	.	.	01	15
II	8.1	7.9	7.6	7.9	082.0	04.2	86	64	80	77	36	077	015.4	04	02	-	18	-	-	.	.	.	.	14	17	13	02	08	10	01	.	.	.	.	.	01	14
III	8.0	7.5	6.9	7.5	127.9	04.7	79	55	71	68	22	076	023.6	20	.	.	10	.	.	.	01	.	02	16	15	09	03	12	07	01	.	.	.	.	.	.	03
IV	6.5	6.3	6.1	6.3	171.5	06.8	79	47	69	65	23	086	024.5	15	.	.	03	06	.	.	.	.	02	11	10	08	03	10	.	.	.	.	.	.	03	01	.
V	7.6	7.7	6.0	7.1	160.2	09.1	86	62	84	77	32	187	022.4	17	.	.	.	04	01	.	.	.	01	13	23	21	07	23	.	.	.	.	.	01	07	03	.
VI	6.6	5.5	4.4	5.5	222.5	12.8	84	60	83	76	41	145	035.1	20	.	.	.	21	03	.	01	.	04	06	17	13	06	17	.	.	.	.	.	01	10	.	.
VII	4.2	5.1	3.7	4.3	261.4	13.5	85	58	86	76	36	110	028.6	02	.	.	.	19	09	.	02	.	09	05	10	08	05	10	.	.	.	.	.	.	07	.	.
VIII	4.0	4.9	3.7	4.2	266.6	13.2	87	55	84	75	38	041	008.6	09	.	.	.	19	10	.	.	.	09	04	09	07	.	09	.	.	.	.	.	.	06	02	.
IX	5.1	5.1	3.2	4.5	198.9	10.2	91	52	86	76	27	016	011.3	01	.	.	03	11	05	.	.	.	08	07	07	02	01	07	.	.	.	.	.	.	01	04	.
X	6.6	6.0	4.8	5.8	145.7	07.1	89	59	86	78	29	059	015.9	23	.	.	.	02	.	.	.	.	07	12	12	11	02	12	.	.	.	.	.	.	.	06	.
XI	7.2	6.8	4.9	6.3	115.2	06.1	87	62	84	78	34	046	016.6	24	.	.	07	.	.	.	01	.	03	10	11	07	01	11	.	.	.	.	.	.	01	03	.
XII	8.4	8.1	7.1	7.9	048.7	04.6	88	76	86	83	55	024	005.8	23	.	01	18	.	.	.	03	.	01	18	13	08	.	08	07	01	01	.	.	.	.	03	05
GOD.	6.7	6.6	5.4	6.3	1839.0	08.0	85	60	81	75	22	907	035.1	10 VI	05	-	81	-	-	.	09	.	47	133	160	116	31	137	34	03	01	.	.	02	35	24	37
PROKUPLJE																																					
BR. ST. 210																																					
H_B = 265 m H_b = - m h_s = 2.0 m h_p = 1.3 m																																					
I	9.3	8.2	7.2	8.2	-	04.8	92	80	90	87	63	032	008.0	17	.	05	20	.	.	.	01	.	.	18	11	07	.	08	04	01	.	.	.	.	.	10	08
II	8.8	7.0	5.9	7.2	-	04.6	87	70	84	80	47	054	013.8	24	01	02	17	.	.	.	05	.	01	13	13	11	01	08	06	01	.	.	.	.	.	07	07
III	7.2	6.4	4.4	6.0	-	05.0	82	55	73	70	23	036	013.2	20	.	.	10	.	.	.	01	02	03	11	07	07	01	07	.	.	.	.	.	.	.	.	.
IV	6.2	6.1	3.3	5.2	-	07.0	81	49	72	68	20	045	011.5	13	.	.	03	07	.	.	04	01	08	08	09	07	02	09	.	.	.	.	.	.	02	09	.
V	6.5	6.8	4.1	5.8	-	09.0	89	63	86	79	30	097	016.3	03	.	.	01	06	.	.	.	.	04	10	17	14	04	17	.	.	.	.	.	.	07	03	.
VI	5.5	5.0	2.6	4.4	-	12.6	87	60	84	77	43	054	015.7	21	.	.	.	22	05	.	.	.	07	01	10	06	03	18	.	.	.	.	.	.	09	01	.
VII	3.1	3.9	2.9	3.3	-	13.5	88	57	85	77	40	052	014.4	06	.	.	.	23	11	.	.	01	18	07	09	07	02	09	.	.	.	.	.	.	07	01	.
VIII	2.8	3.9	2.3	3.0	-	13.2	90	54	86	77	32	021	005.7	03	.	.	.	23	14	.	.	.	16	02	09	07	.	09	.	.	.	.	.	.	07	01	.
IX	4.5	3.6	0.9	3.0	-	10.8	95	58	89	80	32	047	045.5	01	.	.	01	12	05	.	.	.	13	.	02	02	01	02	.	.	.	.	.	.	02	07	.
X	6.6	4.9	4.1	5.2	-	07.3	95	62	90	82	34	066	022.7	23	.	.	03	02	.	.	.	.	07	10	10	08	02	10	02	02	.	.	.	.	.	11	.
XI	5.8	5.3	3.9	5.0	-	06.1	92	63	89	81	42	024	006.6	24	.	.	11	.	.	.	02	.	08	08	09	06	.	09	.	.	.	.	.	.	.	10	.
XII	8.6	7.4	7.1	7.7	-	04.9	89	80	89	86	53	024	009.7	31	.	01	22	.	.	.	01	.	01	19	09	04	.	08	01	.	.	.	.	.	.	18	03
GOD.	6.2	5.7	4.1	5.3	-	08.2	88	62	84	78	20	552	045.5	4. IX	01	08	88	95	35	.	14	04	84	107	115	86	16	106	13	04	.	.	.	.	34	74	18

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
SOKOBANJA φ = 43° 39' N λ = 21° 51' E Gr. ΔG = + 1h 26 min. BR. ST. 211																												
I	-	-01.6	01.2	-00.2	-00.2	03.3	-03.1	14.0	06	-10.5	03	.	.	03	04.7	19	04.0	02	03.0	05	03.4	02	02.0	15	01.9	.	.	47
II	-	-00.3	04.2	01.8	01.9	06.4	-02.2	14.6	06	-13.2	03	02	02.5	03	03.0	08	02.1	03	01.7	07	05.3	19	03.1	10	02.5	.	.	32
III	-	03.1	08.4	06.2	06.0	10.0	01.6	23.0	25	-04.0	13	01	02.0	06	03.7	24	03.0	01	03.0	05	04.8	20	02.8	13	02.0	.	.	23
IV	-	08.4	16.7	11.8	12.2	18.2	06.2	28.1	24	-03.0	05	01	03.0	01	02.0	06	02.2	01	03.0	16	03.1	20	03.4	11	02.0	01	03.8	31
V	-	09.9	16.9	12.6	13.0	18.7	08.0	28.2	11	00.5	03	01	01.0	04	02.0	03	02.0	03	01.3	05	01.6	13	02.0	31	02.7	04	02.0	29
VI	-	15.3	23.5	17.7	18.6	24.7	12.3	31.0	17	06.0	07	01	01.0	05	02.6	09	01.4	01	02.0	03	01.3	17	02.2	12	02.0	01	03.0	41
VII	-	16.6	24.7	18.4	19.5	25.9	13.6	32.5	23	07.5	20	01	01.0	03	02.0	06	02.2	.	.	05	02.6	18	01.9	21	02.2	.	.	39
VIII	-	16.7	25.3	18.6	19.8	26.7	13.4	33.1	08	07.5	28	.	.	03	02.3	09	02.2	07	02.3	04	01.0	07	02.3	16	02.0	.	.	47
IX	-	11.4	22.0	14.3	15.5	23.0	08.5	33.2	12	-03.1	30	01	01.0	08	02.1	04	02.5	02	01.0	.	.	06	01.8	12	02.2	04	02.0	53
X	-	-	-	-	-	-	-	25.0	08,07	-01.3	27	01	02.0	01	02.0	11	02.2	02	02.5	02	01.0	05	02.6	15	01.7	02	02.0	54
XI	-	04.6	11.9	07.6	07.9	13.4	03.0	21.0	01	-03.0	12	01	01.0	.	.	02	02.5	.	.	14	02.6	12	02.9	07	02.0	01	01.0	53
XII	-	00.6	03.9	01.6	01.9	05.2	-00.7	15.7	30	-08.7	21	.	.	.	.	05	03.2	04	03.5	05	02.6	13	02.5	13	01.6	02	03.0	51
GOD.	-	-	-	-	-	-	-	33.2	18 IX	-13.2	3. II	10	01.7	37	02.7	106	02.7	26	02.3	71	02.9	152	02.6	176	02.1	15	02.2	562
NIS φ = 43° 20' N λ = 21° 54' E Gr. ΔG = + 1h 26 min. BR. ST. 212																												
I	743.8	00.2	04.1	01.1	01.7	05.5	-01.3	15.4	15	-07.4	25	02	01.5	.	.	15	02.3	11	01.4	06	01.3	02	01.0	05	01.4	16	02.4	36
II	740.5	00.6	05.8	02.8	03.0	07.8	-00.8	17.2	05	-10.6	18	02	02.0	01	01.0	12	01.1	09	01.3	11	02.2	02	01.5	02	01.0	24	02.5	21
III	741.7	03.7	10.3	06.7	06.8	12.2	02.0	24.0	25	-03.8	02	04	02.5	02	02.0	22	02.3	08	01.4	12	02.3	06	01.7	02	01.0	19	02.1	18
IV	742.3	09.3	17.3	11.6	12.5	18.7	06.2	28.6	24	-02.2	05	02	01.0	01	01.0	11	01.2	07	01.6	12	02.1	05	02.4	06	01.7	22	02.9	23
V	742.5	11.7	17.9	12.6	13.7	19.6	08.5	29.3	11	01.7	02	05	02.6	.	.	08	01.0	04	01.0	06	01.2	04	01.0	09	01.9	28	02.2	29
VI	744.1	17.3	24.6	18.2	19.6	25.8	13.5	32.0	10	07.0	06	02	02.5	03	01.0	11	01.5	07	01.6	01	01.0	02	01.5	03	01.3	19	01.8	42
VII	742.9	17.9	25.5	18.9	20.3	26.7	14.3	32.7	25	09.0	20	09	01.8	.	.	07	01.7	06	01.2	07	01.4	01	01.0	02	01.5	27	02.1	34
VIII	743.1	17.4	26.8	18.9	20.5	28.2	14.1	34.1	21,08	08.5	28	09	01.6	.	.	10	01.3	10	01.4	03	01.0	02	02.0	04	01.8	14	01.9	41
IX	746.6	12.1	23.0	14.3	15.9	23.9	09.9	34.3	13,12	-02.2	30	04	02.8	.	.	11	01.4	05	01.0	01	02.0	07	01.0	03	01.7	25	02.2	34
X	747.0	06.0	15.7	08.9	09.9	16.9	04.5	26.8	08	-02.2	01	03	02.7	01	01.0	12	01.4	04	01.0	06	02.0	05	01.0	05	01.4	17	01.7	40
XI	746.1	03.8	12.7	06.4	07.3	13.8	02.2	22.6	01	-02.0	01	02	01.5	.	.	04	01.0	05	01.0	07	01.4	04	01.8	02	02.0	14	01.8	52
XII	748.0	01.4	04.8	02.5	02.8	05.9	-00.2	18.0	30	-07.3	22	03	01.3	01	01.0	07	01.9	08	01.4	02	01.5	05	01.4	08	01.0	24	02.2	35
GOD.	744.0	08.4	15.7	10.2	11.2	17.1	06.1	34.3	18,15 IX	-10.6	18. II	47	02.0	09	01.2	130	01.6	84	01.3	74	01.8	45	01.5	51	01.5	249	02.2	405
KNJAŽEVAC φ = 43° 34' N λ = 22° 16' E Gr. ΔG = + 1h 29 min. BR. ST. 213																												
I	-	-02.4	00.3	-02.1	-01.6	01.1	-	13.6	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	00.1	05.3	01.9	02.3	06.8	-01.1	17.6	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	02.9	09.5	05.0	05.6	11.0	00.9	24.6	25	-05.8	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	09.1	17.2	11.6	12.4	19.1	06.2	28.8	24	-03.8	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	11.0	18.7	12.8	13.8	20.2	08.4	31.0	11	00.5	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	15.5	24.3	17.2	18.5	25.7	12.6	31.4	30,17	07.2	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	17.2	25.7	18.2	19.8	27.2	13.8	33.2	23	10.0	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	15.3	25.8	17.9	19.2	27.6	12.4	33.0	07	07.2	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	10.1	23.7	13.4	15.2	25.0	08.1	34.5	12	-02.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	06.1	14.9	07.7	09.1	16.0	03.9	27.0	07	-00.5	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	04.8	13.3	06.3	07.7	14.5	02.1	26.8	01	-02.8	08	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-00.2	03.9	00.9	01.4	05.1	-01.9	16.2	01	-09.2	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	07.5	15.2	09.2	10.3	16.6	-	34.5	18 IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ZAJECAR φ = 43° 53' N λ = 22° 18' E Gr. ΔG = + 1h 29 min. BR. ST. 214																												
I	-	-03.4	00.1	-02.2	-01.9	01.1	-05.3	07.5	27,15	-14.3	21	12	01.6	17	03.1	03	01.7	01	01.0	01	01.0	24	02.7	32	02.3	02	02.0	1
II	-	-00.5	04.5	01.6	01.8	06.0	-02.5	17.0	10	-12.8	03	09	02.0	22	02.9	01	03.0	01	02.0	04	02.0	21	03.2	21	03.5	05	03.8	-
III	-	02.9	09.2	05.2	05.6	10.7	00.5	24.2	25	-06.8	03	09	02.3	19	03.6	04	03.2	02	02.0	01	04.0	29	03.2	27	02.9	02	03.5	-
IV	-	08.4	16.7	11.7	12.1	18.5	05.4	30.5	11	-00.1	02	08	02.0	11	02.9	04	02.2	03	01.7	03	03.0	27	02.7	27	02.7	07	03.0	-
V	-	11.6	18.4	12.9	13.9	19.7	08.1	-	-	-	-	09	02.1	07	02.1	02	03.5	03	02.7	05	02.2	24	02.5	33	02.5	10	03.5	-
VI	-	16.9	23.9	17.8	19.1	25.4	12.7	-	-	-	-	07	01.7	06	02.5	02	03.5	05	02.8	08	02.0	35	02.5	19	03.1	08	02.9	-
VII	-	17.6	25.3	18.9	20.2	26.9	13.7	32.6	23	08.1	20	08	02.4	08	02.6	05	02.8	01	04.0	05	02.4	43	02.3	18	01.8	05	03.2	-
VIII	-	16.7	25.5	17.9	19.5	26.7	12.7	33.0	07	06.0	28	20	01.7	05	02.2	07	01.4	01	03.0	02	01.0	13	01.7	42	01.6	03	02.0	-
IX	-	10.8	23.3	13.5	15.3	24.2	08.1	32.0	12	-02.5	30	07	02.7	11	02.6	01	02.0	03	02.7	03	02.3	29	01.8	28	01.9	06	03.3	02
X	-	05.5	14.7	08.0	09.1	15.5	03.5	26.4	07	-02.5	01	12	02.4	12	02.8	05	02.6	01	04.0	.	.	23	02.0	26	02.7	14	02.6	-
XI	-	03.3	12.4	05.5	06.6	13.1	01.1	24.2	01	-04.1	08	08	02.6	04	02.0	01	01.0	07	02.4	07	02.7	33	02.5	24	02.0	05	02.4	01
XII	-	-00.8	04.3	00.6	01.2	05.0	-02.8	-	-	-	-	09	01.6	12	02.3	01	04.0	02	01.5	03	03.7	30	02.4	19	02.7	17	02.9	-
GOD.	-	07.4	14.9	09.3	10.2	16.1	04.6	-		-		118	02.0	134	02.8	36	02.4	30	02.4	42	02.4	331	02.5	316	02.4	84	03.0	04
PIROT φ = 43° 09' N λ = 22° 36' E Gr. ΔG = + 1h 29 min. BR. ST. 215																												
I	-	-00.2	03.7	00.9	01.3	05.7	-02.3	16.5	07	-08.5	22	10	01.3	01	01.0	.	.	20	01.9	05	02.8	01	01.0	01	02.0	07	01.6	48
II	-	-00.7	04.7	01.6	01.8	07.0	-02.7	17.0	06	-10.0	18	14	01.4	.	.	.	.	05	01.8	03	02.0	.	.	02	02.0	10	01.7	50
III	-	02.5	08.9	05.2	05.4	11.0	00.3	22.0	25	-06.0	03	15	01.3	.	.	.	.	12	02.1	03	02.3	.	.	01	02.0	13	01.7	49
IV	-	08.5	15.9	11.0	11.6	18.0	05.0	28.0	24	-04.0	05	06	01.5	.	.	.	.	06	01.8	03	02.3	01	01.0	.	.	16	01.3	58
V	-	10.7	17.2	12.2	13.1	19.4	07.6	30.5	11	-01.5	02	06	01.5	.	.	.	.	04	01.5	02	02.0	02	01.0	02	02.0	15	01.5	62
VI	-	16.4	23.4	17.4	18.7	24.8	12.0	30.0	30	07.0	07,02	03	01.0	.	.	01	01.0	02	01.0	06	01.5	02	01.0	01	03.0	12	01.6	63
VII	-	17.3	24.3	18.8	19.8	26.3	13.3	32.5	23	09.5	19	02	02.5	02	01.0	.	.	01	01.0	.	.	04	02.0	07	01.6	18	01.0	59
VIII	-	16.1	25.8	18.3	19.6	27.0	12.6	33.0	08	06.5	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	11.0	22.8	13.3	15.1	23.8	07.9	34.0	13	-02.5	30	.	.	03	01.0	.	.	.	.	.	.	.	.	.	.	21	01.6	66
X	-	05.3	15.3	08.2	09.2	16.5	03.1	26.0	08	-01.5	27	05	01.2	01	01.0	01	01.0	.	.	03	01.0	01	01.0	01	01.0	16	01.6	65
XI	-	02.6	11.9	05.1	06.2	13.0	00.5	22.0	01	-04.0	26	02	01.5	01	01.0	.	.	02	01.0	04	02.0	.	.	.	.	15	01.4	66
XII	-	00.6	04.8	01.8	02.3	05.9	-01.8	20.0	30	-09.5	21	.	.	.	.	.	.	13	02.0	.	.	.	.	01	02.0	27	01.4	52
GOD.	-	07.5	14.9	09.5	10.3	16.5	04.6	34.0	18 IX	-10.0	18 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dim)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dim)	Min	Padavine R mm Σ	Max	Dat.	Broj dana sa: Tn ≤-10,0	Tx ≤0,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) ≤8,0	≥8,0	R mm ≥0,1	≥1,0	≥10,0	●	⚹	⚹	⚹	⚹	▲	▲	℞	≡	▦
BR. ST. 211						**SOKOBANJA**																															
I	-	-	-	-	-	04.2	87	87	88	87	95	048	019.5	02	01	11	25	.	.	.	02	.	-	-	16	07	02	10	10	04	.	.	.	.	.	06	11
II	-	-	-	-	-	04.4	83	78	81	81	42	070	011.0	04	02	03	17	.	.	.	02	02	-	-	18	13	01	10	11	03	.	.	.	.	.	04	11
III	-	-	-	-	-	05.4	83	70	75	76	33	078	017.0	29	.	01	11	.	.	.	05	.	-	-	14	08	05	11	09	06	.	.	.	.	.	.	01
IV	-	-	-	-	-	06.9	79	53	64	65	04	083	017.2	12	.	.	02	06	.	.	03	.	-	-	15	11	03	15	01	01	.	.	.	.	.	.	.
V	-	-	-	-	-	08.6	87	41	80	76	39	092	015.0	03	.	.	.	04	.	.	01	.	-	-	20	15	01	20	01	01	.	.	.	.	03	05	.
VI	-	-	-	-	-	12.1	85	60	80	75	34	048	024.2	18	.	.	.	20	03	.	.	.	-	-	13	11	01	12	.	.	.	.	.	.	04	02	.
VII	-	-	-	-	-	12.8	84	60	81	75	37	083	017.3	08	.	.	.	20	08	01	.	.	-	-	16	09	03	14	.	.	.	.	.	.	08	04	.
VIII	-	-	-	-	-	13.3	82	63	82	75	35	029	011.5	23	.	.	.	22	08	01	.	.	-	-	07	09	01	07	.	.	.	.	.	.	03	.	.
IX	-	-	-	-	-	10.3	87	57	78	74	23	060	038.0	01	.	.	03	11	04	.	.	.	-	-	05	02	01	05	.	.	.	.	.	.	.	05	.
X	-	-	-	-	-	-	-	-	-	-	27	067	017.5	02	.	.	01	02	.	.	.	.	-	-	12	09	03	12	02	02	.	.	.	.	.	04	.
XI	-	-	-	-	-	05.5	81	60	73	71	19	042	013.5	24	.	.	08	.	.	.	02	.	-	-	09	07	02	09	.	.	.	.	.	.	.	02	.
XII	-	-	-	-	-	04.4	85	74	82	80	34	029	007.5	23	.	01	18	.	.	.	03	.	-	-	12	08	.	10	03	01	.	.	.	.	.	10	06
GOD.	-	-	-	-	-	-	-	-	-	-	04	729	038.0	4.IX	03	14	85	85	23	02	18	02	-	-	157	105	23	135	37	18	.	.	.	.	20	42	29
BR. ST. 212						**NIŠ**																															
I	8.8	8.5	7.4	8.2	039.3	04.4	86	72	83	80	50	042	014.9	17	.	05	20	.	.	.	01	.	.	19	15	10	01	10	09	03	.	.	.	.	.	04	13
II	9.1	8.1	7.9	8.3	061.3	04.3	83	63	76	74	34	059	015.1	24	01	02	18	.	.	.	02	.	.	20	19	12	01	10	11	02	.	.	.	.	01	01	10
III	7.7	7.0	5.5	6.7	141.1	04.7	78	52	65	65	24	038	011.7	20	.	.	10	.	.	.	05	.	03	15	13	09	01	11	06	03	.	.	.	.	.	.	.
IV	7.4	6.7	5.4	6.5	164.5	06.8	79	45	68	64	24	052	010.9	12	.	.	03	07	.	.	05	.	02	12	14	10	02	14	01	01	.	.	.	.	02	.	.
V	7.5	7.6	5.9	7.0	159.9	08.8	84	59	81	75	33	114	019.4	23	.	.	.	06	.	.	.	.	02	15	20	17	04	20	.	.	.	.	.	.	07	01	.
VI	5.3	5.7	4.5	5.2	232.5	12.3	80	55	79	72	35	069	016.2	20	.	.	.	22	06	.	.	.	03	03	13	09	03	13	.	.	.	.	.	.	10	.	.
VII	3.4	4.7	3.8	4.0	269.4	13.2	83	56	81	73	33	087	044.1	05	.	.	.	23	10	.	02	.	13	06	11	08	03	11	.	.	.	.	.	.	13	.	.
VIII	3.5	5.0	2.9	3.8	270.0	12.6	83	48	80	70	29	026	009.6	11	.	.	.	24	14	.	01	01	12	04	08	05	.	08	.	.	.	.	.	02	07	.	.
IX	4.5	3.7	2.4	3.6	240.2	09.8	89	46	78	71	19	022	015.5	01	.	.	01	11	07	.	.	.	11	03	04	03	01	04	.	.	.	.	.	.	02	.	.
X	6.6	5.4	5.1	5.7	153.4	07.2	92	58	86	79	29	063	018.1	23	.	.	01	03	.	.	.	.	07	10	12	08	01	12	03	02	.	.	.	.	.	03	.
XI	6.4	6.1	4.6	5.7	116.5	06.0	91	59	84	78	29	034	010.9	11	.	.	08	.	.	.	.	.	05	09	09	05	01	09	.	.	.	.	.	.	.	.	.
XII	8.6	7.8	7.5	8.0	052.0	04.8	88	74	85	82	51	028	010.0	23	.	.	19	.	.	.	01	.	01	20	12	08	01	11	03	01	.	01	.	.	.	02	03
GOD.	6.6	6.4	5.2	6.1	1900.1	07.9	84	57	78	73	19	634	044.1	5.VII	01	07	80	96	37	.	17	01	59	136	150	104	19	133	33	12	.	01	.	02	42	11	26
BR. ST. 213						**KNJAŽEVAC**																															
I	9.7	8.7	8.5	9.0	-	-	-	-	-	-	-	048	019.5	17	-	11	-	.	.	-	.	.	.	24	12	09	02	06	07	01	.	01	.	.	.	05	18
II	8.9	7.3	9.7	8.6	-	-	-	-	-	-	-	070	012.0	17	-	05	-	.	.	-	.	.	.	19	15	12	01	08	08	01	.	.	.	.	.	.	08
III	7.3	6.6	7.5	7.1	-	-	-	-	-	-	-	064	013.4	15	.	.	13	.	.	.	.	.	.	16	09	08	03	08	02	01	.	.	.	.	.	01	.
IV	6.3	6.4	6.6	6.4	-	-	-	-	-	-	-	065	018.2	13	.	.	03	08	.	.	.	.	02	11	12	09	02	12	.	.	.	.	.	.	.	.	.
V	7.1	7.1	7.3	7.2	-	-	-	-	-	-	-	106	016.7	20	.	.	.	05	01	.	.	.	01	15	18	17	02	17	.	.	.	.	.	.	02	01	.
VI	4.7	4.9	5.7	5.1	-	-	-	-	-	-	-	046	-	-	.	.	.	21	07	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	4.0	4.9	4.3	4.4	-	-	-	-	-	-	-	172	049.0	05	.	.	.	25	10	.	.	.	11	08	12	11	06	12	.	.	.	.	.	.	06	.	.
VIII	3.7	5.0	4.6	4.4	-	-	-	-	-	-	-	045	013.8	17	.	.	.	26	10	.	.	.	11	05	11	08	02	11	.	.	.	.	.	.	05	01	.
IX	4.3	4.1	3.0	3.8	-	-	-	-	-	-	-	010	007.3	01	.	.	02	17	05	.	.	.	10	02	03	03	.	03	.	.	.	.	.	.	.	.	.
X	7.5	6.4	5.6	6.5	-	-	-	-	-	-	-	052	013.6	23	.	.	02	01	.	.	.	.	06	14	11	09	03	09	03	01	.	.	.	.	.	07	01
XI	6.0	6.0	4.9	5.6	-	-	-	-	-	-	-	035	010.5	11	.	.	07	01	.	.	.	.	05	10	07	06	01	07	.	.	.	.	.	.	.	02	.
XII	8.4	7.7	7.8	8.0	-	-	-	-	-	-	-	027	011.8	23	.	02	23	.	.	.	.	.	01	19	07	03	02	06	02	01	.	01	.	.	.	04	07
GOD.	6.5	6.3	6.3	6.3	-	-	-	-	-	-	-	740	-	-	-	18	-	104	33	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 214						**ZAJEČAR**																															
I	8.8	8.2	7.6	8.2	044.3	03.4	89	76	87	84	47	032	012.1	02	06	11	28	.	.	.	01	.	01	19	12	07	01	09	04	.	.	01	.	.	.	03	29
II	8.0	7.6	7.1	7.6	087.1	04.1	86	65	80	77	33	055	008.3	12	01	05	18	.	.	.	05	.	01	13	16	13	.	08	09	.	.	01	.	.	.	01	13
III	7.5	6.9	5.7	6.7	129.0	04.7	83	58	74	72	23	094	029.9	15	.	.	15	.	.	.	02	.	03	12	11	10	04	10	06	03	.	.	.	.	.	.	03
IV	6.6	6.7	5.1	6.1	179.0	07.1	84	52	69	68	34	087	021.1	09	.	.	01	05	01	.	01	.	02	09	16	13	04	16	01	01	.	.	.	.	02	01	.
V	6.5	7.3	6.1	6.6	183.5	09.5	88	59	87	78	-	098	029.9	15	.	.	.	.	.	.	02	.	03	12	11	10	04	10	06	03	.	.	.	.	.	.	03
VI	4.5	5.1	5.5	5.1	262.7	13.2	87	60	88	78	-	092	048.2	18	-	-	-	-	-	-	01	.	04	03	10	07	02	10	.	.	.	.	.	01	08	01	.
VII	3.7	4.8	4.2	4.2	290.8	14.4	90	62	89	80	40	118	043.6	08	.	.	.	24	07	.	03	.	12	06	11	09	06	11	.	.	.	.	.	.	09	.	.
VIII	4.4	4.8	3.1	4.1	289.0	13.9	92	59	91	81	38	045	011.0	25	.	.	.	22	04	.	01	.	10	05	09	08	01	09	.	.	.	.	.	.	08	.	.
IX	4.4	3.8	2.6	3.6	257.4	10.3	93	49	86	76	35	017	013.9	01	.	.	02	15	05	.	.	.	07	01	03	03	01	03	.	.	.	.	.	.	01	03	.
X	6.9	5.9	4.6	5.8	138.3	07.2	94	65	88	82	34	047	012.3	23	.	.	04	01	.	.	.	.	07	10	12	08	02	12	03	02	.	.	.	.	.	05	01
XI	6.7	6.3	5.4	6.1	120.9	05.9	89	65	85	79	40	027	010.2	24	.	.	10	.	.	.	01	.	03	11	08	06	02	08	.	.	.	.	.	.	.	07	.
XII	7.0	6.6	6.8	6.8	085.0	04.2	88	74	85	83	-	019	009.6	23	-	-	-	-	-	-	01	.	04	16	11	05	.	08	04	.	.	01	.	.	.	03	08
GOD.	6.2	6.2	5.3	5.9	2061.0	08.2	88	62	84	78	-	731	048.2	18.VI	-	-	-	-	-	-	18	.	57	117	130	99	27	114	33	09	.	03	.	01	28	24	57
BR. ST. 215						**PIROT**																															
I	8.1	7.3	6.8	7.4	-	04.4	88	77	84	83	54	046	012.6	17	.	05	21	.	.	.	.	.	01	16	11	10	01	07	05	.	.	.	.	.	.	02	09
II	8.5	7.0	7.1	7.5	-	04.4	90	75	85	83	40	084	017.8	24	01	02	21	.	.	.	.	.	01	14	15	14	02	10	10	02	.	.	.	.	01	.	11
III	6.7	6.5	4.7	6.0	-	05.1	85	67	77	76	31	060	015.5	20	.	.	13	.	.	.	.	.	05	11	09	09	01	08	03	01	.	.	.	.	01	01	01
IV	5.6	6.3	5.1	5.6	-	06.7	78	54	69	67	24	049	010.4	12	.	.	03	07	.	.	.	.	06	10	11	10	01	11	.	.	.	.	.	.	.	01	.
V	6.3	6.6	5.1	6.0	-	08.5	82	59	81	74	33	119	017.2	03	.	.	01	06	01	.	.	.	04	10	16	15	05	16	.	.	.	.	01	.	03	01	.
VI	4.0	5.4	3.1	4.2	-	11.8	80	55	81	72	37	089	027.5	20	.	.	.	20	01	.	.	.	09	04	15	14	03	15	.	.	.	.	.	.	04	01	.
VII	3.4	4.6	3.2	3.7	-	13.1	83	61	82	75	36	147	038.0	05	.	.	.	23	08	.	.	.	12	06	10	10	07	10	.	.	.	.	.	.	07	.	.
VIII	2.9	4.8	1.8	3.2	-	12.2	84	49	82	72	32	042	-	-	.	.	.	22	10	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	4.2	3.4	0.7	2.8	-	09.0	86	43	79	69	20	016	008.5	01	.	.	03	14	06	.	.	.	13	.	03	03	.	03	.	.	.	.	.	.	.	.	.
X	5.5	4.6	3.9	4.7	-	06.7	91	56	85	77	27	080	020.9	23	.	.	05	02	.	.	.	.	10	09	10	10	03	10	03	01	.	.	.	.	.	07	01
XI	5.2	4.7	3.3	4.4	-	05.6	90	60	85	78	35	038	008.2	23	.	.	10	.	.	.	.	.	12	07	07	06	.	07	.	.	.	.	.	.	.	01	.
XII	6.2	7.1	6.5	7.3	-	04.7	89	76	86	84	48	022	009.1	23	.	01	22	.	.	.	.	.	01	16	09	07	.	08	01	.	.	.	.	.	.	03	03
GOD.	5.7	5.7	4.3	5.2	-	07.7	85	61	81	75	20	792	-		01	08	99	94	26	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dlas)	Max	Min	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12) N č.	j.	NE č.	j.	E č.	j.	SE č.	j.	S č.	j.	SW č.	j.	W	j.	NW č.	j.	C
TOPLI DO — φ = 43° 20' N λ = 22° 41' E Gr. Δ G = + 1h 30 min. — BR. ST. 216																												
I	-	-01.3	02.9	-00.5	00.1	04.4	-03.0	14.3	07	-12.6	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-01.8	02.6	-00.5	00.0	04.4	-03.7	11.9	06	-12.1	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	01.5	07.2	03.5	03.9	08.4	-00.1	19.0	25	-08.0	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	07.2	13.4	08.4	09.4	15.0	04.0	24.8	24	-04.1	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	09.0	14.8	09.4	10.7	16.1	06.2	27.7	11	-01.8	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	14.1	21.4	14.3	16.0	22.5	10.2	27.8	30	04.6	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	16.1	22.5	15.6	17.4	24.2	12.4	30.1	23	07.2	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	14.9	23.9	16.1	17.8	25.1	12.2	30.9	08	06.9	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	10.3	21.2	12.5	14.1	21.7	07.8	31.7	12	-02.4	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	05.2	13.5	07.2	08.3	14.4	03.0	22.8	08	-01.9	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	03.3	10.3	04.5	05.7	11.2	01.3	20.4	01	-03.2	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-00.8	03.1	00.4	00.8	04.0	-02.6	14.3	30	-09.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	06.5	13.1	07.6	08.7	14.3	04.0	31.7	12 IX	-12.6	22 I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
DIMITROVGRAD — φ = 43° 01' N λ = 22° 45' E Gr. Δ G = + 1h 29 min. — BR. ST. 217																												
I	722.0	-00.6	03.0	00.5	00.9	04.4	-02.2	14.2	15	-08.2	20	.	.	.	.	13	03.0	43	02.8	.	.	.	.	09	02.3	25	03.9	03
II	718.5	-00.9	04.3	00.6	01.2	06.1	-02.4	16.5	06	-10.1	22	.	.	.	.	08	02.2	27	02.2	01	04.0	01	02.0	13	02.5	27	03.4	07
III	720.1	02.3	08.9	04.4	05.0	10.3	00.5	22.3	25	-07.5	03	01	02.0	.	.	08	03.2	38	02.6	02	03.5	01	04.0	08	02.6	30	03.2	05
IV	721.0	07.7	15.3	09.6	10.6	17.2	04.4	-	-	-	-	.	.	01	01.0	04	03.0	40	02.4	01	03.0	01	04.0	07	01.9	32	03.8	04
V	721.2	10.3	16.8	11.4	12.4	18.3	07.3	29.5	11	-02.3	02	.	.	01	03.0	14	01.8	20	02.0	01	01.0	02	04.0	11	02.0	35	04.0	09
VI	723.3	15.6	22.9	16.5	17.9	24.1	11.6	-	-	-	-	01	02.0	.	.	08	02.5	27	02.3	.	.	.	.	14	02.1	27	03.3	13
VII	722.1	16.9	24.2	17.6	19.0	25.8	13.3	-	-	-	-	.	.	02	01.0	09	02.2	31	02.0	01	01.0	01	01.0	09	02.1	34	03.2	06
VIII	722.4	15.8	25.3	17.3	18.9	26.7	12.9	33.0	08	06.9	28	.	.	03	02.3	06	01.8	39	02.1	.	.	.	.	04	02.2	26	03.8	15
IX	725.4	10.0	22.6	12.4	14.3	23.2	07.7	33.0	11	-03.1	30	.	.	.	.	07	02.0	34	02.1	.	.	.	.	08	02.0	29	03.4	12
X	725.5	05.3	14.9	07.9	09.0	15.9	03.9	24.7	08	-02.8	26	.	.	.	.	07	02.4	37	02.1	02	02.5	02	01.5	11	01.9	29	02.8	05
XI	724.6	02.4	11.6	04.8	05.9	12.4	01.0	20.0	01	-04.6	26	.	.	01	03.	15	02.5	40	02.2	.	.	.	.	12	01.9	21	03.4	11
XII	725.9	-00.2	04.1	01.2	01.6	04.9	-01.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	722.7	07.0	14.5	08.7	09.7	15.8	04.7	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
PEĆ — φ = 42° 40' N λ = 20° 18' E Gr. Δ G = + 1h 21 min. — BR. ST. 218																												
I	716.3	00.8	02.8	01.7	01.7	04.1	-00.6	13.2	01	-06.5	20	03	02.0	04	01.2	06	01.3	05	01.0	11	01.9	11	02.2	09	01.7	.	.	44
II	713.2	00.2	05.0	02.1	02.4	06.1	-01.3	15.6	06	-1[illegible].2	18	06	01.8	11	02.2	06	01.8	06	01.7	08	01.2	11	01.5	13	02.5	04	03.2	19
III	714.6	03.1	08.9	05.7	04.9	10.1	01.7	22.8	27	-05.0	02	10	02.3	10	02.1	03	02.0	07	01.6	12	02.3	10	02.6	20	02.9	03	11.7	18
IV	715.9	09.0	15.1	11.1	11.6	16.4	06.2	26.0	24	-01.4	05,04	09	02.0	17	01.8	04	01.2	08	01.5	10	02.3	09	02.8	19	02.6	08	02.4	06
V	716.6	11.4	16.5	13.0	13.5	17.8	08.2	26.4	11	01.0	02	08	02.0	12	02.0	08	01.5	07	01.9	10	01.7	10	02.4	22	02.6	04	03.2	12
VI	718.5	16.8	23.1	18.8	19.4	24.5	12.8	30.7	10	05.0	04	08	02.2	14	01.6	13	01.7	05	01.6	10	01.4	11	02.4	14	01.6	.	.	15
VII	717.2	18.1	24.5	20.0	20.6	26.2	14.4	31.3	23	07.8	20,19	04	02.0	07	01.7	10	01.8	10	01.5	15	01.7	10	01.6	18	02.2	02	01.5	17
VIII	717.5	17.9	25.5	19.8	20.7	26.7	13.7	32.7	08	07.6	27,13	05	01.6	09	01.9	07	01.9	11	01.6	14	01.4	11	01.8	15	02.1	03	02.3	18
IX	720.4	13.3	22.0	15.9	16.8	22.7	10.4	31.2	12	-01.2	30	04	02.2	04	02.0	07	01.4	09	01.6	09	02.0	14	01.9	12	02.6	02	03.5	29
X	720.4	07.1	15.1	10.2	10.7	16.2	05.5	24.3	09	00.3	26	07	01.4	07	01.9	06	02.2	04	01.5	17	01.6	08	01.8	20	02.4	01	02.0	23
XI	719.5	03.9	10.9	05.9	06.6	11.8	02.4	19.0	01	-02.7	12	08	01.5	05	01.8	04	01.5	04	02.2	09	01.9	10	01.8	13	01.5	02	02.5	35
XII	720.5	00.1	04.7	01.5	01.9	05.6	-01.6	16.2	30	-08.1	21	04	01.2	03	01.3	02	01.5	04	01.5	12	01.8	14	01.6	17	02.2	03	01.3	34
GOD.	717.6	08.5	14.5	10.5	11.0	15.7	06.0	32.7	8.VIII	-1[illegible].2	48.II	76	01.9	103	01.8	76	01.7	80	01.6	137	01.8	129	02.0	192	02.3	32	02.4	270
SKIVIJANE-DJAKOVICA — φ = 42° 26' N λ = 20° 21' E Gr. Δ G = + 1h 21 min. — BR. ST 219																												
I	-	01.1	03.3	02.1	02.2	04.6	-00.1	15.3	07	-05.9	21	.	.	30	02.0	.	.	.	.	.	.	14	03.1	.	.	.	.	49
II	-	00.5	05.9	02.5	02.8	07.1	-01.3	15.4	06	-14.2	18	.	.	22	02.0	.	.	.	.	.	.	34	03.9	.	.	01	02.0	27
III	-	03.1	10.2	06.0	06.3	11.3	01.3	21.8	27	-04.6	03	.	.	30	02.1	.	.	.	.	.	.	46	02.8	.	.	.	.	17
IV	-	08.6	15.3	10.6	11.3	16.6	05.2	27.9	24	-02.4	05	.	.	12	01.9	.	.	.	.	.	.	50	02.8	.	.	.	.	28
V	-	11.0	17.6	12.1	13.2	18.8	07.5	-	-		-	02	02.0	30	02.1	.	.	.	.	.	.	31	02.4	.	.	01	02.0	29
VI	-	16.2	24.2	18.1	19.1	25.9	11.7	30.7	11	06.1	04	03	01.3	07	02.3	.	.	.	.	.	.	21	02.5	.	.	11	01.8	48
VII	-	26.1	19.1	20.3	-	-	-	-	-		-	11	01.4	05	01.2	.	.	.	.	02	01.0	05	03.2	09	01.7	04	01.2	57
VIII	-	16.7	26.9	18.3	20.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	12.4	23.0	14.6	16.2	24.1	-	31.0	13		-	19	01.8	04	02.0	.	.	.	.	01	01.0	.	.	02	01.5	.	.	64
X	-	06.3	16.3	09.4	10.4	17.4	-	24.5	09		-	19	02.0	.	.	01	01.0	.	.	01	02.0	01	03.0	21	03.0	01	02.0	49
XI	-	04.2	11.9	06.0	07.0	13.3	-	19.6	04		-	10	02.0	.	.	02	02.5	.	.	10	03.5	.	.	17	02.3	.	.	51
XII	-	-00.5	05.0	00.8	01.5	-	-	-	-	-	-	11	01.7	.	.	01	02.0	.	.	04	02.2	.	.	19	02.4	.	.	58
GOD.	-	08.8	14.9	10.1	-	-	-	-				-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
ISTOK — φ = 42° 47' N λ = 20° 30' E Gr. Δ G = + 1h 22 min. — BR. ST 220																												
I	-	01.2	03.1	02.2	02.2	04.8	00.0	14.0	07	-06.3	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	01.4	05.7	03.0	03.3	06.8	-00.4	16.8	06	-10.0	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	03.5	09.5	05.9	06.2	10.6	01.6	21.5	27	-05.6	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	09.2	15.3	10.9	11.6	16.5	05.5	26.7	26	-02.8	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	11.7	17.0	12.1	13.2	17.8	07.9	25.2	11	01.9	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	17.4	23.2	17.6	18.9	24.6	11.8	30.0	18	06.3	06,05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	18.4	25.0	18.8	20.3	26.5	13.0	31.5	25,24	07.9	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	19.1	25.6	18.7	20.6	26.7	13.2	32.1	07	06.8	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	13.9	21.8	14.9	16.3	22.6	09.0	30.4	11	-01.7	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	07.2	15.4	09.4	10.3	17.0	05.1	26.4	10	01.1	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	04.5	11.0	06.3	07.0	12.6	02.3	19.4	01	-01.4	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	00.8	04.9	01.6	02.2	06.0	-01.4	15.5	31	-08.[illegible]	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	09.0	14.8	10.1	11.0	16.0	05.6	32.1	7.VIII	-1[illegible]	48.II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana n, sa: Tn ≤ -20,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⚹	⚹	⚹	∽	▲	▲	⊤	≡	▦
BR. ST. 216																																					
I	8.6	7.7	6.8	7.7	-	-	-	-	-	-	-	062	019.9	17	04	07	23	.	.	.	.	.	.	17	14	10	02	08	08	.	.	.	.	.	.	02	12
II	8.6	7.9	7.9	8.1	-	-	-	-	-	-	-	160	040.5	04	01	06	21	.	.	.	.	.	01	17	20	17	05	08	14	02	.	.	.	.	.	.	21
III	7.5	7.5	6.3	7.1	-	-	-	-	-	-	-	089	028.6	15	.	01	16	.	.	.	.	.	02	16	12	08	03	08	09	05	.	.	.	.	.	06	03
IV	6.7	7.4	4.5	6.2	-	-	-	-	-	-	-	080	011.0	03	.	.	05	.	.	.	.	.	04	10	12	11	03	09	05	02	.	.	.	.	.	.	.
V	7.0	8.0	6.4	7.1	-	-	-	-	-	-	41	137	015.5	25	.	.	01	02	.	.	.	.	03	14	19	17	06	19	.	.	.	.	.	.	03	02	.
VI	5.2	6.4	4.1	5.3	-	-	-	-	-	-	48	099	-	-	.	.	.	12	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	3.9	6.1	3.5	4.5	-	-	-	-	-	-	41	127	036.9	06	.	.	.	16	01	.	.	.	09	06	12	10	04	12	.	.	.	.	.	.	06	01	.
VIII	3.1	5.9	2.5	3.8	-	-	-	-	-	-	35	041	030.4	11	.	.	.	16	03	.	.	.	09	02	05	03	01	05	.	.	.	.	.	01	04	.	.
IX	3.3	4.1	1.8	3.1	-	-	-	-	-	-	34	017	013.7	01	.	.	02	08	03	.	.	.	14	01	03	03	01	03	.	.	.	.	.	.	.	01	.
X	5.6	5.2	4.5	5.1	-	-	-	-	-	-	30	083	027.8	23	.	.	06	.	.	.	.	.	11	09	10	08	02	08	02	.	.	.	.	.	.	06	.
XI	5.8	5.8	4.1	5.2	-	-	-	-	-	-	35	062	013.7	09	.	.	11	.	.	.	.	.	07	10	07	06	03	07	01	01	.	.	.	.	.	03	.
XII	7.6	7.4	6.9	7.3	-	-	-	-	-	-	-	046	009.2	23	.	06	24	.	.	.	.	.	03	16	11	11	.	08	03	.	.	.	.	.	.	05	03
GDO.	6.1	6.6	4.9	5.9	-	-	-	-	-	-	-	1003	-		03	20	109	54	07	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 217																																					
I	8.5	7.9	7.3	7.9	048.0	04.1	86	73	81	80	46	036	006.2	23	.	05	21	.	.	.	06	.	01	17	14	06	.	10	04	.	.	.	.	.	.	06	06
II	8.7	7.4	7.1	7.8	080.0	03.9	83	64	81	76	36	092	019.2	24	02	03	19	.	.	.	03	01	01	14	19	14	03	10	14	01	.	.	.	.	.	01	15
III	7.4	6.8	4.9	6.4	134.6	04.3	78	53	72	68	16	058	016.7	16	.	01	12	.	.	.	08	.	01	10	13	09	02	09	06	02	.	.	.	.	.	.	03
IV	6.8	7.7	5.1	6.5	161.0	06.4	80	49	73	67	-	039	008.9	13	-	-	-	-	-	-	11	.	01	12	16	11	.	16	03	01	.	.	.	.	04	.	.
V	6.9	7.5	6.0	6.8	177.9	08.1	83	56	81	74	33	140	009.1	17	.	.	01	02	.	.	08	.	.	18	14	08	.	11	03	01	.	.	.	.	.	02	12
VI	4.5	5.4	4.1	4.7	251.6	11.2	82	54	80	72	-	066	033.5	19	-	-	-	-	-	-	04	.	02	03	16	10	02	16	.	.	.	.	.	01	11	01	.
VII	3.5	4.8	3.7	4.0	263.8	12.2	83	55	83	73	-	135	044.3	05	-	-	-	-	-	-	02	.	12	06	11	10	04	11	.	.	.	.	.	.	14	01	.
VIII	3.0	4.6	2.1	3.2	287.9	11.4	83	46	82	70	24	044	027.4	23	.	.	.	21	06	.	05	.	12	02	07	06	01	07	.	.	.	.	.	.	09	01	.
IX	3.7	3.0	1.4	2.7	274.9	08.2	87	37	77	67	19	024	012.0	01	.	.	04	09	05	.	05	.	13	.	04	03	02	04	.	.	.	.	.	.	.	.	.
X	5.6	5.2	4.5	5.1	158.9	06.5	89	55	84	76	19	084	022.2	17	.	.	02	.	.	.	03	.	10	09	11	11	03	11	03	03	.	.	.	.	.	01	01
XI	5.6	5.9	3.6	5.0	129.8	05.3	88	57	83	76	26	022	005.6	23	.	.	09	.	.	.	03	.	05	07	08	07	.	08	.	.	.	-	-	-	-	-	-
XII	7.8	7.1	7.5	7.4	062.1	04.3	87	72	85	81	-	022	006.2	23	.	.	.	.	.	.	06	.	01	17	14	06	.	10	04	.	.	.	.	.	.	06	06
GDO.	6.0	6.1	4.8	5.6	2030.5	07.2	84	55	80	73	-	762	044.3	5.VII	-	-	-	-	-	-	64	01	59	115	147	101	17	123	39	08	.	-	-	-	-	-	-
BR. ST. 218																																					
I	9.3	9.4	8.8	9.2	014.9	04.6	87	83	86	85	35	132	039.1	17	.	05	19	.	.	.	02	.	.	26	14	11	07	11	05	.	.	.	.	.	01	05	07
II	7.6	7.7	6.4	7.2	086.4	04.2	82	64	78	75	27	090	016.4	24	01	02	18	.	.	.	04	.	.	10	15	13	04	12	07	03	.	.	.	.	01	01	12
III	7.4	7.5	5.7	6.8	121.9	04.6	76	57	68	67	22	126	029.1	15	.	.	11	.	.	.	03	.	04	15	14	12	04	13	07	04	.	.	.	.	01	.	03
IV	6.4	6.5	4.9	5.9	172.6	06.0	71	50	60	60	24	088	033.8	09	.	.	03	03	.	.	06	.	02	09	12	12	02	10	02	.	.	.	.	.	01	.	01
V	7.1	7.6	6.0	6.9	160.3	07.5	75	55	66	65	32	094	018.8	21	.	.	.	02	.	.	04	.	01	12	17	10	04	17	01	.	.	.	.	01	07	.	.
VI	4.9	6.5	4.8	5.4	223.8	10.8	74	52	65	64	41	026	006.8	01	.	.	.	18	01	.	.	.	02	04	15	07	.	15	.	.	.	.	.	.	10	.	.
VII	4.1	5.5	4.5	4.7	-	12.0	76	53	69	66	30	062	013.8	17	.	.	.	22	03	.	02	.	06	06	13	11	01	13	.	.	.	.	.	.	07	.	.
VIII	3.6	5.5	3.5	4.2	250.2	11.5	75	46	68	63	32	043	021.9	31	.	.	.	22	04	.	.	.	06	03	07	05	02	07	.	.	.	.	.	.	10	.	.
IX	3.7	4.7	2.3	3.5	225.9	09.4	80	48	67	65	29	009	006.1	01	.	.	01	09	01	.	.	.	11	04	05	03	.	05	.	.	.	.	.	.	01	.	.
X	5.3	4.9	4.1	4.8	168.6	06.8	85	55	74	72	29	113	037.6	23	.	.	.	.	.	.	01	.	10	09	11	09	04	11	.	.	.	.	.	.	02	.	.
XI	6.0	5.7	4.7	5.5	121.2	05.9	88	66	85	79	41	054	015.2	17	.	.	08	.	.	.	01	.	06	08	11	06	03	11	.	.	.	.	.	.	01	01	.
XII	5.9	5.9	4.7	5.5	090.0	04.3	82	71	81	78	28	066	017.3	29	.	04	21	.	.	.	04	.	06	11	11	07	03	08	04	02	.	.	.	.	03	07	04
GDO.	5.9	6.4	5.0	5.8	-	07.3	79	58	72	69	22	903	039.1	仟 1	01	11	81	76	09	.	27	.	54	117	145	106	34	133	26	09	.	.	.	01	45	14	27
BR. ST. 219																																					
I	-	-	-	-	-	05.0	91	86	91	89	57	162	041.4	17	.	06	18	.	.	.	.	01	-	-	17	14	05	14	04	01	.	.	.	.	.	04	06
II	7.9	7.5	7.7	7.7	-	05.0	86	75	85	82	36	137	021.8	19	04	01	16	.	.	.	03	02	.	14	16	13	06	11	06	01	.	.	.	.	01	01	13
III	7.6	5.4	6.2	6.4	-	05.1	82	61	74	72	25	126	024.6	15	.	.	14	.	.	.	.	01	03	13	14	11	05	13	03	02	.	.	.	.	.	01	.
IV	6.0	5.9	6.4	6.1	-	06.9	78	56	72	69	20	128	034.3	09	.	.	03	03	.	.	01	.	05	13	13	09	06	12	01	.	.	.	.	.	.	.	01
V	6.5	6.9	5.9	6.5	-	-	-	-	-	-	-	094	034.0	21	-	-	-	-	-	-	.	.	04	12	14	11	03	14	.	.	.	.	.	.	01	.	.
VI	3.4	4.4	3.7	3.8	-	-	-	-	-	-	-	048	015.0	01	.	.	.	22	05	.	.	01	10	03	08	07	02	08	.	.	.	.	.	01	01	.	.
VII	-	-	-	-	-	-	-	-	-	-	-	059	016.5	17	-	-	-	-	-	-	.	.	-	-	06	06	04	06	.	.	.	.	.	.	04	01	.
VIII	-	-	-	-	-	-	-	-	-	-	-	048	021.5	31	-	-	-	-	-	-	.	.	-	-	05	05	02	05	.	.	.	.	.	.	02	.	.
IX	-	-	-	-	-	-	-	-	-	-	-	021	012.0	01	-	.	-	15	03	-	.	.	-	-	03	03	01	03	.	.	.	.	.	.	.	.	.
X	-	-	-	-	-	-	-	-	-	-	-	148	041.0	22	-	.	-	.	.	-	01	03	-	-	10	10	05	10	02	02	.	.	.	.	.	.	.
XI	-	-	-	-	-	-	-	-	-	-	-	077	019.1	17	-	.	-	.	.	-	02	01	-	-	11	10	03	11	.	.	.	.	.	.	.	01	.
XII	-	-	-	-	-	-	-	-	-	-	-	084	018.3	29	-	-	-	-	-	-	01	.	-	-	09	09	05	07	02	.	.	.	.	.	.	05	-
GDO.	-	-	-	-	-	-	-	-	-	-	-	1132	041.4	仟 1	-	-	-	-	-	-	08	09	-	-	126	108	47	114	18	06	.	.	.	01	09	13	-
BR. ST. 220																																					
I	9.5	9.1	9.1	9.3	-	-	-	-	-	-	40	094	035.1	17	.	06	18	.	.	.	-	-	.	25	10	09	04	09	03	01	.	.	.	.	.	06	04
II	-	-	-	-	-	-	-	-	-	-	21	084	018.3	24	01	.	16	.	.	.	-	-	-	-	13	11	02	13	03	02	.	.	.	.	.	04	-
III	-	-	-	-	-	-	-	-	-	-	-	056	013.6	15	.	.	13	.	.	.	-	-	-	-	11	11	01	11	04	04	.	.	.	.	.	02	-
IV	-	-	-	-	-	-	-	-	-	-	29	057	013.8	09	.	.	03	04	.	.	.	.	-	-	12	11	03	11	03	03	.	.	.	.	04	01	.
V	-	-	-	-	-	-	-	-	-	-	17	084	026.2	29	.	.	.	02	.	.	.	.	-	-	15	12	02	15	.	.	.	.	.	.	06	.	.
VI	-	-	-	-	-	-	-	-	-	-	29	032	011.1	30	.	.	.	19	01	.	.	.	-	-	07	07	01	07	.	.	.	.	.	.	08	01	.
VII	-	-	-	-	-	-	-	-	-	-	36	084	028.6	05	.	.	.	23	04	.	.	.	-	-	08	08	02	08	.	.	.	.	.	01	06	01	.
VIII	-	-	-	-	-	-	-	-	-	-	37	039	012.1	12	.	.	.	21	05	.	.	.	-	-	06	06	01	06	.	.	.	.	.	.	07	01	.
IX	-	-	-	-	-	-	-	-	-	-	34	030	013.4	01	.	.	01	10	02	.	.	.	-	-	03	03	02	03	.	.	.	.	.	.	.	02	.
X	-	-	-	-	-	-	-	-	-	-	49	075	023.1	23	.	.	.	02	.	.	.	-	15	07	09	07	02	09	.	.	.	.	.	.	01	02	.
XI	-	-	-	-	-	-	-	-	-	-	46	030	010.8	17	.	.	10	.	.	.	-	-	-	-	07	06	01	07	.	.	.	.	.	.	.	01	.
XII	-	-	-	-	-	-	-	-	-	-	38	044	013.2	31	.	01	20	.	.	.	-	-	-	-	07	07	02	05	02	.	.	.	.	.	02	05	.
GDO.	-	-	-	-	-	-	-	-	-	-	-	709	035.1	仟 1	01	07	81	81	12	.	-	-	-	-	108	98	23	104	15	10	.	.	.	01	34	26	-

TOPLI DO — H_a = 700 m H_b = - m h_v = 2,0 m h_p = 1,5 m

DIMITROVGRAD — H_a = 446 m H_b = 446,8 m h_v = 2,0 m h_p = 1,2 m

PEĆ — H_a = 498 m H_b = 500,8 m H_v = 2,0 m h_p = 1,5 m

SKIVIJANE-DJAKOVICA — H_a = 415 m H_b = - m h_v = 2,0 m h_p = 1,5 m

ISTOK — H_a = 465 m H_b = - m h_v = 2,0 m h_p = 1,5 m

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dim)	MEX	MIN	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.	J.	Č.
φ = 42° 38' N λ = 20° 34' E Gr. Δ G = + 1h 22 min.																												**KLINA** BR. ST. 221
I	-	1.0	03.7	02.2	02.2	05.2	-00.2	15.5	07	-07.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	00.5	05.9	02.7	02.9	07.2	-01.2	15.0	06	-10.7	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	03.3	10.5	05.9	06.4	11.5	01.6	22.5	27	-05.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	08.2	16.4	10.5	11.4	17.2	04.6	27.6	24	-04.0	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	11.1	18.1	12.8	13.7	19.0	07.4	27.4	10	-01.9	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	17.8	25.9	19.4	20.7	27.0	12.9	33.3	23	07.0	20,19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	16.2	27.0	19.1	20.3	28.1	12.5	34.0	08	07.5	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	11.5	23.3	14.9	16.1	24.1	08.3	32.0	12,11	-03.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	05.8	16.2	09.6	10.3	17.3	03.9	25.0	09	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	02.4	12.1	05.8	06.5	12.0	00.7	20.5	01	-05.2	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-01.2	09.6	00.9	01.6	06.2	-02.8	15.0	30	-10.5	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-				-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 42° 13' N λ = 20° 44' E Gr. Δ G = + 1h 23 min.																												**PRIZREN** BR. ST. 222
I	-	01.2	03.7	02.6	02.5	05.1	00.3	17.5	07	-06.0	21	14	01.1	23	01.6	09	01.2	09	01.6	08	01.4	08	02.4	06	02.2	03	01.3	13
II	-	02.5	05.8	03.8	04.0	07.5	00.7	15.8	06	-10.6	18	03	02.0	22	02.0	09	02.1	01	01.0	03	02.0	19	02.1	18	02.8	04	01.8	05
III	-	03.9	10.3	06.7	06.9	11.7	02.6	24.6	27	-03.4	02	06	01.7	15	02.3	11	02.2	13	01.3	09	01.8	16	02.2	14	02.4	07	01.9	02
IV	-	09.7	15.8	11.7	12.3	17.0	07.3	27.3	24	-00.6	04	04	01.5	17	02.2	11	01.5	05	01.4	06	01.5	12	01.8	22	02.7	05	03.2	08
V	-	11.7	17.7	13.6	14.2	19.3	09.7	28.4	11	-00.4	02	10	01.5	17	02.2	09	01.7	08	02.1	09	01.7	10	01.7	17	02.4	04	02.5	09
VI	-	17.4	25.1	19.8	20.5	26.5	14.1	32.6	18	07.4	04	10	01.7	14	01.7	06	01.8	11	01.5	06	01.3	16	01.4	13	02.0	07	01.6	09
VII	-	18.6	25.5	20.8	21.4	27.5	15.5	34.2	23	10.1	19	07	01.7	24	01.9	08	01.6	19	01.5	05	01.4	14	01.7	12	02.3	03	02.3	01
VIII	-	17.9	27.6	21.6	22.1	28.8	15.5	36.2	08	09.3	28	13	01.5	17	01.8	11	01.3	10	02.1	10	01.4	13	01.2	09	01.9	08	01.1	02
IX	-	13.0	22.9	17.4	17.6	23.8	11.1	32.7	12	-00.8	30	13	01.5	17	01.8	10	01.3	11	01.5	06	01.5	19	01.4	06	01.3	05	01.2	03
X	-	07.4	15.8	11.2	11.4	17.3	06.1	23.3	11	00.0	17	12	01.6	11	02.0	07	01.3	13	01.4	11	01.5	10	01.5	16	02.4	08	01.6	05
XI	-	05.6	12.0	07.9	08.3	13.4	04.0	19.1	04	-02.4	28	05	01.2	12	01.8	07	01.6	10	01.4	14	01.4	20	01.8	13	02.7	02	01.0	07
XII	-	00.9	05.0	02.3	02.6	06.2	-00.5	18.8	30	-07.7	21	10	01.0	26	01.8	09	01.6	09	01.6	07	01.3	11	01.6	10	01.7	03	01.3	08
GOD.	-	09.2	15.6	11.6	12.0	17.0	07.2	36.2	8.VIII	-10.6	18.II	107	01.5	215	01.9	105	01.6	119	01.6	94	01.5	168	01.7	156	02.3	59	01.7	72
φ = 42° 53' N λ = 20° 52' E Gr. Δ G = + 1h 24 min.																												**KOSOVSKA MITROVICA** BR. ST. 223
I	-	00.3	02.7	01.2	01.6	04.2	-00.9	15.0	07	-07.7	21	12	03.2	03	01.7	05	03.0	15	02.6	14	01.4	07	01.3	10	01.4	07	02.7	20
II	-	-00.1	04.2	01.6	01.8	05.5	-01.6	-	-	-	-	10	03.5	03	01.7	01	01.0	12	02.5	10	03.3	11	03.9	04	02.8	22	03.1	11
III	-	02.3	08.7	05.0	05.2	09.9	01.0	21.0	27	-05.5	02	09	03.9	08	02.2	02	02.0	14	02.6	13	03.7	10	03.3	06	01.3	17	02.8	14
IV	-	07.5	15.3	09.6	10.5	16.3	04.6	26.5	24	-04.0	05	06	04.7	05	02.4	03	03.3	09	02.6	18	03.7	16	03.6	02	01.5	16	04.1	15
V	-	09.9	16.2	11.8	12.4	17.8	07.0	27.0	11	-02.0	02	07	03.6	04	02.2	.	.	10	01.4	09	03.3	07	04.6	10	01.9	33	03.1	19
VI	-	15.2	22.8	17.3	18.1	24.5	11.3	30.2	18	06.3	06	07	03.1	04	02.8	03	01.7	01	01.0	06	02.3	09	02.8	15	01.5	29	02.3	16
VII	-	16.5	24.6	18.0	19.3	26.0	12.9	32.4	23	06.0	20	05	02.4	08	02.2	02	02.5	09	02.1	04	02.5	11	02.0	08	01.5	27	03.0	19
VIII	-	15.9	25.2	17.5	19.0	26.5	12.2	32.8	08	05.5	28	05	01.6	08	01.9	03	01.7	03	02.0	04	02.5	11	01.9	08	02.5	26	02.3	25
IX	-	10.9	22.0	12.8	14.6	22.6	08.0	31.6	12	-01.6	30	10	02.4	04	02.0	03	01.3	06	02.8	06	01.6	06	01.5	11	01.8	27	02.3	17
X	-	05.8	15.2	08.4	09.5	16.1	03.9	24.1	09	-03.2	01	12	03.2	04	02.2	01	01.0	17	02.1	06	01.8	05	02.2	02	01.0	23	02.6	23
XI	-	-	-	-	-	-	-	19.4	03,01	-04.1	12	07	03.3	05	01.6	02	04.0	13	02.0	03	02.7	06	04.8	03	01.7	26	02.8	25
XII	-	-00.2	04.6	01.3	01.7	05.3	-01.8	13.0	30	-09.5	21	04	03.2	05	02.6	03	02.0	12	02.4	04	02.5	06	02.2	10	01.1	37	02.6	12
GOD.	-	-	-	-	-	-	-	-				94	03.2	61	02.1	28	02.3	121	02.3	91	02.8	109	02.9	89	01.7	290	02.8	216
φ = 42° 39' N λ = 21° 09' E Gr. Δ G = + 1h 25 min.																												**PRIŠTINA** BR. ST. 224
I	710.4	-00.4	02.3	00.4	00.7	03.8	-02.3	14.4	07	-12.2	30	14	02.9	06	02.0	07	03.0	22	02.3	09	01.7	03	01.3	01	01.0	06	01.8	25
II	707.4	-00.7	03.8	01.1	01.3	05.2	-02.7	13.2	06,05	-13.3	18	15	03.1	07	02.7	03	01.3	10	02.0	20	03.0	06	04.3	03	02.0	10	02.6	10
III	708.8	02.2	08.9	04.4	05.0	10.3	00.2	21.5	27	-07.4	02	15	03.0	09	01.4	11	02.1	12	02.9	15	02.9	07	02.6	04	01.5	09	02.2	11
IV	710.2	07.6	14.8	09.4	10.3	16.2	04.6	26.4	24	-03.5	05	16	03.0	05	02.2	08	01.4	13	02.2	13	02.5	16	03.8	04	02.0	03	02.3	12
V	710.7	09.9	15.9	11.3	12.1	17.2	06.9	27.1	11	-01.8	02	14	02.8	11	01.5	04	01.2	07	01.7	05	02.6	15	03.1	06	02.2	20	02.6	11
VI	712.8	15.2	23.4	17.0	18.2	24.2	10.7	30.3	18	04.5	05,06	17	02.1	11	02.1	09	01.3	04	02.0	09	01.8	09	02.2	05	01.4	15	01.9	11
VII	711.6	16.4	24.1	18.3	19.3	25.5	12.3	32.1	23	06.8	19	26	02.6	11	02.1	05	02.6	04	02.0	05	02.2	06	02.3	03	02.0	11	02.2	22
VIII	711.8	15.6	25.7	18.3	19.5	26.9	12.1	32.9	08	06.2	28	14	02.3	08	01.6	07	01.3	06	01.5	12	01.5	05	01.8	05	02.3	08	02.4	28
IX	714.6	10.9	21.6	13.7	15.8	22.4	08.4	31.3	12	-02.0	30	22	03.1	14	02.0	07	01.7	02	01.5	05	01.4	05	01.6	02	01.0	07	01.7	26
X	714.5	05.6	14.6	08.5	09.3	15.9	03.5	23.8	09	-01.0	01	25	02.8	08	02.1	10	01.3	03	02.3	10	02.1	07	01.7	07	02.3	05	02.2	18
XI	713.7	02.6	10.8	04.7	05.7	11.8	00.8	19.5	01	-04.4	12	14	02.4	12	01.5	05	01.2	07	02.3	13	01.8	04	03.2	02	01.8	09	02.2	24
XII	714.5	-00.3	04.3	01.0	01.5	05.0	-02.4	12.7	01	-09.9	21	12	02.5	10	01.6	05	01.6	13	03.2	08	01.6	05	01.8	01	01.8	18	02.5	29
GOD.	711.8	07.0	14.2	09.0	09.8	15.4	04.3	32.9	8.VIII	-13.3	18.II	204	02.7	112	01.9	81	01.6	103	02.3	124	02.2	88	02.7	43	01.8	113	02.3	227
φ = 42° 23' N λ = 21° 10' E Gr. Δ G = + 1h 25 min.																												**UROŠEVAC** BR. ST. 225
I	-	-00.9	02.0	00.6	00.6	03.4	-02.3	14.8	07	-14.0	30	16	01.6	01	03.0	09	02.3	22	03.0	04	01.8	07	01.4	02	02.0	20	02.6	12
II	-	-01.0	04.0	01.1	01.3	04.9	-02.6	14.0	10,06	-13.6	18	16	02.0	01	02.0	01	03.0	16	02.4	04	02.0	10	02.8	10	02.1	25	02.2	01
III	-	02.1	08.6	04.5	05.0	09.7	00.5	20.7	27	-08.1	02	26	02.0	07	02.0	04	02.0	22	03.5	03	01.3	10	01.7	07	02.6	19	02.3	.
IV	-	07.4	14.8	10.1	10.6	15.8	04.8	26.1	24	-03.1	05	26	02.0	03	01.7	03	01.7	18	02.2	04	01.8	13	02.8	07	04.1	15	01.9	.
V	-	10.2	16.3	11.3	12.3	16.9	07.5	26.3	11	-01.8	02	22	01.7	03	01.3	03	02.3	09	01.4	04	01.2	08	02.1	13	04.4	29	02.7	.
VI	-	15.7	23.2	16.2	17.8	23.8	11.0	30.4	18	04.6	05	10	01.7	03	01.7	03	02.0	08	01.9	03	01.3	21	02.2	05	03.2	37	01.8	.
VII	-	16.4	23.5	17.6	18.8	24.9	12.9	32.0	23	06.9	20	13	01.8	03	02.0	01	02.0	07	02.4	06	01.3	25	01.6	16	02.2	22	02.3	.
VIII	-	16.6	25.8	18.3	19.7	26.7	12.6	32.1	08	07.4	28	25	02.0	01	02.0	01	02.0	09	02.3	02	02.0	11	02.2	19	02.7	25	02.9	.
IX	-	11.3	21.5	13.6	15.8	22.1	08.7	30.6	12	-01.9	30	21	01.9	04	02.2	.	.	03	02.0	01	01.0	07	01.9	19	02.2	35	02.2	.
X	-	05.7	14.6	08.4	09.5	15.6	03.8	23.4	09,08	-00.3	17	15	01.6	01	01.0	.	.	10	02.3	02	02.0	12	01.6	11	02.1	49	02.3	01
XI	-	02.5	10.4	04.8	05.6	11.1	01.2	19.0	01	-03.9	12	16	02.1	03	01.0	02	02.5	17	02.2	01	01.0	10	01.5	05	01.6	32	02.2	04
XII	-	-00.5	03.8	00.6	01.1	04.4	-02.1	13.1	01	-08.9	21	19	01.5	01	02.0	03	02.3	05	02.8	07	01.9	09	02.5	16	02.4	32	02.1	02
GOD.	-	07.1	14.1	08.9	09.8	14.9	04.7	32.1	8.VIII	-14.0	30.I	223	01.8	26	01.8	30	02.2	146	02.5	44	01.6	142	02.0	130	02.6	334	02.2	20

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dim)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dim)	Min	Padavine R mm Σ	Max	Dat.	Broj dana u mesecu: Tn ≤ -20.0	Tx < 0.0	Tn < 0.0	Tx ≥ 25.0	Tx ≥ 30.0	Tn ≥ 20.0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 3.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	●	●	●	●	●	●	●	●	●
BR. ST. 221																																					
I	9.6	9.6	9.3	9.5	-	-	-	-	-	-	-	111	038.2	17	.	05	17	.	.	.	-	-	.	27	13	13	03	12	03	02	.	.	.	.	.	07	-
II	8.0	7.8	7.6	7.8	-	-	-	-	-	-	-	061	014.5	24	02	.	18	.	.	.	-	-	02	17	11	10	02	09	04	01	.	.	.	.	.	02	-
III	7.9	6.9	5.5	6.7	-	-	-	-	-	-	-	065	012.6	15	.	.	13	.	.	.	-	-	03	12	10	10	02	10	.	.	.	.	.	.	.	.	.
IV	-	-	-	-	-	-	-	-	-	-	-	063	-	-	.	.	03	04	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	01
V	7.3	7.9	6.7	7.3	-	-	-	-	-	-	-	099	022.4	29	.	.	01	02	.	.	.	.	01	14	13	12	04	13	.	.	.	.	.	.	03	02	.
VI	-	-	-	-	-	-	-	-	-	-	-	025	008.4	21	-	-	-	-	-	-	-	-	-	-	09	05	.	09	.	.	.	.	.	.	-	-	.
VII	3.4	3.7	3.7	3.6	-	-	-	-	-	-	-	074	020.0	06	.	.	.	24	07	.	.	.	12	03	07	06	04	07	.	.	.	.	.	.	-	.	.
VIII	2.6	4.4	2.7	3.2	-	-	-	-	-	-	-	037	015.5	31	.	.	.	25	12	.	.	.	11	02	05	05	02	05	.	.	.	.	.	.	01	.	.
IX	2.8	3.5	1.8	2.7	-	-	-	-	-	-	-	014	008.6	01	.	.	01	13	06	.	.	.	14	02	04	04	.	04	.	.	.	.	.	.	.	.	.
X	7.3	4.2	3.1	4.9	-	-	-	-	-	-	-	094	042.5	23	-	.	-	01	.	-	-	-	07	08	08	07	02	08	.	.	.	.	.	.	.	07	.
XI	7.0	4.4	4.3	5.2	-	-	-	-	-	-	-	039	020.6	16	.	.	12	.	.	.	-	-	04	07	08	06	01	08	.	.	.	.	.	.	.	09	.
XII	7.1	5.3	5.3	5.9	-	-	-	-	-	-	-	070	027.0	31	01	03	25	.	.	.	-	-	07	11	08	06	02	06	03	01	.	.	.	.	.	06	-
GOD.	-	-	-	-	-	-	-	-	-	-	-	752	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 222																																					
I	9.5	9.2	9.1	9.3	019.4	04.9	89	81	85	85	42	116	042.3	17	.	06	13	.	.	.	05	01	.	28	15	09	04	13	05	.	.	.	.	.	.	08	05
II	7.9	7.7	7.4	7.6	083.6	04.6	77	67	76	74	43	125	023.3	08	01	01	13	.	.	.	16	04	.	11	15	13	06	10	08	01	.	.	.	.	04	.	10
III	7.3	6.3	5.9	6.5	141.1	05.0	79	56	69	68	25	108	033.0	15	.	.	07	.	.	.	16	03	03	11	14	11	03	12	06	03	.	.	.	.	.	.	02
IV	6.7	7.0	5.7	6.5	159.1	06.5	72	52	63	62	22	063	014.6	12	.	.	02	06	.	.	16	04	03	12	14	11	02	13	03	01	.	.	.	.	03	01	01
V	6.7	7.4	6.2	6.8	139.9	08.1	78	55	70	68	35	079	021.4	29	.	.	01	05	.	.	12	01	02	13	16	13	01	16	.	.	.	.	.	.	06	.	.
VI	3.8	4.8	3.9	4.2	261.3	10.9	73	47	64	61	27	036	016.0	21	.	.	.	23	08	01	10	.	06	04	12	07	01	12	.	.	.	.	.	.	08	01	.
VII	3.1	4.7	3.4	3.7	286.9	12.5	76	52	68	66	37	076	027.0	05	.	.	.	25	08	.	10	01	13	05	10	09	03	10	.	.	.	.	.	.	08	.	.
VIII	2.8	4.3	2.4	3.2	288.4	11.6	77	43	59	60	28	026	010.7	31	.	.	.	26	15	01	08	.	12	02	05	04	01	05	.	.	.	.	.	.	07	.	.
IX	3.2	3.9	2.2	3.1	238.4	09.8	85	49	61	65	26	013	006.5	01	.	.	01	13	04	.	03	.	14	02	04	03	.	04	.	.	.	.	.	.	03	.	.
X	5.1	4.6	4.6	4.8	177.4	07.2	87	59	71	72	35	132	034.4	23	.	.	.	.	.	.	08	01	11	09	11	09	05	11	02	.	.	.	.	.	02	02	01
XI	5.7	5.2	3.7	4.9	125.9	06.2	85	62	78	75	39	072	024.3	11	.	.	05	.	.	.	09	01	09	07	12	11	02	12	.	.	.	.	.	.	.	02	.
XII	6.2	6.2	5.5	6.0	087.1	04.5	85	72	82	80	35	068	016.0	02	.	04	21	.	.	.	07	01	07	13	12	07	04	11	03	.	.	.	.	.	02	04	03
GOD.	5.7	5.9	5.0	5.6	2008.5	07.6	80	57	70	69	22	914	042.3	17.I	01	11	63	98	35	02	120	17	80	117	140	107	32	129	27	05	.	.	.	.	45	18	22
BR. ST. 223																																					
I	9.4	8.3	8.1	8.6	-	05.0	93	91	92	92	74	081	031.8	17	.	07	20	.	.	.	01	.	.	22	13	08	03	09	06	01	02	.	.	.	.	04	-
II	-	-	-	-	-	04.8	88	79	91	86	49	065	015.5	24	-	-	-	-	-	-	08	.	-	14	12	01	09	07	01	.	.	.	.	.	02	-
III	-	-	-	-	-	-	-	-	-	-	-	047	017.2	20	.	.	10	.	.	.	04	02	-	-	11	07	01	11	05	.	.	.	.	.	.	.	.
IV	-	-	-	-	-	-	-	-	-	-	-	049	016.5	13	.	.	02	04	.	.	06	06	-	-	08	06	02	08	01	01	.	.	.	.	01	.	.
V	-	-	-	-	-	-	-	-	-	-	-	073	017.5	29	.	.	01	02	.	.	01	02	-	-	19	12	02	19	.	.	.	.	.	.	06	01	.
VI	-	-	-	-	-	-	-	-	-	-	-	070	024.2	01	.	.	.	18	02	.	02	.	-	-	09	08	02	09	.	.	.	.	.	.	03	.	.
VII	-	-	-	-	-	-	-	-	-	-	-	061	021.2	07	.	.	.	22	05	.	.	01	-	-	06	05	03	06	.	.	.	.	.	.	02	01	.
VIII	2.4	4.0	2.9	3.1	-	-	-	-	-	-	-	034	013.4	09	.	.	.	21	05	.	02	.	14	02	07	06	01	07	.	.	.	.	.	.	02	02	.
IX	3.0	3.1	2.3	2.8	-	-	-	-	-	-	-	036	013.2	05	.	.	01	09	03	.	01	.	11	01	04	04	01	04	.	.	.	.	.	.	01	02	.
X	5.9	4.1	4.8	4.9	-	-	-	-	-	-	-	076	029.5	23	.	.	02	.	.	.	.	.	09	09	09	07	03	09	01	01	.	.	.	.	.	01	.
XI	6.0	4.4	4.5	5.0	-	-	-	-	-	-	-	034	009.3	16	.	.	12	.	.	.	02	03	06	01	09	07	.	09	.	.	.	.	.	.	.	02	.
XII	7.1	5.9	5.6	6.2	-	-	-	-	-	-	-	063	028.0	31	.	03	21	.	.	.	03	03	04	10	07	05	03	07	.	.	.	.	.	.	.	10	.
GOD.	-	-	-	-	-	-	-	-	-	-	-	689	031.8	17 I	-	-	-	-	-	-	30	17	-	-	116	87	22	107	20	04	02	.	.	.	14	25	-
BR. ST. 224																																					
I	9.4	9.4	8.4	9.1	023.8	04.4	89	81	87	86	59	067	031.6	17	01	08	21	.	.	.	04	.	.	25	13	08	05	07	08	.	01	.	.	.	.	09	09
II	8.3	7.8	6.0	7.3	081.7	04.0	82	68	78	76	41	069	017.1	24	03	04	18	.	.	.	10	04	.	11	16	11	02	10	09	.	.	.	.	.	.	01	12
III	7.3	6.8	5.0	6.4	133.7	04.5	81	55	71	69	24	038	017.2	20	.	.	13	.	.	.	09	01	05	12	12	06	01	10	04	01	01	.	.	.	.	.	01
IV	7.2	6.8	4.9	6.3	173.9	05.8	76	47	65	63	22	047	013.3	13	.	.	03	04	.	.	12	01	02	12	11	06	02	09	03	01	.	.	01	.	02	.	.
V	7.4	7.8	5.8	7.0	163.6	07.5	81	56	75	71	30	140	024.5	29	.	.	01	02	.	.	05	.	02	12	19	14	05	19	02	01	.	.	01	.	07	01	.
VI	4.0	5.4	4.6	4.7	240.4	10.7	81	50	72	68	32	018	011.1	21	.	.	.	19	01	.	.	.	03	04	07	03	01	07	.	.	.	.	.	.	06	.	.
VII	2.9	4.8	4.0	3.9	281.2	11.6	82	53	74	70	34	070	021.7	06	.	.	.	20	02	.	05	.	12	07	07	05	04	07	.	.	.	.	.	.	10	.	.
VIII	3.0	4.4	2.7	3.4	291.0	11.1	84	45	71	67	32	028	009.4	31	.	.	.	22	04	.	07	.	13	03	07	05	.	06	.	.	.	.	.	.	07	02	.
IX	3.4	3.5	2.3	3.1	239.3	09.1	89	47	74	70	21	036	011.7	05	.	.	02	11	03	.	03	.	14	02	09	05	01	09	.	.	.	.	.	.	04	03	.
X	5.4	5.1	4.6	5.0	171.0	06.6	90	57	79	75	26	078	036.3	23	.	.	04	.	.	.	03	.	11	10	12	07	02	12	03	02	.	.	01	.	.	05	01
XI	5.9	5.7	4.8	5.5	127.3	05.5	90	62	83	79	38	032	008.0	16	.	.	12	.	.	.	04	.	07	07	11	08	.	11	.	.	.	.	.	.	.	02	.
XII	7.7	6.5	6.1	6.8	086.2	04.3	84	72	82	79	41	033	010.6	29	.	03	23	.	.	.	08	01	02	15	13	07	01	10	04	.	.	.	.	.	.	06	03
GOD.	6.0	6.2	4.9	5.7	2013.1	07.1	84	57	75	72	21	676	036.3	25 X	04	15	97	78	10	.	70	07	71	120	137	85	24	117	33	05	02	.	03	.	36	29	26
BR. ST. 225																																					
I	9.0	9.0	8.3	8.8	025.7	04.4	89	82	87	86	57	073	031.7	17	01	07	21	.	.	.	01	.	.	20	13	08	02	07	08	.	.	.	.	.	.	04	14
II	8.3	7.4	6.4	7.4	074.2	04.0	82	69	79	77	32	095	018.1	24	03	07	18	.	.	.	01	.	.	13	18	13	02	09	10	.	.	.	.	.	.	02	18
III	7.9	6.6	3.7	6.1	133.1	04.8	80	61	76	72	29	062	015.0	29	.	01	12	.	.	.	03	01	03	10	15	09	03	11	08	.	.	.	.	.	01	.	06
IV	6.8	7.1	4.2	6.0	174.8	06.3	79	52	67	66	28	044	015.1	13	.	.	03	01	.	.	01	.	02	07	12	09	01	09	04	.	.	.	.	.	01	.	.
V	6.8	6.9	4.1	6.0	167.5	07.9	81	59	78	73	33	098	017.6	29	.	.	01	02	.	.	01	.	01	07	17	15	02	17	.	.	.	.	.	.	04	.	.
VI	4.5	5.4	2.8	4.2	270.0	11.2	83	53	80	72	34	038	013.0	12	.	.	.	15	02	.	.	.	03	02	10	06	01	10	.	.	.	.	.	.	07	.	.
VII	4.5	5.7	3.9	4.7	269.8	12.3	84	58	84	75	33	133	040.0	06	.	.	.	20	02	.	.	.	08	06	10	10	05	10	.	.	.	.	.	.	11	.	.
VIII	3.5	5.1	2.7	3.8	288.0	12.3	86	50	79	72	36	014	004.6	31	.	.	.	22	04	.	.	.	09	02	06	04	.	06	.	.	.	.	.	.	07	.	.
IX	4.6	4.5	2.4	3.9	231.6	09.9	91	53	81	75	26	032	012.3	01	.	.	01	11	03	.	.	.	08	02	07	04	01	07	.	.	.	.	.	.	01	.	.
X	6.7	5.5	4.0	5.4	179.9	07.0	92	82	85	80	33	088	025.0	23	.	.	01	.	.	.	.	.	06	10	12	10	03	11	02	.	.	.	.	.	01	05	01
XI	6.7	5.5	4.7	5.6	138.4	05.6	90	67	86	81	25	046	009.6	11	.	.	10	.	.	.	.	.	06	09	10	09	.	10	.	.	.	.	.	.	01	.	.
XII	7.8	6.5	5.0	6.5	077.4	04.3	84	75	87	82	42	042	014.1	03	.	08	21	.	.	.	.	.	03	13	09	05	01	07	02	.	.	01	.	.	.	05	02
GOD.	6.4	6.3	4.4	5.7	2030.4	07.5	85	61	80	75	25	765	040.0	6.VII	04	23	88	71	11	.	07	01	49	101	139	102	21	114	34	.	.	01	.	.	33	17	41

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Sred. (Dies)	Max	Min	Max	Dat.	Min	Dat.	Učestina pravaca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W j.	NW č.	NW j.	C č.
BUJANOVAC — φ = 42° 27' N λ = 21° 47' E Gr. ΔG = + 1h 26 min. — BR. ST. 226																											
I	-	-04.9	-01.0	-03.3	-03.1	-00.4	-07.2	06.0	31	-26.0	13	13	02.6	03	03.7	19	01.7	02	01.0	07	02.4	02	02.0	01	02.0	.	.	46
II	-	00.9	05.6	03.6	03.4	06.8	-00.4	12.5	16	-14.6	12	02	02.5	01	02.0	18	02.0	.	.	26	02.5	02	02.5	01	03.0	.	.	34
III	-	02.5	07.5	05.1	05.1	08.5	01.0	16.2	16	-03.8	07	.	.	02	01.5	32	01.8	04	04.0	19	03.0	.	.	.	.	01	02.0	39
IV	-	04.1	14.9	08.3	09.4	16.1	03.2	26.0	28	-03.0	10	08	02.2	.	.	10	02.0	01	01.0	14	02.5	06	02.0	05	03.0	01	04.0	45
V	-	13.7	24.7	18.1	18.6	25.9	10.0	33.2	30	06.0	24,22	04	03.2	02	03.5	18	01.7	.	.	16	02.6	.	.	02	02.5	01	02.0	50
VI	-	14.8	27.[illegible]	17.3	17.9	24.2	11.4	30.0	25,02	07.2	28	04	02.8	02	03.0	08	02.2	02	02.5	08	03.1	01	02.0	07	03.6	01	03.0	57
VII	-	14.7	23.9	18.0	18.6	25.4	11.7	30.8	08	07.0	15	13	02.8	01	03.0	14	02.4	01	01.0	06	02.8	.	.	03	02.0	02	03.0	53
VIII	-	14.6	27.2	20.0	20.4	28.2	11.8	34.5	15	07.0	27	04	02.5	01	04.0	16	02.3	01	04.0	10	01.8	04	02.2	01	04.0	.	.	56
IX	-	11.9	24.0	16.4	17.2	24.8	10.3	31.5	03	04.5	30,23	06	03.0	02	02.5	08	02.2	02	01.0	11	02.0	.	.	04	03.5	01	02.0	56
X	-	05.0	17.9	10.0	10.7	-	01.6	-	-	-03.0	23,22	03	03.0	.	.	18	02.2	.	.	10	02.2	01	01.0	.	.	01	03.0	60
XI	-	04.1	12.5	08.5	08.3	13.7	00.6	-	-	-09.8	30,29	04	02.8	01	03.0	11	02.2	04	01.2	22	03.5	04	02.2	03	02.7	.	.	41
XII	-	-00.5	01.3	00.0	00.2	02.4	-02.9	13.6	06	-13.5	23	03	03.7	02	02.0	23	01.7	01	06.0	19	02.6	01	04.0	.	.	.	.	44
GOD.	-	06.9	15.1	10.2	10.6	-	04.3	-		-26.0	13. I	64	02.8	17	02.8	195	02.0	18	02.3	168	02.7	21	02.2	27	03.0	08	02.8	577
VRANJE — φ = 42° 33' N λ = 21° 55' E Gr. ΔG = + 1h 26 min. — BR. ST. 227																											
I	722.8	-04.8	-01.6	-03.6	-03.4	-00.4	-06.5	06.4	31	-21.5	13	07	03.0	37	02.4	09	03.2	01	02.0	02	01.0	08	02.4	05	02.2	05	02.2	19
II	718.2	00.7	05.5	02.7	02.9	06.4	-00.6	12.9	16	-11.4	12	03	03.3	25	02.6	06	03.2	.	.	03	02.3	09	02.7	27	03.0	02	01.5	09
III	719.4	02.0	06.8	04.3	04.4	07.9	01.2	16.0	16	-04.2	07	07	03.0	39	02.6	09	02.7	.	.	01	02.0	09	03.2	15	02.5	03	02.0	10
IV	721.2	06.1	14.2	09.6	09.9	15.6	03.9	25.4	28	-02.3	10	12	02.4	32	02.3	04	02.5	.	.	08	02.6	10	02.6	09	02.4	03	02.7	12
V	721.8	15.0	24.0	18.3	18.9	25.2	11.8	32.4	29	05.9	09	12	02.7	31	02.1	05	02.6	01	02.0	04	03.0	13	02.8	10	02.4	05	01.6	12
VI	718.9	15.5	21.6	16.9	17.7	23.1	12.8	29.6	25	08.5	29,28	14	02.6	28	02.4	06	02.2	04	02.0	04	02.2	09	02.1	09	02.9	03	02.0	13
VII	722.7	16.2	23.2	18.3	19.0	24.6	13.0	29.3	08	08.3	16,02	16	03.1	51	02.2	07	02.9	01	03.0	02	02.5	03	01.7	01	03.0	07	03.0	05
VIII	721.3	16.8	26.6	20.2	21.0	27.9	14.0	34.5	16	09.4	21	12	02.4	34	02.2	05	03.6	04	01.8	01	03.0	10	02.6	05	03.0	09	02.7	13
IX	723.7	14.0	23.4	17.3	18.0	24.4	12.4	31.3	03	07.0	23	16	01.9	24	02.3	11	02.6	01	02.0	03	02.7	05	02.4	06	01.8	01	03.0	23
X	726.3	06.0	17.8	11.0	11.4	18.7	04.6	24.6	01	00.8	22	14	02.6	31	02.0	09	02.8	02	01.0	02	01.5	07	01.7	02	03.0	01	03.0	25
XI	722.9	04.8	13.0	08.3	08.6	14.4	03.0	21.3	14	-07.9	29	06	01.7	18	02.3	03	02.3	.	.	03	01.3	14	02.2	22	02.9	03	02.0	21
XII	717.8	-00.8	01.0	-00.6	-00.3	02.0	-03.0	14.6	06	-12.0	23	02	02.0	44	02.4	09	03.0	01	01.0	04	01.8	07	01.7	10	02.7	.	.	16
GOD.	721.5	07.6	14.6	10.2	10.7	15.8	05.6	34.5	16 VIII	-21.5	13. I	121	02.6	394	02.3	83	02.8	15	01.8	37	02.2	104	02.4	121	02.7	42	02.4	178
KUKAVICA — φ = 42° 45' N λ = 21° 59' E Gr. ΔG = + 1h 27 min. — BR. ST. 228																											
I	-	-06.1	-03.9	-05.4	-05.2	-02.2	-08.2	05.5	17	-16.0	12	10	03.3	32	02.2	04	02.0	02	01.0	07	02.4	25	02.5	05	01.6	05	02.4	03
II	-	-02.8	-00.4	-02.1	-01.8	00.9	-04.3	05.5	16	-14.5	12,11	.	.	06	01.7	06	01.3	03	01.7	09	03.4	46	02.9	06	02.3	05	02.0	03
III	-	-01.7	00.9	-00.8	-00.6	01.8	-02.8	09.0	16	-09.0	22	04	02.0	24	02.2	13	01.8	06	01.5	09	02.0	27	02.3	03	02.0	.	.	07
IV	-	02.7	07.1	03.8	04.4	08.4	00.9	19.0	30	-04.5	19,18	16	02.7	12	02.0	21	01.7	.	.	04	02.2	27	03.4	03	01.7	06	02.7	01
V	-	13.0	17.8	13.2	14.3	18.9	10.0	26.5	29	04.5	22,09	09	02.1	15	01.7	07	01.0	02	01.0	06	02.0	34	02.4	02	01.5	06	02.7	12
VI	-	11.8	15.1	11.4	12.4	16.6	09.1	23.5	18	05.0	08	03	01.0	15	01.9	10	01.4	.	.	13	01.7	30	02.6	03	01.7	04	02.0	12
VII	-	13.2	16.5	12.0	13.4	17.4	10.4	23.5	08	05.5	15,12	09	02.1	40	01.9	16	01.2	02	01.5	03	01.0	04	01.2	02	02.5	08	02.4	09
VIII	-	14.8	20.3	14.6	16.1	21.0	13.8	27.3	15	07.5	29	05	01.8	19	01.5	18	01.3	01	01.0	09	02.2	27	02.1	01	03.0	02	01.5	11
IX	-	12.5	16.9	12.3	13.5	17.6	10.3	25.3	04	07.5	29	05	02.6	24	01.8	22	01.5	03	01.7	04	01.2	22	02.7	01	02.0	01	02.0	08
X	-	05.9	11.0	06.5	07.5	12.0	04.2	19.0	01	-01.5	31	09	02.7	37	01.9	28	01.4	.	.	02	01.5	09	01.9	.	.	03	02.7	05
XI	-	04.7	08.5	05.4	06.0	09.6	02.7	19.0	04	-10.0	28	04	02.2	02	02.5	02	01.5	01	02.0	07	03.6	54	03.0	10	02.1	03	03.0	07
XII	-	-02.7	-01.4	-02.6	-02.3	00.0	-05.0	07.5	06	-14.0	22	03	05.0	15	01.9	08	02.0	07	02.1	02	02.0	39	02.4	06	02.2	06	03.2	07
GOD.	-	05.4	09.0	05.7	06.5	10.2	03.3	27.3	15 VIII	-16.0	12. I	77	02.5	241	01.9	155	01.5	27	01.6	75	02.2	344	02.6	42	02.0	49	02.5	85
VLASOTINCE — φ = 42° 58' N λ = 22° 08' E Gr. ΔG = + 1h 29 min. — BR. ST. 229																											
I	-	-04.5	-00.9	-03.0	-02.8	00.2	-06.6	09.0	14	-23.6	13	03	01.3	04	01.0	12	01.4	.	.	12	01.4	04	01.5	08	01.5	01	01.0	49
II	-	01.7	06.0	03.6	03.7	07.5	-00.2	14.5	16	-09.0	11	03	01.0	05	01.2	20	01.6	02	01.5	16	01.7	04	02.0	08	01.4	.	.	26
III	-	02.6	07.2	04.4	04.6	08.2	00.9	18.3	16	-05.0	22,10	08	01.0	05	01.2	13	02.8	01	01.0	12	01.3	09	01.0	14	01.1	02	01.5	29
IV	-	07.8	15.4	10.9	11.2	16.3	04.8	26.5	30	-01.5	10	05	01.4	02	01.5	18	01.8	01	01.0	13	01.4	08	01.8	20	01.8	03	01.3	20
V	-	16.5	25.1	18.5	19.7	26.5	13.0	34.5	29	08.0	24,09	05	01.8	02	01.0	20	01.3	06	01.5	10	01.2	06	01.2	08	01.5	.	.	36
VI	-	16.2	22.2	17.7	18.5	23.9	13.2	30.5	25	10.0	28,27	01	01.0	09	01.0	18	01.1	05	01.0	10	01.3	05	01.0	08	01.8	02	01.0	37
VII	-	16.7	23.9	18.6	19.5	25.3	13.9	31.0	08	10.5	16,02	01	02.0	07	01.4	16	01.2	01	01.0	08	01.1	04	01.2	17	01.4	01	01.0	38
VIII	-	-	-	-	-	28.3	13.3	34.0	25,16	09.0	08	01	02.0	18	01.2	14	01.6	03	01.3	07	01.3	04	01.2	09	01.4	05	01.6	32
IX	-	14.4	23.9	18.2	18.7	24.9	12.8	32.5	04	06.5	29,28	04	02.0	13	01.7	08	01.5	01	01.0	.	.	05	01.8	08	01.4	.	.	51
X	-	05.4	17.8	10.9	11.2	18.5	03.6	26.0	01	-01.5	21	02	02.5	03	01.3	13	01.4	03	01.3	08	01.2	02	01.5	10	01.3	02	01.0	50
XI	-	06.7	14.8	08.9	09.8	15.9	04.6	25.0	14	-05.0	29	01	01.0	05	01.4	28	01.3	04	01.0	12	02.5	04	01.2	03	02.0	01	01.0	32
XII	-	-01.0	01.0	-00.8	-00.4	02.3	-03.0	17.5	06	-13.0	23	04	01.0	04	01.0	09	01.3	05	01.2	12	01.2	09	01.6	12	01.1	.	.	38
GOD.	-	-	-	-	-	16.5	05.9	34.5	29 VI	-23.6	13. I	38	01.4	77	01.3	189	01.5	32	01.2	120	01.5	64	01.4	125	01.4	17	01.3	433
PREDEJANE — φ = 42° 50' N λ = 22° 08' E Gr. ΔG = + 1h 29 min. — BR. ST. 230																											
I	-	-04.6	-01.1	-03.5	-03.2	-00.4	-06.0	08.9	31	-15.1	13	40	01.9	06	01.5	04	01.5	12	01.8	16	02.7	.	.	.	.	04	02.8	11
II	-	00.4	05.5	02.2	02.6	07.3	-00.7	14.6	16	-08.5	12	22	02.3	06	01.8	04	02.0	25	02.2	18	02.6	.	.	.	.	02	02.0	07
III	-	01.7	07.1	03.8	04.1	08.2	01.0	18.0	16	-04.2	07	37	02.2	12	01.6	07	01.6	18	01.7	12	02.4	02	03.5	.	.	.	.	05
IV	-	05.9	14.6	08.7	09.5	16.0	03.4	26.9	30	-02.6	10	26	02.4	05	01.8	15	01.5	18	01.7	15	02.1	03	02.3	.	.	04	02.5	04
V	-	15.0	24.5	16.0	17.9	25.7	10.9	33.6	29	06.5	25	19	02.5	01	02.0	13	01.5	25	01.6	16	02.4	04	02.2	01	02.0	03	03.0	11
VI	-	15.4	21.8	15.9	17.2	23.4	12.6	30.6	24	08.5	29	14	01.9	08	01.5	07	01.3	12	01.6	10	02.0	04	01.8	.	.	07	02.1	28
VII	-	15.7	22.8	16.9	18.1	24.5	12.5	30.8	08	07.9	16	22	02.2	12	01.6	13	01.6	17	01.5	02	02.0	.	.	.	.	06	02.8	21
VIII	-	16.0	26.4	17.4	19.3	27.8	13.2	34.3	15	09.5	29,27	15	02.4	06	01.7	09	01.6	20	01.6	07	01.3	05	01.8	.	.	05	02.4	26
IX	-	12.9	23.4	15.1	16.6	24.4	11.4	33.3	04	05.8	27	19	02.5	03	02.0	03	01.7	13	01.5	07	01.6	01	02.0	02	02.5	03	02.3	39
X	-	03.9	16.8	07.8	09.1	17.5	03.1	26.2	01	-02.1	21	27	02.4	06	01.5	02	01.5	08	01.4	02	02.0	01	02.0	.	.	05	02.6	42
XI	-	05.5	13.9	07.3	08.5	15.1	03.4	23.2	14	-06.3	29	08	02.2	02	01.0	08	01.2	36	01.9	22	02.5	02	01.5	.	.	01	02.0	11
XII	-	-01.5	01.0	-00.9	-00.6	02.3	-03.0	18.5	06	-12.4	23	37	02.1	06	02.0	03	01.0	15	01.9	12	02.3	01	03.0	.	.	.	.	19
GOD.	-	07.2	14.7	08.9	09.9	16.0	05.2	34.3	15 VIII	-15.1	13. I	286	02.2	73	01.6	88	01.5	219	01.7	139	02.3	23	02.1	03	02.3	40	02.5	224

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana s: Tn ≤ -30,0	Tx < 0,0	Tn < 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	P (0-12) ≥ 6	≥ 8	Nm (0-10) < 8,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	✱	✱	≡	≈	▲	▲	T	≡	▦
SIJARINSKA BANJA BR. ST. 226 — H_s = 955 m H_b = - m h_s = 2.0 m h_z = 1.0 m																																					
I	9.5	9.1	8.4	9.0	027.9	-	-	-	-	-	63	063	022.7	17	.	05	19	.	.	.	05	01	.	24	10	09	02	05	06	.	.	.	.	.	.	03	11
II	8.8	7.8	7.8	8.1	058.3	-	-	-	-	-	13	107	019.5	17	03	02	19	.	.	.	02	01	02	18	19	14	03	09	11	01	.	.	.	.	.	02	13
III	8.1	6.9	5.1	6.7	108.8	05.0	82	57	78	72	25	047	010.5	20	.	.	12	.	.	.	04	02	03	14	10	08	02	07	05	02	.	.	.	.	.	01	.
IV	7.6	6.4	5.3	6.5	150.5	-	-	-	-	-	28	061	018.4	13	.	.	04	05	.	.	.	.	03	12	10	10	02	10	02	01	.	.	.	.	.	01	01
V	-	-	-	-	150.6	-	-	-	-	-	40	130	022.2	22	.	.	01	03	.	.	.	.	-	-	17	14	06	17	01	01	.	.	.	.	02	03	.
VI	6.5	4.7	4.2	5.1	196.8	-	-	-	-	-	52	074	027.3	01	.	.	.	17	01	.	.	.	06	08	11	10	02	11	.	.	.	.	.	.	06	07	.
VII	4.0	4.6	4.3	4.3	241.2	-	-	-	-	-	42	088	021.9	06	.	.	.	20	03	.	.	.	12	09	09	08	04	09	.	.	.	.	.	.	02	02	.
VIII	3.4	4.2	3.8	3.8	235.5	-	-	-	-	-	44	041	016.2	17	.	.	.	22	04	.	.	.	14	05	08	08	02	08	.	.	.	.	.	.	05	.	.
IX	5.7	4.8	2.3	4.3	183.1	-	-	-	-	-	32	042	032.4	01	.	.	02	10	06	.	.	.	10	05	05	04	01	05	.	.	.	.	.	.	.	09	.
X	6.4	5.8	5.2	5.8	117.9	-	-	-	-	-	46	115	033.0	22	.	.	01	.	.	.	01	.	11	16	10	10	04	10	02	02	.	.	.	.	.	01	.
XI	6.7	6.0	5.6	6.1	084.7	-	-	-	-	-	34	046	015.2	24	.	.	10	.	.	.	.	01	06	13	09	08	01	09	.	.	.	.	.	.	.	04	.
XII	8.8	7.5	7.2	7.8	037.5	04.7	90	76	85	84	49	035	011.3	31	.	04	22	.	.	.	02	03	01	17	07	06	01	06	01	.	.	.	.	.	.	06	02
GOD.	-	-	-	-	1592.8	-	-	-	-	-	13	849	033.0	18 X	03	11	90	77	14	.	14	08	-	-	125	109	30	106	28	07	.	.	.	.	15	39	27
BUJANOVAC BR. ST. 227 — H_s = 400 m H_b = - m h_s = 2.0 m h_z = 1.5 m																																					
I	9.2	9.3	9.0	9.2	-	05.0	90	83	89	87	59	078	030.2	17	.	07	17	.	.	.	02	.	.	23	13	06	03	08	07	.	.	.	.	.	.	01	08
II	8.2	6.9	7.2	7.4	-	04.7	87	73	90	83	49	060	-	-	02	.	17	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	7.5	6.9	4.7	6.4	-	05.6	85	59	82	75	32	060	018.2	05	.	.	11	.	.	.	02	.	04	11	10	07	02	09	01	.	.	.	.	.	.	.	.
IV	6.4	6.3	4.2	5.6	-	07.1	82	53	70	68	-	036	008.4	12	.	-	-	-	-	-	01	.	06	09	13	06	.	12	02	01	.	.	01	.	02	.	.
V	6.8	6.8	5.0	6.2	-	08.7	89	58	75	74	33	102	025.5	29	.	.	02	03	.	.	01	.	06	13	14	13	03	14	.	.	.	.	.	.	03	01	.
VI	-	-	-	-	-	12.0	88	57	69	71	38	021	010.0	21	.	.	.	23	03	.	.	01	-	-	07	04	01	07	.	.	.	.	.	.	02	01	.
VII	-	-	-	-	-	13.1	88	56	77	74	43	092	026.4	18	.	.	.	23	08	.	.	.	-	-	09	07	03	09	.	.	.	.	.	.	08	.	.
VIII	-	-	-	-	-	13.0	91	55	78	75	27	025	012.6	11	.	.	.	24	09	.	01	.	-	-	06	06	01	06	.	.	.	.	.	.	06	02	.
IX	3.5	2.6	2.0	2.7	-	10.1	91	48	80	73	28	068	056.0	01	.	.	02	11	05	.	.	.	15	02	05	03	01	05	.	.	.	.	.	.	.	01	.
X	5.5	4.2	3.3	4.3	-	07.3	93	61	75	76	40	088	026.4	23	.	.	03	.	.	.	.	.	13	09	08	08	03	08	02	01	.	.	.	.	.	08	01
XI	6.0	5.1	3.7	5.0	-	05.6	90	67	76	78	43	029	010.2	11	.	.	13	.	.	.	.	.	08	09	09	08	01	09	.	.	.	.	.	.	01	02	.
XII	7.7	6.6	6.1	6.8	-	04.6	87	77	79	81	54	028	-	-	01	01	21	.	.	.	02	.	06	15	-	-	-	-	-	-	-	-	-	-	.	.	-
GOD.	-	-	-	-	-	08.1	88	62	78	76	-	687	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VRANJE BR. ST. 228 — H_s = 458 m H_b = 460.4 m h_s = 2.0 m h_z = 1.2 m																																					
I	9.2	9.2	9.3	9.2	027.1	04.7	87	80	86	84	56	059	020.7	17	.	07	20	.	.	.	01	.	.	27	16	07	03	11	08	01	.	.	01	.	.	03	13
II	8.5	8.1	6.8	7.8	078.2	04.2	86	66	76	76	34	069	015.3	24	01	02	18	.	.	.	02	01	01	17	18	13	02	11	12	02	01	.	.	.	01	01	09
III	7.6	7.4	6.0	7.0	134.5	04.8	81	56	68	68	32	062	013.6	15	.	01	08	.	.	.	04	.	02	16	13	07	03	09	06	02	.	.	.	.	.	01	01
IV	7.9	7.3	5.6	6.9	170.2	06.5	78	51	63	64	24	039	010.3	12	.	.	02	05	.	.	04	.	.	13	16	07	01	15	04	01	.	.	01	.	02	01	.
V	7.2	7.6	5.7	6.8	168.0	07.8	80	55	72	69	30	106	017.7	25	.	.	.	02	.	.	02	.	02	11	19	14	03	18	02	.	.	.	.	01	04	01	.
VI	4.3	5.9	4.3	4.9	253.3	10.8	78	51	68	66	35	039	015.9	21	.	.	.	21	02	.	01	.	05	05	12	04	02	12	.	.	.	.	.	.	01	01	.
VII	3.3	4.8	3.8	4.0	295.0	11.9	80	51	70	67	32	065	016.0	17	.	.	.	22	07	.	.	.	09	04	10	07	04	10	.	.	.	.	.	.	10	01	.
VIII	3.5	5.5	2.8	4.0	286.7	11.6	80	48	70	66	27	032	014.7	11	.	.	.	21	08	.	.	.	12	04	10	06	01	10	.	.	.	.	.	01	09	02	.
IX	3.7	4.1	2.6	3.5	256.7	09.1	84	46	65	65	24	033	027.8	01	.	.	01	10	05	.	02	.	12	02	02	02	01	02	.	.	.	.	.	.	01	.	.
X	5.3	5.2	4.8	5.1	175.4	07.0	89	57	78	75	34	081	031.0	23	.	.	01	.	.	.	.	.	11	11	10	08	03	10	03	01	.	.	.	.	.	04	01
XI	6.6	5.7	4.3	5.5	124.0	05.6	89	64	81	78	37	026	006.9	09	.	.	08	.	.	.	01	.	04	10	10	05	.	09	.	.	.	.	.	.	.	05	.
XII	8.2	7.2	7.2	7.5	065.9	04.6	87	76	85	83	50	036	008.9	02	.	04	20	.	.	.	.	.	02	17	15	09	.	09	05	.	.	.	01	.	.	09	03
GOD.	6.3	6.5	5.3	6.0	2035.0	07.4	83	58	73	71	24	647	031.0	15 X	01	14	78	81	22	.	17	01	60	137	151	89	23	126	40	07	01	.	03	02	28	29	27
KUKAVICA BR. ST. 229 — H_s = 1250 m H_b = - m h_s = 2.0 m h_z = 1.5 m																																					
I	7.4	7.4	7.6	7.4	-	03.7	86	86	87	86	69	075	021.4	17	07	08	24	.	.	.	.	.	03	18	12	08	02	04	10	01	.	.	.	.	.	14	19
II	7.8	7.0	7.3	7.4	-	03.4	82	84	83	83	59	138	021.1	24	06	14	21	.	.	.	02	.	.	14	20	18	05	05	19	03	.	.	.	.	.	09	24
III	7.0	5.8	6.2	6.4	-	03.8	81	77	81	79	36	082	016.2	15	02	06	23	.	.	.	02	.	01	09	13	11	04	04	10	01	.	.	01	.	.	09	20
IV	6.7	6.0	5.7	6.2	-	05.7	82	74	80	79	46	075	016.4	19	.	02	10	.	.	.	01	.	04	11	14	11	03	10	07	.	.	.	01	.	01	06	01
V	6.7	6.1	5.5	6.1	-	06.6	87	77	84	83	46	240	050.4	19	.	.	06	.	.	.	.	.	02	10	15	15	10	10	06	01	.	.	.	.	02	09	04
VI	4.1	4.9	4.0	4.3	-	09.8	81	72	82	78	47	099	030.4	20	.	.	.	.	.	.	.	.	06	05	11	10	02	11	.	.	.	.	01	.	03	02	.
VII	3.2	4.3	3.9	3.8	-	11.1	83	74	87	81	43	114	029.6	18	.	.	.	02	.	.	.	.	11	04	08	08	06	08	.	.	.	.	.	.	06	07	.
VIII	3.2	4.1	3.1	3.5	-	10.2	75	65	77	72	38	050	018.2	12	.	.	.	05	.	.	.	.	11	02	07	07	02	07	.	.	.	.	.	.	06	02	.
IX	3.6	3.1	2.6	3.1	-	07.9	78	65	74	72	37	042	021.3	01	.	.	02	04	.	.	.	.	12	01	04	03	02	04	.	.	.	.	.	.	.	02	.
X	5.3	4.6	4.6	4.8	-	06.2	86	75	85	82	40	110	043.9	23	.	03	07	.	.	.	.	.	11	08	11	08	03	06	06	.	.	.	.	.	.	05	06
XI	5.4	4.5	3.8	4.6	-	-	-	-	-	-	-	048	014.8	09	.	.	14	.	.	.	.	.	09	08	09	06	02	06	06	01	.	.	.	.	.	04	05
XII	7.4	6.5	6.2	6.7	-	03.8	86	84	85	85	51	064	017.4	02	.	13	23	.	.	.	.	01	04	15	09	08	02	02	07	.	.	.	.	.	.	10	16
GOD.	5.6	5.4	5.0	5.4	-	-	-	-	-	-	-	1137	050.4	19 V	15	46	130	11	.	.	05	01	74	105	133	113	43	77	71	07	.	.	03	.	18	79	95
VLASOTINCE BR. ST. 230 — H_s = 270 m H_b = - m h_s = 2.0 m h_z = 1.5 m																																					
I	8.0	7.5	7.0	7.5	-	-	-	-	-	-	-	074	033.0	17	01	05	15	.	.	.	.	.	.	16	10	09	02	08	07	05	.	.	.	.	.	03	12
II	7.9	7.1	6.2	7.1	-	-	-	-	-	-	-	134	034.5	04	02	02	16	.	.	.	.	.	03	13	16	15	04	11	08	03	.	.	.	.	.	05	11
III	6.6	6.3	5.9	6.3	-	-	-	-	-	-	-	058	031.5	20	.	.	05	.	.	.	.	.	02	11	13	07	02	13	02	01	01	.	.	.	.	05	.
IV	6.3	6.6	5.1	6.0	-	-	-	-	-	-	-	065	016.0	12	.	.	.	06	.	.	.	.	04	11	11	09	04	11	.	.	.	.	.	.	01	01	.
V	6.9	6.7	6.1	6.6	-	09.3	82	66	82	77	38	116	019.5	25	.	.	.	06	.	.	.	.	02	11	19	14	04	19	01	01	.	.	.	.	-	03	.
VI	5.3	5.1	5.6	5.4	-	-	-	-	-	-	-	069	018.0	21	.	.	.	23	04	.	.	.	04	08	13	09	03	13	.	.	.	.	.	.	-	.	.
VII	4.1	5.3	4.8	4.7	-	-	-	-	-	-	-	108	025.5	05	.	.	.	23	08	01	.	.	07	07	10	09	05	10	.	.	.	.	.	.	-	.	.
VIII	3.5	4.5	4.2	4.1	-	-	-	-	-	-	-	036	011.0	11	.	.	.	24	13	.	.	.	10	05	07	04	02	07	.	.	.	.	.	.	02	.	.
IX	4.1	3.2	2.6	3.3	-	10.2	86	52	74	71	32	027	018.5	01	.	.	01	13	06	.	.	.	13	02	06	02	01	06	.	.	.	.	.	.	.	06	.
X	5.9	4.7	4.7	5.1	-	07.9	88	66	86	80	31	096	035.5	23	.	.	.	02	.	.	.	.	09	10	10	10	02	10	03	02	.	.	.	.	.	08	01
XI	6.5	5.3	4.2	5.4	-	06.4	84	66	77	76	32	036	010.0	11	.	.	03	.	.	.	.	.	06	10	07	06	01	07	.	.	.	.	.	.	.	02	.
XII	8.5	7.1	7.5	7.7	-	-	-	-	-	-	-	023	010.0	02	.	02	19	.	.	.	.	.	01	17	06	03	01	05	02	01	.	.	.	.	.	07	01
GOD.	6.1	5.8	5.3	5.8	-	-	-	-	-	-	-	842	035.5	25 X	03	09	59	97	31	01	.	.	61	121	128	97	31	120	23	13	01	.	.	.	-	40	25

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C Tm 7	14	21	Sred. (Dles)	Max	Min	Max	Dat.	Min	Dat.	Cestina pravca i srednja jačina vetra HD, Fm (0-12) N d.	j.	NE d.	j.	E d.	j.	SE d.	j.	S d.	j.	SW d.	j.	W	j.	NW d.	j.	C d.
PREDEJANE $\varphi = 42^\circ 50'$ N $\lambda = 22^\circ 08'$ E Gr. $\Delta G =$ + 1h 29 min. BR. ST. 231																												
I	-	00.9	03.8	01.8	02.1	05.4	-00.5	15.2	13,07	-07.3	20	22	02.0	04	02.2	10	01.9	23	02.0	21	02.7	03	02.3	.	.	04	01.8	06
II	-	-00.5	04.7	01.5	01.8	06.5	-02.0	15.5	10,06	-11.2	18	24	02.5	07	01.7	04	01.0	23	02.0	14	02.0	.	.	.	.	01	04.0	11
III	-	03.4	09.6	05.5	06.0	11.5	01.6	23.3	25	-04.5	03,02	27	02.3	05	02.0	07	01.3	28	01.8	16	02.3	03	02.3	.	.	03	03.0	04
IV	-	08.3	16.0	10.4	11.3	17.8	05.4	27.5	24	-02.4	05	22	02.1	05	01.6	07	01.4	29	01.6	15	02.2	02	02.5	01	02.0	03	02.7	06
V	-	10.8	17.4	11.6	12.9	18.6	08.0	29.0	11	00.1	02	24	02.4	07	01.9	08	01.6	20	01.6	08	02.5	01	02.0	01	02.0	04	02.5	20
VI	-	16.2	23.3	16.6	18.2	25.0	12.5	-	-	-	-	21	02.2	04	01.8	09	01.4	16	01.4	14	01.7	.	.	01	02.0	04	02.5	21
VII	-	16.8	24.5	17.7	19.2	26.1	13.9	32.3	25	09.1	20	21	02.1	05	01.6	07	01.1	17	01.5	09	01.9	01	02.0	.	.	07	02.4	26
VIII	-	15.8	25.4	17.4	19.0	27.1	13.5	33.7	21	08.5	28	20	02.0	04	01.5	08	01.2	20	01.6	04	01.5	.	.	02	02.0	03	02.0	32
IX	-	11.2	21.7	12.9	14.7	22.8	09.4	34.0	13	-01.6	30	23	02.3	09	01.7	04	01.2	13	01.7	06	01.7	.	.	01	01.0	06	02.7	28
X	-	06.2	14.8	07.9	09.2	16.2	04.9	26.2	07	00.0	17	34	02.2	05	01.4	02	02.0	16	01.6	11	02.3	.	.	.	.	04	03.0	21
XI	-	03.8	11.8	05.5	06.7	12.5	02.4	22.1	03	-02.0	26,12	18	02.1	03	01.7	07	01.3	21	01.8	23	02.3	01	03.0	.	.	03	03.0	14
XII	-	01.2	04.9	01.7	02.4	05.7	-00.7	17.2	30	-06.5	21	27	02.1	08	02.0	03	01.7	16	02.1	15	02.8	.	.	01	02.0	03	02.7	20
GOD.	-	07.8	14.8	09.2	10.3	16.3	05.7	-		-		283	02.2	66	01.8	76	01.4	242	01.7	194	02.2	11	02.3	07	01.9	45	02.6	209
SURDULICA $\varphi = 42^\circ 41'$ N $\lambda = 22^\circ 11'$ E Gr. $\Delta G =$ + 1h 29 min. BR. ST. 232																												
I	-	00.0	02.8	01.4	01.5	04.4	-01.6	14.5	07	-09.5	21	02	01.5	.	.	29	01.5	05	01.0	04	01.5	04	01.0	04	01.5	04	01.2	41
II	-	-00.3	03.9	01.5	01.6	05.7	-02.4	14.5	10	-11.0	18	04	02.5	01	02.0	15	01.5	05	01.4	.	.	06	01.0	14	01.1	08	01.4	31
III	-	03.2	09.4	05.3	05.8	10.6	00.8	21.6	27	-06.4	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	08.2	15.6	10.3	11.1	17.2	05.5	27.5	24	-02.5	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	10.3	17.1	11.7	12.7	18.1	07.8	28.6	11	00.2	03,02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	15.6	23.6	17.0	18.3	24.5	12.7	31.7	18	07.4	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	17.0	24.5	18.1	19.4	25.7	14.1	31.5	23	08.5	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	16.6	25.5	18.4	19.7	26.8	13.9	33.0	08	09.5	28	02	01.5	01	02.0	22	01.5	06	01.2	01	01.0	06	01.5	04	01.2	06	01.2	45
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	06.7	15.0	09.5	10.2	16.5	04.5	24.5	08	00.0	17,16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	03.0	10.7	05.5	06.2	11.4	01.3	20.9	01	-03.0	30,29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	00.2	04.0	01.5	01.8	04.7	-01.7	15.8	30	-08.2	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GOD.	-	-	-	-	-	-	-	-		-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VLASINA $\varphi = 42^\circ 44'$ N $\lambda = 22^\circ 21'$ E Gr. $\Delta G =$ + 1h 29 min. BR. ST. 233																												
I	-	-04.2	-00.1	-03.2	-02.7	02.1	-06.5	10.7	07	-16.5	24,21	05	01.6	03	01.7	.	.	05	01.6	01	02.0	07	03.4	.	.	08	01.2	64
II	-	-04.0	-00.5	-02.9	-02.6	02.0	-06.6	08.1	11,06	-18.5	22	12	02.0	02	01.0	.	.	.	.	03	03.0	12	02.4	01	03.0	15	01.9	39
III	-	-01.5	03.2	-00.1	00.4	04.4	-03.6	14.7	27	-18.5	03	07	01.7	04	02.5	01	01.0	07	02.1	04	01.5	10	03.1	02	04.0	07	01.3	51
IV	-	04.7	09.4	05.1	06.1	11.5	01.0	21.0	24	-07.6	05	12	02.1	04	02.0	.	.	.	.	01	02.0	16	02.7	01	02.0	13	01.7	43
V	-	06.2	10.4	06.4	07.4	12.0	03.3	22.6	11	-06.0	02	11	01.7	04	01.5	.	.	06	01.8	01	01.0	02	02.0	02	02.0	14	01.9	53
VI	-	13.0	17.3	11.9	13.5	18.7	07.9	24.5	18	02.5	05,04	06	01.8	05	01.2	01	02.0	01	01.0	.	.	01	02.0	.	.	07	01.1	69
VII	-	14.4	18.9	12.9	14.8	20.2	09.5	26.0	23	04.5	19,18	01	01.0	06	01.5	03	01.0	02	01.5	.	.	01	02.0	.	.	05	01.4	75
VIII	-	13.5	19.6	12.4	14.5	21.3	09.3	26.5	08	03.1	28	05	01.4	01	01.0	01	02.0	03	01.3	.	.	.	.	02	01.5	10	01.7	71
IX	-	07.8	16.9	08.4	10.4	17.9	04.9	26.8	13	-05.7	30	08	01.1	03	01.3	01	01.0	08	01.6	.	.	.	.	02	01.5	03	02.0	65
X	-	03.9	09.5	04.2	05.5	11.7	-	23.5	09	-	-	03	02.0	07	01.4	02	01.0	03	01.7	.	.	02	02.0	.	.	04	03.2	72
XI	-	01.5	08.0	02.6	03.7	09.9	-	19.5	03	-	-	03	03.0	05	01.0	04	02.0	.	.	01	02.0	02	02.5	04	01.2	03	02.0	68
XII	-	-02.9	01.1	-02.8	-01.8	02.7	-05.6	11.7	01	-13.4	18	15	03.5	.	.	.	.	.	.	02	02.0	08	03.0	.	.	03	01.0	65
GOD.	-	04.4	09.5	04.6	05.8	11.2	-	26.8	13.IX	-		88	02.1	44	01.5	13	01.5	35	01.7	13	02.0	61	02.8	14	02.0	92	01.7	735
BOSILJGRAD $\varphi = 42^\circ 30'$ N $\lambda = 22^\circ 28'$ E Gr. $\Delta G =$ + 1h 29 min. BR. ST 234																												
I	-	-01.4	03.4	00.4	00.7	04.5	-02.4	13.3	07	-10.2	21	.	.	02	01.5	.	.	10	01.3	.	.	23	01.7	01	01.0	04	01.8	53
II	-	-01.8	04.6	00.5	00.9	06.0	-02.6	13.3	06	-09.9	22	.	.	.	.	.	.	09	01.0	.	.	23	01.3	.	.	07	02.0	50
III	-	00.7	08.3	03.4	04.0	09.2	-00.6	20.9	27	-00.4	02	01	02.0	01	01.0	.	.	20	01.5	.	.	16	01.4	.	.	01	01.0	54
IV	-	06.4	14.4	09.0	09.7	16.3	03.4	26.3	24	-03.3	05	.	.	.	.	01	01.0	19	01.5	.	.	15	01.7	01	01.0	01	04.0	53
V	-	09.6	16.9	10.4	11.3	16.5	04.6	26.8	11	-01.0	26	.	.	01	01.0	.	.	25	01.4	.	.	11	01.5	.	.	.	.	56
VI	-	15.1	21.7	15.4	16.9	23.3	08.5	29.4	18	01.9	07	.	.	.	.	.	.	29	01.3	.	.	15	01.6	.	.	.	.	46
VII	-	16.9	23.0	16.9	18.4	25.4	09.8	31.3	23	04.6	20	.	.	.	.	.	.	36	01.2	01	01.0	21	02.1	.	.	02	03.0	33
VIII	-	16.2	24.2	16.9	18.6	25.8	09.3	31.3	08	05.0	13	.	.	.	.	.	.	24	01.1	.	.	18	01.6	.	.	.	.	51
IX	-	10.5	22.2	13.4	14.9	23.0	05.5	31.4	11	-05.7	30	.	.	.	.	.	.	19	01.4	.	.	17	01.5	.	.	.	.	54
X	-	04.5	14.8	07.4	08.5	15.9	-	-	-	-	-	.	.	.	.	.	.	16	01.2	.	.	19	01.4	.	.	02	02.5	56
XI	-	00.4	11.2	02.7	04.3	12.5	-	21.8	02	-	-	.	.	.	.	.	.	17	01.2	.	.	05	01.6	.	.	.	.	68
XII	-	-02.6	04.9	-00.5	00.3	06.0	-02.0	14.3	30	-	-	.	.	.	.	.	.	12	01.2	.	.	14	01.6	.	.	03	02.3	64
GOD.	-	06.2	14.0	08.0	09.0	15.4	-	-		-		01	02.0	04	01.2	01	01.0	236	01.3	01	01.0	197	01.6	02	01.0	15	02.3	638
PLJEVLJA SR CRNA GORA $\varphi = 43^\circ 21'$ N $\lambda = 19^\circ 21'$ E Gr. $\Delta G =$ + 1h 17 min. BR. ST. 235																												
I	691.3	-01.2	03.1	-00.2	00.4	04.5	-02.8	14.4	06	-12.6	30	03	02.0	04	01.8	.	.	06	02.8	10	03.3	02	02.5	04	01.5	05	01.6	59
II	688.9	-03.2	02.4	-00.5	-00.5	04.4	-05.2	11.6	05	-22.4	18	03	02.0	01	02.0	02	02.5	03	02.3	12	03.4	03	02.7	02	02.0	09	01.6	49
III	690.2	00.3	06.9	03.1	03.3	08.7	-01.4	16.6	25	-11.7	02	02	01.5	05	01.4	04	01.8	10	03.0	13	03.5	05	04.6	03	02.3	04	02.0	47
IV	692.2	05.3	12.8	07.2	08.2	14.3	02.6	24.1	23	-06.6	05	02	01.5	03	02.3	01	03.0	05	03.2	24	03.4	04	02.5	04	02.0	05	01.4	42
V	693.3	07.4	13.8	09.7	10.1	15.4	05.0	24.1	10	-01.3	26	05	01.8	04	01.5	01	01.0	02	02.0	05	03.8	05	03.2	03	02.3	13	02.2	55
VI	695.6	12.3	21.4	14.9	15.9	23.3	09.4	29.0	17	02.2	07	04	02.0	04	02.0	.	.	.	.	08	03.1	05	01.8	04	01.5	03	02.0	62
VII	694.5	13.4	22.5	16.3	17.1	24.2	10.0	31.4	22	03.6	20	09	01.9	04	02.0	04	01.8	.	.	09	03.1	01	02.0	04	01.8	07	02.0	55
VIII	694.7	12.4	24.3	15.9	17.1	25.5	09.4	33.0	07	04.0	28	06	02.0	03	02.3	03	02.0	.	.	05	02.6	01	02.0	09	01.8	04	01.8	62
IX	697.4	08.0	20.6	11.5	12.9	22.0	05.9	32.4	11	-06.4	30	09	01.8	02	02.0	01	02.0	02	01.5	02	01.5	02	03.5	04	02.0	01	02.0	67
X	696.9	03.0	13.8	06.1	07.3	15.3	01.3	23.6	10,09	-04.0	01	10	01.7	01	01.0	.	.	01	02.0	03	04.3	03	02.3	01	04.0	08	01.5	66
XI	695.8	01.2	09.6	04.0	04.7	11.6	-01.0	19.7	01	-06.8	12	02	02.0	01	02.0	01	03.0	03	01.7	11	03.1	.	.	01	02.0	.	.	71
XII	696.3	-02.5	03.3	-01.3	-00.4	04.4	-05.1	13.4	30	-13.5	18	07	01.4	01	01.0	02	03.0	02	02.0	08	02.0	01	01.0	04	01.5	01	04.0	67
GOD.	693.9	04.7	12.9	07.2	08.0	14.5	02.3	33.0	7.VIII	-22.4	18. II	62	01.8	33	01.8	19	02.1	34	02.6	110	03.2	32	02.8	43	01.9	60	01.9	702

Mesec	Oblačnost Nm (0-10) 7	14	21	Povpr. (Dnevni)	Temperatura zraka °C	Vlažnost zraka Um % 7	14	21	Povpr. (Dnevni)	Min	Padavine R mm Σ	Max	Št.	Tm ≤ -20.0	Tx ≤ -10.0	Tn ≤ 0.0	Tx ≥ 25.0	Tx ≥ 30.0	Tn ≥ 20.0	F (0-12) ≥ 6	F (0-12) ≥ 8	Nm (0-10) < 2.0	R mm > 0.0	≥ 0.1	≥ 1.0	≥ 10.0	●	✱	≡	△	≈	▲	▲	⊤	≡	▦
BR. ST. 231					**PREDEJANE**																															
I	9.1	8.2	8.5	8.6	-	04.8	89	79	87	85	46	078	025.7	17	.	07	20	.	.	.	01	.	.	21	16	09	02	11	08	01	.	.	.	.	.	02	12
II	9.0	8.4	7.4	8.3	-	04.4	90	71	85	82	48	128	024.1	04	01	03	16	.	.	.	01	.	.	18	22	15	06	13	15	03	01	.	.	.	.	01	16
III	8.1	7.6	5.8	7.2	-	05.3	84	63	79	75	31	079	018.6	21	.	.	08	.	.	.	.	.	02	16	14	09	04	10	08	02	.	.	01	.	01	.	03
IV	7.3	7.0	5.5	6.6	-	07.6	86	59	79	75	30	066	013.4	13	.	.	03	06	.	.	.	.	01	13	13	11	02	13	05	05	.	.	.	01	03	02	.
V	7.8	7.6	6.5	7.3	-	09.3	90	66	89	82	41	176	028.3	19	.	.	.	04	.	.	.	.	.	15	21	14	07	21	02	02	.	.	.	01	05	03	.
VI	5.3	5.5	4.4	5.1	-	13.0	88	65	90	81	-	091	032.5	20	-	-	-	-	-	-	.	.	05	05	13	08	03	13	.	.	.	.	.	.	09	02	.
VII	4.7	5.4	4.1	4.7	-	13.9	91	64	90	82	47	090	025.7	18	.	.	.	21	08	.	01	.	07	08	10	08	04	10	.	.	.	.	.	.	11	05	.
VIII	4.0	5.3	2.9	4.1	-	13.7	95	61	91	82	44	068	034.3	12	.	.	.	22	09	.	.	01	11	06	10	06	02	10	.	.	.	.	.	02	08	10	.
IX	4.9	4.8	2.9	4.2	-	10.4	95	57	90	80	35	029	022.5	01	.	.	01	10	05	.	.	.	10	04	05	04	01	05	.	.	.	.	.	.	.	05	.
X	7.6	5.5	5.2	6.1	-	07.6	96	66	94	86	37	098	028.1	23	.	.	.	02	.	.	.	.	05	13	12	09	03	12	03	02	.	.	.	.	.	06	01
XI	7.6	6.0	4.2	5.9	-	06.2	93	66	90	83	39	054	015.7	23	.	.	06	.	.	.	.	.	03	10	09	06	02	09	.	.	.	.	.	.	.	03	.
XII	9.2	7.3	7.4	8.0	-	04.9	90	77	90	86	56	040	013.3	02	.	04	22	.	.	.	.	.	01	20	15	09	01	12	06	02	.	.	.	.	.	02	06
GOD.	7.0	6.6	5.4	6.3	-	08.4	90	66	87	81	-	997	034.3	18.VII	-	-	-	-	-	-	03	01	45	149	160	108	37	139	47	17	01	.	01	04	37	41	38
BR. ST. 232					**SURDULICA**																															
I	8.5	8.5	8.5	8.5	-	-	-	-	-	-	-	042	021.2	17	.	07	20	.	.	.	.	.	.	21	13	08	02	06	07	.	.	.	.	.	.	01	13
II	6.9	7.6	7.1	7.2	-	-	-	-	-	-	-	113	021.5	24	01	04	18	.	.	.	.	.	01	11	21	17	04	09	15	01	.	.	.	.	.	01	16
III	6.2	5.5	5.9	5.9	-	-	-	-	-	-	-	070	-	-	.	.	12	.	.	.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	049	015.2	13	.	.	03	05	.	.	.	.	-	-	12	11	02	10	02	.	.	.	.	.	.	01	.	01
V	6.4	6.9	5.4	6.1	-	09.9	91	79	87	85	38	144	021.8	19	.	.	.	04	.	.	.	.	-	-	17	17	06	17	02	02	.	.	.	01	02	02	.
VI	3.8	4.3	3.5	3.9	-	-	-	-	-	-	-	075	026.5	21	.	.	.	18	02	.	.	.	08	04	11	08	04	11	.	.	.	.	.	.	.	-	.
VII	3.6	4.9	3.6	3.9	-	-	-	-	-	-	-	124	035.7	11	.	.	.	22	06	.	.	.	09	06	08	07	05	08	.	.	.	.	.	01	02	.	.
VIII	3.0	4.5	2.6	3.4	-	-	-	-	-	-	-	062	029.5	03	.	.	.	21	08	.	.	.	14	03	08	08	01	08	.	.	.	.	.	02	05	01	.
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	4.5	4.5	4.7	4.6	-	-	-	-	-	-	-	096	043.6	23	.	.	.	.	.	.	.	.	-	-	09	09	02	09	02	01	.	.	.	.	.	01	01
XI	5.5	5.2	4.3	5.0	-	-	-	-	-	-	-	040	012.2	11	.	.	09	.	.	.	01	.	06	08	09	07	01	09	.	.	.	.	.	.	.	01	.
XII	7.8	6.8	6.1	6.9	-	-	-	-	-	-	-	044	012.2	02	.	04	22	.	.	.	.	.	03	13	13	10	01	08	06	.	.	.	.	.	.	03	07
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BR. ST. 233					**VLASINA**																															
I	7.4	7.4	6.6	7.1	-	-	-	-	-	-	-	059	016.2	17	09	09	25	.	.	.	01	.	04	15	16	08	02	08	11	02	01	.	.	.	.	08	23
II	8.0	7.8	7.6	7.8	-	-	-	-	-	-	-	174	035.6	24	09	13	25	.	.	.	01	.	01	15	22	16	06	07	22	05	01	.	.	.	.	05	28
III	6.8	7.4	6.2	6.8	-	-	-	-	-	-	-	059	010.0	15	03	05	25	.	.	.	02	.	03	15	17	11	01	03	17	01	01	.	.	.	.	07	26
IV	6.9	7.3	5.7	6.6	-	-	-	-	-	-	-	046	007.8	15	.	02	11	.	.	.	.	.	05	13	16	09	.	11	08	01	02	.	.	.	01	03	04
V	7.2	8.1	5.8	7.1	-	-	-	-	-	-	-	192	028.0	03	.	.	05	.	.	.	.	.	02	13	23	17	07	21	07	05	.	.	.	.	03	07	05
VI	4.4	5.7	4.7	4.9	-	10.9	85	85	96	88	68	053	013.9	20	.	.	.	.	.	.	.	.	07	06	13	09	01	13	.	.	.	.	.	.	06	01	.
VII	4.2	6.4	4.4	5.0	-	-	-	-	-	-	-	090	025.8	05	.	.	.	01	.	.	.	.	07	08	09	09	05	09	.	.	.	.	.	.	11	03	.
VIII	3.2	5.0	2.9	3.7	-	-	-	-	-	-	-	025	007.0	12	.	.	.	05	.	.	.	.	12	03	10	06	.	10	.	.	.	.	.	.	06	.	.
IX	3.1	4.0	1.8	3.0	-	09.3	84	83	95	88	48	024	015.2	01	.	.	06	05	.	.	.	.	15	01	04	02	01	04	.	.	.	.	.	.	.	.	.
X	5.7	5.3	5.1	5.3	-	-	-	-	-	-	-	073	024.1	23	-	02	-	.	.	.	01	.	11	13	10	09	02	09	04	03	01	.	.	.	.	06	06
XI	5.4	4.9	3.1	4.5	-	-	-	-	-	-	-	054	016.5	09	-	.	-	.	.	-	.	.	11	07	08	07	01	06	06	01	.	.	01	.	01	03	05
XII	7.5	6.8	6.4	6.9	-	-	-	-	-	-	-	052	018.0	02	04	11	25	.	.	.	02	.	04	15	15	11	01	07	11	03	.	.	.	.	.	08	23
GOD.	5.8	6.3	5.0	5.7	-	-	-	-	-	-	-	901	035.6	24.II	-	42	-	11	.	-	07	.	82	124	163	114	27	108	86	21	06	.	01	.	28	51	120
BR. ST. 234					**BOSILJGRAD**																															
I	8.7	8.2	7.9	8.3	-	-	-	-	-	-	-	043	014.1	07	01	06	19	.	.	.	.	.	.	19	08	07	02	04	04	.	.	.	.	.	.	10	02
II	7.5	7.1	6.2	7.0	-	-	-	-	-	-	-	094	016.0	04	.	02	19	.	.	.	.	.	01	13	13	12	05	07	09	.	.	.	.	.	.	02	13
III	7.1	5.5	4.1	5.6	-	-	-	-	-	-	-	088	028.7	29	.	01	16	.	.	.	.	.	08	11	11	11	03	09	03	.	.	.	.	.	.	01	.
IV	6.1	4.6	4.1	4.9	-	-	-	-	-	-	-	042	007.2	07	.	.	04	02	.	.	.	.	06	08	11	11	.	08	03	.	.	.	.	.	.	.	01
V	6.0	6.7	5.8	6.2	-	-	-	-	-	-	-	080	017.0	29	.	.	02	02	.	.	.	.	05	12	18	15	03	18	01	.	.	.	.	.	.	01	01
VI	3.5	5.0	3.5	4.0	-	10.6	76	97	81	72	32	082	046.5	28	.	.	.	14	.	.	.	.	08	03	07	06	03	07	.	.	.	.	.	.	.	.	.
VII	3.1	4.9	3.5	3.9	-	-	-	-	-	-	-	119	053.8	05	.	.	.	20	02	.	.	.	10	05	11	09	03	11	.	.	.	.	.	.	05	.	.
VIII	3.0	4.0	1.8	2.9	-	11.5	79	94	78	71	36	032	012.9	09	.	.	.	20	03	.	.	.	15	02	07	04	02	07	.	.	.	.	.	.	-	.	.
IX	-	-	-	-	-	09.6	83	99	77	73	41	018	016.1	01	.	.	02	10	04	.	.	.	-	-	02	02	01	02	.	.	.	.	.	.	.	01	.
X	-	-	-	-	-	-	-	-	-	-	-	080	037.2	17	-	-	-	-	-	-	.	.	-	-	08	07	03	07	02	.	.	.	.	.	.	04	02
XI	-	-	-	-	-	-	-	-	-	-	-	031	006.3	09	-	.	-	-	.	-	.	.	-	-	07	07	.	07	.	.	.	.	.	.	.	05	.
XII	6.6	5.1	5.1	5.6	-	-	-	-	-	-	-	056	021.0	31	-	03	-	.	.	-	.	.	03	08	10	09	02	08	02	.	.	.	.	.	.	05	03
GOD.	-	-	-	-	-	-	-	-	-	-	-	765	053.8	5.VII	-	-	-	-	-	-	.	.	-	-	113	100	27	95	24	.	.	.	.	.	.	29	22
BR. ST. 235					**PLJEVLJA**																															BR CRNA GORA
I	9.0	8.1	6.4	7.8	341.4	04.2	90	73	87	83	53	106	032.6	02	01	08	23	.	.	.	03	01	01	19	14	11	04	07	18	.	.	.	.	.	.	06	21
II	8.9	8.7	6.8	8.1	-	03.5	86	65	77	76	47	080	013.3	16	06	05	21	.	.	.	03	01	.	16	17	13	03	08	13	.	.	.	.	.	01	04	20
III	7.7	6.5	5.3	6.5	131.4	04.1	82	58	71	71	27	075	027.8	06	01	01	16	.	.	.	03	02	02	11	15	07	03	10	09	02	.	.	.	.	.	01	08
IV	6.0	7.6	5.3	6.3	-	05.1	79	47	67	64	24	072	028.4	15	.	.	07	.	.	.	04	02	01	10	10	07	02	07	05	.	.	.	01	.	.	01	-
V	7.7	8.4	6.5	7.9	129.7	06.7	86	58	76	73	27	085	017.9	29	.	.	01	.	.	.	.	.	.	16	19	14	02	16	04	.	.	.	.	.	.	03	02	.
VI	7.4	7.2	5.7	6.1	199.7	09.7	89	51	78	73	25	036	009.0	21	.	.	.	16	.	.	.	.	.	06	18	13	.	18	.	.	.	.	.	.	.	10	07	.
VII	5.1	6.1	3.5	4.9	244.3	10.6	90	52	80	74	26	070	030.1	17	.	.	.	18	04	.	.	.	07	08	08	06	03	08	.	.	.	.	.	.	02	05	.
VIII	6.2	6.0	1.9	4.7	227.6	10.1	92	43	80	72	23	022	012.4	25	.	.	.	19	05	.	.	.	06	03	09	04	01	09	.	.	.	.	.	.	03	09	.
IX	6.4	4.5	2.8	4.6	191.8	08.0	96	43	83	74	13	029	012.2	18	.	.	05	11	04	.	.	.	09	07	07	04	01	07	.	.	.	.	.	.	02	10	.
X	8.4	4.6	4.5	5.8	146.0	06.1	95	57	88	80	20	106	032.1	23	.	.	11	.	.	.	02	.	04	11	08	06	04	08	02	.	.	.	.	.	01	13	03
XI	7.9	6.0	4.2	6.0	110.2	05.1	92	62	87	80	29	073	017.4	16	.	.	17	.	.	.	01	.	03	08	10	09	03	10	01	.	.	.	.	.	.	09	.
XII	7.9	6.3	5.9	6.7	074.5	03.8	87	69	87	81	29	038	009.2	26	06	04	24	.	.	.	.	.	04	15	12	10	.	08	04	.	.	.	.	.	01	10	19
GOD.	7.4	6.7	4.7	6.2	-	06.4	88	56	80	75	13	612	032.4	2.I	14	18	127	64	13	.	16	06	37	130	147	104	26	116	48	02	.	.	01	.	23	77	-

| Mesec | Vazdušni pritisak Pm mm | Temperatura vazduha °C: 7 | 14 | 21 | Srednji dnevni | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | Broj dana sa [illegible] | Broj dana sa [illegible] | Broj dana sa

Mesec	Oblačnost mm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e mm	Um % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Rmax	Rmax	Broj dana n sa: Tn ≤-10,0	Tx ≤-10,0	Tn ≤0,0	Tx ≤25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) <2.0	>8.0	R mm ≥0.1	≥1.0	≥10.0	●	●	●	●	●	●	●	●	●	●
BR. ST. 236																																					
I	9.4	8.3	8.1	8.6	029.9	04.4	89	76	89	85	57	132	037.1	02	.	04	20	.	.	.	.	.	20	14	11	05	11	07	.	.	.	.	.	.	.	.	–
II	7.5	7.7	7.0	7.4	075.3	03.8	85	58	77	73	36	094	021.2	17	04	03	20	.	.	.	01	.	.	10	11	11	03	08	06	.	.	.	.	.	01	01	16
III	7.6	6.0	4.9	6.2	139.6	04.3	86	52	73	70	27	090	024.6	29	.	.	13	.	.	.	01	.	03	08	15	11	03	11	06	01	.	.	.	.	.	01	05
IV	6.0	7.1	5.9	6.3	176.0	05.6	83	46	70	66	16	106	040.7	15	.	.	03	02	.	.	01	.	03	12	11	10	04	09	03	.	.	.	.	.	01	.	02
V	8.0	7.6	6.4	7.3	135.9	07.1	88	56	78	74	19	089	022.0	23	.	.	.	01	.	.	.	.	01	16	17	13	03	17	02	.	.	.	.	.	03	03	.
VI	8.6	6.4	3.6	6.2	203.1	10.1	90	51	82	74	28	054	014.9	21	.	.	.	18	.	.	01	.	.	04	13	08	02	13	.	.	.	.	.	.	04	07	.
VII	7.0	4.7	3.5	5.1	253.3	11.1	90	50	83	74	34	050	020.6	07	.	.	.	23	05	.	01	.	05	06	10	06	02	10	.	.	.	.	.	.	03	08	.
VIII	7.5	5.1	2.9	5.2	236.0	10.6	92	43	81	72	26	027	010.0	02	.	.	.	21	10	.	.	.	02	04	07	05	01	07	.	.	.	.	.	.	02	09	.
IX	9.0	4.4	2.3	5.2	170.7	08.5	94	44	84	74	20	026	014.0	18	.	.	02	10	07	.	.	.	01	05	05	03	01	05	.	.	.	.	.	.	.	15	.
X	8.8	4.5	4.5	6.0	125.2	06.3	91	54	87	77	33	083	040.2	23	.	.	01	01	.	.	.	.	02	10	07	05	03	07	02	02	.	.	.	.	.	12	02
XI	9.3	5.8	5.1	6.7	081.0	05.2	92	62	88	81	31	091	034.1	16	.	.	15	.	.	.	.	.	.	11	10	10	03	10	.	.	.	.	.	.	.	14	.
XII	7.4	6.1	5.9	6.5	069.9	03.9	88	68	86	81	28	050	015.1	31	01	06	26	.	.	.	01	.	03	12	12	10	02	08	04	.	.	.	.	.	05	03	.
GOD.	8.0	6.1	5.0	6.4	1695.9	06.7	89	55	81	75	16	892	040.7	15 IV	05	13	100	76	22	.	06	.	20	118	132	103	32	116	30	03	.	.	.	.	19	73	–
BR. ST. 237																																					
I	8.2	8.0	6.9	7.7	058.6	07.6	88	77	86	84	32	501	081.0	17	.	.	.	.	.	.	03	03	01	17	23	22	12	23	.	.	.	.	.	.	01	.	.
II	7.2	7.8	6.8	7.3	081.9	06.1	74	65	76	72	32	227	067.2	19	.	.	04	.	.	.	09	.	03	16	13	11	06	13	.	.	.	.	.	01	05	.	.
III	6.8	6.3	4.6	5.9	169.1	06.4	69	60	74	68	27	279	055.8	04	.	.	01	.	.	.	07	02	05	10	14	13	07	14	.	.	.	.	.	01	05	.	.
IV	6.7	6.4	5.8	6.3	198.9	08.6	81	65	78	75	31	314	124.8	08	.	.	.	.	.	.	07	.	02	10	15	14	07	15	.	.	.	.	.	.	04	02	.
V	5.4	6.2	4.3	5.3	266.6	10.0	77	61	76	71	32	089	033.0	23	.	.	.	01	.	.	03	.	06	07	14	08	02	14	.	.	.	.	.	.	05	.	.
VI	3.1	3.6	2.4	3.0	323.8	14.7	76	62	78	72	35	013	006.2	07	.	.	.	25	05	04	.	.	12	01	07	04	.	07	.	.	.	.	.	.	03	.	.
VII	2.4	3.1	1.8	2.4	344.7	15.4	73	55	73	67	34	046	021.0	06	.	.	.	28	17	14	02	.	17	01	08	05	02	08	.	.	.	.	.	.	04	.	.
VIII	2.5	3.5	1.6	2.5	317.3	16.5	76	62	77	72	35	187	133.5	31	.	.	.	30	15	14	.	.	19	02	05	05	03	05	.	.	.	.	.	.	11	.	.
IX	2.2	2.9	1.3	2.1	292.1	13.4	69	60	71	67	25	015	014.8	01	.	.	.	22	01	01	01	.	19	02	01	01	01	01	.	.	.	.	.	.	.	.	.
X	4.2	4.4	3.4	4.0	212.5	10.3	81	63	81	75	28	103	064.2	02	.	.	.	04	.	.	04	02	12	08	04	04	03	04	.	.	.	.	.	.	05	.	.
XI	6.0	5.9	4.9	5.6	138.7	09.1	83	72	85	80	34	137	027.0	15	.	.	.	.	.	.	04	04	06	10	13	09	07	13	.	.	.	.	.	.	03	.	.
XII	5.0	5.4	3.9	4.8	129.9	07.0	80	66	78	75	24	162	060.2	26	.	.	.	.	.	.	06	01	10	07	12	12	04	12	.	.	.	.	.	01	06	.	.
GOD.	5.0	5.3	4.0	4.7	2534.1	10.4	77	64	77	73	24	2073	133.5	31 VIII	.	.	05	110	38	33	46	12	112	91	129	108	54	129	.	.	.	.	.	03	52	02	.
BR. ST. 238																																					
I	7.6	7.3	5.8	6.9	–	–	–	–	–	–	–	843	147.3	13	07	.	26	.	.	.	01	01	04	16	17	15	12	16	02	01	.	.	.	.	.	03	04
II	6.5	7.6	5.8	6.6	–	–	–	–	–	–	–	324	068.6	15	11	03	25	.	.	.	01	.	05	13	16	13	10	13	06	02	.	.	.	.	.	01	17
III	6.2	5.4	5.0	5.5	–	–	–	–	–	–	–	504	108.6	04	10	.	28	.	.	.	04	02	07	10	12	12	08	12	05	01	.	.	.	.	.	.	26
IV	6.1	5.6	4.5	5.4	–	–	–	–	–	–	–	590	219.2	09	.	.	05	.	.	.	02	01	06	08	13	12	09	11	02	.	.	.	.	.	.	.	02
V	4.9	6.0	4.0	5.0	–	–	–	–	–	–	–	209	050.6	23	.	.	.	.	.	.	.	.	04	06	13	09	05	13	.	.	.	.	.	.	.	.	.
VI	2.5	4.1	1.6	2.8	–	–	–	–	–	–	–	072	029.6	07	.	.	.	15	.	.	.	.	12	01	06	05	04	06	.	.	.	.	.	.	.	.	.
VII	2.3	3.3	1.1	2.2	–	–	–	–	–	–	–	134	058.4	17	.	.	.	19	03	.	03	.	21	02	07	05	05	07	.	.	.	.	.	.	.	.	.
VIII	1.4	4.0	1.4	2.3	–	–	–	–	–	–	–	092	037.6	31	.	.	.	19	03	.	.	.	17	.	08	08	03	08	.	.	.	.	.	.	.	.	.
IX	1.7	2.3	0.8	1.6	–	–	–	–	–	–	–	.	000.0	28	.	.	09	13	02	.	.	.	19	.	.	.	.	.	.	.	.	.	.	.	.	.	.
X	4.1	3.4	2.1	3.2	–	–	–	–	–	–	–	157	076.4	22	.	.	24	02	.	.	.	.	14	06	05	05	04	05	.	.	.	.	.	.	.	02	.
XI	5.7	5.0	3.9	4.9	–	–	–	–	–	–	–	574	191.2	22	03	.	24	.	.	.	01	.	10	10	12	12	08	12	.	.	.	.	.	.	.	02	.
XII	4.8	4.7	3.5	4.4	–	–	–	–	–	–	–	586	214.6	30	04	.	26	.	.	.	01	.	12	09	11	08	07	11	03	01	.	.	.	.	.	.	04
GOD.	4.5	4.9	3.3	4.2	–	–	–	–	–	–	–	4085	219.2	9 IV	38	03	147	68	08	.	13	04	131	81	120	104	75	114	18	05	.	.	.	.	.	08	53
BR. ST. 239																																					
I	7.7	7.5	6.8	7.3	–	07.5	89	76	88	85	23	410	096.8	17	.	.	07	.	.	.	06	.	02	16	21	19	10	21	.	.	.	.	.	.	02	.	.
II	6.9	7.1	5.8	6.6	–	06.1	76	64	77	72	31	151	047.0	19	.	.	05	.	.	.	08	.	04	13	15	12	04	15	03	02	.	.	.	.	03	.	.
III	6.2	5.6	5.5	5.8	–	06.4	75	59	78	71	32	236	049.2	04	.	.	04	.	.	.	08	03	06	12	15	13	07	15	.	.	.	.	.	.	05	.	.
IV	6.0	5.5	4.5	5.3	–	08.6	82	61	82	75	35	181	048.9	09	.	.	01	.	.	.	08	01	05	07	15	13	06	15	.	.	.	.	.	.	03	02	.
V	4.9	5.9	3.6	4.8	–	09.9	73	59	77	70	27	090	030.0	29	.	.	.	01	.	.	03	.	07	07	12	09	03	12	.	.	.	.	.	.	03	.	.
VI	2.1	3.5	1.5	2.4	–	14.5	71	59	84	71	42	009	004.2	07	.	.	.	25	07	.	02	.	15	.	06	03	.	06	.	.	.	.	.	.	01	.	.
VII	2.0	3.7	1.5	2.4	–	14.9	66	53	76	65	35	065	040.2	17	.	.	.	28	17	02	01	.	19	01	07	04	02	07	.	.	.	.	.	.	04	.	.
VIII	2.1	3.6	1.9	2.5	–	16.8	78	62	84	75	43	166	106.5	31	.	.	.	31	13	.	01	.	19	03	07	06	04	07	.	.	.	.	.	.	02	.	.
IX	1.2	2.2	0.6	1.3	–	12.6	76	54	78	69	31	005	004.6	01	.	.	.	22	04	01	03	.	23	01	01	01	.	01	.	.	.	.	.	.	.	.	.
X	3.9	4.3	2.7	3.6	–	09.9	84	66	81	77	32	133	075.7	02	.	.	.	03	.	.	04	.	14	06	08	04	04	08	.	.	.	.	.	.	02	.	.
XI	5.2	4.8	3.3	4.4	–	08.7	88	75	83	82	33	208	067.6	15	.	.	.	.	.	.	05	01	13	09	12	12	07	12	01	.	.	.	01	.	03	.	.
XII	5.3	4.8	4.0	4.7	–	06.4	84	64	79	75	18	181	074.0	26	.	.	07	.	.	.	08	.	12	08	12	10	06	12	.	.	.	.	.	.	05	.	.
GOD.	4.5	4.9	3.5	4.3	–	10.2	78	62	80	73	18	1835	106.5	31 VIII	.	.	24	110	41	03	57	05	139	83	131	106	53	131	04	02	.	.	01	.	33	02	.
BR. ST. 240																																					
I	7.6	7.9	6.2	7.3	058.2	08.7	95	87	96	93	45	264	048.3	17	.	.	.	.	.	.	01	01	04	16	20	19	09	20	.	.	.	.	.	.	01	.	.
II	7.2	7.4	6.2	6.9	083.1	07.6	86	78	88	84	40	117	027.4	01	.	.	01	.	.	.	.	02	02	14	16	13	03	16	.	.	.	.	.	01	05	.	.
III	6.1	5.2	4.8	5.4	170.7	08.2	84	77	88	83	39	166	049.0	12	.	.	.	.	.	.	.	03	07	11	14	11	05	14	.	.	.	.	.	.	01	.	.
IV	6.9	4.7	3.8	5.1	178.6	10.9	94	87	93	91	52	142	037.6	08	.	.	.	.	.	.	.	01	06	08	15	13	04	15	.	.	.	.	.	.	04	.	.
V	5.0	3.5	3.6	4.0	228.4	12.1	87	79	90	85	38	060	027.2	23	.	.	.	01	.	.	01	.	15	07	14	07	02	14	.	.	.	.	.	.	02	.	.
VI	2.7	3.0	0.5	2.1	292.6	17.6	85	78	93	85	35	009	002.7	03	.	.	.	22	03	02	.	.	15	.	06	03	.	06	.	.	.	.	.	.	01	.	.
VII	2.2	2.7	1.5	2.1	305.1	18.9	83	75	93	84	36	055	034.3	17	.	.	.	27	11	06	.	.	19	01	05	03	02	05	.	.	.	.	.	.	03	.	.
VIII	2.0	3.0	1.5	2.1	285.5	20.6	91	86	93	90	46	066	027.9	31	.	.	.	30	04	12	.	.	20	02	06	06	03	06	.	.	.	.	.	.	05	.	.
IX	1.7	2.3	1.0	1.6	281.0	15.5	84	72	84	80	37	.	.	.	.	.	.	23	.	02	.	02	21	01	.	.	.	.	.	.	.	.	.	.	.	.	.	.
X	4.4	3.9	3.1	3.8	189.9	11.8	90	79	92	87	42	051	020.2	02	.	.	.	01	.	.	02	.	16	09	07	05	03	07	.	.	.	.	.	.	01	.	.
XI	5.7	6.1	5.6	5.8	126.0	10.5	92	83	93	89	47	102	019.6	09	.	.	.	.	.	.	.	.	08	12	13	10	05	13	.	.	.	.	.	.	02	.	.
XII	5.0	5.3	3.8	4.7	124.8	07.9	87	76	89	84	28	085	020.0	28	.	.	.	.	.	.	01	.	13	11	14	08	05	14	.	.	.	.	.	.	02	.	.
GOD.	4.7	4.6	3.5	4.2	2323.9	12.5	88	79	91	86	28	1117	049.0	18 XI	.	.	01	104	18	22	05	09	146	92	130	98	41	130	.	.	.	.	.	01	27	.	.

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C 7	14	21	Sred. (Dnev)	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	Ext.	Čestina pravaca i srednja jačina vetra nD, Pm (0-12) N		NE		E		SE		S		SW		W		NW		C
												č.	j.	č.	j.	č.	j.	č.	j.	č.	j.	č.	j.		j.	č.	j.	č.
CETINJE φ = 42° 24' N λ = 18° 56' E Gr. ΔG = + 1h 16 min.																												BR. ST. 241
I	-	02.7	06.3	02.8	03.6	08.7	00.3	13.4	06	-10.2	24	.	.	.	.	05	01.6	14	02.1	13	02.4	.	.	.	.	01	01.0	60
II	-	-01.4	04.4	-01.2	00.1	07.3	-04.7	13.0	09	-16.0	18	.	.	01	02.0	01	02.0	10	02.1	06	02.3	08	01.9	02	02.5	01	02.0	55
III	-	03.3	07.8	03.4	04.5	10.6	-01.0	19.0	23	-08.9	01	02	01.0	01	02.0	.	.	18	01.7	10	02.1	01	04.0	01	01.0	02	02.0	58
IV	-	08.3	12.7	08.4	09.4	16.5	03.4	26.1	27	-04.5	07	02	02.5	03	02.3	01	02.0	34	02.1	04	02.2	03	02.3	.	.	03	02.7	40
V	-	11.2	16.2	11.0	12.4	18.9	09.3	23.5	11	05.9	01	.	.	02	02.0	.	.	30	01.9	.	.	09	01.6	.	.	04	02.5	48
VI	-	17.8	23.7	16.3	18.5	26.1	14.4	30.6	30,29	10.0	04,03	.	.	03	01.3	05	01.6	20	01.8	03	01.3	01	01.0	.	.	.	.	58
VII	-	19.4	25.6	18.0	20.2	28.9	15.6	33.4	25	10.4	20	.	.	01	01.0	04	01.2	19	01.6	03	01.3	04	01.2	03	01.3	02	01.5	57
VIII	-	18.9	25.4	17.2	19.7	28.1	13.8	33.2	08,07	07.2	27	.	.	03	01.3	05	01.2	26	01.6	02	01.5	02	01.5	.	.	.	.	55
IX	-	11.2	23.1	10.7	13.9	25.3	08.3	30.6	13	01.2	25	.	.	03	02.0	03	01.7	23	01.6	02	01.0	04	02.0	.	.	01	01.0	54
X	-	05.5	15.7	05.2	07.9	17.9	00.3	24.9	11	-02.4	12	.	.	02	01.5	04	02.2	36	02.0	02	04.0	01	02.0	.	.	.	.	48
XI	-	02.3	11.1	02.8	04.8	12.8	-00.6	18.6	05	-04.3	13	.	.	02	01.5	03	01.7	38	01.8	06	02.7	03	02.0	.	.	02	02.0	36
XII	-	-01.0	07.3	-00.9	01.1	09.1	-03.5	14.0	03	-09.2	21	01	01.0	02	01.5	.	.	18	02.2	09	04.4	03	02.3	.	.	05	02.0	55
GOD.	-	08.2	14.9	07.8	09.7	17.5	04.6	33.4	15 VII	-16.0	18 II	05	01.6	23	01.7	31	01.6	286	01.9	60	02.5	39	01.9	06	01.6	21	02.1	624
NIKŠIĆ φ = 42° 46' N λ = 18° 57' E Gr. ΔG = + 1h 16 min.																												BR. ST. 242
I	702.7	02.0	05.4	03.2	03.5	06.4	01.1	11.0	06	-06.5	23	30	02.8	09	02.1	.	.	08	02.5	29	03.2	.	.	01	02.0	03	02.3	13
II	700.8	-00.2	03.0	01.1	01.3	04.2	-01.4	09.6	07	-14.0	18	32	03.0	11	02.4	01	01.0	10	02.0	21	03.3	01	06.0	01	03.0	02	01.5	05
III	702.1	01.5	07.6	03.9	04.3	08.4	00.2	16.0	26,25	-06.6	02	25	02.8	11	02.2	01	01.0	08	02.0	26	03.5	01	03.0	05	02.2	02	01.5	14
IV	704.1	07.2	12.3	08.2	09.0	13.3	04.8	24.4	24	-02.1	05	26	03.1	05	02.2	01	01.0	09	02.6	36	03.9	01	05.0	01	02.0	02	01.5	09
V	704.7	09.9	14.6	11.0	11.6	16.0	07.3	23.0	10	02.0	02	31	02.8	11	02.7	01	02.0	10	02.0	20	03.4	.	.	02	02.0	07	02.3	11
VI	706.8	15.5	21.8	16.9	17.8	23.3	12.2	28.6	17	04.6	04	29	02.2	12	02.2	05	02.0	04	02.2	21	03.1	03	02.7	01	02.0	03	01.7	12
VII	705.2	17.9	24.2	19.0	20.0	25.5	14.1	32.4	23	06.8	19	31	02.6	18	02.4	05	01.6	02	01.5	25	03.1	01	02.0	01	03.0	04	02.8	06
VIII	705.7	16.8	25.2	18.4	19.7	26.8	14.0	33.9	07	09.0	28	36	01.7	11	01.1	03	01.3	02	03.5	19	03.3	04	02.8	05	02.4	02	01.5	11
IX	707.8	13.4	23.1	15.8	17.0	24.0	11.5	31.2	11	02.2	30	37	02.6	22	02.4	01	03.0	.	.	16	03.1	01	02.0	01	03.0	04	02.2	08
X	707.7	06.5	15.3	09.3	10.1	16.4	05.3	25.5	11	01.4	25	35	02.8	19	02.2	01	02.0	01	03.0	23	03.3	02	02.0	03	02.0	03	02.3	06
XI	707.2	04.6	10.9	06.1	06.9	11.6	03.0	18.0	01	-02.0	13	28	02.4	11	02.5	02	01.5	13	02.2	14	02.9	04	02.2	01	02.0	03	02.7	14
XII	707.2	00.8	06.9	02.7	03.3	07.9	-00.4	14.6	02	-07.5	21	29	03.0	14	02.6	01	02.0	07	02.1	20	03.5	02	03.5	03	01.0	08	03.4	09
GOD.	705.2	08.0	14.2	09.6	10.4	15.3	06.0	33.9	7 VIII	-14.0	18 II	369	02.6	154	02.3	22	01.7	74	02.2	270	03.3	20	02.9	25	02.1	43	02.4	118
VIRPAZAR φ = 42° 14' N λ = 19° 05' E Gr. ΔG = + 1h 16 min.																												BR. ST. 243
I	-	05.4	08.1	05.9	06.3	09.3	02.6	17.2	07	-03.2	21	.	.	21	02.5	03	01.3	04	02.2	01	01.0	54	01.9	04	01.0	01	01.0	05
II	-	04.7	07.9	05.7	06.0	09.3	01.8	16.2	07	-05.0	18	.	.	13	02.5	.	.	02	01.5	.	.	56	02.3	05	01.2	03	02.7	05
III	-	06.2	11.7	08.5	08.7	12.8	02.8	20.0	26	-01.8	02	.	.	23	02.6	.	.	02	02.5	.	.	53	02.5	06	01.7	01	01.0	08
IV	-	11.2	16.0	11.2	12.4	16.5	06.3	27.4	25	02.0	07,05	.	.	21	03.4	.	.	04	02.0	.	.	48	03.1	04	01.0	06	01.3	07
V	-	12.3	19.8	14.2	15.1	20.4	07.0	29.0	10	01.8	03	.	.	21	02.8	.	.	06	01.8	.	.	59	02.1	01	01.0	.	.	06
VI	-	20.1	25.9	22.1	22.5	26.1	12.1	31.0	28	09.5	01	01	01.0	17	02.0	.	.	02	01.5	08	01.0	44	01.6	02	01.0	.	.	16
VII	-	25.6	31.8	26.8	27.7	32.2	11.9	37.0	29	09.5	19	.	.	22	02.0	.	.	01	01.0	.	.	43	01.8	03	01.0	03	01.7	21
VIII	-	23.5	29.0	24.8	25.6	29.1	12.0	37.0	06	10.0	24,10	.	.	20	01.6	.	.	02	01.5	08	01.0	49	01.2	.	.	.	.	14
IX	-	16.4	26.4	18.4	19.9	26.8	09.8	32.0	14	00.8	30	01	02.0	36	02.2	.	.	.	.	06	01.0	24	01.1	01	01.0	01	01.0	21
X	-	09.6	17.4	11.6	12.5	17.8	07.0	25.0	13,12	01.0	26	.	.	32	02.2	.	.	01	01.0	04	01.0	39	01.3	06	01.0	03	01.3	08
XI	-	06.1	12.0	07.4	08.2	12.4	03.6	15.0	15	00.2	28	.	.	22	02.2	01	01.0	01	02.0	05	01.0	44	01.5	08	01.0	01	01.0	08
XII	-	02.0	10.8	05.3	05.8	11.3	00.4	15.6	03	-06.5	19	.	.	28	02.2	.	.	.	.	02	01.0	54	02.3	03	01.0	.	.	06
GOD.	-	11.9	18.1	13.5	14.2	18.7	06.4	37.0	29 VII	-06.5	19 XII	02	01.5	276	02.3	04	01.2	25	01.8	34	01.0	567	02.0	43	01.1	19	01.5	125
BAR φ = 42° 06' N λ = 19° 06' E Gr. ΔG = + 1h 16 min.																												BR. ST. 244
I	758.9	09.2	11.8	09.2	09.8	13.1	06.5	17.6	06	-00.2	23	01	02.0	34	02.9	14	01.9	14	02.9	12	04.2	03	01.7	05	02.6	02	02.0	08
II	757.2	07.6	11.0	08.7	09.0	12.5	05.5	16.9	04	-03.6	18	02	04.0	31	04.2	13	02.2	07	02.3	15	03.9	06	04.3	08	03.8	.	.	02
III	758.2	08.9	13.0	09.7	10.4	14.6	06.1	22.1	26	01.1	09	04	04.8	39	03.3	08	02.5	10	03.5	10	04.3	07	03.4	13	02.9	02	03.5	.
IV	759.9	11.9	15.7	12.4	13.1	17.2	09.2	23.4	20	03.5	05	09	02.8	26	02.7	05	01.8	10	02.5	19	03.3	09	02.2	08	03.4	.	.	04
V	759.8	15.8	18.7	15.1	16.2	20.3	11.9	27.4	10	05.4	02	13	02.4	30	02.3	08	01.6	08	01.9	06	03.2	15	02.1	06	03.3	04	01.8	03
VI	760.8	21.7	24.3	20.3	21.7	26.0	16.5	32.0	18	10.8	04	07	02.4	34	02.1	08	01.5	01	02.0	01	04.0	08	02.1	21	02.6	01	02.0	09
VII	758.6	23.7	26.0	21.8	23.3	27.7	18.4	33.6	13	13.4	19	04	02.2	34	02.3	08	01.6	02	01.5	04	02.5	06	02.3	22	02.5	02	01.5	11
VIII	759.3	23.3	27.2	22.5	23.9	28.4	19.1	32.2	09	16.6	29	06	03.0	38	01.8	09	01.4	03	02.7	04	02.5	09	02.4	17	02.9	.	.	07
IX	761.6	19.8	24.9	19.7	21.0	26.9	16.2	30.4	13	10.8	27,26	09	03.0	43	02.6	05	01.6	.	.	01	02.0	05	02.4	20	02.6	.	.	07
X	762.7	13.9	18.9	14.3	15.3	20.2	11.1	25.3	13	07.4	26	06	03.8	48	02.6	06	01.8	09	03.2	02	01.5	08	02.0	13	02.4	.	.	01
XI	762.9	12.0	16.6	12.7	13.5	17.5	09.2	19.8	05	03.0	12	08	03.1	33	02.3	06	01.7	15	02.9	05	02.8	11	02.8	07	02.6	01	03.0	04
XII	763.5	08.9	13.1	09.0	10.0	14.3	05.3	18.8	30	-00.4	21	12	03.2	37	02.7	15	02.5	13	03.5	05	02.2	09	01.9	02	01.5	.	.	.
GOD.	760.3	14.7	18.4	14.6	15.6	19.9	11.2	33.6	13 VII	-03.6	18 II	81	03.0	427	02.6	105	01.9	92	02.9	84	03.4	96	02.4	142	02.8	12	02.2	56
TITOGRAD φ = 42° 26' N λ = 19° 17' E Gr. ΔG = + 1h 17 min.																												BR. ST. 245
I	755.0	05.2	09.1	06.5	06.8	10.5	04.1	15.6	07	-03.5	23,22	15	05.1	.	.	01	04.0	06	05.0	09	03.3	.	.	01	02.0	04	03.8	57
II	753.2	04.6	08.3	05.8	06.1	09.6	03.2	15.0	06	-05.0	18	28	05.1	.	.	.	.	11	04.4	05	02.8	03	04.3	05	01.6	07	03.1	25
III	754.1	06.9	12.6	08.7	09.2	13.8	05.4	22.2	26	-01.6	09	25	04.8	01	01.0	03	02.3	14	04.9	13	03.5	03	02.7	05	02.0	05	04.4	24
IV	755.8	10.9	16.5	12.5	13.1	17.7	08.7	26.8	25	01.3	06	18	04.6	.	.	.	.	18	04.3	12	04.0	05	02.8	03	02.0	05	04.2	29
V	755.6	14.3	19.9	15.9	16.5	21.1	11.8	28.0	10	06.3	02	22	04.1	.	.	.	.	07	03.6	12	03.1	02	03.0	02	02.0	13	04.2	35
VI	756.4	21.0	27.7	22.9	23.6	28.7	18.2	33.4	18	10.6	04	20	04.0	03	03.7	.	.	11	04.4	12	04.0	.	.	02	03.0	13	03.5	29
VII	754.0	23.5	29.6	24.7	25.6	31.0	20.1	36.0	23	12.6	19	26	04.8	02	05.5	01	04.0	17	04.2	10	03.6	.	.	01	03.0	10	03.0	26
VIII	754.7	23.0	30.5	24.6	25.7	31.6	20.5	37.0	07	14.0	24	24	02.8	03	03.3	01	03.0	05	04.0	17	03.4	.	.	04	02.5	14	03.0	25
IX	757.4	19.6	27.0	21.1	22.2	27.7	17.7	33.2	12	10.6	30	36	04.3	08	02.6	.	.	14	02.9	09	02.4	.	.	.	.	05	04.6	18
X	758.9	12.2	18.8	14.1	14.8	19.8	10.5	27.3	09	03.4	26	37	03.9	.	.	01	02.0	15	03.4	09	02.3	.	.	.	.	05	04.0	26
XI	759.0	08.6	14.4	10.1	10.8	15.2	06.7	21.8	05	00.8	26	27	03.6	02	04.5	01	02.0	14	03.4	04	03.2	04	01.5	01	01.0	02	05.5	35
XII	759.7	04.4	10.3	06.3	06.8	11.6	02.4	18.8	02	-04.0	21	24	04.6	07	02.3	.	.	13	04.2	07	02.1	01	01.0	.	.	06	03.3	35
GOD.	756.2	12.8	18.7	14.4	15.1	19.9	10.8	37.0	7 VIII	-04.0	18 II	302	04.3	26	03.0	08	02.7	145	04.0	119	03.2	18	02.7	24	02.1	89	03.7	364

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlas)	Insolacija broj sati	Vlažnost vazduha p_m mm	U_m % 7	14	21	Sred. (Dlas)	RH%	Padavine R mm Σ			Broj dana sa: Tn ≤ -30,0	Tn ≤ -20,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	P(0-12) ≥ 6	≥ 8	Nm(0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⚹	⚹	△	∽	▲	▲	R T	⁜	▦
CETINJE																																					
BR. ST. 241																																					
I	8.3	8.5	8.5	8.4	-	05.4	87	79	88	84	42	974	150.3	13	01	.	15	.	.	.	.	.	04	25	24	23	18	21	04	.	.	.	.	.	.	.	04
II	8.4	7.8	8.5	8.2	-	03.8	75	71	76	74	13	194	019.6	18	05	.	26	.	.	.	.	.	.	19	12	12	09	11	07	01	.	.	.	.	.	.	23
III	8.3	7.7	8.5	8.2	-	05.3	82	71	88	81	44	325	071.4	28	.	.	20	.	.	.	01	01	01	18	15	15	11	15	05	.	.	.	.	.	.	.	22
IV	7.1	6.8	7.8	7.3	-	06.3	74	62	74	70	30	488	129.5	02	.	.	07	02	.	.	.	.	.	13	14	14	09	12	03	.	.	.	.	.	.	01	03
V	6.1	6.1	7.0	6.4	-	07.5	80	49	80	69	26	130	070.6	23	.	.	.	.	.	.	.	.	01	09	07	07	05	07	.	.	.	.	.	.	.	.	.
VI	3.9	4.2	2.5	3.5	-	09.7	65	45	66	59	31	011	007.3	03	.	.	.	22	03	.	.	.	09	03	03	02	.	03	.	.	.	.	.	.	.	.	.
VII	2.0	3.8	2.3	2.7	-	10.5	62	42	68	57	28	052	040.0	18	.	.	.	26	14	.	.	.	16	01	05	04	01	05	.	.	.	.	.	.	.	.	.
VIII	3.4	5.1	2.8	3.8	-	10.5	66	44	69	60	14	165	059.5	30	.	.	.	24	14	.	.	.	11	02	07	07	05	07	.	.	.	.	.	02	.	.	.
IX	2.5	4.8	2.5	3.3	-	09.4	85	54	83	74	42	030	028.6	28	.	.	.	16	02	.	.	.	09	01	02	02	01	02	.	.	.	.	.	.	.	.	.
X	4.3	6.0	4.1	4.8	-	06.1	83	58	76	73	34	112	068.9	22	.	.	14	.	.	.	01	.	05	06	07	07	02	07	.	.	.	.	.	.	.	.	.
XI	6.3	7.1	6.8	6.7	-	05.5	89	65	89	81	38	303	057.2	20	.	.	12	.	.	.	01	.	.	11	09	09	08	09	.	.	.	.	.	01	.	.	.
XII	5.1	6.0	4.9	5.3	-	04.0	87	54	87	76	24	440	120.2	30	.	.	28	.	.	.	04	02	10	11	11	11	07	11	03	.	.	.	.	.	.	.	05
GOD.	5.5	6.2	5.5	5.7	-	07.0	77	57	78	71	13	3184	150.3	15 I	06	.	122	90	33	.	07	03	66	119	116	113	76	110	22	01	.	.	.	03	.	01	57
NIKŠIĆ																																					
BR. ST. 242																																					
I	8.0	7.9	7.0	7.6	062.3	05.0	85	74	82	81	29	450	077.5	17	.	.	14	.	.	.	10	02	02	17	22	17	09	22	05	03	.	.	.	.	02	09	-
II	7.1	7.5	6.8	7.1	089.0	04.0	80	67	77	75	35	266	040.0	19	01	02	17	.	.	.	14	07	04	14	19	17	09	13	09	01	.	.	.	01	07	06	16
III	6.2	5.8	4.5	5.5	157.3	04.4	78	57	73	69	26	304	046.8	15	.	01	15	.	.	.	16	07	08	10	14	12	10	12	08	03	01	.	.	01	03	03	-
IV	6.7	7.4	5.5	6.5	147.8	05.9	77	57	73	69	23	434	154.0	09	.	.	04	.	.	.	15	03	02	10	14	13	07	13	04	01	.	.	.	.	03	02	04
V	5.7	7.5	5.8	6.3	187.1	07.0	73	59	71	68	23	103	034.4	23	.	.	.	.	.	.	16	01	01	08	13	11	03	13	01	.	.	.	.	.	07	.	.
VI	3.9	5.3	2.4	3.9	270.9	10.2	75	53	70	66	27	071	029.8	24	.	.	.	15	.	.	07	01	06	01	09	08	03	09	.	.	.	.	.	.	04	01	.
VII	2.7	4.4	2.1	3.1	323.1	10.8	70	49	66	62	26	054	031.3	17	.	.	.	17	04	01	14	01	14	03	06	04	02	06	.	.	.	.	.	.	06	.	.
VIII	2.7	5.4	1.8	3.3	277.3	10.8	74	45	71	63	23	056	022.9	31	.	.	.	20	09	.	07	02	10	02	12	08	02	12	.	.	.	.	.	.	09	.	.
IX	2.1	3.6	0.9	2.2	274.5	08.0	67	36	59	54	13	011	006.7	01	.	.	.	13	02	.	09	01	16	.	03	03	.	03	.	.	.	.	.	.	01	.	.
X	4.1	3.9	3.4	3.8	211.7	06.3	77	53	74	68	20	123	048.5	02	.	.	.	02	.	.	08	01	14	06	07	06	04	07	.	.	.	.	.	.	03	02	.
XI	5.8	5.7	4.8	5.4	138.2	05.7	81	64	82	76	25	212	061.8	15	.	.	05	.	.	.	15	04	08	11	13	11	07	13	.	.	.	.	.	.	03	.	.
XII	5.1	5.0	4.3	4.8	149.4	04.1	79	56	74	70	21	278	062.8	26	.	.	17	.	.	.	18	10	11	08	10	09	06	08	04	01	.	.	.	.	04	04	05
GOD.	5.0	5.8	4.1	5.0	2288.6	06.8	76	55	72	68	13	2362	154.0	8 IV	01	03	72	67	15	01	149	40	96	90	142	119	62	131	31	09	01	.	.	02	57	27	-
VIRPAZAR																																					
BR. ST. 243																																					
I	8.4	7.8	7.2	7.8	-	05.9	86	71	81	79	47	434	078.6	17	.	.	09	.	.	.	01	04	05	20	18	18	13	18	01	.	.	.	.	.	.	01	01
II	7.2	7.5	7.5	7.4	-	05.3	79	66	73	73	24	233	056.6	24	.	.	10	.	.	.	07	.	04	18	14	13	07	13	04	02	.	.	.	.	.	.	04
III	5.8	5.7	5.3	5.6	-	05.9	78	56	74	69	16	248	064.2	20	.	.	04	.	.	.	05	02	05	08	10	09	07	09	03	.	.	.	.	01	.	.	01
IV	6.3	6.3	5.4	6.0	-	07.4	74	54	77	68	22	479	135.0	09	.	.	.	02	.	.	08	06	06	11	12	12	10	12	.	.	.	.	.	.	.	.	.
V	4.0	5.1	3.8	4.3	-	08.3	76	48	72	65	27	110	037.6	29	.	.	.	02	.	.	06	.	09	06	07	06	04	07	.	.	.	.	.	.	01	.	.
VI	3.1	3.8	1.5	2.8	-	14.8	80	63	74	72	43	022	012.0	14	.	.	.	20	07	.	.	.	10	.	03	03	01	03	.	.	.	.	.	.	.	.	.
VII	1.8	2.4	1.5	1.9	-	17.3	66	53	67	62	34	030	012.0	06	.	.	.	31	22	.	.	.	21	02	04	04	01	04	.	.	.	.	.	.	.	.	.
VIII	3.2	3.7	1.8	2.9	-	17.0	76	59	72	69	40	116	090.8	31	.	.	.	27	13	.	.	.	19	04	04	04	02	04	.	.	.	.	.	.	.	.	.
IX	0.9	1.3	0.5	0.9	-	10.0	76	38	69	61	16	001	000.8	01	.	.	.	23	09	.	.	.	25	.	01	.	.	01	.	.	.	.	.	.	.	.	.
X	3.4	3.6	2.4	3.1	-	07.7	89	48	79	72	11	230	140.6	02	.	.	.	02	.	.	01	.	16	06	06	06	04	06	.	.	.	.	.	.	.	07	.
XI	5.9	5.6	4.8	5.4	-	06.4	91	59	85	78	25	374	115.8	23	.	.	.	.	.	.	02	01	09	12	10	10	06	10	.	.	.	.	.	01	.	.	.
XII	5.2	5.0	4.6	4.9	-	04.9	90	49	74	71	10	434	090.8	28	.	.	12	.	.	.	06	03	13	12	12	12	10	12	01	01	.	.	.	.	.	.	.
GOD.	4.6	4.8	3.9	4.4	-	09.3	80	55	74	69	10	2711	140.6	84 X	.	.	35	107	51	.	36	16	142	99	101	97	65	99	09	03	.	.	.	02	01	08	06
BAR																																					
BR. ST. 244																																					
I	7.7	7.9	7.0	7.5	077.1	07.3	78	71	79	76	28	280	060.8	17	.	.	01	.	.	.	05	02	02	20	21	17	09	21	.	.	.	.	.	.	.	.	.
II	7.6	7.6	6.9	7.4	090.0	06.2	72	59	72	67	24	173	047.8	24	.	.	01	.	.	.	19	07	02	14	16	13	04	15	01	01	.	.	.	02	06	.	.
III	6.9	6.2	4.9	6.0	185.2	06.1	64	57	66	62	22	194	046.5	12	.	.	.	.	.	.	14	06	03	10	14	11	07	14	.	.	.	.	.	.	05	.	.
IV	6.9	6.1	5.8	6.3	181.1	08.2	73	66	71	70	33	148	036.0	15	.	.	.	.	.	.	08	02	04	12	14	13	05	14	.	.	.	.	.	.	06	03	.
V	5.7	6.1	4.5	5.5	248.6	10.2	72	69	76	72	32	116	070.0	23	.	.	.	01	.	.	09	.	06	06	13	09	02	13	.	.	.	.	.	.	07	.	.
VI	3.5	3.0	2.4	3.0	324.8	14.9	72	74	76	74	35	016	006.8	21	.	.	.	19	04	02	05	01	13	02	07	05	.	07	.	.	.	.	.	.	03	.	.
VII	2.3	2.4	1.9	2.2	343.2	16.2	68	73	76	73	37	036	012.0	02	.	.	.	27	05	07	02	.	20	02	06	04	02	06	.	.	.	.	.	.	06	.	.
VIII	2.1	3.3	1.8	2.4	322.3	16.2	68	68	76	70	39	133	122.3	31	.	.	.	30	06	07	06	03	18	02	04	03	01	04	.	.	.	.	.	.	06	.	.
IX	1.8	1.8	1.7	1.8	291.1	12.7	60	65	70	65	27	003	003.0	01	.	.	.	24	01	02	11	.	21	01	01	01	.	01	.	.	.	.	.	.	.	.	.
X	4.8	4.1	3.6	4.2	207.6	09.8	72	69	76	72	23	194	081.6	02	.	.	.	01	.	.	07	.	13	09	09	08	03	09	.	.	.	.	.	.	03	.	.
XI	5.9	5.8	4.6	5.4	136.3	08.9	76	69	76	74	27	091	019.0	09	.	.	.	.	.	.	08	01	08	11	13	08	04	13	.	.	.	.	.	.	04	.	.
XII	5.3	5.8	4.2	5.1	139.3	06.2	64	60	67	64	28	132	040.4	26	.	.	02	.	.	.	10	01	09	09	13	07	06	13	.	.	.	.	.	.	05	.	.
GOD.	5.0	5.0	4.1	4.7	2546.6	10.2	69	66	73	69	22	1516	122.3	84 VIII	.	.	04	102	16	18	104	23	119	98	131	99	43	130	01	01	.	.	.	02	51	03	.
TITOGRAD																																					
BR. ST. 245																																					
I	8.4	8.3	7.1	7.9	068.0	06.0	84	69	83	79	40	333	043.7	13	.	.	05	.	.	.	07	04	02	22	19	15	11	19	.	.	.	.	.	.	02	.	.
II	7.4	8.0	6.8	7.4	088.7	05.2	73	62	75	70	32	208	029.6	19	.	.	06	.	.	.	15	09	03	15	21	16	08	20	04	01	.	.	01	.	03	01	-
III	6.9	6.3	4.8	6.0	185.4	05.9	71	55	73	66	33	206	048.0	15	.	.	02	.	.	.	11	06	06	12	14	12	08	14	01	.	.	.	.	.	01	.	.
IV	6.7	7.3	5.8	6.6	188.8	08.2	80	59	77	72	33	269	050.5	08	.	.	.	03	.	.	10	06	02	12	15	13	07	15	.	.	.	.	.	.	05	.	.
V	6.2	7.4	5.4	6.3	218.9	09.1	72	51	69	64	36	079	038.0	23	.	.	.	04	.	.	19	04	.	09	12	07	02	12	.	.	.	.	.	.	04	.	.
VI	4.4	5.4	3.5	4.5	310.1	13.6	71	48	66	62	32	025	008.5	07	.	.	.	24	16	08	13	02	04	03	09	06	.	09	.	.	.	.	.	.	04	.	.
VII	2.6	3.8	2.3	2.9	343.7	15.7	70	52	68	63	38	077	050.0	17	.	.	.	28	20	17	11	04	15	03	07	07	02	07	.	.	.	.	.	.	05	.	.
VIII	2.5	3.4	1.6	3.2	297.8	12.5	58	38	56	51	26	116	057.0	31	.	.	.	29	21	19	10	01	10	02	03	03	02	03	.	.	.	.	.	.	07	.	.
IX	2.2	3.4	1.5	2.4	301.0	10.8	58	41	56	52	25	.	000.0	18	.	.	.	23	09	07	13	06	17	01	.	.	.	.	.	.	.	.	.	.	01	.	.
X	4.5	4.7	3.5	4.2	221.8	08.0	67	51	70	63	30	170	071.8	02	.	.	.	05	.	.	12	07	15	08	07	06	04	07	.	.	.	.	.	.	05	.	.
XI	6.2	5.8	4.5	5.5	147.5	07.0	79	60	76	72	31	214	053.6	16	.	.	.	.	.	.	10	05	08	11	13	12	07	13	.	.	.	.	.	.	02	.	.
XII	5.4	5.6	4.5	5.2	141.6	05.1	75	56	71	67	23	188	034.8	26	.	.	09	.	.	.	08	08	08	10	12	12	07	12	01	01	.	.	.	.	04	.	.
GOD.	5.3	6.0	4.3	5.2	2513.3	08.9	71	53	70	65	23	1885	071.8	81 X	.	.	22	116	66	51	139	62	90	108	132	109	58	131	06	02	.	.	01	.	43	01	-

Mesec	Vazdušni pritisak Fm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Srednji (Dnevni)	Max	Min	Max	Min	Min	Ext.	Učestalost pravaca i srednja jačina vetra nD, Fm (0-12): N č.	N j.	NE č.	NE j.	E č.	E j.	SE č.	SE j.	S č.	S j.	SW č.	SW j.	W	W j.	NW č.	NW j.	C č.
KOLAŠIN																												
φ = 42° 50' N λ = 19° 32' E Gr. ΔG = + 1h 18 min.																												BR. ST. 246
I	677.0	-00.9	02.9	00.2	00.6	03.9	-02.3	10.3	13 -11.4	30	27	02.4	04	02.0	.	.	03	01.0	23	01.8	09	02.0	.	.	.	.	27
II	674.9	-02.9	01.7	-01.1	-00.9	03.3	-04.3	08.7	04 -21.2	18	24	01.9	05	02.8	.	.	.	.	18	02.6	17	02.5	.	.	.	.	20
III	676.3	-02.0	05.3	00.4	01.0	06.3	-03.4	14.2	25 -13.6	02	20	02.1	01	01.0	01	01.0	02	01.5	26	02.2	14	02.4	01	03.0	.	.	28
IV	678.6	03.9	10.7	05.2	06.3	11.9	01.1	23.4	23 -05.9	05	14	02.2	02	01.5	.	.	01	01.0	29	02.0	20	02.4	.	.	01	01.0	29
V	679.5	06.5	12.7	07.7	08.7	14.2	03.9	22.0	10 -02.1	02	18	01.7	11	01.8	.	.	.	.	16	01.6	11	01.9	02	01.0	01	01.0	34
VI	682.1	11.1	20.4	12.7	14.2	22.0	07.8	27.0	28 03.2	04	16	01.4	06	01.2	.	.	02	01.0	14	01.5	12	01.8	01	01.0	01	03.0	38
VII	680.9	13.0	22.2	14.0	15.8	23.2	09.1	30.2	23 02.8	19	26	02.3	04	02.2	.	.	.	.	17	01.8	08	01.9	.	.	.	.	36
VIII	681.4	11.6	22.8	13.9	15.6	24.5	09.1	30.6	07 02.8	28	13	01.5	04	01.5	01	01.0	01	02.0	11	01.3	09	01.8	.	.	01	01.0	53
IX	683.4	07.5	19.8	10.2	11.9	21.0	05.6	29.8	11 -05.4	30	29	02.0	04	02.2	.	.	.	.	08	01.4	06	01.2	01	01.0	.	.	52
X	682.7	02.5	12.9	05.0	06.4	14.1	01.0	22.4	09 -02.6	01	33	02.2	03	01.7	.	.	.	.	11	01.9	10	01.8	.	.	.	.	36
XI	681.7	01.3	09.6	03.2	04.3	10.6	-00.4	22.2	03 -06.4	12	23	01.7	02	01.0	.	.	.	.	23	01.5	06	01.3	.	.	.	.	36
XII	681.6	-02.8	04.4	-00.5	00.2	05.2	-04.2	13.4	02 -12.7	21	28	02.2	03	01.7	.	.	.	.	20	02.2	08	02.0	.	.	01	02.0	33
GOD.	680.0	04.1	12.1	05.9	07.0	13.4	01.9	30.6	7. VIII -21.2	18 II	271	02.0	49	01.8	02	01.0	09	01.2	216	01.9	130	02.0	05	01.4	05	01.6	400
IVANGRAD																												
φ = 42° 50' N λ = 19° 52' E Gr. ΔG = + 1h 19 min.																												BR. ST. 247
I	699.0	-01.3	03.1	-00.1	00.4	04.5	-03.0	13.9	05 -12.4	30	05	02.2	10	01.9	01	01.0	09	02.2	09	03.0	09	03.1	03	01.7	12	01.8	33
II	696.4	-01.3	03.5	-00.1	00.5	05.3	-04.0	14.3	05 -22.0	18	11	01.6	07	01.6	.	.	02	03.5	14	03.1	18	02.6	.	.	17	01.9	1[illegible]
III	697.9	00.4	07.7	02.8	03.5	09.7	-01.7	19.1	26 -09.4	21	05	01.4	08	01.6	03	01.7	12	01.8	11	02.5	19	02.1	02	02.0	19	01.6	1[illegible]
IV	699.7	06.4	13.0	07.0	08.3	14.5	02.2	25.4	23 -04.3	05	04	02.0	08	02.4	03	02.0	11	02.8	13	03.2	24	03.8	04	02.0	05	02.2	1[illegible]
V	700.5	08.6	14.6	09.1	10.3	16.0	04.9	26.3	10 -00.8	02	01	02.0	21	02.4	03	01.3	05	02.2	05	02.2	20	03.8	.	.	12	03.1	26
VI	702.8	13.5	22.2	14.1	16.0	23.6	08.6	29.9	10 02.2	05	02	02.0	15	02.4	.	.	.	.	10	02.8	19	03.0	01	03.0	19	02.6	24
VII	701.3	15.4	24.0	15.9	17.8	25.1	10.2	31.6	22 03.4	19	04	02.5	10	02.7	02	02.0	02	02.5	02	04.0	17	03.1	03	01.7	22	02.8	31
VIII	701.3	14.5	25.4	15.7	17.8	26.5	09.5	33.2	07 03.2	28	01	03.0	15	02.3	02	02.0	04	02.5	05	03.2	14	02.6	01	02.0	11	02.5	29
IX	704.3	09.1	21.7	10.8	13.1	22.5	05.9	32.3	11 -06.1	30	04	03.0	09	02.1	02	02.5	03	02.0	03	02.3	10	02.0	.	.	20	02.3	39
X	704.1	03.1	14.2	05.3	07.0	15.6	01.1	24.5	10 -02.5	29	10	02.8	05	02.0	02	02.0	05	02.2	11	02.2	15	02.3	01	02.0	19	02.4	25
XI	702.6	00.8	09.9	02.8	04.1	11.9	-00.8	19.1	05 -06.6	13	10	02.1	07	02.4	01	02.0	09	02.0	14	02.3	15	02.6	06	01.3	07	02.1	21
XII	704.0	-03.0	02.6	-01.3	-00.7	04.4	-04.2	13.1	30 -10.8	21	08	01.9	05	01.8	03	01.7	04	01.5	05	03.2	13	02.2	02	01.0	17	02.2	36
GOD.	701.2	05.5	13.5	06.8	08.2	15.0	02.4	33.2	7. VIII -22.0	18 II	65	02.1	120	02.2	22	01.8	66	02.2	102	02.8	193	02.8	23	01.7	180	02.3	324
ULCINJ																												
φ = 41° 55' N λ = 19° 13' E Gr. ΔG = + 1h 17 min.																												BR. ST. 248
I	750.7	07.3	09.9	07.7	08.2	10.9	05.3	15.2	16 -01.0	21	.	.	28	02.9	45	02.8	07	03.1	07	05.4	.	.	04	02.5	02	02.5	.
II	748.9	06.6	09.8	07.7	07.9	10.6	04.6	15.9	06 -04.0	18	02	02.5	26	02.7	19	02.8	04	03.2	11	04.5	04	05.0	11	05.1	07	02.6	.
III	749.8	08.5	12.6	09.8	10.2	13.8	06.2	21.6	26 00.4	02	01	03.0	15	02.7	31	02.6	06	02.3	13	03.9	02	06.5	06	04.3	19	03.3	.
IV	751.6	11.9	15.6	12.5	13.1	17.1	09.5	23.0	21,20 03.0	05,04	02	01.5	19	02.3	21	02.4	05	03.0	15	03.4	03	03.7	06	02.8	15	03.2	04
V	751.7	15.0	18.7	15.2	16.0	20.0	11.5	27.9	10 05.2	03	01	02.0	15	02.2	23	02.1	07	01.9	08	02.1	.	.	17	02.4	19	03.1	03
VI	752.7	20.8	25.3	21.0	22.0	26.7	17.7	31.1	26 11.2	04	01	01.0	22	02.0	22	02.0	04	01.2	02	02.0	01	02.0	18	02.6	15	03.3	05
VII	750.5	23.0	27.7	23.1	24.2	29.1	19.8	35.0	13 12.6	19	05	01.2	22	02.1	22	02.0	.	.	04	03.0	03	01.7	09	02.8	21	03.0	07
VIII	751.2	22.8	27.9	23.3	24.3	29.1	20.3	32.6	19 16.4	27	03	01.3	27	02.0	21	02.0	.	.	03	03.7	02	02.0	16	02.8	16	03.1	04
IX	753.5	19.1	26.0	20.9	21.7	26.9	17.3	31.4	12 10.2	30	02	01.5	31	02.5	25	02.8	02	02.0	.	.	.	.	10	03.0	16	02.6	04
X	754.6	13.3	18.9	15.4	15.8	20.2	11.0	27.2	10 05.4	24	01	01.0	32	02.6	23	02.5	03	03.0	07	03.9	02	03.0	12	02.2	11	02.6	02
XI	754.7	11.0	15.3	12.3	12.7	16.4	09.1	20.3	05 05.4	12	01	03.0	31	02.6	30	02.7	02	02.0	12	03.8	03	02.3	08	03.8	03	05.7	.
XII	755.3	07.2	11.4	08.4	08.8	12.2	05.3	17.8	02 -00.2	21	03	03.7	23	02.7	38	02.9	07	02.1	09	04.4	04	04.5	05	03.2	03	02.7	01
GOD.	752.1	13.9	18.3	14.8	15.4	19.4	11.5	35.0	13.VII -04.0	18 II	22	01.9	291	02.5	320	02.5	47	02.4	91	03.8	24	03.6	122	03.0	147	03.1	30
SR MAKEDONIJA																												
POPOVA ŠAPKA																												
φ = 42° 01' N λ = 20° 53' E Gr. ΔG = + 1h 24 min.																												BR. ST. 249
I	-	-03.3	-00.2	-03.3	-02.5	01.2	-05.9	07.3	07 -16.7	20	06	01.2	15	01.1	02	01.0	03	01.0	04	01.2	03	01.7	.	.	01	01.0	59
II	-	-04.0	-01.3	-03.7	-03.2	00.8	-06.9	08.3	05 -15.6	17	01	02.0	01	02.0	.	.	04	01.0	.	.	06	04.7	12	05.5	34	03.7	26
III	-	-02.8	01.6	-01.5	-01.0	02.9	-05.2	10.8	27 -16.3	02	.	.	01	01.0	01	02.0	01	04.0	.	.	18	03.6	09	03.2	41	02.2	22
IV	-	03.0	05.8	02.7	03.6	07.3	00.1	15.4	24 -10.4	05	.	.	.	.	.	.	02	01.5	01	02.0	22	03.0	09	02.4	35	02.4	21
V	-	04.8	07.3	04.5	05.3	08.5	01.9	17.9	11 -05.7	02	.	.	03	01.7	06	01.7	15	01.4	.	.	05	03.6	04	05.5	40	02.8	20
VI	-	11.7	13.5	11.0	11.8	15.0	07.9	20.5	18 -00.7	03	04	02.2	09	01.8	01	01.0	10	01.9	.	.	02	02.5	05	02.6	42	02.4	17
VII	-	13.0	14.3	12.1	12.9	15.8	09.1	21.0	23 07.0	18	06	01.5	12	01.1	02	01.0	22	01.5	04	03.2	03	02.7	01	03.0	17	01.7	26
VIII	-	13.5	15.6	12.7	13.6	16.8	10.0	23.0	08 04.0	27	03	01.7	25	01.4	.	.	10	01.2	.	.	11	02.5	01	05.0	20	02.8	23
IX	-	09.6	11.8	09.3	10.0	12.9	06.7	21.3	11 -04.6	29	04	02.0	08	01.6	01	01.0	18	01.7	01	02.0	01	02.0	.	.	23	01.7	34
X	-	04.5	06.8	04.7	05.1	08.3	02.0	15.0	31 -07.0	25	.	.	04	01.2	02	02.0	12	01.8	01	03.0	10	03.0	01	02.0	28	02.6	35
XI	-	03.2	05.5	03.0	03.7	07.2	00.2	14.4	04 -06.6	12	01	02.0	01	03.0	.	.	02	01.5	.	.	09	02.2	10	03.5	24	02.6	43
XII	-	-01.8	-00.1	-01.7	-01.3	02.0	-04.5	11.5	01 -13.4	18	02	02.0	01	02.0	.	.	03	01.7	10	02.5	08	03.9	05	03.2	35	03.3	29
GOD.	-	04.3	06.7	04.2	04.8	08.2	01.3	23.0	8 VIII -16.7	20 I	27	01.7	80	01.4	15	01.5	102	01.6	21	02.4	98	03.1	57	03.7	340	02.6	355
TETOVO																												
φ = 42° 00' N λ = 20° 58' E Gr. ΔG = + 1h 24 min.																												BR. ST. 250
I	-	00.3	02.7	01.4	01.5	04.1	-00.9	12.8	07 -08.0	26	02	01.5	.	.	.	.	01	02.0	01	01.0	15	02.8	05	02.6	28	01.9	41
II	-	00.2	05.6	02.6	02.7	07.4	-01.4	17.0	07 -14.0	18	17	01.4	15	01.1	.	.	02	02.0	03	01.3	09	02.8	03	01.0	03	01.0	32
III	-	02.8	09.8	06.0	06.2	12.3	01.2	23.5	27 -04.6	02	11	01.4	11	01.4	04	01.0	04	01.0	14	01.5	07	01.4	01	01.0	02	01.0	39
IV	-	08.9	16.5	11.7	12.2	18.3	05.7	27.4	24 -02.5	05	09	01.1	09	01.3	02	01.5	04	01.2	04	03.2	13	02.8	02	01.5	04	02.5	43
V	-	11.6	17.7	13.2	14.0	19.7	07.6	27.4	11 -01.0	02	23	02.2	08	01.4	.	.	03	02.0	07	01.3	05	01.6	01	04.0	04	02.2	39
VI	-	16.8	24.7	18.0	19.4	26.3	11.1	33.0	18 04.0	05	12	01.3	06	01.3	03	01.0	03	01.0	03	01.0	05	01.6	01	01.0	02	01.0	53
VII	-	17.8	26.1	19.9	20.9	27.5	13.2	33.5	23 06.0	19	20	01.4	05	01.2	01	02.0	01	01.0	07	01.1	06	01.0	.	.	03	02.0	50
VIII	-	17.0	27.2	20.0	21.0	28.8	12.4	34.0	07 06.4	28	13	01.6	04	01.0	.	.	03	01.0	04	02.0	02	01.0	.	.	02	02.0	65
IX	-	11.7	23.4	14.8	16.1	24.4	08.9	33.0	12 -02.5	30	13	01.1	06	01.0	.	.	01	02.0	04	01.0	.	.	.	.	01	01.0	62
X	-	05.5	15.8	08.6	09.6	17.1	03.5	24.5	09 -02.6	26	11	01.1	13	01.2	.	.	04	01.2	08	01.2	02	01.0	01	01.0	01	01.0	50
XI	-	01.6	11.3	04.7	05.6	12.4	00.3	21.0	02 -04.0	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-00.8	04.9	01.0	01.5	05.6	-02.0	13.0	03 -07.5	21,19	04	01.5	03	01.0	01	01.0	05	01.0	06	01.2	02	01.0	.	.	04	01.0	68
GOD.	-	07.8	15.5	10.2	10.9	17.0	05.0	34.0	7 VIII -14.0	18 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Oles)	Insolacija broj sati	Vlažnost vazduha e mm	Un % 7	14	21	Sred. (Oles)	Fis	Padavine R mm Σ	max	Broj dana n sa: Tn ≤-20,0	Tx ≤-10,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	≥8	Nm(0-10) <8,0	>8,0	R mm ≥0,1	≥1,0	≥10,0	●	≈	≡	≋	∿	▲	▲	RT	≡	≋
KOLAŠIN																																					
BR. ST. 246																																					
I	9.1	8.2	8.3	8.6	052.8	04.7	96	85	95	92	53	374	065.4	02	01	03	18	.	.	.	02	.	.	23	24	18	09	15	13	.	.	.	.	.	02	04	18
II	8.1	8.5	7.8	8.1	066.1	04.0	94	78	91	88	50	325	039.8	14	06	05	18	.	.	.	03	03	.	17	23	18	13	13	15	01	.	.	.	.	01	.	19
III	7.4	6.5	5.7	6.5	135.2	04.3	94	68	91	84	35	306	075.0	06	02	02	24	.	.	.	01	01	04	13	19	16	10	10	17	02	.	.	.	.	01	.	29
IV	6.9	7.6	6.2	6.9	147.3	06.0	92	68	86	82	32	460	123.8	09	.	.	11	.	.	.	.	.	01	14	18	15	07	13	08	01	.	.	01	.	03	.	04
V	7.9	8.3	7.3	7.8	157.4	07.2	94	70	91	85	40	135	051.5	23	.	.	03	.	.	.	.	.	.	17	20	15	03	17	04	.	.	.	.	.	05	04	-
VI	7.0	5.9	4.0	5.7	219.8	10.6	97	65	95	86	41	082	018.4	12	.	.	.	10	.	.	.	.	.	07	12	10	04	12	.	.	.	.	.	.	07	13	.
VII	4.3	5.1	3.1	4.1	269.7	11.8	97	65	97	86	42	086	052.2	17	.	.	.	14	01	.	.	.	11	06	10	08	01	10	.	.	.	.	.	01	04	07	.
VIII	6.4	5.8	2.6	4.9	239.7	11.4	97	60	98	85	32	050	022.4	31	.	.	.	15	01	.	01	.	03	03	10	07	02	10	.	.	.	.	.	.	09	14	.
IX	6.3	3.8	2.1	4.1	226.5	08.8	98	56	93	82	30	026	009.9	05	.	.	05	08	.	.	.	.	07	04	06	04	.	06	.	.	.	.	.	.	02	12	.
X	7.8	5.1	4.2	5.7	165.7	06.4	98	67	98	88	36	232	079.9	23	.	.	11	.	.	.	01	01	05	12	12	06	05	09	04	.	.	.	.	.	02	09	01
XI	6.6	6.2	5.0	5.9	112.3	05.6	97	72	93	88	31	285	083.6	16	.	.	17	.	.	.	.	.	06	13	15	13	07	14	06	.	.	.	01	.	01	01	02
XII	6.3	5.5	6.1	6.0	115.9	04.2	95	72	89	85	34	252	054.2	31	04	03	25	.	.	.	02	02	07	11	15	11	07	10	08	01	.	.	.	.	03	.	10
GOD.	7.0	6.4	5.2	6.2	1908.4	07.1	95	68	93	85	30	2613	123.8	9 IV	13	13	132	47	02	.	10	07	44	140	184	141	68	139	75	05	.	.	02	01	40	64	-
IVANGRAD																																					
BR. ST. 247																																					
I	9.2	8.4	8.3	8.6	-	03.9	83	70	84	79	47	125	037.3	02	01	06	24	.	.	.	07	03	.	24	14	10	04	09	07	.	.	.	.	.	.	04	-
II	8.6	7.5	8.0	8.0	-	03.4	74	53	74	67	41	113	037.4	16	05	06	21	.	.	.	04	02	.	16	13	11	04	07	09	01	.	.	.	.	01	02	-
III	6.8	6.4	6.1	6.4	-	04.0	80	52	72	68	32	109	033.2	06	.	01	21	.	.	.	04	.	03	12	14	12	03	12	07	02	.	.	.	.	01	.	05
IV	5.4	6.8	6.8	6.3	-	05.3	72	50	69	64	26	134	053.4	09	.	.	09	02	.	.	10	02	03	11	14	11	04	12	06	01	.	.	.	.	01	.	02
V	6.6	7.4	7.2	7.1	-	06.4	77	53	74	68	26	090	018.8	23	.	.	02	01	.	.	18	03	01	13	19	14	02	17	03	.	.	.	.	.	02	.	.
VI	4.9	6.8	5.3	5.7	-	09.3	76	48	79	68	27	049	015.3	21	.	.	.	16	.	.	11	03	03	09	18	12	01	18	01	.	.	.	.	01	09	04	.
VII	3.2	5.1	3.9	4.1	-	10.5	79	47	80	69	31	099	023.4	17	.	.	.	21	04	.	08	02	11	06	08	08	05	08	01	.	.	.	.	01	05	01	.
VIII	3.3	5.5	3.9	4.2	-	10.2	79	43	81	68	24	033	016.1	31	.	.	.	21	08	.	10	02	09	03	06	06	01	06	.	.	.	.	.	.	04	.	.
IX	5.2	4.4	3.0	4.2	-	08.1	88	41	83	71	20	035	016.8	18	.	.	05	11	05	.	01	.	10	04	04	04	02	04	.	.	.	.	.	.	02	03	.
X	8.3	5.4	4.4	6.0	-	05.7	89	51	86	76	25	119	047.3	23	.	.	12	.	.	.	07	03	04	12	08	06	05	08	02	01	.	.	.	.	.	10	02
XI	7.8	6.4	5.6	6.6	-	04.7	89	56	83	76	29	099	031.4	16	.	.	16	.	.	.	11	01	04	12	10	10	03	10	01	01	.	.	.	01	.	07	.
XII	6.7	7.1	5.9	6.6	-	03.5	85	66	81	77	31	084	018.8	26	02	08	26	.	.	.	08	04	04	15	11	11	07	09	04	02	.	.	.	.	01	05	05
GOD.	6.3	6.4	5.7	6.2	-	06.2	80	52	78	70	20	1089	053.4	9 IV	08	21	136	72	17	.	99	25	52	137	139	115	36	120	41	08	.	.	.	03	24	36	-
ULCINJ																																					
BR. ST. 248																																					
I	7.5	7.7	6.7	7.3	078.5	06.4	78	69	78	75	33	273	045.7	02	.	.	03	.	.	.	02	03	01	16	19	18	09	19	.	.	.	.	.	.	06	.	.
II	7.5	7.1	6.6	7.1	103.0	05.7	72	58	71	67	34	173	030.2	19	.	.	03	.	.	.	12	04	02	12	17	15	06	16	02	.	.	.	.	01	04	.	.
III	6.5	5.9	5.0	5.8	187.5	05.8	65	55	64	61	29	166	041.5	20	.	.	.	.	.	.	06	03	04	11	13	12	05	13	.	.	.	.	.	04	06	.	.
IV	6.7	6.0	4.6	5.8	193.3	08.1	75	64	71	70	30	142	026.2	06	.	.	.	.	.	.	06	.	05	09	15	15	05	15	.	.	.	.	.	03	06	02	.
V	5.3	5.6	4.3	5.1	259.7	09.2	70	60	69	66	32	083	023.1	18	.	.	.	01	.	.	05	.	07	08	13	08	04	13	.	.	.	.	.	01	07	.	.
VI	3.8	2.9	3.2	3.3	322.5	13.3	71	58	68	65	32	016	005.5	19	.	.	.	24	05	04	.	.	12	03	06	04	.	06	.	.	.	.	.	.	02	.	.
VII	2.4	2.5	2.0	2.3	341.7	13.8	66	53	63	61	34	064	057.6	17	.	.	.	26	14	14	04	.	20	01	06	03	01	06	.	.	.	.	.	.	04	.	.
VIII	2.1	2.9	1.7	2.2	328.0	14.9	65	58	68	64	30	064	061.4	31	.	.	.	30	13	20	01	01	21	02	02	02	01	02	.	.	.	.	.	.	05	01	.
IX	1.6	1.8	1.1	1.5	296.8	11.4	62	48	57	56	18	018	010.2	01	.	.	.	22	06	07	01	.	22	01	01	01	01	01	.	.	.	.	.	.	02	.	.
X	4.1	4.0	3.1	3.7	206.2	09.0	69	61	68	66	33	163	085.7	02	.	.	.	05	.	.	08	.	14	06	10	09	04	10	.	.	.	.	.	.	05	.	.
XI	6.1	5.2	4.5	5.3	163.8	07.8	72	62	71	68	31	103	027.4	10	.	.	.	.	.	.	06	01	08	10	12	10	04	12	.	.	.	.	.	01	05	.	.
XII	5.2	5.8	3.6	4.9	139.9	05.6	66	58	64	63	24	107	049.8	26	.	.	01	.	.	.	09	03	10	07	12	09	02	12	.	.	.	.	.	01	05	.	.
GOD.	4.9	4.8	3.9	4.5	2620.9	09.2	69	58	67	65	18	1372	085.7	2 X	.	.	07	108	38	45	60	15	126	86	126	106	42	125	02	.	.	.	.	11	57	03	.
POPOVA ŠAPKA																																					SR MAKEDONIJA
BR. ST. 249																																					
I	5.3	6.2	4.4	5.3	-	-	-	-	-	-	23	132	061.6	17	07	12	27	.	.	.	.	.	09	08	15	14	03	07	10	.	.	.	.	.	.	07	31
II	6.7	6.1	5.2	6.0	-	-	-	-	-	-	26	110	022.3	08	09	12	25	.	.	.	09	02	04	10	18	14	04	.	18	.	.	.	.	.	01	04	28
III	6.7	5.5	3.5	5.2	-	03.0	72	67	67	69	30	177	057.5	15	05	08	26	.	.	.	05	.	04	06	17	15	04	02	16	.	.	.	.	.	.	04	31
IV	6.4	5.7	4.6	5.6	-	03.8	66	61	66	64	29	100	025.7	12	01	02	14	.	.	.	01	01	06	09	17	11	04	09	12	02	.	.	.	.	01	02	23
V	5.8	7.4	5.3	6.1	-	05.2	76	74	78	76	37	099	028.2	21	.	02	10	.	.	.	02	01	04	08	22	17	02	14	09	.	.	.	.	01	03	03	07
VI	3.3	5.8	2.0	3.7	-	06.6	64	62	62	63	22	034	011.6	01	.	.	02	.	.	.	01	.	07	02	12	08	01	11	02	.	.	.	.	.	05	01	01
VII	2.5	5.4	2.7	3.5	-	08.2	70	75	73	73	32	139	037.7	06	.	.	.	.	.	.	.	.	12	04	13	10	04	13	.	.	.	.	.	.	08	03	.
VIII	1.6	3.6	2.4	2.5	-	07.5	63	62	66	64	37	009	002.6	31	.	.	.	.	.	.	02	.	18	02	04	04	.	04	.	.	.	.	.	.	04	03	.
IX	2.3	4.1	2.3	2.9	-	06.3	66	67	68	67	28	036	017.5	01	.	.	04	.	.	.	.	.	13	01	06	04	02	06	.	.	.	.	.	.	02	03	.
X	4.6	4.5	3.7	4.2	-	04.5	70	68	69	69	22	098	028.6	04	.	.	10	.	.	.	01	.	11	06	13	08	04	10	08	03	.	.	.	.	.	09	05
XI	4.3	3.9	2.0	3.4	-	03.5	61	61	59	60	15	076	023.9	10	.	01	14	.	.	.	01	.	13	03	12	08	03	07	09	.	.	.	.	.	.	02	09
XII	4.7	4.9	3.8	4.5	-	02.8	65	66	67	66	17	080	029.7	02	03	12	24	.	.	.	03	01	11	07	16	08	03	04	14	01	.	.	.	.	01	06	20
GOD.	4.5	5.3	3.5	4.4	-	-	-	-	-	-	15	1090	061.6	17 I	25	49	156	.	.	.	25	05	112	66	165	121	34	87	98	06	.	.	.	01	25	47	155
TETOVO																																					
BR. ST. 250																																					
I	10.0	9.4	8.4	9.3	-	04.6	90	83	88	87	61	114	054.0	17	.	05	17	.	.	.	.	.	.	26	17	11	03	13	06	01	.	.	.	.	.	10	06
II	8.4	8.2	6.6	7.8	-	04.1	80	62	78	73	28	105	018.2	17	03	01	17	.	.	.	01	.	.	14	15	13	05	09	08	01	.	.	.	.	01	01	12
III	8.2	7.5	5.2	7.0	-	04.8	82	54	70	69	28	139	060.0	15	.	.	11	.	.	.	.	.	03	13	12	09	05	10	05	02	.	.	.	.	01	.	03
IV	7.7	6.8	4.9	6.4	-	06.9	78	50	66	65	31	059	019.0	12	.	.	02	07	.	.	04	01	02	11	09	09	02	08	01	.	.	.	.	.	01	.	.
V	7.5	7.3	5.9	6.9	-	07.6	75	51	68	65	24	063	020.0	21	.	.	01	06	.	.	02	01	03	14	18	13	02	18	.	.	.	.	.	01	03	.	.
VI	4.0	6.4	4.1	4.8	-	10.8	74	47	71	64	30	016	008.7	21	.	.	.	23	01	.	.	.	06	04	07	05	.	07	.	.	.	.	.	.	06	.	.
VII	3.6	5.2	4.0	4.4	-	12.8	80	52	74	69	30	135	053.6	05	.	.	.	24	10	.	.	.	08	05	13	08	03	13	.	.	.	.	.	01	10	.	.
VIII	2.9	5.5	2.6	3.7	-	12.4	78	51	71	67	30	005	004.6	31	.	.	.	28	14	.	.	.	10	03	02	01	.	02	.	.	.	.	.	.	05	.	.
IX	3.9	4.5	3.6	4.0	-	09.6	88	43	77	69	20	029	020.8	01	.	.	01	15	04	.	.	.	11	04	04	03	01	04	.	.	.	.	.	.	03	.	.
X	6.2	5.1	4.5	5.3	-	06.8	90	53	83	76	28	079	030.0	23	.	.	03	.	.	.	.	.	10	11	11	07	02	11	02	.	.	.	.	.	02	01	.
XI	5.4	5.6	4.2	5.1	-	05.3	91	58	84	78	29	038	007.7	23	.	.	12	.	.	.	01	.	08	08	10	08	.	10	.	.	.	.	.	.	.	02	.
XII	6.7	6.8	6.2	6.5	-	04.5	91	75	90	85	39	089	029.2	31	.	.	23	.	.	.	.	.	06	17	11	10	04	10	04	02	.	.	.	.	02	05	01
GOD.	6.2	6.5	5.0	5.9	-	07.5	83	56	76	72	20	871	060.0	15 III	03	06	87	103	35	.	08	02	67	130	129	97	27	115	26	06	.	.	.	02	34	19	22

		Temperatura vazduha °C										Učestlina pravaca i srednja jačina vetra nD, Fm (0-12)																
		Tm										N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (Dan)							n.	j.	n.	j.	n.	j.	n.	j.	n.	j.	n.	j.		j.	n.	j.	n.
KUMANOVO																												
$\varphi = 42^\circ 08'$ N $\lambda = 21^\circ 43'$ E Gr. Δ G = + 1h 27 min.																												BR. ST. 251
I	-	01.5	04.1	02.5	02.7	05.2	00.5	16.3	07	-06.3	21	26	03.0	05	03.2	.	.	04	01.0	08	02.5	25	01.2	.	.	18	01.9	07
II	-	00.1	06.2	02.7	02.9	07.3	-01.1	17.2	06	-09.3	18	31	02.9	14	01.9	.	.	04	01.5	03	01.3	15	01.7	.	.	15	01.5	02
III	-	02.9	11.0	06.2	06.6	11.6	01.6	23.7	27	-06.6	03	13	03.8	11	02.4	01	03.0	10	01.5	12	01.8	20	01.8	.	.	18	03.3	06
IV	-	08.6	17.4	12.0	12.5	18.8	06.0	27.7	27	-03.0	05	17	03.9	10	01.5	02	01.5	06	01.8	03	01.3	28	01.5	02	02.0	18	01.8	04
V	-	11.7	18.5	13.3	14.2	19.6	08.7	28.0	11	00.6	02	11	02.6	14	02.1	01	02.0	08	01.8	07	01.6	11	01.1	.	.	36	03.0	05
VI	-	17.5	25.1	19.2	20.3	26.3	13.1	33.5	18	05.5	06	31	01.9	11	01.6	.	.	04	01.5	04	01.0	04	01.8	01	01.0	24	01.9	18
VII	-	18.5	26.8	20.4	21.5	28.0	15.2	35.8	23	06.8	19	21	02.1	17	01.6	.	.	01	01.0	01	03.0	07	01.7	01	01.0	36	02.5	09
VIII	-	17.7	28.0	20.5	21.7	29.0	15.1	35.3	08	10.3	28	26	02.2	21	01.5	.	.	06	01.0	05	01.6	03	01.0	02	01.0	24	01.6	06
IX	-	13.0	23.6	15.8	17.0	24.2	11.2	32.9	13	00.3	30	30	02.4	06	02.5	.	.	05	01.0	.	.	01	01.0	.	.	48	02.0	.
X	-	06.9	16.1	09.4	10.5	17.2	05.2	24.8	08	-00.3	01	28	02.6	11	01.5	.	.	05	02.4	04	02.2	05	01.2	.	.	38	01.7	02
XI	-	02.4	11.7	05.0	06.0	12.5	01.1	19.8	04,02	-03.8	13	19	02.8	05	02.2	.	.	03	01.0	.	.	12	01.1	.	.	37	02.0	14
XII	-	00.2	05.4	01.8	02.3	05.9	-01.1	14.3	31	-09.8	21	08	03.1	01	04.0	.	.	02	02.0	04	02.2	11	01.6	01	01.0	43	01.8	23
GOD.	-	08.4	16.2	10.7	11.5	17.2	06.3	35.3	8 VIII	-09.8	21 XII	261	02.7	126	01.9	04	02.0	58	01.5	51	01.8	142	01.4	07	01.3	355	02.1	91
KRATOVO																												
$\varphi = 42^\circ 05'$ N $\lambda = 22^\circ 09'$ E Gr. Δ G = + 1h 29 min.																												BR. ST. 252
I	-	01.4	03.5	02.0	02.2	05.2	-00.8	14.2	07	-10.2	21	08	01.9	.	.	12	01.9	12	02.2	04	02.5	07	01.9	14	01.7	12	01.8	24
II	-	00.9	05.0	03.2	03.1	07.0	-00.9	14.9	06	-10.5	18	04	01.5	04	01.8	11	01.5	15	02.8	10	02.6	08	02.1	09	02.2	09	02.1	14
III	-	03.9	09.3	06.5	06.6	11.1	01.8	20.3	27	-05.6	03	07	02.1	07	01.6	18	01.4	24	02.6	14	02.3	10	02.2	04	02.5	01	03.0	08
IV	-	10.8	15.2	11.7	12.4	17.3	06.2	-	-	-	-	07	02.0	02	01.5	19	01.6	20	02.4	13	02.5	09	02.1	09	02.7	05	02.4	06
V	-	11.3	16.2	12.9	13.3	18.1	08.1	25.4	11	02.8	02	13	01.8	06	01.8	10	01.4	21	02.0	05	02.2	07	02.1	11	01.9	13	02.4	07
VI	-	16.7	22.9	18.7	19.3	24.5	12.8	30.7	18	06.0	02	05	01.2	07	01.7	14	01.6	11	01.5	10	01.6	05	02.0	12	02.0	06	02.0	20
VII	-	16.7	25.1	19.9	20.4	26.7	13.9	31.6	23	08.0	19	03	02.0	04	01.8	11	01.5	21	02.1	02	01.5	05	01.4	10	01.5	11	01.8	26
VIII	-	18.1	26.6	20.6	21.5	27.6	14.4	32.1	21	08.9	28	04	02.0	04	01.5	07	01.4	00	01.8	17	01.8	14	01.4	10	01.8	04	01.8	25
IX	-	12.5	22.1	16.6	17.0	23.8	10.5	32.2	11	-00.4	30	02	02.0	05	01.6	16	01.1	16	01.2	03	01.3	07	01.7	14	02.1	06	02.2	21
X	-	07.7	14.8	10.3	10.8	16.3	06.0	23.0	09	-00.5	26	04	02.0	05	01.2	08	01.2	21	02.0	03	01.0	09	01.7	11	01.5	08	02.8	24
XI	-	04.3	11.6	06.8	07.4	12.7	02.5	20.4	03	-03.0	28	01	03.0	03	01.7	20	01.8	22	02.0	05	02.0	04	02.0	16	01.7	02	02.5	17
XII	-	00.9	05.1	02.0	02.5	06.0	-00.9	14.0	01	-07.5	21,19	04	02.8	.	.	09	01.1	19	02.3	07	02.4	11	01.5	15	02.1	07	02.9	21
GOD.	-	08.8	14.8	10.9	11.4	16.4	06.1	-	-	-		42	01.9	47	01.6	155	01.5	210	02.1	93	02.1	96	01.8	135	01.9	84	02.2	213
KRIVA PALANKA																												
$\varphi = 42^\circ 12'$ N $\lambda = 22^\circ 20'$ E Gr. Δ G = + 1h 29 min.																												BR. ST. 253
I	700.0	00.4	03.1	01.5	01.6	04.8	-01.0	16.6	07	-09.4	21	01	02.0	28	01.9	01	03.0	02	01.0	03	06.0	37	01.7	04	01.5	02	01.5	15
II	696.8	-00.5	04.5	01.7	01.8	06.2	-01.7	15.2	06	-12.7	18	.	.	47	02.2	02	03.0	.	.	06	05.2	21	02.8	01	02.0	02	02.0	05
III	698.6	02.4	09.1	04.9	05.3	10.3	01.4	20.7	27	-06.7	03	.	.	57	02.1	04	02.8	01	02.0	06	05.7	22	02.8	01	04.0	.	.	02
IV	700.0	08.1	15.1	10.3	11.0	17.0	05.4	25.6	25,24	-02.2	05	03	02.3	44	02.1	.	.	01	02.0	03	04.0	30	02.9	06	03.0	.	.	03
V	700.3	10.0	16.0	10.9	11.9	17.4	07.2	27.2	11	00.1	02	04	02.2	48	01.8	01	01.0	01	02.0	.	.	21	02.4	04	04.8	01	02.0	13
VI	702.5	16.3	22.6	16.9	18.2	24.0	11.9	30.4	18	05.7	02	02	02.0	55	01.8	01	01.0	01	03.0	.	.	19	01.9	03	02.3	05	02.0	04
VII	701.3	17.5	24.7	18.1	19.6	26.2	13.8	31.1	23	08.8	19	.	.	68	02.1	.	.	.	.	01	03.0	19	02.2	03	02.3	01	02.0	01
VIII	701.8	16.7	25.9	18.0	19.7	27.1	13.7	32.6	08	08.6	27	01	02.0	63	02.0	.	.	01	01.0	.	.	21	02.8	02	02.0	02	02.0	03
IX	704.3	12.1	23.0	14.4	16.0	24.0	10.0	32.2	12	-00.6	30	01	00.0	66	02.2	02	03.0	01	02.0	.	.	16	02.3	.	.	03	02.3	01
X	704.1	06.6	14.7	08.7	09.7	16.1	05.0	23.2	09	-01.4	26	02	03.0	62	02.5	02	01.5	.	.	03	04.3	23	02.6	01	03.0	.	.	.
XI	703.3	03.4	11.0	04.5	05.9	12.0	01.7	21.1	04	-03.0	12	01	03.0	58	02.4	01	01.0	.	.	02	01.0	20	02.3	02	03.0	.	.	06
XII	704.0	-00.1	05.0	01.3	01.9	06.0	-01.7	14.2	30	-07.8	19	02	03.0	49	01.8	01	01.0	01	02.0	05	06.2	28	02.3	02	02.0	02	02.0	03
GOD.	701.4	07.7	14.6	09.3	10.2	15.9	05.5	32.6	8 VIII	-12.7	48 II	17	02.3	645	02.1	15	02.2	09	01.8	29	05.0	227	02.4	29	02.8	18	02.0	56
DEBAR																												
$\varphi = 41^\circ 31'$ N $\lambda = 20^\circ 32'$ E Gr. Δ G = + 1h 22 min.																												BR. ST. 254
I	-	01.5	04.0	02.6	02.7	05.5	00.6	15.6	07	-07.8	21,20	17	01.8	06	01.2	01	01.0	17	02.1	06	03.0	.	.	01	01.0	24	01.8	21
II	-	00.7	04.7	02.6	02.7	06.3	-	13.2	06	-	-	17	01.5	04	01.5	02	01.5	08	01.9	15	02.0	02	02.5	02	01.5	19	01.8	15
III	-	03.3	09.7	06.5	06.5	10.6	01.7	21.0	27,25	-06.2	02	08	01.8	04	01.0	01	07.0	21	02.1	12	02.8	04	01.2	.	.	20	02.1	23
IV	-	08.1	15.4	11.3	11.5	17.3	06.5	28.0	22	-02.2	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	10.5	16.7	12.7	13.2	18.5	08.5	28.0	10	03.2	03	11	01.5	05	01.0	06	02.0	13	01.5	04	01.8	01	04.0	01	02.0	26	02.1	26
VI	-	15.5	24.0	18.6	19.2	25.5	12.3	31.4	18	06.4	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	17.1	25.4	20.2	20.7	27.0	14.2	32.2	23	07.0	19	03	02.0	15	01.5	13	01.4	08	01.9	01	02.0	.	.	07	02.0	22	02.0	24
VIII	-	17.5	27.4	21.4	21.9	28.6	14.5	33.6	08	11.0	12	01	01.0	08	01.4	07	01.1	08	01.1	03	02.3	01	02.0	05	02.8	24	01.9	36
IX	-	13.5	23.2	17.9	18.2	24.2	11.6	32.0	12	02.8	30	10	01.7	11	01.0	03	02.3	01	01.0	01	02.0	.	.	03	02.7	27	02.1	34
X	-	06.0	15.6	09.3	10.0	17.3	03.7	24.0	10,09	-01.4	26	04	01.5	04	01.2	01	01.0	.	.	08	01.0	01	02.0	08	01.0	03	01.3	64
XI	-	03.2	11.6	06.0	06.7	12.8	01.6	19.5	21	-03.0	26,12	04	02.2	.	.	.	.	03	01.3	18	01.9	.	.	14	01.3	03	01.7	48
XII	-	00.7	05.7	02.7	02.9	06.4	-00.6	14.6	29	-08.4	21	02	03.0	.	.	01	04.0	02	01.5	48	02.2	10	01.7	04	01.5	02	01.5	24
GOD.	-	08.1	15.3	11.0	11.4	16.7	-	33.6	8 VIII	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
STRUGA																												
$\varphi = 41^\circ 11'$ N $\lambda = 20^\circ 41'$ E Gr. Δ G = + 1h 23 min.																												BR. ST. 255
I	-	02.1	05.9	03.6	03.8	07.3	00.1	16.5	07	-08.0	23	11	01.6	12	02.6	.	.	10	02.5	06	01.5	06	01.8	02	01.0	28	02.1	18
II	-	01.9	05.4	03.0	03.3	07.6	-00.5	15.0	05	-14.0	18	13	02.5	10	02.3	04	02.0	11	03.2	11	03.8	11	03.8	.	.	18	02.4	06
III	-	03.0	08.9	05.6	05.8	11.5	00.2	22.0	27,26	-07.0	01	09	02.0	10	02.3	.	.	18	02.5	17	02.9	08	03.8	.	.	25	02.9	06
IV	-	07.9	14.1	09.3	10.2	16.1	03.6	25.0	20	-02.0	07	07	02.7	13	03.0	.	.	28	02.4	12	01.7	04	05.2	.	.	11	02.5	15
V	-	10.2	16.2	11.3	12.2	18.5	06.3	27.8	11	02.0	03	09	02.0	11	01.9	02	01.0	18	02.6	09	01.9	10	03.5	03	02.0	12	02.5	19
VI	-	14.6	22.2	17.5	17.9	23.6	10.1	30.0	17	04.3	05	06	02.3	12	02.3	01	01.0	19	02.2	19	02.5	05	03.0	01	01.0	06	03.0	21
VII	-	16.7	25.0	19.3	20.1	26.2	12.5	31.0	24	06.0	20	13	01.8	11	01.8	02	01.0	18	01.9	05	01.8	08	02.1	.	.	14	01.9	22
VIII	-	16.7	25.5	20.2	20.6	26.9	12.9	33.5	09	-	-	12	01.2	10	01.4	01	01.0	06	02.2	10	01.4	17	01.8	02	02.0	13	01.5	22
IX	-	12.8	21.9	15.5	16.4	23.4	10.1	27.5	16,13	00.6	30	08	01.5	13	02.3	.	.	06	02.0	06	02.2	09	01.4	01	01.0	27	01.3	20
X	-	07.8	15.5	09.4	10.5	17.1	04.3	22.8	12	00.2	27	06	01.3	11	02.0	.	.	30	02.2	02	03.0	07	02.1	.	.	29	01.7	08
XI	-	04.1	11.9	06.1	07.0	13.9	01.5	17.8	01	-04.2	12	06	01.0	17	02.1	01	01.0	15	02.3	03	01.7	04	01.5	01	01.0	31	01.4	12
XII	-	00.9	06.6	02.6	03.2	08.3	-01.8	15.8	01	-06.9	21	10	01.4	08	02.4	.	.	09	02.7	13	02.2	07	02.6	01	01.0	34	01.6	11
GOD.	-	08.2	14.9	10.3	10.9	16.7	04.9	33.5	9 VIII	-		110	01.8	138	02.2	11	01.4	188	02.4	113	02.3	96	02.6	11	01.5	248	01.9	180

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e mm	Um % 7	14	21	Sred. (Dies)	Min	Padavine R mm M	Max	Int.	Broj dana sa: Tn ≤0,0	Tn ≤0,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	F(0-12) ≥6	F(0-12) ≥8	Nm(0-10) ≤2,0	Nm(0-10) ≤5,0	R mm ≥0,1	R mm ≥1,0	R mm ≥10,0	●	☆	☆	☆	☁	▲	▲	T	■	■
KUMANOVO																																					
BR. ST. 251															H_a = 338 m H_b = - m h_a = 2,1 m h_b = 1,5 m																							
I	9.2	9.1	9.0	9.1	-	05.0	88	79	85	84	47	042	016.8	17	.	06	13	.	.	.	07	.	.	26	08	06	02	07	01	.	.	.	.	.	.	08	03
II	7.9	5.8	6.2	6.6	-	04.5	84	68	79	78	38	034	009.1	24	.	.	17	.	.	.	03	.	01	09	12	08	.	11	03	01	.	.	.	.	.	07	02
III	6.5	5.6	4.5	5.5	-	05.3	82	58	73	71	32	024	007.3	05	.	.	09	.	.	.	06	.	08	11	10	04	.	09	01	.	.	.	.	.	01	04	.
IV	6.1	6.0	4.5	5.5	-	06.5	76	44	62	61	29	015	005.6	12	.	.	02	07	.	.	04	.	09	10	08	05	.	08	.	.	.	.	.	.	01	.	.
V	5.7	6.9	6.2	6.3	-	07.9	76	47	72	65	27	065	018.7	21	.	.	.	05	.	.	.	.	05	11	12	11	02	.	.	.	.	.	.	.	02	.	.
VI	1.9	5.8	4.4	4.0	-	11.0	73	45	68	62	29	032	016.1	20	.	.	.	23	06	.	.	.	06	02	05	04	02	05	.	.	.	.	.	.	05	.	.
VII	2.9	3.8	3.1	3.3	-	12.5	77	47	71	65	30	059	020.1	06	.	.	.	23	13	.	01	.	14	05	10	06	03	10	.	.	.	.	.	01	11	.	.
VIII	2.3	4.2	2.8	3.1	-	11.5	78	39	66	61	28	028	021.5	11	.	.	.	26	15	.	02	02	14	03	06	04	01	06	.	.	.	.	.	01	.	06	.	.
IX	2.2	3.3	2.2	2.6	-	09.3	79	41	68	63	26	024	017.7	01	.	.	.	15	05	.	.	.	16	01	03	03	01	03	.	.	.	.	.	.	.	.	.
X	5.3	3.8	2.7	3.9	-	07.1	89	54	81	75	29	094	027.1	17	.	.	01	.	.	.	.	.	11	05	08	08	05	08	01	01	.	.	.	.	.	02	.
XI	5.5	4.7	3.3	4.5	-	05.6	90	60	85	78	34	012	004.0	23	.	.	10	.	.	.	02	.	11	09	08	05	.	08	.	.	.	.	.	.	.	04	.
XII	7.7	6.6	6.9	7.1	-	04.8	89	77	88	85	40	040	013.3	31	.	.	18	.	.	.	01	.	03	17	10	07	02	09	01	.	.	.	.	.	.	12	03
GOD.	5.3	5.5	4.6	5.1	-	07.6	81	54	74	70	25	469	027.1	14 X	.	06	70	99	39	.	26	02	98	107	100	71	18	84	07	02	.	.	01	01	26	37	08
KRATOVO																																					
BR. ST. 252															H_a = 640 m H_b = - m h_a = 2,0 m h_b = 1,5 m																							
I	6.2	7.2	8.3	7.9	-	05.0	89	84	87	87	48	068	020.0	17	01	07	17	.	.	.	.	.	02	19	09	09	03	08	01	.	.	.	.	.	.	12	03
II	6.9	6.2	6.6	6.6	-	05.0	89	78	84	84	50	085	015.1	24	01	01	18	.	.	.	.	.	02	11	13	13	05	10	05	02	.	.	.	.	.	03	07
III	6.6	6.0	4.9	5.9	-	05.3	79	65	73	72	32	051	018.2	05	.	.	12	.	.	.	.	01	03	08	07	07	01	06	01	.	.	.	.	01	.	04	.
IV	5.6	5.3	4.6	5.2	-	06.1	66	48	58	57	-	068	025.5	25	-	-	-	-	-	-	.	.	06	07	11	08	03	10	02	01	.	.	.	.	.	01	.
V	5.5	5.7	6.6	5.9	-	07.8	80	56	71	69	-	084	022.1	01	.	.	.	01	.	.	.	.	01	07	13	12	02	13	.	.	.	.	.	.	01	01	.
VI	3.0	3.9	3.7	3.5	-	10.4	74	50	64	63	33	008	005.3	01	.	.	.	19	01	.	.	.	05	01	04	02	.	04	.	.	.	.	.	.	02	.	.
VII	2.6	4.1	3.6	3.4	-	13.6	84	65	76	75	19	143	040.2	05	.	.	.	25	04	.	.	.	10	03	11	10	06	11	.	.	.	.	.	02	08	01	.
VIII	2.8	3.4	3.1	3.1	-	13.1	79	54	71	68	37	078	034.2	22	.	.	.	25	10	.	.	.	08	01	05	05	03	05	.	.	.	.	.	01	02	.	.
IX	2.3	2.6	2.1	2.3	-	08.4	78	40	57	58	20	008	003.1	01	.	.	01	14	05	.	.	.	18	.	03	03	.	03	.	.	.	.	.	.	.	01	.
X	4.1	4.5	4.4	4.3	-	07.0	81	61	72	71	36	123	022.0	03	.	.	01	.	.	.	.	.	11	06	09	09	06	09	02	.	.	.	.	.	.	07	.
XI	4.2	3.3	2.4	3.3	-	05.5	82	57	74	71	34	019	011.3	17	.	.	07	.	.	.	.	.	11	04	06	04	01	04	.	.	.	.	.	.	.	03	.
XII	6.0	5.7	4.4	5.4	-	04.8	89	74	86	83	42	032	012.9	26	.	01	21	.	.	.	.	.	06	08	09	05	01	07	02	.	.	.	.	.	.	05	02
GOD.	4.8	4.8	4.6	4.7	-	07.7	80	61	72	71	-	767	040.2	5 VII	-	-	-	-	-	-	.	01	83	75	100	87	31	92	13	03	.	.	.	04	13	38	12
KRIVA PALANKA																																					
BR. ST. 253															H_a = 691 m H_b = 695.6 m h_a = 2,0 m h_b = 1,5 m																							
I	9.1	8.9	8.6	8.9	056.2	04.5	87	78	83	83	49	052	016.0	17	.	08	18	.	.	.	02	.	01	27	12	06	03	09	04	.	.	.	.	.	.	06	04
II	7.3	7.7	6.4	7.1	109.6	03.8	83	59	72	71	30	069	012.8	24	01	.	17	.	.	.	-	-	01	12	16	12	01	11	08	.	.	.	.	.	.	02	09
III	7.3	6.8	5.3	6.4	159.0	04.5	78	54	70	68	26	054	015.3	05	.	.	09	.	.	.	05	02	-	-	16	11	01	13	06	03	.	.	.	.	02	.	02
IV	7.0	6.9	4.5	6.1	179.8	05.9	75	46	62	61	23	033	009.0	13	.	.	03	02	.	.	03	.	01	10	11	07	.	11	.	.	.	.	.	.	03	.	.
V	6.8	7.6	6.2	6.9	183.8	07.5	80	54	77	71	31	105	035.1	01	.	.	.	02	.	.	03	.	02	14	18	16	03	18	01	01	.	.	.	.	06	.	.
VI	2.6	6.0	4.0	4.2	283.2	10.3	75	51	71	65	29	046	012.0	21	.	.	.	19	01	.	01	.	02	03	09	08	01	09	.	.	.	.	.	01	06	.	.
VII	2.5	5.1	4.2	3.9	314.6	11.6	77	51	73	67	37	172	097.0	05	.	.	.	22	03	.	01	.	09	05	12	08	04	12	.	.	.	.	.	01	14	.	.
VIII	2.7	5.1	2.2	3.3	309.4	10.6	75	42	67	62	28	009	004.3	09	.	.	.	24	08	.	03	02	15	01	05	03	.	04	.	.	.	.	.	.	08	.	.
IX	2.3	3.6	1.4	2.4	277.4	08.1	74	39	63	59	26	012	006.2	05	.	.	01	13	04	.	.	.	17	.	02	02	.	02	.	.	.	.	.	.	02	.	.
X	4.7	4.9	4.0	4.6	193.1	06.5	83	55	79	72	31	074	016.3	24	.	.	03	.	.	.	05	.	12	09	09	08	03	09	01	.	.	.	.	.	.	.	01
XI	4.9	4.7	2.5	4.0	158.9	05.2	80	56	81	72	31	030	011.8	11	.	.	08	.	.	.	01	.	10	05	08	05	01	08	.	.	.	.	.	.	01	02	.
XII	6.0	5.6	4.5	5.4	-	04.1	81	64	79	74	45	023	006.8	02	.	01	23	.	.	.	05	.	09	10	10	06	.	07	04	.	.	.	.	.	.	02	03
GOD.	5.3	6.1	4.5	5.3	-	06.9	79	54	73	68	23	679	097.0	5 VII	01	09	82	82	16	.	-	-	-	-	128	92	17	113	24	04	.	.	.	02	42	12	19
DEBAR																																					
BR. ST. 254															H_a = 675 m H_b = - m h_a = 2,1 m h_b = 1,5 m																							
I	9.5	9.2	9.2	9.3	-	04.5	73	77	74	75	09	121	030.8	03	.	05	13	.	.	.	01	.	01	28	12	12	04	10	04	01	.	.	.	.	.	04	-
II	7.8	7.7	7.2	7.5	-	04.4	71	73	73	73	55	168	035.6	16	-	02	-	.	.	-	.	.	.	13	16	16	06	11	07	.	.	.	.	.	.	.	13
III	6.5	6.7	6.0	6.4	-	04.9	79	61	65	68	12	121	027.4	28	.	.	09	.	.	.	02	.	03	13	11	11	05	10	02	01	.	.	.	.	.	.	03
IV	6.2	6.9	6.3	6.4	-	06.1	76	50	62	63	-	082	018.4	12	.	.	02	04	.	.	-	-	03	14	12	11	04	10	02	.	.	.	.	.	.	.	.
V	6.0	7.4	6.5	6.6	-	07.6	81	54	68	68	18	050	012.4	21	.	.	.	02	.	.	.	.	.	09	12	12	01	12	.	.	.	.	.	.	.	.	.
VI	3.1	5.7	3.4	4.1	-	09.7	78	44	58	60	21	033	016.8	03	.	.	.	22	03	.	.	.	07	04	06	04	02	06	.	.	.	.	.	.	.	.	.
VII	3.0	5.1	4.0	4.0	-	11.7	80	50	65	65	28	076	022.8	05	.	.	.	24	05	.	.	.	10	05	09	07	03	09	.	.	.	.	.	.	.	.	.
VIII	2.2	4.2	3.2	3.2	-	11.7	77	44	61	61	29	038	012.0	11	.	.	.	26	13	.	.	.	10	01	05	05	03	05	.	.	.	.	.	.	.	.	.
IX	2.5	4.0	3.0	3.2	-	08.9	77	41	57	58	23	028	023.0	01	.	.	.	14	05	.	.	.	14	01	03	02	01	03	.	.	.	.	.	.	.	.	.
X	4.2	5.1	4.5	4.6	-	06.8	89	56	79	75	30	107	045.0	23	.	.	01	.	.	.	.	.	13	10	07	06	04	05	02	.	.	.	.	.	01	.	01
XI	6.0	6.6	6.0	6.2	-	05.9	92	62	86	80	39	105	026.0	10	.	.	07	.	.	.	.	.	05	13	07	07	05	07	.	.	.	.	.	.	.	02	.
XII	6.3	6.5	6.1	6.4	-	04.8	88	74	86	83	38	090	031.5	31	.	.	18	.	.	.	.	.	-	-	08	07	04	07	01	.	.	.	.	.	.	02	01
GOD.	5.3	6.3	5.4	5.7	-	07.2	80	57	69	69	-	1019	045.0	23 X	-	07	-	42	26	-	-	-	-	-	108	100	42	95	18	02	.	.	.	.	01	08	-
STRUGA																																					
BR. ST. 255															H_a = 695 m H_b = - m h_a = 2,0 m h_b = 1,4 m																							
I	9.0	7.5	7.6	8.0	-	05.3	87	84	87	86	56	113	032.0	17	.	01	12	.	.	.	01	.	03	22	13	13	04	12	01	.	.	.	.	.	.	.	01
II	7.7	7.4	6.8	7.3	-	05.2	85	83	86	85	53	165	032.0	24	01	.	14	.	.	.	05	.	.	14	17	17	06	11	06	.	.	.	.	.	.	.	-
III	6.4	6.4	5.2	6.0	-	05.5	83	73	80	79	-	134	030.1	28	.	.	14	.	.	.	05	01	05	11	11	11	06	09	02	.	.	.	.	.	.	.	02
IV	6.2	6.5	5.7	6.1	-	06.9	80	66	72	73	27	070	014.0	08	.	.	04	01	.	.	01	01	05	10	12	11	03	12	.	.	.	.	.	.	.	.	.
V	5.9	6.5	6.4	6.3	-	07.5	80	56	72	69	33	042	011.5	21	.	.	.	02	.	.	01	.	04	12	10	08	02	10	.	.	.	.	.	.	.	.	.
VI	2.9	5.5	4.6	4.4	-	10.4	76	54	71	67	40	026	008.5	22	.	.	.	15	01	.	.	.	08	04	06	06	.	06	.	.	.	.	.	.	.	.	.
VII	2.6	5.1	3.9	3.9	-	11.6	79	50	70	66	29	032	012.5	17	.	.	.	2[illegible]	01	.	.	.	12	04	05	04	01	05	.	.	.	.	.	.	.	.	.
VIII	2.2	4.1	2.4	2.9	-	11.5	78	50	64	64	30	017	011.2	25	-	.	-	24	02	-	.	.	16	02	03	03	01	03	.	.	.	.	.	.	.	.	.
IX	2.3	2.9	2.8	2.6	-	09.8	78	52	74	68	30	026	019.2	01	.	.	.	13	.	.	.	.	16	03	04	02	01	04	.	.	.	.	.	.	.	.	.
X	4.4	5.0	3.9	4.4	-	07.2	80	61	81	74	29	094	037.0	23	.	.	.	.	.	.	.	.	13	08	06	06	04	06	.	.	.	.	.	.	.	.	.
XI	4.3	4.0	4.1	4.1	-	06.2	89	68	82	79	47	064	015.0	09	.	.	09	.	.	.	.	.	12	06	08	08	02	08	.	.	.	.	.	.	.	.	.
XII	5.9	5.7	4.5	5.4	-	04.8	86	72	83	80	38	089	048.3	31	.	.	22	.	.	.	.	.	09	12	13	08	03	09	04	.	.	.	.	.	01	.	03
GOD.	5.0	5.6	4.8	5.1	-	07.7	81	64	76	74	-	872	048.3	31 XII	-	01	-	78	04	-	13	02	103	108	108	97	33	95	13	.	.	.	.	.	01	.	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Dšms)	Max	Min	Max	Dat.	Min	Dat.	Čestina pravaca i srednja jačina vetra nD, Fm (0-12): N B.	N J.	NE B.	NE J.	E B.	E J.	SE B.	SE J.	S B.	S J.	SW B.	SW J.	W	W J.	NW B.	NW J.	C B.
φ = 41° 32' N λ = 20° 42' E Gr. △G = + 1h 23 min.																												
I	647.3	-01.8	01.6	-01.0	-00.5	03.2	-03.3	10.5	07	-13.0	20	01	02.0	07	01.7	13	02.6	13	03.7	01	05.0	03	04.0	06	01.3	18	02.1	31
II	644.9	-02.7	00.0	-01.5	-01.4	02.3	-04.4	08.8	05	-18.0	18	05	01.8	05	01.6	11	01.9	04	03.2	02	02.5	02	04.5	14	03.9	29	03.7	12
III	646.8	-01.2	03.6	00.6	00.9	05.6	-02.6	16.2	27	-10.6	03	07	02.1	06	01.8	17	02.2	05	03.0	03	04.7	10	03.6	10	03.1	15	01.9	20
IV	649.4	04.1	09.1	05.1	05.9	10.6	01.6	20.0	25,23	-09.1	05	05	02.0	08	02.1	13	01.5	09	03.2	02	02.5	18	03.8	03	04.0	25	03.0	07
V	649.8	06.5	10.7	06.9	07.7	12.3	03.6	22.5	10	-03.2	02	06	02.0	06	01.5	15	01.5	07	02.7	01	02.0	10	02.6	05	03.2	28	03.1	15
VI	653.0	12.5	18.0	12.1	13.7	19.2	07.9	24.5	18	00.1	04	02	03.0	07	01.9	23	01.8	05	01.2	03	02.3	03	01.3	05	02.2	29	02.7	13
VII	652.0	13.6	19.8	14.1	15.4	21.2	09.8	26.8	23	03.0	19	05	01.8	04	01.2	17	01.5	08	01.8	04	02.2	04	02.0	06	03.2	21	02.2	24
VIII	652.6	13.5	20.1	13.9	15.3	21.7	09.9	26.4	08,07	03.8	28	05	02.6	05	01.0	35	01.7	07	01.6	03	01.3	05	03.6	06	03.3	19	03.1	08
IX	654.0	09.4	18.1	10.8	12.3	19.2	07.4	26.8	10	-03.1	30	06	02.5	04	01.8	36	01.6	07	02.0	.	.	01	03.0	02	02.0	21	03.1	13
X	652.8	04.0	10.7	05.3	06.3	11.9	02.3	19.5	09	-03.4	26,25	09	03.2	03	02.0	26	01.5	05	01.2	04	03.2	05	03.2	02	03.0	22	02.8	17
XI	652.0	02.6	08.2	03.3	04.3	09.3	00.7	20.0	03	-05.7	26	12	02.8	03	02.7	20	01.8	09	01.8	03	01.3	01	05.0	08	02.5	23	03.0	11
XII	651.5	-02.2	03.1	-01.0	-00.3	04.2	-03.5	09.9	30	-11.7	18	07	02.1	06	02.7	19	01.7	15	02.7	04	02.0	04	03.0	02	02.0	18	02.1	18
GOD.	650.5	04.9	10.2	05.7	06.6	11.7	02.4	26.8	10 IX	-14.0	48 II	70	02.4	64	01.8	245	01.7	94	02.5	30	02.5	66	03.3	69	03.0	268	02.8	189
φ = 41° 42' N λ = 20° 45' E Gr. △G = + 1h 23 min.																												
I	-	-02.1	01.5	-01.2	-00.7	03.3	-03.9	10.6	07	-14.0	1	04	02.0	13	02.5	02	02.0	.	.	02	02.0	29	02.7	10	02.3	03	02.3	30
II	-	-01.8	01.1	-01.1	-00.7	02.6	-03.7	09.3	06	-14.6	13	.	.	08	03.1	.	.	.	.	01	02.0	49	04.1	03	02.3	04	02.5	19
III	-	-00.5	03.9	01.1	01.4	05.3	-01.9	15.8	27	-10.7	02	.	.	20	03.0	02	03.0	.	.	.	.	45	03.4	.	.	01	03.0	25
IV	-	04.9	09.6	05.7	06.4	11.2	03.0	21.0	24,23	-05.6	05	.	.	08	03.1	.	.	.	.	.	.	57	03.0	.	.	01	03.0	24
V	-	06.9	11.2	07.2	08.1	12.6	04.4	22.3	10	-01.6	03	.	.	19	02.6	.	.	.	.	.	.	36	03.6	01	03.0	.	.	37
VI	-	13.0	17.9	12.9	14.2	19.2	09.0	25.0	18	02.1	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	14.3	18.3	14.1	15.2	20.1	10.8	25.0	23	04.4	19	.	.	30	02.9	.	.	.	.	.	.	21	03.2	.	.	.	.	42
VIII	-	15.0	20.5	14.6	16.1	21.6	11.3	28.6	08	05.8	28	.	.	19	02.8	01	02.0	.	.	.	.	29	03.2	.	.	.	.	44
IX	-	10.3	16.3	11.1	12.2	17.4	08.2	26.6	11	-01.5	30	.	.	37	02.8	.	.	.	.	.	.	06	03.0	.	.	.	.	47
X	-	05.2	10.2	05.7	06.7	12.1	02.8	19.4	31	-03.3	26	.	.	21	02.8	.	.	.	.	.	.	36	03.5	.	.	.	.	36
XI	-	03.4	08.7	04.6	05.3	10.2	01.6	19.4	03	-04.5	12	.	.	17	02.4	.	.	.	.	.	.	47	03.1	.	.	.	.	26
XII	-	-01.3	02.5	-00.8	-00.1	04.4	-02.7	11.0	01	-08.6	18	.	.	23	02.2	.	.	.	.	.	.	24	03.3	.	.	.	.	46
GOD.	-	05.6	10.1	06.2	07.0	11.7	03.2	28.6	8 VIII	-14.6	48 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 41° 07' N λ = 20° 48' E Gr. △G = + 1h 23 min.																												
I	693.9	02.7	05.6	03.3	03.8	06.6	01.1	14.3	07	-06.8	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	691.5	02.2	05.3	03.3	03.5	06.7	00.3	12.7	05	-12.5	18	20	02.2	01	02.0	01	03.0	.	.	24	03.5	21	02.7	08	02.8	05	02.0	04
III	692.8	03.1	08.8	05.8	05.9	10.4	01.6	20.0	26	-04.0	02	23	02.6	02	01.5	02	01.0	.	.	26	02.6	13	02.6	13	02.3	08	02.1	06
IV	694.9	07.7	13.7	09.7	10.2	14.7	05.1	23.4	24	-02.3	05	14	02.2	04	02.0	.	.	03	01.7	20	02.8	22	02.4	10	02.2	03	01.3	14
V	695.0	10.1	15.3	11.4	12.1	17.0	07.2	26.4	11	00.5	02	20	01.8	04	01.0	.	.	01	02.0	21	02.3	21	02.1	08	02.2	05	01.8	13
VI	697.3	15.7	22.2	17.5	18.2	23.6	11.8	29.0	18	05.4	02	18	02.0	04	01.2	.	.	01	01.0	22	02.0	13	02.0	05	01.6	08	01.5	19
VII	695.7	17.7	24.8	19.5	20.3	26.2	14.0	31.1	24	06.1	19	29	02.0	04	02.2	.	.	01	02.0	17	01.9	12	02.3	06	02.0	05	01.8	19
VIII	696.5	16.9	25.9	19.8	20.6	27.1	14.2	32.4	08	10.0	28	25	01.6	01	01.0	.	.	01	01.0	20	01.8	18	02.1	04	02.8	09	01.6	15
IX	698.2	13.4	22.8	16.6	17.3	23.9	11.7	29.9	12	02.5	30	39	02.4	01	03.0	03	03.3	.	.	15	01.8	12	01.8	01	02.0	09	01.7	10
X	698.3	07.5	14.8	10.4	10.8	16.1	05.9	20.5	09	00.8	26	36	02.2	07	02.3	.	.	01	02.0	26	02.4	11	02.2	03	02.0	08	01.6	01
XI	697.8	04.8	11.3	06.7	07.4	12.4	03.1	17.3	05	-02.0	12	31	02.1	03	01.7	.	.	02	02.0	17	02.1	21	02.0	02	02.0	07	01.9	07
XII	698.1	01.7	06.5	02.9	03.5	07.3	-00.3	14.6	01	-06.2	18	33	02.2	02	01.5	02	01.0	02	02.5	17	03.3	12	02.1	04	01.8	16	02.0	05
GOD.	695.8	08.6	14.8	10.6	11.1	16.0	06.3	32.4	8 VIII	-12.5	48 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 41° 48' N λ = 20° 55' E Gr. △G = + 1h 24 min.																												
I	-	00.2	02.4	01.2	01.3	03.8	-01.1	16.2	07	-07.5	23,22	20	02.2	05	01.8	.	.	01	02.0	01	02.0	06	04.0	.	.	02	02.0	58
II	-	00.0	05.2	01.4	02.0	06.9	-02.7	16.0	06	-18.2	18	04	02.2	07	02.4	.	.	01	02.0	.	.	26	04.6	.	.	11	02.5	35
III	-	02.7	09.7	05.6	05.9	11.1	00.6	23.0	27	-05.3	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	08.9	15.7	09.9	11.1	17.4	04.9	26.0	25,24	-02.0	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	11.8	17.3	11.6	13.1	18.7	07.6	26.6	11	-01.0	03	03	02.3	11	02.6	.	.	.	.	02	02.0	22	04.3	.	.	24	02.7	31
VI	-	17.2	24.1	17.7	19.2	25.7	11.5	32.2	18	05.7	06	02	02.5	19	02.3	.	.	05	02.8	01	04.0	11	02.9	.	.	16	02.2	36
VII	-	17.9	25.0	18.8	20.1	26.7	12.2	-	-	-	-	06	02.0	06	02.2	.	.	03	02.3	.	.	14	03.1	.	.	21	02.3	43
VIII	-	17.1	26.1	18.4	20.0	27.2	11.7	33.0	08	07.0	29,28	03	02.0	12	02.5	.	.	.	.	01	03.0	12	03.6	.	.	14	02.6	51
IX	-	12.4	21.7	13.7	15.4	22.7	08.5	30.0	12	-01.3	30	10	02.2	08	02.1	.	.	.	.	.	.	02	02.0	.	.	23	02.5	47
X	-	06.0	14.9	08.5	09.4	16.3	02.8	22.6	08	-02.4	26	12	02.2	12	02.3	.	.	01	02.0	04	04.0	09	03.0	.	.	14	02.6	41
XI	-	02.4	10.9	04.2	05.4	11.7	-00.3	18.6	02	-03.5	29,12	12	02.2	13	02.2	.	.	.	.	01	05.0	03	03.0	.	.	09	02.1	52
XII	-	-00.6	04.7	00.6	01.3	06.1	-03.2	15.5	01	-07.5	19	13	02.2	14	02.1	.	.	04	03.5	01	02.0	07	02.6	.	.	03	02.3	51
GOD.	-	08.0	14.8	09.3	10.4	16.2	04.4	-	-			-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 41° 31' N λ = 20° 58' E Gr. △G = + 1h 24 min.																												
I	-	01.1	04.2	02.8	02.7	05.5	00.4	17.0	07	-08.2	21	34	01.9	12	02.2	05	01.4	08	01.8	17	01.7	01	03.0	06	01.5	04	02.2	06
II	-	01.6	06.2	03.4	03.6	07.4	00.1	15.3	06,05	-14.0	18	22	02.5	09	02.6	09	01.4	09	01.8	29	03.5	02	03.0	.	.	04	01.8	.
III	-	02.4	10.7	05.8	06.2	11.7	01.4	23.0	27	-05.0	03	28	03.0	07	02.1	08	01.8	05	02.2	32	02.7	03	01.7	01	05.0	07	02.1	02
IV	-	07.3	16.6	10.4	11.2	17.6	04.7	26.5	24	-02.5	05	20	02.3	12	02.9	05	02.2	08	02.0	31	03.0	02	03.5	02	01.5	04	01.5	06
V	-	09.0	18.5	12.3	13.0	19.1	07.3	29.0	11	01.2	02	26	02.3	08	02.0	09	02.0	01	02.0	40	02.5	.	.	02	01.5	03	01.7	04
VI	-	14.9	25.0	16.8	18.4	26.2	10.8	32.8	18	04.5	05	12	01.7	10	02.0	09	01.9	08	01.9	24	02.2	02	01.5	03	02.3	05	01.4	17
VII	-	17.2	27.0	19.3	20.7	28.0	13.1	33.2	23	06.5	19	23	02.3	07	02.6	12	01.8	02	01.5	29	02.3	.	.	08	02.1	.	.	12
VIII	-	15.8	28.5	19.2	20.7	29.5	12.5	35.5	08	09.0	24	11	01.9	05	02.6	17	01.7	02	02.0	32	02.4	01	02.0	04	02.0	01	04.0	20
IX	-	11.1	24.7	16.6	17.2	25.5	09.6	34.0	11	-01.0	30	32	02.8	09	02.7	13	01.6	03	01.3	20	01.8	.	.	02	02.0	01	02.0	10
X	-	04.8	17.3	09.3	10.2	18.4	03.5	25.5	09,08	-02.0	26	23	02.7	03	01.7	07	02.7	01	01.0	29	01.9	03	01.7	02	01.5	09	01.9	16
XI	-	02.3	13.4	06.0	06.9	14.0	01.3	21.0	01	-03.5	27,12	31	02.2	06	02.2	14	01.6	01	02.0	24	01.8	02	02.0	03	01.7	03	02.0	06
XII	-	-00.6	05.4	01.3	01.8	06.0	-01.9	14.5	01	-08.5	21	22	02.2	07	02.0	15	01.7	02	01.5	30	01.9	.	.	10	01.9	03	01.0	04
GOD.	-	07.2	16.5	10.3	11.0	17.4	05.2	35.5	8 VIII	-14.0	48 II	284	02.4	95	02.3	123	01.8	50	01.8	337	02.4	16	02.2	43	01.9	44	01.8	103

LAZAROPOLE — BR. ST. 256

MAVROVI ANOVI — BR. ST. 257

OHRID — BR. ST. 258

GOSTIVAR — BR. ST. 259

KIČEVO — BR. ST. 260

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dnev)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dnev)	Min	Padavine R mm Σ	Max	Tmax	Broj dana s: Tn ≤ 10,0	Tn ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 0,0	Tn ≥ 20,0	F (0-12) ≥ 6	≥ 8	Nm (0-10) < 2,0	> 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⚲	✱	≋	≈	▲	▲	⊓ T	≡	▦
BR. ST. 256							**LAZAROPOLE**																														
																																					H_a = 1132 m H_b = 1321,3 m h_a = 2,0 m h_b = 1,5 m
I	7,4	7,6	6,4	7,1	068,5	03,9	88	77	87	84	42	133	057,0	17	05	05	21	.	.	.	03	.	03	15	12	11	04	05	09	.	.	.	.	.	.	04	31
II	8,5	8,2	7,7	8,1	069,0	03,3	85	70	79	78	12	141	039,6	16	04	09	20	.	.	.	11	02	.	15	18	15	05	06	16	01	.	.	.	01	02	.	-
III	6,9	6,5	5,2	6,2	136,7	03,4	77	58	72	69	21	219	052,7	15	03	03	23	.	.	.	.	.	03	11	16	12	05	08	13	02	.	.	.	.	.	.	27
IV	6,9	7,0	6,3	6,7	153,3	04,3	75	52	64	64	14	103	027,6	08	.	01	11	.	.	.	.	.	01	14	17	12	03	13	09	03	.	01	.	.	.	.	-
V	6,2	7,5	6,2	6,6	133,2	05,4	81	54	72	69	19	073	020,1	21	.	.	03	.	.	.	06	.	02	12	17	14	03	15	06	04	.	.	.	.	03	01	.
VI	3,5	6,0	2,4	4,0	229,5	07,1	71	44	67	61	24	045	012,7	30	.	.	.	.	.	.	01	.	07	03	09	06	02	09	01	01	.	.	.	.	07	.	.
VII	3,5	5,9	3,6	4,3	261,1	09,0	77	52	77	69	23	086	016,0	04	.	.	.	03	.	.	02	.	08	04	13	11	04	12	01	.	.	.	01	.	10	.	.
VIII	2,5	5,9	2,7	3,7	276,5	08,7	80	48	73	67	27	062	027,1	03	.	.	.	05	.	.	02	.	10	02	12	07	02	12	.	.	.	.	.	.	07	.	.
IX	3,6	4,6	2,8	3,7	-	06,7	80	61	68	63	15	021	015,9	01	.	.	02	09	.	.	.	.	11	03	03	02	01	03	.	.	.	.	.	.	01	.	.
X	4,7	4,9	4,1	4,6	179,4	05,1	87	52	79	73	20	163	058,0	23	.	.	05	.	.	.	03	.	13	10	10	08	06	10	03	02	.	.	.	.	01	.	03
XI	5,1	5,4	3,9	4,8	147,0	04,0	68	53	71	64	11	116	022,2	11	.	.	11	.	.	.	04	.	09	07	12	09	06	10	04	01	.	.	.	.	01	.	-
XII	5,6	6,1	4,9	5,5	-	03,3	78	60	73	71	20	159	077,8	31	02	03	24	.	.	.	04	.	08	11	14	09	05	06	10	02	.	.	.	.	01	01	-
GOD.	5,4	6,3	4,7	5,4	-	05,4	78	55	73	69	11	1321	077,8	31 XII	14	21	120	13	.	.	36	02	75	107	153	116	46	109	72	16	.	01	01	01	33	06	-
BR. ST. 257							**NAVROVI ANOVI**																														
																																					H_a = 1240 m H_b = - m h_a = 2,1 m h_b = 1,6 m
I	6,9	7,1	7,7	7,2	078,5	03,8	88	74	88	84	47	196	066,4	17	07	09	21	.	.	.	.	.	01	11	15	14	06	08	11	04	.	.	.	.	.	08	31
II	7,8	7,0	6,6	7,1	097,3	03,3	82	64	78	75	-	222	038,8	16	04	10	18	.	.	.	06	01	.	08	20	18	08	10	13	03	.	.	.	.	.	06	24
III	6,6	5,9	5,6	6,0	164,7	03,6	76	65	73	71	33	209	047,6	15	01	03	22	.	.	.	.	02	03	08	13	12	06	08	10	05	.	.	.	.	01	09	27
IV	6,5	6,2	5,8	6,2	183,7	04,6	70	57	67	65	26	193	027,6	12	.	01	09	.	.	.	02	01	.	09	14	14	05	10	06	01	.	.	.	.	.	01	04
V	6,1	6,5	6,1	6,2	174,7	05,5	73	57	72	67	29	092	024,6	21	.	.	03	.	.	.	04	.	01	07	20	19	02	19	06	05	.	.	.	01	04	02	02
VI	3,6	5,9	4,3	4,6	240,9	-	-	-	-	-	-	060	014,6	01	.	.	.	01	.	.	.	.	04	03	11	09	02	11	01	01	.	.	.	01	05	.	.
VII	3,9	5,4	4,4	4,6	281,6	08,9	71	58	73	67	32	119	038,0	15	.	.	.	01	.	.	01	.	03	03	12	09	04	12	.	.	.	.	.	.	08	01	.
VIII	2,6	4,7	3,4	3,6	297,9	08,6	68	49	67	62	31	042	025,8	17	.	.	.	05	.	.	02	.	09	02	06	05	01	06	01	.	.	.	.	01	04	.	.
IX	3,8	4,1	3,2	3,7	238,6	07,4	75	55	72	67	32	018	011,8	01	.	.	01	03	.	.	.	.	08	03	05	05	01	05	.	.	.	.	.	.	.	02	.
X	4,8	4,7	3,8	4,5	192,4	-	-	-	-	-	-	136	048,6	23	.	.	05	.	.	.	04	.	12	07	10	10	04	07	04	01	.	.	.	.	01	04	05
XI	4,9	4,8	4,1	4,6	144,9	-	-	-	-	-	-	120	024,0	10	.	.	11	.	.	.	01	.	09	06	11	10	04	10	06	03	.	.	.	.	.	02	-
XII	6,9	5,1	5,2	5,8	120,2	03,4	79	64	75	73	27	129	034,3	31	.	02	24	.	.	.	01	01	03	07	11	10	04	06	07	02	.	.	.	.	.	03	10
GOD.	5,4	5,6	5,0	5,3	2215,4	-	-	-	-	-	-	1476	066,4	17 I	12	21	114	18	.	.	21	05	53	74	148	135	47	112	65	25	.	.	.	03	23	34	-
BR. ST. 258							**OHRID**																														
																																					H_a = 760 m H_b = 760,6 m h_a = 2,0 m h_b = 1,4 m
I	9,2	8,2	7,8	8,4	051,5	05,2	87	77	88	84	41	124	036,2	17	.	01	11	.	.	.	03	02	.	22	16	12	04	14	04	02	.	.	.	.	02	01	.
II	8,3	7,5	6,5	7,4	081,7	04,6	83	70	77	76	43	099	015,5	16	01	.	14	.	.	.	06	03	01	13	22	14	05	14	13	04	01	.	.	.	04	.	04
III	6,7	6,6	5,1	6,2	166,6	04,8	76	58	71	69	24	097	022,9	15	.	.	10	.	.	.	05	01	04	11	13	08	05	11	02	.	.	.	.	.	01	.	01
IV	7,0	6,6	5,4	6,4	182,1	04,5	78	57	72	69	34	066	015,5	13	.	.	02	.	.	.	05	02	02	11	12	11	01	12	02	02	.	.	.	.	01	01	.
V	6,3	7,3	4,5	6,0	195,9	07,6	81	58	76	72	38	051	014,1	01	.	.	.	01	.	.	.	.	-	-	15	08	02	15	.	.	.	.	.	.	04	.	.
VI	3,2	5,4	2,3	3,7	285,2	10,5	78	53	69	67	35	023	006,3	21	.	.	.	15	.	.	.	.	08	02	10	06	.	10	.	.	.	.	.	.	09	01	.
VII	2,8	4,6	2,6	3,3	299,9	11,7	76	51	69	65	32	026	009,2	18	.	.	.	22	03	.	01	01	14	02	10	06	.	10	.	.	.	.	.	.	11	.	.
VIII	2,3	4,0	1,9	2,7	294,3	11,1	74	45	65	61	32	018	009,1	12	.	.	.	24	05	.	.	.	13	02	05	04	.	05	.	.	.	.	.	.	08	.	.
IX	2,8	3,3	1,9	2,6	248,0	09,0	71	44	63	60	23	020	011,7	01	.	.	.	13	.	.	.	.	17	02	05	04	01	05	.	.	.	.	.	.	02	.	.
X	4,3	4,7	2,9	4,0	186,4	07,0	84	59	74	72	41	080	027,7	23	.	.	.	.	.	.	01	.	12	04	09	08	03	09	.	.	.	.	.	.	02	.	.
XI	5,1	5,1	3,4	4,5	149,9	06,0	84	65	79	76	42	079	016,2	09	.	.	03	.	.	.	.	.	08	05	12	09	04	12	.	.	.	.	.	.	01	.	.
XII	6,2	5,9	4,6	5,6	108,3	04,7	83	69	79	77	40	055	016,9	03	.	.	17	.	.	.	05	02	06	10	14	08	02	12	02	.	.	.	.	.	02	01	01
GOD.	5,4	5,8	4,1	5,1	2249,8	07,4	79	58	73	70	23	738	036,2	17 I	01	01	57	75	08	.	26	11	-	-	143	98	27	129	23	08	01	.	.	.	47	04	11
BR. ST. 259							**GOSTIVAR**																														
																																					H_a = 525 m H_b = - m h_a = 2,1 m h_b = 1,5 m
I	9,2	8,8	8,7	8,9	-	04,4	82	84	85	83	60	142	045,0	17	.	05	18	.	.	.	01	.	.	24	15	15	06	10	06	.	.	.	.	.	.	07	10
II	8,0	6,9	6,6	7,2	-	04,8	80	81	81	81	31	126	022,0	16	04	01	17	.	.	.	05	01	.	08	15	15	07	10	07	01	.	.	.	.	.	04	16
III	5,0	3,8	3,6	4,3	-	05,4	80	69	75	75	28	144	042,0	15	.	.	10	.	.	.	-	-	-	-	14	14	05	08	10	04	.	.	.	.	.	01	06
IV	5,8	6,2	4,5	5,5	-	06,7	76	55	70	67	30	076	022,0	12	.	.	01	04	.	.	06	01	-	-	11	10	03	10	01	.	.	.	.	.	.	.	.
V	6,0	7,3	5,4	6,2	-	08,3	74	60	76	70	43	058	019,0	29	.	.	01	03	.	.	.	02	01	07	11	09	02	11	.	.	.	.	.	.	01	.	.
VI	3,9	6,5	4,1	4,8	-	11,0	72	52	69	65	30	026	010,0	21	.	.	.	22	03	.	.	.	03	03	10	07	01	10	.	.	.	.	.	.	.	.	.
VII	3,9	5,6	4,2	4,6	-	13,4	76	66	76	73	-	089	034,6	06	-	-	-	-	-	-	.	.	10	03	09	09	03	09	.	.	.	.	.	.	03	.	.
VIII	2,5	5,5	2,7	3,5	-	-	-	-	-	-	-	.	000,0	12	.	.	.	24	05	.	.	.	10	01	.	.	.	.	.	.	.	.	.	.	.	.	.
IX	3,4	3,9	2,8	3,4	-	10,2	83	58	81	74	38	014	009,0	01	.	.	01	10	01	.	.	.	11	02	02	02	.	02	.	.	.	.	.	.	.	.	.
X	4,7	4,5	4,2	4,5	-	06,9	79	65	81	75	45	101	035,0	23	.	.	06	.	.	.	01	.	14	09	11	08	04	11	02	.	.	.	.	.	.	.	02
XI	5,2	5,0	4,4	4,8	-	05,2	82	60	82	75	33	049	015,0	17	.	.	13	.	.	.	.	.	10	09	08	07	03	08	.	.	.	.	.	.	.	03	.
XII	6,2	5,8	5,3	5,8	-	04,2	82	77	81	80	46	090	022,0	29	.	.	27	.	.	.	.	.	06	14	10	10	03	08	02	.	.	.	.	.	.	06	02
GOD.	5,3	5,8	4,7	5,3	-	-	-	-	-	-	-	915	045,0	17 I	-	-	-	-	-	-	-	-	-	-	116	106	37	97	28	05	.	.	.	.	04	21	36
BR. ST. 260							**KIČEVO**																														
																																					H_a = 620 m H_b = - m h_a = 2,1 m h_b = 1,5 m
I	9,0	8,4	8,1	8,5	-	05,0	92	83	88	87	47	129	040,0	17	.	02	14	.	.	.	.	.	01	23	13	10	04	10	05	02	.	.	.	.	.	16	-
II	7,9	7,8	6,6	7,4	-	04,5	81	67	79	76	38	103	026,9	16	02	01	12	.	.	.	02	01	.	12	19	12	03	13	11	03	.	.	.	.	01	05	-
III	7,2	6,9	4,5	6,2	-	04,9	85	51	74	70	21	147	052,8	15	.	.	10	.	.	.	04	01	04	11	12	09	04	10	03	01	.	.	.	.	.	04	02
IV	7,2	6,6	5,0	6,3	-	06,4	82	45	70	66	18	076	022,1	08	.	.	05	04	.	.	03	.	02	11	11	08	03	11	.	.	.	.	.	.	.	.	.
V	7,0	7,3	6,5	6,9	-	07,4	83	45	74	67	26	044	018,8	21	.	.	.	04	.	.	03	01	04	16	14	09	01	14	.	.	.	.	.	.	05	04	.
VI	2,9	6,2	2,8	4,0	-	10,3	75	45	76	65	28	026	008,6	04	.	.	.	22	05	.	.	.	07	04	08	07	.	08	.	.	.	.	.	.	07	.	.
VII	3,7	4,7	3,4	3,9	-	11,9	77	45	73	65	31	088	050,0	06	.	.	.	25	11	.	.	.	11	04	09	09	02	09	.	.	.	.	.	.	07	.	.
VIII	2,7	4,9	2,5	3,4	-	10,7	78	36	67	61	24	017	011,4	03	.	.	.	27	16	.	.	.	14	03	05	04	01	05	.	.	.	.	.	.	05	03	.
IX	3,5	3,6	3,8	3,6	-	09,1	86	40	65	63	20	018	011,4	01	.	.	01	17	09	.	01	.	12	04	03	03	01	03	.	.	.	.	.	.	02	02	.
X	6,5	4,8	4,0	5,1	-	06,8	90	52	80	74	29	099	023,5	23	.	.	02	02	.	.	01	.	08	07	08	08	05	08	02	02	.	.	.	.	01	12	01
XI	5,0	5,0	3,8	4,6	-	05,6	90	52	83	75	28	051	015,0	11	.	.	07	.	.	.	02	.	07	04	10	07	02	10	.	.	.	.	.	.	.	03	.
XII	7,2	6,2	5,4	6,3	-	04,5	88	71	88	82	37	061	015,2	31	.	01	22	.	.	.	.	.	04	11	13	09	03	09	05	.	.	.	.	.	01	06	05
GOD.	5,8	6,0	4,7	5,5	-	07,3	83	52	76	70	18	859	042,8	45 III	02	04	73	101	41	.	16	03	74	110	125	95	29	110	26	08	.	.	.	.	29	55	-

Mesec	Vazdušni pritisak Pm mb	Temperatura vazduha °C Tm 7	14	21	Sred. (Dnev)	Max	Min	Amp	Ext.	Min	Ext.	Učestalost pravaca i srednja jačina vetra nD, Fm (0-12) N		NE		E		SE		S		SW		W		NW		C
												n.	f.	n.	f.	n.	f.	n.	f.	n.	f.	n.	f.		f.	n.	f.	n.
RESEN — φ = 41° 05' N λ = 21° 01' E Gr. Δ G = + 1h 24 min. — BR. ST. 261																												
I	-	01.6	04.8	02.4	02.8	05.9	00.0	14.3	07	-08.0	21	07	01.4	01	02.0	11	03.3	05	01.8	08	02.2	09	02.1	10	02.1	01	02.0	41
II	-	00.8	04.8	02.0	02.4	06.1	-01.5	12.6	08	-17.0	18	03	01.3	04	02.2	08	02.4	06	02.3	10	03.4	26	03.3	02	03.0	04	01.5	21
III	-	01.8	08.1	04.0	04.5	09.5	00.1	22.2	27	-05.2	03,02	10	01.6	09	02.0	10	02.4	01	01.0	15	03.9	14	03.1	10	02.6	03	01.7	21
IV	-	07.1	13.6	08.4	09.4	15.0	04.0	23.7	24	-03.5	07	09	01.8	03	01.0	06	02.2	01	02.0	12	02.8	13	02.4	15	02.9	02	04.0	29
V	-	09.6	14.9	10.0	11.1	16.4	05.8	25.0	11	00.2	02	09	01.9	03	02.0	10	03.3	03	02.7	10	02.2	11	02.3	08	02.1	04	02.0	35
VI	-	15.5	22.3	15.2	17.0	23.2	09.4	29.2	18	02.0	05	07	02.4	07	02.1	05	02.0	01	01.0	04	01.2	09	02.0	11	02.5	02	02.5	44
VII	-	17.0	23.9	16.8	18.6	24.9	11.4	30.0	23	03.2	19	10	01.5	11	02.5	09	02.6	03	02.0	05	02.4	06	02.2	06	01.5	07	01.6	36
VIII	-	16.5	25.1	17.3	19.0	26.2	10.5	32.5	09	06.2	24	05	02.0	02	01.0	03	02.0	03	02.0	06	01.8	10	01.3	05	02.0	08	01.5	51
IX	-	12.3	21.9	13.9	15.5	22.6	07.8	29.8	11	-05.4	30	04	01.5	07	02.1	13	03.0	06	01.8	05	02.2	06	01.3	06	01.7	04	01.0	39
X	-	05.4	14.6	07.7	08.8	15.7	03.9	22.0	08	-01.2	26	05	01.4	09	02.0	05	03.8	09	02.9	15	02.6	16	02.4	02	02.5	05	01.4	27
XI	-	02.5	11.5	04.9	05.9	12.8	00.7	20.6	04	-04.2	13,12	08	02.6	07	01.9	04	05.0	03	01.7	03	01.3	18	01.9	03	03.0	02	02.0	42
XII	-	00.0	05.6	01.1	01.9	06.5	-02.3	14.7	01	-09.0	18	06	01.5	03	02.0	12	03.5	05	01.6	08	03.0	15	01.9	05	02.6	05	01.2	34
GOD.	-	07.5	14.3	08.6	09.7	15.4	04.2	32.5	9 VIII	-17.0	18 II	83	01.8	66	02.0	96	03.0	46	02.1	101	02.7	153	02.3	83	02.4	47	01.7	420
MAKEDONSKI BROD — φ = 41° 31' N λ = 21° 13' E Gr. Δ G = + 1h 25 min. — BR. ST. 262																												
I	-	02.1	06.0	03.1	03.5	06.4	00.7	16.2	07	-10.2	21	04	02.0	.	.	.	.	01	02.0	08	02.5	.	.	.	.	.	.	NO
II	-	01.4	07.6	03.7	04.1	08.0	-00.4	16.8	06	-10.5	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	04.0	11.6	05.9	06.8	12.2	00.8	22.6	27	-06.5	03	04	03.0	.	.	.	.	01	04.0	11	02.5	.	.	.	.	01	04.0	76
IV	-	07.3	16.9	09.8	11.0	17.2	03.9	26.2	27,24	-04.2	05	05	02.0	.	.	01	02.0	03	02.7	06	02.0	03	02.7	.	.	.	.	72
V	-	09.5	18.1	12.2	13.0	18.8	06.4	27.2	11	01.0	25	04	02.0	.	.	01	02.0	05	02.4	15	03.3	.	.	02	02.0	.	.	66
VI	-	13.6	24.8	15.6	17.4	25.4	09.6	31.5	18	03.8	05	.	.	.	.	01	02.0	02	02.0	08	02.5	03	02.7	01	02.0	01	06.0	74
VII	-	17.2	27.6	17.8	20.1	28.1	12.5	33.8	26	05.0	19	04	02.0	.	.	.	.	02	03.0	13	02.3	01	02.0	.	.	.	.	73
VIII	-	17.5	29.9	18.6	21.2	30.2	10.8	35.2	08	04.8	28	.	.	.	.	.	.	10	02.2	13	02.6	.	.	.	.	.	.	73
IX	-	12.8	25.2	15.0	17.0	25.3	07.6	34.4	11	-04.0	30	02	03.0	.	.	.	.	03	02.7	06	02.3	03	02.7	.	.	02	03.0	74
X	-	05.8	17.6	07.9	09.8	17.9	02.2	24.8	09	-04.0	01	06	02.3	.	.	.	.	13	02.2	04	02.0	01	02.0	.	.	.	.	69
XI	-	02.7	13.6	05.0	06.6	13.7	-00.2	20.2	03	-05.5	29,28	02	02.0	01	02.0	.	.	03	02.0	05	02.4	.	.	.	.	01	04.0	78
XII	-	-01.2	06.2	00.1	01.3	06.5	-03.6	16.0	01	-11.0	21	04	03.0	01	04.0	01	02.0	03	02.0	11	02.2	.	.	.	.	.	.	73
GOD.	-	07.7	17.1	09.6	11.0	17.5	04.2	35.2	8 VIII	-11.0	21 XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
KRUŠEVO — φ = 41° 22' N λ = 21° 15' E Gr. Δ G = + 1h 25 min. — BR. ST. 263																												
I	-	-00.8	01.2	-00.1	00.0	02.7	-02.2	11.7	07	-11.0	21	02	01.5	10	01.4	08	01.2	05	01.2	05	02.2	05	04.2	19	02.7	04	01.5	35
II	-	-01.0	01.2	-00.3	-00.1	02.6	-02.6	09.5	06	-12.0	18	09	02.1	05	01.0	02	01.0	04	01.2	06	03.0	20	02.8	25	03.0	02	01.5	11
III	-	01.1	04.2	02.5	02.6	05.7	-00.3	16.7	27	-10.0	02	10	03.2	05	02.6	10	01.1	12	01.3	12	02.3	08	02.8	22	02.1	.	.	14
IV	-	06.8	10.3	07.3	07.9	11.4	04.4	20.7	25	-03.7	05	13	01.8	05	02.4	05	01.2	07	01.6	11	02.1	22	02.7	15	02.6	04	01.5	08
V	-	08.1	11.2	08.6	09.1	12.3	05.9	21.0	11	-01.2	03	14	02.1	09	01.3	10	01.3	08	01.5	03	01.3	07	01.6	18	03.2	06	02.2	18
VI	-	15.0	18.2	15.3	16.0	19.4	12.0	25.8	18	02.4	03	09	01.8	16	01.1	14	01.1	04	01.2	04	01.8	10	01.6	06	02.3	11	01.9	16
VII	-	16.2	20.1	16.7	17.4	21.2	13.3	26.5	23	06.7	19	08	01.5	28	01.6	11	01.3	03	01.7	04	02.8	11	02.9	10	02.6	05	02.2	13
VIII	-	17.1	21.8	17.4	18.4	22.5	14.2	29.4	08	08.0	27	07	01.6	17	01.7	08	01.4	08	01.5	04	02.8	05	04.0	11	02.6	06	03.0	27
IX	-	13.0	17.7	14.0	14.7	18.3	10.7	26.4	11	-00.2	30	10	02.2	21	01.8	14	01.6	13	02.3	.	.	02	02.5	02	02.5	04	02.2	24
X	-	07.1	10.7	08.1	08.5	11.8	04.8	17.5	31	-02.6	25	09	02.8	16	01.4	12	01.2	07	02.3	06	02.8	03	03.0	14	02.8	08	02.1	18
XI	-	05.2	09.0	05.9	06.5	09.8	03.1	17.5	03	-03.2	12	16	02.8	04	01.9	05	01.2	02	02.0	07	02.0	11	03.1	26	03.6	03	02.7	16
XII	-	-00.2	01.9	00.6	00.7	03.7	-01.6	11.7	01	-08.5	17	15	02.5	10	01.5	11	01.1	02	03.0	10	02.9	08	03.1	10	03.1	01	02.0	26
GOD.	-	07.3	10.6	08.0	08.5	11.8	05.1	29.4	8 VIII	-12.0	18 II	122	02.3	146	01.6	110	01.2	75	01.7	72	02.4	112	02.8	178	02.8	54	02.1	226
BITOLA — φ = 41° 03' N λ = 21° 22' E Gr. Δ G = + 1h 25 min. — BR. ST. 264																												
I	709.0	02.0	04.7	02.8	03.1	05.5	00.9	17.2	07	-06.8	21	22	01.9	10	01.4	03	01.3	09	02.3	16	02.8	05	02.2	04	03.0	08	02.0	16
II	705.9	01.8	06.3	03.4	03.7	07.9	-00.4	17.2	07	-10.6	18	17	02.6	14	02.3	04	01.2	07	03.3	07	03.4	07	04.3	12	03.4	06	02.3	10
III	707.5	03.3	10.2	06.6	06.7	11.5	01.9	22.2	27	-05.0	03	16	02.4	06	02.3	02	02.0	18	03.2	20	03.8	04	03.0	05	03.4	12	02.2	10
IV	709.0	08.4	16.0	10.9	11.6	17.7	05.8	26.4	28	-02.5	07	17	02.5	09	01.8	04	01.5	14	02.1	17	02.9	05	03.8	05	05.0	09	03.0	10
V	709.1	11.1	17.0	12.8	13.4	18.4	08.1	26.1	16	03.0	04	22	02.1	05	02.4	05	01.6	06	02.7	09	02.7	07	03.3	10	04.6	12	03.8	17
VI	711.3	16.7	24.0	18.1	19.2	25.3	11.5	32.2	18	03.1	05	23	02.0	06	02.3	03	01.3	06	01.8	12	01.5	04	02.2	09	03.4	12	02.4	15
VII	709.7	17.7	25.8	19.7	20.7	26.4	13.2	32.8	23	06.4	19	30	02.1	08	01.2	03	01.3	04	02.2	09	02.0	03	01.3	13	03.0	12	02.4	11
VIII	710.2	17.2	27.2	20.7	21.4	28.8	12.5	35.5	08	06.4	28	17	02.0	10	02.0	05	02.0	08	02.1	09	02.3	03	01.3	10	03.0	11	02.7	20
IX	712.7	12.8	23.7	16.3	17.3	24.8	09.6	32.5	11	-02.4	30	18	02.3	09	01.8	05	02.4	07	01.9	08	01.8	05	01.6	05	01.4	11	02.4	22
X	712.9	04.8	16.1	09.7	10.3	17.6	04.0	24.2	08	-02.6	26	20	02.6	06	02.3	02	01.5	09	02.8	11	03.1	03	01.3	07	02.7	09	02.1	26
XI	712.3	01.7	13.0	05.7	06.5	13.8	00.4	20.5	01	-03.9	28	16	02.2	09	02.2	.	.	11	02.3	05	02.0	08	02.0	06	01.5	11	01.5	24
XII	713.2	-00.1	05.5	01.2	01.9	06.7	-01.9	17.6	01	-10.2	21	18	01.7	09	01.8	04	02.2	06	04.0	10	04.0	07	01.7	01	01.0	10	01.7	28
GOD.	710.2	08.2	15.8	10.7	11.3	17.0	05.5	35.5	8 VIII	-10.6	18 II	236	02.2	101	02.0	40	01.7	105	02.6	133	02.8	61	02.5	87	03.2	123	02.4	209
SKOPJE — = 41° 57' N = 21° 38' E Gr. G = + 1h 27 min. — BR. ST. 265																												
I	741.2	02.1	05.0	02.8	03.2	06.0	01.0	16.7	07	-06.6	25	15	03.2	16	02.8	04	01.2	08	02.6	07	02.4	02	01.0	01	01.0	07	02.0	33
II	737.7	00.5	07.1	03.3	03.5	08.5	-00.7	17.7	10	-10.0	18	13	02.8	10	02.4	03	01.0	05	01.8	06	02.3	09	01.6	11	02.4	07	02.6	20
III	739.0	03.2	12.0	06.9	07.2	13.3	01.8	24.4	27	-06.2	03	18	03.0	12	02.3	04	01.2	19	02.4	09	02.3	04	02.2	06	01.5	07	03.1	14
IV	739.7	09.0	18.4	11.8	12.8	19.8	05.8	29.2	27	-03.7	05	14	03.1	08	02.2	09	01.8	14	02.7	04	02.2	04	02.0	11	02.6	05	02.6	21
V	739.8	12.1	19.5	13.7	14.8	20.7	08.4	28.4	11	-01.0	02	12	02.9	10	02.0	06	02.0	10	02.4	10	01.9	01	02.0	10	03.1	12	02.3	22
VI	741.3	17.7	26.3	20.1	21.0	27.6	12.3	34.0	18	04.6	05	19	02.9	12	02.6	07	01.3	08	01.8	07	02.0	02	01.5	05	02.0	07	02.9	23
VII	739.7	19.3	27.7	21.6	22.5	29.0	15.2	34.6	23	07.6	19	23	03.1	09	02.7	07	01.9	05	02.2	07	02.1	03	02.0	07	02.0	10	02.3	22
VIII	740.0	18.3	29.4	22.4	23.1	30.5	14.6	36.0	08	07.5	28	13	03.2	09	02.7	06	02.0	13	01.8	05	02.2	02	01.0	07	02.3	11	01.9	27
IX	743.3	13.6	25.2	17.3	18.4	26.1	11.3	34.6	11	-00.6	30	24	03.1	15	02.6	03	01.7	02	01.0	01	02.0	07	01.7	05	02.0	11	02.5	22
X	744.0	07.1	17.1	10.5	11.3	18.4	05.5	25.8	09	00.2	01	17	02.8	10	02.6	02	01.5	12	03.0	05	01.8	.	.	10	01.7	04	01.8	32
XI	743.8	02.2	12.1	04.7	05.9	13.0	00.4	20.9	01	-04.3	13	18	03.1	05	02.8	03	01.0	06	01.7	06	01.7	01	01.0	06	01.5	07	01.7	38
XII	745.4	-00.2	05.5	01.5	02.1	06.4	-01.8	13.6	31,26	-10.1	21	18	02.4	04	02.2	06	01.3	08	02.5	05	01.4	04	01.2	05	01.4	10	02.4	33
GOD.	741.2	08.7	17.1	11.4	12.2	18.3	06.2	36.0	8 VIII	-10.1	21 XII	204	03.0	120	02.5	60	01.6	110	02.3	72	02.0	39	01.6	84	02.1	98	02.3	307

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e m	U m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Dat.	Broj dana s a. Tn ≤0.0	Tx ≤0.0	Tn ≤0.0	Tx ≥25.0	Tx ≥30.0	Tn ≥20.0	P(0-12) ≥6	≥8	Nm(0-10) ≤8.0	≥8.0	R mm ≥0.1	≥1.0	≥10.0	●	✱	✱	△	≈	▲	▲	T	≡	▦
BR. ST. 261						**RESEN**																															H_o = 881 m H_b = - m h_o = 1.9 m h_r = 1.7 m
I	8.5	8.1	7.3	8.0	-	05.0	90	80	89	86	51	087	021.0	07	.	02	15	.	.	.	03	.	.	18	11	11	03	10	02	01	01	.	.	.	.	02	02
II	8.1	8.0	6.4	7.5	-	04.5	79	75	84	80	61	103	016.1	17	03	01	15	.	.	.	10	.	.	12	15	13	04	10	09	01	.	.	.	.	01	.	-
III	7.1	6.4	5.0	6.2	-	04.9	86	64	81	77	34	101	020.0	05	.	.	16	.	.	.	05	.	05	13	11	09	05	09	06	03	.	.	.	.	.	.	-
IV	6.5	6.6	5.2	6.1	-	06.7	81	62	78	74	44	068	017.3	08	.	.	04	.	.	.	03	.	04	10	11	10	01	11	01	.	.	.	.	.	01	.	.
V	5.9	7.4	5.2	6.2	-	07.6	81	61	83	75	42	053	020.5	21	.	.	.	01	.	.	.	.	04	09	14	13	01	14	.	.	.	.	.	.	02	.	.
VI	3.4	5.7	3.4	4.2	-	10.7	75	56	81	71	35	026	014.2	21	.	.	.	14	.	.	01	.	09	04	06	04	01	06	.	.	.	.	.	.	08	.	.
VII	3.2	5.1	2.4	3.5	-	11.3	75	53	78	68	33	032	009.4	18	.	.	.	20	01	.	01	.	10	03	07	06	.	07	.	.	.	.	.	.	09	.	.
VIII	2.7	4.3	2.8	3.3	-	10.6	74	46	73	64	21	008	004.4	12	.	.	.	21	04	.	01	.	09	02	03	02	.	03	.	.	.	.	.	.	04	.	.
IX	3.6	3.3	2.3	3.0	-	08.4	75	42	73	63	08	016	016.5	01	.	.	01	12	.	.	.	.	15	04	01	01	01	01	.	.	.	.	.	.	01	.	.
X	4.2	4.8	3.7	4.3	-	06.7	88	58	86	77	40	096	036.0	23	.	.	02	.	.	.	04	.	14	07	08	08	05	08	.	.	.	.	.	.	.	.	.
XI	4.6	5.0	2.7	4.1	-	05.4	87	59	84	77	-	066	013.0	23	.	.	12	.	.	.	02	.	10	03	09	07	03	09	.	.	.	.	.	01	.	.	.
XII	6.5	5.3	4.4	5.4	-	04.5	87	71	88	82	42	044	017.0	31	.	.	23	.	.	.	03	.	08	08	09	07	01	06	04	.	.	.	.	.	01	.	01
GOD.	5.4	5.8	4.2	5.2	-	07.2	81	60	81	74	-	700	036.0	25 X	03	03	88	68	05	.	33	.	88	93	105	91	25	94	22	05	01	.	.	01	27	02	-
BR. ST. 262						**MAKEDONSKI BROD**																															H_o = 545 m H_b = - m h_o = 2.0 m h_r = 1.5 m
I	9.6	9.2	8.3	9.0	-	05.5	93	80	91	88	62	083	026.8	17	01	02	11	.	.	.	.	.	01	26	15	10	03	13	02	.	.	.	.	.	.	03	-
II	8.8	8.3	5.9	7.6	-	05.1	86	67	83	79	-	084	027.0	16	02	.	14	.	.	.	.	01	.	11	17	13	01	11	07	.	.	.	.	.	.	01	10
III	7.3	6.3	5.0	6.2	-	05.5	83	57	80	73	28	116	029.8	15	.	.	10	.	.	.	01	.	03	08	11	10	04	08	03	.	.	.	.	.	.	.	02
IV	7.0	6.7	4.6	6.1	-	06.6	80	48	74	67	30	040	009.5	08	.	.	06	06	.	.	.	.	.	08	08	08	.	07	.	.	.	.	.	.	.	.	.
V	7.2	7.1	6.1	6.8	-	08.0	83	56	76	72	-	049	011.4	29	.	.	.	02	.	.	02	.	05	16	10	10	02	10	.	.	.	.	.	.	01	05	.
VI	4.1	5.5	1.9	3.8	-	10.6	83	49	78	70	34	035	020.2	21	.	.	.	20	02	.	02	.	05	02	04	04	01	04	.	.	.	.	.	.	03	03	.
VII	3.7	4.5	3.0	3.7	-	12.2	79	50	77	68	33	040	009.8	09	.	.	.	25	08	.	.	.	12	04	07	07	.	07	.	.	.	.	.	.	01	03	.
VIII	3.4	4.3	1.6	3.1	-	11.7	75	40	70	62	27	.	.	.	.	.	.	30	20	.	01	.	11	.	.	.	.	.	.	.	.	.	.	.	02	01	.
IX	4.1	3.5	2.6	3.4	-	10.0	85	44	72	67	28	005	004.9	02	.	.	03	18	09	.	.	.	09	02	01	01	.	01	.	.	.	.	.	.	.	02	.
X	7.8	4.6	3.5	5.3	-	07.2	95	56	81	77	34	061	024.4	23	.	.	06	.	.	.	.	.	05	09	06	06	01	06	02	02	.	.	.	.	.	17	01
XI	6.6	5.2	3.2	5.0	-	06.0	93	59	86	79	40	035	016.8	10	.	.	16	.	.	.	.	.	04	06	05	04	01	05	.	.	.	.	.	.	.	07	.
XII	6.5	5.7	4.6	5.6	-	04.5	91	69	92	84	42	048	021.8	31	02	.	24	.	.	.	.	.	07	10	09	09	01	07	02	.	.	.	.	.	01	02	03
GOD.	6.3	5.9	4.2	5.5	-	07.7	85	56	80	73	-	596	029.8	15 VI	05	02	90	101	39	.	06	01	62	102	93	82	14	79	16	02	.	.	.	.	08	44	-
BR. ST. 263						**KRUŠEVO**																															H_o = 1230 m H_b = - m h_o = 2.1 m h_r = 1.7 m
I	8.0	8.8	6.6	7.8	-	04.2	86	85	86	86	48	079	030.0	17	03	08	19	.	.	.	01	.	02	17	11	11	02	05	07	.	.	.	.	.	01	11	14
II	7.2	7.9	5.9	7.0	-	03.7	82	78	80	80	48	074	020.0	08	02	08	18	.	.	.	05	.	.	09	15	14	02	05	13	01	.	.	.	.	.	02	18
III	7.5	7.1	4.2	6.2	-	04.0	76	73	74	74	29	091	023.4	15	01	05	18	.	.	.	01	.	03	09	12	12	04	07	07	.	.	.	.	.	.	05	17
IV	7.2	6.9	4.5	6.2	-	05.2	72	60	70	67	29	056	013.4	13	.	.	07	.	.	.	.	.	.	10	15	10	03	10	06	.	.	.	.	.	.	.	01
V	5.9	7.2	5.5	6.2	-	06.6	77	70	77	75	38	082	018.6	01	.	.	02	.	.	.	01	.	02	11	19	14	02	17	02	.	.	.	01	01	08	01	.
VI	3.3	6.2	3.5	4.3	-	09.1	70	63	67	66	35	052	022.1	13	.	.	.	01	.	.	.	.	06	03	11	08	01	11	.	.	.	.	.	.	11	01	.
VII	3.4	5.4	3.4	4.1	-	10.2	73	61	68	67	39	046	008.3	07	.	.	.	02	.	.	01	.	08	03	09	09	.	09	.	.	.	.	.	.	14	02	.
VIII	2.5	5.6	2.2	3.5	-	08.9	61	46	60	56	32	012	005.5	25	.	.	.	09	.	01	01	.	07	02	05	04	.	05	.	.	.	.	.	.	06	.	.
IX	3.7	4.2	3.6	3.8	-	07.4	66	49	60	58	26	005	003.0	01	.	.	01	04	.	.	.	.	12	04	05	01	.	05	.	.	.	.	.	.	03	01	.
X	5.0	5.4	3.8	4.7	-	06.0	77	68	73	73	40	100	030.1	23	.	.	04	.	.	.	01	.	10	06	10	09	03	09	04	.	.	.	.	.	01	04	02
XI	5.1	5.3	2.4	4.3	-	04.8	71	62	69	67	25	040	008.5	17	.	.	08	.	.	.	04	.	07	04	09	07	.	08	03	.	.	.	.	.	.	01	-
XII	6.7	6.5	4.9	6.0	-	03.9	80	78	79	79	32	065	031.4	31	.	05	22	.	.	.	02	.	04	10	12	08	02	09	05	.	.	.	.	.	01	07	16
GOD.	5.5	6.4	4.2	5.3	-	06.2	74	66	71	70	25	702	031.4	31 XII	06	26	99	16	.	01	17	.	61	88	133	107	19	100	47	01	.	.	01	01	45	35	-
BR. ST. 264						**BITOLA**																															H_o = 586 m H_b = 588.6 m h_o = 2.0 m h_r = 1.6 m
I	9.2	8.7	7.8	8.6	044.4	05.0	89	78	87	85	41	056	020.9	02	.	04	13	.	.	.	11	03	02	23	14	11	01	12	05	03	.	.	.	.	.	06	02
II	6.6	7.8	5.8	6.7	104.0	04.0	76	59	72	69	27	064	015.8	16	01	03	13	.	.	.	17	07	.	08	15	10	02	10	10	02	.	.	.	.	.	03	07
III	7.0	6.9	4.8	6.2	166.6	04.6	78	51	67	65	27	065	019.3	05	.	.	10	.	.	.	17	09	02	09	12	09	02	11	03	02	.	.	01	.	.	.	02
IV	6.3	6.8	5.2	6.1	196.0	06.4	78	47	65	63	27	026	010.2	13	.	.	02	06	.	.	22	05	01	09	10	07	01	10	.	.	.	.	.	.	.	.	.
V	6.0	7.2	6.1	6.5	211.3	07.5	77	52	68	66	28	076	021.3	01	.	.	.	03	.	.	17	02	03	09	15	10	03	15	.	.	.	.	.	.	09	.	.
VI	3.0	5.5	3.8	4.1	301.5	10.0	73	43	65	60	23	040	024.1	21	.	.	.	22	02	.	14	01	05	03	09	06	01	09	.	.	.	.	.	.	06	.	.
VII	3.9	4.8	4.1	4.3	312.2	11.3	76	45	66	62	27	114	046.3	06	.	.	.	24	08	.	11	03	07	03	10	07	04	10	.	.	.	.	.	02	12	.	.
VIII	2.4	4.4	2.1	2.9	321.3	10.1	73	36	55	55	22	005	002.4	04	.	.	.	26	13	.	14	03	11	01	05	03	.	05	.	.	.	.	.	.	07	.	.
IX	3.7	3.7	3.7	3.7	255.3	08.1	75	35	56	56	21	008	006.3	01	.	.	01	16	06	.	04	.	12	03	02	02	.	02	.	.	.	.	.	.	02	.	.
X	4.8	4.9	3.6	4.4	201.2	06.6	90	51	75	72	28	069	015.0	04	.	.	04	.	.	.	12	01	10	06	11	08	03	11	.	.	.	.	.	.	02	04	.
XI	4.2	4.9	3.0	4.0	167.7	05.2	91	49	78	72	-	023	008.4	11	.	.	17	.	.	.	09	03	10	02	08	06	.	08	.	.	.	.	.	.	.	01	.
XII	5.9	6.1	4.5	5.5	112.0	04.4	87	68	86	80	37	038	021.7	31	01	.	23	.	.	.	07	03	06	08	09	06	01	06	05	01	.	.	.	.	01	03	-
GOD.	5.2	6.0	4.5	5.2	2393.5	06.9	80	51	70	67	-	584	046.3	6 VII	02	07	83	97	29	.	159	40	69	84	120	85	18	109	23	08	.	.	01	02	39	17	-
BR. ST. 265						**SKOPJE**																															H_o = 232 m H_b = 233.3 m h_o = 2.0 m h_r = 1.3 m
I	9.8	9.1	8.1	9.0	031.6	05.1	86	76	86	83	51	035	016.5	17	.	04	10	.	.	.	09	.	.	24	11	06	01	09	03	.	.	.	.	.	.	05	01
II	8.2	7.6	5.2	7.0	084.9	04.4	87	57	76	74	35	041	012.3	08	01	.	18	.	.	.	11	01	.	08	13	08	01	10	04	.	.	.	.	.	.	05	-
III	7.0	6.6	4.8	6.1	151.9	05.0	82	49	67	66	25	026	010.4	05	.	.	07	.	.	.	18	01	02	11	10	04	01	10	.	.	.	.	.	.	01	.	.
IV	7.0	6.9	4.5	6.1	175.7	06.7	77	44	62	61	18	016	008.9	13	.	.	02	06	.	.	18	01	01	08	07	03	.	07	.	.	.	.	.	.	01	.	.
V	6.5	7.1	6.0	6.5	173.3	08.1	77	47	70	65	24	058	016.0	21	.	.	01	06	.	.	14	02	03	11	13	11	03	13	.	.	.	.	.	.	05	.	.
VI	2.7	5.8	4.0	4.2	252.5	10.8	73	40	63	59	28	007	003.0	20	.	.	.	23	12	.	15	01	03	02	07	02	.	07	.	.	.	.	.	.	07	.	.
VII	3.0	4.2	4.2	3.8	296.1	12.1	75	43	64	61	23	092	036.0	18	.	.	.	25	17	.	18	02	10	03	09	07	05	09	.	.	.	.	.	.	12	.	.
VIII	2.5	4.5	2.4	3.1	296.2	11.3	73	36	56	55	25	003	002.6	25	.	.	.	26	21	.	16	03	13	02	05	01	.	04	.	.	.	.	.	.	08	.	.
IX	2.4	3.6	2.4	2.8	247.2	08.8	74	36	57	56	17	018	012.8	01	.	.	01	19	07	.	16	03	14	01	03	03	01	03	.	.	.	.	.	.	01	.	.
X	5.5	4.7	4.4	4.9	174.0	07.2	88	52	77	72	28	061	012.4	23	.	.	.	02	.	.	10	.	10	10	08	07	03	08	01	01	.	.	.	.	.	01	.
XI	5.8	4.8	4.0	4.9	136.8	05.9	90	58	83	77	32	009	002.5	11	.	.	14	.	.	.	10	.	09	07	06	03	.	06	.	.	.	.	.	.	.	07	.
XII	6.6	6.5	5.5	6.2	075.9	04.6	89	71	87	82	33	025	009.7	02	01	01	20	.	.	.	11	.	04	12	10	07	.	08	02	.	01	.	.	.	.	11	03
GOD.	5.6	6.0	4.6	5.4	2096.1	07.5	80	50	70	67	17	391	036.0	18 VII	02	05	73	109	57	.	166	14	69	99	102	62	15	94	10	01	01	.	.	.	35	29	-

Mesec	Vazdušni pritisak Pm mm	Temperatura vazduha °C: Tm 7	Tm 14	Tm 21	Tm Sred. (Tsis)	Tmax	Tmin	Tmax	Dat.	Tmin	Dat.	Učestina pravaca i srednja jačina vetra m/s, Fm (0-12): N F.	N J.	NE F.	NE J.	E F.	E J.	SE F.	SE J.	S F.	S J.	SW F.	SW J.	W F.	W J.	NW F.	NW J.	C F.
φ = 41° 59' N λ = 21° 31' E Gr. Δ G = + 1h 26 min. TRUBAREVO BR. ST. 266																												
I	-	02.0	05.0	03.1	03.3	09.7	01.1	16.0	07	-05.5	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	01.0	07.1	03.8	04.0	08.0	-00.3	17.7	10	-08.0	18	20	01.1	01	02.0	22	01.0	07	01.1	.	.	10	01.3	05	01.2	17	02.0	02
III	-	03.4	12.0	07.3	07.5	12.6	02.1	23.5	27	-04.5	03	21	01.1	01	01.0	25	01.0	22	01.2	01	01.0	03	01.0	03	01.0	11	01.7	06
IV	-	08.7	18.3	12.9	13.2	19.4	06.1	28.6	27	-02.2	05	10	01.1	.	.	27	01.0	14	01.1	04	01.0	10	01.8	09	01.8	09	01.7	07
V	-	12.2	19.8	14.8	15.4	20.7	09.4	28.0	11	00.5	02	08	01.4	.	.	16	01.0	22	01.2	03	01.0	14	01.6	08	01.4	12	02.0	10
VI	-	17.8	26.6	20.3	21.2	27.8	12.9	34.0	18	06.5	04,05	02	01.0	.	.	11	01.0	26	01.1	09	01.0	22	01.0	09	01.1	03	01.0	08
VII	-	19.1	28.1	22.3	23.0	29.4	15.5	35.2	23	08.4	19	.	.	01	01.0	15	01.0	29	01.2	05	01.0	20	01.2	13	01.2	04	01.5	06
VIII	-	18.0	29.5	22.2	23.0	30.4	14.4	36.2	08	07.5	28	03	01.0	02	01.0	12	01.1	26	01.1	07	01.0	07	01.3	02	01.5	13	01.4	21
IX	-	12.1	25.3	15.6	17.1	26.4	10.2	34.0	12	-01.5	30	05	01.0	02	01.0	02	01.0	09	01.1	12	01.0	26	01.2	07	01.0	04	01.0	23
X	-	06.4	17.5	09.3	10.6	19.1	04.3	26.4	09	-01.0	01	01	01.0	04	01.0	03	01.0	06	01.0	16	01.0	28	01.0	11	01.3	04	01.0	20
XI	-	01.9	12.6	04.2	05.7	13.9	-00.1	23.0	04	-04.0	29,12	04	01.0	10	01.0	01	01.0	06	01.2	11	01.0	24	01.0	06	01.0	04	01.8	24
XII	-	-00.4	06.0	01.5	02.2	07.3	-02.0	15.0	26	-09.0	21	02	01.0	04	01.0	.	.	11	01.1	18	01.0	26	01.0	07	01.0	07	01.7	18
GOD.	-	08.5	17.3	11.4	12.2	18.4	06.1	36.2	8 VIII	-09.0	21 XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 41° 20' N λ = 21° 34' E Gr. Δ G = + 1h 26 min. PRILEP BR. ST. 267																												
I	701.9	01.4	04.1	02.3	02.5	05.3	00.3	17.2	07	-08.4	21	05	03.8	15	02.8	.	.	.	.	13	03.5	04	01.5	02	01.0	01	01.0	53
II	699.0	01.8	05.8	02.9	03.4	07.1	00.3	15.7	06	-10.0	18	05	02.8	18	03.6	01	01.0	.	.	21	03.9	17	03.4	03	01.3	.	.	19
III	700.5	03.2	09.7	06.0	06.2	11.1	02.1	22.7	27	-05.5	02	06	03.7	20	03.4	01	01.0	.	.	24	03.7	11	02.5	03	02.0	02	01.0	26
IV	702.0	09.0	15.8	10.9	11.7	17.6	06.5	26.5	24	-01.5	07	04	03.5	13	03.2	.	.	.	.	24	03.0	14	03.3	04	02.2	.	.	31
V	702.2	10.9	16.5	12.1	12.9	18.1	08.0	26.6	11	02.3	02	08	02.6	19	02.5	01	01.0	02	04.0	11	02.9	19	02.2	03	01.7	.	.	30
VI	704.4	16.8	23.7	18.2	19.2	25.2	12.9	32.8	18	-	-	05	02.0	27	02.4	01	03.0	02	02.5	04	02.0	06	01.5	07	02.3	.	.	38
VII	703.0	17.9	25.6	19.9	20.8	27.1	14.6	32.4	23	06.2	19	05	02.6	39	02.4	.	.	.	.	05	03.6	13	02.0	01	01.0	03	02.0	27
VIII	703.5	18.2	27.3	21.1	21.9	28.7	14.9	35.6	08	09.1	28	04	01.8	31	02.2	.	.	.	.	05	02.6	11	02.1	06	02.0	02	02.5	34
IX	705.9	14.0	23.2	17.2	17.9	24.4	11.9	32.9	13,11	00.7	30	17	03.1	35	02.8	.	.	01	01.0	.	.	06	02.0	03	01.7	.	.	28
X	705.8	06.8	15.6	10.1	10.7	16.9	05.5	24.3	08	-01.8	26	09	03.0	18	02.6	01	01.0	.	.	08	04.0	09	01.8	01	01.0	01	01.0	45
XI	705.2	03.8	12.4	06.6	07.3	13.4	02.3	20.7	01	-02.6	12	06	03.7	16	03.1	01	01.0	.	.	05	03.2	09	02.4	05	01.6	02	03.0	46
XII	706.1	00.3	05.6	01.8	02.4	06.8	-00.8	18.1	01	-07.9	21	07	02.3	15	02.0	01	01.0	01	01.0	10	03.1	05	01.8	02	01.0	01	02.0	51
GOD.	703.3	08.7	15.4	10.8	11.4	16.8	06.5	35.6	8 VIII	-		81	02.9	266	02.7	07	01.3	06	02.5	130	03.4	124	02.4	40	01.8	12	01.9	428
φ = 41° 43' N λ = 21° 46' E Gr. Δ G = + 1h 27 min. TITOV VELES BR. ST. 268																												
I	-	02.9	05.7	03.7	04.0	06.7	01.5	16.6	07	-06.5	25	04	01.0	01	01.0	01	01.0	18	02.5	.	.	08	01.5	.	.	43	01.7	18
II	-	02.0	08.2	04.5	04.8	09.5	00.4	20.0	06	-07.0	18	.	.	01	01.0	.	.	09	02.6	03	05.5	18	01.1	.	.	49	02.1	09
III	-	04.2	12.6	07.6	08.0	13.3	03.1	23.5	25	-06.2	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	11.1	19.5	14.3	14.8	20.3	07.9	29.5	27	-01.5	07,05	01	01.0	05	01.4	03	01.7	22	03.7	03	05.0	11	02.2	01	01.0	30	03.3	14
V	-	13.2	20.4	15.9	16.4	21.4	09.3	28.6	11	01.0	02	01	03.0	.	.	01	02.0	18	02.1	01	06.0	04	01.2	.	.	37	02.3	31
VI	-	19.3	27.3	21.7	22.5	28.8	15.0	36.0	18	08.0	06	.	.	02	01.5	.	.	05	01.4	01	01.0	18	01.3	.	.	28	01.8	36
VII	-	20.4	28.4	22.8	23.6	29.8	16.4	35.0	23,03	08.5	19	.	.	.	.	.	.	14	02.0	.	.	07	01.3	.	.	32	02.0	40
VIII	-	19.8	29.6	23.4	24.0	30.9	17.0	35.0	09,07	12.0	13	04	02.5	06	02.0	.	.	06	03.2	02	03.5	07	01.9	.	.	30	02.2	38
IX	-	15.4	25.9	19.6	20.1	26.8	13.6	35.2	12	04.4	29	03	01.3	04	01.8	.	.	02	02.0	04	02.2	04	01.5	01	01.0	52	03.1	20
X	-	08.0	17.0	12.0	12.3	18.4	06.5	25.2	09	01.5	27	01	02.0	.	.	.	.	04	03.2	.	.	04	01.8	01	02.0	41	02.6	47
XI	-	03.2	13.4	06.7	07.5	14.3	01.8	21.0	04	-03.5	13,12	.	.	04	01.0	.	.	03	02.7	.	.	01	01.0	.	.	27	03.6	55
XII	-	02.0	06.9	03.2	03.8	07.9	00.3	20.2	01	-09.0	21	04	03.0	.	.	.	.	12	03.2	03	02.0	14	01.8	01	03.0	20	02.6	39
GOD.	-	10.1	17.9	13.0	13.5	19.0	07.7	36.0	18 VI	-09.0	21 XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 41° 50' N λ = 22° 02' E Gr. Δ G = + 1h 28 min. ERDŽELIJA BR. ST. 269																												
I	-	02.4	05.4	03.8	03.7	06.1	01.4	16.6	07	-08.8	22	.	.	.	.	.	.	13	01.6	.	.	.	.	.	.	26	02.5	54
II	-	01.7	08.3	04.2	04.6	09.4	00.3	18.0	10	-07.6	18	.	.	01	01.0	.	.	08	01.9	.	.	08	02.4	.	.	26	03.2	41
III	-	03.2	13.0	07.0	07.6	13.6	01.6	23.6	27	-07.4	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	09.3	18.7	12.4	13.2	20.2	05.4	29.6	27	-04.4	07	01	01.0	.	.	.	.	21	01.8	.	.	08	01.8	.	.	27	02.9	38
V	-	11.8	20.0	13.9	14.9	21.1	08.2	28.6	11	-01.0	02	.	.	.	.	01	01.0	04	01.5	.	.	05	01.8	01	01.0	26	02.7	56
VI	-	18.0	27.7	20.7	21.8	28.5	12.8	35.4	18	05.5	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	19.2	28.8	21.9	23.0	30.1	15.3	35.0	23	07.6	19	.	.	.	.	.	.	03	01.0	.	.	05	01.4	.	.	45	02.2	40
VIII	-	18.8	30.2	22.9	23.7	31.0	15.1	37.4	20	09.4	28	01	01.0	01	01.0	.	.	09	01.6	.	.	05	01.0	01	01.0	30	02.2	46
IX	-	14.3	26.5	18.5	19.6	26.8	11.0	35.8	11	00.6	30	.	.	01	03.0	.	.	.	.	.	.	03	01.0	.	.	37	02.2	49
X	-	07.3	17.7	10.9	11.7	18.6	05.6	27.4	08	-00.2	27	.	.	.	.	.	.	05	01.2	.	.	.	.	.	.	28	02.6	60
XI	-	02.2	13.6	05.6	06.8	14.3	00.9	22.0	04	-05.2	29	.	.	.	.	.	.	02	01.0	.	.	.	.	.	.	29	02.6	59
XII	-	01.2	06.5	02.0	03.0	07.0	-01.6	15.8	31	-10.4	21,19	.	.	01	02.0	.	.	09	02.1	.	.	.	.	.	.	20	02.6	63
GOD.	-	09.1	18.0	12.0	12.8	18.9	06.3	37.4	20 VIII	-10.4	21 XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
φ = 41° 26' N λ = 22° 02' E Gr. Δ G = + 1h 28 min. KAVADARCI BR. ST. 270																												
I	-	03.2	05.8	04.2	04.3	07.0	01.5	17.5	07	-07.2	22	08	01.2	03	03.3	.	.	01	03.0	01	01.0	.	.	.	.	16	01.6	64
II	-	03.3	08.8	05.2	05.6	10.2	00.8	21.2	15	-10.2	21	04	01.2	04	01.2	01	02.0	09	01.8	02	01.0	10	01.9	.	.	21	02.1	33
III	-	05.3	13.0	08.3	08.7	13.8	03.2	23.4	28	-06.1	03	02	02.0	06	01.7	09	02.3	08	01.9	01	01.0	03	02.0	.	.	22	02.5	42
IV	-	12.1	19.4	13.9	14.8	20.8	08.4	30.1	27	01.5	07	01	02.0	14	01.9	01	01.0	08	01.6	.	.	04	01.2	.	.	20	02.0	42
V	-	14.0	20.2	15.2	16.2	21.0	09.7	28.3	13	09.0	03	02	01.0	06	01.5	03	02.0	08	02.1	01	01.0	04	01.8	.	.	17	01.9	52
VI	-	20.6	27.5	21.4	22.7	28.2	14.9	33.5	30	07.0	05	05	01.0	04	01.5	.	.	01	02.0	02	01.0	02	01.0	01	02.0	17	01.6	58
VII	-	21.6	29.2	22.8	24.0	29.8	16.3	35.5	23	08.5	19	.	.	06	01.5	.	.	.	.	.	.	.	.	.	.	15	01.5	72
VIII	-	22.5	30.4	24.1	25.3	30.8	16.5	34.0	16	09.7	27	.	.	04	02.0	.	.	03	01.0	.	.	01	01.0	.	.	19	01.7	66
IX	-	17.4	26.7	20.5	21.3	26.8	13.0	34.8	13	06.4	26	.	.	.	.	.	.	.	.	.	.	.	.	.	.	21	01.9	69
X	-	09.5	18.4	13.1	13.5	19.1	06.5	24.5	09,08	02.1	26	.	.	.	.	.	.	02	02.0	.	.	.	.	.	.	09	02.4	82
XI	-	04.2	13.5	08.5	08.6	14.0	02.5	21.0	04	-02.5	28	.	.	01	01.0	.	.	.	.	.	.	.	.	.	.	10	02.0	79
XII	-	01.6	06.8	03.7	03.9	07.4	-00.4	18.0	30	-07.4	21	01	01.0	01	02.0	02	02.0	05	01.2	01	01.0	01	02.0	.	.	08	01.9	74
GOD.	-	11.3	18.3	13.4	14.1	19.1	07.7	35.5	23 VIII	-10.2	21 II	23	01.2	49	01.8	16	02.1	45	01.8	08	01.0	25	01.7	01	02.0	195	01.9	733

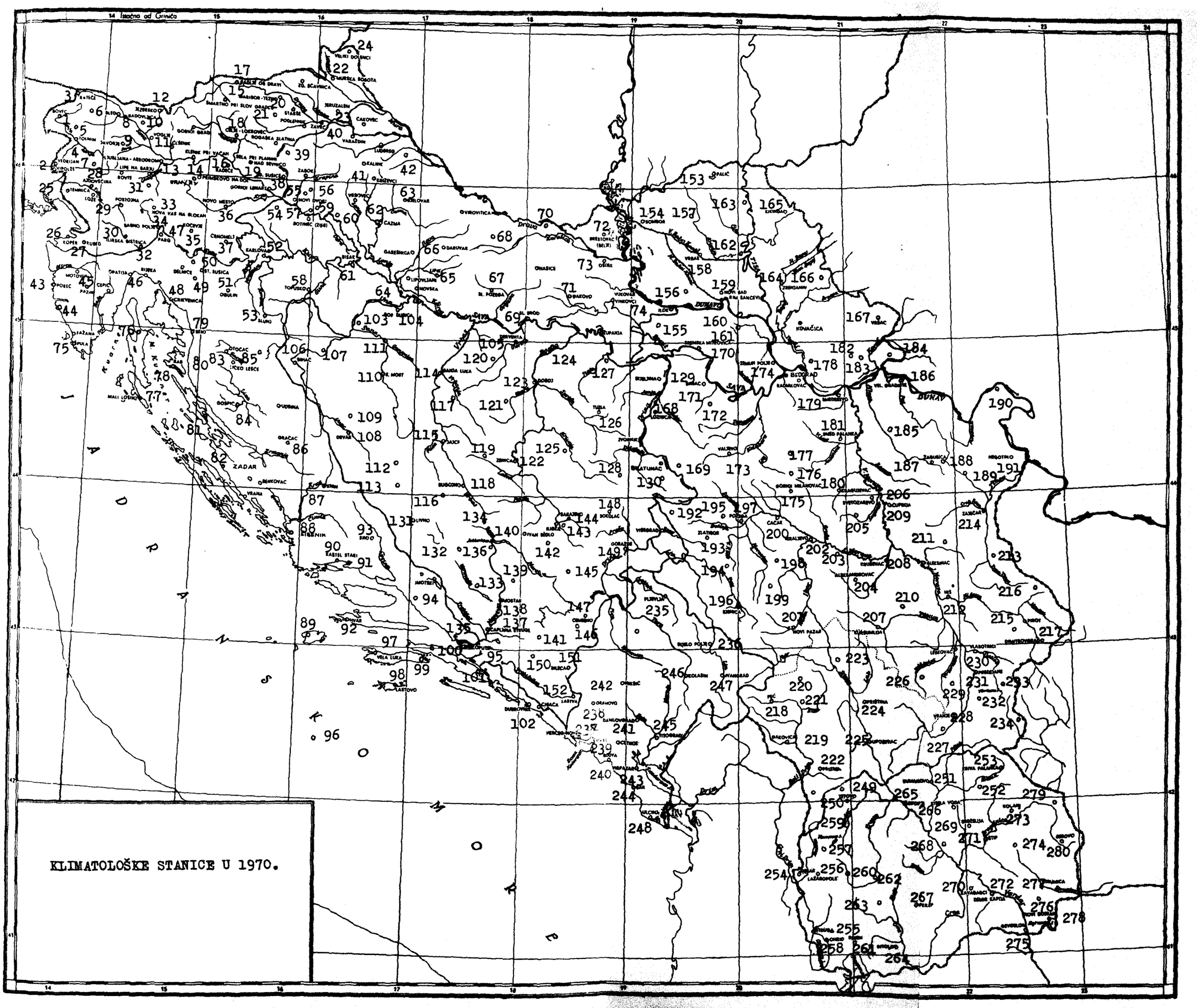
Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlen)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dlen)	min	Padavine R mm Σ	max	broj dana	Tn ≤-10,0	Tn ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tm ≥ 10,0	Tn ≥ 20,0	P (0-12) ≥ 6	P (0-12) ≥ 8	Nm (0-10) < 2.0	> 8.0	R mm ≥ 0.1	≥ 1.0	≥ 10.0	●	⁎	⁎	△	∽	▲	▲	⊤	≡	▦
BR. ST. 266						TRUBAREVO																																H_a = 233 m H_b = - m h_k = 1.9 m h_z = 1.7 m
I	9.6	9.1	8.5	9.1	-	05.4	93	83	91	89	59	038	020.0	17	.	06	10	.	.	.	.	.	.	24	07	05	02	06	01	.	.	.	.	.	.	01	02
II	8.7	7.6	5.7	7.3	-	05.0	88	72	85	82	38	038	016.5	08	.	.	14	.	.	.	.	.	.	10	10	07	01	07	04	01	.	.	.	.	.	03	02
III	7.8	6.0	4.4	6.1	-	06.0	88	64	77	76	30	040	013.0	05	.	.	06	.	.	.	.	.	03	11	08	06	01	06	02	.	.	.	.	.	.	.	02
IV	6.7	5.8	4.1	5.5	-	08.6	85	60	73	73	37	021	007.0	13	.	.	02	06	.	.	.	.	03	08	07	05	.	07	.	.	.	.	.	.	.	.	.
V	6.4	6.8	5.4	6.2	-	11.2	89	74	86	83	56	047	015.8	21	.	.	.	06	.	.	.	.	04	13	10	09	01	10	.	.	.	.	.	.	01	.	.
VI	3.1	6.1	4.0	4.4	-	12.9	79	52	72	68	36	018	008.5	20	.	.	.	23	15	.	.	.	06	03	05	05	.	05	.	.	.	.	.	.	02	.	.
VII	3.4	4.8	4.7	4.3	-	13.7	80	50	68	66	33	056	018.0	18	.	.	.	25	21	01	.	.	08	03	09	08	03	09	.	.	.	.	.	.	02	.	.
VIII	2.6	4.3	3.2	3.4	-	13.6	82	47	68	66	30	005	004.0	26	.	.	.	29	20	.	.	.	12	02	02	01	.	02	.	.	.	.	.	.	.	.	.
IX	2.8	3.6	2.5	3.0	-	11.2	92	50	83	75	32	042	037.0	01	.	.	01	19	08	.	.	.	13	01	02	02	01	02	.	.	.	.	.	.	.	.	.
X	5.1	4.5	4.1	4.6	-	08.2	95	64	91	83	37	085	014.5	17	.	.	01	03	.	.	.	.	10	06	11	11	05	11	.	.	.	.	.	.	.	07	.
XI	5.0	4.2	3.1	4.1	-	05.9	94	64	90	83	41	015	003.5	16	.	.	14	.	.	.	.	.	12	06	05	05	.	05	.	.	.	.	.	.	.	12	.
XII	6.5	6.6	5.7	6.3	-	04.6	90	70	87	83	27	030	010.0	31	.	.	20	.	.	.	.	.	05	13	06	05	01	05	01	.	.	.	.	.	.	08	01
GOD.	5.6	5.8	4.6	5.4	-	08.9	87	62	80	77	27	435	037.0	4 IX	.	06	66	111	64	01	.	.	76	100	82	69	15	75	08	01	.	.	.	.	05	31	07
BR. ST. 267						PRILEP																																H_a = 673 m H_b = 673.5 m h_k = 2.0 m h_z = 1.5 m
I	9.0	8.7	7.9	8.5	039.7	04.7	86	77	84	82	39	050	014.1	02	.	03	14	.	.	.	04	.	03	23	11	07	03	08	03	.	.	.	.	.	.	04	02
II	7.0	7.0	6.2	6.7	084.6	04.0	74	59	69	67	39	054	016.2	01	01	03	13	.	.	.	07	02	.	03	15	09	01	08	09	02	.	.	.	.	.	02	09
III	7.0	6.4	4.3	5.9	158.7	04.5	73	52	66	63	22	052	013.5	05	.	01	09	.	.	.	07	01	03	09	13	09	02	10	05	01	.	.	.	.	.	.	02
IV	6.6	5.8	5.0	5.8	180.9	06.1	71	46	62	60	22	038	016.0	13	.	.	02	06	.	.	05	03	01	08	10	06	01	09	01	.	.	.	.	01	.	.	.
V	6.3	6.7	5.1	6.1	184.4	07.2	74	52	69	65	31	108	024.0	01	.	.	.	02	.	.	04	01	03	07	16	10	05	16	.	.	.	.	.	.	05	.	.
VI	3.0	5.3	3.2	3.8	282.9	09.9	70	45	63	60	30	033	014.9	21	.	.	.	18	05	.	06	01	07	02	13	07	01	13	.	.	.	.	.	.	09	.	.
VII	3.5	4.4	3.1	3.7	304.4	10.7	72	44	61	59	24	056	013.9	06	.	.	.	24	06	01	03	01	07	02	13	09	02	13	.	.	.	.	.	.	13	.	.
VIII	2.1	4.4	2.4	3.0	309.5	09.7	65	35	50	50	20	005	004.7	25	.	.	.	26	14	.	01	02	15	02	01	01	.	01	.	.	.	.	.	.	08	.	.
IX	3.5	3.0	3.8	3.4	267.5	07.5	63	34	49	49	10	003	003.2	01	.	.	.	14	07	.	02	.	11	03	01	01	.	01	.	.	.	.	.	.	01	.	.
X	4.2	4.5	3.5	4.0	201.5	06.5	83	51	71	68	30	062	019.4	23	.	.	01	.	.	.	02	02	12	06	08	07	02	08	.	.	.	.	.	.	.	01	.
XI	4.5	4.7	2.7	4.0	168.7	05.3	81	53	71	68	33	027	007.2	17	.	.	07	.	.	.	04	01	10	06	09	06	.	09	.	.	.	.	.	.	.	.	.
XII	5.8	5.6	4.1	5.2	113.7	04.2	82	64	78	74	36	026	008.2	31	.	01	19	.	.	.	02	01	05	08	09	07	.	06	04	01	.	.	.	.	01	03	03
GOD.	5.2	5.5	4.3	5.0	2296.5	06.7	74	51	66	63	10	514	024.0	4 V	01	08	65	90	32	01	47	15	77	79	119	79	17	102	22	04	.	.	.	01	34	10	16
BR. ST. 268						TITOV VELES																																H_a = 175 m H_b = - m h_k = 2.1 m h_z = 1.7 m
I	9.2	8.8	9.2	9.1	-	05.1	86	78	80	81	54	053	014.8	17	.	04	10	.	.	.	.	.	.	23	08	05	03	07	01	.	.	.	.	.	.	02	01
II	8.2	6.9	4.9	6.7	-	04.6	85	60	70	72	10	013	003.4	20	.	.	11	.	.	.	04	.	01	08	06	05	.	06	01	.	.	.	.	.	.	01	.
III	6.8	5.9	5.1	5.9	-	05.5	81	55	69	68	24	045	015.0	15	.	.	06	.	.	.	06	.	03	09	07	06	01	07	.	.	.	.	.	.	.	.	.
IV	6.6	6.3	5.0	6.0	-	07.4	72	49	57	59	-	033	009.2	13	.	.	02	08	.	.	05	02	06	11	07	06	.	07	.	.	.	.	.	.	02	.	.
V	5.7	6.1	5.4	5.7	-	07.8	69	43	59	57	19	059	012.5	22	.	.	.	06	.	.	02	.	03	06	09	09	02	09	02	02	.	.	.	.	05	.	.
VI	2.1	4.8	2.5	3.1	-	10.4	64	39	53	52	23	008	004.0	04	.	.	.	25	17	01	.	.	11	02	02	02	.	02	.	.	.	.	.	.	03	.	.
VII	2.5	4.1	3.8	3.5	-	11.6	65	42	56	54	27	080	032.0	05	.	.	.	26	18	02	.	.	13	03	06	05	04	06	.	.	.	.	.	.	09	.	.
VIII	1.5	2.5	4.0	2.7	-	11.6	67	39	53	53	26	007	004.8	03	.	.	.	29	22	03	.	.	14	01	02	02	.	02	.	.	.	.	.	.	04	.	.
IX	0.8	0.9	4.0	1.9	-	08.7	66	33	51	50	18	004	004.0	01	.	.	.	19	10	.	03	.	15	.	01	01	.	01	.	.	.	.	.	.	.	.	.
X	4.4	3.3	4.1	3.9	-	07.3	85	56	66	69	26	036	009.0	18	.	.	.	02	.	.	03	.	12	05	07	07	.	07	.	.	.	.	.	.	.	02	.
XI	4.2	2.1	4.2	3.5	-	05.2	84	53	65	67	-	022	010.4	17	.	.	09	.	.	.	03	.	08	03	06	04	01	06	.	.	.	.	.	.	.	05	.
XII	5.7	5.9	6.0	5.9	-	04.8	80	69	80	76	37	035	017.8	31	.	.	16	.	.	.	01	.	06	10	09	05	01	08	02	.	.	.	.	.	.	02	01
GOD.	4.8	4.8	4.8	4.8	-	07.5	75	51	63	63	-	395	032.0	5 VII	.	04	54	115	67	06	27	02	92	81	70	57	12	68	06	02	.	.	.	.	23	12	02
BR. ST. 269						ĐEDJELIJA																																H_a = 253 m H_b = - m h_k = 2.0 m h_z = 1.5 m
I	9.0	8.6	7.6	8.4	-	05.6	91	86	90	89	-	030	012.0	18	.	04	13	.	.	.	.	.	.	19	04	04	02	04	-	.	.	.	.	.	.	04	-
II	6.9	5.9	6.0	6.3	-	05.0	84	65	81	77	39	014	008.5	24	.	.	14	.	.	.	01	.	01	07	04	04	.	04	-	.	.	.	.	.	.	.	-
III	6.4	5.7	4.8	5.6	-	05.6	81	56	73	70	18	015	005.0	15	.	.	09	.	.	.	.	.	-	-	06	05	.	06	.	.	.	.	.	.	.	.	.
IV	3.7	3.2	3.1	3.3	-	07.5	76	51	69	65	30	018	008.5	13	.	.	02	08	.	.	01	.	-	-	04	04	.	04	.	.	.	.	.	.	01	.	.
V	5.5	5.6	4.5	5.2	-	09.5	83	59	79	74	17	058	021.0	01	.	.	01	07	.	.	.	.	06	04	10	10	02	10	.	.	.	.	.	01	01	.	.
VI	2.4	2.4	2.9	2.6	-	12.2	74	46	66	62	28	006	005.4	01	.	.	.	23	16	01	.	.	15	01	02	02	.	02	.	.	.	.	.	.	02	.	.
VII	3.0	3.9	3.8	3.6	-	14.4	75	57	69	67	28	088	019.0	07	.	.	.	28	18	02	.	.	11	04	09	09	04	09	.	.	.	.	.	.	07	.	.
VIII	1.7	2.9	1.9	2.2	-	13.1	77	42	64	61	13	028	012.0	11	.	.	.	29	21	.	02	.	18	01	05	03	01	05	.	.	.	.	.	01	03	.	.
IX	1.4	2.0	2.2	1.9	-	10.3	73	44	59	59	-	002	002.0	05	.	.	.	19	11	.	.	.	18	.	01	01	.	01	.	.	.	.	.	.	.	.	.
X	5.5	3.2	3.5	4.1	-	08.3	88	62	84	78	41	070	020.0	17	.	.	01	01	.	.	.	.	11	04	08	08	03	08	.	.	.	.	.	.	.	.	.
XI	5.2	3.2	2.6	3.6	-	06.2	90	65	85	80	33	004	004.5	17	.	.	11	.	.	.	.	.	11	03	01	01	.	01	.	.	.	.	.	.	.	03	.
XII	7.1	4.1	3.8	5.0	-	04.8	82	71	85	79	29	023	010.0	31	03	.	19	.	.	.	.	.	05	08	04	04	01	04	01	.	.	.	.	.	.	06	.
GOD.	4.8	4.2	3.9	4.3	-	08.5	81	58	75	71	-	356	021.0	4 V	03	04	70	115	66	03	04	.	-	-	58	55	13	58	-	.	.	.	.	02	14	13	-
BR. ST. 270						KAVADARCI																																H_a = 265 m H_b = - m h_k = 2.0 m h_z = 1.4 m
I	9.5	8.7	8.5	8.9	-	05.1	80	74	77	77	44	024	006.8	17	.	04	10	.	.	.	.	.	.	21	07	06	.	06	01	.	.	.	.	.	.	09	01
II	7.4	6.7	5.3	6.5	-	04.7	73	55	72	67	25	032	009.5	01	01	.	12	.	.	.	.	.	.	08	08	08	.	06	04	.	.	.	.	.	.	02	07
III	6.0	5.6	5.1	5.5	-	05.4	73	51	65	63	28	032	011.2	17	.	.	04	01	.	.	01	.	06	10	11	08	01	11	01	.	.	.	.	.	.	.	.
IV	5.8	5.9	4.3	5.3	-	07.1	66	44	60	57	14	025	010.0	13	.	.	.	09	01	.	.	.	08	10	09	06	01	09	.	.	.	.	.	.	.	.	.
V	5.5	6.3	5.6	5.8	-	08.6	70	51	66	62	22	100	023.6	01	.	.	.	08	.	.	.	.	04	09	14	11	04	14	.	.	.	.	.	.	.	.	.
VI	1.9	4.6	3.7	3.4	-	11.5	64	43	57	55	29	033	014.0	23	.	.	.	24	18	.	.	.	-	-	08	05	01	08	.	.	.	.	.	01	-	.	.
VII	2.8	2.9	3.7	3.2	-	13.5	66	47	65	59	30	066	016.5	07	.	.	.	27	21	01	.	.	16	05	06	06	04	06	.	.	.	.	.	.	.	.	.
VIII	1.7	1.5	1.5	1.6	-	14.6	69	44	67	60	33	005	002.4	10	.	.	.	30	21	.	.	.	21	01	02	02	.	02	.	.	.	.	.	.	.	.	.
IX	1.7	2.1	2.5	2.1	-	11.1	65	45	58	56	31	003	002.7	01	.	.	.	18	11	.	.	-	20	01	01	01	.	01	.	.	.	.	.	.	.	.	.
X	4.0	3.5	4.2	3.9	-	08.7	86	62	72	73	26	074	016.0	17	.	.	.	.	.	.	.	.	13	08	08	08	03	08	.	.	.	.	.	.	.	.	.
XI	5.7	5.8	4.6	5.4	-	06.7	82	69	80	77	-	007	002.5	09	.	.	09	.	.	.	.	.	08	08	06	03	.	06	.	.	.	.	.	.	.	06	.
XII	6.2	5.6	5.1	5.6	-	05.0	82	72	78	77	50	032	009.7	07	.	01	17	.	.	.	.	.	08	13	07	06	.	07	02	.	.	.	.	.	.	14	01
GOD.	4.8	4.9	4.5	4.8	-	08.5	73	54	68	65	-	433	023.6	4 V	01	05	52	117	72	01	-	-	-	-	87	70	14	84	08	.	.	.	-	-	-	-	09

Mjesec	Tlak zraka	Temperatura vazduha °C: 7	14	21	Sred. (Dnev.)	Max	Min	Amp.	Dan	Mjesec	Broj dana	Broj mjerenja	N: Br.	Sr.	NE: Br.	Sr.	E: Br.	Sr.	SE: Br.	Sr.	S: Br.	Sr.	SW: Br.	Sr.	W: Br.	Sr.	NW: Br.	Sr.	C: Br.
STIP																													
φ = 41° 45' N λ = 22° 11' E Gr. Δ G = + 1h 29 min.																													BR. ST. 271
I	732.6	02.2	04.7	03.3	03.4	05.9	01.0	15.5	07	-07.1	21	03	02.3	08	01.5	01	02.0	23	05.1	07	03.0	08	02.1	11	03.5	14	04.0	18
II	729.0	01.5	07.1	04.2	04.2	08.6	00.5	17.4	15	-10.3	21	09	01.6	03	01.7	03	02.0	13	05.7	08	03.0	07	03.6	04	04.5	21	04.7	16
III	730.5	04.2	11.6	07.8	07.9	12.8	03.2	22.1	25	-04.4	03	04	02.8	07	01.4	.	.	27	05.1	12	03.8	05	04.0	04	02.8	21	04.8	13
IV	731.4	09.4	17.5	13.1	13.3	19.2	07.4	28.4	27,25	-01.4	05	02	02.5	03	01.0	02	03.5	24	05.1	07	02.7	10	03.2	04	04.2	22	04.0	16
V	731.5	12.1	18.7	14.4	14.9	20.2	09.9	27.0	15	01.7	02	06	02.3	02	01.5	06	01.5	16	03.9	09	02.8	06	02.5	02	03.0	29	04.5	17
VI	733.0	18.1	26.1	20.9	21.5	28.0	14.8	33.4	18	07.6	05	05	01.6	05	02.4	04	01.8	11	03.9	03	02.7	06	01.7	05	01.4	26	03.4	25
VII	731.3	19.2	27.7	22.0	22.7	29.4	16.4	35.0	23	09.1	19	05	02.4	06	01.7	02	02.5	08	03.9	09	02.0	06	01.8	08	02.4	26	03.7	23
VIII	732.0	19.2	29.3	23.0	23.6	30.3	16.8	37.0	08	11.0	28	08	02.1	03	02.3	08	02.6	14	03.5	04	03.5	06	01.5	11	03.4	15	03.8	24
IX	734.9	13.6	25.3	19.0	19.3	26.3	12.4	34.8	13	01.0	30	01	02.0	02	01.5	05	01.8	07	02.3	07	01.7	03	02.0	19	03.5	17	03.5	29
X	735.6	07.9	16.5	11.3	11.8	17.8	06.7	25.5	08	00.0	26	09	01.4	.	.	02	02.0	10	05.1	05	02.2	09	01.4	14	03.6	16	03.7	29
XI	735.2	03.3	12.6	07.0	07.5	13.4	02.3	21.3	04	-03.2	30	07	01.7	01	01.0	04	01.5	08	04.1	05	01.2	03	01.0	13	03.2	14	03.4	35
XII	736.7	00.6	05.6	02.7	02.9	06.7	-00.4	16.3	30	-08.7	21	01	01.0	03	02.7	15	05.7	05	02.8	07	01.3	02	01.0	11	03.1	14	04.3	35
GOD.	732.8	09.3	16.9	12.4	12.8	18.2	07.6	37.0	8 VIII	-10.3	24 II	60	01.9	43	01.7	52	03.1	166	04.5	83	02.5	71	02.3	106	03.3	235	04.0	280
DEMIR KAPIJA																													
φ = 41° 25' N λ = 22° 15' E Gr. Δ G = + 1h 29 min.																													BR. ST. 272
I	750.9	03.7	06.4	04.7	04.9	07.5	02.1	17.4	07	-06.0	22	.	.	01	01.0	28	04.4	03	04.7	.	.	.	.	19	01.9	13	01.8	29
II	747.2	02.8	09.0	05.3	05.6	10.3	01.3	21.7	15	-11.5	21	01	02.0	.	.	18	04.0	07	03.9	01	01.0	05	01.4	09	02.2	12	02.3	31
III	748.5	05.1	12.5	08.6	08.7	13.5	04.2	24.2	25	-04.9	03	02	01.0	01	02.0	31	04.4	08	03.0	03	01.3	05	01.2	06	01.8	12	02.7	25
IV	749.1	10.9	19.1	14.2	14.6	20.7	08.8	30.0	24	-00.2	07	02	01.5	.	.	34	04.4	03	02.7	02	01.5	.	.	04	02.5	14	02.6	31
V	749.0	13.4	20.5	15.4	16.2	21.6	10.6	28.0	15	03.6	02	02	01.5	.	.	26	03.3	05	02.2	01	01.0	02	01.5	09	02.4	14	02.6	34
VI	750.2	19.4	27.8	21.4	22.5	29.0	15.6	33.4	30,29	07.2	04	.	.	.	.	17	03.3	05	02.0	01	02.0	03	01.0	07	01.3	16	01.8	41
VII	748.6	20.3	29.0	23.0	23.8	30.5	17.1	35.8	23	11.3	19	02	01.0	01	02.0	13	02.8	03	03.0	02	01.5	.	.	12	01.9	11	01.9	49
VIII	749.1	20.2	30.3	23.6	24.4	31.1	17.5	36.7	08	13.5	13	01	01.0	.	.	15	03.5	12	02.8	01	02.0	.	.	04	01.5	19	02.3	41
IX	752.2	14.8	26.6	19.7	20.2	27.5	13.0	35.3	13	02.1	30	02	01.0	.	.	12	02.8	01	02.0	02	01.0	01	01.0	03	01.3	20	02.0	49
X	753.3	08.4	17.6	12.4	12.7	19.2	07.2	27.0	08	00.4	26	01	01.0	.	.	15	03.4	05	03.2	02	01.0	05	01.0	10	01.3	16	01.9	39
XI	753.2	03.3	13.3	07.5	07.9	14.3	02.2	21.5	01	-03.4	29	.	.	.	.	16	03.9	02	03.0	03	02.0	02	01.0	03	02.0	15	01.8	49
XII	755.1	01.1	06.5	03.3	03.6	07.4	-00.2	18.6	31	-09.3	21	01	01.0	01	03.0	13	05.5	02	05.5	.	.	01	02.0	13	02.2	12	01.8	50
GOD.	750.5	10.3	18.2	13.3	13.8	19.4	08.3	36.7	8 VIII	-11.5	24 II	14	01.2	04	02.0	238	03.9	56	03.1	18	01.4	24	01.2	99	01.9	174	02.1	468
KOČANI																													
φ = 41° 55' N λ = 22° 25' E Gr. Δ G = + 1h 20 min.																													BR. ST. 273
I	-	02.6	05.9	03.8	04.0	06.9	00.3	19.2	07	-07.7	21	02	02.5	02	02.0	01	02.0	09	02.6	01	02.0	22	02.5	03	02.7	02	02.5	51
II	-	01.7	07.8	04.5	04.6	09.2	-00.5	18.7	06	-10.4	18	01	02.0	08	02.1	.	.	15	02.3	.	.	20	03.1	01	03.0	05	03.0	34
III	-	04.6	12.6	07.9	08.2	13.4	02.0	25.2	27	-04.0	03	04	02.0	10	02.3	01	02.0	22	02.2	01	03.0	17	03.1	02	03.0	06	02.7	30
IV	-	10.4	18.9	13.1	13.9	19.9	06.4	28.4	25	-01.3	07	01	02.0	10	02.3	01	02.0	14	02.5	01	04.0	27	03.1	03	03.0	06	02.7	27
V	-	12.8	19.8	14.7	15.6	21.0	08.7	29.4	11	01.7	02	02	02.5	13	02.3	.	.	14	02.3	02	01.5	25	02.8	04	03.0	08	03.1	25
VI	-	18.8	26.5	20.6	21.7	27.9	13.7	33.6	18	07.5	02	01	02.0	04	02.0	.	.	27	02.2	04	02.0	16	03.0	02	03.5	08	02.5	28
VII	-	19.9	28.1	21.2	22.6	29.6	15.0	34.2	23	07.2	19	.	.	02	01.5	.	.	31	02.0	06	03.0	23	02.5	01	04.0	05	02.8	25
VIII	-	19.3	28.5	21.7	22.8	30.0	15.2	35.2	08	10.0	28	.	.	02	02.0	.	.	26	02.2	05	02.4	25	02.4	01	01.0	03	03.0	31
IX	-	13.5	25.8	18.2	18.9	26.8	10.5	34.0	11	-00.4	30	02	02.0	02	02.0	.	.	26	02.3	03	03.0	26	02.5	01	03.0	02	03.0	28
X	-	08.1	17.6	11.6	12.2	18.9	05.4	25.0	08	-02.4	26	.	.	03	02.3	.	.	23	02.1	06	02.5	21	02.5	.	.	08	02.6	32
XI	-	03.2	13.7	06.3	07.4	14.3	00.7	21.0	01	-05.0	12	04	02.5	04	01.8	.	.	22	02.1	05	02.8	10	01.9	.	.	04	02.0	41
XII	-	00.2	06.7	02.8	03.2	07.5	-01.9	16.0	30	-09.5	21	04	02.8	03	01.7	01	02.0	14	02.3	03	03.7	11	02.0	02	02.5	07	03.1	48
GOD.	-	09.6	17.7	12.2	12.9	18.8	06.3	35.2	8 VIII	-10.4	18 II	21	02.3	63	02.1	04	02.0	243	02.2	37	02.7	243	02.7	20	02.9	64	02.8	400
RADOVIŠ																													
φ = 41° 38' N λ = 22° 27' E Gr. Δ G = + 1h 30 min.																													BR. ST. 274
I	-	02.2	04.7	03.2	03.3	06.0	00.9	15.0	07	-06.9	21	06	05.2	01	04.0	21	02.1	13	02.2	06	03.3	07	03.3	23	03.8	07	04.6	09
II	-	01.0	07.2	03.6	03.8	08.4	-00.2	17.2	15	-10.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	04.1	11.0	07.0	07.3	12.2	02.7	23.4	25	-04.6	03	09	03.3	.	.	19	03.0	16	02.8	06	01.2	09	02.3	12	04.1	11	04.3	11
IV	-	10.2	17.5	11.9	12.9	18.8	07.2	28.0	24	-00.6	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	12.5	18.9	13.6	14.6	20.1	08.9	26.0	15,11	01.0	03	14	05.2	01	01.0	17	02.6	04	03.2	10	02.4	01	01.0	12	03.0	19	05.5	15
VI	-	18.4	26.6	19.7	21.1	27.8	13.7	33.0	24	06.7	04	04	03.2	02	03.0	05	02.4	07	02.9	09	02.1	08	03.2	12	03.0	15	03.9	28
VII	-	20.2	28.2	20.3	22.3	29.3	15.5	34.0	23	10.0	19	09	02.8	01	02.0	07	02.6	02	03.5	07	02.4	07	02.4	16	03.1	23	03.9	21
VIII	-	19.9	29.1	21.5	23.0	30.1	15.8	35.5	08	09.9	28	07	04.3	03	05.7	09	02.7	04	02.0	06	02.5	08	02.9	07	02.1	17	04.2	32
IX	-	14.6	25.9	17.2	18.7	26.6	11.8	34.9	11	01.4	30	09	03.9	02	02.0	02	01.0	01	01.0	02	03.5	06	03.2	24	02.3	14	04.1	30
X	-	08.6	17.1	10.6	11.7	18.0	06.9	25.0	08	00.4	26	07	05.4	.	.	01	01.0	10	03.3	03	01.3	14	02.2	16	02.0	14	04.6	28
XI	-	04.2	12.7	06.0	07.2	13.7	02.6	21.1	01	-02.2	27	08	04.1	01	03.0	05	02.4	12	01.7	06	01.3	03	01.7	20	03.0	15	03.4	20
XII	-	01.7	06.6	02.6	03.4	07.4	-00.2	14.3	31	-07.0	19	07	04.6	.	.	06	02.2	11	01.9	10	02.5	04	01.8	13	02.8	20	04.4	22
GOD.	-	09.8	17.1	11.4	12.4	18.2	07.1	35.5	8 VIII	-10.0	24 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GEVGELIJA																													
φ = 41° 09' N λ = 22° 30' E Gr. Δ G = + 1h 30 min.																													BR. ST. 275
I	-	04.0	07.3	04.7	05.2	08.3	02.7	14.6	01	-04.4	25	24	03.8	01	01.0	03	01.0	03	02.0	08	01.0	01	01.0	03	01.0	20	03.2	30
II	-	03.0	10.4	05.4	06.0	11.7	02.0	20.2	15	-03.6	13	22	03.8	.	.	.	.	08	01.5	07	01.4	02	01.5	03	02.3	14	03.6	28
III	-	05.1	12.9	08.1	08.5	14.0	03.8	22.4	25	-05.4	03	14	03.6	01	06.0	06	01.2	12	01.5	01	01.0	03	01.7	01	02.0	18	04.3	37
IV	-	11.1	19.8	13.9	14.7	21.3	07.9	30.0	23	00.8	05	12	03.3	01	02.0	08	01.1	23	01.7	04	01.0	.	.	01	01.0	15	04.5	26
V	-	14.0	20.9	15.6	16.5	22.3	10.5	29.4	12	06.4	03	19	03.3	03	02.0	10	01.2	14	01.4	07	01.4	.	.	02	01.5	24	03.5	14
VI	-	20.6	27.2	21.5	22.7	29.2	15.4	33.4	29	08.0	05	19	02.9	01	02.0	11	01.2	06	01.2	05	01.2	04	01.8	01	01.0	14	03.1	29
VII	-	22.0	30.1	22.8	24.4	31.0	17.6	36.2	23	08.4	20	20	03.0	01	02.0	08	01.1	11	01.5	03	01.7	01	01.0	.	.	23	03.3	26
VIII	-	21.7	30.7	23.8	25.0	31.9	17.3	36.4	08	11.6	28	09	02.4	02	01.0	07	01.4	13	01.7	04	01.2	01	01.0	02	01.0	22	03.0	33
IX	-	17.1	27.1	18.9	20.5	28.1	13.9	35.4	10	06.0	30	14	03.1	03	02.3	02	01.0	12	01.4	02	01.5	.	.	.	.	21	02.7	36
X	-	09.9	19.0	11.6	13.0	20.7	07.6	27.0	08,07	03.2	27	14	02.9	03	03.0	02	01.0	09	01.2	02	01.5	.	.	.	.	21	03.4	42
XI	-	04.9	15.8	07.3	08.8	16.5	02.9	25.0	04	-03.8	13	13	03.2	02	02.5	02	01.0	07	01.1	03	01.0	04	01.0	02	01.0	17	03.6	40
XII	-	02.3	09.0	04.2	04.9	09.6	00.6	15.0	03	-09.8	19	18	04.4	01	03.0	01	01.0	06	01.2	01	01.0	04	01.0	01	06.0	17	03.6	44
GOD.	-	11.3	19.2	13.2	14.2	20.4	08.5	36.4	8 VIII	-09.8	19 XII	198	03.4	19	02.4	60	01.2	124	01.5	47	01.2	20	01.3	16	01.7	226	03.4	385

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dies)	Insolacija broj sati	Vlažnost vazduha e_m mm	U_m % 7	14	21	Sred. (Dies)	Min	Padavine R mm Σ	Max	Det.	Broj dana na: Tn ≤0,0	Tx ≤0,0	Tn ≤0,0	Tx ≥25,0	Tx ≥30,0	Tn ≥20,0	P(0-13) ≥6	≥8	Nm(0-10) ≤8,0	≥8,0	R mm ≥0,1	≥1,0	≥10,0	●	≡	▲	▲	≡	▦
ŠTIP																																	
BR. ST. 271																																	
I	9.0	8.8	7.4	8.4	032.8	05.2	88	78	84	83	56	026	008.0	07	.	05	13	.	.	.	15	03	01	22	12	05	.	09	03	.	.	.	.	.
II	7.5	7.0	5.7	6.8	110.9	04.5	84	60	73	72	37	033	010.6	01	01	.	14	.	.	.	17	03	.	09	11	07	01	09	03	.	.	.	.	.
III	6.8	6.8	4.4	6.0	166.2	05.1	76	51	65	64	28	017	004.3	15	.	.	07	.	.	.	22	05	04	09	12	05	.	12	.	.	.	.	.	.
IV	6.8	6.6	4.6	6.0	190.5	06.8	79	46	58	61	21	026	007.7	13	.	.	01	07	.	.	21	04	02	07	11	08	.	11	.	.	.	.	.	.
V	6.7	7.0	5.5	6.4	211.1	08.1	80	51	65	65	29	068	027.2	01	.	.	.	05	.	.	16	02	02	11	13	08	02	13	.	.	.	.	.	.
VI	2.9	5.9	4.2	4.3	269.2	10.2	69	40	53	54	24	023	011.5	25	.	.	.	23	12	01	12	03	05	02	10	03	01	10	.	.	.	.	.	.
VII	3.2	4.7	3.4	3.8	312.0	12.1	75	44	61	60	28	065	026.5	07	.	.	.	27	19	01	16	03	08	03	10	05	02	10	.	.	.	.	.	.
VIII	2.3	4.4	3.0	3.2	307.5	11.2	69	35	54	53	25	005	001.6	10	.	.	.	27	19	02	13	.	10	02	04	03	.	04	.	.	.	.	.	.
IX	2.5	3.9	2.0	2.8	273.6	08.8	74	36	51	54	22	017	015.7	01	.	.	.	19	10	.	13	.	12	.	02	02	01	02	.	.	.	.	.	.
X	5.2	4.4	3.4	4.3	199.3	07.5	88	56	76	73	31	112	041.1	17	.	.	.	01	.	.	10	01	11	07	10	09	05	10	.	.	.	.	.	.
XI	4.3	4.8	2.4	3.8	159.7	06.0	92	59	79	77	35	010	002.4	24	.	.	10	.	.	.	08	01	11	02	06	05	.	06	.	.	.	.	.	.
XII	6.3	5.7	4.5	5.5	094.2	04.7	86	71	83	80	39	021	011.9	31	.	01	19	.	.	.	12	03	05	09	09	04	01	08	03	01	.	01	.	.
GOD.	5.3	5.8	4.2	5.1	2327.0	07.5	80	52	66	66	21	423	041.1	11 X	01	06	64	109	60	04	175	28	71	83	110	64	13	104	09	01	.	01	.	.
DEMIR KAPIJA																																	
BR. ST. 272																																	
I	9.4	9.0	8.4	8.9	-	05.5	86	74	80	80	49	018	004.8	18	.	02	12	.	.	.	07	.	01	23	13	05	.	11	03	.	.	.	.	01
II	7.4	7.2	5.0	6.5	-	04.6	81	53	69	67	15	058	026.3	20	01	.	11	.	.	.	05	.	.	07	12	10	01	10	04	01	.	.	.	.
III	6.5	6.6	3.9	5.7	-	05.5	77	52	66	65	22	052	021.8	17	.	.	06	.	.	.	06	.	04	10	11	08	01	10	01	.	.	.	.	.
IV	6.9	6.7	4.9	6.1	-	07.3	74	45	59	59	18	023	008.2	13	.	.	01	08	01	.	04	.	04	10	11	07	.	11	.	.	.	.	.	.
V	6.2	6.8	4.8	5.9	-	08.5	75	47	66	63	24	083	024.4	01	.	.	.	10	.	.	02	.	03	09	13	10	03	13	.	.	.	.	.	.
VI	3.1	5.0	4.2	4.1	-	11.4	70	39	60	56	25	046	013.4	21	.	.	.	24	17	01	.	.	06	01	10	05	03	10	.	.	.	.	.	.
VII	3.0	3.9	3.5	3.5	-	13.0	74	45	60	60	29	075	035.1	07	.	.	.	28	22	03	.	.	09	03	11	08	02	11	.	.	.	.	.	.
VIII	2.1	3.9	2.6	2.9	-	12.2	72	37	55	55	23	005	002.3	25	.	.	.	30	21	04	01	.	12	02	04	02	.	04	.	.	.	.	.	.
IX	2.7	3.8	2.2	2.9	-	09.1	72	33	51	52	23	001	000.5	05	.	.	.	19	11	.	.	.	14	01	02	.	.	02	.	.	.	.	.	.
X	4.8	4.5	3.2	4.2	-	08.0	89	56	75	74	38	064	018.4	17	.	.	.	02	.	.	01	.	11	04	09	07	02	09	.	.	.	.	.	.
XI	5.4	5.3	2.4	4.4	-	06.0	91	58	76	75	41	007	002.5	09	.	.	10	.	.	.	02	.	07	04	06	02	.	06	.	.	.	.	.	.
XII	6.5	6.3	4.9	5.9	-	04.9	88	70	81	80	38	018	005.0	23	.	02	21	.	.	.	04	01	06	10	07	05	.	05	03	.	.	.	.	.
GOD.	5.3	5.8	4.2	5.1	-	08.0	79	50	66	65	15	450	035.1	7 VII	01	04	61	121	72	08	32	01	77	84	109	69	12	102	11	01	.	.	.	01
KOČANI																																	
BR. ST. 273																																	
I	9.5	8.6	6.8	8.3	-	-	-	-	-	-	-	037	009.0	07	.	03	16	.	.	.	.	.	01	20	11	07	.	10	01	.	.	.	.	.
II	7.6	7.1	5.5	6.7	-	-	-	-	-	-	-	062	015.0	20	01	.	17	.	.	.	01	.	01	10	13	10	02	09	04	.	.	.	.	.
III	6.7	6.2	3.8	5.6	-	05.8	81	56	76	71	34	046	012.3	16	.	.	10	01	.	.	02	.	04	05	11	08	01	10	01	.	.	.	.	.
IV	5.9	6.0	4.2	5.4	-	07.7	78	49	68	65	28	039	009.6	13	.	.	02	08	.	.	.	.	04	08	09	07	.	09	.	.	.	.	.	.
V	5.5	6.9	4.7	5.7	-	09.0	77	54	71	67	-	075	030.0	01	.	.	.	06	.	.	02	.	02	05	14	11	03	14	.	.	.	.	.	.
VI	2.4	5.5	3.6	3.8	-	12.7	75	53	68	65	37	038	014.6	21	.	.	.	24	13	.	02	.	05	02	10	07	01	10	.	.	.	.	.	.
VII	2.3	4.3	3.5	3.3	-	14.6	79	57	73	70	39	090	020.6	08	.	.	.	28	18	.	.	.	10	02	14	12	04	14	.	.	.	.	.	.
VIII	2.4	4.7	1.8	3.0	-	14.7	82	57	71	70	40	038	015.7	09	.	.	.	28	18	01	.	.	11	01	05	05	01	05	.	.	.	.	.	.
IX	2.1	3.1	1.5	2.2	-	11.0	80	50	67	66	40	006	003.5	01	.	.	01	20	10	.	.	.	16	.	03	02	.	03	.	.	.	.	.	.
X	4.7	4.5	3.9	4.4	-	08.6	91	67	81	80	43	084	017.0	24	.	.	01	01	.	.	.	.	10	06	08	08	04	08	.	.	.	.	.	.
XI	4.0	4.2	2.6	3.6	-	06.7	92	69	88	83	57	016	004.4	11	.	.	11	.	.	.	01	.	13	03	07	07	.	07	.	.	.	.	.	.
XII	6.9	5.9	4.4	5.8	-	05.2	91	78	87	85	60	021	006.1	31	.	01	22	.	.	.	01	.	07	11	09	07	.	08	03	03	.	.	.	.
GOD.	5.0	5.6	3.9	4.8	-	-	-	-	-	-	-	552	030.0	1 V	01	04	80	116	59	01	09	.	84	73	114	91	16	107	09	03	.	.	.	.
RADOVIŠ																																	
BR. ST. 274																																	
I	8.0	8.2	8.0	8.1	-	05.3	93	81	86	87	52	030	007.6	07	.	04	14	.	.	.	07	02	02	19	11	09	.	09	02	.	.	.	.	.
II	7.1	6.0	5.4	6.2	-	04.7	86	66	77	76	32	066	021.3	20	01	.	14	.	.	.	03	04	03	06	14	09	02	10	06	02	.	.	.	.
III	6.4	6.3	4.3	5.6	-	05.6	81	63	74	73	-	048	018.2	05	.	.	06	.	.	.	06	01	04	08	11	10	01	11	.	.	.	.	.	.
IV	5.3	6.2	4.6	5.3	-	07.2	76	51	68	65	22	032	009.5	03	.	.	02	07	.	.	09	04	06	07	14	06	.	13	01	.	.	.	.	.
V	5.4	6.2	4.5	5.4	-	08.6	76	55	73	68	34	086	021.2	03	.	.	.	05	.	.	08	07	05	04	16	14	03	16	.	.	.	.	.	.
VI	1.8	4.6	3.3	3.2	-	10.9	70	42	63	58	23	020	007.7	25	.	.	.	23	13	.	03	01	07	.	05	04	.	05	.	.	.	.	.	.
VII	2.2	4.3	3.1	3.2	-	13.2	72	48	74	65	28	100	035.5	07	.	.	.	27	20	.	01	02	11	03	13	11	03	13	.	.	.	.	.	.
VIII	2.0	3.5	2.1	2.5	-	12.4	72	41	65	59	28	006	004.9	09	.	.	.	29	19	.	04	04	13	02	02	02	.	02	.	.	.	.	.	.
IX	2.2	2.9	1.2	2.1	-	09.2	74	36	60	56	23	008	005.1	02	.	.	.	19	10	.	04	02	18	.	03	02	.	03	.	.	.	.	.	.
X	4.8	4.2	3.3	4.1	-	08.2	91	61	83	78	40	071	016.7	17	.	.	.	01	.	.	04	04	12	07	09	08	03	09	.	.	.	.	.	.
XI	4.0	3.3	2.0	3.1	-	06.1	90	61	81	77	18	008	003.2	11	.	.	07	.	.	.	03	04	15	04	06	04	.	06	.	.	.	.	01	01
XII	6.5	4.6	4.7	5.3	-	05.0	89	72	84	82	42	019	005.8	03	.	.	19	.	.	.	03	04	08	10	08	05	.	08	01	01	.	.	.	.
GOD.	4.6	5.0	3.9	4.5	-	08.0	80	56	74	70	-	494	035.5	7 VII	01	04	62	111	62	.	55	39	104	70	112	84	12	105	10	03	.	.	.	01
GEVGELIJA																																	
BR. ST. 275																																	
I	7.3	6.8	6.8	6.9	-	05.7	86	74	83	81	46	061	015.6	01	.	.	11	.	.	.	03	01	05	16	15	13	02	15	.	.	.	.	.	.
II	5.9	6.2	3.7	5.3	-	06.2	86	77	85	82	34	036	014.1	01	.	.	08	.	.	.	06	.	02	05	06	05	02	05	01	.	.	.	.	.
III	5.7	6.5	4.5	5.6	-	06.3	82	61	81	75	24	100	035.7	05	.	.	04	.	.	.	06	.	05	10	10	09	02	10	.	.	.	.	.	.
IV	5.1	5.5	3.5	4.7	-	08.4	79	52	71	67	31	070	044.4	06	.	.	.	09	01	.	03	.	04	05	06	05	01	06	.	.	.	.	01	02
V	3.7	6.3	4.0	4.7	-	09.1	73	51	69	64	28	115	060.1	18	.	.	.	10	.	.	03	.	08	07	10	08	03	10	.	.	.	.	01	02
VI	1.8	4.3	2.6	2.9	-	12.0	65	45	63	58	30	021	019.2	21	.	.	.	25	18	02	.	.	13	.	05	02	01	05	.	.	.	.	.	.
VII	2.5	2.9	2.6	2.7	-	13.6	68	43	66	59	30	048	029.2	07	.	.	.	28	23	07	.	.	17	02	06	06	01	06	.	.	.	.	.	.
VIII	1.6	2.8	1.5	2.0	-	13.2	67	40	62	56	24	003	001.7	10	.	.	.	30	23	03	.	.	20	01	02	02	.	02	.	.	.	.	.	.
IX	2.6	3.1	1.1	2.3	-	10.3	66	38	65	56	21	012	010.4	01	.	.	.	27	13	01	.	.	20	01	02	02	01	02	.	.	.	.	.	.
X	4.8	4.3	2.5	3.9	-	08.4	88	54	82	75	32	048	019.4	17	.	.	.	08	.	.	01	.	14	05	07	07	01	07	.	.	.	.	.	.
XI	4.1	3.4	1.7	3.0	-	06.5	83	56	85	75	33	007	004.2	23	.	.	09	01	.	.	02	.	16	03	04	03	.	04	.	.	.	.	.	.
XII	5.4	5.8	3.9	5.0	-	05.2	84	65	83	77	42	039	015.4	23	.	.	12	.	.	.	04	01	09	11	07	07	02	07	.	.	.	.	.	.
GOD.	4.2	4.8	3.2	4.1	-	08.7	77	54	74	68	21	560	060.1	18 V	.	.	44	134	78	13	28	02	133	66	80	69	16	79	01	.	.	.	02	13

Mjesec	Vanredni pritisak Pa mm	Temperatura vazduha °C										Učestina pravaca i srednja jačina vetra m/s, Fm (0-13)																							
		7	14	21	Sred. (Dnev)	Max	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C
												f.	j.	f.	j.	f.	j.	f.	j.	f.	j.	f.	j.		j.	f.	j.	f.
VALANDOVO — $\varphi = 41^\circ 19'$ N $\lambda = 22^\circ 34'$ E Gr. $\Delta G = +1h\ 30$ min. — BR. ST. 276																																			
I	-	04.1	07.2	05.2	05.4	08.3	02.9	15.0	07	-05.0	22	02	02.5	03	01.3	•	•	11	02.4	01	01.0	02	01.5	•	•	39	03.2	35
II	-	02.9	10.1	05.6	06.1	11.4	01.7	20.0	15	-04.8	21	05	02.4	07	01.1	•	•	05	01.6	06	03.0	02	01.0	•	•	29	03.5	30
III	-	05.4	12.7	08.7	08.8	13.8	04.1	23.0	25	-04.0	03	•	•	10	01.4	•	•	10	01.8	12	02.5	•	•	•	•	34	03.8	27
IV	-	11.6	19.4	14.3	14.9	20.9	08.7	29.9	28	02.3	05	•	•	11	01.5	•	•	12	02.8	08	03.0	02	02.0	•	•	29	03.9	28
V	-	13.2	20.8	15.9	16.5	22.0	10.7	28.5	12	05.5	03	01	02.0	09	02.1	•	•	07	02.0	06	03.2	03	02.3	•	•	40	03.7	27
VI	-	19.4	27.7	21.7	22.6	29.0	15.9	33.0	30	09.0	06	•	•	12	01.8	•	•	07	02.1	06	02.0	05	01.8	•	•	33	03.3	27
VII	-	21.4	29.4	23.7	24.5	30.7	18.1	35.6	23	11.5	20	01	01.0	11	01.5	•	•	06	02.0	06	02.7	06	02.8	•	•	40	03.6	23
VIII	-	20.9	30.6	25.0	25.3	31.5	18.1	36.4	08	14.5	28	01	02.0	11	01.8	•	•	04	02.8	09	02.4	06	02.7	•	•	26	03.9	36
IX	-	16.4	26.9	20.7	21.2	27.7	14.1	34.5	12,10	06.8	30	•	•	09	01.8	•	•	01	03.0	08	01.6	08	02.4	01	04.0	31	04.1	32
X	-	10.7	18.6	13.1	13.8	20.0	08.6	27.0	08	04.4	31	•	•	05	02.0	03	02.0	06	02.3	05	01.4	02	02.0	•	•	31	03.7	41
XI	-	06.3	15.4	09.5	10.2	16.1	04.9	24.8	01	-01.6	13	•	•	01	03.0	•	•	06	01.7	02	01.5	03	01.3	•	•	35	03.6	43
XII	-	03.3	08.9	05.0	05.6	09.7	01.8	15.2	31	-07.2	19	01	04.0	02	03.5	•	•	07	02.7	03	01.3	03	01.3	•	•	35	03.9	42
GOD.	-	11.3	19.0	14.0	14.6	20.1	09.1	36.4	8 VIII	-07.2	19 XII	11	02.4	91	01.7	03	02.0	82	02.2	72	02.3	42	02.1	01	04.0	402	03.7	391
STRUMICA — $\varphi = 41^\circ 26'$ N $\lambda = 22^\circ 39'$ E Gr. $\Delta G = +1h\ 31$ min. — BR. ST. 277																																			
I	-	02.6	05.9	04.4	04.3	07.3	01.8	14.8	01	-04.2	22	08	01.0	06	01.0	03	01.0	09	01.6	02	01.0	15	01.0	04	01.2	27	01.9	19
II	-	00.5	07.7	03.4	03.8	09.5	-00.7	18.5	15	-15.2	22	01	03.0	05	01.4	04	01.2	09	01.7	01	02.0	10	01.9	06	01.7	24	02.2	24
III	-	04.4	12.1	07.9	08.1	13.3	03.1	23.0	25	-04.4	03	06	01.0	10	01.1	09	01.1	13	01.5	05	02.4	17	01.4	03	01.7	26	02.0	04
IV	-	10.1	18.8	13.2	13.9	20.3	07.1	28.6	23	-00.1	05	03	01.0	03	01.3	02	01.0	16	01.7	08	02.2	29	01.7	04	01.0	26	02.0	05
V	-	12.5	20.1	14.5	15.4	21.5	09.3	28.0	11	03.6	02	01	02.0	06	01.0	01	01.0	11	01.2	06	01.5	24	01.6	02	02.0	27	02.7	15
VI	-	18.3	26.8	20.2	21.4	28.2	13.4	32.0	18	07.0	05,04	•	•	01	02.0	02	01.5	09	01.0	04	01.2	15	01.7	07	01.9	28	01.8	24
VII	-	19.4	28.8	20.5	22.3	29.6	15.2	35.1	24	07.5	19	01	01.0	10	01.1	03	01.0	07	01.4	01	02.0	28	01.5	06	01.0	29	01.3	08
VIII	-	19.1	29.5	21.3	22.8	30.1	14.5	34.5	08,07	09.8	28	03	01.7	02	01.0	04	01.0	07	01.7	02	02.0	22	01.5	10	01.1	28	02.0	15
IX	-	13.5	24.2	18.4	19.1	26.9	10.7	34.2	12	01.5	26	07	01.3	04	01.2	01	01.0	08	01.2	01	01.0	09	01.9	15	01.2	22	01.6	23
X	-	07.9	18.7	11.4	12.4	19.9	05.3	26.0	08	-01.4	26	01	01.0	02	01.0	06	01.0	07	01.7	05	01.0	16	01.2	08	01.1	16	01.7	32
XI	-	02.1	13.8	05.6	06.8	14.5	00.5	22.2	04	-03.8	27	07	01.4	05	01.0	05	01.0	11	01.3	10	01.0	11	01.2	10	01.1	15	01.5	16
XII	-	-00.9	07.1	02.1	02.6	08.2	-01.9	-	-	-	-	07	01.3	04	01.0	04	01.0	13	01.2	12	01.8	10	01.1	04	01.5	17	02.2	22
GOD.	-	09.1	18.0	11.9	12.7	19.1	06.5	-		-		45	01.3	58	01.1	44	01.1	120	01.4	57	01.6	200	01.5	79	01.3	285	01.9	207
NOVI DOJRAN — $\varphi = 41^\circ 13'$ N $\lambda = 22^\circ 43'$ E Gr. $\Delta G = +1h\ 31$ min. — BR. ST. 278																																			
I	-	04.3	06.9	04.6	05.1	07.6	02.8	13.8	07	-04.0	20	•	•	10	02.4	02	02.5	•	•	01	02.0	•	•	•	•	35	04.5	45
II	-	04.2	09.5	05.4	06.1	09.9	02.4	16.4	07	-04.5	18	02	03.5	•	•	03	04.3	•	•	01	02.0	•	•	•	•	30	04.9	48
III	-	06.3	11.3	07.4	08.1	12.2	04.5	20.0	25	-01.5	03	•	•	02	02.5	08	03.9	•	•	04	02.2	•	•	•	•	30	05.4	49
IV	-	11.7	18.0	12.5	13.7	19.1	08.6	28.0	24	04.0	05	•	•	•	•	07	03.0	01	04.0	06	01.8	•	•	•	•	24	05.3	52
V	-	14.4	19.8	14.7	15.9	21.2	11.0	28.3	12	05.0	03	01	02.0	•	•	01	04.0	02	01.5	03	02.0	•	•	•	•	39	04.3	47
VI	-	20.7	27.3	20.6	22.3	28.0	16.4	32.2	15,14	11.0	06,01	02	01.0	•	•	•	•	•	•	•	•	•	•	•	•	31	03.5	57
VII	-	22.0	29.0	22.5	24.0	29.6	18.9	33.6	24	14.8	07	•	•	•	•	01	01.0	•	•	•	•	•	•	•	•	35	03.6	57
VIII	-	22.7	29.5	23.1	24.6	30.5	19.7	35.4	07	16.4	25	01	01.0	•	•	02	02.0	01	01.0	02	01.0	•	•	•	•	17	03.7	70
IX	-	18.3	25.4	19.7	20.8	26.1	16.2	32.0	11,10	08.0	30	•	•	•	•	•	•	•	•	03	01.0	•	•	•	•	37	04.1	50
X	-	11.7	17.5	13.2	13.9	18.7	09.8	24.0	13,08	05.0	26	•	•	•	•	04	03.2	01	02.0	•	•	•	•	•	•	33	04.3	55
XI	-	07.9	14.2	09.3	10.2	14.7	06.5	21.6	03	03.0	18	01	02.0	•	•	05	02.4	•	•	•	•	•	•	•	•	27	05.3	57
XII	-	04.3	08.4	05.7	06.0	09.0	02.5	13.8	04	-04.1	21	01	02.0	•	•	04	02.0	•	•	•	•	•	•	•	•	38	04.9	50
GOD.	-	12.4	18.1	13.2	14.2	18.9	09.9	35.4	7 VIII	-04.5	18 II	08	02.0	12	02.4	37	03.0	05	02.0	20	01.7	•	•	•	•	376	04.5	637
DELČEVO — $\varphi = 41^\circ 58'$ N $\lambda = 22^\circ 46'$ E Gr. $\Delta G = +1h\ 31$ min. — BR. ST. 279																																			
I	-	01.0	04.9	02.5	02.7	05.9	-00.5	16.8	07	-09.5	22	04	02.8	09	02.1	01	01.0	10	02.7	07	03.7	10	01.8	09	01.9	07	02.1	36
II	-	-00.2	06.2	02.6	02.8	07.3	-02.1	15.0	07,06	-13.5	18	07	03.1	07	02.3	03	01.7	09	02.0	15	03.5	08	02.9	09	02.4	05	02.8	21
III	-	02.5	09.7	05.5	05.8	10.7	00.6	21.5	27	-07.0	03	10	03.8	07	02.7	•	•	09	04.3	14	02.1	04	03.0	08	03.0	11	02.8	30
IV	-	07.8	16.4	10.4	11.4	17.3	03.8	26.0	24	-03.5	05	01	02.0	08	03.1	02	01.0	11	03.5	09	03.9	07	02.6	17	02.7	06	03.2	29
V	-	10.4	17.2	12.3	13.0	18.1	06.4	28.8	11	00.0	03	05	01.8	06	03.5	03	01.7	05	01.8	16	01.5	08	02.0	15	02.7	10	02.9	25
VI	-	16.1	23.6	17.9	18.9	24.9	10.5	31.5	18	03.5	06,05	10	01.9	05	02.0	02	01.0	07	02.0	14	01.4	07	02.7	15	02.4	09	02.7	21
VII	-	17.8	25.6	19.3	20.5	26.8	13.1	31.5	23	06.4	20	05	01.4	09	03.3	06	01.5	11	02.2	17	01.4	09	02.0	10	01.6	05	03.0	21
VIII	-	16.2	26.5	19.5	20.4	27.7	12.1	33.5	08	07.0	28	09	02.1	10	02.9	02	01.0	10	02.5	11	01.6	17	02.2	14	01.9	02	02.0	18
IX	-	10.8	23.4	15.4	16.2	24.1	08.0	31.5	13,11	-02.5	30	11	02.2	09	02.8	01	01.0	07	01.6	17	01.2	09	02.2	08	02.2	07	02.9	21
X	-	05.7	15.2	08.6	09.6	16.2	03.9	23.0	08	-02.0	27	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	01.4	12.3	04.1	05.4	12.7	-00.1	20.0	04,01	-04.5	12	05	01.6	07	02.7	02	02.0	07	02.0	08	01.2	06	02.3	16	02.1	04	03.2	35
XII	-	-01.6	05.9	01.0	01.4	06.4	-03.0	13.5	31,30	-12.0	21	02	01.5	05	03.0	•	•	10	03.6	09	03.2	09	01.4	16	01.8	12	02.7	30
GOD.	-	07.3	15.6	09.9	10.7	16.5	04.4	33.5	8.VIII	-13.5	18 II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
BEROVO — $\varphi = 41^\circ 43'$ N $\lambda = 22^\circ 51'$ E Gr. $\Delta G = +1h\ 31$ min. — BR. ST. 280																																			
I	687.7	-00.4	04.1	01.3	01.6	05.4	-01.7	14.2	07	-09.8	22	17	01.6	01	01.0	•	•	18	02.4	07	02.0	06	01.5	01	01.0	02	01.5	41
II	684.5	-02.1	04.8	00.5	00.9	06.7	-03.9	13.2	06	-19.0	18	08	01.5	03	01.3	01	01.0	08	02.8	05	02.8	07	01.6	01	02.0	06	01.7	45
III	686.5	01.1	07.8	03.5	04.0	09.2	-00.1	20.0	27	-10.2	03	13	01.9	02	01.5	•	•	10	02.7	13	02.2	10	01.8	02	02.0	08	01.4	35
IV	688.2	06.5	14.2	08.1	09.2	15.9	03.6	24.0	24	-03.8	05	06	02.2	01	03.0	02	01.0	05	02.6	10	02.6	15	02.2	01	02.0	10	01.7	40
V	688.3	08.9	15.0	09.5	10.7	16.7	05.5	25.3	11	-02.2	02	11	01.3	01	02.0	01	01.0	05	01.8	07	02.3	06	01.8	02	03.0	19	01.8	41
VI	690.8	14.2	21.9	15.0	16.6	23.6	09.1	29.4	18	01.8	05	21	01.8	•	•	01	01.0	02	02.0	02	02.5	07	02.4	01	01.0	08	01.9	48
VII	689.4	15.9	24.1	16.6	18.3	25.3	11.5	30.1	23	04.8	20	19	02.2	•	•	03	01.7	•	•	02	03.0	07	02.7	01	02.0	09	02.0	52
VIII	690.2	14.5	24.4	16.5	18.0	25.7	10.4	30.6	08	04.3	28	14	01.9	03	01.0	•	•	01	01.0	02	02.5	11	02.5	02	01.0	05	01.8	55
IX	692.2	08.9	21.3	12.0	13.6	22.3	06.2	30.2	11	-04.6	30	11	01.8	02	01.0	•	•	03	01.7	•	•	02	01.5	03	01.3	12	01.5	57
X	691.9	04.2	14.1	06.3	07.7	15.3	02.5	23.2	08	-02.4	27	09	01.4	•	•	01	01.0	02	03.5	05	02.6	05	02.2	01	02.0	13	01.6	57
XI	691.0	00.0	12.0	02.6	04.3	12.8	-01.2	22.3	03	-06.0	12	16	01.8	01	01.0	•	•	02	02.0	05	01.8	05	01.2	01	02.0	04	01.5	56
XII	691.5	-02.2	04.8	-00.2	00.6	06.1	-03.7	13.3	01	-12.2	19	16	01.9	•	•	01	01.0	06	02.5	09	02.7	01	01.0	•	•	01	01.0	59
GOD.	689.4	05.8	14.0	07.6	08.8	15.4	03.2	30.6	8.VIII	-16.0	18.II	61	01.8	14	01.4	10	01.2	62	02.4	67	02.4	82	02.0	16	01.7	97	01.7	586

Mesec	Oblačnost Nm (0-10) 7	14	21	Sred. (Dlim)	Insolacija broj sati	Vlažnost vazduha e_m mm	Um % 7	14	21	Sred. (Dlim)	Min	Padavine R mm Σ	Max	Dat.	Broj dana n sa: Tn ≤ -10,0	Tx ≤ 0,0	Tn ≤ 0,0	Tx ≥ 25,0	Tx ≥ 30,0	Tn ≥ 20,0	F(0-12) Nm(0-10) ≥ 6	≥ 8	≤ 3,0	≥ 8,0	R mm ≥ 0,1	≥ 1,0	≥ 10,0	●	⚡	*	△	≈	▲	▲	T	≡	▦
VALANDOVO																																					
BR. ST. 276																																					
I	7.3	7.0	7.1	7.1	-	05.7	81	75	82	79	50	037	012.8	07	.	.	10	.	.	.	.	.	06	17	10	10	01	10	.	.	.	.	.	.	.	.	.
II	6.3	5.4	4.6	5.4	-	05.1	81	56	76	71	23	039	018.0	01	.	.	08	.	.	.	01	.	04	05	06	06	01	06	01	.	.	.	.	.	.	02	03
III	5.9	6.0	3.4	5.1	-	06.0	80	56	74	70	21	096	028.6	05	.	.	04	.	.	.	.	.	08	08	09	08	04	09	.	.	.	.	.	01	01	.	.
IV	4.9	5.8	3.1	4.6	-	08.2	74	51	66	64	26	049	020.0	06	.	.	.	09	.	.	.	.	09	04	05	05	02	05	.	.	.	.	.	.	.	.	.
V	5.2	6.2	4.4	5.3	-	09.1	77	54	66	66	21	100	030.4	03	.	.	.	09	.	.	.	.	05	07	07	07	04	07	.	.	.	.	.	01	.	.	.
VI	1.9	4.3	3.7	3.3	-	12.3	72	47	60	60	28	030	012.5	28	.	.	.	26	18	02	.	.	09	.	05	05	01	05	.	.	.	.	.	.	.	.	.
VII	2.4	3.7	2.5	2.9	-	14.3	74	50	63	62	35	032	014.2	16	.	.	.	28	22	06	.	.	14	03	04	04	01	04	.	.	.	.	.	.	.	.	.
VIII	1.6	3.5	2.3	2.4	-	14.0	74	45	57	59	18	.	.	.	.	.	.	30	23	03	02	.	14	01	.	.	.	.	.	.	.	.	.	.	.	.	.
IX	2.7	2.7	0.8	2.1	-	10.5	70	41	55	55	23	016	016.4	01	.	.	.	20	11	.	.	.	19	01	01	01	01	01	.	.	.	.	.	.	.	.	.
X	4.6	3.9	3.1	3.9	-	08.7	84	59	75	73	34	072	025.0	17	.	.	.	04	.	.	.	.	12	03	08	08	03	08	.	.	.	.	.	.	.	02	.
XI	3.5	3.6	2.2	3.1	-	06.6	82	57	72	70	31	010	005.8	23	.	.	03	.	.	.	.	.	17	04	04	04	.	04	.	.	.	.	.	.	.	.	.
XII	5.6	5.3	3.5	4.8	-	05.3	79	65	76	73	29	028	011.6	23	.	.	13	.	.	.	01	.	09	09	04	03	02	04	.	.	.	.	.	.	.	.	.
GOD.	4.3	4.8	3.4	4.2	-	08.8	77	54	68	66	18	509	030.4	5 V	.	.	38	126	74	11	04	.	126	62	63	61	20	63	01	.	.	.	.	02	01	04	03
STRUMICA																																					
BR. ST. 277																																					
I	8.7	8.4	8.2	8.4	-	05.7	91	83	87	87	56	039	012.5	31	.	.	11	.	.	.	.	.	02	22	09	07	01	08	01	.	.	.	.	.	.	12	01
II	6.6	6.0	4.0	5.5	-	04.7	89	64	81	78	23	036	023.7	20	02	.	13	.	.	.	.	01	04	07	07	04	01	05	02	.	.	.	.	.	.	07	04
III	6.1	5.8	4.7	5.5	-	06.0	87	61	76	75	23	056	013.4	21	.	.	05	.	.	.	.	.	07	09	10	09	02	09	01	.	.	.	.	.	.	01	01
IV	4.9	5.6	4.4	5.0	-	07.8	81	50	67	66	29	043	021.0	06	.	.	01	08	.	.	.	.	08	07	08	07	01	08	.	.	.	.	.	.	.	.	.
V	4.7	5.8	4.4	5.0	-	08.9	81	52	71	68	32	088	035.5	03	.	.	.	07	.	.	02	.	07	05	09	09	02	09	.	.	.	.	.	.	.	.	.
VI	1.9	4.6	3.5	3.3	-	11.8	74	45	66	62	32	031	024.2	21	.	.	.	25	14	.	.	.	06	.	06	03	01	06	.	.	.	.	.	.	.	.	.
VII	1.8	3.2	2.6	2.5	-	14.8	84	55	79	72	35	117	046.6	07	.	.	.	28	21	.	.	.	18	01	10	10	02	10	.	.	.	.	.	.	.	.	.
VIII	1.6	2.6	1.5	1.9	-	12.8	76	43	66	62	27	001	001.1	10	.	.	.	30	19	.	.	.	18	02	01	01	.	01	.	.	.	.	.	.	.	.	.
IX	2.1	2.4	1.3	1.9	-	10.0	81	40	61	61	26	002	001.6	02	.	.	.	20	10	.	.	.	19	01	01	01	.	01	.	.	.	.	.	.	.	.	.
X	4.8	3.7	3.0	3.9	-	08.1	88	55	83	75	36	061	026.5	17	.	.	02	02	.	.	.	.	12	03	08	07	02	08	.	.	.	.	.	.	.	02	.
XI	3.3	3.1	1.7	2.7	-	05.9	91	57	85	78	39	014	009.0	23	.	.	16	.	.	.	.	.	18	04	04	02	.	04	.	.	.	.	.	.	.	05	.
XII	5.5	5.6	4.2	5.1	-	04.8	87	70	89	82	-	016	004.5	31	-	-	-	-	-	-	01	.	07	09	07	04	.	06	01	.	.	.	.	.	.	04	.
GOD.	4.3	4.7	3.6	4.2	-	08.4	84	56	75	72	-	504	046.0	4 VII	-	-	-	-	-	-	03	01	126	70	80	64	12	75	05	.	.	.	.	.	.	31	06
NOVI DOJRAN																																					
BR. ST. 278																																					
I	7.7	7.5	6.6	7.3	-	05.9	87	81	83	84	56	048	021.5	07	.	.	08	.	.	.	05	02	05	17	11	10	01	11	.	.	.	.	.	.	.	.	.
II	6.6	4.5	4.4	5.2	-	05.4	81	66	77	74	30	044	023.0	01	.	.	06	.	.	.	08	02	05	07	06	05	02	05	01	.	.	.	.	.	.	01	02
III	6.3	6.0	4.8	5.7	-	06.1	79	63	78	73	30	085	027.5	05	.	.	02	.	.	.	11	02	08	10	09	08	03	09	.	.	.	.	.	.	.	.	.
IV	5.1	4.9	3.5	4.5	-	08.4	76	56	73	68	34	026	012.3	06	.	.	.	06	.	.	06	02	10	07	05	05	01	05	.	.	.	.	.	01	.	.
V	5.1	5.2	4.9	5.1	-	09.6	76	60	72	70	33	069	032.5	03	.	.	.	06	.	.	09	.	09	09	09	08	02	09	.	.	.	.	.	.	02	.	.
VI	2.0	2.7	2.7	2.5	-	13.3	68	55	66	63	29	081	030.5	21	.	.	.	24	10	.	04	01	13	.	07	07	04	07	.	.	.	.	.	01	03	.	.
VII	3.0	2.8	2.6	2.8	-	14.7	70	54	70	64	31	089	064.0	07	.	.	.	28	19	09	06	.	16	02	04	04	02	04	.	.	.	.	.	.	04	.	.
VIII	1.9	2.7	1.7	2.1	-	14.1	63	52	64	60	28	005	003.2	11	.	.	.	30	23	18	05	.	18	02	02	02	.	02	.	.	.	.	.	.	03	.	.
IX	2.8	2.3	1.7	2.3	-	11.7	68	51	64	61	36	027	027.0	01	.	.	.	18	07	.	11	.	16	02	01	01	01	01	.	.	.	.	.	.	.	.	.
X	5.6	4.5	4.3	4.8	-	09.3	83	68	79	77	45	081	035.5	17	.	.	.	.	.	.	09	01	10	07	09	08	02	09	.	.	.	.	.	.	.	.	.
XI	3.3	2.6	2.6	2.8	-	07.1	84	64	77	75	40	012	007.0	23	.	.	.	.	.	.	08	01	18	05	05	04	.	05	.	.	.	.	.	.	02	.	.
XII	4.9	5.3	4.4	4.9	-	05.6	80	72	78	77	45	022	011.5	23	.	.	08	.	.	.	06	03	11	08	04	04	01	04	.	.	.	.	.	.	.	.	.
GOD.	4.5	4.2	3.7	4.2	-	09.3	76	61	73	70	28	589	064.0	4 VII	.	.	24	112	59	27	88	14	139	76	72	66	19	71	01	.	.	.	.	01	15	01	02
DELČEVO																																					
BR. ST. 279																																					
I	8.6	7.7	8.4	8.2	-	05.0	89	79	88	85	52	035	010.2	18	.	06	16	.	.	.	01	01	01	18	12	07	01	08	04	.	.	.	.	.	.	08	02
II	6.9	6.2	5.5	6.2	-	04.5	89	69	80	79	36	075	013.9	16	02	.	19	.	.	.	03	02	01	07	12	11	02	08	05	.	.	.	.	.	01	05	08
III	6.4	6.0	5.5	6.0	-	04.8	80	58	74	71	29	050	016.0	29	.	.	12	.	.	.	03	02	04	13	13	10	01	12	01	.	.	.	.	.	01	.	.
IV	5.7	6.5	3.9	5.4	-	06.4	80	47	68	65	15	055	011.0	15	.	.	05	06	.	.	04	02	06	11	14	09	02	14	01	.	.	.	.	.	05	.	.
V	5.0	6.2	4.8	5.3	-	07.7	81	52	72	68	25	107	033.0	03	.	.	.	02	.	.	03	.	06	07	17	14	02	17	01	.	.	.	.	.	07	01	01
VI	2.3	5.6	3.0	3.7	-	10.5	77	47	70	65	15	052	017.8	23	.	.	.	20	02	.	01	02	11	03	09	07	03	09	.	.	.	.	.	.	03	01	.
VII	2.4	4.5	2.2	3.0	-	12.2	79	51	70	67	36	068	022.0	06	.	.	.	24	04	.	03	01	14	03	10	08	02	10	.	.	.	.	.	.	07	01	.
VIII	2.2	4.6	2.2	3.0	-	11.1	80	43	66	63	27	011	007.0	26	.	.	.	23	11	.	.	02	12	01	05	03	.	05	.	.	.	.	.	.	07	.	.
IX	1.9	3.0	0.6	1.8	-	08.3	82	39	63	61	21	018	015.5	01	.	.	01	16	06	.	03	.	21	.	05	01	01	05	.	.	.	.	.	.	02	.	.
X	4.8	4.4	2.4	3.9	-	06.9	90	58	82	76	40	084	018.0	04	.	.	03	.	.	.	05	.	13	04	10	09	04	08	03	.	.	.	.	.	.	09	01
XI	4.0	3.8	1.3	3.0	-	05.8	89	66	91	82	38	021	009.0	11	.	.	16	.	.	.	02	01	12	01	07	05	.	07	.	.	.	.	.	.	01	16	.
XII	6.5	4.9	5.0	5.5	-	04.9	89	84	92	88	58	026	010.4	31	04	01	22	.	.	.	03	03	08	10	10	06	01	10	03	03	.	.	.	.	.	04	.
GOD.	4.7	5.3	3.7	4.6	-	07.3	83	57	76	72	15	602	033.0	5 V	06	07	94	91	23	.	31	16	109	78	124	90	19	113	18	03	.	.	.	.	34	45	12
BEROVO																																					
BR. ST. 280																																					
I	8.5	8.2	7.5	8.1	062.9	04.6	90	75	88	84	47	029	008.3	18	.	06	16	.	.	.	.	.	01	18	12	10	.	08	04	.	.	.	.	.	.	07	04
II	7.4	7.7	6.0	7.0	107.3	03.7	92	57	80	76	32	042	009.3	16	05	.	20	.	.	.	01	.	01	11	17	09	.	07	11	.	.	.	.	.	.	01	16
III	7.3	7.5	5.1	6.6	146.2	04.5	85	57	80	74	26	047	010.5	05	01	01	16	.	.	.	02	.	03	14	15	09	01	10	06	01	.	.	.	.	01	.	06
IV	7.1	7.6	4.2	6.3	169.7	06.1	85	50	78	71	25	052	013.6	13	.	.	06	.	.	.	.	.	01	12	10	08	02	08	02	.	.	.	.	.	01	.	01
V	6.0	8.3	5.1	6.5	173.5	07.2	84	55	84	74	29	115	050.8	03	.	.	01	01	.	.	.	.	02	09	15	13	02	14	03	.	.	.	.	02	08	.	02
VI	2.2	6.8	3.8	4.3	245.1	09.6	83	46	77	68	27	016	003.6	02	.	.	.	17	.	.	.	.	-	-	07	07	.	07	.	.	.	.	.	.	07	.	.
VII	3.1	6.1	2.9	4.0	280.0	11.0	82	48	79	70	25	030	011.8	15	.	.	.	20	01	.	.	.	-	-	08	08	01	08	.	.	.	.	.	.	12	.	.
VIII	2.8	5.2	2.2	3.4	311.0	10.2	83	42	75	67	27	029	021.0	03	.	.	.	20	01	.	01	.	09	01	05	04	01	05	.	.	.	.	.	.	08	.	.
IX	3.1	4.7	1.7	3.2	271.1	07.5	88	36	74	66	20	028	010.4	01	.	.	03	09	01	.	.	.	14	02	05	04	01	05	.	.	.	.	.	.	02	01	.
X	5.2	5.4	3.8	4.8	185.0	06.1	91	54	89	78	25	060	012.2	04	.	.	07	.	.	.	01	.	09	07	09	08	02	08	02	.	.	.	.	.	.	.	01
XI	4.4	5.1	2.4	3.9	177.5	04.8	92	50	88	77	20	018	005.9	11	.	.	22	.	.	.	.	.	10	05	05	04	.	05	.	.	.	.	.	.	.	01	.
XII	6.5	6.5	4.6	5.9	104.7	04.0	90	64	86	80	31	032	006.8	31	04	01	25	.	.	.	.	.	07	13	11	09	.	09	04	.	.	.	.	.	.	.	04
GOD.	5.3	6.6	4.1	5.3	2234.0	06.6	87	52	81	73	20	498	050.8	5 V	10	08	116	67	03	.	05	.	-	-	119	93	10	94	32	01	.	.	.	02	39	10	34


KLIMATOLOŠKE STANICE U 1970.